

HA NAM PROVINCE PEOPLE'S COMMITTEE

**PREPARATORY SURVEY
ON HA NAM PROVINCE INVESTMENT
CLIMATE IMPROVEMENT PROJECT
IN VIETNAM**

FINAL REPORT

**VOLUME II
APPENDICES**

MARCH 2019

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VOLUME II: APPENDICES

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**APPENDIX1:
SEWERAGE SECTOR**

1. Standards related to the Project (Sewerage Sector)

1.1 QCVN 28:2010/BTNMT

The maximum value (C_{max}) of the factors and pollutants in the medical wastewater when being discharged from the outlet is calculated as follows:

$$C_{max} = C \times K$$

In particular: C is the value of the factors and the pollutants as the basis for calculating C_{max} , specified in **Table 1.1**. K is the coefficient of the scale and the form of the medical facility, specified in **Table 1.2**. The factors of pH, *total coliforms*, *Salmonella*, *Shigella* and *Vibrio cholera* in the medical wastewater, use the coefficient K=1.

Table 1.1 Value of C of Pollution Factors

No.	Factor	Unit	Value of C	
			A	B
1	pH	-	6.5 – 8.5	6.5 – 8.5
2	BOD ₅ (20 ⁰ C)	mg/l	30	50
3	COD	mg/l	50	100
4	Total suspended solid (TSS)	mg/l	50	100
5	Sulfur (in H ₂ S)	mg/l	1.0	4.0
6	Ammonium (in N)	mg/l	5	10
7	Nitrate (in N)	mg/l	30	50
8	Phosphate (in P)	mg/l	6	10
9	Vegetable oil and animal fat	mg/l	10	20
10	Gross α activity	Bq/l	0.1	0.1
11	Gross β activity	Bq/l	1.0	1.0
12	<i>Gross coliforms</i>	MPN/ 100ml	3000	5000
13	<i>Salmonella</i>	Bacteria/100ml	Not found	Not found
14	<i>Shigella</i>	Bacteria/100ml	Not found	Not found
15	<i>Vibrio cholerae</i>	Bacteria/100ml	Not found	Not found

Notes:
 The factor of gross α activity and β activity are only applicable to the medical facilities that use radioactive sources. In Table 1:
 Column A provides the value of C of the factors and the pollutants as the basis for calculating the limits in medical wastewater when being discharged into the sources of water for living. Column B provides the value of C of the factors and the pollutants as the basis for calculating the limits in medical wastewater when being discharged into the sources of water not for living.
 The medical wastewater being discharged into the common sewer of residential areas shall apply the value of C in column B. The medical wastewater being discharged into the collecting system and taken to concentrated sewage treatment site must be sterilized, other factors and pollutants shall apply the provisions of the operators of the concentrated sewage treatment system.

Table 1.2 Value of K-Factor

Type	Scope	Value of K- factor
Hospital	> = 300 beds	1,0
	< 300 beds	1,2
Other clinics		1,2

1.2 QCVN 14:2008/BTNMT

1.2.1 General Provisions

1.2.1.1 Scope of adjustment

This regulation specifies the permissible maximum value of the pollution parameters in the domestic wastewater being discharged into the environment. Do not apply this Regulation for domestic wastewater discharged into the concentrated wastewater treatment system.

1.2.1.2 Subjects of application

This regulation applies to public institutions, armed forces barracks, service facilities, apartment buildings and residential areas and businesses discharging domestic wastewater into the environment.

1.2.1.3 Explanation of terms

In this Regulation, the terms below are construed as follows:

- 1) Domestic wastewater is the wastewater discharged from human activities of people such as eating, drinking, bathing, personal hygiene.
- 2) The water resource receiving wastewater is the surface water resource or coastal waters with a specified purpose of use and is the place where the wastewater is discharged into.

1.2.2 Technical Regulations

1.2.2.1 Permissible maximum value of pollution parameters in domestic wastewater

Permissible maximum value of pollution parameters in domestic wastewater as being discharged into the water resource receiving wastewater must not exceed C_{max} value calculated as follows:

$$C_{max} = C \times K$$

In which:

C_{max} is the permissible maximum concentration of pollution parameters in domestic wastewater as being discharged into the receiving water resource calculated by milligram per liter of wastewater (mg/l);

C is the concentration values of pollution parameters specified in **Section 1.2.2.2**.

K is a coefficient taking into account the size and type of services facilities, public facilities and condominium specified in **Section 1.2.2.3**.

Do not apply the formula for calculating the permissible maximum concentration in effluent for parameter pH and total coliforms.

1.2.2.2 C value of pollution parameters as a basis for calculating the permissible maximum value

C value of pollution parameters as a basis for calculating the permissible maximum value C_{max} in domestic wastewater as being discharged into water resources receiving wastewater as specified in **Table 1.3**.

Table 1.3 Value of pollution parameters as a basis for calculating the permissible maximum value in domestic wastewater

No.	Parameter	Unit	C value	
			A	B
1	pH	-	5 - 9	5 - 9
2	BOD ₅ (200C)	mg/l	30	50
3	Total suspended solids (TSS)	mg/l	50	100
4	Total dissolved solids	mg/l	500	1000
5	Sulfide (as H ₂ S)	mg/l	1.0	4.0
6	Ammonium (as N)	mg/l	5	10
7	Nitrate (NO ₃ ⁻) (as N)	mg/l	30	50
8	Animal fat and vegetable grease	mg/l	10	20
9	Total surface-active substances	mg/l	5	10
10	Phosphate (PO ₄ ³⁻) (as P)	mg/l	6	10
11	Total coliforms	MPN/ 100ml	3,000	5,000

In which:

- Column A specifies value of pollution parameters as a basis for calculating the permissible maximum value in domestic wastewater as being discharged into water resources used for the purpose of domestic water supply (with water quality equivalent to that in column A1 and A2 of the national technical Regulation on surface water quality).

- Column B specifies C value of pollution parameters as a basis for calculating the permissible maximum value in domestic wastewater as being discharged into water resources not used for the purpose of domestic water supply (with water quality equivalent to that in column B1 and B2 of the

national technical Regulation on surface water or coastal water quality).

1.2.2.3 Value of K coefficient

Depending on the type, size and area of use of service facilities, public facilities, apartment buildings and residential areas, businesses, the K value is applied under **Table 1.4**.

Table 1.4 Value of K coefficient corresponding to type of service facilities, public facilities, apartment buildings

Type of facilities	Size and area of use of facilities	Value of K coefficient
1. Hotel, rest house	From 50 rooms or hotel rated 3 stars or higher	1
	Less than 50 rooms	1.2
2. Agencies, offices, schools, research institutions	Greater than or equal to 10,000 m ²	1.0
	Less than 10,000 m ²	1.2
3. Department stores, supermarkets	Greater than or equal to 5,000 m ²	1.0
	Less than 5,000 m ²	1.2
4. Markets	Greater than or equal to 1,500 m ²	1.0
	Less than 1,500 m ²	1.2
5. Restaurants, food stores	Greater than or equal to 500 m ²	1.0
	Less than 500 m ²	1.2
6. Production facilities, armed force barracks	From 500 people or more	1.0
	Less than 500 people	1.2
7. Condominiums, residential areas	From 50 apartments or more	1.0
	Less than 50 apartments	1.2

2. Water Supply Plan in Hospital

2.1 Hospital Area

Hospital area includes three communes, namely, Liem Tiet, Liem Tuyen, Dinh Xa. At present, clean water is supplied by Rural Clean Water Center (RCWC). RCWC has two water supply plants servicing water to the communes, as shown in **Table 2.1**.

In addition, Hanwako also install water supply pipe with diameter 600 mm in the hospital area for the future demand in the area.

Table 2.1 Water Supply Plan of RCWC

	Present Capacity (m ³ /day)...(1)	Population ... (2)	Future Capacity (2030) (m ³ /day)...(3)	Population for Future Capacity... (4)	(1)/1000×(2) (L/capita/day)	(3)/1000×(4) (L/capita/day)
WTP, covering Liem Tiet, Liem Tuyen	1,200	8,116	4,500 ²⁾	12,778	148	352 ²⁾
WTP, covering Dinh Xa	1,200	13,921	8,000	43,721	86 ¹⁾	183

Note 1) Water supply per capita is not large because most of household use together with water from RCWC and groundwater.

Note 2) Water supply per capita is large because the future capacity is set including water demand Back Mai and Viet Duc Hospitals

Source: RCWC

3. Comparison Review of the Processing Method

Item	Conventional Activated Sludge Process	Oxidation Ditch Process	Sequencing Batch Process	Pre-treated Trickling Filtration Process	
Summary	Conventional Activated Sludge Process consists of Primary setting tank, Reaction tank and Final setting tank. Also, this process utilizes activated sludge microorganisms. Currently, it is adopted in many Wastewater Treatment Plant.	Oxidation Ditch Process consists of Reaction tank, Final setting tank. This process omits the Primary setting tank. The operation management is easy by adopting mechanical aeration.	Sequencing Batch Process consists of only one Reaction tank. Also, this process is an activated sludge process in which Inflow, Reaction, Precipitation and Effluent is done in the reaction tank. It is difficult to operation and maintenance of this process.	Pre-treated Trickling Filtration Process consists of Floating Sponge Filtration, High-rate Trickling Filtration, Final Solids-Liquid Separator. This process is biofilm treatment method of filtration and microorganisms attached to filter material. It is an alternative wastewater treatment technology of conventional activated sludge process.	
Process Flow					
Consideration of Design Removal Ratio	BOD: 90~95% SS: 90~95%	BOD: 90~95% SS: 90~95%	BOD: 90~95% SS: 90~95%	BOD: 90% SS: 90%	
Evaluation	○	○	○	○	
Required land Area	Small area	Large area	Small area	Small area	
Evaluation	○	△	○	○	
Design Sludge Generation Volume	Many sludge	Few sludge	Many sludge	Few sludge	
Evaluation	△	○	△	○	
Power Consumption Amount	・0.4kwh/m3	・0.8kwh/m3	・0.9kwh/m3	・0.1kwh/m3	
Evaluation	○	△	△	○	
Operation	Ordinarily	Easy	Very Difficult	Easy	
Evaluation	○	◎	△	◎	
Maintenance	Ordinarily	Easy	Difficult	Easy	
Evaluation	○	◎	△	◎	
Estimated Construction Costs Case of Q=3,000m3/d	Initial Cost (Civil engineering and Architecture)	・354 million yen	・380 million yen	・448 million yen	・395 million yen
	Initial Cost (Mechanical and Electric)	・528 million yen	・431 million yen	・526 million yen	・498 million yen
	Electricity Cost(15years)	$0.4\text{kwh/m}^3 \times 3,000\text{m}^3/\text{d} \times 365\text{days} \times 20\text{yen/m}^3 \times 15\text{years} \approx 130\text{ million yen}$	$0.8\text{kwh/m}^3 \times 3,000\text{m}^3/\text{d} \times 365\text{days} \times 20\text{yen/m}^3 \times 15\text{years} \approx 260\text{ million yen}$	$0.9\text{kwh/m}^3 \times 3,000\text{m}^3/\text{d} \times 365\text{days} \times 20\text{yen/m}^3 \times 15\text{years} \approx 300\text{ million yen}$	$0.1\text{kwh/m}^3 \times 3,000\text{m}^3/\text{d} \times 365\text{days} \times 20\text{yen/m}^3 \times 15\text{years} \approx 40\text{ million yen}$
	Life Cycle Cost	1,012 million yen(337,000yen/m3)	1,071 million yen(357,000yen/m3)	1,274 million yen(425,000yen/m3)	933 million yen(311,000yen/m3)
Evaluation	○	△	△	◎	
Comprehensive Evaluation	○	○	△	◎	

4. Flow Calculation

Flow Calculation Table - 1/5

Hospital Area **Treatment Area**
 Unit flow **0.000103** $\text{m}^3/\text{s} \cdot \text{ha}$

No	Inflow No	Treatment Area			Design Wastewater Flow				Section Characteristics							Remarks						
		Unit Area	Total Area	Flow per hectare	Domestic		Factory		Other	Total WW Flow	Diameter	Slope	Velocity	Capacity	Length		Invert EL		Ground EL		Cover	
					ha	ha	$\text{m}^3/\text{s} \cdot \text{ha}$	m^3/s									$\text{m}^3/\text{s} \cdot \text{ha}$	m^3/s	m^3/s	mm	%	m/s
25		45.25	45.25		0.005				0.005	HDPE @ 300	2.1	0.8	0.035	260.00	-0.979	1.33	2.00					
25A-1	F1 F2	3.27	(74.22) 122.74		0.013				0.013	HDPE @ 300	2.1	0.8	0.035	231.00	-1.525 -2.010	1.33 1.75	2.55 3.45					
25A-2	G7	14.81	(4.55) 142.10		0.015				0.015	HDPE @ 300	2.1	0.8	0.035	790.00	-2.010 -3.669	1.75 2.20	3.45 5.56					
26-1	F3,F4	7.42	(147.78) 297.30		0.031				0.031	HDPE @ 300	2.1	0.8	0.035	347.00	0.391 -0.338	2.20 1.24	1.50 1.27					
26-2	G8	18.55	(23.28) 339.13		0.035				0.035	HDPE @ 300	2.1	0.8	0.035	655.00	-0.763 -2.139	1.24 1.24	1.69 3.07					
2	1-2	15.72	(36.70) 391.55		0.040				0.040	RC @ 400	2.4	0.9	0.085	578.00	-2.239 -3.626	3.55 3.65	5.33 6.81					
3	15	18.23	(30.66) 440.44		0.045				0.045	RC @ 400	2.4	0.9	0.085	575.00	-3.626 -5.006	3.65 3.65	6.81 8.19					
4	18	0.46	(86.82) 527.72		0.054				0.054	RC @ 400	2.4	0.9	0.085	50.00	-5.006 -5.126	3.65 3.65	8.19 8.31					
5	20-2 F8	2.32	(22.44) 552.48		0.057				0.057	RC @ 400	2.4	0.9	0.085	255.00	-5.126 -5.738	3.65 3.63	8.31 8.91					
6	23	8.50	(62.17) 623.15		0.064				0.064	RC @ 400	2.4	0.9	0.085	742.00	-5.738 -7.519	3.63 3.50	8.91 10.56					
9	11	2.39	(242.14) 867.68		0.089				0.089	RC @ 500	1.7	0.9	0.142	210.00	-7.619 -7.976	3.50 3.65	10.56 11.06					
10	G11	40.30	(22.02) 930.00		0.096				0.096	RC @ 500	1.7	0.9	0.142	1004.00	-7.976 -9.683	3.65 3.65	11.06 12.76					
	Flow to WWTP																					

Flow Calculation Table - 2/5

Hospital Area **Treatment Area**
 Unit flow **0.000103** $m^3/s \cdot ha$

No	Inflow No	Treatment Area		Design Wastewater Flow				Section Characteristics							Remarks					
		Unit Area	Total Area	Domestic		Factory		Total WW Flow	Diameter	Slope	Velocity	Capacity	Length	Invert EL		Ground EL		Cover		
				Flow per hectare	WW Flow	Flow per hectore	WW Flow							Upper		Lower	Upper	Lower	Upper	Lower
F1		54.00	54.00		0.006			0.006	HDPE @ 300	2.1	0.8	0.035	1140.00	0.991	-1.403	3.30	3.20	2.00	4.29	
	Flow to 25A-1																			
F2		20.22	20.22		0.002			0.002	HDPE @ 300	2.1	0.8	0.035	424.00	0.891	0.001	3.20	3.20	2.00	2.89	
	Flow to 25A-1																			
G7		4.55	4.55		0.000			0.000	HDPE @ 300	2.1	0.8	0.035	150.00	-0.429	-0.744	1.88	3.20	2.00	3.64	
	Flow to 25A-2																			
F3		28.01	28.01		0.003			0.003	HDPE @ 300	2.1	0.8	0.035	705.00	0.891	-0.590	3.20	2.20	2.00	2.48	
	Flow to 26-1																			
27		13.31	13.31		0.001			0.001	HDPE @ 300	2.1	0.8	0.035	316.00	0.801	0.137	3.11	2.20	2.00	1.75	
	Flow to 26-1																			
27A	G6	33.64	65.18		0.007			0.007	HDPE @ 300	2.1	0.8	0.035	976.00	-0.323	-2.373	2.70	3.20	2.71	5.26	
	Flow to 26-1																			
G6		18.23	18.23		0.002			0.002	HDPE @ 300	2.1	0.8	0.035	340.00	0.391	-0.323	2.70	2.13	2.00	2.14	
	Flow to 27A																			
F4		54.59	54.59		0.006			0.006	HDPE @ 300	2.1	0.8	0.035	992.00	0.891	-1.192	3.20	2.20	2.00	3.08	
	Flow to 26-1																			
G8		23.28	23.28		0.002			0.002	HDPE @ 300	2.1	0.8	0.035	460.00	0.203	-0.763	2.51	3.35	2.00	3.80	
	Flow to 26-2																			
1-1		16.05	16.05		0.002			0.002	HDPE @ 300	2.1	0.8	0.035	415.00	1.141	0.270	3.45	2.03	2.00	1.45	
	Flow to 2																			
1-2	G9	9.07	36.70		0.004			0.004	HDPE @ 300	2.1	0.8	0.035	456.00	-1.035	-1.993	2.03	3.55	2.76	5.23	
	Flow to 2																			
G9		11.58	11.58		0.001			0.001	HDPE @ 300	2.1	0.8	0.035	360.00	-0.279	-1.035	2.03	2.03	2.00	2.76	
	Flow to 1-2																			

Flow Calculation Table - 3/5

Hospital Area
 Treatment Area
 0.000103 m³/s · ha

No	Inflow No	Treatment Area		Design Wastewater Flow					Section Characteristics							Remarks					
		Unit Area	Total Area	Domestic		Factory		Other	Total WW Flow	Diameter	Slope	Velocity	Capacity	Length	Invert EL		Ground EL		Cover		
				Flow per hectare	WW Flow	Flow per hectore	WW Flow								Flow per hectore		WW Flow	Upper	Lower	Upper	Lower
ha	m ³ /s · ha	m ³ /s	m ³ /s · ha	m ³ /s	m ³ /s · ha	m ³ /s	m ³ /s · ha	m ³ /s	mm	%	m/s	m ³ /s	m	m	m	m	m	m			
F5		23.56	23.56	0.002					0.002	HDPE @ 300	2.1	0.8	0.035	520.00	0.891	-0.201	3.20	3.20	2.00	3.09	
15		7.10	30.66	0.003					0.003	HDPE @ 300	2.1	0.8	0.035	398.00	-0.201	-1.037	3.20	3.65	3.09	4.38	
	Flow to 3																				
18	17-2	7.05	(79.77) 86.82	0.009					0.009	RC @ 300	3.0	0.8	0.036	420.00	-1.376	-2.636	3.50	3.65	4.52	5.93	
	Flow to 4																				
17-1		29.48	29.48	0.003					0.003	HDPE @ 300	2.1	0.8	0.035	415.00	1.041	0.170	3.35	3.50	2.00	3.02	
17-2	G5	4.30	(12.91) 46.69	0.005					0.005	HDPE @ 300	2.1	0.8	0.035	213.00	-0.402	-0.849	3.50	3.50	3.59	4.04	
	Flow to 18																				
G5		12.91	12.91	0.001					0.001	HDPE @ 300	2.1	0.8	0.035	330.00	0.291	-0.402	2.60	3.50	2.00	3.59	
	Flow to 17-2																				
G4		11.28	11.28	0.001					0.001	HDPE @ 300	2.1	0.8	0.035	310.00	0.291	-0.360	2.60	3.60	2.00	3.65	
19		21.80	33.08	0.003					0.003	HDPE @ 300	2.1	0.8	0.035	484.00	-0.360	-1.376	3.60	3.60	3.65	4.57	
	Flow to 18																				
20-1		19.09	19.09	0.002					0.002	HDPE @ 300	2.1	0.8	0.035	660.00	0.791	-0.595	3.10	3.65	2.00	3.94	
20-2		3.35	22.44	0.002					0.002	HDPE @ 300	2.1	0.8	0.035	330.00	-0.595	-1.288	3.65	3.65	3.94	4.63	
	Flow to 5																				

Flow Calculation Table - 4/5

Hospital Area
 Treatment Area
 0.000103 m³/s · ha

No	Inflow No	Treatment Area		Design Wastewater Flow						Section Characteristics						Remarks					
		Unit Area	Total Area	Domestic		Factory		Other	Total WW Flow	Diameter	Slope	Velocity	Capacity	Length	Invert EL		Ground EL		Cover		
				Flow per hectare	WW Flow	Flow per hecter	WW Flow								Flow per hector		WW Flow	Upper	Lower	Upper	Lower
ha	ha	m ³ /s · ha	m ³ /s	m ³ /s · ha	m ³ /s · ha	m ³ /s	m ³ /s	m ³ /s	mm	%	m/s	m ³ /s	m	m	m	m	m	m	m		
21		10.59	10.59		0.001				0.001						0.791	3.10	2.00				
			(30.76)												0.039	2.80	2.45				
23	22	8.33	49.68		0.005				0.005					-1.019	2.80	3.51					
														-2.237	3.63	5.56					
	Flow to 6																				
24		9.81	9.81		0.001				0.001					0.491	2.80	2.00					
			(15.84)											0.197	2.80	2.29					
22	G3	5.11	30.76		0.003				0.003					-0.542	2.80	3.03					
	Flow to 23													-1.019	2.80	3.51					
G3		15.84	15.84		0.002				0.002					0.491	2.80	2.00					
	Flow to 22-2													-0.542	2.80	3.03					
F8		12.49	12.49		0.001				0.001					1.191	3.50	2.00					
	Flow to 6													0.246	3.63	3.08					
12-1		3.97	3.97		0.000				0.000					1.191	3.50	2.00					
			(0.00)											0.830	3.50	2.36					
12-2	G10	11.14	15.11		0.002				0.002					-0.720	3.50	3.91					
			(48.45)											-2.186	3.30	5.18					
13-1	F6	2.57	66.13		0.007				0.007					-2.186	3.30	5.13					
														-2.462	3.30	5.41					
13-2		12.43	78.56		0.008				0.008					-2.462	3.30	5.41					
			(40.80)											-3.632	3.41	6.69					
14	F7	28.47	147.83		0.015				0.015					-4.436	3.50	7.47					
			(15.61)											-4.436	3.50	7.47					
8	7-2	0.42	163.86		0.017				0.017					-4.604	3.50	7.64					
	Flow to 9																				
G10		0.00	0.00		0.000				0.000					-0.279	2.03	2.00					
	Flow to 12-2													-0.720	3.50	3.91					
F6		48.45	48.45		0.005				0.005					1.241	3.55	2.00					
	Flow to 13-1													-0.166	3.30	3.16					

Flow Calculation Table - 5/5

Hospital Area **Treatment Area**
 Unit flow **0.000103** $m^3/s \cdot ha$

No	Inflow No	Treatment Area		Design Wastewater Flow				Section Characteristics							Remarks					
		Unit Area	Total Area	Domestic		Factory		Total WW Flow	Diameter	Slope	Velocity	Capacity	Length	Invert EL		Ground EL		Cover		
				Flow per hectare	WW Flow	Flow per hectore	WW Flow							Upper		Lower	Upper	Lower	Upper	Lower
ha	ha	$m^3/s \cdot ha$	m^3/s	$m^3/s \cdot ha$	m^3/s	m^3/s	m^3/s	mm	%	m/s	m^3/s	m	m	m	m	m	m	m		
F7		40.80	40.80		0.004			0.004	HDPE @ 300	2.1	0.8	0.035	725.00	1.341	-0.182	3.65	3.41	2.00	3.28	
Flow to 14																				
7-1		9.84	9.84		0.001			0.001	HDPE @ 300	2.1	0.8	0.035	313.00	1.341	0.684	3.65	3.50	2.00	2.51	
7-2		5.77	15.61		0.002			0.002	HDPE @ 300	2.1	0.8	0.035	336.00	0.681	-0.025	3.50	3.50	2.51	3.22	
Flow to 8																				
F9		10.01	10.01		0.001			0.001	HDPE @ 300	2.1	0.8	0.035	530.00	1.141	0.028	3.45	3.50	2.00	3.16	
11	G1 G2	1.86	(66.41) 78.28		0.008			0.008	HDPE @ 300	2.1	0.8	0.035	193.00	-1.539	-1.944	3.50	3.50	4.73	5.14	
Flow to 9																				
G1		49.68	49.68		0.005			0.005	HDPE @ 300	2.1	0.8	0.035	800.00	0.141	-1.539	2.45	3.50	2.00	4.73	
Flow to 11																				
G2		16.73	16.73		0.002			0.002	HDPE @ 300	2.1	0.8	0.035	660.00	0.741	-0.645	3.05	3.50	2.00	3.84	
Flow to 11																				
G11		22.02	22.02		0.002			0.002	HDPE @ 300	2.1	0.8	0.035	480.00	-0.309	-1.317	2.00	3.65	2.00	4.66	
Flow to 11																				
F10		0.00	0.00		0.000			0.000	HDPE @ 300	2.1	0.8	0.035	1070.00	1.191	-1.056	3.50	3.50	2.00	4.25	
Flow to 11																				

5. Capacity Calculation (Wastewater Treatment Plant)

▪ Capacity Calculation of Raw Water Pump Pit (Target Year: 2030)

Planning Division	Contents (Target Year: 2030)																
Item																	
1. Flow Conditions																	
(1) Sewage Influent Pipe Diameter	500 mmφ H.P																
(2) Sewage Influent Pipe Gradient	1.7 ‰																
(3) Ground Height	+3.650 M																
(4) Sewage Influent Pipe Bottom High	-9.683 M																
(5) Full Pipe Flow Rate	0.156 m ³ /sec (Manning = 0.013)																
(6) Full Pipe Velocity	0.793 m/sec (Manning = 0.013)																
2. Design Flow Rate																	
(m ³ /d)																	
(m ³ /min)																	
(m ³ /sec)																	
	<table border="1"> <thead> <tr> <th>Average Daily</th> <th>Maximum Daily</th> <th>Maximum Hourly</th> <th>Maximum Hourly+Return Water</th> </tr> </thead> <tbody> <tr> <td>2,300</td> <td>3,000</td> <td>3,900</td> <td>4,837</td> </tr> <tr> <td>1.60</td> <td>2.08</td> <td>2.71</td> <td>3.36</td> </tr> <tr> <td>0.027</td> <td>0.035</td> <td>0.045</td> <td>0.056</td> </tr> </tbody> </table>	Average Daily	Maximum Daily	Maximum Hourly	Maximum Hourly+Return Water	2,300	3,000	3,900	4,837	1.60	2.08	2.71	3.36	0.027	0.035	0.045	0.056
Average Daily	Maximum Daily	Maximum Hourly	Maximum Hourly+Return Water														
2,300	3,000	3,900	4,837														
1.60	2.08	2.71	3.36														
0.027	0.035	0.045	0.056														
3. Flow Sheet	<pre> graph TD SI[Sewage Influent] --> IG[Inlet Gate] IG --> SU[Screen Unit] SU --> RWPP[Raw Water Pump Pit] RWPP --> SP[Sewage Pump] SP --> DP[Delivery Pipe] DP --> GC[Grit Chamber] GC --> WTP[Water Treatment Plant] RW[Return Water] --> RWPP </pre>																

Planning Division	Contents (Target Year: 2030)		
Item			
4. Sewage Influent Pipe			
	Average Daily	Maximum Daily	Maximum Hourly
Velocity(m/sec)	0.594	0.640	0.686
Water Depth (m)	0.141	0.161	0.184
Flow Ratio	0.173	0.224	0.288
Velocity Ratio	0.749	0.807	0.865
Water Depth Ratio	0.282	0.322	0.368
Sewage Influent Pipe Water Level(M)	-9.542	-9.522	-9.499
Outflow Head Loss(m)	+0.018	+0.021	+0.024
Gate Chamber Inlet Water Level(M)	-9.560	-9.543	-9.523
5. Inlet Gate			
(1)Gate Chamber Inlet Water Level			
Average Daily	-9.560 M		
Maximum Daily	-9.543 M		
Maximum Hourly	-9.523 M		
(2)Gate Chamber Bottom High	-9.700 M		
(3)Gate Pass Water Depth	Gate Chamber Inflow Water Level – Gate Chamber Bottom High		
Average Daily	-9.560 – (-9.700) = 0.140 m		
Maximum Daily	-9.543 – (-9.700) = 0.157 m		
Maximum Hourly	-9.523 – (-9.700) = 0.177 m		
(4)Gate Specification			
Type	Motor drive type		
Gate Size	W 0.40 m × H 0.40 m × 1 (Use Only One Gate)		
Motor Power	0.75 kw		
(5)Gate Pass Velocity			
Average Daily	0.027/(0.140×0.4×1) = 0.482 m/sec		
Maximum Daily	0.035/(0.157×0.4×1) = 0.557 m/sec		
Maximum Hourly	0.045/(0.177×0.4×1) = 0.636 m/sec		
(6)Gate Head Loss			
Average Daily	1.5×0.482 ² / (2×9.8) = 0.018 m		
Maximum Daily	1.5×0.557 ² / (2×9.8) = 0.024 m		
Maximum Hourly	1.5×0.636 ² / (2×9.8) = 0.031 m		

Planning Division	Contents (Target Year: 2030)
6. Screen Unit	
(1)Screen Inflow Water Level	Gate Chamber Inflow Water Level — Gate Head Loss
Average Daily	$-9.560 - 0.018 = -9.578 \text{ m}$
Maximum Daily	$-9.543 - 0.024 = -9.567 \text{ m}$
Maximum Hourly	$-9.523 - 0.031 = -9.554 \text{ m}$
(2)Screen Bottom High	-9.800 m
(3)Screen Water Depth	Screen Inflow Water Level — Screen Bottom High
Average Daily	$-9.578 - (-9.800) = 0.222 \text{ m}$
Maximum Daily	$-9.567 - (-9.800) = 0.233 \text{ m}$
Maximum Hourly	$-9.554 - (-9.800) = 0.246 \text{ m}$
(4)Screen Specification	
Type	Motor drive
Effective width	25 mm
Bar Thickness	9 mm
Installation Angle	70°
Waterway Width	Width 0.9m × 1 Waterway (Use Only One Waterway)
(5)Approach Velocity	
Average Daily	$0.027 / (0.222 \times 0.9 \times 1) \times (25+9) / 25 = 0.184 \text{ m/sec}$
Maximum Daily	$0.035 / (0.233 \times 0.9 \times 1) \times (25+9) / 25 = 0.227 \text{ m/sec}$
Maximum Hourly	$0.045 / (0.246 \times 0.9 \times 1) \times (25+9) / 25 = 0.276 \text{ m/sec}$
(6)Pass Velocity	Clogging Rate = 50%
Average Daily	$0.184 / 0.50 = 0.370 \text{ m/sec}$
Maximum Daily	$0.227 / 0.50 = 0.450 \text{ m/sec}$
Maximum Hourly	$0.276 / 0.50 = 0.550 \text{ m/sec}$
(7)Head Loss	$2.34 \times \sin\theta \times (t/b)^{(4/3)} \times V^2 / (2 \times g)$
Average Daily	$2.34 \times \sin 70^\circ \times (9 / 25)^{(4/3)} \times 0.370^2 / (2 \times 9.8) = 0.004 \text{ m}$
Maximum Daily	$2.34 \times \sin 70^\circ \times (9 / 25)^{(4/3)} \times 0.450^2 / (2 \times 9.8) = 0.006 \text{ m}$
Maximum Hourly	$2.34 \times \sin 70^\circ \times (9 / 25)^{(4/3)} \times 0.550^2 / (2 \times 9.8) = 0.009 \text{ m}$

Planning Division	Contents (Target Year: 2030)																						
Item																							
7. Sewage Pump																							
(1) Pump Well Water Level	Screen Inflow Water Level — Screen Head Loss																						
Average Daily	-9.578 — 0.004 = -9.582 m																						
Maximum Daily	-9.567 — 0.006 = -9.573 m																						
Maximum Hourly	-9.554 — 0.009 = -9.563 m																						
(2) Pump Capacity	<table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr> <th>Pump Number</th> <th>Pump Capacity (m3/min)</th> <th colspan="2">Number (unit)</th> </tr> </thead> <tbody> <tr> <td>NO.1</td> <td>4.0</td> <td>2</td> <td>Standby 1</td> </tr> <tr> <td>NO.2</td> <td>—</td> <td>—</td> <td>Standby —</td> </tr> </tbody> </table>				Pump Number	Pump Capacity (m3/min)	Number (unit)		NO.1	4.0	2	Standby 1	NO.2	—	—	Standby —							
Pump Number	Pump Capacity (m3/min)	Number (unit)																					
NO.1	4.0	2	Standby 1																				
NO.2	—	—	Standby —																				
(3) Pump Diameter	$D = 146 \times \left(\frac{Q}{V} \right)^{0.5}$ <p>Q : Pump Capacity of 1 units (m3/min) V : Velocity (m/sec)</p> <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr> <th></th> <th>Pump Capacity (m3/min)</th> <th>Velocity (m/sec)</th> <th>Pump Diameter (mm)</th> <th>Pump Caliber of Decision (mm)</th> </tr> </thead> <tbody> <tr> <td rowspan="2">NO.1</td> <td rowspan="2">4.0</td> <td>1.5</td> <td>238</td> <td rowspan="2">200</td> </tr> <tr> <td>3.0</td> <td>169</td> </tr> <tr> <td rowspan="2">NO.2</td> <td rowspan="2">—</td> <td>1.5</td> <td>—</td> <td rowspan="2">—</td> </tr> <tr> <td>3.0</td> <td>—</td> </tr> </tbody> </table>					Pump Capacity (m3/min)	Velocity (m/sec)	Pump Diameter (mm)	Pump Caliber of Decision (mm)	NO.1	4.0	1.5	238	200	3.0	169	NO.2	—	1.5	—	—	3.0	—
	Pump Capacity (m3/min)	Velocity (m/sec)	Pump Diameter (mm)	Pump Caliber of Decision (mm)																			
NO.1	4.0	1.5	238	200																			
		3.0	169																				
NO.2	—	1.5	—	—																			
		3.0	—																				
(4) Delivery Pipe	$V = \frac{Q / 60}{\pi/4 \times D^2}$ $hf = 10.666 \times \left(\frac{Q}{60 \times C} \right)^{1.85} \times D^{-4.87} \times L$ <p>V : Velocity (m/sec) Q : Pump Capacity (m3/min) D : Pipe Diameter (m) hf : Head Loss(m) L : Pipe Length (m) C : Flow Rate Coefficient=110</p> <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr> <th></th> <th>Pipe Diameter (mm)</th> <th>Velocity (m/sec)</th> <th>Pipe Length (m)</th> <th>Head Loss (m)</th> </tr> </thead> <tbody> <tr> <td>Pipe 1</td> <td>300</td> <td>0.94</td> <td>30</td> <td>0.13</td> </tr> </tbody> </table>					Pipe Diameter (mm)	Velocity (m/sec)	Pipe Length (m)	Head Loss (m)	Pipe 1	300	0.94	30	0.13									
	Pipe Diameter (mm)	Velocity (m/sec)	Pipe Length (m)	Head Loss (m)																			
Pipe 1	300	0.94	30	0.13																			
(5) Pump Head	<p style="text-align: center;">Actual Head = Pipe Top Level - Pump Well HWL Total Head = Actual Head + Delivery Pipe Loss + Pump Around Loss (Practical = 1.5m)</p> <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr> <th></th> <th>Pipe Top Level (M)</th> <th>The Pump Well HWL(M)</th> <th>Actual Head (m)</th> <th>Total Head (m)</th> </tr> </thead> <tbody> <tr> <td>Pipe 1</td> <td>12.00</td> <td>-9.56</td> <td>21.6</td> <td>23.2</td> </tr> </tbody> </table>					Pipe Top Level (M)	The Pump Well HWL(M)	Actual Head (m)	Total Head (m)	Pipe 1	12.00	-9.56	21.6	23.2									
	Pipe Top Level (M)	The Pump Well HWL(M)	Actual Head (m)	Total Head (m)																			
Pipe 1	12.00	-9.56	21.6	23.2																			

Planning Division	Contents (Target Year: 2030)
8. Overground Grit Chamber	
(1) Inlet Gate	
1) Plan Water Quantity	4,837 m ³ /d = 0.045 m ³ /sec
2) Gate Chamber Inlet Water Level	+12.200 M
3) Gate Chamber Bottom High	+11.200 M
4) Gate Pass Water Depth	Gate Chamber Inflow Water Level – Gate Chamber Bottom High +12.200 – (+11.200) = 1.000 m
5) Gate Specification	
Type	Motor Drive Type
Gate Size	W 0.4 m × H 0.4 m × 1 (Use Only One Gate)
Motor Power	0.75 kw
6) Gate Pass Velocity	0.045 / (1.000 × 0.4 × 1) = 0.113 m/sec
7) Gate Head Loss	1.5 × 0.113 ² / (2 × 9.8) = 0.001 m
(2) Grit Chamber	
1) Plan Water Quantity	4,837 m ³ /d = 0.045 m ³ /sec
2) Water Area Load	1,800 m ³ /m ² · d
3) Required Water Area	4,837 / 1,800 = 2.7 m ²
4) Shape Size	Width 1.5 × Length 2.0 m × 1 Pond (Use Only One Pond)
5) Water Area	1.5 × 2.0 × 1 = 3.0 m ²
6) Grit Chamber Bottom High	11.100 M
7) Water Depth	Gate Chamber Inflow Water Level – Grit Chamber Bottom High 12.200 – 11.100 = 1.000 m
8) Examination	
Actual Water Area Load	4,837 / 3.0 = 1,612 m ³ /m ² · day
Pass Flow Rate	0.045 / (1.5 × 1.0 × 1) = 0.030 m/s
Residence Time	2.0 / 0.030 = 67 sec
9) Grit Removal Pump	
Type	Sand Pump
Specification	φ 100.0 mm × V 0.5 m ³ /min × H 5.0m × 1 Unit
Motor Power	0.75 kw

▪ Capacity Calculation of Wastewater Treatment Plant (Target Year: 2030)

Item	Contents (Target Year: 2030)																									
1. Design Parameters																										
(1)Design Flow Rate																										
①Average Daily Flow Rate(DA)	2,300	m3/d=	1.60	m3/min=	0.027	m3/sec																				
②Maximum Daily Flow Rate(DM)	3,000	m3/d=	2.08	m3/min=	0.035	m3/sec																				
③Maximum Hourly Flow Rate (HM)	3,900	m3/d=	2.71	m3/min=	0.045	m3/sec																				
(2)Design Influent Quality																										
①BOD	220	mg/l	(P-BOD 88 mg , S-BOD 132 mg/L) * P-BOD:Particulate BOD , S-BOD:Soluble BOD																							
② SS	250	mg/l																								
③T-N	43	mg/l																								
④T-P	7	mg/l																								
(3)Removal Ratio is Assumed (Total System)																										
①BOD	≧	90.0	%	(Removal Ratio of 90% was Confirmed on Demonstration Experiment)																						
②SS	≧	90.0	%	(Removal Ratio of 90% was Confirmed on Demonstration Experiment)																						
③T-N	≧	55.0	%	(Removal Ratio of 55-58% was Confirmed on Demonstration Experiment)																						
④T-P	≧	80.0	%	(Removal Ratio of 80-85% was Confirmed on Demonstration Experiment)																						
(4)Design Effluent Quality																										
①BOD	=	22	mg/l	≧	30	mg/l																				
②SS	=	25	mg/l	≧	50	mg/l																				
③T-N	=	19	mg/l	≧	35	mg/l																				
④T-P	=	1	mg/l	≧	6	mg/l																				
<div style="border: 1px solid black; padding: 5px; display: inline-block;"> QCVN14:2008/BTNMT Cvalue:A </div>																										
Sewage Influent and Return Water flow into the Raw Water Pump Pit..																										
Also,The Return Water is Sludge Thickener Supernatant and Dehydrated Filtrate.																										
<table border="1"> <thead> <tr> <th>Item</th> <th>Sewage Influent</th> <th>Return Water</th> <th>Total (Influent Quality is Average)</th> </tr> </thead> <tbody> <tr> <td>Flow Rate (m3/d)</td> <td>3,000</td> <td>937</td> <td>3,937</td> </tr> <tr> <td>BOD (mg/L)</td> <td>220</td> <td>143</td> <td>202</td> </tr> <tr> <td>S-BOD (mg/L)</td> <td>132</td> <td>74</td> <td>118</td> </tr> <tr> <td>SS (mg/L)</td> <td>250</td> <td>143</td> <td>224</td> </tr> </tbody> </table>							Item	Sewage Influent	Return Water	Total (Influent Quality is Average)	Flow Rate (m3/d)	3,000	937	3,937	BOD (mg/L)	220	143	202	S-BOD (mg/L)	132	74	118	SS (mg/L)	250	143	224
Item	Sewage Influent	Return Water	Total (Influent Quality is Average)																							
Flow Rate (m3/d)	3,000	937	3,937																							
BOD (mg/L)	220	143	202																							
S-BOD (mg/L)	132	74	118																							
SS (mg/L)	250	143	224																							

Item	Contents (Target Year: 2030)								
2. Floating Sponge Filter(FSF)									
(1) Sewage Influent									
	<table border="1" data-bbox="582 264 885 347"> <tr> <td>Flow Rate(m³/d)</td> <td>3,937</td> </tr> <tr> <td>BOD(mg/L)</td> <td>202</td> </tr> <tr> <td>S-BOD(mg/L)</td> <td>118</td> </tr> <tr> <td>SS(mg/L)</td> <td>224</td> </tr> </table>	Flow Rate(m ³ /d)	3,937	BOD(mg/L)	202	S-BOD(mg/L)	118	SS(mg/L)	224
Flow Rate(m ³ /d)	3,937								
BOD(mg/L)	202								
S-BOD(mg/L)	118								
SS(mg/L)	224								
(2) Facility Size									
① Design Filtration rate	= 250 m/d								
② Required Filtration Area	= Flow Rate 3,937 m ³ /d ÷ Design Filtration rate 250 m/d = 15.7 m ²								
③ Number of Tank	= 2 Tanks								
④ Area of Tank	= 15.7 m ² ÷ 2 Tank = 7.9 m ²								
⑤ Shape of Tank	Square								
⑥ Size of Tank									
• Width	= 2.5 m								
• Length	= 7.9 m ² ÷ 2.5 m = 3.149 → 3.5 m								
⑦ Filtration Area per Tank	= 8.8 m ² /Tanks								
⑧ Actual Filtration Rate	3,937 m ³ /d ÷ 8.8 m ² /Tank × 2 Tank = 223.7 m/d								
(3) Removal Performance									
① SS Removal Ratio	= $\frac{-0.0915 \times \text{Filtration Rate (m/d)} + 80.059}{-0.0915 \times 224 \text{ m/d} + 80.059}$ = 59.6 %								
② P-BOD Removal Ratio	= $\frac{0.9143 \times \text{SS Removal Ratio}(\%)}{0.9143 \times 59.6}$ = 54.5 %								
③ S-BOD Removal Ratio	= 0 % (Filtration Equipment can not remove S- BOD.)								
(4) Sewage Effluent									
① SS Concentration	= $\frac{224 \text{ mg/l} \times (100 - 59.6)}{90.7 \text{ mg/l} \times 100}$								
② P-BOD Removal Ratio	= $\frac{(202 - 118) \text{ mg/l} \times (100 - 54.5)}{38.0 \text{ mg/L} \times 100}$								
③ S-BOD Removal Ratio	= $\frac{118 \times (100 - 0.0)}{118.1 \text{ mg/l} \times 100}$								
④ BOD Concentration	= P-BOD + S-BOD = 38.0 + 118.1 = 156.1 mg/l								
(5) Washing Drainage									
① Average Filtration Loss Head	= Set to 40 cm								
② SS Inflow Surface Area Loading	= $(40 \div 0.5124)^2 \times (1 \div 1.1747)$ = 40.8 kg/m ² ·d (SS Inflow Surface Area Loading when Washing Frequency is 24 times / day)								
③ SS Inflow Surface Area Loading per Washing	= 40.8 ÷ 24 = 1.7 kg / m ² ·times								
④ Washing Frequency	= $\frac{223.7 \text{ m/d} \times 224 \text{ mg/L}}{29.5 \text{ times/d} \times 1000} = 1.7$								
⑤ Per time Washing Drainage Rate	= Filtration Area (m ²) × Washing height (m/time) = 17.6 × 1.5 m ³ /times = 26.4 m ³ /times								
⑥ Washing Drainage Rate	= 26.4 m ³ /times × 29.5 times/d = 779 m ³ /d								
(6) Solid Balance									
① Filtered Effluent SS	= $(3,937 - 779) \text{ m}^3/\text{d} \times 90.7 \text{ mg/L} \div 1000$ = 286 kg/d								
② Washing Drainage SS	= $\frac{3,937 \text{ m}^3/\text{d} \times 224 \text{ mg/l}}{597 \text{ (kg/d)} (\Rightarrow \text{To the Drain Tank})} = 286 \text{ kg/d}$								

Item	Contents (Target Year: 2030)
3. High-rate Trickling Filter(HTF)	
(1)Sewage Influent	
①Flow Rate	= 3,158 m ³ /d
②Sewage Influent BOD Rate	= 3,158 m ³ /d × 156.1 mg/l / 1,000 = 493 kgBOD/d
③Sewage Influent SS Rate	= 3,158 m ³ /d × 90.7 mg/l / 1,000 = 286 kgBOD/d
(2)Facility Size	
①BOD Volumetric Loading	The BOD obtained by subtracting the Flow Rate × 15 mg-BOD/ L from the Sewage Influent BOD is set to 1.6 kg / m ³ ·d. (Japan specification 26B can achieve 15 mg /L or less as treated water BOD at 1.6 kg / m ³ ·d. Overseas specifications are calculated assuming that parts exceeding 1.6 kg / m ³ ·d will shift to treated water. = 1.6 kg/m ³ ·d
②Filter Bed Volumetric	= 493 kgBOD/d ÷ 1.6 kg/m ³ ·d = 308.125 m ³ = 278 (m ³)
③Filter Bed Height	= 2.3 m is set.
④Filter Bed Area	= 278 m ³ ÷ 2.3 m = 121.1 m ²
⑤Area of 1tank per	= 81 m ² /Tanks is set.
⑥Number of Tank	= 121.1 m ² ÷ 81 m ² /Tank = 1.5 tanks ⇒ 2 Tanks
⑦Actual BOD Volumetric Loading	= 492.9 ÷ (81 × 2.3 × 2) = 1.32 kg/m ³ ·d
⑧Shape of Tank	Square
⑨Size of Tank	
•Width	= 9.0 m
•Length	= 9.0 m
⑩Area of 1tank per	= 81 m ² /Tanks
⑪Filter Bed Height	= 2.3 m
⑫Bottom Height of Filter Bed	= 0.7 m
(3)Washing Drainage	
①Washing Frequency	Weekly make 1 time washing
②Water Level Height at Washing	From the filter media surface 0.4 m
③Washing Drainage Rate	= (81 m ² /Tank × 2 Tank × (0.7 + 0.4) m + 81 m ² /Tank × 2 Tank × 2.3 m × Carrier Porosity 0.9) × 1 time/week ÷ 7 day/week = 73.4 (m ³ /d)
(4)Sewage Effluent	
①SS Concentration	= 6.2335 × Ln(BOD Volumetric Loading) + 22.233 = 6.2335 × Ln 1.323 kg/m ³ ·d + 22.233 = 24.0 mg/l
②SS Rate	= (3158 - 73.4) m ³ /d × 24.0 mg/L ÷ 1000 = 74 kg/d
③P-BOD (Particulate BOD)	= SS Concentration mg/L × P-BOD vs SS Ratio = 24.0 mg/l × 1.4008 = 33.6 mg/l
④S-BOD (Solute BOD) (Filter Bed Height 2.3 m Conversion)	= (0.7538 × Ln(BOD Volumetric Loading) + 2.6562) × 9.87715 × 2.3 ^ -0.92 ÷ 4.25 + 15 = (0.7538 × Ln 1.323 kg/m ³ ·d + 2.6562) × 9.87715 × 2.3 ^ -0.92 ÷ 4.25 + 15 = 18.1 mg/l
⑤BOD(mg/L)	= P-BOD mg/L + S-BOD mg/L = 33.6 mg/l + 18.1 mg/l = 51.7 mg/l
(5)Solid Balance	
①Washing Drainage SS	= 3,158 m ³ /d × 90.7 mg/l ÷ 1000 × 0.12 = 33.7 (kg/d) (⇒To the Drain Tank)

Item	Contents (Target Year: 2030)
4. Final Solids-Liquid Separator (SLS)	
(1) Sewage Influent	
①Flow Rate	= 3,084 m ³ /d
(2)Facility Size	
①Design Filtration rate	= 150 m/d
②Required Filtration Area	= Flow Rate 3,084 m ³ /d ÷ Design Filtration rate 150 m/d = 20.6 m ²
③Number of Tank	= 2 Tanks
④Area of Tank	= 20.6 m ² ÷ 2 Tanks = 10.3 m ²
⑤Shape of Tank	Square
Size of Tank	
•Width	= 3.0 m
•Length	= 10.3 m ² ÷ 3.0 m = 3.427 → 3.5 m
⑥Filtration Area per Tank	= 10.5 m ² /Tanks
⑦Actual Filtration Rate	= 3,084 m ³ /d ÷ 10.5 m ² /Tanks × 2 Tanks = 146.9 m/d
(3)Removal Performance	
①SS Removal Ratio	= 0.2549 × Sewage Influent SS Rate mg/l + 78.088 = 0.2549 × 24 mg/l + 78.088 = 84.2 %
②S-BOD Removal Ratio	= 0 % (Filtration Equipment can not remove S- BOD.)
(4)Sewage Effluent	
①SS Concentration	= 24 mg/l × (100 - 84.2) ÷ 100 = 3.79 mg/l
②P-BOD Removal Ratio	= 3.79 mg/l × 1.4008 = 5.31 mg/l
③S-BOD Removal Ratio	= 18.1 × (100 - 0.0) ÷ 100 = 18.1 mg/l
④BOD Concentration	= P-BOD + S-BOD = 5.3 + 18.1 = 23.4 mg/l
(5)Washing Drainage	
①SS Inflow Surface Area Loading per Washing	= 3,084 m/d × 24 mg/l ÷ 21.0 m ² ÷ 1000 = 3.5 kgSS / m ² ·times
②Washing Interval	= 20 hr/d
③Washing Drainage Time	= 0.5 hr/times
④Washing Drainage Rate	= 3,084 × 24 ÷ 20 × 0.5 ÷ 24 = 77 m ³ /d
(6)Solid Balance	
①Effluent SS	= Effluent SS mg/l × (Flow Rate m ³ /d - Washing Drainage Rate m ³ /d) ÷ 1000 = 3.79 mg/l × (3,084 m ³ /d - 77 m ³ /d) ÷ 1000 = 11 kg/d
②Total generated sludge SS	= Washing Drainage SS kg/d + Settling Sludge SS kg/d = 74 kg/d - 11 kg/d = 63 kg/d
③Washing Drainage SS	= Final filtration total generated sludge kg/d × Final filtration total generated sludge / Final filtration tank sludge ratio (-) = 63 kg/d × 0.6 = 38 kg/d (⇒To the Drain Tank)
④Settling Sludge SS	= Total generated sludge kg/d - Washing Drainage SS kg/d = 63 kg/d - 38 kg/d = 25 kg/d (⇒To the Drain Tank)
⑤Settling Sludge SS Concentration	= 4,090 mg/l (From the result of demonstration experiment)
⑥Settling Sludge Volume	= Settling Sludge SS kg/d ÷ Settling Sludge SS Concentration mg/l × 1000 = 25 kg/d ÷ 4,090 mg/l × 1000 = 6 (m ³ /d)

Item	Contents (Target Year: 2030)																																																									
<p>(7) SLS Settling Sludge Transfer Pump</p> <p>① Pump Capacity</p> <p>② Liquid Specific Gravity (γ)</p> <p>③ Head Loss(H)</p> <p>④ Pump Shaft Power</p> <p>⑤ Motor Output</p> <p>⑥ Specifications</p>	$= \frac{6 \text{ m}^3/\text{d}}{0.10} \div 2 \text{ Times/d} \div 15 \text{ min/Time} \div 2 \text{ Tanks}$ $= \frac{1.0}{10} \text{ to set}$ $P_s = \frac{0.163 \cdot \gamma \cdot Q \cdot H}{0.7} = 0.24 \text{ kw}$ $P = P_s \times (1 + \alpha) \quad (\alpha: \text{Margin})$ $= 0.24 \times (1 + 0.15)$ $= 0.27 \text{ kw} \rightarrow 0.3 \text{ kw (Catalogue Value)}$ <p>Type Centrifugal Pump</p> <p>Discharge Diameter 100 A</p> <p>Pump Capacity 0.10 m³/min</p> <p>Pump Head 10 m</p> <p>Motor Output 0.3 kw</p> <p>Number 3 Pumps (Including Standby of 1 Pumps)</p>																																																									
<p>5. Drain Tank</p> <p>(1) Drainage Volume</p> <p>(2) Capacity of the Drainage Tank</p> <p>* The capacity of the drainage tank shall be the capacity that can accept the total of one wash drainage per tank of FSF, HTF, SLS.</p> <p>① 1 Tank · 1 Washing Drainage Volume</p> <ul style="list-style-type: none"> • FSF Washing Drainage Rate • HTF Washing Drainage Rate • SLS Washing Drainage Rate • Capacity of the Drainage Tank <p>② Number of Tank</p> <p>(3) Sludge Transfer Pump (Drain Tank to Sludge Thickening)</p> <p>The Capacity of the Sludge Transfer Pump is set based on the Generation Interval of Each Washing Drainage .</p>	<table border="1" data-bbox="582 638 1284 817"> <thead> <tr> <th></th> <th>Drainage Volume m³/d</th> <th>SS Concentration mg/L</th> <th>Solids kg-DS/d</th> </tr> </thead> <tbody> <tr> <td>FSF Washing Drainage Rate</td> <td>779</td> <td>767</td> <td>597</td> </tr> <tr> <td>HTF Washing Drainage Rate</td> <td>73</td> <td>459</td> <td>34</td> </tr> <tr> <td>SLS Washing Drainage Rate</td> <td>77</td> <td>487</td> <td>38</td> </tr> <tr> <td>SLS Settling Sludge Volume</td> <td>6</td> <td>4,090</td> <td>25</td> </tr> <tr> <td>Total</td> <td>936</td> <td>741</td> <td>693</td> </tr> </tbody> </table> $= 13 \text{ m}^3$ $= 256.77 \text{ m}^3$ $= 32 \text{ m}^3$ $= 13 + 256.77 + 32 = 302 \text{ m}^3 \Rightarrow 350 \text{ m}^3$ $= 1 \text{ Tanks}$ <table border="1" data-bbox="555 1153 1337 1288"> <thead> <tr> <th rowspan="2"></th> <th>A</th> <th>B</th> <th>C</th> <th>D</th> <th>E</th> <th rowspan="2">A/E</th> </tr> <tr> <th>1 Tank · 1 Time per (m³/time · tank)</th> <th>Washing Frequency (time/day · tank)</th> <th>Number of Tank (tank)</th> <th>Number of Washing Cycles (time/day)</th> <th>Washing Interval (minute)</th> </tr> </thead> <tbody> <tr> <td>FSF</td> <td>13</td> <td>29.5</td> <td>2</td> <td>59</td> <td>24.4</td> <td>0.54</td> </tr> <tr> <td>HTF</td> <td>256.77</td> <td>0.14</td> <td>2</td> <td>0.3</td> <td>5,460</td> <td>0.05</td> </tr> <tr> <td>SLS</td> <td>32</td> <td>1.20</td> <td>2</td> <td>2.4</td> <td>650</td> <td>0.05</td> </tr> </tbody> </table>		Drainage Volume m ³ /d	SS Concentration mg/L	Solids kg-DS/d	FSF Washing Drainage Rate	779	767	597	HTF Washing Drainage Rate	73	459	34	SLS Washing Drainage Rate	77	487	38	SLS Settling Sludge Volume	6	4,090	25	Total	936	741	693		A	B	C	D	E	A/E	1 Tank · 1 Time per (m ³ /time · tank)	Washing Frequency (time/day · tank)	Number of Tank (tank)	Number of Washing Cycles (time/day)	Washing Interval (minute)	FSF	13	29.5	2	59	24.4	0.54	HTF	256.77	0.14	2	0.3	5,460	0.05	SLS	32	1.20	2	2.4	650	0.05
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<p>① Pump Capacity</p> <p>② Liquid Specific Gravity (γ)</p> <p>③ Head Loss(H)</p> <p>④ Pump Shaft Power</p> <p>⑤ Motor output</p> <p>⑥ Specifications</p> <p>(4) HTF Washing Drainage Transfer Pump</p> <p>① Pump Capacity</p> <p>② Liquid Specific Gravity (γ)</p> <p>③ Head Loss(H)</p> <p>④ Pump Shaft Power</p> <p>⑤ Motor output</p> <p>⑥ Specifications</p>	$= (0.54 + 0.05 + 0.05) \div 1 = 0.64 \text{ m}^3/\text{min}$ $= \frac{1.0}{10} \text{ m}$ $P_s = \frac{0.163 \cdot \gamma \cdot Q \cdot H}{0.7} = 1.48 \text{ kw}$ $P = P_s \times (1 + \alpha) \quad (\alpha: \text{Margin})$ $= 1.48 \times (1 + 0.15)$ $= 1.71 \text{ kw} \rightarrow 2.0 \text{ kw (Catalogue Value)}$ <p>Type Submersible Pump</p> <p>Discharge Diameter 150 A</p> <p>Pump Capacity 0.7 m³/min</p> <p>Pump Head 10 m</p> <p>Motor Output 2.0 kw</p> <p>Number 2 Pumps (Including Standby of 1 Pumps)</p>																																																									
	$= 0.05 \text{ m}^3/\text{min} \div 2 \text{ Pumps} = 0.024 \text{ m}^3/\text{min}$ $= \frac{1.0}{10} \text{ m}$ $P_s = \frac{0.163 \cdot \gamma \cdot Q \cdot H}{0.7} = 0.05 \text{ kw}$ $P = P_s \times (1 + \alpha) \quad (\alpha: \text{Margin})$ $= 0.05 \times (1 + 0.15)$ $= 0.06 \text{ kw} \rightarrow 0.1 \text{ kw (Catalogue Value)}$ <p>Type Submersible pump</p> <p>Discharge Diameter 100 A</p> <p>Pump Capacity 0.05 m³/min</p> <p>Pump Head 10 m</p> <p>Motor Output 0.1 kw</p> <p>Number 2 Pumps</p>																																																									

Item	Contents (Target Year: 2030)
(5) SLS Washing Drainage Tank	
SLS 1 Tank Capacity shall be accepted for 20 minutes of Washing Drainage .	
①Washing Drainage Volume for 20 minutes	= 10 m ³ /d ÷ 24 ÷ 60 ÷ 0 × 20 = 1 m ³
②Washing Drainage Tank Volume	= 25 m ³
③Number of Tank	= 1 Tanks
(6) SLS Washing Drainage Transfer Pump	
①Pump Capacity	= 0.05 m ³ /min ÷ 1 Pumps = 0.05 m ³ /min
②Liquid Specific Gravity (γ)	= 1.0
③Head Loss(H)	= 10 m
④Pump Shaft Power	$P_s = \frac{0.163 \cdot \gamma \cdot Q \cdot H}{0.7} = 0.12 \text{ kw}$
⑤Motor output	$P = P_s \times (1 + \alpha) \quad (\alpha: \text{Margin})$ = 0.12 × (1 + 0.15) = 0.13 kw → 0.2 kw (Catalogue Value)
⑥ Specifications	Type Submersible pump
	Discharge Diameter 100 A
	Pump Capacity 0.10 m ³ /min
	Pump Head 10 m
	Motor Output 0.2 kw
	Number 2 Pumps (Including Standby of 1 Pumps)
6. Sludge Thickening	
(1) Sludge Thickener	
①Maximum Daily Flowrate	= 936 m ³ /d
②Number of Tank	= 1 Tanks
③Design Water Area Load	= Below 30 m ³ /d
④Require Water Area	= 936 m ³ /d ÷ 30 m ³ /d ÷ 1 Tanks = 31.2 m ² /Tanks
⑤Water Depth	= 4 m
⑥Diameter of Tank	= 6.5 m
⑦Area of Tank	= 33.2 m ² /Tanks
⑧Surface Loading	= 936 m ³ /d ÷ 33.2 m ² = 28.2 m ³ /d
⑨Solid Material Load	= 693 kg/d ÷ 33.2 m ² = 20.9 kg/m ² ·d
⑩Retention time	= 33.2 m ² /Tanks × 1 Tanks × 4 m ÷ 936 m ³ /d × 24 = 3.40 hr
⑪Performance	
•Density of Concentrated Sludge	= 1.0 %
•Solid Capture Rate	= 85.0 %
⑫Thickened Sludge	
•Solids SS	= Total Solids (kgSS/d) × Solid Capture Rate (%) = 693 kg/d × 85 (%) × 0.01 = 589 kg/d
•Thickened Sludge Volume	= Solids kg/d / Density of Concentrated Sludge % = 589 kg/d / 1.0 % × 100 ÷ 1000 = 59 m ³ /d
•SS Concentration	= Solids SS kg/d / Thickened Sludge Volume m ³ /d × 1000 = 589 kg/d / 59 m ³ /d × 1000 = 10,000 mg/l
•Thickener Effluent	= Drainage Volume m ³ /d - Thickened Sludge Volume m ³ /d = 936 m ³ /d - 59 m ³ /d = 877 (m ³ /d)
•Thickener Effluent Solids SS	= Total Solids (kgSS/d) × (1 - Solid Capture Ratio) = 693 kg/d × (1 - 0.85) = 104 (kg/d)
•SS Concentration	= Solids SS kg/d / Thickener Effluent m ³ /d × 1000 = 104 kg/d / 877 m ³ /d × 1000 = 119 mg/l
•BOD	= SS Concentration mg/l × Primary Thickener Effluent BOD / SS ratio = 119 mg/l × 1.0 = 119 mg/l

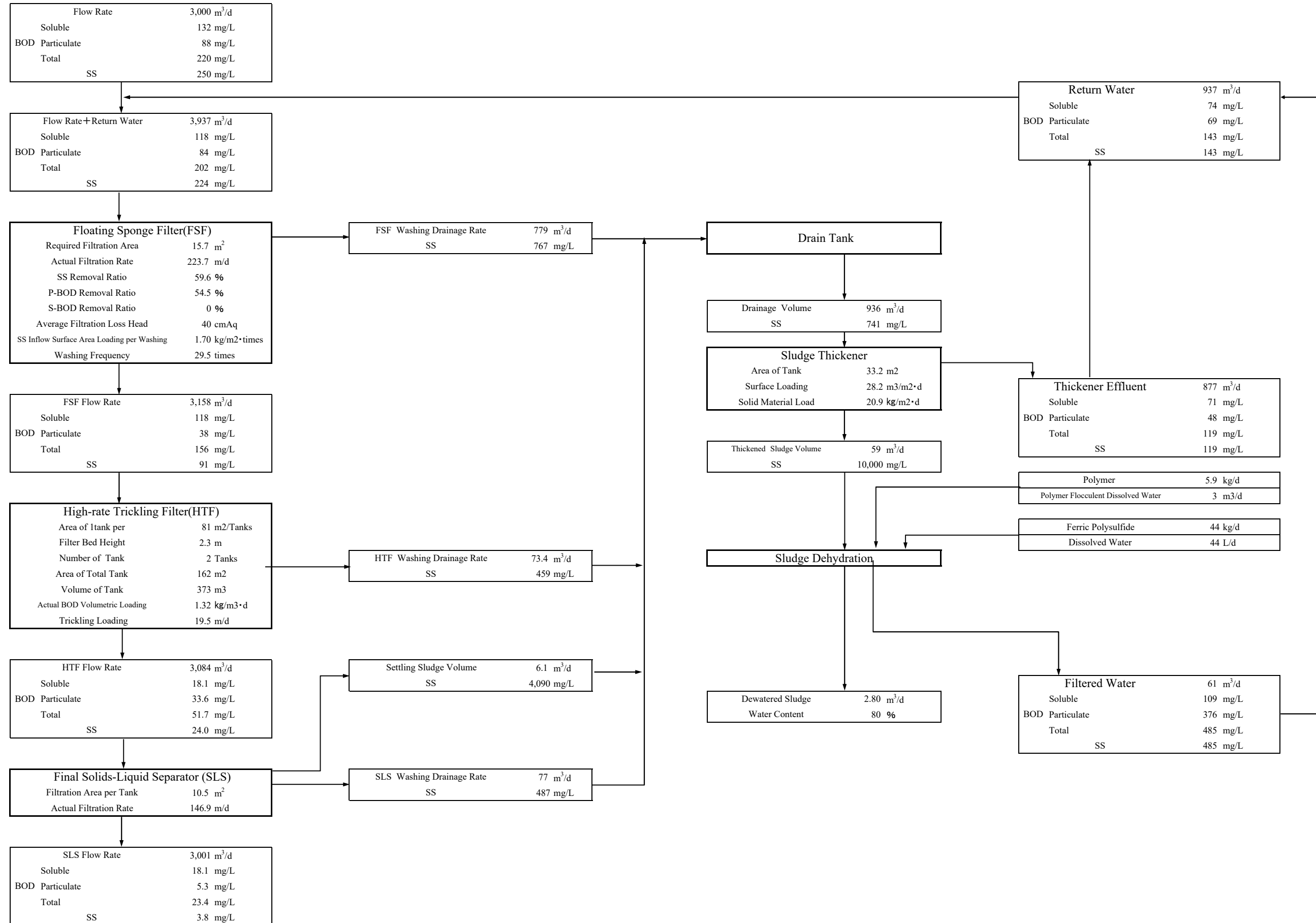
Item	Contents (Target Year: 2030)
<p>(2) Sludge Thickener Transfer Pump</p> <p>①Thickened Sludge Volume</p> <p>②Pump Capacity</p> <p>③Liquid Specific Gravity (γ)</p> <p>④Head Loss(H)</p> <p>⑤Pump Shaft Power</p> <p>⑥Motor Output</p> <p>⑦ Specifications</p>	<p>= 59 m³/d</p> <p>= 59 m³/d ÷ 360 min/d ÷ 1 pumps = 0.16 m³/min</p> <p>= 1.0</p> <p>= 10 m</p> <p>$P_s = \frac{0.163 \cdot \gamma \cdot Q \cdot H}{0.7} = 0.38$ kw</p> <p>$P = P_s \times (1 + \alpha)$ (α: Margin) = 0.38 × (1 + 0.15) = 0.44 kw → 0.5 kw (Catalogue Value)</p> <p>Type Centrifugal Pump</p> <p>Discharge Diameter 80 A</p> <p>Pump Capacity 0.20 m³/min</p> <p>Pump Head 10 m</p> <p>Motor Output 0.5 kw</p> <p>Number 2 Pumps (Including Standby of 1 Pumps)</p>
<p>7. Sludge Dehydration</p>	
<p>(1) Sludge Storage Tank</p>	
<p>The Sludge Storage Tank should be a Capacity that can store one day of Thickened Sludge.</p>	
<p>①Thickened Sludge Volume</p> <p>②Number of Tank</p> <p>③Req. Volume</p> <p>④Size of tank</p> <ul style="list-style-type: none"> •Water Depth •Width •Length <p>⑤Volume</p>	<p>= 59 m³/d</p> <p>= 1 Tanks</p> <p>= 59 m³/d ÷ 1 Tanks ÷ 1 day = 59 m³/tanks</p> <p>= 3.0 m</p> <p>= 3.5 m</p> <p>= 6.5 m</p> <p>= 3.5 m × 6.5 m × 3.0 m = 68 m³</p>
<p>(2) Dehydrator Supply Pump</p>	
<p>①Thickened Sludge Volume</p> <p>②Pump Capacity</p> <p>③Head Loss(H)</p> <p>④Specifications</p>	<p>= 59 m³/d</p> <p>= 59 m³/d ÷ 24 hr/d ÷ 2 Pumps = 1.23 m³/hr</p> <p>= 15 m</p> <p>Type Uniaxial Screw Pump</p> <p>Discharge Diameter 100 A</p> <p>Pump Capacity 1.3 m³/hr</p> <p>Pump Head 15 m</p> <p>Motor Output 3.7 kw</p> <p>Number 3 Pumps (Including Standby of 1 Pumps)</p>
<p>(3) Dehydrator</p>	
<p>①Sludge Concentration</p> <p>②Sludge Weight</p> <p>③Operation Conditions</p> <p>④Supply Solid Weight</p> <p>⑤Specifications</p>	<p>= 1.0 %</p> <p>= 59 m³/d × 1.0 % × 0.01 × 1,000 kg/m³ = 589 kg/d</p> <p>= 24 hr/d and 7 days in a week</p> <p>= 589 kg/d ÷ 24 hr/d × 7 ÷ 7 days ÷ 2 unit = 12 kg/h</p> <p>Type Volute Dewatering Press(SUS)</p> <p>Supply Sludge Concentration 1.0 %</p> <p>Capacity Max 20 kg/h (Catalogue Value)</p> <p>SS Recovery ≥ 95 %</p> <p>Sludge Cake Moisture Content ≤ 80 %</p> <p>Motor Output 3.95 kw</p> <p>Number 2 units</p>

Item	Contents (Target Year: 2030)
<p>(4) Chemical Injection System</p> <p>① Polymer Injection Pump</p> <ul style="list-style-type: none"> • Dewatering Capacity • Injection Rate • Injection Dose • Solution concentration • Req. Volume • Flexibility • Pump Capacity • Specifications <p>② Polymer Solution Tank</p> <ul style="list-style-type: none"> • Retention Time • Req. Volume • Number of Tank • Specifications <p>③ Ferric Polysulfide Injection Pump</p> <ul style="list-style-type: none"> • Dewatering Capacity • Injection Rate • Injection Dose • Solution Density • Req. Volume • Flexibility • Pump Capacity • Specifications <p>④ Ferric Polysulfide Solution Tank</p> <ul style="list-style-type: none"> • Retention Time • Req. Volume • Number of Tank • Specifications 	<p>= 12 kg-DS/h</p> <p>= 1.0 % to Set</p> <p>= 12 kg-DS/h × 0.01 = 0.12 kg/h</p> <p>= 0.2 %</p> <p>= 0.12 ÷ 0.002 ÷ 60 min = 1.0 L/min</p> <p>= 0.5 ~ 1</p> <p>= 0.5 ~ 1.0 L/min</p> <p>Type Diaphragm Metering Pump</p> <p>Discharge 40 A</p> <p>Diameter</p> <p>Pump Capacity 0.5~1.0 L/min</p> <p>Motor Output 0.1 kw</p> <p>Number 2 Pumps (Including Standby of 1 Pumps)</p> <p>Max. Discharge Pressure 0.3 Mpa</p> <p>= 2 hr</p> <p>= 1.02 L/min × 120 min ÷ 1000</p> <p>= 0.12 m3/Tanks → 0.5 m3/Tanks</p> <p>= 2 Tanks</p> <p>Type Circle Tank</p> <p>Volume 0.5 m3</p> <p>Number 2 Tanks</p> <p>Agitator 2 Unit/Tank(1.5kw)</p> <p>= 12 kg-DS/h</p> <p>= 15 %</p> <p>= 12 kg-DS/h × 0.15 = 1.8 kg-DS/h</p> <p>= 1.45</p> <p>= 1.8 ÷ 1.45 ÷ 60 min = 0.02 L/min</p> <p>= 0.5 ~ 1.5</p> <p>= 0.011 ~ 0.032 L/min</p> <p>→ 0.1 ~ 0.3 L/min</p> <p>Type Diaphragm Metering Pump</p> <p>Discharge 15 A</p> <p>Diameter</p> <p>Pump Capacity 0.1~0.3 L/min</p> <p>Motor Output 0.1 kw</p> <p>Number 2 Pumps (Including Standby of 1 unit)</p> <p>Discharge Pressure 0.5 Mpa</p> <p>= 1 days = 24 hr</p> <p>= 1.8 kg-DS/h ÷ 1.45 × 24 hr</p> <p>= 0.1 m3/Tanks</p> <p>= 1 Tanks</p> <p>Type Circle Tank</p> <p>Volume 0.1 m3</p> <p>Number 1 Tanks</p> <p>Agitator 1 Unit/Tank(0.1kw)</p>
<p>(5) Cake Hopper</p> <p>* Cake Hopper Volume is Calculated Based on Maximum Daily Flowrate .</p> <p>① Sludge Volume</p> <p>② SS Recovery Rate</p> <p>③ Sludge Amount per a Day</p> <p>④ Sludge Amount per a Day</p> <p>⑤ Water Content</p> <p>⑥ Dewatered Sludge</p> <p>⑦ No of Hopper</p> <p>⑧ Req. Volume</p> <p>⑨ Specifications</p> <p>(6) Filtered Water</p> <p>① Thickened Sludge Volume</p> <p>② Polymer Flocculent Dissolved Water</p> <p>③ Water content in Sludge Cake</p> <p>④ Filtered Water Volume</p> <p>⑤ SS in Filtered Water</p> <p>⑥ Filtered Water SS</p> <p>⑦ Filtered Water BOD</p> <p>⑧ Filtered Water S-BOD</p>	<p>= 12 kg/d × 2 Units × 24 hr/d × 7 / 7</p> <p>= 589 kg/d</p> <p>= 95 %</p> <p>= 589 kg/d × 0.95</p> <p>= 560 kg/d = 0.6 t-DS/d</p> <p>= 560 kg-DS/d</p> <p>= 80 %</p> <p>= 560 / (1 - 80 %) ÷ 1000</p> <p>= 2.8 m3/d</p> <p>= 2 Units</p> <p>= 1.4 m3/d → 2.0 m3/Units</p> <p>Type Auto Cut Gate Type</p> <p>Volume 2.0 m3</p> <p>Motor Output 1.5 kw × 2</p> <p>Number 2 Units</p> <p>= 59 m3/d</p> <p>= 3 m3/d</p> <p>= 1 m3/d</p> <p>= 61 m3/d</p> <p>= 29 kg/d</p> <p>= 485 mg/l</p> <p>= 485 mg/l</p> <p>= 109 mg/l</p>

Item	Contents (Target Year: 2030)
<p>8. Chlorination</p> <p>(1)Chlorination Tank * Chlorination Tank volume is Calculated based on Maximum Daily Flowrate .</p> <p>①Maximum Flow rate = 3,084 m3/d ②Contact Time = 15 min ③Number of Tank = 1 Tanks ④Req. Volume of Tank = 3,084 m3/d × 15 min/d ÷ 1,440 ÷ 1 Tanks = 32 m3 ⑤Shape of Tank Rectangular ⑥Size of Tank •Width = 1.5 m •Length = 30.0 m •Effective Depth = 1.5 m •Volume of Tank = 68 m3</p> <p>(2)Sodium Hypochlorite Dosing Pump * Sodium Hypochlorite Dosing Pump Volume is Calculated Based on Maximum Hourly Flowrate.</p> <p>①Disinfection Volume = 3,900 m3/d ②Dosing Rate = 3 mg/L ③Disinfectant Concentration = 10 % ④Disinfectant Density = 1.1 t/m3 ⑤Dosing Pump Capacity = 3,900 m3/d × 3 mg/L ÷ 10 % ÷ 1.1 = 0.07 L/min ⑥Specifications Type Diaphragm Metering Pump Pump Capacity 0.2 L/min Motor Output 0.2 kw Number 2 Units (Including Standby) Max.Discharge Pressure 1.0 Mpa</p> <p>(3)Sodium Hypochlorite Storage ①Storage Time = 2.5 days ② Req. Volume = 0.07 L/min × 1,440 min/d × 2.5 days × 10⁻³ = 0.27 m3/Tanks → 0.7 m3/Tanks ③Number of Tank = 1 tanks ④Specification Type Circle Tank Volume 0.7 m3 Number 1 Tanks</p>	
<p>9. Polishing Pond</p> <p>Design Inflow = 3,000 m3/d Size Width= 50.0 m (Effective width= 41.0 m) (Slope, 1:1) Length= 83.0 m (Effective length= 74.0 m) Depth= 4.5 m (Effective depth= 2.0 m)</p> <p>Number of pond 1 pond Required retention time 2.0 days Effective volume 41.0 m x 74.0 m x 2.0 m x 1 pond = 6,068 m3 Retention time 6,068 m3 ÷ 3,000 m3/day = 2.0 days</p>	
<p>10. Water Discharge</p> <p>(1)Outfall Pump * Water Discharge Pump is calculated based on Maximum Hourly Flowrate .</p> <p>①Pump Capacity = 2.77 m3/min = QMax ②Pump Distribution = QMax = 2.77 m3/min ③Pump Head ④Specification for Pressure Piping •Diameter φ 250 mm •Number 1 pipe •Highest Level (End of Pipe) + 3.400 M •Length 500 m</p> <p>(2)Head Loss at Pressure Pipe (PP) Pumping Flow Rate(Maximum) Q = QMax = 2.77 m3/min = 0.046 m3/sec</p> <p>①Cross Section A = 0.25 m² × π × 1/4 = 0.049 m2 ②Flow Rate V = 0.046 / 0.049 = 0.9 m/s ③Loss Calculation • Head Loss hf = 10.666 × (0.046 / 110)^{1.85} × 0.25^{-4.87} × 500 = 2.57 m • Outlet Loss h0 = 1.0 × 0.9² / 2g = 0.045 m • Total H = hf + h0 = 2.62 m ④Head Loss Around Pump H = 1.5 m</p> <p>⑤Actual Pump Head H = (Highest Level - Pumping Level) = 3.400 M - -2.500 M = 5.900 m ⑥Total Pump Head H = (Actual Pump Head + Pressure Pipe + Around Pump) = 5.900 + 2.62 + 1.50 = 10.019 m → 11 m</p> <p>⑦Motor Output •Pumping Flow Rate Q 2.8 m3/min •Liquid Specific Gravity γ 1.0 •Pump Efficiency η 0.7 •Pump Shaft Power Ps = $\frac{0.163 \cdot \gamma \cdot Q \cdot H}{\eta} = 7.09$ kw</p> <p>⑧Motor Output P = Ps × (1 + α) (α: Margin) = 7.09 × (1 + 0.15) = 8.15 kw → 11.0 kw (Catalogue Value)</p> <p>⑨Specifications Type Submersible Pump Diameter 250 A Motor Output 11.0 kw Total Pump Head 11 m Pump Capacity 3.0 m3/min Number 2 Pump (Including Standby of 1 Pump)</p>	

Item	Contents (Target Year: 2030)
<p>8. Chlorination</p> <p>(1)Chlorination Tank * Chlorination Tank volume is Calculated based on Maximum Hourly Flowrate(Wet) .</p> <p>①Maximum Flow rate = 17,000 m3/d ②Contact Time = 15 min ③Number of Tank = 1 Tanks ④Req. Volume of Tank = 17,000 m3/d × 15 min/d ÷ 1,440 ÷ 1 Tanks = 177 m3</p> <p>⑤Shape of Tank Rectangular ⑥Size of Tank •Width = 1.5 m •Length = 45.0 m •Effective Depth = 1.5 m •Volume of Tank = 101 m3 •Volume of Outfall Pipe = 98.1 m3 •Total Volume = 199.4 m3</p> <p>(2)Sodium Hypochlorite Dosing Pump * Sodium Hypochlorite Dosing Pump Volume is Calculated Based on Maximum Hourly Flowrate(Wet).</p> <p>①Disinfection Volume = 17,000 m3/d ②Dosing Rate = 3 mg/L ③Disinfectant Concentration = 10 % ④Disinfectant Density = 1.1 t/m3 ⑤Dosing Pump Capacity = 17,000 m3/d × 3 mg/L ÷ 10 % ÷ 1.1 = 0.32 L/min</p> <p>⑥Specifications Type Diaphragm Metering Pump Pump Capacity 0.40 L/min Motor Output 0.2 kw Number 2 Units (Including Standby) Max.Discharge Pressure 1.0 Mpa</p> <p>(3)Sodium Hypochlorite Storage ①Storage Time = 2.5 days ② Req. Volume = 0.32 L/min × 1,440 min/d × 2.5 days × 10⁻³ = 1.16 m3/Tanks → 1.5 m3/Tanks ③Number of Tank = 1 tanks ④Specification Type Circle Tank Volume 1.5 m3 Number 1 Tanks</p>	
<p>9. Water Discharge</p> <p>(1)Outfall Pump * Water Discharge Pump is calculated based on Maximum Hourly Flowrate (Wet).</p> <p>①Pump Capacity = 11.81 m3/min = QMax ②Pump Distribution = QMax = 11.81 m3/min ③Pump Head ④Specification for Pressure Piping •Diameter φ 500 mm •Number 1 pipe •Highest Level (End of Pipe) + 3.400 M •Length 500 m</p> <p>(2)Head Loss at Pressure Pipe (PP) Pumping Flow Rate(Maximum) Q= QMax= 11.81 m3/min= 0.197 m3/sec</p> <p>①Cross Section A= 0.50 m² × π × 1/4 = 0.196 m2 ②Flow Rate V= 0.197 / 0.196 = 1.0 m/s ③Loss Calculation • Head Loss hf= 10.666 × (0.197 / 110)^{1.85} × 0.50^{-4.87} × 500 = 1.29 m • Outlet Loss h0= 1.0 × 1.0² / 2g = 0.051 m •Total H=hf + h0 = 1.34 m ④Head Loss Around Pump H= 1.5 m</p> <p>⑤Actual Pump Head H= (Highest Level - Pumping Level) = 3.400 M - -2.500 M = 5.900 m ⑥Total Pump Head H=(Actual Pump Head + Pressure Pipe + Around Pump) = 5.900 + 1.34 + 1.50 = 8.740 m → 9 m</p> <p>⑦Motor Output •Pumping Flow Rate Q 5.9 m3/min •Liquid Specific Gravity γ 1.0 •Pump Efficiency η 0.7 •Pump Shaft Power Ps= $\frac{0.163 \cdot \gamma \cdot Q \cdot H}{\eta}$ = 12.37 kw</p> <p>⑧Motor Output P= Ps × (1 + α) (α: Margin) = 12.37 × (1 + 0.15) = 14.23 kw → 17.5 kw (Catalogue Value)</p> <p>⑨Specifications Type Submersible Pump Diameter 500 A Motor Output 17.5 kw Total Pump Head 9 m Pump Capacity 6.0 m3/min Number 3 Pump (Including Standby of 1 Pump)</p>	

•Solid Balance Calculation :Target Year: 2030



▪ Capacity Calculation of Raw Water Pump Pit (Target Year: After 2035)

Planning Division	Contents (Target Year: After 2035)																
Item																	
1. Flow Conditions																	
(1) Sewage Influent Pipe Diameter	500 mmφ H.P																
(2) Sewage Influent Pipe Gradient	1.7 ‰																
(3) Ground Height	+3.650 M																
(4) Sewage Influent Pipe Bottom High	-9.683 M																
(5) Full Pipe Flow Rate	0.156 m ³ /sec (Manning = 0.013)																
(6) Full Pipe Velocity	0.793 m/sec (Manning = 0.013)																
2. Design Flow Rate																	
(m ³ /d)																	
(m ³ /min)																	
(m ³ /sec)																	
	<table border="1" style="width: 100%; text-align: center;"> <thead> <tr> <th>Average Daily</th> <th>Maximum Daily</th> <th>Maximum Hourly</th> <th>Maximum Hourly+Return Water</th> </tr> </thead> <tbody> <tr> <td>4,900</td> <td>6,000</td> <td>8,300</td> <td>10,173</td> </tr> <tr> <td>3.40</td> <td>4.17</td> <td>5.76</td> <td>7.06</td> </tr> <tr> <td>0.057</td> <td>0.069</td> <td>0.096</td> <td>0.118</td> </tr> </tbody> </table>	Average Daily	Maximum Daily	Maximum Hourly	Maximum Hourly+Return Water	4,900	6,000	8,300	10,173	3.40	4.17	5.76	7.06	0.057	0.069	0.096	0.118
Average Daily	Maximum Daily	Maximum Hourly	Maximum Hourly+Return Water														
4,900	6,000	8,300	10,173														
3.40	4.17	5.76	7.06														
0.057	0.069	0.096	0.118														
3. Flow Sheet	<pre> graph TD SI[Sewage Influent] --> IG[Inlet Gate] IG --> SU[Screen Unit] SU --> RWPP[Raw Water Pump Pit] RW -- Return Water --> RWPP RWPP --> SP[Sewage Pump] SP --> DP[Delivery Pipe] DP --> GC[Grit Chamber] GC --> WTP[Water Treatment Plant] style GC stroke-dasharray: 5 5 </pre>																

Planning Division	Contents (Target Year: After 2035)		
Item			
4. Sewage Influent Pipe			
	Average Daily	Maximum Daily	Maximum Hourly
Velocity(m/sec)	0.731	0.769	0.834
Water Depth (m)	0.209	0.233	0.284
Flow Ratio	0.365	0.442	0.615
Velocity Ratio	0.922	0.970	1.052
Water Depth Ratio	0.418	0.466	0.568
Sewage Influent Pipe Water Level(M)	-9.474	-9.450	-9.399
Outflow Head Loss(m)	+0.027	+0.030	+0.036
Gate Chamber Inlet Water Level(M)	-9.501	-9.480	-9.435
5. Inlet Gate			
(1)Gate Chamber Inlet Water Level			
Average Daily	-9.501 M		
Maximum Daily	-9.480 M		
Maximum Hourly	-9.435 M		
(2)Gate Chamber Bottom High			
	-9.700 M		
(3)Gate Pass Water Depth			
	Gate Chamber Inflow Water Level – Gate Chamber Bottom High		
Average Daily	-9.501 – (-9.700) = 0.199 m		
Maximum Daily	-9.480 – (-9.700) = 0.220 m		
Maximum Hourly	-9.435 – (-9.700) = 0.265 m		
(4)Gate Specification			
Type	motor drive type		
Gate Size	W 0.40 m × H 0.40 m × 2		
motor Power	0.75	kw	
(5)Gate Pass Velocity			
Average Daily	$0.057 / (0.199 \times 0.4 \times 2) = 0.358$ m/sec		
Maximum Daily	$0.069 / (0.220 \times 0.4 \times 2) = 0.392$ m/sec		
Maximum Hourly	$0.096 / (0.265 \times 0.4 \times 2) = 0.453$ m/sec		
(6)Gate Head Loss			
Average Daily	$1.5 \times 0.358^2 / (2 \times 9.8) = 0.010$ m		
Maximum Daily	$1.5 \times 0.392^2 / (2 \times 9.8) = 0.012$ m		
Maximum Hourly	$1.5 \times 0.453^2 / (2 \times 9.8) = 0.016$ m		

Planning Division	Contents (Target Year: After 2035)
6. Screen Unit	
(1)Screen Inflow Water Level	Gate Chamber Inflow Water Level — Gate Head Loss
Average Daily	-9.501 — 0.010 = -9.511 m
Maximum Daily	-9.480 — 0.012 = -9.492 m
Maximum Hourly	-9.435 — 0.016 = -9.451 m
(2)Screen Bottom High	-9.800 m
(3)Screen Water Depth	Screen Inflow Water Level — Screen Bottom High
Average Daily	-9.511 — (-9.800) = 0.289 m
Maximum Daily	-9.492 — (-9.800) = 0.308 m
Maximum Hourly	-9.451 — (-9.800) = 0.349 m
(4)Screen Specification	
Type	Motor drive
Effective width	25 mm
Bar Thickness	9 mm
Installation Angle	70°
Waterway Width	Width 0.9m × 1 Waterway (Use Only One Waterway)
(5)Approach Velocity	
Average Daily	$0.057 / (0.289 \times 0.9 \times 1) \times (25+9) / 25$ = 0.298m/sec
Maximum Daily	$0.069 / (0.308 \times 0.9 \times 1) \times (25+9) / 25$ = 0.339m/sec
Maximum Hourly	$0.096 / (0.349 \times 0.9 \times 1) \times (25+9) / 25$ = 0.416 m/sec
(6)Pass Velocity	Clogging Rate = 50%
Average Daily	0.298 / 0.50 = 0.600 m/sec
Maximum Daily	0.339 / 0.50 = 0.680 m/sec
Maximum Hourly	0.416 / 0.50 = 0.830 m/sec
(7)Head Loss	$2.34 \times \sin\theta \times (t/b)^{4/3} \times V^2 / (2 \times g)$
Average Daily	$2.34 \times \sin 70^\circ \times (9 / 25)^{4/3}$ $\times 0.600^2 / (2 \times 9.8) = 0.010\text{m}$
Maximum Daily	$2.34 \times \sin 70^\circ \times (9 / 25)^{4/3}$ $\times 0.680^2 / (2 \times 9.8) = 0.013\text{m}$
Maximum Hourly	$2.34 \times \sin 70^\circ \times (9 / 25)^{4/3}$ $\times 0.830^2 / (2 \times 9.8) = 0.020\text{m}$

Planning Division	Contents (Target Year: After 2035)																						
Item																							
7. Sewage Pump																							
(1) Pump Well Water Level	Screen Inflow Water Level — Screen Head Loss																						
Average Daily	-9.511 — 0.010 = -9.521 m																						
Maximum Daily	-9.492 — 0.013 = -9.505 m																						
Maximum Hourly	-9.451 — 0.020 = -9.471 m																						
(2) Pump Capacity	<table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr> <th>Pump Number</th> <th>Pump Capacity (m3/min)</th> <th colspan="2">Number (unit)</th> </tr> </thead> <tbody> <tr> <td>NO.1</td> <td>4.0</td> <td>2</td> <td>Standby 1</td> </tr> <tr> <td>NO.2</td> <td>4.0</td> <td>1</td> <td>Standby —</td> </tr> </tbody> </table>				Pump Number	Pump Capacity (m3/min)	Number (unit)		NO.1	4.0	2	Standby 1	NO.2	4.0	1	Standby —							
Pump Number	Pump Capacity (m3/min)	Number (unit)																					
NO.1	4.0	2	Standby 1																				
NO.2	4.0	1	Standby —																				
(3) Pump Diameter	$D = 146 \times \left(\frac{Q}{V} \right)^{0.5}$ <p>Q : Pump Capacity of 1 units (m3/min) V : Velocity (m/sec)</p> <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr> <th></th> <th>Pump Capacity (m3/min)</th> <th>Velocity (m/sec)</th> <th>Pump Diameter (mm)</th> <th>Pump Caliber of Decision (mm)</th> </tr> </thead> <tbody> <tr> <td rowspan="2">NO.1</td> <td rowspan="2">4.0</td> <td>1.5</td> <td>238</td> <td rowspan="2">200</td> </tr> <tr> <td>3.0</td> <td>169</td> </tr> <tr> <td rowspan="2">NO.2</td> <td rowspan="2">4.0</td> <td>1.5</td> <td>238</td> <td rowspan="2">200</td> </tr> <tr> <td>3.0</td> <td>169</td> </tr> </tbody> </table>					Pump Capacity (m3/min)	Velocity (m/sec)	Pump Diameter (mm)	Pump Caliber of Decision (mm)	NO.1	4.0	1.5	238	200	3.0	169	NO.2	4.0	1.5	238	200	3.0	169
	Pump Capacity (m3/min)	Velocity (m/sec)	Pump Diameter (mm)	Pump Caliber of Decision (mm)																			
NO.1	4.0	1.5	238	200																			
		3.0	169																				
NO.2	4.0	1.5	238	200																			
		3.0	169																				
(4) Delivery Pipe	$V = \frac{Q / 60}{\pi/4 \times D^2}$ $hf = 10.666 \times \left(\frac{Q}{60 \times C} \right)^{1.85} \times D^{-4.87} \times L$ <p>V : Velocity (m/sec) Q : Pump Capacity (m3/min) D : Pipe Diameter (m) hf : Head Loss(m) L : Pipe Length (m) C : Flow Rate Coefficient=110</p> <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr> <th></th> <th>Pipe Diameter (mm)</th> <th>Velocity (m/sec)</th> <th>Pipe Length (m)</th> <th>Head Loss (m)</th> </tr> </thead> <tbody> <tr> <td>Pipe 1</td> <td>300</td> <td>1.89</td> <td>30</td> <td>0.13</td> </tr> </tbody> </table>					Pipe Diameter (mm)	Velocity (m/sec)	Pipe Length (m)	Head Loss (m)	Pipe 1	300	1.89	30	0.13									
	Pipe Diameter (mm)	Velocity (m/sec)	Pipe Length (m)	Head Loss (m)																			
Pipe 1	300	1.89	30	0.13																			
(5) Pump Head	<p style="text-align: center;">Actual Head = Pipe Top Level - Pump Well HWL Total Head = Actual Head + Delivery Pipe Loss + Pump Around Loss (Practical = 1.5m)</p> <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr> <th></th> <th>Pipe Top Level (M)</th> <th>The Pump Well HWL(M)</th> <th>Actual Head (m)</th> <th>Total Head (m)</th> </tr> </thead> <tbody> <tr> <td>Pipe 1</td> <td>12.00</td> <td>-9.47</td> <td>21.5</td> <td>23.1</td> </tr> </tbody> </table>					Pipe Top Level (M)	The Pump Well HWL(M)	Actual Head (m)	Total Head (m)	Pipe 1	12.00	-9.47	21.5	23.1									
	Pipe Top Level (M)	The Pump Well HWL(M)	Actual Head (m)	Total Head (m)																			
Pipe 1	12.00	-9.47	21.5	23.1																			

Planning Division	Contents (Target Year: After 2035)			
Item				
(6)Calculation of Pump Output	$P = \frac{0.163 \times \gamma \times Q \times H}{n} \times (1 + \alpha)$			
	P : Pump Output (kw)			
	γ : Weight per Unit Volume of the Liquid Being Pumped (kg/l) : 1.0			
	Q : Pump Capacity (m3/min)			
	H : Total Head(m)			
	n : Pump Efficiency			
	α : Margin			
		Pump Efficiency	Margin	Pump Output (kw)
	NO.1	0.7	0.15	26.8
	NO.2	0.7	0.15	26.8
Request Value			53.6	
(7)Pump Specification	Type	Submergible Pump with Screw Blade Suction Type		
	Specifications	φ200 4.0m3/min 25 m	φ200 4.0m3/min 25 m	
	Pump Capacity	4.0 m3/min	4.0 m3/min	
	Pump Output of Decision	30.0 kw	30.0 kw	
	Number(unit)	2 Unit (Standby1Unit)	1 Unit	
				60.0 kw
(8)Overview of the Water Level etc	Sewage Influent Pipe Bottom High	-9.683	-9.683	-9.683
	Gate Chamber Bottom High	-9.700	-9.700	-9.700
	Screen Bottom High	-9.800	-9.800	-9.800
	Screen Inflow Water Level	-9.511	-9.492	-9.451
	Pump Well Water Level	-9.521	-9.505	-9.471
		Average Daily	Maximum Daily	Maximum Hourly

Planning Division	Contents (Target Year: After 2035)
8. Overgrand Grit Chamber	
(1) Inlet Gate	
1) Plan Water Quantity	10,173 m ³ /d = 0.096 m ³ /sec
2) Gate Chamber Inlet Water Level	+12.200 M
3) Gate Chamber Bottom High	+11.200 M
4) Gate Pass Water Depth	Gate Chamber Inflow Water Level – Gate Chamber Bottom High +12.200 – (+11.200) = 1.000 m
5) Gate Specification	
Type	Motor Drive Type
Gate Size	W 0.4 m × H 0.4 m × 2
motor Power	0.75 kw
6) Gate Pass Velocity	0.096 / (1.000 × 0.4 × 2) = 0.120 m/sec
7) Gate Head Loss	1.5 × 0.120 ² / (2 × 9.8) = 0.001 m
(2) Grit Chamber	
1) Plan Water Quantity	10,173 m ³ /d = 0.096 m ³ /sec
2) Water Area Load	1,800 m ³ /m ² · d
3) Required Water Area	10,173 / 1,800 = 5.7 m ²
4) Shape Size	Width 1.5 × Length 2.0 m × 2 Pond
5) Water Area	1.5 × 2.0 × 2 = 6.0 m ²
6) Grit Chamber Bottom High	11.100 M
7) Water Depth	Gate Chamber Inflow Water Level – Grit Chamber Bottom High 12.200 – 11.100 = 1.000 m
8) Examination	
Actual Water Area Load	10,173 / 6.0 = 1,696 m ³ /m ² · day
Pass Flow Rate	0.096 / (1.5 × 1.0 × 2) = 0.032 m/s
Residence Time	2.0 / 0.032 = 63 sec
9) Grate Removal Pump	
Type	Sand Pump
Specification	φ 100.0 mm × V 0.5 m ³ /min × H 5.0m × 2 Unit
motor Power	0.75 kw

• Capacity Calculation of Wastewater Treatment Plant (Target Year: After 2035)

Item	Contents (Target Year: After 2035)																									
1. Design Parameters																										
(1) Design Flow Rate																										
① Average Daily Flow Rate(DA)	4,900	m ³ /d=	3.40	m ³ /min=	0.057	m ³ /sec																				
② Maximum Daily Flow Rate(DM)	6,000	m ³ /d=	4.17	m ³ /min=	0.069	m ³ /sec																				
③ Maximum Hourly Flow Rate (HM)	8,300	m ³ /d=	5.76	m ³ /min=	0.096	m ³ /sec																				
(2) Design Influent Quality																										
① BOD	220	mg/l	(P-BOD 88 mg , S-BOD 132 mg/L) * P-BOD: Particulate BOD , S-BOD: Soluble BOD																							
② SS	250	mg/l																								
③ T-N	43	mg/l																								
④ T-P	7	mg/l																								
(3) Removal Ratio is Assumed (Total System)																										
① BOD	≧ 90.0	%	(Removal Ratio of 90% was Confirmed on Demonstration Experiment)																							
② SS	≧ 90.0	%	(Removal Ratio of 90% was Confirmed on Demonstration Experiment)																							
③ T-N	≧ 55.0	%	(Removal Ratio of 55-58% was Confirmed on Demonstration Experiment)																							
④ T-P	≧ 80.0	%	(Removal Ratio of 80-85% was Confirmed on Demonstration Experiment)																							
(4) Design Effluent Quality																										
			<div style="border: 1px solid black; padding: 5px; width: fit-content; margin: auto;"> QCVN14:2008/BTNMT Cvalue:A </div>																							
① BOD	= 22	mg/l	≧	30	mg/l																					
② SS	= 25	mg/l	≧	50	mg/l																					
③ T-N	= 19	mg/l	≧	35	mg/l																					
④ T-P	= 1	mg/l	≧	6	mg/l																					
(5) Sewage Influent and Influent Quality considering Return water																										
Sewage Influent and Return Water flow into the Raw Water Pump Pit . Also, The Return Water is Sludge Thickener Supernatant and Dehydrated Filtrate.																										
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Item	Sewage Influent	Return Water	Total (Influent Quality is Average)																							
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Item	Contents (Target Year: After 2035)								
2. Floating Sponge Filter(FSF)									
(1) Sewage Influent									
	<table border="1" data-bbox="582 264 885 347"> <tr> <td>Flow Rate(m³/d)</td> <td>7,873</td> </tr> <tr> <td>BOD(mg/L)</td> <td>202</td> </tr> <tr> <td>S-BOD(mg/L)</td> <td>118</td> </tr> <tr> <td>SS(mg/L)</td> <td>225</td> </tr> </table>	Flow Rate(m ³ /d)	7,873	BOD(mg/L)	202	S-BOD(mg/L)	118	SS(mg/L)	225
Flow Rate(m ³ /d)	7,873								
BOD(mg/L)	202								
S-BOD(mg/L)	118								
SS(mg/L)	225								
(2) Facility Size									
① Design Filtration rate	= 250 m/d								
② Required Filtration Area	= Flow Rate 7,873 m ³ /d ÷ Design Filtration rate 250 m/d = 31.5 m ²								
③ Number of Tank	= 4 Tanks								
④ Area of Tank	= 31.5 m ² ÷ 4 Tank = 7.9 m ²								
⑤ Shape of Tank	Square								
⑥ Size of Tank									
• Width	= 2.5 m								
• Length	= 7.9 m ² ÷ 2.5 m = 3.149 → 3.5 m								
⑦ Filtration Area per Tank	= 8.8 m ² /Tanks								
⑧ Actual Filtration Rate	7,873 m ³ /d ÷ 8.8 m ² /Tank × 4 Tank = 223.7 m/d								
(3) Removal Performance									
① SS Removal Ratio	= -0.0915 × Filtration Rate (m/d) + 80.059 = -0.0915 × 224 m/d + 80.059 = 59.6 %								
② P-BOD Removal Ratio	= 0.9143 × SS Removal Ratio(%) = 0.9143 × 59.6 = 54.5 %								
③ S-BOD Removal Ratio	= 0 % (Filtration Equipment can not remove S- BOD.)								
(4) Sewage Effluent									
① SS Concentration	= 225 mg/l × (100 - 59.6) ÷ 100 = 90.7 mg/l								
② P-BOD Removal Ratio	= (202 - 118)mg/l × (100 - 54.5) ÷ 100 = 38.0 mg/L								
③ S-BOD Removal Ratio	= 118 × (100 - 0.0) ÷ 100 = 118.2 mg/l								
④ BOD Concentration	= P-BOD + S-BOD = 38.0 + 118.2 = 156.2 mg/l								
(5) Washing Drainage									
① Average Filtration Loss Head	= Set to 40 cm								
② SS Inflow Surface Area Loading	= (40 ÷ 0.5124) ^ (1 / 1.1747) = 40.8 kg/m ² ·d (SS Inflow Surface Area Loading when Washing Frequency is 24 times / day)								
③ SS Inflow Surface Area Loading per Washing	= 40.8 ÷ 24 = 1.7 kg / m ² ·times								
④ Washing Frequency	= 223.7 m/d × 225 mg/L ÷ 1000 ÷ 1.7 = 29.5 times/d								
⑤ Per time Washing Drainage Rate	= Filtration Area (m ²) × Washing height (m/time) = 35.2 × 1.5 m/times = 52.8 m ³ /times								
⑥ Washing Drainage Rate	= 52.8 m ³ /times × 29.5 times/d = 1,559 m ³ /d								
(6) Solid Balance									
① Filtered Effluent SS	= (7,873 - 1,559) m ³ /d × 90.7 mg/L ÷ 1000 = 573 kg/d								
② Washing Drainage SS	= 7,873 m ³ /d × 225 mg/l ÷ 1000 - 573 kg/d = 1,195 (kg/d) (⇒ To the Drain Tank)								

Item	Contents (Target Year: After 2035)
3. High-rate Trickling Filter(HTF)	
(1)Sewage Influent	
①Flow Rate	= 6,314 m ³ /d
②Sewage Influent BOD Rate	= 6,314 m ³ /d × 156.2 mg/l / 1,000 = 986 kgBOD/d
③Sewage Influent SS Rate	= 6,314 m ³ /d × 90.7 mg/l / 1,000 = 573 kgBOD/d
(2)Facility Size	
①BOD Volumetric Loading	The BOD obtained by subtracting the Flow Rate × 15 mg-BOD/ L from the Sewage Influent BOD is set to 1.6 kg / m ³ ·d. (Japan specification 26B can achieve 15 mg /L or less as treated water BOD at 1.6 kg / m ³ ·d. Overseas specifications are calculated assuming that parts exceeding 1.6 kg / m ³ ·d will shift to treated water. = 1.6 kg/m ³ ·d
②Filter Bed Volumetric	= 986 kgBOD/d - 95 kgBOD/d ÷ 1.6 kg/m ³ ·d = 557 (m ³)
③Filter Bed Height	= 2.3 m is set.
④Filter Bed Area	= 557 m ³ ÷ 2.3 m = 242.3 m ²
⑤Area of 1 tank per	= 81 m ² /Tanks is set.
⑥Number of Tank	= 242.3 m ² ÷ 81 m ² /Tank = 3.0 tanks ⇒ 4 Tanks
⑦Actual BOD Volumetric Loading	= 986.3 ÷ (81 × 2.3 × 4) = 1.32 kg/m ³ ·d
⑧Shape of Tank	Square
⑨Size of Tank	
•Width	= 9.0 m
•Length	= 9.0 m
⑩Area of 1 tank per	= 81 m ² /Tanks
⑪Filter Bed Height	= 2.3 m
⑫Bottom Height of Filter Bed	= 0.7 m
(3)Washing Drainage	
①Washing Frequency	Weekly make 1 time washing
②Water Level Height at Washing	From the filter media surface 0.4 m
③Washing Drainage Rate	= (81 m ² /Tank × 4 Tank × (0.7 + 0.4) m + 81 m ² /Tank × 4 Tank × 2.3 m × Carrier Porosity 0.9) × 1 time/week ÷ 7 day/week = 146.7 (m ³ /d)
(4)Sewage Effluent	
①SS Concentration	= 6.2335 × Ln(BOD Volumetric Loading) + 22.233 = 6.2335 × Ln 1.324 kg/m ³ ·d + 22.233 = 24.0 mg/l
②SS Rate	= (6314 - 146.7) m ³ /d × 24.0 mg/L ÷ 1000 = 148 kg/d
③P-BOD (Particulate BOD)	= SS Concentration mg/L × P-BOD vs SS Ratio = 24.0 mg/l × 1.4008 = 33.6 mg/l
④S-BOD (Solute BOD) (Filter Bed Height 2.3 m Conversion)	= (0.7538 × Ln(BOD Volumetric Loading) + 2.6562) × 9.87715 × 2.3 ^ -0.92 ÷ 4.25 + 15 = (0.7538 × Ln 1.324 kg/m ³ ·d + 2.6562) × 9.87715 × 2.3 ^ -0.92 ÷ 4.25 + 15 = 18.1 mg/l
⑤BOD(mg/L)	= P-BOD mg/L + S-BOD mg/L = 33.6 mg/l + 18.1 mg/l = 51.7 mg/l
(5)Solid Balance	
①Washing Drainage SS	= 6,314 m ³ /d × 90.7 mg/l ÷ 1000 × 0.12 = 67.4 (kg/d) (⇒To the Drain Tank)

Item	Contents (Target Year: After 2035)
4. Final Solids-Liquid Separator (SLS)	
(1) Sewage Influent	
①Flow Rate	= 6,168 m ³ /d
(2)Facility Size	
①Design Filtration rate	= 150 m/d
②Required Filtration Area	= Flow Rate 6,168 m ³ /d ÷ Design Filtration rate 150 m/d = 41.1 m ²
③Number of Tank	= 4 Tanks
④Area of Tank	= 41.1 m ² ÷ 4 Tanks = 10.3 m ²
⑤Shape of Tank Size of Tank	Square
•Width	= 3.0 m
•Length	= 10.3 m ² ÷ 3.0 m = 3.426 → 3.5 m
⑥Filtration Area per Tank	= 10.5 m ² /Tanks
⑦Actual Filtration Rate	6,168 m ³ /d ÷ 10.5 m ² /Tanks × 4 Tanks = 146.8 m/d
(3)Removal Performance	
①SS Removal Ratio	= 0.2549 × Sewage Influent SS Rate mg/l + 78.088 = 0.2549 × 24 mg/l + 78.088 = 84.2 %
②S-BOD Removal Ratio	= 0 % (Filtration Equipment can not remove S- BOD.)
(4)Sewage Effluent	
①SS Concentration	= 24 mg/l × (100 - 84.2) ÷ 100 = 3.79 mg/l
②P-BOD Removal Ratio	= 3.79 mg/l × 1.4008 = 5.31 mg/l
③S-BOD Removal Ratio	= 18.1 × (100 - 0.0) ÷ 100 = 18.1 mg/l
④BOD Concentration	= P-BOD + S-BOD = 5.3 + 18.1 = 23.4 mg/l
(5)Washing Drainage	
①SS Inflow Surface Area Loading per Washing	= 6,168 m/d × 24 mg/l ÷ 42.0 m ² ÷ 1000 = 3.5 kgSS / m ² ·times
②Washing Interval	= 20 hr/d
③Washing Drainage Time	= 0.5 hr/times
④Washing Drainage Rate	= 6,168 × 24 ÷ 20 × 0.5 ÷ 24 = 154 m ³ /d
(6)Solid Balance	
①Effluent SS	= Effluent SS mg/l × (Flow Rate m ³ /d - Washing Drainage Rate m ³ /d) ÷ 1000 = 3.79 mg/l × (6,168 m ³ /d - 154 m ³ /d) ÷ 1000 = 23 kg/d
②Total generated sludge SS	= Washing Drainage SS kg/d + Settling Sludge SS kg/d = 148 kg/d - 23 kg/d = 125 kg/d
③Washing Drainage SS	= Final filtration total generated sludge kg/d × Final filtration total generated sludge / Final filtration tank sludge ratio (-) = 125 kg/d × 0.6 = 75 kg/d (⇒To the Drain Tank)
④Settling Sludge SS	= Total generated sludge kg/d - Washing Drainage SS kg/d = 125 kg/d - 75 kg/d = 50 kg/d (⇒To the Drain Tank)
⑤Settling Sludge SS Concentration	= 4,090 mg/l (From the result of demonstration experiment)
⑥Settling Sludge Volume	= Settling Sludge SS kg/d ÷ Settling Sludge SS Concentration mg/l × 1000 = 50 kg/d ÷ 4,090 mg/l × 1000 = 12 (m ³ /d)

Item	Contents (Target Year: After 2035)																																	
<p>(7) SLS Settling Sludge Transfer Pump</p> <p>① Pump Capacity</p> <p>② Liquid Specific Gravity (γ)</p> <p>③ Head Loss(H)</p> <p>④ Pump Shaft Power</p> <p>⑤ Motor Output</p> <p>⑥ Specifications</p>	$= \frac{12 \text{ m}^3/\text{d}}{0.10 \text{ m}^3/\text{min}/\text{Tanks}} \div 2 \text{ Times/d} \div 15 \text{ min/Times} \div 4 \text{ Tanks}$ $= \frac{1.0}{10} \text{ to set}$ $P_s = \frac{0.163 \cdot \gamma \cdot Q \cdot H}{0.7} = 0.24 \text{ kw}$ $P = P_s \times (1 + \alpha) \quad (\alpha: \text{Margin})$ $= 0.24 \times (1 + 0.15)$ $= 0.27 \text{ kw} \rightarrow 0.3 \text{ kw (Catalogue Value)}$ <p>Type Centrifugal Pump</p> <p>Discharge Diameter 100 A</p> <p>Pump Capacity 0.10 m³/min</p> <p>Pump Head 10 m</p> <p>Motor Output 0.3 kw</p> <p>Number 6 Pumps (Including Standby of 2 Pumps)</p>																																	
<p>5. Drain Tank</p>																																		
<p>(1) Drainage Volume</p>	<table border="1"> <thead> <tr> <th></th> <th>Drainage Volume m³/d</th> <th>SS Concentration mg/L</th> <th>Solids kg-DS/d</th> </tr> </thead> <tbody> <tr> <td>FSF Washing Drainage Rate</td> <td>1,559</td> <td>767</td> <td>1,195</td> </tr> <tr> <td>HTF Washing Drainage Rate</td> <td>147</td> <td>459</td> <td>67</td> </tr> <tr> <td>SLS Washing Drainage Rate</td> <td>154</td> <td>487</td> <td>75</td> </tr> <tr> <td>SLS Settling Sludge Volume</td> <td>12</td> <td>4,090</td> <td>50</td> </tr> <tr> <td>Total</td> <td>1,872</td> <td>741</td> <td>1,387</td> </tr> </tbody> </table>		Drainage Volume m ³ /d	SS Concentration mg/L	Solids kg-DS/d	FSF Washing Drainage Rate	1,559	767	1,195	HTF Washing Drainage Rate	147	459	67	SLS Washing Drainage Rate	154	487	75	SLS Settling Sludge Volume	12	4,090	50	Total	1,872	741	1,387									
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<p>(2) Capacity of the Drainage Tank</p> <p>* The capacity of the drainage tank shall be the capacity that can accept the total of one wash drainage per tank of FSF, HTF, SLS.</p>																																		
<p>① 1 Tank · 1 Washing Drainage Volume</p> <p>· FSF Washing Drainage Rate</p> <p>· HTF Washing Drainage Rate</p> <p>· SLS Washing Drainage Rate</p> <p>· Capacity of the Drainage Tank</p> <p>② Number of Tank</p>	$= 13 \text{ m}^3$ $= 256.77 \text{ m}^3$ $= 32 \text{ m}^3$ $= 13 + 256.77 + 32 = 302 \text{ m}^3 \Rightarrow 350 \text{ m}^3$ $= 2 \text{ Tanks}$																																	
<p>(3) Sludge Transfer Pump (Drain Tank to Sludge Thickening)</p> <p>The Capacity of the Sludge Transfer Pump is set based on the Generation Interval of Each Washing Drainage .</p>	<table border="1"> <thead> <tr> <th rowspan="2"></th> <th>A</th> <th>B</th> <th>C</th> <th>D</th> <th>E</th> <th rowspan="2">A/E</th> </tr> <tr> <th>1 Tank · 1 Time per (m³/time · tank)</th> <th>Washing Frequency (time/day · tank)</th> <th>Number of Tank (tank)</th> <th>Number of Washing Cycles (time/day)</th> <th>Washing Interval (minute)</th> </tr> </thead> <tbody> <tr> <td>FSF</td> <td>13</td> <td>29.5</td> <td>4</td> <td>118</td> <td>12.2</td> <td>1.08</td> </tr> <tr> <td>HTF</td> <td>256.77</td> <td>0.14</td> <td>4</td> <td>0.6</td> <td>2,730</td> <td>0.09</td> </tr> <tr> <td>SLS</td> <td>32</td> <td>1.20</td> <td>4</td> <td>4.8</td> <td>325</td> <td>0.10</td> </tr> </tbody> </table>		A	B	C	D	E	A/E	1 Tank · 1 Time per (m ³ /time · tank)	Washing Frequency (time/day · tank)	Number of Tank (tank)	Number of Washing Cycles (time/day)	Washing Interval (minute)	FSF	13	29.5	4	118	12.2	1.08	HTF	256.77	0.14	4	0.6	2,730	0.09	SLS	32	1.20	4	4.8	325	0.10
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<p>① Pump Capacity</p> <p>② Liquid Specific Gravity (γ)</p> <p>③ Head Loss(H)</p> <p>④ Pump Shaft Power</p> <p>⑤ Motor output</p> <p>⑥ Specifications</p>	$= (1.08 + 0.09 + 0.10) \div 2 = 0.64 \text{ m}^3/\text{min}$ $= \frac{1.0}{10} \text{ m}$ $P_s = \frac{0.163 \cdot \gamma \cdot Q \cdot H}{0.7} = 1.48 \text{ kw}$ $P = P_s \times (1 + \alpha) \quad (\alpha: \text{Margin})$ $= 1.48 \times (1 + 0.15)$ $= 1.71 \text{ kw} \rightarrow 2.0 \text{ kw (Catalogue Value)}$ <p>Type Submersible Pump</p> <p>Discharge Diameter 150 A</p> <p>Pump Capacity 0.7 m³/min</p> <p>Pump Head 10 m</p> <p>Motor Output 2.0 kw</p> <p>Number 4 Pumps (Including Standby of 2 Pumps)</p>																																	
<p>(4) HTF Washing Drainage Transfer Pump</p> <p>① Pump Capacity</p> <p>② Liquid Specific Gravity (γ)</p> <p>③ Head Loss(H)</p> <p>④ Pump Shaft Power</p> <p>⑤ Motor output</p> <p>⑥ Specifications</p>	$= 0.09 \text{ m}^3/\text{min} \div 4 \text{ Pumps} = 0.024 \text{ m}^3/\text{min}$ $= \frac{1.0}{10} \text{ m}$ $P_s = \frac{0.163 \cdot \gamma \cdot Q \cdot H}{0.7} = 0.05 \text{ kw}$ $P = P_s \times (1 + \alpha) \quad (\alpha: \text{Margin})$ $= 0.05 \times (1 + 0.15)$ $= 0.06 \text{ kw} \rightarrow 0.1 \text{ kw (Catalogue Value)}$ <p>Type Submersible pump</p> <p>Discharge Diameter 100 A</p> <p>Pump Capacity 0.05 m³/min</p> <p>Pump Head 10 m</p> <p>Motor Output 0.1 kw</p> <p>Number 4 Pumps</p>																																	

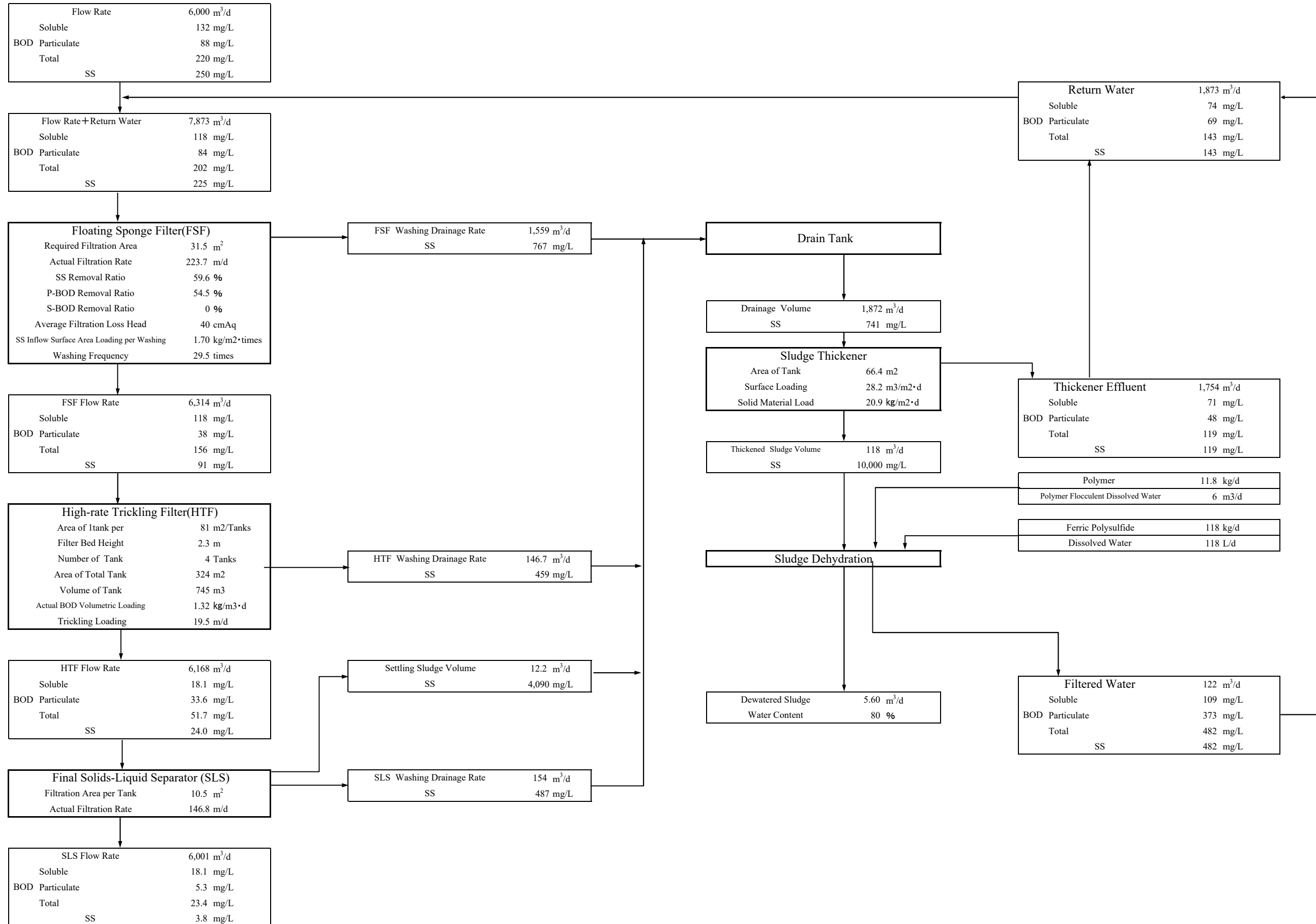
Item	Contents (Target Year: After 2035)
(5) SLS Washing Drainage Tank	
	SLS 1 Tank Capacity shall be accepted for 20 minutes of Washing Drainage .
①Washing Drainage Volume for 20 minutes	= 6,168 m ³ /d ÷ 24 ÷ 60 ÷ 4 × 20 = 21 m ³
②Washing Drainage Tank Volume	= 25 m ³
③Number of Tank	= 2 Tanks
(6) SLS Washing Drainage Transfer Pump	
①Pump Capacity	= 0.10 m ³ /min ÷ 0 Pumps = #DIV/0! m ³ /min
②Liquid Specific Gravity (γ)	= 1.0
③Head Loss(H)	= 10 m
④Pump Shaft Power	$P_s = \frac{0.163 \cdot \gamma \cdot Q \cdot H}{0.7} = 0.23 \text{ kw}$
⑤Motor output	P= P _s × (1 + α) (α: Margin) = 0.23 × (1 + 0.15) = 0.26 kw → 0.2 kw (Catalogue Value)
⑥ Specifications	Type Submersible pump Discharge Diameter 100 A Pump Capacity 0.10 m ³ /min Pump Head 10 m Motor Output 0.2 kw Number 4 Pumps (Including Standby of 2 Pumps)
6. Sludge Thickening	
(1) Sludge Thickener	
①Maximum Daily Flowrate	= 1,872 m ³ /d
②Number of Tank	= 2 Tanks
③Design Water Area Load	= Below 30 m ³ /d
④Require Water Area	= 1,872 m ³ /d ÷ 30 m ³ /d ÷ 2 Tanks = 31.2 m ² /Tanks
⑤Water Depth	= 4 m
⑥Diameter of Tank	= 6.5 m
⑦Area of Tank	= 33.2 m ² /Tanks
⑧Surface Loading	= 1,872 m ³ /d ÷ 66.4 m ² = 28.2 m ³ /d
⑨Solid Material Load	= 1,387 kg/d ÷ 66.4 m ² = 20.9 kg/m ² ·d
⑩Retention time	= 33.2 m ² /Tanks × 2 Tanks × 4 m ÷ 1,872 m ³ /d × 24 = 3.40 hr
⑪Performance	
•Density of Concentrated Sludge	= 1.0 %
•Solid Capture Rate	= 85.0 %
⑫Thickened Sludge	
•Solids SS	= Total Solids (kgSS/d) × Solid Capture Rate (%) = 1,387 kg/d × 85 (%) × 0.01 = 1,179 kg/d
•Thickened Sludge Volume	= Solids kg/d / Density of Concentrated Sludge % = 1,179 kg/d / 1.0 % × 100 ÷ 1000 = 118 m ³ /d
•SS Concentration	= Solids SS kg/d / Thickened Sludge Volume m ³ /d × 1000 = 1,179 kg/d / 118 m ³ /d × 1000 = 10,000 mg/l
•Thickener Effluent	= Drainage Volume m ³ /d - Thickened Sludge Volume m ³ /d = 1,872 m ³ /d - 118 m ³ /d = 1,754 (m ³ /d)
•Thickener Effluent Solids SS	= Total Solids (kgSS/d) × (1 - Solid Capture Ratio) = 1,387 kg/d × (1 - 0.85) = 208 (kg/d)
•SS Concentration	= Solids SS kg/d / Thickener Effluent m ³ /d × 1000 = 208 kg/d / 1,754 m ³ /d × 1000 = 119 mg/l
•BOD	= SS Concentration mg/l × Primary Thickener Effluent BOD / SS ratio = 119 mg/l × 1.0 = 119 mg/l

Item	Contents (Target Year: After 2035)
<p>(2) Sludge Thickener Transfer Pump</p> <p>①Thickened Sludge Volume</p> <p>②Pump Capacity</p> <p>③Liquid Specific Gravity (γ)</p> <p>④Head Loss(H)</p> <p>⑤Pump Shaft Power</p> <p>⑥Motor Output</p> <p>⑦ Specifications</p>	<p>= 118 m³/d</p> <p>= 118 m³/d ÷ 360 min/d ÷ 2 pumps = 0.16 m³/min</p> <p>= 1.0</p> <p>= 10 m</p> <p>$P_s = \frac{0.163 \cdot \gamma \cdot Q \cdot H}{0.7} = 0.38$ kw</p> <p>$P = P_s \times (1 + \alpha)$ (α: Margin) = 0.38 × (1 + 0.15) = 0.44 kw → 0.5 kw (Catalogue Value)</p> <p>Type Centrifugal Pump</p> <p>Discharge Diameter 80 A</p> <p>Pump Capacity 0.20 m³/min</p> <p>Pump Head 10 m</p> <p>Motor Output 0.5 kw</p> <p>Number 4 Pumps (Including Standby of 2 Pumps)</p>
<p>7. Sludge Dehydration</p>	
<p>(1) Sludge Storage Tank</p>	
<p>The Sludge Storage Tank should be a Capacity that can store one day of Thickened Sludge.</p>	
<p>①Thickened Sludge Volume</p> <p>②Number of Tank</p> <p>③Req. Volume</p> <p>④Size of tank •Water Depth •Width •Length</p> <p>⑤Volume</p>	<p>= 118 m³/d</p> <p>= 2 Tanks</p> <p>= 118 m³/d ÷ 2 Tanks ÷ 1 day = 59 m³/tanks</p> <p>= 3.0 m</p> <p>= 3.5 m</p> <p>= 6.5 m</p> <p>= 3.5 m × 6.5 m × 3.0 m = 68 m³</p>
<p>(2) Dehydrator Supply Pump</p>	
<p>①Thickened Sludge Volume</p> <p>②Pump Capacity</p> <p>③Head Loss(H)</p> <p>④Specifications</p>	<p>= 118 m³/d</p> <p>= 118 m³/d ÷ 24 hr/d ÷ 3 Pumps = 1.64 m³/hr</p> <p>= 15 m</p> <p>Type Uniaxial Screw Pump</p> <p>Discharge Diameter 100 A</p> <p>Pump Capacity 1.3 m³/hr</p> <p>Pump Head 15 m</p> <p>Motor Output 3.7 kw</p> <p>Number 6 Pumps (Including Standby of 2 Pumps)</p>
<p>(3) Dehydrator</p>	
<p>①Sludge Concentration</p> <p>②Sludge Weight</p> <p>③Operation Conditions</p> <p>④Supply Solid Weight</p> <p>⑤Specifications</p>	<p>= 1.0 %</p> <p>= 118 m³/d × 1.0 % × 0.01 × 1,000 kg/m³ 1,179 kg/d</p> <p>= 24 hr/d and 7 days in a week</p> <p>= 1,179 kg/d ÷ 24 hr/d × 7 ÷ 7 days ÷ 3 unit = 16 kg/h</p> <p>Type Volute Dewatering Press(SUS)</p> <p>Supply Sludge Concentration 1.0 %</p> <p>Capacity Max 20 kg/h (Catalogue Value)</p> <p>SS Recovery ≧ 95 %</p> <p>Sludge Cake Moisture Content ≦ 80 %</p> <p>Motor Output 3.95 kw</p> <p>Number 3 units</p>

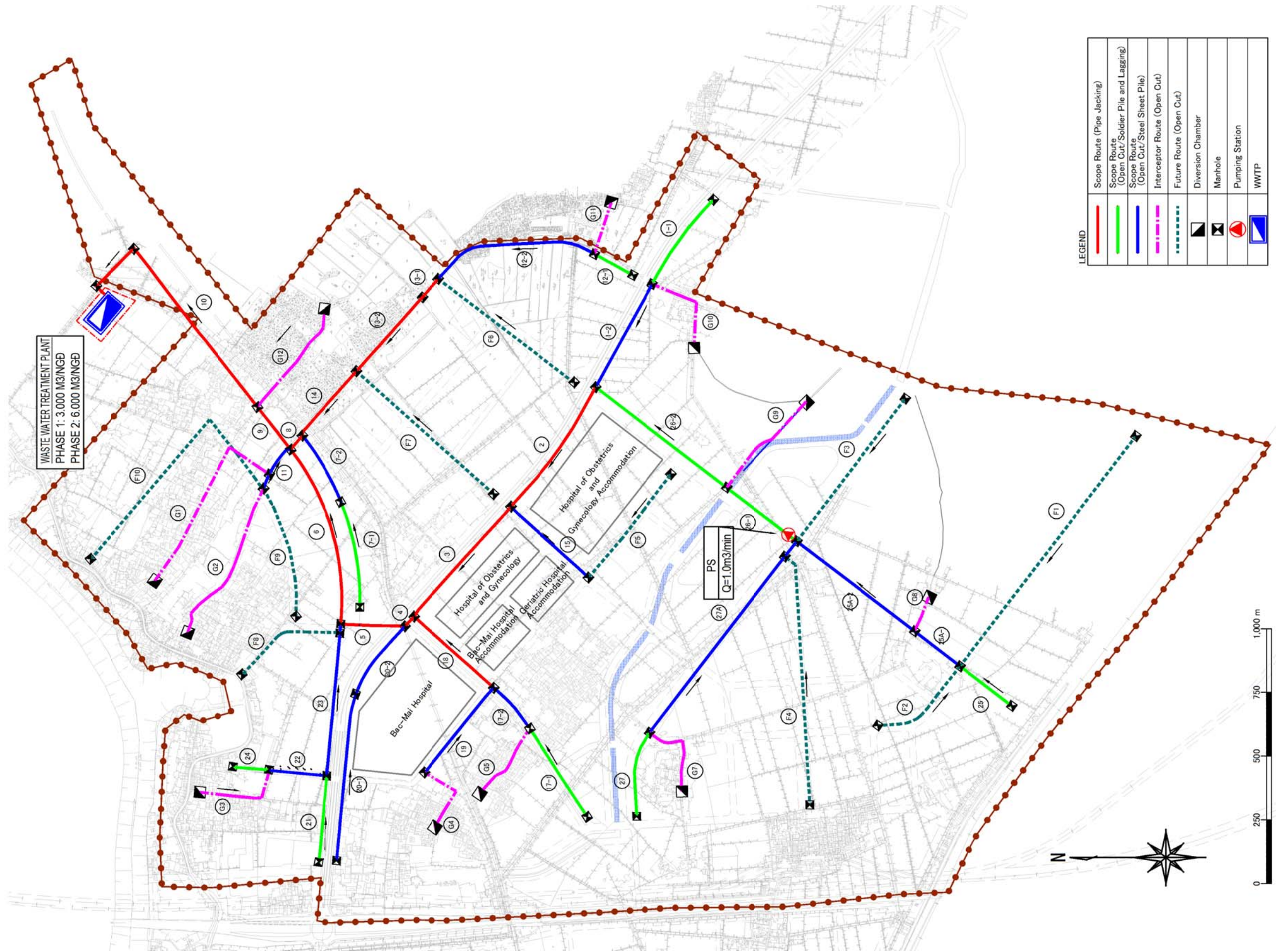
Item	Contents (Target Year: After 2035)
<p>(4) Chemical Injection System</p> <p>① Polymer Injection Pump</p> <ul style="list-style-type: none"> • Dewatering Capacity • Injection Rate • Injection Dose • Solution concentration • Req. Volume • Flexibility • Pump Capacity • Specifications <p>② Polymer Solution Tank</p> <ul style="list-style-type: none"> • Retention Time • Req. Volume • Number of Tank • Specifications <p>③ Ferric Polysulfide Injection Pump</p> <ul style="list-style-type: none"> • Dewatering Capacity • Injection Rate • Injection Dose • Solution Density • Req. Volume • Flexibility • Pump Capacity • Specifications <p>④ Ferric Polysulfide Solution Tank</p> <ul style="list-style-type: none"> • Retention Time • Req. Volume • Number of Tank • Specifications 	<p>= 16 kg-DS/h</p> <p>= 1.0 % to Set</p> <p>= 16 kg-DS/h × 0.01 = 0.16 kg/h</p> <p>= 0.2 %</p> <p>= 0.16 ÷ 0.002 ÷ 60 min = 1.4 L/min</p> <p>= 0.5 ~ 1</p> <p>= 0.7 ~ 1.4 L/min</p> <p>Type Diaphragm Metering Pump</p> <p>Discharge 40 A</p> <p>Diameter</p> <p>Pump Capacity 0.5~1.0 L/min</p> <p>Motor Output 0.1 kw</p> <p>Number 3 Pumps (Including Standby of 2 Pumps)</p> <p>Max. Discharge Pressure 0.3 Mpa</p> <p>= 2 hr</p> <p>= 1.36 L/min × 120 min ÷ 1000</p> <p>= 0.16 m3/Tanks → 0.5 m3/Tanks</p> <p>= 4 Tanks</p> <p>Type Circle Tank</p> <p>Volume 0.5 m3</p> <p>Number 4 Tanks</p> <p>Agitator 4 Unit/Tank(1.5kw)</p> <p>= 16 kg-DS/h</p> <p>= 15 %</p> <p>= 16 kg-DS/h × 0.15 = 2.5 kg-DS/h</p> <p>= 1.45</p> <p>= 2.5 ÷ 1.45 ÷ 60 min = 0.03 L/min</p> <p>= 0.5 ~ 1.5</p> <p>= 0.014 ~ 0.042 L/min</p> <p>→ 0.1 ~ 0.3 L/min</p> <p>Type Diaphragm Metering Pump</p> <p>Discharge 15 A</p> <p>Diameter</p> <p>Pump Capacity 0.1~0.3 L/min</p> <p>Motor Output 0.1 kw</p> <p>Number 4 Pumps (Including Standby of 2unit)</p> <p>Discharge Pressure 0.5 Mpa</p> <p>= 1 days = 24 hr</p> <p>= 2.5 kg-DS/h ÷ 1.45 × 24 hr</p> <p>= 0.1 m3/Tanks</p> <p>= 2 Tanks</p> <p>Type Circle Tank</p> <p>Volume 0.1 m3</p> <p>Number 2 Tanks</p> <p>Agitator 2 Unit/Tank(0.1kw)</p>
<p>(5) Cake Hopper</p> <p>* Cake Hopper Volume is Calculated Based on Maximum Daily Flowrate .</p> <p>① Sludge Volume</p> <p>② SS Recovery Rate</p> <p>③ Sludge Amount per a Day</p> <p>④ Sludge Amount per a Day</p> <p>⑤ Water Content</p> <p>⑥ Dewatered Sludge</p> <p>⑦ No of Hopper</p> <p>⑧ Req. Volume</p> <p>⑨ Specifications</p> <p>(6) Filtered Water</p> <p>① Thickened Sludge Volume</p> <p>② Polymer Flocculent Dissolved Water</p> <p>③ Water content in Sludge Cake</p> <p>④ Filtered Water Volume</p> <p>⑤ SS in Filtered Water</p> <p>⑥ Filtered Water SS</p> <p>⑦ Filtered Water BOD</p> <p>⑧ Filtered Water S-BOD</p>	<p>= 16 kg/d × 3 Units × 24 hr/d × 7 / 7</p> <p>= 1,179 kg/d</p> <p>= 95 %</p> <p>= 1,179 kg/d × 0.95</p> <p>= 1,120 kg/d = 1.1 t-DS/d</p> <p>= 1,120 kg-DS/d</p> <p>= 80 %</p> <p>= 1120 / (1 - 80 %) ÷ 1000</p> <p>= 5.6 m3/d</p> <p>= 3 Units</p> <p>= 1.9 m3/d → 2.0 m3/Units</p> <p>Type Auto Cut Gate Type</p> <p>Volume 2.0 m3</p> <p>Motor Output 1.5 kw × 2</p> <p>Number 3 Units</p> <p>= 118 m3/d</p> <p>= 6 m3/d</p> <p>= 1 m3/d</p> <p>= 122 m3/d</p> <p>= 59 kg/d</p> <p>= 482 mg/l</p> <p>= 482 mg/l</p> <p>= 109 mg/l</p>

Item	Contents (Target Year: After 2035)
<p>8. Chlorination</p> <p>(1)Chlorination Tank * Chlorination Tank volume is Calculated Based on Maximum Daily Flowrate .</p> <p>①Maximum Flow rate = 6,168 m3/d ②Contact Time = 15 min ③Number of Tank = 1 Tanks</p> <p>④Req. Volume of Tank = $6,168 \text{ m}^3/\text{d} \times 15 \text{ min}/\text{d} \div 1,440 \div 1 \text{ Tanks}$ = 64 m3</p> <p>⑤Shape of Tank Rectangular ⑥Size of Tank •Width = 1.5 m •Length = 30.0 m •Effective Depth = 1.5 m •Volume of Tank = 68 m3</p> <p>(2)Sodium Hypochlorite Dosing Pump * Sodium Hypochlorite Dosing Pump Volume is Calculated Based on Maximum Hourly Flowrate.</p> <p>①Disinfection Volume = 8,300 m3/d ②Dosing Rate = 3 mg/L ③Disinfectant Concentration = 10 % ④Disinfectant Density = 1.1 t/m3 ⑤Dosing Pump Capacity = $8,300 \text{ m}^3/\text{d} \times 3 \text{ mg}/\text{L} \div 10 \% \div 1.1$ = 0.16 L/min</p> <p>⑥Specifications Type Diaphragm Metering Pump Pump Capacity 0.16 L/min Motor Output 0.2 kw Number 2 Units (Including Standby) Max.Discharge Pressure 1.0 Mpa</p> <p>(3)Sodium Hypochlorite Storage ①Storage Time = 2.5 days ② Req. Volume = $0.16 \text{ L}/\text{min} \times 1,440 \text{ min}/\text{d} \times 2.5 \text{ days} \times 10^{-3}$ = 0.57 m3/Tanks → 0.7 m3/Tanks ③Number of Tank = 1 tanks ④Specification Type Circle Tank Volume 0.7 m3 Number 1 Tanks</p>	
<p>9. Polishing Pond</p> <p>Design Inflow = 6,000 m3/d Size Width= 50.0 m (Effective width= 41.0 m) (Slope, 1:1) Length= 83.0 m (Effective length= 74.0 m) Depth= 4.5 m (Effective depth= 2.0 m)</p> <p>Number of pond 2 ponds Required retention time 2.0 days Effective volume 41.0 m x 74.0 m x 2.0 m x 2 ponds = 12,136 m3 Retention time 12,136 m3 ÷ 6,000 m3/day = 2.0 days</p>	
<p>9. Water Discharge</p> <p>(1)Outfall Pump * Water Discharge Pump is calculated based on Maximum Hourly Flowrate .</p> <p>①Pump Capacity = 5.88 m3/min = QMax ②Pump Distribution = QMax = 5.88 m3/min ③Pump Head ④Specification for Pressure Piping •Diameter φ 250 mm •Number 2 pipe •Highest Level (End of Pipe) + 3.400 M •Length 500 m</p> <p>(2)Head Loss at Pressure Pipe (PP) Pumping Flow Rate(Maximum) Q= QMax = 2.94 m3/min = 0.049 m3/sec</p> <p>①Cross Section A= 0.25 m² × π × 1/4 = 0.049 m2 ②Flow Rate V= 0.049 / 0.049 = 1.0 m/s ③Loss Calculation • Head Loss hf= 10.666 × (0.049 / 110)^{1.85} × 0.25^{-4.87} × 500 = 2.88 m • Outlet Loss h0= 1.0 × 1.0² / 2g = 0.051 m •Total H=hf + h0 = 2.93 m ④Head Loss Around Pump H= 2.0 m</p> <p>⑤Actual Pump Head H= (Highest Level - Pumping Level) = 3.400 M - -2.500 M = 5.900 m ⑥Total Pump Head H= (Actual Pump Head + Pressure Pipe + Around Pump) = 5.900 + 2.93 + 2.00 = 10.830 m → 11 m</p> <p>⑦Motor Output •Pumping Flow Rate Q 2.8 m3/min •Liquid Specific Gravity γ 1.0 •Pump Efficiency η 0.7 •Pump Shaft Power Ps = $\frac{0.163 \cdot \gamma \cdot Q \cdot H}{\eta} = 7.17 \text{ kw}$</p> <p>⑧Motor Output P= Ps × (1 + α) (α: Margin) = 7.17 × (1 + 0.15) = 8.25 kw → 11.0 kw (Catalogue Value)</p> <p>⑨Specifications Type Submersible Pump Diameter 250 A Motor Output 11.0 kw Total Pump Head 11 m Pump Capacity 3.0 m3/min Number 3 Pump (Including Standby of 1 Pump)</p>	

•Solid Balance Calculation :Target Year: After 2035)



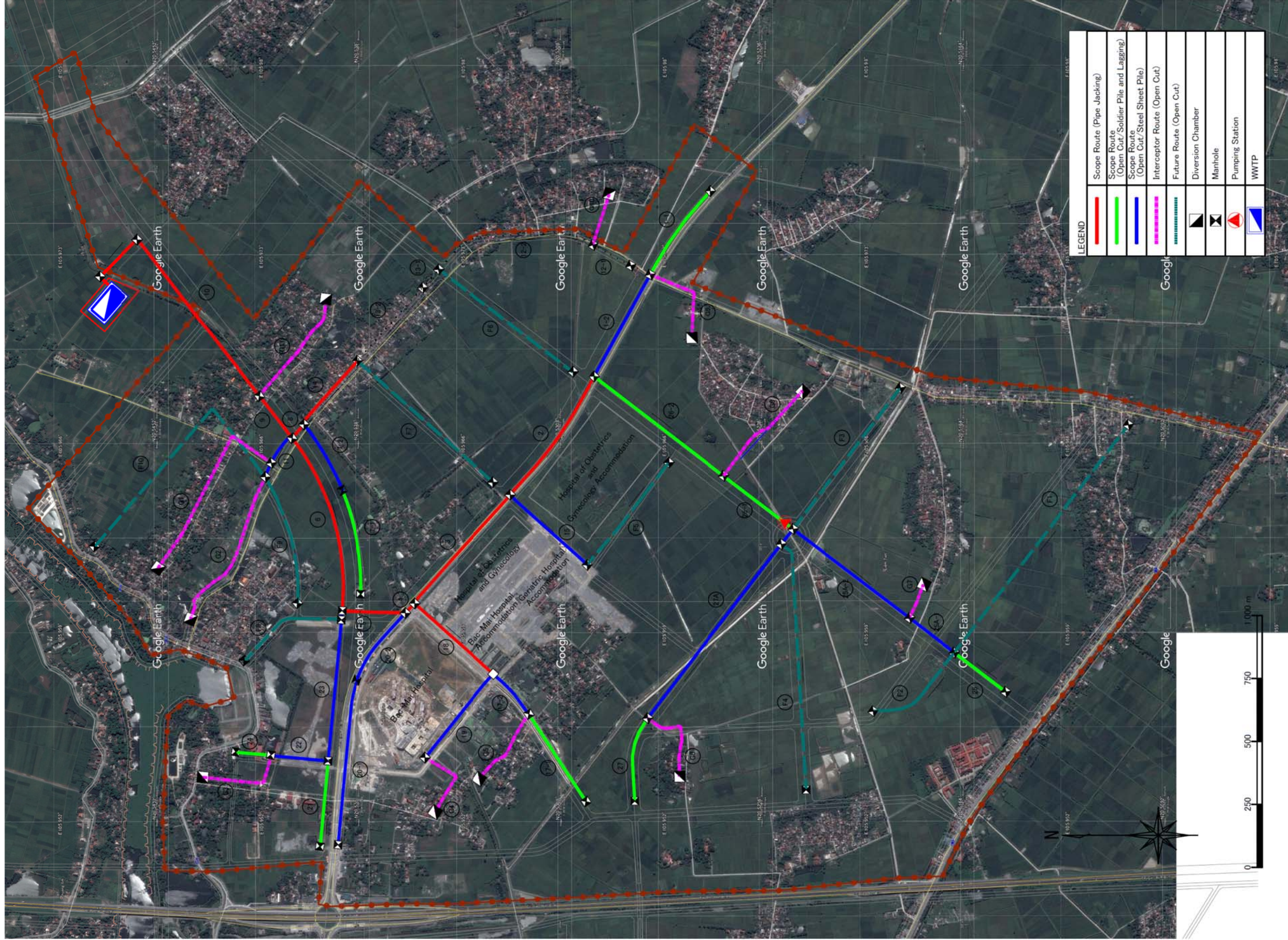
6. Drawings



LEGEND

	Scope Route (Pipe Jacking)
	Scope Route (Open Cut/Soldier Pile and Lagging)
	Scope Route (Open Cut/Steel Sheet Pile)
	Interceptor Route (Open Cut)
	Future Route (Open Cut)
	Diversion Chamber
	Manhole
	Pumping Station
	WWTP

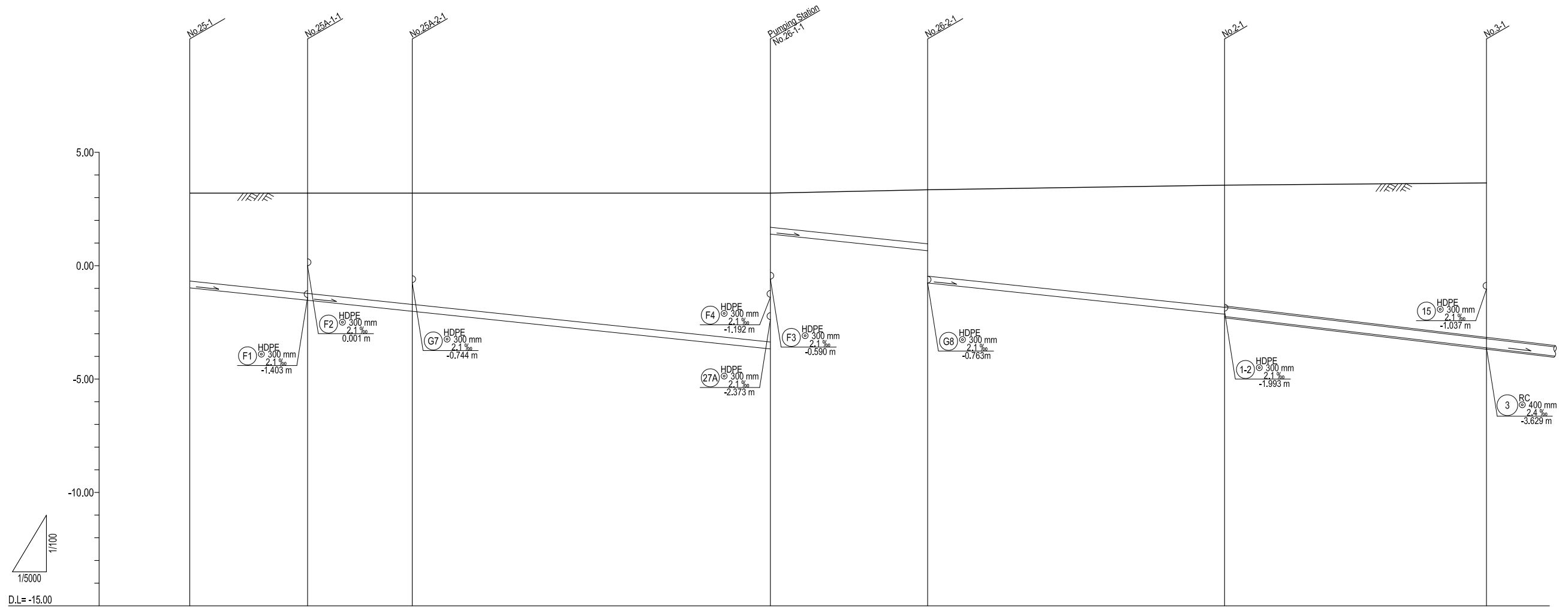
General Layout of Sewer Network



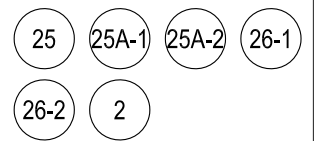
General Layout of Sewer Network (with Image of Present Development Condition)

Profile of Main Sewer

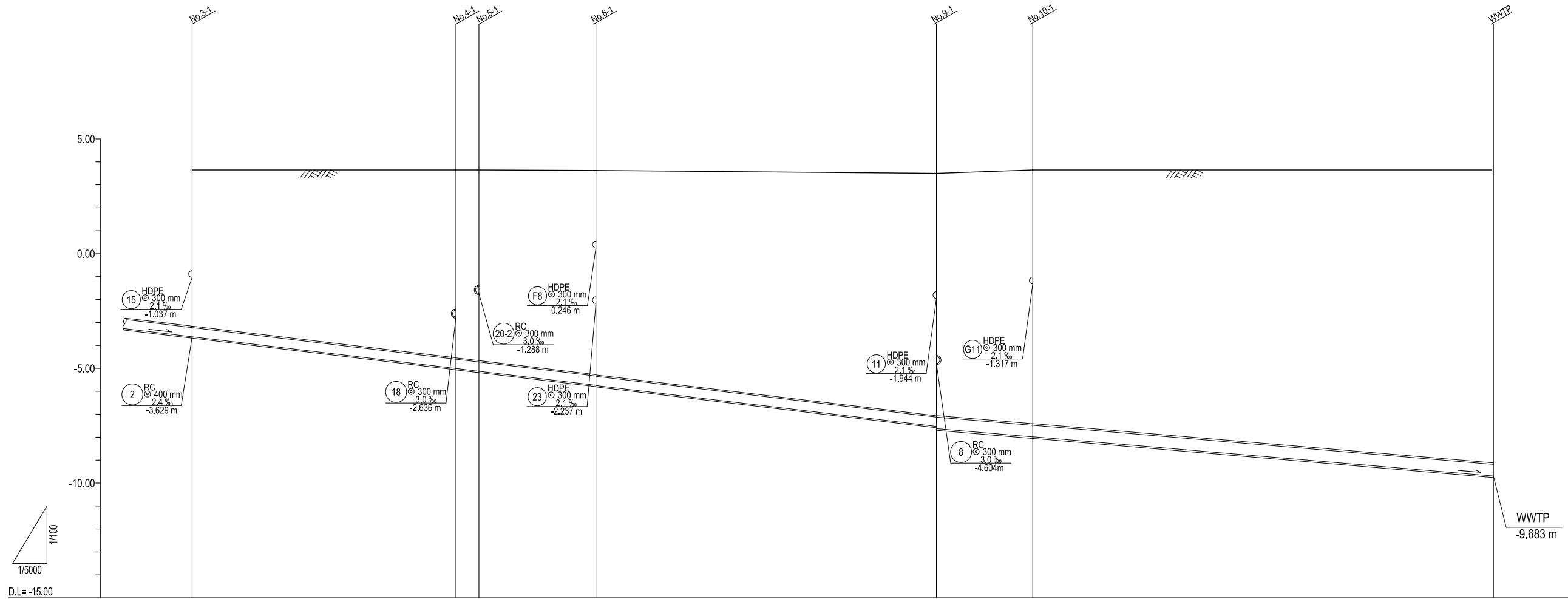
Scale $V = 1:100$
 $L = 1:5000$



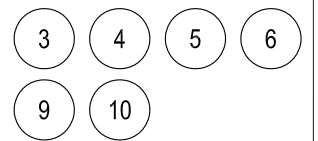
No	25		25A-1		25A-2			26-1		26-2		2	
DIAMETER	HDPE @ 300		HDPE @ 300		HDPE @ 300			HDPE @ 300		HDPE @ 300		RC @ 400	
GRADIENT	2.1 ‰		2.1 ‰		2.1 ‰			2.1 ‰		2.1 ‰		2.4 ‰	
LENGTH	260.0 m		231.00m		790.00m			347.00m		655.00m		578.00m	
GROUND ELEVATION (FH)	3.20		3.20		3.20			3.20		3.35		3.55	
COVERING DEPTH	3.87		4.42		4.90			6.66 2.50		3.38 3.80		5.38 5.33	
INVERT ELEVATION	-0.979		-1.525		-2.010			-3.669 -0.391		-0.338 -0.763		-2.139 -2.239	
ACCUMULATED	0.00		260.00		491.00			1281.00		1628.00		2283.00	



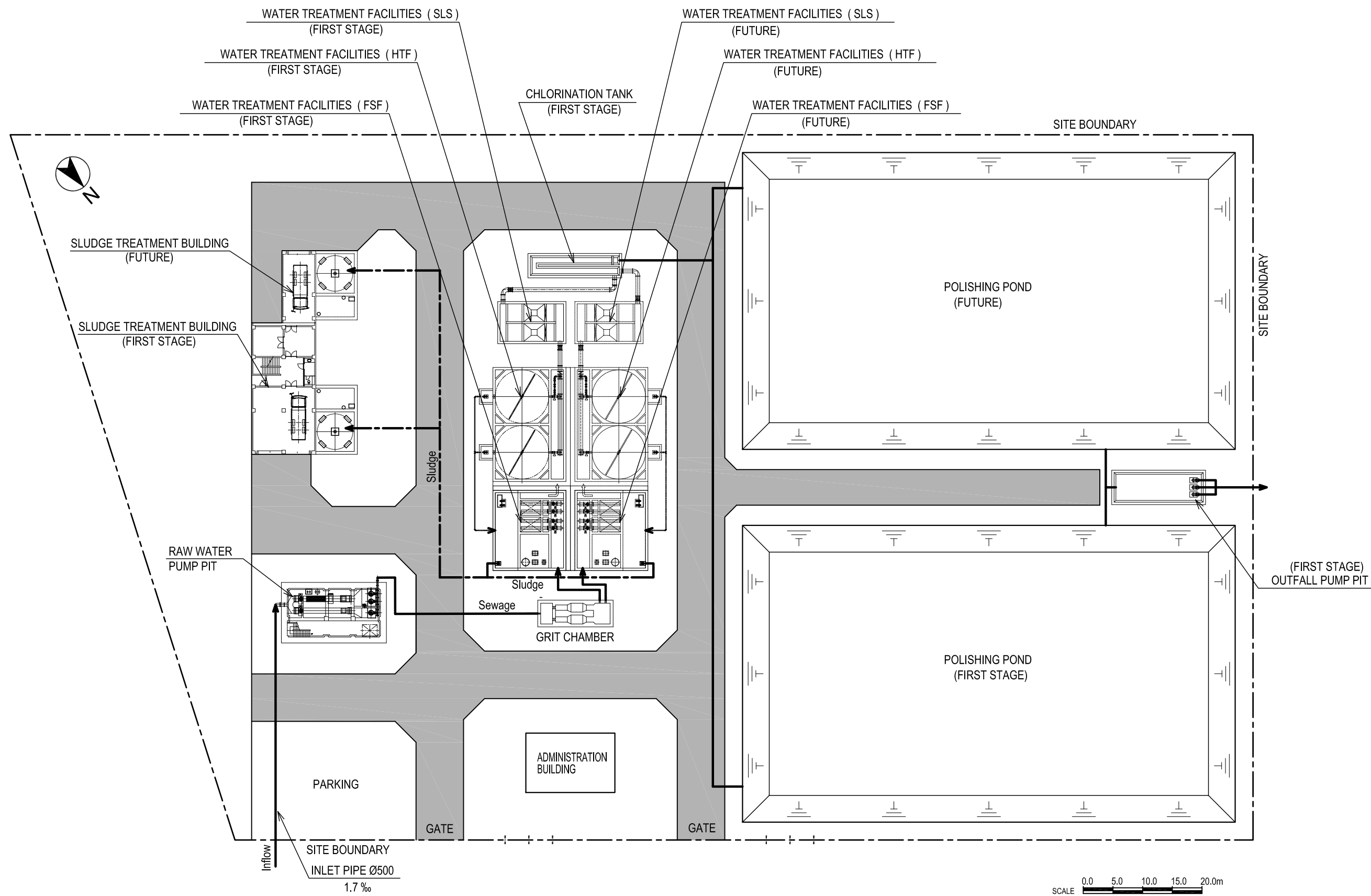
NAME OF DRAWINGS	PROFILE OF MAIN SEWER (1/2)	SCALE: A1 V=1/100 H=1/5000 A3 V=1/200 H=1/10000
DESIGNED BY	JICA SURVEY TEAM	



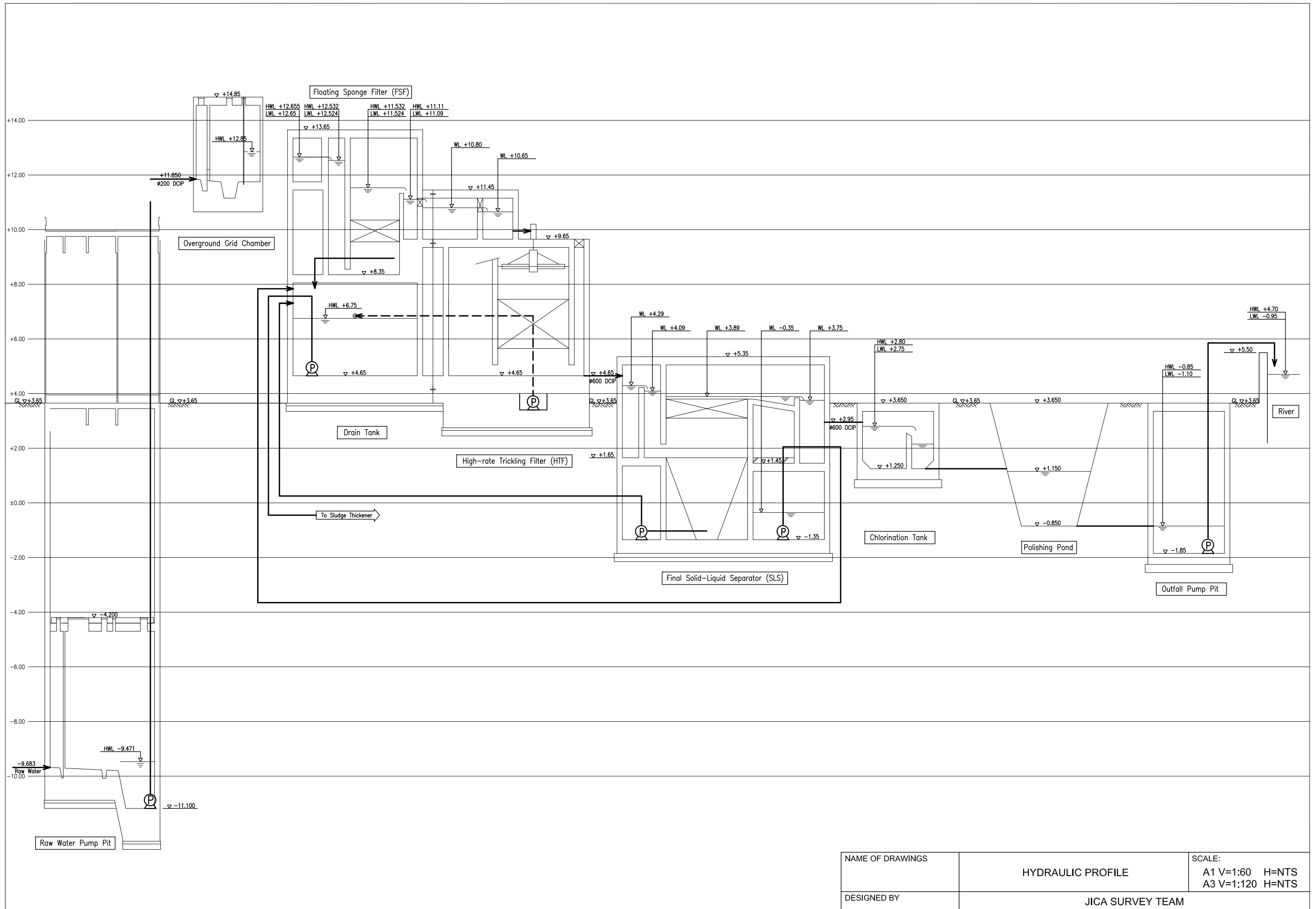
No		3	4	5	6	9	10		
DIAMETER		RC 400	RC 400	RC 400	RC 400	RC 500	RC 500		
GRADIENT		2.4 ‰	2.4 ‰	2.4 ‰	2.4 ‰	1.7 ‰	1.7 ‰		
LENGTH		575.0 m	50.0 m	255.0 m	742.00m	210.00m	1004.00m		
GROUND ELEVATION (FH)	3.65		3.65	3.65		3.50	3.65	3.65	
COVERING DEPTH	6.81		8.19	8.31	8.91	10.56	10.55	11.06	12.76
INVERT ELEVATION	-3.626		-5.006	-5.126	-5.738	-7.519	-7.619	-7.976	-9.683
ACCUMULATED	2861.00		3436.00	3486.00	3741.00	4483.00	4693.00		5697.00



NAME OF DRAWINGS	PROFILE OF MAIN SEWER (2/2)	SCALE: A1 V=1/100 H=1/5000 A3 V=1/200 H=1/10000
DESIGNED BY	JICA SURVEY TEAM	

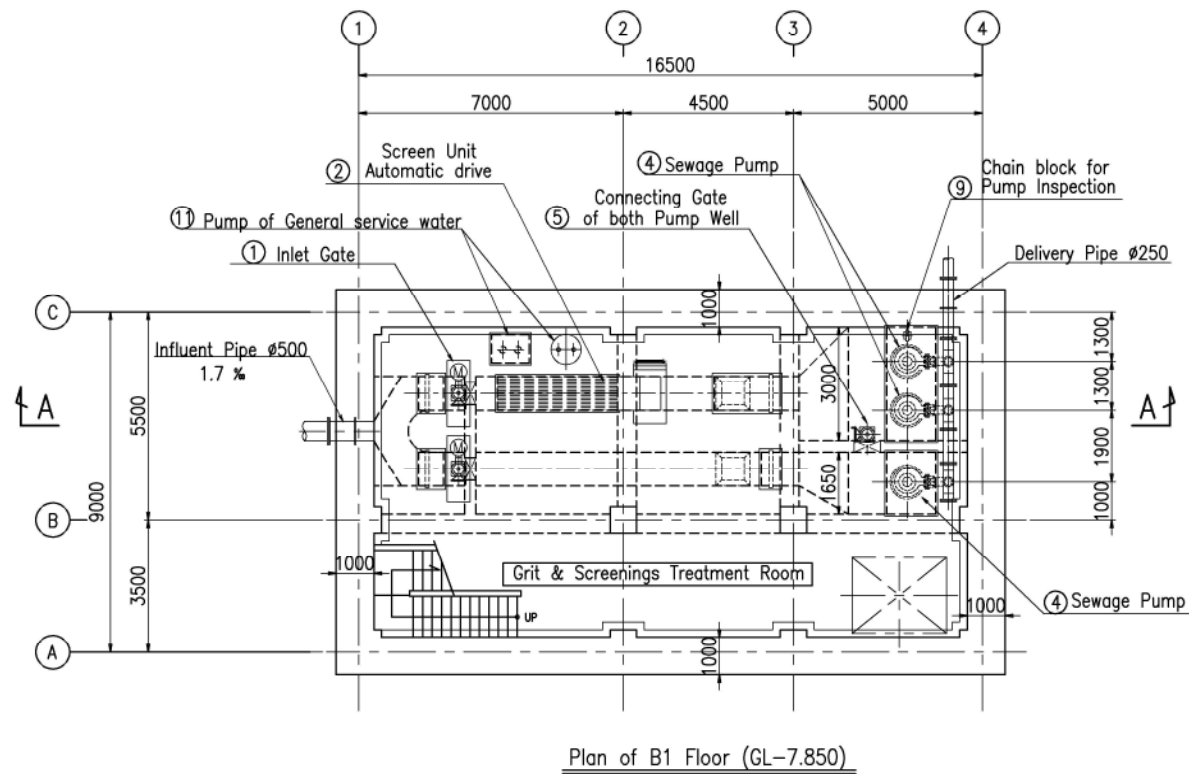
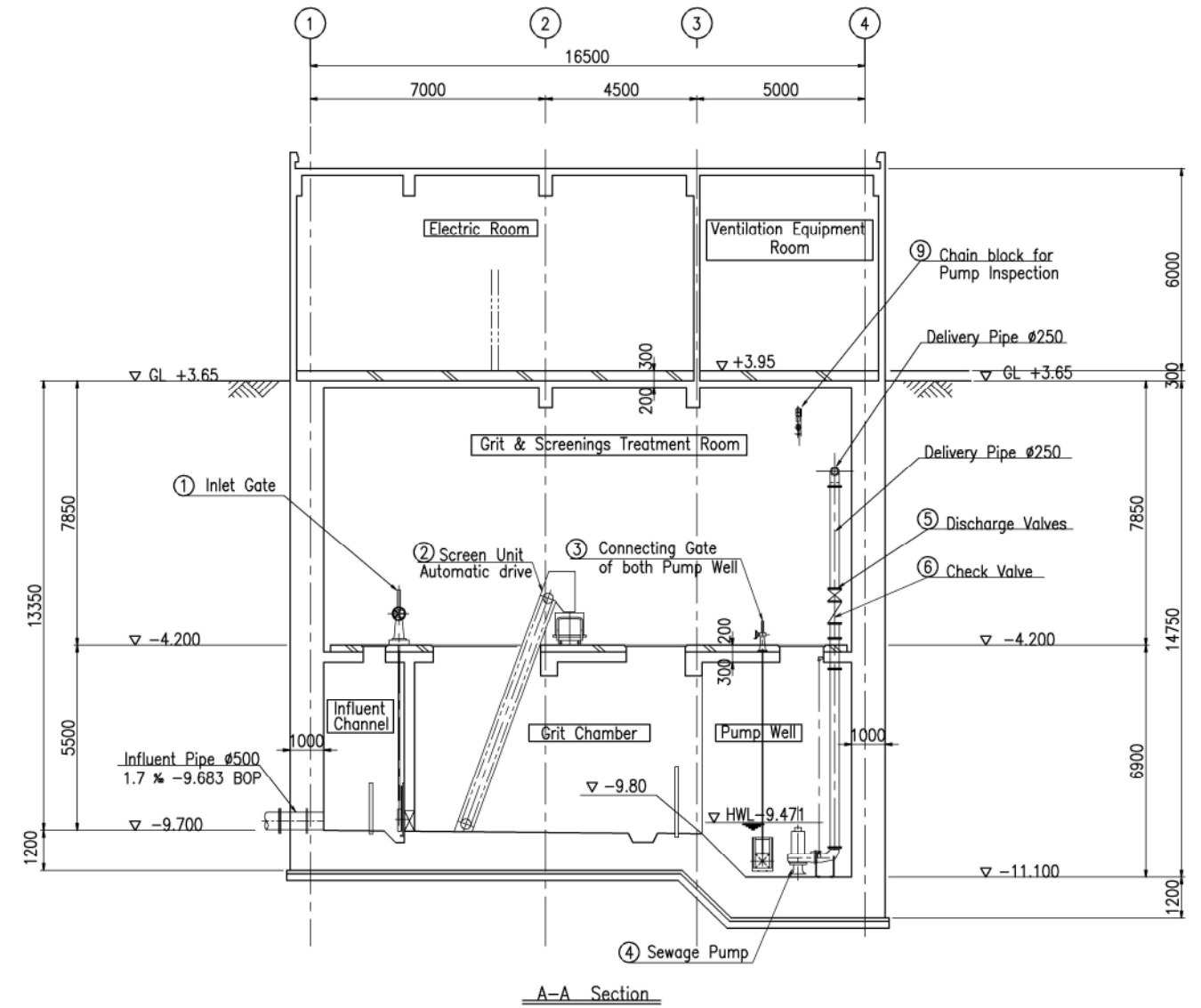
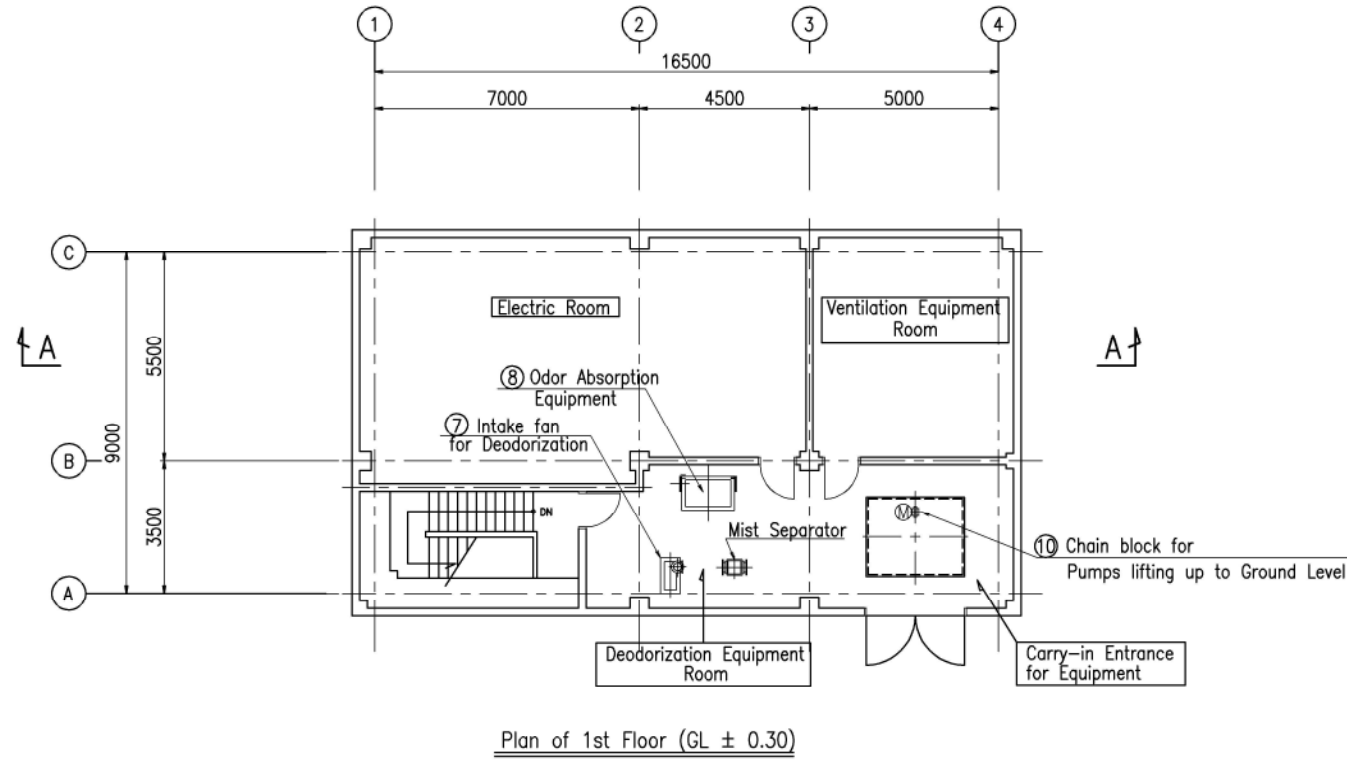


NAME OF DRAWINGS	GENERAL LAYOUT	SCALE:
DESIGNED BY	JICA SURVEY TEAM	



NAME OF DRAWINGS	HYDRAULIC PROFILE	SCALE: A1 V=1:60 H=NTS A3 V=1:120 H=NTS
DESIGNED BY	JICA SURVEY TEAM	

Raw Water Pump Pit

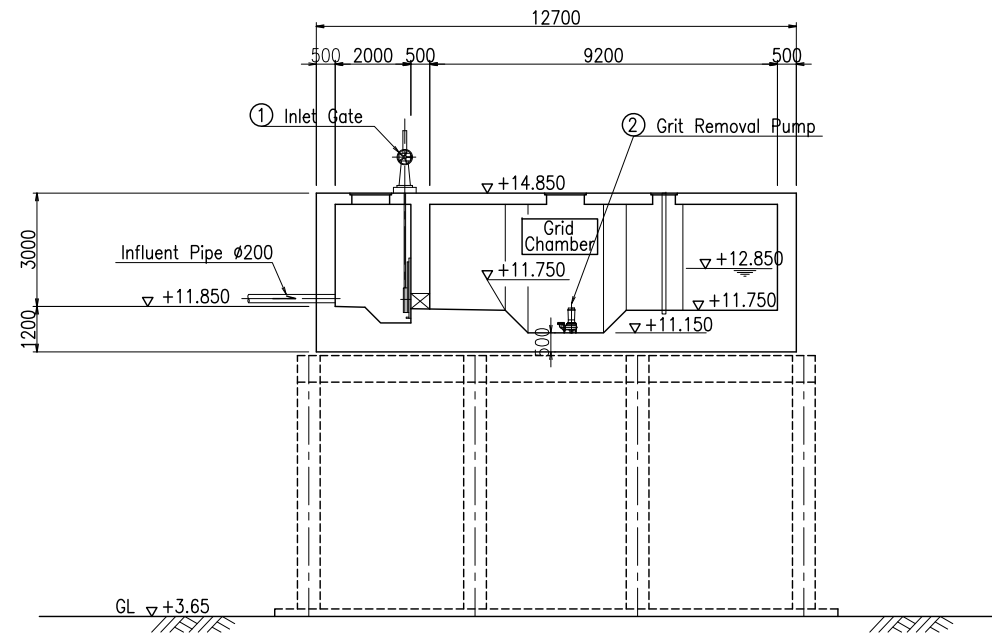


No.	①	②	③	④	⑤	⑥
Equipment	Inlet Gate	Screen Unit of Automatic drive	Connecting Gate of both Pump Well	Sewage Pump	Discharge Valves	Check Valve
Specification	Cast iron made, Motor drive type	Motor Drive	Cast iron made, Manual drive type	Submersible Pump with Screw blade suction type	Manual operation	Swing model
Model, Size & Capacity	B:400mmxH:400mm	Water course B:900mmxD:5.7m x Screen opening Size:25mm	W:500mmxH:500mm	φ200x4.0m ³ /minx25m	φ200	φ200
Motor Power(kW)	0.75	0.4		30 : 2units (30 : 1unit)		
Unit	Future 2, First Stage -	Future 1, First Stage -	Future 1, First Stage -	Future 3(1), First Stage 2(1)	Future 3, First Stage -	Future 3, First Stage -
Remarks						
No.	⑦	⑧	⑨	⑩	⑪	
Equipment	Intake fan for Deodorization	Odor Absorption Equipment	Chain block for Pump Inspection	Chain block for Pumps lifting up to Ground Level	Pump of General service water	
Specification	Turbo fan Single Suction Type	Upright model, Dry filter	Manual	Motor Drive Chain block	Automatic supply unit	
Model, Size & Capacity	10m ³ /min	10m ³ /min	Lift capacity: 0.5t	Lifting Capacity: 1.0t	1m ³	
Motor Power(kW)	0.75	-		0.8	1.5x2	
Unit	Future 1, First Stage -	Future 1, First Stage -	Future 1, First Stage -	Future 1, First Stage -	Future 1, First Stage -	
Remarks						

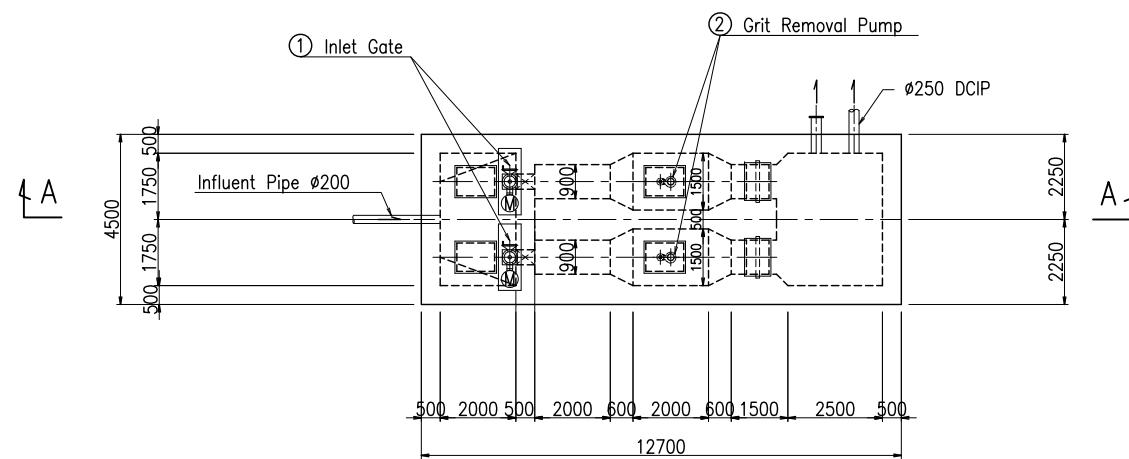
Notes:

- 1. () : Stand-by
- 2. First Stage : Up to 2030
Future : Year after 2035

NAME OF DRAWINGS	RAW WATER PUMP PIT	SCALE:	A1 1:100 A3 1:200
DESIGNED BY	JICA SURVEY TEAM		



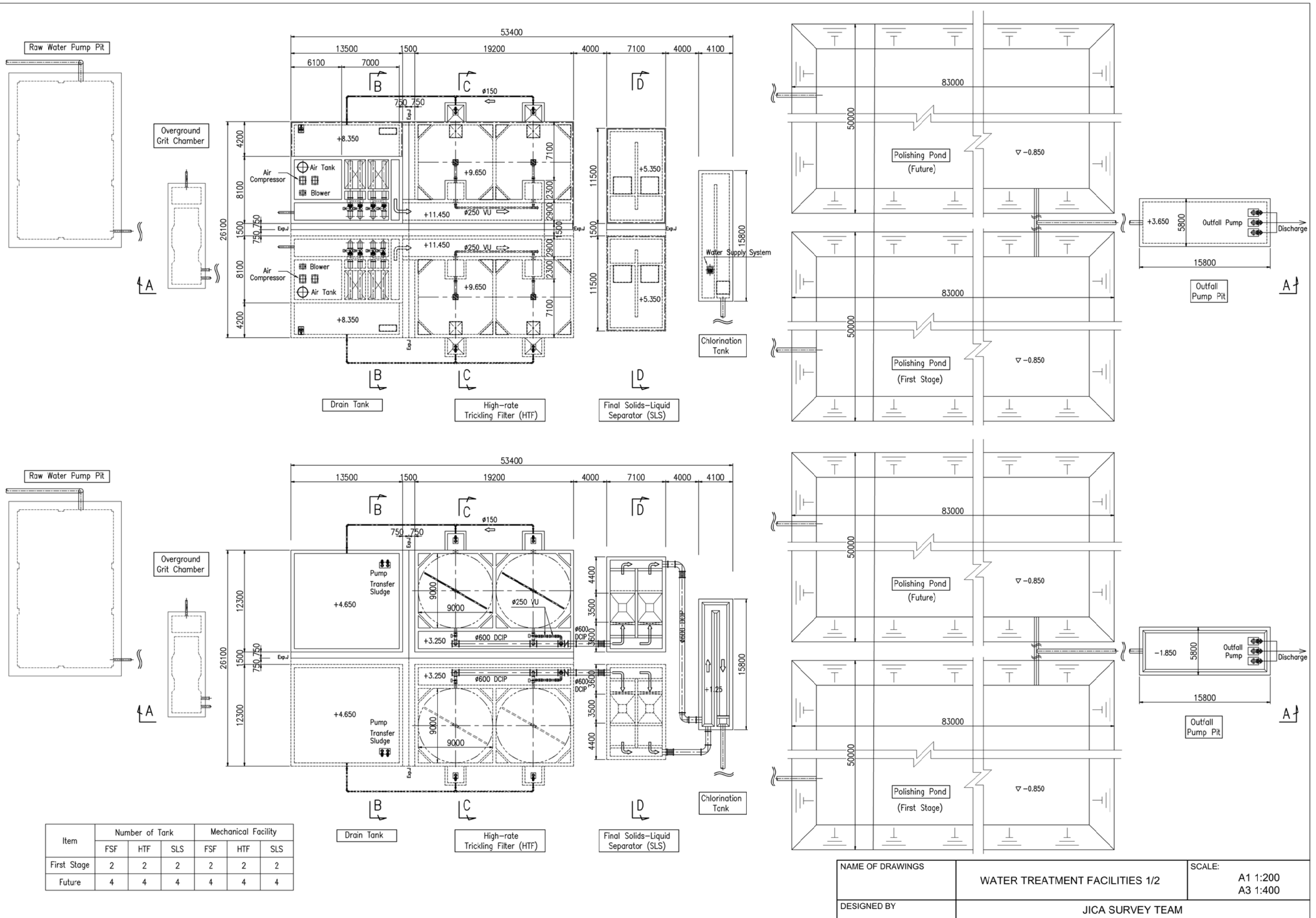
A - A SECTION



PLAN

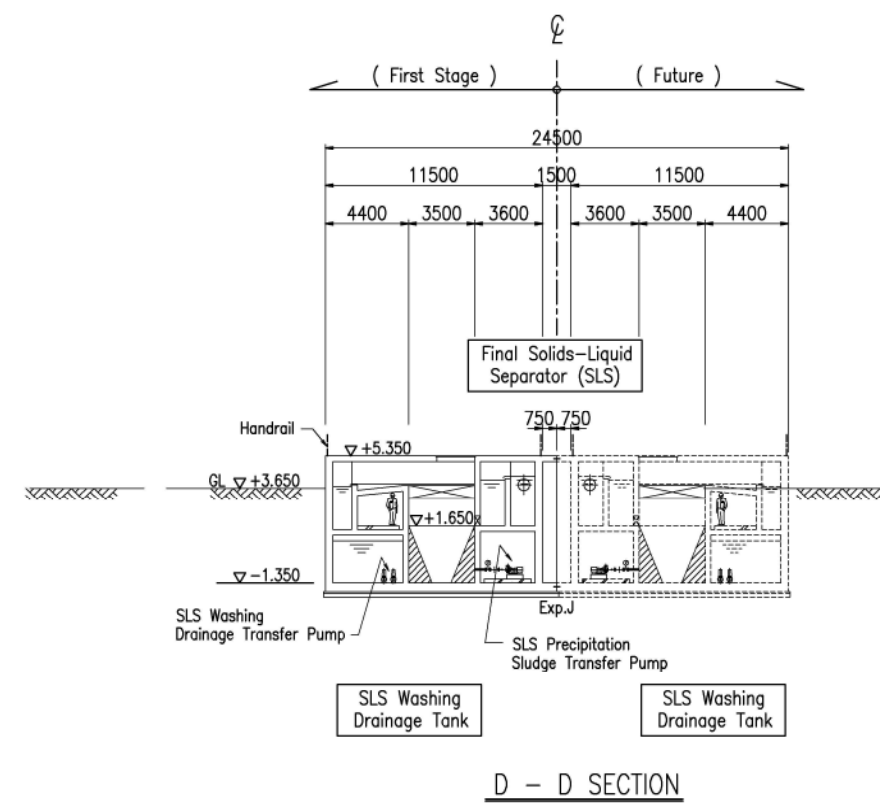
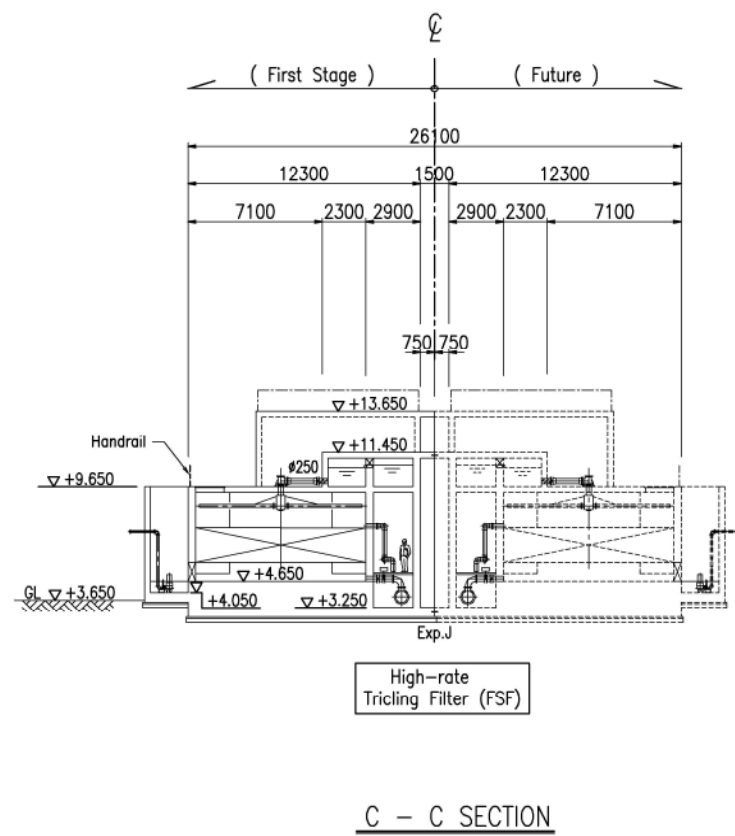
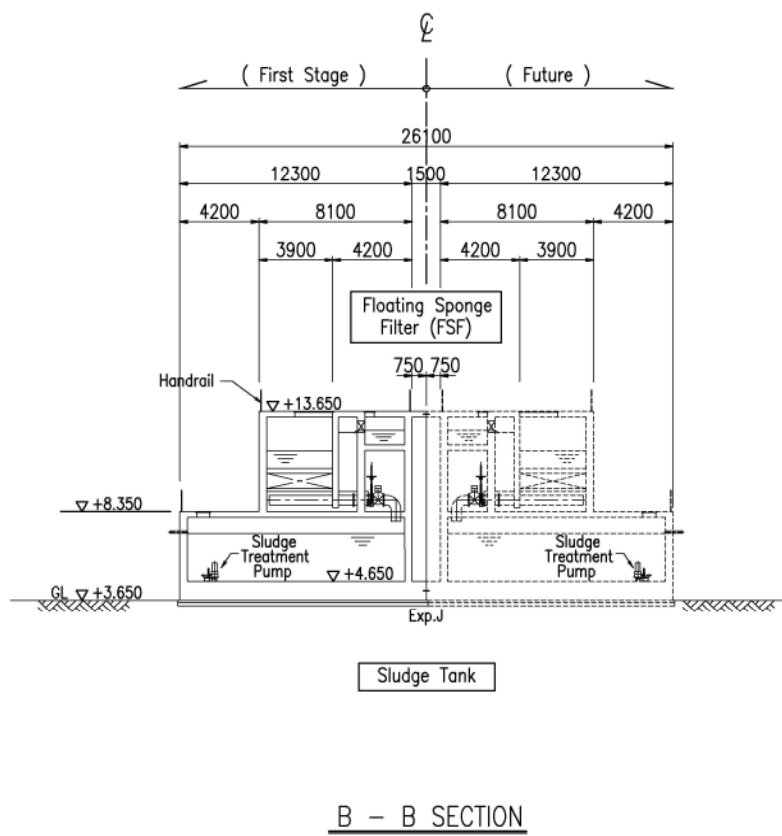
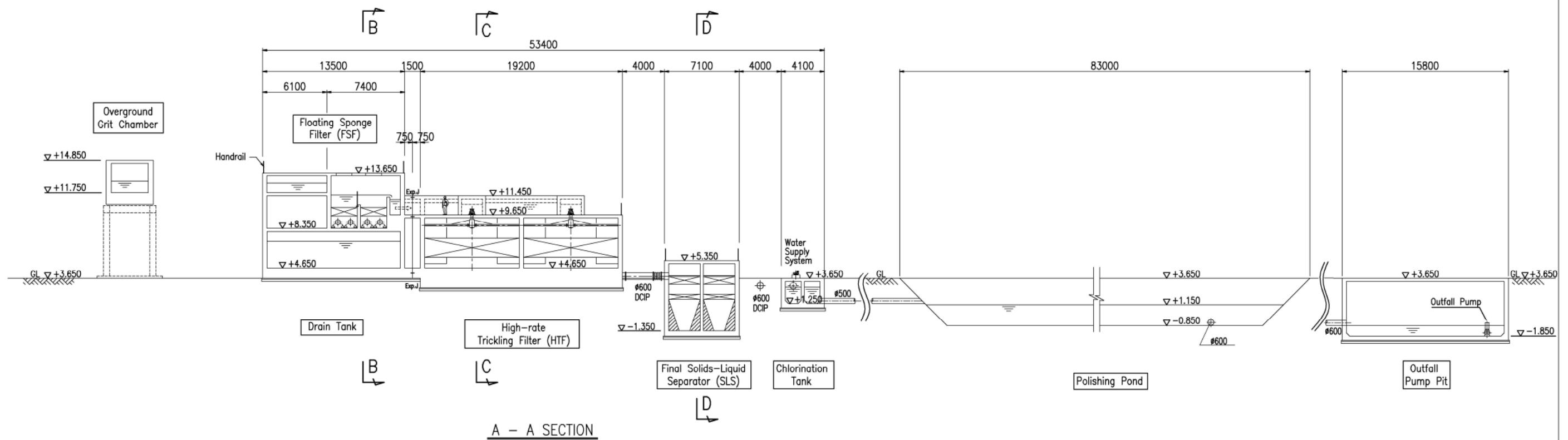
No.	①	②	
Equipment	Inlet Gate	Grit Removal Pump	
Specification	Cast iron made, Motor drive type	Sand Pump	
Model, Size & Capacity	B:400mmxH:400mm	ø100x0.5m ³ /minx15m	
Motor Power(kW)	0.75	-	
Unit	2	2	
Remarks			

NAME OF DRAWINGS	OVERGROUND GRIT CAMBER	SCALE: A1 1:100 A3 1:200
DESIGNED BY	JICA SURVEY TEAM	

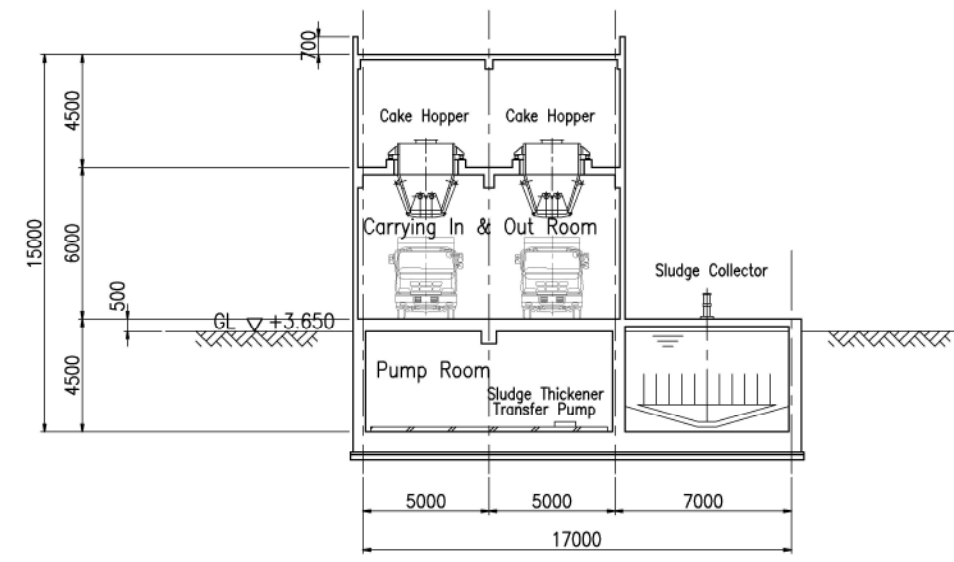
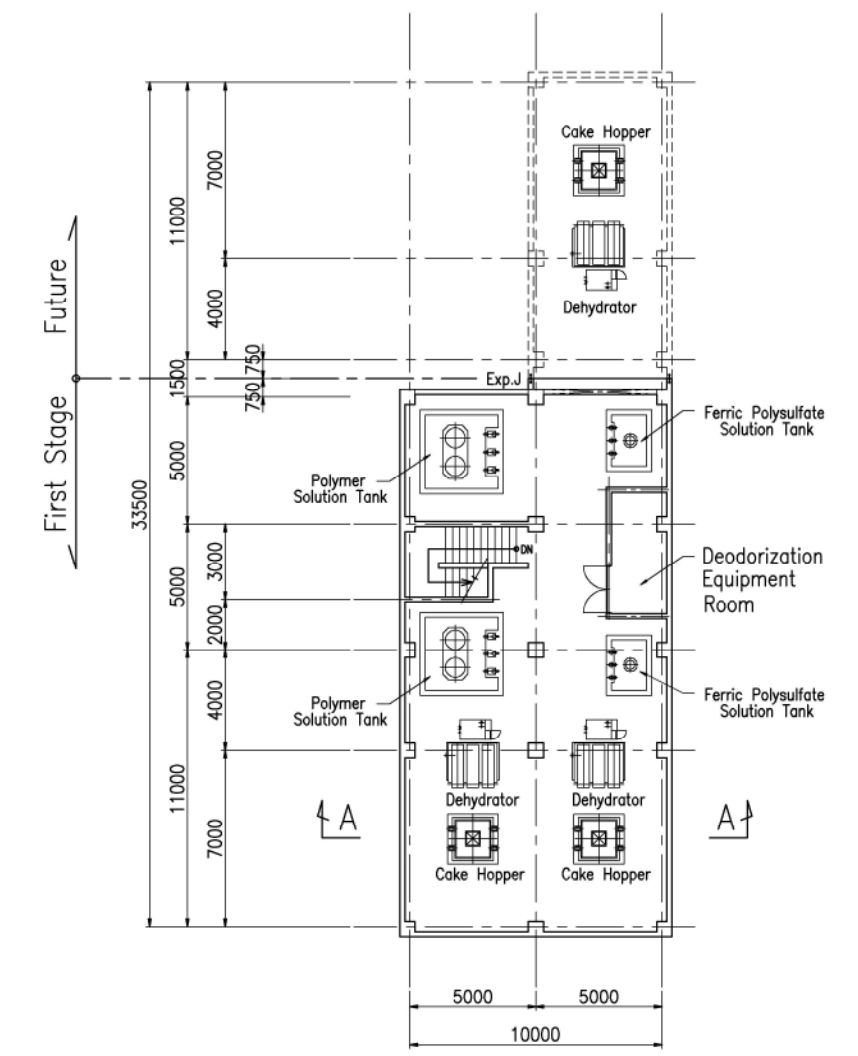
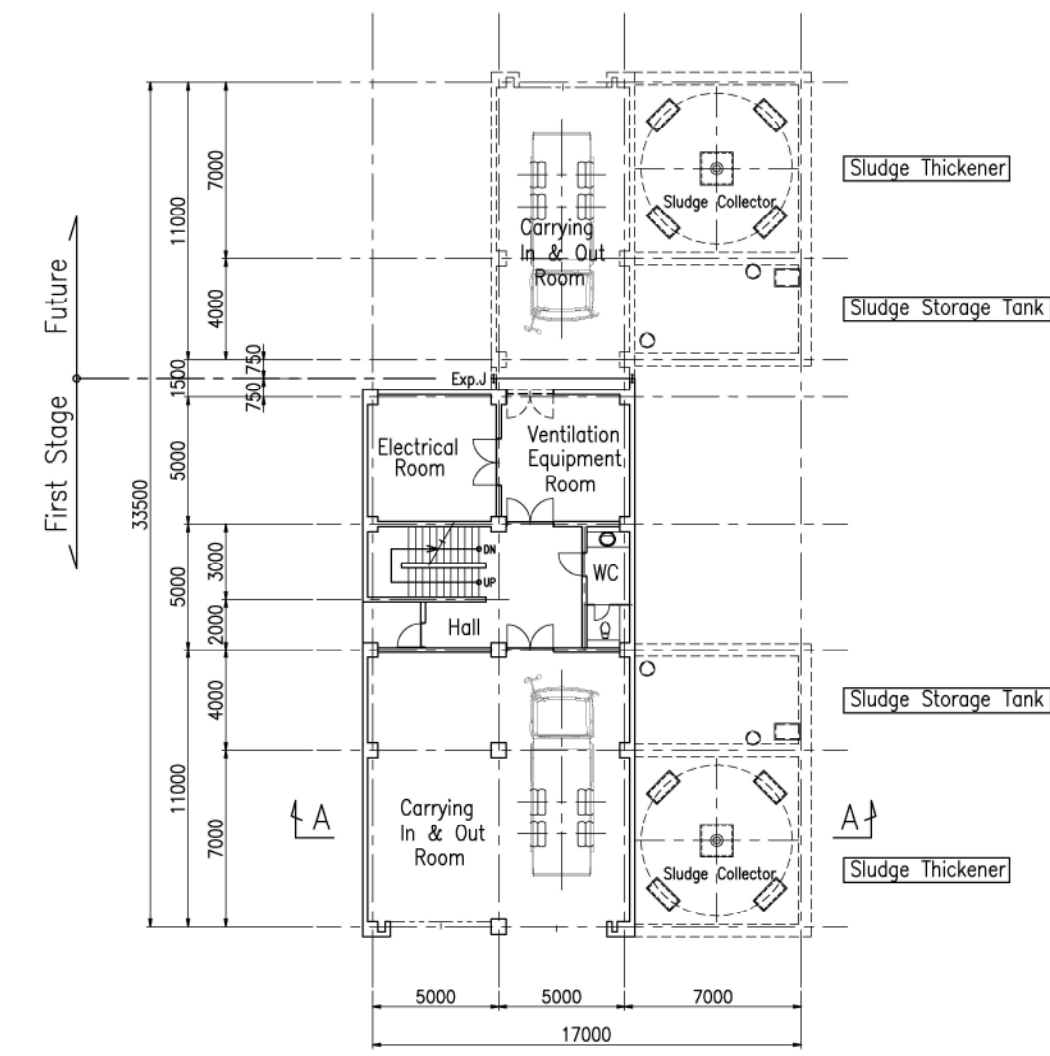
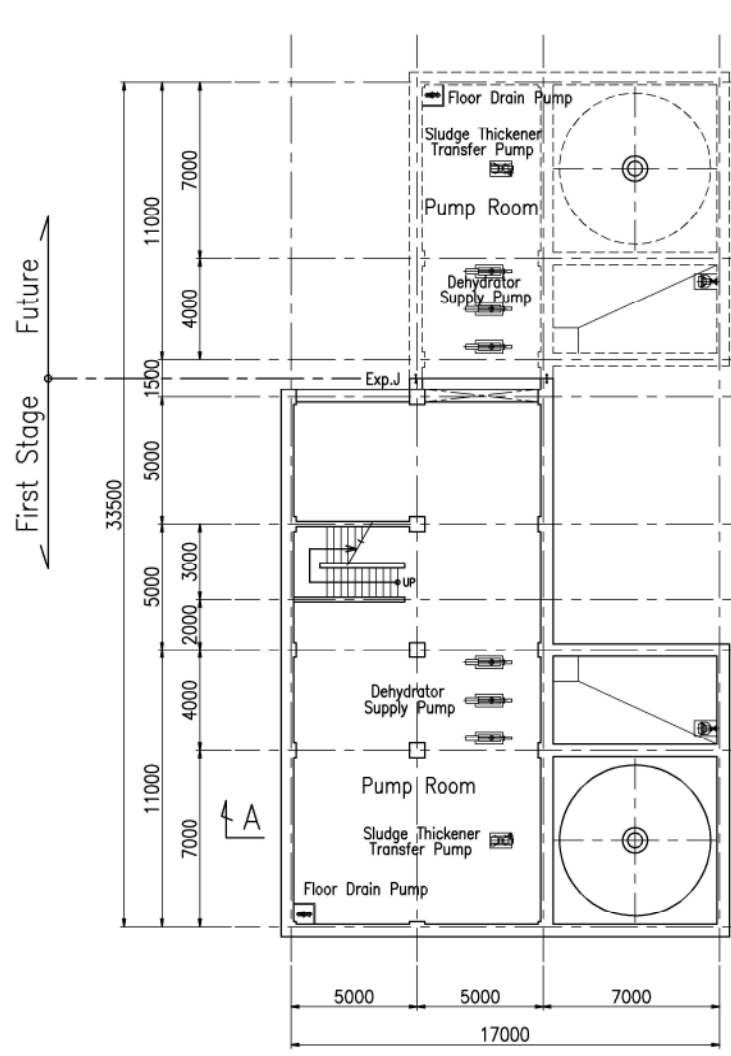


Item	Number of Tank			Mechanical Facility		
	FSF	HTF	SLS	FSF	HTF	SLS
First Stage	2	2	2	2	2	2
Future	4	4	4	4	4	4

NAME OF DRAWINGS	WATER TREATMENT FACILITIES 1/2	SCALE:
DESIGNED BY	JICA SURVEY TEAM	A1 1:200 A3 1:400



NAME OF DRAWINGS	WATER TREATMENT FACILITIES 2/2	SCALE:
DESIGNED BY	JICA SURVEY TEAM	A1 1:200 A3 1:400



NAME OF DRAWINGS	SLUDGE TREATMENT BUILDING	SCALE: A1 1:150 A3 1:300
DESIGNED BY	JICA SURVEY TEAM	

7. Cost Breakdown (Sewerage Sector)

(1) Cost Breakdown (Sewer)

1) Summary of Direct Cost

	Quantity	Unit	Unit Price		Cost				Total			
			Foreign	Local	Foreign		Local		JPY	VND		
			JPY	VND	JPY	VND	(JPY)	(VND)	JPY	VND		
D300-OC		m										
H<=3.0m	4,583	m	0	6,850,000	0	31,393,550,000	149,433,298		149,433,298		149,433,298	31,393,550,000
H > 3.0m	9,972	m	0	22,825,472	0	227,615,604,631	1,083,450,278		1,083,450,278		1,083,450,278	227,615,604,631
Manhole(OC)	522	set	0	93,480,000	0	48,796,560,000	232,271,626		232,271,626		232,271,626	48,796,560,000
Manhole(DC)	12	set	0	130,870,000	0	1,570,440,000	7,475,294		7,475,294		7,475,294	1,570,440,000
D300-PJ	902	m	64,440	9,318,872	58,124,880	8,405,622,544	40,010,763		98,135,643		98,135,643	20,616,731,788
D400-PJ	2,605	m	76,500	11,062,907	199,282,500	28,818,871,433	137,177,828		336,460,328		336,460,328	70,684,942,861
D500-PJ	1,214	m	88,560	12,806,941	107,511,840	15,547,626,374	74,006,702		181,518,542		181,518,542	38,134,147,382
Shaft(PJ)	36	set	0	529,480,000	0	19,061,280,000	90,731,693		90,731,693		90,731,693	19,061,280,000
Manhole(PJ)	36	set	0	295,590,000	0	10,641,240,000	50,652,302		50,652,302		50,652,302	10,641,240,000
Pump Station	1	L.S	0	1,390,650,000	0	1,390,650,000	6,619,494		6,619,494		6,619,494	1,390,650,000
Total	19,276	m			364,919,220	393,241,444,981	1,871,829,278		2,236,748,498		2,236,748,498	469,905,146,662

2) Cost Breakdown

Table of Contents

D300-(OC: Open-Cut)	
H <= 3.0m	Page 1
H > 3.0m	Page 5
Manhole (OC: Open-Cut)	Page 6
Manhole (DC: Diversion Chamber)	Page 11
D300-PJ (Pipe Jacking)	Page 16
D400-PJ (Pipe Jacking)	Intermediate value of D300 and D500
D500-PJ (Pipe Jacking)	Page 16
Shaft (PJ) (Pipe Jacking)	Page 17
Manhole (PJ) (Pipe Jacking)	Page 20
Pump Station	Page 24

SUMMARY CONSTRUCTION COST ESTIMATES
PROJECT: INVESTMENT CLIMATE IMPROVEMENT PROJECT IN HA NAM PROVINCE

ITEM: PIPE D315 - HTMB

No.	Item	Code	Formula	Cost
I	DIRECT COST			
0	<i>Technology section</i>			920,000.0
1	<i>Materials</i>	VL	A	1,299,176.0
	+ Based on direct unit cost	A1	Cost calculation sheet	1,236,976.0
	+ Difference of materials	CL	Cost compensation sheet	62,200.0
	Sub-Total	A	A1 + CL	1,299,176.0
2	<i>Man Power</i>	NC	NC1	1,231,133.0
	+ Based on direct unit cost	B1	Cost calculation sheet	1,383,296.0
	Multiple with a factor specified for construction man power	NC1	B1 x 0,89	1,231,133.4
3	<i>Construction Equipment</i>	M	C	3,396,607.0
	+ Based on direct unit cost	C1	Cost calculation sheet	3,744,260.0
	+ Difference of equipment	CLMay	Cost compensation sheet	-347,653.0
	Sub-Total	C	C1 + CLMay	3,396,607.0
	Total of Direct Cost	T	VL + NC + M	6,846,916.0

COST ESTIMATE OF WORK ITEMS

STRENGTHENING THE ENVIRONMENTAL INVESTMENT OF HA NAM PROVINCE

DRAINAGE PIPE D315 - HTMB

NO.	Code	Work name / Quantity description	Unit	Quantity	Unit Price			Amount					
					Material	Labor	Machinery	Material	V.L.phu	Labor	Machinery		
		DRAINAGE PIPE D315 - HTMB											
1	AL.22111 HM	Groove cutting, the yard is casted by dry cutting method, groove 1x4	10m	0.220	226,659.0	120,601.0	61,767.0	49,865.0	0.0	26,532.2	13,588.7		
2	AA.22415	Removal of road asphalt concrete pavement, removed thickness <= 7 cm	100m2	0.010	215,050.0	775,015.0	3,000,840.0	2,172.0	0.0	7,827.7	30,308.5		
3	AB.25114	Foundation excavation, foundation width <=6 m, by excavator <=0.8 m3, soil grade IV	100m3	0.004		1,640,369.0	1,717,355.0	0.0	0.0	5,741.3	6,010.7		
4	AB.41414	Soil hauling by dump truck, distance <=1000m, 5T truck, soil grade IV	100m3	0.004			2,416,827.0	0.0	0.0	0.0	10,392.4		
5	AB.42314	Subsequent soil hauling distance of <=7 km by 5T dump truck, soil grade IV	100m3	0.004			3,753,192.0	0.0	0.0	0.0	16,138.7		
6	TT	Formed steel pile depreciation (I200x110x5)	ton	0.028	14,700,000.0			410,130.0	0.0	0.0	0.0		
7	AC.22512	Formed steel pile driving (U, J shape) height >100 mm on the ground, pile length <=10 m, soil grade II	100m	0.264		1,105,814.0	7,021,822.0	0.0	0.0	291,934.9	1,853,761.0		
8	AC.23110	Formed steel pile extraction, soil retaining wall by steel pipes, working platform on the ground	100m	0.264		628,518.0	4,548,706.0	0.0	0.0	165,928.8	1,200,858.4		
9	AI.11221	Fabrication of steel bracing	ton	0.000	16,436,654.0	1,539,310.0		6,574.7	0.0	615.7	0.0		
10	AI.61131	Erection of steel bracing	ton	0.038	522,878.0	957,793.6	2,440,009.6	19,660.2	0.0	36,013.0	91,744.4		
11	TT	Depreciation of 10mm thick steel plate	ton	0.006	15,636,000.0			87,561.6	0.0	0.0	0.0		
12	AC.11710 -VD	Construction of soil retaining wall by steel plates	100m2	0.062			8,990,275.2	0.0	0.0	553,801.0	0.0		
13	AB.11622	Soil excavation to install pipeline, cable line without creating slope, soil grade II	m3	0.238			331,105.0	0.0	0.0	78,968.5	0.0		

NO.	Code		Work name / Quantity description	Unit	Quantity	Unit Price			Amount								
	Unit price	Material				Labor	Machinery	Material	V.L.phy	Labor	Machinery						
			<i>Minus destruction quantity:</i>														
			-0.043296														
14	AB.25112		Foundation excavation, foundation width <=6 m, by excavator <=0.8 m3, soil grade II	100m3	0.021			1,235,839.0		1,059,463.0	0.0	0.0	26,570.5				22,778.5
15	AB.66143		Sand filling by tamper, required compactness K=0,95	100m3	0.002		11,590,000.0	968,849.0		918,884.0	23,180.0	0.0	1,937.7				1,837.8
16	AB.13412		Sand filling for pipeline, drain pipe	m3	0.033		118,218.0	117,314.0			3,924.8	0.0	3,894.8				0.0
17	AB.66142		Sand filling by tamper, required compactness K=0,90	100m3	0.003		11,590,000.0	938,510.0		863,081.0	34,770.0	0.0	2,815.5				2,589.2
18	AB.65120		Sand filling by tamper, required compactness K=0,90	100m3	0.017			2,088,759.0		1,620,018.0	0.0	0.0	34,673.4				26,892.3
19	AB.41412		Soil hauling by dump truck, distance <=1000m, 5T ruck, soil grade II	100m3	0.007					1,890,812.0	0.0	0.0	0.0				13,613.8
20	AB.42312		Subsequent soil hauling distance of 4 km by 5T dump truck, soil grade II	100m3	0.007					3,036,672.0	0.0	0.0	0.0				21,864.0
			<i>Return</i>														
21	AD.11211		Construction of macadam sub-base course, road expansion	100m3	0.002		24,424,000.0	992,397.0		3,336,509.0	53,732.8	0.0	2,183.3				7,340.3
22	AD.11221		Construction of macadam base course, road expansion	100m3	0.002		24,424,000.0	1,086,911.0		3,241,313.0	53,732.8	0.0	2,391.2				7,130.9
23	AD.23225		Laying asphalt concrete pavement, medium size aggregate asphalt concrete, compacted thickness 7 cm	100m2	0.010			602,527.0		623,689.0	0.0	0.0	6,085.5				6,299.3
24	AD.26222		Manufacturing of medium size aggregate asphalt concrete at 50-60 ton/h batching	100 ton	0.002		117,672,450.0	1,291,994.0		7,973,598.0	200,043.2	0.0	2,196.4				13,555.1
25	AD.24213		Spraying bituminous oil as binding course at 1,0 kg bitumen/m2	100m2	0.010		1,872,822.0	68,852.0		413,769.0	18,915.5	0.0	695.4				4,179.1
26	AD.23233		Laying asphalt concrete pavement, fine aggregate asphalt concrete, compacted thickness 5 cm	100m2	0.010			437,127.0		528,895.0	0.0	0.0	4,415.0				5,341.8
27	AD.26223		Manufacturing of fine aggregate asphalt concrete at 50-60 ton/h batching plant	100 ton	0.001		126,523,695.0	1,353,517.0		7,973,598.0	151,828.4	0.0	1,624.2				9,568.3
			<i>0,1115/100 = 0,0011</i>														
28	AD.24211		Spraying of binding course by bituminous oil at 0,5 kg bitumen/m2	100m2	0.010		834,867.0	68,852.0		413,769.0	8,432.2	0.0	695.4				4,179.1

NO.	Code		Work name / Quantity description	Unit	Quantity	Unit Price			Amount					
	Unit price					Material	Labor	Machinery	Material	V.L.phy	Labor	Machinery		
29	AD.27243		Hauling of black macadam, asphalt concrete from batching plant to site at 4km distance by 12 ton truck	100 ton	0.003						0.0	0.0	0.0	15,656.4
30	AD.27253		Hauling of black macadam, asphalt concrete from batching plant to the site, subsequent 1km, 12 ton truck	100 ton	0.003						0.0	0.0	0.0	18,243.7
31	TT		Other works		0.100	1,124,523.2	1,257,541.4	3,403,872.4			112,452.3	0.0	125,754.1	340,387.2
	THM		TOTAL: DRAINAGE PIPE D315 - HTMB								1,236,976	0.0	1,383,296	3,744,260

1. Installation cost of sewer pipe with DN 300 mm of open cut area

No	Quantity	Unit	Unit Price (JPY)		Cost (JPY)		Total	
			Foreign JPY	Local VND	Foreign JPY	Local VND	JPY	VND
1-1	1.22	m3		403,460	0	493,835	2,329	493,835
1-2	5.18	m3		28,197	0	146,174	689	146,174
1-3	1.08	m3		438,201	0	473,257	2,232	473,257
1-4	3.35	m3		164,230	0	550,005	2,594	550,005
1-5	0.81	m3		52,043	0	42,155	199	42,155
1-6	1.05	m3		225,427	0	237,375	1,120	237,375
1-7	0.32	m3		686,831	0	222,533	1,050	222,533
1-9	1.62	m2		11,771	0	19,069	90	19,069
1-10	1.62	m2		16,054	0	26,007	123	26,007
1-11	1.62	m2		14,942	0	24,206	114	24,206
1-12	1.62	m2		28,702	0	46,497	219	46,497
1-13	0.19	Ton		1,641,656	0	304,199	1,435	304,199
1-14	0.25	Ton		1,533,333	0	389,697	1,838	389,697
1-15	0.47	Ton		65,785	0	30,610	144	30,610
1-16	2.79	Ton		6,969	0	19,455	92	19,455
1-17	1.00	m		10,581	0	10,581	50	10,581
1-18	0.07	m3		1,155,277	0	83,180	392	83,180
1-19	0.05	m3		716,739	0	32,253	152	32,253
1-20	23.40	m		11,211	0	262,329	1,237	262,329
1-21	40.00	m		336,039	0	13,441,565	63,404	13,441,565
1-22	40.00	m		144,562	0	5,782,479	27,276	5,782,479
1-23	6.48	m3		21,025	0	136,241	643	136,241
1-24	6.48	m3		7,989	0	51,772	244	51,772
1-25	Total (Installation cost of DN 300 mm pipe per meter)				0	22,825,472	107,667	22,825,472

SUMMARY CONSTRUCTION COST ESTIMATES
PROJECT: INVESTMENT CLIMATE IMPROVEMENT PROJECT IN HA NAM PROVINCE

ITEM: MANHOLE TYPE-1

No.	Item	Code	Formula	Cost
I	DIRECT COST			
1	<i>Materials</i>	<i>VL</i>	A	45,004,684.0
	+ Based on direct unit cost	A1	Cost calculation sheet	42,731,766.0
	+ Difference of materials	CL	Cost compensation sheet	2,272,918.0
	Sub-Total	A	A1 + CL	45,004,684.0
2	<i>Man Power</i>	NC	NC1	19,572,099.0
	+ Based on direct unit cost	B1	Cost calculation sheet	21,991,122.0
	Multiple with a factor specified for construction man power	NC1	B1 x 0,89	19,572,098.6
3	<i>Construction Equipment</i>	M	C	28,903,529.0
	+ Based on direct unit cost	C1	Cost calculation sheet	31,172,543.0
	+ Difference of equipment	CLMay	Cost compensation sheet	-2,269,014.0
	Sub-Total	C	C1 + CLMay	28,903,529.0
	Total of Direct Cost	T	VL + NC + M	93,480,312.0

COST ESTIMATE OF WORK ITEMS
STRENGTHENING THE ENVIRONMENTAL INVESTMENT OF HA NAM PROVINCE

TYPE 1 MANHOLE

NO.	Code Unit price HM	Work name / Quantity description	Unit	Quantity	Unit Price			Amount		
					Material	Labor	Machinery	Material	Labor	Machinery
1	AL.22111	TYPE 1 MANHOLE Groove cutting, the yard is casted by dry cutting method, groove 1x4	10m	1.5616	226,659.0	120,601.0	61,767.0	353,950.7	188,330.5	96,455.3
2	AA.22415	Removal of road asphalt concrete pavement, removed thickness <=7 cm	100m2	0.1249	215,050.0	775,015.0	3,000,840.0	26,859.7	96,799.4	374,804.9
3	AB.25114	Foundation excavation, foundation width <=6 m, by excavator <=0,8 m3, soil grade IV	100m3	0.0437		1,640,369.0	1,717,355.0	0.0	71,684.1	75,048.4
4	AB.41414	Soil hauling by dump truck, distance <=1000m, 5T truck, soil grade IV	100m3	0.0537			2,416,827.0	0.0	0.0	129,783.6
5	AB.42314	Subsequent soil hauling distance of <=7 km by 5T dump truck, soil grade IV	100m3	0.0537			3,753,192.0	0.0	0.0	201,546.4
6	TT	Formed steel pile depreciation (I200x110x5)	tán	0.1986	14,700,000.0			2,919,420.0	0.0	0.0
7	AC.22512	Formed steel pile driving (U, I shape) height >100 mm on the ground, pile length <=10 m, soil grade II	100m	1.8739		1,105,814.0	7,021,822.0	0.0	2,072,184.9	13,158,192.2
8	AC.23110	Formed steel pile extraction, soil retaining wall by steel pipes, working platform on the ground	100m	1.8739		628,518.0	4,548,706.0	0.0	1,177,779.9	8,523,820.2
9	AI.11221	Fabrication of steel bracing	ton	0.0066	16,436,654.0	1,539,310.0		108,481.9	10,159.4	0.0
10	AI.61131	Erection of steel bracing	ton	0.5631	522,878.0	957,793.6	2,440,009.6	294,432.6	539,333.6	1,373,969.4

NO.	Code	Work name / Quantity description	Unit	Quantity	Unit Price			Amount			
					Material	Labor	Machinery	Material	Labor	Machinery	
11	TT	Depreciation of 10mm thick steel plate	ton	0.0388	15,636,000.0				606,676.8	0.0	0.0
12	AC.11710 -VD	Construction of soil retaining wall by steel plates	100m2	0.5153					0.0	4,632,688.8	0.0
13	AB.11442	Excavation of column, pier foundation, manhole, width >1 m, depth >1 m, soil	m3	4.1226					0.0	867,213.6	0.0
14	AB.25112	Foundation excavation, foundation width <=6 m, by excavator <=0,8 m3, soil grade II	100m3	0.3710					0.0	458,496.3	393,060.8
15	AB.13412	Sand filling for pipeline, drain pipe	m3	0.8918	118,218.0				105,426.8	104,620.6	0.0
16	AB.66142	Sand filling by tamper, required compactness K=0,90	100m3	0.0803	11,590,000.0				930,677.0	75,362.4	69,305.4
17	AB.65120	Sand filling by tamper, required compactness K=0,90	100m3	0.2047					0.0	427,569.0	331,617.7
18	AB.41412	Soil hauling by dump truck, distance <=1000m, 5T truck, soil grade II	100m3	0.2075					0.0	0.0	392,343.5
19	AB.42312	Subsequent soil hauling distance of 4 km by 5T dump truck, soil grade II	100m3	0.2075					0.0	0.0	630,109.4
20	AF.11111	Concrete manufacturing by mixer - manual casting, foundation lining concrete, 4x6 aggregate, width <=250 cm, grade 100	m3	0.7027	551,165.0				387,303.6	201,826.7	35,391.5
21	AF.31115	Concrete manufactured at site batching plant or commercial concrete, casted by pump, foundation concrete, foundation width <=250 cm, M300	m3	1.7714	1,024,817.0				1,815,360.8	304,547.9	164,086.6
22	AF.82511	Formwork for cast-in-place concrete, formwork for long foundation	100m2	0.0322	1,449,697.0				46,680.2	93,202.6	0.0

NO.	Code	Work name / Quantity description	Unit	Quantity	Unit Price			Amount		
					Material	Labor	Machinery	Material	Labor	Machinery
23	AF.61120	Fabrication and erection of rebar for cast-in-place concrete, foundation rebar, diameter <=18 mm	tán	0.2214	16,281,026.0	1,828,754.0	470,798.0	3,604,619.2	404,886.1	104,234.7
24	AF.32115	Concrete manufactured at site batching plant or commercial concrete, casted by pump, wall concrete, thickness <=45cm, height <=4m, grade 300	m3	5.4052	1,181,880.0	561,344.0	115,098.0	6,388,297.8	3,034,176.6	622,127.7
25	AF.82111	Formwork for cast-in-place concrete, metal formwork, wall formwork, square column, rectangular column, girder, bracing, height <=16 m	100m2	0.3680	3,243,995.0	9,044,990.0	637,657.0	1,193,790.2	3,328,556.3	234,657.8
26	AF.61321	Fabrication and erection of rebar for cast-in-place concrete, wall rebar, diameter <=18 mm, wall height <= 4 m	tán	0.6756	16,281,026.0	2,449,302.0	470,798.0	10,999,461.2	1,654,748.4	318,071.1
27	TT	Composite manhole cover plate	pce	1.0000	2,850,000.0			2,850,000.0	0.0	0.0
28	AG.42111	Installation of precast concrete structures, manual installation of precast concrete structures, weight <= 50 kg	pce	1.0000	2,509.0	35,443.0		2,509.0	35,443.0	0.0
29	AD.11211	Construction of macadam sub-base course, road expansion	100m3	0.0250	24,424,000.0	992,397.0	3,336,509.0	610,600.0	24,809.9	83,412.7
30	AD.11221	Construction of macadam base course, road expansion	100m3	0.0188	24,424,000.0	1,086,911.0	3,241,313.0	459,171.2	20,433.9	60,936.7
31	AD.23225	Laying asphalt concrete pavement, medium size aggregate asphalt concrete, compacted thickness 7 cm	100m2	0.1249		602,527.0	623,689.0	0.0	75,255.6	77,898.8
32	AD.26222	Manufacturing of medium size aggregate asphalt concrete at 50-60 ton/h batching	100 ton	0.0207	117,672,450.0	1,291,994.0	7,973,598.0	2,435,819.7	26,744.3	165,053.5

NO.	Code	Work name / Quantity description	Unit	Quantity	Unit Price			Amount		
					Material	Labor	Machinery	Material	Labor	Machinery
33	AD.24213	Spraying bituminous oil as binding course at 1,0 kg bitumen/m2	100m2	0.1249	1,872,822.0	68,852.0	413,769.0	233,915.5	8,599.6	51,679.7
34	AD.23233	Laying asphalt concrete pavement, fine aggregate asphalt concrete, compacted thickness 5 cm	100m2	0.1249		437,127.0	528,895.0	0.0	54,597.2	66,059.0
35	AD.26223	Manufacturing of fine aggregate asphalt concrete at 50-60 ton/h batching plant	100 ton	0.0190	126,523,695.0	1,353,517.0	7,973,598.0	2,403,950.2	25,716.8	151,498.4
36	AD.24211	Spraying bituminous oil as binding course at 0,5 kg bitumen/m2	100m2	0.1249	834,867.0	68,852.0	413,769.0	104,274.9	8,599.6	51,679.7
37	AD.27243	Hauling of black macadam, asphalt concrete from batching plant to the site, distance 4km, 12 ton truck	100 ton	0.0412			5,398,760.0	0.0	0.0	222,428.9
38	AD.27253	Hauling of black macadam, asphalt concrete from batching plant to the site, subsequent 1km, 12 ton truck	100 ton	0.0412			6,290,933.0	0.0	0.0	259,186.4
39	TT	Other works		0.1000	38,500,868.6	19,667,553.0	27,540,821.8	3,850,086.9	1,966,755.3	2,754,082.2
	THM	TOTAL: TYPE 1 MANHOLE						42,731,766	21,991,122	31,172,543

SUMMARY CONSTRUCTION COST
PROJECT: INVESTMENT CLIMATE IMPROVEMENT PROJECT IN HA NAM PROVINCE

Item: Diversion Chamber

No.	Item	Code	Formula	Cost
1	DIRECT COST			
1	<i>Materials</i>	<i>VL</i>	A	77,487,430
	+ Based on direct unit cost	A1	Cost calculation sheet	80,671,426
	+ Difference of materials	CL	Cost compensation sheet	-3,183,996
	Sub-Total	A	A1 + CL	77,487,430
2	<i>Man Power</i>	<i>NC</i>	NC1	34,862,931
	+ Based on direct unit cost	B1	Cost calculation sheet	39,171,832
	Multiple with a factor specified for construction man power	NC1	B1 x 0,89	34,862,931
3	<i>Construction Equipment</i>	<i>M</i>	C	18,522,925
	+ Based on direct unit cost	C1	Cost calculation sheet	21,653,980
	+ Difference of equipment	CLMay	Cost compensation sheet	-3,131,055
	Sub-Total	C	C1 + CLMay	18,522,925
	Total of Direct Cost	T	VL + NC + M	130,873,286

COST ESTIMATE OF WORK ITEMS
STRENGTHENING THE ENVIRONMENTAL INVESTMENT OF HA NAM PROVINCE

Diversion Chamber

NO.	Code Unit	Work name / Quantity description	Unit	Quantity	Unit Price			Amount			
					Material	Labor	Machinery	Material	Labor	Machinery	
		<i>DIVISION CHAMBER</i>									
		<i>Wooden pile</i>									
111	AC.22512	Driving formed steel pile >100mm on the ground, pile length <=10m, soil grade II (coefficient of material lost during construction 1,17%X 1 monthg+3,5%/driving or extraction=4,67% to be revised directly in the norm)	100m	1.195	1,062,191	1,105,814	7,021,822	1,268,893	1,321,005	8,388,269	
112	AC.23110	Extraction of formed steel pile, retaining wall made by steel pipe, construction of working platform on the ground	100m	1.195		628,518	4,548,706	0	750,828	5,433,884	
113	Al.11211	Fabrication of steel bracing (depreciation 1,17%) <i>Bracing strut I120:</i>	tán	0.023	17,231,969	3,179,488	350,007	403,228	74,400	8,190	
		<i>Steel plate:</i>									
114	Al.63311	Installation, removal of steel frame, working platform on the ground <i>Longitudinal bracing strut I120:</i>	tán	1.214	323,753	2,244,708	1,793,672	393,166	2,725,973	2,178,235	
115	AC.11710	Construction of diaphragm wall <i>Steel plate:</i>	100m2	0.451		8,990,275		0	4,054,614	0	
		<i>Demolishment</i>									
116	AA.21322	Demolishment of cement brick floor	m2	18.517		17,542		0	324,818	0	

NO.	Code Unit	Work name / Quantity description	Unit	Quantity	Unit Price			Amount		
					Material	Labor	Machinery	Material	Labor	Machinery
117	AB.41424	Soil hauling by 7T dump truck, distance <=1000m, soil grade IV	100m3	0.011			2,208,554	0	0	24,515
118	AB.42224	Subsequent soil hauling distance of <=4 km by 7T dump truck, soil grade IV (next 4km) <i>Excavation and filling</i>	100m3	0.011			3,174,796	0	0	35,240
119	AB.11443	Excavation for column, pier, manhole foundation, width >1 m, depth >1 m, soil	m3	14.385		305,420		0	4,393,375	0
120	AB.25123	Foundation excavation, foundation width <=6 m, by <=1,25 m3 excavator, soil grade III	100m3	0.336		1,512,942	1,253,993	0	507,743	420,840
121	AB.65130	Soil filling by tamper, required compactness K=0,95	100m3	0.227		2,405,381	1,865,587	0	546,022	423,488
122	AB.41423	Soil hauling by 7T dump truck, distance <=1000m, soil grade III	100m3	0.253			2,070,520	0	0	522,806
123	AB.42223	Subsequent soil hauling distance of <=4 km by 7T dump truck, soil grade III (next 4km) <i>Restoration</i>	100m3	0.253			2,898,728	0	0	731,929
124	AD.12121	Construction of cement reinforced yellow sand base course, batching plant 30 m3/h, 6% cement reinforced yellow sand	100m3	0.009	43,261,187	6,852,265	7,271,121	398,003	63,041	66,894
125	AK.55320	Pavement of yard, road base, sidewalk by interlocking brick, thickness 5.5 cm, fine sand cement mortar grade 75	m2	18.517	50,500	30,717		935,088	568,774	0
126	AC.11112	<i>Construction</i> Driving of <=2.5 m long bamboo pile	100m	5.335	525,321	394,695		2,802,588	2,105,698	0

NO.	Code Unit	Work name / Quantity description	Unit	Quantity	Unit Price			Amount		
					Material	Labor	Machinery	Material	Labor	Machinery
127	AK.98110	Construction of base lining stone course by Dmax <=4 stone	m2	2.668	238,500	349,702		636,199	932,830	0
128	AF.11121	Concrete manufacturing by mixer - manual casting, foundation lining concrete, 4x6 aggregate, width >250 cm, grade 100	m3	1.331	551,165	238,673	50,365	733,601	317,674	67,036
129	AF.11224	Concrete manufacturing by mixer - manual casting, foundation concrete, 1x2 aggregate, width >250 cm, grade 250	m3	3.210	860,197	398,462	50,657	2,761,232	1,279,063	162,609
130	AF.12124	Concrete manufacturing by mixer - manual casting, straight wall concrete, 1x2 aggregate, thickness <=45 cm, height <=16 m, grade 250	m3	6.644	968,708	925,341	116,964	6,436,096	6,147,966	777,109
131	AF.12414	Concrete manufacturing by mixer - manual casting, roof floor concrete, 1x2 aggregate, grade 250	m3	1.826	813,735	543,802	94,720	1,485,880	992,983	172,959
132	AF.81111	Formwork for cast-in-place concrete, wooden formwork, long foundation formwork, machine base	100m2	0.044	4,026,971	2,984,333		177,187	131,311	0
133	AF.81311	Formwork for cast-in-place concrete, wooden formwork, straight wall formwork, thickness <=45 cm	100m2	0.528	4,101,517	6,563,997		2,165,601	3,465,790	0
134	AF.81151	Formwork for cast-in-place concrete, wooden formwork, roof floor formwork	100m2	0.077	4,626,005	6,367,881		356,202	490,327	0
135	AF.61110	Fabrication and installation of rebar for cast-in-place concrete, foundation rebar, diameter <=10 mm	tán	0.011	16,224,107	2,482,193	98,488	178,465	27,304	1,083

NO.	Code Unit	Work name / Quantity description	Unit	Quantity	Unit Price			Amount		
					Material	Labor	Machinery	Material	Labor	Machinery
136	AF.61120	Fabrication and installation of rebar for cast-in-place concrete, foundation rebar, diameter <=18 mmống	tán	0.451	16,281,026	1,828,754	470,798	7,342,743	824,768	212,330
137	AF.61311	Fabrication and installation of rebar for cast-in-place concrete, wall rebar, diameter <=10 mm, wall height <= 4 m	tán	0.022	16,224,107	2,988,718	98,488	356,930	65,752	2,167
138	AF.61321	Fabrication and installation of rebar for cast-in-place concrete, wall rebar, diameter <=18 mm, wall height <= 4 m	tán	1.575	16,281,026	2,449,302	470,798	25,647,500	3,858,385	741,648
139	AF.61331	Fabrication and installation of rebar for cast-in-place concrete, wall rebar, diameter >18 mm, wall height <= 4 m	tán	0.044	16,191,302	1,995,403	483,904	712,417	87,798	21,292
140	AF.61721	Fabrication and installation of rebar for cast-in-place concrete, roof floor rebar, height <=16 m, diameter >10 mm	tán	0.300	16,280,598	2,392,290	497,629	4,884,179	717,687	149,289
141	AF.11213	Concrete manufacturing by mixer - manual casting, foundation concrete, 1x2 aggregate, width <=250 cm, grade 200	m3	1.600	746,940	331,715	50,657	1,194,731	530,578	81,026
142	TT	Composite manhole cover plate	cái	2.000	6,620,000			13,240,000	0	0
143	TT	Composite manhole cover plate	cái	1.000	2,320,000			2,320,000	0	0
	TT	Other works		0.050	76,829,930	37,306,507	20,622,838	3,841,497	1,865,325	1,031,142
	THM	TOTAL: DIVERSION CHAMBER						80,671,426	39,171,832	21,653,980

Break down of Construction cost of SEWAGE SECTOR

3&5. Installation of sewer pipe by Jacking method

No	Items	Formula	Quantity	Unit	Unit Price (JPY)		Cost (JPY)		Total			
					Foreign	Local	Foreign	Local	JPY	VND	JPY	VND
					JPY	VND	JPY	VND				
3	φ300	Sub-Total	1,000.0	m	64,440	9,318,872	64,440,000	9,318,872,000	47,246,681	111,686,681	22,028,931,172	
		RC Pipe D300mm				4,026,022		4,026,022,480		20,411,934		
		Pipe Jacking Grout			1,076	1,295,978	1,076,343	1,295,977,552	6,570,606			
		Other Materials			799	1,511,558	799,455	1,511,558,076	7,663,599			
		Soil Stabilizer				30,469		30,469,302	154,479			
		Other Materials			28,484	343,090	28,484,002	343,090,454	1,739,469			
		Labour			34,080	2,111,754	34,080,199	2,111,754,137	10,706,593			
		Equipment			88,560	12,806,941	88,560,000	12,806,941,000	64,931,191			
		Sub-Total			1,000.0	m			6,044,161,519	30,643,899		
		RC Pipe D500mm					2,361	2,601,677	2,360,787	2,601,677,407	13,190,504	
5	φ500	Pipe Jacking Grout			1,241	1,310,963	1,241,280	1,310,963,342	6,646,584			
		Other Materials				36,517		36,516,835	185,140			
		Soil Stabilizer				399,783		399,782,682	2,026,898			
		Other Materials			38,106	2,413,839	38,105,842	2,413,839,215	12,238,165			
		Labour			46,852		46,852,091					
		Equipment										
		Sub-Total			1,000.0	m			6,044,161,519	30,643,899		
		RC Pipe D500mm					2,361	2,601,677	2,360,787	2,601,677,407	13,190,504	
		Pipe Jacking Grout					1,241	1,310,963	1,241,280	1,310,963,342	6,646,584	
		Other Materials						36,517	36,516,835	185,140		
Soil Stabilizer					399,783		399,782,682	2,026,898				
Other Materials					38,106	2,413,839	38,105,842	2,413,839,215	12,238,165			
Labour					46,852		46,852,091					
Equipment												
Sub-Total			1,000.0	m			6,044,161,519	30,643,899				
RC Pipe D500mm					2,361	2,601,677	2,360,787	2,601,677,407	13,190,504			
Pipe Jacking Grout					1,241	1,310,963	1,241,280	1,310,963,342	6,646,584			
Other Materials						36,517	36,516,835	185,140				
Soil Stabilizer					399,783		399,782,682	2,026,898				
Other Materials					38,106	2,413,839	38,105,842	2,413,839,215	12,238,165			
Labour					46,852		46,852,091					
Equipment												
Sub-Total			1,000.0	m			6,044,161,519	30,643,899				
RC Pipe D500mm					2,361	2,601,677	2,360,787	2,601,677,407	13,190,504			
Pipe Jacking Grout					1,241	1,310,963	1,241,280	1,310,963,342	6,646,584			
Other Materials						36,517	36,516,835	185,140				
Soil Stabilizer					399,783		399,782,682	2,026,898				
Other Materials					38,106	2,413,839	38,105,842	2,413,839,215	12,238,165			
Labour					46,852		46,852,091					
Equipment												
Sub-Total			1,000.0	m			6,044,161,519	30,643,899				
RC Pipe D500mm					2,361	2,601,677	2,360,787	2,601,677,407	13,190,504			
Pipe Jacking Grout					1,241	1,310,963	1,241,280	1,310,963,342	6,646,584			
Other Materials						36,517	36,516,835	185,140				
Soil Stabilizer					399,783		399,782,682	2,026,898				
Other Materials					38,106	2,413,839	38,105,842	2,413,839,215	12,238,165			
Labour					46,852		46,852,091					
Equipment												
Sub-Total			1,000.0	m			6,044,161,519	30,643,899				
RC Pipe D500mm					2,361	2,601,677	2,360,787	2,601,677,407	13,190,504			
Pipe Jacking Grout					1,241	1,310,963	1,241,280	1,310,963,342	6,646,584			
Other Materials						36,517	36,516,835	185,140				
Soil Stabilizer					399,783		399,782,682	2,026,898				
Other Materials					38,106	2,413,839	38,105,842	2,413,839,215	12,238,165			
Labour					46,852		46,852,091					
Equipment												
Sub-Total			1,000.0	m			6,044,161,519	30,643,899				
RC Pipe D500mm					2,361	2,601,677	2,360,787	2,601,677,407	13,190,504			
Pipe Jacking Grout					1,241	1,310,963	1,241,280	1,310,963,342	6,646,584			
Other Materials						36,517	36,516,835	185,140				
Soil Stabilizer					399,783		399,782,682	2,026,898				
Other Materials					38,106	2,413,839	38,105,842	2,413,839,215	12,238,165			
Labour					46,852		46,852,091					
Equipment												
Sub-Total			1,000.0	m			6,044,161,519	30,643,899				

SUMMARY CONSTRUCTION COST ESTIMATES
PROJECT: INVESTMENT CLIMATE IMPROVEMENT PROJECT IN HA NAM PROVINCE

ITEM: SHAFT FOR PIPE JACKING

No.	Item	Code	Formula	Cost
I	DIRECT COST			
1	<i>Materials</i>	VL	A	128,389,185
	+ Based on direct unit cost	A1	Cost calculation sheet	125,803,272
	+ Difference of materials	CL	Cost compensation sheet	2,585,913
	Sub-Total	A	A1 + CL	128,389,185
2	<i>Man Power</i>	NC	NC1	161,327,176
	+ Based on direct unit cost	B1	Cost calculation sheet	181,266,490
	Multiple with a factor specified for construction man power	NC1	B1 x 0,89	161,327,176
3	<i>Construction Equipment</i>	M	C	239,766,017
	+ Based on direct unit cost	C1	Cost calculation sheet	280,594,143
	+ Difference of equipment	CLMay	Cost compensation sheet	-40,828,126
	Sub-Total	C	C1 + CLMay	239,766,017
	Total of Direct Cost	T	VL + NC + M	529,482,378

COST ESTIMATE OF WORK ITEMS

STRENGTHENING THE ENVIRONMENTAL INVESTMENT OF HA NAM PROVINCE

SHAFT FOR UNDERGROUND PIPE JACKING

NO.	Code	Unit Price	Work name / Quantity description	Unit	Quantity	Unit Price			Amount			
						Material	Labor	Machinery	Material	Labor	Machinery	
	HM		SHAFT FOR UNDERGROUND PIPE JACKING									
			SHAFT EXCATION									
1	AB.25213		Foundation excavation, foundation width <=10 m, by excavator <=0,8 m3, soil grade III	100m3	4.990		592,636	1,275,913	0	2,957,017		6,366,296
2	TT		Wooden pile depreciation IV (3,5%+1,17% depreciation)	ton	5.596	16,800,000			94,012,800	0		0
3	AC.27120		wooden pile pressing by hydraulic	100m	14.434		5,080,128	8,038,564	0	73,327,584		116,030,241
4	AC.27120		wooden pile pressing by hydraulic compressor (exposed section NC&Mx0.75)	100m	1.312		3,810,096	6,028,923	0	4,999,608		7,911,153
5	AC.27110		Wooden pile extraction by hydraulic compressor	100m	15.746		1,689,438	5,359,043	0	26,602,567		84,385,635
6	AI.11211		Fabrication of bracing strut (1,17% depreciation)	ton	0.085	17,231,969	3,179,488	350,007	1,464,717	270,257		29,751
			H SHAPE STEEL 300X300:									
			V7 SHAPE STEEL:									
7	AI.61141		Erection of connecting steel bracing by rivet (LD và TD NC&Mx1.6)	ton	7.265	592,178	7,571,126	7,017,786	4,301,936	55,001,205		50,981,405
8	AB.65120		Soil filling by tamper, required compactness K=0,90	100m3			2,088,759	1,620,018	0	0		0
			Excavation quantity:									
			Minus concrete quantity:		4.990							

NO.	Code		Work name / Quantity description	Unit	Quantity	Unit Price			Amount			
	Unit Price	Material				Labor	Machinery	Material	Labor	Machinery		
			<i>Minus crushed stone quantity:</i>									
9	AF.31213		Site batching plant manufactured or commercial concrete, casted by pump, base concrete, grade 200	m3	4.234	874,237	125,404	92,336		3,701,170	530,910	390,914
10	AB.41412		Soil hauling by dump truck, distance <=1000m, 5T truck, soil grade II <i>Excavated quantity - compressed quantity:</i>	100m3				1,890,812		0	0	0
11	AB.42312		Subsequent soil hauling distance of <=7 km by 5T dump truck, soil grade II	100m3	0.000			3,036,672		0	0	0
12	AK.98120		Foundation lining stone layer using Dmax<=6 stone	m3	6.350	214,500	330,799			1,362,161	2,100,706	0
13	AF.32113		Site batching plant manufactured or commercial concrete, casted by pump, wall concrete, thickness <=45cm, height <=4m, grade 200	m3	6.912	1,021,196	561,344	115,098		7,058,507	3,880,010	795,557
14	AF.82111		Formwork for cast-in-place concrete, metal formwork, wall formwork, square column, rectangular column, beam, shoring, height <=16 m	100m2	0.207	3,243,995	9,044,990	637,657		672,805	1,875,931	132,250
15	AF.61321		Fabrication and erection of rebar for cast-in-place concrete, wall rebar, diameter <=18 mm, wall height <= 4 m	ton	0.445	16,281,026	2,449,302	470,798		7,238,544	1,088,960	209,317
16	TT		<i>Other works</i>		0.050	119,812,640	172,634,753	267,232,517		5,990,632	8,631,738	13,361,626
	THM		TOTAL: SHAFT FOR UNDERGROUND PIPE JACKING							125,803,272	181,266,490	280,594,143

SUMMARY CONSTRUCTION COST ESTIMATES

PROJECT: INVESTMENT CLIMATE IMPROVEMENT PROJECT IN HA NAM PROVINCE

ITEM: MANHOLE TYPE-2

No.	Item	Code	Formula	Cost
I	DIRECT COST			
1	<i>Materials</i>	<i>VL</i>	A	208,499,712
	+ Based on direct unit cost	A1	Bảng dự toán hạng mục	200,540,739
	+ Difference of materials	CL	Theo bảng bù giá	7,958,973
	Sub-Total	A	A1 + CL	208,499,712
2	<i>Man Power</i>	<i>NC</i>	NC1	60,481,985
	+ Based on direct unit cost	B1	Bảng dự toán hạng mục	67,957,286
	Multiple with a factor specified for construction man power	NC1	B1 x 0,89	60,481,985
3	<i>Construction Equipment</i>	<i>M</i>	C	26,606,572
	+ Based on direct unit cost	C1	Bảng dự toán hạng mục	24,915,072
	+ Difference of equipment	CLMay	Theo bảng bù giá	1,691,500
	Sub-Total	C	C1 + CLMay	26,606,572
	<i>Total of Direct Cost</i>	<i>T</i>	VL + NC + M	295,588,269

COST ESTIMATE OF WORK ITEMS

STRENGTHENING THE ENVIRONMENTAL INVESTMENT OF HA NAM PROVINCE

TYPE 2 MANHOLE

NO.	Code Unit	Work name / Quantity description	Unit	Quantity	Unit Price			Amount				
					Material	Labor	Machinery	Material	Labor	Machinery		
	HM	TYPE 2 MANHOLE										
1	AA.22211	Concrete structure demolition by driller, reinforced concrete	m3	7.040	27,900	442,936	343,385	196,416	3,118,269	2,417,430		
2	AA.22212	Concrete structure demolition by driller, non-reinforced concrete	m3	4.312		412,237	180,263	0	1,777,566	777,294		
3	AA.22221	Stony brick tructure demolition by driller	m3	6.468		361,804	162,737	0	2,340,148	1,052,583		
4	AB.55311	Stone mixture shoveled to transportation means by <=1,25m3 bucket excavator	100m3	0.178		241,909	1,403,441	0	43,108	250,093		
5	AB.53411	Stone hauling by 5 ton dump truck within <=1000 m distance	100m3	0.178			3,214,380	0	0	572,803		
6	AB.54311	Subsequent hauling <=7 km (4km) of stone by 5 ton dump truck	100m3	0.178			4,156,944	0	0	740,767		
7	AB.13412	Sand filling for pipeline, drain pipe base	m3	1.349	118,218	117,314		159,429	158,210	0		
8	AB.66142	Sand filling by tamper, required compactness K=0,90	100m3	0.121	11,590,000	938,510	863,081	1,407,026	113,935	104,778		
9	AB.65120	Soil filling by tamper, required compactness K=0,90	100m3	1.747		2,088,759	1,620,018	0	3,649,271	2,830,333		
10	AB.41412	Soil hauling by 5T dump truck, distance <=1000m, soil grade II	100m3	1.025			1,890,812	0	0	1,937,893		
11	AB.42312	Subsequent hauling of 4 km by 5T dump truck, soil grade II	100m3	1.025			3,036,672	0	0	3,112,285		
12	AF.11111	Concrete manufacturing by mixer - manual casting, foundation lining concrete, 4x6 aggregate, width <=250 cm,grade 100	m3	1.758	551,165	287,216	50,365	968,838	504,868	88,532		

NO.	Code Unit	Work name / Quantity description	Unit	Quantity	Unit Price			Amount		
					Material	Labor	Machinery	Material	Labor	Machinery
13	AF.31115	Concrete manufactured at site batching plant or commercial concrete, casted by pump, foundation concrete, foundation width <=250 cm, M300	m3	7.920	1,024,817	171,925	92,631	8,116,551	1,361,646	733,638
14	AF.82511	Formwork for cast-in-place concrete, formwork for long foundation	100m2	0.085	1,449,697	2,894,491		122,789	245,163	0
15	AF.61120	Fabrication and erection of rebar for cast-in-place concrete, foundation rebar, diameter <=18 mm	ton	0.990	16,281,026	1,828,754	470,798	16,118,216	1,810,467	466,090
16	AF.32115	Concrete manufactured at site batching plant or commercial concrete, casted by pump, wall concrete, thickness <=45cm, height <=4m, grade 300	m3	42.049	1,181,880	561,344	115,098	49,696,636	23,603,842	4,839,733
17	AF.82111	Formwork for cast-in-place concrete, metal formwork, formwork for wall, square column, girder, bracing, height <=16 m	100m2	0.931	3,243,995	9,044,990	637,657	3,018,862	8,417,268	593,404
18	AF.61321	$2 \times (3+1.7) \times 9/100 = 0.846$ Fabrication and erection of rebar for cast-in-place concrete, wall rebar, diameter <=18 mm, wall height <= 4 m	ton	6.307	16,281,026	2,449,302	470,798	102,689,315	15,448,483	2,969,464
19	AF.32315	Concrete manufactured at site batching plant or commercial concrete, casted by pump, girder, bracing, roof floor concrete, grade 300	m3	1.560	1,024,817	561,344	115,098	1,598,715	875,697	179,553
20	AF.61711	Fabrication and erection of rebar for cast-in-place concrete, roof floor rebar, height <=16 m, diameter <=10 mm	ton	0.236	16,224,107	3,207,993	100,458	3,828,889	757,086	23,708
21	AF.82311	Formwork for cast-in-place concrete, metal formwork, formwork for roof floor, height <=16 m	100m2	0.060	3,616,509	7,679,263	637,657	216,991	460,756	38,259

NO.	Code Unit	Work name / Quantity description	Unit	Quantity	Unit Price			Amount			
					Material	Labor	Machinery	Material	Labor	Machinery	
22	TT	Composite manhole cover plate	pce	1.000	2,850,000				2,850,000	0	0
23	AG.42111	Manual installation of various precast concrete structures, weight <= 50 kg	pce	1.000	2,509	35,443			2,509	35,443	0
24	TT	Other works		0.050	190,991,180	64,721,225	23,728,640		9,549,559	3,236,061	1,186,432
	THM	TOTAL: TYPE 2 MANHOLE							200,540,739	67,957,286	24,915,072

SUMMARY CONSTRUCTION COST ESTIMATES
PROJECT: INVESTMENT CLIMATE IMPROVEMENT PROJECT IN HA NAM PROVINCE

ITEM: Pumping Station

No.	Item	Unit	Quantity	Cost
I	DIRECT COST			
0	<i>Technology section</i>	<i>Station</i>	1	173,660,000.0
1	<i>Construction section</i>	<i>Station</i>	1	589,850,000.0
2	<i>Electrical section</i>	<i>Station</i>	1	127,140,000.0
3	<i>Equipment section</i>	<i>Station</i>	1	500,000,000.0
	Total of Direct Cost	<i>T</i>		1,390,650,000.0

SUMMARY CONSTRUCTION COST

PROJECT: INVESTMENT CLIMATE IMPROVEMENT PROJECT IN HA NAM PROVINCE

Item: Pumping Station - Construction Portion

No.	Item	Code	Formula	Cost
I	DIRECT COST			
1	<i>Materials</i>	<i>VL</i>	<i>A</i>	307,934,742
	+ Based on direct unit cost	A1	Cost calculation sheet	310,219,054
	+ Difference of materials	CL	Cost compensation sheet	-2,284,312
	Sub-Total	A	A1 + CL	307,934,742
2	<i>Man Power</i>	<i>NC</i>	<i>NC1</i>	156,628,017
	+ Based on direct unit cost	B1	Cost calculation sheet	175,986,536
	Multiple with a factor specified for construction man power	NC1	B1 x 0,89	156,628,017
3	<i>Construction Equipment</i>	<i>M</i>	<i>C</i>	125,289,495
	+ Based on direct unit cost	C1	Cost calculation sheet	137,112,182
	+ Difference of equipment	CLMay	Cost compensation sheet	-11,822,687
	Sub-Total	C	C1 + CLMay	125,289,495
	Total of Direct Cost	T	VL + NC + M	589,852,254

COST ESTIMATE OF WORK ITEMS

STRENGTHENING THE ENVIRONMENTAL INVESTMENT OF HA NAM PROVINCE

WASTEWATER PUMPING STATION (WWPS) - CONSTRUCTION COMPONENT

NO.	Code		Work name / Quantity description	Unit	Quantity	Unit Price			Amount			
	Unit price	HM				Material	Labor	Machinery	Material	Labor	Machinery	
			WASTEWATER PUMPING STATION - CONSTRUCTION COMPONENT									
1		TT	Depreciation of wooden pile u	kg	1,377.107	16,800.				23,135,396	0	0
			WWPS									
2		AC.27120	Pressing wooden pile by hydraulic	100m	3.581		5,080,128.		8,038,564.	0	18,190,414	28,783,686
			WWPS									
3		AC.27110	Wooden pile extraction by hydraulic compressor	100m	3.581		1,689,438.		5,359,043.	0	6,049,371	19,189,125
4		AC.22512	Driving formed steel pile (U, I shape) height >100 mm on the ground, pile length <=10 m	100m	0.628	1,062,191.	1,105,814.	7,021,822.	666,844	694,230	4,408,300	
5		AC.23110	Formed steel pile extraction, soil retaining wall by steel pipes, working platform on the	100m	0.628		628,518.	4,548,706.	0	394,584	2,855,678	
6		Al.11211	Fabrication of steel bracing (depreciation 1,17%)	ton	0.027	17,231,969.	3,179,488.	350,007.	460,094	84,892	9,345	
			WWPS:									
			Manhole HG2:									
7		Al.63311	Erection, removal of steel rafter frame, working platform on the ground	ton	0.557	323,753.	2,244,708.	1,793,672.	180,428	1,250,976	999,613	
			WWPS:									
			Manhole HG2:									
8		AC.11710	Installation, removal of 5mm thick retaining wall by steel plate	100m2	0.439		5,618,922.		0	2,469,516	0	
			Manhole HG2:									
			CONSTRUCTION COMPONENT									

NO.	Code		Work name / Quantity description	Unit	Quantity	Unit Price			Amount		
	Unit price						Material	Labor	Machinery	Material	Labor
9	AB.11443		Excavation of column, pier foundation, manhole, width >1 m, depth >1 m, soil WWPS:	m3	13.679		305,420.		0	4,177,749	0
10	AB.25123		Foundation excavation, foundation width <=6 m, by excavator <=1,25 m3, soil grade III	100m3	1.231		1,512,942.	1,253,993.	0	1,862,432	1,543,665
11	AB.13113		Foundation soil filling, required compactness K=0,95 (10%)	m3	6.649		141,586.		0	941,448	0
					13.679						
					1.982						
			<i>Minus manhole occupied volume:</i>								
12	AB.65130		Soil filling by tamper, required compactness K=0,95 (90%)	100m3	0.598		2,405,381.	1,865,587.	0	1,439,380	1,116,367
13	AB.41423		Soil hauling by dump truck, distance <=1000m, 7T truck, soil grade III	100m3	0.703			2,070,520.	0	0	1,455,369
					13.679						
					6.649						
14	AB.42223		Subsequent soil hauling distance of <=4 km by 7T dump truck, soil grade III (4km)	100m3	0.703			2,898,728.	0	0	2,037,516
15	AF.11111		Concrete manufacturing by mixer - manual casting, foundation lining concrete, 4x6 aggregate, width <=250 cm, grade 100	m3	0.975		551,165.	50,365.	537,221	279,949	49,091
16	AF.11121		Concrete manufacturing by mixer - manual casting, foundation lining concrete, 4x6 aggregate, width >250 cm, grade 100 WWPS:	m3	1.007		551,165.	50,365.	555,133	240,391	50,728
17	AF.81111		Formwork for cast-in-place concrete, wooden formwork, long foundation formwork, WWPS:	100m2	0.100		4,026,971.		403,100	298,732	0
18	AF.81311		Formwork for cast-in-place concrete, wooden formwork, formwork for straight wall, thickness <=45 cm	100m2	0.827		4,101,517.		3,393,185	5,430,395	0

NO.	Code		Work name / Quantity description	Unit	Quantity	Unit Price			Amount		
	Unit price	Material				Labor	Machinery	Material	Labor	Machinery	
19	AF.81151		Formwork for cast-in-place concrete, wooden formwork, formwork for roof floor WMPS:	100m2	0.079	4,626,005.	6,367,881.		364,992	502,426	0
20	AF.61110		Fabrication and installation of rebar for cast-in-place concrete, foundation rebar, diameter <=10 mm	ton	0.013	16,224,107.	2,482,193.	98,488.	209,291	32,020	1,271
21	AF.61120		Fabrication and installation of rebar for cast-in-place concrete, foundation rebar, diameter <=18 mm	ton	0.455	16,281,026.	1,828,754.	470,798.	7,409,495	832,266	214,260
22	AF.61312		Fabrication and installation of rebar for cast-in-place concrete, wall rebar, diameter <=10 mm, wall height <=16 m	ton	0.032	16,224,107.	3,096,163.	116,801.	519,171	99,077	3,738
23	AF.61322		Fabrication and installation of rebar for cast-in-place concrete, wall rebar, diameter <=18 mm, wall height <=16 m	ton	5.122	16,281,026.	2,675,155.	496,558.	83,386,531	13,701,341	2,543,221
24	AF.61721		Fabrication and installation of rebar for cast-in-place concrete, roof floor rebar, height <=16 m, diameter >10 mm	ton	0.044	16,280,598.	2,392,290.	497,629.	717,974	105,500	21,945
25	AF.11214		Concrete manufacturing by mixer - manual casting, foundation concrete, 4x6 aggregate, width <=250 cm, grade 250	m3	2.547	813,735.	331,715.	50,657.	2,072,664	844,911	129,028
26	AF.11224		Concrete manufacturing by mixer - manual casting, foundation concrete, 1x2 aggregate, width >250 cm, grade 250	m3	2.636	860,197.	398,462.	50,657.	2,267,135	1,050,186	133,512
27	AF.12124		Concrete manufacturing by mixer - manual casting, straight wall concrete, 1x2 aggregate, thickness <=45 cm, height <=16	m3	22.492	968,708.	925,341.	116,964.	21,788,665	20,813,232	2,630,813
28	AI.13111		Fabrication of steel structures embedded in concrete, weight of one structure <=10 kg	ton	0.068	18,224,164.	8,946,545.	1,946,178.	1,239,243	608,365	132,340

NO.	Code		Work name / Quantity description	Unit	Quantity	Unit Price			Amount		
	Unit price	Material				Labor	Machinery	Material	Labor	Machinery	
29	AI.64211		Embedding steel structure in concrete, weight of one structure <=10 kg	tán	0.068	677,143.	3,945,960.	592,912.	46,046	268,325	40,318
30	AF.12414		Concrete manufacturing by mixer - manual casting, roof floor concrete, 1x2 aggregate, grade 250	m3	1.491	813,735.	543,802.	94,720.	1,213,360	810,863	141,237
31	AE.26214		Construction of unburnt brick 6,5x10,5x22, construction of manhole, valve chamber,	m3	1.789	1,098,877.	701,680.	9,066.	1,966,221	1,255,516	16,222
32	AK.21124		Plastering outer wall, 1,5 cm thick, cement mortar grade 75	m2	12.993	9,102.	61,434.	793.	118,261	798,200	10,303
33	AK.42114		Troweling 1,0 cm thick of grade 75 mortar for eaves, louver, gutter	m2	3.479	8,672.	27,882.	755.	30,173	97,010	2.627
34	AG.11414		Fabrication of precast concrete structures, slab, louver, lintel, aggregate 1x2, grade 250	m3	0.938	801,807.	519,821.	28,902.	752,416	487,800	27,122
35	AG.31311		Fabrication, installation, removal of formwork of precast concrete, wooden formwork, slab, apron formwork	100m2	0.046	353,654.	5,182,029.		16,268	238,373	0
36	AG.13221		Fabrication, installation of rebar for precast concrete, slab, window, apron, cantilever spoke	ton	0.098	16,224,107.	3,749,603.	98,488.	1,589,963	367,461	9,652
37	AG.42131		Manual installation of precast concrete structures, various precast concrete structures, weight <= 250 kg	pce	12.000	5,855.	106,328.		70,260	1,275,936	0
	TT		Other works		1.000	155,109,527.	87,993,268.2	68,556,091.1	155,109,527	87,993,268	68,556,091
	THM		TOTAL : WWPS- CONSTRUCTION COMPONENT						310,219,054	175,986,536	137,112,182

SUMMARY CONSTRUCTION COST
PROJECT: INVESTMENT CLIMATE IMPROVEMENT PROJECT IN HA NAM PROVINCE

Item: Pumping Station - Lighting System

No.	Item	Code	Formula	Cost
I	DIRECT COST			
1	<i>Materials</i>	<i>VL</i>	A	121,110,089
	+ Based on direct unit cost	A1	Cost calculation sheet	116,585,495
	+ Difference of materials	CL	Cost compensation sheet	4,524,594
	Sub-Total	A	A1 + CL	121,110,089
2	<i>Man Power</i>	<i>NC</i>	NC1	5,269,370
	+ Based on direct unit cost	B1	Cost calculation sheet	5,587,879
	Multiple with a factor specified for construction man power	NC1	B1 x 0,943	5,269,370
3	<i>Construction Equipment</i>	<i>M</i>	C	757,569
	+ Based on direct unit cost	C1	Cost calculation sheet	830,485
	+ Difference of equipment	CLMay	Cost compensation sheet	-72,916
	Sub-Total	C	C1 + CLMay	757,569
	Total of Direct Cost	T	VL + NC + M	127,137,028

COST ESTIMATE OF WORK ITEMS

STRENGTHENING THE ENVIRONMENTAL INVESTMENT OF HA NAM PROVINCE

WASTEWATER PUMPING STATION - LIGHTING

NO.	Code	Unit price	Work name / Quantity description	Unit	Quantity	Unit Price			Amount			
						Material	Labor	Machinery	Material	Labor	Machinery	
	HM		PUMPING STATION - LIGHTING SYSTEM									
			<i>On-land station</i>									
1	AB.11512		Excavation of canal, ditch width <=3 m, depth <=1 m, soil class II	m3	0.200		184,061		0		36,812	0
2	AB.25212		Footing excavation, footing width <=10 m, by excavator <=0,8 m3, soil class II	100m3	0.039		481,391	1,008,199	0		18,678	39,118
3	AB.13113		Foundation soil filling, required compactness K=0,95	m3	0.300		141,586		0		42,476	0
4	AB.65130		Soil filling by tamper, required compactness K=0,95	100m3	0.039		2,405,381	1,865,587	0		93,329	72,385
5	BA.20102		Installation of ready-made lightning rod	cọc	3.000	94,940	62,855		284,820		188,565	0
6	BA.20202		Flat steel 40x4	m	5.000	12,753	4,889	1,547	63,765		24,445	7,735
			<i>Power cable for Pumping Station</i>									
7	AB.11512		Excavation of drainage trench, width <=3 m, depth <=1 m, soil grade II	m3	1.473		184,061		0		271,067	0
8	AB.25212		Foundation excavation, width <=10 m, by excavator of <=0,8 m3, soil grade II	100m3	0.280		481,391	1,008,199	0		134,693	282,094
9	AB.13113		Foundation soil filling, required compactness K=0,95	m3	1.473		141,586		0		208,514	0

NO.	Code		Work name / Quantity description	Unit	Quantity	Unit Price			Amount		
	Unit price	Material				Labor	Machinery	Material	Labor	Machinery	
10	AB.13113		Foundation soil filling, required compactness K=0,95	m3	0.302		141,586		0	42,717	0
11	TT		Cable warning net	m	100.000	1,000			100,000	0	0
12	CS.2.03.10		Underground cable CXV/DSTA(3x35+1x16)mm2 - 0,6/1kV	100m	1.720	28,233,950	349,192		48,562,394	600,610	0
13	CS.2.03.10		Underground cable CXV(4x4)mm2 - 0,6/1kV	100m	0.205	5,271,402	349,192		1,080,637	71,584	0
14	CS.2.03.10		Underground cable CXV(4x1,5)mm2 - 0,6/1kV	100m	0.172	2,320,899	349,192		399,195	60,061	0
			<i>PS panel</i>								
15	TT		Outdoor 2-layer panel case, grey color electrostatic painting of 1,5mm thick.	tủ	1.000	1,400,000			1,400,000	0	0
16	BA.19302		Attomat MCB-3P-20A	cái	1.000	306,000	69,838		306,000	69,838	0
17	BA.19302		Attomat chống giật RCCB-3P-16A	cái	2.000	306,000	69,838		612,000	139,676	0
18	BA.19201		Attomat MCB-1P-10A	cái	1.000	40,845	25,607		40,845	25,607	0
19	BA.19302		Contacto 3p-18A	cái	2.000	306,000	69,838		612,000	139,676	0
20	BA.19104		Heat relay 6-9A	cái	2.000	96,900	51,215		193,800	102,430	0
21	BA.19104		Intermediate relay	cái	2.000	96,900	51,215		193,800	102,430	0
22	TT		Wiring terminal	bộ	1.000	16,091			16,091	0	0
23	BA.19104		Meter	cái	2.000	96,900	51,215		193,800	102,430	0
24	BA.18101		Push button + lamp	cái	3.000	11,758	18,624		35,274	55,872	0
25	BA.18101		Warning light	cái	3.000	11,758	18,624		35,274	55,872	0
26	TT		Isolating transformer 1000VA-	cái	1.000	340,000			340,000	0	0
27	TT		Bridge rectification 24 VAC	cái	1.000	1,205,000			1,205,000	0	0
28	TT		3-terminal level measuring switch	cái	1.000	1,143,000			1,143,000	0	0
			<i>Panel foundation</i>								
29	AB.11412		Foundation excavation for column, pier, manhole, width <=1 m, depth <=1 m,	m3	0.196		240,695		0	47,128	0
30	AF.11213		Concrete manufacturing by mixer - manual casting, foundation lining concrete, 1x2 aggregate, width <=250	m3	0.275	746,940	331,715	50,657	205,110	91,089	13,910

NO.	Code		Work name / Quantity description	Unit	Quantity	Unit Price			Amount		
	Unit price					Material	Labor	Machinery	Material	Labor	Machinery
31	AF.81111		Formwork for cast-in-place concrete, wooden formwork, for long foundation or machine base	100m ²	0.023	4,026,971	2,984,333		92,218	68,341	0
32	TT		Foundation concrete frame M16x950x350x500	bộ	1.000	1,000,000			1,000,000	0	0
33	TT		HDPE pipe 65/50	m	5.000	35,545			177,725	0	0
	TT		Other works		1.000	58,292,747	2,793,940	415,242	58,292,747	2,793,940	415,242
	THM		TOTAL: WARD QUANG TRUNG - WASTEWATER PUMPING STATION						116,585,495	5,587,879	830,485

8. Cost Breakdown (Allocation of Cost from LCB-4 to ICB-2)

LCB-4 Allocation of Sidewalk from LCB-4 to ICB-2 (North-South Cross Section)

	Category	Items	Qty	Unit	Unit Cost		Total Cost
1. Original Plan (LCB-4 Full Implementation)	Embankment Work	Excavation (by machine)	89,260	m3	17,860	VND/m3	1,594,183,600
		Backfill (by machine)	89,260	m3	8,395	VND/m3	749,337,700
		Embankment (by machine)	341,198	m3	173,451	VND/m3	59,181,134,298
		Transportation of soil	26,778	m3	12,457	VND/m3	333,573,546
		Removal of Excavated Unsuitable Soil	26,778	m3	32,457	VND/m3	869,133,546
		Slope Protection	8,820	m2	69,579	VND/m2	613,686,780
	Rain Water Drainage	L gutter	5,880	m	661,504	VND/m	3,889,646,225
		U Ditch with Cover (1,000*1,000)	5,880	m	3,758,419	VND/m	22,099,503,720
		Catch Basin (1,200*1,200)	196	nos.	11,099,351	VND/nos	2,175,472,796
	Pavement Work at Sidewalk	Base Course (Crushed Stone 10cm)	45,142	m2	33,146	VND/m2	1,496,284,356
		Sand and Mortar Buffer	45,142	m2	44,044	VND/m2	1,988,244,378
		Interlocking Block	45,142	m2	120,258	VND/m2	5,428,714,295
		Concrete Curb	5,880	m	155,062	VND/m	911,764,560
	Sidewalk (Allocation Portion)	Embankment Work	Excavation (by machine)	6,050	m3	17,860	VND/m3
Backfill (by machine)			6,050	m3	8,395	VND/m3	50,789,750
Embankment (by machine)			24,200	m3	173,451	VND/m3	4,197,514,200
Transportation of soil			1,815	m3	12,457	VND/m3	22,609,455
Removal of Excavated Unsuitable Soil			1,815	m3	32,457	VND/m3	58,909,455
Slope Protection			3,450	m2	69,579	VND/m2	240,047,550
Rain Water Drainage		L gutter	0	m	661,504	VND/m	0
		U Ditch with Cover (1,000*1,000)	0	m	3,758,419	VND/m	0
		Catch Basin (1,200*1,200)	0	nos.	11,099,351	VND/nos	0
Pavement Work at Sidewalk		Base Course (Crushed Stone 10cm)	12,386	m2	33,146	VND/m2	410,546,356
		Sand and Mortar Buffer	12,386	m2	44,044	VND/m2	545,528,984
		Interlocking Block	12,386	m2	120,258	VND/m2	1,489,515,588
		Concrete Curb	2,200	m	155,062	VND/m	341,136,400
Diffrence (1-2)		Embankment Work	Excavation (by machine)	83,210	m3	17,860	VND/m3
	Backfill (by machine)		83,210	m3	8,395	VND/m3	698,547,950
	Embankment (by machine)		316,998	m3	173,451	VND/m3	54,983,620,098
	Transportation of soil		24,963	m3	12,457	VND/m3	310,964,091
	Removal of Excavated Unsuitable Soil		24,963	m3	32,457	VND/m3	810,224,091
	Slope Protection		5,370	m2	69,579	VND/m2	373,639,230
	Rain Water Drainage	L gutter	5,880	m	661,504	VND/m	3,889,646,225
		U Ditch with Cover (1,000*1,000)	5,880	m	3,758,419	VND/m	22,099,503,720
		Catch Basin (1,200*1,200)	196	nos.	3,758,420	VND/m	736,650,320
	Pavement Work at Sidewalk	Base Course (Crushed Stone 10cm)	32,756	m2	33,146	VND/m2	1,085,738,000
		Sand and Mortar Buffer	32,756	m2	44,044	VND/m2	1,442,715,394
		Interlocking Block	32,756	m2	120,258	VND/m2	3,939,198,707
		Concrete Curb	3,680	m	155,062	VND/m	570,628,160
	Total Cost (VND)						
	Category	Items	Qty	Unit	Unit Cost		Total Cost
Remove the duplicate part for Embankment Work between Road and Sewerage	Embankment Work	Excavation (by machine)	3,850	m3	17,860	VND/m3	68,761,000
		Backfill (by machine)	3,850	m3	8,395	VND/m3	32,320,750
		Embankment (by machine)	24,200	m3	173,451	VND/m3	4,197,514,200
		Transportation of soil	1,155	m3	12,457	VND/m3	14,387,835
		Removal of Excavated Unsuitable Soil	1,155	m3	32,457	VND/m3	37,487,835
		Slope Protection	3,450	m2	69,579	VND/m2	240,047,550
	Rain Water Drainage	L gutter	0	m	661,504	VND/m	0
		U Ditch with Cover (1,000*1,000)	0	m	3,758,419	VND/m	0
		Catch Basin (1,200*1,200)	0	nos.	3,758,420	VND/m	0
	Pavement Work at Sidewalk	Base Course (Crushed Stone 10cm)	12,386	m2	33,146	VND/m2	410,546,356
		Sand and Mortar Buffer	12,386	m2	44,044	VND/m2	545,528,984
		Interlocking Block	12,386	m2	120,258	VND/m2	1,489,515,588
		Concrete Curb	2,200	m	155,062	VND/m	341,136,400
	Total Cost (VND)						

LCB-4 Allocation of Sidewalk from LCB-4 to ICB-2 (East-West Cross Section)

	Category	Items	Qty	Unit	Unit Cost		Total Cost
1. Original Plan (LCB-4 Full Implementation)	Embankment Work	Excavation (by machine)	38,200	m3	17,860	VND/m3	682,252,000
		Backfill (by machine)	38,200	m3	8,395	VND/m3	320,689,000
		Embankment (by machine)	70,758	m3	173,451	VND/m3	12,273,122,350
		Transportation of soil	11,460	m3	12,457	VND/m3	142,757,220
		Removal of Excavated Unsuitable Soil	11,460	m3	32,457	VND/m3	371,957,220
		Slope Protection	4,680	m2	69,579	VND/m2	325,629,720
	Rain Water Drainage	L gutter	3,120	m	661,504	VND/m	2,063,893,915
		U Ditch with Cover (1,000*1,000)	3,120	m	3,758,419	VND/m	11,726,267,280
		Catch Basin (1,200*1,200)	104	nos.	11,099,351	VND/nos	1,154,332,504
	Pavement Work at Sidewalk	Base Course (Crushed Stone 10cm)	25,501	m2	33,146	VND/m2	845,239,904
		Sand and Mortar Buffer	25,501	m2	44,044	VND/m2	1,123,144,462
		Interlocking Block	25,501	m2	120,258	VND/m2	3,066,640,332
		Concrete Curb	3,120	m	155,062	VND/m	483,793,440
	Sidewalk (Allocation Portion)	Embankment Work	Excavation (by machine)	5,460	m3	17,860	VND/m3
Backfill (by machine)			5,460	m3	8,395	VND/m3	45,836,700
Embankment (by machine)			21,840	m3	173,451	VND/m3	3,788,169,840
Transportation of soil			1,638	m3	12,457	VND/m3	20,404,566
Removal of Excavated Unsuitable Soil			1,638	m3	32,457	VND/m3	53,164,566
Slope Protection			2,340	m2	69,579	VND/m2	162,814,860
Rain Water Drainage		L gutter	0	m	661,504	VND/m	0
		U Ditch with Cover (1,000*1,000)	0	m	3,758,419	VND/m	0
		Catch Basin (1,200*1,200)	0	nos.	11,099,351	VND/nos	0
Pavement Work at Sidewalk		Base Course (Crushed Stone 10cm)	9,917	m2	33,146	VND/m2	328,708,882
		Sand and Mortar Buffer	9,917	m2	44,044	VND/m2	436,784,348
		Interlocking Block	9,917	m2	120,258	VND/m2	1,192,598,586
		Concrete Curb	1,560	m	155,062	VND/m	241,896,720
Diffrence (1-2)		Embankment Work	Excavation (by machine)	32,740	m3	17,860	VND/m3
	Backfill (by machine)		32,740	m3	8,395	VND/m3	274,852,300
	Embankment (by machine)		48,918	m3	173,451	VND/m3	8,484,952,510
	Transportation of soil		9,822	m3	12,457	VND/m3	122,352,654
	Removal of Excavated Unsuitable Soil		9,822	m3	32,457	VND/m3	318,792,654
	Slope Protection		2,340	m2	69,579	VND/m2	162,814,860
	Rain Water Drainage	L gutter	3,120	m	661,504	VND/m	2,063,893,915
		U Ditch with Cover (1,000*1,000)	3,120	m	3,758,419	VND/m	11,726,267,280
		Catch Basin (1,200*1,200)	104	nos.	11,099,351	VND/nos	1,154,332,504
	Pavement Work at Sidewalk	Base Course (Crushed Stone 10cm)	15,584	m2	33,146	VND/m2	516,531,022
		Sand and Mortar Buffer	15,584	m2	44,044	VND/m2	686,360,114
		Interlocking Block	15,584	m2	120,258	VND/m2	1,874,041,746
		Concrete Curb	1,560	m	155,062	VND/m	241,896,720
	Total Cost (VND)						
	Category	Items	Qty	Unit	Unit Cost		Total Cost
Remove the duplicate part for Embankment Work between Road and Sewerage	Embankment Work	Excavation (by machine)	3,900	m3	17,860	VND/m3	69,654,000
		Backfill (by machine)	3,900	m3	8,395	VND/m3	32,740,500
		Embankment (by machine)	21,840	m3	173,451	VND/m3	3,788,169,840
		Transportation of soil	1,170	m3	12,457	VND/m3	14,574,690
		Removal of Excavated Unsuitable Soil	1,170	m3	32,457	VND/m3	37,974,690
		Slope Protection	2,340	m2	69,579	VND/m2	162,814,860
	Rain Water Drainage	L gutter	0	m	661,504	VND/m	0
		U Ditch with Cover (1,000*1,000)	0	m	3,758,419	VND/m	0
		Catch Basin (1,200*1,200)	0	nos.	11,099,351	VND/nos	0
	Pavement Work at Sidewalk	Base Course (Crushed Stone 10cm)	9,917	m2	33,146	VND/m2	328,708,882
		Sand and Mortar Buffer	9,917	m2	44,044	VND/m2	436,784,348
		Interlocking Block	9,917	m2	120,258	VND/m2	1,192,598,586
		Concrete Curb	1,560	m	155,062	VND/m	241,896,720
	Total Cost (VND)						

LCB-4 Allocation of Sidewalk from LCB-4 to ICB-2 (Both CrossRoad)

	Category	Items	Qty	Unit	Unit Cost		Total Cost
1. Original Plan (LCB-4 Full Implementation)	Embankment Work	Excavation (by machine)	127,460	m3	17,860	VND/m3	2,276,435,600
		Backfill (by machine)	127,460	m3	8,395	VND/m3	1,070,026,700
		Embankment (by machine)	411,956	m3	173,451	VND/m3	71,454,256,648
		Transportation of soil	38,238	m3	12,457	VND/m3	476,330,766
		Removal of Excavated Unsuitable Soil	38,238	m3	32,457	VND/m3	1,241,090,766
		Slope Protection	13,500	m2	69,579	VND/m2	939,316,500
	Rain Water Drainage	L gutter	9,000	m	661,504	VND/m	5,953,540,140
		U Ditch with Cover (1,000*1,000)	9,000	m	3,758,419	VND/m	33,825,771,000
		Catch Basin (1,200*1,200)	300	nos.	11,099,351	VND/nos	3,329,805,300
	Pavement Work at Sidewalk	Base Course (Crushed Stone 10cm)	70,643	m2	33,146	VND/m2	2,341,524,260
		Sand and Mortar Buffer	70,643	m2	44,044	VND/m2	3,111,388,841
		Interlocking Block	70,643	m2	120,258	VND/m2	8,495,354,627
		Concrete Curb	9,000	m	155,062	VND/m	1,395,558,000
Sidewalk (Allocation Portion)	Embankment Work	Excavation (by machine)	11,510	m3	17,860	VND/m3	205,568,600
		Backfill (by machine)	11,510	m3	8,395	VND/m3	96,626,450
		Embankment (by machine)	46,040	m3	173,451	VND/m3	7,985,684,040
		Transportation of soil	3,453	m3	12,457	VND/m3	43,014,021
		Removal of Excavated Unsuitable Soil	3,453	m3	32,457	VND/m3	112,074,021
		Slope Protection	5,790	m2	69,579	VND/m2	402,862,410
	Rain Water Drainage	L gutter	0	m	661,504	VND/m	0
		U Ditch with Cover (1,000*1,000)	0	m	3,758,419	VND/m	0
		Catch Basin (1,200*1,200)	0	nos.	11,099,351	VND/nos	0
	Pavement Work at Sidewalk	Base Course (Crushed Stone 10cm)	22,303	m2	33,146	VND/m2	739,255,238
		Sand and Mortar Buffer	22,303	m2	44,044	VND/m2	982,313,332
		Interlocking Block	22,303	m2	120,258	VND/m2	2,682,114,174
		Concrete Curb	3,760	m	155,062	VND/m	583,033,120
Diffrence (1-2)	Embankment Work	Excavation (by machine)	115,950	m3	17,860	VND/m3	2,070,867,000
		Backfill (by machine)	115,950	m3	8,395	VND/m3	973,400,250
		Embankment (by machine)	365,916	m3	173,451	VND/m3	63,468,572,608
		Transportation of soil	34,785	m3	12,457	VND/m3	433,316,745
		Removal of Excavated Unsuitable Soil	34,785	m3	32,457	VND/m3	1,129,016,745
		Slope Protection	7,710	m2	69,579	VND/m2	536,454,090
	Rain Water Drainage	L gutter	9,000	m	661,504	VND/m	5,953,540,140
		U Ditch with Cover (1,000*1,000)	9,000	m	3,758,419	VND/m	33,825,771,000
		Catch Basin (1,200*1,200)	300	nos.	11,099,351	VND/nos	3,329,805,300
	Pavement Work at Sidewalk	Base Course (Crushed Stone 10cm)	48,340	m2	33,146	VND/m2	1,602,269,022
		Sand and Mortar Buffer	48,340	m2	44,044	VND/m2	2,129,075,509
		Interlocking Block	48,340	m2	120,258	VND/m2	5,813,240,453
		Concrete Curb	5,240	m	155,062	VND/m	812,524,880
Total Cost (VND)							122,077,853,741
	Category	Items	Qty	Unit	Unit Cost		Total Cost
Remove the duplicate part for Embankment Work between Road and Sewerage	Embankment Work	Excavation (by machine)	7,750	m3	17,860	VND/m3	138,415,000
		Backfill (by machine)	7,750	m3	8,395	VND/m3	65,061,250
		Embankment (by machine)	46,040	m3	173,451	VND/m3	7,985,684,040
		Transportation of soil	2,325	m3	12,457	VND/m3	28,962,525
		Removal of Excavated Unsuitable Soil	2,325	m3	32,457	VND/m3	75,462,525
		Slope Protection	5,790	m2	69,579	VND/m2	402,862,410
	Rain Water Drainage	L gutter	0	m	661,504	VND/m	0
		U Ditch with Cover (1,000*1,000)	0	m	3,758,419	VND/m	0
		Catch Basin (1,200*1,200)	0	nos.	11,099,351	VND/nos	0
	Pavement Work at Sidewalk	Base Course (Crushed Stone 10cm)	22,303	m2	33,146	VND/m2	739,255,238
		Sand and Mortar Buffer	22,303	m2	44,044	VND/m2	982,313,332
		Interlocking Block	22,303	m2	120,258	VND/m2	2,682,114,174
		Concrete Curb	3,760	m	155,062	VND/m	583,033,120
Total Cost (VND)							13,683,163,614