TO CR of JICA Timor-Leste OFFICE

Project Title: The Project for the Capacity Development of Road Services in the Democratic Republic of Timor-Leste

Version of the Sheet: Ver.5 (Term: March, 2016 - March, 2019)

Name: Hisashi MUTO

<u>Title: Team Leader/ Road Maintenance1</u> Submission Date: 16th July, 2018

- < I. Summary (all achievements are as of 31st March, 2018) >
- 1. Progress
- 1-1 Progress of Inputs
- 1-1-1 Japanese side

< Short-term experts dispatched to Timor-Leste>

NO	Name	Title	Dispatched Period to Timor-Leste	Changes or delay
			(1 st) 8 th Mar - 10 th Apr, 2016	None
			(2 nd) 14 th Jun - 25 th Jun, 2016	
			(3 rd) 1 st Sep - 18 th Sep, 2016	
4		Team Leader/ Road	(4 th) 23 th Jan - 19 th Feb,2017	
1	Hisashi MUTO	Maintenance 1	(5 th) 24 th Mar - 2 nd Apr, 2017	
			(6 th) 18 th Aug- 10 th Sep, 2017	
			(7 th) 24 th Nov- 14 th Dec, 2017	
			(8 th) 2 nd Feb- 4 th Mar, 2018	
		Deputy Team Leader/	(1 st) 8 th Mar – 15 th Apr, 2016	None
		Road Maintenance 2	(2 nd) 14 th Jun - 13 th Jul, 2016	
2	Makoto MATSUURA		(3 rd) 20 th Sep - 14 th Oct,2016	
			(4 th) 1 st Dec - 16 th Dec,2016	
			(5 th) 23 th Jan - 19 th Feb,2017	
3	Mitsuhide SAITO	Deputy Team Leader/	(1 st) 24 th Mar - 9 th Apr, 2017	Note: Mr.
		Road Maintenance 2	(2 nd) 9 th Jun- 25 th Jun, 2017	Mitsuhide
			(3 rd) 16 th Oct- 12 th Nov,2017	Saito was
			(4 th) 16 th Feb - 11 th Mar,2018	replaced Mr.
				Matsuura in
				Deputy Team
				Leader post.

1 Supervision (2"d) 24" Sep - 14" Oct,2016 (3") 19" Jun - 5" Jul, 2017 (4") 21" Aug-4" Oct,2017 (5") 14" Nor- 21" Dec,2017 (5") 14" Nor- 21" Dec,2017 (5") 14" Nor- 21" Dec,2017 (5") 14" Mar, 2018 5 Sueo HIROSE Quality Control/ Road Repair (1") 29" Mar - 17" Apr, 2016 (3") 14" Aug -12" Sep, 2016 (5") 23" Jan - 22" Feb,2017 (5") 14" Aug -3" Sep, 2017 (5") 14" Aug -3" Sep, 2017 (5") 14" Aug -3" Sep, 2017 (5") 14" Aug -3" Sep, 2017 None 6 Shutaro SAKANAKA Disaster Restoration (1") 11" May - 31" May, 2016 (3") 12" Sep - 6" Oct, 2016 (4") 13" Feb - 8" Mar, 2018 None 7 Kazuharu KOISHIKAWA Disaster Restoration2 (1") 3" Mar - 24" Mar, 2018 (8") 2" Mar - 18" Mar, 2018 Note: This position has been created to assist drafting guideline on slop protection and landslide investigation, etc. Mr.	4	Johji KOIZUMI	Road Construction	(1 st) 19 th Jul -17 th Aug, 2016	None
6 Sueo HIROSE Quality Control/ Read Repair (3") 19" Jun- 5" Jul, 2017 (4") 21" Aug- 4" Oct,2017 (5") 14" Nov- 21" Dec,2017 (6") 30" Jan- 4" Mar, 2018 None 5 Sueo HIROSE Quality Control/ Read Repair (1"9) 28" Mar - 17" Apr, 2016 (3") 14" Aug - 12" Sep, 2017 (6") 4" Aug- 3" Sep, 2017 (6") 4" Aug- 3" Sep, 2017 (7") 4" Aug- 3" Sep, 2017 (6") 16" Feb - 18" Mar, 2018 None 6 Shutaro SAKANAKA Disaster Restoration (4") 13" Feb - 6" Mar, 2017 (5") 17" Apr - 7" May, 2017 (6") 23" Oct - 12" Nov, 2017 (7") 16" Jan- 4" Feb, 2018 (8") 2" Mar - 18" Mar, 2018 None 7 Kazuharu KOISHIKAWA Disaster Restoration2 (1") 3" Mar - 24" Mar, 2018 (1") 3" Mar - 24" Mar, 2018 Note: This position has been created to assist drafting guideline on slop protection assist drafting guideline on slop			Supervision	(2 nd) 24 th Sep - 14 th Oct,2016	
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KOISHIKAWA and landslide investigation, etc. Mr. Koishikawa was assigned for	7		Disaster Restoration2		-
etc. Mr. Koishikawa was assigned for		KOISHIKAWA			-
etc. Mr. Koishikawa was assigned for					investigation,
was assigned for					_
assigned for					Koishikawa
					was
					assigned for
					this position

				since March
				2018.
			(1 st) 17 th Mar - 15 th Sep, 2016	None
		Road Design/ Project	(2 nd) 21 st Jun - 13 th Jul, 2016	
8	Yoshiyuki AKAGAWA	Coordinator	(3 rd) 12 th Sep - 6 th Oct, 2016	
			(4 th) 13 th Feb - 5 th Mar, 2017	
			(1 st) 31 st Jul- 30 th Aug, 2017	Note: Mr.
			(2 nd) 16 th Oct - 23 rd Nov, 2017	Brooker-Jone
			(3 rd) 2 nd Feb - 4 th Mar, 2018	s was
~	Nicholas	Road Design/ Project		replaced Mr.
9	BROOKER-JONES	Coordinator		Akagawa in
				Project
				Coordinator
				post.
10	Kenji MINEGISHI	Structure Design	(1 st) 5 th Apr - 24 th Apr, 2016	None
			(2 nd) 5 th Jul - 4 th Aug, 2016	
			(3 rd) 14 th Nov- 13 th Dec,2016	
			(4 th) 12 th May- 11 th Jun, 2017	
			(5 th) 1 st Sep- 1 st Oct,2017	
			(6 th) 3 rd Nov- 17 th Dec, 2017	
11	Takashi SAITO	Database	(1 st) 19 th Jul - 24 th Aug, 2016	None
			(2 nd) 3 rd Oct - 14 th Oct, 2016	
			(3 rd) 13 th Mar- 12 th Apr, 2017	
			(4 th) 16 th Jun- 2 nd Jul, 2017	
			(5 th) 18 th Aug- 1 st Oct, 2017	
			(6 th) 16 th Feb- 4 th Mar 2018	
12	Masahiko HAYASHI	Landslide	(1 st) 16 th Jun- 28 th June, 2017	Note: Activity
			(2 nd) 27 th Oct - 9 th Dec, 2017	on Landslide
				analysis was
				approved by
				2 nd JCC; Mr.
				Hayashi was
				assigned in
				June 2017.
13	Sohshi MIKAMI	Topographical	(1 st) 19 th Jun- 16 th Jul, 2017	Note: Activity
		Analysis		on Landslide

				analysis was
				approved by
				2 nd JCC; Mr.
				Mikami was
				assigned in
				June 2017.
14	Nao TSUJIMURA	Evaluation/Monitoring	Resident in Timor-Leste	None

< Equipment and materials >

NO	Items	Qty	Unit price	Unit	Total amount
1	Desktop computer	1	1,150	USD	1,150
2	Inclinometer assembly	1		JPY	
3	Dokenbo assembly	1		JPY	

(Remark: Equipment and materials which have a durable years for 2 years and are more than JPY50,000 are listed.)

1-1-2 Timor-Leste side

• Counterpart (C/P) personnel (from MPWTC and DRBFC)

NO	Name	Title of the Project	Engaged Period
1	Rui Hernani F. Guterres	Project Director	20th Feb 2018- at present
2	Milton Ramanata C.Monteiro	Project Manager	20 th Feb 2018- at present
3	Joao Gama	C/P staff	8 th Mar 2016 – at present
4	Joao Pedro Amaral	C/P staff	8 th Mar 2016 – at present
5	Joao Gregorio	C/P staff	8 th Mar 2016 – at present

• Equipment and materials for the project office

NO	Items	Qty	Unit
1	Office space (including desks and chairs)	1	room

1-2 Progress of Activities

NO	Activity	Achievement level
1.1	To review existing management structure and condition of maintenance and rehabilitation for major roads	 JICA Expert Team proposed idea of personal exchange of DRBFC during 3rd JCC. The idea was suggested in order to secure an organized coordination system under the appropriate division of roles among its staff, and formulate a technical staff organization so as to clarify where the responsibility and each competence.
1.2	To conduct periodic/routine inspection.	 JICA Expert Team drafted plan of road inspection for maintenance and rehabilitation works in 2018. This plan was proposed in 3rd JCC in initiation of the March, 2018.
1.3	To update the database based on the inspection result and repair/rehabilitation works of road and bridges.	 JICA Expert Team taught staff of Dept. Maintenance entering inspection result of 2017 of Reg.1 and 4 into GIS database. After technical transfer training, road data among the A08 and A11 (total length of 67.5km) has been compiled into GIS database by trainee.
1.4	To formulate maintenance and repair/rehabilitation plans for next cycle.	 2018 budget plan for maintenance was formulated based on inspection.
1.5	To implement emergency inspections and repair/rehabilitation works when necessity arises.	 JICA Expert Team conducted emergency inspection at Jakarta II landslide in Ainaro, A02.
1.7	To propose framework of road maintenance/rehabilitation for major roads	 JICA Expert Team drafted framework of integration work among the both department of Construction and Maintenance in order to strengthen maintenance capacity. This idea was proposed in 3rd JCC in initiation of the March, 2018. In order to allow better control of each area of responsibility, design and construction separation order method was proposed in 3rd JCC.
2.1	To identify typical rehabilitation/repair work as case study	 In 3rd JCC, below two (2) case study sites and action plan for each site were proposed. (Totally 6 sites were identified.)

		1. Box culvert planning, design and construction of drainage which located in upper section of
		Beduku-Sarlala(Ex.Japan) ongoing rehabilitation project ;
		 Safety control and quality control using check list in Humboe- Letefoho emergency work project.
2.2.	To conduct the case studies for the planning, design check and construction supervision of the project.	 JICA Expert Team conducted safety lecture and observation/practicing safety event. JICA Expert Team conducted OJT on underground data collection by inclinomere in Aituto landslide area. During training, C/P and relevant entities (IPG, UNTL) learned following contents; How to connect devices; How to collect mass movement data; How to collect mass movement data; JICA Expert Team provided lecture on how to operate total station. JICA Expert Team conducted room lecture of mix design for asphalt concrete. After room lecture, trainees observed Marshall Test in the laboratory and another day, field observation of quality control using check list.
2.3	To propose preferable structures for construction management for repair/rehabilitation works through case studies.	 JICA Expert Team proposed site management method using check list for quality control during 3rd JCC.
3.3	To acquire necessary knowledges of civil engineering for design through classroom lectures and case studies.	 JICA Expert Team conducted repeat trainings calculation of stability in order to improve trainee's skills on slope collapse countermeasure design. JICA Expert Team delivered classroom lecture of shear strength test using 'Dokenbo'. After classroom lecture, C/P learned how to do penetration test and share strength test in the field. JICA Expert Team delivered classroom lecture of groin study. This classroom lectures introduced groin as an example of disaster management for Loes river morphological change. Through site inspection, DRBFC technical staff identified damage of embankment; trainees studied this river flow velocity in order to set up groin structures.
3.4	To prepare the technical guideline of investigation and design.	 Guidelines of scouring measures and cross culvert design have been drafted. JICA Expert Team conducted explanation each contents of guideline of scouring. Both before having explanation and after the fact, JICA Expert Team implemented test for leaners judging degree of comprehension of learners based on result of test.

1-3 Achievement of Output

	Indicators of Outputs	Achievement level
1.1	More than 30% of requested budget for road maintenance are distributed.	After election of 2017, the fiscal budget proposal of 2018 has been deliberated by 7th coalition government. However, this proposal has been

		rejected. Until now, GOTL is running by short term budget every two months; and resumption of the budget deliberation will be after the re-election in May, 2018.Achievement level of this output is not ready to be measured.
1.2	Improved road database is utilized for	49% of target national roads condition data have been
	preparation of the annual work plan of	updated into GIS database.
	road maintenance.	
2.1	At least 3 case studies for both	Four (4) sites proposed for case studies, have
	construction and design are	approved in February, 2017 in the 2 nd JCC.
	conducted. (Totally 6 case studies)	
2.2	More than 60% of trainees pass the	Baseline survey resulted that percentage of
	achievement test for construction	examinees exceeded the passing line by respective
	supervision and design.	subject was a) design: 28%, b) quality control: 8%.
3	Technical guideline of investigation	Technical guideline for Scouring has been drafted; it
	and design for slope protection,	will be finalized in March, 2018.
	drainage and measures against	
	scouring are prepared.	

1-4 Achievement of the Project Purpose

Indicators of Project Purpose	Achievement level
Total length of maintained national roads were became 400km.	Achievement level of this output is not ready to be measured.

1-5 Changes of Risks and Actions for Mitigation

 After national election, regime change has been occurred in TL. New government proposed development program and fiscal budget plan; however both development program and budget plan have been rejected by parliament. Timor-Leste President calling for a new legislative election following political impasse in the country. GOTL is running by short term budget every two months; and resumption of the budget deliberation will be after the new legislative election in coming May, 2018.

1-6 Progress of Actions undertaken by JICA

- JICA Timor-Leste shared important information and documents with JICA Expert Team.
- JICA Timor-Leste assisted visa acquisition process for JICA Expert Team.

1-7 Progress of Actions undertaken by Gov. of Timor-Leste

- DRBFC shared necessary information and documents with JICA Expert Team.
- DRBFC has prepared the drawings of road and bridge maintenance based on the road inspection.

1-8 Progress of Environmental and Social Considerations (if applicable)

• No activities for the progress of Environmental and Social Considerations are undertaken.

1-9 Progress of Considerations on Gender/Peace Building/Poverty Reduction (if applicable)

- Not Applicable so far.
- 1-10 Other remarkable/considerable issues related/affect to the project (such as other JICA's projects, activities of counterparts, other donors, private sectors, NGOs etc.)
- No other issues are confirmed so far.

2. Delay of Work Schedule and/or Problems (if any)

• Based on the PDM, the project activities have been implemented as planned.

3. Modification of the Project Implementation Plan

3-1 PO

• PO is not modified from the Monitoring Sheet ver.1.

3-2 Other modifications on detailed implementation plan

• No other modification of the detailed implementation plan is confirmed.

4. Preparation of Gov. of Timor-Leste toward after completion of the Project

• The Gov. of Timor-Leste tries to secure the budget for road maintenance so that the capacity enhancement of DRBFC for road maintenance which is the Project Purpose will be sustainable and contribute to the achievement of Overall Goal.

< II. Project Monitoring Sheet I & II >

• Project Monitoring Sheet I & II are attached as PM Form I and II.

Project Title: The Project for Capacity Development of Road Services in Timor-Leste (CDRS)

MS	ver-3	

Version 3

Dated 11th March, 2018 Implementing Agency: Ministry of Public Works, Transport and Communications Target Group: Officials of Direstorate of Road, Bridge and Flood Control (DRBFC) Period of Project: (Three (3) years) Project Site: Whole Timor-Leste Model Site Narrative Summary Remarks Objectively Verifiable Indicators Means of Verification Important Assumption Overall Goal The maintenance conditions of major roads are OG1 More than 60% of major national roads is in good Budget and staff will be secured a ndicator has been set up and Periodic Road Inspection satisfactory levels. Traffic volume is not increased more than expected. nproved in TL ondition approved in 2nd JCC on ebruary 2017. Project Purpose Capacity of DRBFC for maintenance of major roads in Total length of maintained national roads become the whole country is enhanced. 400km. Periodic Road Inspection Enough number of DRBFC staff ndicator has been set up and he HQs and regional offices is ensured as planned. approved in 2nd JCC on ebruary 2017. Budget for road maintenance and Outputs Output 1: Appropriate road maintenance and rehabilitation for major roads is realized in accordance with annual work plan and annual budget plan. 1-1 More than 30% of requested budget for road maintenance are distributed. udget Report Budget for road maintenance and -2 Inspection handwritten ray ata of 2017 inputted to GIS atabase (67.5km) nanagement is ensured. The trained DRBFC personnel continue to work for the Project (They do not quit the Project) 1-2 Improved road database is utilized for preparing the annual work plan of road maintenance. Ionitoring Sheet Dutput 2: Capacity of DRBFC construction management for maintenance and rehabilitation ncluding slope protection is improved through case studies in the whole country. 2-1. At least 3 case studies for construction and 3 case studies for design are conducted (Totally 6 case Monitoring Sheet 1. Progress of case study at tes where approved by 2nd CC; 2 another case study site en natural disasters wil Inforese studies fo studies). not occur which may destroy construction works under case 2-2. More than 60 % of trainees pass the achievement Achievement test studies Schedule of completion of Output 3: Technical guideline of investigation and 3. Technical guideline of investigation and design for Technical guideline prepared design for maintenance and rehabilitation are provided as a tool for more appropriate design slope protection, drainage and measures against chnical guideline was oposed in 3rd JCC. scouring are prepared. cluding slope protection Activities Inpu The Timor-Leste Side Assignment of C/Ps Project Director The Japanese Side 1. Dispatch of the Japanese experts Short-term experts: - Team leader / Road maintenance 1 1.1 To review existing management structure condition of maintenance and rehabilitation for major DRBFC's budget necessary for he Project is allocated by TL he Project is overnment. Project Manager DRBFC Staff oads. I.2 To conduct periodic/routine inspection. - learn leader / koad maintenance 1 Deputy team leader / koad maintenance 2 Road construction supervision - Quality control / Road repair - Disaster restoration - Road design / Project coordinator - Structure design 2. Assignment of Trainees In accordance of necessity 1.3 To update the database based on the inspection esult and repair/rehabilitation works of roads and ridges. 3. Facillities and Equipment Project office Database - Evaluation / Monitoring - Other areas if needed .4 To formulate maintenance and repair/rehabilitatio Equipment and tools sues: Due to political factor lans for next cycle. 1.5 To implement emergency inspections and epair/rehabilitation works when necessity arises. evelopment program and budg an for 2018 was rejected by Recurrent costs Expenses for equipment maintenance Spare parts Facilities and equipment In accordance with necessity of activities liament Transportation fees of C/Ps and trainees untermeasures: Identified 1.6 To undertake appropriate road naintenance/rehabilitation works by following annual work and budget plans which reflect priorities within he limited budget. Expenses for contract-out of works Necessary expenditures for case studies C/Ps' wages and allowances ngoing project implementing by lulti-year budget in order to carr ut case study. Training in Japan In accordance with necessity of activities 1.7 To propose appropriate framework of road naintenance and rehabilitation for major roads. 2.1 To identify typical rehabilitation and repair works of major roads in the whole country as case studies. 2.2 To conduct the case studies for the planning, design and construction supervision of the project 2.3 To propose preferable structures for construction nanagement for repair/rehabilitation and maintenand works through case studies. 3.1 To review existing technical documents for road maintenance and rehabilitation. 3.2 To review and identify factors of failure from past examples of damaged rehabilitation and construction vorks 3.3 To acquire necessary knowledges of civil engineering for design through classroom lectures and case studies. 3.4 To prepare the technical guideline of investigation and design. 3.5 To reflect the lessons learned from case studies to he technical guideline 3.6 To disseminate the technical guideline for ncerned parties

Project N	/lonite	orin	g Si	heet	II (F	Revi	sion	of F	lan	of C)pera	atio	n)							Version 3 Dated 11th March, 20	18
Project Title: The Project for the Capa	city C Plan)eve	20 [.]		t of		d Se 017	rvic		<u>n th</u> 2018		emo	<u>cra</u>		epu		: of 2020		or-Leste(CDRS)		litoring
Inputs	Actual	I			_	I	Π	_	1	I 1	I IV		Π	Π	_	1	C]]	I IV		Issue	Solution
Expert Team Leader/Road Maintenance 1 /Mr. Hisashi MUTO	Plan														тп	Ш	m		_	-	-
/Mr. hisashi MUTO Deputy Team Leader/Road Maintenance 2 /Mr. Makoto MATSUURA Deputy Team Leader/Road Maintenance 2	Plan Actual	(П	<u>nn</u>	П		F		Ħ	Ħ	H	Ħ			2017 March, Mr.Matsuura resigned.	-
/Mr. Mitsuhide SAITO	Plan Actual	⊞	П					П		П			Ш	Ш	П	П	П	Ħ	Mr. Mitsuhide Saito was replaced Mr.	-	Mr. Mitsuhide Saito was dispatched as successor o
Road Construction Supervision /Mr. Johii KOIZUMI Quality Control/Road Repair	Plan Actual Plan	Ħ	Ш		Ш					П		曲	Ħ	曲	Ħ	Щ	Ш	Ш		-	-
/Mr. Sueo HIROSE Disaster Restoration	Actual Plan	Ħ			Ħ			Ħ		Ħ		Ħ	Ħ	ĦĦ	Ħ	Ħ	Ħ	Ħ		- 2017 July, Mr.Sakanaka	- He will continue his
/Mr. Shutaro SAKANAKA Road Design/Project Coordinator	Actual Plan	Ħ						H		Ш	Ш		Ш	Ħ	Ш	Ш	Ш	Ш		resigned. 2017 July, Mr.Akagawa	assignment with loan
/Mr. Yoshivuki AKAGAWA Road Design/Project Coordinator	Actual Plan Actual	曲		╏╏╿	Ш			Ш		Ш		Ħ	Ш		Ш	Ш	丗	Ш	Mr. Brooker-Jones was replaced Mr.	resigned.	Mr. Brooker-Jones was dispatched as successor of
/Mr. Nicholas BROOKER-JONES Structure Design /Mr. Kenji MINEGISHI	Plan Actual	曲	Ĥ					Ħ	ΠH	H		Ħ	Ħ	ΗH	Ħ	Н	Ħ			-	-
Database /Mr. Takashi SAITO Landslide	Plan Actual	⊞						Н		Ш				Ш	Ш		Н		Activity on Landslide analysis was Activity on Landslide analysis was	-	-
/Mr. Masahiko HAYASHI Topographical Analysis	Plan Actual Plan	ttt	+	ЦЦ	盽			Ħ			ĦĦ	Ħ		Ħ		Ш	Ш	ĦH	Activity on Landslide analysis was Activity on Landslide	-	-
/ <u>Mr. Sohshi MIKAMI</u> Evaluation/Monitoring	Actual Plan	曲	Н	H	Ħ	Ħ			HT	Ш	Ħ			Ħ	Ħ	Н	Ħ	Ħ	analysis was	-	-
Ms. Nao TSUJIMURA Equipment	Actual									Ш							П			-	-
	Plan Actual Plan	曲	Ш		Ħ			Ħ		Ħ		Ħ	Ħ		Ħ	Ħ	Ħ	ĦĦ			
	Actual Plan Actual	▦					HH	Ш	Ш		Ħ			Ħ		Щ	Ш				
		Ħ	Ш		Ħ	ĦĦ		Ħ	ĦĦ	丗	ĦĦ	Ħ	Ħ	ĦĦ	井	Ħ	Ħ		_		
_																					
Training in Japan	Plan	曲	Ш	₩	雦	Ш		Щ	Ш	Ħ		雔	曲	Ш	⋕	Щ	₩	Щł			
In-country/Third country Training	Plan Actual Plan Actual	曲	벢		曲	曲		Ħ	Щİ	丗		曲	Ш	Ш	\parallel	Щ	Ш	Ш	1		
Activities	Actual	Щ	20		Щ		017	Щ		2018	ш	μt	20	111	Щ	Ш	2020	Ш	Responsible Organization		
Sub-Activities	Actual	1	I	I		I	Π		1	II I	I IV		I				1	I N		Achievements	Issue & Countermeasure
Output 1: Appropriate road maintenance and rehabil 1.1 To review existing management structure and	litation Plan	for n	najor	roads	s is re	alized	in ac	cord	ance	with	annua	al wor	rk pla	n and	ann	ual b	udge	*t 		Orgaization and personal	
condition of maintenance and rehabilitation for major roads	Actual	Ш		Ш	Ħ	Ш	Шİ	Ш	Ш	Ш	Ш	Π	Ш	Ш	Ħ	Ш	Π	Ш	1	exchange have been proposed at 3rd JCC	
1.2 To conduct the periodic/routine inspection	Plan Actual	Щ		₩∏	Щ	ļ	╢╢	Щ	ЩТ	Щ	ЩĪ	Щ	ЩŢ	Щ	ЦĪ	Щ	H	Щ∏		Inspection plan for 2018 and IRI inspection system were	
1.3 To update the database based on the inspection	Actual	╟╫	╢	₩₩	₩	╟╫	₩₩	₩	₩	₩	₩₩	₩	╟╢	╢╢	╢	₩	₩	₩₩		proposed in 3rd JCC. 2017 inspection raw data	Issue: As result of the Parliament election, regime
result and repair/rehabilitation works of roads and bridges	Actual	HH	₩	╀╫	₩	₩	┡╫┼	₩	₩		₩₩	₩	₩╢	₩	₩	₩	₩	╢╢	-	were inputted into GIS database.(67.5km)	change was occurred. Due to political factor, budget
1.4 To formulate maintenance and	Plan	┢╫╢	₩	╢		╟╫		H	┞┼┤	╢		₩	╟╫	$\parallel \parallel$	╢	₩	₩	╢╢		2018 budget plan for maintenance was	plan for 2018 was rejected Activities of 1.2, 1.3, 1.4, 1
repair/rehabilitation plans for next cycle	Actual	Ш	Ш	Ш		Ш		Ш	Ш	Ш		Ш	Ш	Ш	⋣け	Ш	Ш	Ш		formulated based on inspection	will be delayed. Countermeasure: 2018
1.5 To implement emergency inspections and	Plan	Ш			\prod				∭	∏∏		\prod		\prod			∏	∭		Emergency inspection on A02 at Jakarta II in Ainaro	inspection work will carry o with integration working
repair/rehabilitation works when necessity arises	Actual	Ш	Ш	∭		Ш					Ш	Ш	\square	Ш	Ш	Ш	Ш	Ш		was conducted.	members of Dept. Project and Dept. Maintenance in order to increase work
1.6 To undertake appropriate road maintenance/ rehabilitation works by following annual work and hudgest along which a first an article within the limited	Plan	Щ	Щ	ЦП	Į	Щ	ЩТ		Щ	Щ	ЩТ	Щ	Щ	Щ	ЩĪ	Щ	Щ	Щ			order to increase work efficiency.
budget plans which reflect priorities within the limited budget	Actual	Щ	Щ	$\parallel \parallel$	Щ	Щ		Ш	Щ	Щ	Щ	Щ	Щ	Щ	Щ	Щ	Щ	Щ	ļ	Integration work	ļ
 To propose appropriate framework of road maintenance/rehabilitation for major roads 	Plan Actual	HH	₩	╢╢	₩	\mathbb{H}	╢╢	╢	₩₩	₩		╉╫┥	╟╢	₩	╢	╢	₩	╢╢	-	Integration work among the both department of Construction and	
Output 2: Capacity of DRBFC construction manager		r mai	nten	ancea	and re	ehabil	itation	is ir	nprov	ed th	rough	n cas	e stu	dies in	h the	who	le co	untry	1	construction and	
including slope protections	Plan	Ш					Ш	Ш	Ш	Ш	Ш	Ш	Ш	m	Ш	Ш	Ш	Ш		2 case study sites and action plan for each site	1
2.1 To identify typical rehabilitation and repair works of major roads in the whole country as case studies	Actual	HH					┞┼┼	ℍ	₩	₩	₩₩	₩	HH	╢╢	₩	₩	₩	⊞	-	were proposed in 3rd JCC. (totally 6 sites were	
2.2 To conduct the case studies for the planning,	Plan	ĦĦ	П					H		Ħ		Ħ			Ħ	Ħf	Ħf			identified Safety lecture and observation/practicing safety	
design check, and construction supervision of the project	Actual	ĦĦ	$^{++}$									Ħ			Ħ	Ħf	Ħf			event were conducted; OJT on mass movement	
2.3 To propose preferable structures for	Plan	ittt	\mathbf{H}					m		₩						Ħf	₩			data collection by Check list for quality control	
construction management for repair/rehabilitation works through case studies	Actual	Ш		Ш	Π			Π		Ш		Ш		Ш	Π		Ш			have been proposed during 3rd JCC	
Output 3: Technical guideline of investigation and d including slope protection.	esign fo	or ma	ainte	nance	and	rehab	ilitatio	n ar	e prov	ided	as a t	ool fo	or mo	ore ap	prop	riate	desi	gn			
3.1 To review existing technical documents for road	Plan	Π		Ш	Ш	Ш	Ш	Ш	Ш	Ш	Ш	Ш	Ш	Ш	Ш	Ш	Ш	Ш			
maintenance and rehabilitation	Actual	ЩĮ	Ш		Щ	Щ	₩	Щ	₩	Щ	Шſ	Щ	Щ	Щ	Щ	Щ	Щ	Щ			
3.2 To review and identify factors of failure from past examples of damaged rehabilitation and coordination works.	Plan	Щ	Ш		Щ	Щ	₩	Щ	$\parallel \parallel$	Щ	$\parallel \parallel$	Щ	Щ	Щ	Щ	Щ	Щ	Щ	-		
construction works 3.3 To acquire necessary knowledges of civil	Actual	HH	H		╢	Ш		Н	₩₩	₩	₩₩	₩	₩	₩	╢	₩	₩	₩₩		classroom lectures on	
3.3 To acquire necessary knowledges of civil engineering for design through classroom lectures and case studies	Actual	Щ	Щ			Щ		Щ	$\parallel \parallel$	₩	₩₩	₩	ЩI	₩	╢	Щ	₩	Щ	-	share strength test and penetration test by 'Dokenbo', groin study were	
3.4 To prepare the technical guideline of	Plan	╟╫	₩	┞╎╎╿				╢	╢╢	₩	₩₩	₩	╟╢	╢╢	╢	╢	₩	₩₩		conducted Draft guide line of scouring	
investigation and design	Actual	Ш	Ш	Ш	Ħ	Ш		Ш	Ш		Ш	Ħ	Ш	Ш	⋣	Ш	Ш	Ш		measures and cross culvert design have been prepared	
3.5 To reflect the lessons learned from case studies to the technical guideline	Plan	Щ	Щ	ЦП	Щ	ЩТ	Щ	Щ	Щ	Щ	ЩŢ	Щ	Щ	Щ	Щ	Щ	Щ	Щ			
3.6 To disseminate the technical guideline for	Actual	╟╫	₩	╢╢	₩	\mathbb{H}	₩₩	╢	₩	₩	╢╢	₩	₩₩	₩	╢	╢	₩	₩₩			
concerned parties	Actual	Ш	Ш	Ш	Ш	丗	Ш	Ħ	Ш	Ш		Ш	Ш	Ш	Ш	Ш	Ш	Ш			
Duration / Phasing	Plan Actual	Ħ	Ħ		Ħ	Ħ	₩Ī	H	₩Ī	Ħ	⊞Ī	Ħ	Ð	Ħ	Ħ	Ħ	Ħ	⊞Ī			
Monitoring Plan	Plan		20	16		2	017			2018			20	19			2020		Bomorko	Issue	Solution
Monitoring	Actual	I	111			гітг		111	TTTT		[111	111			TTT	TTT	I IV			
Joint Coordination Committee	Plan Actual Plan	曲	Ħ	₩	HF.	ЩŦ	₩	H	H	Ħ	HП	Æ	開	冊	冊	冊	冊	HП		-	-
Set-up the Detailed Plan of Operation Submission of Monitoring Sheet	Plan Actual Plan	曲				Ħ	▦		Ħ	⋕	⊞	Ħ	曲	曲	⊞	田	田	曲	1	-	-
Joint Monitoring	Actual Plan Actual	ЩŦ	⋕			Ħ	╟╟		ЩĮ	Ħ	₩	Ħ	Ħ	卌	⋕	Щ	Ħ	ЩĮ	-	-	-
Post Monitoring	Plan	曲	Η	Ħ		Ħ	曲	Ш	Ш	Ħ	Ħ	曲	田	田	Ħ	Ħ	Ħ	Ш			
Reports/Documents	Plan Actual Plan	曲	卄	₩	雦	Щŧ	╞╫╫	曲	HH.	丗		曲	曲	曲	井	卄	丗	Щł	1		
Technical Guideline																	曲	Ш			
Project Completion Report	Plan		TT						Ш	Ш			HTT	Ħ			冊	Щ			
Public Relations	/	411	ш		44-	ΗН	ΗН	Щ	ΗН	##	нн	44	щμ	111	44	ш	444	ΗН	+		I
	Plan Actual Plan Actual	ΗН	₩	┼┼┼	++++	HH	++++	Ht	HH	₩	₩₩	HH	HH	ΗH	₩	₩	₩	HH			

TO CR of JICA Timor-Leste OFFICE

Project Title: The Project for the Capacity Development of Road Services in the Democratic Republic of Timor-Leste

Version of the Sheet: Ver.6 (Term: July, 2018 – October, 2018)

Name: Hisashi MUTO

<u>Title: Team Leader/ Road Maintenance1</u> Submission Date: 31st October, 2018

- < I. Summary (all achievements are as of 31st October, 2018) >
- 1. Progress
- 1-1 Progress of Inputs
- 1-1-1 Japanese side

< Short-term experts dispatched to Timor-Leste>

NO	Name	Title	Dispatched Period to Timor-Leste	Changes or delay
1	Hisashi MUTO	Team Leader/ Road Maintenance 1	$\begin{array}{c} (1^{st}) \ 8^{th} \ Mar - 10^{th} \ Apr, \ 2016 \\ (2^{nd}) \ 14^{th} \ Jun - 25^{th} \ Jun, \ 2016 \\ (3^{rd}) \ 1^{st} \ Sep - 18^{th} \ Sep, \ 2016 \\ (4^{th}) \ 23^{rd} \ Jan - 19^{th} \ Feb, \ 2017 \\ (5^{th}) \ 24^{th} \ Mar - 2^{nd} \ Apr, \ 2017 \\ (6^{th}) \ 18^{th} \ Aug - 10^{th} \ Sep, \ 2017 \\ (7^{th}) \ 24^{th} \ Nov - 14^{th} \ Dec, \ 2017 \\ (8^{th}) \ 2^{nd} \ Feb - 4^{th} \ Mar, \ 2018 \\ (9^{th}) \ 8^{th} \ Jun - 1^{st} \ Jul, \ 2018 \end{array}$	None
			$(10^{\text{th}})19^{\text{th}}$ Sep – 12^{th} Oct, 2018	
2	Makoto MATSUURA	Deputy Team Leader/ Road Maintenance 2	 (1st) 8th Mar – 15th Apr, 2016 (2nd) 14th Jun – 13th Jul, 2016 (3rd) 20th Sep – 14th Oct,2016 (4th) 1st Dec – 16th Dec,2016 (5th) 23rd Jan – 19th Feb,2017 	None
3	Mitsuhide SAITO	Deputy Team Leader/ Road Maintenance 2	$(3^{rt}) 23^{rt}$ Jun – 9 th Apr, 2017 $(2^{nd}) 9^{th}$ Jun – 25 th Jun, 2017 $(3^{rd}) 16^{th}$ Oct – 12 th Nov,2017 $(4^{th}) 16^{th}$ Feb – 11 th Mar,2018	Note: Mr. Mitsuhide Saito replaced Mr.
			$(5^{\text{th}}) 26^{\text{th}} \text{Apr} - 16^{\text{th}} \text{May},2018$	Matsuura in

			(6 th) 7 th Sep – 28 th Sep,2018	Deputy Team
				Leader post.
4	Johji KOIZUMI	Road Construction	(1 st) 19 th Jul – 17 th Aug, 2016	None
		Supervision	(2 nd) 24 th Sep – 14 th Oct,2016	
			(3 rd)19 th Jun – 5 th Jul, 2017	
			(4 th) 21 st Aug – 4 th Oct,2017	
			(5 th) 14 th Nov – 21 st Dec,2017	
			(6 th) 30 th Jan – 4 th Mar, 2018	
			(7 th) 8 th Jun – 1 st Jul, 2018	
			(8 th) 7 th Sep – 13 th Oct, 2018	
			(1 st) 28 th Mar – 17 th Apr, 2016	None
			(2 nd)13 th May – 11 th Jun, 2016	
			(3 rd) 14 th Aug – 12 th Sep, 2016	
5	Sueo HIROSE	Quality Control/ Road	(4 th) 7 th Oct – 14 th Oct, 2016	
		Repair	(5 th) 23 rd Jan – 22 nd Feb,2017	
			(6 th) 4 th Aug – 3 rd Sep, 2017	
			(7 th) 16 th Feb – 18 th Mar, 2018	
			(1 st) 11 th May – 31 st May, 2016	None
			(2 nd) 28 th Jun – 21 st Jul, 2016	
			(3 rd) 12 th Sep – 6 th Oct, 2016	
			(4 th) 13 th Feb – 8 th Mar, 2017	
6	Shutaro SAKANAKA	Disaster Restoration	(5 th) 17 th Apr – 7 th May, 2017	
			(6 th) 23 rd Oct – 12 th Nov, 2017	
			(7 th) 16 th Jan – 4 th Feb, 2018	
			(8 th) 2 nd Mar – 18 th Mar, 2018	
			(9 th) 1 st Jun – 17 th Jun, 2018	
			(1 st) 3 rd Mar – 25 th Mar, 2018	Note:
			(2 nd) 15 th Jun – 8 th Jul, 2018	Disaster
			(3 rd) 7 th Sep – 30 th Sep, 2018	Restoration 2
				has been
7	Kazuharu	Disaster Restoration2		created as
	KOISHIKAWA			new position;
				Mr.
				Koishikawa
				was
				assigned for

				this position
				in March
				2018.
			(1 st) 17 th Mar – 15 th Sep, 2016	None
		Pood Docian/ Project	$(2^{nd}) 21^{st}$ Jun – 13 th Jul, 2016	NONE
8	Yoshiyuki AKAGAWA	Road Design/ Project		
		Coordinator	(3 rd) 12 th Sep – 6 th Oct, 2016	
			(4 th) 13 th Feb – 5 th Mar, 2017	
			(1 st) 31 st Jul – 30 th Aug, 2017	Note: Mr.
			(2 nd) 16 th Oct – 23 rd Nov, 2017	Brooker-Jone
	Nicholas	Road Design/ Project	(3 rd) 2 nd Feb – 4 th Mar, 2018	s replaced
9	BROOKER-JONES	Coordinator	(4 th) 8 th Jun – 1 st Jul, 2018	Mr. Akagawa
	Dicoonlance		(5 th) 7 th Sep – 30 th Sep, 2018	in Project
				Coordinator
				post.
10	Kenji MINEGISHI	Structure Design	(1 st) 5 th Apr – 24 th Apr, 2016	None
			(2 nd) 5 th Jul – 4 th Aug, 2016	
			(3 rd) 14 th Nov – 13 th Dec,2016	
			(4 th) 12 th May – 11 th Jun, 2017	
			(5 th) 1 st Sep – 1 st Oct,2017	
			(6 th) 3 rd Nov – 17 th Dec, 2017	
			(7 th) 6 th Apr – 13 th May, 2018	
			(8 th) 24 th Aug – 30 th Sep, 2018	
11	Takashi SAITO	Database	(1 st) 19 th Jul – 24 th Aug, 2016	None
			(2 nd) 3 rd Oct – 14 th Oct, 2016	
			(3 rd) 13 th Mar – 12 th Apr, 2017	
			(4 th) 16 th Jun – 2 nd Jul, 2017	
			(5 th) 18 th Aug – 1 st Oct, 2017	
			(6^{th}) 16 th Feb – 4 th Mar 2018	
			$(7^{\text{th}}) 5^{\text{th}}$ May – 19^{\text{th}} May, 2018	
			$(8^{\text{th}}) 28^{\text{th}} \text{Aug} - 11^{\text{th}} \text{Oct}, 2018$	
12	Masahiko HAYASHI	Landslide	(1^{st}) 16 th Jun – 28 th June, 2017	Note: Activity
.2			$(2^{nd}) 27^{th} \text{ Oct} - 9^{th} \text{ Dec}, 2017$	on Landslide
			(3^{rd}) 18 th Mar – 18 th Apr, 2018	analysis was
				approved by 2 nd JCC; Mr.
				Hayashi was

				assigned in
				June 2017.
13	Sohshi MIKAMI	Topographical	(1 st) 19 th Jun – 16 th Jul, 2017	Note: Activity
		Analysis	(2 nd) 18 th Mar – 18 th Apr, 2018	on Landslide
				analysis was
				approved by
				2 nd JCC; Mr.
				Mikami was
				assigned in
				June 2017.
14	Nao TSUJIMURA	Evaluation/Monitoring	Resident in Timor-Leste	None

< Equipment and materials >

NO	Items	Qty	Unit price	Unit	Total amount
1	Desktop computer	1	1,150	USD	1,150
2	Inclinometer assembly	1	1,585,800	JPY	1,585,800
3	Borehole casing	1	404,400	JPY	404,400
4	Dokenbo assembly	1	133,000	JPY	133,000

(Remark: Equipment and materials which have a durable years for 2 years and are more than JPY 50,000 are listed.)

1-1-2 Timor-Leste side

• Counterpart (C/P) personnel (from MPWTC and NDRBFC)

NO	Name	Title of the Project	Engaged Period
1	Rui Hernani F. Guterres	Project Director	20 th Feb 2018 to date
2	Milton Ramanata C. Monteiro	Project Manager	20 th Feb 2018 to date
3	Joao Gama	C/P staff	8 th Mar 2016 to date
4	Joao Pedro Amaral	C/P staff	8 th Mar 2016 to date
5	Joao Gregorio	C/P staff	8 th Mar 2016 to date

• Equipment and materials for the project office

N) Items	Qty	Unit
1	Office space (including desks and chairs)	1	room

1-2 Progress of Activities

NO	Activity	Achievement level
1.2	To conduct periodic/routine inspection.	 Periodic/routine inspection has been done along A03 from Loes to Bobonaro and A04 from Tibar to Gleno; Road inspection using drive recorder has been conducted from Dili to Ermera and Dili to Maliana. Urban & national roads surveys were conducted by Project Department. After 3rd JCC, NDRBFC inspectors were practicing proposed data collection method with drive recorder; video data was used to re-confirm items and efficiency of the data collection was improved.
1.3	To update the database based on the inspection result and repair/rehabilitation works of road and bridges.	 JICA Expert Team conducted training about how to grasp geographic coordination on a map. JICA Expert Team trained staff of Maintenance Department about how to compile inspection results into GIS database continuously. After technical training, the inspection results for a total length of 82.7 km have been compiled into GIS database by trainees. Collected data from urban & national road surveys were inputted into GIS database (16.8 km).
1.4	To formulate maintenance and repair/rehabilitation plans for next cycle.	 Draft 2019 work plan for maintenance and rehabilitation was formulated based on inspection results.
1.5	To implement emergency inspections and repair/rehabilitation works when necessity arises.	 Emergency inspection on A03 at Loes River was conducted. After the inspection, JICA expert team held a seminar to suggest a countermeasure for river bank protection of Loes River.
1.6	To undertake appropriate road maintenance/ rehabilitation works by following annual work and budget plans which reflect priorities within the limited	 Based on inspection results, NDRBFC is preparing 5-year and 2019 annual plans.

	budget.		
2.2.	To conduct the case studies for the planning, design check and construction supervision of the project.	 staff conducted monitori through data collection be water level indicator. (Si JICA Expert Team conservation/practicing coordination meetings, chairperson and comminate out site inspections using (Site: A02 bypass road regarding 1) design. NDR group conducted workslaregarding 1) design flac capacity of culvert. Predivafted guideline. (Site: JICA Expert Team comminate of the construction stage for 1) and 3) construct Humboe-Letefoho) JICA Expert Team examinate of the construct of the construction stage for 1) and 3 construct of the construct of	onducted safety lectures and safety event. During the NDBRFC staff acted as the ttee members and then carried ing checklists for safety patrol. named Ex. Japan Road) nized training to make a plan for BFC inter-departmental working hop to present their culvert plan ood catchment and 2) design esented plan was made using the Sarlala, Ex. Japan Road) nducted explanation meeting to cklists to be utilized in each quality control, 2) safety control
		Subject	Number of the people whose test scores have improved after training
		Landslide investigation	17 people out of 17
		Bridge substructure protection (Scouring and protection block)	5 people out of 14
		Culvert planning and design	6 people out of 11
		Quality control, Safety control and Construction management	N/A Pre-test was given in June; the result of the re-examination after the training will be reported in next reporting period.
		Slope protection	3 people out of 7
3.3	To acquire necessary knowledges of civil engineering for design through classroom lectures and case studies.	bridge substructure production of the design of th	vided classroom lectures about otection design along with the ided classroom lectures for box esign along with the drafted

		 guideline. JICA Expert Team organized a workshop by a geologist from the Public Institute of Petroleum and Geology to introduce landslide phenomena of Timor-Leste and investigation procedure. Repeat lecture about operation of total station was provided by JICA Expert Team.
3.4	To prepare the technical guideline of investigation and design.	 Draft guidelines for slope protection, bridge substructure protection, culvert design, and landslide investigation have been prepared. Draft guidelines for slope protection, bridge substructure protection and culvert design have been submitted to NDRBFC and other entities.
3.5	To reflect the lessons learned from case studies to the technical guideline	 4 focal points of NDRBFC were nominated to compile drafted guidelines. The 4th JCC approved activities to confirm the efficiency and applicability of drafted guidelines. Moreover, drafted guidelines will be introduced to projects other than case studies.

1-3 Achievement of Output

	Indicators of Outputs	Achievement level
1.1	More than 30% of requested budget for road maintenance are distributed.	After the re-election, USD 1,000,000 was secured for road maintenance in 2018. However, this budget has been canceled because of insufficient implementation period. Distribution of the annual budget will be determined at the end of December 2018. Therefore achievement level of this output is not ready to be measured.
1.2	Improved road database is utilized for preparation of the annual work plan of road maintenance.	65% Proposed data collection method with drive recorder was adopted. However, volume of data was insufficient to measure its utilization. Moreover, improvement of the database is not ready to be measured.
2.1	At least 3 case studies for both construction and design are conducted. (Totally 6 case studies)	53% Case studies to improve the capacities of survey and design and safety control were conducted as planned. Implementation of case studies for construction management have been delayed due to delayed budget allocation. Those case studies will be conducted in the project extension period.
2.2	More than 60% of trainees pass the achievement test for construction supervision and design.	Baseline survey results showed that the percentage of examinees exceeded the passing line by respective subject was a) design: 28%, & b) quality control: 8%. In order to grasp the knowledge improvement of trained NDBRFC staff, JICA Expert Team gave mock exams continuously. The trainees' scores from the mock exams have been increasing step by step. The final achievement test will be given after the completion of the case studies. Therefore, achievement level of this output is not ready to be

		measured.
3	Technical guideline of investigation and design for slope protection, drainage and measures against scouring are prepared.	72% Draft guidelines for slope protection, bridge substructure protection, culvert design, and landslide investigation have been prepared. However, checks for whether prepared guidelines can be utilized by NDBRFC have been insufficient. In order to confirm their efficiency and applicability, guidelines will be introduced to projects other than case studies as well as dissemination of guidelines will be conducted in project extension period.

1-4 Achievement of the Project Purpose

Indicators of Project Purpose	Achievement level
Total length of maintained national roads were became 400km.	Achievement level of this output is not ready to be measured.

1-5 Changes of Risks and Actions for Mitigation

1-6 Progress of Actions undertaken by JICA

- JICA Timor-Leste shared important information and documents with JICA Expert Team.
- JICA Timor-Leste assisted visa acquisition process for JICA Expert Team.

1-7 Progress of Actions undertaken by Gov. of Timor-Leste

- DRBFC shared necessary information and documents with JICA Expert Team.
- DRBFC has prepared the drawings of road and bridge maintenance based on the road inspection.

1-8 Progress of Environmental and Social Considerations (if applicable)

• No activities for the progress of Environmental and Social Considerations are undertaken.

1-9 Progress of Considerations on Gender/Peace Building/Poverty Reduction (if applicable)

• Not Applicable so far.

1-10 Other remarkable/considerable issues related/affect to the project (such as other JICA's projects, activities of counterparts, other donors, private sectors,

NGOs etc.)

• No other issues are confirmed so far.

2. Delay of Work Schedule and/or Problems (if any)

• Based on the PDM, the project activities have been implemented as planned.

3. Modification of the Project Implementation Plan

3-1 PO

• PO was modified after the 4th JCC. The latest version was ver.6.

3-2 Other modifications on detailed implementation plan

• General issue:

As a result of the parliamentary election, a regime has change occurred. Due to political factors, the budget plan for 2018 was rejected. Under the influence of delayed budget allocation, implementation of activities 1.2, 1.3, 1.4, 1.6, 2.2, 2.3 and 3.5 has been delayed.

- <u>Countermeasures have been taken by JICA Expert Team:</u>
 - In the coordination meeting between CDRS project and NDRBFC, CDRS Deputy Team Leader requested the Director of NDRBFC to prioritize allocation of the budget for the projects selected for case studies.
 - 2) CDRS team leader suggested to NDBRFC that the 2018 inspection work should be carried out by collaboration between relevant staff of Department of Project and Department of Maintenance in order to increase work efficiency with a limited budget.
- Modifications of implementation plan and project period:

A 9-month extension of project term was approved at the 4th JCC. Those delayed activities mentioned above will be conducted during extension period.

4. Preparation of Gov. of Timor-Leste toward after completion of the Project

• The Gov. of Timor-Leste tries to secure the budget for road maintenance so that the capacity enhancement of NDRBFC for road maintenance which is the Project Purpose will be sustainable and contribute to the achievement of Overall Goal.

< II. Project Monitoring Sheet I & II >

• Project Monitoring Sheet I & II are attached as PM Form I and II.

Project Monitoring Sheet I (Revision of Project Design Matrix)

Version 4 Dated 31st October, 2018

Project Title: The Project for Capacity Development of Road Services in Timor-Leste (CDRS) Implementing Agency: Ministry of Public Works, Transport and Communications Target Group: Officials of Directorate of Roads. Bridges and Flood Control (DRBFC) Period of Project: (Three (3) years and nine(9) month)

Project Site: Whole Timor-Leste	Model Site:				
Narrative Summary	Objectively Verifiable Indicators	Means of Verification	Important Assumption	Achievement	Remarks
Overall Goal					
The maintenance conditions of major roads are improved in TL.	OG1 More than 60% of major national roads is in good Periodic Road Inspection		Budget and staff will be secured at satisfactory levels. Traffic volume is not increased	Indicator was set up and approved at 2nd JCC in	Q.mooth
		-	more than expected.	repruary zui /.	extension of
Project Purpose					project term was
Capacity of DRBFC for maintenance of major roads in Total length of maintained national roads become the whole country is enhanced.	Total length of maintained national roads become 400km.	Periodic Road Inspection	RBFC staff in I offices is	Indicator was set up and approved at 2nd JCC in	approved at 4th .ICC
			ensured as planned.	February 2017.)
			Budget for road maintenance and management is ensured.		
Outputs					
Output 1: Appropriate road maintenance and 1-1 More than 30% of reque rehabilitation for main: roads is realized in accordance maintenance are distributed	1-1 More than 30% of requested budget for road maintenance are distributed	Budget Report	Budget for road maintenance and 1-1.N/A	1-1.N/A	
with annual work plan and annual budget plan.		-		1-∠. co.%	
	1-2 Improved road database is utilized for preparing the Monitoring Sheet annual work plan of road maintenance.		The trained DRBFC personnel continue to work for the Project		
Output 2: Capacity of DRBFC construction	2-1. At least 3 case studies for construction and 3 case	Monitorina Sheet	(They do not quit the Project)	2-1.53%	evtension of
ation In case	studies for design are conducted (Totally 6 case studies)		Unforeseen natural disasters will	2-2. N/A	project term was
			construction works under case		approved at 4th
	2-2. More than 60 % of trainees pass the achievement	Achievement test	studies.		JCC.
Technical guideline of investigation and maintenance and rehabilitation are provided or more appropriate design including slope	 Technical guideline of investigation and design for slope protection, drainage and measures against scouring are prepared. 	Technical guideline prepared		3.72%	
protection.					

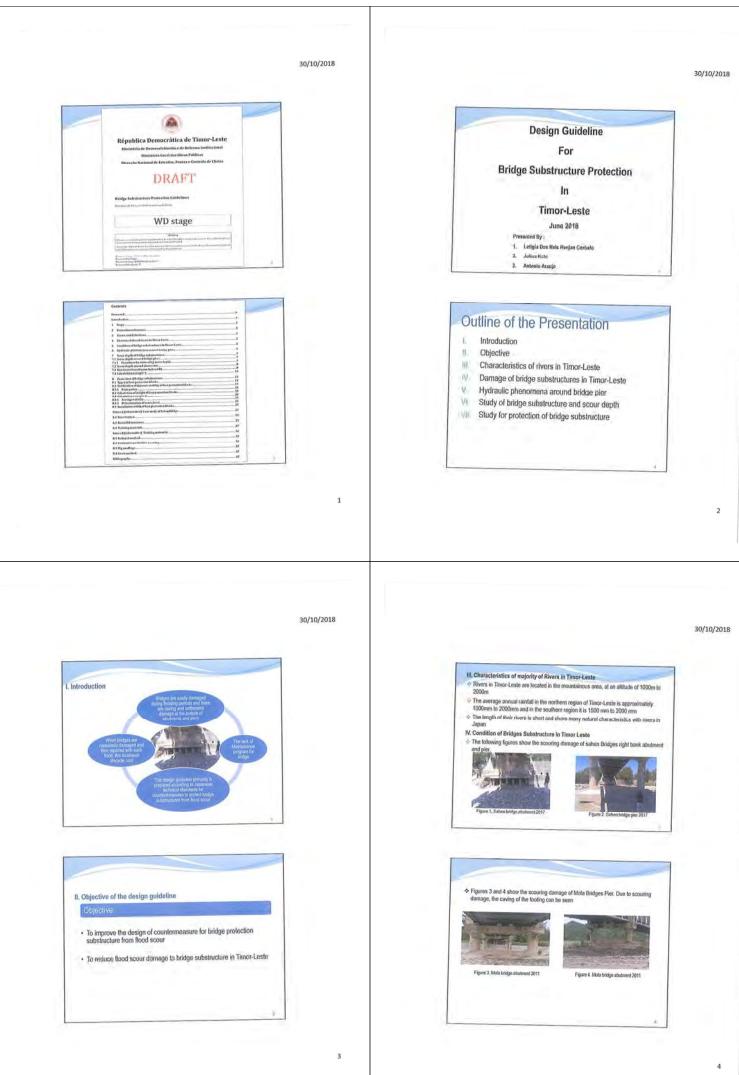
Activities	Inputs		Pre-Conditions
	The Japanese Side		
1.1 To review existing management structure condition 1. Dispatch of the Japanese experts	1. Dispatch of the Japanese experts	1. Assignment of C/Ps	DRBFC's budget necessary for the
of maintenance and rehabilitation for major roads.	Short-term experts:	- Project Director	Project is allocated by TL
1.2 To conduct periodic/routine inspection.	 Learn leader / Koad maintenance 1 Deputy team leader / Road maintenance 2 	- Project Manager - DRBFC Staff	government.
-	- Road construction supervision		
1.0 To the product of the determinant of the second se	- Quality control / Road repair	2. Assignment of Trainees	
1.3 to update the database based on the inspection result and renain/rehabilitation works of roads and	- Ulsaster restoration - Road design / Project coordinator	In accordance of necessity	
result and repaintenabilitation works of roads and hriddae	- Structure design	3. Facilities and Equipment	<pre></pre>
	- Database	- Project office	
1.4 To formulate maintenance and repair/rehabilitation		Equipment and tools	Issue: As a result of the second
plans for next cycle.		-	parliamentary election, regime
1.5 To implement emergency inspections and		4. Recurrent costs	change has occurred.
repair/rehabilitation works when necessity arises.	2. Facilities and equipment	- Expenses for equipment maintenance	Implementation of activities 1.2,
	In accordance with necessity of activities	- Spare parts	1.3, 1.4, 1.6, 2.2, 2.3 and 5.5 have
 To undertake appropriate road maintenance/rehabilitation works by following annual 	3. Training in Japan	 Transportation fees of C/Ps and trainees Expenses for contract-out of works 	been delayed due to delayed budget allocation.
work and budget plans which reflect priorities within the hit accordance with recessity of activities limited budget	וון מרכטוממווכם שונון וופרפסטונץ טו מעועוופט	- INECESSALY EXPENDINES TOLICASE SIGNES - C/PS' wades and allowances	
			Countermeasure:
1.7 To propose appropriate framework of road			1) In the coordination meeting
maintenance and rehabilitation for major roads.			between CDRS project and C/P,
			CDRS deputy team leader
			requested the director of DKBFC
2.1 To identify typical rehabilitation and repair works of			to prioritize allocation of budget for
major roads in the whole country as case studies.			the projects selected for case
2.2 To conduct the case studies for the planning			suures. 2) 2018 inspection work were
Asian and construction supervision of the project			carried out with integration of
			relevant staff of Dept. Project and
2.3 To propose preferable structures for construction			Dept. Maintenance in order to
management for repair/rehabilitation and maintenance			increase work efficiency with
works through case studies.			limited budget.
			3) 9-month extension of project
3.1 To review existing technical dog ments for road			delaved activities mentioned
maintenance and rehabilitation.			above will be conducted during
3.2 To review and identify factors of failure from past			extension period
examples of damaged rehabilitation and construction			
works.			
3.3 To acquire necessary knowledges of civil			
engineering for design trifough classioorn lectures and 3.4 To prepare the technical quideline of investigation			
and design.			
3.5 To reflect the lessons learned from case studies to			
the technical guideline.			
3.6 I o disseminate the technical guideline for			
concerned parties.			

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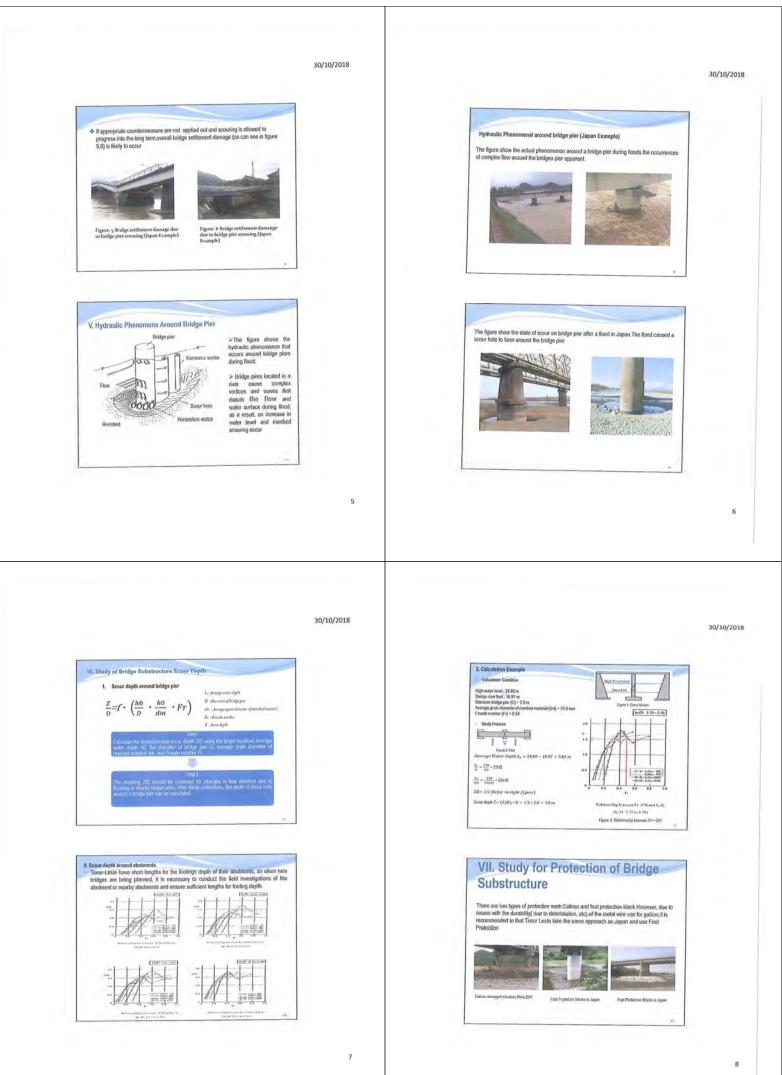
No. 10. 10. 10. 10. 10. 10. 10. 10. 10. 10	Project	Monitoring Sheet I	ll (Revision of Plan of Ope	ation)		Version 6 Dated 31st October, 2018	-
Prime Prime <	Project Title: The Project for the Capa				r-Leste(CDRS)		toring
	Inputs Event	Anture 1 T T T				lssue	Solution
	Team Leader/Road Maintenance 1	Plan Modify					
	/Mr. Makoto MATSUURA	Plan Actual				2017 March, Mr. Matsuura resigned.	
	/Mr. Mitsuhide SAITO	Modfy Actual			replaced Mr. Matsuura in Deputy		
Processor Proc	/Mr. Johji KOIZUMI	Modify					
Processor Proc	/Mr. Sueo HIROSE	Plan Modify Actual				-	
	/Mr. Shutaro SAKANAKA	Actual	▋▋▋▋▋▌▋▋▋▋▋▋▋<mark>▋</mark>▋▋▋	┝┥╋╋┥╊┼╢┥╋╬┥╊╋╢┥╋╋┥╋╋┥		-	
Abel A fermine Bel A fer	/Mr. Kazuharu KOISHIKAWA Road Design/Project Coordinator	Actual Plan			-	55	Mr. Brooker-Jones was dispatched as successor of Mr.
Abel A fermine Bel A fer	Road Design/Project Coordinator	Plan Modify			Mr. Brooker-Jones replaced Mr.	-	Akagawa.
Abel A fermine Bel A fer	Structure Design Mr. Kenii MINEGISHI	Plan Modify			Akagawa In Project	-	
Abel A fermine Bel A fer	Database	Plan Modify				-	
Abel A fermine Bel A fer		Plan Actual			Activity on Landslide analysis was		-
Abel A fermine Bel A fer	/Mr. Sohshi MIKAMI Evaluation/Monitoring	Plan Actual Plan			analysis was	-	•
Abel A fermine Bel A fer	Ms. Nao TSUJIMURA	Actual				-	•
Abel A fermine Bel A fer		Plan Actual Plan Actual			Office use These equipments		
		Plan			landslide mass movement Test equipment to grasp		
Part And Part An	-	Plan Actual	╊╋╋╗╋╋╋╋	╞╫╫╫╫╫╫╫╫╫╫╢	land penetration.		
Image: Note: Solution: Solutio: Solutio: Solutio: Solution: Solution: Solution: Solution: Solut		Actual					
Image: Control (Control (C	In-country Inita country Training	Actual		<u></u>			
Image: State Stat		Actual I II III IV				Achievements	Issue & Countermeasures
Import Mail <	 1.1 To review existing management structure and condition of maintenance and rehabilitation for 	Plan	IS realized in accordance with annu	ai work plan and annual budget plan	JICA expert team	Organizational and personnel exchanges were proposed at 3rd JCC.	
Normal Action Normal Action<		Plan			GOTL: NDR8FC Dept	1) Periodic/routine inspection has been done aloon 403 from Loes to Maliana:	
No. No. No. No. No. No. No. No. No. No.		Actual			Project NDBBEC Dept	to Maliana. 3) Urban & national road surveys were conducted by Dept. Project.	
No. No. No. No. No. No. No. No. No. No.	result and repair/rehabilitation works of roads and	Modify Actual			Maintenance and Dept. Project, JICA expert		Issue: As a result of the parliamentary election, regime change occurred. Due to political factors, budget plan for 201
Non-specific constrained of the second of the sec		Plan			NDRBFC Dept.		was rejected. Activities of 1.2, 1.3, 1.4, 1.6 have been delayed Countermeasure: 1) 2018 inspection work will be carried out
Number of the state o		Plan	╂┼┼┼┼┼┟╋╹┼┼┼┼┼┼┍╋		team assists this activity. NDRBFC; JICA	Emergency inspection on A03 at Loes River was conducted;	Dept. Maintenance in order to increase work efficiency. 2) Extension of project term was approved at 4th JCC; those
Application Main Main <td>repair/rehabilitation works when necessity arises</td> <td>Modify Actual</td> <td></td> <td></td> <td>expert team assists this activity.</td> <td>JICA expert team suggested countermeasure for river bank protection.</td> <td>delayed activities will be conducted during extension period.</td>	repair/rehabilitation works when necessity arises	Modify Actual			expert team assists this activity.	JICA expert team suggested countermeasure for river bank protection.	delayed activities will be conducted during extension period.
Processes Processes	rehabilitation works by following annual work and budget plans which reflect priorities within the	Modify			Project; JICA expert	Based on inspection results NDRBFC prepared draft 5-year and 2019 annual plans.	
1.1. Concernence 1.1. Concernence <td< td=""><td>1.7 To propose appropriate framework of road</td><td>Modify</td><td></td><td></td><td></td><td>Maintenance in order to strengthen maintenance capacity was</td><td></td></td<>	1.7 To propose appropriate framework of road	Modify				Maintenance in order to strengthen maintenance capacity was	
1 1	Output 2: Capacity of DRBFC construction manage					proposed as and doc.	
	2.1 To identify typical rehabilitation and repair works	s			IICA evoert teom	2 case study sites and action plan for each site were proposed in 3rd	
2.7. Consists in the plane. 1.0.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1	of major roads in the whole country as case studies	Actual	done		SIGTOOPERICAN		
2) 10 <td< td=""><td></td><td>Plan</td><td></td><td></td><td></td><td></td><td></td></td<>		Plan					
Product Product <t< td=""><td>design check, and construction supervision of the</td><td>Modify</td><td></td><td></td><td>secure budget for the</td><td>OJT on mass movement data collection by inclinometer was conducted;</td><td>allocation.</td></t<>	design check, and construction supervision of the	Modify			secure budget for the	OJT on mass movement data collection by inclinometer was conducted;	allocation.
Area Area <th< td=""><td>project</td><td></td><td></td><td></td><td>selected for case</td><td>control of asphalt concrete were delivered; Workshop of culvert planning was conducted;</td><td>CDRS project and C/P, CDRS deputy team leader requested the director of DRBFC to prioritize allocation of budget for the</td></th<>	project				selected for case	control of asphalt concrete were delivered; Workshop of culvert planning was conducted;	CDRS project and C/P, CDRS deputy team leader requested the director of DRBFC to prioritize allocation of budget for the
Normal production management for majority and balance of a main structure of a majority of		Actual				Draned checklists were introduced.	projects selected for case studies. 2) Extension of project term was approved at 4th JCC; those delayed activities will be conducted during extension period.
a. 1. The original table of the multiple of the	construction management for repair/rehabilitation	Plan Modify			JICA expert team		
11 To review ending technical converts real 0	Output 3: Technical guideline of investigation and	design for maintenance a	and rehabilitation are provided as a	tool for more appropriate design			
3.2 To row and largely function of lature from models data on the model of lature from models data on the model of lature from models data on the model of lature from models data on the model	3.1 To review existing technical documents for road				JICA expert team	JICA expert team reviewed existing technical documents,	
point runcion wold Attem U <td>3.2 To review and identify factors of failure from</td> <td>Plan</td> <td>pne</td> <td></td> <td></td> <td>JICA expert team identified factors affecting structural failure /</td> <td></td>	3.2 To review and identify factors of failure from	Plan	pne			JICA expert team identified factors affecting structural failure /	
And Margen Vision Margen Vi	construction works		one		JICK expert team	inspection results.	
A. To prepare the technical gladdine of methods of gladdine of adding and design. Methods of methods of gladdine of adding adding of methods of methods of methods of methods of methods. Description and design. Description and description and description and description and description and description and description and description and description and description and description and description and description and description and description and description and description and descri	engineering for design through classroom lectures	Plan	╉┥┫╋┿┿┩╎╎╎╋┿┿┥╎╵╵		JICA expert team	schedule	
Intersection Action Intersection Action Intersection Action	3.4 To prepare the technical guideline of	Plan	done			Draft guidelines for slope protection, bridge substructure protection	
3.5 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude ware 1.1 To reflex the issone issand from case stude 1.1 To reflex the issone issand from case stude 1.1 To reflex the issone issand from case stude 1.1 To reflex the issone issand from case stude 1.1 To reflex the issone issand from case stude 1.1 To reflex the issone issand from case stude 1.1 To reflex the issone issand from case stude 1.1 To reflex the issone issand from case stude 1.1 To reflex the issone issand from case stude 1.1 To reflex the issone issand from	investigation and design				NDRBFC Dept.	and culvert design have been prepared.	
As To deseminate the technical guideline for concerned parties Prior I	3.5 To reflect the lessons learned from case studies to the technical guideline	S Modify Actual			Project, chief of planning section and		protection, bridge substructure protection and culvert design)
Image: Note of a partices Image:	3.6 To disseminate the technical guideline for	Plan			ICA expert team and		Countermeasure: In order to confirm their efficiency and applicability, guidelines will be introduced to projects other
Hais 2016 2017 2018 2019 2020 Remarks Bernarks Bernarks Besu Solution Initiating I <tdi< td=""></tdi<>		Actual			C/P		inan case studies.
Control ng Plan Annu 2 1	Duration / Phasing						
Joint Monitoring Part Mark	Monitoring Plan Monitoring					Issue	Solution
Joint Monitoring Part Mark		Plan IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII			9-month extension of	-	
Joint Monitoring Part Mark		Modfy Actual			approved by 4th JCC. In the extension period, additional JCCs and	-	
Bits Bits <th< td=""><td></td><td>Modily Actual</td><td></td><td></td><td>monitoring activities will be conducted.</td><td>Submission of monitoring sheet Ver.5 was delayed.</td><td>In urue io improve project management, internal coordination meetings of CDRS expert team have been held.</td></th<>		Modily Actual			monitoring activities will be conducted.	Submission of monitoring sheet Ver.5 was delayed.	In urue io improve project management, internal coordination meetings of CDRS expert team have been held.
Bits Bits <th< td=""><td></td><td>Actual Plan Actual</td><td></td><td></td><td><u> </u></td><td>-</td><td></td></th<>		Actual Plan Actual			<u> </u>	-	
Ham Ham <td>Reports/Documents</td> <td>Plan Actual</td> <td></td> <td></td> <td></td> <td></td> <td></td>	Reports/Documents	Plan Actual					
Project Completion Report Transmission of project Completion will be portioned. Project Completion will be portioned. Submission of project Completion will be portioned.		Plan Modily Modily Actual			9-m onth extension of project period has been approved by 4th JCC.	Checks for whether prepared guidelines can be utilized by C/P have been insufficient.	During extension period, guidelines will be introduced to projects other than case studies.
Process Process <t< td=""><td></td><td>Actual</td><td></td><td></td><td>1</td><td>Project completion will be postponed.</td><td>Submission of project completion report will be postponed to December 2019.</td></t<>		Actual			1	Project completion will be postponed.	Submission of project completion report will be postponed to December 2019.
Ervent or opening ceremony for a UJI Stee Actual 111111111111111111111111111111111111	information to road users	Plan Actual Plan			1		
	Event or opening ceremony for a OJT site	Actual Plan Actual			<u> </u>		

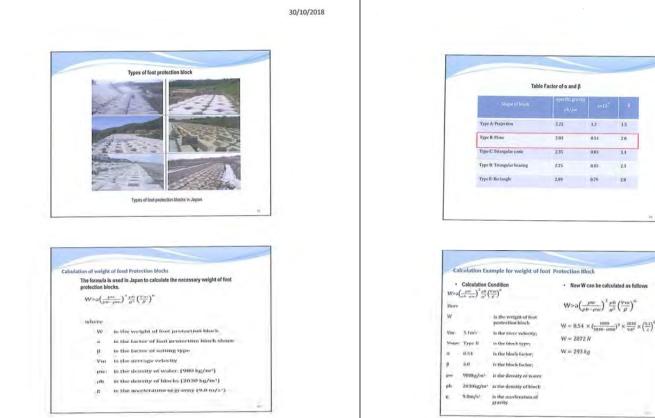
Attachment 1

Design Guideline for Bridge sub structure Protection in Timor Leste on 12 June 2018



A3-163





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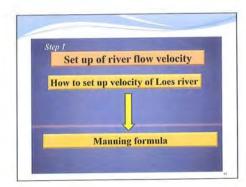
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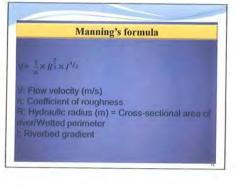
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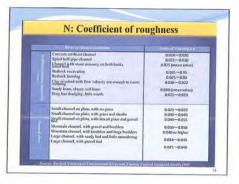


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	and a	Shares in the state of some state	++++++++++++++++++++++++++++++++++++++	
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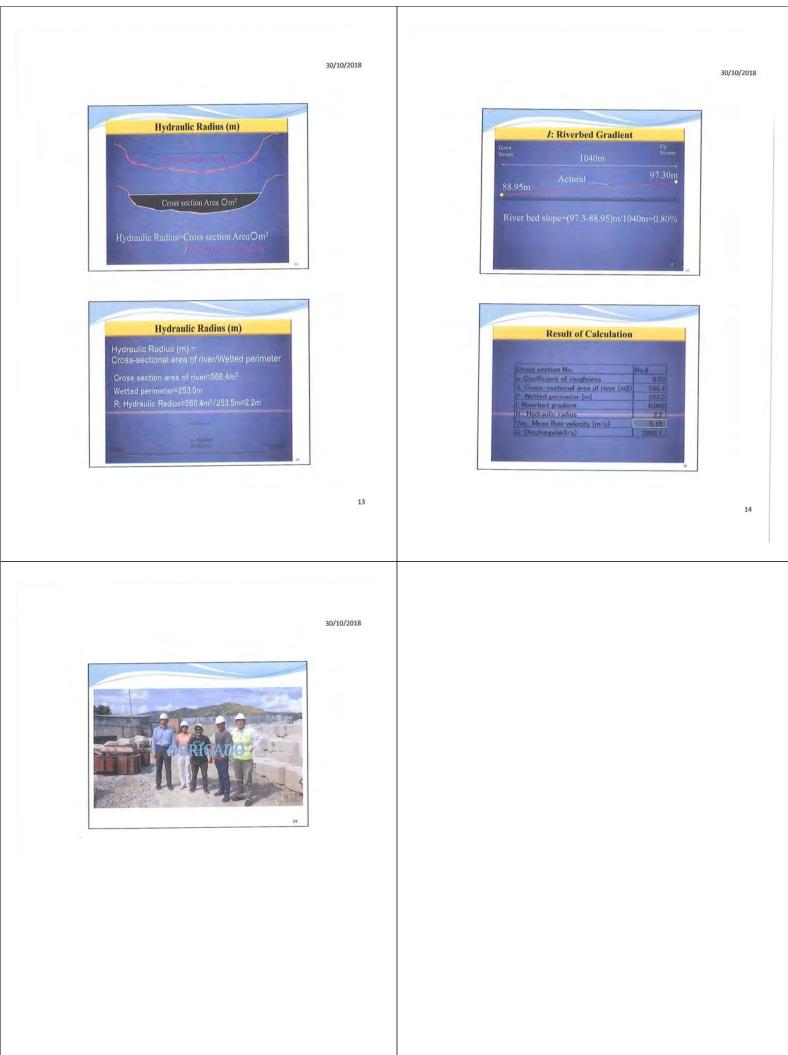






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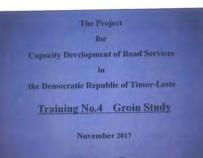


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Attachment 2

Groin Study Using Loes River on 13 June 2018

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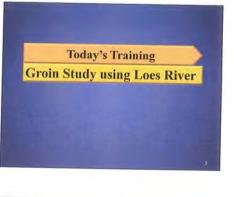
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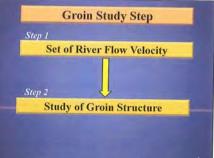


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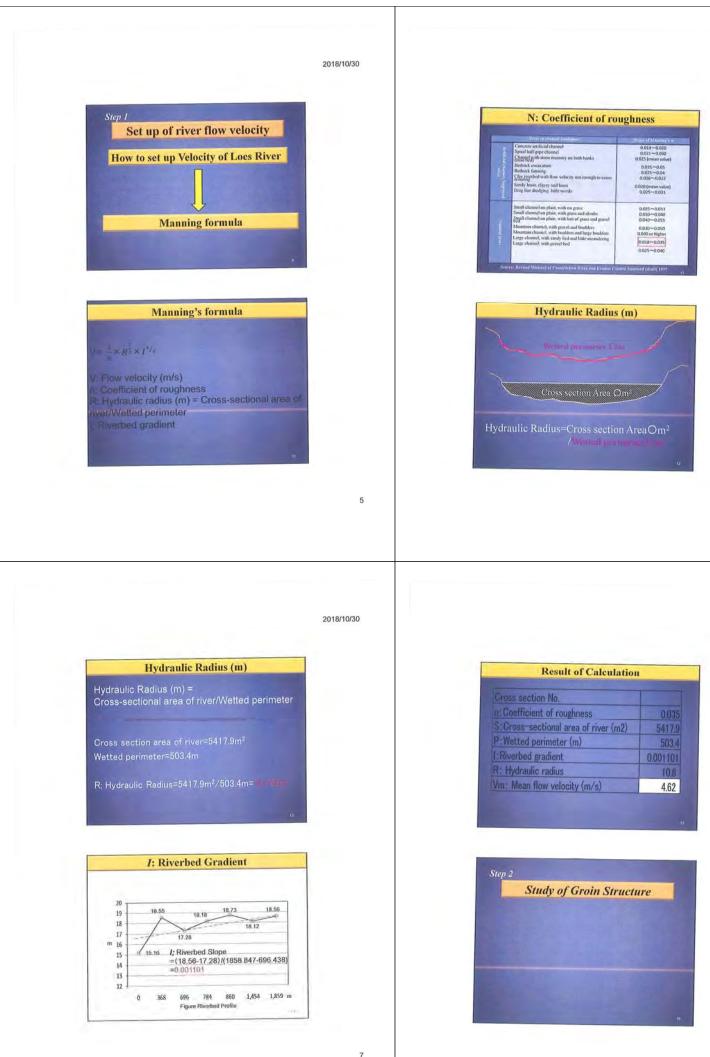






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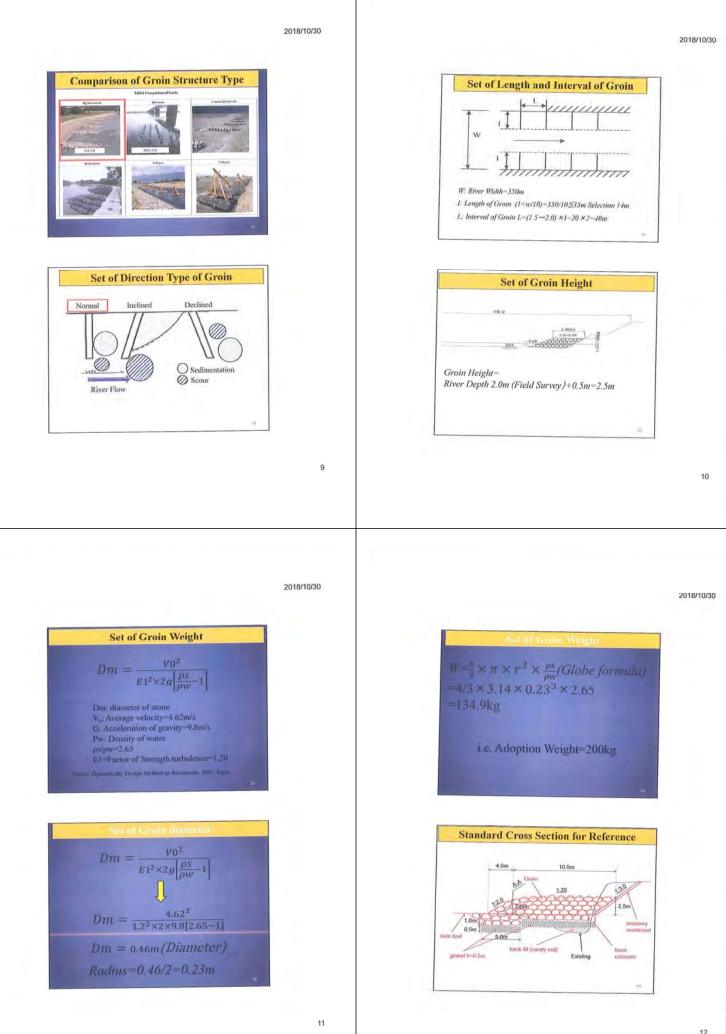
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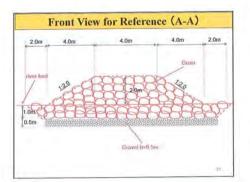
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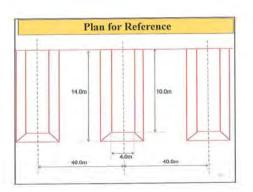
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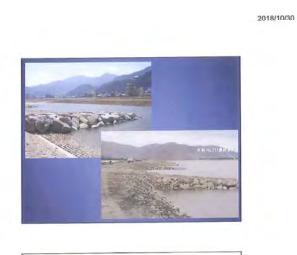








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Attachment 3

Explanation of Guideline for Box Culvert planning and Design on 21st June 2018

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A.3. Data collection.... A.4. Rainfall analysis ... A.5. Design flood.... A.6. Design capacity.... A.7. Conditions of flow.. A.8. Protection works ... A.9. Design remarks ... A.10. Calculation notes.

Annex A (informative) Case study of Sesurai Culvert... A.1.Introduction A.2.Site Conditions...... A.3.Data collection......

Annex B (informative) Training materials... B.I.Shummary of case study.... B.2.Catchment and river profile.... B.3.Design food. B.4.Design capacity of culvert.... B.5.Erosion protection... B.6.Design remarks...

Annex C (informative) Weather stations in Timor-Leste..... C.1.Current locations of weather stations (Seeds of Life).... C.2.Historical locations of weather stations (Seeds of Life)...

Although every effort has been made to ensure the accuracy and applicability of the information contained within this document, the authors cannot accept any liability or legal responsibility for any errors, for any omissions or for any other reason whatsoever.

Road Guidelines — Drainage — Culvert Design

Diretrízes Rodoviárias — Drenayem — Desenho de Alcatrão

DG stage

Républica Democrática de Timor-Leste Ministério de Desenvolvimento e de Reforma Institucional Ministério Geral das Obras Públicas

Direcção Nacional de Estradas, Pontes e Controlo de Cheias

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Document type: Technical Specification Document subtype: Document stage: (UG) Oran Guideline Decument language: E

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Acknowledgements

Feedback:

The Project for Capacity Development of Road Services in the Independent Republic of Timor-Leste wishes to thank all parties involved in preparing and revising the Colvert Design guideline.

In support of the project, the officials of the Ministry of Development and Institutional Reform: M. R. M. Cruz, J. L. C. C. P. Mestro and J. Santas; and the officials of the Ministry of Public Works: C. M. Henrique and especially R. H. F. Guterres; are bereby acknowledged.

In contributing to the preparation of this document, the officials of the DNEPCC: M. R. Monteiro, J. P. Amaral, J. M. G. Sousa, J. G. Carlvalho, J. M. L. Guiteres and N. Jobato; and the International Labour Organization's cli(01) bechical assistance (can of the Roads for Development Support Program (R4D-SP): S. O. Asare, K. H. Myaing, S. Done, S. F. Eghali, V. Sam and D. H. Singh; are hereby acknowledged.

In addition, the Seeds of Life Program: S. Bacoo Is bereby acknowledged.



Any positive feedback for possible incorporation into future editions would be appreciated. Please send such comments or feedback to the below address.

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Introduction

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Foreword

September, 2018

September, 2018

This guideline was developed by IICA Project for Capacity Development of Road Services in the Independent Republic of Timor-Leste in collaboration with the Directão Nacional de Estradar, Pontes e Controlo de Cheire (DNEPCC, National Oirectorate a Roads, Ericliges and Floads Conitrol') for the purpose of developing institutional capacity regarding drainage design of cross culverts.

In the interest of constructing high quality and economically viable government infrastructure to serve the nation, this guideline for optimal design of drainage components was prepared by the JICA Project for Capacity Development of Road Services in the Independent Republic of Thuror-Leste (CDRS) in collaboration with the Direcção Nacional de Estradas, Ponies e Control of Cheias (DNEPCC, National Directorate d Roads, Bridges and Fload Control') of the Ministério Geral das Obras Públicas ('Ministry of Public Works'). We would like to thank JICA for their continuing support.

Japan International Cooperation Agency (JICA) has been conducting a technical cooperation project for tevelopment of capacity regarding road services, which is called CDBS, in order to facilitate the DNEPCC in properly managing and maintaining the road infrastructure that is the basis of social and economic activities. To this end, IICA has here dispatching a team of espects fram March 2016 to August 2019. As a result of collaborative work with counterparts of the DNEPCC, this guideline for testign of outverts has been finalized. Unperformed and the contribute to infrastructure development and maintenance, and to the enhancement of friendly relations between our two countries.

Finally, I wish to express my sincere appreciation to the officials of the Government of the Democratic Republic of Timor-Leste for their close cooperation with the expert team.

The purpose of drainage design is to ensure reasonable capacity of drainage facilities, which means specifying culver's with sufficient drainage capacity to accommodate probable volumes of stormwater and at reasonable construction voits comparies to their becent to economic activities. Within the context of raid crossings, the purpose of hox culverts is to ensure the protection of road structures and at road. heers.

The chronology of editions are as follows:

September 2010 First edition in English

The main changes compared to the previous edition are as follows:

No changes

Road Guidelines — Drainage — Culvert Design

1 Scope

This guideline aims to provide practical information for planning and design of box raiverts for the purpose of culvert construction or reconstruction. This guideline does not cover culvert rehabilitation or repair. The design methodologies presented here have been recommended on the basis that they are way in application and consistent in approach.

For information regarding construction and maintenance on site, please see the relevant section in the Standard Specifications (Section 600 - Drainage and Slope Protection Structures) (1).

The language used in this guideline is generally Latinate to facilitate comprehension by the engineers of the directorate

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

- Standard Specifications (2014) (1)
- Bridge Design Manual (2010) (2)
- Road Geometric Design Standards (2010) (3)

3 Terms and definitions

For reference, a glossary of terms and their equivalent meaning in Tetun, Portuguese or Indonesian, and Japanese luss been included at the back of this guideline.

For the purpose of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at http://www.electropedia.org/
- ISO Online browsing platform: available at https://www.iso.org/chu
- 3.1

catchment area of land where all of the water that is under it or drains off of it goes into the same place [SOURCE: ISO 14055-1:2017(en), 3.2.19]

3.2

cuivert transverse drain or waterway structure under a road, railway, or canal, or through an embankment, in the form of a large pipe or enclosed channel

[SOURCE: ISO 6707-1:2017(en), 3.1.2.33] © DNEPCC 2018 - All rights reserved

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3.3 return period

average number of years in which a stated action statistically is exceeded once [SOURCE: ISO 12494:2017(en), 3.8]

3.4 river

natural body of water flowing continuously or intermittently along a well-defined course into an ocean, sea, lake, inland depression, marsh, or other watercourse [SOURCE: ISO 5667-6:2014(en), 3.9]

2.5

3.5 subcritical flow flow in an open channel at less than critical velocity, that has a Froude number of less than unity, and in which small surface disturbances can travel upstream [SOURCE: ISO 772:2011(en), 1.7]

3.6 supercritical flow flow in an upen channel at more than settical velocity, that has a Proude number of greater than unity, and in which small surface disturbances cannot travel opstream [SOURCE: 150 772:2011(en), 1.8]

3.7

A.r watercourse channel on or below the earth's surface, through which water may flow (SOURCE: ISO 6107-7:2006(en); 50)

3.8

wetted perimeter crintact length between a stream of flowing water and its containing open channel, measured in a direction normal to the flow

[SOURCE: ISO 772:2011(en), 1.54]



4.1 Selection of structure

The first step in planning is selection of the most appropriate type of structure for crossing a waterchurse. The two main types of structure for crossing are bridges and cuberts. They both have advantages and disadvantages, as shown in Figure 4.1. There may also be other factors that an engineer needs to consider. If shorting is a more appropriate, then please refer to the *Bridge Design Manual* (2).

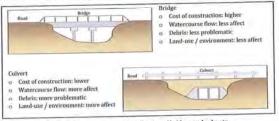


Figure 4.1 — Comparison of application of bridges and culverts

4.2 Overview of culverts

There are various shapes (rectangular box, circular pipe, elliptical pipe, arch pipe, etc.), materials (concrete, corrugated stee), etc.) and inlets (wing walls, flat headwall, square edge at crown, bevel at crown, etc.). This guideline will primarily cover box culverts made of concrete, The parts of a culvert are shown in Figure 4.2 and Figure 4.3.

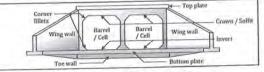


Figure 4.2 — Parts of a culvert on front elevation

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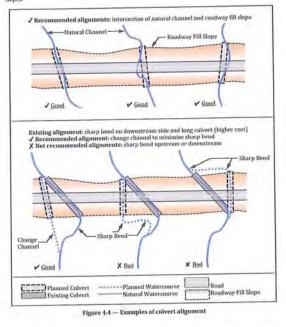
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In principle, the geometry of a box culvert (width, gradient and bottom elevation) should be similar to the original watercoarse in order to reduce sedimentation or erosion. The gradient should be more than (3) 0.5% or 0005 m/m to reduce sedimentation, and less than (5) 10% or 0.100 m/m to ensure workability & prevent suppage.

4.4 Alignment of culverts

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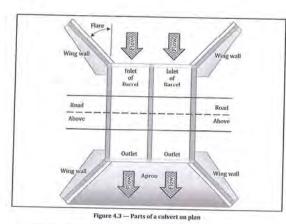
Culvert alignment is important for the function of the culvert and watercourse. If possible, the infer and outlet of the culvert should be located in the natural channel at the intersection with the roadway fill slopes.



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4.3 Application of culverts

Proportion (height : width)

Gradient of culvert

There are limitations to the application of culvert structures. The recommended range of application for each barcel of a concrete bax culvert is shown in Table 4.1. It is possible to design beyond these limitations with sufficient consideration of structural design and traffic loads.

The proportion of a culvert (height : width) is normally in the range of 1 : 1 to 1 : 3. 'The most hydraulically efficient proportion is 1 : 2. However, the most normal proportion for road culverts is 1 : 1, because the culvert must structurally support the loads from traffic.

Property	Minimum	Maximum
Height, D	0.75 m 750 mm	5.0 m 5000 mm
Width, B	0.45 m 450 mm	6.5 m 6500 mm
Cover depth (of material) above top plate	0.5 m 500 mm	0,00 1111

1:1

0.5% or 0.005 m/m

1:3

10% or 0.100 m/m

An outline of the stages for the process of design are shown in Figure 4.5.

Protection works	 Selection of protection measure and size 	Section 9
1 C		
pen-channel hydraulics	Calculation of culvert capacity for discharge Calculation of flow type and velocity	Section 8
and the second	O Selection of culvert size	1
10		
	a Calculation of flood discharge	
	a Assessment of run-off coefficient	section /
Flood calculation	 Calculation of rainfall intensity 	Section 7
	Calculation of catchment area Calculation of time of concentration	
~		-
- 611	 Calculation of daily rainfall for design 	Section 6
Rainfall analysis	O Frequency analysis	Section 6
1		
	O Rainfall data	
Data collection	O Cartographic (map) / geospatial data	Section 5
A NUMBER OF A	Basic site information Topographic data	1

In some cases, a simplified process for design could be adopted, as shown in Figure 4.6. This process is based on adoption of a rainfall intensity of 200 mm/hour from the *Bridge Design Manual* (2). However, this process may result in excessive or insufficient designs and should be used with caution. This process should only be used for small applications on minor routes, such as rural local roads.

Data collection	 Basic site information Cartographic (map) / geospatial data 	Section 5
Flood calculation	Calculation of catchment area Rainfall intensity = 200 mm/hour Assessment of run-off coefficient	Section 7
-UL	O Calculation of flood discharge	
Open-channel hydraulics	Selection of culvert size Calculation of culvert capacity for discharge Calculation of flow type and velocity	Section 8
- Alle		
Protection works	 Selection of protection measure and size 	Section 9

Figure 4.6 — Outline of simplified process for design

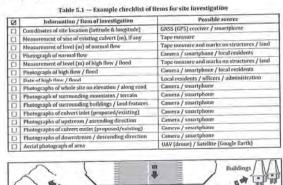
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5 Data collection

The design of culverty requires an understanding of the site conditions. The following section outlines the various information that should be collected through site investigations and desk studies (off-site investigations).

5.1 Basic site investigation

A basic site investigation should be implemented on site for every culvert design. This information will be necessary for planning and also support the decisions made in the process of design regarding run-off. Examples of the information that is required are shown in Table 5.1 and Figure 5.1.



100 Gill . 10 Upstre: Outlet 🕼 D (mb Inlet 6 10 Mountains **[] -40 Flow le Road

Figure 5.1 — Diagram of site photography

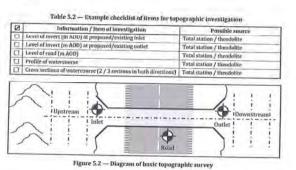
5.2 Topographic Investigation

If possible, a topographic investigation should be implemented on site. This information will be necessary for planning and will form a fundamental part of the design calculations regarding the watercourse gradient. In addition, this information can improve the accuracy of a design and facilitate the verification of results. An example of the information that is required is shown in Table 5.2.

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5.3 Cartographic Investigation

δ cartographic investigation should be implemented off-site for every culvert design. This map / geospatial information will form a fundamental part of the design calculations regarding the catchment. An example of the information that is required is shown in Table 5.3.

Table 5.3 - Example checklist of i

2	Information / Item of Investigation	Possible source
	Cartographic map (7755 series of 1:50,000 maps, etc.)	In-house resources (Mapping & GIS)
	Digital elevation model (GIS DEM raster)	In-house resources (Mapping & GIS)
	Watercourse line [GIS vector]	In-house resources (Mapping & GIS
	Road line (GIS vector)	In-house resources (Mapping & GIS)

5.4 Rainfall data

A pluvial investigation should be implemented off-site for every culveri design. This rainfall data will form a fundamental part of the design calculations regarding the rainfall intensity. An example of the information that is required is shown in Table 3.

Table 5.4 - Example checklist of items for pluvial investigation

12	Information / Item of investigation	Possible source
	Monthly rainfall data	In-bouse resources / relevant authority (see Annex C)
	Daify rainfall data	In-house resources / relevant authority (see Annex C)
D	Short-Interval / hourly rainfall data	(currently unavailable in Timor-Leste)

The availability of rainfall data will influence the design. The following are considered ideal characteristics for a set of rainfall data • 1+ stations in the catchment or near the catchment

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In this case, the process of design can utilise intensity-duration frequency (IDF) curves, as chown in Figure 5.3. The advantage of IDF curves is that storms can be accurately predicted. The disadvantage in that the development of IDF curves requires a significant amount of rainfall data. N

Frequency Analysis	Development of IDF Curves	Rainfall Intens
100 C	IDF curves in the process of	

- Currently, the method of IDF curves cannot be utilised in Timor-Leste, because of the limited length and limited detail of rainfall data. The following is a summary of characteristics for rainfall data in Timor-Leste:
- Currently 82 statiums in operation across Timor-Leste (on average, 1 for every 180 km²) Monthly rainfall records exist from 1950s (for 36 stations with gaps) Daily rainfall records exist for 40 weather stations (approximate availability) Long record of 49 evers for daily rainfall in bill (with gaps) Short records of 7 11 years for daily rainfall in biter areas (approximately)

In this case, only daily rainfail data is available, so the process of design in Timor-Leste can inflice the Monomole formula in the process of design, as shown in Figure 5A. The Monomole formula is used to derive an approximation of rainfail intensity for any storm duration from daily rainfail data. The advantage of the Monomole formula is simplicity. However, the disensity is that the approximation of storms with short duration (6 hours or less) may not be accurate. The Monomole formula is explained in more detail in Section 7A.

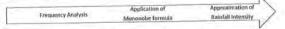
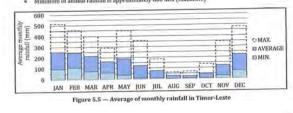


Figure 5.4 — Mononobe formula in the process of design

The rainfall varies depending on the region. The average of the monthly rainfall across the whole country is shown in Figure 5.5. In addition, the variance between the regions is indicated with the following summaries

- aries: Average of annual rainfall is approximately 1700 mm (whole country) Maximum of annual rainfall is approximately 3100 mm (Same) Minimum of annual rainfall is approximately 600 mm (Manatuto)
- ż

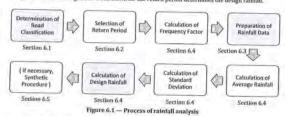


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6 Rainfall analysis

Ratufail analysis reflects the hydrological risk for a road, and ensures protection against probable floods. The input of this process is a long record of daily rainfail, and the output is a maximum probable daily rainfail, also called the design daily rainfail.

The design daily rainfall is determined by analysis of historical rainfall records. The historical rainfall records show the relationship between the frequency of accurrence of storms; and the magnitude of storms. The frequency of occurrence for a probable storm / design storm is called the 'return period'. The prediction of the magnitude of the storm for the return period' determines the design rainfall.



6.1 Classification of roads

According to the Road Geometric Design Standards (3), the roads in Timor-Leste are classified as shown

Rural Roads	Roads outside towns and cities.
National Roads	 Atterial roads are centres of national and international linportance and roads transinsting at international boundaries connecting nation'to signitian and road road road roads and provides high level of service for long distance novement of goods and prople and thus to/front central corridors for especially heavy vehicles. These roads link locations where change of transport mode is provide.
Regional Roads.	 Roads that provides more local purposes, serve mainly traffic within regions and districts at lower speeds and shorter distances. Roads that serve as collector of traffic to/from local network to the nutrinon road network.
Local Roads	 Local roads rounseting sub-district capitals to villages and more remote areas with agricultural potential.
Urban Roads	Local roads inside towns and cities.
Urban Arterial Roads	 An Drban Arterial Road is a continuous road with partial access tonarol, for through traffic within urban areas. Basically it conveys traffic frum residential areas to the vicinity of the contral butmess district or from one part of a city to another

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which does not intend to penetrate the city centre. A/terial masks do not penetrate identifiable neighbourhoods. Smooth traffic flow it essential since it carries large traffic volume. A collector road is a road with partial access control designed to serve on a collector or distributor of traffic between the arterial and the local road systems: Collectors are the major roads that penetrate and serve identifiable neighbourhoods, commercial areas and industrial areas. Urban Collector Roads The local street system is the basic road network within a neighbourhood and provides direct access to abuiting load. They are links to the vollector read and thus serve short trip lengths. Through traffic abould be discouraged. Urban Local Boards

The return period reflects the hydrological risk for a road. The selection of an appropriate mitigation of risk depends on the economic value / importance of a road asset. The lalance between the cost of the road asset and the cost to protect the road asset is important: inadequate protection may allow damage of a road asset and a loss of economic value; excessive protection will cause unnecessary expenditure and an uneconomical solution.

The return period (years) represents probability of occurrence. The return period does not represent a guaranteed period without flooding and it is not related to the design life of a road. The probability of occurrence has an inverse relationship to the magnitude of rainfail events. Therefore, a long return period equids a low probability, which means a high magnitude of rainfail event.

Table 6.2 — Recommended returns period of rainfall for culverts (4) (6)

Road class	Level of drainage capacity	Return period of rainfall
National Roads / Urban Arterial Roads	High	10 years
Regional Roads / Urban Collector Roads	Medium	7 years
Local Roads / Urban Local Roads	Low	5 years

The classification of a road is related to its economic value. Therefore, selection of a return period is recommended based on the classification of a road, as shown in Table 6.2. The return period may be modified by the engineer in situations where a higher level of drainage capacity is desirable. For example, roads that are designed for exervice of major national assets and where the level of risk must be agreed in conjunction with other national authorities.

6.3 Preparation of rainfall data

The rainfall data for frequency analysis is the maximum of daily rainfall per annum. The preparation of rainfall data for analysis should be implemented in the following manner:

- 1. Acquisition of daily rainfall data
- I. Acquisition of daily rainfall data
 Z. Examination of all data (365 days) in same annum (coeval data)
 Selection of maximum cainfall value (1 day) per annum
 Repetition of 2 and 3 (above) for every annum

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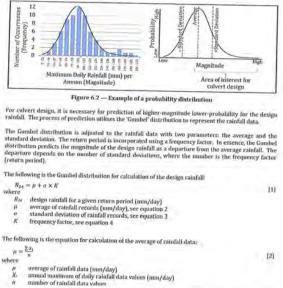
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Complete rainfall records are necessary for analysis. The confirmation of data integrity should be implemented in the following manner:

- If data contains null or erroneous values (for example, " ** " or " -- " or " NA "), deletion of
- these values is necessary
 If data for 1 annum is missing approximately 90 days (¼ annum) of data, then that annum is invalid and cannot be utilized for analysis

6.4 Frequency analysis

Prequency analysis utilises a probability distribution for the prediction of design rainfall. A probability distribution is a general relationship between the frequency and the magnitude. The probability distribution conforms to the rainfall data, similar to a trend line (or line of tendency). An example of a probability distribution on a bell-shaped diagram is shown in Figure 6.2.



- INOTE in spreadsheet not
- re, this can be calculated using the AVERAGE function) 12

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[3]

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$\sigma = \sqrt{\frac{\Sigma(X_i - \mu)^3}{n - 1}}$ where

- standard deviation of rainfall data annual maximum of daily rainfall data values (mm/day) average of rainfall records (mm/day) number of rainfall data values 0 .X
- - eadsheet software, this can be calculated using the STDEV or STDEV.5 Ruscia

The following is the equation for calculation of the standard deviation of rainfall data:

The following is the equation for calculation of the frequency factor (incorporation of return period): [4]

 $\mathcal{K} = -\frac{\sqrt{6}}{\pi} \times \left(\gamma + \ln\left(\ln\frac{\tau}{\tau-i}\right)\right)$

INOTEIN

- where
- frequency factor (normally between -1 and 5) Pi mathematical constant = 3,14159 Kulor-Mascheroni crustiant = 0,5772 return period (years), see Table 6,2 preadulout suftware, this can be celestated using the SQRT, PL and LM foretions] (NUTE: in spreadsheet st

6.5 Synthetic procedure

In many cases in Timur-Leste, it is necessary to implement a synthetic [compensative] procedure. The reason is that most locations only have short records of rainfall data (see Section 5.4). Therefore, currently, Dill is the only location with minfall data that is suitable for frequency analysis. Using the frequency analysis of design daily rainfall for Dill, it is possible to synthesise for other locations by scaling up / down (escalate / diversate) using the ratio of average annual rainfall as a moltipiler. The procedure of deriving daily rainfall for any target location in Timor-Leste using Dill as a basis is shown in Table 6.3. Table 6.3.

Table 6.3 — Synthetic procedure for deriving daily rainfall for a target location

Return period of rainfall	Design daily rainfall in Dill, R24 (mm/day)		Ratio of annual cainfall (multiplier)
10 years	131.4		(Target Location / Dili)
7 years	122.5	×	(mm/940 mm)
5 years	113.6	-	

For reference, a list of target locations and derived design daily rainfall are shown in Table 6.4.

DI

Alicon

Baucro

Betano

Alas

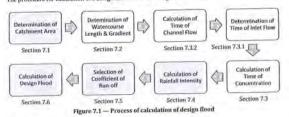
Target location

Algarve (Fazenda)

Atauro (Man-Meta)

7 Design flood

The calculation of design flood determines the volume of water that will be discharged from the catchment during the design rainfall. The design flood determines the required capacity of the colvert. The procedure for calculation of a design flood is shown in Figure 7.1.



^{7.1} Catchment are:

A catchment is an area of land that drains to a point of interest, such as a cuivert, as shown in Pigure 7.2. All water flow that originates inside the catchment area passes the point of interest before proceeding downstream. The watershell is the boundary between a catchment and its neighbour catchment. The extent of the watershell foundary) can be identified by comercing the surrounding points with highest elevation, such a mountain summits, hilltopis, ridges, saddles and spurs as shown in Figure 7.3.



The size of a catchment has an important influence on the calculation of nun-off. The size is expressed as area in terms of lon² (1 km² = 1,000,000 m² = 100 ha). Topographical maps (1:50,000, such as 7755 series) can be used for determination of catchment area. However, smaller scale maps (1:10,000) or geographic formation system (GS) data are recommended to small catchments. It is important for the designer in visit a site personally to obtain an impression of the characteristics of the catchment:

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In addition to the total catchment area, calculation of the sub-catchment areas is required if locations have distinctly different types of (errain. The boundary of terrain types can be analysed by site investigation, by satellite imagery or by land cover data.

7.2 Watercourse properties

Similar to Section 7.1, watercourse properties can be measured with topographical maps, CAD software or GIS. If possible, a request for information should be made to the GIS & Mapping Section of DNEPCC.

The watercourse properties required for calculation of time of concentration are the length and the gradient. The length of a watercourse (*L*) should be measured from the furthest discernible start of a watercourse to the point of interest, as shown in Figure 7.4.

Start of Watercourse Watershed Length of W Ro (Cu

Figure 7.4 - Measurement of length of watercourse

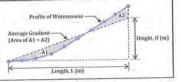


Figure 7.5 — Calculation of average gradient of watercourse

7.3 Time of concentration

The time of concentration is required for the calculation of rainfall intensity. The time of concentration is the time for water in flow from the furthest point in the watershed ()e, the unsuntain) to the point of interest (*Je.* the culvert). Different areas of a watershed contribute in run-off at different times after rainfall begins. Time at which all parts of the watershed contributes to her non-off and the same as shown in Figure 7.6. The time of concentration is calculated with equation 5.

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2.59 1.63 293.8 2432 316.5 339. Dare 1533 185.2 199.9 214.2 353.0 185.6 213.2 3.12 1.63 1.88 Fatsibessi 2929 381.3 409. 1536 199.9 214. 1765 229.3 246. Hato-Builico 2.57 292. 314.7 272.0 2418 337. 2.22 llice 2090 297 Laga 0.82 770 93.0 100.2 107. 90.6 196.6 Laivai 696 0.74 84.1 97.3 211.3 1.61 Lauter 1511 182.5 167.1 Liquica 1383 180.0 193.3 Lore 1.78 1669 201.6 217.2 233.2 Lospalos 1918 2.04 231,7 249,6 268.0 1.82 1707 206.2 222.2 238.6 268.4 79.4 139.3 Maliana 2062 2.19 249.1 85.2 Manatute 610 0.65 1.14 129,3 Oeruss 1070 149,5 2.07 272.2 (Jassi) 1948 235,3 253.5 Quelicai 1728 1.84 208. 224.9 3117 3,32 405.3 435.6 Solliada 2396 7.55 289,4 311.0 334.6 Sital 1355 1.44 163.7 176.3 189.4 Totuala L61 1511 82.5 196,0 211.2 Uatolari 1879 2.00 227.0 244.5 262.0 85.3 213.1 91.9 229.6 Vemasse 706 0.75 Venilale 1764 1.88 1.68 246. Viguegu 1577 190.5 205.2 220.4 Zumalai 1328 1.41 160,4 172.8 185.6 OTE AV of the Ministry of Agriculture, Fo d by recent rainfall data if possib re, For [MATF] for the period 1950s - 1990s. These should be supple © DNEPCC 2018 - All rights reserved

Table 6.4 - List of target locations and derived design daily rainfail

5 years

113.6

237.

225.

105.2

289.8

145.9

156.8

Multiplie

2.82 2653

2.09

1.38

Design dally rainfall, R24 (mm/day)

turn p

7 years

1223

345.

255.7

243.4

312.2

157.

168.9

10 years

131.4

370.0

274.6

261. 121.

335.

1611

181.4

Average

n/day)

940 1,00

1965

1870 1.99

671 0.93

2399

1209 1.29

1298

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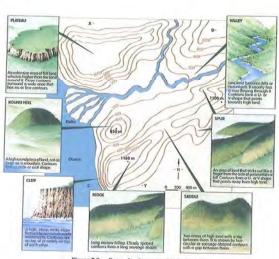


Figure 7.3 — Example of topographic features

Measurement techniques for area include; transferring the catchment outline onto square-lined paper using tracing paper; Importing and acaling maps into computer aided design (CAD) software; and using digital elevation models (DEMs, data) and spatial data in a geographic information systems (CISs, software). Usage of CISs is the recommended measurement technique for accurate results. If possible, a request for information should be made to the CIS & Mapping Section of DNEPCC.

The GIS & Mapping Section can analyse a catchment either by delineating a watershed based on contours (in other words, drawing a polygon shape file to represent a catchment) or by using algorithms to derive watersheds from digital elevation models (DEMs). Examples of algorithms for delineation include 'rwatershed' and 'rwater canter' in GRASS Tools of QGIS colvare, and 'Watershed' in Spatial Analyst toolbox of ArcGIS activare. An example sequence for delineating a watershed from a DEM is as follows:

- Step 1) Fill the depressions in the DEM Step 2) Calculate flow directions Step 3) Calculate flow directions Step 3.1 Choose the point of interest ("Outlet" in QGIS and "Pour Point" in ArcGIS) o Step 3.2) Delineate the watershed o Step 3.2) Delineate the watershed o Step 3.2) Delineate the watershed

 $t_r = t_e + t_f$

7.3.1 Time for inlet flow

Catchment type

Mountainous land

Cut slopes

Urban areas

1/ = L

where

18

7.3.2 Time for channel flow

watercour

The following is the equation for calculation of time of concentration

time of concentration (hours) time of flow from watershed to watercourse (hours), see Table 7.1 time of flow from start of watercourse to point of discharge (hours)

Start of War

Figure 7.6 - Time of concentration

The time for inlet flow is the time for surface flow to travel from the watershed to the start of the

Table 7.1 - Inlet flow times (4)

Inlet time (minutes)

15.0 - 30.0

3.0 - 5.0

5.0

The time for channel flow is the time for surface flow to travel from the start of the watercourse to the point of interest (cuivert). The Kraven Fornula is an empirical equation based on basin data.

Table 7.2 — Velocity of run-off (4)

> 0.010 m/m

~ 0.005 mim

0.005 - 0.010 m

The following is the Kraven Formula for calculation of the time for channel flow:

watercourse length (m) velocity of run-off (m/s), see Table 7.2

Gr

> 1 / 100

1/200-1/100

<1/20

time of flow from start of watercourse to point of discharge (hours)

int of watercourse, G

> 1.0%

0.5% - 1.0%

Watershed

nt of Interest (Culvert

Inlet Flow

7.4 Intensity of rainfall

[5]

10)

171

us), see equation 6

Mé

et Flow

Road

Inlet time (hours)

0.25 - 0.50

0.05 - 0.083

0.083

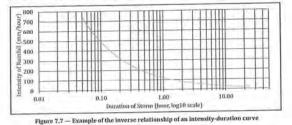
Velocity of run-off, W (m/s)

3.5

3.0

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Generally, storm intensity is inversely proportionate to storm duration for most climates. This inverse relationship means that shorter-duration storms have higher intensity of rainfall and lenger-duration storms have lower intensity of rainfall, as shown in Figure 7.7.



The design intensity of rainfall is when the duration of a storm is equal to the time of concentration, as shown by (b) in Figure 7.0. As shown in (a), when the duration of a storm is less than the time of concentration, then all of the catchinent area is not discharging to the culvert, so it is not the maximum discharge. As shown in (c), when the duration of a storm is more than the time of concentration, then the intensity of rainfall will be lower, so it is shown to the maximum discharge. The of concentration is when all parts of the vatershed start to contribute to the run-off from the basin and this is when the design intensity of rainfall occurs.

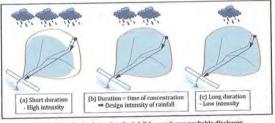


Figure 7.8 — Design intensity of rainfall for maximum probable discharge

As mentioned in Section 5.4, there is insufficient rainfall data in Timor-Leste for creation of intensity-duration curves, such as Figure 7.7. The Monomobe Formula is an empirical equation for estimation of intensity of rainfall. It is a practical solution for applications with few rainfall data.

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(9)

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The following is the Mononobe Formula for calculation of the rainfall intensity:

- $l = \frac{R_{24}}{74} \times \left(\frac{24}{4}\right)^{6.0}$
- where
 - Rpi
 - rainfall intensity (mm/hour) design daily rainfall (mm/day), see Section & time of concentration (hours), see equation 5 t

The disadvantage of the Mononobe Formula is that it may not accurately predict intensity of rainfall for source with a abort duration (+6 hours). It is recommended that Timor-Leste collects rainfall data at 15-minute, 30-minute, 1-hour, 2-hour, 3-hour, 6-hour, 12-hour and 24-hour intervals in all weather stations. Provided this data can be collected, intensity-duration/requency (IDF) charts could be developed by 2050 and hydrological design techniques could be refined.

7.5 Coefficient of run-off

Run-off is water from rainfall that flows on the surface (In other words, surface flow). The amount of rainfall that becomes run-off flow depends on the amount of water lost by infiltration and evaporation. This loss of water due to infiltration and evaporation is represented by a coefficient of run-off. Therefore, the coefficient of run-off is the proportion of rainfall that becomes run-off.

nded coefficients of run-off, C, are shown in Table 7.3. A higher coefficient of run-off indicates rainfall becomes run-off, and likewise a lower coefficient of run-off indicates the less rainfall Recommended coer that more rainfall b-becomes run-off.

If you a catchment area contains different types of terrain, then application of a weighted coefficient is recommended. The weighted coefficient should be calculated as shown in equation 0.

Table 7.3 - Coefficients of run-off (4)

Terrain type	Cuefficient of run-off	Average value
Road surfaces and sloped surfaces	0.70 - 1.00	0.85
Steep mountainous land	0.75 - 0.90	0.83
Genille mountainous land	0.70 - 0.60	0.75
Undulating land and woods	0.50 - 0.75	0.63
Flat farmlands	0.45-0.60	0.53
Flice paddy (fields)	0.70 - 0.80	0.75
Urban areas	0.60 - 0.90	0.75
Foreit zones	0.20 - 0.40	0.30
Catchment areas of mountain streams	0.75 - 0.85	0.80
Catchment areas of small rivers on that land	0.45 - 0.75	0.60
Catchment areas of major rivers of which more than half run on flat land	0.50-0.75	0.63

The following is the equation for calculation of a weighted coefficient of run-off:

 $C = \frac{(c_1 \times A_1 + c_2 \times A_2 + \cdots + c_n \times A_n)}{(A_1 \times A_2 + \cdots + A_n)}$

where

Cin

weighted enefficient of run-off (dimensionless) coefficients of run-off for different types of terrain (dimensionless), see Table 7.3 areas of calchments with different types of terrain (m?), see Section 7.1 A.

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[0]

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The following is the Rational Method equation for calculation of peak discharge: where Qr C $Q_P = \frac{1}{3.6} \times C \times I \times A$ peak discharge or design flood of a watercourse (m²/s) coefficient of run-off, see Table 7.3 rainfall intensity (mm/hour), see equation 7 catchment area of watercourse (km²)

7.6 Rational method

As mentioned in Section 4.5, a simplified process for design lossed on adoption of a rainfall intensity of 200 mm/hour from the *Bridge Design Manual* (2) could be used for small applications on minor routes, such as rural local roads. For reference, design floods of the simplified process are shown to Table 7.4. Table 7.4 — Examples of design floods for small applications using the simplified process

The Rational Method shall be applied for calculation of a design flood. It was first proposed in 1851 by an Irsh engineer called Mulvaney. It is based on a simplistic relationship between estufull and run-off for empirical prediction of discharge from a catchment. This method is appropriate for the following design conditions:

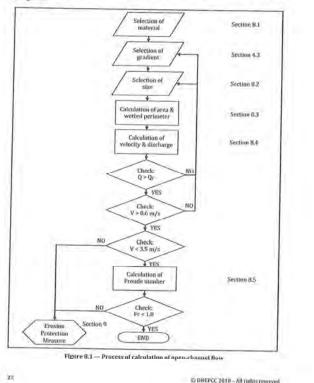
The limitation of application to catchments < 15.0 km² is because the coefficient of run-off cannot accurately represent water storage (or hydrologically complex catchments). The method assumes that intensity of rainfall is uniform over the catchausmich hence, the peak run-off is assumed to occur when deration of a storm equals the time of concentration.

Calculation of peak discharge
 Ingauged after (without streamflow / river data)
 Beterministic analysis based on rainfall
 Calculations without significant water storage (no lakes, no ponds, no wetlands, etc.)
 Applicable < 15.0 km² (7)
 Best suited < 0.0 km² (7)

Coeffic			Desig	n flood, Q	r. (m2/s)	for a catch	ment are	aof		
ient of run- off, C	0,1 km²	0.2 km²	0.3 km²	0.4 km²	0.5 km²	0.6 Icm ²	0.7 km²	0.8 km²	0.9 km ⁷	1.0 km²
0.20	1.2	23	3.4	4.5	5.6	6.7	7.8	8.9	10.0	11.2
0.30	1.7	3.4	5.0	6.7	8.4	10.0	11.7	13.4	15.0	16,7
0.40	23	4.5	6.7	0.9	11.2	13.4	15.6	17.8	20.0	22.3
0.45	25	5.0	7.5	10.0	12.5	15.0	17.5	20.0	22.5	25.0
0.50	2.8	5.6	8.4	11.2	13.9	16.7	19,5	22.3	25.0	27.8
0.55	3.1	6.2	9.2	12.3	15.3	18.4	21.4	24.5	27.5	30,0
0.60	3.4	6.7	10.0	13.4	16.7	20.0	23.4	26.7	30.0	33.4
0.65	3.7	7.3	10.9	14.5	18.1	21.7	25.3	ZB.9	32.5	36.2
0.65	3.9	7.0	11.7	15.6	19.5	23.4	27.3	31.2	35.0	383
0.70	4.2	8.4	12.5	16.7	20.9	25.0	29.2	33,4	37.5	- 148.5
0.80	4.5	8.9	13.4	17.8	22.3	26.7	31.2	35.6	40,0	44.
0.85	4.8	9.5	14.2	18.9	23.7	28.4	33.1	37,6	42.5	47.3
0.00	50	10.0	15.0	20.0	25.0	30.0	35.0	40.0 0 mm/hour	45.0	50.

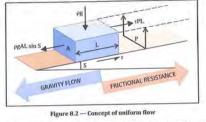
8 Open-channel hydraulics

Open-channel hydraulics is characterised by water flowing under gravity and at atmospheric pressure due to the water surface being in contact with the air (a free surface). The process of design is outlined in Figure 8.1



8.1 Material of culverts

The material (and condition) of a channel determines the roughness. The roughness is the representation of the frictional resistance of the boundary shear force. For uniform flow calculations, the gravity forces must balance the frictional resistance forces which constitute the boundary shear force (t). This concept is outlined in Figure 8.2.



The roughness is represented in the calculation of flow by the Manning number, n. The normal material for construction of box culverts is concrete. The recommended values of Manning number for concrete are shown in Table 8.1.

	- Recommended values of Manning number (4)
--	--	----

Material of culvert	Manning number, r
Concrete: Cast in-situ concrete Factory-made concrete products	0.015

8.2 Size of culvert

It is recommended that selection of the size of a culvert is in accordance with the relevant structural design atandard. For reference, the size of culverts are shown in Table 8.2, Table 8.3 and Table 8.4.

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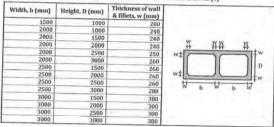
(10)

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Width, b (mm)	Height, D (muit)	Thickness of wall & fillets, w (nm)
1000	1000	160
1000	1500	170
1000	2000	180
2000	1000	220
2000	1500	230
2000	2000	250
2000	2500	260
2000	3000	200
3000	1500	280
3000	2000	300
3000	2500	300
3000	3000	300

Table 8.3 — Standard dimensions for double culverts (9)



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Width, b (mm)	Height, D (mm)	Thickness of wall & fillets, w (mm)	
1500	1000	160	
1500	1500	170	
1500	2000	180	
1500	2500	220	
1500	3000	260	
2000	1000	200	
2000	1500	220	wt C C C C C C
2000	2000	250	
2000	2500	260	wt LILI,
2000	3000	300	
2500	1500	280	W b W b W b W
2500	2000	280	
2500	2500	280	
2500	3000	300	
3000	1500	300	
3000	2000	300	
3000	2500	300	
3000	3000	300	

B.3 Geometry of culverts

The geometry of a culveri affects the frictional resistance. In addition to the boundary roughness, frictional resistance will increase as the size of the boundary increases. The size of the boundary is calculated as follows.

The area is the cross-sectional area of llow in the direction normal (perpendicular) to the direction of Bow, The wetted perimeter is the length of the perimeter that is in contact with the flow measured in the direction normal (perpendicular) to the direction of flow. The hydraulic radius is the ratio of the area to the wetted perimeter, as shown in equation 10. The surface width is the width of the channel at the free surface.

The following is the general equation for calculation of hydraulic radius:

- $R = \frac{\Lambda}{c}$
 - hydraulic radius (m) cross-sectional area of flow (m²) wetted perimeter (m)
- where R A P

The equations for calculating the properties for geometries of some channels are shown in Table 8.5. This guideline is concerning box culverts, so equations for rectangular geometries shall be applied. The equations for trapezoidal and circular geometries have been provided for reference only.

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	Table 8.5 — Geometri	c properties for channel	· · · · · · · · · · · · · · · · · · ·
Ğcometry			
	Rectangle (box)	Trapezold	Circle (pipe)
Area of flow, A (m ²)	$b \times y$	$(b + x \times y) \times y$	$\frac{1}{8} \times (\theta - \sin \theta) \times D^2$
Wetted perimeter, P (m)	6+2×9	$b+2 \times y \times \sqrt{1+x^2}$	$\frac{1}{2} \times \theta \times D$
Hydraulic radius, R (m)	$\frac{h \times y}{h + 2 \times y}$	$\frac{(b+x\times y)\times y}{b+2\times y\times \sqrt{1+x^2}}$	$\frac{1}{4} \times \left(1 - \frac{\sin \theta}{\theta}\right) \approx D$
Surface width, B (m)	6	$b + 2 \times x \times y$	$\left(\sin\frac{\theta}{2}\right) \times D$
Angle of flow, 0 (nadians).			$2 \times \cos^{-1} \left(1 - 2 \times \frac{y}{p}\right)$
b base width (m) y depth of flow (m) D internal height or width per 1-m he width per 1-m he Ø angle of flow (radius)	diameter (m) light of side slope (m)		

8.4 Design capacity of culverts

The design capacity of discharge for culverts is calculated with equation 11. The design capacity should be more than the design flowd, $(Q > Q_2)$.

4.	$=\frac{A^{79}\times S_0^{72}}{\mu^2/3\times n}$	D.0
here		
0	design capacity of culvert (m [#] /s)	
A	area of flow (m ²)	
P	wetted perimeter (m)	
Sa	gradient of culvert (m/m)	

[12]

[14]

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The following is the general equation for calculation of discharge: $0 = A \times V$

where

- design capacity of culvert (m³/s) area of flow (m²) velocity of flow (m/s), see equation 13 QAV
- 26

(13)

Sedimentation and debris affects the hydraulic performance of culverts. A margin of 20% of cross-sectional area (A) is recommended for anticipation of sedimentation. In other words, depth of flow should be designed as less than or equal to 80% of the internal height of a box culvert ($\gamma \leq 0.8 \times D$).

The following is the Manning equation for calculation of velocity for culverts:

 $V = \frac{1}{n} \times R^{2/3} \times S_0^{1/2}$

where

- velocity of flow (m/s) Manning coefficient of roughness, see Table 8.1 hydraulic radius (m), see Section 8.3 culvert gradient (m/m) R 50

The velocity of flow affects the erosion and sedimentation of a culvert. The normal range of velocity of flows are $0.5 \text{ m/s} \le \sqrt{3.5} \text{ m/s}$. In order to reduce the amount of sedimentation, it is recommended that flow velocities are more than 0.6 m/s if not, regular maintenance should be considered. In order to reduce the amount of erosion, it is recommended that flow velocities are less than 3.5 m/s} if not, erosin protection measures should be considered.

Sh	e of culve	rt		D	esign cap	acity, Q. (n'/s) for (gradient o	ſ	C
b (m)	D (m)	y (m)	0.5%	1.0%	1.5%	2.0%	2.5%	3.0%	5.0%	7.0%
1.0	1.0	0.8	1.72	2,43	2.98	3.44	3.84	4.21	5.44	6.43
1.0	1.5	1.2	2.83	4,00	1.89	5.65	6.32	6.92	8.93	10,57
1.0	2.0	1.6	3.96	5.61	6.67	7.93	11.86	9.71	12.53	14,83
1.5	1.0	0.8	3.00	4.25	5.20	6.01	6.72	7.30	9.50	11.24
1.5	1.5	1.7	5.07	7.17	8.78	\$0.14	11.33	12.41	15,03	18.96
1.5	2.0	1.6	7.23	10.22	12.52	14.46	16.16	17.70	22,86	27.0
1.5	2.5	2.0	9.44	13.35	16.35	10.88	21.11	23.13	29,86	35,33
1.5	3.0	2.4	11.69	16.53	20.24	23.37	26.13	28,63	36.95	43.73
2.0	1.0	8.0	4.39	6.21	7.61	11.79	9.62	10.76	13.89	16.44
2.0	1.5	1/2	7.55	10.68	13.08	15.11	16.89	18.50	23,88	28.26
2.0	2.0	1.6	10.91	15.43	18.90	21.83	24,40	26,73	34.51	40.94
2.0	2.5	2.0	14.39	20,25	24.92	28.78	32.18	35.25	45.51	53.04
2.0	3.0	2.4	17.94	25.37	31.07	35.88	40,11	43.94	\$6.73	67.17
2.5	1.5	1.2	10,20	14,42	17.66	20.39	22.80	24.98	32.25	38.15
2.5	2.0	1.6	14.07	21.06	25.79	29.78	33.30	36.47	47.09	55.77
2.5	2.5	2.0	19.79	27.98	34.27	39.58	44.25	48.47	62.58	74.04
25	20	2.4	24.82	35.10	42.99	49.64	\$5.49	60.79	78.48	92.86

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44.21 51.04 57.07

Protection measures are necessary where eronion can occur. Outlets of culverts are more problematic and examples of erosion are shown in Figure 9.1. Generally, erosion occurs where:

Figure 9.1 — Examples of erosion at culvert outlets (7)

Erosion upstream of culverts is rarely a problem if inlets have standard wing walls. In case of erosion, provision of stone pliching or gabion mat, or construction of a concrete apron between the wing walls is usually sufficient. Stone pliching of size 200 mm and for a distance of twice the culvert height is normal, as shown in Figure 9.2. A concrete apron at the infet is shown in Figure 9.3.

Barrel

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Figure 9.2 — Inlet protection using stone pitching / gabion mat

velocity of flow is high / flow is supercritical, see Sections 8.4 and 8.5 direction of flow changes rapidly (i.e. sharp bends), see Section 4.4

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9 Protection works

9.1 Inlet protection

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0.5 Type of flow

hi addition to velocity of flow, the type of flow should be considered when assessing if erosion protection measures are necessary. The type of flow can be considered with the Froude number, as shown in Figure 8.3. The Froude number indicates the flow type as follows:

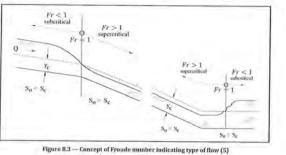
- Fr > 1 : supercritical flow (fast) Fr = 1 : critical flow (change point) Fr < 1 : subcritical flow (slow) .
- .
- The following is the equation for calculation of Fronde number and simplification for box culverts:
- $F_{i}^{\nu} = \frac{\nu}{(y \times \nu)^{0.5}} = \left(\frac{Q_{\mu}^{2} \times h}{g \times (y_{\mu} \times b)^{2}}\right)^{0.5}$ where

- where Fr

- $\label{eq:provide number (dimensionless) velocity of flow (m/s) gravitational acceleration (m/s^2) = 9.81 m/s^3 depth of flaw (n) pieak discharge or design fload of a waterenurse (m³/s) normal depth of flow (m) base width of evolver (m) gravitational acceleration (m/s³) = 9.81 m/s³$ r.
- 5-D

Normal depth of flow, y_{in} can be calculated by changing the depth of flow, y_i and subsequently recalculating the area, A_i and wetted perimeter, P_i for equation 11 until the design capacity is equal to the design flow ($Q = Q_P$). Alternatively, the Newton-Raphson Method may also be used for efficient convergence of $Q = Q_P$.

In addition to high velocity of flow, erosion protection measures at outlets should be considered for supercritical flows where $F_7 > 1$. Recommundations for selection and dimensions of erosion protection measures are outlined in section 9.





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Wing wall



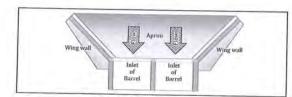


Figure 9.3 — Inlet protection using runcrete apron

9.2 Outlet protection

Erosion downstream of culverts is more frequent because of the change in velocity of flow. The change in velocity of flow is because of the difference in cross-section and roughness of channel. The purpose of protection measures is to reduce the velocity until it is similar to the flow in the natural channel.

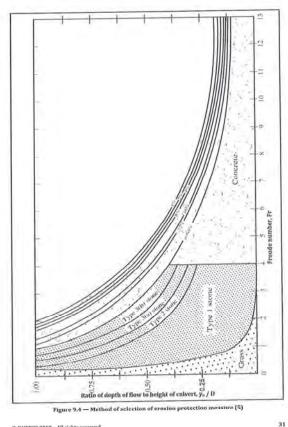
Erosion protection measures are a standard part of construction for outlets. For normal applications, measures for outlets are similar to infest, as shown in Figure 0.2 and Figure 0.3. In cases where erosion is a serious contern, a structure for energy dissipation is recommonded. The following structures are possible solutions for erosion protection at outlets:

- Type 1 stone stilling basin, see Figure 9.5
- Type 2 stone stilling basin, see Figure 9.6 Type 3(a) and 3(b) stone stilling basins, see Figure 9.7 and Figure 9.8 Type 5 concrete stilling basin, see Figure 9.9

9.2.1 Selection of protection measure

The method for selection of an appropriate erosion protection measure is shown in Figure 9.4. Two lines should be drawn perpendicular to axes. The intersection of two lines shows the recommended measure.

Normal flow depth at the outlet and Proude number are required for this selection method. Normal flow depth and subsequently the Froude number for box culverts can be calculated according to Section II.5. The y-axis is ratio of the normal depth of flow to the height of culvert, y_e/D , and the x-axis is the Froude number, f_P .





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9.2.2 Detailing of protection measures

The recommended dimensions and construction of erosion protection measures are shown in Figure 9.6, Figure 9.7, Figure 9.8 and Figure 9.9.

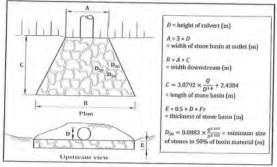
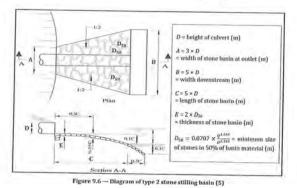
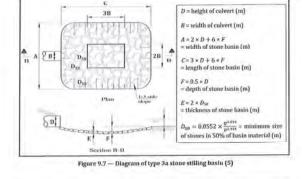
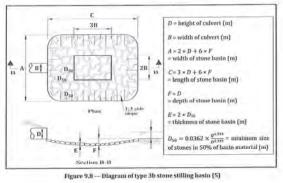


Figure 9.5 — Díagram of type 1 stone stilling basin (5)







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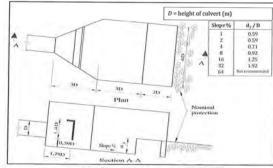


Figure 9.9 - Diagram of type 5 concrete stilling basin (5)



lingfinh	Tetun / Portuguese/ Indonesian	Tapanese
Alignment	Alinhamento / Penjajaran	線型
Allowance height	Altura / Tunjangan tinggi	余拓高
Annual maximum daily rainfall	Chuva diária máxima anual	年最大日降雨量
Annual rainfall	Chuvas anuais	和期時詳議
Area (cross-section of flow)	Área (seção transversal do fluxo)	通水断面情
Artificial channel	Canal artificial / Saluran buatan	人工水路
Rasin	Bacia/Baskom	違威
Catastrophe	Catastrophe / Malapetaka	世書
Catchment area	Área de captação / Area tangkapan	巢水地城
Channel profile	Perfil do canal	講形版面
Coefficient	Coeficiente	体数
Critical depth	Profundidade crítica / Kedalaman kritis	庭辨谱度
Critical flow	Fluxa critico / Aliran kritis	限界の流れ
Departure	Partida	缅范計算
Depth (of flow)	Profumilidade (do fluxo) / Kedalaman (arus)	水滨
Discharge	Descarga	排水
Discharge capacity	Capacidade de descarga / Merancang kapasitas debit	通水量
Duration	Duração	304100
Elongated	Alongada /Memanjang	伸びた
Emptrical	Empírico	経動的
Ernsion protection measure	Medida ninsa atu prvene erosaun	设介防止工法
Evaporation	Evaporação	燕発
Extrapolation	Extrapolação	外师
Factor	Fator	因子
Flood hazard	Perigo de inundação / Bahaya banjir	洪水の危険
Flow	Fluxo / Mengalir	読れ
Frequency	Frequência	周波粒
Friction	Atrito / Gesekan	厚旗
Frictional resistance	Resistência à fricção / Resistensi gesekan	きしか反応
Froude pumiler	Nural Froude	フルード故
Gradient	Gradiente/Kemiringan	流路勾配
Gradient / bed slope	Gradiente / Encosta do rio / lereng sungai	均配
Gravitational acceleration	Aceleração gravitacional / Percepatan gravitasi	重力加速度
Headwates	Kedalaman air di Upstream	上版
Height of colvert (internal)	Altura do cais (interno) / Tinggi gornng- gorong (internal)	逝き
Hydraulic jump	Salto hidráulico / Lampatan hidrolík	雞水
Hydraulic mean depth	Profundidade média hidráulica / Hydraulic mean depth	man a carrier
Hydraulic radius	Rato hidráulico / Radius hidrolik	轻泽
Infiltration	Infiltração	浸潤
Influence	Influência	能W
Interpolation	Interpolação	内博
Lag	Atraso/ Ketinggalan	時差 (遅れ)
Limitation	Limitação	新用
Longitudinal section	Seção longitudinal	BERGIN
Magnitude	Magnitude	マガニチュード

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English	Tetun / Portuguese/ Indonesian	Japanese
Manning's roughumss confficient	Exeliciente de rugosidade de Manning / Koefisien kekasaran Manning	和理经验
Maximum 24-hour rainfall / Probable daily rainfall	Chuva máxima de 24 horas / Chuva diária provável	除乎目時而象
Mean	Média	驱防
Natural channel	Canal natural / Saluran alami	自然水路
Newton-Raphson method	Metodo Newthon-Raustion	ニュートン・ウアソン社
Normal depth	Kedalaman normal	- 界直水流
Normal flew	Aliran normal	暴滅の流れ
Occurrence	Ocorréncia / Kejadian	発生
Peak	Pico/ Puncak	ビーク (最大)
Ponding	Ponding/ Kolam	たん水
Prediction	Predição	子淵
Probability	Probabilidade	藏街
Probability distribution	Distribuição de probabilidade	建中分布
Rainfall	Chuva / Precipitação	13:01
Rainfall intensity	Intensidade da chuva	每曲強度
Rational Method	Método Racional (hídrología)	合理式
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	Média ponderada	加重平均
fetted perimeter	Perímetro molhado / Perímeter erbasah/Keliling basah	周辺
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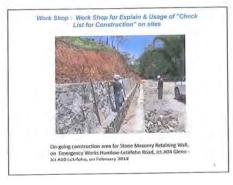
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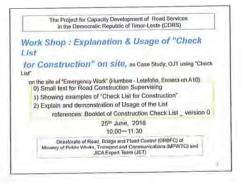
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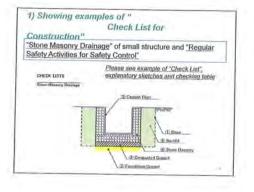
Attachment 4

Workshop "Explanation & Usage of checklist for Construction on Site on 25 June 2018





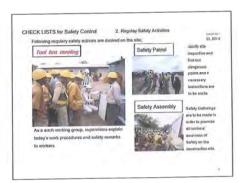




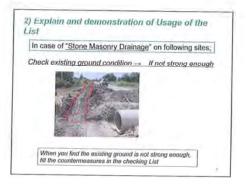
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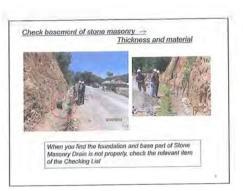
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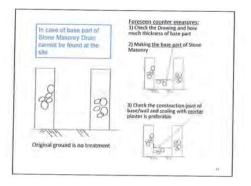
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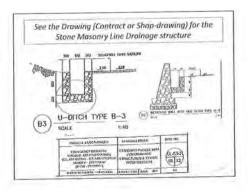


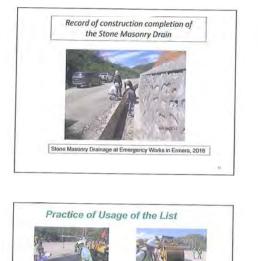


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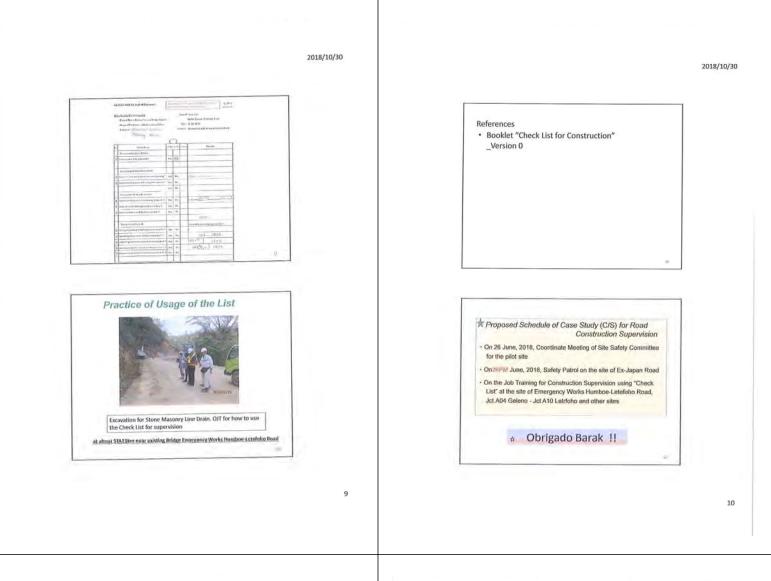




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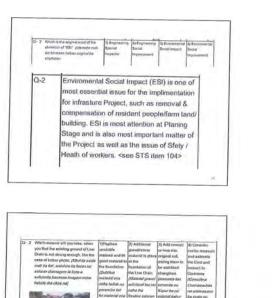
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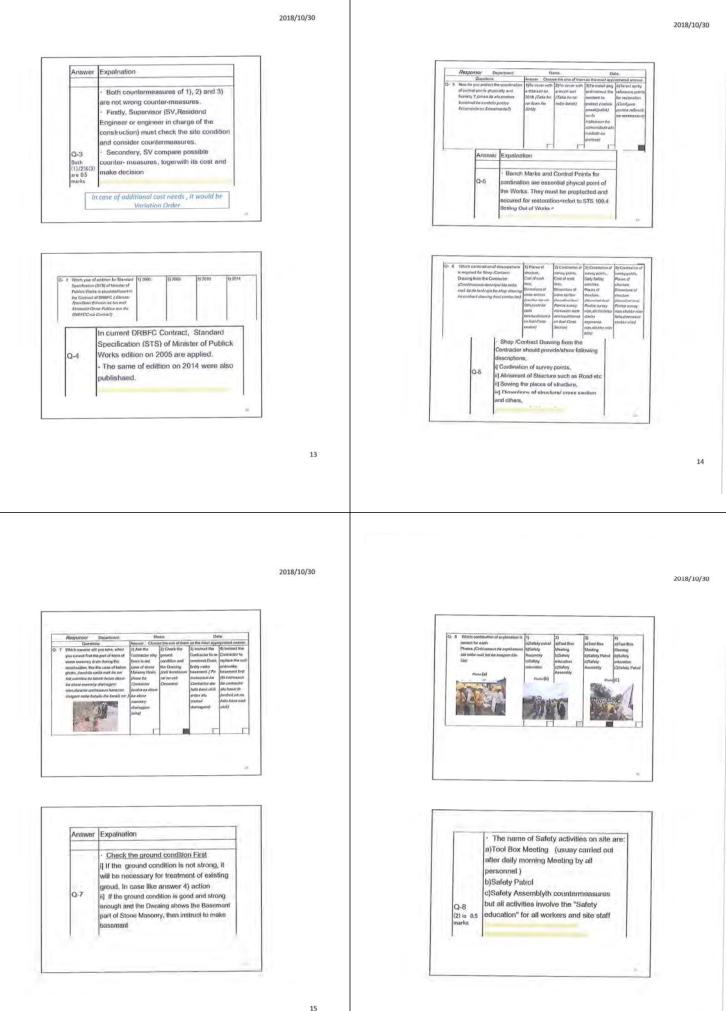
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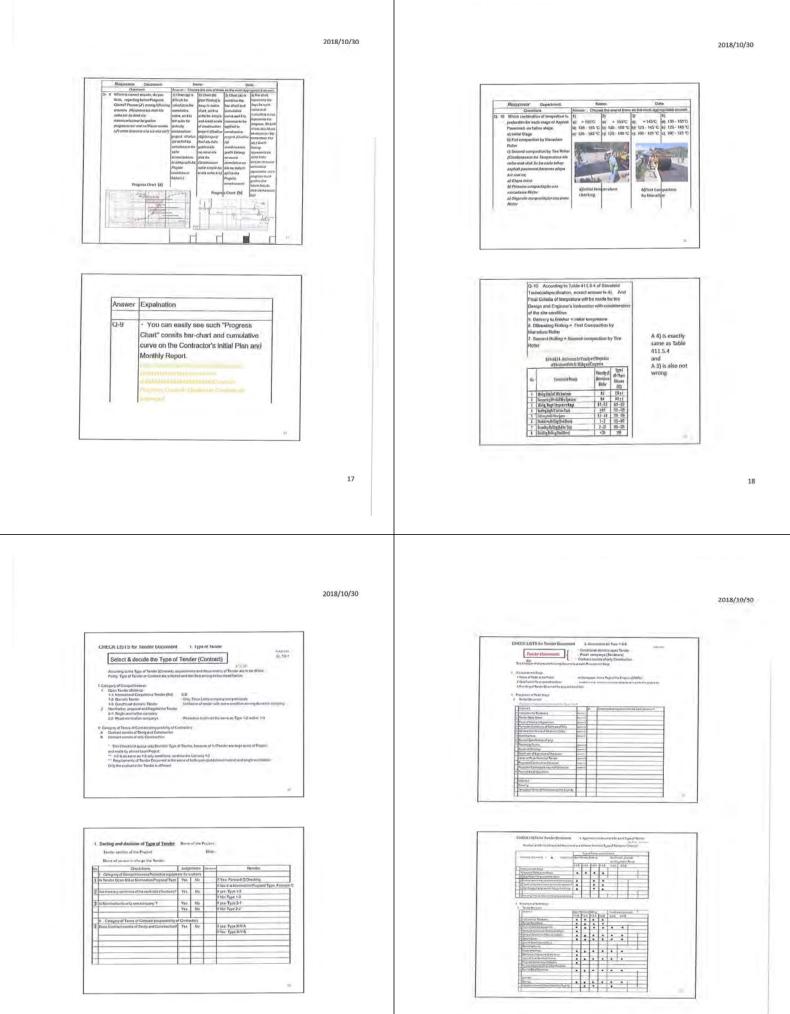




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Attachment 5

Record of 1st Coordination Meeting of Site safety patrol and record of 1st safety patrol by DRBFC on 26 June 2018

The Project for the Capacity Development of Road Services in the Democratic Republic of Timor Leste (CDRS

The Depend for the Canasity Development of Road Services in the Democratic Resublic of Timer Leste (CDRS)

Enclosure :

29 June, 2018

Record of Coordination Meeting of Site Safety Committee and Safety Patrol by DRBEC (For Case Study activity of CDRS project; Safety Patrol by DRBEC)

Members of Site Safety Committee for DRBFC Safety Activities

This is the record of the Coordination Meeting of Site Safety Committee and Safety Patrol by DRBFC for said Case Study of CDRS project. Date/places and the record of the discussions in the Meeting and Pinding of dangorous

point are follows. Reference information is shown herewith in the attachments.

1, Date and Places

 Coordination Maeting of Site Safety Committee Time and Date : 10:00 - 11:20, Tuesday 26 June, 2018 Venue : Conference room of DRBFC, Dili
 Safety Patrol by DRBFC

Time and Date : 14:30 - 16:30, Tuesday 26 June, 2018

- Plnem (D): STA 18+300, Footway construction using precast concrete block Constructed by "Survise" management by "NTN"
 STA 7 – 8km, Stone Masoury Retaining Wall
 - Constructed by "Mijori" management by "Jonise"

2. Discussions in the Meeting

Opening speech by Mr. Nazario, a coordinator of the Committee, with explaining the
objective of the meeting for pilot safety patrol by DRBFC and how to coordinate the
member of the safety patrol and introduce the member of afety committee, what kind
of the activities the committee member will do during the Patrol.

* After Mr. Nazario finish the speech CDRS Expert continue the meeting with the

 Ancer any relation initial the spectra CDRS is part contained the intering write the explanation of Safety patrol procedure, objective of the safety patrol and explanation of usage checklist for safety patrol.

Agenda and attendance list are referred to the attachments #1 '3. Following question/answer and discussion were made during the Coordination Meeting:

literard of Courdiantian Meeting and 1= Safety Patrot by DRBSC

Question / Answer

1) Selection of the committee member and Who in charge of the Committee Q1/ Contractor: Base on the procedure of safety patrol on slide number 7, in first part

(a) Contactor base on the procession of same y parts on same number 7, in max part mention "Organize the site by safety committee", the question is who will in charge for this committee?

A2/ CDRS advisor: Firadly Director of DRBFC instructed the Construction Department in carry out Safety activities and organize the Site Safety Committee. And the Chief of Construction Dept. requested contractors to participate such Safety Activities and other observing member were selected by each Department Chief's recommendation. Usually, safety patrol conducted by contractor consist the Client, the Consultant and Financial support, but this safety patrol is introduce to DRBFC, that's why it's conducted by DRBFC, but still including the contractor and the consultant.

2) How approach the initiative of Safety Activity

Q2/ JICA representative: How you approach this initiative to the Director?

A2/CDRS adviser: In 2016 and 2017, we conducted Lectures for Safety and Observations of Safety activities on Up Comoro Bridge construction site. In those activities, explanation of the importance of Safety and introduced to execution of Safety Activities

And it is made of the understanding of the Director because of the without Instruction/Initiative from the Director, any action cannot start with.

3) Objective of Safety Patrol

Q3/ Contractor: what is the objective of this safety patrol?

9

AB/JICA representative: the goal is to ensure the safety of workers, because if safety is guaranteed the project will automatically run smoothly, activities undertaken in safety patrol are inspection of the project site and discussing about what is found on the project site and recommend to the contractor to repair.

Comments / Suggestions

CS1/ Coordinator of the Committee: DRBFC appreciates the initiative form JICA EXPERT Team (CDRS), how to implemented safety Patrol in the Future.

 $\mathrm{CS2}\prime$ DRBFC member: It's better for the sufety patrol us also including another ministry like SEFOPE

Record of Coordination Meeting and 1º Safety Patrol by DRDFC

The Project for the Capacity Development of Road Services in the Democratic Republic of Timor Leste (CDRS)

CS3/ some of the contractor are not concerned about of safety issues because no budget for safety equipment, that is one of reason.

CS4/ Contractor: this meeting is pre-design, it's would be better to invite ADN because sometimes we put the safety worker as importance issues but they did not pay attention, because they think it's not necessary. They have no knowledge of safety

patrol they only know about safety management.

3. Findings of dangerous points and counter measures.

(): STA 18+300, Footway construction using precast concrete block (Constructed by "Sunrise" management by "NTN")

Finding out dangerous point

 Temporary Exit /Entering point looks danger for vehicles because there is no indication from main road to temporary detour road before Chines Quarry Factory

2) Workers don't wear safety hebnet

Expecting counters measures

- 1) To put signboard to show the detour road Exit/ Entrances
- 2) To instruct contractor to let workers to wear safety apparatus

②: STA 7 - 8km, Stone Masonry Retaining Wall (Constructed by "Mijori" management by "Jonise")

Finding out dangerous point

- 1) There is much dust on the site with affecting everybody's healthy condition
- 2) In some work group, workers don't wear safety helmet
- 3) In Rainy season, slope of weak ground is likely to cause the slope collapse and it
- becomes danger for workers.

Expecting counter- measures

1.1) To carry out watering to the dusty road

1-2) To wear musk preventing such dust from the workers

2) To instruct contractor to let workers to wear safety apparatus

Attachment1: Attendance List

2: Photos of Works Shop

3: Agenda of Site Safety Committee

- 4: Hand-out material of presentation of Explanation for Safety Patrol
- 5. Check List for Safety Patrol used on the site on 26 June 2018
 - 3 Record of Coordination Meeting and 1+ Safety Patrol by DRBFC

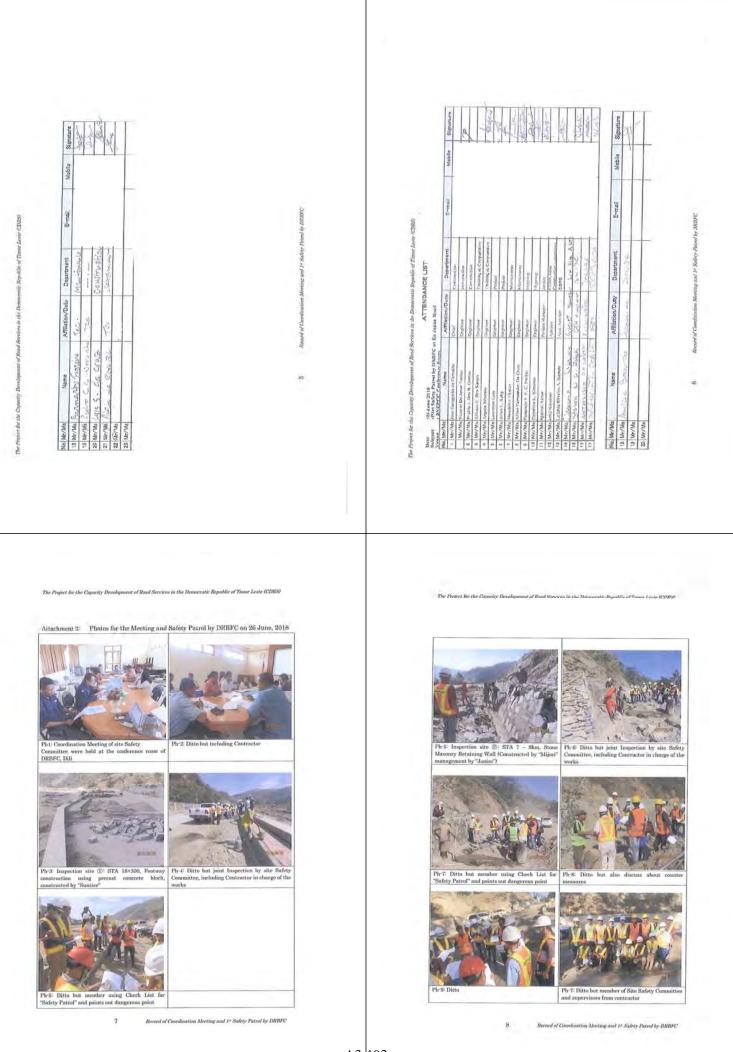
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Record of Coordination Meeting and 1º Safety Par-

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Attachment 3: Agenda of Site Safety Committee Coordination Meeting

For Site Safety Committee for "Safety Patrol by DRBFC"

(Rapat Koordinesi untuk Penilie Keselamatan di lokesi untuk "Pelnili Keselamatan oleh DNEPCC")

Date: Tuesday 26 June, 2018

Time: 10:00 - 11:30 Venue: Conference Room, DRBFC Head quarter, Dill

	AGENDA
09:50 - 10:00	Arrival and Reception for proposed site Safety Committee member attendance
10:00 - 10:10	Opening Address: (Kota Sambutan J Eng. Joao Gregorio de Carvalho Chief of Dep. Construction of DRBFC and Chairman of pilot Site Safety Committee
10:10-10:20	Introduction of the member of pilot Site Safery Committee (Pengenalan anggola panilia dan perconkohan Keselamatan lokasi Proyek) See propored List of member of the Committee (Listat daftar usalan anggola panilia)
10:20 - 10:35	2. Explanation of procedure of Safety Patrol (Peopolasan prosedur dari Patroli Roselarnatan) CDRS, Expert Mr. J. Koizumi (Road Construction Supervision)
10:35 - 11:00	3. Discussion idecision of the Date and Place of 1 ^{4th} Safety Patrol ¹⁴ (Disbusideepidusan langgal dan tempal untuk "Patroli Kosolamatan" Pertama diadatan) See the location Map of Ex-Japan Road construction site (Lihat peta lokasi konstrukto Ex-Japan Road)
11:55 - 11:00	Closing Remarks
11:00	Adjourn

References: 1. Proposed member of "Site Safety Committee" 2. Location Map of Ex-Japan Road construction site 3. Draft of "Check List of Safety Control" on site (Draft Unluk "Check last of Safety Control of Induse Broads)

9 Record of Coordination Meeting and 1st Safety Patrol by DRBFC

Reference 1: Coordination Meeting

Draft of Member of pilot "Site Safety Committee" F. Is and a strength

Party	Role in the	Title and	Name of member	Correspondence	
	Committee	Department	(Draft only)		
DRBFC	Chair person	Chief of Construction Dept.	Eng. Joso Geregorio de Carvalho		
	Coordinator	Engineer in charge of proposed site	Eng. Nazario De Jesus Freitas		
	Sub- coordinator	Construction Dept.	Eng. Pricilla I. Dos R. Gomas		
	Observer	Representative of Training &	Mr. Alfredo E. Dos Santos	-	
	Observer	Cooperation Dept Ditto but Project Dept	Mr Angelo Riberiro Eng. Lourenco, Chief of Planning	t	
			Eng. Julius L. Kelty, Planning Section	1	
	Observer	Ditto but Maintenance Dept	Eng. Mourinho Tilman, Coordinator of Region 2		
		1	Eng. Altino Fernasades Da Costa, Region 2		
	Ohserver	Ditto but Highway Dept	Mr. Fernando F. F. C. Freitas	1	
		-	Mr. Selestino E. Nimenes		
Contrac -to:	Jonise	Project Manager	Mr. Syahrul Akbar	F	
		engineer in charge of Safety	XX	T	
	NTN (NATUREZ A TIMOP	Project Manager or engineer in charge	23	F	
	NAROMAN L44)	of Safety Ditto	bb.	T	
	Mijori	FM or Haff in charge Sufery	çe-		
	Soucise	PM er Stiff in charge Safery	dđ		
CDRS	Advisor(Ad)	CDRS, Road Construction Supervisor	Mr. Johji Koizumi		
	Assistant Ad. and Interpreter	Civil Engineer	Ms Letichia Silveira A. Barreto	1.1	

10 Record of Coordination Mosting and 1st Safety Pairod by DRDFC

Attachment 4: Hand-out material of presentation of Explanation for Safety Patrol

The Project for the Capacity Development of Road Services in the Democratic Republic of Timor Leste (CDRS)





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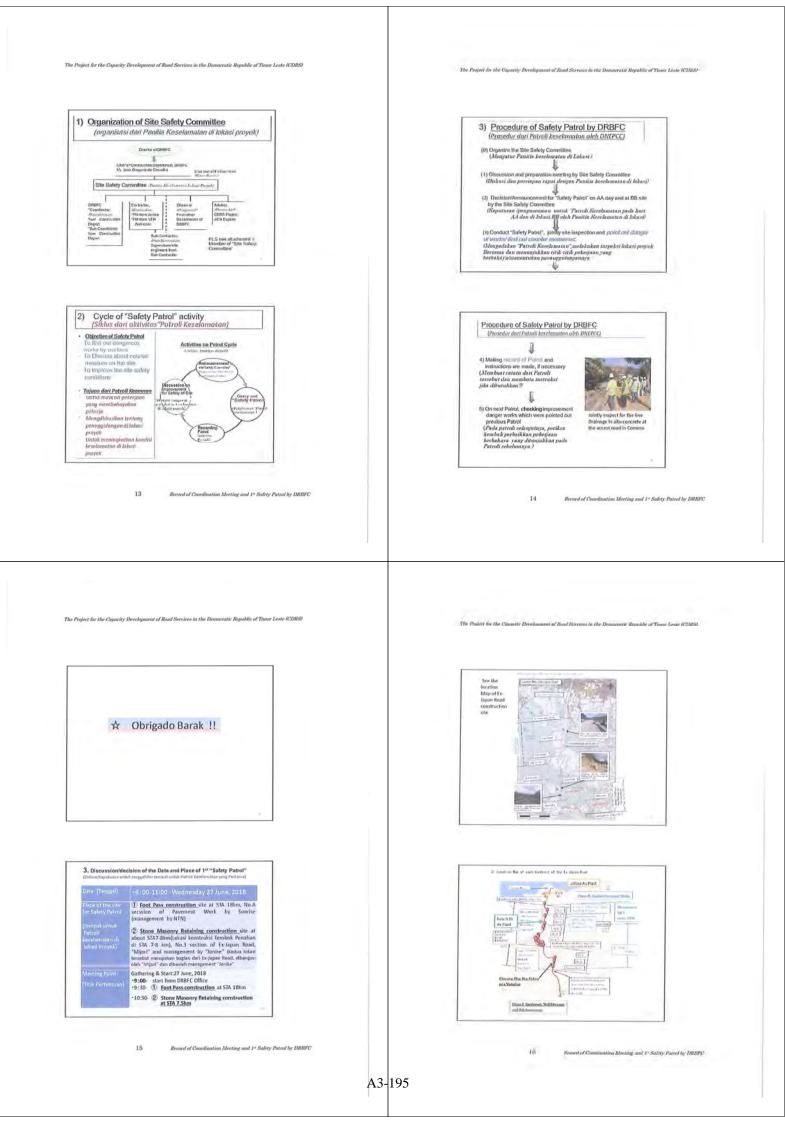
The Project for Capacity Development of Road Services in the Democratic Republic of Timor-Leste (CDRS)

2. Explanation of procedure of "Safety Patrol" by DRBFC (Penjelasan prosedur dari "Patroli Keselamatan" oleh DNEPCG)

26th June, 2018

National Directorate of Road, Bridge and Flood Control (NDRBFC) and JICA Expert Team (JET)

12 Record of Coordination Monting and 1º Safety Patrol by DRHFC



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Record of Coordination Meeting and 1st Safety Patrol by DRBFC

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21 Record of Coordination Meeting and P^a Safety Patrol by DRBFC

The Propert for the Capacity Development of Road Services in the Democratic Republic of Timor Leate (CDRS)

22 Record of Coordination Meeting and 1st Safety Patrol by DRBFC

Attachment 6

Introduction of Guideline of Slope Protection Gravity Retaining Wallon 11 September 2018

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Road Guidelines-Slope Protection-Retaining Wall and Slope Collapese

DG stage

Républica Democrática de Timor-Leste Ministério de Desenvolvimento e de Reforma Institucional

Ministério Geral das Obras Públicas

Direcção Nacional de Estradas, Pontes e Controlo de Cheias

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Document type: Technical Specification Document subtype: Document stage: (WD) Working Draft / (CD) Committee Draft / (DG) Draft Guideline / (FDG) Final Draft Document Janguage: E

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Foreword

In the interest of constructing high quality and economically viable government infrastructure to serve the nation, this guideline for optimal design of slope protection components was prepared by the JICA Project for Capacity Development of Road Services in the Democratic Republic of Timor-Leste (CDRS) in collaboration with the Direcção Nacional de Estradas, Pontes e Controlo de Chelas (DNEPCC, 'National Directorate of Roads, Bridges and Flood Control') of the Ministério Geral das Obras Públicas ('Ministry of Public Works'). We would like to thank [ICA for their continuing support.

September, 2018

His Excellency-

Minister for Development and Institutional Reform Ministério de Desenvolvimento e de Reforma Institucional

Japan International Cooperation Agency []ICA] has been conducting a technical cooperation project for development of capacity regarding road services, which is called CDRS, in order to facilitate the DNEPCC in properly managing and maintaining the road infrastructure that is the basis of sucial and economic activities. To this end, IICA has been dispatching a team of experts from March 2016 to August 2019. As a result of collaborative work with counterparts of the DNEPCC, this guideline for slope protection has been finalized. Those that this guideline will contribute to infrastructure development and maintenance, and to the enhancement of friendly relations between our two countries.

Finally, I wish to express my sincere appreciation to the officials of the Government of the Demacratic Republic of Timor-Leste for their close cooperation with the expert team.

September, 2018

Masalumi NAGAISHI

Chief Representative of JICA Timor-Leste Office

Japan International Cooperation Agency



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Introduction

This guideline was developed by JICA Project for Capacity Development of Road Services in the Democratic Republic of Timor-Leste in collaboration with the Direcção Nacional de Estrados, Pontes e Controlo de Checies (DNEPCC, National Directorate of Roads, Bridges and Flood Control¹) for the purpose of developing institutional capacity regarding slope protection.

Generally speaking, design in civil engineering must stands on geological information and survey drawings instead of impression at the site, Therefore this guideline starts with "Minimum Required Information for Design".

Most of all projects use the common drawings in Timor-Leste. However how many in-house engineers are conscience backgrounds of them, in other words their original design. The guideline treats stability calculations of gravity retaining walls in the common drawings in order to present hints for better user of the common drawings. On the other hand, stability acluisation of gravity retaining wall is front door for other structures design, Maxter of the calculation has got a step to higher level.

Existing countermeasures against slope collapse in Timor-Leste are mainly re-cutting. And existing slope protection methods are vegetation and cover sheet. These means must face limit in many cases of shallow slope collapse. Combination of sewing bar and surface cover structure seems one of most adequate countermeasure against shallow slope collapse. Therefore this method shall be introduced into Timor-Leste to control shallow slope collapse.

There are other types of slope disaster such as rock fall, rock mass failure, mass movement (land slide), debris flow and embankment collapse. This guideline locus on slope collapse on cut or natural slope because of secure capacity development. The project provides other guideline named Slope Profection-Mass movement.

Road Guidelines—Slope Protection—Retaining Wall and Slope Collapse

1 Scope

This guideline consists of three themes, investigation, gravity retaining wall and slope protection.

When some problem in civil engineering occurs the first step of procedure shall be scientific investigation. The investigation must include ground shape and substance. Clause 4 presents minimum required information for design.

Clause 5 to 7 treat gravity retaining wall. Clause 5 shows design procedure of gravity retaining wall. Clause 6 aims to support users of the common drawing in case of selection. Characteristics of Type1 and Type2 are shown. Not of all falled retaining walls are due to shortage of bearing capacity of foundation ground. Clause 7 handles this matter.

Clause B to 12 treat slope stability. Clause 8 and 9 present general information of slope and slope disaster as background knowledge of slope stability. Clause 10 introduces a method of slope stability calculation. Clause 11 is influence analysis on safety factor of slope by surface gradient, shear strength and ground water. Clause 21 is design example of combination of sewing bar and surface cover structure against shallow slope collapse on a cut slope.

This guideline focuses on slope collapse on cut or natural slope because of secure capacity development.

2 Normative references

There are no normative references in this document.

3 Terms and definitions

For the purposes of this document, the following terms and definitions apply,

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at https://www.bouo.g/obu

3,1 retaining wall

wall supporting backfill soil, embankment soil or a cut slope

[SOURCE:150 23469:2005(en),3.46]

3.2

earth pressure pressure from soil on a wall or an embedded portion of a structure [SOURCE: SO 23459:2005(en),3.11]

3.3

bearing capacity of the soil hearing capacity or the soil maximum permissible stress on the foundation soil that provides adequate safety against hearing failure of the soil, or settlement of the foundation of such magnitude as to trapair the structure [SOURCE:ISO 28842:2013(en),3.9]

4 Investigation (Minimum Required Information for Design)

Phenomenon of slope disaster is that ground moves downward by gravity force under influence of water. Therefore Information of ground shape and content, water condition just at disaster occurring can be said the minimum required information for countermeasure design. In many cases water condition is unknown because of no observation so estimation is alternative for it. Survey gives information of ground shape, Geological investigation gives information of ground content.

4.1 Ground Shape

Representative cross section is vital for countermeasure basic design. We can get it easily by cross section survey at the site.

In detail design plan with contour map, longitudinal section and cross sections are necessary as ground shape information. We can study placement, coverage and matching with surroounding land on the plan. And plan must have bench mark which can be found in-site by peg or pin, Longitudinal section fulfils the function to show road longitudinal gradient and elevation and location of survey point. Cross sections of survey point present working area and construction quantity.

Basically geologist iv in charge of geological investigation and civil engineer is an user of geological information however the civil engineer should approach actively geological knowledge to become a smart user. If there is no geologist in the project civil engineer must get geological information by himself.

(1) Geomorphologic approach

Ground shape reflexes ground content, Geomorphologic approach is the first atep of geological investigation. We can get aerial or satellite photo through the internet easily. The photo teaches us ground shape around the target point. Geologist figures out detail geomorphic characteristics such as colluvial deposit, alluvial fan, mass movement fluvial terrace and so on from aerial stereo photograph.

Typical geological contests of mountainside is shown in next figure. When road goes near ridge line weathered soil often appears on cut slope, and near bottom of valley we often face colluvial deposit. These two have potential of

collapse because of unconsolidated layers



Figure 4.1 Birds-eye view of satellite photo

240 Rig

Adapted from bibl. [1] Figure 4.2 Typical mountainside structure

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(2) Surficial geological observation

Surficial geological observation targets; to collect geological information at exposure which can be found cut alope and gully sides, to observe ground water condition through gully stream, trace of flow, apring, and to confirm site-scale geomorphic impression.

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2

(3) Mechanical boring and standard penetration test

(c) inclusion to ing and standard perioritation (e) Most popular mean of geological investigation is mechanical boring and standard penetration text for soil layer. Of course it takes cost and time however there is no other choice to get clear evidence of ground content. N-value since standard penetration test is linked evaluation of hearing capacity and shear strength. Therefore it can be said that N-value is like a common ruler of soil layer. There is a weak point of N-value when a layer has rich gravel, the gravel messes N-value too much bigger. bigger.

Figure 4.3 Mechanical boring and SPT

de s

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(4) Other penetration tests

There are some types of penetration test by man power as shown in figure 4.4. These test can execute far cheaper than mechanical baring but have limits in allowable layer and depth. In the project one Dokenbo is provided to DRBFC for simple geological investigation. Usage manual is compiled as Annex A.

terth in

Table 4.1 Characteristics of penetration tests

	tanderd Periotration Test STT	Displited Dyn Pola Long Depertmilian Test	Saunding, (124)	Partable Constitution task	Prospect of the Sell Level Strength Construction (Seat Defeat to)
Driving Mithia	Dynamic Hammering by Weight	Dynamic Hansmoring by Weight	Static Pushing by Weight and Turning by Hand	Static Pushing by Hand	Static Pushing by Hand
Power Portability	Mechanical Power Un-portable	Man power 16kgf / 1set	Man power More than 100kgf	Man power	Man power 4.5kgf / 1set
	Sampler 451mm	Cone dp75mm	Screw-point \$33.3mm	Cone @28.6mm	Cone diSeam
Rod Disméter We sha and Stroke	440.5mm 63.5kgt, 760mm	ф16mm 5kgf, 500mm	¢19mm 5,15,25,50,75,100kgf	\$16mm	\$10mm
Unit toolog Longth	30cm, Pre-Blow 15cm	10cm	25cm	Every 10cm	At the Point
	All Soil Layer Except Gravel Layer	All Soil Layer Except Gravel Layer	All Soil Layer Except Gravel Layer	Clayery Layer	Soll Layer except Dense Sandy Layer
	Limitless	15m	15mi	Sm	Sm
	SPT- N: Number of hammering per 30cm penetration	N _e : Number of hammering per 10cm penetration	N _{ta} : Number of half revolution per Im penetration	D: Pushing Load q.: Penetration resistance	W: Pushing Load q _a : Penetration strength
	King of penetration test So many past results Established outcome usage With boring	Downsized SPT	Common test for house foundation in Japan	Test only for solt soil layer	Good for slope investigation Multi use for Soil depth prospection Penetration test Shear strength test

Simplified dynamic cone penetration test



Swedish sounding test

Portable cone penetration test



Prospect rod for soil layer strength Dokenbo





Figure 4.4 Penetration tests by man power

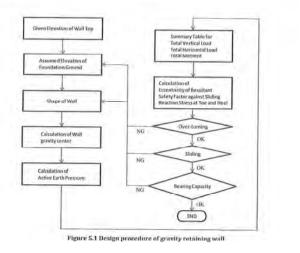
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5 Design of Gravity Retaining Wall

Design of gravity retaining wall seems an entrance door of civil engineering design. It is simple but included an useful method. If you understand it then you have easier way to approach other structures such as gabion wall, bridge abutment, debris flow barrier dam, gravity concrete dam and so on. That why the guideline treats this theme.

5.1 Design Procedure

Gravity retaining wall often applies as stop of embankment, Design procedure of gravity retaining wall is shown in Figure 5.1. The procedure mainly consist of stability catenlation. Self-standing structures such as bridge abutment and gravity data take similar procedure therefore understanding the procedure is good for first step of youth civil engineers.



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5.2 Each step of the procedure

Each step of the procedure will describe along an example as below.

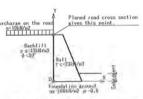


Figure 5.2 Example gravity retaining wall

(1) Given position of roadside wall top

Planed road cross section usually gives position of roadside wall top.

(2) Assumed elevation of wall bottom

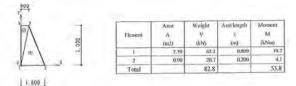
Revation of wall bottom depends on foundation ground condition because the ground must bear the wall. Embedment depth which is distance between ground surface and wall bottom shall be larger than 0.5m

(3) Shape of wall

You can select shape of wall from the common drawings. You also can set up an original shape. In this example type 1 H=3m is selected.

(4) Calculation of wall gravity center

The wall is divided into some simple figure such as triangle to calculate gravity center easily. The excel worksheet can calculate gravity center when you give coordinates of divided triangles with horizontal

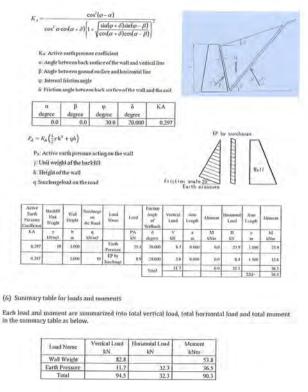


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(5) Calculation of active earth pressure

Retaining wall folds backfill soil then backfill soil gives active earth pressure to the retaining wall. There are some methods to calculate active earth pressure, here we use Coulomb's formul



Sliding Over-turning Bearing Capacity of Foundation Ground

Figure 5.3 Three check points of stability index

(8) Calculation of eccentricity of resultant

(7) Three check points of stability index

X-coordinate of resultant is given as below.

 $X = \frac{\Sigma M}{\Sigma V} = \frac{90.9}{94.5} = 0.956m$

Eccentricity of the resultant is given as below

 $z = X - \frac{\theta}{2} = 0.956 - 0.900 = 0.056m$

Allowable eccentricity is B/6=0.300m, therefore the resultant drops within the middle third, check point against over-turning is passed.

 $e = 0.056m < \frac{n}{6} = 0.300m$ OK

(9) Calculation of safety factor against sliding Safety factor against sliding is given as below. The factor is bigger than 1.5 then check point against sliding is passed

 $F_{S} = \frac{\mu \Sigma \Psi}{\Sigma H} = \frac{n 6 \times 94.5}{32.1} = 1.76 > 1.5 \text{ OK}$

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(10) Calculation of reaction stresses at wall toe and heel

Reaction stresses at wall toe and lieel are given as below

 $q_{l} = \frac{\Sigma V}{\mu} \left(1 + \frac{\omega e}{\mu} \right) = \frac{94.5}{1.000} \times \left(1 + \frac{\omega \times 0.056}{1.000} \right) = 62.3 \, kN/m^{2}$

 $q_h = \frac{\Sigma V}{n} \left(1 - \frac{4\pi}{n}\right) = \frac{945}{1.000} \times \left(1 - \frac{6\times0.056}{1.000}\right) = 49.6 \, kN/m^3$

The stresses are smaller than allowable stress 200kN/m2 then check point against bearing capacity B passed.

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Retaining wall must pass three check points of stability index. They are over-turning, sliding and bearing capacity of foundation ground. They are checked by eccentricity of resultant, safety factor against sliding and reaction stress at wall toe and level.



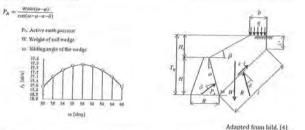
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5.3 Active Earth Pressure by Backfill

When a slope stands just behind of the wall trial wage method is applied for active earth pressure calculation instead of Coolomb's equation. The earth pressure is presented as next equation. W is weight of the wage, when sliding angle ω is assigned then W ran he calculated. Maximum value of PA is trajected earth pressure value.



We must determine unit weight and shear strength of backfill for earth pressure calculation. We can refer next table for it.

Table 5.1 Unit weight and shear strength of backfill

	Unit weight.		
The strength	(k#1/m3)	(degree)	(kN/m²)
	20	35	o
	19	30	0
	18	25	0

Adapted from bibl. [8]

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5,4 Foundation Ground

We also need to determine allowable bearing capacity and friction coefficient between wall and foundation ground. We can refer table 5.2 for it. If you face more weak ground then you can refer Table 5.3 and 5.4.

Most of all failed retaining walls are due to shortage of bearing capacity of foundation ground. Estimating bearing capacity is one of the most difficult matter for engineer. Durable ground such as base rock layer or diluvium layer has no problem. In contrast weak ground such as collovium or heavily weathered rock requires us correct evaluation. Geological information through investigation help us to evaluate the ground. Classification, oldness and SPT-N (Standard penetration test N-value) are reliable information. Direct observation of foundation ground during working is last chance for evaluation.

Table 5.2 Allowable bearing capacity and friction coefficient of foundation ground

Pyre Informations around Rest Truck June Rest Truck June Set Truck, Mathiane				Unconfined compressive strength	SPT N vale
		(k21/m²)		(ktt/m²)	
		1,000		10,000 and up	
		600	0.7	10,000 and up	
	Soft rock, Mudstone	300		1,000 and up	-
	Deme one	600	0.6		
	Not dense one	300	0.6		
	Dense one	300	0.6		30 to 50
	Mediumone	200	4.6		70 to 30
	Very stiff one	200	0.5	200 to 400	15 to 30
	Still one	100	0.5	100 to 200	10 to 15

Adapted from bibl. [8]

Table 5.3 Index on site to estimate bearing capacity for sandy layer

	Very loose	Reinforcement bar \$\phi13mm\$ easily penetrates by the hand.	0	Less than 4
	Loose	Scoop-able by the hand with shovel	50	4 to 10
	Medium	Reinforcement bar \$13mm easily penetrates by the hand with 2.2kgf hammer.	100	10 to 15
Sandy (nýr)		Same as above Some effort is required.	200	15 to 30
	Dense	Same as above Depth reaches approx. 30cm.	300	30 to 50
	Very dense	Same as abave Emitting metallic sound Depth reaches approx. Scm.	300	Greater tha 50

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Table 5.4 Index on site to estimate bearing capacity for clayey layer

	Very soft	Fist easily penetrates about 10cm depth.	0	Less than 2
	Soft	Thumb easily penetrates about 10cm depth	20	2 to 4
	Medium	Thumb penetrates about 10cm with medium effort.	50	4 to 8
Flayev Lover	stiff	Thumb dents the surface with normal effort and penetrates with much effort	100	8 to 15
	Very stiff	Remove-able with spade	200	15 to 30
	Hard	Removing requires pickax	200	Greater than 30

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6 Gravity Retaining Wall in the Common drawings

DRBPC has the common drawings which frequently appear in many projects for labor-saving about drafmage, cross-culvert, retaining wall, gabion, pavement and so on. This chapter treats gravity retaining wall in the common drawings.

6.1 Shape of the Walls

There are two types of gravity retaining wall in the common drawings, these shapes are shown as below. Type1 has vertical backside and around 1:0.4 gradient on front side. In contrast Type 2 has inverse 1:0.45 to 0.49 gradient on back side and 1:0.1 gradient on front side. Width of top is 0.6 m for bath type.

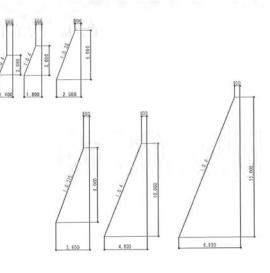
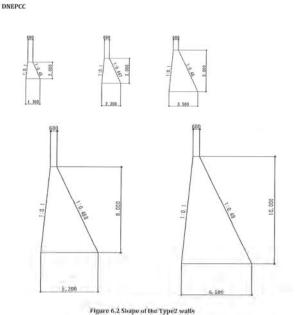


Figure 6.1 Shape of the Type 1 walls

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6.2 Result of stability calculation

These tables show the results of stability calculations on the Type1 and Type2. Calculation conditions are; backfill height is as same as wall top, backfill surface is bortzon, earth pressure is calculated under backfill unit weight 19kH/m³ and friction angle 30deg, road surcharge 10kH/m² on road surface.

Table 6.1 Result of Type1 stability calculation

Walk Build:				Farth Presson		Aanad Some		Articl Semanary		Aread Semenary		untu -	Biorng Capacity
Walitangka H	inie Wilth D	CS_Arcs	Foul LP PA	Vanimal I P PAV LN/10	Donnana 1F PAH NSa	Security EV	Xigna (H XH XH	Summe Manufatt SM KNm	Expension Longin B	6478	Max Beautien Miteen gmax kN/m2		
	1.40	2.00	17.24	5.93	16.70	31.90	16.30	57.43	1001	-0.09	-40,4		
- 1	1:00	3.60	34.54	0.74	32.27	9151	32.25	84.00	11011	0.03	54.5		
	2.50	2.78	85.45	29.24	\$0.12	307.54	\$9.32	22910	0.144	0.13			
	1.00	16.50	204.95	69.96	192.22	456.36	192.23	654.19	0.766	0.84			
14	4.60	26.00	317.11	105.12	293.35	794.77	201.12	1,332,30	0.410	0.33	105.		
- 14	640		680.11	232.61		1.478.61	6 VF 07	3,779.74	10.73.9	0.67	1713		

Table 6.2 Result of Type2 stability calculation

	Will Hody			Earth Preasure		1	and Seminary		Decente	ielly.	Being Cignully
vvan stalajet 19	itaar walat. 10	A	PA PA	Vortent EP PAV MCm	PAR	Kamanii V 2.V	Xunn.H 2H 3N	Manara Moncar IM KNm	Decembrie Length	le/B	Max Beachies Smenn April 10 AN 102
	1.70	2.51	30.00	21.56	22.15	74.46	22.13	52 37	0.147	0.12	- 66.5
1							41.39	129.99	0.231	0.16	1010
3	2.30	4.8	67.85	41.42	41.39	141.12					
	3.50	10.25	138.85	113.57	111.06	349.37	10.06	-443.93	8-465	0.00	179.0
	130	- 23.60	181.56	275.80	266.59	318.66	366.50	1.520.60	0.792	(19)	217/
	4.93				407.08	1 799 59	417 118	2 786 91	1 002	0.03	361

6.3 Over-turning Condition

Safety against over-turning is evaluated that resultant force drops within the middle third area of the wall bottom base. This criterion means that there is no tension zone in the base as shown in Figure 6.3.

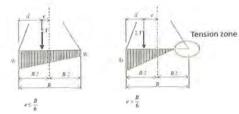


Figure 6.3 Correlation between eccentricity and distribution of ground reaction stress

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It can be given by next equation.

$e \leq \frac{B}{6}$ $\frac{6e}{B} \le 1$

Ge/B which should be called ratio of eccentricity is shown in next figure. All walls pass check point for middle third. This check point does not relate foundation ground but shape of wall and backfill earth pressure. Minus zone of the ratio means that the resultant force drops within heel half side of the wall base.

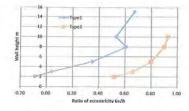


Figure 6.4 Over-turning condition of the walls

6.4 Sliding Condition

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Safety factor against sliding is given by next equation.

 $F_S = \frac{\mu \Sigma V}{\Sigma H} \ge 1.5$ $\mu \geq \frac{1.5 \Sigma H}{\Sigma V}$

Requested friction coefficient between wall and foundation can be calculated by the equation as below figure. Refer table 5.2 (riction coefficients are; base rock layer 0.7, gravel and sandy layer 0.6, clayey layer 0.5. Therefore TypeI with over 7m height must stand on base rock layer, with 3m to 6m height must stand on more than sandy layer and with 2m height can stand on even clayey layer. In contrast TypeZ with all height has no problem about sliding condition.

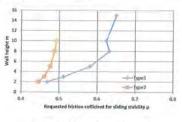


Figure 6.5 Sliding condition of the walls

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6.5 Bearing Capacity Condition

Reaction stress must be smaller than allowable bearing capacity of foundation ground. Maximum reaction stress of foundation ground usually arises at wall too. It can calculated by next equation.

$q_t = \frac{\Sigma V}{\mu} \left(1 + \frac{\delta e}{\mu} \right)$

Type1 has an advantage in this point because the stress is smaller than Type2 at the same wall height. Refer table 5.2 to 5.4 allowshife bearing capacities are; base rock layer 300 to 1,000kN/m², gravel layer 300 to 600kN/m², sandy layer 0 to 3000kN/m³ and clayer 10 to 2000kN/m², in mountain area we very often meet colluvial deposit which consists of clayer matrix and gravel. Clayer matrix can reach to stiff stage at the best condition so that bearing capacity stays around 100kN/m². We can roughly say that soil gravand in mountain area can bear Type1 H54m and Type2 H52m only. Therefor high wall D>5m in mountain area schoold stand on base rock layer because of bearing capacity.

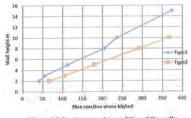


Figure 6.6 Bearing capacity condition of the walls

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6.6 Adequacy of the Types

When you choose the type of gravity wall you shall pay attention below items about adequacy of the type

(1) Cross section area	38	1	1	I T	
Next figure presents comparison of cross section area between Type1 and Type2. Type1 has advantage in this point, more specifically Type1 is cheaper than TypeZ at the same wall height.	Wall Neget m	J	0		

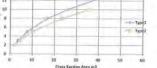


Figure 6.7 Comparison of cross section area

(2) Foundation ground

Type2 has advantage on sliding condition as we studied in section 6.4 but Type1 has advantage on bearing capacity condition as section 6.5. These two conditions are trade off relation, Type1 has smaller 29 than Type2, it can be advantage because of smaller reaction stress of against bearing capacity and can be disadvantage because of smaller resistance force against aliding.

(3) Land form

Figure 6.7 presents adequacy for slope ground. When wall is on hurizontal ground necessary wall height is 5m same for both types. For instance how about on 30deg slope? Type1 needs additional 1.052m to touch the ground at the toe. Type2 can touch the ground with 0.647m addition. Therefore Type2 has adequacy for slope ground.

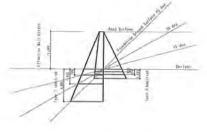
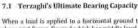
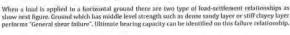


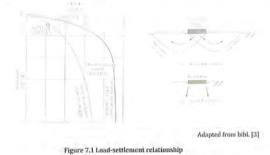
Figure 6.8 Adequacy for slope ground

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As described in section 5.4 estimation of bearing capacity of foundation ground is one of the most difficult matter for engineer. Reference values are given in table 5.2 to 5.4 in section 5.4. This chapter presents another approach for bearing capacity.



Terzaghi who seems the father of soil mechanics made up an equation for ultimate baring capacity as

$\frac{Q}{B} = cN_e + q_z N_q + \frac{1}{2}\gamma_e B N_y$

7 Bearing Capacity

Q: Ultimate bearing capacity of the foundation ground

B: Width of Base c: Cohesion of the foundation ground

qs: Uniform load on the foundation grou nd (Surcharge loads)

yt: Unit weight of the foundation ground Ne, Nq, Ny: Coefficient of bearing capacity

 $N_c = 2(K_{\mu}^{1.5} + K_{\mu}^{0.5})$ $N_q = K_{\mu}^2$ $N_y = \frac{1}{2}(K_{\mu}^{2.5} - K_{\mu}^{0.6})$

 $K_{0} = tan^{2} \left(\frac{n}{4} + \frac{n}{2} \right)$

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7.2 Influence of shear strength for ultimate bearing capacity

When we calculate ultimate bearing capacity by Tergaph's equation we need to set unit weight, cohesion and internal friction angle of the ground. Here we try to know how these values influence the result on two example.

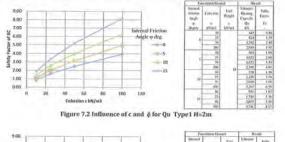
Example1; Type1, H=2m, 2V=51.90kN, 2H=16.20kN, e=-0.021m Result Figure 7.2

Example2; Type1, H=3m, EV=94.54kN, EH=32.27kN, e=-0.011m Result Figure 7.3

 $F_s = \frac{q_u}{\Sigma v} \ge 3$

- Fs: Safety factor of bearing capacity Qu: Ultimate bearing capacity ΣV: Total vertical load

Influence of ground shear strength values is big. Therefore we should be careful for setting the values. If the ground allows Dokenbo shear strength test, we can get some hint from the test result.



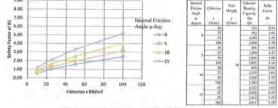


Figure 7.3 Influence of c and \$ for Qu Type1 H=3m



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7.3 Influence of front side slope for ultimate bearing capacity

In mountain area we often have no other choice but setting wall near slope. Here we try to know how front side slope influence the bearing capacity on two example.

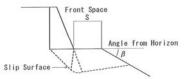


Figure 7.4 Front space and slope angle in case of wall stands near slope

[Calculation conditions]

Resultant forces and eccentricity come from Type LH=3m

Example1; Clayey foundation ground, q=15deg, c=50kN/m², y=18kN/m³

Example2; Sandy foundation ground, $\phi{=}30deg,\,c{=}10kN/m^2,\,\gamma{=}19kN/m^3$

(1) Case of clayey foundation ground

Under S=0m and B=45deg ultimate bearing capacity decreases 55% of horizontal ground in case of clayey ground. Under S=2m Qu stays over 90% therefore we can say 2m front space is effective against influence of front slope in case of clayey ground.

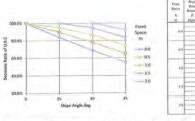


Figure 7.5 Influence of front side slope on clayey foundation gro

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General General Qui NN LINNA Lase . turs toor ft

3.7521 3.7524 3.8754 BAR MAR MAR MAR

[2] Case of sandy foundation ground

Under S=0m and B=45deg ultimate bearing capacity decreases 26% of horizontal ground in case of sondy ground. Under S=2m and B=45deg Qu still decreases 50%. Sandy ground is more sensitive to the influence of front side slope than clayey ground. Therefore we should pay more attention to this case.

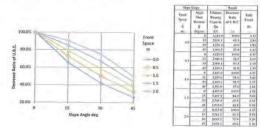


Figure 7.6 Influence of front side slope on sandy foundation ground

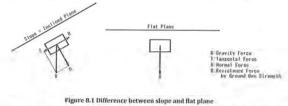


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8 Slope

8.1 Classification of Slope

What is a slope? Slope is not flat but inclined plane, Land in mountain area consists of a lot of slopes. In contrast water surface is not inclined but flat plane. What is the difference between land and water? Water has no shear strength. Land, it means soil and rock mass, can keep its sloped shape against gravity tangential force by its own shear strength. In other word, land bears gravity at all times.



Slope primarily can be classified natural slope and embankment slope. Natural slope can be divided original, collapsed and cut slopes. The table shows characteristics of slopes. Only embankment slope consists of banking material therefore we can control its strength in construction.

Table 8.1 Slope classification and characteristics

Classification			
Natural Slope	Natural Terrain	Natural Ground	Complexity Inhomogeneous Random – Selected material Homogeneous
Collapsed Slope	Collapsed Gradient		Inhomogeneous
Cut Slope	Cut Gradient		
Embankment Slope	Embankment Gradient	Banking Material	material

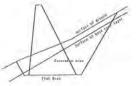
0.2 Natural Slope

Mountain is ordinary made of rock mass except thin soil surface layers. In contrast alluvial plane has thick soil layers. Typical natural slope surface composition is shown in Figure 6.2. Colluvial deposit and weathered soil are surface soil layers. Colluvial deposit has moved by collapse in the past however weathered soil stays on the original position. Collapse often occurs within soil layers because of its weakness.

When collapse occurs in rock layer rock mass almost always brakes along cracks. Strength along the cracks dominate over rock layer collapse.

7.4 Step Cut Foundation

As described in section 6.5 High wall H>5m in mountain area should stand on base rock layer because of bearing capacity. In such case flat foundation requires huge excavation as show right.



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Step cut foundation can solve this problem. Examples are shown in figure 7.7.



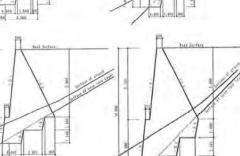


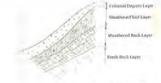
Figure 7.7 Examples of step cut foundation

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Ground water stays in void of soil layers and cracks of rock layers. Increase of ground water very often triggers collapse.



Adapted from bibl. [2]

Figure 8.2 Natural slope surface composition

8.3 Cut Slope

Cut slope is weaker than original slope because of holow reasons. Frist, cutting makes ground stress condition change, Compression stress sometimes changes into tension stress. This phenomenon is called as stress-release. Another, cut gradient must be steeper than original natural slope.



Cut slope is exposed to the air as naked. Rain run off crodes and weathering goes on little by little. Slaking makes nuclstone he broken into pieces. Drainage and slope protection are countermeasures against them.





Slaking

Erosion

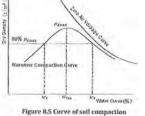
Figure 8.4 Erosion and weathering on the cut slope

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8.4 Embankment Slope

8.4.1 Embaukment Body

We can select embankment material and compaction procedure. Necessary conditions for strong embankment are; material has good grain size distribution, water content is near the optimum water content and compaction energy is suitable. Then embankment can get high density near maximum dry density, it means the embankment has laigh shear strength near maximum strength.



Adequate gradients for embankment are shown in table B.Z. Erosion and weathering occur on embankment slope as same as cut slope.

Table 8.2 Adequate gradients for embankment

Banking materials	Height of embankment (m)	Standard gradient	Remarks
Well-graded Sand (5), gravel, and sand mixed with grave		1:1.5 to 1: .8	To be applied to embankments
(G)	5m to 15m	1:1.8 to 1:2.0	with sufficient bearing capacity at foundation ground,
Poorly-graded Sand (SG)	Less than 10m	1:1.8 to 1:2.0	which is not affected by inundation.
Rock masses (including muck)	Less than 10m	1:1.5 to 1:1.8	Typical unified soll classification are shown in ()
	10m to 20m	1:1.8 to 1:2.0	for reference.
Sandy soil (SF), hard clayey soils and hard clay (hard		1:1.5 to 1:1.8	In case of exception of standard slope is needed the
clayey soils and clay of alluvium, loam, etc.)	5m to 10m	1:1.8 to 1:2.0	stability calculation.
Volcanic cohesive soils (V)	Less than 5m	1:1.8 to 1:2.0	

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9 Slope Disaster

9.1 Classification of Slope Disaster

Figure 9.1shows one of classification on slope disaster. Classification gives you first step to understand what lapping at the disaster site. Table 9.1 gives characteristics of each types, Main subject of this guideline is T1 slope collapse.

TIDO 2 CADADE THE 3 FALLA DE MASA Tipo 4 al Slope is in Tw in for Turne

Figure 9.1 Classification on slope disaster

Table 9.1 Characteristics of each disaster

		Move -ment	Topography	Moving Material	Molsture	Scale	-Speed
10 1	Slope collapse	Slide	Mild - Steep, Low - High slope	Weathered Rock, Soil	Moist	Small-Medium (<5,000m ³)	Rapid
1 2	Rock fall	Fall	Steep, High slope	Rock	Dry	Very Small (<5m ³)	Extremely rapid
r a	mass failure	Topple, Slide, Fail	Steep, Very high slope	Rock	Dry	Medium-Large (>100m ³)	Rapid
T 4	Mass movement	Slide	Gentle slope with characteristic landform	Soil, Debris, Rock	Moist	Large (>5,000m ³)	Slow
15		Flow	Stream Mountainside	Debris, Mud	Liquid	Medium-Large (>1,000m ³)	Rapid
	Road collapse	Slide	Embankment slope	Fill material	Moist- Wet	Small (<1,000m ³)	Rapid

T2 rock fall is common phenomena you have seen somewhere. T3 rock mass failure is special and large scale disaster not often occurs. T4 mass movement (land slide) is commonly the largest scale. Moving hody keeps its shape but breaks into pieces and moving speed is very slow as millimetre per day. However it can be finally changed into collapse and run down.T5 debris flow consists of very thick mud water and debris. Large size debris concentrate to the top of flow and it shows high destructive rapability. T6 road collapse is special because it occurs in artificial embankment.



8.4.2 Boundary between embankment and foundation ground

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Cause for collapse on embankment slope very often come from boundary between embankment and foundation ground. Typical collapses on embankment are shown in figure 8.6. Key points against the collapses are bench cut (step cut), underground drainage and surface drainage.

Figure 8.6 Typical collapse on the embankment slope

water from the or

Sliding serface along the boundary

Adapted from bibl. [2]



T3 Rock mass failure

T5 Debris flow Figure 9.2 Example photograph of rare disasters

9.2 Principle of Slope Disaster Countermeasure

There are 4 principles against slope disaster as shown table 9.2. Control work and deterrence work try to make the slope be stable directly. Control work expects the slope to get stability by itself. Deterrence work gives structural force to get balance with moving force. Traffic protection work try to protect traffic and let the slope be. When you have huge size obstruction, there is a possibility that avoidance plan is the hest answer.

Table 9.2 Principle of slope disaster countermeasure

Classification	Principle
Control work	Control work makes the ground itself be stable. This is basic means of countermeasure. Represented by adoption of adequate slope gradient, subsurface drainage and so on.
	Structure deters soil mass movement by proportioning force. This work is broadly classified two. One counteracts moving force by structure's own weight as retaining wall. Another counteracts by structure's tension or stiffness as anchor or pile.
Traific Protection work	Instead of treating disaster phenomenon directly, protection work protects road / traffic solely. Represented by catch wall, rock fall protection fence, rock shed and so on
	When size of disaster phenomenon is too large to treat from technical point or cost, road avoids disaster point by route change, bridge, tunnel etc. Avoidance plan must be reasonable than countermeasure works.

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9.3 Representative Countermeasure

Representative countermeasure is shown in table 9.3, Each disaster type has a column and each principle has a row.

Table 9.3 Representative Countermeasure

			74 Missimovement	TS Debris flow	Th Road callspice
Cutting with adequate slope gradient Subsurface drainage	Removing of source rock	Removing of source rock mass	Surface water drainage Shallow groundwater drainage Deep groundwater drainage Earth removal works Counter weight embankment	Mountainside works Valley works	Embankment with adequate slope gradient Groundwater drainage
Shotcrete frame Sewing bar works Anchor works	Mortar spraying Concrete pitching Cover type rock fall prevention net Shotcrete cirb Rock bolt works	Wire rope works Adhesive bonding works Rock bolt works	warks Pile works Anchor works	None	Retaining wall Reinforced soil rotaining wall Anchor works
Catch wall	Rock fall protection fence Pocket type rock fall protection net Rock shed	None	None	Keeping of enough flow section Debris flow shed Opened check dam	None

9.4 Countermeasure NDRBFC shall introduce at the First

9.4.1 Target disaster type

Target disaster type at the first shall be T1 slope collapse because;

T1 slope collapse occurs Irequently everywhere. Existing countermeasure recut has limitation and cannot reach definitive solution.

T2 rock fall can be solved by introduce metallic structures such as rock fall protection fence or roch fall prevention net. Rock fall phenomenon is simpler than slope collapse phenomenon therefore civil engineer can solve rock fall problem easier than slope collapse problem.

T3 rock mass failure, T4 mass movement and T5 debris flow occur at certain points not everywhere and not so frequent. Countermeasures against these types generally need high level technology and high cost, Introduction priority seems lower than T1 countermeasure.

To road collapse can be solved by construction methodology such as density control by suitable compaction, bunch cut on the foundation ground and underground drainage.

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9.4.2 Existing countermeasure against slope collapse

Domestic contractor has heavy earth work machines so earth work is the existing methods in Timor-Leste. Countermeasure by earth work against slope collapse is recut. Re-cutting with adequate slope gradient is representative way of control works. There are two ways for recut, recut with gentler gradient and recut on the deeper line. When the road stands near the ridge line these methods can adopt. However the road locates on mountainside then this method application becomes impossible hecause recut line cannot louch the ground surface line till top of the slope.

Ex the Store The Read Store

Presit on the darper lies there is the space for Call 1963

Figure 9.3 Two ways for recut

Table 9.4 Adequate gradient for cut slope

Soil class	sification	Cut Slope Height	Gradient	
Hard rock			1:0.3 to 1:0.8	/
Soft rock			1:0.5 to 1:1.2	/
Sand	Not dense, and poorly graded		1:1.5 to	/
	Dense	Less than 5m	1:0.8 to 1:1.0	
		5 to 10m	1:1.0 to 1:1.2	
Sandy soil	Not dense	Less than 5m	1:1.0 to 1:1.2	
		5 to 10m	1:1.2 to 1:1.5	
	Dense, or well graded	Less than 10m	1:0.8 to 1:1.0	
Sandy soil mixed		10 to 15m	1:1.0 to 1:1.2	
with gravel or	Not dense, or poorly	Less than 10m	1:1.0 to 1:1.2	
rock masses	grade	10 to 15m	1:1.2 to 1:1.5	
Clayey soil		0 to 15m	1:0.8 to 1:1.2	
Clayey soil mixed with		Less than 5m	1:1.0 to 1:1.2	
rock masses or cobble-		5 to 10m	1:1.2 to 1:1.5	
stone				
		Adapted fr	om bibl. [8]	

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9.4.3 Prospective countermeasure against slope collapse

Combination of sewing har and surface cover structure is representative countermeasure of deterrence works. The bars sew unstable soil to stable one and the cover structure distributes sewing effect all around. This method can adopt where recut cannot adopt. This method has wide coverage and ao many actual achievement in Ipapar. Most popular casting is deform reinforcing har for sewing bar and shotcrete frame for surface cover structure.

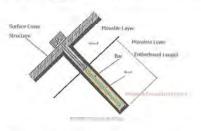


Figure 9.4 Basis of sewing bar and surface cover structure



Figure 9.5 Example of most popular casting

10 Slope Stability Calculation

10.1 Calculating Formula

Calculating formula of slope stability is necessary in order to treat the problem in a quantitative way. We use the simplest one named "Simplified formula" as shown below.

 $F_{S} = \frac{\sum [e_{l}t_{l} + (W_{l} - u_{l}b_{l})cosa_{l}taaq_{l}]}{\sum W_{l}sina_{l}}$

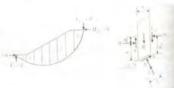


Figure 10.1 Explanation of simplified formula

Sliding surface is supposed as circular arc. Sliding body is divided into a slices by vertical slice lines and slices are treated as rigid bodies. Assumed condition " Acting forces on both side of the slices are even" clanges the problem into statically determinate one. That is why named simplified.

10.2 Calculating Conditions

10.2.1 Shape Information

When we execute the slope stability calculation we need to set up shape information; ground surface line, groundwater surface line, soil layer boundary line and sliding surface line.Gross section survey gives ground surface line. Geological investigation such as outcrop observation and drilling gives hint for groundwater surface line and soil layer boundary line.Groundwater surface line is supposed higher position than usual when collapse occurs. Sliding surface is estimated from shape of actual collapse.

6-11.11 Ground Surface Ground Water Surface Layers Stiding Surface

Figure 10.2 Shape Information

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10.2.2 Soll Characteristics

Soil characteristics are also necessary for the calculation. They are unit weight of sliding body and shear strength of sliding surface.

You can set up unit weight easily because the value stands narrow range. Wet unit weight γ_1 takes 17 to 19 kN/m³ and saturated unit weight γ_{24} takes 18 to 20 kN/m³.

In contrast setting up shear strength is very difficult problem. There are tests to get shear strength such as Dokenbo vane cone test on site and tri-axial compressive strength test in laboratory. However value by test distributes wide range and compatibility between test-value and stability calculation is not so good. Therefore in practical problem reverse calculation method is applied to set shear strength very often.

When collapse occurs the safety factor is estimated as 1.0. It means that the collapse is just on balance so sliding force equals to resistance force. Before reverse calculation one of shear strength factor c (colosion) or ϕ (internal friction angle) should be set on some reason. Then another strength factor ϕ or c can be get by calculation because there is only one unknown in the formula.

10.3 Excel worksheets for slope stability calculation

In the project excel worksheets for slope stability calculation are prepared for training and practical

You input slope gradient and collapse size (height and vertical depth), the worksheet calculates sliding circle (radius and theta). After that other worksheet divides sliding body into 6 slices and calculates values in the slope stability calculation formula with summary table. You can get not only safety factor but also cohesion c or inner friction angle q in reverse calculation.

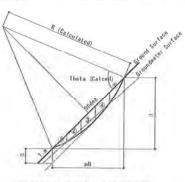
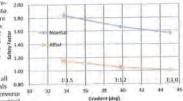


Figure 10.3 Sliding circle arc in the excel sheet

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When collapse occurs on some cut slope, recutting with milder gradient comes into countermeasure candidate at first. Figure 180 11.1 shows how slope gradient influences 160 safety factor. When slope gradient is 11.2 safety factor becomes 1.05. When 11.5 gradient unexpectedly gets small increase 51.00 on safety factor. 100

11 Influence of factors in slope stability calculation formula



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Collapse conditions; slope gradient 1:1.0, all saturated (ground water surface equals 0.86 ground surface), e=30deg, c=7.23kN/m2 (reverse racle), r_{x=2}=20kN/m2/size (height=5m, vertical ilepth=2.07m)

Figure 11.1 Influence of slope gradient

11.2 Shear Strength

factor

11.1 Slope Gradient

Shear strength of sliding surface consists of cohesion c and inner friction angle φ . Both of them has direct influence to safely factor. C has stronger influence than φ . This fact indicates when you execute reverse calculation φ should be set and c should be calculated.

Before you face actual problem you should know how each factor in the formula influences on safety

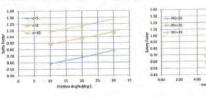


Figure 11.2 Influence of shear strength

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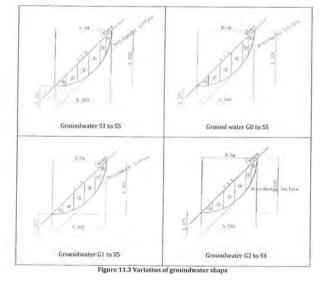
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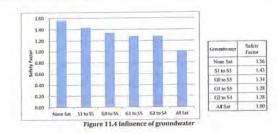
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11.3 Ground Water

Shape of groundwater surface also has influence to safety factor. Here 6 variations of water shape are calculated. None of slices is under groundwater, all of slices are under groundwater and medium portion as shown in figure 11.3.



Result is shown in figure 11.4. Safety factor goes down along groundwater rising. Lower portion of aliding body works for resistance. When buoyancy by groundwater acts these portion resistance force by friction decreases then safety factor gets down. Lateral borehole drainage can be effective rountermeasure when they are set at adequate position.



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12 Design Example of Countermeasure against Shallow Slope Collapse

12.1 Design Procedure

Figure 12.1 presents design procedure of sewing bar and surface cover structure.

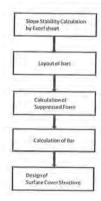


Figure 12.1 Design procedure of sewing bar and surface cover structure

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12.3 Layout of bars

Interval of bars are trade-off relationship between bar diameter and number of bars. Long interval of bars leads large diameter and smaller number of bars. Short interval leads opposite result. Interval of bars generally distributes. 15m to 3m. 2m can be applied for broad cases.

In the example horizontal interval "m" is 2 meters and number of sewing bars on the collapse "n" equals 7,

Figure 12.2 Layout of bars

12.4 Calculation of Suppressed Force

Suppressed force is calculated on below formula.

$r \sum_{i=1}^{n} \sum_{j=1}^{n} \sum_$	$\frac{d_i + (W_i - u_i b_i) \cos \alpha_i \tan \varphi_i}{2} = 1.00$
r ₁₄ =	$\sum W_i \sin \alpha_i = 1.00$
$F_{in} = \sum_{i=1}^{n} ($	$J_i + (W_i - u_i b_i) \cos \alpha_i \tan \varphi_i) + P_T \tan \varphi_i = 1.20$
1 10	STUL 1

$$F_{12} = \frac{\sum W_i \sin \alpha_i}{\sum W_i \sin \alpha_i} = \Delta F_1 = 0.20$$

$$F_f = \frac{\Delta F_1}{\sum W_i \sin \alpha_i} = \Delta F_1 = 0.20$$

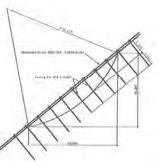
$$F_f = \frac{\Delta F_1}{\sum W_i \sin \alpha_i}$$

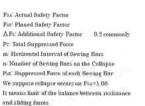
 $P_{i2} = \frac{m}{n} P_{I}$

In the example calculation executes as below, we get $\Sigma Wsinu=242.12kN$ from the summary table of the excel worksheet.

 $P_T = \frac{\Delta F_V \sum W \sin a}{\tan a} = \frac{0.2 \times 242.12}{\tan 20} = 83.87 kN$

 $P_{eB} = \frac{m}{n} P_T = \frac{2}{7} \times 83.87 = 23.96 kN$





12.2 Slope Stability Calculation

In the example slope stability calculation is executes as below.

lipst data of Slope Scalely Calculate Shape of ground surfac Weipte W 32.09 35.80 116.21 116.90 43.14 17.29 Arca Alpha deg 13: 34: 45: 55: 63: -18 Bright m2 1.600 4.791 5.812 5.718 3.144 m 10.14 81 2.438 2.638 2.985 3.423 151 15.2 129 8.35 33.65 63.50 83.55 adient out Manable Errer dep0 2.603 ML depth Grandwater denk r level is as Ge 23.05 Unit scents 18.0 Wattw kN/m) and Phil Target & Fa kNAnk kNAnk tarated UW 20.0 Waler UW 0.8 Calculation Type IF IT made Fa deg Cale Type 11 how de suiter at ow Phi and Ft, Tinget in W este IP IF angle deg 30.0 If If angle 410 Exsiting safety factor is is KNINIZ 10.83 ES Fa 1.00

C. Gives c and Fs. Target to Phil

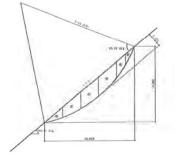


Figure 12.2 Cross section of Slope stability calculation

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12.5 Calculation of Bar

12.5.1 Selection of sewing bar

Reinforcing bar D16 is selected as serving bar. There is possibility that bar will corrode and Jose its: cross section in the future. Diameter Juan is margin for corrosion then cross section is $A{=}176$ num³. Tension stress is calculated as below. The value is smaller than allowable value.

 $\sigma = \frac{p_{c0}}{4} = \frac{21.94 \times 10^4}{17 n} = 136 \le 200 N / mm^2$

12.5.2 Embedment length

The bar is fixed in moveless layer, it is called embedment. If embedment length of the bar passes two check points then the bar can bear against drawing out. They are friction between ground and grout and friction between grout and bar.

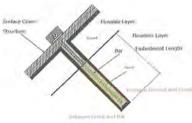


Figure 12.3 Check points of embankment length

12.5.2.1 Calculation of embedment length between ground and grout

Necessary embedment length between ground and grout is calculated on below formula.

 $l_b = \frac{p_{eB}F_{ab}}{\pi \cdot d \cdot \tau} = \frac{23.96 \times 10^3 \times 2.0}{\pi \times 65 \times 0.14} = 1676mm \rightarrow 2.0m$

is: Necessary embediment length between ground and grout to not draw out

Fsb: Safety factor for draw out; Standard value 2.0

d: Drilling diameter, 65mm is popular diameter

r: Ultimate skin friction resistance;

Assumption condition: Gravel layer N-value=20

Then r=0.14 N/mm²

Standard value of ultimate skin friction resistance is shown in table 12.1.

Gr	USFR N/mm		
Base rock	Hard p	ock	1.2
	Soft ro	ck	0.8
	Weathered	1 rock	0.5
	Hard pan		0.5
	N-value	10	0.08
		20	0.14
Gravel Layer		30	0.20
		40	0.28
		30	0.36
		10	0.08
Sandy soil	N-value	20	0.14
		30	0.18
		40	0.23
		ô0	0.24
Ch	Nev soil		0.8×C

12.5.2.2 Calculation of embedment length between grout and har

Necessary embedment length between grout and bar is calculated on below formula.

 $l_b' = \frac{p_{eB}}{\pi \cdot D \cdot \tau_{00}} = \frac{23.96 \times 10^3}{\pi \times 15.9 \times 1.4} = 343 mm < 1676 mm$

P6: Necessary embedment length between grout and bar to not draw out

D: Diameter of bar D16 -> D=15.9mm

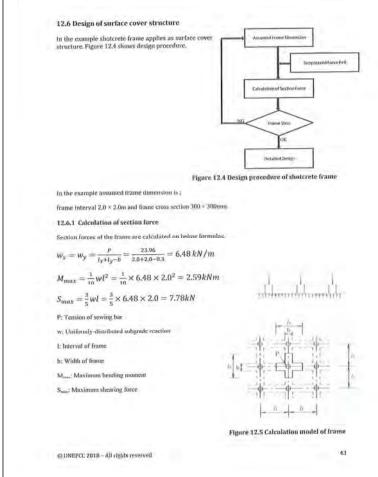
 $\tau_{\rm hat}$ Ultimate skin friction resistance $\tau_{\rm hat}{=}1.4N/ram^2$

Standard value of allowable adhesion stress between grout and deformed bar is shown in table 12.1.

DRSG $\sigma a(N/mm^2)$	18	24	30	Over 40
AAS T to(N/mm ²)	1.4	1.6	1.8	2.0

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12.6.2 Check for frame stress

Check for frame stress is implemented in conditions as rectaugular cross section, single reinforcement concrete and allowable stress design method. All of three stresses pass the check as below.

	Fran	10 CTOSE SC	ction		
	Item	Unit	Value	M	emo
Member width		cm	30.0		
	Member height	cm	30.0		
	effective height	cm	23.5		
Cross-section area of reinforcing bar		mm2	253.4	D13 * 2 Standard Layout	
	Resul	t of calcul	ation		
	Item	Unit	Calculated	Allowed	Judgement
	Compression of concrete	N/mm2	1.24	6.00	OK
Stress	Tension of R.F. bar	N/mm2	47.95	180.00	OK
_	Avelage alien:	N/mm2	0.110	0.400	OK

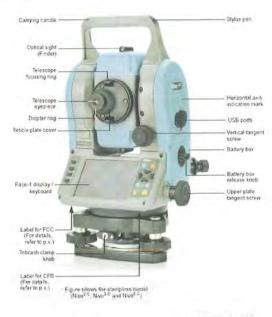
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Annex A (informative)

How to use the Total Station

A.1 Part names

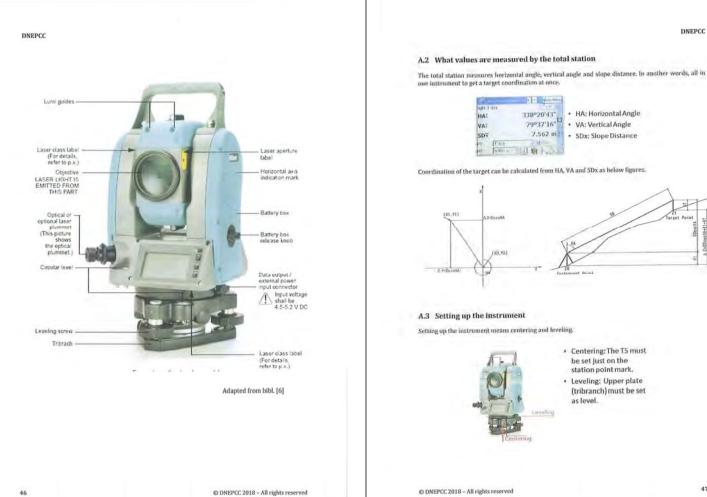


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[Procedure]

- ① The surveyor sets the tripod head as level as and as central as possible.
- Ite places the instrument on the tripod head.
- (3) He inserts the tripod mounting screw into the instrument.
- (i) He levels the instrument adjusting tripod leg length after that using leveling screw.
- The slides instrument on the tripod head by loosening mounting screw to centering with checking by optical plummet.
- (0) He repeats leveling and centering till both conditions are within allowable circles.
- $\overline{ \mathscr{O} }$. If there is only one station point in simple survey such as one cross section, then centering can be skipped.

[How to use the leveling screws]

Left thumb reads level bobble.

Gentle.

Two leveling screws are turned at one time by both thumbs and lint fingers to different direction. It means both thumbs go inside or go outside. Slow and constit.

A.4 General procedure of simple survey

- (f) The surveyor establishes two station points one for instrument another for back sight.
- 2 He sets the instrument on the station point, measures instrument height.
- ② He focuses on the back sight station point, and sets HA=0. Then X axis is set from the station point to the back sight point.
- (i) He orders the pole-man to put the pole on first targer point.
- (6) He focuses on the reflector or the target and pushes the button to measure the slope distance.
- 60 He pushes the button to record and write down target name, target height and the values HA, VA, SD on the field note.
- 0 . He returns the procedure 0 to 0 for all other target points.
- (8) If there is only one station point in simple survey such as one cross section only, then the procedure (1) to (2) can be skipped.

A.5 Calculation of coordination from field Note

The project provides an excel worksheet for calculation of coordination from field note.

[Input table]

Shitket	lestransent Height	ment Targer			1	Heratomai		Venical Angle			Slope Distance
Name		Name Number Height		Heish	Aiek						
-		and the second se	1.2	- 01	den	deg wint:	second	det	minute	second	(11)
Roonti	1.21	Cients A	1	0.95	15	32	- 3	-91	58	24	\$ 27.
(e)einer	1.21	Ceener B	7	1.07	318	-44	38	-91	23	- 21	2.45
	1.21	Click	3	2.49	21	38	. 8	70	10	- 41	3.718
	1.21	ConnerC	4	3.25	50	7	2	74	33	15	7,598
	1.21	Conser D	5	3.24	95	.15	41	75		- 31	7.991
_			1	-	-					-	
		1	1.1.1			1 1			1.0	-	-

[Output table]

Target	X.	Y	z
	m	m	m
1.	6.728	4.805	-0.025
-2	1,840	-1.614	-0.005
3	3,142	1.642	+0.002
4	4.696	5,620	0.003
5	-0.754	7.695	0.000
1			

A.6 Target points of cross section survey

What kind of points do you need when you draw a cross section. The answer is points where the gradient of ground surface is changing.

Boundary of materials is also needed, asphalt, concrete, soil and so on.

Small structure such as drainage, guard wall and so on can be measured by tape except one point of it instead of survey all.



A.7 Station point

Role of station point is to connect site and drawings. Surveyor makes survey products, Design engineer makes design drawing on the survey products, Contractor constructs along the design drawings. If there is no station point at the site the contractor cannot decide position of works.

There are two types of station point, one is temporary and another is permanent station. Temporary station is made with such as wood peg and plus for striking into pavement. In contrast permanent station is made with durable concrete peg or block to keep the position. Permanent station is often point of reference.

Peg and Pin for Station









Point of reference has authorized coordination. Administrative agencies maintain them





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Annex B (informative) How to use the Dokenbo

B.1 General Information of Dokenbo

What is Dokenbo? Equipment for Soil layer prospection consists of 1)Cone 2)Rod 450mm 3)Rod 500mm × 9 4)Handle 5)Vane cone 6)Load meter 7)Dial torque wrench 8)Open-end wrench × 2 9)Connection sleeve 10)Carry bag 上間 ioii Lev 強度 Strength 検査 kensa 15 Rod Bo

Public Works Research Institute PWRI in Japan developed Dokenbo and got patent in Japan. Anyone can use Dokenbo but only permitted one can make Dokenbo

B.2 Usage of Dokenbo



(1) Soil layer depth prospection (2) Penetration test by spring load meter (3) Shear strength test by dial torque wrench

with vane cone

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B.3 Important caution Dokenbo has two strict prohibitions;



The rods connects each other by right-screw. Therefore,

Never turn anticlockwise

when the Dokenbo is in the soil layer. If you do connection screw is released and apical end is lost in the soil layer.

Dokenbo is designed for static use. Therefore,

Never hit top by hammer

to penetration.

If you do Dokenbo would buckle up or get broken.

B.4 Soil layer depth prospection

B.4.1 Procedure



- Apical end is the cone, top end is the handle.
- Set Dokenbo on prospect point, push the handle statically and slowly by investigator's own power.
- Dokenbo penetrates no more, then rod length from the surface is depth of soil layer. Investigator can read using 10cm scale mark on the rod.

B.4.2 Distribution of prospect points

- Random way; Investigator choices prospect points where soil layer seems deep. Maximum depth represents soil layer depth of the target slope.
- Regular way; Prospect points are distributed along preset line such as cross section line, contour line or fall line. All prospect points must have position information such as coordinate values.

B.5 Penetration test





 Investigator penetrates Dokenbo till measurement depth.

(2) Investigator push Dokenbo through load meter slowly, when Dokenbo goes into action then investigator reads load meter.

(3) Investigator fills data on 'Data Sheet for Dokenbo Penetration Test'.

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[[]Developer and patent]



B.5.2 Data sheet

- There are two ways of DPT. One is Normal Test. · Weight of Rods is counted in calculation of
 - penetration strength qdk.

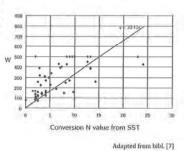
Dau Shert for Dalambo Penetration Ten a for in so at a

· Another is simplified Test. Weight of rods is not counted in calculation of apparent penetration strength qdk'.

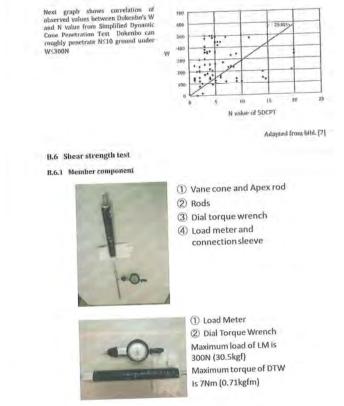
		1	Data !	Sheet for	Dokent	in Pene	iratio	n Tet	1		
Mei.	_	_				Daw	_	14	in them	_	_
inst			_	_		lina cipi	ur				
Grand C Gater Co		£				-					
- But	iitet t	10	Activity	Case do Tro	126	ACCR 19	SWEAKS ?	10100	0		
(also	11105	Enger, (r	e			Cime 107	Gammin C	A YEL			
Dept	ort Vite of		of Dark	Petatanie Tanà		Tanaty	Dept				
0	1	NN.	1.00	42		1.1		16	VEP-	-	
1.10	130	2105	1 1	111	-		TT	T	T	T	TT
1.6	- 336	2,800		1.57						1	
-4.00	320	32322	1	1.73							

B.5.3 Correlation of other tests' result

Next graph shows correlation of observed values between Dokenbo's W and conversion N value from Swedish Sounding Test. Dokenbo can roughly penetrate N ≤ 10 ground under W<300N.



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B.6.2 Procedure

This test needs two persons, operator is the leader of the test and turner is the assistant.

- The operator penetrates Dokenbo to target depth with vaneless normal cone.
- 2 The turner turns Dokenho slowly with dial torque wrench for clockwise under the load mater indicates 0, Maximum value shall be recorded as Torque by skin friction T0.
- The operator replaces normal cone to yane cone.
- ③ The operator sets Dokenbo again at the same depth and adds some load to penetrate vane only into unbroken soil.
- The operator loads vertical planned step load Wi through the load mater.
- (ii) The turner turns Dokenbo slowly with the dial torque wrench for clockwise under the load mater indicates vertical load WI, Maximum torque value is TL
- (2) The turner records test depth, WI and TI on the data sheet.
- (8) The operator pulls Dokenilo out and checks condition of vane cone.
- (1) The turner write remark about attached soil, influence of gravel, and so on.
- This procedure is repeated till getting 5sets; at least 3 sets, of Wi and Ti. Each test must be executed at unbroken soil a little deeper portion of ex-step. When the penetrated hole cannot stand alone then test procedure should change as below,
- 00 The operator try to set vane cone similar depth at other new hole near the skin friction test hole. (2) The operator <u>does not pull out Dokenho each step</u> of the test in order to continue the test and to get 5 sets of Wi and Ti.
- (2) The operator sets the vane cone at 3 to 5cm deeper than existep test to get unbroken soil. B.6.3 Process to get shear strength

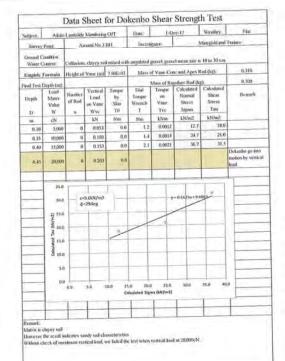
There are two ways to get shear strength from the test result. One is empiric formula way and another is correlation formula way. Correlation formula way needs 3 couples of triaxial compressive CU test and Dokenbo test at least. Therefore the guideline introduces empiric formula way only.

The empiric formula ties the test result to shear strength as below.

$\sigma = 2.4 \times 10^7 \ B_{10}^{*}$ $\tau = 1.5 \times 10^4 \ T_{tr}$	(1) Investigator makes chart of Sigma and Tau.
	(2) He makes linear regression formula.
$W_{tv} = W^{*} + (m_{0} + m \cdot m) \cdot g$	(3) Y-intercept is Cohesion.
$T_{TV} = T - T_0$	(d) Gradient is tangent Phi.
	(5) Phi is Internal friction angle.

B.6.4 Data sheet

The project provides data sheet for Dokenbo shear strength test. Example is shown as below with chart of σ and $\tau.$



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λł 3 1Nn

M.

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1.000 33. 12.0 1.90

Annex C (informative)

Excel worksheets for Stability calculation of gravity retaining wall

C.1 Outline

- The worksheets execute stability calculation of gravity retaining wall, consist of 4sheets, in_put, wall, earth pressure, and summary.
- Wall shape is trapezoid with 4 node points. Backfill is horizontal.
- . Courdinate origin is heel of the wall, front side of the wall is plus direction of x axis and top side of the wall is plus direction of y axis.
- Earth pressure is calculated with Coulomb's formula.
- · Earthquake is out of coverage.

C.2 Worksheets

[In_out]

_	Name of Conditions	Symbol	Nuit	Valu	
Wall	Node1	X, Y	m	0.000	0.000
	Shape Node2	X, Y	m	1.800	0.000
	Node3	X, Y	m	0.600	3,000
	Node4	X, Y	m	0.000	3.000
	Unit weight	ye	kN/m3	23	
Backfill	Unit weight	ys	kN/m3	19	
	Internal friction angle	4	deg.	30	
Foundation	Allowable bearing capacity	Qa	kN/m2	200	
	Friction coefficient wall and foundat	ion ji	ND	0.6	
Road	Surcharge on the Road	ý.	kN/m2	10	

Annex D (informative) Excel worksheets for slope stability calculation

Calculation

type

1.30

R

10.0

1.00

Given condition

ς, φ φ., Fs

C, Fs

Target

Fs

The worksheets execute slope stubility calculation, consist of 3sheets, In. put, Cal_EUT and Calc

 Ground water is flat face, it is handled as running through the node point. Simplified formula is applied for safety factor calculation.

There are 3 types of calculation combination of given condition and target.

Inter data of 2

Heath m 10.00

adient einfe

ML depth n 2.601

G 115 gr

Weitw LNini 18.0

Water UW kN/m3 98

happ of general methods

Movable taver depil

Unit weight

Gio er depih

[Waff]

Element	Area A (m2)	Weight V (kN)	Ann length X	Mument M (kNm)
1	2.70	62.1	0.938)	49.7
2	0.90	20.7	0.200	4.1
Total	-	82.8		53.8

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D.1 Outline

D.2 Worksheets (In_put)

 Slope collapse is presumed as circular sliding. • The slope is flat face with uniform gradient, Sliding size is given through height and depth of sliding. Sliding body is divided into 6 slices automatically.

 $F_{1}^{*} \equiv \frac{\sum (cf_{1} + (\mathcal{H}_{1}^{*} - u_{i}b_{1})\cos \alpha_{i} \tan \phi_{i})}{\sum (cos \alpha_{i} \tan \phi_{i})}$

 $\sum H'_{i} \sin \alpha_{i}$

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[Earth pressure]

u degre		 legree	degs	ee	ð degree		A			
	0.0	0,0		30.0	20.00	0	0.297			
Active Earth Paraman Cuefficiant	Ban Attill Und Weight	Well Strigts	Surchauge en the Road	kand Name	Lond	Feksion Angle af Walback	Veneal Land	Ann Length	Meesem	Hormony) Lond
KA	1 Lym1	h	P ENVinZ		PA kN	A deper	V AN	1. 10	M VNm	H LN
0.292	19			Earth Pressure	25.4	20.000	3.7	0.000	0.0	21.9
j.297		100	-10	IP by Sorthoge		20140		0.000	80	84
		-	-			Total	11.7		80	72.3

[Summary]

Summary table for loads and Moments

Lamil Name	Vertical Loost kN	Horizontal Lossid KN	Monural kNm	
Wall Weight	\$2,8		53.8	
Earth Pressure	11.7	32.3	30.5	
Total	94.5	32,3	981.3	

Three check paints of stability index Differentiering

	X-coordinate of resultant	N-	0.956	005
	X-coordinate of bottom center	13/2-	0.900	191
	Eccentricity of resultant	2.00	0.056	115
	Allowable eccentricity	13/6	0.300	111
	tudgment		OK	
) Slide				
	Tenal vertical load	ΣV-	94.5	
	Testal brizontal lood	211-	32.3	
	Friction coefficient	B	0.6	
	Safety factor of sliding	Es=	1.76	
	Judgment		OK	
) Hearig	e capacity		- 64	
	Reaction stress at wall's loc-	xqr=	62.3	
	Reaction stress at walks heel.	xybr-	49,6	
	Allowable stress (Rearing capacity)	10.4	200,0	
	Judameni		OK	

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						DNEPC	C
1 A A A A A A A A A A A A A A A A A A A	1.4833299 0.9961947 0.7853982 0.7071088 1.2217335 0.9396926 1.0471976 0.8660254 1.134464 0.9060703 1.0821041 0.8829476 1.0646508 0.8746197 1.069886 0.8746197 1.069886 0.8746197 1.069886 0.8746197 1.0698583 0.8769783 1.0693533 0.8769783 1.0693543 0.8769783	Cosise The Left 0.0871557 0.0160699 0.02701088 0.4142156 0.3402010 0.07622 0.5 0.0269992 0.4226183 0.2216903 0.46403716 0.259617 0.4840376 0.259617 0.4840376 0.259617 0.4840376 0.259617 0.4803759 0.259615 0.4803596 0.259617	0.2560328 0.2560328 0.2560328 0.2560328 0.2560328 0.2560328 0.2560328 0.2560328 0.2560328 0.2560328 0.2560328 0.2560328 0.2560328 0.2560328	0.011916406 -0.034338124 -0.006704784 0.002584797 -0.000206412 0.000723573 -2.04485E-05 7.25397E-05	Sip coole	ब्रोग मिर्म 84 9 म इ	6 5 14.1544 13.5985 16.2541

	Ansk	Length		Weight	WcoiAlph	WinAld	
Element	Alpha	1	Area	W			
	dee		012	LN .	kN	IN	
-	15.5	2.490	1.603	12.06	15.19	8.55	
.1	24.5	2.638	4.291	85,82	36.02	35.65	
2		2.905	5.812	116.23	39.07	65.50	
3	34.3	3.423	5,718	114.36	24,14	81.55	
4	45.5	2.105	2.157	43.14	0.00	35.4	
5	55.2	2.712	0.860	17.21	(1.00)	15,43	
- 6- Tenal	63.7	16.273	thirtor.		114:42	242.43	

30

A. Given c and Phi, Target is Fa

IP cohesion	kN/m2	0
IP IF mgk	deg	30
fis-		

II. Given Phi and Fs, Target is a

IP IF angle	deg

- ESE kN/m2 10.82 e

C Given c and Fs, Target is Phi

IP cohesion	kts/m2	
ES Ph		
Phi		

Calculation Type Cale Type treat slip surface i IF vibesin KNIm iP IF mpk dig Exclusion safety factor ES Fs

A3-215

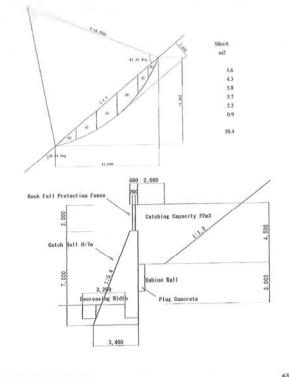
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Annex E (informative) Catch wall E.1 General information of catch wall Catch wall which is introduced here is combination of gravity retaining wall and rock fail protection fence. Catching capacity is decided based on mass of collapsing soil. The wall has durability against impact force of collapsing soil. Patchine exencity for exilipand soil Pock fall protection ferror Gravity retaining mall [Characteristics] Classified into traffic protection works . Steel fence can reduce weight of top portion. . Catching capacity must be bigger than collapsing soil The wall must hear impact force by collapsing 62 © DNEPCC 2018 - All rights reserved

E.2 Catching capacity

Catching capacity is decided based on mass of collapsing soil. In this example scale of slope collapse is estimated as the drawing. Mass (Gross section) is 20.4m², Catching capacity becomes 22m² when additional height is 4.5m as below. Rock fence II=2m is often adopted for the combination:



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E.3 Design procedure

① Catching capacity decides elevation of the fence top.

- $\textcircled{\sc c}$ $\sc c$ Blevation of the wall top is often decided 2m down from the fence top.
- Wall shape can be selected from Type1 of the common drawings. Original shape is also adoptable.
- (1) Calculation of impact force.
- (iii) Same as stability calculation of ordinary gravity retaining wall

E.4 Stability calculation

[Calculation conditions]

Calculation conditions of catch wall consists of local values which is decided case by case and standard values which is used commonly.

Items	Symbol	Doit	Local Value	Standard Value
Items for Calculation of Impact Force				
Possible Collapsing Height	н	m	40	1
Slope Gradient	Bu	deg.	35	-
Gradient between Slope-end and Wall	- ed	deg.	0	
Distance between Slope-end and Wall	Xb	m		
Height of Moving Soil	hara	m		1.0
Density of Moving Soil	ps	tim		1.8
Specific Weight of Moving Soil	D	DL	1	2.6
Volumetric Concentration of Moving Soil	6	DL	1	0.5
Acceleration of Gravity	r	m/t=		9.5
Coefficient of Huid Resistance	fly	DL		0.025
Coefficient of Impact Force absorption	a"	DL		0.0
Internal Friction Angle of Moving Soil	\$d.	der.	35	4.4
General Items			1	
Unit Weight of Wall Constate	10	kN/m ⁴	1	20.56
Unit Weight of Backfill Soil	·/b	hN/m1	36	
Unit Weight of Moving Soil	7	kN/m?	15	
Internal Friction Angle of Backfill Suil	- Φ Ιι	deg	35	
Priction Angle between Wall and Soil	õ	deg	-23.3	2/3Φh

(Allowable value on stability check)

Stability checks are implemented on three situations as normal, impact force acting (collapse just occurring) and collapsed soil earth pressure acting (after collapse occurred). Each situation has different allowable value as below.

	Over turning Eccentric Length e o	Ehiling Balery Factor II	Bearing Capacity Reaction Force is
Normal	Emailer than B/0 Middle Third	Bigges shan 1.5	Smaller than qu/3=300 kN/m ²
Impact Force Arting	Smaller than 8/3	Bigger than 1.0	Bmaller than qu=900 kN/m ²
Collapsed Soil farth Pressure Artury	Smaller than B/3	Bigger than 1.2	Smaller than qu/2=450 kN/m

[Calculation of impact force]

Impact force is calculated by below equation. Excel worksheets are provided.

 $\Gamma = \alpha^{+} + \Gamma \equiv$

- I : Impact Pressure on the Wall (kN/m2)
- Ital Pressure by Moving Soil
- a^{\prime} = Coefficient of Impact Pressure absorption

 $\mathrm{Ext} = -\mu_{\pi^{+}\pi^{+}} g \star \mathrm{hen} ~ (1 - \frac{\mathrm{ho}}{\mathrm{a}} - (1 - \exp(\frac{-2 \star a \star \mathrm{H}}{\mathrm{hen}} \star \sin \theta_{\pi^{-}})) \cos^{2} (-\theta_{\pi^{-}} - \theta_{\pi^{+}})) \exp(-\frac{-2 \star a \star \mathrm{Ho}}{\mathrm{hen}})$ 1 • Mi___))]]

$$+ \frac{bd}{a} (1 - exp(\frac{-2 + a}{ba}))$$

$$a = \frac{2}{(a-1)C+1}$$
 fb

$$t_0 = 100 + 1$$

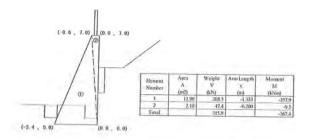
by $= \cos \theta_{\pm} (t_0, \theta_{\pm} - \frac{(\sigma - 1)C}{(\alpha - 1)C + 1} \tan \phi d$

$$=\cos \theta + (\tan \theta) = -\frac{1}{(\alpha - 1)C \pm 1} \tanh \phi d$$

Item	Symbol	Unit	Value
	a	DL	0.027778
Coefficient	bu	DL	0.370430
- Sector Control - Contro	Ind	DL.	-0.311203
Pressure of Moving Soil	Fam	kN/m2	106,39
Impact Pressure on the Wall	F	kN/m2	53,20
Instact Pressure Acting Area	Asur	m2	1.00
Inwact Force	Fc	kN	53.2

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[Wall body weight and gravity center]



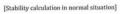
[Coulomb's active earth pressure]

Earth pressure is calculated by Coulomb's formilia. One is earth pressure in normal situation. Another is in collapsed soil earth pressure acting situation.

legree :	depart	daysee	digues .	80	Y LN/m2		khem.	ANI-WAT	PA3	SPA IN	PAH	PAY
0.0	0.6	35.0	23 233	0.754	78 18	45	44.47	6	8.00	31.32	111.0	19.6

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Normal Condition Backfill Soll Earth Pressure Acting



Condition			Namual		
	Vertical Loads	Amtesysh	Horizontal Luads	AnuLengih	Moneni
Lands	¥.			¥	M
	(6N)	tmi	0.50	000	(\$2\ins)
Wall Body	315.9		0.0		-367,
Earth Pressure	17.6	0.000	+40.8	1.500	-61.
	333.5	_	-40.8		-428.
Three Check P	oints of Stabili	ty Imlex			
I) Over-turning					
	X coordinate of	2V	:x>-	-1.285	
	X coordinate of		Xe-	3,400	
	X creationic of		501-	0.000	
	Width of Base		10	3:400	
	X coordinate of	Link for SV	Xa-	2.833	
	Judgment			OK	
	Eccentric Lengt	ih.	1010	-0.415	
	MkIdle-third/2			0.567	
	Shape of React	ins Force	1.1	Tespezoidal Sh	ape
2) Sliding					
	Friction Coeffic	lent	H=-	0.6	
	Sliding Safety F	actor	Ware-	4.90	
	Needed Safety	Factor	Exer	1.50	
	Indgment			OK	
3) Bearing Cap	acity of Found	ation Ground			
	Reaction Force	ut Wall Toe	vyk-	26.3	
	Reaction Force	at Wall Heel	dir.	169.9	
		ing Capacity	194	300	
	Aboavable Breat				

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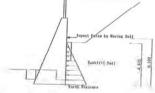
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Impact Force and Normal Earth Pressure Acting



Summary of Load and Moment

Condition		In	t		
lonis	Venical Londs V (kN)	Ann Length A	Horiaantal Locals H (kN)	Arni Leogth y (m)	Moment M (kNm)
Wall Body	315.9	-	0.0		-367.4
Earth Pressure	17.6	0,000	-40.8	1,500	-61.2
Impact Force			-53.2	5.000	-266.0
	333.5		-94.0		_694.6

Three Check Points of Stability Index

1) Over-tur	ning		
	X coordinate of XV	X-	-2.081
	X coordinate of Wall Foo	Xt=	3.400
	X coordinate of Wall Heel	Xir-	0.000
	Width of Base	O'r=	3.400
	X coordinate of Limit for EV	Xu-	-2.833
	Judgment		OK .
	Eccentric Length	0	0.383
	Middle-third/2		0.567
	Stape of Reaction Force		Trape zoided Shape
2) Sliding			
	Friction Coefficient	H-	0.6
	Sliding Safety Factor	B-	2.13
	Needed Safety Factor	Fiar	1.00
	Judgment		OK
3) Bearing C	apacity of Foundation Ground		
	Reaction Force at Wall Toc	-qt	[64.4]
	Reaction Force at Wall Heel	ale-	31.8
	Allowable Bearing Capacity	qu-	900
	Judgment	0.052	ок

[Stability calculation in collapsed soil earth pressure acting]

Collapsed Soil and Backfill Soil Earth Pressure Acting



Summary of Load and Moment

Condition		Culliqued Soil Earth Pressure Acting			
Londs	Vertical Lesuls V (kN)	AmsLength x (m)	Horizontal Loads H (LN)	Ann Leagth y (m)	Moment M (kNm)
Wall Body	315.9		0.0		-367.4
A8 Earth P.	70,4	0.000	-163.3	3.000	-489.9
	386.3		-163.3		-857,3

Three Check Points of Stability Index

1) Over-turning

1) Over-tui	ning		
	X coordinate of XV	Nr.	-2.219
	X coordinate of Wall Ton	70=	-3.400
	X coordinate of Wall Heel	Ma	0.000
	Width of Base	Alle-	3,400
	X coordinate of Linux for XV	Nav	+2.833
	Judgment		OK
	Eccentric Length	0	0.519
	Middle-third/2		0.567
	Shape of Reaction Force		Traparoidal Shape
2) Sliding			
	Friction Coefficient	10-	0.6
	Sliding Sufery Factor	The .	1.42
	Needed Safety Factor	Fan-	1.20
	Judgment		ок
3) Bearing	Capacity of Foundation Ground		
	Reaction Force at Wall Toe	qt=	217.7
	Reaction Force at Wall Heel	ah-	9.6
	Allowable Bearing Capacity	qa**	-450
	Judgment	1	OK.

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E.5 Comparison of other countermeasure

This catch wall design example is competitive countermeasure to combination of sewing har and shotcrete frame presented in clause 12. Comparison table is shown as helow.

Item	A. Sewing Bar and Shotcrete Frame	B. Catch Wall
Principle Classification	Deterrence Work	Traffic Protection Work
Out line	The bar sews the collapsing still to unmoving ground, the frame distributes the bar force to collapsing soil.	Catch wall protects traffic from collapsed debris by own catching capacity. Catch wall must bear impact force by the debris
Quantity per 10m	Shotcrete frame: 370m Sewing Bar: 100, 400m	Wall concrete: 140m3 Rock fence: 10m
D.C. cost per 10m In Japan		
Others	No loss	Road width 3.2m loss
Maintenance	Nothing	Debris shall be removed after collapse.
Selection	No demerits but high cost.	Low cost but some demerits.

Characteristics of catch wall can be summarized as below.

- Catch wall can be lower cost than other countermeasure in many cases.
- A certain level of space to place the wall base is required along foot of the slope. Therefore eatch wall is not adequate to place a narrow place such as foot of steep slope.
- A certain level of bearing capacity of foundation ground is required along slope side of the road. This is the absolute requirement.
- Debris shall be removed after collapse to keep space for next collapse.
- If the target slope collapse is expansive to upper portion of slope, impact force can increase because
 of higher potential to the catch wall. Possible collapsing height in the design conditions must be
 decided with deep consideration.

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Bibliography

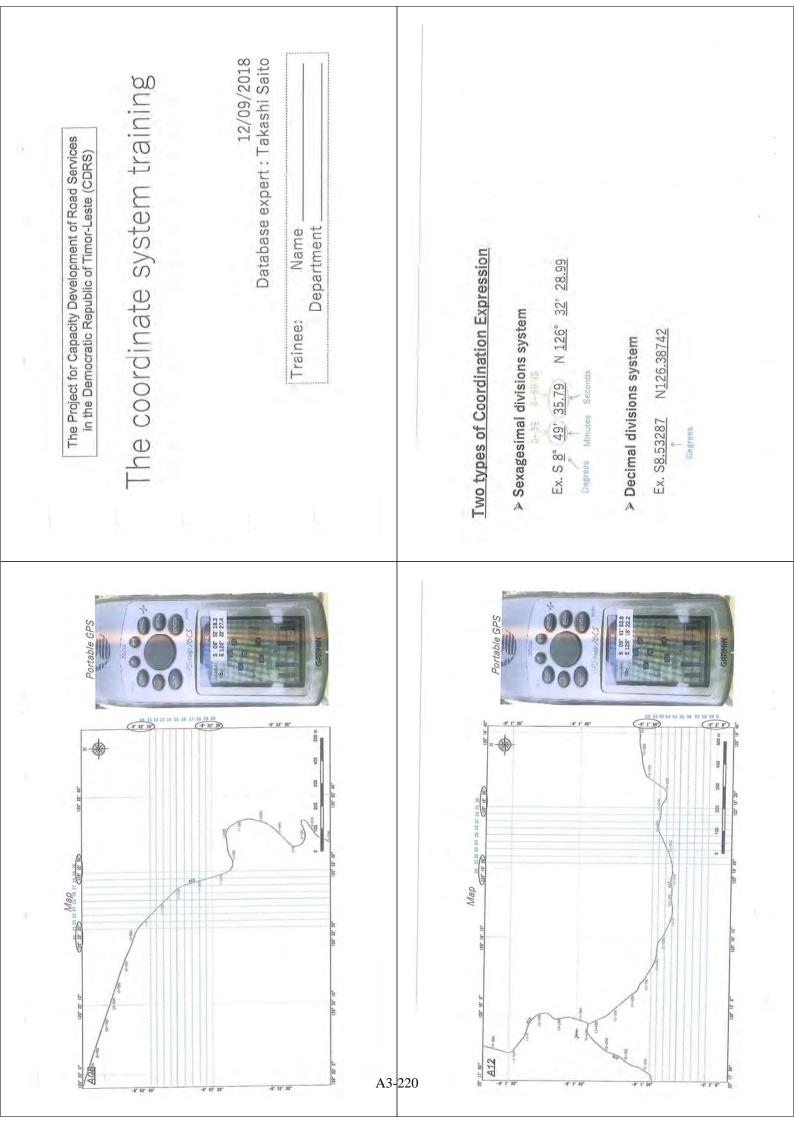
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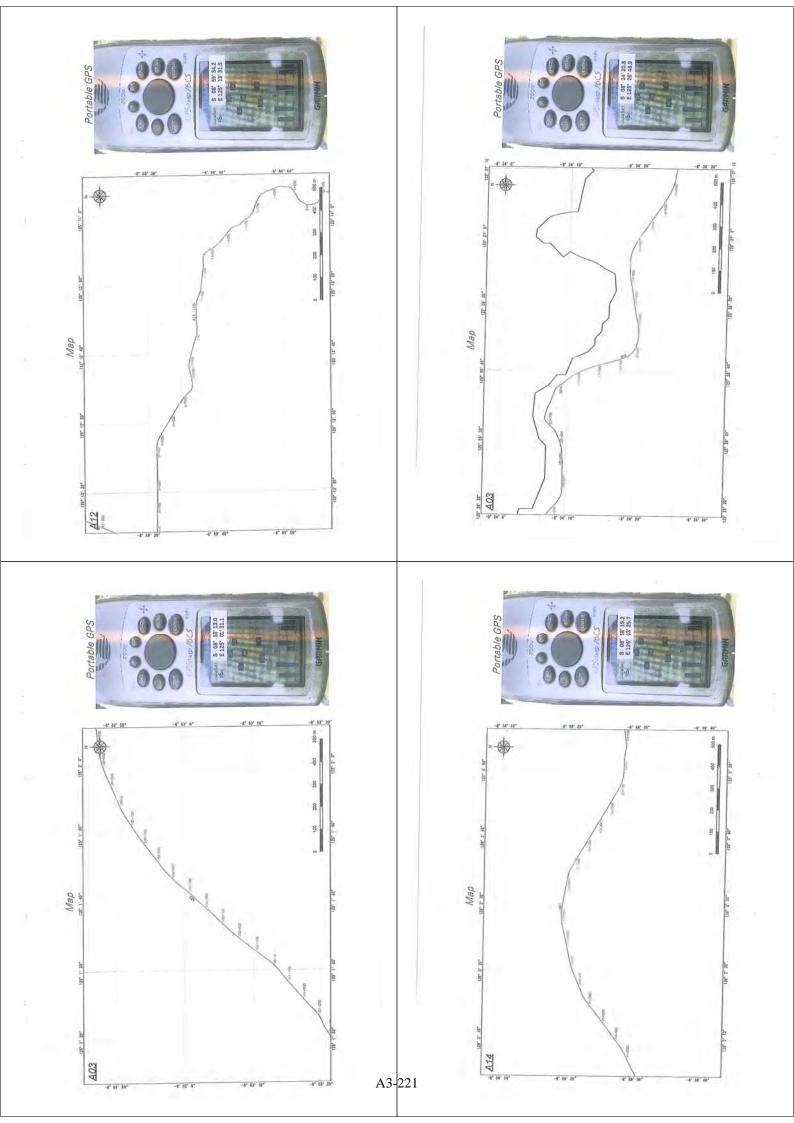
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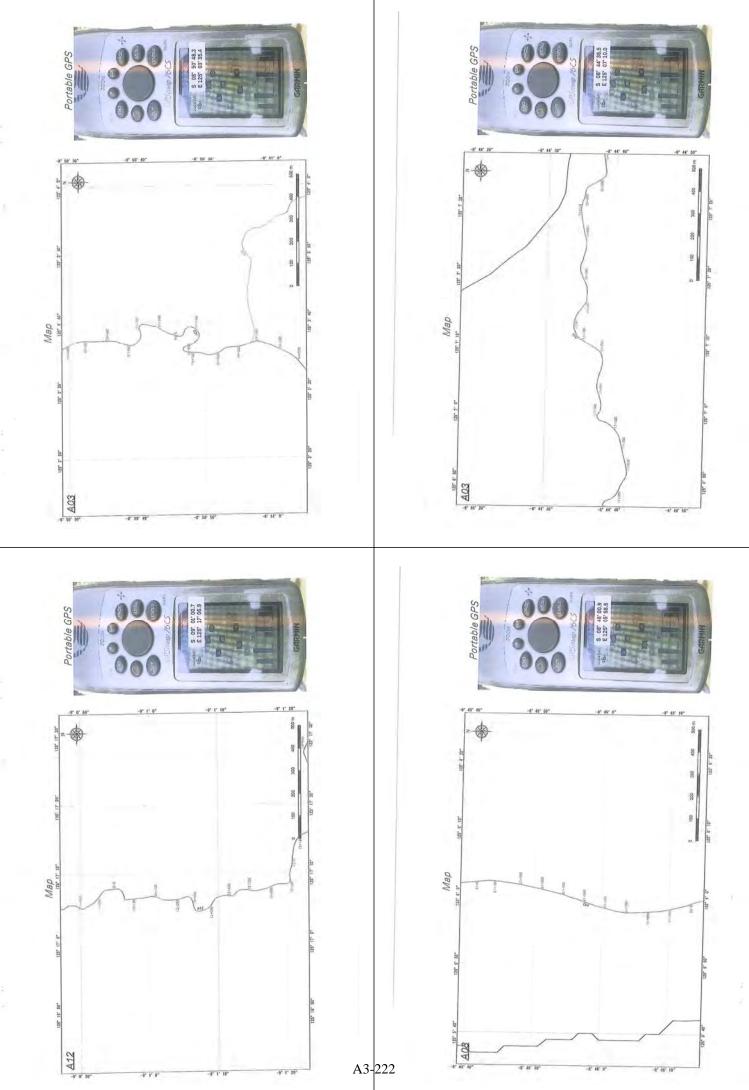
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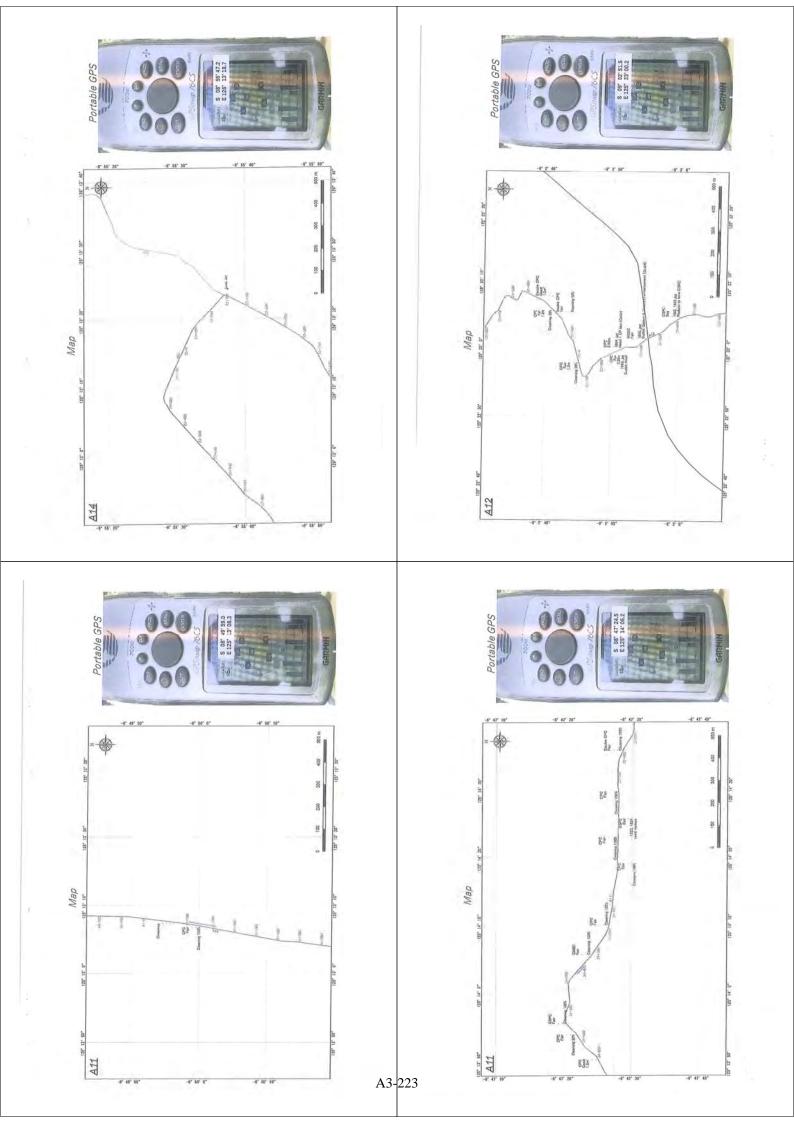
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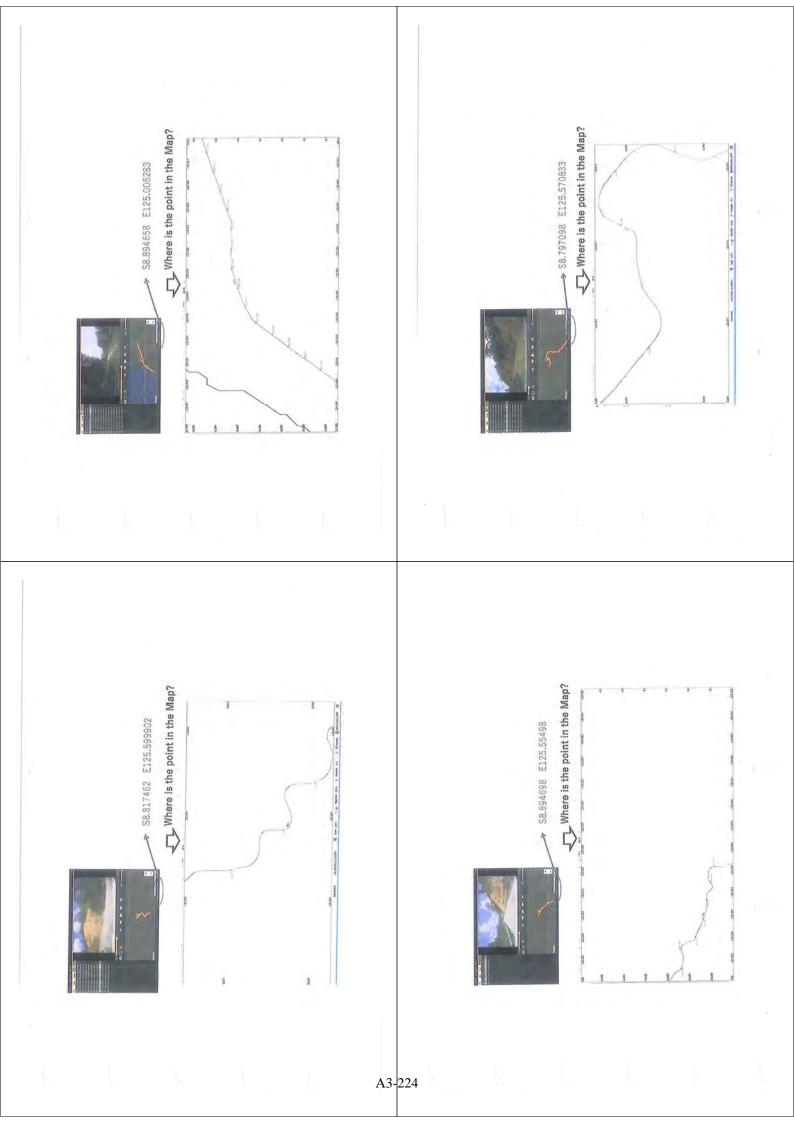
The Coordinate System Training on 12 September 2018

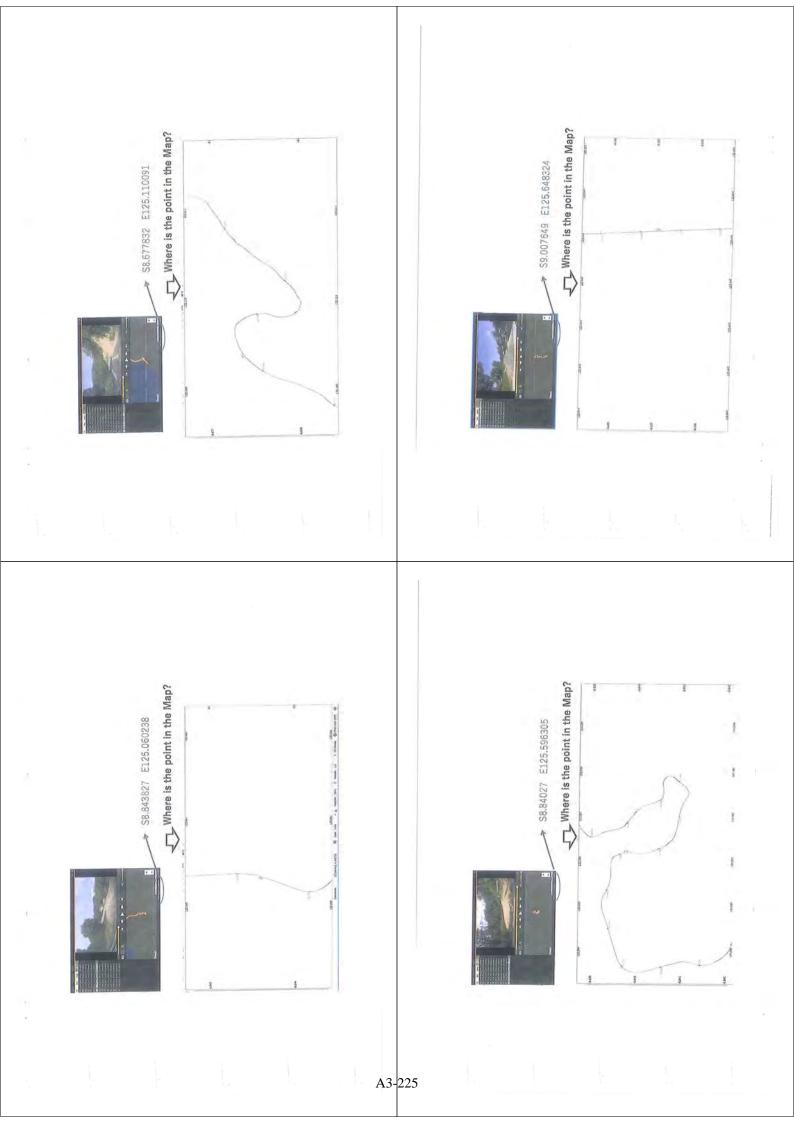


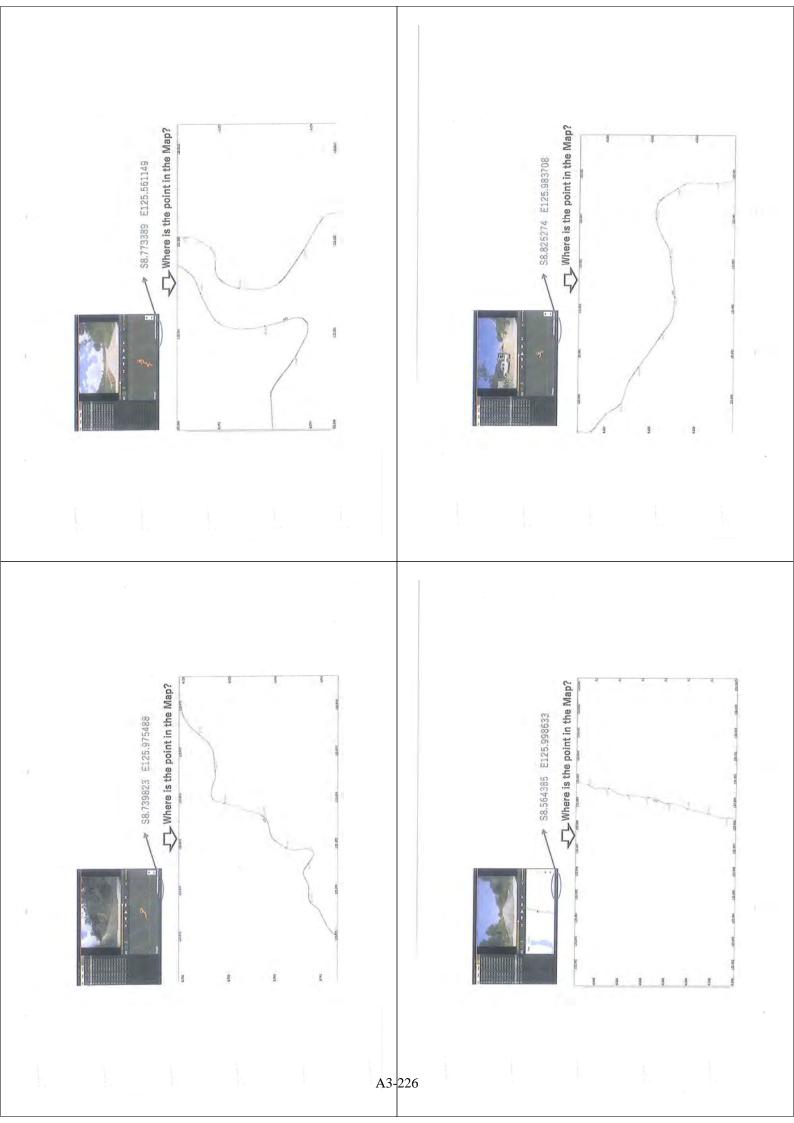


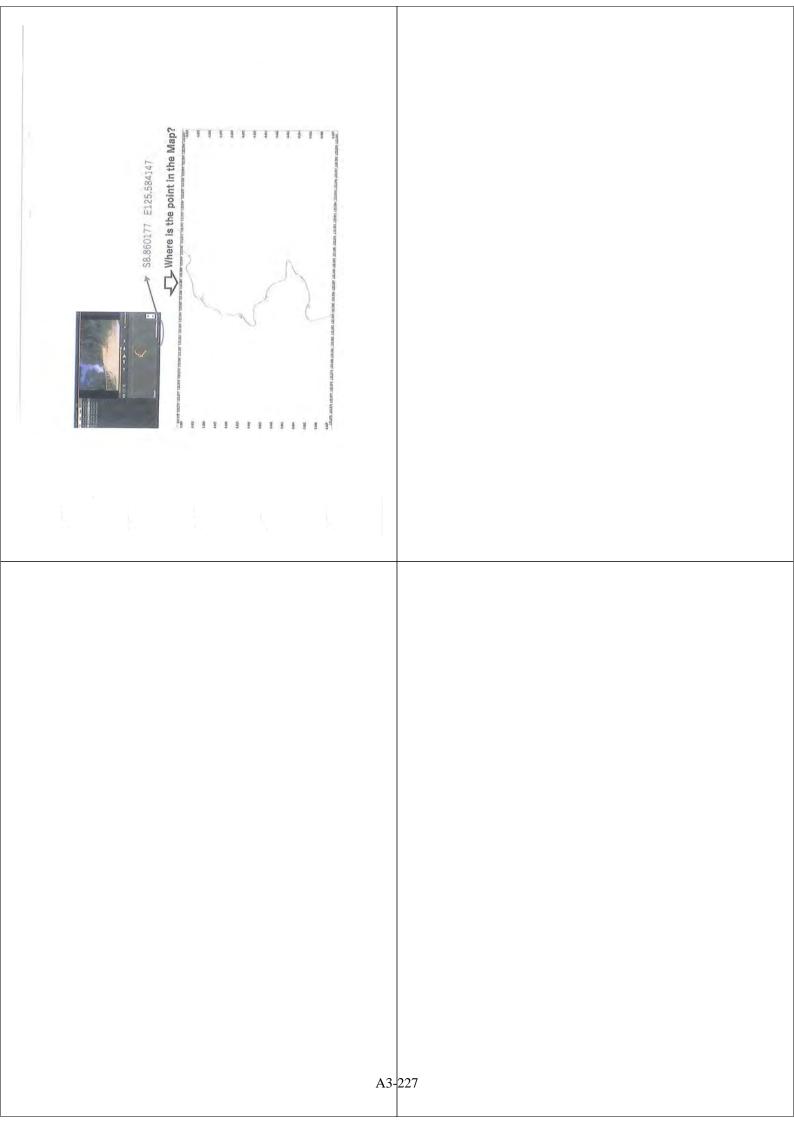








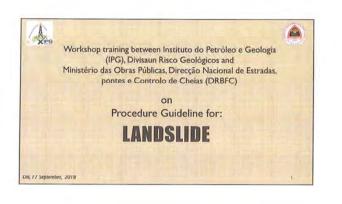




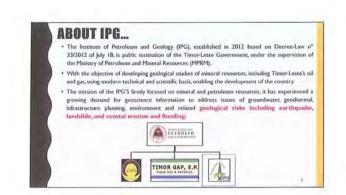
Explanation procedure Guideline for Landslide by IPG Geologist on 17 September 2018



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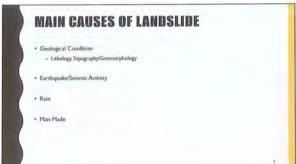
CONTENTS	
About IPG	
Introduction	
What is Landslide	
 Various Types of Landslides 	
 Main Causes of Landslides 	
 Flow Chart of Landslide Investigation 	
Preliminary Investigation	
Detail Investigation	
 Aitotu Landslide Case Study 	
 Slope Stability Analysis 	
Possible Future Mitigation	



WHAT IS LANDSLIDE?	

10/30/2018 WHAT IS LANDSLIDE? Landslide: - Phenomenon where mountain slopes move in a large scale. Geological Condition · Downward movement of earth masses causing by the action of - Lishology. Topography/Geomorphology gravity. Earthquake/Seismic Activity - Rainfall-Induced - Earthquake-Induced · Rain 34 · Man-Made Resta. INTRODUCTION **VARIOUS TYPES OF LANDSLIDE** Rotational Landslide · Timor-Leste is a mountainous country, most of the major roads are The surface of r constructed by cutting hillshades.

- · Landslide are large-scale movement phenomena of the ground, and their movement are slow, that it is generally difficult to recognize their existence at the initial stage of the activity.
- · Landslide and slope failures has damage many of he roads in Timor-Leste. · Different Protection from general slope protection are required for the
- investigation and the countermeasures of landslide. · The geological hazard impacts in the population are in the level of Moderate-
- High based on some official data from IPG, Timor-Leste. · As studied/identified and observed by the IPG-Geological Hazard Division.
- there are numbers of areas which are prone to the geological hazard.



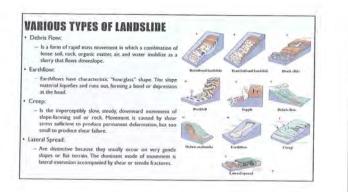
- roughly surface.
- Translational Landslide: In this type of slide, the land planar surface with little rot lide mass moves along a tion or backward tilting ack Slide
- A block slide is consist of a si move descert
- Falis are abrupt such as rocks steep slopes or Topple
- Topping failures are distinguished by the forward rotation al a units about some pivotal point, below or low in the unit under the actions of gravity and forces exerted by adjacent units or by fluids in cracks



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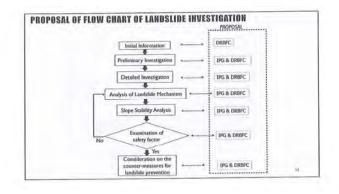
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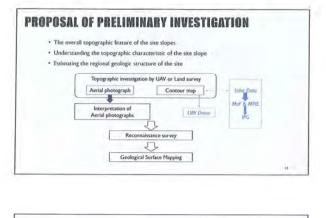


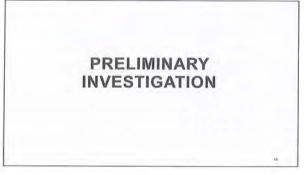




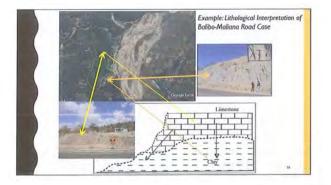
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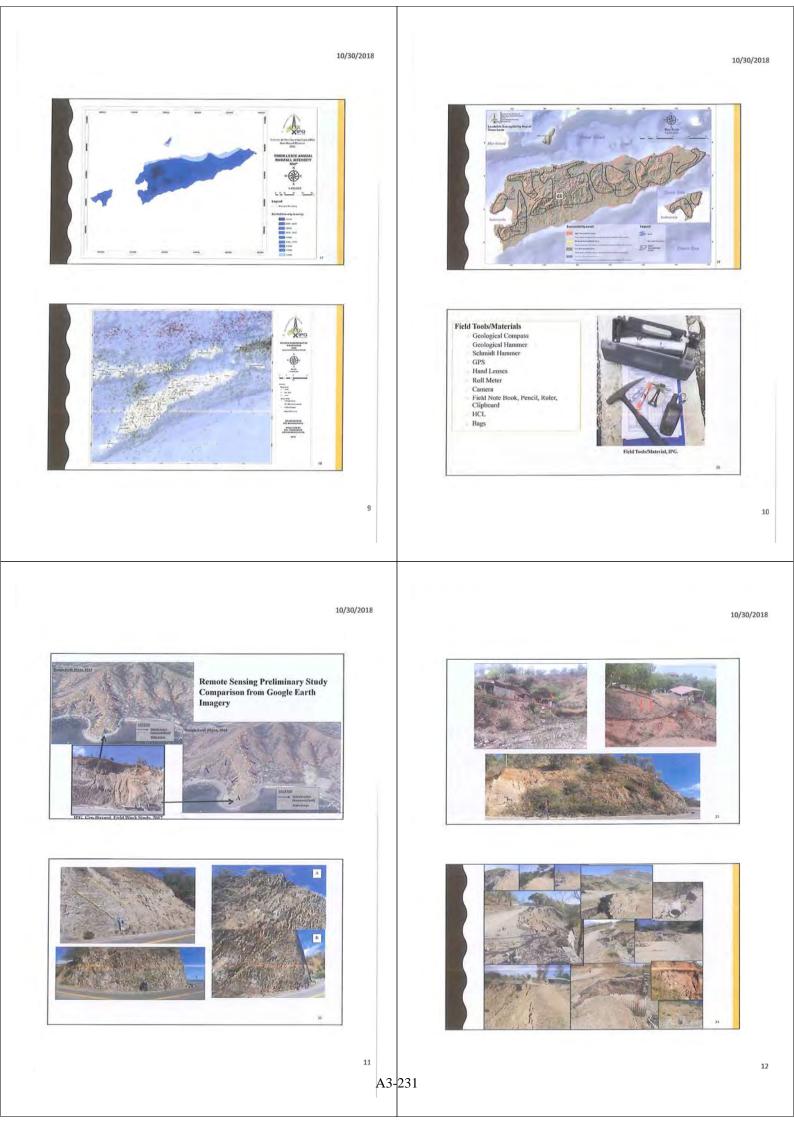


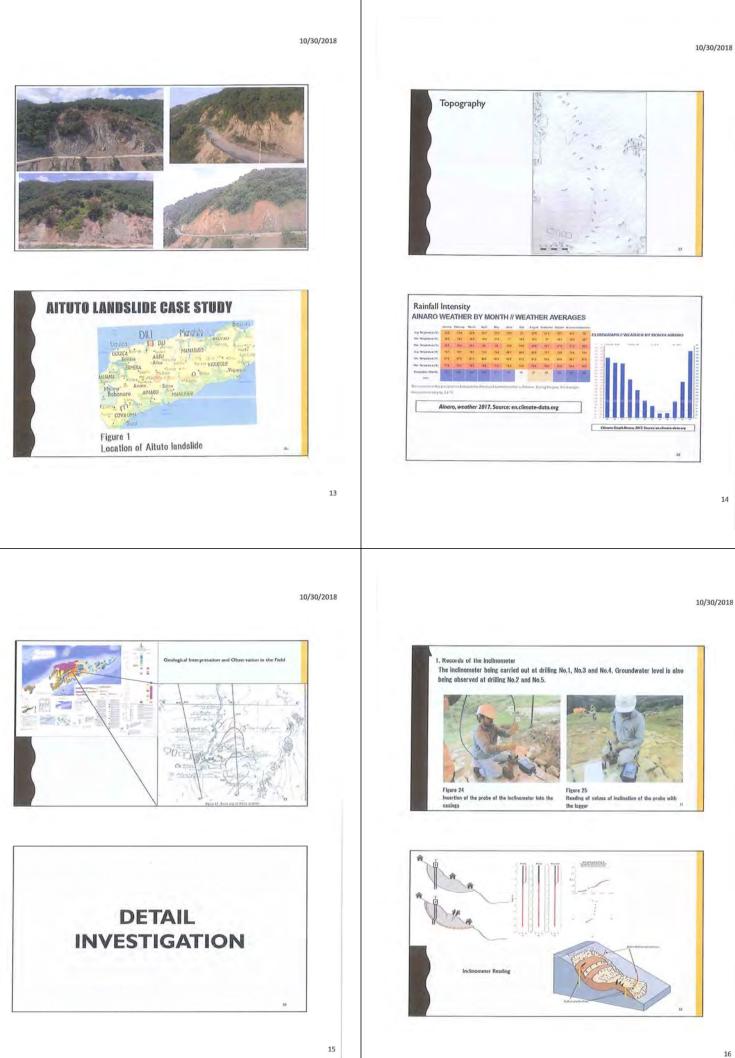
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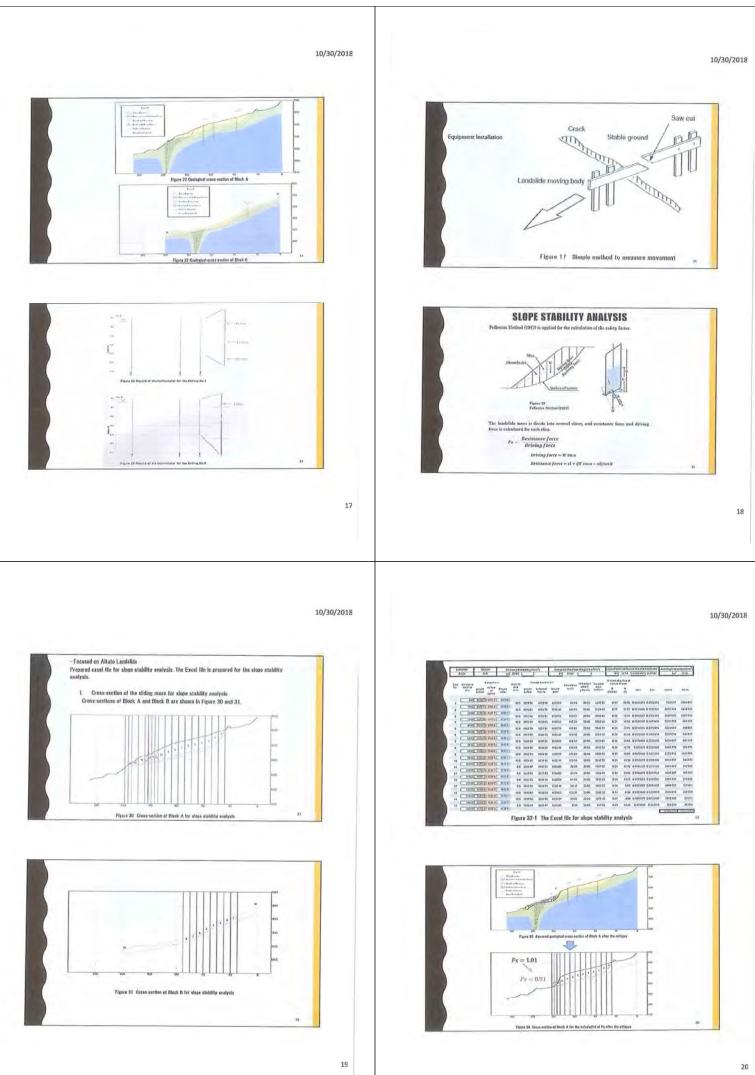
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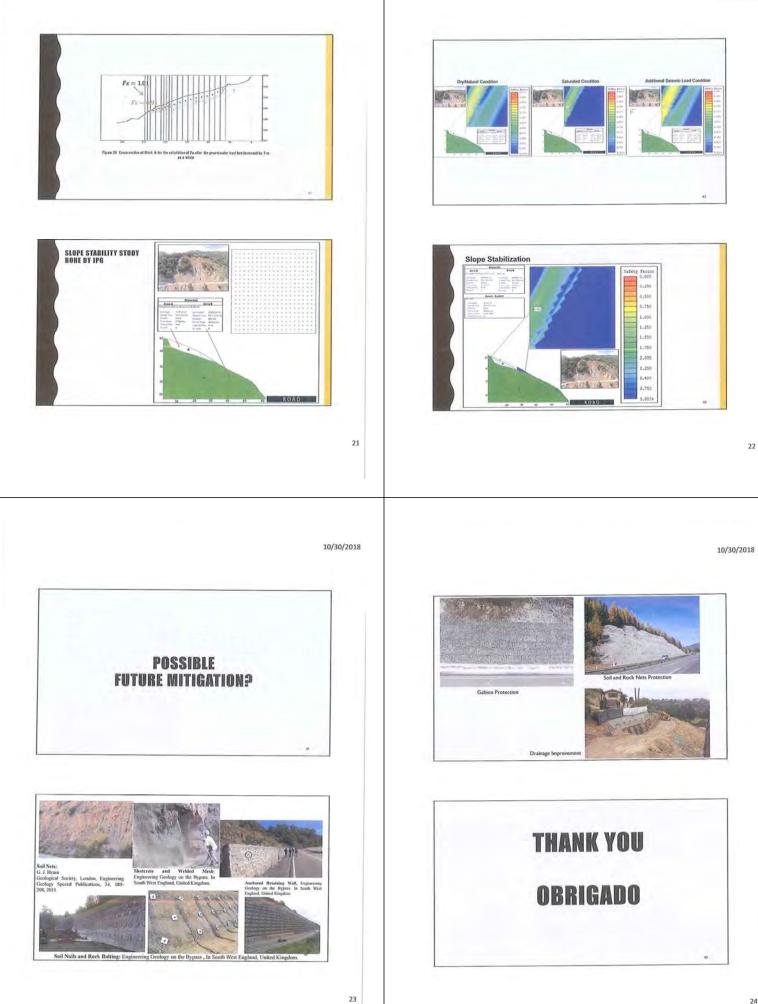
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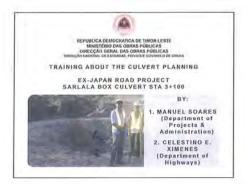
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Training about the Culvert planning and case study sarlala box culvert Ex-japan road project sta. 3+100 by DRBFC Engineer on 18 and 28 September 2018



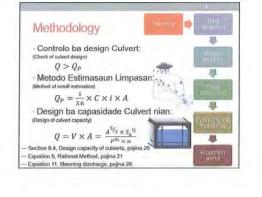




Generalidade proposito ba Culvert

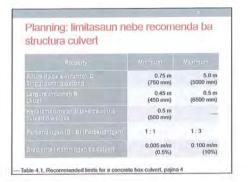
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Introduction, pagina vil



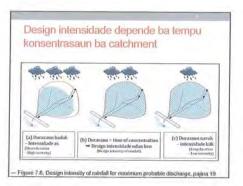
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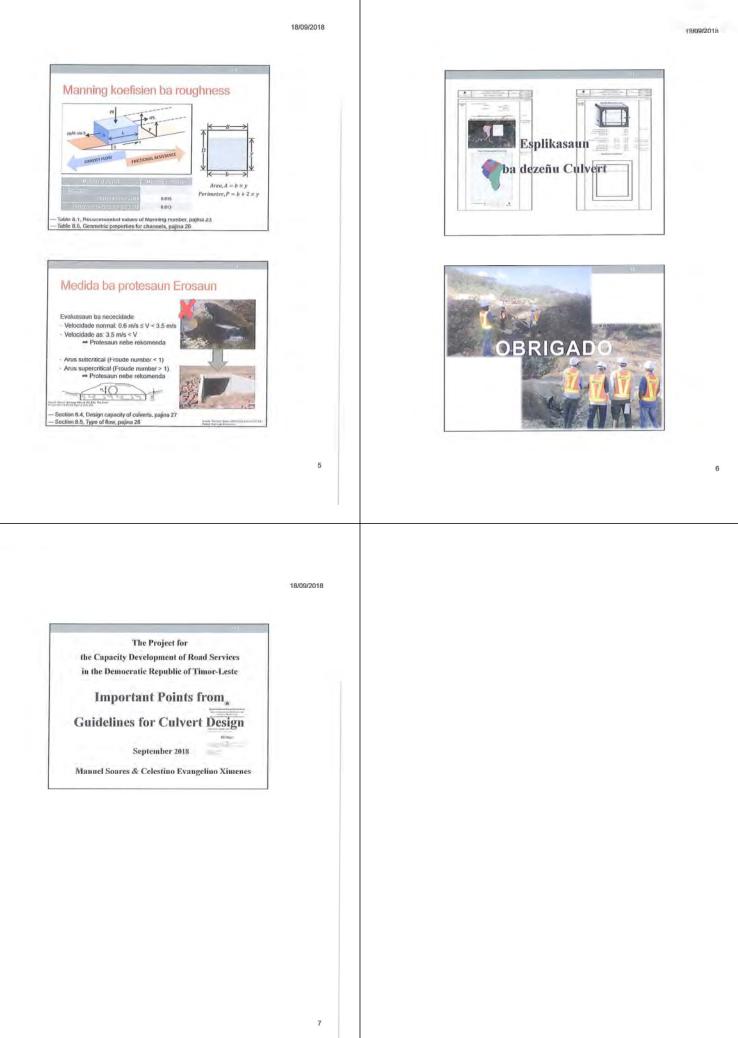




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Record of 2ndCoordination Meeting of Site safety patrol and record of 2nd safety patrol by DRBFC on 19 September 2018

The Pressel for the Connerty Development of Bood Services in the Domocratic Republic of Timor Leste (CDBR)

27 Sentember, 2018

Record of 2nd Coordination Meeting of Site Safety Committee and 2nd Safety Patrol by DRBFC (For Case Study activity of CDRS project; Safety Patrol by DRBFC)

Narano De Jeus Freitas, Coordinator of Site Safety Committee, Engineer of Construction Department

This is the record of 2nd Coordination Meeting of Site Safety Committee and 2nd Safety Patrol by DRBFC for said Case Study of CDBS project. Date/places and the record of the discussions in the Meeting and Finding of dauguro points are follows: Reference information is shown herewith in the attachmenta.

I. Data and Places

Enclas

- 1) 2nd Coordination Meeting of Site Safety Committee : 14:30 - 15:00, Wednesday 19 September, 2018 Time and Date Venue : Conference room of DRBFC, Dili
- 2) 2nd Safety Patrol by DRBFC 15:00 - 17:00, Wednesday 19 September, 2018 Time and Date
- C): STA 17+850 STA 18+100, Aggregate Base Course Macea Constructed by "Sunrise" management by "NTN"
 - (2) STA 7 Skm, Stone Masonry Retaining Wall
 - Constructed by "Mejori" management by "Jourse
 - 2): STA 6+270, RC double (910 dai) Pipe Culvert Constructed by "Junise"

2. Minutes of 2rd Coordination Meeting of Site Safety Committee Opening Address:

Mr. Joan Gregorio de Carvalho, Chief of Dop. Construction of DRBFC and Chairman of pilot Site Safety Committee, made an opening speech;

Thank you very much for attending the Meeting however you are so busy. This Meeting is to be held for Safety Activities, such as Safety Patrol at the site of Ex-Japan Road construction, where is located from the middle stream of Compro River to the junction point with National Road A02.

First of all, member of the Site Safety Committee are introduced

x

Record of 2= Coordination Meeting and 2nd+ Safety Patrol by DRBFO

The Project for the Canacity Develop ent of Road Services in the De

Coordinator : Nazario, Martinho

Sub-coordinator : Pricilla

Observer : Alfredo, Angelo, Lourenco, Julius, Mousinho, Altino, Fernando, Colostino Contractor: Jonise, NTN, Mejori, Sunrise

CDRS Advisor: Mr. Knizumi, Ms. Tereso

Secondary, Explanation for Safety equipment (goods) are made by the Chair Man-We are instructing that workers on the construction site must wear safety believed through Contractor. And also, it is recommended to wear the safety vest which is colored and have reflection tape.

Each safety goods have each functions and objectives. For example, safety helmet aim to protect the head of worker when worker is hit by dropping material or he falls down at the place high incidentally. However, it is hot at construction aite and many workers do not wear safety belinet and color vest.

What we can do are il letting the workers know the objectives of color vest, safety helmet. masks and goggles and ill making the workers wear such safety goods, at least, if they are provided such safety goods.

Place and work items for 2nd Safety Patrol

Eng. Nazario De Jesus Freitas, Coordinator of the Committee, explained the status quo of the site and following working site are decided the inspection points for 2nd Safety Patrol as stated as above 1. Date and Place 2).

Engineers from the Contractor in charge of each works also participate in the Salety Patrol

Question / Answer and Discussions

Q/Comments: Mr. Fernando F. F. C. Freitas, Observor / Highway Department: These activities are the activity as a Case Study (C/S) of the Project?

Safety Patrol and Meetings have been already conducted several times. However outstanding matter had been pointed out at the previous Patrol, but such pointed out safety issue has not improved on the site yet. In such case, it will be better to discu regarding counter measures, such as which kind of penalties would be imposed to the Contractor by the DRBFC as an Employer of the Works, isn't it?

-One example of Safety issue of one Highway Project, which he is in charge of, were explained: in the Contract of that Project, i) there is a certain work item that the Contractor should provide "Officer of Environmental Social Impact" and the cost of which is allocated and ii) implementation of safety activities are clearly stated in the

Record of 2nd Coordination Meeting and 2nd+ Safety Patrol by DRBFC

The Project for the Capacity Development of Road Services in the Democratic Republic of Timor Lette (CDRS

Contract Docum

Therefore, when SEPFOPE instructs the counter measures for safety during Safety Pairol, the Contractor may be imposed the penalty. Consequently, the awareness for sufety at the site become increase and the Contractor takes more attention for sufety neasures in order not to be charged penalty.

But, on the mustruction sites of Ex-Japan Road, work items for Environmental Social Impact and Safety Activities are not stated and no cost is allocated in the Contract. Therefore, carrying out of Safety Patrol again on the site like Ex-Japan Road cannot bring effective results regarding safety, isn't it ?

A/Comments: Mr. Angelo Riberiro, Observer /Training & Cooperation Department: On previous meeting for 1st Safety Patrol, the agenda were discussed already.

We understand that the budget and Contract of our Works will not be changed.

It is one idea that meaning and position of this Case Study, Safety Patrol by DRBPC, are the exercise in which the Employer, Contractor and Workers il think of counter measure for Safety is important and ii) change their mind for Safety measures-

A/Comments: Mr. Jana Gregoria de Carvalho, Chairman / Chief of Dep.

Objective of these activities for Safety is not "Imposing penalty against Contractor." As Mr. Angelo mentioned, the objective is that everybody's awareness for Safety will be enlightened in the activities of C/S

Through these activities; it is expecting that i) both the Employer, we DRBFC, and Contractors recognize the importance of the Safety and ii) implementation of safety activities will be stated and the cost of safety will be allocated in the Contract in our further Project.

3. Record of 2nd Safety Patrol by DRBFC

(D: STA 17+850 - STA 18+100, Aggregate Base Course Constructed by "Sunrise" management by "NTN"

Finding out dangerous point

1) There are Warning/precaution signboards are set both end of the working area, but the "Police Line" (temporary safety guard hence between the working area and the open for public transportation)

2) All the workers on the site does not wear helmet and safety vest.

Instructions / expecting counter measures/ comments

1) To put "Police Line" for separation between working area and open public area. 2) To instruct contractor to lot all workers to wear safety goods

Record of \$= Construction Meeting and 2nds Salinty Pairol by DRIPT

The Project for the Capacity Development of Road Services in the Democratic Republic of Timor Leste (CDRS)

* The Contractor are required that the Contractor recognize the importance of Safety Patrol on site because Safety Control is very essential issue

(2): STA 7 - Bkm, Stone Masonry Retaining Wall

Constructed by "Mejori" management by "Jonizo" Finding out dangerous point 1) Only three workers wear helmet and some of worker wear slip/ have fost. 2) Workers don't wear safety helmet 2) There is no watchmen and warning sign board 3) the site is very dusty Instructions / expecting counter me 1) The Contractor must provide safety goods, safety helmste and color vest and worker should wear anne boots for protection of his foot 2) To put warning sign board and/or watchmen, especially near construction machines 2) To watering to reduce dusty condition

122: STA 6+270,RC double (910 dai) Pipe Culvert. Constructed by "Jonise"

Finding out dangerous point

1) Finishing works for the top of Retaining Wall is High Place (about 3-4m high from the bottom) and it is danger without working platform.

2) The Contractor provide helmets but actually worker does not wear helmet and some of them are bare foot.J

3) There is no warning hoard for open traffic go through just beside the working excavated hole.

Instruction Expecting counter- measures / comments

1) To prepare and use the scaffolding for the works where workers will work at the high place, such as top finishing Retaining Wall construction. 1-2) To wear muck preventing such dust from the workers

2) The Contractor must let all workers wear safety goods, safety helmuts and color vest and worker should wear some boots for protection of his foot 3) To put warning sign board, watchmen and Police Line more clearly

* DRBFC, as the Employer of the Project, and Contractor must follow instructions /safety procedures by Safety Patrol.

Attachment1: Attendance List

2: Photos of 2nd Meeting & 2nd Safety Patrol

3: Check List for 2nd Safety Patrol used on the site on 19 September

4: Agenda and reference information for Safety Activities of the Meeting

Record of 2nd Coordination Meeting and 2nd⁴ Safety Patrol by DRBFC

Republic of Timor Leste (CDRS)

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Attach

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	Mr	Martinho B. De Sous:	Engineer	Construction			1970
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in	Mr	Angelo Riberiro	Administrator	Training at Cooperation			SULLA
10	Mr	Lourenco Luis	Engineer	Project			-
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Report of 9-4 Coordination Monting and 2nd+ Safety Patrol by DRHFC

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The Project for the Capacity Development of Boad Services in the Democratic Republic of Timor Leste (CDRS)

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Record of 2nd Coordination Meeting and 2nds Safety Patrol by DRBFC

The Project for the Capacity Development of Road Services in the Democratic Republic of Timus Loris (UDRS)

The Project for the Capacity Development of Road Services in the Democratic Republic of Timor Leste (CDR)

Attachment 3: Check List for 2nd Safety Patrol used on the site on 19 September

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9 Record of 2rd Countrianting Advoting and Sody Safety Paired by DRDPC

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Record of 2rd Coordination Meeting and 2nd⁺ Safety Patrol by DRBFC

10

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The Project for the Capacity Development of Road Services in the Democratic Republic of Timor Leste (CDRS)

11 Record of 2nd Coordination Alecting and 2nd Suday Patrol to OBBEC

12 Record of 2nd Coordination Meeting and 2nd+ Safety Patrol by DRBFC

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The Project for the Capacity Development of Road Services in the Democratic Republic of Timer Lette (CDRS)

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The Project for the Capacity Development of Boad Develops in the Democratic Republic of Timor Lesis (CHRS)

Martin Capetr Campartia mobile presidents there

Attachment 4: Agenda and reference information for Safety Activities of the Meeting

14 Record of 2rd Coordination Meeting and 2nd⁺ Safety Patrol by DRBFC

The Project for the Capacity Development of Road Services in the Democratic Republic of Timur Leste (CDRS)

Parent of 21 Coordination Alerting a

d and Sales Faind by DRIPPO

Attachment 4: Agenda and reference information for Safety Activities of the Meeting

The Project for Capacity Development of Road Services in the Democratic Republic of Timor-Leste (CDRS)

Coordination Meeting

For Site Safety Committee for 2rd "Safety Patrol by DRBFC" (Recal Kondow under Partis Researdance locas under Paroi Researdance (Recal Kondow under Paroi Researdance) yorg Re-2 elektDiEPCC"

Date: Wednesday 19 September, 2018

18

Time: 10:00 - 11:00 Venue: Conference Room, DRBFC Head quarter, Dili

National Directorate of Road, Bridge and Flood Control (NDRBFC) and pilot Site Safety Committee

	AGENDA
\$2:53+10:00	Are, vid and Rocepturn for proposed into Safety Committee member saturadance
1232 1040	Oproving oddi vos přiku Satellarite (p. a.), hiro Larasu of the member Sing, Yano Gregoria da Carvallos Chief of Deg. Consorcedan of DRDFC and Chierann ef přise Safory Consolition See Lin ef members of the Site Safory Consolitor glanar carbine mano margoza parmay
1313-10:25	Reporting the 1° Softer Match Add on 24 June 2018 Soft of manager of 5, "Constant on Meeting and 1° Softer Parts
13.25 - 10,19	 Phonese the place and water times for 2ⁿ Suber Parel held on the aborean US Separabor 2018 See the Economics of the ^{2nd} Suberg Parel
12.12-1.49	3 Q'A and Burnein reporting Solidy Autobiev Solidy Parel Adjuste (Clening)

16 Record of 9rd Coordination Monthly and 2nd Subity Faind by DRBR

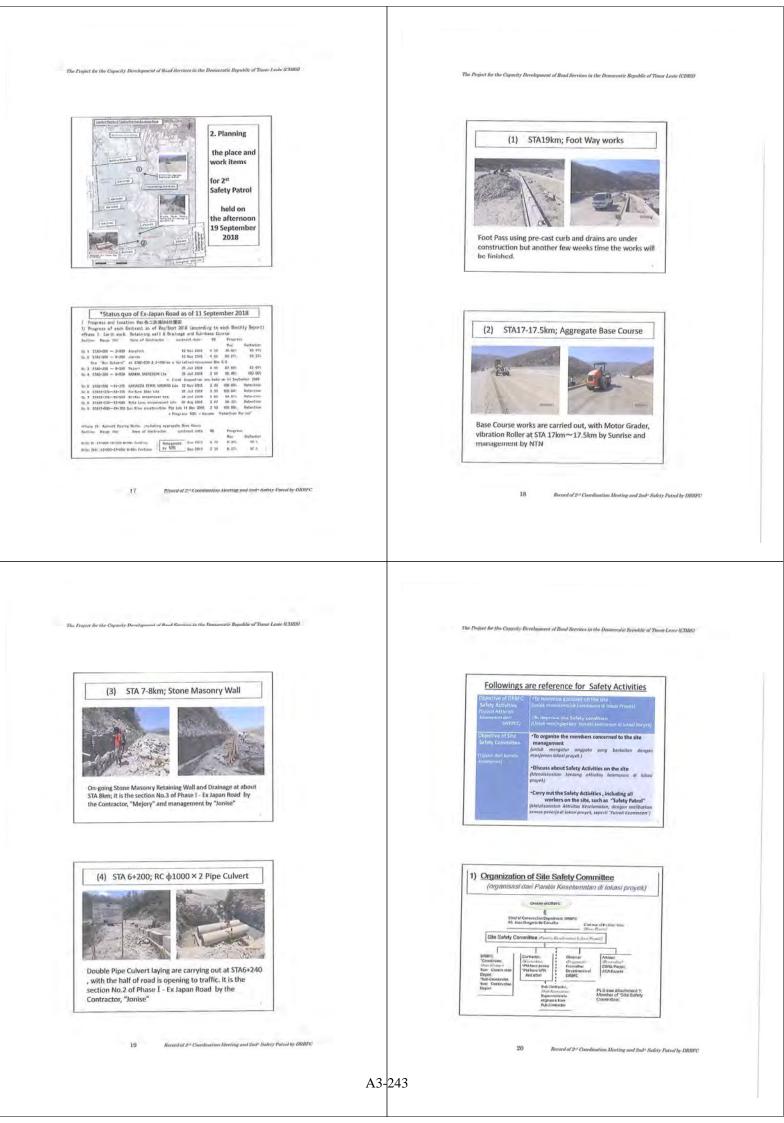
The Project for the Capacity Development of Road Services in the Democratic Republic of Timor Leste (CDRS)

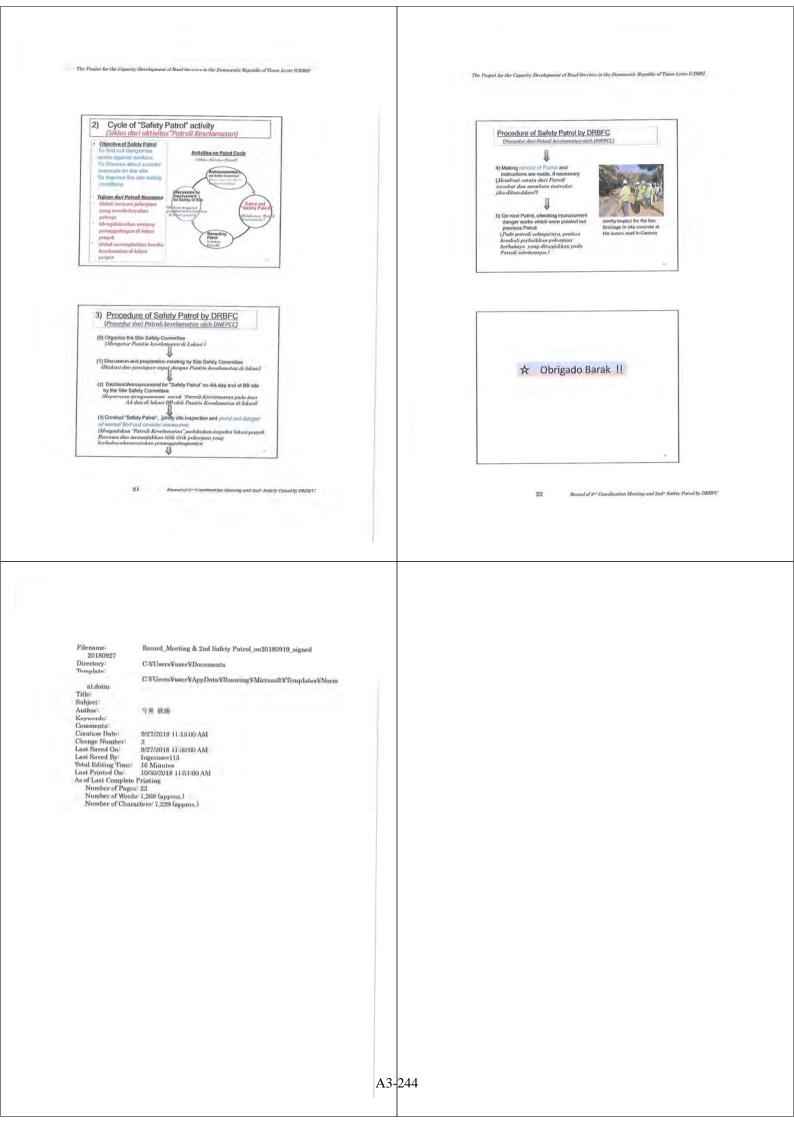
Member of pilot "Site Safety Committee" = For Case Study of "Safety Patiol by DRBFC" at pilot site on Ex-Japan Road =

Party	Role in the	Title and	Name of member	Correspondence
1	Contunittee	Department	(Draft only)	
DRBFC	Chair person	Chiefof Construction Dept.	Eug Joso Geospario de Carvalho	1
	Coordinator	Engineer is charge	Eng. Navacia De Jasus	78550598
		of proposed site	Freitas	interio fenticali idead.com
	Coordinator	Engineer in charge	Eng. Martinha B. De	77253074
	1.000	of proposed site (Parement norks)	Sousa	build light the state of the st
	Sub-	Construction Dept.	Eng. Pricilla 1. Dos R.	73391216
	coordinator		Góman	enehdizi
				yahas ayns
	Observer	Representative of Training &:	Mr. Alfreda E. Dos Santos	77131601
		Cooperation Dept.	Mr. Angelo Riberina	77243393
	Observer	Ditto bitt	Eng Lourneo, Chief of Planning	
		Project Dept	Eng. Julius L. Kelty,	-
		1.	Planning Section	77491305
	Observer	Ditto kut	Eng Moutinho Tilman	
		Maintenance Dept	Coordinator of Region 2	
			Eng. Altino Fernandes Da Costa, Region 2	and the second s
	Observer	Ditlo hut	Mr Fernando F. F. C.	77051326
		Highway Dept	Freitas	
		10 A. A. A. A. A. A. A. A. A. A. A. A. A.	Mr. Seleshoo E. Nimenes	77285549
Contrac	Jonise	Project Manager	Mr. Syahrsil Akbar	77553987
-tut		enginees in charge, of Safety	XX	
	NTN	Project Managers	Ms. Hartoill	73152969
	OCATURE FA TIMOR NAROSTAN LAG		Mr. Januario	77239675
	Mijeri	Fit is half to there	DE .	
	Finisher	3deb	44	
	Sumise	PSC or EndF in thirst Safety	dd	
CDRS	Advisor(Ad)	CDR5, Road	Mr. Johji Keimini	76467974
	1 and a start	Construction		johji keinusi (j ingerasocoim
	Assistant Ad	Civil England	Me Letichia Silveira A	77717549
	and Interporter	1	Barrelo	ti chiabaneto il mini Lecni

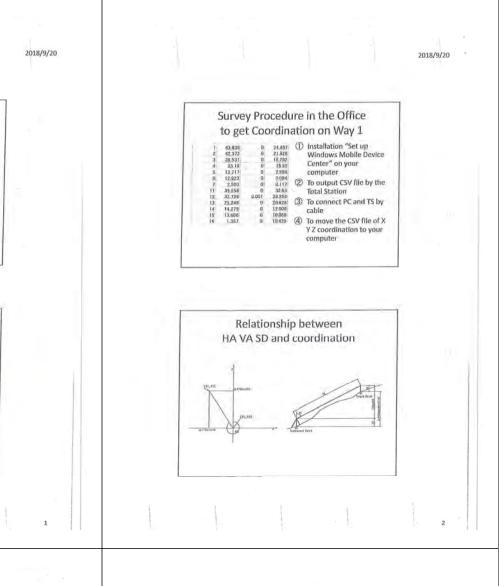
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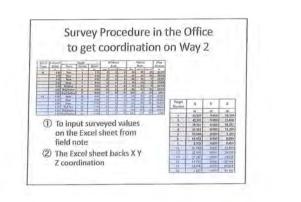
Record of 2nd Coordination Meeting and 2nd⁺ Safety Patrol by DRBFC





Slope Collapse countermeasure dtudy base on site observation on 20 September 2018





Slope Collapse countermeasure

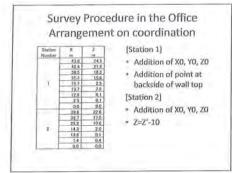
Study Based on Site Observation

Survey Procedure in the Office Evaluation of Countermeasure Idea

CDRS 20th Sep. 2018

Isolated Cross Section Survey

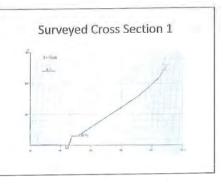
at the site on 14th Sep.





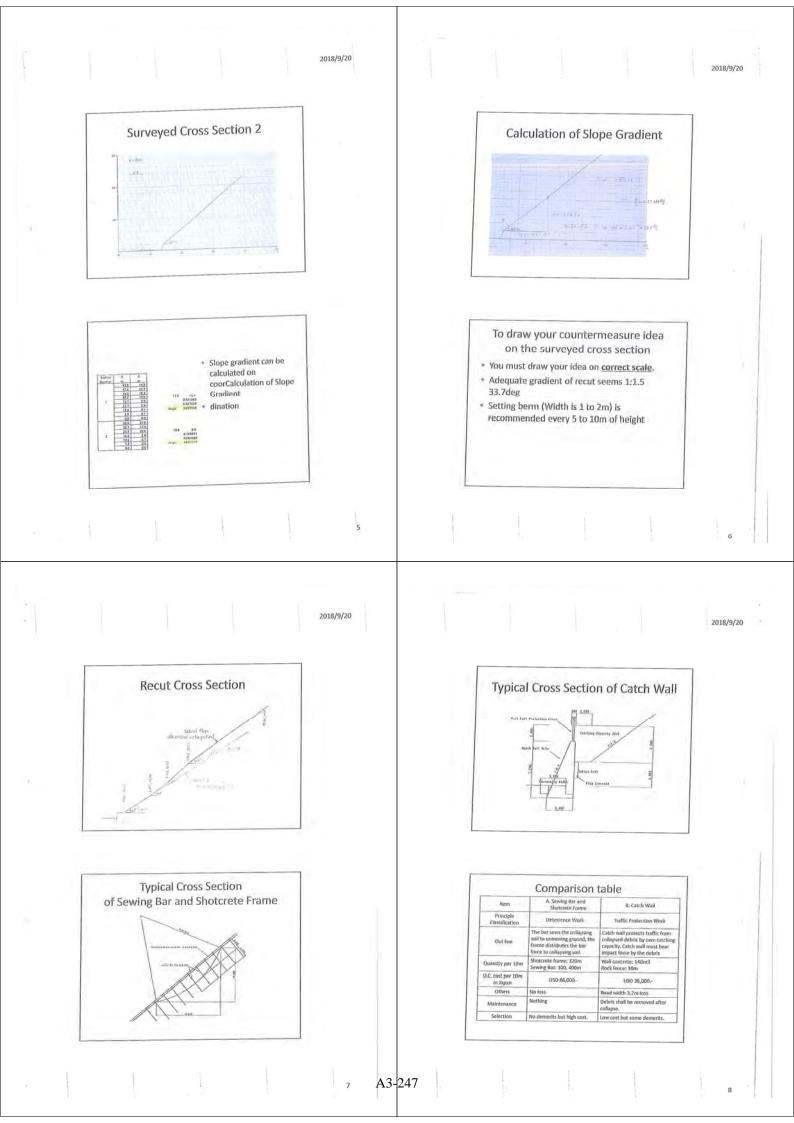
2018/9/20

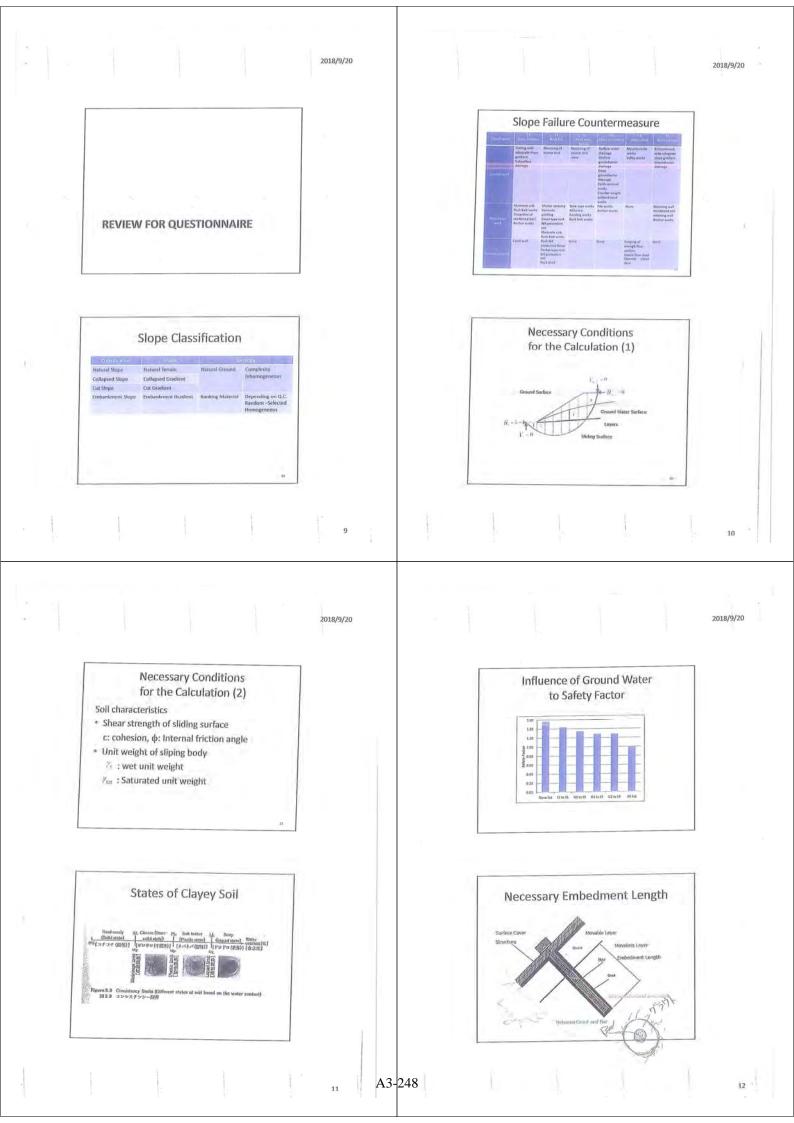
- Section paper is convenience for drawing.
- Selection of scale: Paper must be bigger than cross section
- * To draw X axis and Z axis
- · To plot all points one by one
- To tie point to point by line

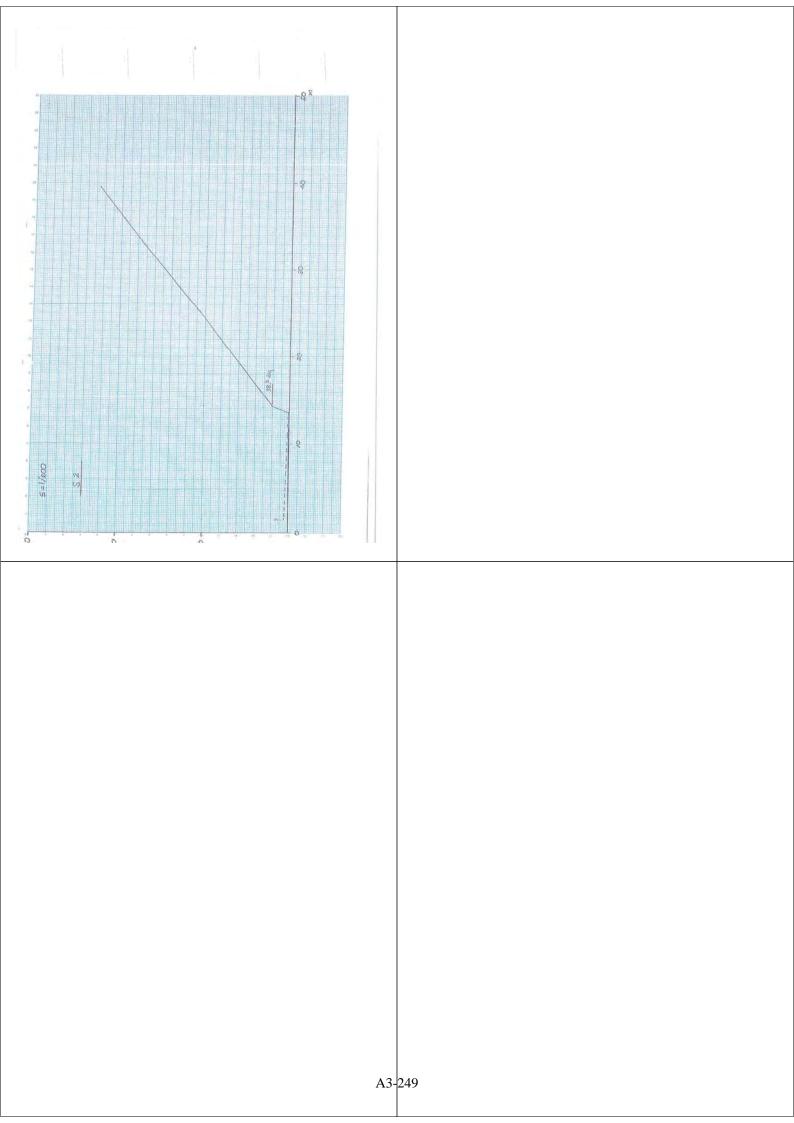


3

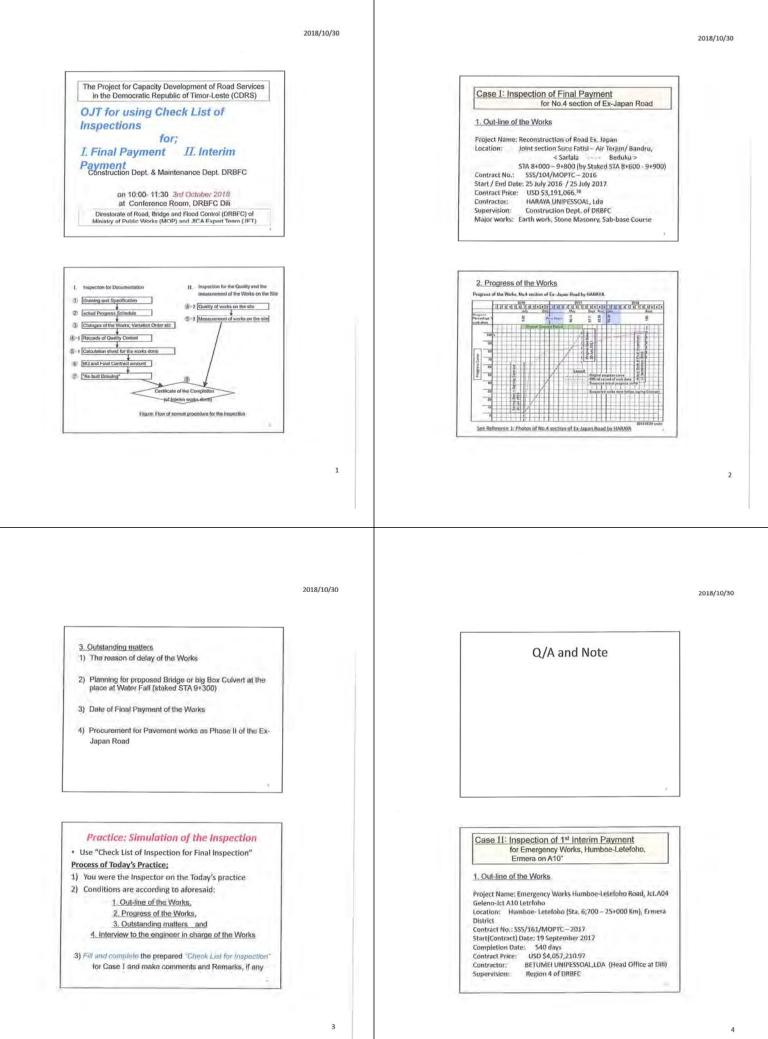
2018/9/20







OJT for using Checklist of inspection for I. Final Payment and II. Interim Payment on 3rd October 2018



2018/10/30

Bain a	ork Itemi	100	al Contract	Price is no	begradh- Sc
No. Item	Item Description	(Unit	Chighnal Quantity	Unit Price (US\$)	Revised Quantity
202.1	Excavition Common and Bock Excavition	Cu.m.	19,882.50	3.80	43,106.50
204.1	Sob grade preparation	Sq.m.	62,500.00	0.85	62,500.00
301	Aggregate Sub-Base Course	Cana	23,900.00	39.19	32,594.70
303	Crushed Aggregate Base Course	\$4m	12,000.00	67.84	1,576.26
601.1#	Reinforced concrete pipe culvert, 1000mm (dia)	Lm	42.00	283.44	154.00
605	Stone Masonry	Gum	17,578.00	76.53	19,825.68
610	Gabion Wall	Cum	3,400.00	68.95	1,150.00
New Rev	114				
202.2	Rock Excavation	Cum	-	\$1.85	42,152.50
204.2	Removal Existing Asphall	Sam	-	2.22	15,300.00
601.24	Reinforced concrete pipe columit, 1200mm (dia)	Let	-	156.76	68.00
601.34	Reinforced concrete pipe colvert, 600mm (dia)	Les	-	179.22	26.0)
101	Relocation of Public Utilities (Compensation for Plantation of College)	U	-	34,150.00	1.00

2. Progress of the Works

- 1) The Works commenced on September, 2017
- The Progress as of December 2017 was 36 %
 The Claim for 1st Interim Payment was made, with the amount about 1 M\$ (one million US\$)
- The Works have been suspended from Jan to June, 2017
- The Contractor submitted "Variation Order No.1" on 1st June, 2018
- 6) The Works resumed (re-started) on 9th June, 2017



7

A3-252

5



STA 18km; proposed 2 X 61200mm Pipe Culvert (New litem; 621.24) was completed as 4 Valation on 12 September; 2018 (only working sketch of by the Contractor was provided) cituated incom (Stat, memo No.21):

Course (item:301) Material. Samples are now testing at Laboratory for its quality assurance on 12 September, 2018 «Qualed from Ph/RES, memo No.21>

are now was provided) ssurance was provided) «Quoted from PhL4, men

3. Outstanding matters

- The test result of proposed material for "Sub-Base Course" has not yet been submitted by the Contractor
- Without approval of the material of Sub-Base Course, such works has started and the Contractor insists the works have been done at some parts.
- The location/position/area of works, such as Sub-Base Course, Retaining Wall, are not shown on the Drawing
- Detailed shop drawing for 2×1200mm Pipe Culvert at STA18km has not yet been submitted from the Contractor. It is one of new work item of Variation No.1



Gabion Box Retaining Wall, Existing, steef corugated pipe (2m dia) arr used for remedial work. Some of aid steel pie is found deformed from round stape on 13 February, 2018 «Quoted from Ph9, memo No.17»

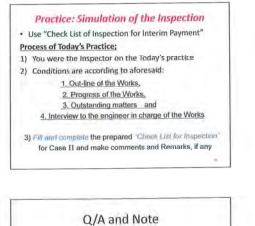
On-going construction area for Stone missionly Retaining Wall and Unic Drainage on 13 February, 2018

d from Ph10, memo No 175

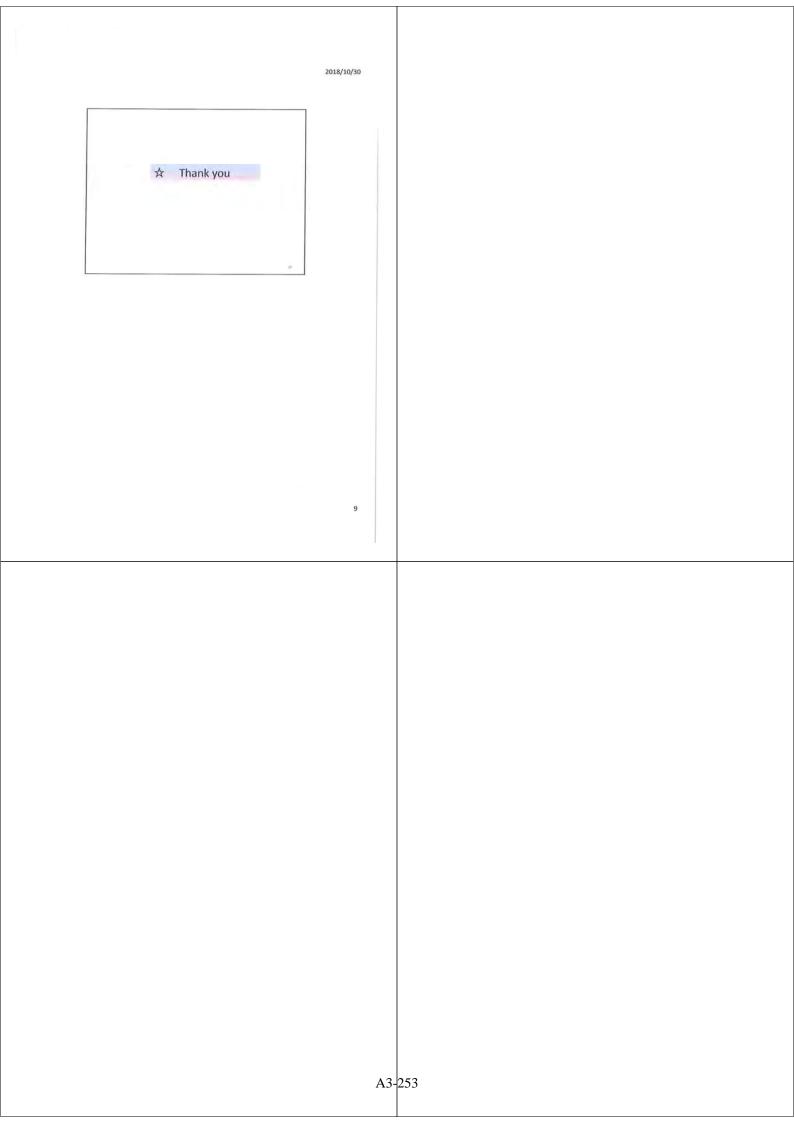


STA2-3 km Sub-Grade leveling and preparation for Sub-Base course; grave material from Geleon River. And impection of leveling and compaction by Macadam Roller on 28 June, 2018 «Quated Irom Pb3, memo No.19» STA at about 13km near existing , Bridge, Stone Masonry Retaining Wall. Checking Quality of the works using Eheck List for Construction: "Stone Masonry Retaining Wall": on 28 June, 2018 +Quoted from PhS, memo No.19>

2018/10/30



References: Photos, No.4 of Ex-Japan Road by "Haraya" 1st Invoice for works accomplished on Emergency Works Humboe-Letefolio "Jable of QC points on Section 301, 302 & 303 aggregate course in SPC "Copy of custificate of completion of No.4 section of Ex-Japan Rd (if any) 2018/10/30

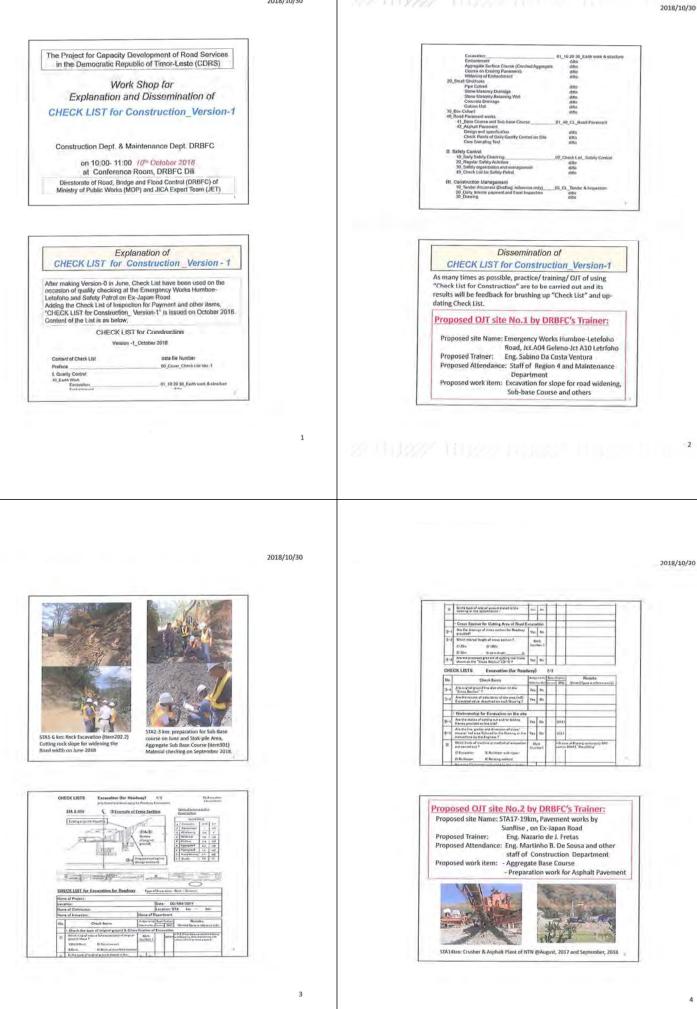


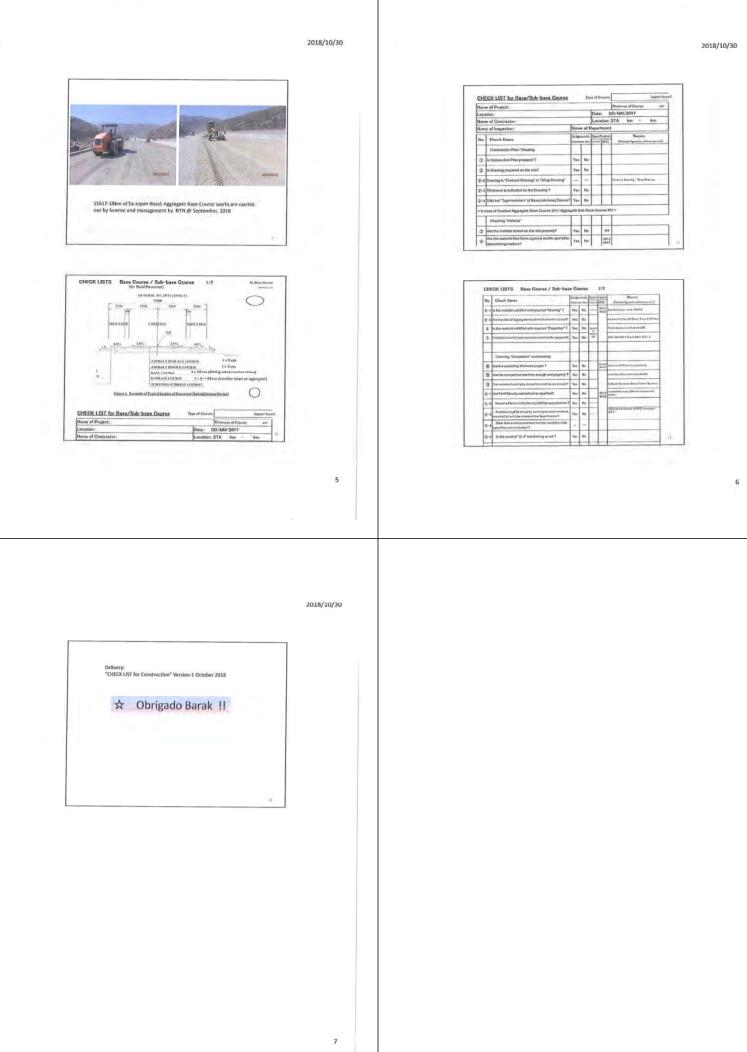
Workshop for Explanation & Dissemination of Checklist for Construction Version_1 on 10 October 2018

2018/10/30

2

4





TO CR of JICA Timor-Leste OFFICE

Project Title: The Project for the Capacity Development of Road Services in the Democratic Republic of Timor-Leste

Version of the Sheet: Ver.7 (Term: October 2018 – March 2019)

Name: Hisashi MUTO

<u>Title: Team Leader/ Road Maintenance1</u> Submission Date: 31st March, 2019

- < I. Summary (all achievements are as of 31st March, 2019) >
- 1. Progress
- 1-1 Progress of Inputs
- 1-1-1 Japanese side

< Short-term experts dispatched to Timor-Leste>

NO	Name	Title	Dispatched Period to Timor-Leste	Changes or delay
1	Hisashi MUTO	Team Leader/ Road Maintenance 1	(1 st) 8 th Mar – 10 th Apr, 2016 (2 nd) 14 th Jun – 25 th Jun, 2016 (3 rd) 1 st Sep – 18 th Sep, 2016 (4 th) 23 rd Jan – 19 th Feb, 2017 (5 th) 24 th Mar – 2 nd Apr, 2017 (6 th) 18 th Aug – 10 th Sep, 2017 (7 th) 24 th Nov – 14 th Dec, 2017 (8 th) 2 nd Feb – 4 th Mar, 2018 (9 th) 8 th Jun – 1 st Jul, 2018 (10 th)19 th Sep – 12 th Oct, 2018 (11 th)14 th Nov – 8 th Dec, 2018 (12 th)10 th Mar – 31 st Mar, 2019	None
2	Makoto MATSUURA Mitsuhide SAITO	Deputy Team Leader/ Road Maintenance 2 Deputy Team Leader/	 (1st) 8th Mar – 15th Apr, 2016 (2nd) 14th Jun – 13th Jul, 2016 (3rd) 20th Sep – 14th Oct ,2016 (4th) 1st Dec – 16th Dec, 2016 (5th) 23rd Jan – 19th Feb, 2017 (1st) 24th Mar – 9th Apr, 2017 	None Note: Mr.
		Road Maintenance 2	(2 nd) 9 th Jun – 25 th Jun, 2017 (3 rd) 16 th Oct – 12 th Nov,2017	Mitsuhide Saito

			(4 th) 16 th Feb – 11 th Mar,2018	replaced Mr.
			(5 th) 26 th Apr – 16 th May,2018	Matsuura in
			(6 th) 7 th Sep – 28 th Sep,2018	Deputy Team
			(7 th) 15 th Feb – 17 th Mar, 2019	Leader post.
4	Johji KOIZUMI	Road Construction	(1 st) 19 th Jul – 17 th Aug, 2016	None
		Supervision	(2 nd) 24 th Sep – 14 th Oct,2016	
			(3 rd)19 th Jun – 5 th Jul, 2017	
			(4 th) 21 st Aug – 4 th Oct,2017	
			(5 th) 14 th Nov – 21 st Dec,2017	
			(6 th) 30 th Jan – 4 th Mar, 2018	
			(7 th) 8 th Jun – 1 st Jul, 2018	
			(8 th) 7 th Sep – 13 th Oct, 2018	
			(9 th) 7 th Feb – 23 rd Mar, 2019	
			(1 st) 28 th Mar – 17 th Apr, 2016	None
	Sueo HIROSE		(2 nd)13 th May – 11 th Jun, 2016	
			(3 rd) 14 th Aug – 12 th Sep, 2016	
5		Quality Control/ Road	(4 th) 7 th Oct – 14 th Oct, 2016	
5		Repair	(5 th) 23 rd Jan – 22 nd Feb,2017	
			(6 th) 4 th Aug – 3 rd Sep, 2017	
			(7 th) 16 th Feb – 18 th Mar, 2018	
			(8 th) 1 st Mar – 23 rd Mar, 2019	
			(1 st) 11 th May – 31 st May, 2016	None
			(2 nd) 28 th Jun – 21 st Jul, 2016	
			(3 rd) 12 th Sep – 6 th Oct, 2016	
			(4 th) 13 th Feb – 8 th Mar, 2017	
6	Shutaro SAKANAKA	Disaster Restoration	(5 th) 17 th Apr – 7 th May, 2017	
			(6 th) 23 rd Oct – 12 th Nov, 2017	
			(7 th) 16 th Jan – 4 th Feb, 2018	
			(8 th) 2 nd Mar – 18 th Mar, 2018	
			(9 th) 1 st Jun – 17 th Jun, 2018	
			(1 st) 3 rd Mar – 25 th Mar, 2018	Note:
			(2 nd) 15 th Jun – 8 th Jul, 2018	Disaster
7	Kazuharu	Disaster Restoration2	(3 rd) 7 th Sep – 30 th Sep, 2018	Restoration 2
	KOISHIKAWA			has been
				created as a
				new position;

				Mr.
				Koishikawa
				was
				assigned to
				this position
				in March
				2018.
			(1 st) 17 th Mar – 15 th Sep, 2016	None
		Road Design/ Project	(2 nd) 21 st Jun – 13 th Jul, 2016	
8	Yoshiyuki AKAGAWA	Coordinator	(3 rd) 12 th Sep – 6 th Oct, 2016	
			(4 th) 13 th Feb – 5 th Mar, 2017	
			(1 st) 31 st Jul – 30 th Aug, 2017	Note: Mr.
			(2 nd) 16 th Oct – 23 rd Nov, 2017	Brooker-Jone
			(3 rd) 2 nd Feb – 4 th Mar, 2018	s replaced
9	Nicholas	Road Design/ Project	(4 th) 8 th Jun – 1 st Jul, 2018	Mr. Akagawa
	BROOKER-JONES	Coordinator	(5 th) 7 th Sep – 30 th Sep, 2018	in Project
			(6 th) 26 th Feb – 21 st Mar, 2019	Coordinator
				post.
10	Kenji MINEGISHI	Structure Design	(1 st) 5 th Apr – 24 th Apr, 2016	None
			(2 nd) 5 th Jul – 4 th Aug, 2016	
			(3 rd) 14 th Nov – 13 th Dec,2016	
			(4 th) 12 th May – 11 th Jun, 2017	
			(5 th) 1 st Sep – 1 st Oct,2017	
			(6 th) 3 rd Nov – 17 th Dec, 2017	
			(7 th) 6 th Apr – 13 th May, 2018	
			(8 th) 24 th Aug – 30 th Sep, 2018	
11	Takashi SAITO	Database	(1 st) 19 th Jul – 24 th Aug, 2016	None
			(2 nd) 3 rd Oct – 14 th Oct, 2016	
			(3 rd) 13 th Mar – 12 th Apr, 2017	
			(4 th) 16 th Jun – 2 nd Jul, 2017	
			(5 th) 18 th Aug – 1 st Oct, 2017	
			(6 th) 16 th Feb – 4 th Mar 2018	
			(7 th) 5 th May – 19 th May, 2018	
			(8 th) 28 th Aug – 11 th Oct, 2018	
			(9 th) 19 th Feb – 21 st Mar, 2019	
12	Masahiko HAYASHI	Landslide	(1 st) 16 th Jun – 28 th June, 2017	Note: Activity

			(2 nd) 27 th Oct – 9 th Dec, 2017	on Landslide
			(3 rd) 18 th Mar – 18 th Apr, 2018	analysis was
				approved by
				2 nd JCC; Mr.
				Hayashi was
				assigned in
				June 2017.
13	Sohshi MIKAMI	Topographical	(1 st) 19 th Jun – 16 th Jul, 2017	Note: Activity
		Analysis	(2 nd) 18 th Mar – 18 th Apr, 2018	on Landslide
				analysis was
				approved by
				2 nd JCC; Mr.
				Mikami was
				assigned in
				June 2017.
14	Nao TSUJIMURA	Evaluation/Monitoring	Resident in Timor-Leste	None

< Equipment and materials >

NO	Items	Qty	Unit price	Unit	Total amount
1	Desktop computer	1	1,150	USD	1,150
2	Inclinometer assembly	1	1,585,800	JPY	1,585,800
3	Borehole casing	1	404,400	JPY	404,400
4	Dokenbo assembly	1	133,000	JPY	133,000

(Remark: Equipment and materials which have a service life of 2 years and are more than JPY 50,000 are listed.)

1-1-2 Timor-Leste side

• Counterpart (C/P) personnel (from MPWTC and NDRBFC)

NO	Name	Title of the Project	Engaged Period
1	Rui Hernani F. Guterres	Project Director	20 th Feb, 2018, to date
2	Milton Ramanata C. Monteiro	Project Manager	20 th Feb, 2018, to 28 th Feb, 2019
	Joao Mario Gama de Sousa		1 st Mar, 2019, to date
3	Simao G. Armindo Laranjinha	C/P staff	1 st Mar, 2019, to date
4	Joao Pedro Amaral	C/P staff	8 th Mar, 2016, to date
5	Joao Gregorio	C/P staff	8 th Mar, 2016, to date

• Equipment and materials for the project office

NO	Items	Qty	Unit
1	Office space (including desks and chairs)	1	room

1-2 Progress of Activities

NO	Activity	Achievement level
1.2	To conduct periodic/routine inspection.	 Periodic/routine inspection has been done along A03, A04, A06, A08, A11, A12 and A16 (173 km). Road inspection using drive recorder has been conducted (1419 km).
1.3	To update the database based on the inspection result and repair/rehabilitation works of road and bridges.	 In 5th JCC, C/P requested repetition of training for operation of GIS database; after 5thJCC, JICA Expert Team repeated training of GIS operation. Data from urban & national road surveys were inputted into GIS database (173 km).
1.5	To implement emergency inspections and repair/rehabilitation works when necessity arises.	 During this monitoring period, C/P did not request support from CDRS regarding emergency inspections; JICA expert team proposed continuation of support for C/P carrying out emergency inspections; proposal was approval in 5th JCC.
1.6	To undertake appropriate road maintenance/ rehabilitation works by following annual work and budget plans which reflect priorities within the limited budget.	 Based on inspection results, NDRBFC is preparing 5-year and 2019 annual plans. NDRBFC has secured an annual budget for maintenance and rehabilitation works in 2019 (Infrastructure fund: 150,508,000 USD + Line of Ministry budget: 12,386,000 USD).
2.2.	To conduct the case studies for the planning, design check and construction supervision of the project.	 IPG and NDRBFC integration team conducted monitoring of the slope mass movement through data collection by inclinometer and underground water level indicator (Site: Aituto landslide). On-the-job training for payment inspection using checklists was conducted (site: A02 bypass road called Ex-Japan Road). On-the-job training for quality control of stone masonry retaining wall using checklists was conducted (site: Humboe-Letefoho).

		 was carried out with ILO JICA expert tea inter-departmental work design guideline; inte scrutinized a propose concluded that the design amendments (site: Sarla JICA Expert Team examples 	am supported NDRBFC king group using the culvert r-departmental working group d design from a contractor, gn was excessive and suggested ala, Ex-Japan Road). hined knowledge improvement of The test results for each subject
		Subject	Number of the people whose test scores have improved after training
		Landslide investigation	17 people out of 17
		Bridge substructure protection (Scouring and protection block)	5 people out of 14
		Culvert planning and design	6 people out of 11
		Quality control, Safety control and Construction management	N/A Pre-test was given in June; after pre-test, based on request of C/P, contents of checklists have been increased. In this monitoring period, JICA expert team revised contents of examination. The result of the re-examination will be reported in next reporting period.
		Slope protection	3 people out of 7
3.5	To reflect the lessons learned from case studies to the technical guideline	 guideline; C/P scrutiniz contractor, concluded th suggested amendments In order to standardize construction supervision C/P requested JICA technical documents as NDRBFC; JICA expert dissemination of guidelir Municipal administration requested repeat semi expert team proposed 	e planning, design check and of the project in all works in TL, expert team to launch those s official documents of MoP or team conducted workshops for

3.6	To disseminate the technical guideline for concerned parties	•	JICA Expert Team organized workshops to disseminate the technical guidelines; NDRBFC inter-departmental working group conducted a workshop to present their culvert plan regarding 1) design flood of catchment and 2) design capacity of culvert; guidelines and checklists were disseminated to the representatives of municipal
			administrations and higher education institutes.

1-3 Achievement of Output

	Indicators of Outputs	Achievement level		
1.1	More than 30% of requested budget for road maintenance are distributed.	December 2018, NDRBFC budget plan for 2019 with a 450,221,000.90 USD; the o shown in the below table.	a total amount of	
		National roads	7,230,800 USD	
		Municipal roads	9,666,400 USD	
		Urban roads	1,560,000 USD	
		Rural roads	18,051,000 USD	
		Maintenance roads and bridges	13,632,000 USD	
		Bridge construction	2,395,000 USD	
		River protection	1,050,000 USD	
		Highway	4,788,000 USD	
		Environment and	60,000 USD	
		kilometer posts		
		Emergency works	2,500,000 USD	
		Ongoing projects	384,190,700 USD	
		General administration	5,098,000 USD	
		February 2019, an annual tamount of 162,894,000 details of each item are sho Infrastructure fund for roads	USD was approved; the	
		Infrastructure fund for bridges	9,979,000 USD	
		Infrastructure fund for maintenance and rehabilitation	12,997,000 USD	
		Line of Ministry budget	12,386,000USD	
		down per work. Therefore, achievement le ready to be measured.	to be evaluated and break evel of this output is not	
1.2	Improved road database is utilized for preparation of the annual work plan of road maintenance.	insufficient to measure	nethod with drive recorder volume of data was its utilization. Moreover, base is not ready to be	

2.1	At least 3 case studies for both construction and design are conducted. (Totally 6 case studies)	60% Case studies to improve the capacities of survey and design and safety control were conducted as planned. Implementation of case studies for construction management using checklists have been delayed due to delayed budget allocation. However, through OJT, JICA expert team compiled draft checklists twice. (The latest version 3 has been drafted.) Those case studies will be conducted in the project extension period.
2.2	More than 60% of trainees pass the achievement test for construction supervision and design.	Baseline survey results showed that the percentage of examinees exceeded the passing line by respective subject was a) design: 28%, & b) quality control: 8%. In order to grasp the knowledge improvement of trained NDBRFC staff, JICA Expert Team gave mock exams continuously. The trainees' scores from the mock exams have been increasing step by step. The final achievement test will be given after the completion of the case studies. Therefore, achievement level of this output is not ready to be measured.
3	Technical guideline of investigation and design for slope protection, drainage and measures against scouring are prepared.	 90% Draft guidelines for slope protection, bridge substructure protection, culvert design, and landslide investigation have been prepared. However, checks for whether prepared guidelines can be utilized by NDBRFC have been insufficient. In order to confirm their efficiency and applicability, JICA expert team carried out workshops for dissemination; guidelines and checklists were disseminated to the representatives of municipal administrations and higher education institutes. Dissemination of guidelines will be continued in the project extension period.

1-4 Achievement of the Project Purpose

Indicators of Project Purpose	Achievement level
Total length of maintained national roads were became 400km.	JICA expert team collected IRI data of all national roads; a collaborative working team of JICA experts from CADEFEST and CDRS projects have analyzing the data; a solid figure will be reported in the next monitoring period.

1-5 Changes of Risks and Actions for Mitigation

1-6 Progress of Actions undertaken by JICA

- JICA Timor-Leste shared important information and documents with JICA Expert Team.
- JICA Timor-Leste assisted visa acquisition process for JICA Expert Team.

1-7 Progress of Actions undertaken by Gov. of Timor-Leste

- DRBFC shared necessary information and documents with JICA Expert Team.
- DRBFC has prepared the drawings of road and bridge maintenance based on the road inspection.

1-8 Progress of Environmental and Social Considerations (if applicable)

- No activities for the progress of Environmental and Social Considerations are undertaken.
- 1-9 Progress of Considerations on Gender/Peace Building/Poverty Reduction (if applicable)
- Not Applicable so far.

1-10 Other remarkable/considerable issues related/affect to the project (such as other JICA's projects, activities of counterparts, other donors, private sectors, NGOs etc.)

• No other issues are confirmed so far.

2. Delay of Work Schedule and/or Problems (if any)

• Based on the PDM, the project activities have been implemented as planned.

3. Modification of the Project Implementation Plan

3-1 PO

• PO was modified after the 4th JCC. The latest version was ver.6.

3-2 Other modifications on detailed implementation plan

General issue:

As a result of the parliamentary election, a regime has change occurred. Due to political factors, the budget plan for 2018 was rejected. Under the influence of delayed budget allocation, implementation of activities 1.2, 1.3, 1.4, 1.6, 2.2, 2.3 and 3.5 has been delayed.

- <u>Countermeasures have been taken by JICA Expert Team:</u>
 - In the coordination meeting between CDRS project and NDRBFC, CDRS Deputy Team Leader requested the Director of NDRBFC to prioritize allocation of the budget for the projects selected for case studies.
 - CDRS team leader suggested to NDBRFC that the 2018 inspection work should be carried out by collaboration between relevant staff of Department of Project and Department of Maintenance in order to increase work efficiency with a limited budget.

• Modifications of implementation plan and project period:

A 9-month extension of project term was approved at the 4th JCC. Those delayed activities mentioned above will be conducted during extension period.

4. Preparation of Gov. of Timor-Leste toward after completion of the Project

• The Gov. of Timor-Leste tries to secure the budget for road maintenance so that the capacity enhancement of NDRBFC for road maintenance which is the Project Purpose will be sustainable and contribute to the achievement of Overall Goal.

< II. Project Monitoring Sheet I & II >

• Project Monitoring Sheet I & II are attached as PM Form I and II.

Project Monitoring Sheet I (Revision of Project Design Matrix)

Project Title: The Project for Capacity Development of Road Services in Timor-Leste (CDRS)

Implementing Agency: Ministry of Public Works, Transport and Communications

Target Group: Officials of Direstorate of Road, Bridge and Flood Control (DRBFC)

Period of Project: (Three (3) years)					
Project Site: Whole Timor-Leste	Model Site:				
Narrative Summary	Objectively Verifiable Indicators	Means of Verification	Important Assumption	Achievement	Remarks
Overall Goal The maintenance conditions of major roads are improved in TL.	OG1 More than 60% of major national roads is in good condition.	Periodic Road Inspection	red at ed	Indicator has been set up and approved in 2nd JCC on February 2017.	
Project Purpose Capacity of DRBFC for maintenance of major roads in Total length of maintained national roads become the whole country is enhanced. 400km.	Total length of maintained national roads become 400km.	Periodic Road Inspection	Enough number of DRBFC staff in Indicator has been set up and the HQs and regional offices is approved in 2nd JCC on ensured as planned. February 2017. Budget for road maintenance and management is ensured.	Indicator has been set up and approved in 2nd JCC on February 2017.	
distribution and distribution and BFC construction ince and rehabilitation is improved through case ty.	 The second database is utilized for preparing budget report maintenance are distributed. 1-2 Improved road database is utilized for preparing Monitoring Sheet the annual work plan of road maintenance. 2-1. At least 3 case studies for construction and 3 case Monitoring Sheet studies for design are conducted (Totally 6 case studies). 2-2. More than 60 % of trainees pass the achievement Achievement test test for construction supervision and design. 3. Technical guideline of investigation and design for store to repared. 	Monitoring Sheet Monitoring Sheet Achievement test Technical guideline prepared	The trained DRBFC personnel continue to work for the Project (They do not quit the Project) Unforeseen natural disasters will not occur which may destroy construction works under case studies.	indicator has been set up and approved in 2nd JCC on February 2017. 2-1. 1 site for construction and 3 sites for design are selected.	
increand sobe protected.					

Version 3 Dated 31st August, 2017

Activities	Inputs		Pre-Conditions
	е	The Timor-Leste Side	
 To review existing management structure condition of maintenance and rehabilitation for major roads. To conduct periodic/routine inspection. 	 Dispatch of the Japanese experts Short-term experts: Team leader / Road maintenance 1 Deputy team leader / Road maintenance 2 	 Assignment of C/Ps Project Director Project Manager DRBFC Staff 	DRBFC's budget necessary for the Project is allocated by TL government.
 To update the database based on the inspection result and repair/rehabilitation works of roads and bridges. 	 Road construction supervision Quality control / Road repair Disaster restoration Road design / Project coordinator Structure design 	 Assignment of Trainees In accordance of necessity Facilities and Equipment 	<issues and="" countermesures=""></issues>
 1.4 To formulate maintenance and repair/rehabilitation plans for next cycle. 5.To implement emergency inspections and repair/rehabilitation works when necessity arises. 		 Frugeviolute Equipment and tools 4. Recurrent costs Expenses for equipment maintenance Spare parts 	
 To undertake appropriate road maintenance/rehabilitation works by following annual work and budget plans which reflect priorities with in the limited budget. 	 Training in Japan accordance with necessity of activities 	 Transportation fees of C/Ps and trainees Expenses for contract-out of works Necessary expenditures for case studies C/Ps' wages and allowances 	
 T to propose appropriate framework of road maintenance and rehabilitation for major roads. 			
 To identify typical rehabilitation and repair works of major roads in the whole country as case studies. 			
2.2 To conduct the case studies for the planning, design and construction supervision of the project.			
2.3 To propose preferable structures for construction management for repair/rehabilitation and maintenance works through case studies.			
 To review existing technical documents for road maintenance and rehabilitation. 2. To review and identify factors of failure from past examples of damaged rehabilitation and construction works. 			
 3.10 acquire necessary knowledges of civil engineering for design through classroom lectures and case studies. 			
 3.4 To prepare the technical guideline of investigation and design. 			
3.5 To reflect the lessons learned from case studies to the technical guideline.			
 To disseminate the technical guideline for concerned parties. 			

Project Monitoring Sheet II (Revision of Plan of Operation)

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 <td xpert . Team Leader/Road Maintenance 1 /Mr. Hisashi MUTO /Mr. Hisashi MUTO Deputy Team Leader/Road Maintenance 2 /Mr. Makoto MATSUURA Mr. Mitsuhide Saito was dispatched as successor of Mr arch 2017, Mr. Matsuura resigned. Deputy Team Leader/Road Maintenance 2 /Mr. Mitsuhide SAITO Mr. Mitsuhide Saito replaced Mr. Matsuura as Deput Road Construction Supervision /Mr. Johji KOIZUMI Quality Control/Road Rep /Mr. Sueo HIROSE Disaster Restoration /Mr. Shutaro SAKANAKA Disaster Restoration 2 /Mr. Kazuharu KOISHIKAWA his position has been created to assist drafting gu Ir. Koishikawa was assigned for this position in March 201 /Mr. Kazunaru KOSHIKAWA Road Design/Project Coordinator /Mr. Yoshiyuki AKAGAWA Road Design/Project Coordinator /Mr. Nicholas BROOKER-JONES fr. Brooker-Jones was dispatched as successor of Mr July 2017, Mr. Akagaw replaced Mr. Akagawa as Projec Structure Design /Mr. Kenji MINEGISHI Database /Mr. Takashi SAITO Landslide <u>/Mr. Masahiko HAYASHI</u> Topographical Analysis <u>/Mr. Sohshi MIKAMI</u> Activity on Landslid analysis was Activity on Landslid analysis was Evaluation/Monitoring Ms. Nao TSUJIMURA sktop comp linometer assembly se equipment chased to more rehole casing kenbo assembly raining in Japan -country/Third country Training
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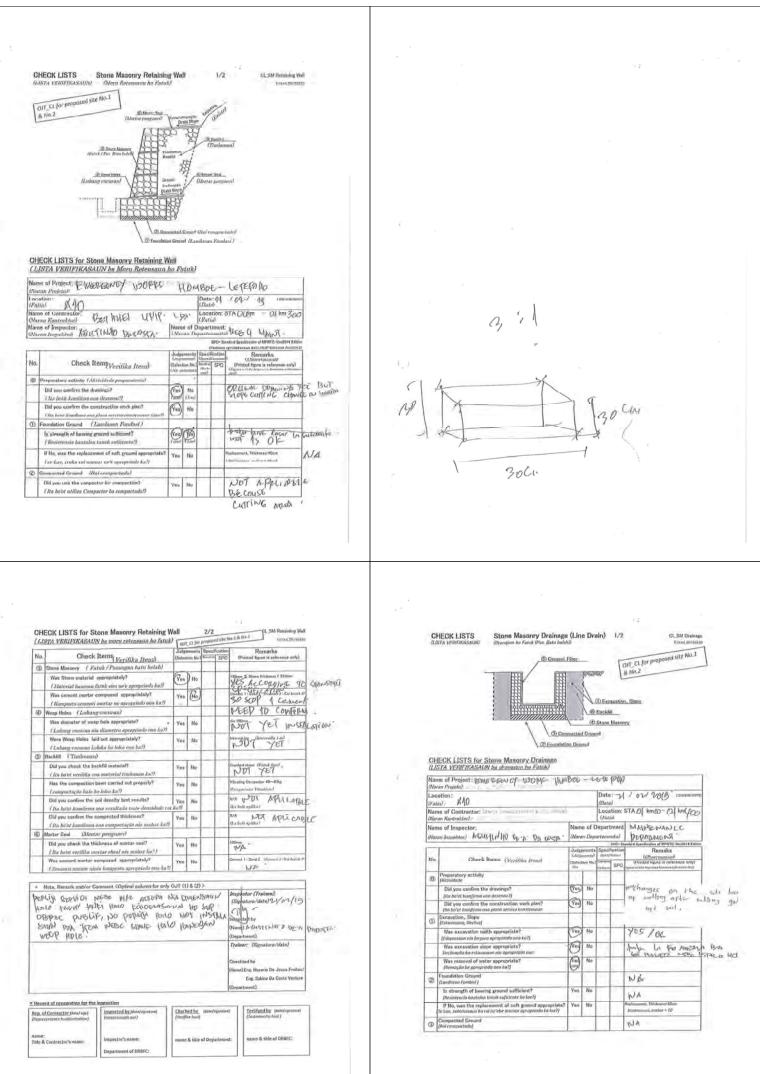
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 3.1 To review existing technical documents for ror maintenance and rehabilitation 3.2 To review and identify factors of failure from past examples of damaged rehabilitation and construction works. JICA expert team reviewed existing technical documents, such as specifications and drawings from past projects. JICA expert team JICA expert team identified factors affecting structural failu / road damage using baseline survey results and road inspection results JICA expert tean 3.3 To acquire necessary knowledges of civil engineering for design through classroom lecture and case studies m lectures for civil engineering design schedule. peat lecture about operation of total station was provided. 3.4 To prepare the technical guideline of investigation and design aft guidelines for slope protection, bridge substructure p d culvert design have been prepared. JICA expert team NDRBFC Dept. Project, chief of planning section a JICA expert team pert team supported C/P using the cul 3.5 To reflect the lessons learned from ca studies to the technical guideline cks for whether prepared guid and JICA expert team and C/P 3.6 To disseminate the technical guid sts were disseminated to the icipal administrations and higher lonitoring Plan Issue
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OJT using Checklist in Humboe-Letefoho on 21 February 2019



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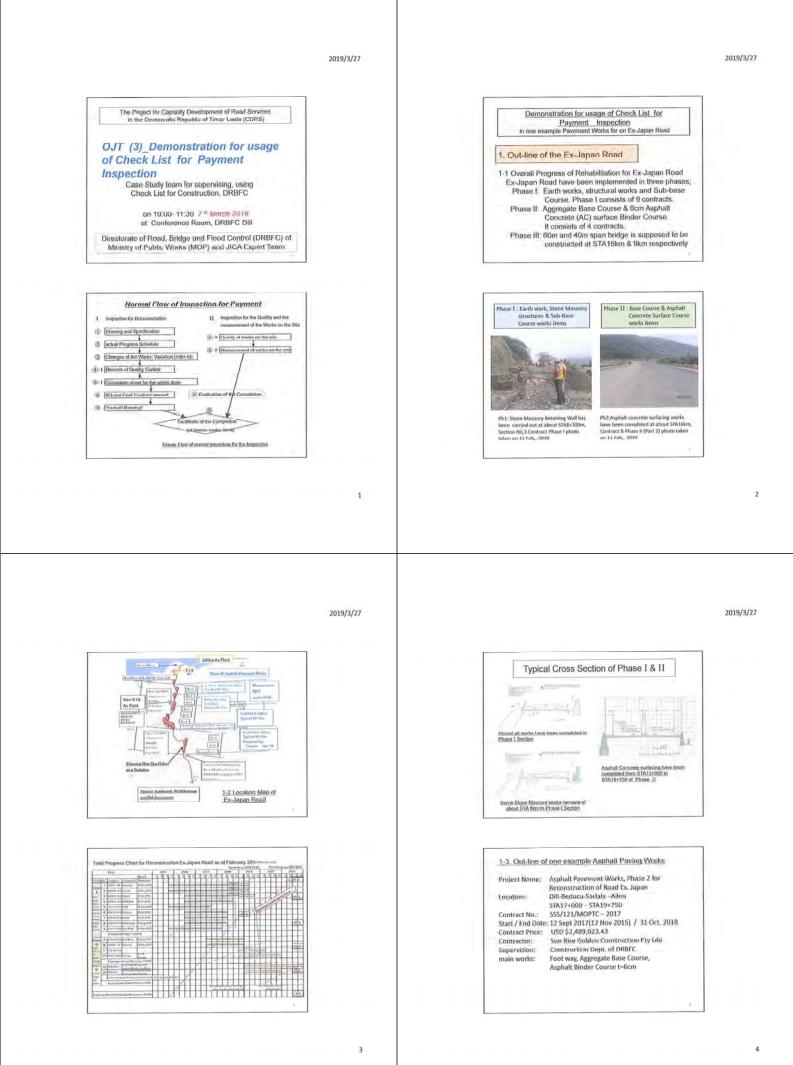
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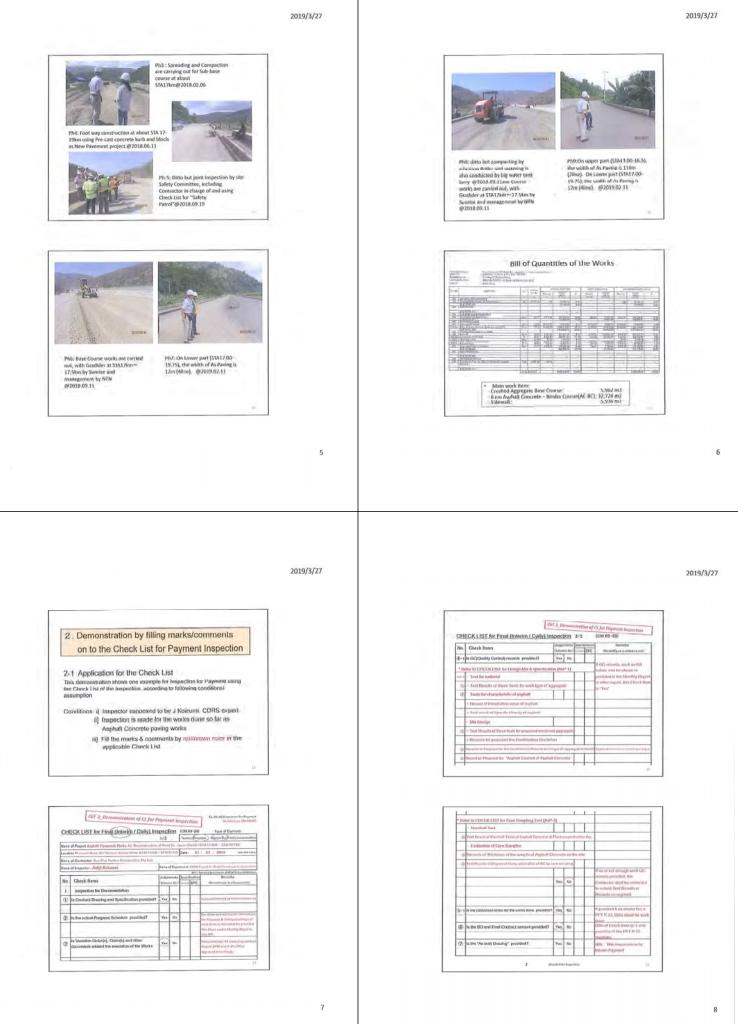
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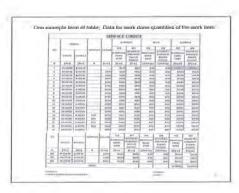
OJT_ Demonstration for usage of Checklist for payment inspection on 7 Mach 2019





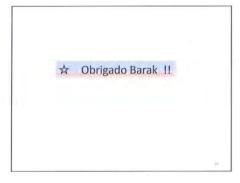
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References & Questionnaire 1) Please fill or marks on to the delivered "OJT3_Check List of Inspection for Payment" by yourself like a demonstration, referring to the Check List for Asphalt Pavement 2) Please write any comments and opinion regarding to "Check List for Construction", process of Inspection for work done on to the last column of sample Check List titled: " IV. Note, Remark and/or Comment References: #1: Check List of Inspection for Payment (Questionnaire, OJT-3) #2: Check List for Asphalt Pavement (OJT-3)



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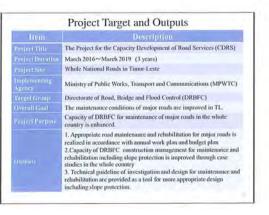
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Collaborative workshop on culvert planning/Design check on 14 March 2019

Â * REPÚBLICA DEMOCRATICA DE TIMOR-LESTE MINISTÉRIO DAS OBRASI PÚBLICAS DIRECÇÃO GERAL DAS DBINAS PÚBLICAS COADACIÓNEL DE EMINADA, PONTIN E CONTROLO DE CHEMA ONE-DAY TRAINING WORKSHOP ON CULVERT DESIGN / PLANNING Topic / Activity Speaks Tune 03:30 - 10:00 Ny Hersel Mat Ny Augustus Ar Ny Juda M. Gr 10.00-10.00 10:20-11:00 15:00-11:15 19:00 - 13:15 (1:15 - 12:15 (2:15 - 13:00 13:00 - 14:00 Mr Calu also F. Kes us. Dert of High 15 Mars an, Dopt of Projects & Ad Fragerilation, Case Shally of Sa 12-05-12-05 Cyser Frimen hat the Interiors, CORSI 14:45 - 15:15 16:15 - 15:30 Rap-up and Quiz: Lessons Learnt Al participants HID-SP & DRBF

14/03/2019





Culvert Workshop: CDRS Greeting

Culvert Workshop: Case Study

14/03/2019

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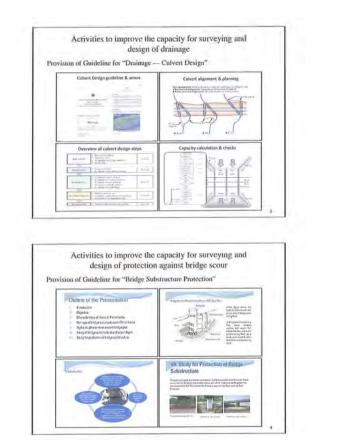
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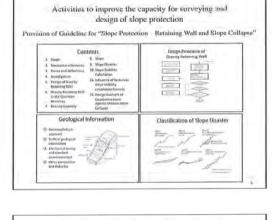
Culvert Workshop: CDRS Greeting

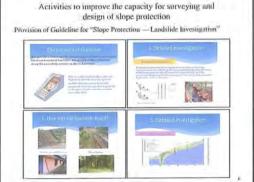
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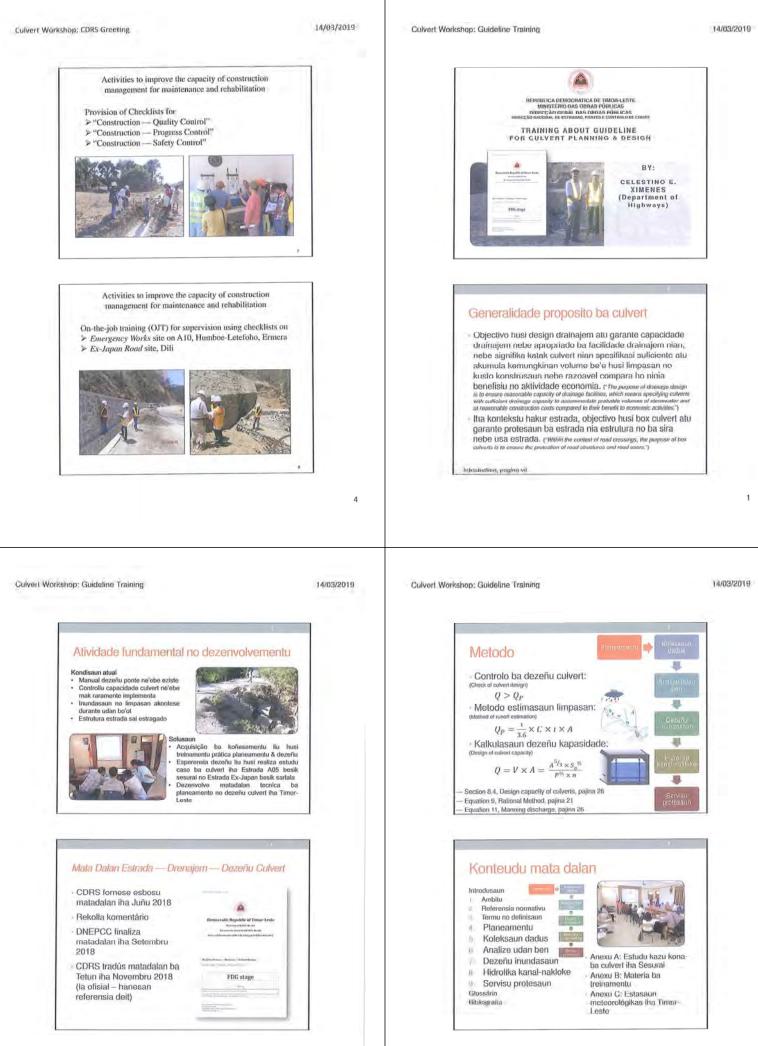
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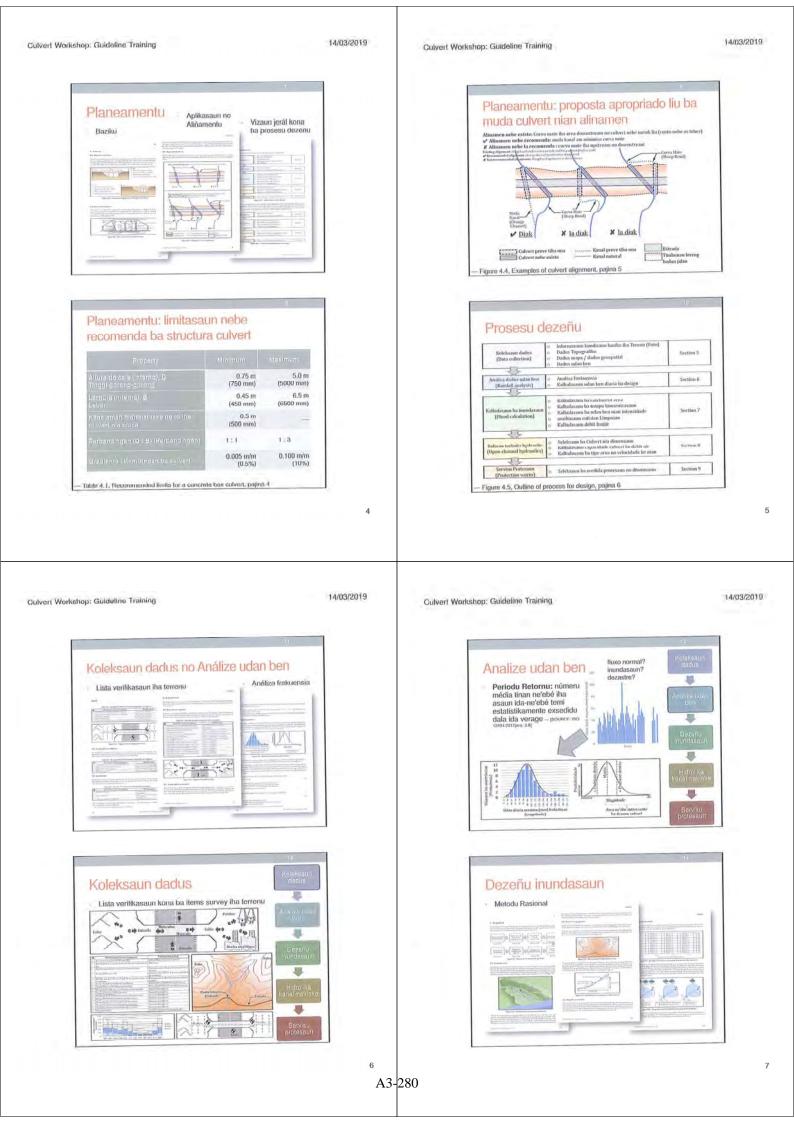
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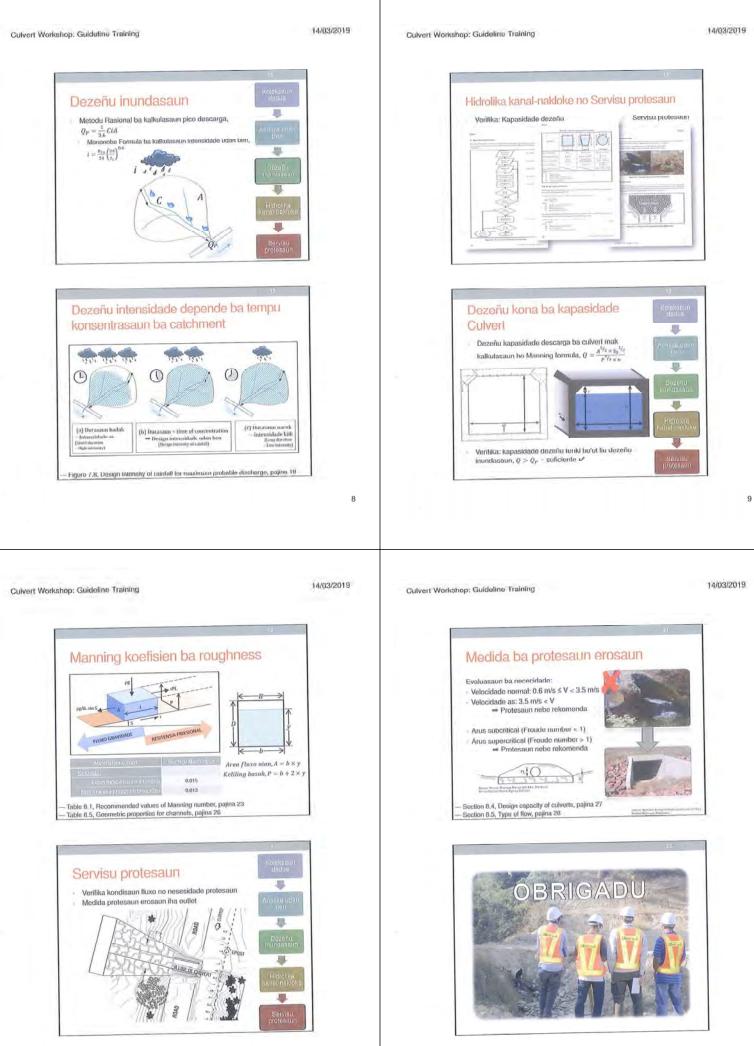












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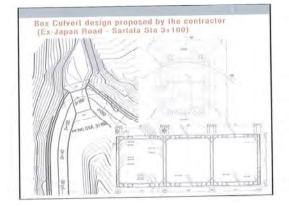
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Ex-Japan Culvert

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BY: MANUEL SOARES (Department of Projects & Administration) 14/03/2019

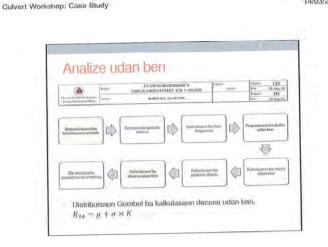
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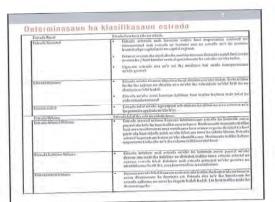




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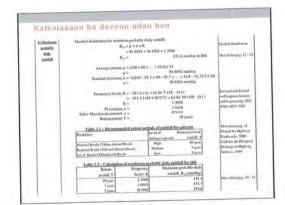
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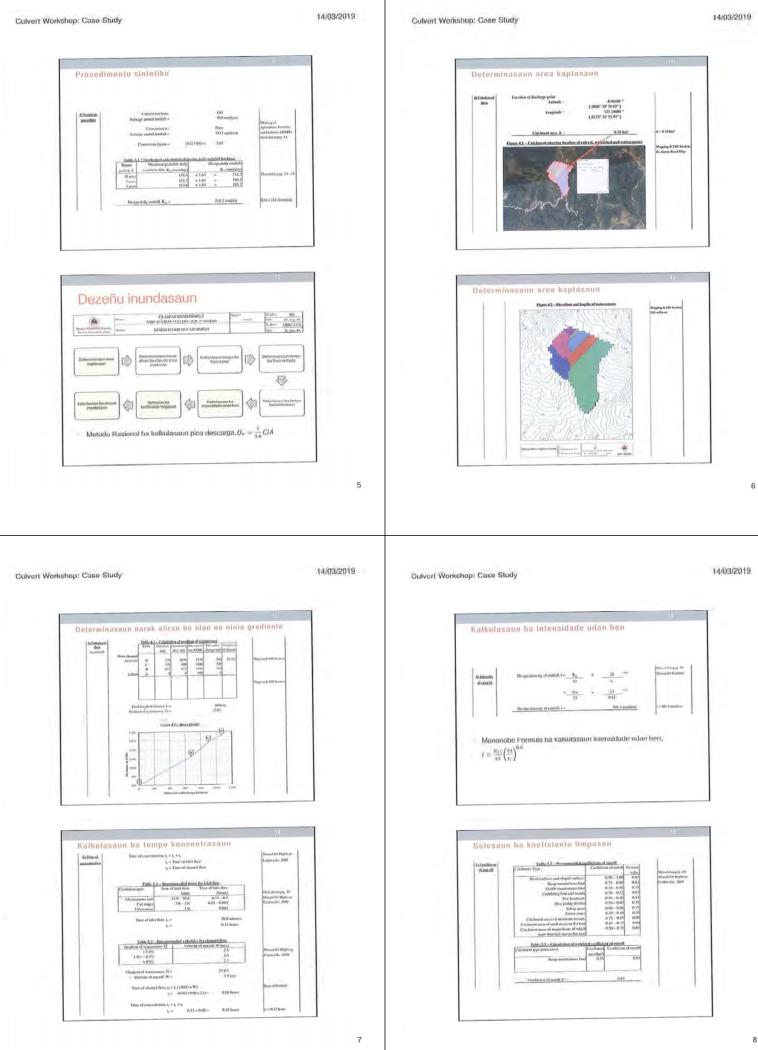
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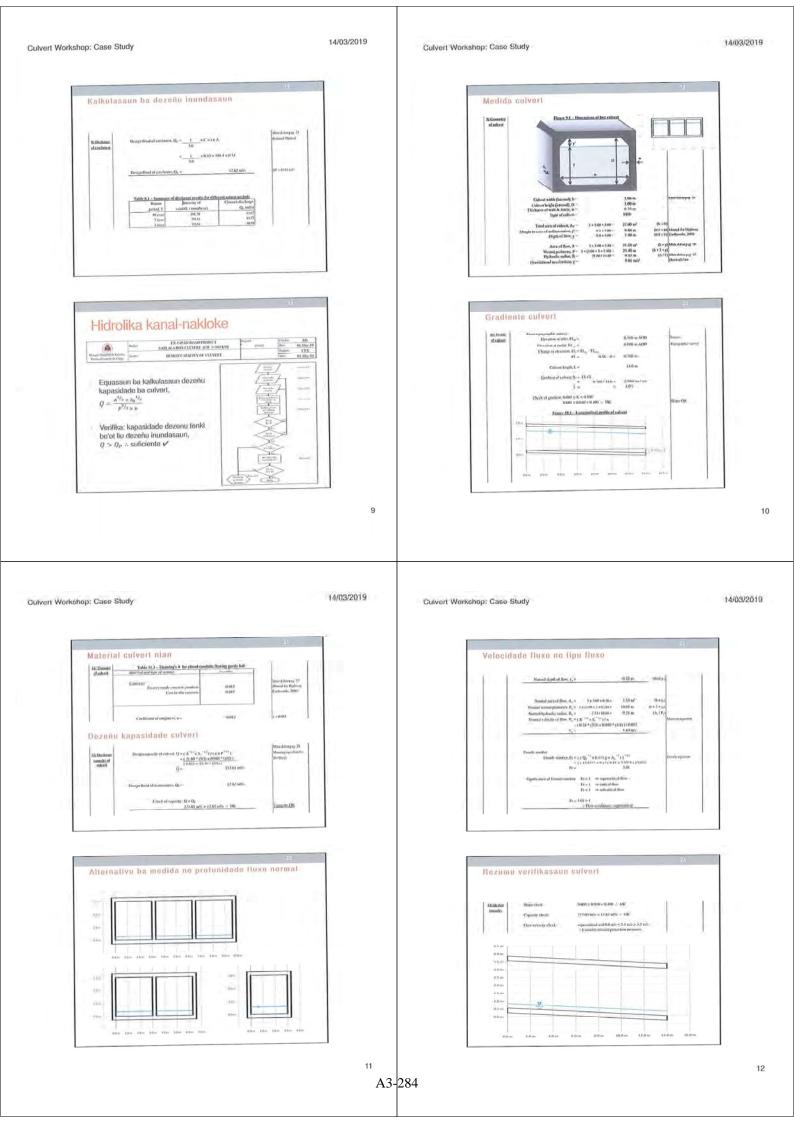
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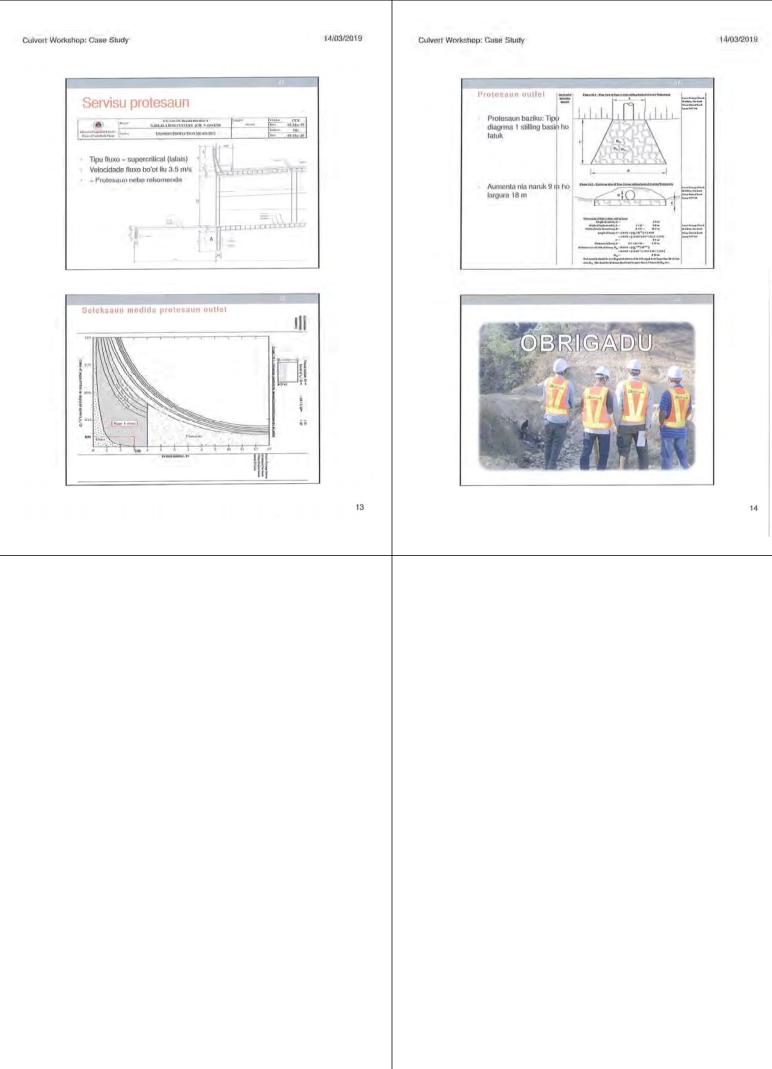




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Attachment 4

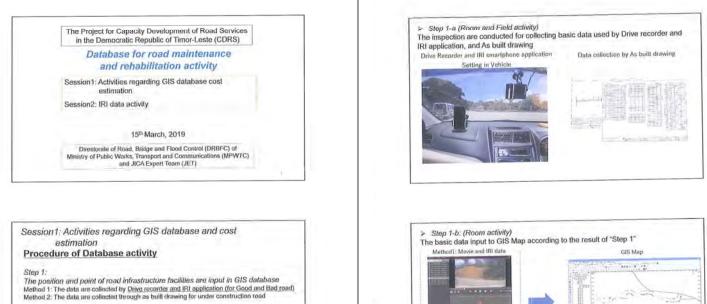
CDRS workshop for Guideline and Checklist on 15 March 2019

3/27/2019

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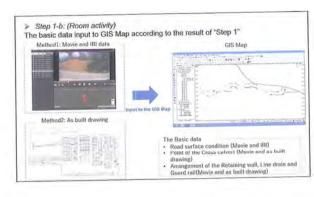
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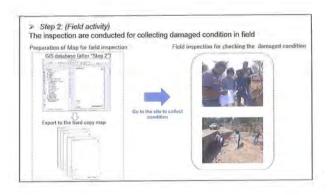
Step2: The inspection are conducted for collecting damaged condition

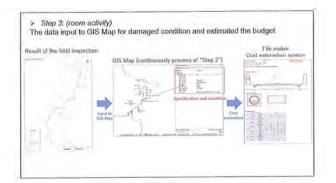
Step3: The damaged condition data are input to GIS and estimated the budget

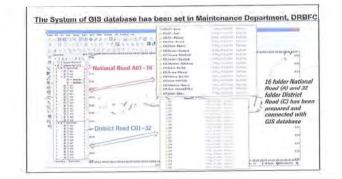


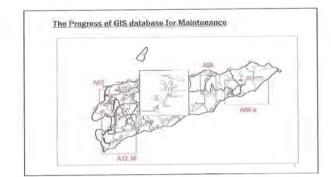


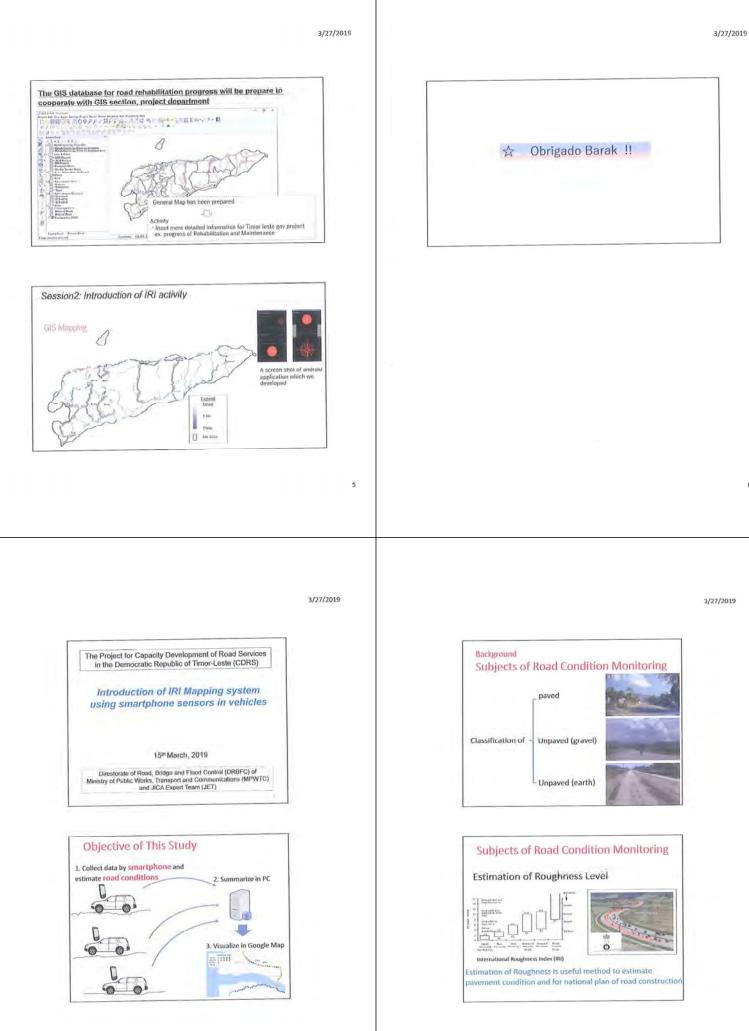
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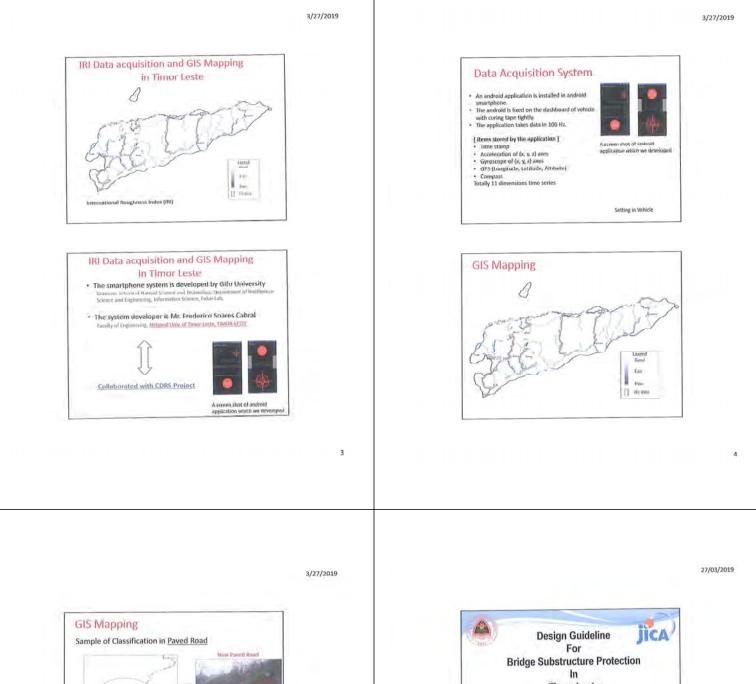








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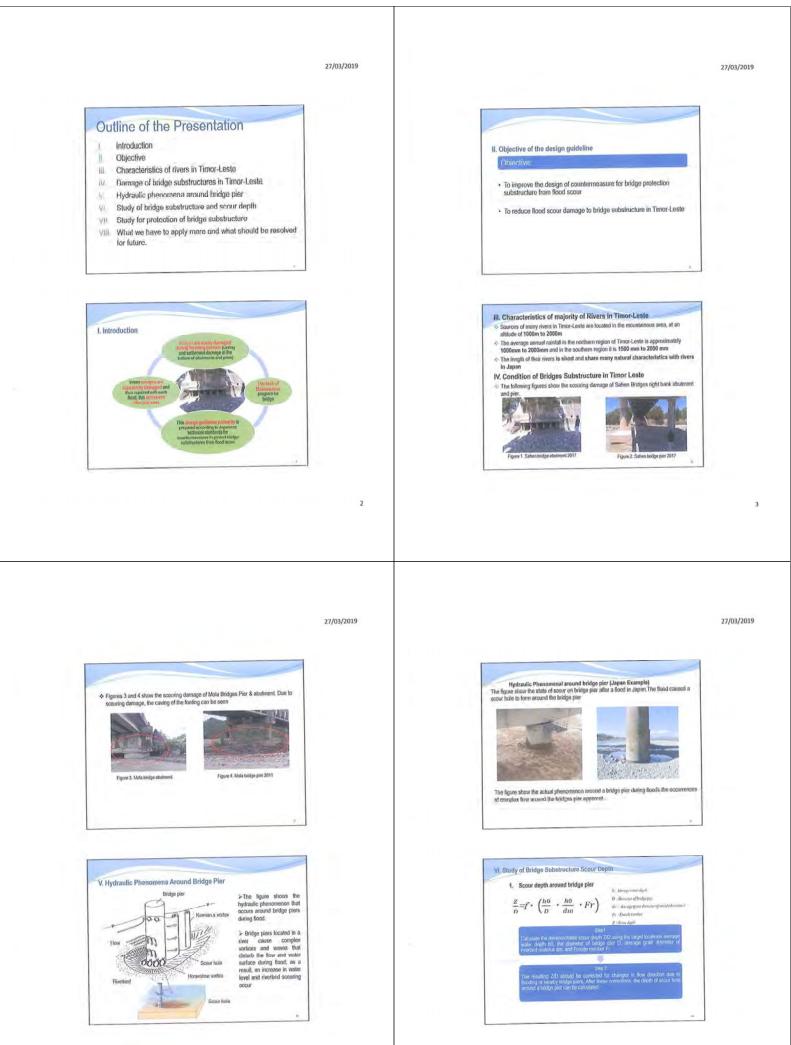


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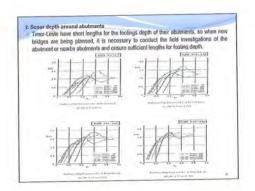


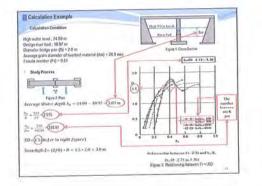


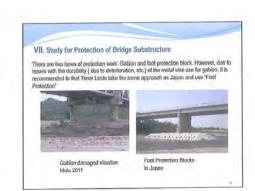
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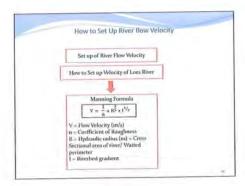
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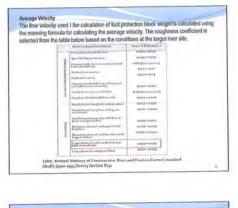
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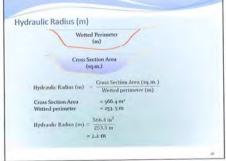


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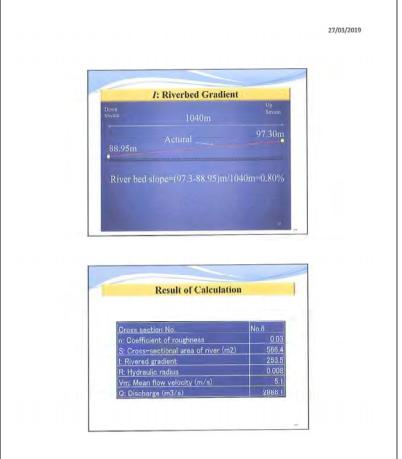




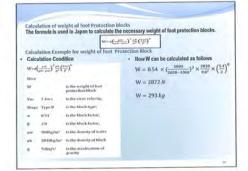


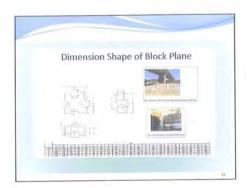


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27/03/2019

VII. What we have to apply more and what should be resolved for future.

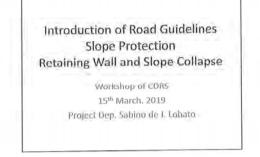
What we can do at the moment is that We prepared design and cost estimate of budget for project implementation. Howev ho formula and the slandraid as guideline to resolve bridge substructure protection, therefore, the cost estimate were not included bridge protection design.

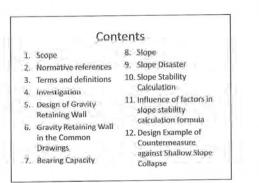
Therefore detailed survey, detail design, datail estimate budget for bridge protection can be provided based on the guideline so we have to apply formula on each project. And the monitoring is algorithment for not only quality control but also feedback for design checking in maintenance department.

However it is still insufficient that requirement of engineering justification from decision maker. Hence, it maybe no budget for monitoring at the site and no arrangement for facility

maxes: relace, it mays an outoget on maximum g at the same and no arrengement for text for engineers. — Therefere we propose that decision maker should consider further engineering instillical and training apportunity in DRBFC. — Regarding formwork of foot protection like Comoro No. 3 Bridge, it is needed to obtain formwork with its revally, so DRBFC should keep one set of the form work at least.







12

A3-292

27/03/2019

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Annex

Annex A How to Use the Total Station Annex B How to Use the Dokenbo Annex C Excel Worksheets for Stability Calculation of Gravity Retaining Wall Annex D Excel Worksheets for Slope Stability Calculation

Annex E Design Example of Catch Wall

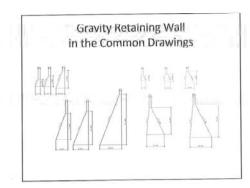
Investigation of Ground Shape

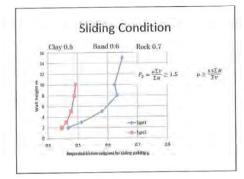
· Design must stand on actual surveyed cross section at least. Total Station makes cross section survey

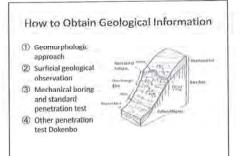
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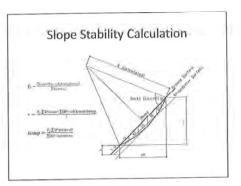


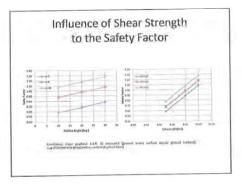


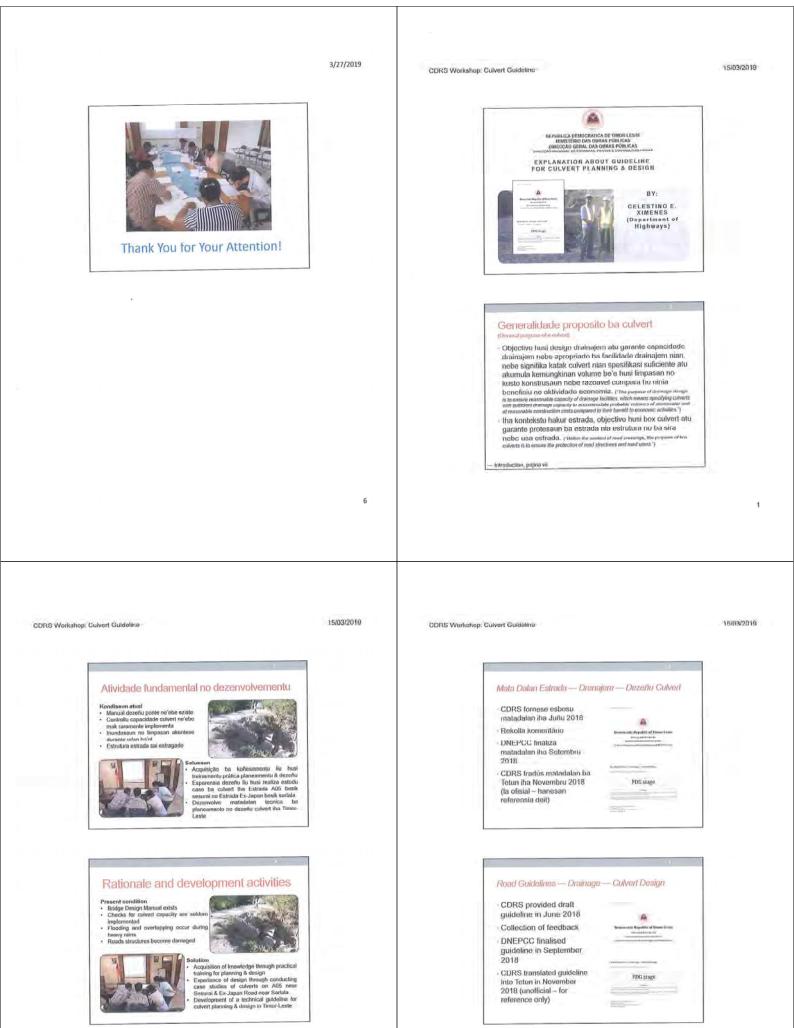


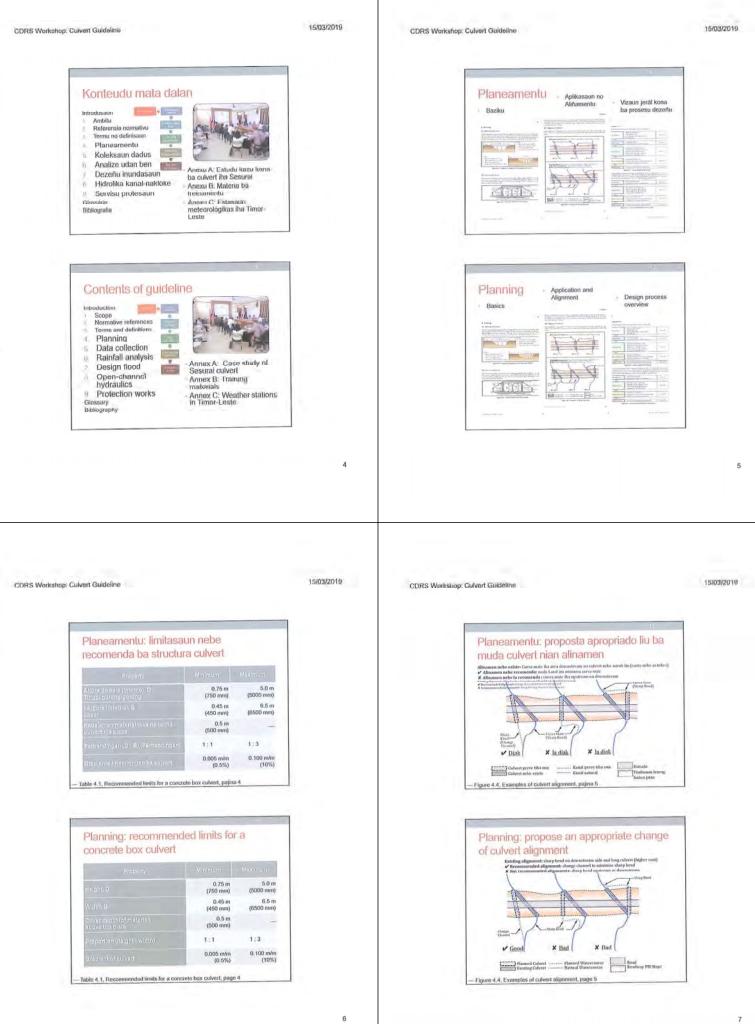


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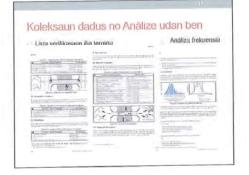
CDRS Workshop: Culvert Guideline

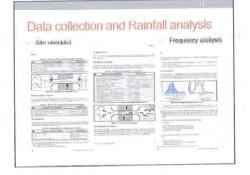
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CDRS Workshop: Culvert Guideline

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CDRS Workshop: Culvert Guideline

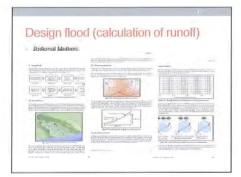
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CDR5 Workshop: Culvert Guideline

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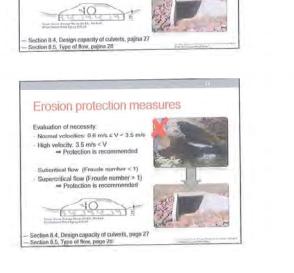
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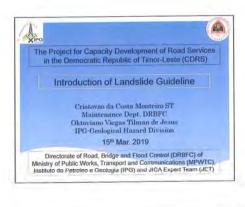


Medida ba protesaun erosaun

Evaluaisaun ba nececidade: - Velocidade normal: 0.6 m/s = V < 3.5 m/s - Velocidade as: 3.5 m/s < V = Protesaun nebe rekomenda - Arus suberrilical (Froude number < 1) - Arus superrilical (Froude number > 1) = Protesaun nebe rekomenda

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3/27/2019

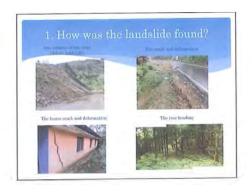


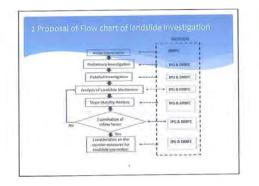
ontents of Guideline

The guideline introduces the general approach how to investigate the mass movement landslide. The process of the contents is along the case study activity on Aituto Landslide



This is a slide in which the surface of rupture is curved concavely upward and the slide movement is roughly rotational about an axis that is parallel to the ground surface and transverse across the slide.

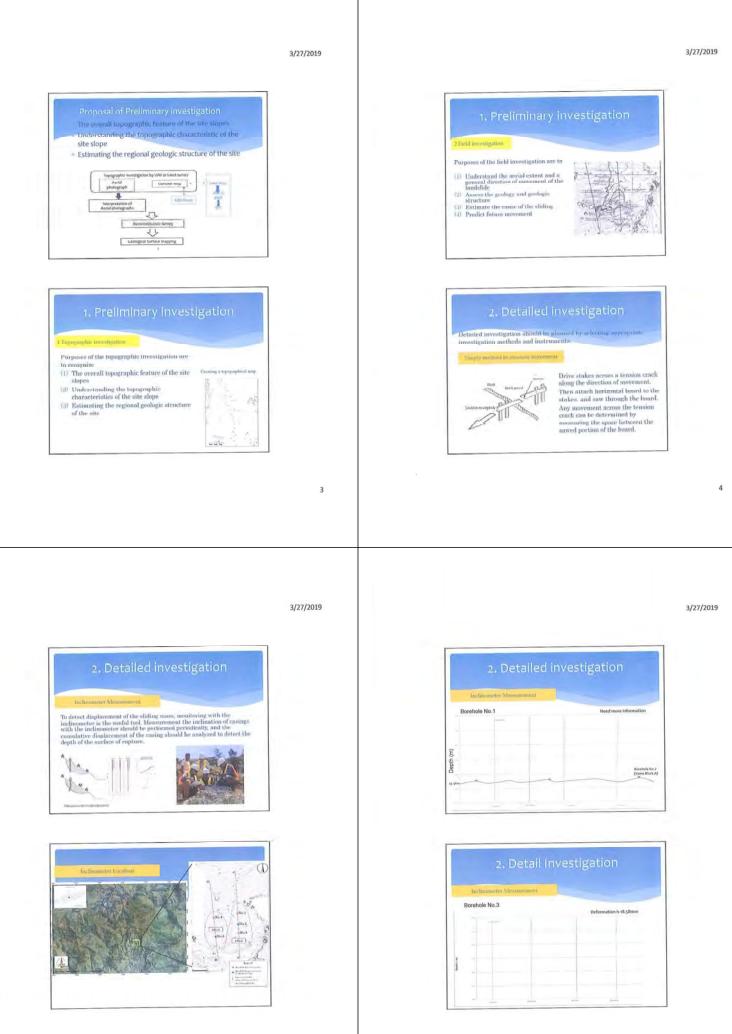


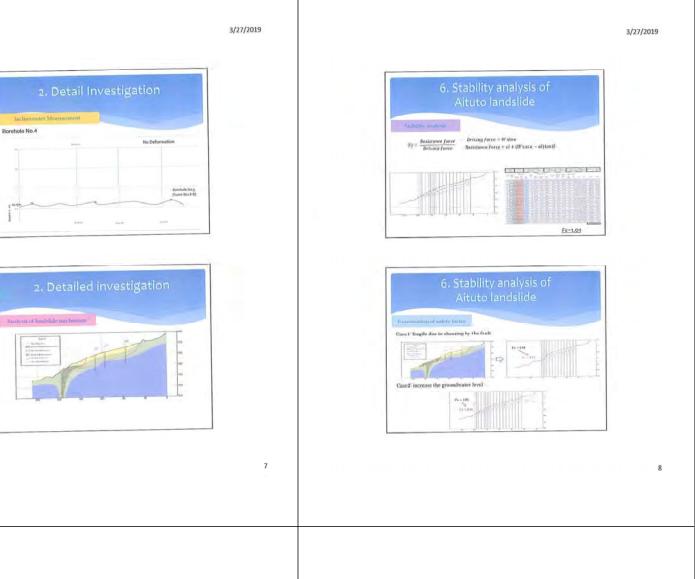


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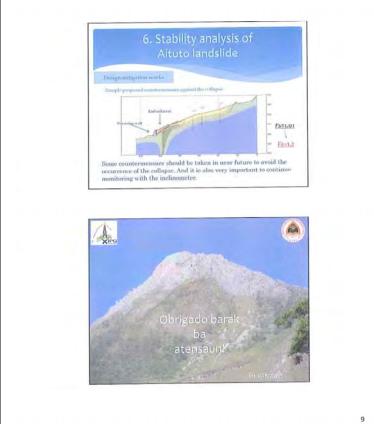
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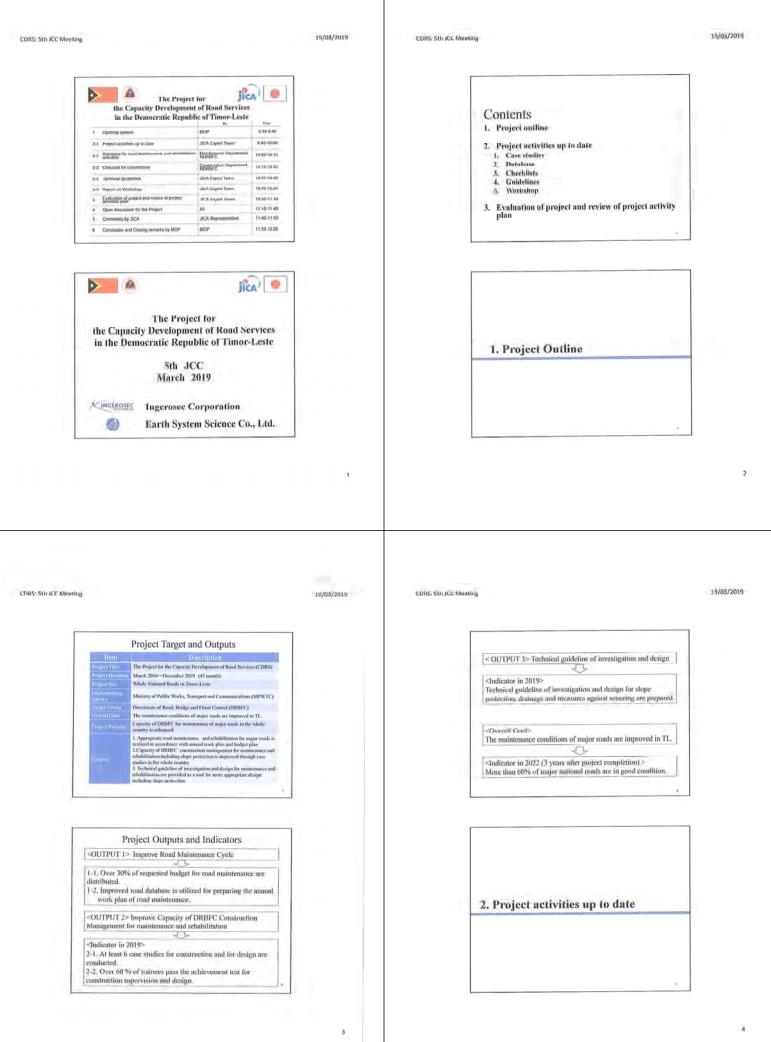






Attachment 5

5th Joint Coordinating Committee on the project for the Capacity Development of Road Services (CDRS) on 19 March 2019





19/03/2019

5

CDRS: 5th JCC Meeting

CDRS: 5th JCC Meeting



CDR5: 5th ICC Meeting

 Image: sector

Case study sites

Case study activities



CDRS: 5th JCC Meeting 10/03/#019





Activities to improve the capacity for surveying and design of drainage

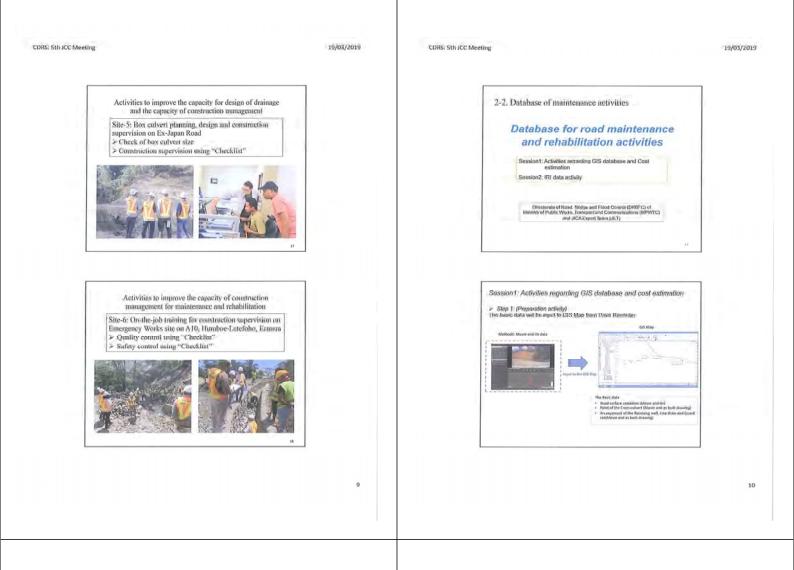


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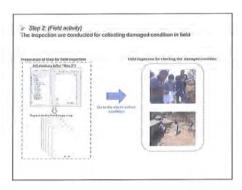
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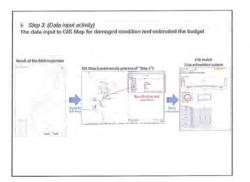
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19/03/2019



CDRS: Sth JCC Meeting 19/68/2019





CDRS: 5th ICC Meeting

19/01/2019



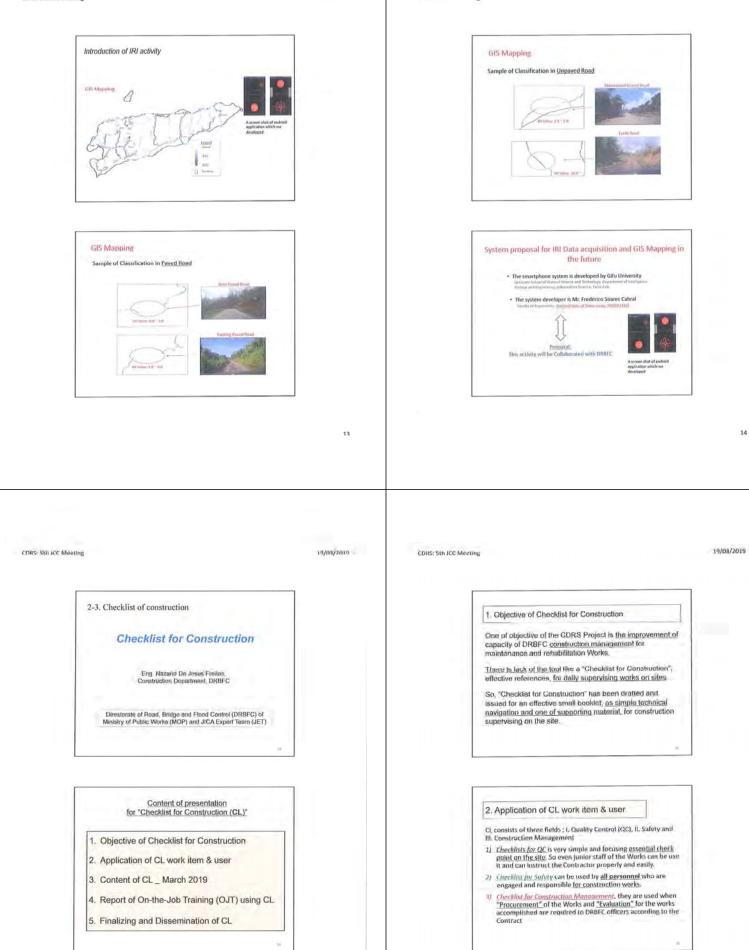


CDR5: 5th JCC Meeting

19/03/2019

CDR5: 5th ICC Meeting

19/03/2019



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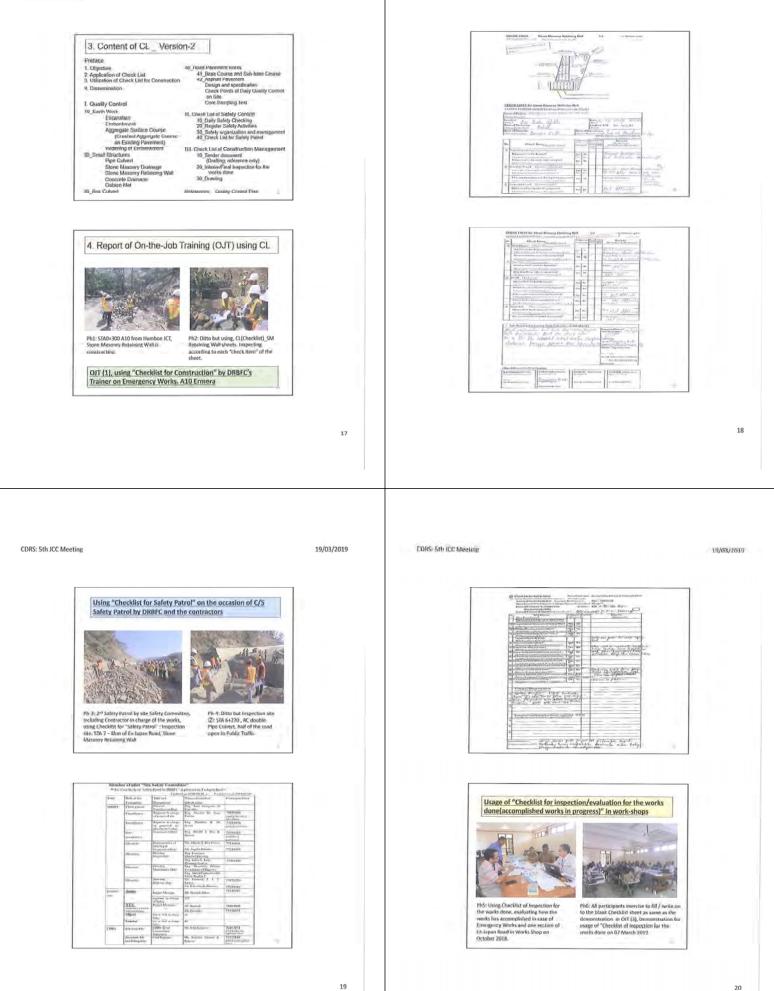
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CDRS: 5th JCC Meeting

19/03/2019

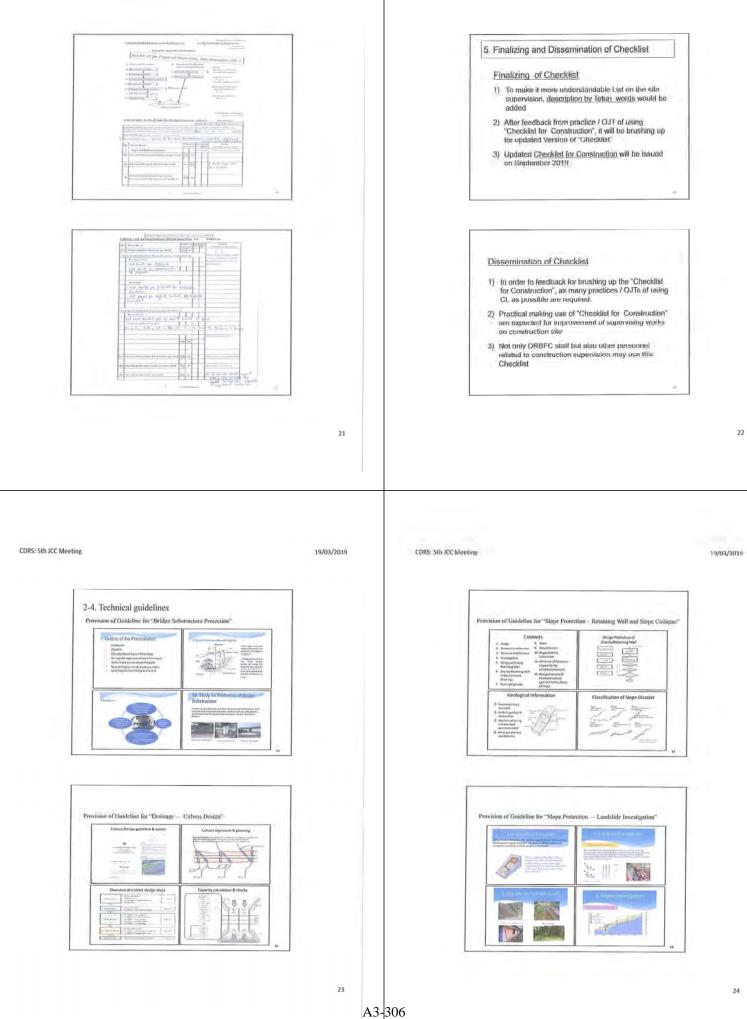
CDRS: 5th JCC Meeting

19/03/2019



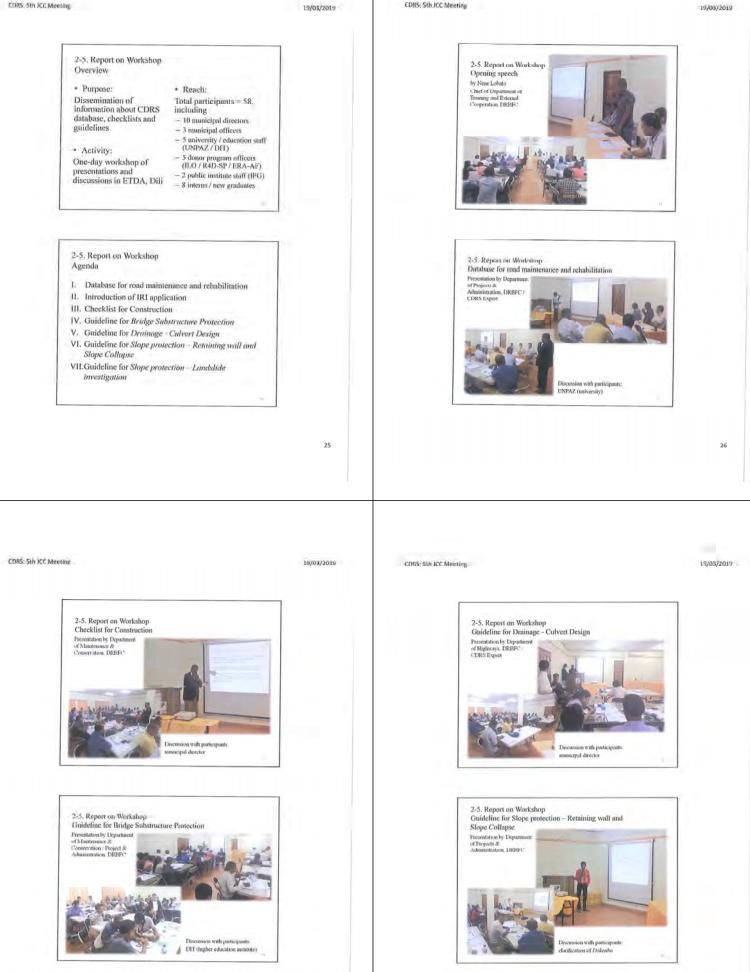
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CORS: 5th JCC Meeting

19/03/2019

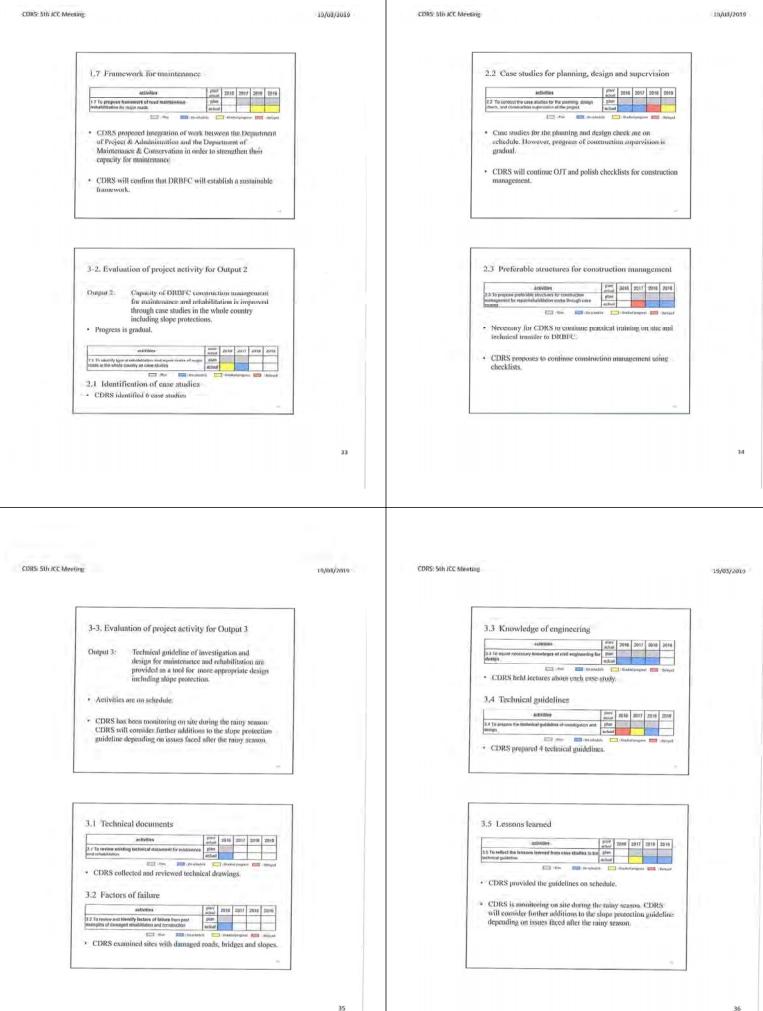


27

A3-307

CDRS: 5th JCC Meeting CORS: 5th JCC Meeting 19/03/2019 19/03/2019 3-1. Evaluation of project activity for Output 1 2-5. Report on Workshop Guideline for Slope protection - Landslide investigation Presentation by Geological Hazard Devision, Instituto do Petroleo e Geologia (IPG) Appropriate road maintenance and rehabilitation for major roads is realized in accordance with annual work plan and Output 1: annual budget plan · Progress is gradual. activities 1516 plan 1 1 To review exis ing management st n na e 1.1 Management structure and maintenance conditions Dis ath pa · Completed: DRBFC agreed to use GIS database, ticipant unicipal officer 1.2 Periodic / routine inspections activities 1.2 To conduct the periodic/routine Inspection 3. Evaluation of project and review of 120.56 122 project activities plan · Site inspection of A03,A04,A06,A08,A11,A12,A16 173 km * Site inspection using drive recorder of A01, A02, A03, A04, A05, A06, A07, A08, A09, A11, A12,A13,A14 1419 km Not enough to practical training on site
 July 2019 30 29 19/03/2019 CORS: 5th JCC Meeting 19/03/2015 CORS 500 JCC Meeting 1.5 Emergency inspections 1.3 Database updates activities. activities 2017 2016 2019 1.5 To implement emergency inspections an repurce arbitration works when necessity a 1.3 To update the database based on the inspection result and repair/celabilitation works of roads and tridees plan 100 100 · CDRS supported DRBFC works on A03, Loes river (scouring, · DRBFC has completed update of 173 km of national roads in the database. large sandbag) and Jakarta II emergency work - DRBFC plans to input the inspection results for 1171 km · In 2019, CDRS plans to support emergency work when the · DRBFC will continue to input the inspection results and necessity arises. update the database. CDRS will facilitate cooperation between the Department of Project & Administration and the Department of Maintenance & Conservation. 1.4 Maintenance plans 1.6 Annual work and budget plans 2019 1.6 To undertake appropriate road maintenance/ stratitution works to fellowing annual work and budge! 1.4 To formulate maitenance and repain/rehabilited plan for rest syste Slowing annual w Ges within the Tro (CC) - Pa E.J. (8) in the · DRBFC prepared drafts of 5-year and annual plans. DRBFC completed process of result inspection to request budget with CDRS assistance. CDRS is reviewing the plans regarding appropriateness and priority. CDRS will then advise DRBFC about updating these * DRBFC construction on site and update of database are gradually progressing. plans. · It is necessary for DRBFC to plan for the next cycle

A3-308



CONS: 5th JCC Meeting

19/03/2019

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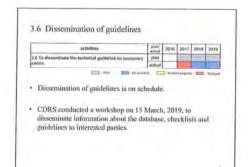
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Thank you for your attention Obrigadu Barak !!

19/03/2019

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JICA O



3-4. Other

- Activity schedule for CDRS assistance
- As necessary, CDRS will consider further additions to the slope protection guideline depending on issues faced after the rainy season.
- > CDRS will continue to update the database.
- CDRS will continue to utilize the checklists on site.
 CDRS will conduct a training workshop about the
- database and checklists in August 2019.
- CDRS will hold the 6th JCC meeting in September 2019.

Minutes of the 5th Joint Coordinating Committee (ICC) For

The Project for the Capacity Development of Road Services in the Democratic Republic of Timor-Leste

The 5th Joint Coordinating Committee for the Project for the Capacity Development of Road Services in the Democratic Republic of Timor-Leste (hereinafter referred to as "the Project") was held on 19th March, 2019, under the chairmanship of Mr. Jaeo M. Ganna de Sousa, Director for DRBFC, Ministry of Public Works.

The chairman and members of the JCC have agreed to make these Minutes of Meeting and the overall work plan of the Project in 2019 based on the mutual understandings reached through the discussion, as attached hereto.

Dili, 21 March 2019

Mr. Hisashi MUTO

Team Leader The Project for the Capacity Development of Road Services in the Democratic Republic of Timor-Leste

Mr. Kur Hernhni Frontas Guterres, Director General for Public Work, Ministry of Public Works in the Democratic Republic of Timor-Leste

THE ATTACHED DOCUMENT

The 5th JCC for the Project was held on 19th March, 2019, at the conference room of the Director General for Public Works. The JCC consisted of the 6 agenda items shown in (1), and the subsequent decisions made are shown in (11).

- (I) The JCC consisted of 6 agenda items:
- 1. Opening of JCC
- 2. Presentation of Project activities up to date
- 3. Evaluation of Project and review of project activities plan
- Open discussion about the Project
 Comments by JICA
- 3, Comments by JICA
- 6. Conclusion and closing remarks

(II) Decisions made:

a The JICA Team reported the works done and reason of delays in the implementation of activities for each outputs during last year. In order to disseminate the project output to the relating parties, the JICA Team proposed a further training activities proposed during the remaining project period for road inspection and database, Check List (CL) training to municipal public works, Guide Line (GL) work shop training to municipal and relating parties.

Timor-Leste side stakeholders agreed to the proposed activities of the project period: moreover, Timor-Leste side stakeholders requested the JICA Team to consider further cooperation to support.

b Member of Municipal Public works expressed the importance of the Design GL and CL for their works, but the training to them is not fully conducted. Therefor they request either JICA team or the Director of DRBFC consider the training to municipal engineers during the period exceeding the JICA's assignment period. JICA Team replay the main target of this project is the capacity development of DRBFC staff for maintenance of National Kond and the assignment of this project is fixed and difficult to expand the period without approval of JICA.

But at the same time The Team understands the necessity of dissemination of GL/CL to Regional Offices of DRBFC which were already discontered and sifted to each municipalities, therefor further training of GL/CL to monicipalities will be conducted during remaining pariod. And during the training to DRBFC staff, Training of Trainer (TOT) was also conducted with using not only English

version but also Tetun version being prepared. Therefor by using this version and the trainers, DRBFC can support to train to the municipal engineers. DRBFC replayed to consider such support to the municipality and request JICA team to prepare Tetun/Indonesia version for final approval.

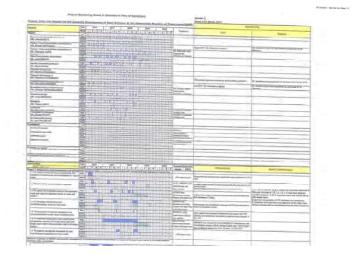
- c Member of Municipal public works request JICA term to prepare and submit the veport of this project including the activities done and outputs. JICA Term answered the project completion report shall be prepared and submit before the final JICE on this September for the acceptance of the report which is including the project activities done and output results. And also the Term will send GL/CL date to all attendants of work shop during 15th March, 2019 and 5th JICE and well.
- d Member of IPG expressed many thanks to the Project including TOT for the sustainability. Training of technical development and monitoring of Land Slide at Manatuto with clase cooperation conducted with IPG and DRBFC.
- e Member of DRBFC request the Team that the GL/CL is very useful therefor official approval by the minister is necessary. JICA Team also request DRBFC to get approval by either the minister or the
- Director General for registration of official document. The Director of DRBFC agreed the request and will conduct the proper action. I JICA made some comments that JICA feel good progress and outputs of the
- project including close comparation with IPG for GL, and also cooperation with UNTL not only for read inspection by IRI but also UNTL research activities and CL is useful for quality, progress and safety control of construction works on site. JICA also pointing that referring to some comments made, remaining some issues shall be identified by next final JCC and also if such issues required JICA's cooperation, plaque prepare official request by this and of August to JICA's
- g DRBFC side requested the Team to continue the strengthening of Trainers for the training of GL/GL and also to continue the cooperation with R4D for the establishment of Data base of road network. DRBFC also requested to JICA further cooperation of the technical transfer project for Disaster Prevention of road network with simple bridge management and also request the master plan study of Dili road development and Peasibility Study of Priority Project. JICA side confirmed such request need more discussion and preparation of

official request to JICA. Appendix:: LAttendant List of 5th JCC

2. Work Plan in 2019

	DNEPCC/Trainiae & COOP	JONG as Service									DNEPCC-Maintenanen Dave	DNIPCC.Mainteeneer Dure							
DNEPCC	-		TPC.Dac	MOP Banera		-				MOP Etmera	DNEPCC-Mai	DNIFCCAN	CDRS-11C+						
Director	Chief of Department	AMIIation/Duty	Director	Director	Road Construction SP	GIS database	Representative Dir.	Interim Director	Chief Tech Advisor	Director	Staff	Staff	Engineer						
-	Nene Lobato	Name	Eugenio sonres	Pedra Alexandre	Johji KOIZUMI	Takashi SAITO	Bendito Belo	Fonsatio A. da C. Reis	Augustus Asare	Sertorio Pereiro	Podra Carga Raul Norouha	Filoniena C.C. de Almeida	Lettetta S. A. Barreto						
chung	Mr/Ms	Mr/Ms	Mr/Ms	Mr/Ms	MITIMIS	Mr/Ms	Mr/Ms	Mr/Ms	Mr/Ms	Mr/Ms	Mr/Ms	Mr/Ms	Mr/Ms	Mr/Ms	Mr/Ms	Mr/Ms	Mr/Ms	Mr/Ms	
	18	No.	10	50	51	55	53	5	25	56	1	58		-	-	32	-	3	1

8	Venue: Conference room of DG office in Mandarin						
No.	Mervie	Name	Affiliation/Duty	Depictment	Email	Mahibe	Simulation
	Mr/Ms	Profisio Feroandes Xavier	In-house Concultant	JICA			Intendec
-	Mr/Ms	Devi Emanuel	Director	MOP Liquit:			1
m	Mr/Ms	Guspar V.P. Amara)	Director	MOP Allen			1
	Mr/Ms	JoséM. da Casta	Director	MOP Altaro			1
in.	MERMS	Vazario de Jesus Freitas	Englneer	DNEPCC			
5	Mir/Mis	Sues HIROSE	QIC	IICA Exect Texts			
-	Mir/Mis	Hadashi MUTO	Tenn Leader	CDPS-JICA			L
	Mr/Ms	Simio Laradjahn	Engineer	DNEPCC/ProjectDupt.			1
	MUMA	Aleixe H, G, L da Cruz	Diretor	MOP Dill	1		
8	DUL/INE	Fernando F. F. C. Freins	Chief of Department	DIVEPCC/Migh way			1
	MeNUs	Nichhas Brooker-Japes	Road Disign/Project COOD	CDRS-JICA			1
12	DAT-ING	Hermiane Amarol	12410	34D	1		
12	Mr/Ms	Nagaistii Masafumi	CR	lick			
17	BURNH	Octaviana S. da Carvalho	PO.	JICA	-		
10	Mc/Ns	Emilio des Santos	PR	JICA	-		
16	Mente	India Consult in Consult.	and an				



Attachment 6

Seminar for GIS database operation & IRI activities introduction on 20 March 2019

