

*Japan International Cooperation Agency*  
*Ministry of Energy and Mines of the Republic of Peru*

**Master Plan Study  
for Rural Electrification  
by Renewable Energy  
in the Republic of Peru**

**Appendix**

**Final Report**

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**Electric Power Development Co., Ltd.  
Nippon Koei Co., Ltd.  
Tokyo - Japan**

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## **Appendix I Construction Cost Estimation**

**Appendix I-1 Construction Cost for Cachiyacu Power Station*****I. Summary of Construction Cost for Cachiyacu Power Station***

Unit: US\$

<i>Work Item</i>	<i>Construction Cost</i>	<i>Remarks</i>
<b><i>1. Preliminary Works</i></b>	<b>19,646</b>	
(1) Access Road	7,053	
(2) Facilities for Construction Office	3,078	Cost of Civil Works x 0.05
(3) Transportation cost	9,515	488.20ton x \$19.49/ton
<b><i>2. Cost for Environmental Measures</i></b>	<b>615</b>	Cost of Civil Works x 0.01
<b><i>3. Civil Works</i></b>	<b>61,577</b>	
(1) Weir	2,221	
(2) Intake	2,912	
(3) Settling Basin	2,715	
(4) Headrace	4,416	
(5) Head Tank	6,605	
(6) Penstock & Spillway Channel	33,199	
(7) Power House	8,327	
(8) Outlet	1,182	
(9) Miscellaneous Work	0	
<b><i>4. Hydraulic Equipment</i></b>	<b>50,500</b>	
(1) Gate & Screen	1,790	
(2) Penstock	1,607	
(3) PVC (φ400)	27,383	
(4) PVC (φ200)	11,359	
(5) Others	8,361	
<b><i>5. Electrical Equipment</i></b>	<b>35,000</b>	
<b><i>6. Direct Cost</i></b>	<b>167,338</b>	1.+2.+3.+4.+5.
<b><i>7. Engineering Cost</i></b>	<b>16,734</b>	6. x 0.1: Detailed Design and Supervision
<b><i>8. Contingent Budget</i></b>	<b>15,928</b>	6. x 0.095
<b><i>9. IGV</i></b>	<b>38,000</b>	19.00%
<b><i>10. Total Cost</i></b>	<b>238,000</b>	

**II. Detailed Statement of Transportation Cost for Cachiyacu Power Station**

<i>Items</i>	<i>Unit</i>	<i>Quantity</i>	<i>Remarks</i>
<b>(1) Wier</b>		<b>17.05</b>	
a. Cements	ton	3.57	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		13.24	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.23	
<b>(2) Intake</b>		<b>27.42</b>	
a. Gate	ton	0.14	
b. Screen		0.06	
c. Cements		5.68	Cement: 0.27ton per concrete 1m <sup>3</sup>
d. Coarse aggregate		21.05	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
e. Reinforcement Bars		0.48	
<b>(3) Settling Basin</b>		<b>17.43</b>	
a. Cements	ton	3.48	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		12.90	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		1.05	
<b>(4) Headrace</b>		<b>7.14</b>	
a. PVC (φ400)	ton	7.14	Weight: 1,040m x 41.214kg/6m
<b>(5) Head Tank</b>		<b>36.36</b>	
a. Cements	ton	7.43	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		27.52	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		1.40	
<b>(6) Penstock &amp; Spillway Channel</b>		<b>329.60</b>	
a. Penstock Steel (φ200)	ton	0.52	
b. Penstock PVC (φ200)		2.73	Weight: 327m x 50.000kg/6m
c. Cements		69.37	Cement: 0.27ton per concrete 1m <sup>3</sup>
d. Coarse aggregate		256.91	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
e. Reinforcement Bars		0.09	
<b>(7) Power House</b>		<b>49.70</b>	
a. Cements	ton	10.13	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		37.51	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		2.07	
<b>(8) Outlet</b>		<b>3.51</b>	
a. Cements	ton	0.64	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		2.39	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.47	
<b>(9) Subtotal</b>		<b>488.20</b>	
<b>(10) Transportation Cost</b>		<b>9,515</b>	(9) x \$19.49/ton

**III. Detailed Statement of Civil Works Cost for Cachiyacu Power Station**

Unit: US\$

<b>Work Items</b>	<b>Unit</b>	<b>Unit Price</b>	<b>Quantity</b>	<b>Cost</b>	<b>Remarks</b>
<b>(1) Wier</b>				<b>2,221</b>	
a. Excavation	m <sup>3</sup>	5.53	67.0	370	
b. Concrete	m <sup>3</sup>	93.05	13.2	1,231	
c. Reinforcement Bars	ton	1,070.00	0.2	250	
d. Others	-			370	(a+b+c) x 0.2 (including coffer dam construction, etc.)
<b>(2) Intake</b>				<b>2,912</b>	
a. Excavation	m <sup>3</sup>	5.53	10.9	60	
b. Concrete	m <sup>3</sup>	93.05	21.1	1,958	
c. Reinforcement Bars	ton	1,070.00	0.5	515	
d. Others	-			379	(a+b+c) x 0.15 (including coffer work, etc.)
<b>(3) Settling Basin</b>				<b>2,715</b>	
a. Excavation	m <sup>3</sup>	5.53	27.2	150	
b. Concrete	m <sup>3</sup>	93.05	12.9	1,200	
c. Reinforcement Bars	ton	1,070.00	1.0	1,119	
d. Others	-			246	(a+b+c) x 0.10 (including other works)
<b>(4) Headrace</b>				<b>4,416</b>	
a. Excavation	m <sup>3</sup>	5.53	665.6	3,680	
b. Concrete	m <sup>3</sup>	93.05	0.0	0	
c. Reinforcement Bars	ton	1,070.00	0.0	0	
d. Others	-			736	(a+b+c) x 0.20 (including filling works)
<b>(5) Head Tank</b>				<b>6,605</b>	
a. Excavation	m <sup>3</sup>	5.53	118.9	657	
b. Concrete	m <sup>3</sup>	93.05	27.5	2,560	
c. Reinforcement Bars	ton	1,070.00	1.4	1,501	
d. Others	-			1,887	(a+b+c) x 0.40 (including gate, screen)
<b>(6) Penstock &amp; Spillway Channel</b>				<b>33,199</b>	
a. Excavation	m <sup>3</sup>	5.53	1118.6	6,185	
b. Concrete	m <sup>3</sup>	93.05	256.9	23,905	
c. Reinforcement Bars	ton	1,070.00	0.1	91	
d. Others	-			3,018	(a+b+c) x 0.10 (including filling works)
<b>(7) Power House</b>				<b>8,327</b>	
a. Excavation	m <sup>3</sup>	5.53	127.4	704	
b. Concrete	m <sup>3</sup>	93.05	37.5	3,490	
c. Reinforcement Bars	ton	1,070.00	2.1	2,212	
d. Others	-			1,921	(a+b+c) x 0.30 (including drainage work, wooden)
<b>(8) Outlet</b>				<b>1,182</b>	
a. Excavation	m <sup>3</sup>	5.53	54.5	301	
b. Concrete	m <sup>3</sup>	93.05	2.4	222	
c. Reinforcement Bars	ton	1,070.00	0.5	505	
d. Others	-			154	(a+b+c) x 0.15 (including coffer work, etc.)
<b>(9) Miscellaneous Work</b>	-			<b>0</b>	Σ(1)-(8) x 0.05 not consider
<b>(10) Subtotal</b>				<b>61,577</b>	

**IV. Detailed Statement of Hydraulic Equipment Cost for Cachiyacu Power Station**

Unit: US\$

<i>Work Items</i>	<i>Unit</i>	<i>Unit Price</i>	<i>Quantity</i>	<i>Cost</i>	<i>Remarks</i>
<b>(1) Weir &amp; Spillway</b>				<b>0</b>	
a. Gate	ton	8,811.04	0.00	0	
<b>(2) Intake</b>				<b>1,790</b>	
a. Gate	ton	8,811.04	0.14	1,234	
b. Screen	ton	8,811.04	0.06	556	
<b>(3) Penstock Steel (φ200)</b>	ton	3,100.00	0.52	<b>1,607</b>	
<b>(4) PVC (φ400) for headrace</b>	m	26.33	1,040	<b>27,383</b>	
<b>(5) Penstock PVC (φ200) C-10</b>	m	34.74	327	<b>11,359</b>	
<b>(6) Subtotal</b>				<b>42,139</b>	
<b>(7) Others</b>				<b>8,361</b>	19.84%
<b>(8) Total</b>				<b>50,500</b>	



## V. Quantity

<b>(1) Weir</b>					
Excavation:	$V_e =$	$8.69 \times (H_d \times L)^{1.14}$	$=$	<b>67.01</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$8.64 \times (H_d^2 \times L)^{0.726}$	$=$	<b>13.24</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.0274 \times V_c^{0.830}$	$=$	<b>0.23</b>	(ton)
Weight of Gate:	$W_g =$	$0.145 \times Q_f^{0.692}$	$=$	<b>0.00</b>	(ton) (unconsidered)
Where,					
$H_d$ :	Height of Dam =	<b>0.30</b>	(m)		
$L$ :	Length of Dam =	<b>20.00</b>	(m)		
<b>(2) Intake</b>					
Excavation:	$V_e =$	$171 \times (R \times Q)^{0.666}$	$=$	<b>10.89</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$147 \times (R \times Q)^{0.470}$	$=$	<b>21.05</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.0145 \times V_c^{1.15}$	$=$	<b>0.48</b>	(ton)
Weight of Gate:	$W_g =$	$1.27 \times (R \times Q)^{0.533}$	$=$	<b>0.14</b>	(ton)
Weight of Screen:	$W_s =$	$0.701 \times (R \times Q)^{0.582}$	$=$	<b>0.06</b>	(ton)
Where,					
$D$ :	Diameter of Waterway =	<b>0.50</b>	(m)		
$R$ :	Radius of Waterway =	<b>0.25</b>	(m)	$D/2$	Assumption; Waterway Gradient = 1/1,000
$Q$ :	Maximum Discharge =	<b>0.064</b>	(m <sup>3</sup> /s)		
<b>(3) Settling Basin</b>					
Excavation:	$V_e =$	$515 \times Q^{1.07}$	$=$	<b>27.19</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$169 \times Q^{0.936}$	$=$	<b>12.90</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.120 \times V_c^{0.847}$	$=$	<b>1.05</b>	(ton)
Weight of Gate:	$W_g =$	$0.910 \times Q^{0.613}$	$=$	<b>0.17</b>	(ton)
Weight of Screen:	$W_s =$	$0.879 \times Q^{0.785}$	$=$	<b>0.10</b>	(ton)
Where,					
$Q$ :	Maximum Discharge =	<b>0.064</b>	(m <sup>3</sup> /s)		
<b>(4) Headrace</b>					
<b>In the case of PVC<math>\phi</math>400:</b>					
Excavation:	$V_e = B \times H \times L$		$=$	<b>665.60</b>	(m <sup>3</sup> )
Concrete:	$V_c = ((H \times t \times 2) + (B + 2t) \times t) \times L$		$=$	-	(m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.577 \times (V_c/L)^{0.888} \times L$		$=$	-	(ton)
Where,					
$Q$ :	Maximum Discharge =	<b>0.064</b>	(m <sup>3</sup> /s)		
$L$ :	Length of Channel =	<b>1,040.00</b>	(m)		
$B$ :	Width of Channel =	<b>0.80</b>	(m)		for excavation (2D from RIBLOC Brochure)
$H$ :	Height of Channel =	<b>0.80</b>	(m)		for excavation (2D from RIBLOC Brochure)
$t$ :	Thickness of Concrete =	-	(m)		
<b>(5) Head Tank</b>					
Excavation:	$V_e =$	$808 \times Q^{0.697}$	$=$	<b>118.94</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$197 \times Q^{0.716}$	$=$	<b>27.52</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.051 \times V_c$	$=$	<b>1.40</b>	(ton)
Where,					
$Q$ :	Maximum Discharge =	<b>0.064</b>	(m <sup>3</sup> /s)		

**(6) Penstock & Spillway Channel**

**Penstock (Steel)φ200:**

Excavation:	$V_{e1} =$	$10.9 \times D_m^{1.33} \times L$	$=$	42.30 (m <sup>3</sup> )
Concrete:	$V_{c1} =$	$2.14 \times D_m^{1.68} \times L$	$=$	4.73 (m <sup>3</sup> )
Reinforcement Bars	$W_{r1} =$	$0.018 \times V_c$	$=$	0.09 (ton)

Where,

$D_m$ : avg. Diameter of Penstock =	0.20 (m)
L: Length of Penstock =	33.00 (m)

Weight of Penstock	$W_{p1} = 7.85 \times \pi \times D_m \times t_m \times 10^{-3} \times 1.15 \times L$	$=$	0.52 (ton)
Thickness of Penstock:	$t_m = 0.0362 \times H \times D_m + 2$	$=$	2.77 (mm)

Where,

$W_{p1}$ : Weight of Penstock	0.52 (ton)	(Tensile allowable Stress: 1,150 kgf/cm <sup>2</sup> )
$t_m$ : Thickness of Penstock	2.77 (mm)	
$D_m$ : avg. Diameter of Penstock =	0.20 (m)	
H: Design Head =	106.50 (m)	(Intake Water Level - Tailrace Water Level)
L: Length of Penstock =	33.00 (m)	

**Penstock (PVC)φ200:**

Excavation:	$V_e = B \times H \times L$	$=$	247.51 (m <sup>3</sup> )
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Where,

Q: Maximum Discharge =	0.064 (m <sup>3</sup> /s)	
L: Length of Channel =	327.00 (m)	
B: Width of Channel =	0.87 (m)	from TUBOPLAST Brochure
H: Height of Channel =	0.87 (m)	from TUBOPLAST Brochure

**Spillway Channel:**

	$(B \times H)^{0.5} = 1.09 \times Q^{0.379}$	$=$	0.38
Excavation:	$V_e = 6.22 \times ((B \times H)^{0.5})^{1.04} \times L$	$=$	828.82 (m <sup>3</sup> )
Concrete:	$V_c = H \times t \times 2 + (B + 2t) \times L$	$=$	252.18 (m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.577 \times (V_c/L)^{0.888} \times L$	$=$	0.00 (ton)

Where,

Q: Maximum Discharge =	0.064 (m <sup>3</sup> /s)
L: Length of Channel =	360.00 (m)
B: Width of Channel =	0.40 (m)
H: Height of Channel =	0.60 (m)
t: Thickness of Concrete =	0.15 (m)

**Total Quantity of Penstock and Spillway Channel:**

Excavation:	$V_e =$	$V_{e1} + V_{e2}$	$=$	1,118.62 (m <sup>3</sup> )
Concrete:	$V_c =$	$V_{c1} + V_{c2}$	$=$	256.91 (m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$W_{r1} + W_{r2}$	$=$	0.09 (ton)
Weight of Penstock	$W_p =$	$W_{p1}$	$=$	0.52 (ton)

**(7) Power House**

Excavation:	$V_e = 97.8 \times (Q \times H e^{2/3} \times n^{1/2})^{0.727}$	$=$	127.36 (m <sup>3</sup> )
Concrete:	$V_c = 28.1 \times (Q \times H e^{2/3} \times n^{1/2})^{0.795}$	$=$	37.51 (m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.046 \times V_c^{1.05}$	$=$	2.07 (ton)

Where,

Q: Maximum Discharge =	0.064 (m <sup>3</sup> /s)
He: Effective Head =	106.50 (m)
n: quantity Unit of Turbine =	1.00

**(8) Outlet**

Excavation:	$V_e =$	$395 \times (R \times Q)^{0.479}$	$=$	54.50 (m <sup>3</sup> )
Concrete:	$V_c =$	$40.4 \times (R \times Q)^{0.684}$	$=$	2.39 (m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.278 \times V_c^{0.610}$	$=$	0.47 (ton)

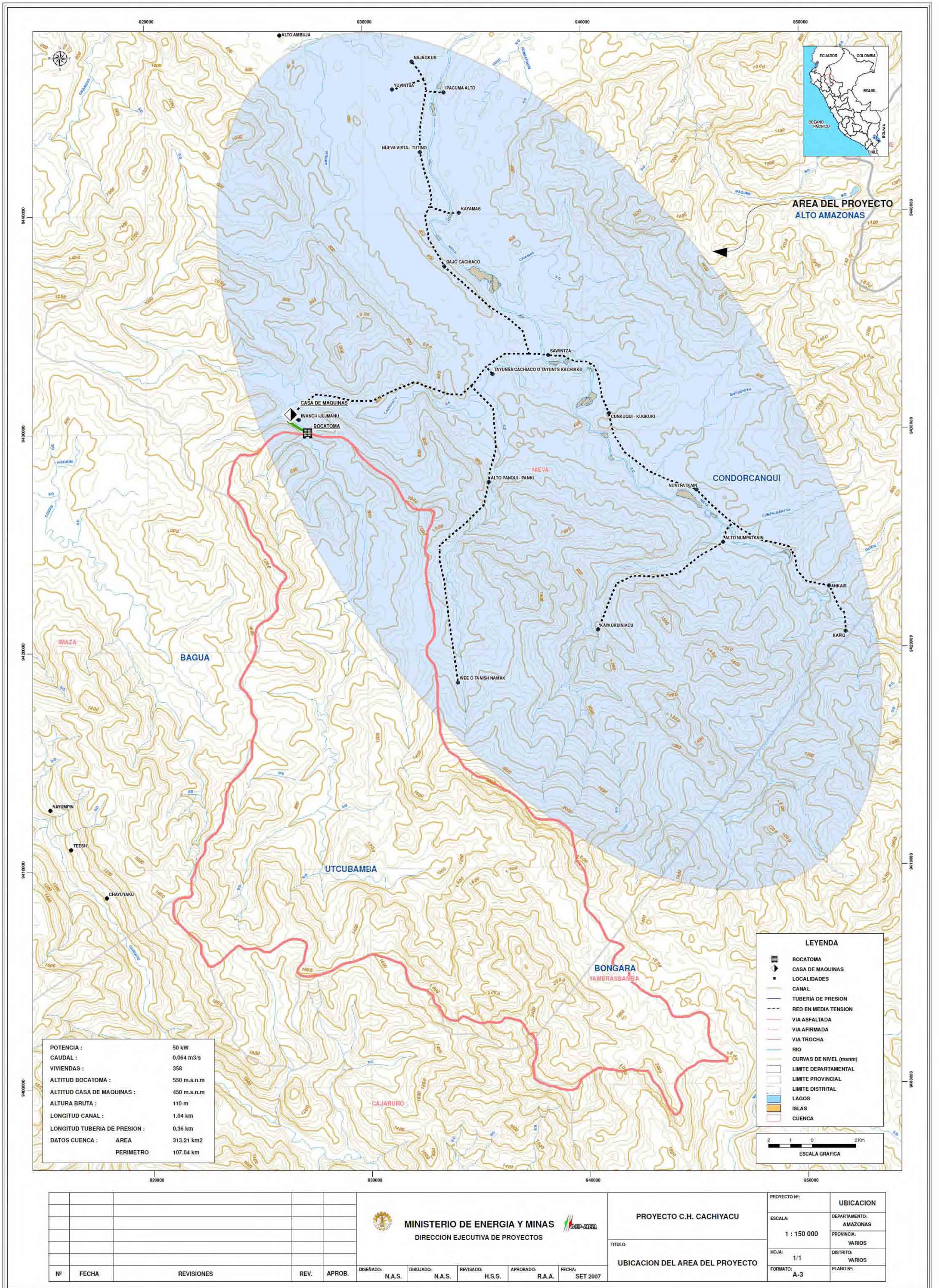
Where,

D: Diameter of Waterway =	0.50 (m)	
R: Radius of Waterway =	0.25 (m)	D/2
Q: Maximum Discharge =	0.064 (m <sup>3</sup> /s)	

**VI. Unit Price**                      1USD =        3.00    S/. (as of November, 2007)

<b>(1) Civil Works</b>		
Excavation		
Open	:	<b>5.53</b> (US\$/m <sup>3</sup> ) * (8.70+2.35) x 0.5 = \$5.53/m <sup>3</sup> , from CAPAECO and Fainal study on Omia <Human power and Machine excavation>
Tunnel	:	-
Concrete		
Open	:	<b>93.05</b> (US\$/m <sup>3</sup> ) * from CAPAECO (average of foundation, wall and structure concrete)
Tunnel	:	-
Reinforcement Bar	:	<b>1,070.00</b> (US\$/ton) *\$1.07/kg, from CAPAECO
<b>(2) Hydraulic Equipment</b>		
Gate & Screen	:	<b>8,811.04</b> (US\$/ton) * from final study on Omia
Steel Penstock	:	<b>3,100.00</b> (US\$/ton) including installation
PVC (φ400)	:	<b>26.33</b> (US\$/m) RIB LOC for Headrace
PVC (φ200)	:	<b>34.74</b> (US\$/m) 80% of TUBOPLAST( φ 315) for Penstock (C-10) = 43.42 x 0.8 = 34.74
<b>(3) Others</b>		
Access Road	:	<b>5,877.89</b> (US\$/m) Construction of Unpaved Road (3.0m Width)
<b>(4) Transportation Cost</b>		
Chachapoyas to the site	:	<b>19.49</b> (US\$/ton) 320km

# Cachiyacu Map



## Appendix I-2 Construction Cost for Palcapampa Power Station

### I. Summary of Construction Cost for Palcapampa Power Station

Unit: US\$

<i>Work Item</i>	<i>Construction Cost</i>	<i>Remarks</i>
<b>1. Preliminary Works</b>	<b>21,199</b>	
(1) Access Road	14,106	
(2) Facilities for Construction Office	2,156	Cost of Civil Works x 0.05
(3) Transportation cost	4,937	373.97ton x \$14.83/ton
<b>2. Cost for Environmental Measures</b>	<b>431</b>	Cost of Civil Works x 0.01
<b>3. Civil Works</b>	<b>43,121</b>	
(1) Weir	2,221	
(2) Intake	2,168	
(3) Settling Basin	1,598	
(4) Headrace	5,392	
(5) Head Tank	4,293	
(6) Penstock & Spillway Channel	21,426	
(7) Power House	5,144	
(8) Outlet	879	
(9) Miscellaneous Work	0	
<b>4. Hydraulic Equipment</b>	<b>52,000</b>	
(1) Gate & Screen	1,286	
(2) Penstock	1,073	
(3) PVC (φ400)	33,439	
(4) PVC (φ200)	7,573	
(5) Others	8,629	
<b>5. Electrical Equipment</b>	<b>24,800</b>	
<b>6. Direct Cost</b>	<b>141,551</b>	1.+2.+3.+4.+5.
<b>7. Engineering Cost</b>	<b>14,155</b>	6. x 0.1: Detailed Design and Supervision
<b>8. Contingent Budget</b>	<b>13,294</b>	6. x 0.094
<b>9. IGV</b>	<b>32,110</b>	19.00%
<b>10. Total Cost</b>	<b>201,110</b>	

**II. Detailed Statement of Transportation Cost for Palcapampa Power Station**

<i>Items</i>	<i>Unit</i>	<i>Quantity</i>	<i>Remarks</i>
<b>(1) Wier</b>		<b>17.05</b>	
a. Cements	ton	3.57	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		13.24	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.23	
<b>(2) Intake</b>		<b>20.62</b>	
a. Gate	ton	0.10	
b. Screen		0.04	
c. Cements		4.28	Cement: 0.27ton per concrete 1m <sup>3</sup>
d. Coarse aggregate		15.85	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
e. Reinforcement Bars		0.35	
<b>(3) Settling Basin</b>		<b>9.96</b>	
a. Cements	ton	1.98	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		7.33	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.65	
<b>(4) Headrace</b>		<b>8.72</b>	
a. PVC (φ400)	ton	8.72	Weight: 1,270m x 41.214kg/6m
<b>(5) Head Tank</b>		<b>23.60</b>	
a. Cements	ton	4.82	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		17.87	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.91	
<b>(6) Penstock &amp; Spillway Channel</b>		<b>219.81</b>	
a. Penstock Steel (φ200)	ton	0.35	
b. Penstock PVC (φ200)		1.82	Weight: 218m x 50.000kg/6m
c. Cements		46.26	Cement: 0.27ton per concrete 1m <sup>3</sup>
d. Coarse aggregate		171.33	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
e. Reinforcement Bars		0.06	
<b>(7) Power House</b>		<b>30.79</b>	
a. Cements	ton	6.28	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		23.26	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		1.25	
<b>(8) Outlet</b>		<b>2.37</b>	
a. Cements	ton	0.43	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		1.58	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.37	
<b>(9) Subtotal</b>		<b>332.93</b>	
<b>(10) Transportation Cost</b>		<b>4,937</b>	(9) x \$14.83/ton

**III. Detailed Statement of Civil Works Cost for Palcapampa Power Station**

Unit: US\$

<b>Work Items</b>	<b>Unit</b>	<b>Unit Price</b>	<b>Quantity</b>	<b>Cost</b>	<b>Remarks</b>
<b>(1) Wier</b>				<b>2,221</b>	
a. Excavation	m <sup>3</sup>	5.53	67.0	370	
b. Concrete	m <sup>3</sup>	93.05	13.2	1,231	
c. Reinforcement Bars	ton	1,070.00	0.2	250	
d. Others	-			370	(a+b+c) x 0.2 (including coffer dam construction, etc.)
<b>(2) Intake</b>				<b>2,168</b>	
a. Excavation	m <sup>3</sup>	5.53	7.3	40	
b. Concrete	m <sup>3</sup>	93.05	15.9	1,474	
c. Reinforcement Bars	ton	1,070.00	0.3	372	
d. Others	-			282	(a+b+c) x 0.15 (including coffer work, etc.)
<b>(3) Settling Basin</b>				<b>1,598</b>	
a. Excavation	m <sup>3</sup>	5.53	14.3	78	
b. Concrete	m <sup>3</sup>	93.05	7.3	682	
c. Reinforcement Bars	ton	1,070.00	0.6	693	
d. Others	-			145	(a+b+c) x 0.10 (including other works)
<b>(4) Headrace</b>				<b>5,392</b>	
a. Excavation	m <sup>3</sup>	5.53	812.8	4,494	
b. Concrete	m <sup>3</sup>	93.05	0.0	0	
c. Reinforcement Bars	ton	1,070.00	0.0	0	
d. Others	-			898	(a+b+c) x 0.20 (including filling works)
<b>(5) Head Tank</b>				<b>4,293</b>	
a. Excavation	m <sup>3</sup>	5.53	78.1	431	
b. Concrete	m <sup>3</sup>	93.05	17.9	1,662	
c. Reinforcement Bars	ton	1,070.00	0.9	974	
d. Others	-			1,226	(a+b+c) x 0.40 (including gate, screen)
<b>(6) Penstock &amp; Spillway Channel</b>				<b>21,426</b>	
a. Excavation	m <sup>3</sup>	5.53	628.8	3,477	
b. Concrete	m <sup>3</sup>	93.05	171.3	15,942	
c. Reinforcement Bars	ton	1,070.00	0.1	60	
d. Others	-			1,947	(a+b+c) x 0.10 (including filling works)
<b>(7) Power House</b>				<b>5,144</b>	
a. Excavation	m <sup>3</sup>	5.53	82.3	454	
b. Concrete	m <sup>3</sup>	93.05	23.3	2,164	
c. Reinforcement Bars	ton	1,070.00	1.3	1,339	
d. Others	-			1,187	(a+b+c) x 0.30 (including drainage work, wooden)
<b>(8) Outlet</b>				<b>879</b>	
a. Excavation	m <sup>3</sup>	5.53	40.8	225	
b. Concrete	m <sup>3</sup>	93.05	1.6	147	
c. Reinforcement Bars	ton	1,070.00	0.4	393	
d. Others	-			114	(a+b+c) x 0.15 (including coffer work, etc.)
<b>(9) Miscellaneous Work</b>	-			<b>0</b>	Σ(1)-(8) x 0.05 not consider
<b>(10) Subtotal</b>				<b>43,121</b>	

**IV. Detailed Statement of Hydraulic Equipment Cost for Palcapampa Power Station**

Unit: US\$

<i>Work Items</i>	<i>Unit</i>	<i>Unit Price</i>	<i>Quantity</i>	<i>Cost</i>	<i>Remarks</i>
<b>(1) Weir &amp; Spillway</b>				<b>0</b>	
a. Gate	ton	8,811.04	0.00	0	
<b>(2) Intake</b>				<b>1,286</b>	
a. Gate	ton	8,811.04	0.10	895	
b. Screen	ton	8,811.04	0.04	391	
<b>(3) Penstock Steel (φ200)</b>	ton	3,100.00	0.35	<b>1,073</b>	
<b>(4) PVC (φ400) for headrace</b>	m	26.33	1,270	<b>33,439</b>	
<b>(5) Penstock PVC (φ200) C-10</b>	m	34.74	218	<b>7,573</b>	
<b>(6) Subtotal</b>				<b>43,371</b>	
<b>(7) Others</b>				<b>8,629</b>	19.90%
<b>(8) Total</b>				<b>52,000</b>	



## V. Quantity

<b>(1) Weir</b>					
Excavation:	$V_e =$	$8.69 \times (H_d \times L)^{1.14}$	$=$	<b>67.01</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$8.64 \times (H_d^2 \times L)^{0.726}$	$=$	<b>13.24</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.0274 \times V_c^{0.830}$	$=$	<b>0.23</b>	(ton)
Weight of Gate:	$W_g =$	$0.145 \times Q_f^{0.692}$	$=$	<b>0.00</b>	(ton) (unconsidered)
Where,					
$H_d$ :	Height of Dam =	<b>0.30</b>	(m)		
$L$ :	Length of Dam =	<b>20.00</b>	(m)		
<b>(2) Intake</b>					
Excavation:	$V_e =$	$171 \times (R \times Q)^{0.666}$	$=$	<b>7.28</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$147 \times (R \times Q)^{0.470}$	$=$	<b>15.85</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.0145 \times V_c^{1.15}$	$=$	<b>0.35</b>	(ton)
Weight of Gate:	$W_g =$	$1.27 \times (R \times Q)^{0.533}$	$=$	<b>0.10</b>	(ton)
Weight of Screen:	$W_s =$	$0.701 \times (R \times Q)^{0.582}$	$=$	<b>0.04</b>	(ton)
Where,					
$D$ :	Diameter of Waterway =	<b>0.50</b>	(m)		
$R$ :	Radius of Waterway =	<b>0.25</b>	(m)	D/2	Assumption; Waterway Gradient = 1/1,000
$Q$ :	Maximum Discharge =	<b>0.035</b>	(m <sup>3</sup> /s)		
<b>(3) Settling Basin</b>					
Excavation:	$V_e =$	$515 \times Q^{1.07}$	$=$	<b>14.25</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$169 \times Q^{0.936}$	$=$	<b>7.33</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.120 \times V_c^{0.847}$	$=$	<b>0.65</b>	(ton)
Weight of Gate:	$W_g =$	$0.910 \times Q^{0.613}$	$=$	<b>0.12</b>	(ton)
Weight of Screen:	$W_s =$	$0.879 \times Q^{0.785}$	$=$	<b>0.06</b>	(ton)
Where,					
$Q$ :	Maximum Discharge =	<b>0.035</b>	(m <sup>3</sup> /s)		
<b>(4) Headrace</b>					
<b>In the case of PVCφ400:</b>					
Excavation:	$V_e = B \times H \times L$		$=$	<b>812.80</b>	(m <sup>3</sup> )
Concrete:	$V_c = ((H \times t \times 2) + (B + 2t) \times t) \times L$		$=$	-	(m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.577 \times (V_c/L)^{0.888} \times L$		$=$	-	(ton)
Where,					
$Q$ :	Maximum Discharge =	<b>0.035</b>	(m <sup>3</sup> /s)		
$L$ :	Length of Channel =	<b>1,270.00</b>	(m)		
$B$ :	Width of Channel =	<b>0.80</b>	(m)		for excavation (2D from RIBLOC Brochure)
$H$ :	Height of Channel =	<b>0.80</b>	(m)		for excavation (2D from RIBLOC Brochure)
$t$ :	Thickness of Concrete =	-	(m)		
<b>(5) Head Tank</b>					
Excavation:	$V_e =$	$808 \times Q^{0.697}$	$=$	<b>78.10</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$197 \times Q^{0.716}$	$=$	<b>17.87</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.051 \times V_c$	$=$	<b>0.91</b>	(ton)
Where,					
$Q$ :	Maximum Discharge =	<b>0.035</b>	(m <sup>3</sup> /s)		

**(6) Penstock & Spillway Channel**

**Penstock (Steel)φ200:**

Excavation:	$V_{e1} = 10.9 \times D_m^{1.33} \times L$	=	28.20 (m <sup>3</sup> )
Concrete:	$V_{c1} = 2.14 \times D_m^{1.68} \times L$	=	3.15 (m <sup>3</sup> )
Reinforcement Bars	$W_{r1} = 0.018 \times V_c$	=	0.06 (ton)

Where,

$D_m$ : v.g. Diameter of Penstock =	0.20 (m)
L: Length of Penstock =	22.00 (m)

Weight of Penstock	$W_{p1} = 7.85 \times \pi \times D_m \times t_m \times 10^{-3} \times 1.15 \times L$	=	0.35 (ton)
Thickness of Penstock:	$t_m = 0.0362 \times H \times D_m + 2$	=	2.77 (mm)

Where,

$W_{p1}$ : Weight of Penstock	0.35 (ton)	(Tensile allowable Stress: 1,150 kgf/cm <sup>2</sup> )
$t_m$ : Thickness of Penstock	2.77 (mm)	
$D_m$ : v.g. Diameter of Penstock =	0.20 (m)	
H: Design Head =	106.90 (m)	(Intake Water Level - Tailrace Water Level)
L: Length of Penstock =	22.00 (m)	

**Penstock (PVC)φ200:**

Excavation:	$V_e = B \times H \times L$	=	165.00 (m <sup>3</sup> )
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Where,

Q: Maximum Discharge =	0.035 (m <sup>3</sup> /s)	
L: Length of Channel =	218.00 (m)	
B: Width of Channel =	0.87 (m)	from TUBOPLAST Brochure
H: Height of Channel =	0.87 (m)	from TUBOPLAST Brochure

**Spillway Channel:**

	$(B \times H)^{0.5} = 1.09 \times Q^{0.379}$	=	0.31
Excavation:	$V_e = 6.22 \times ((B \times H)^{0.5})^{1.04} \times L$	=	435.57 (m <sup>3</sup> )
Concrete:	$V_c = H \times t \times 2 + (B + 2t) \times L$	=	168.18 (m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.577 \times (V_c/L)^{0.888} \times L$	=	0.00 (ton)

Where,

Q: Maximum Discharge =	0.035 (m <sup>3</sup> /s)
L: Length of Channel =	240.00 (m)
B: Width of Channel =	0.40 (m)
H: Height of Channel =	0.60 (m)
t: Thickness of Concrete =	0.15 (m)

**Total Quantity of Penstock and Spillway Channel:**

Excavation:	$V_e = V_{e1} + V_{e2}$	=	628.77 (m <sup>3</sup> )
Concrete:	$V_c = V_{c1} + V_{c2}$	=	171.33 (m <sup>3</sup> )
Reinforcement Bars	$W_r = W_{r1} + W_{r2}$	=	0.06 (ton)
Weight of Penstock	$W_p = W_{p1}$	=	0.35 (ton)

**(7) Power House**

Excavation:	$V_e = 97.8 \times (Q \times H e^{2/3} \times n^{1/2})^{0.727}$	=	82.27 (m <sup>3</sup> )
Concrete:	$V_c = 28.1 \times (Q \times H e^{2/3} \times n^{1/2})^{0.795}$	=	23.26 (m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.046 \times V_c^{1.05}$	=	1.25 (ton)

Where,

Q: Maximum Discharge =	0.035 (m <sup>3</sup> /s)
He: Effective Head =	106.90 (m)
n: quantity Unit of Turbine =	1.00

**(8) Outlet**

Excavation:	$V_e = 395 \times (R \times Q)^{0.479}$	=	40.81 (m <sup>3</sup> )
Concrete:	$V_c = 40.4 \times (R \times Q)^{0.684}$	=	1.58 (m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.278 \times V_c^{0.610}$	=	0.37 (ton)

Where,

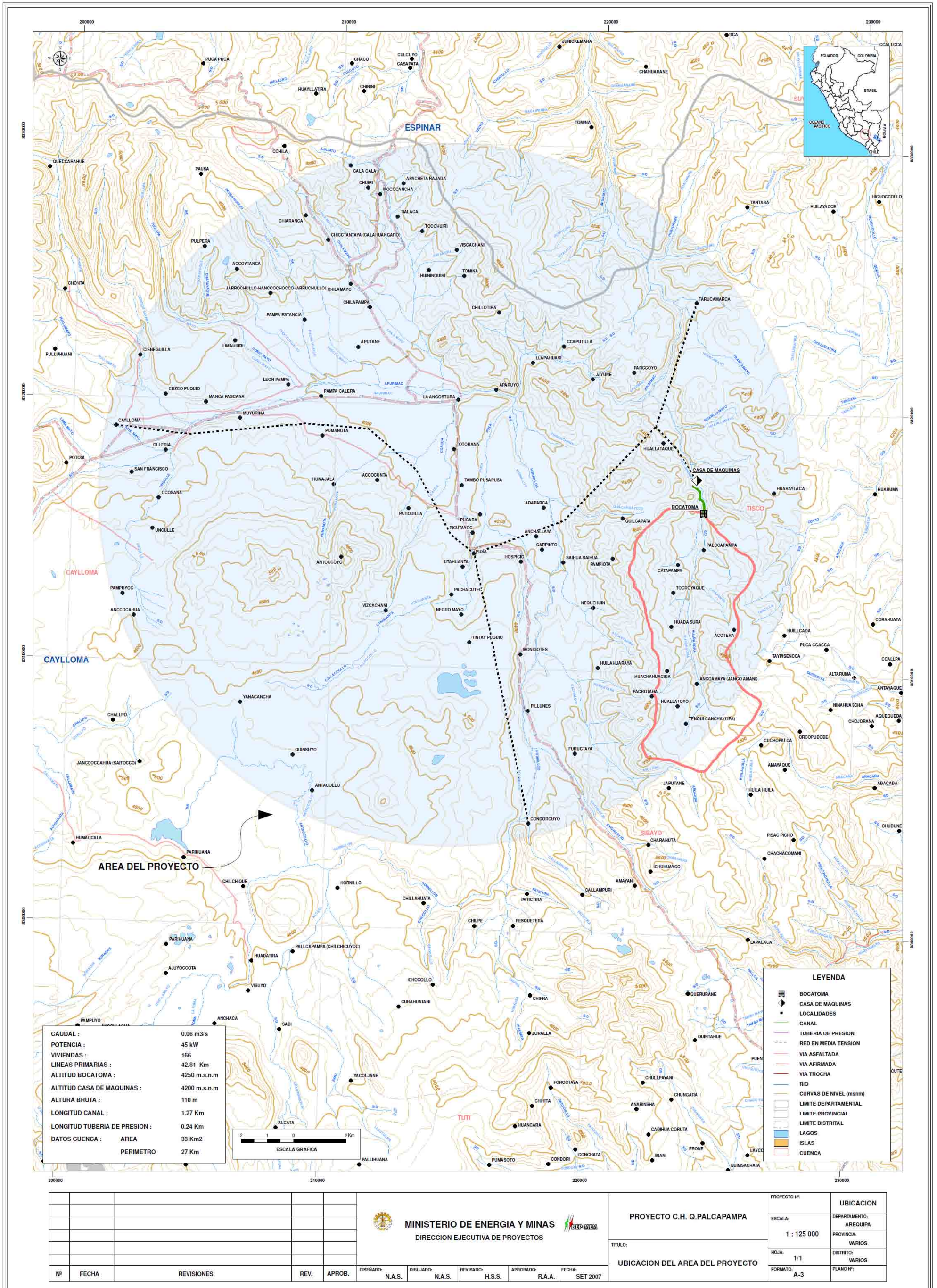
D: Diameter of Waterway =	0.50 (m)
R: Radius of Waterway =	0.25 (m) D/2
Q: Maximum Discharge =	0.035 (m <sup>3</sup> /s)

<span style="background-color: yellow; border: 1px solid black; display: inline-block; width: 10px; height: 10px;"></span>	: Input Cell
<span style="background-color: lightgreen; border: 1px solid black; display: inline-block; width: 10px; height: 10px;"></span>	: Calculation Cell
<span style="background-color: lightpurple; border: 1px solid black; display: inline-block; width: 10px; height: 10px;"></span>	: Reference Cell

**VI. Unit Price**      1USD = **3.00** S/. (as of November, 2007)

<b>(1) Civil Works</b>		
Excavation		
Open	: <b>5.53</b> (US\$/m <sup>3</sup> )	* (8.70+2.35) x 0.5 = \$5.53/m <sup>3</sup> , from CAPAECO and Fainal study on Omia <Human power and Machine excavation>
Tunnel	:      - (US\$/m <sup>3</sup> )	
Concrete		
Open	: <b>93.05</b> (US\$/m <sup>3</sup> )	* from CAPAECO (average of foundation, wall and structure concrete)
Tunnel	:      - (US\$/m <sup>3</sup> )	
Reinforcement Bar	: <b>1,070.00</b> (US\$/ton)	*\$1.07/kg. from CAPAECO
<b>(2) Hydraulic Equipment</b>		
Gate & Screen	: <b>8,811.04</b> (US\$/ton)	* from final study on Omia
Steel Penstock	: <b>3,100.00</b> (US\$/ton)	including installation
PVC (φ400)	: <b>26.33</b> (US\$/m)	RIB LOC for Headrace
PVC (φ200)	: <b>34.74</b> (US\$/m)	80% of TUBOPLAST( φ 315) for Penstock (C-10) = 43.42 x 0.8 = 34.74
<b>(3) Others</b>		
Access Road	: <b>979.65</b> (US\$/m)	Repair Work for Existing Unpaved Road
<b>(4) Transportation Cost</b>		
Arequipa to the site	: <b>14.83</b> (US\$/ton)	185km

# Palcapampa Map



**Appendix I-3 Construction Cost for La Majada Power Station*****I. Summary of Construction Cost for La Majada Power Station***

Unit: US\$

<i>Work Item</i>	<i>Construction Cost</i>	<i>Remarks</i>
<b><i>1. Preliminary Works</i></b>	<b>16,152</b>	
(1) Access Road	3,526	
(2) Facilities for Construction Office	4,620	Cost of Civil Works x 0.05
(3) Transportation cost	8,006	697.39ton x \$11.48/ton
<b><i>2. Cost for Environmental Measures</i></b>	<b>924</b>	Cost of Civil Works x 0.01
<b><i>3. Civil Works</i></b>	<b>92,414</b>	
(1) Weir	2,221	
(2) Intake	3,347	
(3) Settling Basin	3,487	
(4) Headrace	12,608	
(5) Head Tank	8,089	
(6) Penstock & Spillway Channel	51,489	
(7) Power House	9,813	
(8) Outlet	1,360	
(9) Miscellaneous Work	0	
<b><i>4. Hydraulic Equipment</i></b>	<b>120,800</b>	
(1) Gate & Screen	2,092	
(2) Penstock	0	
(3) PVC (φ500)	79,173	
(4) PVC (φ200)	19,454	
(5) Others	20,081	
<b><i>5. Electrical Equipment</i></b>	<b>41,100</b>	
<b><i>6. Direct Cost</i></b>	<b>271,390</b>	1.+2.+3.+4.+5.
<b><i>7. Engineering Cost</i></b>	<b>27,139</b>	6. x 0.1: Detailed Design and Supervision
<b><i>8. Contingent Budget</i></b>	<b>26,471</b>	6. x 0.098
<b><i>9. IGV</i></b>	<b>61,750</b>	19.00%
<b><i>10. Total Cost</i></b>	<b>386,750</b>	

**II. Detailed Statement of Transportation Cost for La Majada Power Station**

<i>Items</i>	<i>Unit</i>	<i>Quantity</i>	<i>Remarks</i>
<b>(1) Wier</b>		<b>17.05</b>	
a. Cements	ton	3.57	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		13.24	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.23	
<b>(2) Intake</b>		<b>31.35</b>	
a. Gate	ton	0.16	
b. Screen		0.07	
c. Cements		6.49	Cement: 0.27ton per concrete 1m <sup>3</sup>
d. Coarse aggregate		24.05	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
e. Reinforcement Bars		0.56	
<b>(3) Settling Basin</b>		<b>22.67</b>	
a. Cements	ton	4.54	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		16.82	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		1.31	
<b>(4) Headrace</b>		<b>16.32</b>	
a. PVC (φ500)	ton	16.32	Weight: 1,900m x 51.522kg/6m
<b>(5) Head Tank</b>		<b>44.55</b>	
a. Cements	ton	9.11	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		33.72	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		1.72	
<b>(6) Penstock &amp; Spillway Channel</b>		<b>502.74</b>	
a. Penstock Steel (φ200)	ton	0.00	
b. Penstock PVC (φ200)		4.67	Weight: 560m x 50.000kg/6m
c. Cements		105.89	Cement: 0.27ton per concrete 1m <sup>3</sup>
d. Coarse aggregate		392.18	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
e. Reinforcement Bars		0.00	
<b>(7) Power House</b>		<b>58.51</b>	
a. Cements	ton	11.92	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		44.14	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		2.45	
<b>(8) Outlet</b>		<b>4.21</b>	
a. Cements	ton	0.78	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		2.90	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.53	
<b>(9) Subtotal</b>		<b>697.39</b>	
<b>(10) Transportation Cost</b>		<b>8,006</b>	(9) x \$11.48/ton

**III. Detailed Statement of Civil Works Cost for La Majada Power Station**

Unit: US\$

<b>Work Items</b>	<b>Unit</b>	<b>Unit Price</b>	<b>Quantity</b>	<b>Cost</b>	<b>Remarks</b>
<b>(1) Wier</b>				<b>2,221</b>	
a. Excavation	m <sup>3</sup>	5.53	67.0	370	
b. Concrete	m <sup>3</sup>	93.05	13.2	1,231	
c. Reinforcement Bars	ton	1,070.00	0.2	250	
d. Others	-			370	(a+b+c) x 0.2 (including coffer dam construction, etc.)
<b>(2) Intake</b>				<b>3,347</b>	
a. Excavation	m <sup>3</sup>	5.53	13.2	72	
b. Concrete	m <sup>3</sup>	93.05	24.1	2,238	
c. Reinforcement Bars	ton	1,070.00	0.6	601	
d. Others	-			436	(a+b+c) x 0.15 (including coffer work, etc.)
<b>(3) Settling Basin</b>				<b>3,487</b>	
a. Excavation	m <sup>3</sup>	5.53	36.8	203	
b. Concrete	m <sup>3</sup>	93.05	16.8	1,565	
c. Reinforcement Bars	ton	1,070.00	1.3	1,402	
d. Others	-			317	(a+b+c) x 0.10 (including other works)
<b>(4) Headrace</b>				<b>12,608</b>	
a. Excavation	m <sup>3</sup>	5.53	1900.0	10,507	
b. Concrete	m <sup>3</sup>	93.05	0.0	0	
c. Reinforcement Bars	ton	1,070.00	0.0	0	
d. Others	-			2,101	(a+b+c) x 0.20 (including filling works)
<b>(5) Head Tank</b>				<b>8,089</b>	
a. Excavation	m <sup>3</sup>	5.53	144.9	801	
b. Concrete	m <sup>3</sup>	93.05	33.7	3,137	
c. Reinforcement Bars	ton	1,070.00	1.7	1,840	
d. Others	-			2,311	(a+b+c) x 0.40 (including gate, screen)
<b>(6) Penstock &amp; Spillway Channel</b>				<b>51,489</b>	
a. Excavation	m <sup>3</sup>	5.53	1865.7	10,317	
b. Concrete	m <sup>3</sup>	93.05	392.2	36,492	
c. Reinforcement Bars	ton	1,070.00	0.0	0	
d. Others	-			4,680	(a+b+c) x 0.10 (including filling works)
<b>(7) Power House</b>				<b>9,813</b>	
a. Excavation	m <sup>3</sup>	5.53	147.8	817	
b. Concrete	m <sup>3</sup>	93.05	44.1	4,107	
c. Reinforcement Bars	ton	1,070.00	2.5	2,625	
d. Others	-			2,264	(a+b+c) x 0.30 (including drainage work, wooden)
<b>(8) Outlet</b>				<b>1,360</b>	
a. Excavation	m <sup>3</sup>	5.53	62.4	345	
b. Concrete	m <sup>3</sup>	93.05	2.9	269	
c. Reinforcement Bars	ton	1,070.00	0.5	569	
d. Others	-			177	(a+b+c) x 0.15 (including coffer work, etc.)
<b>(9) Miscellaneous Work</b>	-			<b>0</b>	Σ(1)-(8) x 0.05 not consider
<b>(10) Subtotal</b>				<b>92,414</b>	

**IV. Detailed Statement of Hydraulic Equipment Cost for La Majada Power Station**

Unit: US\$

<i>Work Items</i>	<i>Unit</i>	<i>Unit Price</i>	<i>Quantity</i>	<i>Cost</i>	<i>Remarks</i>
<b>(1) Weir &amp; Spillway</b>				<b>0</b>	
a. Gate	ton	8,811.04	0.00	0	
<b>(2) Intake</b>				<b>2,092</b>	
a. Gate	ton	8,811.04	0.16	1,436	
b. Screen	ton	8,811.04	0.07	656	
<b>(3) Penstock Steel (φ200)</b>	ton	3,100.00	0.00	<b>0</b>	
<b>(4) PVC (φ500) for headrace</b>	m	41.67	1,900	<b>79,173</b>	
<b>(5) Penstock PVC (φ200) C-10</b>	m	34.74	560	<b>19,454</b>	
<b>(6) Subtotal</b>				<b>100,719</b>	
<b>(7) Others</b>				<b>20,081</b>	19.94%
<b>(8) Total</b>				<b>120,800</b>	



## V. Quantity

<b>(1) Weir</b>					
Excavation:	$V_e =$	$8.69 \times (H_d \times L)^{1.14}$	$=$	<b>67.01</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$8.64 \times (H_d^2 \times L)^{0.726}$	$=$	<b>13.24</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.0274 \times V_c^{0.830}$	$=$	<b>0.23</b>	(ton)
Weight of Gate:	$W_g =$	$0.145 \times Q_f^{0.692}$	$=$	<b>0.00</b>	(ton) (unconsidered)
Where,					
$H_d$ :	Height of Dam =	<b>0.30</b>	(m)		
$L$ :	Length of Dam =	<b>20.00</b>	(m)		
<b>(2) Intake</b>					
Excavation:	$V_e =$	$171 \times (R \times Q)^{0.666}$	$=$	<b>13.15</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$147 \times (R \times Q)^{0.470}$	$=$	<b>24.05</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.0145 \times V_c^{1.15}$	$=$	<b>0.56</b>	(ton)
Weight of Gate:	$W_g =$	$1.27 \times (R \times Q)^{0.533}$	$=$	<b>0.16</b>	(ton)
Weight of Screen:	$W_s =$	$0.701 \times (R \times Q)^{0.582}$	$=$	<b>0.07</b>	(ton)
Where,					
$D$ :	Diameter of Waterway =	<b>0.50</b>	(m)		
$R$ :	Radius of Waterway =	<b>0.25</b>	(m)	$D/2$	Assumption; Waterway Gradient = 1/1,000
$Q$ :	Maximum Discharge =	<b>0.085</b>	(m <sup>3</sup> /s)		
<b>(3) Settling Basin</b>					
Excavation:	$V_e =$	$515 \times Q^{1.07}$	$=$	<b>36.84</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$169 \times Q^{0.936}$	$=$	<b>16.82</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.120 \times V_c^{0.847}$	$=$	<b>1.31</b>	(ton)
Weight of Gate:	$W_g =$	$0.910 \times Q^{0.613}$	$=$	<b>0.20</b>	(ton)
Weight of Screen:	$W_s =$	$0.879 \times Q^{0.785}$	$=$	<b>0.13</b>	(ton)
Where,					
$Q$ :	Maximum Discharge =	<b>0.085</b>	(m <sup>3</sup> /s)		
<b>(4) Headrace</b>					
<b>In the case of PVCφ500:</b>					
Excavation:	$V_e = B \times H \times L$		$=$	<b>1,900.00</b>	(m <sup>3</sup> )
Concrete:	$V_c = ((H \times t \times 2) + (B + 2t) \times t) \times L$		$=$	<b>-</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.577 \times (V_c/L)^{0.888} \times L$		$=$	<b>-</b>	(ton)
Where,					
$Q$ :	Maximum Discharge =	<b>0.085</b>	(m <sup>3</sup> /s)		
$L$ :	Length of Channel =	<b>1,900.00</b>	(m)		
$B$ :	Width of Channel =	<b>1.00</b>	(m)		for excavation (2D from RIBLOC Brochure)
$H$ :	Height of Channel =	<b>1.00</b>	(m)		for excavation (2D from RIBLOC Brochure)
$t$ :	Thickness of Concrete =	<b>-</b>	(m)		
<b>(5) Head Tank</b>					
Excavation:	$V_e =$	$808 \times Q^{0.697}$	$=$	<b>144.95</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$197 \times Q^{0.716}$	$=$	<b>33.72</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.051 \times V_c$	$=$	<b>1.72</b>	(ton)
Where,					
$Q$ :	Maximum Discharge =	<b>0.085</b>	(m <sup>3</sup> /s)		

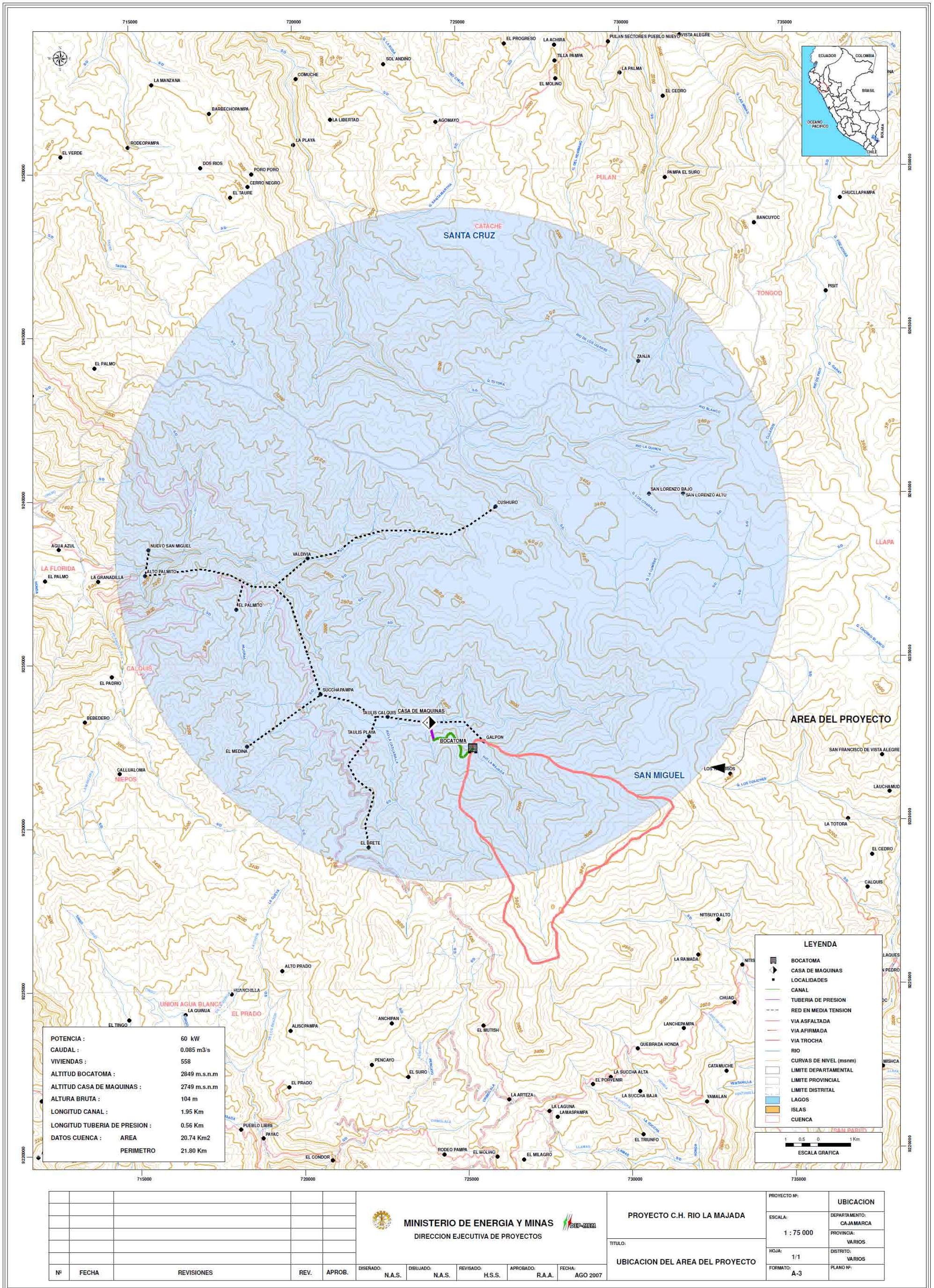
<b>(6) Penstock &amp; Spillway Channel</b>									
<b>Penstock (Steel)φ200:</b>									
Excavation:	$V_{e1} = 10.9 \times D_m^{1.33} \times L$	=	0.00 (m <sup>3</sup> )						
Concrete:	$V_{c1} = 2.14 \times D_m^{1.68} \times L$	=	0.00 (m <sup>3</sup> )						
Reinforcement Bars	$W_{r1} = 0.018 \times V_c$	=	0.00 (ton)						
Where,									
$D_m$ : v.g. Diameter of Penstock =	0.00 (m)								
L: Length of Penstock =	0.00 (m)								
Weight of Penstock	$W_{p1} = 7.85 \times \pi \times D_m \times t_m \times 10^{-3} \times 1.15 \times L$	=	0.00 (ton)						
Thickness of Penstock:	$t_m = 0.0362 \times H \times D_m + 2$	=	2.00 (mm)						
Where,									
$W_{p1}$ : Weight of Penstock	0.00 (ton)	(Tensile allowable Stress: 1,150 kgf/cm <sup>2</sup> )							
$t_m$ : Thickness of Penstock	2.00 (mm)								
$D_m$ : v.g. Diameter of Penstock =	0.00 (m)								
H: Design Head =	94.60 (m)	(Intake Water Level - Tailrace Water Level)							
L: Length of Penstock =	0.00 (m)								
<b>Penstock (PVC)φ200:</b>									
Excavation:	$V_e = B \times H \times L$	=	423.86 (m <sup>3</sup> )						
Where,									
Q: Maximum Discharge =	0.085 (m <sup>3</sup> /s)								
L: Length of Channel =	560.00 (m)								
B: Width of Channel =	0.87 (m)	from TUBOPLAST Brochure							
H: Height of Channel =	0.87 (m)	from TUBOPLAST Brochure							
<b>Spillway Channel:</b>									
	$(B \times H)^{0.5} = 1.09 \times Q^{0.379}$	=	0.43						
Excavation:	$V_e = 6.22 \times ((B \times H)^{0.5})^{1.04} \times L$	=	1,441.86 (m <sup>3</sup> )						
Concrete:	$V_c = H \times t \times 2 + (B + 2t) \times L$	=	392.18 (m <sup>3</sup> )						
Reinforcement Bars	$W_r = 0.577 \times (V_c/L)^{0.888} \times L$	=	0.00 (ton)						
Where,									
Q: Maximum Discharge =	0.085 (m <sup>3</sup> /s)								
L: Length of Channel =	560.00 (m)								
B: Width of Channel =	0.40 (m)								
H: Height of Channel =	0.60 (m)								
t: Thickness of Concrete =	0.15 (m)								
<b>Total Quantity of Penstock and Spillway Channel:</b>									
Excavation:	$V_e = V_{e1} + V_{e2}$	=	1,865.72 (m <sup>3</sup> )						
Concrete:	$V_c = V_{c1} + V_{c2}$	=	392.18 (m <sup>3</sup> )						
Reinforcement Bars	$W_r = W_{r1} + W_{r2}$	=	0.00 (ton)						
Weight of Penstock	$W_p = W_{p1}$	=	0.00 (ton)						
<b>(7) Power House</b>									
Excavation:	$V_e = 97.8 \times (Q \times H e^{2/3} \times n^{1/2})^{0.727}$	=	147.80 (m <sup>3</sup> )						
Concrete:	$V_c = 28.1 \times (Q \times H e^{2/3} \times n^{1/2})^{0.795}$	=	44.14 (m <sup>3</sup> )						
Reinforcement Bars	$W_r = 0.046 \times V_c^{1.05}$	=	2.45 (ton)						
Where,									
Q: Maximum Discharge =	0.085 (m <sup>3</sup> /s)								
He: Effective Head =	94.60 (m)								
n: quantity Unit of Turbine =	1.00								
<b>(8) Outlet</b>									
Excavation:	$V_e = 395 \times (R \times Q)^{0.479}$	=	62.43 (m <sup>3</sup> )						
Concrete:	$V_c = 40.4 \times (R \times Q)^{0.684}$	=	2.90 (m <sup>3</sup> )						
Reinforcement Bars	$W_r = 0.278 \times V_c^{0.610}$	=	0.53 (ton)						
Where,									
D: Diameter of Waterway =	0.50 (m)								
R: Radius of Waterway =	0.25 (m)	D/2							
Q: Maximum Discharge =	0.085 (m <sup>3</sup> /s)								
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**VI. Unit Price**

1USD = **3.00** S/. (as of November, 2007)

<b>(1) Civil Works</b>		
Excavation		
Open	: 5.53 (US\$/m <sup>3</sup> )	* (8.70+2.35) x 0.5 = \$5.53/m <sup>3</sup> , from CAPAECO and Fainal study on Omia <Human power and Machine excavation>
Tunnel	: - (US\$/m <sup>3</sup> )	
Concrete		
Open	: 93.05 (US\$/m <sup>3</sup> )	* from CAPAECO (average of foundation, wall and structure concrete)
Tunnel	: - (US\$/m <sup>3</sup> )	
Reinforcement Bar	: 1,070.00 (US\$/ton)	*\$1.07/kg, from CAPAECO
<b>(2) Hydraulic Equipment</b>		
Gate & Screen	: 8,811.04 (US\$/ton)	* from final study on Omia
Steel Penstock	: 3,100.00 (US\$/ton)	including installation
PVC (φ500)	: 41.67 (US\$/m)	RIB LOC for Headrace
PVC (φ200)	: 34.74 (US\$/m)	80% of TUBOPLAST( φ 315) for Penstock (C-10) = 43.42 x 0.8 = 34.74
<b>(3) Others</b>		
Access Road	: 979.65 (US\$/m)	Repair Work for Existing Unpaved Road
<b>(4) Transportation Cost</b>		
Cajamarca to the site	: 11.48 (US\$/ton)	88km

# La Majada Map



**Appendix I-4 Construction Cost for Quebrada Honda Power Station*****I. Summary of Construction Cost for Quebrada Honda Power Station***

Unit: US\$

<i>Work Item</i>	<i>Construction Cost</i>	<i>Remarks</i>
<b>1. Preliminary Works</b>	<b>7,579</b>	
(1) Access Road	2,351	
(2) Facilities for Construction Office	2,058	Cost of Civil Works x 0.05
(3) Transportation cost	3,170	287.48ton x \$11.03/ton
<b>2. Cost for Environmental Measures</b>	<b>411</b>	Cost of Civil Works x 0.01
<b>3. Civil Works</b>	<b>41,167</b>	
(1) Weir	1,282	
(2) Intake	2,582	
(3) Settling Basin	2,185	
(4) Headrace	6,625	
(5) Head Tank	5,539	
(6) Penstock & Spillway Channel	15,411	
(7) Power House	6,497	
(8) Outlet	1,046	
(9) Miscellaneous Work	0	
<b>4. Hydraulic Equipment</b>	<b>57,500</b>	
(1) Gate & Screen	1,564	
(2) Penstock	0	
(3) PVC (φ400)	41,074	
(4) PVC (φ150)	5,318	
(5) Others	9,544	
<b>5. Electrical Equipment</b>	<b>24,800</b>	
<b>6. Direct Cost</b>	<b>131,457</b>	1.+2.+3.+4.+5.
<b>7. Engineering Cost</b>	<b>13,146</b>	6. x 0.1: Detailed Design and Supervision
<b>8. Contingent Budget</b>	<b>12,397</b>	6. x 0.094
<b>9. IGV</b>	<b>29,830</b>	19.00%
<b>10. Total Cost</b>	<b>186,830</b>	

**II. Detailed Statement of Transportation Cost for Quebrada Honda Power Station**

<i>Items</i>	<i>Unit</i>	<i>Quantity</i>	<i>Remarks</i>
<b>(1) Wier</b>		<b>9.48</b>	
a. Cements	ton	1.98	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		7.35	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.14	
<b>(2) Intake</b>		<b>24.40</b>	
a. Gate	ton	0.12	
b. Screen		0.05	
c. Cements		5.06	Cement: 0.27ton per concrete 1m <sup>3</sup>
d. Coarse aggregate		18.74	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
e. Reinforcement Bars		0.42	
<b>(3) Settling Basin</b>		<b>13.86</b>	
a. Cements	ton	2.76	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		10.24	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.86	
<b>(4) Headrace</b>		<b>10.72</b>	
a. PVC (φ400)	ton	10.72	Weight: 1,560m x 41.214kg/6m
<b>(5) Head Tank</b>		<b>30.47</b>	
a. Cements	ton	6.23	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		23.06	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		1.18	
<b>(6) Penstock &amp; Spillway Channel</b>		<b>156.74</b>	
a. Penstock Steel (φ150)	ton	0.00	
b. Penstock PVC (φ150)		0.93	Weight: 175m x 32.000kg/6m
c. Cements		33.12	Cement: 0.27ton per concrete 1m <sup>3</sup>
d. Coarse aggregate		122.68	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
e. Reinforcement Bars		0.00	
<b>(7) Power House</b>		<b>38.83</b>	
a. Cements	ton	7.92	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		29.32	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		1.60	
<b>(8) Outlet</b>		<b>2.99</b>	
a. Cements	ton	0.54	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		2.02	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.43	
<b>(9) Subtotal</b>		<b>287.48</b>	
<b>(10) Transportation Cost</b>		<b>3,171</b>	(9) x \$11.03/ton

**III. Detailed Statement of Civil Works Cost for Quebrada Honda Power Station**

Unit: US\$

<i>Work Items</i>	<i>Unit</i>	<i>Unit Price</i>	<i>Quantity</i>	<i>Cost</i>	<i>Remarks</i>
<b>(1) Wier</b>				<b>1,282</b>	
a. Excavation	m <sup>3</sup>	5.53	42.2	233	
b. Concrete	m <sup>3</sup>	93.05	7.3	683	
c. Reinforcement Bars	ton	1,070.00	0.1	153	
d. Others	-			213	(a+b+c) x 0.2 (including coffer dam construction, etc.)
<b>(2) Intake</b>				<b>2,582</b>	
a. Excavation	m <sup>3</sup>	5.53	9.2	51	
b. Concrete	m <sup>3</sup>	93.05	18.7	1,744	
c. Reinforcement Bars	ton	1,070.00	0.4	451	
d. Others	-			336	(a+b+c) x 0.15 (including coffer work, etc.)
<b>(3) Settling Basin</b>				<b>2,185</b>	
a. Excavation	m <sup>3</sup>	5.53	20.9	115	
b. Concrete	m <sup>3</sup>	93.05	10.2	952	
c. Reinforcement Bars	ton	1,070.00	0.9	920	
d. Others	-			198	(a+b+c) x 0.10 (including other works)
<b>(4) Headrace</b>				<b>6,625</b>	
a. Excavation	m <sup>3</sup>	5.53	998.4	5,521	
b. Concrete	m <sup>3</sup>	93.05	0.0	0	
c. Reinforcement Bars	ton	1,070.00	0.0	0	
d. Others	-			1,104	(a+b+c) x 0.20 (including filling works)
<b>(5) Head Tank</b>				<b>5,539</b>	
a. Excavation	m <sup>3</sup>	5.53	100.1	553	
b. Concrete	m <sup>3</sup>	93.05	23.1	2,146	
c. Reinforcement Bars	ton	1,070.00	1.2	1,258	
d. Others	-			1,582	(a+b+c) x 0.40 (including gate, screen)
<b>(6) Penstock &amp; Spillway Channel</b>				<b>15,411</b>	
a. Excavation	m <sup>3</sup>	5.53	469.3	2,595	
b. Concrete	m <sup>3</sup>	93.05	122.7	11,415	
c. Reinforcement Bars	ton	1,070.00	0.0	0	
d. Others	-			1,401	(a+b+c) x 0.10 (including filling works)
<b>(7) Power House</b>				<b>6,497</b>	
a. Excavation	m <sup>3</sup>	5.53	101.7	562	
b. Concrete	m <sup>3</sup>	93.05	29.3	2,728	
c. Reinforcement Bars	ton	1,070.00	1.6	1,708	
d. Others	-			1,499	(a+b+c) x 0.30 (including drainage work, wooden)
<b>(8) Outlet</b>				<b>1,046</b>	
a. Excavation	m <sup>3</sup>	5.53	48.4	267	
b. Concrete	m <sup>3</sup>	93.05	2.0	187	
c. Reinforcement Bars	ton	1,070.00	0.4	456	
d. Others	-			136	(a+b+c) x 0.15 (including coffer work, etc.)
<b>(9) Miscellaneous Work</b>	-			<b>0</b>	Σ(1)-(8) x 0.05 not consider
<b>(10) Subtotal</b>				<b>41,167</b>	

**IV. Detailed Statement of Hydraulic Equipment Cost for Quebrada Honda Power Station**

Unit: US\$

<i>Work Items</i>	<i>Unit</i>	<i>Unit Price</i>	<i>Quantity</i>	<i>Cost</i>	<i>Remarks</i>
<b>(1) Weir &amp; Spillway</b>				<b>0</b>	
a. Gate	ton	8,811.04	0.00	0	
<b>(2) Intake</b>				<b>1,564</b>	
a. Gate	ton	8,811.04	0.12	1,082	
b. Screen	ton	8,811.04	0.05	482	
<b>(3) Penstock Steel (φ150)</b>	ton	3,100.00	0.00	<b>0</b>	
<b>(4) PVC (φ400) for headrace</b>	m	26.33	1,560	<b>41,074</b>	
<b>(5) Penstock PVC (φ150) C-10</b>	m	30.39	175	<b>5,318</b>	
<b>(6) Subtotal</b>				<b>47,956</b>	
<b>(7) Others</b>				<b>9,544</b>	19.90%
<b>(8) Total</b>				<b>57,500</b>	



## V. Quantity

### (1) Weir

Excavation:	$V_e =$	$8.69 \times (H_d \times L)^{1.14}$	$=$	<b>42.21</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$8.64 \times (H_d^2 \times L)^{0.726}$	$=$	<b>7.35</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.0274 \times V_c^{0.830}$	$=$	<b>0.14</b>	(ton)
Weight of Gate:	$W_g =$	$0.145 \times Q_f^{0.692}$	$=$	<b>0.00</b>	(ton) (unconsidered)

Where,

$H_d$ :	Height of Dam =	<b>0.20</b>	(m)
$L$ :	Length of Dam =	<b>20.00</b>	(m)

### (2) Intake

Excavation:	$V_e =$	$171 \times (R \times Q)^{0.666}$	$=$	<b>9.24</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$147 \times (R \times Q)^{0.470}$	$=$	<b>18.74</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.0145 \times V_c^{1.15}$	$=$	<b>0.42</b>	(ton)
Weight of Gate:	$W_g =$	$1.27 \times (R \times Q)^{0.533}$	$=$	<b>0.12</b>	(ton)
Weight of Screen:	$W_s =$	$0.701 \times (R \times Q)^{0.582}$	$=$	<b>0.05</b>	(ton)

Where,

$D$ :	Diameter of Waterway =	<b>0.50</b>	(m)	
$R$ :	Radius of Waterway =	<b>0.25</b>	(m)	$D/2$ Assumption; Waterway Gradient = 1/1,000
$Q$ :	Maximum Discharge =	<b>0.050</b>	(m <sup>3</sup> /s)	

### (3) Settling Basin

Excavation:	$V_e =$	$515 \times Q^{1.07}$	$=$	<b>20.88</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$169 \times Q^{0.936}$	$=$	<b>10.24</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.120 \times V_c^{0.847}$	$=$	<b>0.86</b>	(ton)
Weight of Gate:	$W_g =$	$0.910 \times Q^{0.613}$	$=$	<b>0.15</b>	(ton)
Weight of Screen:	$W_s =$	$0.879 \times Q^{0.785}$	$=$	<b>0.08</b>	(ton)

Where,

$Q$ :	Maximum Discharge =	<b>0.050</b>	(m <sup>3</sup> /s)
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### (4) Headrace

In the case of PVC $\phi$ 400:

Excavation:	$V_e = B \times H \times L$	$=$	<b>998.40</b>	(m <sup>3</sup> )
Concrete:	$V_c = ((H \times t \times 2) + (B + 2t) \times t) \times L$	$=$	-	(m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.577 \times (V_c/L)^{0.888} \times L$	$=$	-	(ton)

Where,

$Q$ :	Maximum Discharge =	<b>0.050</b>	(m <sup>3</sup> /s)	
$L$ :	Length of Channel =	<b>1,560.00</b>	(m)	
$B$ :	Width of Channel =	<b>0.80</b>	(m)	for excavation (2D from RIBLOC Brochure)
$H$ :	Height of Channel =	<b>0.80</b>	(m)	for excavation (2D from RIBLOC Brochure)
$t$ :	Thickness of Concrete =	-	(m)	

### (5) Head Tank

Excavation:	$V_e =$	$808 \times Q^{0.697}$	$=$	<b>100.14</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$197 \times Q^{0.716}$	$=$	<b>23.06</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.051 \times V_c$	$=$	<b>1.18</b>	(ton)

Where,

$Q$ :	Maximum Discharge =	<b>0.050</b>	(m <sup>3</sup> /s)
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**(6) Penstock & Spillway Channel**

**Penstock (Steel)φ150:**

Excavation:	$V_{e1} =$	$10.9 \times D_m^{1.33} \times L$	$=$	0.00 (m <sup>3</sup> )
Concrete:	$V_{c1} =$	$2.14 \times D_m^{1.68} \times L$	$=$	0.00 (m <sup>3</sup> )
Reinforcement Bars	$W_{r1} =$	$0.018 \times V_c$	$=$	0.00 (ton)

Where,

$D_m$ : avg. Diameter of Penstock =	0.00 (m)
L: Length of Penstock =	0.00 (m)

Weight of Penstock	$W_{p1} = 7.85 \times \pi \times D_m \times t_m \times 10^{-3} \times 1.15 \times L$	$=$	0.00 (ton)
Thickness of Penstock:	$t_m = 0.0362 \times H \times D_m + 2$	$=$	2.00 (mm)

Where,

$W_{p1}$ : Weight of Penstock	0.00 (ton)	(Tensile allowable Stress: 1,150 kgf/cm <sup>2</sup> )
tm: Thickness of Penstock	2.00 (mm)	
$D_m$ : avg. Diameter of Penstock =	0.00 (m)	
H: Design Head =	96.90 (m)	(Intake Water Level - Tailrace Water Level)
L: Length of Penstock =	0.00 (m)	

**Penstock (PVC)φ150:**

Excavation:	$V_e = B \times H \times L$	$=$	103.76 (m <sup>3</sup> )
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Where,

Q: Maximum Discharge =	0.050 (m <sup>3</sup> /s)	
L: Length of Channel =	175.00 (m)	
B: Width of Channel =	0.77 (m)	from TUBOPLAST Brochure
H: Height of Channel =	0.77 (m)	from TUBOPLAST Brochure

**Spillway Channel:**

	$(B \times H)^{0.5} = 1.09 \times Q^{0.379}$	$=$	0.35
Excavation:	$V_e = 6.22 \times ((B \times H)^{0.5})^{1.04} \times L$	$=$	365.54 (m <sup>3</sup> )
Concrete:	$V_c = H \times t \times 2 + (B + 2t) \times L$	$=$	122.68 (m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.577 \times (V_c/L)^{0.888} \times L$	$=$	0.00 (ton)

Where,

Q: Maximum Discharge =	0.050 (m <sup>3</sup> /s)
L: Length of Channel =	175.00 (m)
B: Width of Channel =	0.40 (m)
H: Height of Channel =	0.60 (m)
t: Thickness of Concrete =	0.15 (m)

**Total Quantity of Penstock and Spillway Channel:**

Excavation:	$V_e =$	$V_{e1} + V_{e2}$	$=$	469.30 (m <sup>3</sup> )
Concrete:	$V_c =$	$V_{c1} + V_{c2}$	$=$	122.68 (m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$W_{r1} + W_{r2}$	$=$	0.00 (ton)
Weight of Penstock	$W_p =$	$W_{p1}$	$=$	0.00 (ton)

**(7) Power House**

Excavation:	$V_e = 97.8 \times (Q \times H_e^{2/3} \times n^{1/2})^{0.727}$	=	<b>101.67</b>	(m <sup>3</sup> )
Concrete:	$V_c = 28.1 \times (Q \times H_e^{2/3} \times n^{1/2})^{0.795}$	=	<b>29.32</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.046 \times V_c^{1.05}$	=	<b>1.60</b>	(ton)

Where,




Q: Maximum Discharge =	<b>0.050</b>	(m <sup>3</sup> /s)
He: Effective Head =	<b>96.90</b>	(m)
n: quantity Unit of Turbine =	<b>1.00</b>	

**(8) Outlet**

Excavation:	$V_e = 395 \times (R \times Q)^{0.479}$	=	<b>48.42</b>	(m <sup>3</sup> )
Concrete:	$V_c = 40.4 \times (R \times Q)^{0.684}$	=	<b>2.02</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.278 \times V_c^{0.610}$	=	<b>0.43</b>	(ton)

Where,

D: Diameter of Waterway =	<b>0.50</b>	(m)
R: Radius of Waterway =	<b>0.25</b>	(m)      D/2
Q: Maximum Discharge =	<b>0.050</b>	(m <sup>3</sup> /s)

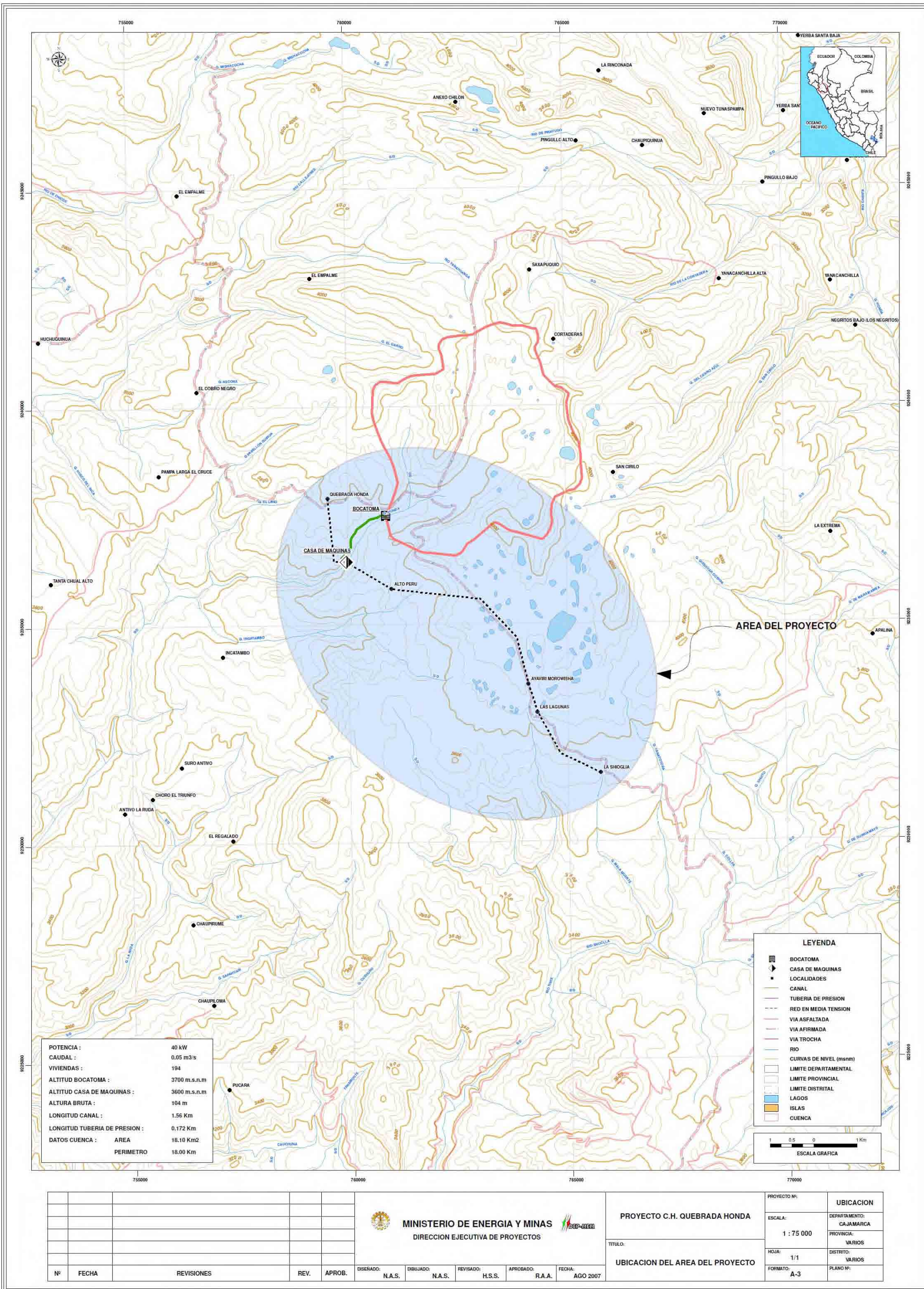
	: Input Cell
	: Calculation Cell
	: Reference Cell

**VI. Unit Price**

1USD = **3.00** S/. (as of November, 2007)

<b>(1) Civil Works</b>		
Excavation		
Open	:	<b>5.53</b> (US\$/m <sup>3</sup> ) * (8.70+2.35) x 0.5 = \$5.53/m <sup>3</sup> , from CAPAECO and Fainal study on Omia <Human power and Machine excavation>
Tunnel	:	- (US\$/m <sup>3</sup> )
Concrete		
Open	:	<b>93.05</b> (US\$/m <sup>3</sup> ) * from CAPAECO (average of foundation, wall and structure concrete)
Tunnel	:	- (US\$/m <sup>3</sup> )
Reinforcement Bar	:	<b>1,070.00</b> (US\$/ton) *\$1.07/kg, from CAPAECO
<b>(2) Hydraulic Equipment</b>		
Gate & Screen	:	<b>8,811.04</b> (US\$/ton) * from final study on Omia
Steel Penstock	:	<b>3,100.00</b> (US\$/ton) including installation
PVC (φ400)	:	<b>26.33</b> (US\$/m) RIB LOC for Headrace
PVC (φ150)	:	<b>30.39</b> (US\$/m) 80% of TUBOPLAST( φ 315) for Penstock (C-10) = 43.42 x 0.7 = 30.39
<b>(3) Others</b>		
Access Road	:	<b>979.65</b> (US\$/m) Repair Work for Existing Unpaved Road
<b>(4) Transportation Cost</b>		
Cajamarca to the site	:	<b>11.03</b> (US\$/ton) 75km

# Quebrada Honda Map



## Appendix I-5 Construction Cost for Yerba Buena Power Station (in the case of PVC for Headrace)

### I. Summary of Construction Cost for Yerba Buena Power Station

Unit: US\$

<i>Work Item</i>	<i>Construction Cost</i>	<i>Remarks</i>
<b>1. Preliminary Works</b>	<b>8,039</b>	
(1) Access Road	0	
(2) Facilities for Construction Office	3,318	Cost of Civil Works x 0.05
(3) Transportation cost	4,721	Cajamarca to the site, 454ton x \$10.4/ton
<b>2. Cost for Environmental Measures</b>	<b>663</b>	Cost of Civil Works x 0.01
<b>3. Civil Works</b>	<b>66,373</b>	
(1) Weir	2,798	
(2) Intake	5,384	
(3) Settling Basin	4,448	
(4) Headrace	8,599	
(5) Head Tank	9,850	
(6) Penstock & Spillway Channel	20,674	
(7) Power House	12,407	
(8) Outlet	2,213	
(9) Miscellaneous Work	0	
<b>4. Hydraulic Equipment</b>	<b>109,000</b>	
(1) Gate & Screen	3,560	
(2) Penstock	1,610	
(3) PVC (φ600)	77,571	
(4) PVC (φ315)	8,249	
(5) Others	18,010	
<b>5. Electrical Equipment</b>	<b>52,800</b>	
<b>6. Direct Cost</b>	<b>236,875</b>	1.+2.+3.+4.+5.
<b>7. Engineering Cost</b>	<b>23,688</b>	6. x 0.1: Detailed Design and Supervision
<b>8. Contingent Budget</b>	<b>23,438</b>	6. x 0.099
<b>9. IGV</b>	<b>53,960</b>	19.00%
<b>10. Total Cost</b>	<b>337,960</b>	

**II. Detailed Statement of Transportation Cost for Yerba Buena Power Station**

<i>Items</i>	<i>Unit</i>	<i>Quantity</i>	<i>Remarks</i>
<b>(1) Wier</b>		<b>23.17</b>	
a. Cements	ton	4.86	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		18.01	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.30	
<b>(2) Intake</b>		<b>49.52</b>	
a. Gate	ton	0.27	
b. Screen		0.13	
c. Cements		10.24	Cement: 0.27ton per concrete 1m <sup>3</sup>
d. Coarse aggregate		37.93	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
e. Reinforcement Bars		0.95	
<b>(3) Settling Basin</b>		<b>29.28</b>	
a. Cements	ton	5.88	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		21.77	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		1.63	
<b>(4) Headrace</b>		<b>17.29</b>	
a. PVC (φ600)	ton	17.29	Weight: 1,300m x 79.8kg/6m = 17.3ton
<b>(5) Head Tank</b>		<b>54.28</b>	
a. Cements	ton	11.09	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		41.09	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		2.10	
<b>(6) Penstock &amp; Spillway Channel</b>		<b>198.62</b>	
a. Penstock Steel (φ300)	ton	0.52	
b. Penstock PVC (φ315)		3.89	Weight: 190m x 122.833kg/6m = 3.9ton
c. Cements		41.27	Cement: 0.27ton per concrete 1m <sup>3</sup>
d. Coarse aggregate		152.84	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
e. Reinforcement Bars		0.10	
<b>(7) Power House</b>		<b>73.87</b>	
a. Cements	ton	15.04	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		55.70	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		3.13	
<b>(8) Outlet</b>		<b>7.94</b>	
a. Cements	ton	1.52	Cement: 0.27ton per concrete 1m <sup>3</sup>
b. Coarse aggregate		5.63	Coarse aggregate: 1ton per concrete 1m <sup>3</sup>
c. Reinforcement Bars		0.80	
<b>(9) Subtotal</b>		<b>453.97</b>	
<b>(10) Transportation Cost</b>		<b>4,721</b>	(9) x \$10.4/ton: Cajamarca to Yerba Buena

**III. Detailed Statement of Civil Works Cost for Yerba Buena Power Station**

Unit: US\$

<i>Work Items</i>	<i>Unit</i>	<i>Unit Price</i>	<i>Quantity</i>	<i>Cost</i>	<i>Remarks</i>
<b>(1) Wier</b>				<b>2,798</b>	
a. Excavation	m <sup>3</sup>	5.53	60.7	335	
b. Concrete	m <sup>3</sup>	93.05	18.0	1,675	
c. Reinforcement Bars	ton	1,070.00	0.3	322	
d. Others	-			466	(a+b+c) x 0.2 (including coffer dam construction, etc.)
<b>(2) Intake</b>				<b>5,384</b>	
a. Excavation	m <sup>3</sup>	5.53	25.1	138	
b. Concrete	m <sup>3</sup>	93.05	37.9	3,529	
c. Reinforcement Bars	ton	1,070.00	0.9	1,015	
d. Others	-			702	(a+b+c) x 0.15 (including coffer work, etc.)
<b>(3) Settling Basin</b>				<b>4,448</b>	
a. Excavation	m <sup>3</sup>	5.53	49.5	273	
b. Concrete	m <sup>3</sup>	93.05	21.8	2,026	
c. Reinforcement Bars	ton	1,070.00	1.6	1,745	
d. Others	-			404	(a+b+c) x 0.10 (including other works)
<b>(4) Headrace</b>				<b>8,599</b>	
a. Excavation	m <sup>3</sup>	5.53	1296.0	7,166	
b. Concrete	m <sup>3</sup>	93.05	0.0	0	
c. Reinforcement Bars	ton	1,070.00	0.0	0	
d. Others	-			1,433	(a+b+c) x 0.20 (including filling works)
<b>(5) Head Tank</b>				<b>9,850</b>	
a. Excavation	m <sup>3</sup>	5.53	175.7	971	
b. Concrete	m <sup>3</sup>	93.05	41.1	3,823	
c. Reinforcement Bars	ton	1,070.00	2.1	2,242	
d. Others	-			2,814	(a+b+c) x 0.40 (including gate, screen)
<b>(6) Penstock &amp; Spillway Channel</b>				<b>20,674</b>	
a. Excavation	m <sup>3</sup>	5.53	807.6	4,465	
b. Concrete	m <sup>3</sup>	93.05	152.8	14,221	
c. Reinforcement Bars	ton	1,070.00	0.1	109	
d. Others	-			1,879	(a+b+c) x 0.10 (including filling works)
<b>(7) Power House</b>				<b>12,407</b>	
a. Excavation	m <sup>3</sup>	5.53	182.8	1,011	
b. Concrete	m <sup>3</sup>	93.05	55.7	5,182	
c. Reinforcement Bars	ton	1,070.00	3.1	3,351	
d. Others	-			2,863	(a+b+c) x 0.30 (including drainage work, wooden)
<b>(8) Outlet</b>				<b>2,213</b>	
a. Excavation	m <sup>3</sup>	5.53	99.3	549	
b. Concrete	m <sup>3</sup>	93.05	5.6	523	
c. Reinforcement Bars	ton	1,070.00	0.8	853	
d. Others	-			288	(a+b+c) x 0.15 (including coffer work, etc.)
<b>(9) Miscellaneous Work</b>				<b>0</b>	Σ(1)-(8) x 0.05 not consider
<b>(10) Subtotal</b>				<b>66,373</b>	



**IV. Detailed Statement of Hydraulic Equipment Cost for Yerba Buena Power Station**

Unit: US\$

<i>Work Items</i>	<i>Unit</i>	<i>Unit Price</i>	<i>Quantity</i>	<i>Cost</i>	<i>Remarks</i>
<b>(1) Weir &amp; Spillway</b>				<b>0</b>	
a. Gate	ton	8,811.04	0.00	0	
<b>(2) Intake</b>				<b>3,560</b>	
a. Gate	ton	8,811.04	0.27	2,407	
b. Screen	ton	8,811.04	0.13	1,153	
<b>(3) Penstock Steel (φ315)</b>	ton	3,100.00	0.52	<b>1,610</b>	
<b>(4) PVC (φ600) for headrace</b>	m	59.67	1,300	<b>77,571</b>	
<b>(5) Penstock PVC (φ315) C-10</b>	m	43.42	190	<b>8,249</b>	
<b>(6) Subtotal</b>				<b>90,990</b>	
<b>(7) Others</b>				<b>18,010</b>	19.79%
<b>(8) Total</b>				<b>109,000</b>	

## V. Quantity

<b>(1) Weir</b>					
Excavation:	$V_e =$	$8.69 \times (H_d \times L)^{1.14}$	$=$	<b>60.68</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$8.64 \times (H_d^2 \times L)^{0.726}$	$=$	<b>18.01</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.0274 \times V_c^{0.830}$	$=$	<b>0.30</b>	(ton)
Weight of Gate:	$W_g =$	$0.145 \times Q_f^{0.692}$	$=$	<b>0.00</b>	(ton) (unconsidered)
Where,					
$H_d$ :	Height of Dam =	<b>0.50</b>	(m)		
$L$ :	Length of Dam =	<b>11.00</b>	(m)		
<b>(2) Intake</b>					
Excavation:	$V_e =$	$171 \times (R \times Q)^{0.666}$	$=$	<b>25.08</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$147 \times (R \times Q)^{0.470}$	$=$	<b>37.93</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.0145 \times V_c^{1.15}$	$=$	<b>0.95</b>	(ton)
Weight of Gate:	$W_g =$	$1.27 \times (R \times Q)^{0.533}$	$=$	<b>0.27</b>	(ton)
Weight of Screen:	$W_s =$	$0.701 \times (R \times Q)^{0.582}$	$=$	<b>0.13</b>	(ton)
Where,					
$D$ :	Diameter of Waterway =	<b>1.00</b>	(m)		
$R$ :	Radius of Waterway =	<b>0.50</b>	(m)	$D/2$	Assumption; Waterway Gradient = 1/1,000
$Q$ :	Maximum Discharge =	<b>0.112</b>	(m <sup>3</sup> /s)		
<b>(3) Settling Basin</b>					
Excavation:	$V_e =$	$515 \times Q^{1.07}$	$=$	<b>49.48</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$169 \times Q^{0.956}$	$=$	<b>21.77</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.120 \times V_c^{0.847}$	$=$	<b>1.63</b>	(ton)
Weight of Gate:	$W_g =$	$0.910 \times Q^{0.613}$	$=$	<b>0.24</b>	(ton)
Weight of Screen:	$W_s =$	$0.879 \times Q^{0.785}$	$=$	<b>0.16</b>	(ton)
Where,					
$Q$ :	Maximum Discharge =	<b>0.112</b>	(m <sup>3</sup> /s)		
<b>(4) Headrace</b>					
<b>In the case of PVC<math>\phi</math>600:</b>					
Excavation:	$V_e = B \times H \times L$		$=$	<b>1,296.00</b>	(m <sup>3</sup> )
Concrete:	$V_c = ((H \times t \times 2) + (B + 2t) \times t) \times L$		$=$	-	(m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.577 \times (V_c/L)^{0.888} \times L$		$=$	-	(ton)
Where,					
$Q$ :	Maximum Discharge =	<b>0.112</b>	(m <sup>3</sup> /s)		
$L$ :	Length of Channel =	<b>900.00</b>	(m)		Existing canal = 400m among total length of 1,300m
$B$ :	Width of Channel =	<b>1.20</b>	(m)		for excavation (2D from RIBLOC Brochure)
$H$ :	Height of Channel =	<b>1.20</b>	(m)		for excavation (2D from RIBLOC Brochure)
$t$ :	Thickness of Concrete =	-	(m)		
<b>(5) Head Tank</b>					
Excavation:	$V_e =$	$808 \times Q^{0.697}$	$=$	<b>175.68</b>	(m <sup>3</sup> )
Concrete:	$V_c =$	$197 \times Q^{0.716}$	$=$	<b>41.09</b>	(m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$0.051 \times V_c$	$=$	<b>2.10</b>	(ton)
Where,					
$Q$ :	Maximum Discharge =	<b>0.112</b>	(m <sup>3</sup> /s)		

**(6) Penstock & Spillway Channel**

**Penstock (Steel)φ315:**

Excavation:	$V_{e1} =$	$10.9 \times D_m^{1.33} \times L$	$=$	43.96 (m <sup>3</sup> )
Concrete:	$V_{c1} =$	$2.14 \times D_m^{1.68} \times L$	$=$	5.66 (m <sup>3</sup> )
Reinforcement Bars	$W_{r1} =$	$0.018 \times V_c$	$=$	0.10 (ton)

Where,

$D_m$ : avg. Diameter of Penstock	$=$	0.30 (m)
L: Length of Penstock	$=$	20.00 (m)

Weight of Penstock	$W_{p1} = 7.85 \times \pi \times D_m \times t_m \times 10^{-3} \times 1.15 \times L$	$=$	0.52 (ton)
Thickness of Penstock:	$t_m = 0.0362 \times H \times D_m + 2$	$=$	3.05 (mm)

Where,

$W_{p1}$ : Weight of Penstock	$=$	0.52 (ton)	(Tensile allowable Stress: 1,150 kgf/cm <sup>2</sup> )
$t_m$ : Thickness of Penstock	$=$	3.05 (mm)	
$D_m$ : avg. Diameter of Penstock	$=$	0.30 (m)	
H: Design Head	$=$	97.00 (m)	(Intake Water Level - Tailrace Water Level)
L: Length of Penstock	$=$	20.00 (m)	

**Penstock (PVC)φ315:**

Excavation:	$V_e = B \times H \times L$	$=$	160.82 (m <sup>3</sup> )
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Where,

Q: Maximum Discharge	$=$	0.112 (m <sup>3</sup> /s)	
L: Length of Channel	$=$	190.00 (m)	
B: Width of Channel	$=$	0.92 (m)	from TUBOPLAST Brochure
H: Height of Channel	$=$	0.92 (m)	from TUBOPLAST Brochure

**Spillway Channel:**

	$(B \times H)^{0.5} = 1.09 \times Q^{0.379}$	$=$	0.48
Excavation:	$V_e = 6.22 \times ((B \times H)^{0.5})^{1.04} \times L$	$=$	602.80 (m <sup>3</sup> )
Concrete:	$V_c = H \times t \times 2 + (B + 2t) \times L$	$=$	147.18 (m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.577 \times (V_c/L)^{0.888} \times L$	$=$	0.00 (ton)

Where,

Q: Maximum Discharge	$=$	0.112 (m <sup>3</sup> /s)
L: Length of Channel	$=$	210.00 (m)
B: Width of Channel	$=$	0.40 (m)
H: Height of Channel	$=$	0.60 (m)
t: Thickness of Concrete	$=$	0.15 (m)

**Total Quantity of Penstock and Spillway Channel:**

Excavation:	$V_e =$	$V_{e1} + V_{e2}$	$=$	807.57 (m <sup>3</sup> )
Concrete:	$V_c =$	$V_{c1} + V_{c2}$	$=$	152.84 (m <sup>3</sup> )
Reinforcement Bars	$W_r =$	$W_{r1} + W_{r2}$	$=$	0.10 (ton)
Weight of Penstock	$W_p =$	$W_{p1}$	$=$	0.52 (ton)

**(7) Power House**

Excavation:	$V_e = 97.8 \times (Q \times H_e^{2/3} \times n^{1/2})^{0.727}$	=	<b>182.83</b> (m <sup>3</sup> )
Concrete:	$V_c = 28.1 \times (Q \times H_e^{2/3} \times n^{1/2})^{0.795}$	=	<b>55.70</b> (m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.046 \times V_c^{1.05}$	=	<b>3.13</b> (ton)

Where,




Q: Maximum Discharge =	<b>0.112</b> (m <sup>3</sup> /s)
He: Effective Head =	<b>97.00</b> (m)
n: quantity Unit of Turbine =	<b>1.00</b>

**(8) Outlet**

Excavation:	$V_e = 395 \times (R \times Q)^{0.479}$	=	<b>99.31</b> (m <sup>3</sup> )
Concrete:	$V_c = 40.4 \times (R \times Q)^{0.684}$	=	<b>5.63</b> (m <sup>3</sup> )
Reinforcement Bars	$W_r = 0.278 \times V_c^{0.610}$	=	<b>0.80</b> (ton)

Where,

D: Diameter of Waterway =	<b>1.00</b> (m)	
R: Radius of Waterway =	<b>0.50</b> (m)	D/2
Q: Maximum Discharge =	<b>0.112</b> (m <sup>3</sup> /s)	

	: Input Cell
	: Calculation Cell
	: Reference Cell

**VI. Unit Price**

1USD = **3.00** S/. (as of November, 2007)

<b>(1) Civil Works</b>		
Excavation		
Open	: 5.53 (US\$/m <sup>3</sup> )	* (8.70+2.35) x 0.5 = \$5.53/m <sup>3</sup> , from CAPAECO and Fainal study on Omia <Human power and Machine excavation>
Tunnel	: - (US\$/m <sup>3</sup> )	
Concrete		
Open	: 93.05 (US\$/m <sup>3</sup> )	* from CAPAECO (average of foundation, wall and structure concrete)
Tunnel	: - (US\$/m <sup>3</sup> )	
Reinforcement Bar	: 1,070.00 (US\$/ton)	*\$1.07/kg, from CAPAECO
<b>(2) Hydraulic Equipment</b>		
Gate & Screen	: 8,811.04 (US\$/ton)	* from final study on Omia
Steel Penstock	: 3,100.00 (US\$/ton)	including installation
PVC (φ600)	59.67 (US\$/m)	RIB LOC for Headrace
PVC (φ315)	: 43.42 (US\$/m)	TUBOPLAST for Penstock (C-10), The number of joints is 215. This price include joint price. 190m/6m =30 (joint), 30 x \$2.7 =81\$, 81\$/190m =0.43\$/m, 42.99\$/m (PVC) + 0.43\$/m (joint) = 43.42\$/m
<b>(3) Others</b>		
Access Road	: - (US\$/m)	
<b>(4) Transportation Cost</b>		
Cajamarca to the site	: 10.40 (US\$/ton)	

(1) Yerba Buena

**TRANSPORTATION COST TO YERBABUENA**

ONLY STAGE: (by road)

LIMA - TRUJILLO - CAJAMARCA - YERBABUENA - alternative 1	51.31	US\$/TON
CAJAMARCA - YERBABUENA - alternative 2	10.41	US\$/TON

<b>TOTAL</b>		
FROM LIMA TO YERBABUENA	51.31	US\$/TON
FROM CAJAMARCA TO YERBABUENA	10.41	US\$/TON

**BY ROAD:**

**ALTERNATIVE 1:**

ROUTE	DISTANCE KM	ACCUM. DISTANCE KM	COST S/./ton	ACCUM. COST S/./ton	COST US\$/ton	ACCUM. COST US\$/ton
Lima - Trujillo	557.24	557.24	92.01	92.02	30.67	30.67
Trujillo - Cajamarca	317.87	875.11	52.49	144.51	17.50	48.17
Cajamarca - Yerbabuena	57.00	932.11	9.41	153.92	3.14	51.31

Source: Ministry of Transport and Communications MTC  
Upgraded up to June 2007

Lima - Cajamarca	57.00	57.00	214.20	214.20	71.40	71.40
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Source: Transportes Sanky - Lima. Telf. (01) 98346723

**ALTERNATIVE 2:**

ROUTE	DISTANCE KM	ACCUM. DISTANCE KM	COST S/./ton	ACCUM. COST S/./ton	COST US\$/ton	ACCUM. COST US\$/ton
Cajamarca - Yerbabuena	57.00	57.00	31.22	31.22	10.41	10.41

Source: Ministry of Transport and Communications MTC  
Upgraded up to March 2007  
\*Non confirmed

US\$ 1.00 = S/. 3.00

# Yerba Buena Map

