JAPAN INTERNATIONAL COOPERATION AGENCY (JICA)

P.T. PLN (PERSERO)
THE REPUBLIC OF INDONESIA

FEASIBILITY STUDY ON THE WARSAMSON HYDROELECTRIC POWER DEVELOPMENT PROJECT IN THE REPUBLIC OF INDONESIA

FINAL REPORT

SUPPORTING REPORT

VOLUME-I HYDROLOGICAL ANALYSIS

VOLUME-II TOPOGRAPHIC SURVEY

FEBRUARY 1996

PACIFIC CONSULTANTS INTERNATIONAL

1216696 [3]

VOLUME - I HYDROLOGICAL ANALYSIS

CONTENTS

| | | Page |
|-----------|---|------|
| Chapter 1 | Objectives and Scope of Study | 1 |
| Chapter 2 | Summary of Available Data | 2 |
| 2.1 | Rainfall | 2 |
| 2.2 | Discharge data | 3 |
| 2.3 | | |
| 2.4 | Meteorological data | 3 |
| 2.5 | | 4 |
| Chapter 3 | Hydro-meteorological Conditions of River Basin | 8 |
| Chapter 4 | Study on Natural River Flow | 10 |
| 4.1 | Discharge Rating Curve | 10 |
| 4.2 | Study on Run-off Coefficient and Estimation of River Flow | 14 |
| Chapter 5 | Flood Analysis | 20 |
| 5.1 | | |
| 5.2 | · · · · · · · · · · · · · · · · · · · | |
| 5.3 | Triangular Hydrograph Analysis | 22 |
| Chapter 6 | Study on Sedimentation | 33 |
| 6.1 | Suspended Load | 33 |
| 6.2 | Bed Load | 35 |
| 6.3 | Total Sediment Load (Total-Qsd) | 36 |
| Chapter 7 | Evaporation | 38 |
| Appendice | es · | , |
| Α. | Rainfall Data | |
| В. | Water Level at Malano AWLR | |
| C. | Meteorological Data | |
| D. | Results of Discharge Measurement | |
| E. | Results of Suspended Load Measurement | |
| F. | Tide Level | • |

LIST OF TABLES

| | | Page |
|-----------|---|------|
| Table 4.1 | Areal Rainfall Derived from Thiessen Polygons | 23 |
| Table 4.2 | Study on Run-off Coefficient by Comparing Discharge and Rainfall Data | 24 |
| Table 4.3 | Estimated Monthly River Flow at Dam Site | 28 |
| Table 5.1 | Results of Frequency Analysis for 24-hr Rainfall | 30 |
| Table 5.2 | Probable Rainfall | 31 |
| Table 5.3 | Areal Rainfall | 31 |
| Table 5.4 | Hourly Distribution of Rainfall | 33 |
| Table 5.5 | Probable Flood | 38 |
| Table 6.1 | Results of Suspended Load Measurement | 47 |
| Table 6.2 | Estimated Suspended Load at Dam Site | 48 |
| Table 6.3 | Estimated Bed Load at Dam Site | 51 |
| Table 7.1 | Estimation of Evaporation Rate form Open Water | 54 |

LIST OF FIGURES

| | | Page |
|-----------|--|------|
| Fig. 2.1 | Location Map for Rainfall Gauge and Water Level Gauge Stations | 5 |
| Fig. 2.2 | Availability of Annual / Monthly Hydro-meteorological Data | 6 |
| Fig. 2.3 | Availability of Daily / Monthly Rainfall and Water Level Data | 7 |
| Fig. 3.1 | Simple Moving Average of Annual Rainfall at Sorong Jefman | 9 |
| Fig. 4.1 | Discharge Rating Curve (EL - Q) | 11 |
| Fig. 4.2 | Relation between EL and H (W.L. recorded at Malano AWLR) | 12 |
| Fig. 4.3 | Discharge Rating Curve | 13 |
| Fig. 4.4 | Thiessen Polygon (1) | 15 |
| Fig. 4.5 | Thiessen Polygon (2) | 16 |
| Fig. 4.6 | Thiessen Polygon (3) | 17 |
| Fig. 4.7 | Thiessen Polygon (4) | 18 |
| Fig. 4.8 | Thiessen Polygon (5) | 19 |
| Fig. 4.9 | Thiessen Polygon (6) | 20 |
| Fig. 4.10 | Thiessen Polygon (7) | 21 |
| Fig. 4.11 | Thiessen Polygon (8) | 22 |
| Fig. 4.12 | Specific Mean Discharge at Various Dam Sites in Indonesia | 26 |
| Fig. 4.13 | Flow Duration Curve | 29 |
| Fig 5.1 | Gross Rainfall in % (Case-1) | 32 |
| Fig 5.2 | Gross Rainfall in % (Case-2) | 32 |
| Fig. 5.3 | Cumulative Rainfall | 34 |
| Fig. 5.4 | Hourly Distribution of 24 hours Rainfall | 35 |
| Fig. 5.5 | Concept of Triangular Hydrograph | 36 |
| Fig. 5.6 | Gross Rainfall (Case-1) | 39 |
| Fig. 5.7 | Gross Rainfall (Case-2) | 39 |
| Fig. 5.8 | Effective Rainfall (Case-1) | 39 |
| Fig. 5.9 | Effective Rainfall (Case-2) | 39 |
| Fig. 5.10 | Direct Run-off Curve | 40 |
| Fig. 5.11 | Hydrograph for T = 200 yrs (Case-1) | 41 |

| Fig. 5.12 | Hydrograph for T = 200 yrs (Case-2) | 41 |
|-----------|---------------------------------------|------------|
| Fig. 5.13 | Probable Flood Discharge (Case-1) | 42 |
| Fig. 5.14 | Probable Flood Discharge (Case-2) | 43 |
| Fig. 5.15 | Curves from Creager's Equation | 4 4 |
| Fig. 6.1 | Results of Suspended Load Measurement | 46 |
| Fig. 6.2 | Suspended Load Rating Curve | 46 |

CHAPTER 1 OBJECTIVES AND SCOPE OF STUDY

Analysis and estimation of the river flow, flood discharge and sedimentation, as well as other hydrological parameters, at the proposed project site are essential in determining the technically optimum development scale and design conditions for the facilities to be built.

During the feasibility study (F/S), the following works were carried out;

- collection of meteorological data, precipitation data, discharge data and other data which have been taken at the existing observation stations in and around the river basin
- visiting the project site as well as some of the observation stations, to assess a hydrological conditions where they are located
- site survey, undertaken by PLN, to obtain supplementary hydro-meteorological data,
- thorough analysis of the hydrological parameters which were required for the optimization study

The data collection was continued up to the Feasibility-grade Design Stage in which a thorough hydrological analysis was carried out. The analysis covers the estimation of natural river flow, flood discharge, sedimentation and evaporation.

CHAPTER 2 SUMMARY OF AVAILABLE DATA

Hydro-meteorological data such as rainfall, water levels, atmospheric air temperature and so forth were collected during this F/S. However, it is regrettable to say that there are too many missing records at the existing observation stations. It is essential that improvements to the present situation are made so that the data can be collected continuously.

The following is the summary of data obtained at the observation stations including the new stations established during this F/S.

2.1 Rainfall

There are 20 rain-gauging stations in and around the Warsamson river basin including the new station established by PLN during this F/S. All the rainfall data available at present are exhibited in Appendix A.

The rain-gauging stations, WSN-1 ~ WSN-6, were established by PLN and have been operated since 1991. The station at Sorong Jefman was established by BMG, and since 1920 the rainfall has been observed. The other stations, excluding the new station, were installed by other organizations and the registration of data was terminated before 1987.

The operation of the new station was started in 1995. This station is located near WSN-1 for obtaining not only rainfall data but also other meteorological data.

The locations of the above stations and the availability of data are shown in Figs. 2.1, 2.2 and 2.3.

(1) WSN-1 ~ WSN-6

Data taken at WSN-1 ~ WSN-6 could be most useful for the hydrological analysis of the project since these stations are located in and near the Warsamson river basin, and daily rainfall data has been collected. However, there are too many missing records as shown in Figs. 2.2 and 2.3. This was caused by mechanical trouble with recorders, imperfect maintenance and so forth. Due care has to be taken for data collection.

(2) Sorong Jefman

This station is located relatively close to the project area. Rainfall data over a long period of time is available only at this station in the Sorong area although there is a long break in the records from 1942 to 1957. Maximum daily rainfall records up to 1990 were also recorded at this station as shown in Table A.2 of Appendix A.

During this F/S, recent rainfall data was collected from BMG in Jakarta and Sorong Jefman, but only monthly rainfall data was completely recorded.

(3) New station at Malano

Instruments such as an evaporimeter, a barometer, a sunshine recorder, a thermometer, an automatic rain gauge, a wind vane and an anemometer were supplied by JICA and installed by PLN at this station. It's operation began in 1995. In the project area, only this station is collecting meteorological data, and these data will be very useful for the project in the future.

2.2 Discharge Data

Long term discharge data is of vital importance in determining the technically optimum development scale and design conditions for the plant facilities to be built. It is, however, to be regretted that the discharge measurements carried out at the Malano gauging station by Pt. Wiratman & Associates and Pt. Geo Ace under contract with PLN, were only for certain periods which effected the discharge rating curves, but they may be no longer applicable to the present river conditions. By using the instrument supplied by JICA, PLN undertook the discharge measurements at the Malano gauging station (Malano AWLR) to produce a new discharge rating curve.

Appendix D exhibits the results of discharge measurements during this F/S.

2.3 Water Level

Malano AWLR was installed by PLN and started operation in March 1991. It is regrettable to say that water levels also have not been recorded continuously and that data is lacking for large parts of the years as shown in Fig. 2.3.

All data collected are exhibited in Table B.1 of Appendix B. It is of vital importance to maintain the automatic water level recorder properly and collect data continuously.

2.4 Meteorological Data

Meteorological data is available at the meteorological station class II Jefman in the Sorong area, which has been operated by BMG. At this station, data such as wind speed, rainfall, air temperature and humidity have been collected.

In addition, meteorological data has been collected by PLN at the new Malano station since February, 1995.

All the data are exhibited in Appendix C.

2.5 Other Data

(1) Sedimentation

In the project area, no research, except for the study in the Pre-F/S, was carried out on the sedimentation range before the conducting of this F/S. In order to examine the study results in the Pre-F/S Report, the suspended load of the Warsamson river was measured by PLN at the Malano AWLR in the course of this F/S. Data obtained is exhibited in Appendix E.

(2) Tidal level

The discharge point of the proposed hydropower plant will be located downstream of the waterfall, where the water level may be affected by the tidal levels. Therefore, during this F/S, an automatic water level recorder was installed downstream of the waterfall for measuring water levels and clarifying the influence due to the tidal levels. In order to examine the correlation between the tidal levels at Sorong Port and the river estuary, the tidal levels near the estuary were also measured.

The observation records are shown in Appendix F.

(3) Topographic maps

In order to clarify the locations of the existing rain-gauge stations, an area of the river basin and a length of the Warsamson river, topographic maps with scales of 1/250,000 and 1/63,300 were used.

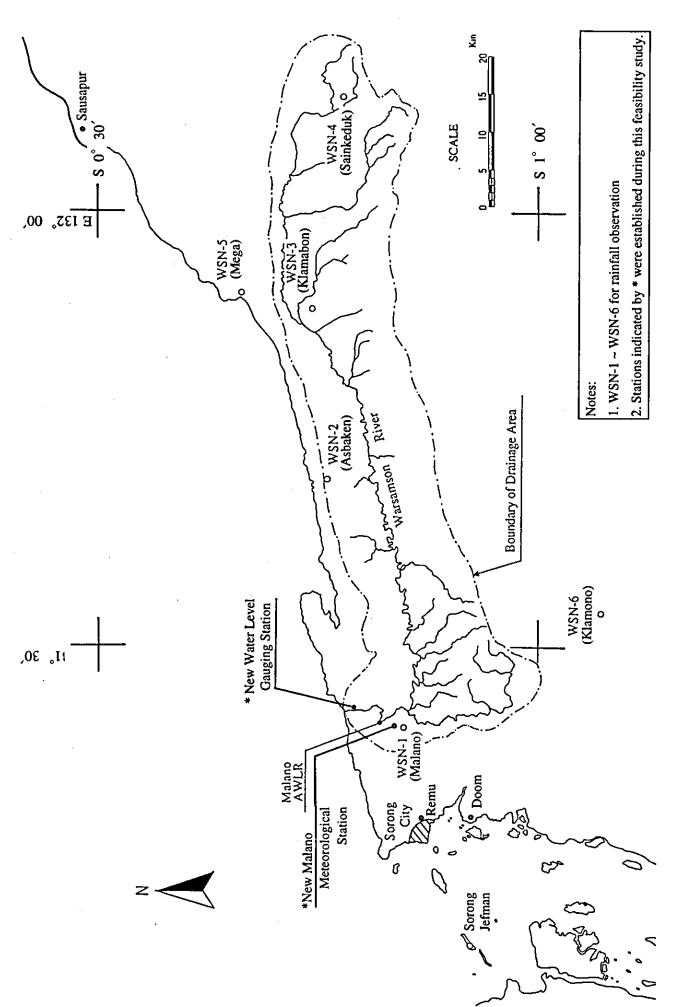


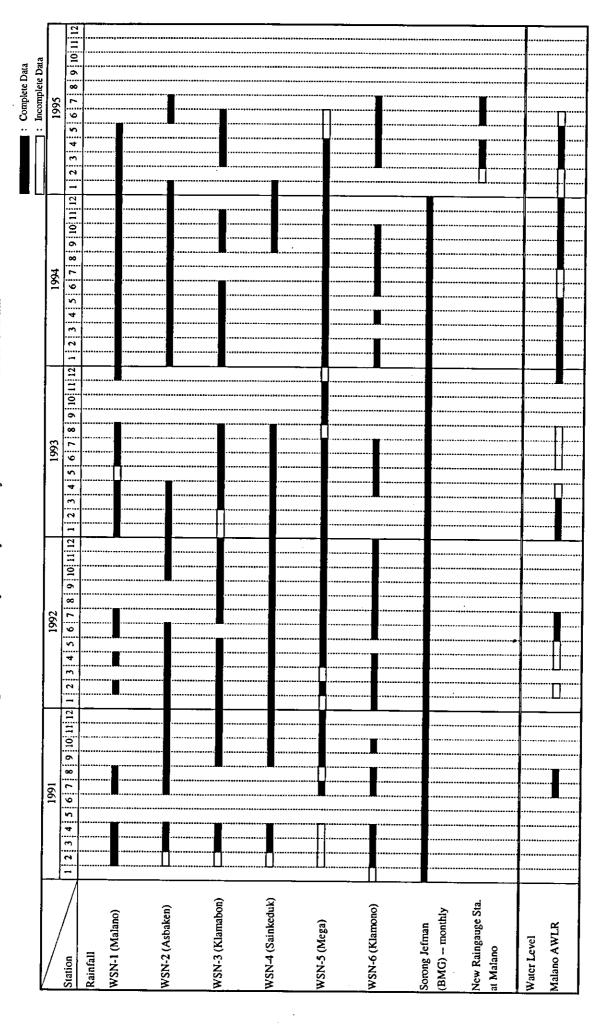
Fig. 2.1 Location Map for Rainfall Gauge and Water Level Gauge Stations

Fig. 2.2 Availability of Annual / Monthly Hydro-meteorological Data

Complete data

1920 s/d 47 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 28 41 ε. Γ Pertamina Perkbunan Рюрсиу Pertanian Pertanian Pertanian Pertanian Katholik BMG BMG PLN PLN PLN P.N PLN PLN PLN PLN 00°53'S • 131°17'E 01°07'S • 131°30'E 00°30'S • 132°05'E 01°17'S • 132°11'E 01°11'S • 132°29'E 00°45'S • 131°30'E 00°58'S • 131°07'E 01°06'S • 131°31'E 00°53'S • 131°17'E 00°48'S • 133°04'E 00°04'S • 130°59'E 00°40'S • 131°53'E 01°06'S • 131°21'E 00°47'S • 132°07'E 00°46'S • 131°00'E 00°47'S • 132°07'E 01°51'S • 131°24'E 00°56'S • 131°07'E 01°26'S • 132°23'E 00°39'S • 132°07'E Location 5 150 350 150 375 8 8 8 375 38 田田 Station No. 608/504d 1648/504c D648/499d 0414/506 1404/49 1604/5041 6279499 0412/506 0402/499 0408/499 004/498n 0204/522 WSN-2 WSN-3 WSN4 WSN-5 WSN-6 WSN-1 II. River Water Level 1. Sorong - Jefman 2. Sorong - Remu 3. Sorong - Doom 1. Malano AWLR 1. Sorong Jefman 20. New Malano 2. New Malano Station Name 16. Klamabon 17. Sainkeduk 19. Klamono 4. Klamono 5. Sausapur 6. Ayamaru 15. Asbaken 8. Ayawasi 7. Atinyo I. Rainfall 9. Wefiani 12. Makbon III. Climate 14. Malano 11. Kebare 10. Kebar 18. Mega 13. Mega

Fig. 2.3 Availability of Daily / Monthly Rainfall and Water Level Data



CHAPTER 3 HYDRO-METEOROLOGICAL CONDITIONS OF RIVER BASIN

The river basin, which is covered by dense forest, is bounded by a mountain range with Mount Sagawawi (673 m) in the south and Mount Mayalon (686 m) in the north. The form of the basin is very narrow (about 15 km wide x 95 km long) and it generally has flat features with many isolated hills. The catchment areas are about 1,460 km² at the proposed dam site and about 1,412 km² at Malano AWLR.

According to the site reconnaissance, miscellaneous weathered rocks, such as mudstone, tuff, siltstone and so forth, are distributed in the upstream area, and most of the area is covered by residual soil and dense tropical vegetation. It seems that the permeability is low, but water retentivity is high because of the dense vegetation.

The Warsamson river flows from east to west for a total length of about 190 km, including the Sumrem river (about 32 km long) which flows in the most upstream area, and reaches the Pacific Ocean at Dan Pier Strait in the north of Irian Jaya. The slope of the river bed is estimated as about 1/1,500 ~ 1/3,000 except for the Sumrem river and the stretch between the waterfall and the Malano bridge.

According to the meteorological data at Sorong Jefman, the average temperature is about 28 °C and the average humidity is about 81 %. It is said that the climate in this area is influenced by the West and East monsoon, but it rains almost every month and a clear dry season cannot be seen from the rainfall data at the gauging stations (WSN-1 ~ WSN-6 and Jefman).

Annual rainfall at Sorong Jefman varies from 1,793 to 4,098 mm according to Table A.2 of Appendix A. The annual rainfall from 1958 to 1994 and for 5-year moving averages are shown in Fig. 3.1. According to the figure, dry years and wet years come in a cycle of 4 to 6 years, and a long cycle change extending 14 years also exists.

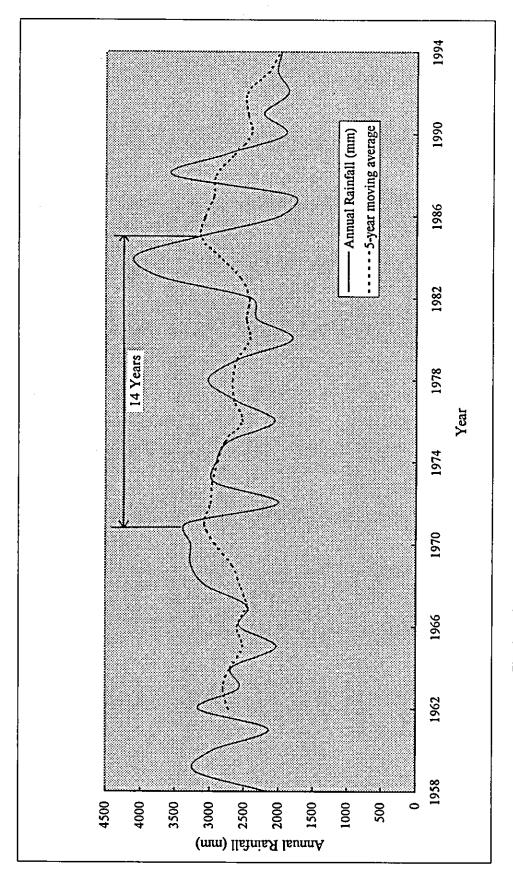


Fig. 3.1 Simple Moving Average of Annual Rainfall at Sorong Jefman

CHAPTER 4 STUDY ON NATURAL RIVER FLOW

4.1 Discharge Rating Curve

By using the results of discharge measurements undertaken by PLN during this F/S

(Appendix D), a new rating curve shown in Fig. 4.3 was produced.

First, a discharge rating curve toward the elevation of the water surface (h) was produced by

regression analysis as shown in Fig. 4.1 since "h" was recorded during the discharge

measurement.

Secondly, the correlation between the elevation of the water surface (h) and reading at the

existing Malano AWLR (H) was examined (Fig. 4.2). This work is necessary to estimate the

river flow from water level records at Malano AWLR in the past and in the future.

Finally, Fig. 4.3 was obtained by interpolating the h-H relation to the equations of the EL-Q

rating curve indicated in Fig. 4.1.

 $Q = 12.294 H^2 + 35.446 H + 4.99 (H < 1.80 m)$

 $Q = 1.1013 H^2 + 96.797H - 69.19 (H \ge 1.80 m)$

Fig. 4.3 compares the rating curves obtained in this F/S and the Pre-F/S completed in 1992.

Both curves cross at the middle, but some difference can be seen at low and high water levels.

This difference is caused by erosion of the river bed and the river banks, sedimentation and/or

errors in the measurement.

Water levels recorded at Malano AWLR were converted to river flows as follows:

River flow up to 1993

: by using the rating curves in the Pre-F/S

River flow from 1994

: by using the rating curves produced in this F/S

The results are exhibited in Appendix B.

10

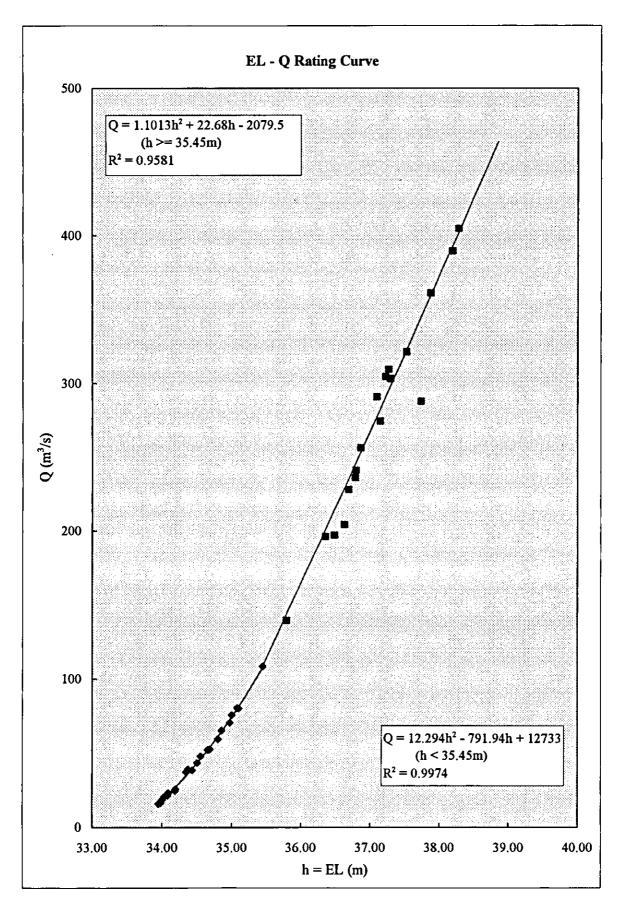


Fig. 4.1 Discharge Rating Curve (EL - Q)

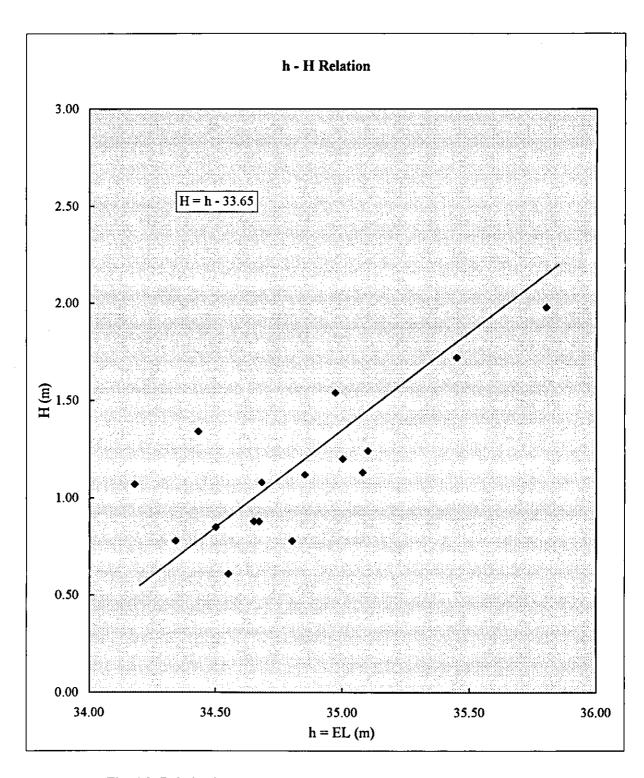


Fig. 4.2 Relation Between EL and H (W.L. recorded at Malano AWLR)

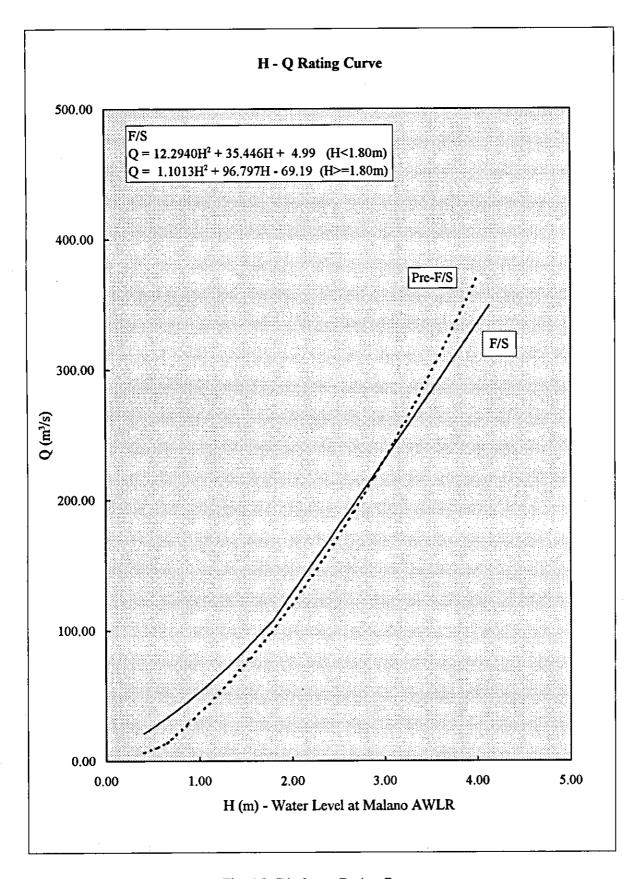


Fig. 4.3 Discharge Rating Curve

4.2 Study on Run-off Coefficient and Estimation of River Flow

The run-off coefficient was estimated based on the rainfall and discharge data obtained, and also by referring to the specific mean discharge used for the planning of other projects in Indonesia.

(1) Estimation of run-off coefficient by using rainfall and discharge data

Table B.1 in Appendix B shows the results of the conversion from the water levels which were observed at Malano AWLR to river flows as mentioned in Section 4.1.

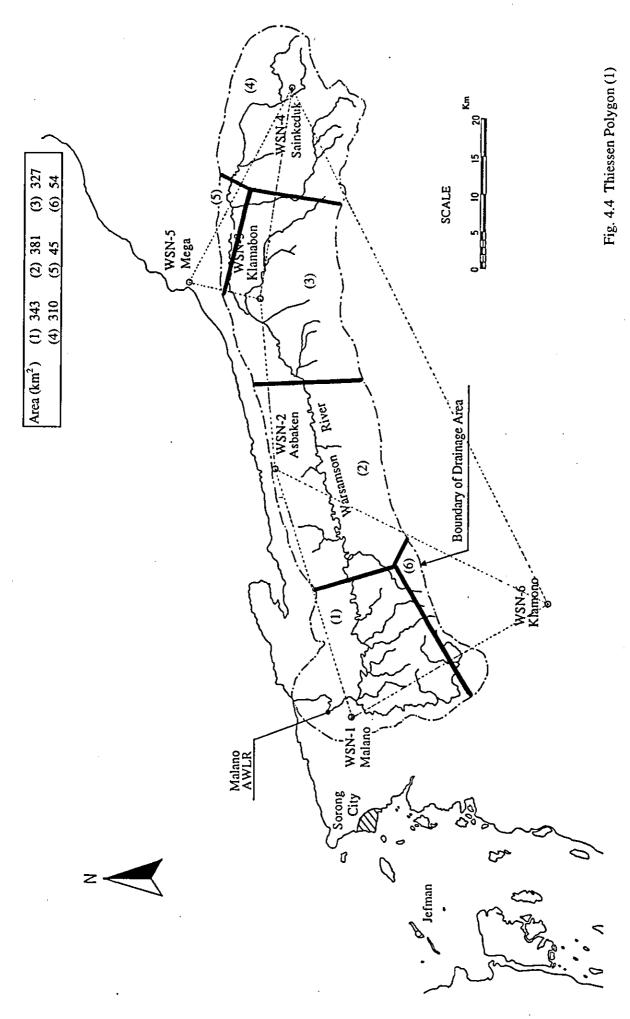
Table A.1 in Appendix A shows the rainfall data observed at WSN-1 ~ WSN-6.

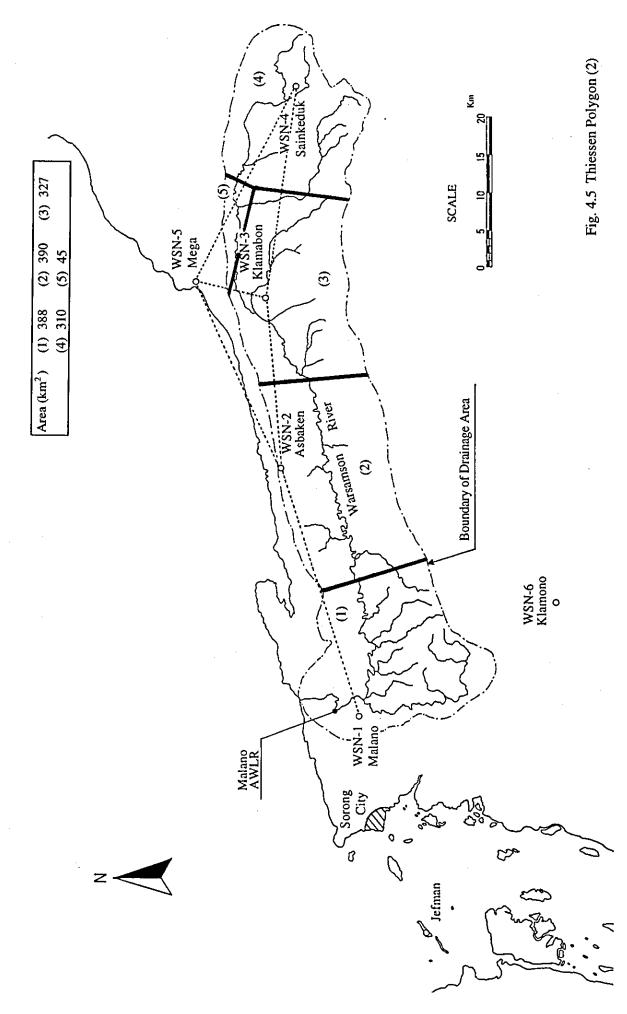
Based on the data shown in the above tables, run-off coefficients were estimated as follows:

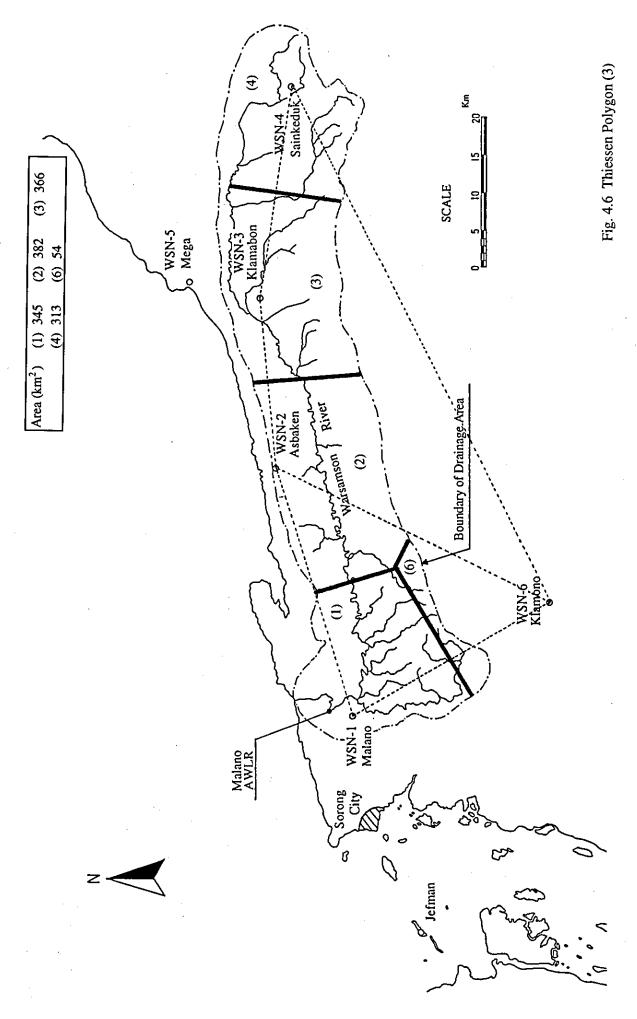
- 1) Monthly rainfall data at WSN-1 ~ WSN-6 were converted to areal rainfall by using Thiessen Polygons (Figs. 4.4 ~ 4.10). Since there is a lack of data, the data for only 19 months were used for these calculations as shown in Table 4.1.
- Average monthly river flows for the above 19 months were obtained from Table B.1 of Appendix B. The river flow in April 1991 was taken from the Pre-F/S report.
- 3) It was found, by comparing the areal rainfall and the river flow as shown in Table 4.2, that an average run-off coefficient of approximately 0.58 is obtained.

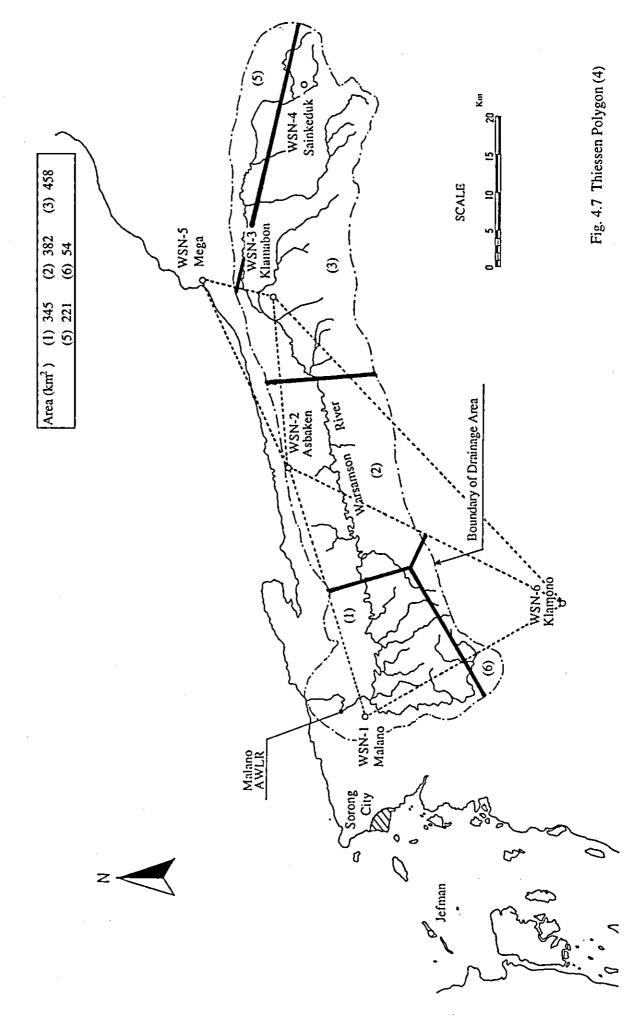
The above result seems to be reasonable considering the site conditions such as topography, soil cover and soil type. It is, however, necessary to review it by collecting more data in the detailed design stage since there are some problems in the above estimation;

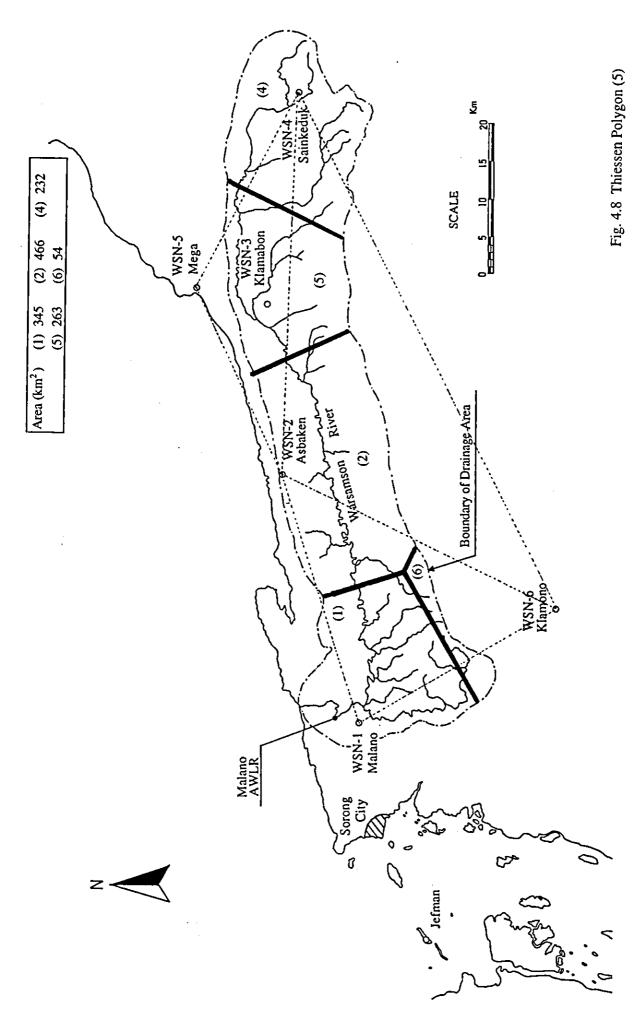
- The volume of data examined is not sufficient.
- Only 6 rain-gauging stations exist in and near the catchment area which has an area of 1,460 km². Also ,the cases where monthly rainfall data at all of the stations are available in the same month is for 4 months only. These facts reduce the reliability of the estimated areal rainfall data and run-off coefficient.
- The estimation was made assuming that rainfall in a certain month runs off in the same month, with some losses. However, it is considered that river flow is affected by antecedent rainfalls in the preceding months as well. This effect could not be examined since there was too much missing of data.



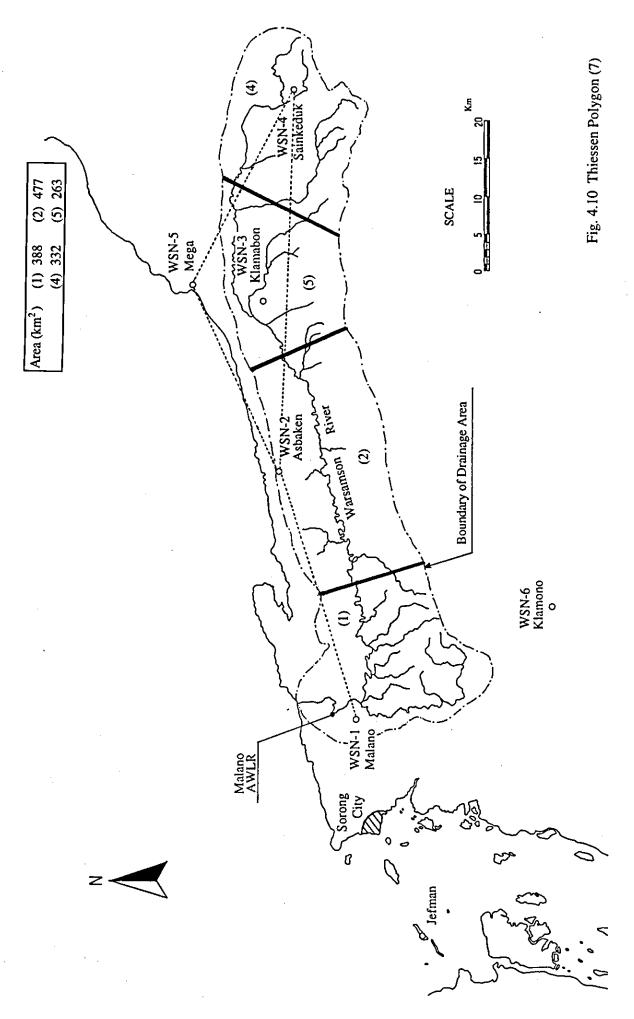








20



22

Table 4.1 Areal Rainfall derived from Thiessen Polygons and Comparison with Monthly Rainfall at Jefman

| Month | 1 | | Jefman | Ratio | | | | | | |
|----------------|---|----------------|----------------|----------------|---------------|---------------|---------------|-----------------|---------|-----------|
| | | WSN-1 | WSN-2 | WSN-3 | WSN-4 | WSN-5 | WSN-6 | Total | | |
| 1991. 3 | Area (kin^2) Weight | 345.0 0.24 | 382.0 0.26 | 366.0 0.25 | 0.21 | x x | 54.0 0.04 | 1460.0 1.0 | | - |
| | Rainfall (mm) Weighted Rainfall (mm) | 380.0 89.8 | 387.5 101.4 | 455.5 114.2 | | x x | 351.5 13.0 | 387.9 | 235.0 | 0.6 |
| 1991.4 | Area (km^2) | 345.0 | 382.0 | 366.0 | | x | 54.0 | 1460.0 | | |
| | Weight Rainfall (mm) | 0.24 156.0 | 0.26 248.5 | 0.25 214.0 | | x x | 0.04 429.0 | 1.0 | | |
| | Weighted Rainfall (mm) | 36.9 | 65.0 | 53.6 | 76.7 | x | 15.9 | 248.1 | 156.0 | 0.6 |
| 1992. 2 | Area (km^2) Weight | 343.0 0.23 | 381.0 0.26 | 327.0 0.22 | | 45.0 0.03 | 54.0 0.04 | 1460.0 1.0 | | |
| | Rainfall (mm) | 151.0 | 186.0 | 227.0 | 111.0 | 127.0 | 248.0 | | | |
| 1992, 4 | Weighted Rainfall (mm) Area (km^2) | 35.5 343.0 | 48.5 381.0 | 50.8 327.0 | | 3.9 45.0 | 9.2 54.0 | 171.5 1460.0 | 50.0 | 0.2 |
| 1772. 4 | Weight | 0.23 | 0.26 | 0.22 | 0.21 | 0.03 | 0.04 | 1.0 | | |
| | Rainfall (mm) Weighted Rainfall (mm) | 119.5 28.1 | 279.0 72.8 | 292.0 65.4 | | 248.0 7.6 | 142.0 5.3 | 238.2 | 100.0 | 0.4 |
| 1992. 6 | Area (km^2) | 345.0 | 466.0 | x | 332.0 | 263.0 | 54.0 | 1460.0 | | · · · · · |
| | Weight Rainfall (mm) | 0.24 266.0 | 0.32 150.0 | X X | 0.23 290.0 | 0.18 209.0 | 0.04 510.0 | 1.0 | | |
| | Weighted Rainfall (mm) | 62.9 | 47.9 | x | 65.9 | 37.6 | 18.9 | 233.2 | 136.0 | 0.58 |
| 1992. 7 | Area (kın^2) Weight | 456.0 0.31 | x | 582.0 0.40 | | x | 88.0 0.06 | 1460.0 1.0 | | |
| | Rainfall (mm) | 109.5 | X X | 444.0 | 222.0 | X X | 299.0 | | | |
| 1002 1 | Weighted Rainfall (mm) | 34.2 | X | 177.0 | 50.8 | X | 18.0 | 280.0 | 191.0 | 0.68 |
| 1993. 1 | Area (km^2) Weight | 388.0 0.27 | 477.0 0.33 | X X | 332.0 0.23 | 263.0 0.18 | X X | 1460.0 1.0 | | |
| | Rainfall (mm) Weighted Rainfall (mm) | 189.5 50.4 | 148.0 48.4 | X X | 238.0 54.1 | 204.0 36.7 | X I | 189.6 | 111.0 | 0.59 |
| 1993. 2 | Area (km^2) | 388.0 | 477.0 | x | 332.0 | 263.0 | x | 1460.0 | | 0.5 |
| | Weight Rainfall (mm) | 0.27 71.0 | 0.33 0.0 | Х Х | 0.23 244.0 | 0.18 187.0 | X I | 1.0 | ŀ | |
| | Weighted Rainfall (mm) | 18.9 | 0.0 | â | 55.5 | 33.7 | x | 108.0 | 114.0 | 1.06 |
| 1993.3 | Area (km^2) | 388.0 | 390.0 | 327.0 | | 45.0 | x | 1460.0 | | |
| | Weight Rainfall (mm) | 0.27 76.5 | 0.27 92.0 | 0.22 202.0 | 279.0 | 0.03 105.0 | X X | 1.0 | | |
| | Weighted Rainfall (mm) | 20.3 | 24.6 | 45.2 | | 3.2 | х | 152.6 | 110.0 | 0.72 |
| 1993. 4 | Area (km^2) Weight | 343.0 0.23 | 381.0 0.26 | 327.0 0.22 | | 45.0 0.03 | 54.0 0.04 | 1460.0 1.0 | | |
| | Rainfall (mm) Weighted Rainfall (mm) | 140.0 32.9 | 63.0 16.4 | 394.0 88.2 | 460.0 97.7 | 112.0 3.5 | 397.0 14.7 | 253.4 | 206.0 | 0.81 |
| 1993. 6 | Area (km^2) | 456.0 | х | 561.0 | | 45.0 | 88.0 | 1460.0 | | 0.01 |
| | Weight Rainfall (mm) | 0.31 25.0 | X X | 0.38 330.0 | 0.21 500.0 | 0.03 201.0 | 0.06 239.0 | 1.0 | | |
| | Weighted Rainfall (mm) | 7.8 | x | 126.8 | 106.2 | 6.2 | 14.4 | 261.4 | 136.0 | 0.52 |
| 1993. 7 | Area (km^2) Weight | 456.0 0.31 | x | 561.0 0.38 | 310.0 0.21 | 45.0 0.03 | 88.0 0.06 | 1460.0 1.0 | | |
| | Rainfall (mm) | 124.0 | X X | 572.0 | 904.0 | 131.0 | 496.0 | | | |
| 1004.1 | Weighted Rainfall (mm) | 38.7 | X | 219.8 | 191.9 | 4.0 | 29.9 | 484.4 | 294.0 | 0.61 |
| 1994. 1 | Area (km^2) Weight | 345.0 0.24 | 382.0 0.26 | 458.0 0.31 | | 221.0 0.15 | 54.0 0.04 | 1460.0 1.0 | | |
| | Rainfall (mm) Weighted Rainfall (mm) | 140.5 33.2 | 44.0 11.5 | 182.0 57.1 | X X | 169.0 25.6 | 156.0 5.8 | 133.2 | 35.0 | 0.26 |
| 1994. 2 | Area (km^2) | 345.0 | 382.0 | 458.0 | : | 221.0 | 54.0 | 1460.0 | 77.0 | 0.20 |
| | Weight Rainfall (mm) | 0.24 46.5 | 0.26 7.0 | 0.31 56.0 | x | 0.15 41.0 | 0.04 163.0 | 1.0 | | |
| | Weighted Rainfall (mm) | 11.0 | 1.8 | 17.6 | X X | 6.2 | 6.0 | 42.6 | 161.0 | 3.78 |
| 1994. 4 | Area (km^2) | 345.0 | 382.0 | 458.0 | x | 221.0 | 54.0 | 1460.0 | 1 | |
| | Weight Rainfall (mm) | 0.24 368.5 | 0.26 1249.0 | 0.31 343.0 | X X | 0.15 168.0 | 0.04 474.0 | 1.0 | | |
| 1004 | Weighted Rainfall (mm) | 87.1 | 326.8 | 107.6 | X | 25.4 | 17.5 | 564.4 | 229.0 | 0.41 |
| 1994. 6 | Area (km^2) Weight | 345.0 0.24 | 382.0 0.26 | 458.0 0.31 | X X | 221.0 0.15 | 54.0 0.04 | 1460.0 1.0 | 1 | |
| | Rainfall (mm) Weighted Rainfall (mm) | 600.0 141.8 | 263.0 68.8 | 171.0 53.6 | X X | 199.0 30.1 | 539.0 19.9 | 314.3 | 326.0 | 1.04 |
| 1994. 10 | Area (km^2) | 343.0 | 381.0 | 327.0 | 310.0 | 45.0 | 54.0 | 1460.0 | 540.0 | 1.04 |
| | Weight Rainfall (mm) | 0.23 239.5 | 0.26 0.0 | 0.22 212.0 | 0.21 87.0 | 0.03 83.5 | 0.04 357.0 | 1.0 | | |
| | Weighted Rainfall (mm) | 56.3 | 0.0 | 47.5 | 18.5 | 2.6 | 13.2 | 138.0 | 191.0 | 1.38 |
| 1994. 11 | Area (km^2) | 388.0 | 390.0 | 327.0 | 310.0 | 45.0 | x | 1460.0 | | |
| | Weight Rainfall (mm) | 0.27 126.5 | 0.27 460.0 | 0.22 176.0 | 0.21 492.0 | 0.03 233.5 | X X | 1.0 | | |
| | Weighted Rainfall (mm) | 33.6 | 122.9 | 39.4 | 104.5 | 7.2 | x | 307.6 | 191.0 | 0.62 |
| 1994. 12 | Area (km^2) Weight | 388.0 0.27 | 477.0 0.33 | x i | 332.0 0.23 | 263.0 0.18 | X X | 1460.0 1.0 | | |
| | Rainfall (mm) Weighted Rainfall (mm) | 48.0 12.8 | 48.0 15.7 | X X | 287.0 65.3 | 217.0 39.1 | X X | 132.8 | 72.0 | 0.54 |
| | signised remited (mill) | 12.0 | 13.7 | ^ 1 | J.J. | 33.1 | | 1,72.0 | Average | 0.82 |

Table 4.2 Study on Run-off Coefficient by comparing discharge and rainfall data

| Remarks | Remarks | | | | | | | rejected | | rejected | | | |
|---------------------------|--------------------------------|-------|-----------|-----------|-------|-------|-----------|----------|--------|----------|-------|-------|-------|
| Run-off Coefficient | Run-off Coefficient | | 0.64 | 19:0 | 0.64 | 0.53 | 76.0 | 2.34 | 0.36 | 1.03 | 0.40 | 0.29 | 0.84 |
| Thiessen's Rainfall | Thiessen's Rainfall (mm) | | 280.0 | 189.6 | 108.0 | 152.6 | 133.2 | 42.6 | 564.4 | 47.8 | 138.0 | 307.6 | 132.8 |
| | 9-NSM | 429.0 | 299.0 | | | | 156.0 | 163.0 | 474.0 | 9.0 | 357.0 | ļ | • |
| | WSN-5 | 1 | 251.0 | 204.0 | 187.0 | 105.0 | 169.0 | 41.0 | 168.0 | 2.0 | 83.5 | 233.5 | 217.0 |
| Rainfall | WSN-4 | 353.0 | 222.0 | 238.0 | 244.0 | 279.0 | , | • | ı | 218.0 | 87.0 | 492.0 | 287.0 |
| Monthly Rainfall | WSN-3 | 214.0 | 444.0 | ı | ı | 202.0 | 182.0 | 56.0 | 343.0 | 1.0 | 212.0 | 176.0 | 1 - |
| | WSN-2 | 250.0 | ı | 148.0 | 0.0 | 92.0 | 44.0 | 7.0 | 1249.0 | 0.0 | 0.0 | 460.0 | 48.0 |
| | WSN-1 | 156.0 | 109.0 | 190.0 | 71.0 | 77.0 | 140.5 | 46.5 | 368.5 | 4.0 | 239.5 | 126.5 | 48.0 |
| Run-off | (mm) | 122.1 | 178.2 | 127.2 | 68.6 | 80.3 | 129.8 | 99.5 | 204.0 | 49.5 | 54.7 | 90.4 | 111.5 |
| Ave. Monthly Discharge | (m3/s) | 66.55 | 94:00 | 67.08 | 40.08 | 42.37 | 68.45 | 58.11 | 111.18 | 26.95 | 28.87 | 49.29 | 58.79 |
| Month | Month | | 1992 Jul. | 1993 Jan. | Feb. | Mar. | 1994 Jan. | Feb. | Apr. | Sep. | Oct. | Nov. | Dec. |

note: Catchment area at Malano AWLR = 1,412.5 km2

0.58

(2) Estimation of run-off coefficient from specific mean discharge

Fig. 4.11 shows the specific mean discharge at various dam sites in Indonesia, on which a regression line is also indicated. For the catchment area of 1,460 km², a specific mean discharge is obtained as about 5.0 m³/s/100 km². This can be converted to a run-off depth as follows;

$$5.0 \text{ (m}^3/\text{s}/100 \text{ km}^2\text{)} \times 365 \times 24 \times 3,600 \times 10^{-5} = 1,577 \text{ mm}$$

On the other hand, the mean annual rainfall at Sorong Jefman in the period from 1983 to 1994 is 2,591 mm (see Table A.2). Therefore, the run-off coefficient is estimated as;

$$\frac{1,577}{2,591} \div 0.61$$

(3) Conclusion

From the studies in (1) and (2), the run-off coefficient is estimated as 0.58 ~ 0.61. However, since the estimation was made by using insufficient data, it is safe to adopt a lower run-off coefficient, 0.5, in this F/S.

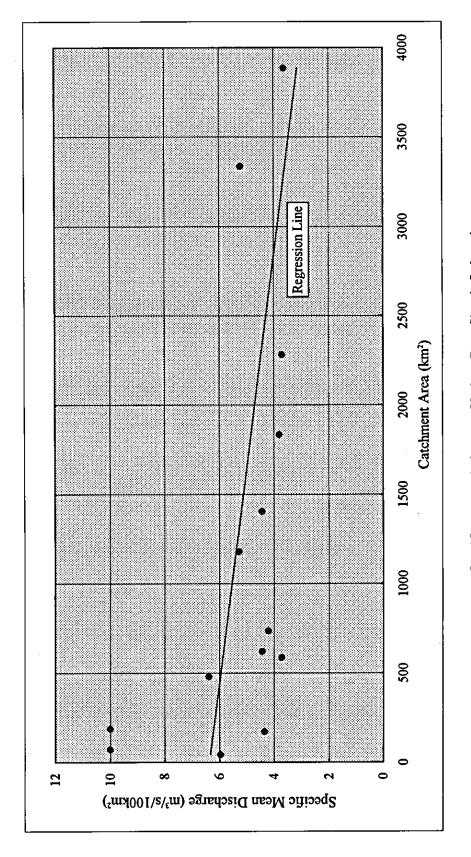


Fig. 4.12 Specific Mean Discharge at Various Dam Sites in Indonesia

4.3 Natural River Flow

Since the rainfall and flow data in the catchment area are insufficient to estimate a long-term river flow, these were derived from the monthly rainfall at Sorong Jefman and the run-off coefficient of 0.5

Before calculating the monthly river flow, the monthly rainfall data at Sorong Jefman was examined by comparing it with those at WSN-1 ~ WSN-6. Table 4.1 shows the results. According to the table, the monthly rainfall at Sorong Jefman is about 82% of the areal rainfall in the catchment area. This does not mean that the monthly rainfall at Sorong Jefman can be increased by 20% for calculating the river flow. However, it can be said, at least, that the river flow derived by the above-mentioned method is on the safe side for the hydropower planning.

Table 4.3 and Fig. 4.12 show the estimated river flow and flow duration curve.

Table 4.3 Estimated Monthly River Flow at Dam Site

(m³/s)

| | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | Average |
|------|-----|-----|----------|------|-----|-----|-----|------------|------|-----|-----|-----|------------|
| 1920 | 16 | 17 | 23 | 122 | 34 | 144 | 32 | 47 | 71 | 67 | 38 | 12 | 52 |
| 1921 | 63 | 64 | 100 | 97 | 75 | 77 | 88 | 65 | 127 | 28 | 71 | 83 | 78 |
| 1922 | 40 | 88 | 41 | 87 | 36 | 92 | 96 | 75 | 65 | 54 | 23 | 49 | 62 |
| 1923 | 116 | 63 | 62 | 82 | 43 | 48 | 33 | 3 | 36 | 31 | 15 | 65 | 50 |
| 1924 | 40 | 98 | 63 | 66 | 108 | 71 | 153 | 81 | 107 | 55 | 89 | 59 | |
| 1925 | 53 | 80 | 67 | 52 | 93 | 88 | 71 | 93 | 61 | 5 | 31 | 56 | |
| 1926 | 38 | 24 | 37 | 95 | 133 | 92 | 140 | 76 | 182 | 49 | 74 | 59 | 84 |
| 1927 | 63 | 30 | 73 | 72 | 111 | 126 | 105 | 33 | 161 | 48 | 69 | 31 | 77 |
| 1928 | 30 | 51 | 61 | 68 | 91 | 90 | 69 | 57 | 47 | 16 | 53 | 58 | 58 |
| 1929 | 53 | 18 | 84 | 80 | 144 | 132 | 64 | 38 | 66 | 49 | 47 | 34 | 68 |
| 1930 | 17 | 47 | 111 | 49 | 56 | 172 | 8 | 7 | 4 | 122 | 43 | 41 | 56 |
| 1931 | 66 | 15 | 29 | 81 | 153 | 189 | 121 | 36 | 90 | 43 | 44 | 39 | 76 |
| 1932 | 30 | 46 | 63 | 63 | 90 | 57 | 143 | 107 | . 53 | 107 | 50 | 71 | 74 |
| 1933 | 55 | 65 | 40 | 44 | 61 | 83 | 102 | 99 | 153 | 62 | 32 | 51 | 70 |
| 1934 | 83 | 52 | 82 | 70 | 83 | 125 | 128 | | 79 | 135 | 98 | 70 | 94 |
| 1934 | 54 | 21 | 57 | 59 | 122 | | 69 | 113 | 48 | 142 | 70 | 50 | 79 |
| | | | | | | 137 | | 112 | | | | 1 | |
| 1936 | 74 | 77 | 107 | 79 | 83 | 84 | 130 | 55 53 | 87 | 141 | 21 | 48 | 83 |
| 1937 | 66 | 58 | 90 70 | 70 | 87 | 126 | 102 | 57 106 | 148 | 97 | 73 | 32 | 84 |
| 1938 | 52 | 27 | 70 | 57 | 96 | 63 | 84 | 196 | 112 | 68 | 45 | 100 | 81 |
| 1939 | 58 | 55 | 24 | 93 | 86 | 119 | 40 | 25 122 | 35 | 8 | 61 | 3 | 50 57 |
| 1940 | 58 | 64 | 59 | 60 | 76 | 90 | 13 | 132 | 44 | 13 | 41 | 30 | 57 |
| 1941 | 34 | 14 | 37 | 90 | 170 | 11 | 24 | 49 | 52 | 55 | 51 | 47 | 53 |
| 1958 | 12 | 27 | 53 | 41 | 50 | 54 | 34 | 132 | 44 | 49 | 46 | 56 | 50 |
| 1959 | 56 | 16 | 29 | 91 | 141 | 150 | 117 | 49 | 52 | 72 | 69 | 47 | 74 |
| 1960 | 83 | 47 | 27 | 54 | 86 | 63 | 237 | 31 | 54 | 25 | 59 | 49 | 68 |
| 1961 | 34 | 62 | 59 | 55 | 39 | 75 | 95 | 31 | 40 | 18 | 41 | 46 | 50 |
| 1962 | 113 | 63 | 35 | 108 | 110 | 93 | 41 | 102 | 38 | 74 | 36 | 63 | 73 |
| 1963 | 76 | 72 | 50 | 72 | 150 | 68 | 84 | 37 | 9 | 9 | 23 | 65 | 60 |
| 1964 | 31 | 83 | 35 | 121 | 62 | 87 | 73 | 40 | 32 | 50 | 46 | 84 | 62 |
| 1965 | 76 | . 8 | 40 | 85 | 80 | 90 | 6 | 10 | 1 | 36 | 72 | 60 | 47 |
| 1966 | 35 | 43 | 38 | 39 | 83 | 73 | 53 | 114 | 62 | 39 | 69 | 62 | 59 |
| 1967 | 91 | 45 | 22 | 76 | 109 | 84 | 96 | 28 | 15 | 47 | 36 | 31 | 57 |
| 1968 | 36 | 18 | 97 | 29 | 46 | 128 | 95 | 56 | 93 | 68 | 106 | 74 | 71 |
| 1969 | 38 | 15 | 112 | 52 | 158 | 68 | 132 | 85 | 28 | 95 | 73 | 45 | 76 |
| 1970 | 53 | 38 | 66 | 77 | 159 | 60 | 126 | 96 | 68 | 34 | 56 | 71 | 76 |
| 1971 | 58 | 61 | 38 | 54 | 131 | 117 | 80 | 119 | 89 | 93 | 55 | 31 | 7 7 |
| 1972 | 45 | 81 | 37 | 47 | 46 | 144 | 19 | 41 | 29 | 9 | 43 | 26 | 47 |
| 1973 | 80 | 33 | 63 | 140 | 97 | 93 | 65 | 100 | 68 | 44 | 23 | 13 | 68 |
| 1974 | 14 | 92 | 27 | 106 | 119 | 87 | 70 | 61 | 80 | 57 | 51 | 47 | 67 |
| 1975 | 43 | 33 | 37 | 78 | 97 | 88 | 63 | 78 | 97 | 39 | 36 | 68 | 63 |
| 1976 | 30 | 63 | 29 | 48 | 88 | 35 | 47 | <i>5</i> 3 | 35 | 87 | 48 | 10 | 48 |
| 1977 | 33 | 56 | 71 | 79 | 79 | 130 | 38 | 49 | 46 | 60 | 44 | 47 | 61 |
| 1978 | 72 | 15 | 144 | 35 | 40 | 91 | 111 | 84 | 82 | 29 | 58 | 74 | 70 |
| 1979 | 15 | 28 | 68 | 78 | 56 | 147 | 26 | 19 | 143 | 20 | 70 | 50 | 60 |
| 1980 | 41 | 41 | 25 | 66 | 75 | 60 | 29 | 52 | 5 | 44 | 37 | 23 | 41 |
| 1981 | 45 | 29 | 62 | 49 | 111 | 32 | 119 | 10 | 84 | 12 | 43 | 49 | 54 |
| 1982 | 38 | 35 | 74 | 55 | 91 | 73 | -] | - | 82 | 33 | 25 | 51 | 56 |
| 1983 | 68 | 10 | 21 | 52 | 134 | 118 | 114 | 144 | 147 | 122 | 41 | 51 | 86 |
| 1984 | 62 | 75 | 59 | 109 | 194 | 105 | 201 | 62 | 162 | 29 | 35 | 42 | 95 |
| 1985 | 38 | 105 | 17 | 42 | 149 | 99 | 66 | 79 | 95 | 70 | 66 | 55 | 73 |
| 1986 | 26 | 46 | 44 | 40 | 41 | 64 | 63 | 15 | 75 | 59 | 32 | 50 | 46 |
| 1987 | 38 | 5 | 60 | 30 | 90 | 42 | 10 | 36 | 16 | 89 | 53 | 25 | 42 |
| 1988 | 55 | 38 | 56 | . 25 | 91 | 90 | 134 | 191 | 92 | 75 | 65 | 66 | 82 |
| 1989 | 34 | 57 | 78 | 86 | 8 | 70 | 85 | 79 | 74 | 107 | 71 | 29 | 65 |
| 1990 | 26 | 35 | 35 | 37 | 60 | 38 | 48 | 37 | 68 | 110 | 18 | 19 | 44 |
| 1991 | 83 | 31 | 64 | 44 | 158 | 53 | 57 | 9 | 1 | 30 | 3 | 77 | 51 |
| 1992 | 4 | 15 | 39 | 28 | 72 | 38 | 52 | 28 | 55 | 117 | 35 | 32 | 43 |
| 1993 | 30 | 34 | 30 | 58 | 98 | 38 | 80 | 13 | 88 | 25 | 39 | 31 | 47 |
| 1994 | 10 | 49 | 64 | 64 | 92 | 92 | 16 | 37 | 0 | 52 | 54 | 20 | 46 |
| Ave. | 49 | 45 | 56 | 68 | 94 | 89 | 79 | 65 | 69 | 58 | 49 | 48 | 64 |

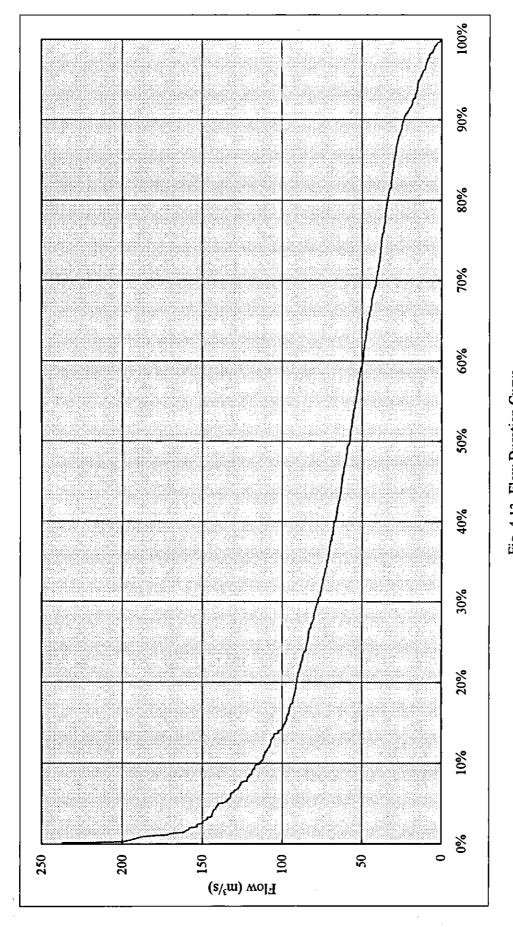


Fig. 4.13 Flow Duration Curve

CHAPTER 5 FLOOD ANALYSIS

There is difficulty in estimating the design flood because of the lack of discharge, flood and rainfall data observed in the project site. One of the methods for estimating the flood discharge is to refer to the specific flood discharge adopted for other projects. However, considering the particular characteristics of the drainage area (for example, Horton's form factor, about 0.045, is quite small), it would not be appropriate to refer to them. It was, therefore, decided to estimate the design flood by applying the triangular hydrograph.

5.1 Probable Rainfall

Rainfall data observed over a long period of time in the drainage area is not available. Instead, the daily rainfall data at Sorong Jefman was used to estimate the probable rainfall since this data is available for a relatively long period and the location of the gauging station is near the project site.

Table A.2 in Appendix A shows the rainfall data at this station, and based on this the frequency analysis was carried out by using the Hazen, Thomas, Gumbel and Iwai methods. Table 5.1 shows the results of the analysis, and the probable rainfall to be used in the subsequent flood analysis is summarized in Table 5.2.

Table 5.1 Results of Frequency Analysis for 24-hr Rainfall

unit (mm)

| T (year) | Hazen | Thomas | Gumbel | Iwai |
|----------|-------|--------|--------|------|
| 2 | 119 | 119 | 119 | 120 |
| 3 | 136 | 137 | 137 | 136 |
| 5 | 154 | 157 | 157 | 154 |
| 10 | 176 | 182 | 181 | 175 |
| 30 | . 208 | 218 | 219 | 205 |
| 50 | 222 | 235 | 236 | 218 |
| 100 | 241 | 257 | 260 | 235 |
| 200 | 260 | 279 | 283 | 253 |
| 300 | 271 | 292 | 296 | 263 |
| 500 | 285 | 308 | 313 | 275 |
| 1000 | 304 | 331 | 336 | 292 |

Table 5.2 Probable Rainfall

| Return Period (yr) | 5 | 10 | 100 | 200 | 300 | 1000 |
|--------------------|-----|-----|-----|-----|-----|------|
| Rainfall (mm) | 157 | 182 | 260 | 283 | 296 | 336 |

The probable rainfall shown in Table 5.2 is point rainfall. For the flood analysis, the point rainfall needs to be converted into the average rainfall on the drainage area (areal rainfall) and its hourly distribution.

Point rainfall has to be multiplied by a reduction factor to convert it into areal rainfall. For obtaining the reduction factor, rainfall data at several stations in the drainage area is necessary. Since the data in the project area is insufficient for this purpose, the areal rainfall was estimated by using the D.A. formula proposed by Horton.

$$P = Po \cdot e^{-a}$$

where.

P : Areal rainfall (mm)

Po : Maximum point rainfall (mm)

 $a : a = kA^n$

k, n : Constants to be determined for each heavy rainfall

The envelope of P/Po for 24-hr rainfall was found, in his study, when k = 0.1 and n = 0.2. Inserting k = 0.1, n = 0.2 and $A = 1,460 \text{ km}^2$, the above formula gives P = 0.65 Po. However, it seems too conservative to use 0.65 for such a wide and slender-shaped drainage area. Therefore, in the table below, P = 0.60 Po is used for deriving areal rainfall from the point rainfall.

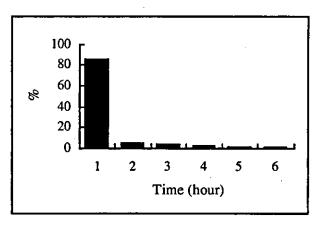
Table 5.3 Areal Rainfall

| Return Period (yr) | 5 | 10 | 100 | 200 | 300 | 1000 |
|---------------------|----|-----|-----|-----|-----|------|
| Areal Rainfall (mm) | 94 | 109 | 156 | 170 | 178 | 202 |

5.2 Hyetograph

The rainfall distribution was studied by using 24-hr rainfall data higher than 50 mm obtained at the stations WSN-1 ~ WSN-6, which is summarized in Table 5.4 and Figs. 5.3 and 5.4. It is known, from Fig. 5.4, that there are mainly two types of distribution. No. 1 indicates that

heavy rainfall occurs only at the beginning, while No. 6 indicates that it occurs in the middle of a storm. Since storm rainfall data is limited in the project area, two types of design hyetographs (Figs. 5.1 and 5.2) derived from Figs. 5.3 and 5.4 were used for estimating the design flood.



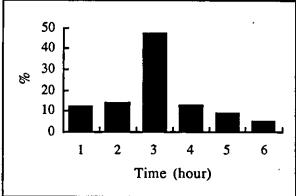


Fig 5.1 Gross Rainfall in % (Case-1)

Fig 5.2 Gross Rainfall in % (Case-2)

5.3 Triangular Hydrograph Analysis

(1) Triangular hydrograph

The concept of the triangular hydrograph and equations, which were obtained empirically by SCS (Soil Conservation Service in U.S.A.) and CHPW (California Highways and Public Works), are shown in Fig. 5.5.

From the available maps including the topographic maps obtained by the aerial photogrammetry, the following figures are obtained:

 $A = 1,460 \text{ km}^2 = 563.2 \text{ mile}^2$

L = 158 km (98.1 miles) of the Warsamson river +32 km (19.9 miles) of the Sumrem river

H = 75 m (246 feet) for the Warsamson river and 700 m (2297 feet) for the Sumrem river

Assuming that D = 1 hr and Q = 1 mm (1/25.4 inch),

$$Tc = 68.8 \text{ hrs},$$
 $Tp = 41.8 \text{ hrs},$ $Tb = 111.6 \text{ hrs}$ $q = 256.7 \text{ ft}^3/\text{s} \ (7.3 \text{ m}^3/\text{s})$

Table 5.4 Hourly Distribution of Rainfall

| Total | 8 | _ | | 8 | | | | 55 | | | | <u>ج</u> | | | 8 | | | | 78 | | | | 911 | | | ٦ | 4 | | | 70 | | | | 57 | | | T | ٦ | 6.6 |
|----------|----------------|--------------|-------------------------------|----------------|--------------|---------------|--------------|----------------|--------------|---------------|---------------|----------------|--------------|--|----------------|--------------|---------------|--------------|----------------|--------------|---------------|--------------|----------------|--------------|---------------|--------------|----------------|--------------|-------------------------------|----------------------------|--------------|---------------|--------------|-------------------|--------------|-------------|---------------|----------|-------------|
| _ | _ | _ | | ╀ | | _ | _ | L | | _ | | _ | | | ╀╌ | _ | _ | _ | - | _ | _ | _ | - | | _ | 4 | | . , | _ | ┞ | _ | _ | - | L | _ | | + | - | 0 |
| 24 | 0 | 8 | 폴 o | - | 8 | <u>ĕ</u> | 0 | 0 | 55 | ğ | 0 | - : | 2 | <u> </u> | | 8 | ğ | 0 | 0 | 78 | <u>ĕ</u> | 0 | 0 | <u>=</u> | <u> </u> | ء ا | o | 4 3 | <u> </u> | 0 | <u>ج</u> | <u>=</u> | 0 | • • | - | <u> </u> | | 2 | ŏ |
| 23 | 0 | ጽ | <u>8</u> • | 0 | 69 | 8 | 0 | 0 | 25 | 8 | 0 | 0 | 3 | <u>8</u> - | 2 | 8 | 9 | 4.5453 | 0 | 78 | 8 | 0 | 0 | 116 | 8 € | 0 | 0 | 4 5 | 3 ∘ | 0 | \$ | 8 | 0 | 0 | 2 | 8 | 0 | 7 | <u>8</u> |
| 22 | 0 | 8 | <u>8</u> 0 | 0 | 8 | 9 | 0 | 0 | 55 | 8 | 0 | 0 | S | <u>8</u> 0 | 0 | 63 | 95.455 | 0 | 0 | 78 | 8 | 0 | 0 | 116 | 8 | ٥ | 0 | ₹ 5 | 3 ≎ | 0 | 8 | 8 | 0 | O. | 5 | 8 | ٥ | ٥ | 99.545 |
| 21 | 0 | 8 | <u> </u> | 0 | \$ | 8 | 0 | 0 | 2 | 8 | 0 | 0 | 3 | <u> </u> | 0 | 63 | 5.455 | • | 0 | % | 8 | 0 | 0 | 116 | 8 | 5 | 0 | * 5 | 3 ∘ | ٥ | 62 | 8 | • | 0 | 5 | 8 | 0 | - | 25.52 |
| _ | \vdash | | <u>8</u> 0 | ╀ | | | | ⊢ | | | - | _ | _ | | ╂╌ | | | _ | | | _ | _ | ⊢ | | | ┪ | | | | ⊢ | | | ⊣ | _ | | | | 3/88 | 39.545 |
| <u> </u> | ┢ | | <u>8</u> - | ╆ | | | _ | ⊢ | | | - | | | | ╆ | | Ξ | | ⊢ | | | _ | - | | | + | _ | | | t- | _ | • | _ | - | | | -+ | 2 | 6.167 |
| \vdash | Н | | § • | ✝ | | | | Н | | | _ | | _ | | †- | _ | _ | | 1- | | | _ | | | | ┪ | _ | | | †- | | | | | | | - 1 | 7 | 9.167 |
| _ | ▙ | | <u>8</u> 0 | ╄ | | | _ | ⊢ | | | - | _ | | | +- | | | | ŀ– | _ | | _ | Н | _ | | 4 | _ | | | ₽ | _ | | _ | _ | | | -+- | 555 | 9.076 |
| | 1 | | <u> </u> | 1 | | | | Г | | 61 | 4 | | | | Т | | C) | 00 | Г | | | | Г | | | 7 | | | | Т | | | | _ | | | | 2 X | 8.742 9 |
| | ├- | _ | <u> </u> | ۲ | | | | ⊢ | | 100 | - | | | _ | ۲ | | ** | 90 | - | | | - | - | | | + | | | | ┢ | | | - | - | | | ٦, | 7 1777 | 5.803 9 |
| | - | - | <u> </u> | t | | | | Н | | _ | ~ | | | _ | ۲ | | - | - | ┝ | | | | - | | | - | | | _ | ╁╌ | | | - | - | _ | | -1. | 2 | 2.561 9 |
| - | } | | <u></u> | ╂╼ | - | - | - | ⊦− | | | _ | _ | | | ╁ | | | | ⊢ | | | | - | | | -+ | | | _ | ╀┈ | | | | - | | | - | 2,78 | 6 699.1 |
| \vdash | - | _ | 80 | † | | | _ | - | | | | - | | | + | | | _ | Н | | | | ┢ | | _ | =† | _ | _ | | ┢╌ | | | _ | | | | -1. | 7 | 0.28 9 |
| - | Н | | <u> </u> | †- | | _ | - | - | _ | ~ | 6 | $\overline{}$ | | _ | t | | 9 | CI | Н | | | | Н | _ | 9 (| , | _ | _ | _ | | _ | | _ | | | | ٦, | <u>*</u> | 3.184 |
| | ⊢ | | <u> </u> | ╁╌ | | | _ | ۱- | | _ | | - | | | ╈ | | _ | | ┥ | | | _ | - | | _ | =+ | | | | t- | | _ | | - | _ | | ۲. | 4 | 5.705 83 |
| - | ├ | _ | <u>8</u> • | +- | | | _ | ⊦− | | | \neg | _ | | | + | | | | ⊢ | | | | - | _ | | -+ | | | _ | +- | | _ | _ | | | | \rightarrow | 0787 | 8.291 8 |
| _ | ⊢ | | 80 | ╀ | | - | | ⊢ | | | _ | _ | _ | | +- | _ | | _ | ⊢ | _ | | - | ⊢ | _ | | + | _ | | | ⊢ | _ | _ | _ | _ | _ | | - | 287 | 5.263 7 |
| 7 | 1 | <u>۾</u> | _ | T | \$ 45 | 64.493 6 | | - | | 4.5455 | $\overline{}$ | | | 98.182 9 | +- | • | 8 | _ | 75. | | ~ | 43.59 8 | Ι. | | 83.621 | 7 | | ; | 3.3514 5 | T | 4 | 97.468 9 | 0 | | | 8 6 | ŀ | 2.5897 | 72.834 7 |
| . 9 | - | 8 | | | 40.5 | 58.696 | | Г | cı | 3.6364 4 | 0 0 | 0 | | 26.38 20.00 | 0 | 5 | 7.5758 7. | 0 | <u>ا</u> | | | ۲, | ┝ | | | 3.0172 | | • | 1.3514 | 36.5 | 11 | | 46.203 | <u>~</u> | | | 31.579 | _ | 67.444 7 |
| | C1 | 2 | % 4 | 2 | 38.5 | 55.797 5 | | 0.5 | CI | _ | 16060 | 52 | _ | 8 3 2 3 3 3 | - | ٠. | 82 | • | - | ۶ì | | 10.256 3 | 91 | | | - | 0.5 | | 0.6757 | 0 | 40.5 | \$1.266 | _ | • | | | _ | | 58.355 6 |
| 4 | _ | 47 | まゃ | 02 | 33 | 53.623 5 | | H | 5. | _ | 0.9091 0. | 0 | _ | 9 2 8 18 2 0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | - | · · | 7.5758 7. | • | ├ | 7 | | 8.9744 10 | 13 | | | , | _ | _ | 0.6757 | 20 | 40.5 | | 0.6329 | _ | | _ | - | - | 44.14 |
| 3 | 1.5 | 46 | ۲ ۳ ۲۵ ۳ | 77 | 77 | 39.13 | | 0.5 | _ | | 0 0001 | 0 | | 0 1.8182 | 5 | 5 | 7.5758 7 | 2.2727 | H | 4 | 5 | 0 | ┝ | _ | | =† | C1 . | | 2.7027 | ┝ | \$ | - | 2.5316 0 | _ | _ | | 1.754 | | 40.076 |
| 2 | 1.5 | | <u></u> | | ę | 4.3478 3 | - | ┞ | 0.5 | 0.9091 | 0 | 0 | _ | 0 1.8182 | 25 | 3.5 | _ | 3.7879 2 | - | 7 | 17.949 I | • | 32 | | | اه | - 52 | | 33.784 | - | 38 | = | Н | ۔ ۔ | | | 40.351 | | 35.194 4 |
| - | £3 | £ | % % | _ | | 4.3478 4. | _ | ┞ | 50 | | 0.9091 | | _ | 1.8182 1. | - | | 1.5152 5 | 5152 3 | 4 | 7 | | 17.949 | 31 | | | 4 | _ | | 47.297 | ├ | 200 | _ | 48.101 | vs. | | | - | | 24 343 |
| _ | mm/h) | ation | Total | - Form | ution | | · | L, | _ | 큠 | $\overline{}$ | mm/h. | | | ╀- | tion | - | [B] | mm | ation | | _ | Ļ | | | _ | Z | | | L, | | | _ | mm/h | | | _ | 1 | |
| Time | Rainfall (mm/h | Accumulation | Accum / Total Rain / Total | Rainfall (mm/h | Accumulation | Accum / Total | Rain / Total | Rainfall (mm/h | Accumulation | Accum / Total | Rain / Total | Rainfall (mm/h | Accumulation | Accum / Total Rain / Total | Rainfall (mm/h | Accumulation | Accum / Total | Rain / Total | Rainfall (mm/h | Accumulation | Accum / Total | Rain / Total | Rainfall (mm/h | Accumulation | Accum / Total | Kain / Total | Rainfall (mm/h | Accumulation | Accum / 10tal Rain / Total | Rainfall (| Accumulation | Accum / Total | Rain / Total | Rainfall (| Accumulation | Accum/Total | Rain / 10 | | |
| F | I. Mega | | | 2. Malano | | | | 3. Malano | (9494) | | - | | (13-10-91) | , | S. Klamono | | | | ě | | | | ouc | (6-6-92) | | 7 | _ | (11-10-92) | | 9. Klamabon Rainfail (mm/h | 14-3-94) | <u></u> - | | kodu | 4493) | | | K/I Ave | Ave. Accum. |
| 1 | | 4 | | ۲ | Ξ | | | €. | 9 | | | 4. | 9 | | 2 | 3 | | | 6 | ÷ | | | 2 | ē | | | œ | Ξ. | | 6 | 5 | | | ġ | ₹ | | | 2 | ź |

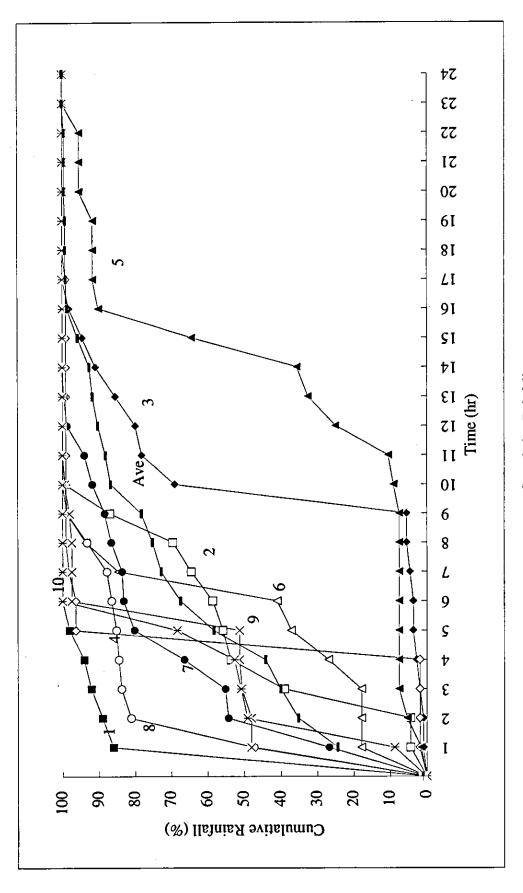


Fig. 5.3 Cumulative Rainfall

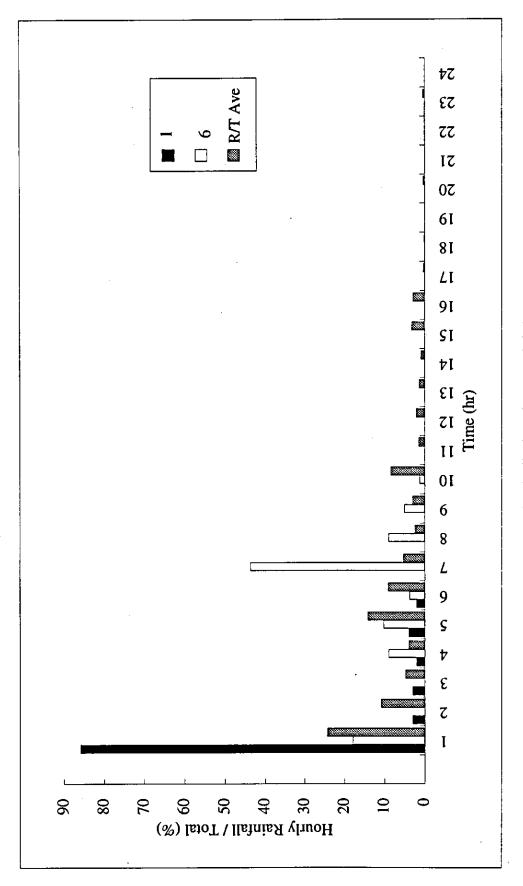
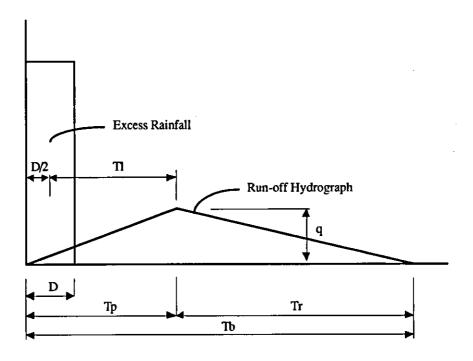


Fig. 5.4 Hourly Distribution of 24hrs Rainfall

However, Tc = 68.8 hrs seems too long since it means that the mean velocity is only 0.77 m/s. It is estimated, from the data shown in the Pre-F/S Report and the discharge measurements during this F/S, that the mean velocity (Vm) during the flood is more than 1.2 m/s. Assuming that Vm = 1.5 m/s, Tc becomes 35.2 hrs and consequently, Tp, Tb and q are obtained as follows:

Tp = 21.6 hrs, Tb = 57.7 hrs,
$$q = 497 \text{ ft}^3/\text{s} (14.1 \text{ m}^3/\text{s})$$

The above figures appear more reasonable than the previous ones. Therefore, these were used for the estimation of the design flood.



- Q: Total runoff in inches
- q: Peak rate (ft 3/s)
- D: Rainfall excess period, hours
- T1: Lag, time from center of excess rainfall to time of peak (hours) = 0.6Tc
- Tc: Time of concentration Travel time of water from hydraulically most distant point to point of interest (hours)
- Tb: Time base of hydrograph (hours) = 2.67Tp
- H: Elevation difference in feet
- L: Length of longest watercourse in miles
- A: Total area of basin in square miles

$$Tc = \left(\frac{11.9L^3}{H}\right)^{0.385}$$

$$Tp = D/2 + 0.6Tc$$

$$q = \frac{484AQ}{Tp}$$

Fig. 5.5 Concept of Triangular Hydrograph

(2) Design flood

For the basic design of the spillway and diversion, the probable floods with return periods of 200 years for a concrete dam, 1000 years for a fill dam and 5 years for a diversion channel were estimated.

200 year flood

An areal rainfall with a return period of 200 years is 170 mm/day according to the study in Section 5.1. This was converted to hourly rainfall by using Figs. 5.3 and 5.4, and consequently, Figs. 5.6 and 5.7 were obtained. Furthermore, from the rainfall in these figures, the loss caused by infiltration and evapotranspiration was deducted to obtain the effective rainfall which produces run-off.

The SCS's guide provides a means whereby an engineer may obtain an estimation of direct run-off from a given amount of rainfall. For obtaining this it is firstly necessary to examine the hydrologic conditions.

Assumptions:

1) Hydrologic soil group --- "C"

Soils having slow infiltration rates when thoroughly wetted.

2) Hydrologic condition class of a forest area --- "IV~V"

Since the drainage area is covered by dense forest and its natural conditions are well preserved, it is assumed that humus is kept in a loose condition with a deep thickness.

From these assumptions, the run-off curve number was estimated as approximately 60.

This is the curve number for the average moisture condition of the drainage area. Since antecedent rainfall is expected prior to the occurrence of the design storm, the curve number should be increased to 78 in accordance with the SCS's guide. The effective rainfall, as referred to in Figs. 5.8 and 5.9, was obtained by using the curve number 78 in Fig. 5.10.

By means of the triangular hydrograph, the flood hydrographs were obtained for the two cases as shown in Figs. 5.11 and 5.12. For the basic design of the spillway, the peak discharge is to be increased by 20%.

Design Flood = $1,740 \times 1.2 \approx 2,100 \text{ m}^3/\text{s}$

For other return periods

By the same procedure as mentioned above, the probable flood discharges for various return periods were estimated as summarized in Table 5.5, Figs. 5.13 and 5.14.

Table 5.5 Probable Flood

| | 1 | | | | | (m^3/s) |
|----------|-----|-----|-------|-------|-------|-----------|
| T (year) | 5 | 10 | 100 | 200 | 300 | 1,000 |
| Case-1 | 778 | 944 | 1,561 | 1,740 | 1,849 | 2,167 |
| Case-2 | 749 | 914 | 1,539 | 1,703 | 1,839 | 2,126 |

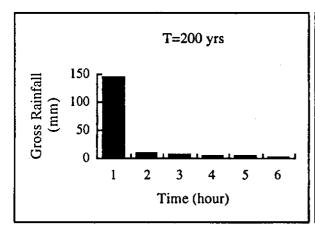
Table 5.6 Design Flood

| | 1 | | | (m ³ /s) |) |
|---|--------------|-----|-------|---------------------|---|
| _ | T (year) | 5 | 200 | 1,000 | |
| | Design Flood | 800 | 2,100 | 2,600 | |

(3) Examination of the design flood for the spillway

Fig. 5.15 shows the curves obtained by Creager's equation, on which the design flood with a 200 year return period estimated above is plotted together with the design floods for several dams in Indonesia. Although it can be seen that all of these lie close to the curves for C = 30 and C = 60, the design flood for the Warsamson HEPP lies on the lower side compared with the others. This seems quite reasonable considering the particular characteristics of the drainage area.

The flood analysis was carried out with many assumptions because of insufficient data. For a review or further study on the flood, it is of vital importance to continuously collect hydrological data for a long period of time in the catchment area.



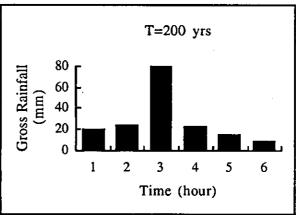
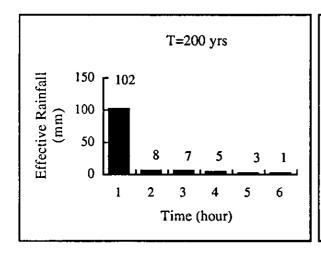


Fig. 5.6 Gross Rainfall (Case-1)

Fig. 5.7 Gross Rainfall (Case-2)



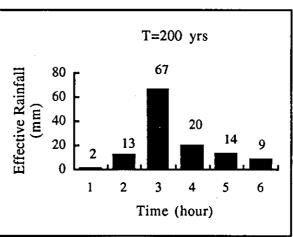
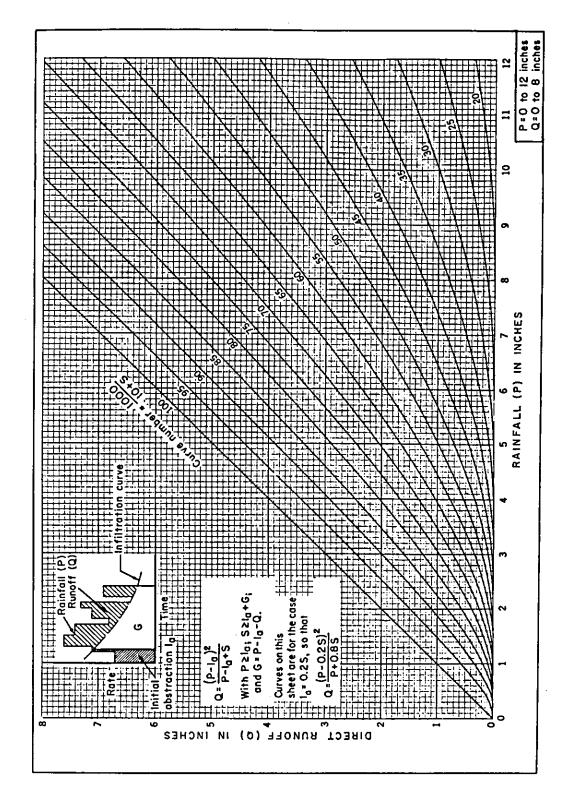


Fig. 5.8 Effective Rainfall (Case-1)

Fig. 5.9 Effective Rainfall (Case-2)



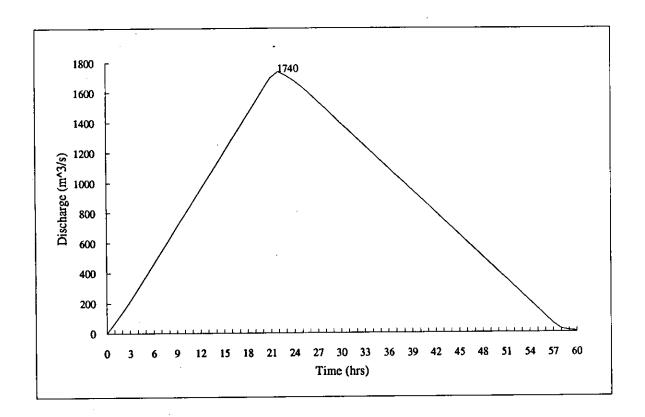


Fig. 5.11 Hydrograph for T=200 yrs (Case-1)

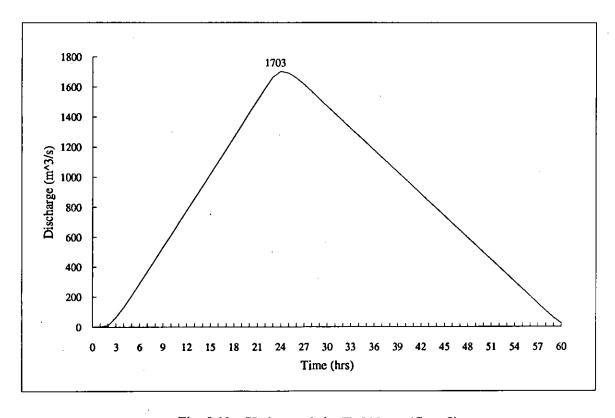


Fig. 5.12 Hydrograph for T=200 yrs (Case-2)

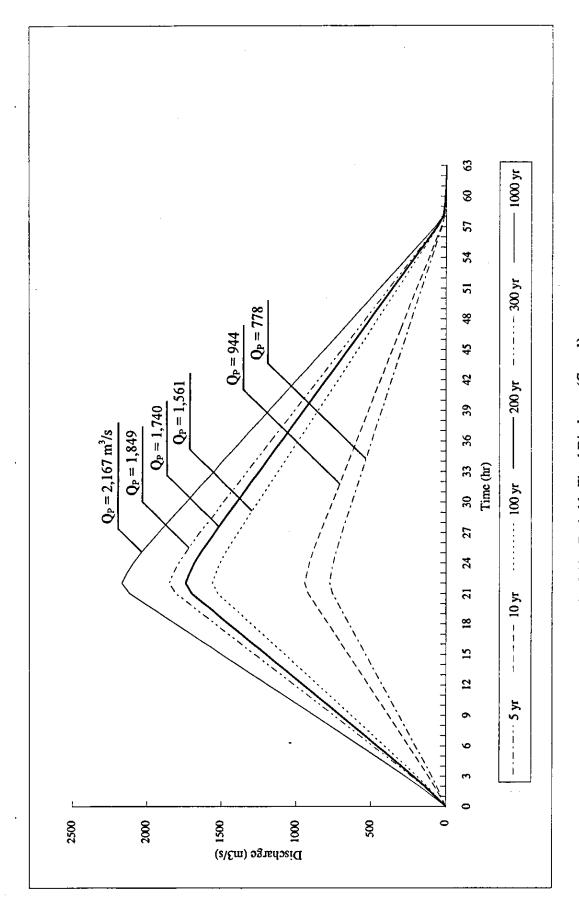


Fig. 5.13 Probable Flood Discharge (Case-1)

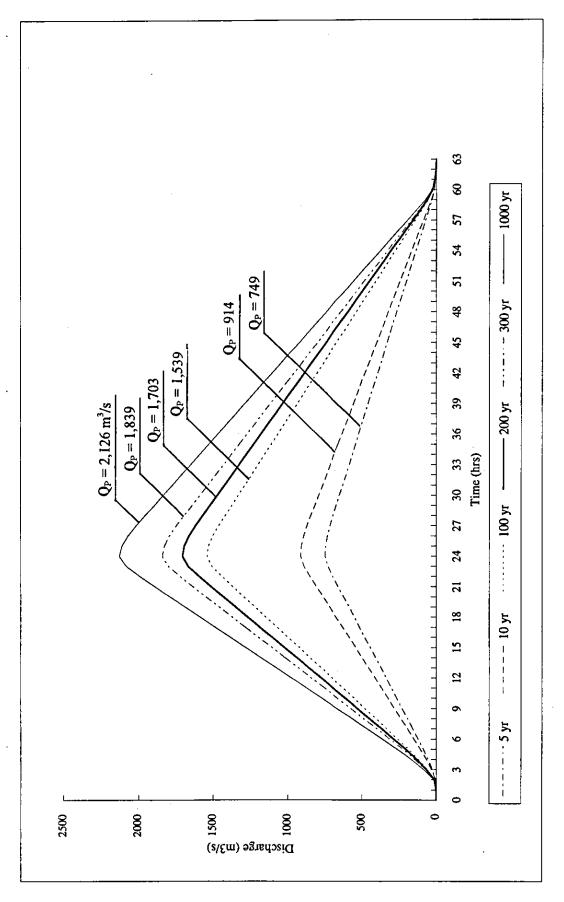


Fig. 5.14 Probable Flood Discharge (Case-2)

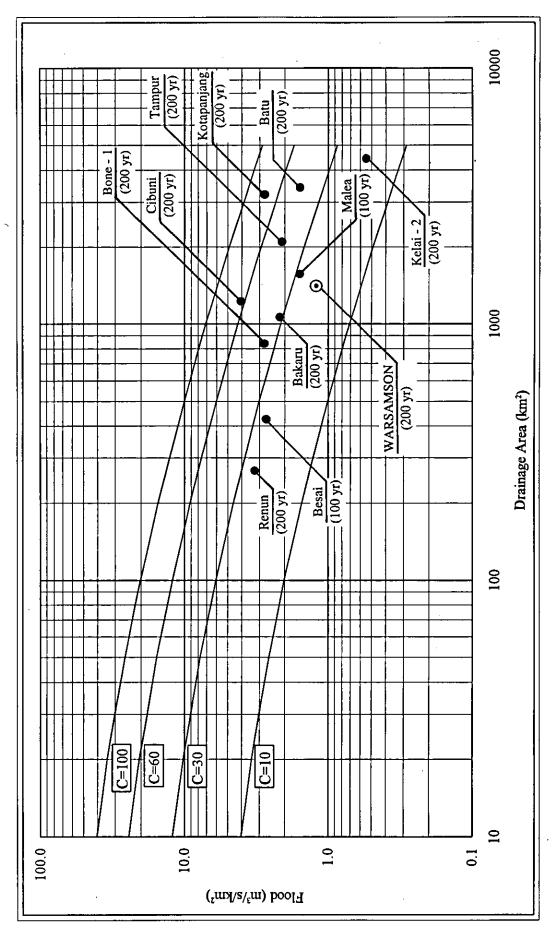


Fig. 5.15 Curves from Creager's Equation

CHAPTER 6 STUDY ON SEDIMENTATION

6.1 Suspended Load

During this F/S, suspended loads were measured at Malano AWLR by PLN, results of which are exhibited in Appendix E. Fig. 6.1 shows the suspended load discharge toward river flow. As can be seen in this figure, points are scattered at random and a good correlation of the two parameters cannot be obtained. It is considered that this was caused by the following reasons;

- 1) In the catchment area, the downstream and the most upstream areas are very hilly but the middlestream area has relatively flat features. In addition, there are variable geological conditions (surface soil) and land cover (vegetation). Therefore, even if sediment load is measured at the same flow, the amount of sediment load produced by erosion varies depending on where the rain falls.
- 2) Extremely high suspended load contents were obtained in a low-flow period from Feb. 3 to Apr. 20, 1995 as seen in Table E.1 of Appendix E. This was probably caused by improper sampling of water, that is to say, samples contained not only suspended load but also a large amount of bed load material.

From the above reasons, after rejecting abnormal and unreliable data, be correlation between suspended load and river flow was re-examined as shown in Table 6.1 and Fig. 6.2. As a result, the following equation was obtained:

$$Qs = 0.000301 \ Q^{2.01}$$

where,

Os: Suspended load discharge (kg/s)

Q: River flow (m³/s)

An annual total of suspended load was calculated using the above equation and the estimated monthly river flow shown in Table 4.3.

Table 6.2 shows that the annual average of suspended load is calculated as 54,347 t/year which is equivalent to about 41,805 m³/year assuming a density of sediment of 1.3 t/m³. It is considered that this figure is low for the catchment area of 1,460 km², and therefore, it is necessary to increase this figure to determine a design sedimentation rate.

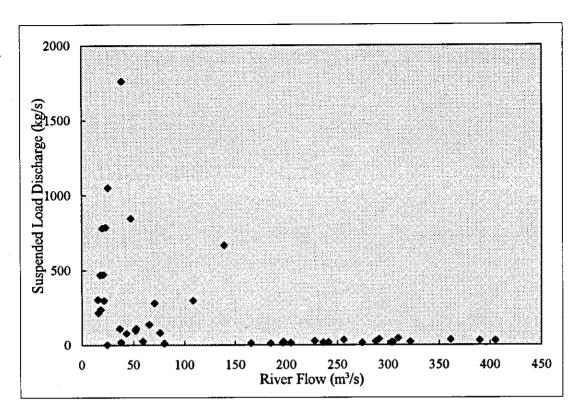


Fig. 6.1 Results of Suspended Load Measurement

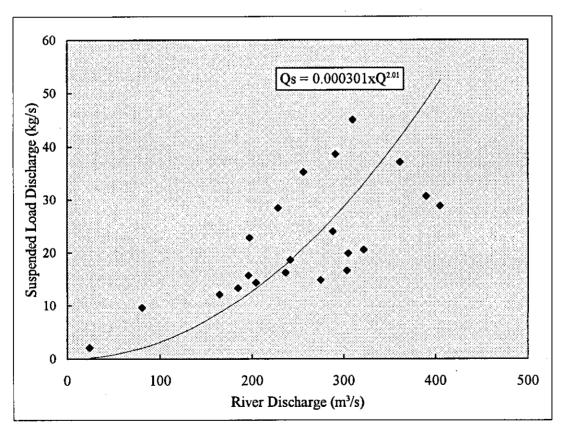


Fig. 6.2 Suspended Load Rating Curve

Table 6.1 Results of Suspended Load Measurement

| No. | Date | Time | Position | Measured S.S Contents (mg/l) | Ave. S.S Contents (mg/l) | Flow (m³/s) | Suspended Load Discharge (kg/s) |
|-----|-----------|-------|-------------------------|---------------------------------|-----------------------------|----------------|------------------------------------|
| 1 | 1-Apr-95 | 11:45 | left middle right | 82.0 150.0 30.0 | 87.3 | 24.34 | 2.1 |
| 2 | 10-Apr-95 | 11:15 | left middle right | 68.0 180.0 112.0 | 120.0 | 80.41 | 9.6 |
| 3 | 7-Aug-95 | 15:28 | left middle right | 86.0 88.0 76.0 | 83.3 | 287.97 | 24.0 |
| 4 | 15-Aug-95 | 12:00 | left middle right | 80.0 70.0 70.0 | | 165.18 | 12.1 |
| 5 | 16-Aug-95 | 15:15 | left middle right | 88.0 84.0 68.0 | | 196.29 | 15.7 |
| 6 | 18-Aug-95 | 17:05 | left middle right | 60.0 66.0 80.0 | 68.7 | 236.25 | 16.2 |
| 7 | 19-Aug-95 | 16:05 | left middle right | 122.0 88.0 98.0 | 102.7 | 361.32 | 37.1 |
| 8 | 21-Aug-95 | 15:30 | left middle right | 76.0 108.0 190.0 | 124.7 | 228.24 | 28.5 |
| 9 | 22-Aug-95 | 10:28 | left middle right | 80.0 84.0 72.0 | 78.7 | 389.73 | 30.7 |
| 10 | 23-Aug-95 | 10:00 | left middle right | 64.0 76.0 92.0 | 77.3 | 241.20 | 18.7 |
| 11 | 24-Aug-95 | 12:32 | left middle right | 89.0 226.0 32.0 | 115.7 | 197.26 | 22.8 |
| 12 | 25-Aug-95 | 11:15 | left middle right | 64.0 82.0 70.0 | 72.0 | 184.66 | 13.3 |

| | | | left | 84.0 | (5.0 | 204.54 | 10.0 |
|-----|-----------|-------|--------|-------|-------|--------|------|
| 13 | 26-Aug-95 | 11:05 | middle | 98.0 | 65.3 | 304.74 | 19.9 |
| | | | right | 14.0 | | | |
| | | | left | 82.0 | | | _ |
| 14 | 27-Aug-95 | 11:10 | middle | 36.0 | 54.0 | 274.57 | 14.8 |
| | | | right | 44.0 | | | |
| | | | left | 82.0 | | | |
| 15 | 29-Aug-95 | 12:15 | middle | 76.0 | 71.3 | 404.91 | 28.9 |
| | | | right | 56.0 | | | |
| | | | left | 48.0 | | | |
| 16 | 30-Aug-95 | 12:30 | middle | 68.0 | 64.0 | 321.67 | 20.6 |
| | | | right | 76.0 | | | |
| | | | left | 80.0 | | | |
| 17 | 31-Aug-95 | 11:45 | middle | 78.0 | 70.0 | 204.29 | 14.3 |
| | | • | right | 52.0 | | | |
| | | | left | 52.0 | | | |
| 18 | 1-Sep-95 | 14:50 | middle | 56.0 | 54.7 | 303.47 | 16.6 |
| ļ l | | | right | 56.0 | | | |
| | | | left | 158.0 | | | |
| 19 | 2-Sep-95 | 12:10 | middle | 156.0 | 132.7 | 291.10 | 38.6 |
| : | | | right | 84.0 | | | |
| | | | left | 138.0 | · | | |
| 20 | 3-Sep-95 | 12:50 | middle | 150.0 | 145.3 | 309.72 | 45.0 |
| | | | right | 148.0 | | | |
| | - | | left | 132.0 | , , | | |
| 21 | 4-Sep-95 | 11:10 | middle | 134.0 | 137.3 | 256.44 | 35.2 |
| | | • | right | 146.0 | | | |

Table 6.2 Estimated Suspended Load at Dam Site

| | | | | | | | | | | (ton) | | | |
|--------------|----------------|--------------|----------------|-----------------|------------------|----------------------|-----------------|-----------------|------------------|----------------|----------------|----------------|------------------|
| Year | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | Total |
| 1920 | 222 | 237 | 457 | 12,230 | 969 | 16,916 | 849 | 1,884 | 4,068 | 3,811 | 1,170 | 124 | 42,937 |
| 1921 | 3,302 | 3,077 | 8,446 | 7,711 | 4,763 | 4,817 | 6,575 | 3,537 | | 670 | 4,068 | 5,823 | 65,942 |
| 1922 | 1,306 | 5,912 | 1,436 | 6,219 | 1,082 | 6,923 | 7,723 | 4,798 | 3,473 | 2,419 | 440 | 1,973 | 43,703 |
| 1923 | 11,451 | 3,048 | 3,273 | 5,439 | 1,552 | 1,903 | 923 | 5 100 | 1,034 | 791 | 179 | 3,507 | 33,107 |
| 1924 | 1,324 | 7,612 | 3,302 | 3,503 | 9,841 | 4,134 | 19,962 | 5,483 | 9,364 | 2,569 | 6,422 | 2,910 | |
| 1925 | 2,394 | 4,902 | 3,749 | 2,227 | 7,244 | 6,300 | 4,225 | 7,373 | 3,008 | 18 | 789 | 2,646 | 44,874 |
| 1926 1927 | 1,183 | 427 686 | 1,165 4,456 | 7,443 4,200 | 14,977 10,347 | 6,838 12,978 | 16,689 9,300 | 4,868 893 | 27,289 21,303 | 1,995 1,906 | 4,503 3,844 | 2,965 | 90,343 74,020 |
| 1927 | 3,302 763 | 2,039 | 3,075 | 3,780 | 6,989 | 6,670 | 3,967 | 2,724 | 1,772 | 200 | 2,252 | 806 2,777 | 37,009 |
| 1929 | 2,370 | 254 | 5,939 | 5,215 | 17,480 | 14,355 | 3,448 | 1,217 | 3,594 | 2,017 | 1,772 | 954 | 58,614 |
| 1930 | 229 | 1,677 | 10,347 | 1,971 | 2,672 | 24,243 | 48 | 35 | 14 | 12,555 | 1,465 | 1,436 | 56,692 |
| 1931 | 3,657 | 177 | 683 | 5,364 | 19,962 | 29,362 | 12,330 | 1,098 | 6,546 | 1,572 | 1,605 | 1,288 | 83,644 |
| 1932 | 736 | 1,639 | 3,302 | 3,208 | 6,822 | 2,682 | 17,280 | 9,643 | 2,276 | 9,742 | 2,016 | 4,257 | 63,602 |
| 1933 | 2,493 | 3,225 | 1,306 | 1,564 | 3,103 | 5,591 | 8,868 | 8,262 | 19,188 | 3,187 | 818 | 2,202 | 59,808 |
| 1934 | 5,823 | 2,017 | 5,633 | 4,036 | 5,861 | 12,861 | 13,828 | 10,709 | 5,105 | 15,474 | 7,801 | 4,127 | 93,274 |
| 1935 | 2,419 | 335 | 2,698 | 2,870 | 12,611 | 15,290 | 3,999 | 10,553 | 1,881 | 17,016 | 3,939 | 2,109 | 75,720 |
| 1936 | 4,660 | 4,695 | 9,692 | 5,141 | 5,861 | 5,783 | 14,306 | 2,493 | 6,138 | 16,950 | 340 | 1,906 | 77,967 |
| 1937 | 3,688 | 2,519 | 6,905 | 4,036 | 6,332 | 13,095 | 8,868 | 2,698 | 17,931 | 7,900 | 4,367 | 849 | 79,187 |
| 1938 | 2,225 | 555 | 4,127 | 2,682 | 7,723 | 3,266 | 6,016 | 32,729 | 10,173 | 3,904 | 1,666 | 8,446 | 83,513 |
| 1939 | 2,777 | 2,261 | 490 | 7,009 | 6,213 | 11,615 | 1,324 | 535 | 1,018 | 51 | 2,980 | 9 | 36,282 |
| 1940 | 2,777 | 3,201 | 2,883 | 2,897 | 4,833 | 6,670 | 136 | 14,792 | 1,564 | 148 | 1,350 | 763 | 42,015 |
| 1941 1958 | 969 113 | 144 555 | 1,165 2,394 | 6,670 | 24,469 2,063 | 101 2, 349 | 479 985 | 2,040 | 2,180 | 2,544 1,995 | 2,109 | 1,884 | 44,754 32,476 |
| 1959 | 2,646 | 184 | 723 | 1,332 6,712 | 16,819 | 2,349 18,484 | 11,559 | 14,792 2,040 | 1,564 2,180 | 4,356 | 1,687 3,875 | 2,646 1,884 | 71,463 |
| 1960 | 5,823 | 1,703 | 607 | 2,399 | 6,253 | 3,208 | 47,877 | 777 | 2,374 | 512 | 2,870 | 2,040 | 76,442 |
| 1961 | 969 | 2,875 | 2,965 | 2,500 | 1,253 | 4,572 | 7,590 | 820 | 1,313 | 277 | 1,388 | 1,735 | 28,257 |
| 1962 | 10,866 | 3,048 | 1,049 | 9,513 | 10,245 | 7,095 | 1,398 | 8,868 | 1,187 | 4,626 | 1,034 | 3,331 | 62,259 |
| 1963 | 4,903 | 3,953 | 2,109 | 4,200 | 18,977 | 3,718 | 5,900 | 1,115 | 65 | 63 | 440 | 3,597 | 49,038 |
| 1964 | 806 | 5,473 | 1,017 | 11,893 | 3,273 | 6,179 | 4,524 | 1,361 | 818 | 2,063 | 1,751 | 6,016 | 45,172 |
| 1965 | 4,833 | 42 | 1,361 | 5,861 | 5,335 | 6,587 | 27 | 79 | 1 | 1,098 | 4,200 | 3,047 | 32,472 |
| 1966 | 1,049 | 1,408 | 1,235 | 1,222 | 5,746 | 4,340 | 2,345 | 11,024 | 3,093 | 1,270 | 3,875 | 3,216 | 39,824 |
| 1967 | 7,031 | 1,509 | 395 | 4,746 | 9,992 | 5,706 | 7,767 | 632 | 179 | 1,841 | 1,034 | 820 | 41,651 |
| 1968 | 1,065 | 245 | 7,945 | 666 | 1,798 | 13,330 | 7,590 | 2,646 | 7,061 | 3,873 | 9,216 | 4,660 | 60,095 |
| 1969 | 1,235 | 170 | 10,605 | 2,227 | 21,046 | 3,718 | 14,731 | 6,055 | 614 | 7,678 | 4,333 | 1,673 | 74,087 |
| 1970 | 2,345 | 1,109 | 3,688 | 4,888 | 21,561 | 2,953 | 13,358 | 7,723 | 3,749 | 938 | 2,577 | 4,192 | 69,081 |
| 1971 | 2,777 | 2,847 | 1,183 | 2,374 | 14,427 | 11,232 | 5,408 | 11,997 | 6,504 | 7,287 | 2,500 | 791 | 69,326 |
| 1972 | 1,694 5,408 | 5,171 | 1,115 | 1,772 | 1,735 | 17,049 7,095 | 285 3,597 | 1,398 | 666 | 67 | 1,524 | 547 | 33,022 |
| 1973 1974 | 173 | 846 6,411 | 3,360 607 | 16,066 9,118 | 7,990 11,997 | 6,179 | 4,160 | 8,400 3,159 | 3,718 5,215 | 1,653 2,750 | 409 2,109 | 142 1,884 | 58,683 53,760 |
| 1975 | 1,552 | 846 | 1,115 | 4,996 | 7,900 | 6,300 | 3,360 | 5,081 | 7,711 | 1,288 | 1,034 | 3,873 | 45,056 |
| 1976 | 763 | 3,120 | 683 | 1,859 | 6,575 | 970 | 1,820 | 2,321 | 990 | 6,373 | 1,881 | 89 | 27,443 |
| 1977 | 908 | 2,337 | 4,225 | 5,032 | 5,225 | 13,747 | 1,217 | 2,040 | 1,729 | 3,020 | 1,569 | 1,884 | 42,933 |
| 1978 | 4,390 | 177 | 17,680 | 1,018 | 1,306 | 6,796 | 10,399 | 5,900 | 5,439 | 709 | 2,708 | 4,592 | 61,114 |
| 1979 | 179 | 593 | 3,904 | 4,996 | 2,620 | 17,657 | 582 | 311 | 16,783 | 347 | 4,003 | 2,063 | 54,039 |
| 1980 | 1,417 | 1,316 | 523 | 3,503 | 4,729 | 2,925 | 723 | 2,225 | 20 | 1,632 | 1,135 | 426 | 20,575 |
| 1981 | 1,714 | 632 | 3,187 | 1,948 | 10,502 | 804 | 11,887 | 84 | 5,822 | 113 | 1,465 | 1,973 | 40,131 |
| 1982 | 1,200 | 941 | 4,558 | 2,424 | 7,031 | 4,367 | - | - | 5,476 | 893 | 484 | 2,202 | 35,490 |
| 1983 | 3,873 | 74 | 376 | 2,227 | 15,162 | 11,450 | 10,971 | 17,546 | 17,657 | 12,555 | 1,350 | 2,155 | 95,397 |
| 1984 | 3,273 | 4,484 | 2,937 | 9,713 | 31,912 | 8,972 | 34,394 | 3,216 | 21,453 | 683 | 986 | 1,494 | 123,517 |
| 1985 | 1,217 | 8,412 | 229 | 1,426 | 18,908 | 8,028 | 3,627 | 5,298 | 7,312 | 4,063 | 3,503 | 2,569 | 64,593 |
| 1986 | 570 | 1,634 | 1,612 | 1,295 | 1,417 | 3,354 | 3,360 | 186 | 4,641 | 2,965 | 804 | 2,086 | 23,923 |
| 1987 | 1,235 | 22 | 3,020 | 706 | 6,822 | 1,426 | 84 | 1,082 | 214 | 6,657 | 2,276 | 512 | 24,054 |
| 1988 | 2,569 | 1,139 | 2,672 | 495 | 6,989 | 6,629 | 15,287 | 30,838 | 6,881 | 4,729 | 3,443 | 3,657 | 85,328 48,904 |
| 1989 | 938 558 | 2,466 | 5,081 | 6,098 | 48 3,020 | 3,971 | 6,095 1,950 | 5,262 | 4,469 3,718 | 9,692 | 4,101 269 | 683 294 | 48,904 25,229 |
| 1990 1991 | 5,861 | 924 742 | 1,001 3,448 | 1,084 1,564 | 3,020 21,266 | 1,152 2,276 | 2,750 | 1,115 71 | 3,/18 1 | 10,143 750 | 269 | 5,045 | 43,781 |
| 1991 | 16 | 164 | 1,270 | 640 | 4,390 | 1,187 | 2,730 | 644 | 2,475 | 11,613 | 986 | 849 | 26,506 |
| 1993 | 763 | 893 | 750 | 2,735 | 8,171 | 1,187 | 5,408 | 130 | 6,340 | 501 | 1,222 | 777 | 28,878 |
| 1994 | 763 | 1,787 | 3,418 | 3,383 | 7,158 | 6,881 | 214 | 1,165 | 0,70 | 2,273 | 2,349 | 320 | 29,024 |
| 4//7 | , , , | 2,707 | 2,710 | 2,000 | .,255 | -,1 | | -, | | | • | | _ |
| | | | | | | | | | | Anı | ual Aver | age | 54,347 |

6.2 Bed Load

Since a measurement of bed load had not been carried out, it was estimated by using the Kalinske-Brown formula. Assuming the river section is rectangular,

$$QB = qBW = 10 \{u^2/(s-1) \text{ gd }\}^2 \text{ udW}$$
(6.2.1)

where,

QB: Bed load discharge (m³/s)

qB: Bed load discharge per unit width (m³/s/m)

u : Friction velocity (m/s) $\Rightarrow \sqrt{gHmi}$

g: Acceleration of gravity = $9.8 \text{ (m/s}^2)$

Hm: Water depth (m)

i : Energy slope = River bed slope

s : Specific gravity of sediment grain

d: Mean grain diameter (m)

W: River width (m)

To simplify the formula (6.2.1) and calculate QB, the following assumptions were made:

- 1) i = 1/2,000 (average river bed slope)
- 2) s = 2.65
- 3) Hm is equivalent to the water level reading (H) at Malano AWLR. Therefore, Hm can be obtained from the equations of the rating curves shown in Fig. 4.3.

$$H_{m} < 1.80 \text{ m } (Q < 108.6 \text{ m}^{3}/\text{s})$$

$$Q = 12.294 \text{ Hm}^{2} + 35.446 \text{ Hm} + 4.99$$

$$H_{m} = \frac{-35.446 + \sqrt{1011.0 + 49.176Q}}{24.588}$$
(6.2.2)

$$H_{\rm m} \ge 1.80 \text{ m } (Q \ge 108.6 \text{ m}^3/\text{s})$$

$$Q = 1.1013 \text{ Hm}^2 + 96.797 \text{ Hm} - 69.19$$

$$H_{\rm m} = \frac{-96.797 + \sqrt{9674.5 + 4.405Q}}{2.2026}$$
(6.2.3)

4) d can be derived from the study by Shields.

$$\frac{u^2}{(s-1) \text{ gd}} \doteqdot 0.05$$

$$u = \sqrt{gHmi}$$

Therefore, from 1) and 2) above,

$$d = \frac{20 \text{ Hmi}}{\text{s-1}} = 6.06 \text{ Hm x } 10^{-3} \text{ (m)}$$
 (6.2.4)

5) W can be obtained from Manning's formula.

$$Q = WHm \times \frac{1}{n} Hm^{2/3} i^{1/2}$$

From 1) and n = 0.035,

$$W = 1.565 \, Q \, Hm^{-5/3} \tag{6.2.5}$$

From 1), 2), 4) and 5) above, the equation (6.2.1) becomes,

$$QB = 1.66 \times 10^{-5} \times QHm^{-1/6}$$
(6.2.6)

Thus, an annual total of bed load can be obtained from the equations (6.2.2), (6.2.3) and (6.2.6) and the estimated monthly river flow shown in Table 4.3.

Table 6.3 shows that the annual average bed load is 32,232 m³/year. This figure is considered to be on the high side (safe side) since it is known that the Kalinske-Brown formula generally gives a higher solution (in which part of the suspended load is included).

Since the bed load obtained above is a nominal volume of bed load material (particles), it has to be converted to a sediment volume by multiplying by 2 (unit weight of particle/unit weight of sediment = $2.65 / 1.3 \div 2$). Consequently, the annual average of sediment by bed load becomes $64,464 \text{ m}^3/\text{year}$.

6.3 Total Sediment Load (Total-Qsd)

From Section 6.1 and 6.2,

Total - Qsd =
$$41,805 + 64,464$$

= $106,269 \text{ m}^3/\text{year}$

Therefore, Total -Qsd per unit area is obtained as;

Total - Qsd' =
$$72.8 \text{ m}^3/\text{km}^2/\text{year}$$

Since an excessive sediment load discharge during a flood is not considered in the above estimation, it is necessary to increase the above Total - Qsd'. For the feasibility - grade design, it is recommended to use 100 m³/km²/year.

Table 6.3 Estimated Bed Load at Dam Site

| | | | | lable | 0.5 | esumate | a Da i | Loau at | | i, | | | |
|--------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|------------------|
| | ſ | . 1 | | | . 1 | _ | | . 1 | . 1 | _ | | (m3) | |
| Year | Jan | Feb | Mar | Арг | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | Total |
| 1920 | 893 | 880 | 1,190 | 4,711 | 1,621 | 5,442 | 1,534 | 2,142 | 2,918 | 2,891 | 1,720 | 718 | 26,659 |
| 1921 1922 | 2,719 1,836 | 2,489 3,296 | 4,075 1,910 | 3,845 3,503 | 3,182 1,696 | 3,138 3,670 | 3,656 3,920 | 2,800 3,192 | 4,866 2,727 | 1,391 2,381 | 2,918 1,149 | 3,469 2,184 | 38,547 31,463 |
| 1922 | 4,659 | 2,479 | 2,709 | 3,306 | 1,974 | 2,111 | 1,588 | 383 | 1,634 | 1,490 | 805 | 2,790 | 25,927 |
| 1924 | 1,846 | 3,751 | 2,719 | 2,737 | 4,354 | 2,938 | 5,963 | 3,380 | 4,183 | 2,443 | 3,552 | 2,576 | 40,442 |
| 1925 | 2,371 | 3,040 | 2,871 | 2,256 | 3,812 | 3,523 | 3,022 | 3,842 | 2,564 | 651 | 1,460 | 2,474 | 31,885 |
| 1926 | 1,761 | 1,090 | 1,750 | 3,787 | 5,250 | 3,650 | 5,509 | 3,211 | 6,719 | 2,194 | 3,048 | 2,597 | 40,566 |
| 1927 | 2,719 | 1,323 | 3,092 | 2,958 | 4,452 | 4,837 | 4,249 | 1,566 | 6,025 | 2,152 | 2,848 | 1,501 | 37,723 |
| 1928 | 1,468 | 2,131 | 2,637 | 2,828 | 3,754 | 3,611 | 2,941 | 2,504 | 2,048 | 858 | 2,266 | 2,525 | 29,572 |
| 1929 | 2,360 | 885 | 3,499 | 3,247 | 5,623 | 5,059 | 2,770 | 1,782 | 2,767 | 2,205 | 2,048 | 1,610 | 33,855 |
| 1930 1931 | 905 2,840 | 1,923 769 | 4,452 1,402 | 2,142 3,286 | 2,484 5,963 | 6,378 6,938 | 525 4,815 | 491 1,707 | 575 3,582 | 4,854 1,984 | 1,890 1,964 | 1,910 1,825 | 28,529 37,077 |
| 1932 | 1,446 | 1,943 | 2,719 | 2,635 | 3,715 | 2,442 | 5,594 | 4,316 | 2,277 | 4,335 | 2,163 | 3,032 | 36,617 |
| 1933 | 2,412 | 2,539 | 1,836 | 1,943 | 2,648 | 3,346 | 4,162 | 4,036 | 5,753 | 2,678 | 1,482 | 2,288 | 35,122 |
| 1934 | 3,469 | 2,079 | 3,420 | 2,908 | 3,479 | 4,818 | 5,067 | 4,521 | 3,217 | 5,327 | 3,864 | 2,991 | 45,161 |
| 1935 | 2,381 | 988 | 2,494 | 2,513 | 4,864 | 5,203 | 2,951 | 4,492 | 2,100 | 5,556 | 2,878 | 2,246 | 38,667 |
| 1936 | 3,152 | 3,044 | 4,326 | 3,227 | 3,479 | 3,395 | 5,145 | 2,412 | 3,484 | 5,547 | 1,036 | 2,152 | 40,398 |
| 1937 | 2,850 | 2,285 | 3,734 | 2,908 | 3,597 | 4,857 | 4,162 | 2,494 | 5,584 | 3,958 | 3,008 | 1,534 | 40,971 |
| 1938 | 2,298 | 1,213 | 2,991 | 2,442 | 3,920 | 2,656 | 3,518 | 7,412 | 4,339 | 2,921 | 1,995 | 4,075 | 39,780 |
| 1939 1940 | 2,525 2,525 | 2,182 2,582 | 1,224 2,566 | 3,689 2,523 | 3,568 3,201 | 4,604 3,611 | 1,846 741 | 1,269 5,222 | 1,623 1,943 | 535 765 | 2,554 1,826 | 460 | 26,079 28,974 |
| 1940 | 1,621 | 711 | 1,750 | 3,611 | 6,523 | 653 | 1,213 | 2,215 | 2,235 | 2,433 | 2,204 | 1,468 2,142 | 27,311 |
| 1958 | 694 | 1,213 | 2,371 | 1,816 | 2,225 | 2,308 | 1,632 | 5,222 | 1,943 | 2,194 | 2,006 | 2,474 | 26,096 |
| 1959 | 2,474 | 781 | 1,435 | 3,621 | 5,528 | 5,659 | 4,678 | 2,215 | 2,235 | 3,062 | 2,858 | 2,142 | 36,688 |
| 1960 | 3,469 | 1,975 | 1,336 | 2,328 | 3,577 | 2,635 | 8,751 | 1,479 | 2,318 | 1,247 | 2,513 | 2,215 | 33,843 |
| 1961 | 1,621 | 2,418 | 2,597 | 2,370 | 1,804 | 3,068 | 3,890 | 1,512 | 1,805 | 974 | 1,848 | 2,069 | 25,974 |
| 1962 | 4,551 | 2,479 | 1,675 | 4,212 | 4,433 | 3,709 | 1,889 | 4,162 | 1,730 | 3,142 | 1,634 | 2,729 | 36,343 |
| 1963 | 3,221 | 2,771 | 2,246 | 2,958 | 5,831 | 2,807 | 3,489 | 1,718 | 561 | 568 | 1,149 | 2,820 | 30,140 |
| 1964 1965 | 1,501 3,201 | 3,252 472 | 1,653 1,868 | 4,653 | 2,709 3,341 | 3,493 3,591 | 3,112 486 | 1,868 613 | 1,482 136 | 2,225 1,707 | 2,037 | 3,518 2,627 | 31,504 24,415 |
| 1966 | 1,675 | 1,786 | 1,793 | 3,415 1,752 | 3,449 | 3,000 | 2,350 | 4,580 | 2,595 | 1,707 | 2,958 2,858 | 2,688 | 30,340 |
| 1967 | 3,764 | 1,839 | 1,123 | 3,118 | 4,383 | 3,375 | 3,929 | 1,358 | 805 | 2,121 | 1,634 | 1,512 | 28,960 |
| 1968 | 1,686 | 892 | 3,968 | 1,361 | 2,100 | 4,895 | 3,890 | 2,474 | 3,701 | 2,911 | 4,154 | 3,152 | 35,184 |
| 1969 | 1,793 | 758 | 4,502 | 2,256 | 6,104 | 2,807 | 5,212 | 3,528 | 1,317 | 3,910 | 2,998 | 2,037 | 37,222 |
| 1970 | 2,350 | 1,616 | 2,850 | 3,158 | 6,169 | 2,544 | 4,990 | 3,920 | 2,817 | 1,599 | 2,400 | 3,012 | 37,425 |
| 1971 | 2,525 | 2,407 | 1,761 | 2,318 | 5,164 | 4,536 | 3,360 | 4,757 | 3,572 | 3,822 | 2,370 | 1,490 | 38,082 |
| 1972 | 2,048 | 3,173 | 1,718 | 2,048 | 2,069 | 5,461 | 986 | 1,889 | 1,361 | 579 | 1,922 | 1,280 | 24,532 |
| 1973 1974 | 3,360 | 1,443 3,413 | 2,739 1,336 | 5,319 4,135 | 3,978 4,757 | 3,709 3,493 | 2,820 3,002 | 4,065 2,668 | 2,807 3,247 | 2,026 2,515 | 1,116 2,204 | 753 2,142 | 34,136 33,723 |
| 1975 | 1,974 | 1,443 | 1,718 | 3,187 | 3,958 | 3,523 | 2,739 | 3,271 | 3,845 | 1,825 | 1,634 | 2,911 | 32,028 |
| 1976 | 1,468 | 2,554 | 1,402 | 2,090 | 3,656 | 1,590 | 2,111 | 2,340 | 1,604 | 3,607 | 2,100 | 636 | 25,158 |
| 1977 | 1,577 | 2,213 | 3,022 | 3,197 | 3,311 | 4,963 | 1,782 | 2,215 | 2,027 | 2,617 | 1,945 | 2,142 | 31,012 |
| 1978 | 3,072 | 769 | 5,651 | 1,623 | 1,836 | 3,640 | 4,462 | 3,489 | 3,306 | 1,424 | 2,452 | 3,132 | 34,856 |
| 1979 | 823 | 1,246 | 2,921 | 3,187 | 2,463 | 5,546 | 1,314 | 1,020 | 5,423 | 1,066 | 2,898 | 2,225 | 30,132 |
| 1980 | 1,900 | 1,771 | 1,258 | 2,737 | 3,172 | 2,534 | 1,435 | 2,298 | 604 | 2,016 | 1,698 | 1,157 | 22,578 |
| 1981 | 2,058 | 1,279 | 2,678 | 2,131 | 4,482 | 1,471 | 4,737 | 624 | 3,405 | 694 | 1,890 | 2,184 | 27,634 |
| 1982 1983 | 1,772 2,911 | 1,508 559 | 3,122 1,100 | 2,339 2,256 | 3,764 5,279 | 3,008 4,575 | 4,571 | 5,632 | 3,316 5,546 | 1,566 4,854 | 1,194 1,826 | 2,288 2,267 | 28,652 41,376 |
| 1984 | 2,709 | 2,984 | 2,586 | 4,251 | 7,330 | 4,106 | 7,574 | 2,688 | 6,044 | 1,402 | 1,601 | 1,942 | 45,218 |
| 1985 | 1,782 | 3,840 | 905 | 1,869 | 5,822 | 3,913 | 2,830 | 3,331 | 3,757 | 2,971 | 2,737 | 2,443 | 36,199 |
| 1986 | 1,302 | 1,902 | 2,005 | 1,794 | 1,900 | 2,686 | 2,739 | 835 | 3,088 | 2,597 | 1,471 | 2,236 | 24,555 |
| 1987 | 1,793 | 453 | 2,617 | 1,394 | 3,715 | 1,869 | 624 | 1,696 | 864 | 3,676 | 2,277 | 1,247 | 22,224 |
| 1988 | 2,443 | 1,668 | 2,484 | 1,206 | 3,754 | 3,601 | 5,298 | 7,221 | 3,660 | 3,172 | 2,716 | 2,840 | 40,062 |
| 1989 | 1,599 | 2,264 | 3,271 | 3,474 | 525 | 2,888 | 3,538 | 3,321 | 3,038 | 4,326 | 2,928 | 1,402 | 32,574 |
| 1990 | 1,291 | 1,497 | 1,642 | 1,666 | 2,617 | 1,709 | 2,173 | 1,718 | 2,807 | 4,413 | 944 | 997 | 23,476 |
| 1991 | 3,479 | 1,367 | 2,770 | 1,943 | 6,132 | 2,277 | 2,515 | 590 | 115 | 1,457 | 422 | 3,261 | 26,327 |
| 1992 1993 | 613 1,468 | 764 1,476 | 1,814 1,457 | 1,339 2,462 | 3,072 4,017 | 1,730 1,730 | 2,319 3,360 | 1,369 729 | 2,359 3,533 | 4,688 1,235 | 1,601 1,752 | 1,534 1,479 | 23,203 24,699 |
| 1993 | 601 | 1,470 | 2,759 | 2,402 | 3,793 | 3,660 | 881 | 1,750 | 0,555 | 2,319 | 2,308 | 1,031 | 23,774 |
| .//- | | . , , , , | -,,,,, | 2,070 | ٠,٠,٠,٠ | 2,000 | 551 | 2, | | -, | augl Aver | | 22,777 |

52

Annual Average

32,232

CHAPTER 7 EVAPORATION

Evaporation was measured at the Malano meteorological station established by PLN during this F/S. However, data is available for 3 months only as exhibited in Appendix C. Therefore, it was decided to estimate an evaporation rate based on the Penman-Monteith equation.

$$E_p = F_{p1}A + F_{p2}D \tag{7.1}$$

where.

Ep : evaporation rate from open water (mm/day)

F_{p1}, F_{p2}: coefficients obtained hereinbelow

A : energy available for evaporation (mm/day)

D: average vapor - pressure deficit (kPa)

(1) Fp1

$$F_{p1} = \frac{\Delta}{\Delta + \gamma} \tag{7.2}$$

$$\Delta = \frac{4,098 \times 0.6108 \exp\left(\frac{17.27T}{237.3 + T}\right)}{(237.3 + T)^2} \text{ (kPa/°C)}$$
 (7.3)

where, T is the average atmospheric air temperature in °C shown in Table C.2 of Appendix C.

$$\gamma = 0.0016286 \frac{P}{\lambda} = 0.0672 \text{ kPa/°C}$$
 (7.4)

where.

$$P = 103.1 \text{ x} \left(\frac{293 - 0.0065Z}{293}\right)^{5.256} = 102.38 \text{ kPa}$$

(Z = 60 m, elevation of water surface)

$$\lambda = 2.501 - 0.002361$$
Ts = 2.4373 MJ/kg (Ts = 27°C, water temperature)

(2) Fp2

$$F_{p2} = \frac{\gamma}{\Delta + \gamma} \times \frac{6.43 (1 + 0.536 \text{ Ua})}{\lambda} = \frac{0.4624}{\Delta + 0.0672}$$
 (7.5)

where, Ua is the average wind speed, assumed as 3.0 m/s based on the wind data in Appendix C.

(3)
$$A = (0.25 + 0.5N) \text{ So} - (0.9N + 0.1)(0.34 - 0.14 \sqrt{\text{ed}}) \sigma T^4$$
 (7.6)

where,

N: cloudiness fraction which is expressed as "Sunshine" in Table C.2 of Appendix C. Since "Sunshine" in the table does not consider rainy days, it shall be decreased by 30%.

So : extraterrestrial radiation, MJ/m²/day = 15.392 dr(ω s sin ϕ sin δ + cos ϕ cos δ sin ω s)

dr : relative distance between the earth and the sun $= 1 + 0.033 \cos \left(\frac{2\pi}{365} J \right)$

J : Julian day number

 ϕ : latitude of site $\Rightarrow 0$

δ : solar declination in radian = 0.4093 sin $\left(\frac{2\pi}{365}J - 1.405\right)$

ωs: sunset hour angle in radians
= arccos (-tan φ tan δ) = 1.57

σ: Stefan - Boltzmann constant = 4.903 x 10⁻⁹ MJ/m²/°K⁴/day

ed : vapor pressure in average conditions

$$\sqrt{\text{ed}} = \frac{0.36 - 0.261 \exp(-7.77 \times 10^{-4} \text{T2})}{0.14} \text{kPa}$$

(4) D

$$D = \frac{0.618}{2} \left\{ exp \left(\frac{17.27 \text{ T max.}}{237.2 + \text{ T max.}} \right) + exp \left(\frac{17.27 \text{ T min.}}{237.2 + \text{ T min.}} \right) \right\} \frac{(1 - \text{Rh})}{100}$$
(7.7)

where,

Tmax., Tmin.: maximum or minimum atmospheric air temperature in °C which is

shown in Table C.2 of Appendix C.

Rh : average relative humidity in decimal fraction which is shown in

Table C.2.

From the equations $(7.1) \sim (7.7)$ and Table C.2, an evaporation rate for each month was obtained as shown in Table 7.1.

Table 7.1 Estimation of Evaporation Rate from Open Water

| | | | | | | | | | | | | | | | | Total (mm) | 1999.0 |
|------|------|------|-------------|------|------|----------------|----------|-------|-------|--------|-------|----------|-------|-------------|-------|------------|------------|
| Dec | 32.0 | 24.5 | 28.2 | 80.2 | 43.1 | 349 | 0.222 | 0.768 | 1.597 | -0.407 | 1.032 | 14.585 | 1.566 | 6.789 | 0.071 | 53 | |
| Nov | 33.0 | 24.6 | 28.3 | 80.2 | 43.1 | 319 | 0.223 | 0.769 | 1.591 | -0.331 | 1.023 | 14.893 | 1.571 | 6.932 | 0.073 | 5.4 | 163.4 |
| Oct | 32.3 | 23.7 | 28.2 | 9.62 | 46.7 | 288 | 0.222 | 0.768 | 1.597 | -0.163 | 1.008 | 15.309 | 1.566 | 7.402 | 0.070 | 8.5 | 179.7 |
| Sep | 32.5 | 23.8 | 27.8 | 81.5 | 43.8 | 258 | 0.218 | 0.764 | 1.622 | 0.044 | 0.991 | 15.240 | 1.549 | 7.147 | 0.071 | 5.6 | 167.3 |
| Aug | 32.8 | 24.4 | 27.6 | 81.8 | 46.6 | 227 | 0.216 | 0.762 | 1.635 | 0.245 | 0.976 | 14.577 | 1.540 | 7.041 | 0.073 | 5.5 | 170.1 |
| Jul | 31.7 | 23.7 | 27.6 | 82.7 | 40.9 | 196 | 0.216 | 0.762 | 1.635 | 0.378 | 896.0 | 13.848 | 1.540 | 6.294 | 0.069 | 4.9 | 152.3 |
| Jun | 32.4 | 24.3 | 28.0 | 83.2 | 45.0 | 991 | 0.220 | 992:0 | 1.610 | 0.406 | 896.0 | 13.691 | 1.558 | 6.503 | 0.072 | 5.1 | 152.9 |
| May | 32.4 | 23.6 | 28.2 | 82.2 | 48.4 | 135 | 0.222 | 0.768 | 1.597 | 0.325 | 776.0 | 14.257 | 1.566 | 7.014 | 0.071 | 5.5 | 170.5 |
| Apr | 32.2 | 23.7 | 28.2 | 80.8 | 44.6 | 105 | 0.222 | 0.768 | 1.597 | 0.160 | 0.992 | 15.078 | 1.566 | 7.132 | 0.070 | 5.6 | 9.791 |
| Mar. | 32.0 | 24.7 | 28.1 | 80.4 | 45.1 | 74 | 0.221 | 0.767 | 1.603 | -0.054 | 1.010 | 15.518 | 1.562 | 7.379 | 0.071 | 5.8 | 179.0 |
| Feb. | 31.8 | 23.1 | 28.1 | 79.6 | 46.8 | 46 | 0.221 | 0.767 | 1.603 | -0.236 | 1.023 | 15.314 | 1.562 | 7.412 | 0.068 | 5.8 | 162.2 |
| Jan. | 31.5 | 24.4 | 28.0 | 81.0 | 44.2 | 15 | 0.220 | 0.766 | 1.610 | -0.373 | 1.032 | 14.791 | 1.558 | 996.9 | 0.069 | 5.4 | 168.9 |
| | (၃) | (၃) | (ටු | (%) | (%) | () | (kPa/°C) | | | | | (mm/day) | | (MJ/m2/day) | (kPa) | (mm/day) | (mm/month) |
| | Tmax | Tmin | T (average) | Rh | Z | J (julian day) | ٥ | Fp1 | Fp2 | 60 | dr | So | γed | А | D | Ep | |

APPENDIX A RAINFALL DATA

Table A.1 Annual Rainfall in and around Catchment Area (except WSN-1~6)

| | | | | | | | | | | | | | (mm) |
|---|----------------|--------|-------|----------------|----------------|----------------|----------------|---|------------------|----------------|----------------|------------------------|--------------------|
| | | | | | | Rain | all Gauge | Station | | _ | | | |
| Year | Kebare | Makbon | Kebar | Ayawasi | Westani | Atinyo | Ayamaru | Sausapor | Sorong Jefman | Sorong Remu | Sorong Doom | Kalmono (Pertamina) | Mega (Pertamina |
| 1920 | - | - | - | - | - | - | - | | 2,244 | • | - | - | - |
| 1921 1922 | - | - | - |] - | - | • | | • | 3,374 2,676 | - |] : | - | - |
| 1923 | - | - | - | - | - | | - | - | 2,148 | - |] | - | - |
| 1924 1925 | • | • | • | - | • | - | - | - | 3,568 | - | - | - | - |
| 1925 | - | - | • | | • | - | - | - | 2,698 3,608 | - | - | | - |
| 1927 | - | | • | - | • | - | • | - | 3,315 | - | - | - | - |
| 1928 1929 | - | - | - | - | 2,193 | - | | - | 2,487 2,926 | - | - | <u>-</u> | - |
| 1930 | - | - | - | - 1 | 2,339 | _ | | - | 2,432 | - | - | _ | |
| 1931 | - | - | - | - | - | - | - | - | 3,275 | - | - | - | - |
| 1932 1933 | - | - | - | - | - | - | _ | - | 3,189 3,043 | | - | - 1 | - |
| 1934 | - | - | - | - | - | - | - | - | 4,040 | - | - | - | - |
| 1935 1936 | - | - | - | - | 2,133 | - | | • | 3,404 3,570 | • | - | - | - |
| 1937 | - | - | - | - | 2,895 | 6,223 | - | - | 3,624 | - | . | - | |
| 1938 | - | • | - | - | 2.041 | 4,879 | 5,584 | 2,710 | 3,520 | - | | - | • |
| 1939 1940 | - | - | 1,903 | - | 2,041 2,310 | 4,689 3,943 | 4,365 3,442 | 1,758 2,270 | 2,169 2,449 | - | : | | • |
| 1941 | - | - | • | - | 2,648 | - | - | - | 2,302 | • | - | - | • |
| 1942 1943 | - | - | - | - | - | 3,482 4,874 | - | | - | • | - | - | - |
| 1944 | | - | |] [| | - | : | • | | - | : | | |
| 1945 | - | - | • | - | • | 7,315 | - | - | - | • | - | . | • |
| 1946 1947 | _ | - | • | - | | 4,578 | _ | - | - | - | - | - | - |
| 1948 | | | • | - | | - | - | - | - | - | | - | |
| 1949 | - | - | - | - | - | • | - | - | - | - | - | - | - |
| 1950 1951 | - | - | • | - | | - | - | - | - | - | - | - | |
| 1952 | • | - | • | - | . | - | 4,897 | - | - | • | - | - | • |
| 1953 1954 | 2,041 | - | • | <u>-</u> | • | • | 4,713 5,591 | 2,408 3,639 | - | - | • | • | • |
| 1955 | 1,624 | - | - | - | | | 6,209 | 3,178 | - | - | - | - | - |
| 1956 | 1.422 | - | - | 5,145 | - | • | 5,571 | 3.197 | - | - | - | - ' | - |
| 1957 1958 | 1,405 1,118 | 2,912 | - | | | : | 3,944 3,585 | 2,998 2,772 | 2,160 | 2,127 | 2,129 | 2,950 | : |
| 1959 | 1,862 | 3,905 | 2,211 | - | - | - | 4,504 | 2,750 | 3,215 | 3,056 | - | 3,680 | • |
| 1960 | 2.048 | 3,525 | 1712 | • | - | • | 4,900 | 2,478 | 2,953 | 3,086 | 2 200 | 4,150 | • |
| 1961 1962 | 1,869 2,419 | 3,212 | 1,712 | 7,110 | : | - | 4,288 5,913 | 3,069 3,361 | 2,139 3,166 | | 2,280 2,904 | 3,596 | - |
| 1963 | 1,980 | - | - | 5,883 | - | - | - | 2,867 | 2,575 | - | - | - | - |
| 1964 1965 | 1,903 1,142 | | • | 6,799 4,101 | : | - | 2,989 | 3,339 | 2,681 2,030 | - | 1,228 | • | - |
| 1966 | - | | • | 4,001 | -] | - | - | - | 2,563 | 1,482 | - | _ [| - |
| 1967 | 1,528 | - | - | 6,160 | - | | - | 2,876 | 2,450 | - | · - | - | - |
| 1968 1969 | - | - | - | 5,455 5,284 | : | - | • [| - | 3,058 3,272 | 3,165 | 2,404 | - | - |
| 1970 | 1,389 | | • | 5,440 | | - | 4,891 | - | 3,273 | 3,451 | - | 2,792 | |
| 1971 1972 | 1,823 1,713 | - | • | 3,920 7,780 | - | | 4,988 4,054 | • | 3,338 2,013 | - | 2,918 2,580 | - | - |
| 1972 | 4,187 | - | - | 7,168 | - 1 | - | 8,096 | : | 2,931 | 3,086 | - | - | - |
| 1974 | 2,329 | - | - | 6,326 | - | - | 4,567 | - | 2,909 | 1,867 | 2,922 | - | • |
| 1975 1976 | - | : | - | 5,238 5,398 | - | - | 5,464 2,935 | | 2,730 2,056 | 2,556 2,656 | - | • | - |
| 1977 | - | - | - | - | - | - | 3,541 | . | 2,626 | 2,917 | • | - | - |
| 1978 1979 | - | 5,264 | - | - | - | - | 4,119 3,383 | 2,901 2,765 | 3,028 | 1,647 | - | • | 2,401 2,580 |
| 1980 | - | 3,158 | - | - | -] | - | 3,383 | 2,765 | 2,583 1,793 | 2,812 2,428 | - | - | 2,38U - |
| 1981 | - | - | - | - | - | - | 5,030 | 2,628 | 2,327 | 3,474 | 3.279 | - | - |
| 1982 1983 | • | | - | - | | - | 3,827 8,334 | 1,937 | 3,702 | 1,908 2,968 | 1,458 2,068 | 3,573 | - |
| 1984 | - | | - | - | | - | 5,864 | - | 4.098 | 3,741 | 3,446 | 3,939 | : |
| 1985 | - | - | - | - | - | - | 6.463 | - | 3,157 | 2,767 | 2,659 | 3,820 | - |
| 1986 1987 | - | - | - | - | - | - | 3,807 5,497 | | 2,000 1,795 | 2,616 2,116 | 2,064 | 3,268 | - |
| 1988 | • | • | - | • | - | • , | • | . | 3,549 | -,1.0 | - | - | - |
| 1989 | • | • | • | - | - | • | • | - | 2,795 | - | - | - 1 | - |
| 1990 1991 | • | | | | - | - | - | - | 1,909 2,222 | - | - | - | - |
| 1992 | - | - | - | - | - [| - | - | - | 1,870 | - | • | • | - |
| 1993 1994 | - | | - | - | - | - | - | - | 2.031 1.973 | -] | - | - | - |
| Mean | 1.877 | 3,662 | 1,942 | 5,700 | 2,365 | 4,997 | 4.818 | 2,792 | 2,776 | 2,663 | 2,452 | 3,529 | 2,490 |
| .,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | 1.077 | 2,002 | .,,, | 5,700 | 2,000 | .,,,, | | -,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | -,,,, | 2,000 | -, +,2 | | 2,470 |

Source: Pre-F/S Report and data obtained at Sorong Jefman

Table A.2 Monthly Rainfall at Sorong Jefman

(mm)

| <u>[</u> | ton I | Feb | Mor I | A == 1 | Mass | Jun | Jul | Aug | Sep | Oct | Nov | Dec | Total | Day N | May |
|------------|-------|------|-------|--------|------|-----|-----|-----|------------|-----|----------|-----|----------|-------|-------|
| | Jan | | Mar | Apr | May | i | | Aug | | | | | | - | |
| 1920 | 60 | 60 | 86 | 434 | 125 | 510 | 117 | 174 | 251 | 247 | 135 | 45 | 2,244 | 75 | (6) |
| 1921 | 230 | 211 | 367 | 345 | 276 | 273 | 324 | 238 | 450 | 104 | 251 | 305 | 3,374 | 109 | (9) |
| 1922 | 145 | 292 | 152 | 310 | 132 | 327 | 351 | 277 | 232 | 197 | 83 53 | 178 | 2,676 | 112 | (9) |
| 1923 | 427 | 210 | 229 | 290 | 158 | 172 | 122 | 10 | 127 | 113 | | 237 | 2,148 | 54 | (4) |
| 1924 | 146 | 337 | 230 | 233 | 396 | 253 | 563 | 296 | 380 | 203 | 315 | 216 | 3,568 | 154 | (9) |
| 1925 | 196 | 266 | 245 | 186 | 340 | 312 | 260 | 343 | 216 | 17 | 111 | 206 | 2,698 | 117 | (5) |
| 1926 | 138 | 79 | 137 | 339 | 488 | 325 | 515 | 279 | 647 | 179 | 264 | 218 | 3,608 | 187 | (8) |
| 1927 | 230 | 100 | 267 | 255 | 406 | 447 | 385 | 120 | 572 | 175 | 244 | 114 | 3,315 | 144 | (6) |
| 1928 | 111 | 175 | 222 | 242 | 334 | 321 | 252 | 209 | 166 | 57 | 187 | 211 | 2,487 | 104 | (5) |
| 1929 | 195 | 61 | 308 | 284 | 527 | 470 | 235 | 140 | 236 | 180 | 166 | 124 | 2,926 | 100 | (5) |
| 1930 | 61 | 156 | 406 | 175 | 207 | 610 | 28 | 24 | 15 | 447 | 151 | 152 | 2,432 | 198 | (6) |
| 1931 | 242 | 51 | 105 | 288 | 563 | 671 | 443 | 133 | 318 | 159 | 158 | 144 | 3,275 | 123 | (5) |
| 1932 | 109 | 157 | 230 | 223 | 330 | 204 | 524 | 392 | 188 | 394 | 177 | 261 | 3,189 | 137 | (7) |
| 1933 | 200 | 216 | 145 | 156 | 223 | 294 | 376 | 363 | 543 | 226 | 113 | 188 | 3,043 | 139 | (2) |
| 1934 | 305 | 171] | 300 | 250 | 306 | 445 | 469 | 413 | 281 | 496 | 347 | 257 | 4,040 | 117 | (8) |
| 1935 | 197 | 70 | 208 | 211 | 448 | 485 | 253 | 410 | 171 | 520 | 247 | 184 | 3,404 | 100 | (8) |
| 1936 | 273 | 265 | 393 | 282 | 306 | 299 | 477 | 200 | 308 | 519 | 73 | 175 | 3,570 | 115 | (3) |
| 1937 | 243 | 191 | 332 | 250 | 318 | 449 | 376 | 208 | 525 | 355 | 260 | 117 | 3,624 | 138 | (10) |
| 1938 | 189 | 90 | 257 | 204 | 351 | 225 | 310 | 720 | 396 | 250 | 161 | 367 | 3,520 | 165 | (8) |
| 1939 | 211 | 181 | 89 | 329 | 315 | 423 | 146 | 93 | 126 | 29 | 215 | 12 | 2,169 | 89 | (4) |
| 1940 | 211 | 219 | 215 | 212 | 278 | 321 | 47 | 485 | 156 | 49 | 145 | 111 | 2,449 | 104 | (6) |
| 1941 | 125 | 46 | 137 | 321 | 623 | 40 | 88 | 181 | 184 | 202 | 181 | 174 | 2,302 | 122 | |
| 1958 | 43 | 90 | 196 | 144 | 182 | 191 | 126 | 485 | 156 | 179 | 162 | 206 | 2,160 | х | . ` [|
| 1959 | 206 | 52 | 108 | 322 | 517 | 533 | 429 | 181 | 184 | 264 | 245 | 174 | 3,215 | x | |
| 1960 | 305 | 160 | 99 | 193 | 316 | 223 | 870 | 112 | 192 | 91 | 211 | 181 | 2,953 | x | |
| 1961 | 125 | 204 | 218 | 197 | 142 | 266 | 348 | 115 | 143 | 67 | 147 | 167 | 2,139 | x | |
| 1962 | 416 | 210 | 130 | 383 | 404 | 331 | 150 | 376 | 136 | 272 | 127 | 231 | 3,166 | x | |
| 1963 | 280 | 239 | 184 | 255 | 549 | 240 | 307 | 134 | 32 | 32 | 83 | 240 | 2,575 | X | |
| 1964 | 114 | 286 | 128 | 428 | 229 | 309 | 269 | 148 | 113 | 182 | 165 | 310 | 2,681 | x | |
| 1965 | 278 | 25 | 148 | 301 | 292 | 319 | 21 | 36 | 1 | 133 | 255 | 221 | 2,030 | x | |
| 1966 | 130 | 143 | 141 | 138 | 303 | 261 | 194 | 419 | 219 | 143 | 245 | 227 | 2,563 | 75 | |
| 1967 | 335 | 148 | 80 | 271 | 399 | 297 | 352 | 101 | 53 | 172 | 127 | 115 | 2,450 | 109 | (7) |
| 1968 | 131 | 61 | 356 | 102 | 170 | 453 | 348 | 206 | 332 | 249 | 377 | 273 | 3,058 | 112 | (6) |
| | 141 | 50 | 411 | 186 | 578 | 240 | 484 | 311 | 98 | 350 | 259 | 164 | 3,272 | 148 | (7) |
| 1969 | | 127 | 243 | 275 | 585 | 214 | 461 | 351 | 241 | 123 | 200 | 259 | 3,273 | 225 | (7) |
| 1970 | | | 138 | 192 | 479 | 416 | 294 | 437 | 317 | 341 | 197 | 113 | 3,338 | | |
| 1971 | 211 | 203 | | | | 512 | 68 | 150 | 102 | 33 | 154 | 94 | 2,013 | 152 | |
| 1972 | 165 | 268 | 134 | 166 | 167 | 331 | 240 | 366 | 240 | 163 | 80 | 48 | 2,931 | 80 | |
| 1973 | 294 | 111 | 232 | 469 | 357 | | | | 240 284 | | 181 | 174 | 2,909 | 117 | (5) |
| 1974 | 53 | 304 | 99 | 375 | 437 | 309 | 258 | 225 | | 210 | | | | | |
| 1975 | 158 | 111 | 134 | 278 | 355 | 312 | 232 | 285 | 345 | 144 | 127 | 249 | 2,730 | 67 | (4) |
| 1976 | 111 | 210 | 105 | 170 | 324 | 123 | 171 | 193 | 121 | 319 | 171 | 38 | 2,056 | 106 | (8) |
| 1977 | 121 | 184 | 260 | 279 | 289 | 460 | 140 | 181 | 164 | 220 | 154 | 174 | 2,626 | 98 | (5) |
| 1978 | | 51 | 530 | 126 | 145 | 324 | 407 | 307 | 290 | 107 | 205 | 271 | 3,028 | 108 | (7) |
| 1979 | | 93 | | | 205 | 521 | 97 | 71 | 508 | 75 | 249 | 182 | 2,583 | 123 | |
| 1980 | | 136 | 92 | 233 | 275 | 213 | 108 | 189 | 18 | 162 | 133 | 83 | 1,793 | 70 | (7) |
| 1981 | | 96 | 226 | 174 | 409 | 112 | 435 | 37 | 300 | 43 | 151 | 178 | 2,327 | 120 | |
| 1982 | | 117 | 270 | 194 | 335 | 260 | X | - x | 291 | 120 | 87. | 188 | 3 703 | 259 | |
| 1983 | | 33 | 78 | 186 | 491 | 420 | 418 | 528 | 521 | 447 | 145 | 186 | 3,702 | 135 | |
| 1984 | | 259 | 217 | 387 | 711 | 372 | 738 | 227 | 574 | 105 | 124 | 155 | 4,098 | 130 | |
| 1985 | | 348 | 61 | 149 | 548 | 352 | 241 | 291 | 336 | 255 | 233 | 203 | 3,157 | 150 | |
| 1986 | | 154 | 161 | 142 | 151 | 228 | 232 | 55 | 268 | 218 | 112 | 183 | 2,000 | 90 | |
| 1987 | | 18 | 220 | 105 | 330 | 149 | 37 | 132 | 58 | 326 | 188 | 91 | 1,795 | | (10) |
| 1988 | | 131 | 207 | 88 | 334 | 320 | 493 | 699 | 326 | 275 | 231 | 242 | 3,549 | 115 | (8) |
| 1989 | | 189 | 285 | 307 | 28 | 248 | 312 | 290 | 263 | 393 | 252 | 105 | 2,795 | 84 | (10) |
| 1990 | | 116 | 127 | 130 | 220 | 134 | 177 | 134 | 240 | 402 | 65 | 69 | 1,909 | 112 | (9) |
| 1991 | 306 | 104 | 235 | 156 | 581 | 188 | 210 | 34 | 3 | 110 | 11 | 284 | 2,222 | x | |
| 1992 | | 50 | | 100 | 265 | 136 | 191 | 102 | 196 | 430 | 124 | 117 | 1,870 | x | |
| 1993 | | 114 | 110 | 206 | 361 | 136 | 294 | 46 | 313 | 90 | 138 | 112 | 2,031 | х | |
| 1994 | | 161 | 234 | 229 | 338 | 326 | 59 | 137 | 0 | 191 | 191 | 72 | 1,973 | x | |
| | | | | | i | | | | <u> </u> | | | | <u> </u> | | |
| Average | 179 | 152 | 204 | 240 | 343 | 316 | 291 | 238 | 245 | 213 | 175 | 176 | 2,776 | | |
| . i verage | | | 204 | | 2.5 | | | | 5 | | | | | ١ | |

x: No Data

(): Month

Sources: -Data obtained at the BMG office in Jefman -Data exhibited in the Prc-F/S report

| Month | | | | | | 1001 | 1 | | | | | |
|---------------|------|------|-------|-------|---|------|-------|--|---|---|--|--|
| Month | | | • | | | 18 | ,, | | | | | |
| Day | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul | Aug. | Sep. | Oct. | Nov. | Dec. |
| | | | | | | | | | | | | |
| 1 | | 0.0 | 0.0 | 2.0 | *************************************** | | 0.0 | | | | | |
| 2 | | 5.0 | 13.0 | 10.0 | | | 6.0 | | | | | |
| 3 | | 3.0 | 41.0 | 4.0 | | | 9.5 | • | | | | |
| 4 | | 24.0 | 0.0 | 0.1 | *************************************** | | 19.0 | | | | 40-11-41-11-41-41-41-41-41-41-41-41-41-41- | |
| 5 | | 0.5 | 0.0 | 1.0 | *************************************** | | 1.0 | | | *************************************** | | |
| 9 | | 5.5 | 0.0 | 4.0 | | | 1.0 | | | | | |
| | | 15.0 | 0.0 | 5.0 | | | 0.0 | | ***** | | | |
| 8 | | 0.5 | 0.0 | 0.0 | *************************************** | | 36.0 | | | | | |
| 6 | | 0.0 | 0.0 | 0.5 | | | 0.5 | | | | > 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - | |
| 10 | N.A. | 28.5 | 0.0 | 0.0 | N.A. | N.A. | 59.5 | | N.A. | N.A. | A.N | N.A. |
| 11 | | 0.0 | 0.0 | 0.0 | | | 11.0 | *************************************** | | | | |
| 12 | | 0.0 | 0.5 | 15.5 | | | 5.0 | | | | | • |
| 13 | | 0.0 | 1.5 | 24.0 | | | 0.0 | | | | | 9 44 189 1 1 1 1 0 0 1 1 1 1 1 0 0 0 0 0 0 0 0 |
| 14 | | 0.0 | 11.0 | 0.6 | *************************************** | | 7.0 | | | | -070440404040404040404040404040404040404 | |
| 15 | | 2.5 | 0.0 | 2.0 | 165016500 | | 53.0 | | | *************************************** | *************************************** | |
| 16 | | 1.0 | 0.0 | 0.0 | · · · · · · · · · · · · · · · · · · · | | 0.0 | *************************************** | | | · estel a ten rational est tentes est | ******************* |
| 17 | | 1.5 | 0.0 | 1.5 | | | 0.0 | *************************************** | | | *************************************** | **************** |
| 18 | | 0.0 | 0.0 | 0.5 | | | 0.0 | 0.0 | | | . 8688 688 888 888 688 688 688 | ************************************** |
| 19 | | 0.0 | 26.0 | 5.5 | | | 0.0 | | | | | |
| 20 | | 3.0 | 10.0 | 0.0 | | | 0.0 | ******* | | **** | | |
| 21 | | 0.0 | 30.0 | 3.5 | | | 0.0 | | | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | | **************** |
| 22 | | 1.0 | 8.0 | 0.0 | | | 0.0 | | | ***** | | *************************************** |
| 23 | | 8.0 | 0.0 | 44.0 | | | 0.0 | | | | | |
| 24 | | 0.0 | 1.0 | 0.5 | | | 0.0 | *************************************** | | | *************************************** | *************************************** |
| 25 | | 0.0 | 34.5 | 0.0 | | | 48.0 | | | | | 47711447144144744754 |
| 26 | | 0.0 | 1.5 | 0.0 | | | 1.0 | | | ************************************** | | 4 10 2 2 2 4 4 5 2 5 4 5 4 5 4 5 4 5 4 5 4 5 |
| 27 | | 0.0 | 58.0 | 21.0 | | | 0.5 | | | | | |
| 28 | | 0.0 | 0.86 | 0.5 | | | 0.0 | *4 7 4 5 7 4 5 7 4 6 7 7 4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | | | | ******************** |
| 29 | | | 15.0 | 0.0 | | | 3.0 | | | | | · 6490+06+0664 FEA 440FE |
| 30 | _ | | 29.0 | 1.0 | | | 3.0 | *4 * 0 * 0 * 0 * 0 * 0 * 0 * 0 * 0 * 0 * | | | | 491414411774104D0414D04 |
| 31 | | | 2.0 | | | | 0.0 | * 4 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | *************************************** | | | ***** |
| | | | | | | | | | | | | 474714 71771 741 7424 7424 |
| Monthly total | | 5.68 | 380.0 | 156.0 | | | 264.0 | 73.5 | | | | |
| Day Max. | | 28.5 | 0.86 | 44.0 | | | 59.5 | 60.5 | | | | |

Ν Dec. Nov. N.A. (mm) Z V Oct. N.A. Sep. Aug. ΑN Daily Rainfall Data at WSN-1 (Malano) 109.5 37.0 Jul 1992 17.0 266.0 42.0 Jun. May N.A. 25.50 11.00 10.00 120.0 35.0 Apr. Table A.3b Mar. N.A. 155.0 46.0 Feb. Ν Jan. Monthly total Day Max. Month 200 Day

84.5 28.0 Dec. Nov. N.A. (mm) 8 N.A. N.A. Sep. 35.5 7.5 Aug. Daily Rainfall Data at WSN-1 (Malano) 24.0 56.0 Jal Jal 1993 25.0 25.0 Jun. 7.0 33.0 4.0 29.0 75.0 33.0 0.0 May KKK XXXXX ĸ KKKK 140.0 36.0 Apr. 76.5 30.0 Table A.3c Mar. 71.0 25.0 Feb. 189.5 88.0 Jan. Monthly total Day Max. Month Day

48.0 18.0 Dec. 26.5 Nov. (mm) 221.5 21.5 21.5 21.0 22.0 23.5 23.5 23.5 20.0 239.5 43.5 Si O 4.0 4.0 Sep. 36.0 15.0 Aug. Daily Rainfall Data at WSN-1 (Malano) 14.5 11.0 Jel Ze 1994 600.0 172.5 Ĭ. 161.5 53.0 May 368.5 55.0 Apr. Table A.3d 197.5 70.5 Mar. 46.5 30.0 Feb. 140.5 42.0 Jan. Month Monthly total Day Max. 2 Day

(mm) Daily Rainfall Data at WSN-1 (Malano) Table A.3e

| _ | | _ | _ | | _ | _ | | _ | _ | | _ | | _ | | _ | | | | | _ | _ | | _ | _ | _ | | _ | | _ | _ | _ | _ | _ | | |
|-------|------|---|---|---------------------------------------|------|---|---|---|--------------------------|---|---|--|---|---|--|---|---|---|---|--|---|-----------------|---|-------------------------------------|---|---|---|---|---|---|------|---|---|---|---------------------------|
| | Dec. | | + 4 0 MA UV 0 VAR 0 N V 0 D 0 0 5 1 1 1 1 1 1 1 1 1 | | | 4 4 4 4 4 4 7 7 4 4 4 4 4 4 4 4 4 4 4 4 | *************************************** | | • | *************************************** | | ************************* | | | | | *************************************** | | | | | | | * * **** *** *** * **** * *** * *** | | ******************************** | | • | *************************************** | *************************************** | | | - Publis in - 1144++948 544+940+ | | |
| | Nov. | | | | | ****** | | | ************************ | | ************************ | + 00 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | | | ************************ | | *************************************** | *************************************** | | ******************** | | *************** | | **** | | *************************************** | | *************************************** | | ************************ | | ******************* | ************ | | |
| | Oct. | | | · · · · · · · · · · · · · · · · · · · | | | | · · · · · · · · · · · · · · · · · · · | | | | | | | | *************************************** | | | *************************************** | | | | | | | | | | | | | | | | |
| | Sep. | | | | | a vido e supe il supe d'ille il delle sobre e | *************************************** | | | | | | | | *********** | | | | **** | | | | | | | | | * | | | | | | | |
| | Aug. | | | | | | - 11-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4 | | | * 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | *************************************** | *************************************** | *************************************** | *************************************** | | | *************************************** | *************************************** | 4 40 4 4 4 4 4 4 4 4 | - 50 100 1000 1000 1000 1000 1000 1000 1 | *************************************** | | | | *************************************** | | *************************************** | | | | | *************************************** | *************************************** | | |
| 1995 | Jul | | | | | | e rit e de di de cada de destarenses refers | - 197 0 190 0 1984 0 190 0 1 100 1 1784 1 | | | | + 147 0 240 1 240 0 220 1 201 7 0 1 1 1 | | | 189 V 19889 9890 98 88 0 8 88 0 8 17 1 | *************************************** | | | | | | | PM PEOP ON 14 PEOP ON 10 PEOP ON 10 | | | | | | *************************************** | ************** | | *************************************** | ***** | | |
| 19 | Jun. | | | | | | | • | | | | | ••••••••••••••••••••••••••••••••••••••• | *************************************** | | | | | | | | | | | | | | | | | | | | | |
| | May | | 31.5 | 7.5 | 58.5 | 8.0 | 0.0 | 17.0 | 0.0 | 6.0 | 12.0 | 8.5 | 0.0 | 23.0 | 24.5 | 0.0 | 51.5 | 0.0 | 7.5 | 0.0 | 17.0 | 2.5 | 4.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0:0 | | 279.0 58.5 |
| | Apr. | | 0.0 | 0.0 | 0.0 | 19.5 | 21.0 | 0.0 | 0.0 | 0.0 | 17.0 | 28.0 | 1.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.5 | 0.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 37.5 | 7.5 | 14.0 | 0.0 | 10.0 | 0.0 | 0.5 | | | 164.0 37.5 |
| | Mar. | | 24.0 | 1.0 | 0.0 | 4.5 | 1.5 | 0.1 | 0.0 | 0.0 | 10.5 | 3.0 | 0:1 | 0.9 | 0.0 | 0.0 | 1:0 | 0.0 | 34.5 | 0.0 | 3.5 | 0.0 | 3.5 | 12.0 | 1.5 | 0.5 | 0.5 | 11.0 | 1.5 | 0.0 | 28.5 | 0.0 | 0:0 | | 150.5 34.5 |
| | Feb. | | 0.5 | 0.5 | 0.9 | 0.0 | 0.0 | 0.0 | 3.0 | 32.5 | 0.0 | 12.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 22.5 | 0.0 | 0.0 | 0.0 | 6.5 | 0.0 | 7.0 | 0.0 | 1.5 | 0.0 | 0.0 | 26.0 | 0.0 | | | | | 118.0 32.5 |
| | Jan. | | 0.0 | 0.0 | 0.0 | 0.0 | 10.0 | 0.0 | 0.0 | 0.0 | 13.0 | 5.0 | 0.0 | 2.5 | 0.0 | 0.0 | 5.5 | 8.5 | 0.0 | 20.5 | 0.0 | 0.0 | 0.0 | 0.0 | 24.0 | 5.5 | 0.9 | 0.0 | 0.0 | 2.5 | 0.0 | 0.0 | 5.0 | | 108.0 |
| Month | Day | | _ | 2 | 3 | 4 | 5 | 9 | 7 | ∞ | 6 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | . 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | - | Monthly total Day Max. |

(mm) Daily Rainfall Data at WSN-2 (Asbaken) Table A.4a

| Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul | Aug. | Sep. | Oct. | Nov. | Dec. |
|---|-------|-------|-------|---------------------------------------|------|-------|------|---|-------|------|-------|
| | | | | | | | | | | | |
| | × | 12.5 | 3.0 | | | 78.0 | 0.0 | 44 | 0.0 | 0.0 | 0.0 |
| | × | 19.0 | 11.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| | × | 36.0 | 0.5 | | | 0:0 | 0.0 | _ | 0.0 | 0.0 | 0.0 |
| | X | 0.0 | 4.0 | | | 56.0 | 0.0 | | 0.0 | 0.0 | 7.0 |
| | × | 1.5 | 31.5 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| *************************************** | × | 0:0 | 2.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 12.0 |
| | X | 1.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 20.0 |
| *************************************** | × | 1.5 | 30.0 | | | 0.0 | 25.0 | 0.0 | 0.0 | 0.0 | 16.0 |
| | X | 0.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.9 |
| Ä. | × | 1.5 | 0.0 | N.A. | N.A. | 4.0 | 0.0 | | 0.0 | 0.0 | 11.0 |
| | X | 0.0 | 0.0 | | | 0.0 | 0.0 | *************************************** | 10.0 | 0.0 | 4.0 |
| *************************************** | × | 0.0 | 0.0 | ***** | | 0.0 | 3.0 | ## 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 27.0 | 0.0 | 42.0 |
| | × | 0.5 | 10.0 | | | 0.1 | 0.0 | | 0.0 | 0.0 | 68.0 |
| | × | 50.5 | 38.0 | | | 24.0 | 0.0 | | 75.0 | 0.0 | 0.6 |
| | × | 18.5 | 1.0 | | | 9.0 | 0.0 | | 63.0 | 0.0 | 5.0 |
| | X | 0.0 | 0.0 | | | 0.0 | 0.0 | | 29.0 | 0.0 | 6.0 |
| | × | 0.0 | 1.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 22.0 |
| | × | 22.5 | 23.5 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 10.0 |
| | × | 0.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 12.0 |
| | × | 36.5 | 7.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 10.0 |
| | 21.5 | 0.9 | 21.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 11.0 |
| | 75.0 | 3.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 11.0 |
| | 13.0 | 4.5 | 10.5 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 26.0 |
| | 30.0 | 1.5 | 18.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | 26.0 |
| | 7.5 | 23.0 | 1.0 | | | 0.1 | 0.0 | | 0.0 | 32.0 | 37.0 |
| | 4.0 | 28.0 | 0.0 | | | 0.6 | 0.0 | | 0.0 | 0.0 | 57.0 |
| | 3.5 | 44.5 | 12.0 | | | 0.0 | 0.0 | | 0.0 | 20.0 | 48.0 |
| | 3.5 | 59.0 | 0.0 | | | 0.0 | 0.0 | | 2.0 | 0.0 | 7.0 |
| | | 7.5 | 0.0 | | | 23.0 | 0.0 | | 0.0 | 0.0 | 4.0 |
| | | 8.0 | 23.5 | · · · · · · · · · · · · · · · · · · · | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| | | 0.0 | | | | 0.0 | 0.0 | | 0'0 | | 0.9 |
| | | • | | | | | | | | | |
| Monthly total | 158.0 | 386.5 | 248.5 | 1 | | 205.0 | 28.0 | 29.0 | 206.0 | 52.0 | 493.0 |
| | 0.57 | 0.80 | 0.00 | | | 0.0/ | 0.07 | 10.01 | | D.2C | 0.80 |

506.0 105.0 Д Ж 45.0 20.0 Nov. (mm) 118.0 27.0 Sci Sep. AZ Aug. NA Daily Rainfall Data at WSN-2 (Asbaken) Z.A. Jel Jel 1992 25.50 25.00 25 150.0 25.0 Jun. 116.0 33.0 May 296.0 32.0 Apr. 92.0 30.0 Table A.4b Mar. 186.0 59.0 Feb. 64.0 23.0 Jan. Month Monthly total Day Max. Day

<u>Б</u> Ϋ́ N.A Nov. (mm) ΝA QCI. ΝĀ Sep. Aug. N.A. Daily Rainfall Data at WSN-2 (Asbaken) ΝA Jul 1993 ΝA Jun. May N.A. 63.0 Apr. 92.0 30.0 Table A.4c Mar. 0.0 Feb. 148.0 60.0 Jan. Monthly total Day Max. Month Day

Dec. Nov. ö ö Sep. Aug. Œ 1994 Iun. May Apr. Mar. Feb. Jan. Month 0 6

Table A.4d

460.0 230.0 (mm) 0.0 0.0 5.0 5.0 Daily Rainfall Data at WSN-2 (Asbaken) 0.0 263.0 60.0 260.0 76.0 179.0 124.0 259.0 48.0 7.0 4.0 44.0 15.0 Monthly total

48.0 31.0

Day Max.

(mm) Daily Rainfall Data at WSN-2 (Asbaken) Table A.4e

| \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | | | | | | 2 | 2 | | | | | |
|--|-------|---|--|---|---|---|-------|---|---|---|---|---|
| Million | | | | | | 2661 | 25 | | | | | |
| Day | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul | Aug. | Sep. | Oct. | Nov. | Dec. |
| | | | | | | | | | | | | |
| _ | 0.9 | | | | | 30.0 | | | | | | |
| 2 | 12.0 | | | | | 18.0 | | | | | | |
| 3 | 0.0 | | | | | 15.0 | | | | | ***** | |
| 4 | 0.0 | 1937 7 290 0 0 0 T C T DO C - 1 C O D T O C O C O C O C O C O C O C O C O C O | | | ***** | 30.0 | | | | | | |
| 5 | 0.0 | | 1 22 6 5 6 6 7 6 7 6 6 7 6 6 7 6 6 7 6 7 6 7 | | | 44.0 | | | *************************************** | *************************************** | 101000000000000000000000000000000000000 | · |
| 9 | 0.0 | | | | ***** | 31.0 | | *************************************** | - 100 0 | · H 0 0 1 0 H 0 2 1 F H 0 7 0 2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | | |
| 7 | 0.0 | | | | | 20.0 | | 25 025 0 m den manda kodil 400 444 a | -090 -034 -054 -054 -054 -054 -054 -054 -054 -05 | | | |
| 8 | 0.0 | | | | *************************************** | 40.0 | | | * 1000 mm = 1-4-7-4 + 00 + 0-6-0 mm = 1 | | | **** |
| 6 | 0.0 | | • 14000001400000000000000000000000000000 | | | 5.0 | | | ************************* | re paga pagas og es aquis em a estar e | | - 1970 1870 1880 1880 1880 1880 1880 18 |
| 10 | 0.0 | | 1 20 3 4 4 5 5 6 7 4 5 5 5 6 5 6 5 6 5 6 5 6 6 6 6 6 6 6 6 | | | 0.9 | | | | ** ***** ** | | ******************** |
| | 41.0 | | | | | 0.0 | | | | | | *************************************** |
| 12 | 0.0 | | | 773777777777777777777777777777777777777 | | 0.0 | | | | | | *************************************** |
| 13 | 0.0 | | 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | | 0.0 | | | | | | ****** |
| 14 | 0.0 | | | | | 0.0 | | | | | | a P 2 II d 4 II II 6 II 6 D 6 D 7 D 7 D 7 D 7 D 7 D 7 D 7 D 7 D |
| 15 | 0.11 | | | | | 12.0 | | | | | | |
| 16 | 18.0 | | | | | 18.0 | | | | | | 1 |
| 17 | 0.09 | | | | | 0.9 | | | | | | |
| 18 | 78.0 | | | | | 13.0 | | | | | | |
| 19 | 5.0 | | | | | 0.01 | | | | | | |
| 20 | 0.0 | | | | | 13.0 | | | | | | |
| 21 | 16.0 | | | | | 22.0 | | | | | | |
| 22 | 17.0 | | | | | 20.0 | | | | | | · · · · · · · · · · · · · · · · · · · |
| 23 | 0.0 | | | | | 5.0 | 20.0 | | | | | |
| 24 | 81.0 | | | | | 11.0 | | | | | | |
| 25 | 10.0 | | | | | 13.0 | | | | | | |
| 26 | 4.0 | | | | | 0.0 | | | | | | |
| 27 | 0.0 | | | | | 0.0 | | | | | | |
| 28 | 0.0 | | | | | 0.0 | | | | | | |
| 29 | 0.0 | | | | | 30.0 | 11.0 | | | | | 1 |
| 30 | 0.0 | | | | | 16.0 | 16.0 | | | | | |
| 31 | 0.0 | 111111111111111111111111111111111111111 | *************************************** | | | 1 | 10.0 | | | | *************************************** | |
| | | | | | | | | | | | | |
| Monthly total | 359.0 | | | | | 428.0 | 704.0 | | | | | |
| Day Iviax. | 01.0 | - | | | | 2 <u>4</u> | 80.0 | | | | | |
| | 1 | | | | | | 1 | | | | | |

(mm) Daily Rainfall Data at WSN-3 (Klamabon) 1991 Table A.5a

352.0 62.0 Dec. 178.0 92.0 Nov. 280.0 69.0 St. 261.0 39.0 Sep. Aug. ΝĀ Ν Ξ ΥV Jun. May A'N 214.0 -67.0 Apr. 455.5 141.0 Mar. 198.0 75.5 Feb. ×× X X X Ν Jan. Month Monthly total Day Max. 2 0 2 Day

Dec. 00000 Nov. (IIIII) ಕ Sep. Aug. Daily Rainfall Data at WSN-3 (Klamabon) Ξ 1992 Ϋ́ Jun. May Apr. Table A.5b Mar. Feb. Jan. Month

255.0 54.0

106.0 28.0

61.0 48.0

193.0 40.0

397.0 55.0

444.0 83.0

261.0 39.0

292.0 88.0

91.0 42.0

227.0 115.0

141.0 42.0

Monthly total Day Max.

(mm) Daily Rainfall Data at WSN-3 (Klamabon) 1993 Table A.5c Month

Dec. Ϋ́ Nov. A A N.A ; 0 N.A Sep. 78.0 Aug. 572.0 156.0 Ξ 25.0 330.0 56.0 Jun. 174.0 43.0 May 394.0 99.0 Apr. 202.0 42.0 Mar. 153.0 59.0 Feb. KK × × × × X X X × 0.0 0.0 Jan. KIKIKIKIKIKIK K K K K XX XXX x x x x XX Monthly total Day Max. 10

Daily Rainfall Data at WSN-3 (Klamabon)

Table A.5d

(IIII)

Ϋ́ Z <u>Б</u> 176.0 34.0 Nov. 212.0 43.0 <u>8</u> 0.1 Sep. Υ Aug. N.A. Jul 1994 171.0 32.0 Jun. 193.0 46.0 May 340.0 57.0 Apr. 483.0 80.0 Mar. 56.0 10.0 Feb. 82.0 58.0 Jan. Monthly total Day Max. Month Day

Dec. Nov. (mm) ö Sep. Aug. Daily Rainfall Data at WSN-3 (Klamabon) Jul 1995 225.0 32.0 Jun. 211.0 $\begin{array}{c} 0.0 \\ 1.0 \\ 2.1 \\ 0.0 \\$ May 222.0 53.0 Apr. 231.0 Table A.5e Mar. Z.A. Feb. AN Jan. Monthly total Day Max. Month Day

252.0 39.0 Dec. 85.5 36.5 Nov. (mm) 0.0 8 49.5 29.0 Sep. Aug. ΝA Daily Rainfall Data at WSN-4 (Sainkeduk) ΝĀ Jul 1991 Ν Jun. May ν V 358.0 56.0 Apr. Table A.6a 324.5 38.5 Mar. 50.0 25.0 Feb. XXXX **x x x x x x** Ν Jan. Month Monthly total Day Max. Day

<u>D</u> 304.0 40.0 Nov. (mm) 564.0 45.0 3300 2400 2400 2400 2400 2200 2000 ö 393.0 43.0 Sep. 237.0 30.0 Aug. Daily Rainfall Data at WSN-4 (Sainkeduk) 222.0 32.0 Ŀ 1992 290.0 46.0 Jun. 15.0 16.0 474.0 100.0 May 278.0 48.0 Apr. 76.0 30.0 Fable A.6b Mar. 111.0 36.0 Feb. 143.5 40.5 Jan. Month Monthly total |∞ |o Day

207.0 31.0

Day Max.

Д З ΑN Nov. N.A. (mm) N.A. 8 Υ Sep. 257.0 72.0 Aug. Daily Rainfall Data at WSN-4 (Sainkeduk) 250000 200000 200000 200000 200000 20000 20000 20000 20000 2000 0.7101 0.201 E 1993 490.0 50.0 Jun. 425.0 64.0 May 460.0 65.0 Apr. 279.0 Table A.6c Mar. $\begin{array}{c} 0.0 \\$ 244.0 26.0 Feb. 238.0 41.0 Jan. Month Monthly total Day Max. 2 = 13 7 ∞ Q 4 9 Day

224.0 225.0 226.0 22 287.0 26.0 Dec. 94.0 16.0 492.0 94.0 Nov. (mm) 87.0 20.0 Sct. 218.0 30.0 Sep. Aug. N.A. Daily Rainfall Data at WSN-4 (Sainkeduk) N.A Jul 1994 N.A. Jun. May Υ Apr. N.A. Table A.6d Mar. N.A. N.A. Feb. N.A. Jan. Month Monthly total Day Max. 10 4 2 0 1 ∞ 0 Day

<u>გ</u> Nov. (mm) S F Sep. Aug. Daily Rainfall Data at WSN-4 (Sainkeduk) Jel 1995 Jun. May Apr. Table A.6e Mar. Feb. 315.0 33.0 Jan. Month Monthly total Day Max. Day

(mm) Daily Rainfall Data at WSN-5 (Mega) Table A.7a

358.0 110.0 Dec. 5.0 Nov. 274.0 150.0 ö 32.0 15.0 Sep. 5.0 2.0 25.0 10.0 2.0 0.0 Aug. × × 25.0 102.0 25.0 Ę 1991 ΝA Jun. May Ϋ́ 18.0 1.0 10.5 36.5 0.0 0.0 0.0 126.5 36.5 1.0 4.0 000 Apr. * * * * * * ×× K K K $\begin{array}{c} 1.10 \\ 45.0 \\ 1.10 \\ 1.$ 284.0 98.5 Mar. × × ×:× 129.0 42.0 Feb. X X X × x x x × Jan. Υ Month Monthly total Day Max. **∞** ο Day

Dec. Nov. (<u>IIII</u>) ö Sep. Aug. Daily Rainfall Data at WSN-5 (Mega) $\begin{array}{c} 0.0 \\$ Jul 1992 May Apr. Table A.7b Mar. Feb. 25.0 25.0 25.0 0.0 0.0 0.0 0.0 Jan. x x x Month Day

41.0

102.0 35.0

205.0 80.0

80.0 23.0

67.0 60.0

288.5 80.0

209.0 66.0

40.0 40.0

248.0 56.0

49.0 15.0

127.0 97.0

28.0 35.0

Monthly total Day Max.

205.0 51.0 Dec. 60.0 12.0 Nov. (mm) 65.0 29.0 . 6 33.0 33.0 295.0 51.0 Sep. 47.0 23.0 3.0 0.5 0.5 0.5 23.0 15.0 Aug. x x x ×× Daily Rainfall Data at WSN-5 (Mega) 22.0 31.0 Ξ 1993 64.5 29.5 Jun. 126.0 52.0 May 12.0 20.0 Apr. 105.0 20.0 Table A.7c Mar. 187.0 38.0 Feb. 204.0 43.0 lan. Month Monthly total Day Max. Day

217.0 40.0 Des. 233.5 63.0 Nov. (mm) 83.5 15.0 8 2.0 Sep. 39.5 11.0 Aug. Daily Rainfall Data at WSN-5 (Mega) 49.5 12.0 Ξ 1994 99.0 39.0 Jun. 15.0 23.0 May 169.0 32.0 Apr. 321.0 44.0 Table A.7d Mar 41.0 9.0 Feb. 169.0 45.0 Jan. Month Monthly total Day Max. Day

(A): Rainfall data measured by an automatic raingauge

| | | | Table A.7e | [. | Daily Rainfa | Daily Rainfall Data at WSN-5 (Mega) | SN-5 (Mega) | | | | (mm) | |
|---------------|-------|-------|------------|-------|---|-------------------------------------|---|---|---|---------------------------------------|---|------|
| Month | | | | | | 1995 | 35 | | | | | |
| Day | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul | Aug. | Sep. | Oct. | Nov. | Dec. |
| | 4.0 | | 0.0 | 0.5 | *************************************** | 0.0 | | | | | ••••••••••••••••••••••••••••••••••••••• | • |
| 2 | 0.0 | | 0.0 | 5.9 | | 0.0 | | | | · · · · · · · · · · · · · · · · · · · | ********* | |
| 3 | 0.0 | 0.5 | 0.3 | 0.3 | 0.0 | 0.0 | | | | | | |
| 4 | 43.0 | | 21.5 | 13.2 | | 0.0 | | | | | | |
| 2 | 4.0 | | 21.1 | 1.5 | | 0.0 | - 1000 m 1000 5 15 20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | | | | | |
| 9 | 5.0 | | 0.0 | 2.4 | 0.8 | 0.0 | | | | | | |
| | 3.0 | | 4.0 | 0.3 | | 4.5 | | | | | | |
| 00 | 0.5 | | 4.6 | 0.3 | 74000000000000000000000000000000000000 | 1.1 | | | | | | |
| 6 | 2.0 | | 9.6 | 0.0 | | 0.7 | | | | | | |
| 10 | 21.0 | | 0.0 | 1.4 | • | 0.0 | | | | | | |
| | 30:0 | | 0.0 | 0.0 | • | 0.0 | | · 4 6 6 9 4 | 7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | | | |
| 12 | 0.0 | | 1.0 | 0.2 | | 0:0 | | *************************************** | | | | |
| 13 | 0.0 | • | 0.0 | 0.0 | | 15.2 | | · * * * * * * * * * * * * * * * * * * * | | | | |
| 14 | 38.0 | | 0.0 | 11.11 | | 1.8 | · · · · · · · · · · · · · · · · · · · | · · · · · · · · · · · · · · · · · · · | 0 | | | |
| 15 | 0.79 | | 0.0 | 5.3 | | 0.5 | | | | | | |
| 16 | 0.0 | | 2.9 | 0.0 | **** | 1.3 | | | | | | |
| 17 | 6.5 | | 6.6 | 0.0 | *************************************** | 16.2 | 1 V 0 II 0 A V 0 0 A A II 0 V 0 V 0 V 0 A A A A A A A A A A A A A | | | | | |
| 18 | 3.5 | | 0.3 | 0.0 | | 3.1 | | | | | | |
| 19 | 28.0 | | 0.2 | 0.0 | | 0.1 | | | | | | |
| 20 | 7.0 | | 0.0 | 1.0 | | 6.71 | | | | | | |
| 21 | 15.0 | | 0.0 | 1.0 | | 5.0 | | | | | | |
| 22 | 3.0 | 42.0 | 23.1 | 0.0 | | 32.0 | | | | | | |
| 23 | 7.5 | 0.0 | 1.9 | 0.0 | | 3.9 | | | | | | |
| 24 | 36.0 | 0.0 | 0.0 | 14.0 | | 0.8 | | | | | | |
| 25 | 2.0 | 1.0 | 0.2 | 1.2 | | 0.0 | | | | | | |
| 26 | 2.5 | 5.0 | 2.5 | 9.0 | | 12.0 | | | | | | |
| 27 | 1.0 | 1.0 | 13.5 | 0.2 | | 1.1 | | | | | | |
| 28 | 1.0 | 2.0 | 0.2 | 0.0 | | 0.8 | | | | | | |
| 29 | 0.5 | | 0.0 | 0.0 | | 0.1 | | | | | | |
| 30 | 0.0 | | 1.1 | 0.0 | | 7.4 | | | | | | |
| 31 | 0.5 | | 0.0 | | 0.0 | | | | | | | |
| , | | ŀ | | | | | | | | | | |
| Monthly total | 331.5 | 185.0 | 117.9 | 60.4 | 40.5 | | | | | | | |
| Day Max. | | - | 23.1 | 14.0 | | | | | | | | |
| | | | (A) | (A) | (A) | (A) | | | | | | |

(mm) Daily Rainfall Data at WSN-6 (Klamono) Table A.8a

Ν̈́Α Dec. Z. Ą. Nov. 219.0 58.0 ಕ N.A. Sep. 48.0 10.0 Aug. 247.0 50.0 E 1991 N.A. Jun. May ΝĀ 429.0 91.0 Apr. 351.5 50.0 Mar. 115.0 36.0 Feb. 0.00000 21.0 18.0 Jan. ×× ×× XXXX ×× × Monthly total Day Max. Month 4 2 9 1 00 Day

(mm) Daily Rainfall Data at WSN-6 (Klamono) Table A.8b

125.0 18.0 Dec. 110.5 30.0 Nov. 186.0 74.0 ö 204.0 50.0 Sep. 201.0 Aug. 299.0 54.0 Ξ 1992 510.0 142.0 Jun. Ϋ́ May 142.0 43.0 Apr. 142.0 37.0 Mar. 248.0 66.0 Feb. 83.0 36.0 Jan. Month Monthly total Day Max. ∞ 0

Dec. Ν̈́Α Nov. N.A (mm) Set. N.A. ΑN Sep. Aug. N.A Daily Rainfall Data at WSN-6 (Klamono) 496.0 89.0 Jul 1993 239.0 104.0 Jun. 43.0 May 397.0 99.0 Apr. Table A.8c Mar. N.A Feb. N.A. N.A. Jan. Month Monthly total Day Max. Day

Ϋ́ Dec. Nov. Ϋ́ ಕ Sep. Aug. Ę 1994 Jun. May Y Z Apr. Mar. N.A. Feb. Jan. Month 2= 9 00 0

9.0 8.0

112.0 25.0

103.0 26.0

539.0 98.0

390.0 73.0

163.0 45.0

156.0 42.0

Monthly total Day Max.

(mm)

Daily Rainfall Data at WSN-6 (Klamono)

 Table A.8d

Table A.8e Daily Rainfall Data at WSN-6 (Klamono)

(mm)

| Month | | | | | | 1005 | 35 | | | | | |
|---------------|--------------|---|-------|---|-------|---|------------------|------|------|---|---|---|
| | | | | | } | | | | | | ; | í |
| Day | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul | Aug. | Sep. | Öçt. | Nov. | Dec. |
| | | | | | | *************************************** | | | | *********** | *************************************** | |
| _ | | | 0.0 | | | 0.1 | | | | | | *************************************** |
| 2 | | | 0.0 | | | 0.1 | | | | 1 | | |
| 3 | | | 0.0 | - | | 0.7 | | | | | | |
| 7 | ************ | | 0.0 | | | 4.3 | | | | | | |
| 2 | | | 0.0 | | | 0.2 | | | | | | |
| 9 | | *************************************** | 0.0 | 0.0 | | 3.3 | 18.8 | | | | | |
| | | | 3.0 | | | 13.7 | | | | | | |
| | | | 16.0 | | | 3.9 | | | | | | |
| 6 | | | 2.0 | | | 29.7 | | | | | | |
| 0[| N.A. | ΑN | 0.0 | | | 0.7 | **** | | | | | |
| 11 | | | 0.9 | | | 18.3 | | | | | | |
| 12 | | | 0.0 | | | 6.7 | | | | | | |
| 13 | | | 0.0 | *************************************** | | 20.5 | | | | | | |
| 14 | | | 0.0 | | | 33.5 | | | | | | |
| 15 | | | 0.0 | | | 0.2 | | | | | | |
| 16 | | *************************************** | 7.0 | **** | | 0.5 | | | | | | |
| 17 | | *************************************** | 7.0 | | | 13.4 | | | | | | |
| 18 | | *************************************** | 0.0 | | | 2.8 | | | | | | |
| 19 | | | 8.0 | | | 1.3 | | | | | *************************************** | |
| 20 | | 714 5 6 6 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | 14.0 | | | 5.3 | | | | | | 100000000000000000000000000000000000000 |
| 21 | | 714 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 2.0 | | | 17.6 | | | | | | |
| 22 | | | 2.0 | | | 0.2 | | | | | | |
| 23 | | | 27.0 | | | 0.1 | | | | | | |
| 24 | | | 7.0 | | | 15.6 | | | | | 4 | |
| 25 | | | 7.0 | | | 0.7 | | | | | - | |
| 26 | | | 3.0 | | | 3.5 | | | | | | |
| 27 | | | 10.0 | Ī | 0.1 | 11.6 | | | | | | |
| 28 | | | 2.0 | 1.0 | 0.0 | 4.3 | | | | | | |
| 29 | | | 2.0 | | 0.1 | 0.2 | | | | | | |
| 30 | | · · · · · · · · · · · · · · · · · · · | 2.0 | 0.0 | 0.0 | 37.7 | | | | | | |
| 31 | | | 2.0 | | 0.1 | | 0.0 | | | | | |
| | | | | | | | | | | | | |
| Monthly total | | | 129.0 | 140.5 | 166.5 | 37.7 | 383.1 | | | | | |
| ì | | | | | € | `€ | (V) | | | | | |
| | | | | | | | | | | | | |

Sep. Aug. Ξ 1995 Jun. May Apr. $\begin{array}{c} 1.6 \\ 0.00 \\ 0.0$ Mar. Feb. ×× ×

Ϋ́

∞ 0

Des.

Nov.

8

(mm)

Daily Rainfall Data at the New Gauging Station

Table A.9

Jan.

Day

Month

(A): Rainfall data measured by an automatic raingauge

605.5

430.6 75.5

245.0 74.5

40.0 40.0

143.8 39.4

Monthly total Day Max.

3

APPENDIX B WATER LEVEL AT MALANO AWLR

Table B.1 Water Level and Calculated Discharge at Malano AWLR (1/5)

| | ا بر | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | - | - | | | |
|------------|---------|-----------|--------|--------|-------|--------|--------|----------|-------|-------|--------|----------|-------|----------|-------|--------|--------|--------|-------|-------------|-------|-------------|-------|-------|-------|----------|-------|-------|-----------|--------|-------|----------|-------|---------|
| (m3/s) | Dec | H(m) | | ••••• | | | | | ••••• | | | N. | | • | | | | ••••• | | | | | ***** | | ••••• | ••••• | ••••• | ***** | ••••• | ••••• | ***** | | ••••• | |
| Ë | | Ħ | _ | | | | | | | | | 2 | | | | | | | | | | | | | | | | | | | | ···- | | |
| | Nov | ٥ | | ***** | | | | | | | | | | ••••• | | | ••••• | | ····· | | | | | | ···· | | ••• | | - | ···· | | ••••• | •••• | |
| | | H(m) | | | | | | | | | | X. | | | | | | | | | | | | | | | | | | | | | | |
| | Oct | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| |) | H(m) | | | •••• | | | | | | | Ϋ́ | | | | | | ••••• | | ••••• | ••••• | | | ••••• | ••••• | | | **** | ••••• | | ***** | ***** | ••••• | |
| | | 0 | 14.97 | 14.36 | | | | | | | | | | | | | | | | | | | | | • | | | | | | | | | 14.66 |
| | Sep | | | ••••• | | | | ••••• | | | | | | ••••• | | •••• | | ••••• | | | | ••••• | | | | | ••••• | | ••••• | ••••• | | | | 17 |
| | | H (m) | 6 0.67 | 2 0.66 | | | · · | · - | - | | · ~ | | - 2 | <u>.</u> | - | er. | - 2 | | | | | <u>.</u> | • | | per . | <u>'</u> | 5 ، | ٠ | | , | | <u>,</u> | 9 | 2 |
| | Aug | 0 | 30.39 | 24.42 | 21.20 | 19.30 | 18.05 | 18.67 | 43.72 | 52.65 | 35.88 | 31.75 | 55.72 | 38.70 | 35.19 | 48.88 | 55.72 | 53.41 | 49.63 | 44.45 | 35.19 | 25.73 | 19.30 | 16.81 | 15.58 | 15.58 | 14.36 | 14.36 | 13.75 | 16.19 | 23.13 | 16.19 | 14.36 | 29.67 |
| | | H(m) | 0.91 | 0.82 | 0.77 | 0.74 | 0.72 | 0.73 | 1.10 | 1.22 | 0.99 | 0.93 | 1.26 | 1.03 | 0.98 | 1.17 | 1.26 | 1.23 | 1.18 | 1.1 | 0.98 | 0.84 | 0.74 | 0.70 | 0.68 | 0.68 | 99.0 | 99.0 | 0.65 | 69.0 | 0.80 | 69.0 | 99.0 | |
| , | Jul | 0 | 83.53 | 83.53 | 82.67 | 112.61 | 189.46 | 118.38 | 95.91 | 88.77 | 80.10 | 103.22 | 73.35 | 90.54 | 90.54 | 120.32 | 272.85 | 126.22 | 81.81 | 66.79 | 52.65 | 43.72 | 36.58 | 20.72 | 32.43 | 23.77 | 24.42 | 99.54 | 70.05 | 44.45 | 30.39 | 27.05 | 35.88 | 81.01 |
| | ĭ | H (m) | 99: | ***** | | 1.92 | 2.65 | 86:1 | 1.74 | | 1.56 | 1.82 | | 1.68 | 1.68 | | 3.32 | | 1.58 | | | 1.10 | 8: | 9.3 | ••••• | 0.81 | | | | E. | 16:0 | 0.86 | 66:0 | •••• |
| | _ | | _ | | _ | | | | | | | _ | | _ | | | | | | | | | _ | _ | _ | | _ | | _ | | _ | | _ | _ |
| | Jun | 0 | ļ | ***** | •••• | •••• | | | | | | | | •••• | | | | | | | | | | ***** | | | | | | ••••• | | **** | | |
| | | H(m) | _ | | | | | | | | | N.A. | | | | | | | | | | | | | | | | | | | | | • | |
| | May | 0 | | ***** | | | | | | | | | | | | ••••• | | | | . . | | • • • • • • | | •••• | | | | | | | | | | |
| | | H(m) | | | | | | | | | | Ϋ́ | | | | | | | | | | | | | | | | | | | | | | |
| | 8. | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Apr | H (m) | | ••••• | ••••• | | · | ••••• | | | ····· | ٠ ۲ | | ••••• | | | | ••••• | | | | ••••• | | | | ••••• | | | •••• | | | •••• | | |
| | | | _ | | | | | | | | | Z | | | | | | | _ | | | | | | | | | | | | | | | _ |
| | Mar | 0 | ļ | | | | | ••••• | | | | | | | ••••• | ••••• | ••••• | | | | | | | | | | | ···· | | ••••• | | | | •••• |
| | | (II) H | | | | | | | | | | × | | | | | | | | | | | | | | | | | | | | | | |
| | Feb | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | H(m) | | | | | | ••,••• | | | | Ž. | | | | | | ***** | | ••••• | | | | ••••• | | | | | ., | ••••• | | ••••• | | |
| 166 | _ | 0 | | | | | | | | | | | | | | | | | • | | | | | | | | | | | | | | | |
| Year: 1991 | Jan | ļ | ļ | ••••• | **** | | ••••• | ***** | | | | < | | | | ***** | | ••••• | | | | | ••••• | ••••• | | | | ••••• | | | ••••• | | | |
| Ye | ية ا | H(m) | _ | | | | | | | | | Y.Y | | | | | | | | | | | | | | | | | _ | | | _ | | 386 |
| | Date | | - | 2 | ٣ | 4 | 2 | 9 | 7 | ∞ | ^ | <u> </u> | = | 12 | == | 7 | 15 | 91 | 17 | <u>×</u> | 19 | 8 | 21 | 77 | ឧ | 72 | ম | 8 | 77 | 88 | 23 | 옷 | 31 | Average |

 (-) No data
 Discharge was Notes:

Discharge was calculated by using the rating curve shown in the Pre-F/S Report H \geq 0.65 m : Q = 13.713 H+2 + 42.599 H - 19.73 H \leq 0.65 m : Q = 23.362 (H + 0.123)*2

Table B.1 Water Level and Calculated Discharge at Malano AWLR (2/5)

| Γ. | 0 | , | | | | | | | | | | • | | | | | | | | | | | | | | | | | | | | | Τ |
|----------|----------|--------------|--------|--------|--------|----------|--------|-------|-------|--------|----------|--------|--------|---------|--------|--------|--------|--------|----------|--------|-----------|--------|----------|--------|--------|--------|---|----------|---|---------|---------|--------|----------|
| 2 | ļ | . | | | ••••• | | | | | | نهد | ••••• | | | •••• | ••••• | ••••• | ••••• | ***** | ••••• | ••••• | ••••• | •••• | ••••• | | | | ••••• | | ••••• | ••••• | ••••• | ļ |
| | E) | | | | | | | | | | X. | | | | | | | | | | | | | | | | | | | | | | Ļ |
| Š | 0 | | | | | | | | | | •••• | •-•• | | | | | | | | | | | | | | | | | · • • • • • • • • • • • • • • • • • • • | ••••• | | • | |
| | H (m) | | | | | | | | | | X. | | | | | | | | | | | | | | | | | | | | | | |
| ĕ | 0 | | | | | | | | | | | | | | | | | | | | | | Ī | | | | | | | | | | Ī |
| ľ | H(m) | - | | ••••• | | | | ••••• | ••••• | ••••• | Z. A. | | | | | | | | | | ***** | ••••• | | | •••• | ••••• | · • • • • • • • • • • • • • • • • • • • | | | ••••• | | ••••• | ļ. |
| ┝ | | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | l |
| જુ | 1 | .ļ | ***** | | | | | | | ••••• | | | | | | | | | | | | | | ••••• | | | | | | | | | |
| L | H (m) | | | | | | | | | | N. | | | | | | | | | | | | | | | | | | | | | | ļ |
| Aug | , 0 | <u>'</u> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | H (m) | | | | | | | | | | Ϋ́ | | | | | | | | | | | | | | | | | | | | ••• | ••••• | ľ |
| Ę | 0 | 39.40 | 36.58 | 34.49 | 33.80 | 32.43 | 31.75 | 31.07 | 30.39 | 29.72 | 29.05 | 32.43 | 37.28 | 43.72 | 50.38 | 70.87 | 27.72 | 116.44 | 466.39 | 153.97 | 110.71 | 27.72 | 93.21 | 90.54 | 86.14 | 80.95 | 82.67 | 143.46 | 164.76 | 152.91 | 178.11 | 214.27 | |
| Ę | H(m) | .+ | 8 | 0.97 | 96.0 | 0.94 | 0.93 | | 16.0 | 0.90 | 68.0 | 0.94 | 1.01 | 1.10 | 1.19 | 1.45 | 1.76 | | 4.60 | 2.33 | . <u></u> | 1.76 | 17.1 | 1.68 | 1.63 | 1.57 | 1.59 | 2.23 | 2.43 | 2.32 | 2.73 | 2.86 | ļ. |
| - | ╁ | 27 | 178.07 | 197.59 | 213.06 | _ | _ | | | 219.13 | 242.83 (| 364.00 | 324.18 | 399.51 | 397.93 | 374.66 | 325.62 | 468.08 | 335.77 4 | 278.22 | 224.04 | 180.32 | 179.19 | 172.47 | 163.67 | 151.85 | 138.31 | 120.32 2 | 87.01 2 | 56.49 2 | 43.72 2 | - 7 | |
| Jun | ٠ | . + | | ***** | | | | | | | ***** | ••••• | | | **** | | | ***** | ••••• | ••••• | ••••• | ***** | | ***** | | | | ***** | | ***** | | | |
| | H (m) | + | 2.55 | 2.72 | 2.85 | | • | ' | | 2.90 | 3.09 | 3.96 | 3.69 | 4.19 | 4.18 | 4.03 | 3.70 | 4.61 | 3.7 | 3.36 | 2.94 | 2.57 | 2.56 | 2.50 | 2.42 | 2.31 | 2.18 | 2.00 | 26. | 1.27 | 1.10 | | ļ |
| May | . 0 | 128.20 | 226.51 | 170.26 | 137.28 | - | | ••••• | | ****** | | | | | | | | | | | | ***** | | | | | | | | | | | 1 |
| | H(m) | 2.08 | 2.96 | 2.48 | 2.17 | • | | | | • | • | | | • | • | | | | , | | | • | | , | • | , | , | | • | • | • | ı | |
| Apr | 0 | 31.07 | 45.18 | 112.61 | 186.01 | 165.85 | 149.73 | | | | | | | | 165.85 | 162.58 | 142.42 | 122.27 | 108.82 | 94.11 | 75.02 | 35.88 | 25.07 | 28.38 | 48.14 | 45.18 | 46.65 | 68.41 | 115.48 | 136.26 | 134.23 | | 47. 20 |
| \ | H (m) | ·+ <i></i> - | 1.12 | 1.92 | | 2.44 | ••••• | | • | • | • | | | • | 2.44 | 2.41 | 2.22 | 2.02 | 1.88 | 1.72 | 1.50 | 8 | 0.83 | 0.88 | 1.16 | 1.12 | 1.14 | 1.42 | 1.95 | 2.16 | 2.14 | ••••• | - |
| _ | \vdash | ╁╴ | | _ | | | | | • | | | | | | - | - | - | | _ | _ | _ | _ | _ | _ | _ | _ | | _ | _ | ~ | _ | 71 | 2001 |
| Mar | 0 | ļ | 8.22 | | | | | | | | | | | | ••••• | | | | | •••• | | | | •••• | | | ••••• | | •••• | ···•• | 33.80 | 17.71 | |
| _ | H(m) | 0.48 | 0.47 | | • | <u>'</u> | • | • | • | • | <u> </u> | • | • | • | • | | • | • | • | • | • | • | | ٠. | • | • | • | • | • | • | 8.0 | 0.87 | L |
| Feb | 0 | | | 13.60 | 18.67 | 16.19 | 60.39 | 78.39 | 55.72 | 35.19 | 33.80 | 13.25 | 11.55 | 10.58 | 9.66 | 96.6 | 43.72 | 168.05 | 172.47 | 109.77 | 71.70 | 34.49 | 17.43 | 12.90 | 10.90 | 10.27 | 10.27 | 99.6 | 8.78 | 8.49 | | | 100 |
| | (E) | ١. | , | 9.0 | 0.73 | 69.0 | 1.32 | 1.54 | 1.26 | 0.98 | 8 | 0.63 | 0.58 | 0.55 | 0.52 | 0.53 | 1.10 | 2.46 | 2.50 | 1.89 | 1.46 | 0.97 | 17.0 | 0.62 | 0.56 | 0.54 | 0.54 | 0.52 | 0.49 | 0.48 | ***** | | |
| Ę | 0 | | | | | | | | | | | | | | • | | | | | | | | | | | | | | | | | | |
| Jan | H(m) | | ••••• | | ***** | | ****** | ••••• | ••••• | ••••• | Ϋ́ | | ****** | | ••••• | ***** | • | | | | | | ***** | | •••• | ***** | | ***** | ••••• | | ***** | ••••• | - |
| <u>چ</u> | Ξ | - | | | | | | | | | <u>z</u> | _ | · · · | _ | | | | _ | ~ | _ | | | <u> </u> | | _ | | | | | | | | <u>.</u> |
| Date | | - | 7 | 3 | 4 | S | 9 | 7 | 90 | Ò | 2 | Ξ | 12 | 33 | 7 | 15 | 16 | 17 | 8 | 6 | ឧ | 77 | 22 | 23 | 2 | 23 | 8 | 27 | 28 | 23 | 옸 | 31 | A |

 (-) No data
 Discharge was Notes:

Discharge was calculated by using the rating curve shown in the Pre-F/S Report $H \ge 0.65 \, \mathrm{m}$: $Q = 13.713 \, H^{\prime}2 + 42.599 \, H \cdot 19.73$ $H \le 0.65 \, \mathrm{m}$: $Q = 23.362 \, (H + 0.123)^{\prime}2$

Table B.1 Water Level and Calculated Discharge at Malano AWLR (3/5)

| | | 0 | 41.55 | 41.55 | 40.12 | 39.40 | 37.99 | 37.99 | 37.28 | 37.28 | 36.58 | 35.19 | 35.19 | 33.80 | 31.75 | 31.07 | 30.39 | 29.05 | 28.38 | 27.05 | 25.73 | 24.42 | 23.13 | 23.13 | 23.13 | 23.13 | 23.13 | 23.13 | 23.13 | 27.71 | 45.92 | 57.26 | 65.17 | 22.54 |
|--------|----------|-------|-------------|--------|--------|----------|--------|----------|---------|----------|----------|---------|--------|--------|------------|--------|---------|---------|--------|----------|---------|----------------|-----------|----------|--------|----------|--------|---------------|-------|----------|--------|--------|-------------|---------|
| (s) |)oc | | | | | | | ••••• | | | | | | ••••• | | | ••••• | | | | | | ••••• | | ••••• | | ••••• | ••••• | | | ••••• | | · · · · · · | |
| (m3/s) | | H (m) | 1.07 | 1.07 | 1.05 | 프 | 1.02 | 1.02 | 1.01 | 1:01 | 100 | 0.98 | 0.98 | 860 | 0.93 | 0.92 | 0.91 | 0.89 | 0.88 | 0.86 | 0.84 | 0.82 | 08.0 | 08.0 | 0.80 | 08.0 | 08:0 | 08.0 | 0.80 | 0.87 | 1.13 | 1.28 | 1.38 | |
| | Nov | O | | | | | | ••••• | | | | | | | . | | | | | •••• | | ·•••• | . | | 55.72 | 52.65 | 50.38 | 48.14 | 46.65 | 45.92 | 44.45 | 43.00 | | 48 36 |
| | | H (m) | | | | • | | | • | | • | | | • | • | | • | | , | • | | | • | | 1.26 | 1.22 | 1.19 | 1.16 | 1.14 | 1.13 | Ξ: | 1.09 | | |
| |) = H | ٥ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Oct | Н (ш) | · | ••••• | ·· | | ••••• | ••••• | ••••• | | | Ý Z | ••••• | | | | | | | | | ••••• | ••••• | | | | | | | ••••• | ••••• | ••••• | ••••• | |
| | | | | | | | | | | | | _ | | | | | | | | | | | | | | | | | | | | | | - |
| | Scp | 0 | . . | | | | | - | | | ···· | ····· | | | | | | | ••••• | ••••• | | | | - | | · | | | | <i>-</i> | | | •••• | |
| | | H(m) | | | | | | | | | | Ä.Ä. | | | | | | | | | | | | | | | | | | | | | | |
| | Aug | 0 | | 164.76 | 159.33 | 151.85 | 145.54 | 133.22 | 101.38 | 85.27 | 11.70 | 66.79 | 63.57 | 61.98 | 60.39 | 59.61 | 58.82 | 57.26 | 56.49 | 54.95 | 52.65 | 51.14 | 48.88 | 47.39 | 45.18 | | | | | | | | | 2 |
| | | H (m) | , | 2.43 | 2.38 | 2.31 | 2.25 | 2.13 | 1.80 | 1.62 | 1.46 | 1.40 | 1.36 | 134 | 1.32 | 131 | 3 | 1.28 | 1.27 | 1.25 | 1.22 | 1.20 | 1.17 | 1.15 | 1.12 | , | • | , | , | , | ' | • | ' | |
| | | o | 459.66 | 175.82 | 130.20 | 150.79 | 201.12 | 179.19 | 152.91 | 183.73 | 226.51 | 233.99 | 197.59 | 140.36 | 123.26 | 118.38 | 116.44 | 107.88 | 100.46 | 93.21 | 116.44 | 10901 | 87.89 | 77.55 | 78.39 | 95.01 | 122.27 | | | | | | | 151 00 |
| | Jul | H (m) | 4.56 4 | 2.53 | 2.10 | 2.30 | 2.75 | 2.56 | 2.32 | 2.60 | 2.96 | 3.02 | 2.72 | 2.20 | 2.03 | 1.98 | .8 | 1.87 | 1.79 | 1.71 | 1.8 | 1.85 | .65 | . 53 | 54 | 1.73 | 2.02 | | | | | | | |
| | _ | H | 4. | | | | | | - 7 | 2. | .2 | <u></u> | -2 | 2. | -7 | | | | | | | _ | _ | _ | _ | | | 9 | 90 | 2 | - 26 | 98 | _ | 3 |
| | Jun | Ö | | 39.40 | 35.19 | 54.18 | 48.88 | 86.14 | | | | | | | | | 195.26 | 144.50 | 103.22 | 112.61 | 66.79 | 55.72 | 43 | 40.12 | 37.6 | 37.28 | 37.28 | 39.40 | 61.18 | 43.00 | 182.59 | 648.86 | ••••• | 10063 |
| | | H(m) | Ŀ | 1.02 | 0.98 | 1.24 | 1.17 | 1.63 | • | ' | • | , | • | • | ' | • | 2.70 | 2.24 | 1.82 | 1.92 | 1.40 | 1.26 | 1.10 | 1.05 | 1.02 | 1.01 | 1.0 | <u>.</u> 요 | 1.33 | 1.08 | 2.59 | 5.60 | | L |
| | May | o | | | 73.35 | 63.57 | 61.18 | 95.01 | 76.70 | 87.89 | 87.89 | 96.81 | 224.04 | 147.63 | 91.43 | 87.89 | 87.01 | 91.43 | 170.26 | 90.54 | 58.04 | 62.77 | 50.38 | 46.65 | 49.63 | 74.19 | | | | | | | | 80 74 |
| | _ | H(m) | , | | 1.48 | 1.36 | 1.33 | 1.73 | 1.52 | 1.65 | 1.65 | 1.75 | 2.94 | 2.27 | 1.69 | 1.65 | 2 | 1.69 | 2.48 | 1.68 | 1.29 | 1.35 | 1.19 | 1.14 | 1.18 | 1.49 | • | 1 | • | 1 | | | • | |
| | | 0 | 47.39 | 81.81 | 81.81 | 90.54 | 09:19 | 02.92 | 27.72 | 94.11 | 80.95 | 135.25 | 240.29 | 189.46 | 145.54 | 166.95 | 123.26 | 140.36 | 87.01 | 93.21 | 75.86 | | | • | | | | | | | • | | | 111 36 |
| | Apr | | ļ. | | 1.58 | •••• | | | 1.76 | | | •••• | | | | | | | | ····· | | | | | | | | | | | | | | = |
| | _ | H(m) | 8 1.15 | 9 1.58 | | 9 1.68 | 9 1.41 | 2 1.52 | | 2 1.72 | 2 1.57 | 9 2.15 | 8 3.07 | 5 2.65 | 2 2.25 | 9 2.45 | 5 2.03 | 5 2.20 | 1 1.64 | 1.7 | 2 1.5 | - - | - 7 | · • | 6 | | | | | <u>.</u> | _ | _ | 7 | _ |
| | Mar | 0 | 35.88 | 35.19 | 31.75 | 30.39 | 30.39 | 29.72 | 36.58 | 45.92 | 43.72 | 47.39 | 37.28 | 31.75 | 58.82 | 51.89 | 46.65 | 52.65 | 68.41 | 70.87 | 55.72 | 48.14 | 43.72 | 36.58 | 30.39 | 31.07 | 37.99 | 54.95 | 44.45 | 40.83 | 39.40 | 33.80 | 31.07 | 17 77 |
| | | H(m) | 0.99 | 0.98 | 0.93 | 0.91 | 0.91 | 0.90 | 1.00 | 1.13 | 1.10 | 1.15 | 1.01 | 0.93 | 1.30 | 1.21 | 1.14 | 1.22 | 1.42 | 1.45 | 1.26 | 1.16 | 1.10 | 1.00 | 0.91 | 0.92 | 1.02 | 1.25 | 1.11 | 9.1 | 1.04 | 96.0 | 0.92 | |
| | Feb | ō | 71.70 | 52.65 | 61.98 | 54.95 | 58.04 | 54.18 | 43.00 | 33.80 | 33.12 | 52.65 | 47.39 | 40.83 | 33.12 | 46.65 | 30.39 | 35.88 | 40.12 | 37.28 | 36.58 | 40.83 | 42.27 | 16.19 | 12.55 | 11.22 | 17.43 | 60.39 | 34.49 | 22.48 | | , | • | 40.08 |
| | Œ. | H(m) | 1.46 | 1.22 | 1.34 | 1.25 | 1.29 | 1.24 | 69: | 8. | 0.95 | 1.22 | 1.15 | 8. | 0.95 | 1.14 | 0.91 | 86. | 1.05 | 101 | 9. | 90. | 80.1 | 69.0 | 190 | 0.57 | 0.71 | 1.32 | 16.0 | 0.79 | • | , | | |
| 1993 | \vdash | | 20.57 | 20.57 | 13.60 | 8.49 | 7.14 | 6.39 | 5.68 | 5.45 (| 5.68 | 4.58 | 3.61 | 3.08 | 2.91 | 5.23 | 58.04 (| 68.41 | 92.32 | 87.01 | 91.43 | 124.24 | 155.04 | 164.76 | 174.70 | 181.45 (| 184.87 | 122.27 | 82.67 | 76.70 | 10.901 | 10.901 | 90.54 | 67.08 |
| | Jan | 0 | ļ | | | | | | | | | ***** | | ••••• | | ••••• | ····· | | | •••• | ••••• | | | | | | | | •••• | **** | •••• | | ••••• | |
| Year: | _ | H(m) | 0.76 | 0.76 | 25. | 0.48 | 0.43 | 0.40 | 0.37 | 0.36 | 0.37 | 0.32 | 0.27 | 0.24 | 0.23 | 0.35 | 1.29 | 1.42 | 1.70 | 25. | 1.69 | 202 | 2.34 | 2.43 | 2.52 | 2.58 | 2.61 | 202 | 1.59 | 1.52 | 1.85 | 1.85 | 1.68 | 5 |
| | Date | | - | 2 | 3 | 4 | ٠, | 9 | 7 | ∞ | 6 | 2 | = | 12 | E 1 | 14 | 15 | 91 | 17 | <u>«</u> | 19 | 8 | 21 | 22 | 23 | 73 | 22 | 92 | 27 | 83 | 53 | 30 | 31 | Average |

Notes:

Discharge was calculated by using the rating curve shown in the Pre-F/S Report H \geq 0.65 m : Q = 13.713 H $^{\prime}$ 2 + 42.599 H $^{\prime}$ 19.73 H \leq 0.65 m : Q = 23.362 (H $^{\prime}$ 0.123) $^{\prime}$ 2 (-) No data
 Discharge was

Table B.1 Water Level and Calculated Discharge at Malano AWLR (4/5)

| | [, | 0 | 32.71 | 32.20 | 44.00 | 60.11 | 86.55 | 73.20 | 72.52 | 72.52 | 72.52 | 71.17 | 70.50 | 70.50 | 68.51 | 68.51 | 68.51 | 69.17 | 66.53 | 65.23 | 65.88 | 65.23 | 63.93 | 61.38 | 59.48 | 55.15 | 51.53 | 48.01 | 44.00 | 39.57 | 35.83 | 33.22 | 34.26 | 58.79 |
|----------|------|--------|---------|----------|----------|----------|----------|----------|----------|----------|----------|--------------|----------|----------|----------|----------|---------------------------------|--------|----------|--------|--------|----------|----------|--------|--------|----------|--------|------------|--------|--------|----------|--------|---------|---------|
| (ш3/s) | Dec | Ê | ļ | | | 1.12 📒 6 | .51 | 32 7 | 131 | 131 | 1.31 | 1.29 | 1.28 | 1.28 | 1.25 6 | 1.25 6 | 1.25 | .26 6 | 1.22 | 1.20 | 121 6 | 1.20 | 1.18 | 1.14 6 | 1.11 | 1.04 | | | 0.85 | | 0.70 | 0.65 | | |
| (m) | ļ | H (m) | 9.04 | 9 0.63 | 5 0.85 | | _ | _ | _ | _ | | - | | | | | _ | _ | _ | | _ | | | | _ | | 0.98 | 4 0.92 | _ | 7.0 | | | 0.67 | -6 |
| | Nov | 0 | 55.76 | 56.99 | 55.15 | 52.13 | 50.35 | 54.54 | 78.71 | 70.50 | 62.65 | | 53.94 | 53.33 | 51.53 | 50.35 | 50.35 | 50.35 | 52.13 | 52.73 | 52.13 | 49.17 | 46.28 | 45.13 | 44.57 | 40.12 | 35.30 | 33.74 | 31.19 | 34.78 | 34.26 | 31.19 | ••••• | 49.29 |
| | | H (m) | 1.05 | 1.07 | <u> </u> | 0.99 | 0.96 | 1.03 | 1.40 | 1.28 | 1.16 | • | 1.02 | 1.01 | 0.98 | 98.0 | 98. | 0.98 | 0.99 | 8.1 | 0.99 | 0.94 | 0.89 | 0.87 | 0.86 | 0.78 | 0.69 | 99.0 | 0.61 | 0.68 | 19.0 | 0.61 | | |
| : | Oct | ŏ | 23.43 | 22.97 | 23.43 | 24.37 | 24.37 | 24.37 | 24.37 | 24.37 | 24.37 | 24.37 | 24.37 | 24.37 | 24.37 | 24.37 | 24.37 | 23.90 | 24.37 | 24.84 | 24.84 | 24.84 | 24.84 | 24.84 | 27.23 | 37.42 | 40.12 | 40.12 | 36.35 | 37.95 | 41.21 | 41.77 | 58.23 | 28.87 |
| | | H (m) | 0.45 | 0.44 | 0.45 | 0.47 | 0.47 | 0.47 | 0.47 | 0.47 | 0.47 | 0.47 | 0.47 | 0.47 | 0.47 | 0.47 | 0.47 | 0.46 | 0.47 | 0.48 | 0.48 | 0.48 | 0.48 | 0.48 | 0.53 | 0.73 | 0.78 | 0.78 | 0.71 | 0.74 | 0.80 | 0.81 | 1.09 | |
| | | 0 | 35.83 | 34.78 | 35.83 | 33.74 | 28.20 | 27.23 | 26.75 | 26.75 | 26.75 | 26.75 | 26.75 | 26.75 | 26.75 | 26.75 | 26.75 | 26.27 | 25.79 | 24.84 | 24.84 | 24.84 | 24.84 | 24.84 | 24.84 | 24.84 | 24.84 | 24.37 | 24.37 | 24.37 | 14.37 | 23.90 | | 26.95 |
| , | Sep | ļ | | | | | | | | | | | | | | | | | | | | | | | ••••• | | | | | | | | | 36 |
| | _ | H(m) | 0 0.70 | 0.68 | 0 0.70 | 7 0.66 | 5 0.55 | 9 0.53 | 3 0.52 | 3 0.52 | 5 0.52 | 3 0.52 | 5 0.52 | 5 0.52 | 8 0.52 | 4 0.52 | 1 0.52 | 6 0.51 | 1 0.50 | 1 0.48 | 5 0.48 | 5 0.48 | 4 0.48 | 6 0.48 | 9 0.48 | 1 0.48 | 1 0.48 | 1 0.47 | 1 0.47 | 1 0.47 | 7 0.47 | 8 0.46 | 96 | 5 |
| | Aug | 0 | 70.50 | | 70.50 | 69.17 | 67.85 | 67.19 | 66.53 | 65.23 | 67.85 | 63.93 | 62.65 | 62.65 | 61.38 | 60.74 | 60.11 | 58.86 | 57.61 | 57.61 | 55.15 | 55.15 | 53.94 | 49.76 | 48.59 | 48.01 | 48.01 | 48.01 | 48.01 | 48.01 | 41.77 | 36.88 | 36.88 | 56.95 |
| | | H (m) | 1.28 | • | 1.28 | 1.26 | 1.24 | 1.23 | 1.22 | 1.20 | 1.24 | 1.18 | 1.16 | 1.16 | 1.14 | 1.13 | 1.12 | 1.10 | 1.08 | 1.08 | 9. | <u>5</u> | 1.02 | 0.95 | 0.93 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.81 | 0.72 | 0.72 | |
| . | Ju. | ŏ | | | | 155.20 | 148.08 | 118.70 | 112.65 | 110.63 | 107.04 | 99.24 | 92.43 | 90.20 | 90.20 | 90.20 | 90.94 | 108.63 | 100.78 | 88.73 | 17.76 | 93.93 | 88.73 | 86.55 | 83.66 | 80.11 | 66.53 | 59.48 | 57.61 | 57.61 | 58.23 | 64.58 | | 92.53 |
| | | Н(ш) | • | 1 | | 2.26 | 2.19 | 8. | 1.84 | 1.82 | 1.78 | 1.68 | 1.59 | 1.56 | 1.56 | 1.56 | 1.57 | 1.80 | 1.70 | 7. | 99: | 19.1 | 1.54 | 1.51 | 1.47 | 1.42 | 1.22 | Ξ | 1.08 | 1.08 | 1.09 | 1.19 | • | |
| | _ | ŏ | 248.72 | 224.91 | 269.52 | 205.33 | 317.70 | 246.65 | 268.48 | 349.37 | 387.63 | 265.36 | 214.60 | 217.69 | 274.74 | 210.48 | 168.45 | 259.11 | 190.95 | | | | | | | | | | | | | | | 254.10 |
| | Jun | Н(ш) | .17 2 | 2.94 2 | 3.37 | 2.75 2 | 3.83 | ••••• | 3.36 | | 4.49 | 3.33 2 | 2.84 2 | 2.87 | 3.42 2 | 2.80 | 2.39 | 3.27 2 | 2.61 | , | | , | | | ······ | | | , | | | | , | | 2 |
| | | | 99 | | | | | 258.07 3 | | 194.03 4 | | 160.29 3 | 133.87 2 | 133.87 2 | 131.85 3 | 129.82 2 | 124.76 2 | 114.66 | 105.46 2 | 10: | 112.65 | 131.85 | 125.77 | 116.68 | 79 | 33 | 135.90 | 3 8 | 149.09 | 18: | 57. | 9. | 162.33 | 99. |
| | May | O G | 354.66 | 1 242.50 | 7 290.41 | 3 244.57 | 3 312.44 | | 5 257.03 | ······ | 3 177.64 | | | | | | | | | 100:01 | | | | | 109.62 | 2 102.33 | | 178.66 | | 128.81 | 5 123.75 | | | 168.06 |
| | | H (m) | 3 4.18 | 3.1 | 3.57 | 3.13 | 3.78 | 3 3.26 | 3.25 | 2.64 | 2.48 | 2.31 | 2.05 | 2.05 | 2.03 | 2.01 | - - - - - - - | 1.86 | 1.76 | 1.69 | 1.84 | 2.03 | 1.97 | 1.88 | | | 2.07 | 1 2.49 | 2.20 | 2.00 | 1.95 | 2.37 | 2.33 | |
| | Apr | 0 | 110.63 | 98.19 | 87.27 | 82.95 | 119.71 | 116.68 | 105.46 | 94.68 | 80.82 | 69.17 | 63.29 | 57.61 | 52.73 | 56.38 | 116.68 | 94.68 | 90.04 | 103.11 | 1000 | 94 68 | 95.43 | 91.69 | 122.74 | 137.93 | 126.79 | 122.74 | 140.97 | 313.49 | 188.90 | 201.22 | | 111.18 |
| | | H (m) | 1.82 | 1.64 | 1.52 | 1.46 | 1.91 | 1.88 | 1.76 | 1.62 | 1.43 | 1.26 | 1.17 | 1.08 | 1.00 | 1.06 | 1.88 | 1.62 | 1.57 | 1.73 | 1.69 | 1.62 | 1.63 | 1.58 | 1.94 | 2.09 | 1.98 | 1.94 | 2.12 | 3.79 | 2.59 | 2.71 | | ١ |
| | Mar | Õ | 33.22 | 32.71 | 32.20 | 31.19 | 31.19 | 127.80 | 147.06 | 100.78 | 94.68 | 88.73 | 132.86 | 166.40 | 169.47 | 203.27 | 250.80 | 129.82 | 119.71 | 162.33 | 135.90 | 122.74 | 136.91 | 151.13 | 102.33 | 81.53 | 70.50 | 66.53 | 89.47 | 90.94 | 89.47 | 126.79 | 149.09 | 111.86 |
| | Ŋ | H (m) | 9.65 | 64 | 0.63 | 19:0 | 19.0 | 85 | 2.18 | 1.70 | 1.62 | 3. | 5.04 | 2.37 | 2.40 | 2.73 | 3.19 | 2.01 | 1.91 | 2.33 | 2.07 | 3 | 2.08 | 2.22 | 1.72 | <u>쿠</u> | 1.28 | 1.22 | 1.55 | 1.57 | 1.55 | | 2.20 | |
| | _ | 0 | 42.88 | 41.77 | 40.67 | 39.57 | 39.03 | 39.03 | 71.85 | 174.57 | 141.98 | 107.04 | 79.41 | 75.94 | 71.85 | 69.17 | 63.29 | 58.23 | 53.94 | 50.35 | 48.01 | 46.28 | 45.70 | 31.69 | 28.20 | 29.68 | 37.95 | 39.03 | 26.27 | 33.74 | | - | | 58.11 |
| | Feb | | | | | | | | | ••• | | | | 1.36 | | 1.26 | | 1.09 | 1.02 | ••••• | | | - | | | | ••••• | | | | | ••••• | | |
| 4 | | H (m) | 3 0.83 | 0 0.8 | 3 0.79 | 1 0.77 | 5 0.76 | 3 0.76 | 9 1.30 | 9 2.45 | 8 2.13 | 1 1.78 | 3 1.41 | | 7 1.30 | | 6 1.17 | | | 3 0.96 | 2 0.92 | 5 0.89 | 3 0.88 | 8 0.62 | 3 0.55 | | 4 0.74 | | 7 0.51 | 1 0.66 | | ~ | - | 2 |
| : 1994 | Jan | 0 | 88.73 | 88.00 | 81.53 | 80.11 | 71.85 | 65.23 | 61.19 | 67.19 | 84.38 | 78.71 | 66.53 | 68.51 | 87.27 | 88.00 | 83.66 | 80.82 | 79.41 | 76.63 | 72.52 | 67.85 | 63.93 | 61.38 | 58.23 | 56.38 | 53.94 | 51.53 | 49.17 | 48.01 | 46.28 | 45.13 | 44.00 | 68.45 |
| Year: | | H (m) | 1.54 | 1.53 | 1.44 | 1.42 | 1.30 | 1.20 | 1.23 | 1.23 | 1.48 | 1.40 | 1.22 | 1.25 | 1.52 | 1.53 | 1.47 | 1.43 | 1.41 | 1.37 | 1.31 | 1.24 | 1.18 | 1.14 | 1.09 | 1.06 | 1.02 | 0.98 | 0.94 | 0.92 | 0.89 | 0.87 | 0.85 | |
| | Date | | - | 2 | 3 | 4 | 5 | 9 | 7 | ∞ | 6 | 01 | = | 12 | 13 | 14 | 15 | 16 | 11 | 18 | 61 | 8 | 21 | 22 | 23 | 75 | 22 | 76 | 11 | 78 | ೱ | 30 | = | Average |

 (-) No data
 Discharge was Notes:

Discharge was calculated by using the rating curve obtained in this F/S H \geq 1.80 m : Q = 1.1013 H^2 + 96.797 H - 69.19 H \leq 1.80 m : Q = 12.294 H^2 + 35.446 H + 4.99

Table B.1 Water Level and Calculated Discharge at Malano AWLR (5/5)

| (s, | Dec | о С | | | | | | | | | | | | | | | | | | | | | ••••• | | | | | •••• | | | | | ·•••• | |
|---------|------|-------------|---------|-----------|---------|---------|---------|---------|---------|---------|---|---------|---------|---------|-----------|----------|----------|----------|----------|----------|---------------------------------------|---------|--------|--------|--------|---------|----------|---------|------------|---------|---------|---------|----------------|---------|
| (m.3/s) | L | (îiii) H | _ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | Ш |
| | Nov | H(m) Q | | | | | | | •••••• | | ••••• | •1•••• | | | ••••• | ••••• | ••••• | 180+40 | ••••• | 150 | | ***** | , | ***** | ***** | ***** | ,,,,,, | -100-1 | ••••• | ••••• | | ****** |)2** 10 | |
| | Oct | Н(ш) Q | | | •••• | | | | | | | ••••• | | | •••• | | ••••• | ••••• | ••••• | | | ***** | ••••• | | ••••• | | | | •••• | | | | | |
| | Sep | H(m) Q | | ••••• | ***** | | | | | | | | | | •••• | | ••••• | | | ••••• | ••••• | | ***** | | ••••• | ****** | | | | | | | | |
| | Aug | ٥ | 383.37 | 416.52 | 388.70 | 375.91 | 413.30 | 369.53 | 348.31 | 385.50 | 413.30 | 407.94 | 365.28 | 252.88 | 173.55 | 132.86 | | | | | | | | | | | | | | | | | | 344.78 |
| | ٧ | H (m) | 4.45 | 4.76 | 4.50 | 4.38 | 4.73 | 4.32 | 4.12 | 4.47 | 4.73 | 4.68 | 4.28 | 3.21 | 2.44 | 2.04 | | ••••• | | | ••••• | | | | ***** | | | | ••••• | | | | ••••• | |
| | _ | 0 | 333.51 | 218.72 | 205.33 | 189.93 | 389.77 | 269.52 | 147.06 | 168.45 | 186.85 | 389.77 | 291.46 | 228.01 | 218.72 | 181.73 | 168.45 | 153.16 | 150.11 | 152.14 | 339.84 | 378.04 | 333.51 | 206.36 | 273.69 | 78.772 | 314.54 | 155.20 | 389.77 | 309.29 | 242.50 | 266.40 | 297.74 | 252.50 |
| , | Jul | H (m) | 3.98 | 2.88 | 2.75 | 2.60 | 4.51 | 3.37 | 2.18 | 2.39 | 2.57 | 4.51 | 3.58 | 2.97 | 2.88 | 2.52 | 2.39 | 2.24 | 2.21 | 2.23 | 4.04 | 4.40 | 3.98 | 2.76 | 3.41 | 3.45 2 | 3.80 | 2.26 | 4.51 | 3.75 | 3.11 | 3.34 2 | 3.64 2 | 7 |
| ; | _ | 0_1 | 34.26 | 33.22 | 32.71 | 31.69 | 30.68 | 30.68 | 30.68 | 103.11 | 183.78 | 146.05 | | 156.21 | 248.72 | 379.10 | 368.46 | 218.72 | 211.51 | 186.85 | 172.53 | 157.23 | 165.38 | 220.78 | 248.72 | 301.94 | 330.34 | 261.19 | 284.14 | 257.03 | 221.82 | 231.11 | _ | 179.44 |
| | Jun | Н (ш) | 0.67 | 0.65 | 0.64 | 0.62 | 0.60 | 0.60 | 0.60 | 1.73 | 2.54 | 2.17 | 1.75 | 2.27 | 3.17 2 | 4.41 | 4.31 | 2.88 | 2.81 | 2.57 | 2.43 I. | 2.28 | 2.36 | 2.90 | 3.17 | 3.68 | 3.95 | 3.29 2 | 3.51 | 3.25 22 | 2.91 2. | 3.00 | | |
| | - | Q H | 81.53 0 | 73.88 0 | 67.85 0 | 66.53 0 | 65.23 0 | 65.23 0 | 63.29 0 | 62.65 | 58.86 2 | 70.50 2 | 104.67 | 90.94 2 | 175.60 3 | 212.54 4 | 133.87 4 | 237.32 2 | 141.98 2 | 103.89 2 | 102.33 2 | 99.24 2 | 96.19 | 94.68 | 90.20 | 82.95 3 | 71.85 3 | 58.23 3 | 49.76 | 44.57 3 | 40.67 | 39.03 | | 91.53 |
| | May | | | ••••• | .24 67 | 22 66 | .20 | 20 65 | .17 | 1.16 62 | .10 58 | 1.28 | 1.75 10 | 1.57 | 2.46 17 | ••••• | ***** | | | 1.74 10 | 1.72 | 89.1 | 26. | 1.62 | .56 90 | 1.46 | 1.30 7.1 | 1.09 | ••••• | ••••• | | | | 6 |
| | - | H (m) | 38 1.44 | 76 1.33 | _ | _ | _ | _ | _ | | | | | | | 35 2.82 | 2.05 | 3.06 | 28 2.13 | _ | _ | _ | _ | _ | _ | | | | 91 0.95 | 24 0.86 | 93 0.79 | 4 0.76 | • | 2 |
| | Apr | 0 | 5 56.38 | 5 49.76 | 5 44.57 | 8 40.12 | 7 45.13 | 3 67.19 | 0 65.23 | 7 63.29 | 3 60.74 | 3 60.74 | 2 60.11 | 7 56.99 | 9 52.13 | 5 50.35 | 2 48.01 | 0 46.85 | 9 46.28 | 3 45.70 | 8 45.70 | 5 44.00 | 43.44 | 41.2 | 41.2 | 40.67 | 5 82.95 | 183.78 | 3 136.91 | 3 99.24 | 1 93.93 | 7 90.94 | | 63.45 |
| | _ | H(m) | 1.06 | 26:0 | 0.86 | 0.78 | 0.87 | 1.23 | 1.20 | 1.17 | ======================================= | 2 1.13 | 0 1.12 | 1.07 | 6.0 | 96:0 | 0.92 | 0.00 | 0.89 | 0.88 | 88.0 | 0.85 | 0.84 | 08.0 | 0.80 | 0.79 | 1.46 | 254 | 3 2.08 | 1.68 | 1.61 | 1.57 | | |
| | Mar | ٥ | 43.44 | 43.44 | 39.03 | 35.30 | 31.69 | 30.68 | 31.19 | 31.69 | 90.94 | 234.22 | 143.00 | 92.43 | 74.56 | 60.74 | 52.13 | 45.70 | 41.21 | 40.67 | 45.70 | 44.57 | 42.88 | 43.44 | 49.76 | 71.17 | 68.51 | 69.17 | 107.83 | 100.01 | 87.27 | 73.20 | 63.93 | 65.47 |
| : | | Н(ш) | 0.84 | 0.84 | 0.76 | 0.69 | 0.62 | 0.60 | 0.61 | 0.62 | 1.57 | 3.03 | 2.14 | 1.59 | 1.34 | 1.13 | 0.99 | 0.88 | 080 | 0.79 | 0.88 | 0.86 | 0.83 | 9.8 | 0.95 | 1.29 | 1.25 | 1.26 | 1.79 | 1.69 | 1.52 | 1.32 | 1.18 | |
| | Feb | O | | | | ••. 4•• | | | | | | ••••• | | | | ••••• | | | | ••••• | · · · · · · · · · · · · · · · · · · · | | | •••• | | | | | | 34.78 | | | | 34.78 |
| | | H(m) | • | • | • | • | | • | • | | • | • | • | | | • | | | | • | • | | • | • | • | • | | • | • | 0.68 | | | | |
| 1995 | Jan | Q | 31.69 | 30.18 | 30.18 | 29.68 | 30.18 | 30.18 | 36.35 | 41.21 | 42.32 | 49.76 | 103.11 | 107.04 | 102.33 | 87.27 | 82.95 | 78.71 | 78.71 | 78.71 | 78.71 | 79.41 | 79.41 | 71.85 | 72.52 | 212.54 | 224.91 | 115.67 | 100.56 | 8.54 | | | | 18.61 |
| Year: | | H(m) | 0.62 | 0.59 | 0.59 | 0.58 | 0.59 | 0.59 | 0.71 | 08.0 | 0.82 | 0.95 | 1.73 | 1.78 | 1.72 | 1.52 | 1.46 | 1.40 | 1.40 | 1.40 | 1.40 | 1.41 | 1.41 | 1.30 | 131 | 2.82 | 2.94 | 1.87 | 1.72 | 39. | • | • | • | |
| | Date | | - | 2 | 3 | 4 | S | 9 | 7 | 00 | 6 | 01 | = | 12 | 13 | 14 | 15 | 16 | 11 | 81 | 61 | 8 | 21 | 22 | 23 | 24 | 25 | 92 | 23 | 78 | 29 | œ | 31 | Average |

 (-) No data
 Discharge was Notes:

Discharge was calculated by using the rating curve obtained in this F/S H \geq 1.80 m : Q = 1.1013 H²2 + 96.797 H \sim 69.19 H \leq 1.80 m : Q = 12.294 H²4 + 35.446 H + 4.99

APPENDIX C METEOROLOGICAL DATA

Table C.1 Meteorological Data at Sorong Jefman (1/2)

| YEAR | 1 2 3 4 5 | Atomospheric Temperature (°C) (max.) 30.8 31.5 32.0 31.0 31.8 | (min.) 24.4 23.1 24.7 23.7 23.6 | (Ave.) 27.7 27.9 28.4 27.3 27.6 | Sunshine (%) | Average Relative Humidity (%) 83 82 82 8 | Number of Rainy Days (day) 17 5 10 | Wind Direction | Wind Speed (knots) (max.) | (min.) |
|------|-----------|---|---------------------------------|---------------------------------|--------------|--|------------------------------------|----------------|---------------------------|--------|
| | 4 5 | 1.0 31.8 | 3.7 23.6 | 7.3 27.6 | • | 83 87 | 15 21 | • | . • | |
| 15 | 9 | 30.4 | 5 25.0 | 5 27.5 | • | 98 | 61 | • | • | • |
| 1983 | 7 | 30.5 | 24.9 | 26.8 | • | 83 | 25 | ٠ | • | |
| | ∞ | 30.2 | 24.8 | 27.6 | • | 87 | 77 | | | |
| | 6 | 30.9 | 24.5 | 27.0 | | 87 | 20 | | | |
| | 10 | 31.0 | 24.7 | 27.1 | • | \$2 | 81 | , | , | , |
| | = | 31.0 | 25.3 | 27.5 | 1 | 83 | 15 | | , | |
| - | 12 | 32.0 | 25.1 | 27.0 2 | | 2 | <u>81</u> | | • | • |
| | _ | 31.1 | 25.0 2 | 27.4 2 | 8 | | 19 | | | |
| | 2 3 | 30.1 30.6 | 25.0 25.1 | 27.0 27.3 | 59 51 | 83 8 | 19 24 | į | | • |
| | 4 | 6 31.1 | .1 25.5 | 3 27.7 | 1 65 | 82 83 | 4 22 | | • | |
| | 5 | 1 31.1 | 5 24.9 | Z.7.2 | 8 | | 23 | • | • | • |
| | 9 | 30.9 | 24.9 | 27.5 | 19 | | 22 | • | • | • |
| 1984 | 7 | 30.4 | 24.3 | 26.5 | 48 | 8 | 25 | • | •. | • |
| | ∞ | 29.9 | 24.5 | 26.7 | 55 | 87 | 13 | • | ı | • |
| | 6 | 30.6 | 24.5 | 26.8 | 19 | 82 | 23 | • | • | • |
| | 9 | 30.2 | 23.7 | 27.5 | 62 | 82 | 으 | | | |
| | = | 31.6 | 26.4 | 28.0 | 21 | ™ | 6 | | | |

| YEAR | | | | | | | 198 | 85 | | | | | _ | | | | | | 1986 | | | | | |
|---|----------------|------|---------------------------------|------|-------|------|------|------|------|------|------|------|------|------|------|--------|--------|--------|---------|---------|-----------|--------|--------|------|
| | | | 2 | 3 | 2 3 4 | 5 | 9 | 7 | 8 | 6 | 01 | = | 12 | 1 | 2 | 3 | 4 | 5 | . 9 | 7 | 6 8 | 10 | | 12 |
| Atomospheric Temperature (°C) (max.) 30.7 30.6 31.5 31.5 30.0 | (T) (max.) | 30.7 | 30.6 | 31.5 | 31.5 | 30.0 | 30.7 | 29.4 | 30.6 | 31.4 | 31.6 | 31.3 | 30.6 | 30.6 | 30.6 | 30.6 | 11.1 | 32.4 3 | 1.5 3 | 31.7 3 | 32.8 32.5 | 5 32.0 | 0 31.5 | 31.3 |
| | (min.) | 26.4 | (min.) 26.4 25.7 25.6 24.7 24.3 | 25.6 | 24.7 | 24.3 | 25.1 | 23.7 | 24.5 | 24.5 | 24.2 | 25.3 | 25.3 | 25.7 | 25.2 | 25.2 | 25.5 2 | 25.4 2 | 25.1 25 | 25.1 23 | 25.4 25.1 | 1 25.3 | 3 25.1 | 25.6 |
| | (Ave.) | 27.5 | (Avc.) 27.5 27.5 28.2 27.8 27.4 | 28.2 | 27.8 | 27.4 | 27.0 | 26.5 | 26.5 | 26.6 | 27.9 | 27.2 | 28.1 | 28.2 | 27.9 | . 6.72 | 28.3 2 | 28.9 2 | 28.3 28 | 28.4 29 | 29.1 28.8 | 8 28.6 | 6 28.3 | |
| Sunshine | (%) | 4 | 46 | 62 | 28 | % | 51 | 4 | 84 | 23 | 8 | 8 | 48 | 55 | 19 | 49 | 8 | 92 | 8 | 63 | 75 80 | 19 (| 8 | 75 |
| Average Relative Humidity (%) | (<u>%</u>) | 8 | 8 | 75 | 78 | 82 | 98 | 62 | 84 | 83 | 25 | 78 | 8 | 81 | 75 | 8 | . 87 | 11 | 7 | 8 | 77 08 | 8 | 8 | 76 |
| Number of Rainy Days (| (day) | 16 | 4 | 6 | 13 | 22 | 81 | 22 | 71 | 22 | 91 | 18 | 22 | 13 | 13 | 25 | 13 | 17 | 13 | 4 | 6 | 22 | 21 | 4 |
| Wind Direction | | • | • | • | • | • | • | • | • | • | | • | • | , | • | | | | • | | , | • | • | • |
| Wind Speed (k | (knots) (max.) | ' | • | | ٠ | • | | | | | | • | , | , | , | | | | | | | • | • | ٠ |
| | (min.) | | ' | • | , | | , | • | • | • | | 4 | , | , | , | , | | , | | | ' | ' | • | ٠ |

| YEAR | | L | | | | | | 1987 | _ | | | | | - | | | | | | 1988 | | | | | |
|---|------------------|----------|--------|--------|-------|---------------------------------|-----|--------|--------|--------|--------|--------|---------|---------------|---------|-----------|---------|---------|---------|-----------|---------|-----------|-----------|-----------|--------|
| | | Ц | | | 3 | 2 3 4 5 | 5 | 9 | 7 | 8 | 6 | 10 | 11 1 | 2 | | 2 3 | 3 4 | | 2 | 9 | | 8 | 1 6 | 1 01 | Τ |
| Atomospheric Temperature (C) (max.) 30.4 31.0 30.3 31.5 31.5 | (C) (max | 30 | 14 3 | 1.0 | 0.3 | . S. | 1.5 | 0.4 | 30.1 | 30.6 | 1.1 | 6.1 | 30.0 | .4 | 1.2 3 | 1.1 31 | 31.0 32 | 32.2 32 | 32.1 31 | 31.2 30 | 30.2 30 | 30.9 31.1 | | 31.2 31.6 | 6 31 |
| | (mi | 24 | 1.5 2: | 5.8 2. | 5.2 2 | (min.) 24.5 25.8 25.2 25.4 25.4 | | 25.5 2 | 25.0 2 | 24.7 2 | 25.3 2 | 25.4 2 | 25.1 25 | 25.7 2 | 25.2 2: | 25.3 26.0 | .0 25.7 | | 25.7 24 | 24.9 24.6 | | 24.9 24 | 24.9 25.1 | .1 25.4 | 4 25.0 |
| | Ϋ́ | 27 | 7.4 28 | 3.1 2 | 7.7 2 | (Avc.) 27.4 28.1 27.7 28.4 28.4 | | 27.9 2 | 27.9 2 | 28.1 2 | 28.4 2 | 28.9 2 | 29.4 29 | 29.3 2 | 29.2 | 28.6 28.5 | .5 28.8 | | 28.3 28 | 28.3 27 | 27.8 27 | 27.3 28.3 | .3 28.6 | .6 29.1 | |
| Sunshine | (%) | | 9 | 62 7 | . 11 | .72 | 74 | 71 | 11 | 74 | 53 | 11 | 9 08 | - 19 | \$ \$9 | 88 62 | 2 67 | | 9 69 | 69 65 | | 76 72 | 2 58 | 8 | 62 |
| Average Relative Humidity (%) | (<u>%</u>) | <u>~</u> | 82 7 | 79 7 | . 82 | 18 | 81 | 82 | 80 | 83 | . 08 | 62 | 82 7 | <u>.</u> ج | 3 11 | 31 8 | 1 7 | 78 8 | 81 8 | 82 82 | | 78 82 | 2 82 | 2 79 | |
| Number of Rainy Days | (day) | _ | 4 | 9 | 91 | 14 | 17 | 9 | S | 12 | 9 | 13 | 14 (| ١,٠ | 12 | 12 1 | 4 | 14 | 19 1 | 15 2 | 22 2 | 24 2 | 20 17 | 7 18 | |
| Wind Direction | | | | , | | ı | | ı | | • | | | | | S | z | z | S-N | S | SE-S SI | SE S- | S-SE N | N-S S-N | z | S-N |
| Wind Speed | (knots) (max.) | · 3 | | | | , | , | , | , | | | | | | 81 | 15 1 | 5 1 | 16 1 | 12 2 | | 5 1 | 12 1 | _ | 7 | 12 |
| | (min.) | .) | | | | ı | , | | , | | , | | 1 | | ব | 5 | | , 9 | _ | 9 | , | 4 | _ | 'n | 7 |

Table C.1 Meteorological Data at Sorong Jefman (2/2)

| YEAR | | Г | | | | | | } | 6861 | | | | | - | | | | | | 86 | | | | | |
|---|----------------|-----------------------|------|------|-----------|------|-------------|--------|------|------|------|------|--------|------|------|------|--------|--------|-----------|--------|--------|--------|--------|---------|------------|
| | | | - | 2 | 2 3 4 5 | 4 | 5 | 9 | 7 | 8 | 6 | 10 | 11 | 12 | 1 | 2 | 3 | 4 | 5 | 9 | 7 | 8 | 6 | 10 | 11 12 |
| Atomospheric Temperature (°C) (max.) 30.7 29.6 30.5 31.3 31.3 | (C) | (max.) | 30.7 | 29.6 | 30.5 | 31.3 | 31.3 | 30.3 | 31.6 | 30.5 | 31.9 | 31.4 | 31.2 | 31.4 | 30.8 | 31.8 | 31.9 | 31.4 | 11.5 3 | 30.6 | 30.7 3 | 10.8 | 32.1 3 | 32.3 3. | 31.6 31.7 |
| | - | (min.) 25.5 25.0 24.9 | 25.5 | 25.0 | 24.9 | 25.2 | 25.7 | 24.3 | 24.6 | 24.9 | 25.0 | 25.0 | 25.6 | 25.4 | 25.4 | 25.7 | 25.8 2 | 25.8 2 | 25.8 2 | 25.4 2 | 25.0 2 | 25.0 2 | 25.0 2 | 24.9 2: | 25.5 25.9 |
| | - | (Ave.) 28.6 28.2 27.7 | 28.6 | 28.2 | 27.7 | 28.7 | 28.5 | 28.5 | 28.4 | 26.5 | 28.6 | 28.2 | 28.7 | 28.1 | 27.9 | 28.5 | 28.6 | 28.6 2 | 28.7 2 | 28.1 2 | 28.1 2 | 27.4 2 | 28.0 2 | 29.0 2 | 28.3 29.3 |
| Sunshine | (%) | • | | | | | , | | 20 | 2 | 22 | | | 1 | | | | | | | | | | , | |
| Average Relative Humidity (%) | (%) | | 83 | 8 | 8 | ≅ | 80 | 8 | 55 | 8 | ≅ | 82 | 8 8 | 82 | 82 | 11 | 81 | 82 | 22 | 83 | 85 | 8 | 83 | 80 | 7 79 |
| Number of Rainy Days | (day) | | 15 | 11 | 9I | 16 | = | 11 | 18 | 4 | 23 | 16 | 18 | 12 | 17 | 13 | 11 | 15 | 14 | 17 | 18 | 14 | 14 | 15 | _ |
| Wind Direction | | | ≱ | ≱ | ≱ | ΝS | ΝS | SW | S-SE | S-SE | S-SE | S-SE | S-SE | N-S | N-N | z | z | N-S | N S-N | N-SE | S | S | E-S | S | Γ Λ |
| Wind Speed (| (knots) (max.) | (max.) | 7 | 7 | 00 | 7 | > | 7 | 7 | 2 | 7 | 7 | ø | 2 | 12 | 15 | 5 | 15 | <u>81</u> | 8 | 81 | ឧ | 22 | 23 | 7 20 |
| | , | (min.) 4 | 4 | 3 | S | 3 | 4 | 3 | 4 | 5 | 3 | 8 | 4 | 3 | ∞ | 6 | 7 | 7 | ~ | = | 11 | 12 | 01 | 01 | 90 |
| | | | | | | | | | | | | | | | | ı | | | | ı | | | | | |

| YEAR | | | | | | | | 1991 | <u> </u> | | | | | H | | | | | | 1992 | | | | | |
|---|---------|-------------------|------|------|----------|---------------------------------|------|------|----------|------|------|----------|--------|------|---------|---------|---------|----------|---------|-----------|--------|--------|--------|------|------|
| | | | - | 2 | 3 | 2 3 4 5 | 5 | 9 | 7 | 8 | 6 | 01 | | 12 | | 2 | 3 | 4 5 | | 6 7 | 8 | | 10 | Ξ | 12 |
| Atomospheric Temperature (C) (max.) 30.8 31.1 30.8 31.0 31.8 | (ဌ) | (max.) | 30.8 | 31.1 | 30.8 | 31.0 | 31.8 | 31.9 | 31.0 | 30.9 | 31.0 | 31.4 | 33.0 3 | 31.8 | l`' | 31.7 31 | 31.1 | 1.8 32.1 | 1 31 | .2 30.3 | 3 31.5 | 5 32.0 | 31.7 | 31.7 | 31.0 |
| | | (min.) | 25.4 | 25.7 | 25.3 | (min.) 25.4 25.7 25.3 25.4 24.9 | 24.9 | 25.1 | 24.9 | | 23.8 | 24.5 | | 24.5 | 25.0 2: | 25.5 25 | | 25.7 25 | | 25.2 24.7 | 7 24.9 | 9 24.0 | 24.8 | 25.1 | 25.3 |
| | | (Ave.) | 28.1 | 28.5 | 28.1 | (Avc.) 28.1 28.5 28.1 28.2 28.4 | 28.4 | 28.5 | 27.9 | 28.0 | 27.4 | 28.0 | 29.0 | 28.1 | | 28.4 28 | 28.3 28 | 28.1 28 | 28.5 28 | 28.2 28.0 | 0 28.4 | | | | 27.6 |
| Sunshine | (%) | | • | , | • | . • | • | ı | | | | | | | | | | | | - 53 | | | | 65 | 2 |
| Average Relative Humidity (%) | (%) | | 62 | 82 | œ | 8 | 81 | 83 | 82 | 62 | 8 | 8 | 83 | 82 | 208 | 8 62 | 8 18 | 80 7 | 79 8 | 82 82 | 8 | 8 | 78 | 81 | 82 |
| Number of Rainy Days | (day) | | 11 | ∞ | 11 | 15 | 21 | 4 | 14 | 6 | 7 | 0 | | - | | 6 1 | 11 1 | | | 14 16 | 3 11 | Ξ | | 13 | Ξ |
| Wind Direction | | | z | z | z | S-SE S-SE | S-SE | S-SE | S | | S-SE | N-S | SE-N N | ≯ż | z | N-NE N- | ш | N-NW S. | S-SE S- | S-SE S-SE | E S-SE | E S-SE | S S-SE | S-W | z |
| Wind Speed | (knots) | (knots) (max.) 15 | 15 | 81 | <u>∞</u> | 10 15 | 15 | 15 | 24 | 23 | 8 | 15 | 12 | 01 | 25 2 | | | | | | | | | | 12 |
| | | (min.) | œ | 2 | 5 | 3 | 4 | 6 | 7 | 9 | 12 | œ | 9 | 9 | 6 | 14 1 | 01 | ° | 1 | 12 11 | 7 | 6 | ∞ | 7 | 7 |

| YEAR | | | | | | | | 199 | [~ | | | | | | | | | | 19 | 94 | | | | | Γ |
|---------------------------------|-------------------|--------------|-------|-------|------|--------|--------|--------|--------|--------|--------|--------|-------------------------------|------------|------------------|--------|----------|------|------|---------------------|------|-------|----------|---|----|
| | | Н | _ | 2 3 4 | 3 | | 5 | 9 | 7 | 8 | 6 | 10 | 10 11 12 | <u> </u> | 2 | 2 3 4 | 4 | 5 6 | 9 | 7 | ∞ | 6 | 10 11 12 | = | 12 |
| Atomospheric Temperature | (C) | ax.) 3 | 0.9 | | 11.4 | 11.3 3 | ı | 32.4 | 31.0 | 31.9 | 31.0 3 | 2.3 3 | 32.3 30.4 30.9 31.4 31.5 30.7 | 9 31 | .4 31.5 | 30.7 | 31.3 | 30.6 | 29.4 | | 29.1 | 31.1 | | | |
| (min.) 25.4 25.3 25.3 25.1 24.3 | Ē | in.) | 5.4 2 | 5.3 | 5.3 | 5.1 2 | | 24.7 2 | 24.8 2 | 24.6 2 | 24.6 2 | 25.3 2 | 24.6 25.1 | 1 25.9 | .9 25.6 2 | 5 25.3 | 25.4 | 25.6 | 24.3 | 24.9 | 24.4 | 24.7 | | | |
| | Ś | (Avc.) | | | | | | | | | | | | - 3.7 | | • | • | • | | • | | | | | |
| Sunshine | (%) | ~ | 8 | 8 | 71 | 58 | 75 | 78 | 99 | 88 | 49 | 89 | 56 67 | 2 | 0 72 | 79 | 8 | 22 | 9 | \$ | • | | | | |
| Average Relative Humidity (%) | (%) | - | . 8/ | 78 | 82 | 82 | 22 | 82 | 81 | 8 | | | 78 76 | 8 | 1 79 | 83 | % | 98 | 98 | 82 | 82 | 8 | | | |
| Number of Rainy Days | (day) | | | | , | , | | , | | | | | | • | | • | • | | • | | • | | | | |
| Wind Direction | | | z | z | z | z | N-SE S | S-SE | S | S-SE S | S-SW N | N-S-N | N-S N-S | | S-N WS-MWN-N S-N | V M-SV | S-N / | S-SW | S-SW | WS-S WS-S WS-S WS-S | S-SW | S-SW | | | |
| Wind Speed | (knots) (max.) 15 | - (`x | 15 | 15 | 17 | = | 11 | 81 | 15 | | 91 | 15 | 8 15 | | 0 18 | 15 | 15 15 | 25 | 23 | 22 | 22 | 25 | | | |
| | (m) | (min.) 4 | 4 | 2 | 5 | 0 | 5 | 0 | 4 | 3 | 0 | S | 5 5 | ~ 1 | S | ۲, | m | " | r. | oc | ۲, | 2 | | | |

Table C.2 Monthly Average of Meteorological Data at Sorong Jefman

| | | | | | | | _ | _ | |
|---|------|------------------|------------------|-------------------------|------------------|------------------|--------------------------|-----------------|-----------------|
| | Dec. | 32.0 | 24.5 | 28.2 | 61.6 | 80.2 | 14.0 | 20.0 | 3.0 |
| | Nov. | 33.0 | 24.6 | 28.3 | 61.6 | 80.2 | 13.8 | 17.0 | 4.0 |
| | Oct. | 32.3 | 23.7 | 28.2 | 66.7 | 79.6 | 14.7 | 20.0 | 3.0 |
| | Sep. | 32.5 | 23.8 | 27.8 | 62.6 | 81.5 | 15.0 | 30.0 | 2.0 |
|) | Aug. | 32.8 | 24.4 | 27.6 | 9.99 | 81.8 | 14.9 | 25.0 | 3.0 |
| | Jul. | 31.7 | 23.7 | 27.6 | 58.4 | 82.7 | 17.9 | 25.0 | 4.0 |
| , | Jun. | 32.4 | 24.3 | 28.0 | 64.3 | 83.2 | 15.5 | 32.0 | 3.0 |
| | May | 32.4 | 23.6 | 28.2 | 69.1 | 82.2 | 18.6 | 25.0 | 3.0 |
| | Apr. | 32.2 | 23.7 | 28.2 | 63.7 | 80.8 | 14.9 | 18.0 | 3.0 |
| • | Мат. | 32.0 | 24.7 | 28.1 | 64.4 | 80.4 | 15.9 | 17.0 | 3.0 |
| | Feb. | 31.8 | 23.1 | 28.1 | 6.99 | 79.6 | 11.3 | 25.0 | 3.0 |
| | Jan. | 31.5 | 24.4 | 28.0 | 63.1 | 81.0 | 14.4 | 25.0 | 4.0 |
| | | (<u>2</u>) | (၃) | (Ç) | (%) | (%) | (day) | (knots) | (knots) |
| | Item | Max. Temperature | Min. Temperature | Average Temperature (C) | Average Sunshine | Average Humidity | Average Rainy Days (day) | Max. Wind Speed | Min. Wind Speed |

Source: BMG Meteorological Station Class II, Jefman, Sorong

Table C.3 Atmospheric Temperature at New Malano Station (1995)

| 1 | <u>-</u> | 8. | 0. | 7 | 0 | 7 | J. | S | 0 | 0 | 4. | 6, | | | | | | | | | | | | | | | | | | | | | | , | ٦ |
|----------------|---------------|------|------|------|------|------|------|------|------|--------|------|------|------|--------|------|------|------|------|--------|------|------|--------|------|------|--------|------|------|------|------|--------|------|----------|---|------|--------------|
| Unit: C | . Min. | | | | | | | | | 22.0 | | 22.3 | _ | | | | | | | | | | | | | | | | | | | <u> </u> | - | - | - |
| Unit September | Max. | 28.4 | 30.6 | 28.2 | 28.8 | 28.0 | 29.0 | 28.8 | 30.5 | 31.0 | 30.5 | 29.0 | 24.8 | | ļ | | | | | | | | | | | | | | | _ | | | Ŀ | 31.0 | - |
| | Mean | 24.2 | 25.6 | 25.0 | 25.0 | 24.1 | 25.0 | 24.9 | 25.8 | 25.5 | 26.0 | 25.3 | 23.7 | | | | | | | | | | | | | | | | | | | | 25.1 | • | - |
| | Min. | 23.0 | 22.9 | 22.9 | 22.9 | 23.6 | 23.1 | 22.1 | 23.2 | 23.0 | 22.5 | 23.0 | 23.0 | 22.5 | 22.2 | 22.1 | 22.9 | 23.0 | 23.0 | 23.2 | 24.0 | 24.0 | 23.0 | 23.1 | 23.1 | 23.0 | 22.2 | 22.1 | 23.0 | 23.0 | 22.6 | 24.0 | ' | • | 22.1 |
| August | Max. | 30.0 | 28.2 | 30.0 | 30.0 | 30.0 | 31.2 | 31.2 | 30.0 | 30.0 | 31.0 | 30.8 | 29.0 | 29.0 | 27.0 | 29.3 | 31.0 | 29.5 | 30.5 | 30.0 | 29.7 | 29.0 | 29.0 | 29.0 | 29.0 | 30.0 | 28.0 | 30.0 | 31.0 | 30.5 | 30.2 | 30.3 | , | 31.2 | , |
| | Mean | 25.2 | 24.2 | 25.0 | 25.7 | 25.6 | 25.9 | 26.0 | 26.0 | 25.4 | 25.4 | 25.9 | 25.4 | 25.2 | 24.6 | 25.7 | 26.0 | 25.4 | 25.5 | 25.6 | 25.8 | 25.4 | 25.4 | 25.2 | 25.1 | 25.5 | 24.1 | 25.5 | 26.2 | 26.0 | 26.1 | 26.3 | 25.4 | · | \cdot |
| | Min. | 23.0 | 23.0 | 23.0 | 23.5 | 23.0 | 23.0 | 22.5 | 23.2 | 23.0 | 22.0 | 23.0 | 23.1 | 22.2 | 22.2 | 22.0 | 22.0 | 22.0 | 23.0 | 22.9 | 22.8 | 22.4 | 22.0 | 22.8 | 22.0 | 22.9 | 22.9 | 22.3 | 24.1 | 22.8 | 23.0 | 23.0 | · | , | 22.0 |
| July | Max. | 31.0 | 31.5 | 30.6 | 30.0 | 31.0 | 31.2 | 29.0 | 30.5 | 29.0 | 29.0 | 27.4 | 30.0 | 28.0 | 29.0 | 27.0 | 30.8 | 31.2 | 30.0 | 30.0 | 30.2 | 30.0 | 30.8 | 29.0 | 30.0 | 29.7 | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 | 30.8 | ļ - | 31.5 | |
| | Mean | 25.7 | 25.8 | 25.8 | 25.9 | 25.4 | 25.6 | 25.5 | 25.6 | 25.2 | 24.9 | 25.0 | 25.4 | 25.0 | 24.8 | 243 | 25.5 | 25.3 | 25.6 | 25.8 | 25.6 | 25.3 | 25.3 | 24.4 | 25.4 | 25.5 | 25.1 | 25.2 | 26.5 | 25.8 | 26.0 | 25.4 | 25.4 | , | ╗ |
| - | Min. | 25.0 | 23.5 | 24.0 | 23.0 | 24.0 | 24.8 | 24.4 | 23.5 | 23.0 | 22.0 | 23.0 | 23.5 | 24.0 | 23.5 | 23.0 | 23.0 | 23.0 | 23.0 | 24.0 | 24.8 | 23.8 | 23.8 | 23.2 | 23.0 | 22.8 | 23.0 | 23.0 | 23.0 | 22.5 | 23.2 | | | , | 22.0 |
| June | Max. | 32.5 | 33.0 | 33.0 | 33.0 | 32.0 | 31.5 | 31.0 | 30.4 | 31.8 | 30.8 | 31.0 | 31.0 | 30.4 | 30.0 | 30.0 | 8.62 | 30.0 | 31.0 | 31.0 | 30.0 | 30.0 | 30.5 | 29.8 | 31.0 | 28.0 | 29.0 | 27.0 | 29.0 | 30.0 | 29.5 | | - | 33.0 | - |
| | Mean | 28.2 | 27.6 | 27.5 | 27.6 | 56.9 | 26.2 | 5.92 | 26.0 | 24.4 | 25.4 | 26.4 | 26.8 | 26.2 | 25.6 | 25.9 | 25.5 | 25.3 | 26.0 | 27.1 | 29.5 | 25.8 | 26.1 | 25.7 | 25.4 | 24.7 | 24.3 | 24.4 | 24.9 | 27.2 | 23.3 | | 26.0 | | |
| F | Min. | 23.6 | 23.2 | 24.0 | 24.0 | 23.5 | 24.5 | 24.0 | 25.0 | 24.8 | 24.8 | 23.9 | 24.2 | 25.0 | 24.0 | 23.0 | 24.0 | 24.0 | 23.2 | 23.5 | 22.2 | 22.8 | 22.5 | 22.6 | 23.0 | 24.0 | 24.0 | 23.0 | 23.0 | 23.5 | 23.5 | 23.0 | | | 22.2 |
| May | Max. | 31.5 | 30.5 | 31.0 | 30.0 | 29.0 | 29.0 | 31.0 | 32.0 | 32.5 | 31.0 | 32.5 | 31.5 | 31.0 | 30.8 | 32.0 | 32.0 | 31.0 | 32.6 | 31.0 | 59.6 | 31.2 | 31.2 | 32.2 | 32.5 | 32.1 | 59.9 | 32.0 | 33.2 | 32.8 | 31.0 | 32.8 | <u> </u> | 32.8 | - |
| | Mean | 26.2 | 26.3 | 56.9 | 21.1 | 797 | 26.0 | 26.1 | 28.1 | 27.2 | 27.3 | 27.6 | 56.9 | 27.2 | 26.3 | 26.8 | 272 | 26.7 | 27.0 | 25.8 | 25.6 | 26.3 | 26.3 | 26.8 | 27.1 | 27.3 | 292 | 56.9 | 27.5 | 27.1 | 27.0 | 26.9 | 26.57 | ٠. | 7 |
| | Min. | 24.0 | 24.0 | 24.0 | 24.1 | 24.0 | 23.5 | 24.0 | 23.7 | 24.0 | 23.0 | | | | 23.2 | 24.0 | 23.9 | 23.8 | 23.1 | 23.0 | 23.0 | | | | | | | | | 23.2 | | | - | • | 22.5 |
| April | - | ┝ | 32.2 | | 32.5 | 30.0 | | | | 31.0 | | 32.0 | | 31.5 | | | | | 31.8 | | | 32.0 | | | | | | | | 33.0 | | | | 33.8 | · · |
| | Mean | - | | | _ | | | | | 26.3 | | | | | | | | | 26.6 | | | | | | | | | | | 26.9 | | | 26.67 | • | |
| - | Min. | | | | | | | | | | 24.0 | | | | | | | | 23.6 | | | 23.8 | | | | | | | | | | 3.5 | - 3 | | 23.1 |
| March | <u> </u> | | | | | | | | | 27.0 2 | | | | | | _ | | | 31.0 2 | | | 33.0 2 | | | | | | | _ | | | | - | 33.0 | - |
| M | Mean M | | 26.9 | | | | | | | 25.1 2 | | | | 27.4 3 | | | | | 27.0 3 | | | | | _ | 26.8 3 | | | | | 27.0 3 | | | 16.91 | | _ |
| | +- | 26 | | | - | | | | | | | | | | | | | | | | | | | | | | | | | 77 | 38 | প্র | 56 | | _ |
| Į. | Min | | | | | | | | | 22.8 | | | 24.2 | | - | | | | 23.0 | | | 24.0 | | | | | | | | | | | <u> </u> | • | - |
| Feburuary | $\overline{}$ | L' | • | 26.5 | 27.5 | 31.0 | 32.0 | 32.0 | 31.0 | 31.0 | 30.5 | 31.9 | 32.0 | 32.4 | 31.5 | 32.5 | 32.0 | 31.5 | 31.5 | 32.0 | 32.0 | 32.0 | 30.0 | 32.0 | 32.0 | 31.0 | 30.2 | 31.0 | 30.8 | | | | | 32.4 | • |
| | Mean | | • | 26.1 | 25.6 | 26.3 | 26.6 | 26.3 | 26.3 | 25.6 | 25.9 | 27.3 | 27.6 | 27.0 | 27.1 | 27.3 | 26.7 | 26.7 | 26.7 | 27.4 | 27.7 | 27.2 | 26.1 | 26.3 | 25.8 | 26.4 | 26.8 | 26.7 | 26.7 | | | | 26.61 | • | ٠ |
| | Date | - | 71 | Ю | 4 | s | ٥ | 7 | ∞ | 6 | 01 | Ξ | 12 | 13 | 7 | 15 | 91 | 11 | 8 | 61 | ន | 21 | 22 | 23 | 24 | XI | 36 | 21 | 28 | 53 | ಜ | 31 | Avc. | Max. | Min. |

Table C.4 Humidity at New Malano Station (1995)

Unit: %

| | Min. | 7. | 11 | 75 | 76 | 75 | 73 | 75 | 8 | 65 | 19 | ফ | 16 | - | | | | | | | | | | | | | | | | | | | | • | ક |
|-----------|------|------|------|------|------|------|------|------|---------------|------|------|-------|------------|------|------|-------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|----------|----------|----------|
| September | Мах. | 26 | 76 | 8 | 8 | 8 | 8 | 8 | 76 | 76 | 76 | 8 | 76 | | | | | | | | | | | | | | | | | | | | • | 76 | ' |
| S | Mean | 93.0 | 88.5 | 92.0 | 808 | 8.16 | 89.5 | 6.68 | 85.1 | 89.2 | 88.7 | 87.5 | 95.4 | | | | | | | | | | | | | | | | | | | | 89.6 | , | ا |
| | Min. | 70 | 2 | 2 | \$ | 65 | 8 | 8 | 8 | 5 | છ | 8 | 75 | 19 | 74 | 20 | 65 | 0/ | 65 | 11 | 9 | 72 | 02 | 72 | 75 | 20 | 92 | 20 | 63 | 9 | 70 | 8 | Ŀ | • | အ |
| August | Max. | 97 | 76 | 88 | 76 | 8 | 6 | 76 | 1.6 | 8 | 16 | 76 | 8 | 26 | 16 | 8 | 26 | 8 | 8 | 6 | 26 | 8 | ጽ | 76 | 97 | 4 | 86 | 66 | 76 | 8 | 86 | 8 | Ŀ | 86 | |
| | Mean | 8.06 | 90.6 | 81.8 | 87.4 | 1.68 | 87.6 | 86.7 | 88.4 | 9.68 | 88.8 | 7.78 | 89.7 | 88.7 | 6'68 | 86.3 | 87.0 | 88.0 | 88.2 | 88.4 | 89.4 | 91.5 | 9.88 | 506 | 91.6 | 6'68 | 93.3 | 89.4 | 87.7 | 88.0 | 87.4 | 88.7 | 1.68 | , | |
| | Min. | 79 | 65 | 65 | 65 | 19 | হ | 9/ | 70 | 8 | 92 | 8 | 8 | 74 | 70 | 7.5 | 8 | 8 | 65 | 65 | 5 | 88 | 8 | 11 | 65 | 92 | 8 | | 62 | 65 | છ | ଓ | <u>'</u> | • | ક્ર |
| July | Мах. | 86 | 76 | 86 | 76 | 16 | 26 | 86 | 26 | 86 | 16 | 26 | 26 | 6 | 86 | 26 | 26 | 86 | 93 | 93 | 8 | 8 | 8 | 8 | 6 | 6 | 6 | 26 | 76 | 76 | 86 | 76 | ŀ | 86 | |
| | Mean | 88.3 | 87.9 | 6.68 | 88.4 | 89.0 | 88.9 | 616 | 8.68 | 91.8 | 90.1 | 91.2 | 88.9 | 87.2 | 90.4 | 9.7 | 86.5 | 87.1 | 88.8 | 88.5 | 89.4 | 90.4 | 88.2 | 91.0 | 89.4 | 89.1 | 90.1 | 88.5 | 988 | 9.98 | 87.1 | 88.0 | 89.1 | , | |
| | Min. | 8 | 26 | 8 | 2 | 2 | Z | 20 | 2 | જ | 20 | 20 | 2 | 2 | જ | જ | 73 | 2 | જ | 89 | ۶ | 2 | 2 | 2 | 19 | 28 | 2 | 8 | 75 | 19 | 2 | | Ŀ | • | 7 |
| Junc | Max. | - 26 | 86 | 6 | 26 | 26 | 16 | 76 | 76 | 76 | 88 | 86 | 8 6 | 86 | 76 | 97 | 86 | 86 | 88 | 76 | 76 | 76 | 16 | 76 | 16 | 16 | 86 | 26 | 6 | 16 | 26 | | Ŀ | 86 | |
| | Mean | 84.3 | 84.4 | 84.0 | 82.3 | 93.0 | 87.2 | 90.2 | 7.06 | 9.68 | 89.0 | 888 | 89.1 | 90.3 | 7.06 | 88.3 | 92:0 | 89.2 | 88.7 | 86.2 | 89.7 | 91.5 | 89.3 | 868 | 9.68 | 91.3 | 92.4 | 97.6 | 90.5 | 89.1 | 0.06 | | 89.1 | • | <u>.</u> |
| | Min. | જ | જ | 20 | 75 | 75 | 92 | 69 | 62 | 63 | 8 | 8 | 65 | 7 | B | 55 | \$3 | Z | 8 | 19 | 22 | Ŗ | 98 | 55 | 62 | ક | 73 | 46 | z | 62 | 62 | 55 | ľ | • | \$ |
| May | Max. | 8 | 86 | 76 | 6 | 26 | 76 | 6 | 8 | 76 | 76 | 8 | 86 | 6 | 6 | 6 | 86 | 26 | 76 | 76 | 76 | 86 | 76 | 76 | 86 | 86 | 6 | 26 | 86 | 86 | 76 | 83 | | 8 | <u>.</u> |
| | Mcan | 89.5 | 873 | 88.3 | 23.1 | 903 | 97.6 | 88.4 | 83.9 | 88.5 | 9.68 | 86.3 | 91.3 | 89.1 | 88.1 | 84.4 | 86.3 | 86.3 | 85.2 | 88.5 | 89.7 | 86.2 | 83.4 | 82.3 | 85.7 | 82.8 | 90.5 | 83.8 | 81.8 | 84.9 | 86.9 | 84.0 | 87.1 | • | |
| | Min. | 8 | 59 | 62 | 22 | 89 | ፠ | 8 | \$ | 62 | * | 28 | 77 | 55 | 53 | ሄ | 55 | 8 | 29 | 8 | 55 | 55 | 55 | 52 | 75 | 63 | 8 | 62 | 62 | 47 | 59 | | ŀ | r | 7 |
| April | Мах. | 86 | 86 | 83 | 8 | 6 | 16 | 86 | 86 | 76 | 6 | 8 | 86 | 86 | 86 | 86 | 86 | 86 | 8 | 86 | \$ | 86 | 86 | 86 | 86 | 26 | 86 | 26 | 76 | 16 | 6 | | <u>.</u> | 8 | ╝ |
| | Mcan | 84.8 | 88.5 | 84.3 | 83.6 | 50.5 | 83.8 | 84.2 | 8 10 10 | 89.4 | 8.08 | 88.4 | 0.06 | 83.5 | 82.1 | 83.1 | 82.7 | 88.3 | 89.2 | 86.3 | 82.8 | 88.3 | 81.3 | 83.5 | 91.4 | 50.5 | 91.4 | 8.98 | 87.2 | 82.2 | 84.0 | | 86.2 | , | |
| | Min. | 19 | 8 | 22 | 83 | 63 | 71 | 8 | 27 | 98 | 22 | 23 | 89 | 19 | 47 | 8 | 59 | 8 | 88 | છ | 8 | 8 | 83 | ß | 8 | 28 | Ş | 62 | 55 | 62 | 8 | 8 | Ŀ | <u>'</u> | \$ |
| March | Max. | 86 | 8 | 8 | 8 | 8 | 88 | 8 | 86 | 8 | 83 | 8 | 8 | 97 | 8 | 86 | 86 | 86 | 86 | 86 | 86 | 6 | 86 | 86 | 6 | 8 | 86 | 83 | 8 | 8 | 88 | 86 | · | 8 | |
| | Mean | 85.5 | 85.2 | 83.4 | 94.6 | 87.0 | 88.0 | 85.7 | 85.0 | 8.9 | 7.06 | 85.6 | 9.98 | 87.8 | 81.4 | 85.9 | 87.8 | 89.7 | 87.5 | 87.7 | 83.3 | 84.9 | 86.7 | 9.68 | 86.7 | 83.6 | 87.1 | 87.1 | 84.9 | 85.2 | 86.0 | 87.6 | 86.7 | • | |
| _ | Mia. | • | • | 8 | 78 | 8 | 55 | 62 | 69 | 8 | 22 | 3 | 88 | 19 | 8 | 53 | 8 | 89 | ક | 57 | 55 | 8 | 19 | 28 | 22 | જ | 63 | 65 | 8 | | | | Ŀ | • | 22 |
| Feburuary | Max. | | 1 | 8 | 86 | 8 | 8 | 901 | 8 | 8 | 80 | 8 | 8 | 8 | 8 | 8 | 86 | 8 | 8 | 88 | 88 | 86 | 8 | 8 | 8 | 8 | 86 | 8 | 8 | | | | ļ. | 8 | |
| | Mcan | ١. | ' | 92.2 | 92.0 | 8.88 | 87.0 | 8.06 | 91.2 | 91.6 | 91.5 | 8.4.8 | 80.7 | 83.8 | 83.5 | 83.6 | 87.2 | 87.7 | 86.3 | 82.8 | 82.2 | 87.2 | 8.06 | 86.1 | 85.9 | 85.8 | 86.3 | 87.5 | 87.0 | | | | 87.1 | 1 | ╝ |
| | Lage | - | 2 | ٣ | 4 | s | ٥ | 7 | ∞ | 6 | 9 | Ξ | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 8 | 21 | 21 | 23 | 24 | ಬ | 56 | 27 | 28 | 53 | 30 | 31 | Avc. | Max. | Min. |

Table C.5 Barometric Pressure at New Malano Station (1995)

| | Min. | 0.966 | 8.566 | 994.8 | 0.966 | 6.966 | 6.966 | 995.9 | 997.0 | 998.4 | 998.9 | 999.5 | 6766 | 0.866 | 998.2 | 997.0 | 7.766 | 997.2 | 998.0 | 998.0 | 997.0 | | | , | | | | | | | | | | , | 994.8 |
|-----------|------|--------|--------|-------|--------|--------|--------|--------|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|--------|--------|-------|--------|-------|
| August | Max. | 8.666 | 0.866 | 87.66 | 998.2 | 6.666 | 10000 | 0.666 | 1000.0 | 0.1001 | 5.1001 | 1002.0 | 1001.0 | 1000.0 | 1000.2 | 0.0001 | 1001.1 | 1000.0 | 1000.3 | 1000.0 | 1000.0 | | | | | | | | | | | | | 1002.0 | - |
| | Mcan | 6766 | 1.766 | 996.5 | 997.3 | 998.4 | 7.866 | 0.866 | 8.866 | 6.666 | 1000.6 | 1000.8 | 4.666 | 1.666 | 9.666 | 999.2 | 999.2 | 6366 | 999.3 | 5.666 | 7.866 | | | | | | - | | | | | | 8.866 | , | • |
| | Min. | 996.2 | 8.966 | 0.966 | 995.3 | 995.0 | 995.0 | 0.966 | 1.766 | 0.766 | 0.766 | 5.766 | 0.766 | 997.0 | 997.0 | 6766 | 1.766 | 6766 | 6766 | 997.2 | 997.5 | 5.766 | 8.766 | 0.666 | 9.96.6 | 5.966 | 0.766 | 997.0 | 6.966 | 87566 | 996.4 | 5.766 | | | 995.0 |
| July | Max. | 999.2 | 0.666 | 9.866 | 8.866 | 8.266 | 998.1 | 6.866 | 999.1 | 1000.2 | 1000.0 | 1000.0 | 1000.0 | 1000.0 | 1.666 | 1000.0 | 1000.0 | 1000.9 | 1000.8 | 1000.0 | 10000 | 1000.0 | 1001.0 | 1001.0 | 1000.5 | 6.666 | 5.666 | 1000.0 | 1000.5 | 999.3 | 0.666 | 1000.0 | | 1001.0 | • |
| | Mean | 998.2 | 998.3 | 97.6 | 997.4 | 7966 | 6966 | 997.1 | 988.6 | 999.1 | 6.866 | 8.866 | 938.6 | 998.7 | 998.3 | 998.5 | 998.5 | 1.666 | 998.5 | 0.666 | 999.2 | 0.666 | 4.666 | 1000.3 | 8.866 | 998.2 | 998.2 | 8.866 | 998.3 | 8.766 | 0.866 | 7.866 | 998.4 | , | , |
| | Min. | 0.966 | 0.966 | 6966 | 0.966 | 7.566 | 0.766 | 997.0 | 997.3 | 9.7.6 | 0.766 | 995.2 | 0.966 | 9.966 | 7.966 | 1.966 | 996.4 | 997.2 | 998.1 | 0.666 | 998.3 | 997.2 | 997.4 | 997.3 | 6766 | 998.1 | 998.0 | 0.866 | 0.866 | 0.766 | 0.766 | | | • | 995.2 |
| June | Мах. | 938.6 | 998.4 | 9.666 | 0.666 | 8.866 | 0.666 | 4.666 | 6.666 | 1000.0 | 8.666 | 1.666 | 0.666 | 1.666 | 7.666 | 1000.0 | 5.866 | 1.666 | 10001 | 1001.1 | 1001.2 | 1000.6 | 1000.8 | 1000.2 | 1000.0 | 1001.0 | 1000.0 | 6.666 | 1000.0 | 999.3 | 1000.0 | | , | 1001.2 | , |
| | Mean | 997.4 | 997.4 | 7.766 | 6766 | 5766 | 998.1 | 998.1 | 938.6 | 9.866 | 998.4 | 997.1 | 8.766 | 998.1 | 998.4 | 998.3 | 7.766 | 998.1 | 999.4 | 1000.0 | 10001 | 999.4 | 7.666 | 999.1 | 999.2 | 4.666 | 999.2 | 6.866 | 6.866 | 998.3 | 8.866 | | 998.5 | , | |
| | Min. | 5966.5 | 997.0 | 995.1 | 994.8 | 995.1 | 996.2 | 996.0 | 995.0 | 995.0 | 995.3 | 0.966 | 0.766 | 8.966 | 0.866 | 0.866 | 8.666 | 1000.0 | 999.1 | 1000.0 | 0.866 | 0.766 | 6766 | 998.1 | 0.766 | 997.0 | 998.5 | 0.866 | 996.5 | 0.966 | 996.3 | 1.966 | | ı | 924.8 |
| May | Max. | 1.666 | 1000.8 | 999.2 | 87.66 | 0.866 | 938.6 | 6.866 | 998.3 | 0.866 | 998.1 | 999.2 | 999.1 | 1000.4 | 4001.0 | 1001.1 | 1001.5 | 1002.9 | 1005.1 | 1001.0 | 1001.0 | 1000.0 | 1000.5 | 1001.7 | 0.1001 | 1000.5 | 1001.0 | 1001.2 | 10000 | 8.866 | 999.5 | 998.4 | , | 1002.9 | • |
| | Mcan | 1.766 | 938.6 | 9.766 | 996.4 | 9.966 | 997.3 | 997.3 | 1.766 | 996.9 | 6.966 | 9.766 | 998.3 | 5865 | 999.3 | 5.666 | 1000.7 | 1001.1 | 10001 | 1001.0 | 7:666 | 8.866 | 999.2 | 8.666 | 999.1 | 7.866 | 999.5 | 8.666 | 9.866 | 997.4 | 0.866 | 6966 | 5.866 | , | |
| | Min. | 8.966 | 7.766 | 997.0 | 996.3 | 997.4 | 996.0 | 995.9 | 6.966 | 998.0 | 6.866 | 8.866 | 998.2 | 998.0 | 997.9 | 997.2 | 997.2 | 996.1 | 6.966 | 997.1 | 995.7 | 995.7 | 995.3 | 0.966 | 0.966 | 997.0 | 8.766 | 8.766 | 8.966 | 8.966 | 996.2 | | | • | 995.3 |
| April | Мах. | 6'866 | 999.5 | 6.666 | 0'666 | 8.666 | 6.666 | 8.866 | 6.666 | 1001.2 | 1002.0 | 1002.3 | 1001.8 | 1001.2 | 1000.9 | 1000.2 | 1000.0 | 8.666 | 1000.0 | 1000.0 | 0.666 | 999.5 | 0.666 | 999.2 | 1000.0 | 1000.0 | 1000.7 | 1000.3 | 999.2 | 0.666 | 6.866 | | | 1002.3 | • |
| | Mean | 97.66 | 998.4 | 5.866 | 998.2 | 8.866 | 0.866 | 997.4 | 998.2 | 999.4 | 1000.6 | 1000.3 | 10001 | 7.666 | 7.666 | 999.2 | 8.866 | 998.4 | 998.5 | 998.5 | 7.766 | 9.766 | 997.5 | 9.266 | 998.2 | 7.866 | 6.866 | 989.1 | 998.3 | 997.9 | 997.5 | | 9.866 | ı | • |
| | Min. | 0'966 | 995.9 | 995.0 | 995.1 | 996.1 | 997.0 | 87.66 | 8.966 | 0.766 | 0.866 | 998.0 | 997.0 | 8.766 | 0.666 | 998.3 | 5.766 | 0.866 | 998.5 | 6.866 | 6766 | 8.766 | 6'966 | 6.966 | 6'966 | 966.1 | 995.0 | 995.0 | 995.2 | 995.2 | 995.2 | 0.966 | • | , | 995.0 |
| March | Мах. | 6.866 | 8.866 | 5.766 | 0.866 | 8.866 | 0.666 | 1000.0 | 9.666 | 1000.8 | 1001.0 | 1001.2 | 1000.0 | 1001.0 | 1001.3 | 1001.8 | 1001.0 | 1002.8 | 1002.1 | 1001.5 | 1002.6 | 100.9 | 6666 | 1000.0 | 1000.1 | 8.666 | 1000.0 | 8.866 | 8.866 | 8.866 | 998.4 | 8:866 | • | 1002.8 | |
| | Mean | 0.799 | 997.3 | 996.2 | 2967 | 997.4 | 0.866 | 998.7 | 998.3 | 6366 | 999.3 | 9.666 | 0.666 | 999.4 | 10001 | 1000.0 | 7:666 | 1000.1 | 1000.5 | 1000.4 | 1000.1 | 999.4 | 998.3 | 998.3 | 998.4 | 997.9 | 996.1 | 1.766 | 997.5 | 8.966 | 997.1 | 997.4 | 998.4 | • | - |
| _ | Min. | ٠ | , | 999.5 | 0.866 | 997.8 | 998.1 | 0.866 | 1.766 | 997.0 | 7.766 | 8.766 | 998.0 | 997.0 | 997.0 | 997.4 | 998.0 | 997.9 | 997.2 | 5.766 | 997.0 | 996.5 | 7.766 | 997.0 | 9.966 | 996.5 | 0.966 | 995.0 | 995.0 | | | | , | , | 995.0 |
| Feburnary | Max. | | , | 7.666 | 1001.0 | 1000.5 | 0.1001 | 1001.0 | 1000.0 | 1000.0 | 8.666 | 1000.0 | 1000.0 | 1000.0 | 1000.0 | 1000.0 | 1000.8 | 1001.0 | 1000.0 | 1000.0 | 1000.0 | 0.666 | 1001.0 | 1000.2 | 1000.0 | 0.666 | 0.666 | 0.666 | 998.0 | | | | | 0.1001 | _ |
| | Mcan | | 1 | 9.666 | 999.3 | 999.3 | 8.666 | 8'666 | 999.1 | 8.866 | 63866 | 8.866 | 0.666 | 998.3 | 998.4 | 6.866 | 999.4 | 999.5 | 999.4 | 0.666 | 938.6 | 0.866 | 0.666 | 999.1 | 9.866 | 998.1 | 9.266 | 997.0 | 0.766 | | | | 8.866 | • | - |
| ٤ | Jac | - | 7 | ო | 4 | S | 9 | 7 | ∞ | ٥ | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 11 | 81 | 19 | 20 | 21 | 22 | 23 | 24 | 23 | 56 | 23 | 82 | 82 | 8 | 31 | Avc. | Max. | Min. |

Table C.6 Wind Speed and Direction at New Malano Station (1995)

| _ | , 10 | | | | | | | _ | | | | | | | | | | | | | | | | | | | | | | | | | T. | |
|-------------|-----------|------|------|----------|-------------|----------|------|----------|-------|----------|----------|------|------|-------------|--------------|------------|------|----------|-------|------|------|------|----------|------|------|------|--------|------|------|------|--------------|--------------|----------|----------|
| | Direc. | • | • | , | , | • | • | , | • | ٠ | • | • | • | , | , | • | , | ' | , | • | ٠ | | ' | ' | • | • | • | • | • | | | _ | | _ |
| nst | Min. | 1.5 | 0.2 | 0.0 | 0.0 | 0.0 | 0.2 | 0.2 | 0.2 | 0.0 | 0.0 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.4 | 0.2 | 0.2 | 0.2 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.2 | 0.2 | 0.2 | | | , 6 |
| August | Max. | 2.0 | 1.5 | 0.1 | 2.0 | 0.1 | 1.8 | 1.5 | 1.8 | 8.0 | 2.0 | 2.8 | 8.1 | 2.5 | 8.1 | 1.8 | 8.1 | 2.2 | 2.0 | 0.1 | 0:1 | 0.5 | 9.1 | 8.1 | 0:1 | 8.0 | 2.4 | 1.8 | 2.2 | 8.0 | 0.5 | | ٠ | 2.8 |
| | Mean | 1.60 | 0.85 | 0.30 | 0.43 | 0.36 | 0.49 | 0.45 | 0.62 | 0.30 | 0.48 | 0.50 | 0.45 | 0.65 | 0.45 | 9.08 | 0.56 | 0.57 | 99.0 | 0.51 | 0.44 | 0.30 | 0.41 | 0.30 | 0.19 | 0.26 | 0.33 | 0.33 | 0.48 | 0.35 | 0.23 | | 0.48 | 1 |
| | Direc. | • | , | , | • | , | • | ı | | , | , | • | • | , | , | | 1 | , | , | , | | | , | | | , | | | | | | | | |
| | Min. | • | • | ı | | | | ı | | , | 1 | , | | , | , | , | • | , | , | • | , | , | , | , | • | · | 0:1 | 0.1 | 1.0 | 0:1 | 0.1 | 1.5 | · | , 4 |
| July | Max. | | , | , | , | • | | • | , | , | • | , | | • | • | • | • | • | | • | | • | , | • | , | , | 2.2 | 5.0 | 2.0 | 0.5 | 2.0 | 2.0 | | 2.0 |
| | Mcan | | | , | , | • | , | | • | , | | • | , | | | • | | | , | , | | · · | , | , | • | | 79. | 1.50 | 1.36 | 1.55 | 1.46 | .63 | 1.52 | |
| $\ \cdot\ $ | Direc. N | W | SE | S-SW | <u>п</u> -п | 見 | Ν̈́ | 35 | SE-E | ш | z | × × | s | 35 | ×Ν | • | , | , | , | _ | | , | , | , | • | , | _ , | | | | - | - | <u> </u> | |
| | Min. D | | - | | | 1.2 | | 6.1 | | | 3 | | £. | 5.1 | <u>X</u> 5:1 | 1.3 | , | , | , | _ | • | , | | , | | , | | • | | | _ | | - | . : |
| May | Max. N | | 2.5 | 2.0 | 2.0 | 1.9 | | 2.2 | | | 2.0 | 3.6 | 3.0 | _ | 2.3 | 4. | | | , | | _ | | , | , | | | | | | | | | | 3.6 |
| | Mcan M | | _ | 1.91 | | | | _ | | | 1.70 | 2.14 | 1.96 | 1.94 | 1.87 | 131 | _ | _ | _ | _ | _ | | _ | _ | _ | | _ | _ | _ | | _ | | 1.85 | <u>.</u> |
| Н | \Box | 2. | 2 | | | | | | | | | | | _ | | _ | (2) | ь | | ы | ≱ | * | <u>*</u> | _ | | | | | _ | _ | ш | | <u> </u> | |
| | ı. Direc. | - | | <u>'</u> | <u>'</u> | <u>'</u> | | <u>'</u> | | <u>.</u> | <u>'</u> | _ | | | | | | <u> </u> | | SE-E | | | | | | | | | | z | | | | |
| April | t. Min. | | 0.5 | 0.5 | 0.5 | 0.5 | 0.7 | 0.5 | | | 0.5 | 0:0 | 1.5 | 1.4 | 1.5 | 1.0 | 1.0 | 0: | _ | 1.2 | | 1.5 | _ | | 2.0 | _ | | | | 2.0 | | | Ŀ | ٠ ٥ |
| | n Max. | | | | | 2.0 | 2.0 | 1.0 | 1 2.0 | 0.5 | 0.5 | 2.0 | 2.5 | 2.1 | 2.2 | 7 2.1 | 2.3 | 1.9 | 1 2.2 | 2.1 | | | 2.0 | | | | | | | 2.5 | | | <u> </u> | 3.0 |
| | . Mean | 1.05 | 0.93 | 1.34 | 0.91 | 0.80 | 0.83 | 0.62 | 0.64 | 0.50 | 0.33 | 1.08 | 1.63 | 1.76 | 1.87 | 1.47 | 99: | 1.63 | 1.83 | 1.78 | 75. | 1.74 | 1.65 | 1.74 | 2.00 | 2.08 | 86.I | 2.05 | 2.15 | 2.10 | 2.02 | | 1.45 | 1 |
| | Direc. | • | ' | , | • | ' | ' | • | • | , | , | ' | ' | ' | , | , | ' | ٠ | ' | • | • | ' | ' | • | ' | ' | • | • | • | • | ' | ' | | |
| March | Min. | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.5 | 0.5 | 0.5 | 0.5 | 0.0 | 0.5 | 0.0 | 1.5 | 0:1 | 0.1 | 1.5 | 1.5 | 1.5 | 1:0 | 0.1 | 1.0 | 0.0 | 0.5 | 0.0 | 0.5 | 0.5 | 0.0 | 20 | 0.5 | 0.5 | ٠ | , 8 |
| Σ | Max. | 2.5 | 2.2 | 2.5 | 1.5 | 1.5 | 2.0 | 2.0 | 2.0 | 0.5 | 2.0 | 2.0 | 2.5 | 2.0 | 2.2 | 2.0 | 2.0 | 2.0 | 2.0 | 2.5 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.5 | 2.0 | 2.0 | 1.5 | 2: | 2.0 | 8:1 | ٠ | 2.5 |
| | Mean | 1.10 | 0.78 | 0.54 | 0.40 | 0.50 | 0.89 | 0.98 | 1.15 | 0.50 | 0.73 | 0.85 | 1.27 | 1.33 | 1.73 | <u>2</u> . | 1.68 | 1.65 | 1.67 | 1.72 | 1.43 | 1.39 | 1.05 | 0.85 | 0.97 | 1.01 | 0.77 | 0.79 | 0.59 | 0.65 | 1.10 | 0.79 | 1.05 | • |
| | Direc. | • | | • | | • | | | | | | | | | | | | • | • | • | • | | • | | | | | • | • | | | | | |
| uary | Min. | , | • | | , | | , | | | • | 0.5 | 0.5 | 0.5 | 0.3 | 2.0 | 0.2 | 0.1 | 0.0 | 0.5 | 0.5 | 0.5 | 0.5 | 0:0 | 0:0 | 0.3 | 0.3 | 0.5 | 0.0 | 0.5 | | | | | , 6 |
| Feburuary | Max. | | , | • | | | • | | , | | 2.0 | 2.2 | 2.0 | 2.0 | 0.3 | 2.0 | 0.5 | 2.0 | 2.2 | 2.0 | 2.2 | 2.0 | 0.5 | 1.5 | 1.0 | 2.0 | 1.5 | 2.2 | 2.5 | | | | | 2.5 |
| | Mean | | , | • | _ | _ | , | 1 | , | | 1.25 | 1.24 | 1.08 | 0.73 | 0.94 | 0.70 | 0.39 | 69.0 | 0.93 | 0.95 | 1.13 | 0.98 | 0.31 | 0.45 | 0.51 | 1.03 | 0.60 | 0.88 | 1.20 | · | | | 0.84 | , |
| Date | ш | | 7 | ٣ | 4 | S | 9 | 7 | œ | 6 | 2 | = | 12 | 13 | 14 | 15 | 91 | 17 | 18 | 61 | 8 | 21 | 77 | 23 | 77 | 22 | 56 | 23 | 28 | 61 | 30 | 31 | Avc. | Max. |

Table C.7 Pan Evapolation at New Malano Station (1995)

Unit: mm

| Data | Fohumen | Morah | A1 | Mari | Tum a | | August |
|------|-----------|-------|-------|----------|----------|------|----------|
| Date | Feburuary | March | April | May | June | July | August |
| 1 | _ | 2.9 | 2.5 | _ | _ | _ | _ |
| 2 | _ | 2.0 | - | 1.1 | _ | _ | _ |
| 3 | _ | 2.4 | 2.1 | - | _ | _ | _ |
| 4 | _ | 2.5 | - | - | 1.5 | _ | _ |
| 5 | _ | 1.7 | = | <u>-</u> | 2.8 | - | 2.1 |
| 6 | _ | 2.0 | 1.2 | - | - | - | _ |
| 7 | _ | 1.4 | - | - | 1.2 | - | - |
| 8 | _ | 1.4 | 1.3 | 1.6 | - | - | - |
| 9 | - 1 | - | - | _ | - | - | 2.7 |
| 10 | - | - | - | 1.0 | - | - | - |
| 11 | _ | 2.2 | 1.7 | 2.0 | | _ | _ |
| 12 | _ | 1.8 | 1.4 | _ | - | _ | |
| 13 | _ | 1.8 | 1.1 | 0.9 | _ | _ | 2.0 |
| 14 | 2.4 | 2.8 | 2.0 | - | _ | _ | - |
| 15 | 3.4 | 1.5 | 1.6 | 1.9 | <u>-</u> | _ | 1.0 |
| 16 | 1.2 | • | 2.4 | 1.7 | 1.2 | _ | - |
| 17 | 2.3 | _ | 1.2 | 2.3 | - | _ | _ |
| 18 | 2.7 | 1.4 | 3.1 | 1.7 | - | - | _ |
| 19 | 2.9 | 2.8 | 1.2 | _ | - | _ | 0.5 |
| 20 | 2.7 | - | 1.8 | - | 1.4 | - | 1.6 |
| | | | | 2.6 | | | |
| 21 | 1.5 | 1.7 | 1.6 | 0.6 | - | - | - |
| 22 | 0.3 | 0.7 | 1.9 | 1.4 | - | - | - |
| 23 | 1.7 | 1.2 | 1.7 | 2.2 | - | - | - |
| 24 | 2.6 | - | - | 1.2 | - | - | - |
| 25 | 0.7 | - | - | - | - | - | - |
| 26 | 1.3 | - | - | - | - | - | - |
| 27 | 3.3 | - | 1.0 | - | - | - | - ! |
| 28 | 1.4 | 1.3 | 1.8 | - | - | - | - |
| 29 | | 1.4 | 2.1 | _ | - | _ | - |
| 30 | | 1.9 | 1.6 | - | - | _ | - |
| 31 | | - | | | | | <u>-</u> |
| Ave. | 2.0 | + 1.3 | 1.2 | 0.6 | 0.3 | 0.0 | 0.3 |
| Max. | 3.4 | 2.9 | 3.1 | 2.3 | 2.8 | 0.0 | 2.7 |
| Min. | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

⁻ Rainy Day

Table C.8 Sunshine Radiation at New Malano Station (1995)

Unit: %

| | | Unit | : % |
|------|-----------|-------|--------------|
| Date | Feburuary | March | April |
| 1 | - | 83.3 | 58.3 |
| 2 | - | 70.8 | 62.5 |
| 3 | - | 75.0 | <i>5</i> 8.3 |
| 4 | 33.3 | 70.8 | 78.3 |
| 5 | - | 70.8 | 50.0 |
| 6 | - | 58.3 | 83.3 |
| 7 | 41.7 | 58.3 | 66.7 |
| 8 | 41.7 | 70.8 | 62.7 |
| 9 | 50.0 | - | 54.2 |
| 10 | 66.7 | 33.3 | 62.5 |
| 11 | 83.3 | 50.0 | |
| 12 | 83.3 | 16.7 | |
| 13 | 66.7 | 45.8 | |
| 14 | 66.7 | 50.0 | |
| 15 | 41.7 | 20.8 | |
| 16 | 66.7 | NA | Į |
| 17 | 50.5 | NA | |
| 18 | 70.8 | NA | |
| 19 | 79.2 | NA | |
| 20 | 79.2 | NA | |
| 21 | 58.3 | NA | |
| 22 | 58.3 | NA | |
| 23 | 66.7 | NA | |
| 24 | 58.3 | 62.5 | ļ |
| 25 | 66.7 | 79.2 | |
| 26 | 79.2 | 58.3 | |
| 27 | 70.8 | 70.8 | |
| 28 | 75.0 | 70.8 | |
| 29 | | 62.5 | |
| 30 | | 70.8 | |
| 31 | | 58.3 | |
| Ave. | 63.3 | 59.4 | 63.7 |
| Max. | 83.3 | 83.3 | 83.3 |
| Min. | 33.3 | 16.7 | 50.0 |

NA: Not available

APPENDIX D RESULTS OF DISCHARGE MEASUREMENT

Table D.1 Results of Discharge Measurement

| No | Date | Water Level in | Water Level Reading at | | Mean Velocity |
|-----|-----------|----------------|------------------------|------------------|---------------|
| | | Elevation (m) | Malano AWLR (m) | Discharge (m³/s) | (m/s) |
| 1 | 3-Feb-95 | 34.19 | | 25.53 | 0.508 |
| 2 | 11-Feb-95 | 34.37 | | 38.93 | 0.662 |
| 3 | 14-Feb-95 | 34.08 | | 21.11 | 0.470 |
| 4 | 15-Feb-95 | 34.04 | | 20.49 | 0.485 |
| 5 | 16-Feb-95 | 34.00 | | 18.09 | 0.438 |
| 6 | 17-Feb-95 | 33.98 | | 16.28 | 0.403 |
| 7 | 18-Feb-95 | 34.03 | | 20.08 | 0.470 |
| 8 | 21-Feb-95 | 34.00 | | 18.00 | 0.436 |
| 9 | 22-Feb-95 | 33.95 | | 15.56 | 0.401 |
| 10 | 23-Feb-95 | 34.09 | | 22.84 | 0.500 |
| 11 | 7-Mar-95 | 34.55 | 0.61 | 47.69 | 0.712 |
| 12 | 27-Mar-95 | 35.80 | 1.98 | 139.44 | 1.082 |
| 13 | 28-Mar-95 | 35.45 | 1.72 | 108.49 | 0.978 |
| 14 | 29-Mar-95 | 34.97 | 1.54 | 70.46 | 0.800 |
| 15 | 30-Mar-95 | 34.43 | 1.34 | 38.21 | 0.615 |
| 16 | 1-Apr-95 | 34.18 | 1.07 | 24.34 | 0.488 |
| 17 | 4-Apr-95 | 34.34 | 0.78 | 36.88 | 0.646 |
| 18 | 5-Apr-95 | 34.80 | 0.78 | 59.39 | 0.744 |
| 19 | 6-Apr-95 | 35.10 | 1.24 | 80.17 | 0.849 |
| 20_ | 7-Apr-95 | 35.00 | 1.20 . | 75.70 | 0.841 |
| 21_ | 10-Apr-95 | 35.08 | 1.13 | 80.41 | 0.825 |
| 22 | 11-Apr-95 | 34.85 | 1.12 | 65.32 | 0.794 |
| 23 | 12-Apr-95 | 34.68 | 1.08 | 52.62 | 0.710 |
| 24 | 17-Apr-95 | 34.65 | 0.88 | 52.07 | 0.713 |
| 25 | 18-Apr-95 | 34.67 | 0.88 | 52.14 | 0.709 |
| 26 | 20-Apr-95 | 34.50 | 0.85 | 43.21 | 0.660 |
| 27 | 7-Aug-95 | 37.74 | | 287.97 | 1.185 |
| 28 | 15-Aug-95 | 35.92 | | 165.18 | 1.145 |
| 29 | 16-Aug-95 | 36.36 | | 196.29 | 1.178 |
| 30 | 18-Aug-95 | 36.79 | | 236.25 | 1.229 |
| 31 | 19-Aug-95 | 37.88 | | 361.32 | 1.426 |
| 32 | 21-Aug-95 | 36.69 | | 228.24 | 1.217 |
| 33 | 22-Aug-95 | 38.19 | | 389.73 | 1.438 |
| 34 | 23-Aug-95 | 36.80 | | 241.20 | 1.251 |
| 35 | 24-Aug-95 | 36.49 | | 197.26 | 1.122 |
| 36 | 25-Aug-95 | 36.28 | | 184.66 | 1.141 |
| 37 | 26-Aug-95 | 37.23 | | 304.74 | 1.408 |
| 38 | 27-Aug-95 | 37.15 | | 274.57 | 1.299 |
| 39 | 29-Aug-95 | 38.28 | | 404.91 | 1.467 |
| 40 | 30-Aug-95 | 37.53 | | 321.67 | 1.381 |
| 41 | 31-Aug-95 | 36.63 | | 204.29 | 1.105 |
| 42 | 1-Sep-95 | 37.30 | | 303.47 | 1.378 |
| 43 | 2-Sep-95 | 37.10 | | 291.10 | 1.391 |
| 44 | 3-Sep-95 | 37.27 | | 309.72 | 1.417 |
| 45 | 4-Sep-95 | 36.87 | | 256.44 | 1.303 |

APPENDIX E

RESULTS OF SUSPENDED LOAD MEASUREMENT

Table E.1 Results of Suspended Load Measurement

| No. | Date | Time | Position | Measured S.S Contents (mg/l) | Ave. S.S Contents (mg/l) | Flow (m³/s) | Suspended Load Discharge (kg/s) |
|-----|-----------|-------|-------------------------|----------------------------------|-----------------------------|----------------|------------------------------------|
| 1. | 3-Feb-95 | 17:00 | left middle right | 168.0 15,756.0 107,580.0 | 41,168.0 | 25.53 | 1,051.0 |
| 2 | 11-Feb-95 | 12:00 | left middle right | 30,008.0 26,944.0 78,720.0 | 45,224.0 | 38.93 | 1,760.6 |
| 3 | 14-Feb-95 | 12:00 | left middle right | 6,220.0 13,244.0 23,040.0 | 14,168.0 | 21.11 | 299.1 |
| 4 | 15-Feb-95 | 9:30 | left middle right | 26,808.0 1,042.0 41,270.0 | 23,040.0 | 20.49 | 472.0 |
| 5 | 16-Feb-95 | 16:30 | left middle right | 27,620.0 2,986.0 9,060.0 | 13,222.0 | 18.09 | 239.2 |
| 6 | 17-Feb-95 | 17:40 | left middle right | 10,488.0 26,730.0 3,070.0 | 13,429.3 | 16.28 | 218.7 |
| 7 | 18-Feb-95 | 9:05 | left middle right | 138.0 94,220.0 22,408.0 | 38,922.0 | 20.08 | 781.7 |
| 8 | 21-Feb-95 | 16:58 | left middle right | 19,876.0 53,480.0 4,960.0 | 26,105.3 | 18.00 | 470.0 |
| 9 | 22-Feb-95 | 12:56 | left middle right | 9,284.0 41,790.0 7,590.0 | 19,554.7 | 15.56 | 304.3 |
| 10 | 23-Feb-95 | 10:55 | left middle right | 216.0 100,240.0 2,940.0 | 34,465.3 | 22.84 | 787.2 |
| 11 | 7-Mar-95 | 10:18 | left middle right | 152.0 41,630.0 11,560.0 | 17,780.7 | 47.69 | 847.9 |
| 12 | 27-Mar-95 | 13:05 | left middle right | 48.0 48.0 14,248.0 | 4,781.3 | 139.44 | 666.7 |

Table E.1 Results of Suspended Load Measurement

| No. | Date | Time | Position | Measured S.S Contents (mg/l) | Ave. S.S Contents (mg/l) | Flow (m³/s) | Suspended Load Discharge (kg/s) |
|-----|-----------|-------|-------------------------|---------------------------------|-----------------------------|----------------|------------------------------------|
| 13 | 28-Mar-95 | 11:00 | left middle right | 16.0 8,060.0 170.0 | 2,748.7 | 108.49 | 298.2 |
| 14 | 29-Mar-95 | 11:15 | left middle right | 64.0 11,782.0 160.0 | 4,002.0 | 70.46 | 282.0 |
| 15 | 30-Mar-95 | 10:40 | left middle right | 88.0 1,332.0 100.0 | 506.7 | 38.21 | 19.4 |
| 16 | 1-Apr-95 | 11:45 | left middle right | 82.0 150.0 30.0 | 87.3 | 24.34 | 2.1 |
| 17 | 4-Apr-95 | 12:15 | left middle right | 2,392.0 6,370.0 190.0 | 2,984.0 | 36.88 | 110.1 |
| 18 | 5-Apr-95 | 10:25 | left middle right | 700.0 320.0 280.0 | 433.3 | 59.39 | 25.7 |
| 19 | 6-Apr-95 | 10:20 | left middle right | 170.0 50.0 280.0 | 166.7 | 80.19 | 13.4 |
| 20 | 7-Apr-95 | 10:00 | left middle right | 3,180.0 60.0 30.0 | 1,090.0 | 75.70 | 82.5 |
| 21 | 10-Apr-95 | 11:15 | left middle right | 68.0 180.0 112.0 | 120.0 | 80.41 | 9.6 |
| 22 | 11-Apr-95 | 12:10 | left middle right | 28.0 6,210.0 140.0 | 2,126.0 | 65.32 | 138.9 |
| 23 | 12-Apr-95 | 11:55 | left middle right | 100.0 210.0 6,196.0 | 2,168.7 | 52.62 | 114.1 |
| 24 | 17-Apr-95 | 11:15 | left middle right | 155.0 216.0 5,290.0 | 1,887.0 | 52.07 | 98.3 |

Table E.1 Results of Suspended Load Measurement

| No. | Date | Time | Position | Measured S.S Contents (mg/l) | Ave. S.S Contents (mg/l) | Flow (m³/s) | Suspended Load Discharge (kg/s) |
|-----|--------------------|-------|-------------------------|---------------------------------|-----------------------------|-------------|------------------------------------|
| 25 | 18 - Apr-95 | 12:10 | left middle right | 156.0 217.0 5,586.0 | 1,986.3 | 52.14 | 103.6 |
| 26 | 20-Apr-95 | 11:55 | left middle right | 160.0 215.0 5,176.0 | 1,850.3 | 43.21 | 80.0 |
| 27 | 7-Aug-95 | 15:28 | left middle right | 86.0 88.0 76.0 | 83.3 | 287.97 | 24.0 |
| 28 | 15-Aug-95 | 12:00 | left middle right | 80.0 70.0 70.0 | 73.3 | 165.18 | 12.1 |
| 29 | 16-Aug-95 | 15:15 | left middle right | 88.0 84.0 68.0 | 80.0 | 196.29 | 15.7 |
| 30 | 18-Aug-95 | 17:05 | left middle right | 60.0 66.0 80.0 | 68.7 | 236.25 | 16.2 |
| 31 | 19-Aug-95 | 16:05 | left middle right | 122.0 88.0 98.0 | 102.7 | 361.32 | 37.1 |
| 32 | 21-Aug-95 | 15:30 | left middle right | 76.0 108.0 190.0 | 124.7 | 228.24 | 28.5 |
| 33 | 22 - Aug-95 | 10:28 | left middle right | 80.0 84.0 72.0 | 78.7 | 389.73 | 30.7 |
| 34 | 23-Aug-95 | 10:00 | left middle right | 64.0 76.0 92.0 | 77.3 | 241.20 | 18.7 |
| 35 | 24-Aug-95 | 12:32 | left middle right | 89.0 226.0 32.0 | 115.7 | 197.26 | 22.8 |
| 36 | 25-Aug-95 | 11:15 | left middle right | 64.0 82.0 70.0 | 72.0 | 184.66 | 13.3 |

Table E.1 Results of Suspended Load Measurement

| No. | Date | Time | Position | Measured S.S Contents (mg/l) | Ave. S.S Contents (mg/l) | Flow (m³/s) | Suspended Load Discharge (kg/s) |
|-----|-------------------|-------|-------------------------|---------------------------------|-----------------------------|-------------|------------------------------------|
| 37 | 26-Aug-95 | 11:05 | left middle right | 84.0 98.0 14.0 | 65.3 | 304.74 | 19.9 |
| 38 | 27-Aug-95 | 11:10 | left middle right | 82.0 36.0 44.0 | 54.0 | 274.57 | 14.8 |
| 39 | 29-Aug-95 | 12:15 | left middle right | 82.0 76.0 56.0 | 71.3 | 404.91 | 28.9 |
| 40 | 30-Aug-95 | 12:30 | left middle right | 48.0 68.0 76.0 | 64.0 | 321.67 | 20.6 |
| 41 | 31-Aug-95 | 11:45 | left middle right | 80.0 78.0 52.0 | 70.0 | 204.29 | 14.3 |
| 42 | 1 - Sep-95 | 14:50 | left middle right | 52.0 56.0 56.0 | | 303.47 | 16.6 |
| 43 | 2-Sep-95 | 12:10 | left middle right | 158.0 156.0 84.0 | 132.7 | 291.10 | 38.6 |
| 44 | 3-Sep-95 | 12:50 | left middle right | 138.0 150.0 148.0 | 145.3 | 309.72 | 45.0 |
| 45 | 4-Sep-95 | 11:10 | left middle right | 132.0 134.0 146.0 | 137.3 | 256.44 | 35.2 |

APPENDIX F

TIDE LEVEL

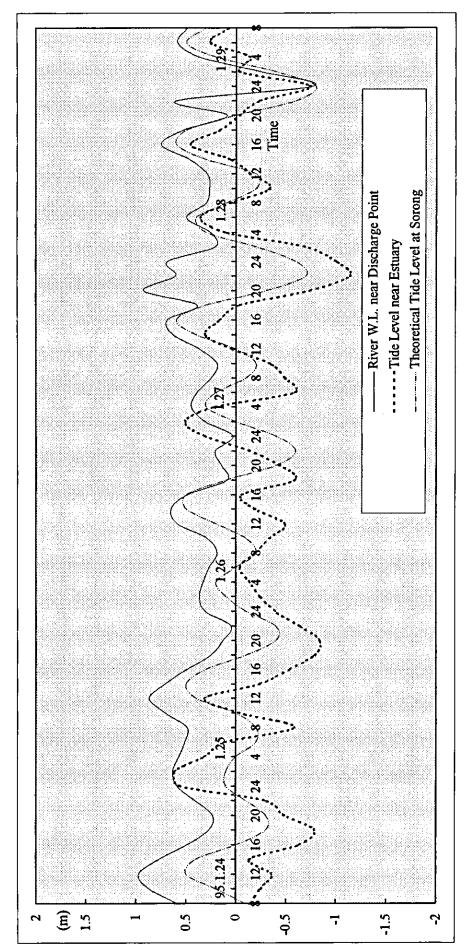


Fig F.1 Results of Water Level Measurement (1/3)

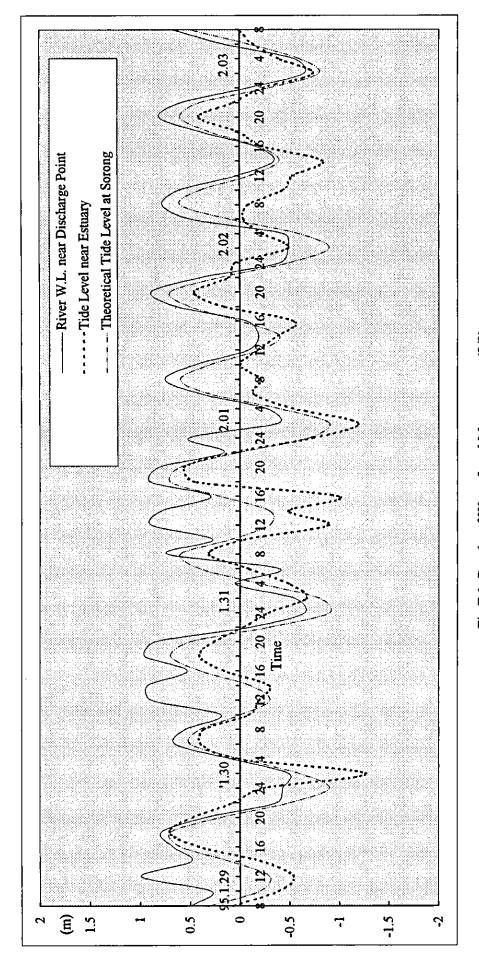


Fig F.1 Results of Water Level Measurement (2/3)

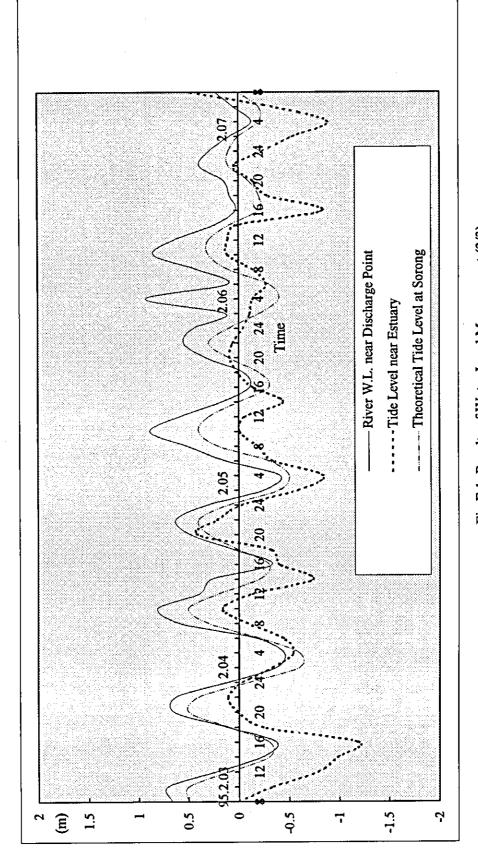


Fig F.1 Results of Water Level Measurement (3/3)

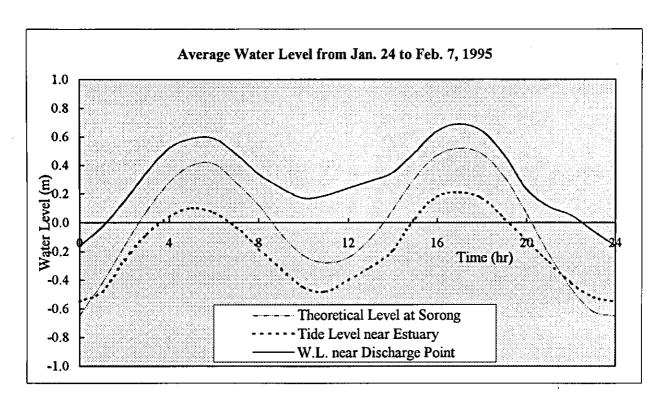


Fig. F.2 Average Water Level

VOLUME - II TOPOGRAPHIC SURVEY

Table of Contents

| CHAPTER 1 PLANNING AND PREPARATION | 1 - 1 |
|---|-------|
| CHAPTER 2 MONUMENTATION | 2 - 1 |
| CHAPTER 3 AERIAL PHOTOGRAPHY | 3 - 1 |
| 3.1. General | 3 - 1 |
| 3.2. Aerial Photography | 3 - 1 |
| 3.3. Post Processing | 3 - 2 |
| 3.4. Coordinate Transformation | 3 - 3 |
| 3.5. Printing and Editing | 3 - 4 |
| 3.6. Personnel and Equipment | 3 - 5 |
| CHAPTER 4 FIELD VERIFICATION | 4 - 1 |
| CHAPTER 5 CONTROL POINT SURVEY | 5 - 1 |
| 5.1. General | 5 - 1 |
| 5.2. GPS Observation | 5 - 1 |
| 5.3. Data Processing | 5 - 2 |
| 5.4. Personnel and Equipment | 5 - 4 |
| CHAPTER 6 LEVELLING | 6 - 1 |
| 6.1. General | 6 - 1 |
| 6.2. Personnel and Equipment | 6 - 1 |
| 6.3. Observation | 6 - 1 |
| 6.4. Computation | 6 - 1 |
| 6.5. Accuracy | 6 - 2 |
| CHAPTER 7 AERIAL TRIANGULATION | 7 - 1 |
| 7.1. General | 7 - 1 |
| 7.2. Aerial Triangulation and Block Adjusment | 7 - 1 |
| 7.3. Personnel and Equipment | 7 - 3 |
| CHAPTER 8 PLOTTING AND EDITING | 8 - 1 |
| 8.1. General | 8 - 1 |
| 8.2 Plotting and Editing | Q _ 1 |

| 8.3.] | Personnel and Equipment | 8 - 2 |
|----------------|--|--------|
| СНАРТЕ | R 9 DRAWING | 9 - 1 |
| 9.1. | General | 9 - 1 |
| 9.2 . 1 | Fair Drawing | 9 - 1 |
| 9.3. | Personnel and Equipment | 9 - 2 |
| СНАРТЕ | R 10 RIVER LONGITUDINAL PROFILING | 10 - 1 |
| 10.1. | General | 10 - 1 |
| 10.2. | Longitudinal Profiling | 10 - 1 |
| 10.3. | Personnel and Equipment | 10 - 1 |
| СНАРТЕ | R 11 RIVER CROSS SECTION | 11 - 1 |
| 11.1. | General | 11 - 1 |
| 11.2. | River Cross Section | 11 - 1 |
| 11.3. | Personnel and Equipment | 11 - 1 |
| | ER 12 TOPOGRAPHIC SURVEY | 12 - 1 |
| | General | 12 - 1 |
| | Topographic Survey | 12 - 1 |
| 12.3. | Personnel and Equipment | 12 - 1 |
| Appendix | 2.1. Type and Size of Monument | |
| | 2.2. Discription of Bench Mark | |
| | 3.1. Flight Index for 1:10,000 | |
| | 3.2. Flight Index for 1:20,000 | |
| | 3.3. Description of Reference Point for Kinematic GPS | |
| | 5.1. Geodetic and UTM Coordinate in ID '74 | |
| | 6.1. Map of Static GPS Network, Traversing and Levelling Route | |
| | 6.2. Final Coordinate and Elevation of GPS Survey | |
| | 9.1. Index Sheet for Map at scale 1: 10,000 | |
| | 9.2. Index Sheet for Map at scale 1: 2,500 | |
| | 9.3. Index Sheet for Map at scale 1:500 | |
| | 11.1. Final Coordinate and Elevation of Main Traverse Route | |
| | 11.2. Azimuth and Distance for Following Survey | |

CHAPTER 1 PLANNING AND PREPARATION

In accordance with the Scope of Wok agreed upon between PT. PLN (PERSERO) and JICA, the JICA Study Team prepared the technical specifications for Aerial Photography and Topographic Survey and made contract with PT. AEROKARTO INDONESIA to coduct survey activities.

In accordance with the Cntract Document, PT. AEROKARTO INDONESIA prepared work plan, time schedule, personnels, instruments, distribution of Bench Mark, survey control network plan, flight plan and permission letters needed for implementation of the work.

Security Clearance for Aerial Photography was obtained from Pussurta ABRI No.SC-065/P/SPA/XII/93 dated on January 21,1994.

CHAPTER 2 MONUMENTATION

16 monuments, which were established in the planning and preparation work for the project, were installed with the type and size as shown in appendix 2.1.

All concrete monuments were described and documented with sketches and photographs providing detailed information about monuments such as coordinates, locations, access etc.

For description and location of concrete monuments, see Appendix 2.2.

CHAPTER 3 AERIAL PHOTOGRAPHY

3.1. General

The aerial photography of the Warsamson Hydroelectric Power Development project was carried out using Wild RC.20 camera by kinematic GPS method.

As reference point, SP.74 (Located at Biak island) was used:

Latitude

1º 10' 04.12100" S

Longitude

136° 05' 23.63200" E

Elevation

124.410 m

The benefit of Kinematic GPS are as follows:

- Especially in the Warsamson area which are covered with dense forest, Kinematic GPS will minimize the need of ground control point and will minimize tree cuting.
- Every Principle point of photograph has coordinates.
- Coordinates of every photo can be obtained immediately after post processing is completed.
- Aerial triangulation activity can be commenced as soon as diapositive is ready.
- A sub meter accuracy can be obtained.

3.2. Aerial Photography

a. Instrument Preparation

Instrument preparation activity consists of instrument setting and testing of GPS instrument which are used on the ground and in an aircraft.

Instrument setting in an aircraft is rather complex because it requires antenna setting, interconection between GPS receiver, camera and computer which must be integrated each other.

There are 5 (five) main elements to be set in an aircraft:

- 1. GPS antenna which is installed at 1.78 meters in front of a camera.
- 2. GPS receiver Trimble 4000 SSE.
- 3. Toshiba Laptop Computer.
- 4. Aerial camera WILD RC-20 FMC.
- 5. External clock (Rubidium).

b. Observation Method

Observation was done by a differential method, where one of receivers was installed on the reference point and the other one in the aircraft, and positions of GPS satellites were simultanously observed.

Using TOPAS software post processing, relative position between the reference point and antenna position on the aircraft was obtained. Center point position of photograph was obtained from aerial triangulation using PAT-B GPS software.

c. Observation Procedure

Before implementing the observation, preparation was done:

- Preparation of sky plot, satellite window, satellite availability before observation.
- Time planning and observation according to sky plot, satellite window, satellite avaibality and weather condition.

Observation was done simultanously, on the reference point and in the aircraft:

- Recording data 1 PPS GPS in the aircraft and 3 seconds data at the reference point.
- Sending GPS time signal from the receiver to the aircraft (after converted in computer) to print on every frame of film.
- Sending exposure signal from the camera to the GPS receiver.
- Recording (down loading) observation datas into diskete for post processing.

3.3. Post Processing

To obtain position of observation points, data 1 PPS from the aircraft and 3 seconds data from the reference point were proceed.

Coordinates of every center point of photograph was obtained after the following correction:

a. Differential Correction.

Differential correction is carried out in two stages and its basic concept is as follows:

- 1. According to a reference point position, an error of carrier phase is computed using 3 seconds data. This error is known as "differential correction".
- 2. Using differential correction from the reference point, to proceed datas from aircraft which have identical error.

As we know there are lot of errors in carrier phase data:

- Tropospheric error.
- Ionospheric error.

- Clock error.
- Multy path error.

According to the reference point position, errors are computed and corrected to antenna position on the aircraft.

b. Clock Correction (Clock error)

As we know, satellite uses an atomic clock and GPS receiver uses oscilator quartz which have different accuracy.

To avoid delay caused by accuracy of oscilator quartz, precise external clock (Rubium, Cesium) was installed which was used in the post processing.

c. Offset Correction

Position of antenna and center camera does not coincide, so center position of camera must be computed and corrected.

d. Position of Center of Photograph Computation

Position of antenna was corrected by correction factor, which was computed formerly.

Center position of camera was computed using aerial triangulation bundle adjustment method.

PAT-B GPS software was used for adjustment.

3.4. Coordinate Transformation

From bundle adjusment computation it was obtained geographic coordinate in WGS '84. Coordinate of photo center in ID '74 was transformed from WGS '84 using DMA (Defence Mapping Agency) formula (according to Bakosurtanal's letter dated on October 28,1991):

$$X$$
 dX 1 - Rz Ry X
 Y = dY + (scale) Rz 1 - Rx Y
 Z (ID '74) dZ - Ry Rx 1 Z (WGS '84)

Transformation parameter used are:

$$dX = -2.691 \text{ m}$$

 $dY = +14.757 \text{ m}$
 $dZ = -4.727 \text{ m}$
 $Rx = 0$ "
 $Ry = 0$ "

$$Rz = + 0.814$$
"
 $K = + 0.600 \text{ PPM } (S = 1 + K)$

Aerial Triangulation was computed in cartesian coordinate system. Formula for the tranformation from geographic coordinate system to cartesian coordinate system are:

$$X = (r + h) \text{ Cos Lat .Cos Lon}$$

 $Y = (r + h) \text{ Cos Lat .Sin Lon}$
 $Z = (r - h) \text{ Sin Lat}$
 a
 $r = \frac{a}{(1 - e2.\text{Sin 2Lat})2}$

3.5. Printing and Editing

a. Processing Film.

Processing of film is a very importand process, due to this step will determine quality of paper print and diapositive film. This step was supervised by a laboratorium supervisor.

b. Annotation.

Every photograph have to be annotated to simplify in finding photograph in the next future. Annotation consist of:

- Roll number of film
- Time of exposure
- Date of exposure
- Project owner
- Location of survey area
- Scale of photograph
- Number of flight line
- Number of photograph every flight line

c. Flight Line Map

Flight line map was made to make easy and fast in finding photograph.

Flight line map was made at scale of 1: 100.000. Number of photograph and number of flight line were included in that map.d. Printing Paper and Diapositive.

Two sets of aerial photograph were printed in double weight paper and one set diapositive printed in film material.

3.6. Personnel and Equipment

Personnels

1. Ir.Indra Ranadireksa : Photography Engineer

2. Ir. Kurniawati : Coordinator

3. Capt. Martono : Pilot

4. Evi Sufina : Mechanic 5. Rochadi Pramugari : Navigator

6. Endang Kusmana : Camera Operator

7. Sugiyo : Laboratory Technician

8. Rachmat Suryana : Laboratory Technician

9. Saidi : Laboratory Technician

10. Budi Riyanto : Annotator
11. Rasmanto : Draftsman

12. Peltu Sudiarto : Security Officer

Equipments

1. Aircraft Taurus King Air Reg. No. PK - VKY

2. Aerial Camera Wild RC - 20 No. 13123

3. Trimvec Kinematic GPS

4. PAT-B GPS Software

5. Rewind processor

6. Developing machine

7. Rinsing machine

8. Contact printer Aerotopograph KG - 30

9. Dryer

10. Dark room facilities

11. Annotation table

12. Drafting table

13. Drafting equipment

14. Camera reproduction

15. Vehicle.

CHAPTER 4 FIELD VERIFICATION

Field verification was executed using 4 times enlarged aerial photograph at scale of 1: 2,500 map and 2 times at scale of 1: 10,000 map.

All objects on the photographs were verified according to the map symbol. Uninterpretable objects were also notated including bridges, roads, rivers, vegetations etc.

All necessary data such as name of villages, Kecamatan, Kabupaten, and its boundary were identified and plotted on the 4 times and 2 times enlarged photograph.

CHAPTER 5 CONTROL POINT SURVEY

5.1. General

Control point survey by GPS observation in Warsamson Hydroelectric Power Development Project is to obtain coordinates of control points which have been established in the survey area. The coordinates will be used to produce topographic map at scale of 1: 10,000 and 1: 2,500.

Distribution of control points are selected on requirement of aerial triangulation, 12 control points were distributed for mapping at scale of 1:10,000 in 200 square km area and 4 control points were distributed for mapping at scale of 1:2,500.

GPS observation network were tied to Doppler Station N.6007/SP5 in Sorong. Coordinate of N.6007/SP5 was obtained from Bakosurtanal.

The coordinates which were obtained from GPS observation are in WGS '84 ellipsoid reference which then transformed to ID '74 as a national ellipsoid reference.

Instruments which were used in this work were GPS receivers Leica System 200 survey type and SKI software version 1.08 from Leica for data processing.

GPS observation have been executed from January 15, 1994 to February 15, 1994 and data processing executed from February 20, 1994 to March 3, 1994.

5.2. GPS Observation

a. Preparation.

Before implementing GPS observation, selecting the control points have to be done in order to fulfill the requirement of aerial triangulation.

Permission letter from Pussurta ABRI was needed for field survey work. Permission Letter was obtained from Pussurta ABRI no. SC-040/D/SPA/XII/93 dated on January 13, 1994.

b. GPS Observation.

Before observation of GPS satellites, almanac collection was done in survey area to obtain the best time for satellite observation according to GDOP and PDOP. Almanac of GPS satellite was made using latitude and longitude argument.

Satellite observation were executed on 16 control points:

W.01, W.02, W.03, W.04, W.05, W.06, W.07, W.08, W.09, W.10, W.11, W.12, W.13, W.14, W.15, W.16

and 8 Spot Elevation Survey:

SPOT.A, SPOT.B, SPOT.C, SPOT.D, SPOT.E, SPOT.F, SPOT.G, SPOT.H

and tied to Doppler Station N.6007/SP5 which it coordinates was given by Bakosurtanal.

Satelitte observation was executed using two GPS receiver Leica system 200 which using dual frequencies for 1 hour and were tied to N.6007/SP5 for 1.5 hours. Cut off angle satellite observation was 15 degrees and observation record rate was 15 seconds. Satellite observations were using differential carrier phase static method.

5.3. Data Processing

Data processing was carried out using SKI software version 1.08 from Leica.

a. Base Line Computation.

Preliminary computation was base line computation. The coordinates of every control points, the length of the base line and the accuracy of measurement were obtained from the base line computation.

b. Network Adjustment.

SKI software version 1.08 from Leica was used for network adjustment. This package program computed network control point in cartesian coordinate with least square adjustment. N.6007/SP5 which has Geodetic and UTM grid coordinates in WGS '84 was used as reference point with its coordinates are as follow:

Geodetic coordinate:

Latitude = $0^{\circ} 52' 30.644370'' S$

Longitude = $131^{\circ} 15' 12.873080'' E$

Elevation = 141.390 m (above ellipsoid reference)

UTM Grid coordinate:

Northing = 750,802.593 m

Southing = 9,903,190.983 m

Elevation = 65.924 m (according to Sorong peil)

c. Datum Transformation.

The result of coordinates from network adjustment were transformed from WGS '84 to ID '74 using transformation parameter:

dX = -2.691 m

dY = + 14.757 m

dZ = -4.727 m

Rx = 0"

Rv = 0"

Rz = + 0.814"

K = + 0.600 PPM (S = 1 + K)

The final result of geodetic coordinate and UTM grid are on ID '74 reference ellipsoid. (See Appendix 5.1)

Accuracy of GPS Observation.

| No. | Point Number | Latitude (meter) | Longitude (meter) | |
|------------|--------------|---------------------|-------------------|--|
| 1. | W.01 | 0.01072 | 0.01934 | |
| 2. | W.02 | 0.01407 | 0.02235 | |
| 3. | W.03 | 0.00892 | 0.01736 | |
| 4. | W.04 | 0.01465 | 0.02282 | |
| 5. | W.05 | 0.00675 | 0.01073 | |
| 6. | W.06 | 0.00459 | 0.00661 | |
| 7 . | W.07 | 0.01566 | 0.02349 | |
| 8. | W.08 | 0.02347 | 0.10192 | |
| 9. | W.09 | 0.02315 | 0.10175 | |
| 10. | W.10 | 0.00388 | 0.00437 | |
| 11. | W.11 | 0.02962 | 0.18020 | |
| 12. | W.12 | 0.00848 | 0.00985 | |
| 13. | W.13 | 0.00467 | 0.00529 | |
| 14. | W.14 | 0.00939 | 0.01131 | |
| 15. | W.15 | 0.01155 | 0.01315 | |
| 16. | W.16 | 0.02296 | 0.10166 | |
| 17. | SPOT.A | 0.00401 | 0.00589 | |
| 18. | SPOT.B | 0.00760 | 0.01466 | |
| 19. | SPOT.C | 0.00759 | 0.01661 | |
| 20. | SPOT.D | 0.01280 | 0.02106 | |
| 21. | SPOT.E | 0.01335 | 0.02155 | |
| 22. | SPOT.F | 0.00765 | 0.01570 | |
| 23. | SPOT.G | 0.03825 | 0.15605 | |
| 24. | SPOT.H | 0.02277 | 0.10162 | |

5.4. Personnel and Equipment:

Personnels:

1. Ir. Mohamad Soleh : Coordinator/Surveyor

2. Ir. Judi : Surveyor

3. Noerqamar Aroeppala : Assistant Surveyor

4. Abdul Gafur : Assistant Surveyor

Equipments:

1. 2 (two) sets of GPS receiver Leica system 200 survey type consist of:

Sensor Wild SR299 No: 100506, 100533. Controller Wild CR233 No: 93183, 93181.

2. Radio Comunication Kenwood : 2 sets

3. Note Book Computers USA COM : 2 sets

4. Generator set Honda : 2 sets

5. SKI Software : 2 sets

CHAPTER 6 LEVELLING

6.1. General

Vertical control points in the Warsamson Hydroelectric Power Development Project were required for aerial triangulation computation. The aerial triangulation result will be used to prepare topographic maps at scale of 1:2,500 and 1:10,000.

Total measurement length of direct levelling was 160.103 km and was tied to Sorong peil BM PLB at the Sorong harbour and BM KTJ in Pertamina estate. Map of levelling route, see Appendix 6.1

6.2. Personnel and Equipment

Personnels:

Suparmanto : Surveyor
 Suwandi : Surveyor
 Widodo : Surveyor
 Abdul Gafur : Supervisor

Equipments:

1. TOPCON ATS 3 : 2 set (Instr. No. C.102 and E.041).
2. WILD NAK 1 : 1 set (Instr. No. 472740).

6.3. Observation

Vertical control point survey was carried out using direct levelling observation and was tied to BM KTJ which has elevation 2.504 m above mean sea level. Bench mark ABT.2 which was proposed in pre feasibility study report was not used, the bench mark does not exist any more because of bridge construction.

Levelling observation was carried out using double standing observation, first observation reads all three thread and second observation only middle.

6.4. Computation

Different elevetion was computed from observation 1 and observation 2. Mean different elevation was obtained from : dh = 1/2 (Obs.1 + Obs.2).

where,

dh: mean different elevation

Obs.1: different elevation from observation 1 Obs.2: different elevation from observation 2

6.5. Accuracy

Discrepancy of levelling observation: +/- 50 mm V-S where S is the length in kilometer of a single run.

| | S | Height Difference | | Error | Tolerance | Remarks |
|-----------------|----------|-------------------|----------|-------|-----------|---------|
| Point | (km) | I | П | (mm) | (mm) | |
| | | (m) | (m) | | | |
| BM KTJ | | | | | | |
| DMKI | 31.9 | 178.675 | 178.645 | 30 | 282 | OK |
| T. Mariat | | 1,0.0,2 | 2,0,0,0 | | | |
| DP. 6 | | | | | | |
| | 24.2 | 11.393 | 11.402 | 9 | 245 | OK |
| W.04 | | | | | | |
| DP. 16 | | | | | *** | |
| *** 00 | 18.7 | 146.166 | 146.152 | 14 | 216 | OK |
| W.08 SPOT. C | | | | | | |
| SPO1.C | 2.2 | 20.849 | 20.854 | 5 | 74 | ок |
| SPOT. F | 2.2 | 20.047 | 20.054 | | '' | ••• |
| W.03 | | | | | | |
| | 5.4 | -31.891 | - 31.929 | 38 | 116 | OK |
| SPOT. D | | | | | | |
| HP.1 | | | | | | |
| | 5.2 | - 64.678 | - 64.666 | 12 | 114 | OK |
| W.10 | | | | | | 1 |
| HP.2 | 2.0 | - 40.885 | - 40.881 | 4 | 70 | ok l |
| W.14 | 2.0 | - 40.865 | - 40.661 | | /* | |
| HP.3 | | | | | | |
| | 2.2 | 24.403 | 24.395 | 8 | 74 | ок |
| W. 12 | | | | | | |
| HP.4 | | | | | | |
| | 5.6 | - 11.406 | - 11.402 | 4 | 119 | OK |
| SPOT. G | | | | | | |
| HP. 5 | 6.1 | - 62.704 | - 62.694 | 10 | 124 | ок |
| W. 11 | J.1 | - 04,704 | - 02.074 | '` | 127 | |
| HP. 6 | 1 | | | | | |
| | 3.4 | - 27.921 | - 27.928 | 7 | 92 | ок |
| SPOT. H | | | | | | |
| HP. 7 | | | | _ | | |
| 137.15 | 1.1 | 28.948 | 28.950 | . 2 | 52 | OK |
| W. 15 | | | | | | |
| HP. 8 | 4.7 | - 5.304 | - 5.296 | 8 | 107 | ok |
| W. 16 | 1 | - 5.504 | - 5,230 | | 107 | ``` |
| HP. 9 | | | | | | |
| | 4.7 | 3.866 | 3.860 | 6 | 109 | ок |
| W. 09 | | | | | | |
| | | | | | | |

CHAPTER 7 AERIAL TRIANGULATION

7.1. General

The Implication and purpose of Aerial Triangulation work is to obtain the coordinates (X,Y,Z) of the aerial photo points. The coordinates were required for the orientation process of each stereo model on the plotting instrument to produce topographic map at scale of 1:10,000 and 1:2,500.

Ground control points resulted from field measurement (GPS survey and levelling survey) were used as reference points.

7.2. Aerial Triangulation and Block Adjusment

The sequence of works to be carried out as follows:

a. Data Collection

All necessary datas were collected and prepared such as:

- Flight index
- Control points coordinate and description
- Calibration report of the aerial camera etc.

b. Planning

Preparation of aerial triangulation was carried out as follows:

- Selecting of the aerial photos.

Total model of the aerial photos were 204 models.

- Control Point Selection

14 horizontal control points and 11 vertical control points were selected as control for the aerial triangulation processing.

c. Preparation

Stages of preparation were carried out as follows:

- Point selection and numbering

Pass points and tie points were selected within the triple overlap area with the Circle notation on the index model.

Numbering system was carried out as follows:

Model number 141 12 0

1 2 3

where,

- 1 = Course number
- 2 = Photo number
- 3 = Principle point
- The horizontal and vertical control points were annotated on the index models as a square (
 ☐), and vertical control points were annotated as triangle ().

The point selection and the numbering were carried out on the 1:20,000 and 1:10,000 scale of the aerial photographs by using a mirror stereoscope.

d. Point Transfer

The selected points and control points on one diapositive film were marked. The points were transferred to adjacent diapositive film by using Wild PUG.4 instrument, and this activity was carried out until the last photos.

e. Index Model

The index model at scale of 1:100.000 was produced.

All point numbers were plotted, to show the relationship between each points in the index model.

f. Measurement of Coordinates

Photo coordinates were observed and measured using a stereo comparator Zeiss Stecometer equipped with digitizer. All points including fiducial mark were measured.

g. Adjustment

The final step of the aerial triangulation is the block adjustment using PAT-B.

Accuracy of the aerial triangulation block adjusment result are as follows:

Standard Deviation of Terrain Points in Units of Terrain System

| Element | Point | Sta | ndard Deviation Va | lue |
|---------|--------|---------|--------------------|-------|
| | Number | Minimum | Maximum | Mean |
| | | | 1 | |
| X | 100 | 0.113 | | |
| Y | 100 | 0.112 | | |
| Z | 100 | 0.232 | | |
| X | 150082 | | 2.927 | |
| Y | 150082 | | 2.987 | |
| Z | 150081 | | 6.226 | |
| x | | | | 0.519 |
| Y | | | | 0.517 |
| Z | | | | 1.301 |
| | | | | |

7.3. Personnel and Equipment

Personnels:

1. Ir.Kurniawati : Photogrammetric Engineer

2. Djudju Sardju : Coordinator

3. Prawito Sumargono : Op. for point selection

4. Sudirman BE : Op. for point selection

5. Maryono : Op. for point transfer6. Rubin Subagja S. : Op. for point transfer

7. Harry Wibowo : Op. for measuring model coordinate

8. Mudjianto SE. : Op. for measuring model coordinate

9. N.Q. Aroeppala : Computer Analyst.

Equipments:

1. Stereoscope : 2 unit

2. Point transfer Wild PUG-4 : 1 unit

3. Stereo Comparator Zeiss Stecometer : 1 unit

4. Computer : 1 unit

5. PAT-B : 1 unit

6. Vehicle : 1 unit

CHAPTER 8 PLOTTING AND EDITING

8.1. General

The implication and purpose of stereo plotting and edit-ing work is to draw details and contour lines using aerial photo diapositives. The photo diapositives were placed on the plate holders of the stereo plotter instrument.

8.2. Plotting and Editing

The sequence of the work was carried out as follows:

a. Data Collection

All necessary datas were collected and prepared for stereo plotting such as:

- Model index of aerial triangulation.
- Print out of aerial triangulation adjustment
- Vertical Control points and description on two times enlarged aerial photographs.
- Field Identification Results on two times enlarged aerial photographs.

b. Preparation.

Preparation of Stereo Plotting was carried out as follows:

- Control Sheets.

Control sheets were produced on polyester base material. Coordinates from block adjusment computation were plotted on control sheets.

Total Control sheets of the stereo plotting were 9 sheets for topographic map at scale of 1: 10,000 and 12 sheets for topographic map at scale of 1: 2,500.

- Models

Total models of the stereo plotting were 70 Models for topographic map at scale of 1:10,000 and 21 Models for topographic map at scale of 1:2,500.

c. Plotting and Editing

Plotting manuscript at scale of 1: 10,000 were carried out using aerial photos at scale of 1: 20,000, and plotting manuscript at scale of 1: 2,500 were carried out using aerial photos at scale of 1: 10,000. Second order precision stereo plotter were used in stereo plotting work.

The sequence of the stereo plotting work are as follows:

- 1. Inner Orientation
- 2. Relative Orientation

- 3. Absolute Orientation
- 4. Plotting of Details, Spot heights, Vegetation boundaries and Contour lines.

Contour Interval for intermediate contour lines are 5 m for map at scale 1: 10,000 and 2 m for map at scale 1: 2,500.

Editing work was carried out on the plotting manuscript by compiling the result of field identification, such as: Symbols, Annotation etc.

d. Result

The final result of plotting and editing works were manuscript map:

- 9 sheets manuscript map at scale of 1:10,000.

- 12 sheets manuscript map at scale of 1: 2,500.

8.3. Personnel and Equipment

Personnels:

1. Ir. Kurniawati : Photogrammetric Engineer

2. Djudju Sardju : Coordinator

3. Prawito Sumargono : Stereo Plotter Operator4. Harry Wibowo : Stereo Plotter Operator

5. N.Q. Areoppala : Stereo Plotter Operator

6. Rochadi P. : Stereo Plotter Operator

7. Mudjianto SE. : Stereo Plotter Operator

8. Sri suhartini : Stereo Plotter Operator
9. Mardius : Computer Operator

10. Triono : Computer Operator

11. Ir. Mohamad Soleh : Editor
12. Ir. Judi : Editor

Equipment:

1. Computer: 2 units2. Roland Plotter: 1 unit3. Plotter Wild A-8: 2 units

5. Drafting table : 3 units

4. Plotter Wild AG-1

: 1 unit

CHAPTER 9 FAIR DRAWING

9.1. General

The implication and purpose of Fair Drawing work is to draw details using symbols and contour lines from manuscript map and other additional datas to provide a true and informative map. Tracing method was used for the drawing.

9.2. Fair Drawing

The sequence of the work was carried out as follows:

a. Data Collection.

All necessary datas were collected and prepared for fair drawing such as :

- Manuscript map.
- Vertical Control points and description on two times enlarged aerial photographs.
- Field Identification Results on two times enlarged aerial photographs.

b. Preparation.

Preparation of Fair Drawing were carried out as follows:

- Drawing Sheets.

Total 25 sheets were prepared which consist of:

11 sheets map at scale of 1: 10,000 and

14 sheets map at scale of 1: 2,500.

Polyester base material drawing sheets size are A1 (55 cm x 80 cm).

Numbering system is as follows (sample for map at scale of 1:10,000):

Sheet number: 11 - 1

where, 11 = Total of sheets.

1 = Sheet number.

- Legend, Symbol.

Legend, symbol and annotation which were used for the map should be approved by the Engineer.

c. Fair Drawing.

Tracing method fair drawing was carried out using drawing pen and black ink from manuscript map at scale of 1:10,000 and 1:2,500.

Fair drawing works are as follows:

- 1. Drawing details
- 2. Spot heights and Contour lines
- 3. Symbols and annotations. On the map, symbols must be matched to legend.
- 4. Vegetation boundaries.

Contour Interval for intermediate contour lines are 5 m for map at scale of 1:10,000 and 2 m for map at scale of 1:2,500.

Other additional information and contour lines were adjusted by the field work.

d. Results.

The final results of the fair drawing are:

- 11 sheets of Topographic maps at scale of 1:10,000.
- 14 sheets of Topographic maps at scale of 1: 2,500.

9.3. Personnel and Equipment

Personnels:

1. Ir. Indra Ranadireksa : Cartographic Engineer

2. Eka Ch. Ruslan : Coordinator

3. Tulus Satmoko : Editor 4. Ir. Umar Senoaji : Editor

5. Budi Riyanto : Draftsman 6. Rasmanto : Draftsman

7. Ahmad Fauzi : Draftsman

8. Ade Sutisna : Draftsman
10. Hartini : Draftsman

11. Triono : Computer Operator
12. Mardius : Computer Operator

Equipments:

Computer : 2 unit
 Roland Plotter : 1 unit
 Drafting table : 9 unit
 Drafting tools : 9 unit

CHAPTER 10 RIVER LONGITUDINAL PROFILING

10.1. General

Work of river longitudinal profiling in the Warsamson Hydroelectric Power Development Project consist of:

- Setting of PVC for Spot Elevation Survey.
- Setting of wooden pegs for 30 200 m interval.
- Traversing and Longitudinal profiling.

10.2. Longitudinal Profiling

Longitudinal profiling has been carried out for 23.6 km along the rivers of: Warsamson, Klalin and Klasmigik.

Traverse survey using Total Station instrument was carried out to obtain coordinate.

Longitudinal profiling along the rivers was carried out using automatic level instrument.

Accuracy of traverse survey obtained:

| Route | Name | Initial | Terminal | Total Length | Accuracy | Tolerance | | | | | | | |
|-------|-------------------------------|--------------|----------|--------------|----------|-----------|--|--|--|--|--|--|--|
| No. | | Point | Point | (Km) | | 1:7,000 | | | | | | | |
| | | | | | | | | | | | | | |
| I | Jalur R | Spot. D | W.03 | 5.1 | 1:30,956 | Ok | | | | | | | |
| Π | Jalur L | R.1 | R' | 2.3 | 1:20,676 | Ok | | | | | | | |
| III | Jalur C | PB.1 | Spot. C | 4.9 | 1:14,083 | Ok | | | | | | | |
| ΙV | Jalur F | Spot. C | Spot. F | 5.5 | 1:10,135 | Ok | | | | | | | |
| V | V S. Klalin 2.0 Open Trav | | | | | | | | | | | | |
| VI | VI S. Klasmigik 6.1 Open Trav | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | Total Distance = 23.6 Km. | | | | | | | | | | | | |
| | | I Ottal Dist | | 25.0 Mil | | | | | | | | | |

Note: Route I and II used only for Topographical Survey.

Two Longitudinal profiles along S.Klalin and two along S.Klasmigik were drawn at scale of 1: 5,000 for horizontal and at scale of 1: 100 for vertical while three longitudinal profiles along S.Warsamson were drawn at scale of 1: 10,000 for horizontal and 1: 200 for vertical. Total number of sheets are 7.

10.3. Personnel and Equipment

Personnels:

1. Rosikin

: Surveyor

2. Suwandi

: Surveyor

3. Suparmanto : Surveyor
4. Warsito : Surveyor
5. Widodo : Surveyor
6. Suyono : Surveyor

Equipments:

Total Station TOPCON : 1 unit
 Theodolite Wild T.0 : 4 unit
 Automatic level Wild NA.2 : 1 unit

CHAPTER 11 RIVER CROSS SECTION

11.1. General

Measurement of River cross section was carried out along S.Warsamson, confluence of S.Klasuwuk and S.Klasway.

Cross section were drawn at scale of 1:200 for horizontal and 1:100 for vertical.

11.2. River Cross Section

River cross section were carried out in 15 places of S.Warsamson and in every confluence of S.Klasaman, S.Klasawuk and S.Klasway.

Total 18 cross section were drawn in 15 sheets cross section map.

11.3. Personnel and Equipment

Personnels:

Rosikin : Warsito
 Suwandi : Widodo
 Suparmanto : Suyono

Equipments:

Total Station TOPCON : 1 unit
 Theodolite Wild T.0 : 4 units
 Automatic level Wild NA.2 : 1 unit

CHAPTER 12 TOPOGRAPHIC SURVEY

12.1. General

Topographic survey were carried out at the proposed main structure site. Topographic survey was measured for mapping at scale of 1:500 with 1 meter interval contour.

12.2. Topographic Survey

Topographic survey were carried out at water fall of S.Warsamson.

Secondary traverse for topographic survey were tied to Route I and Route II which consist of 43 loops. Minimum accuracy obtained in this work is 1/3,500.

Traverse network for topographic survey for map at scale of 1:500 are Route I and Route II. From the secondary traverse detail points were measured by tacheometric method. Total area which were mapped are 0.6 square km. 10 sheets of the maps were drawn at scale of 1:500.

12.3. Personnel and Equipment

Personnels:

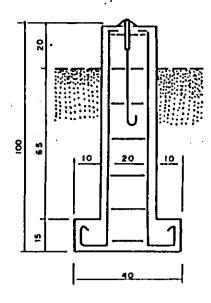
Rosikin : Surveyor
 Suwandi : Surveyor
 Suparmanto : Surveyor
 Warsito : Surveyor
 Widodo : Surveyor
 Surveyor
 Surveyor
 Surveyor

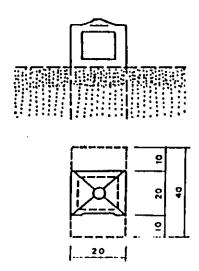
Equipments:

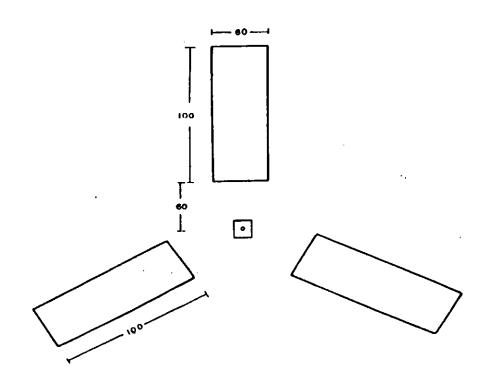
Total Station TOPCON : 1 unit
 Theodolite Wil T.0 : 4 units
 Automatic level Wild NA.2 : 1 unit

APPENDIX 2.1 TYPE AND SIZE OF MONUMENT

TYPE AND SIZE OF MONUMENT



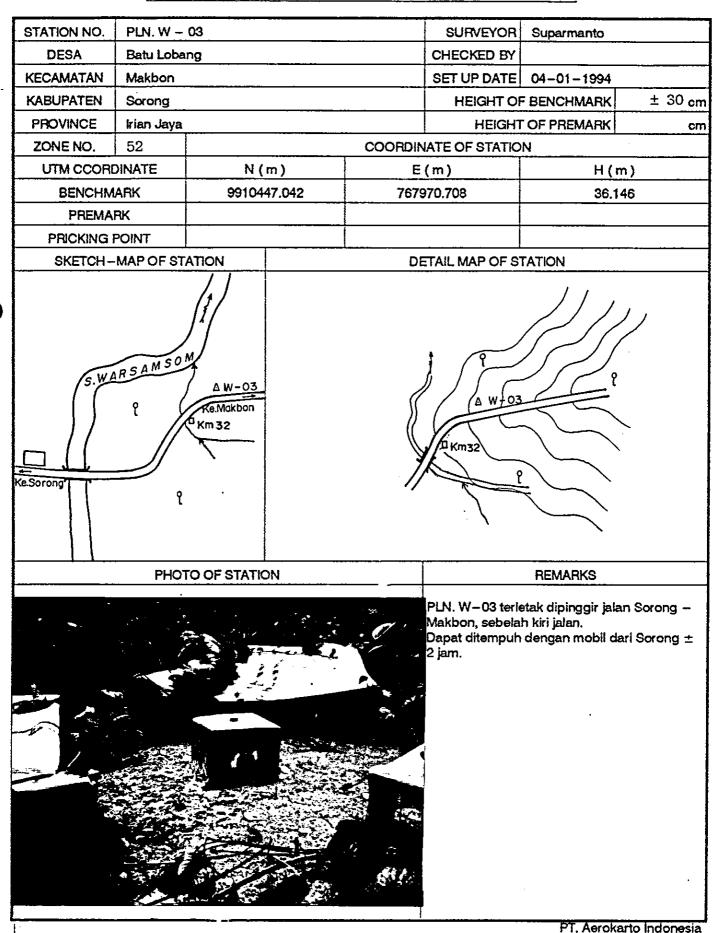


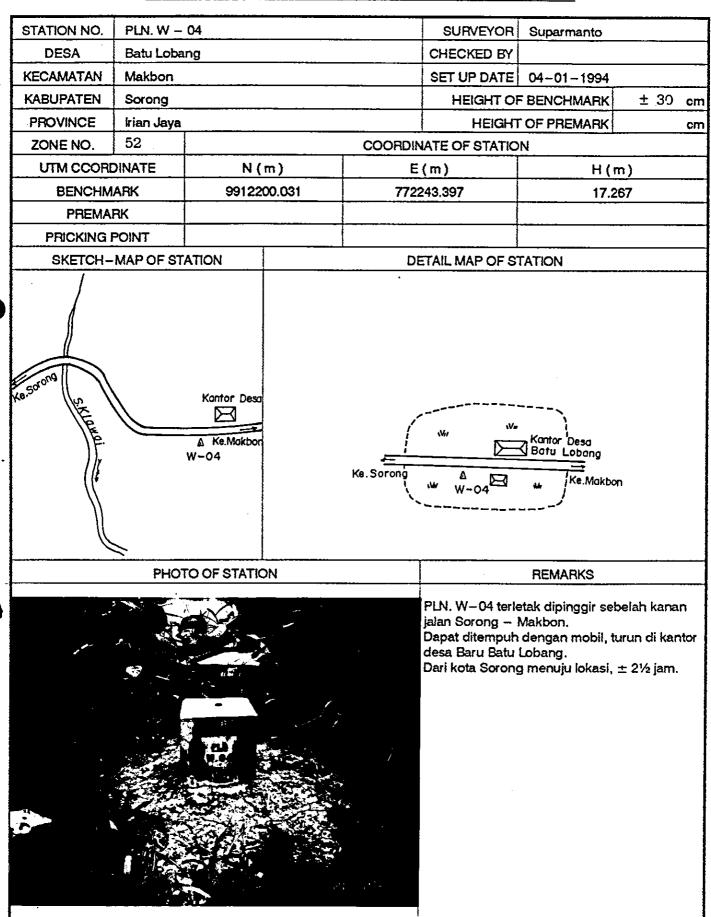


APPENDIX 2.2 DESCRIPTION OF BENCH MARK

| | 77.5 | CRIFIIO | N OF BEN | CH MAR | K AND PRE | MARK | | |
|-------------|------------|---------------------------------------|---------------------------------------|--|---|---|-------------------------|-----------|
| STATION NO. | PLN. W - | 01 | | | SURVEYOR | Cumanana | - | |
| DESA | Batu Loba | ang | | ## ### 6-#### ba | CHECKED BY | Suparmanto | | |
| KECAMATAN | Makbon | | | ······································ | SET UP DATE | OF 04 4004 | | |
| KABUPATEN | Sorong | | · · · · · · · · · · · · · · · · · · · | ************************************** | - | 05-01-1994 BENCHMARK | | |
| PROVINCE | Irian Jaya | | | | | | ± 30 | <u>cm</u> |
| ZONE NO. | 52 | | | COORDU | NATE OF STATIO | OF PREMARK | | cm |
| UTM CCORE | DINATE | N | (m) | | (m) | | · | |
| BENCHM | ARK | | 043.270 | | 493.337 | H (1 | m) | |
| PREMAI | RK | | | 700 | 100.007 | | | |
| PRICKING P | POINT | | | • | | - | · | |
| SKETCH- | MAP OF ST | ATION | <u> </u> | | ETAIL MAP OF ST | ATION | | |
| PANTAI MAL | P (.A. | | | 1 | A BT.MALAYUK W-OI | | | |
| | PHOT | O OF STATIC | N | | | REMARKS | | 寸 |
| | | S S S S S S S S S S S S S S S S S S S | | | PLN. W-01 terlet tempuh melalui la menuju ke pantal dilanjutkan jalan k menuju bukit Mala | ut, dari desa Ba Malaguk naik po aki mengikuti la | tu Lobang erabu ±% k | |
| | | | | ' 94 | | | | |

| - | DES | CRIPTIO | N OF REV | CH MAR | K AND PRE | MARK | |
|-------------|---------------|--------------|------------|-----------------|---------------------------------------|--|----------------------------------|
| STATION NO. | PLN. W - | 02 | | | SURVEYOR | Suparmanto | |
| DESA | Batu Loba | ıng | | | CHECKED BY | | |
| KECAMATAN | Makbon | | | | SET UP DATE | 05-01-1994 | |
| KABUPATEN | Sorong | | | | | BENCHMARK | ± 30 cm |
| PROVINCE | Irian Jaya | | | | HEIGHT | OF PREMARK | cm |
| ZONE NO. | 52 | | | COORDIN | ATE OF STATIO | | |
| UTM CCORE | DINATE | N (| m) | E | (m) | H (; | m) |
| BENCHM | ARK | 99129 | 29.911 | 769 | 126.261 | | • |
| PREMA | RK | | | | | | |
| PRICKING I | POINT | | | | | | |
| | MAP OF ST | ATION | | DI | ETAIL MAP OF ST | TATION | ··· |
| 4 | AUT | | | | | | |
| | | Lobang | | , | | • | |
| | MP. BOTO | Lobelia — | • | | , | | |
| 7 | 7 | | | | / | | |
| | | | | _ | 1 | | |
| | 3)//(| | | . ((| * | | |
| 11 (19) | ///// | () ? | j | የ) } | | | |
| (((Aw-oz | | 1 | | // | (M ((/ - | | |
| 17) 1 (1,0) | | | | | \ \a\w\oz \ | | |
| | //// | 0 | · |) / | (1) (1) | | |
| | $\overline{}$ | | | | | | |
| P + | | | | ۲) | | | |
| | | | | | <i>'</i> | | |
| | PHO | TO OF STATIC | NC | | | REMARKS | |
| | | | | | DINI W. CO tools | | |
| | | | | | PLN. W-02 terle setapak antara p | rtak diatas bukit (rovek pembibita | dipinggir jalan in coklat ke- |
| | | | | | arah desa Batu l | .obang. 🙏 🗀 | |
| | | | | | PLN. W-02 dap ngikuti jalan Sore | at ditempuh den ang Makhon I | gan mobil me- berbenti di |
| | | A Company of | | | proyek pembibita | an coklat lalu bei | rjalan kaki me- |
| | W. | 1 Land | N. Carrie | Service Control | ngikuti jalan seta Dari pembibitan | pak. | • |
| | | 100 | | | Deal bempipitalt | CORIEL, ± 1 72 Jan | 1. |
| | | W 02 | | * | | | |
| | | | | F., | | | |
| 3 | | A A T | 7 8 | 3 | | 4 | |
| | | | | | | , , ,, | |
| | 3 | | | | | i : | |
| | 1 | | 100 mg | | | : | |
| | | | | | | • | |
| | SAN EL | | | | | | 1 |



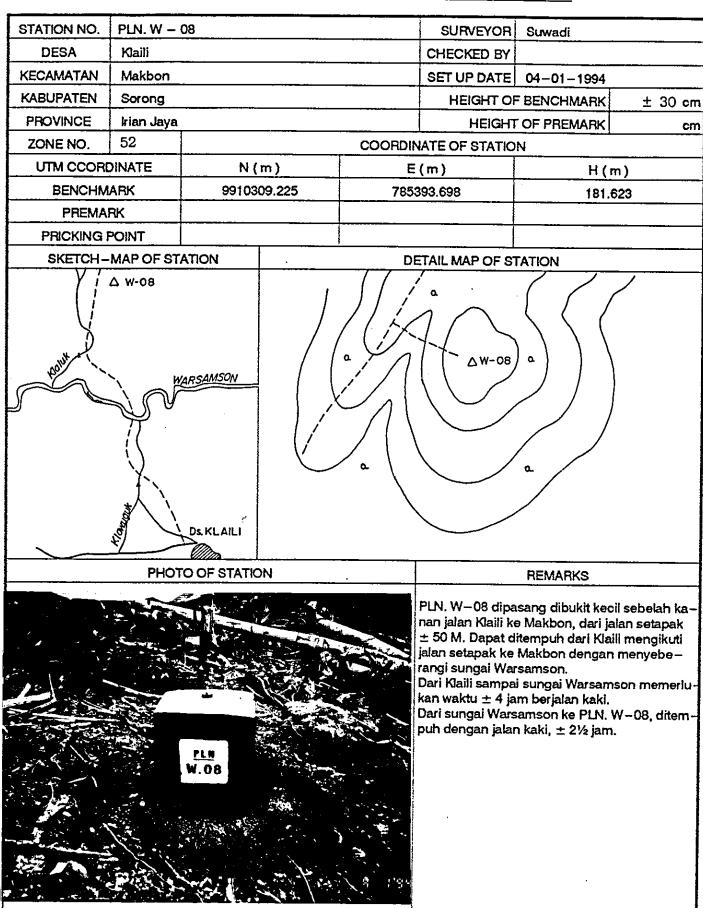


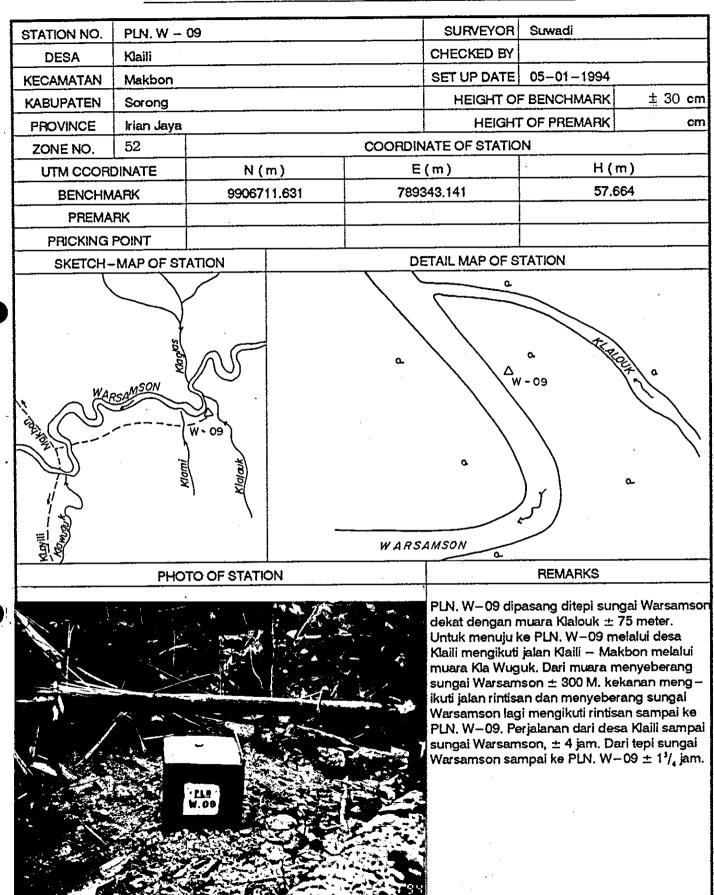
| | <u>===</u> | <u> </u> | <u></u> | <u> </u> | AND IND | 2,12,11111 | |
|-----------------|-------------|-----------------------|----------|-----------------|---------------------------------------|--|--------------------------------|
| STATION NO | D. PLN. W - | 05 | | | SURVEYOR | Widodo | |
| DESA | Malanu, D | ukuh Malanu | | | CHECKED BY | | |
| KECAMATA | N Sorong | | | | SET UP DATE | 08-01-1994 | |
| KABUPATE | Sorong | · | · | | HEIGHT OF | BENCHMARK | ± 30 cm |
| PROVINCE | Irian Jaya | | | | HEIGHT | OF PREMARK | cm |
| ZONE NO. | 52 | | | COORDIN | DINATE OF STATION | | |
| ОТМ СС О | ORDINATE | N(| m) | Ε | (m) | H (r | n) |
| BENC | HMARK | 99069 | 20.231 | 7596 | 52.299 | | |
| PRE | MARK | | | | | | |
| PRICKIN | IG POINT | | | | | | |
| SKETC | H-MAP OF ST | ATION | | DE | TAIL MAP OF S | TATION | |
| W-05A | S.KIOWU | Rolam Suaya Ke.Makbor | Si Re Pl | 05 ^A | | | |
| | PHO* | TO OF STATIC | N | | · · · · · · · · · · · · · · · · · · · | REMARKS | |
| | | 50 | | | 20 M. Dapat dite jalan Menuri me | asang dimuara si empuh dengan m nuju Kolam Buay kaki melalui jala | obil melalui a, dilanjutkan |

| | DES | CRIPTION | OF BEN | ICH MARI | K AND PRE | MARK | |
|-------------|------------|-------------|--------|---------------|---|--|-------------|
| STATION NO. | PLN. W - | 06 | | | SURVEYOR | Suparmanto | |
| DESA | Malanu | | | | CHECKED BY | | |
| KECAMATAN | Sorong | | ····· | | SET UP DATE | 04-01-1994 | |
| KABUPATEN | Sorong | | | | HEIGHT OF | BENCHMARK | ± 30 cm |
| PROVINCE | Irian Jaya | | | | HEIGHT OF PREMARK | | |
| ZONE NO. | 52 | | | COORDIN | IATE OF STATIO | N | |
| UTM CCORE | DINATE | N (| m) | E | (m) | H (r | n) |
| BENCHM | ARK | 99046 | 33.617 | 7635 | 47.284 | 95.4 | 78 |
| PREMA | RK | | | | | | |
| PRICKING I | POINT | | | | | | |
| SKETCH- | MAP OF ST | ATION | DE | TAIL MAP OF S | TATION | | |
| 2 AW | -06 | MAKBON | | Somonos (| 2 A W O O O O O O O O O | P | |
| | PHO | TO OF STATI | NC | | | REMARKS | |
| | | | | | Makbon, disebe | etak dipinggir jala lah kanan jalan k an mobil dari kota | ím. , dapat |

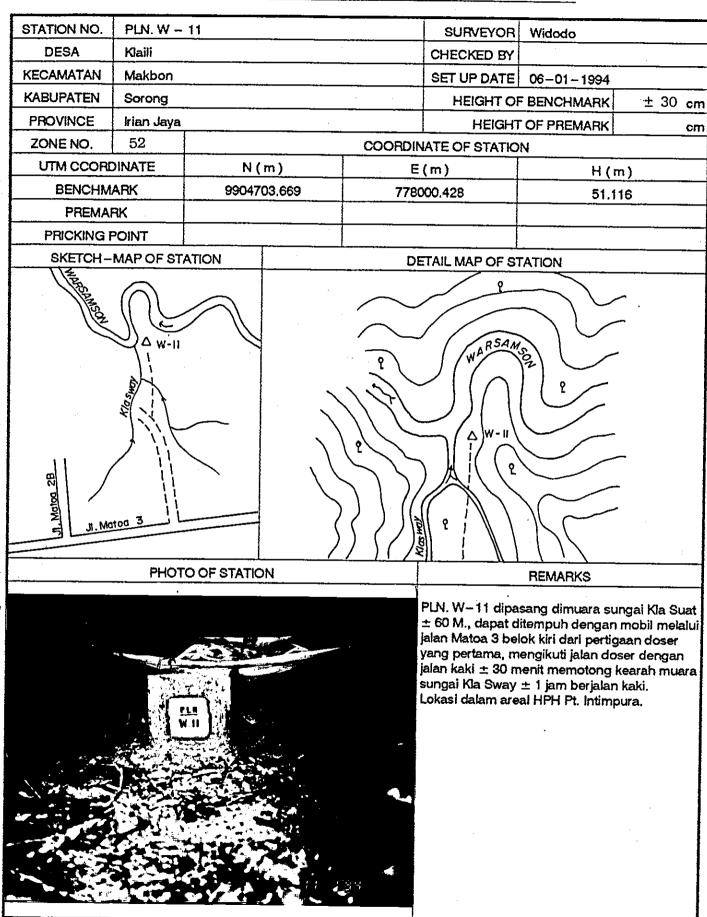


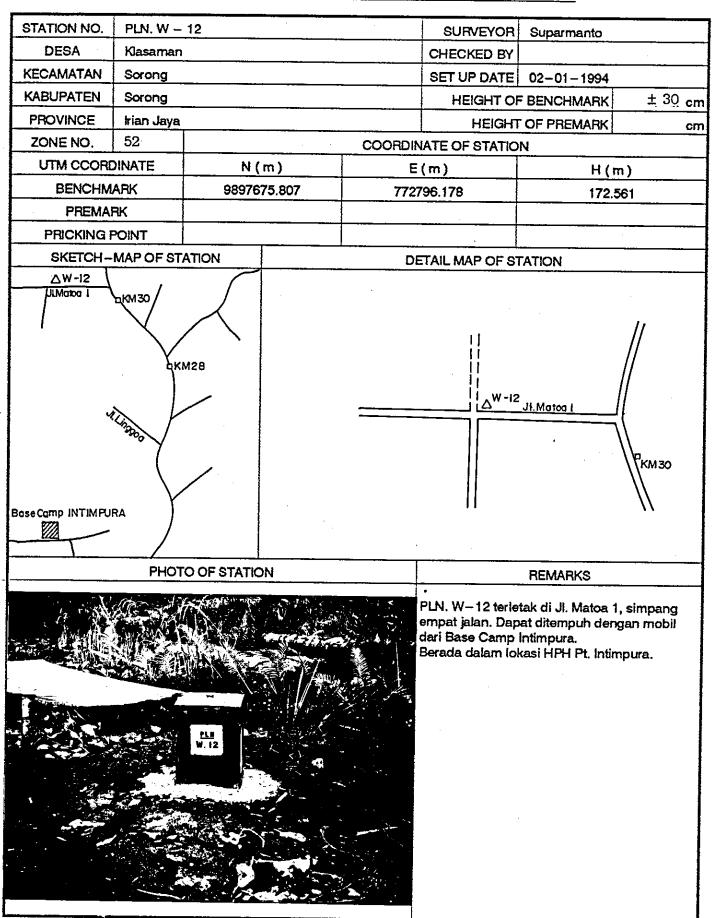
| | DES | CRIPTIO | N OF BEN | CH MAR | K AND PRE | <u>MARK</u> | |
|-------------------|----------------|---------------|------------|---------|--|--|----------------------------|
| STATION NO. | PLN. W - | 07 | | | SURVEYOR | Widodo | |
| DESA | Batu Loba | ing, Dukuh Ba | atu Lobang | | CHECKED BY | | |
| KECAMATAN | Makbon | | | | SET UP DATE | 07-01-1994 | |
| KABUPATEN | Sorong | | | · | HEIGHT OF | BENCHMARK | ± 30 cm |
| PROVINCE | Irian Jaya | | | | | OF PREMARK | cm |
| ZONE NO. | 52 | | | COORDIN | ATE OF STATIO | · | |
| UTM CCORE | DINATE | N (| m) | Ε | (m) | Н(| m) |
| BENCHM | ARK | 99063 | 99.900 | 7695 | 50.663 | | |
| PREMAI | RK | | | | | | |
| PRICKING F | PRICKING POINT | | | | | | |
| SKETCH- | MAP OF ST | ATION | | DE | TAIL MAP OF ST | TATION | |
| rassaman rassaman | W-07 | | | 5 | ₹ | | 2 |
| ļ | PHOT | O OF STATIC | N | | | REMARKS | |
| | | | | | PLN. W-07 dipa ± 30 M. Dapat di alan Sorong - N Berhenti di jemba nasuk kekanan r am. | tempuh dengan Makbon. atan Warsamson | mobil melalui . ± 200 M |





| PROVINCE Iring lava | | , | | | | 7 | | |
|--|-------------|------------|-------------|--------|---------|---|---|--|
| KECAMATAN Sorong KABUPATEN Sorong KABUPATEN Sorong HEIGHT OF BENCHMARK ± 30 or HEIGHT OF PREMARK PROVINCE Irian Jaya HEIGHT OF PREMARK CONDINATE N (m) | STATION NO. | PLN. W - | 10 | | | SURVEYOR | Suparmanto | |
| KABUPATEN Sorong HEIGHT OF BENCHMARK ± 30 or PROVINCE Irian Jeya HEIGHT OF PREMARK or ZONE NO. 52 COOPDINATE OF STATION UTM CCOODINATE N (m) E (m) H (m) BENCHMARK 9898037.920 766537.491 77.033 PREMARK PRICKING POINT SKETCH - MAP OF STATION DETAIL MAP OF STATION DETAIL MAP OF STATION PHOTO OF | DESA | Klasaman | • | | | CHECKED BY | | |
| PROVINCE kitan Jaya HEIGHT OF PREMARK of ZONE NO. 52 COORDINATE OF STATION UTM CCORDINATE N (m) E (m) H (m) BENCHMARK 9898037.920 768537.491 77.033 PREMARK PROKING POINT SKETCH-MAP OF STATION DETAIL MAP OF STATION DETAIL MAP OF STATION PHOTO OF STATION REMARKS PLN. W-10 terietak disimpang tiga jalan, deka jembatan besi, dapat difempuh dengan mobil mengikuti jalan Pertamina masuk dari Km. 18 jalan raya Scorog - Klamoro, belok kekiri mengikuti jalan PT. Intimpura ± 7 Km. | KECAMATAN | Sorong | | | | SET UP DATE | 31-12-1993 | |
| ZONE NO. 52 COOFDINATE OF STATION UTM CCORDINATE N (m) E (m) H (m) BENCHMARK 9898037.920 766537.491 77.033 PREMARK PRICKING POINT SKETCH—MAP OF STATION DETAIL MAP OF STATION Bose Comp BYTIM PURA PHOTO OF STATION PHOTO OF STATION PHOTO OF STATION REMARKS PLN. W—10 terletak disimpang tiga jalan, deka jembatan besi, dapat ditempuh dengan mobil mengikuti jalan Pertamina masuk dari Km. 18 alan raya Sorong— Klamono, belok kekiri mengikuti jalan PyT, intimpura ± 7 Km. | KABUPATEN | Sorong | | | _ | HEIGHT O | BENCHMARK | ± 30 cm |
| TONE NO. 52 UTM CCORDINATE N (m) E (m) H (m) BENCHMARK 9898037.920 766537,491 77.033 PREMARK PRICKING POINT SKETCH—MAP OF STATION DETAIL MAP OF STATION RITIM PURA PHOTO OF STATION PHOTO OF STATION PHOTO OF STATION REMARKS PLN. W—10 terletak disimpang tiga jalan, deka jembatan besi, dapat dilempuh dengan mobil mengikuti jalan Pertamina masuk dari Km. 18 jalan raya Sorong — Klamono, belok kekiri mengikuti jalan PT, intimpura ± 7 Km. | PROVINCE | Irian Jaya | | | - | HEIGHT | OF PREMARK | cm |
| BENCHMARK PRICKING POINT SKETCH—MAP OF STATION Briss Comp BYTM PURA PHOTO OF STATION PHOTO OF STATION PHOTO OF STATION PHOTO OF STATION PLN. W—10 terletak disimpang tiga jalan, deka jembatan besi, dapat ditempuh dengan mobil mengikuti jalan Pertamina mala | ZONE NO. | 52 | | | COORDIN | ATE OF STATIO | N | |
| PRICKING POINT SKETCH—MAP OF STATION Base Comp RITIM PLEA PHOTO OF STATION PHOTO OF STATION PHOTO OF STATION PLANCES PLN. W—10 terletak disimpang tiga jalan, deka jembatan besi, dapat ditempuh dengan mobil mengikuti jalan Pertamina masuk dari Km. 18 jalan raya Sorong — Klamono, belok kekiri mengikuti jalan PT. Intimpura ± 7 Km. | UTM CCORE | DINATE | Ν(| m) | E | (m) | H (1 | m) |
| PRICKING POINT SKETCH-MAP OF STATION DETAIL MAP OF STATION REMARKS PHOTO OF STATION PHOTO OF STATION PHOTO OF STATION REMARKS PLN. W-10 terletak disimpang tiga jalan, deka jembatan besi, dapat ditempuh dengan mobil mengikuti jalan Pertamina masuk dari Km. 18 jalan raya Sorong - Klamon, belok kekiri mengikuti jalan PT. Intimpura ± 7 Km. | BENCHM | ARK | 98980 | 37.920 | 7665 | 537.491 | | - |
| SKETCH-MAP OF STATION Base Comp INTIM PURA PHOTO OF STATION PHOTO OF STATION PHOTO OF STATION REMARKS PLN. W-10 terletak disimpang tiga jalan, deka jembatan besi, dapat ditempuh dengan mobil mengikuti jalan Pertamina masuk dari Km. 18 jalan raya Sorong - Klamono, belok kekiri mengikuti jalan PT. Intimpura ± 7 km. | PREMA | RK | | | - | į | | |
| Base Comp RITIM FURA PHOTO OF STATION PLN. W-10 terletak disimpang tiga jalan, deka jembatan besi, dapat ditempuh dengan mobil mengikuti jalan Pertamina masuk dari Km. 18 jalan raya Sorong – Klamoro, belok kekiri mengikuti jalan PT. Intimpura ± 7 Km. | PRICKING I | POINT | | | | | | ··· |
| Base Comp BITIM PUPA PHOTO OF STATION PLN. W-10 terletak disimpang tiga jalan, deka jembatan besi, dapat ditempuh dengan mobil mengikuti jalan Pertamina masuk dari Km. 18 jalan raya Sorong – Klamono, belok kekiri mengikuti jalan PT. Intimpura ± 7 Km. | SKETCH- | MAP OF ST | ATION | | DE | TAIL MAP OF S | ration . | |
| PLN. W—10 terletak disimpang tiga jalan, deka jembatan besi, dapat ditempuh dengan mobil mengikuti jalan Pertamina masuk dari Km. 18 jalan raya Sorong — Klamono, belok kekiri mengikuti jalan PT. Intimpura ± 7 Km. | SORONG | KM IS | INTIM PURA | | | | AMAN TO THE STATE OF THE STATE | |
| jembatan besi, dapat ditempuh dengan mobil mengikuti jalan Pertamina masuk dari Km. 18 jalan raya Sorong — Klamono, belok kekiri mengikuti jalan PT. Intimpura ± 7 Km. | | PHOT | O OF STATIC | ON | | | REMARKS | |
| PT. Aerokarto Indonesia | | | | | _ | jembatan besi, d mengikuti jalan f jalan raya Soron | apat ditempuh d Pertamina masuk g – Klamono, be | engan mobil dari Km. 18 lok kekiri me- |
| | | | | | | | PT. Aeroka | rto Indonesia |

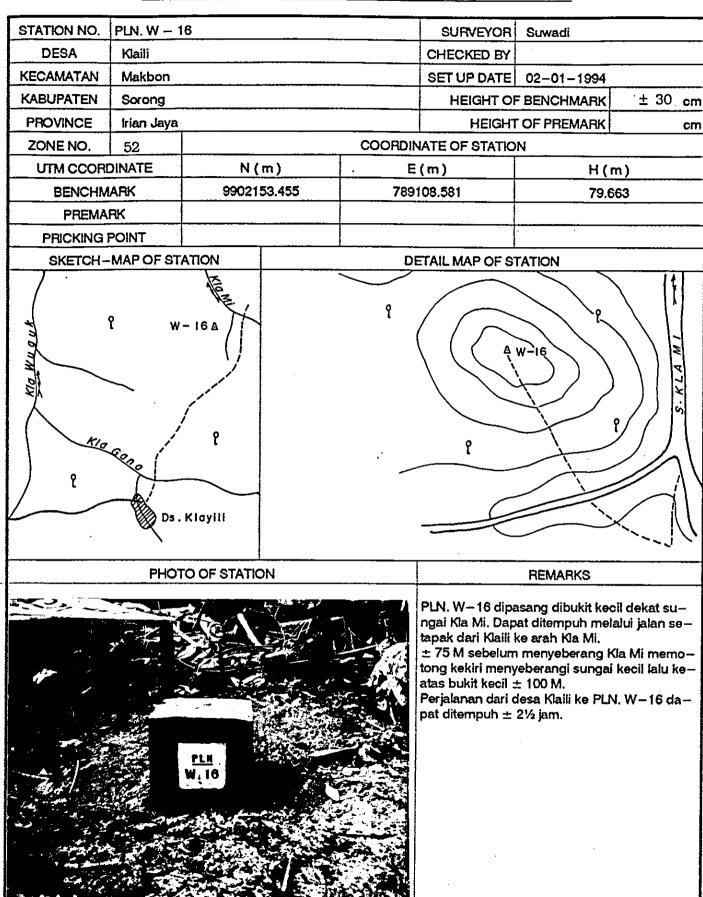




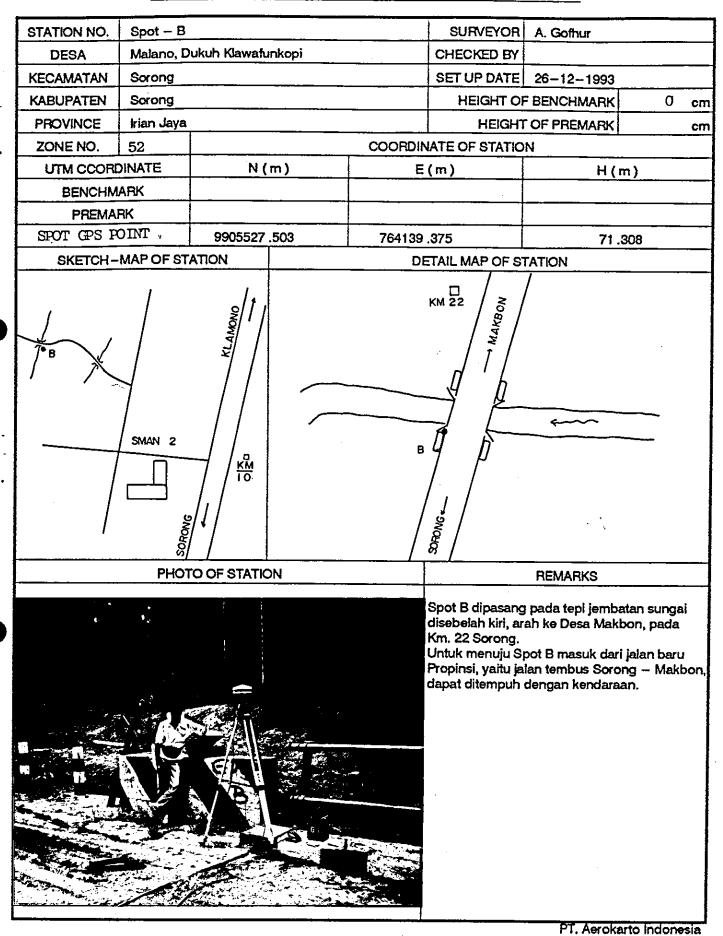
| | | | | | 021 1111111 | KANDIKE | MAKK | | |
|---|--------------|------------|------------------|--------|-------------|---|--|-------------------------------------|-----|
| | STATION NO. | PLN. W - | 13 | | | SURVEYOR | Suparmanto | | |
| | DESA | Klasaman | | | | CHECKED BY | | | |
| | KECAMATAN | Sorong | | | | SET UP DATE | 31-12-1993 | | |
| | KABUPATEN | Sorong | | | | | BENCHMARK | ± 30 | cm. |
| | PROVINCE | Irian Jaya | | | - | | OF PREMARK | | cm |
| | ZONE NO. | 52 | | | COORDIN | ATE OF STATIO | | | |
| | UTM CCORE | INATE | N (| m) | Е | (m) | H (1 | m) | |
| | BENCHM | ARK | 98945 | 86.301 | | 82.409 | 93.4 | | |
| 1 | PREMAI | ₹K | | | | | | | |
| | PRICKING F | POINT | | | | | • | | |
| | SKETCH- | MAP OF ST | ATION | | DE | TAIL MAP OF ST | TATION | | |
| | SOFONG KM 18 | PHOT | KLAMONO KLAMONO | | Pos Jaga | OPERASI OPERASI OW-13 Tohr KANTOR INT | IM PURA | | |
| | | PHOT | O OF STATIC | | | PLN. W—13 terle didalam taman d Dapat ditempuh aya Sorong — K kiri mengikuti jala | isamping Kopera dengan mobil m lamono, pada Kr | asi. elalul jalan m. 18 belol | |

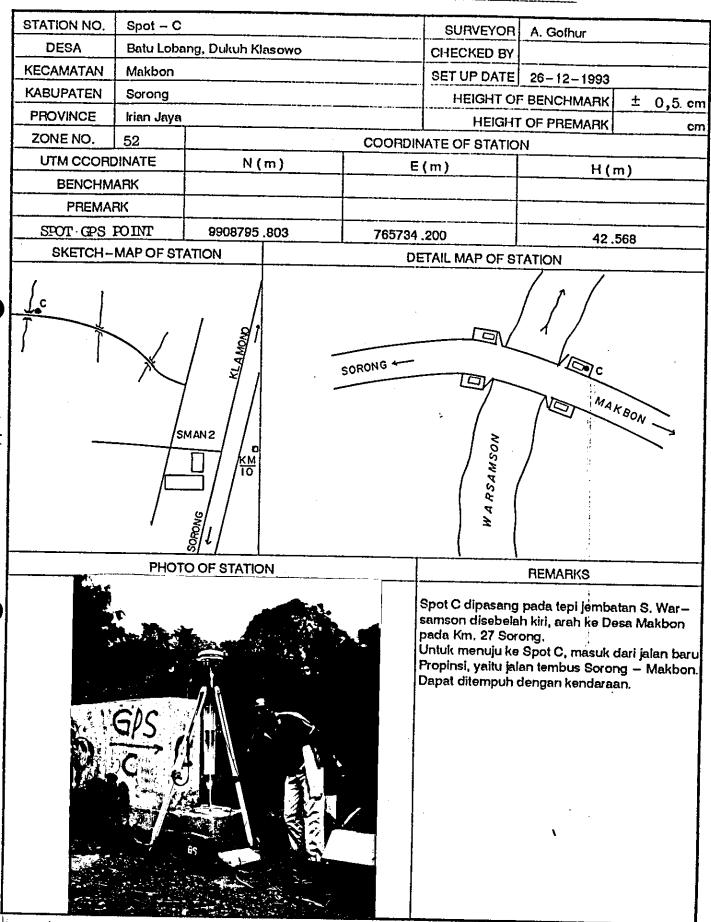
| | | <u>DD0</u> | | | | K MIND I KE | | |
|---|-------------|------------|-------------|--|---------|--|---|------------------------------|
| | STATION NO. | PLN. W - | 14 | | | SURVEYOR | Suparmanto | |
| | DESA | Aimas | | | | CHECKED BY | | |
| - | KECAMATAN | Sorong | | | | SET UP DATE | 31-12-1993 | |
| | KABUPATEN | Sorong | ····· | | | HEIGHT O | BENCHMARK | ± 30. cm |
| | PROVINCE | Irian Jaya | | | | HEIGHT | OF PREMARK | cm |
| | ZONE NO. | 52 | | | COORDIN | NATE OF STATIO | N | |
| | UTM CCORE | DINATE | N(| m) | E | (m) | H (r | n) |
| | BENCHM | ARK | 98959 | 29.122 | 776 | 898.104 | 176.4 | 149 |
| | PREMAI | RK | | | | | | |
| | PRICKING F | POINT | | | | | | |
| | SKETCH- | MAP OF ST | ATION | | D | ETAIL MAP OF S | TATION | |
| | Bose Camp | OKM 2 | | | | KM 30 | W -14 | |
| | | PHOT | O OF STATIC | N | | | REMARKS | |
| | | | | The same of the sa | | PLN. W-14 terle kawasan HPH P Dapat ditempuh Intimpura ± 10 h ke kampung Kla Lokasi dalam are jam dari Sorong. | t. Intimpura. dengan mobil da (m. kearah jalan j ili. eal HPH Pt. Intim | ari Base Camp yang menuju |

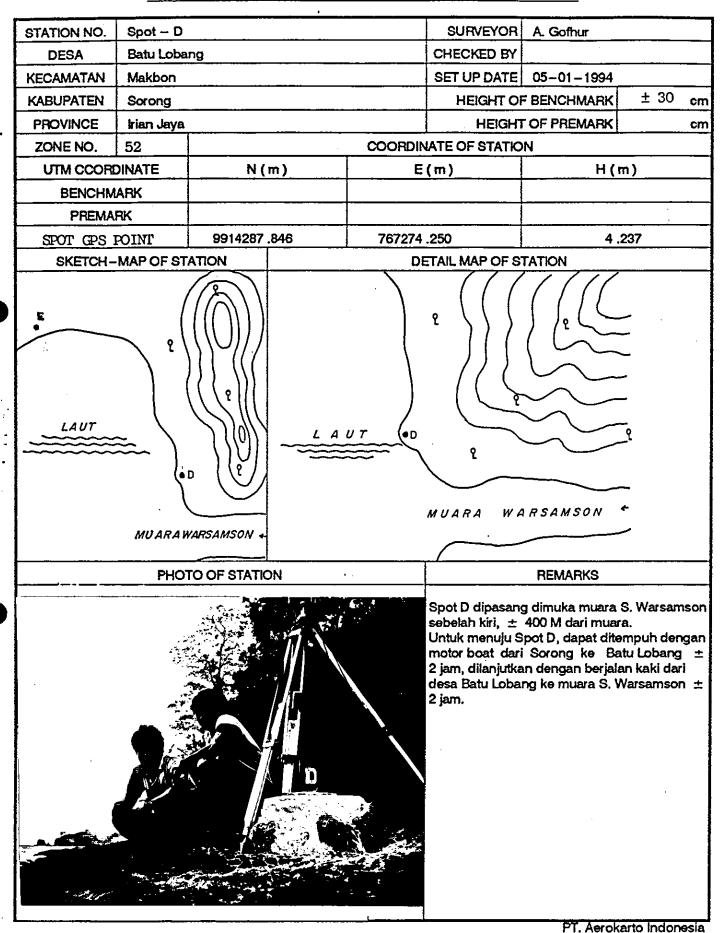
| STATION NO. PLN. W – 15 DESA Kalii CHECKED BY KECAMATAN Makbon SET UP DATE AND 12-1994 KABUPATEN SCYONG HEIGHT OF BENCHMARK TOF PREMARK PROVINCE I in Jaya HEIGHT OF PREMARK COORDINATE OF STATION E(m) H(m) BENCHMARK PRICKING POINT SKETCH—MAP OF STATION DETAIL MAP OF STATION PHOTO OF STATION REMARKS PILI W—15 dipasarg ditepi surgal Kia Gon dari tepi surgal Kia Gon at 300 M memotong kiri menuju bukit kecil. Perjalanan dari desa Kialil ± 45 menit. | | <u>510</u> | CKII IIO | OF DEN | CH MAK | KANDERE | MARK | | |
|--|-------------|------------|-------------|------------|---------|---|--|---|--------------------|
| KECAMATAN Makbon SET UP DATE 30-12-1994 KABUPATEN Sorong HEIGHT OF BENCHMARK ± 3C PROVINCE Irian Jaya HEIGHT OF PREMARK ZONE NO. 52 COORDINATE OF STATION UTM CCORDINATE N (m) E (m) H (m) BENCHMARK 9999402.073 786301.245 128.533 PREMARK PRICKING POINT SKETCH-MAP OF STATION DETAIL MAP OF STATION PHOTO OF STATION PHOTO OF STATION PLN. W-15 dipasarag ditepi sungai Kia Gon dari tepi sungai ± 50 M. Dapat ditempuh dengan mobil melewati jala HPH Pt. Intimpura, menuju desa Klaili. Dari desa Klaili, dana stapak mernyeberang sungai Kia Gona Dari sungai Kia Gona ± 300 M memotorg ki kiri menuju bukit kecil. Perjalanan dari desa Klaili. Perjalanan dari desa Klaili. Perjalanan dari desa Klaili. | STATION NO. | PLN. W - | 15 | • | | SURVEYOR | Suwadi | | |
| KABUPATEN Sorong HEIGHT OF BENCHMARK ± 30. PROVINCE Irian Jaya HEIGHT OF PREMARK ZONE NO. 52 COORDINATE OF STATION UTM CCORDINATE N (m) E (m) H (m) BENCHMARK 9898402.073 786301.245 128.533 PREMARK PRICKING POINT SKETCH—MAP OF STATION DETAIL MAP OF STATION PHOTO OF STATION PHOTO OF STATION PLN. W-15 dipasang ditepi sungai Kla Gondari tepi sungai ± 50 M. Dapat ditempuh dengan mobil melewati jala HPH Pt. Intimpura, menuju desa Klaiti. Dari desa Klaiti, diujung sekolah 5D mengiki, alan satapak menyeberang sungai Kla Gondari sungai kla Gona ± 300 M memotong ke kiri menuju bukit kecil. Perjalanan dari desa Klaiti. Perjalanan dari desa Klaiti. | DESA | Klaili | | | | CHECKED BY | | | |
| PROVINCE Irian Jaya HEIGHT OF PREMARK ZONE NO. 52 CCORDINATE OF STATION UTM CCORDINATE N (m) E (m) H (m) BENCHMARK 9898402.073 786301.245 128.533 PREMARK PRICKING POINT SKETCH—MAP OF STATION DETAIL MAP OF STATION PHOTO OF STATION PHOTO OF STATION REMARKS PLN. W-15 dipasang ditepi sungai Kla Gondari tepi sungai ± 50 M. Dapat ditempuh dengan mobil melewati jala HPH Pt. Infimpura, menuju desa Klaiti. Dari desa Klaiti. Perjalanan dari desa Klaiti. | KECAMATAN | Makbon | | | | SET UP DATE | 30-12-1994 | | |
| PROVINCE Irian Jaya HEIGHT OF PREMARK ZONE NO. 52 COORDINATE OF STATION UTM CCORDINATE N (m) E (m) H (m) BENCHMARK 9899402.073 786301.245 128.533 PREMARK PRICKING POINT SKETCH-MAP OF STATION DETAIL MAP OF STATION PHOTO OF STATION PHOTO OF STATION REMARKS PLN. W-15 dipasang ditepi sungai Kla Gon dari tepi sungai ± 50 M. Dapat ditempuh dengan mobil melewati jala HPH Pt. Intimpura, menuju desa Klaili. Dari desa Klaili. dijung sekolah 50 mengiku jalan setapak menyeberang sungai Kla Gon Dari sungai Kla Gon 2 300 M memotong kiri menuju bukit kecil. Perjalanan dari desa Klaili ± 45 menit. | KABUPATEN | Sorong | | | | HEIGHT OF | BENCHMARK | ± 3 | 30 cm |
| UTM CCORDINATE N (m) E (m) H (m) BENCHMARK 9898402.073 786301.245 128.533 PREMARK PRICKING POINT SKETCH—MAP OF STATION DETAIL MAP OF STATION DETAIL MAP OF STATION PHOTO OF STATION PEMARKS PUN. W-15 dipasang ditepi sungai Kla Gon dari tepi sungai belawati jala HPH Pt. Intimpura, menuju desa Klaili. Dari desa Klaili, dilujung sekolah SD mengiku jalan setapal ka Gona ± 300 M memotong ke kiri menuju bukit kecil. Perjalanan dari desa Klaili ± 45 menit. | PROVINCE | Irian Jaya | | | | HEIGHT | OF PREMARK | | cm |
| BENCHMARK PRICKING POINT SKETCH-MAP OF STATION DETAIL MAP OF STATION DETAIL MAP OF STATION PHOTO OF STATION PHOTO OF STATION PEMARKS PUN. W-15 dipasang ditepi sungai Kia Gon dari tepi sungai kia Gon dari tepi sungai ± 50 M. Dapat ditempuh dengan mebil melewati jala HPH Pt. Intimpura, menuju desa Klaili. Dari desa Klaili, dilujung sekolah SD mengikt jalan setapak menyeberang sungai Kia Gona ± 300 M memotong ki kiri menuju bukit kecil. Perjalanan dari desa Klaili ± 45 menit. | ZONE NO. | 52 | | | COORDIN | NATE OF STATIO | N | | |
| PREMARK PRICKING POINT SKETCH-MAP OF STATION DETAIL MAP OF STATION PHOTO OF STATION PLN. W-15 dipasang ditepi sungai Kia Gondari tepi sungai ± 50 M. Dapat ditempuh dengan mobil melewati jala HPH Pt. Intimpura, menuju desa Klaili. Dari desa Klaili, diujung sekolah SD mengiku jala sungai kia Gona ± 300 M memotong ki kiri menuju bukit kecil. Perjalanan dari desa Klaili ± 45 menit. | UTM CCOR | DINATE | N (| m) | Е | (m) | Н(| m) | |
| PRICKING POINT SKETCH-MAP OF STATION DETAIL MAP OF STATION PHOTO OF STATION PHOTO OF STATION PLN. W-15 dipasang ditepi sungai Kla Gondari tepi sungai ± 50 M. Dapat ditempuh dengan mobil melewati jala HPH Pt. Intimpura, manuju desa Klaili. Dari desa Klaili, diujung sekolah SD mengika jalan setapak menyeberang sungai Kla Gona bari sungai Kla Gona ± 300 M memotong kakiri menuju bukit kecil. Perjalanan dari desa Klaili ± 45 menit. | BENCHM | ARK | 98984 | 02.073 | 786 | 301.245 | | | |
| PHOTO OF STATION PHOTO OF STATION PLN. W-15 dipasang ditepi sungai Kla Gondari tepi sungai E5 M. Dapat ditempuh dengan mobil melewati jala HPH Pt. Intimpura, menuju desa Klaili. Dari desa Klaili, diujung sekolah SD mengik jalan setapak menyeberang sungai Kla Gonz Dari sungai Kla Gonz dari sungai Kla Gonz desa Klaili, diujung sekolah SD mengik jalan setapat menyeberang sungai Kla Gonz dari sungai Kla Gonz dari sungai Kla Gonz dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari desa Klaili diujung sekolah SD mengik jalan setapat dari dari desa Klaili diujung sekolah SD mengik jalan setapat dari dari desa Klaili dari dari desa Klaili dari dari desa Klaili dari dari desa Klaili diujung sekolah SD mengik jalan setapat dari dari desa Klaili dari dari desa Klaili dari dari desa Klaili dari dari dari desa Klaili dari dari dari desa Klaili dari dari dari dari dari desa Klaili dari dari dari dari dari dari dari dar | PREMA | RK | | | | | | | |
| PHOTO OF STATION REMARKS PLN. W-15 dipasang ditepi sungai Kia Gondari tepi sungai ± 50 M. Dapat ditempuh dengan mobil melewati jala HPH Pt. Intimpura, menuju desa Kiaili. Dari desa Kiaili, diujung sekolah SD mengiki jalan setapak menyeberang sungai Kia Gonz Dari sungai Kia Gonz ± 300 M memotong kikir menuju bukit kecil. Perjalanan dari desa Kiaili ± 45 menit. | PRICKING I | POINT | | : | | | | · - · · · · · · · · · · · · · · · · · · | |
| PHOTO OF STATION REMARKS PLN, W-15 dipasang ditepi sungai Kla Gondari tepi sungai ± 50 M. Dapat ditempuh dengan mobil melewati jalah HPH Pt. Intimpura, menuju desa Klaili. Dari desa Klaili, diujung sekolah SD mengiki jalan setapak menyeberang sungai Kla Gondari sungai kla Gond | SKETCH- | MAP OF ST | ATION | | Dŧ | TAIL MAP OF ST | FATION | | |
| PLN. W-15 dipasang ditepi sungai Kla Gondari tepi sungai ± 50 M. Dapat ditempuh dengan mobil melewati jalah HPH Pt. Intimpura, menuju desa Klaili. Dari desa Klaili, diujung sekolah SD mengiku jalan setapak menyeberang sungai Kla Gona Dari sungal Kla Gona ± 300 M memotong kekiri menuju bukit kecil. Perjalanan dari desa Klaili ± 45 menit. | | 10 60 na | V-15 A | | | Δ W- | 2 | K L A G A N | |
| PLN. W-15 dipasang ditepi sungai Kla Gondari tepi sungai ± 50 M. Dapat ditempuh dengan mobil melewati jalah HPH Pt. Intimpura, menuju desa Klaili. Dari desa Klaili, diujung sekolah SD mengikti jalan setapak menyeberang sungai Kla Gond Dari sungai Kla Gondari desa Klaili ± 45 menit. | | PHOT | O OF STATIC | ON REMARKS | | | | | |
| 3 1/8: | | | P. II | | | dari tepi sungai : Dapat ditempuh HPH Pt. Intimpur Dari desa Klaili, o jalan setapak me Dari sungai Kla G kiri menuju bukit | sang ditepi sung ± 50 M. dengan mobil m a, menuju desa liujung sekolah t nyeberang sung iona ± 300 M m kecil. | elewati jal Klaili. SD mengil jai Kla Goi emotong l | lan kuti na. |



| , | | | | | CII IIIII | K AND PRE | MARK | | |
|---|---|------------|--------------|--------|---------------------------------------|--|--|--------------------------------|----|
| | STATION NO. | Spot - A | | | | SURVEYOR | A. Gofhur | | |
| | DESA | Malano, D | ukuh Klawasu | ınkopi | | CHECKED BY | was sell | | |
| | KECAMATAN | Sorong | | | | SET UP DATE | 26-12-1993 | | |
| | KABUPATEN | Sorong | | | | | BENCHMARK | 0 | cm |
| | PROVINCE | Irian Jaya | | | · · · · · · · · · · · · · · · · · · · | | OF PREMARK | | |
| | ZONE NO. | 52 | | | COORDII | NATE OF STATIO | | | cm |
| | UTM CCORD | INATE | N (| m) | | (m) | H (r | n) | |
| | BENCHM | ARK | | | | | 11(1 | ··/ | |
| | PREMARK SPOT GPS POINT 9903770 590 7622 | | | | | | | | |
| | SPOT GPS | POINT | 9903770 | 763292 | .357 | 106 .: | 219 | | |
| | SKETCH-I | MAP OF ST | ATION | | | ETAIL MAP OF ST | | | — |
| | SORONG KLAMONO | | | | SORONG ← | A A A A A A A A A A A A A A A A A A A | / Sungal kecil | | |
| | | PHOT | O OF STATIO | PS | | Spot A dipasang (alur) kecil, Diseb Desa Makbon pad Untuk menuju Sp Propinsi yaitu jala ditempuh dengan | elah kiri jembata da Km. 19 Soron ot A, masuk dari n Sorong ≕ Mak | n, arah ke g. Jalan beru | |







| <u></u> | <u>DES</u> | CKII IIOI | VOI BEN | CH MAK. | K AND FRE | MARK | | | |
|----------------------|---------------------------------------|----------------------------------|--|-----------------------|---|------------------|-------------|--|--|
| STATION NO. | STATION NO. Spot - E | | | | | A. Gofhur | | | |
| DESA | Batu Loba | ing | | | CHECKED BY | | | | |
| KECAMATAN | Makbon | | | | SET UP DATE | 04-01-1994 | | | |
| KABUPATEN | Sorong | | | | HEIGHT OF | BENCHMARK | ± 30 cm | | |
| PROVINCE | Irian Jaya | | | | HEIGHT OF PREMARK cm | | | | |
| ZONE NO. | 52 | | | COORDINATE OF STATION | | | | | |
| UTM CCORDINATE | | N(m) | | E(m) | | H (m) | | | |
| BENCHMARK | | | | | | | | | |
| PREMARK | | | | | | | | | |
| SPOT GPS | SPOT GPS POINT | | 9915378 .500 | | 768359 .216 | | | | |
| SKETCH-MAP OF ST | | ATION | | DETAIL MAP OF ST | | TATION | | | |
| LAUT | | 0 0 0 0 0 0 0 0 0 0 0 0 | | | 1 | | 0 0 | | |
| | _ | _ | | |) | | 0 0 | | |
| | Ds. BAT | U LOBANG | LAUT | | | . J | | | |
| Ds.BATU | | | | | | | | | |
| | | | | | 1177) | | LOBANG- | | |
| | | | | | | | | | |
| | LAUT | ~~ / | | | | كولراسر | | | |
| | | | | | | | | | |
| /// _E)// | | | | | | | | | |
| | | | | | | | | | |
| | | 1 | LAUT | | | | | | |
| | | \ | | | | | | | |
| } | | | | | | • | | | |
| | PHO | TO OF STATIC | | REMARKS | | | | | |
| | | | | | Cnot E dinasana diataa hadit di dan Bata | | | | |
| | | | | | Spot E dipasang diatas bukit di desa Batu – Lobang. Dari desa Batu Lobang ± 250 M. | | | | |
| | a National | A CONTRACTOR | and the same of th | | Untuk menuju Spot E, dapat ditempuh dengan | | | | |
| | | | | | motor boat dari∶ ± 2 jam. | Sorong ke desa l | Batu Lobang | | |
| | e e e e e e e e e e e e e e e e e e e | | g: % | 1 | c. juit. | | ŀ | | |
| 1 1 | · . | /// · = \ \ \ \ | | | | | I | | |
| | | | | | 1 | | | | |
| | // | | | 1 | | | | | |
| | | | + |]· | | | • | | |
| | / | | | | • | | ļ | | |
| | | | | | | | | | |
| | <i>/</i> · | | W. St. March | | | | | | |
| | $\int_{\mathcal{S}} dx dx dx$ | | 2 500 | | | | | | |
| - j | 200 | | | | | | | | |
| 2 120 | | | 45 | | | | | | |
| | | . / ** | | | | | | | |

| NN NO. Spot - G | | | | | A. Goffur | | | |
|--------------------|---|---|---|---|--|--|--|--|
| Klaili | | | | CHECKED BY | | | | |
| Makbon | | | | SET UP DATE | 02-01-1994 | | | |
| Sorong | | | - | HEIGHT OF | BENCHMARK | ± 30 cm | | |
| Irian Jaya | | | HEIGHT OF PREMARK cm | | | | | |
| 52 | | | COORDII | COORDINATE OF STATION | | | | |
| UTM CCORDINATE | | · N(m) | | (m) | H (m) | | | |
| BENCHMARK | | | | | | | | |
| PREMARK | | | | | | | | |
| SPOT GPS POINT | | 9903419 .594 | | .154 | 72 .664 | | | |
| SKETCH-MAP OF STAT | | | | | | | | |
| Matoa - 1 | | | P WARSAMS ON P | | | | | |
| | | | (1) | tempuh dengan i Intimpura ±13 Ki | limuara S. Klasuw mobil dari Base C m dan dilanjutkan | lamp PT. Lialan kaki | | |
| | Klaili Makbon Sorong Irian Jaya 52 DINATE ARK RK POINT MAP OF STA | Klaili Makbon Sorong Irian Jaya 52 DINATE N (ARK RK POINT 9903419 MAP OF STATION | Klaili Makbon Sorong Irian Jaya 52 DINATE N (m) ARK RK POINT 9903419.594 MAP OF STATION | Klaili Makbon Sorong Irian Jaya 52 COORDII DINATE N (m) ENK RK POINT 9903419.594 773971 MAP OF STATION DINATE PHOTO OF STATION | Makbon SET UP DATE Sorong HEIGHT OF Irian Jaya HEIGHT OF STATIO DINATE N (m) E (m) ARK RK POINT 9903419.594 773971.154 MAP OF STATION DETAIL MAP OF ST WARSAMS PHOTO OF STATION Spot G terletak of termpuh dengan intimpura ± 13 K mengikuti jalan s | Makbon SET UP DATE 02-01-1994 Sorong HEIGHT OF BENCHMARK Irian Jaya COORDINATE OF STATION BY SET UP DATE 102-01-1994 HEIGHT OF BENCHMARK HEIGHT OF PREMARK COORDINATE OF STATION BY ARK RK POINT 9903419.594 773971.154 72.6 MAP OF STATION DETAIL MAP OF STATION PHOTO OF STATION REMARKS Spot G terletak dimuara S. Klasum tempuh dengan mobil dari Base o Intimpura ± 13 Km dan dilanjat kar mengikuti jalan setapak menuju kar mengikuti jalan setapak menu | | |

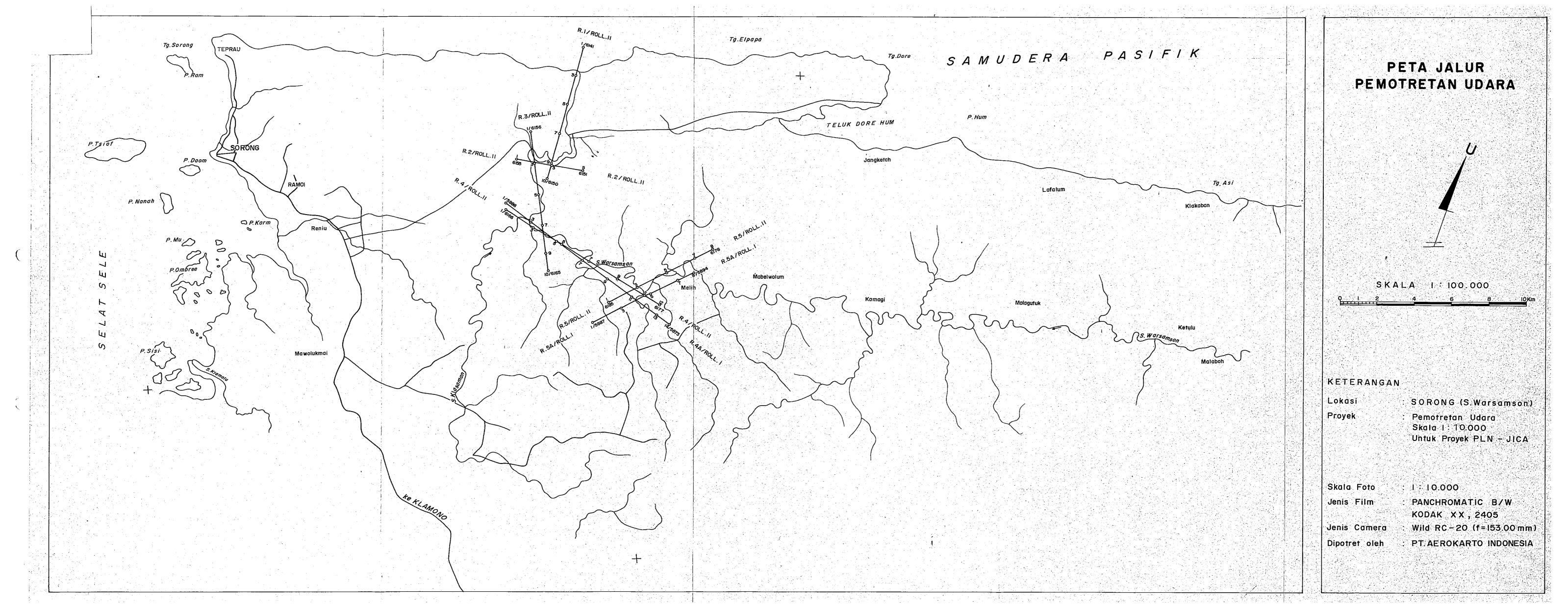
DESCRIPTION OF BENCH MARK AND PREMARK

| | CKII 1101 | | | | | | |
|----------------------|--------------|------|---------|--|--|--|----|
| STATION NO. Spot - H | | | | SURVEYOR | Suwadi | | |
| DESA Klaili | | | | CHECKED BY | - | | |
| KECAMATAN Makbon | | | | SET UP DATE | 31-12-1993 | | |
| KABUPATEN Sorong | | | | HEIGHT OF | BENCHMARK | ± 30 | cm |
| PROVINCE Irian Jayı | 1 | | | HEIGHT | OF PREMARK | | cm |
| ZONE NO. 52 | | | COORDIN | IATE OF STATIO | N | | |
| UTM CCORDINATE | N (| m) | E | (m) | Н (т | n) | |
| BENCHMARK | | | | | | | |
| PREMARK | | | | | | | |
| SPOT CPS POINT | 9900465 | .269 | 784386 | .257 | 70 . | 277 | |
| SKETCH-MAP OF S | TATION | | DE | TAIL MAP OF ST | · | | |
| 1 | S. KLAYILI | | 0 | KLAML! P | a. (a. | a / | |
| PHC | TO OF STATIC | N N | | : | REMARKS | | _ |
| | | | | Spot H dipasang S. Klawuguk, yai M. Dapat ditemp ikuti jalan setapa pat mancing, bar arah muara ± 20 Perjalanan dari d | tu disebelah timu uh dengan jalan k dari desa Klaili ru mengikuti tepi 10 M. | ır muara ± ; kaki meng- kolam tem- sungal ke- | 20 |

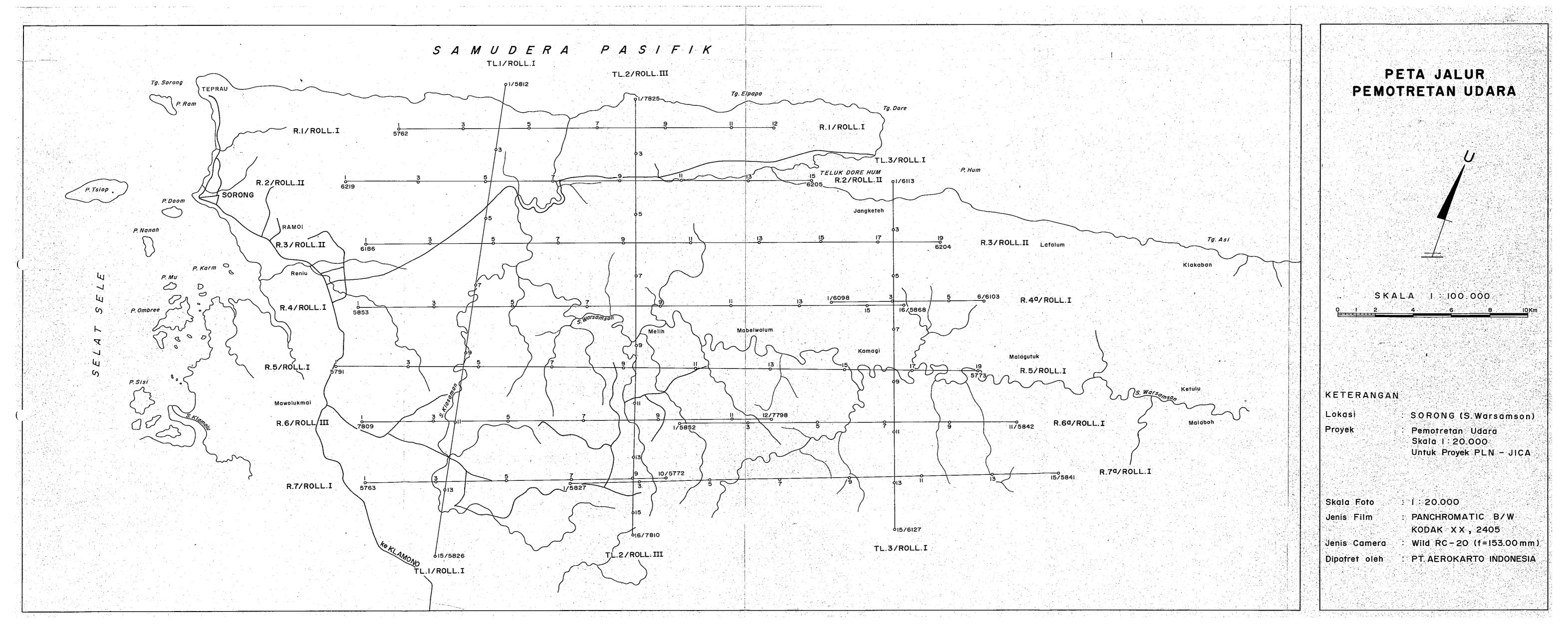
PT. Aerokarto Indonesia

APPENDIX 3.1.

FLIGHT INDEX FOR SCALE 1 : 10,000

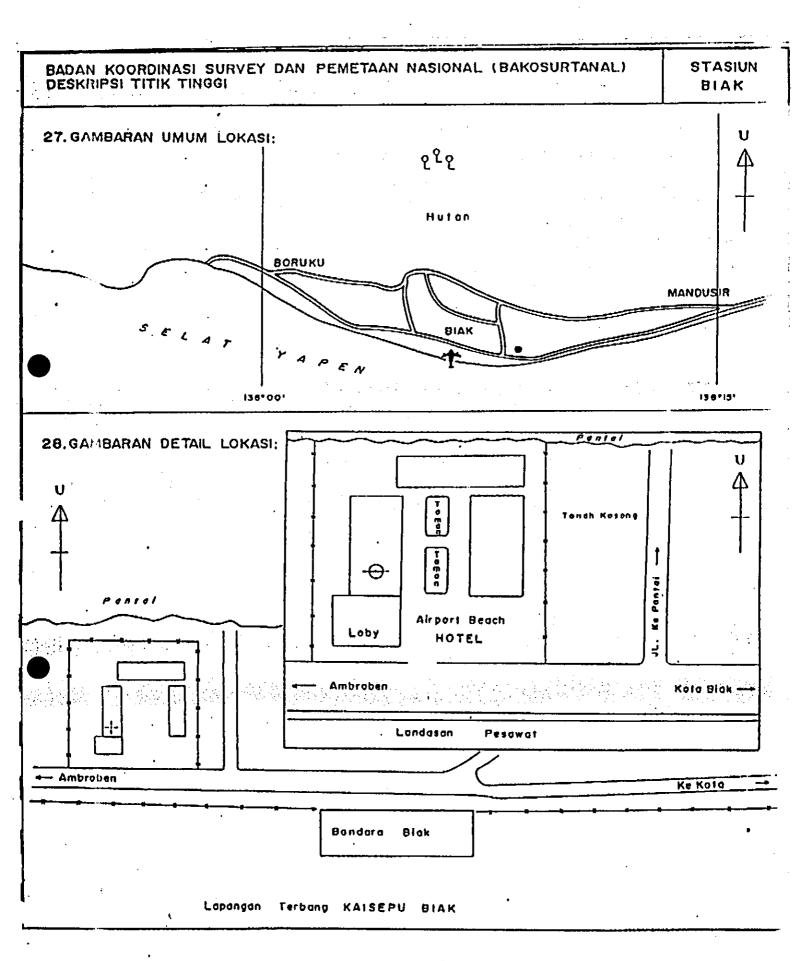


APPENDIX 3.2
FLIGHT INDEX FOR SCALE 1 : 20,000



APPENDIX 3.3

DESCRIPTION OF REFERENCE POINT FOR KINEMATIC GPS



TRIMVEC 6PS RELATIVE POSITIONING SOLUTION SUMMARY: VERSION 92.030MBP

OPTIMUM SOLUTION OUTPUT FILE: MBCMSSA.ont

Start date/time: 1994/ 2/ 2 6:53:66. day of year 33 tow 284040. Stop. date/time: 1994/ 2/ 2 8:36:15. day of year 33 tow 290175.

STATION INFORMATION .

Hot (m) Longitude Latitude Ant (m) 10 5P74 124.410 1:10'04.12100"S 136:05'23.63200"E 0.365 1 88.385 136:06'27.77393"E-1:11'33.96237"8 * BTUK 1,549 2

Origin of station 1 coordinates : User input

COMPUTED VECTOR INFURMATION

Contacted Fixed Normal Section Station Slope ROOF Ghuality Angle (dms) Azimuth (dms) Distance (m) From To Q.080M 144 17 36.50 -000 37 21.02 4 5 5398.342

ALL VECTORS (dx, dy and dz between ECEF Coordinates)

From To dx(m) dy(m) dz(m) dist(m) dh(m) F1% 1 2 -1308.148 -1493.227 -2758.215 3398.342 -36.025

* L1 solution Measurements used: 274 Rejected: 8 RMS (cycles) 0.025

WGS84 coordinates (input)
latitude (d.m.s) 15:111133:9623
longitude (d.m.s) 16:36 6 27:7739
longitude (d.m.s): W223 53 32:2261
ellipsoid height(m): 45:3830

x-coordinate(m): -45954433577 y-coordinate(m): /44211025503 z-coordinate(m): /-1318818986

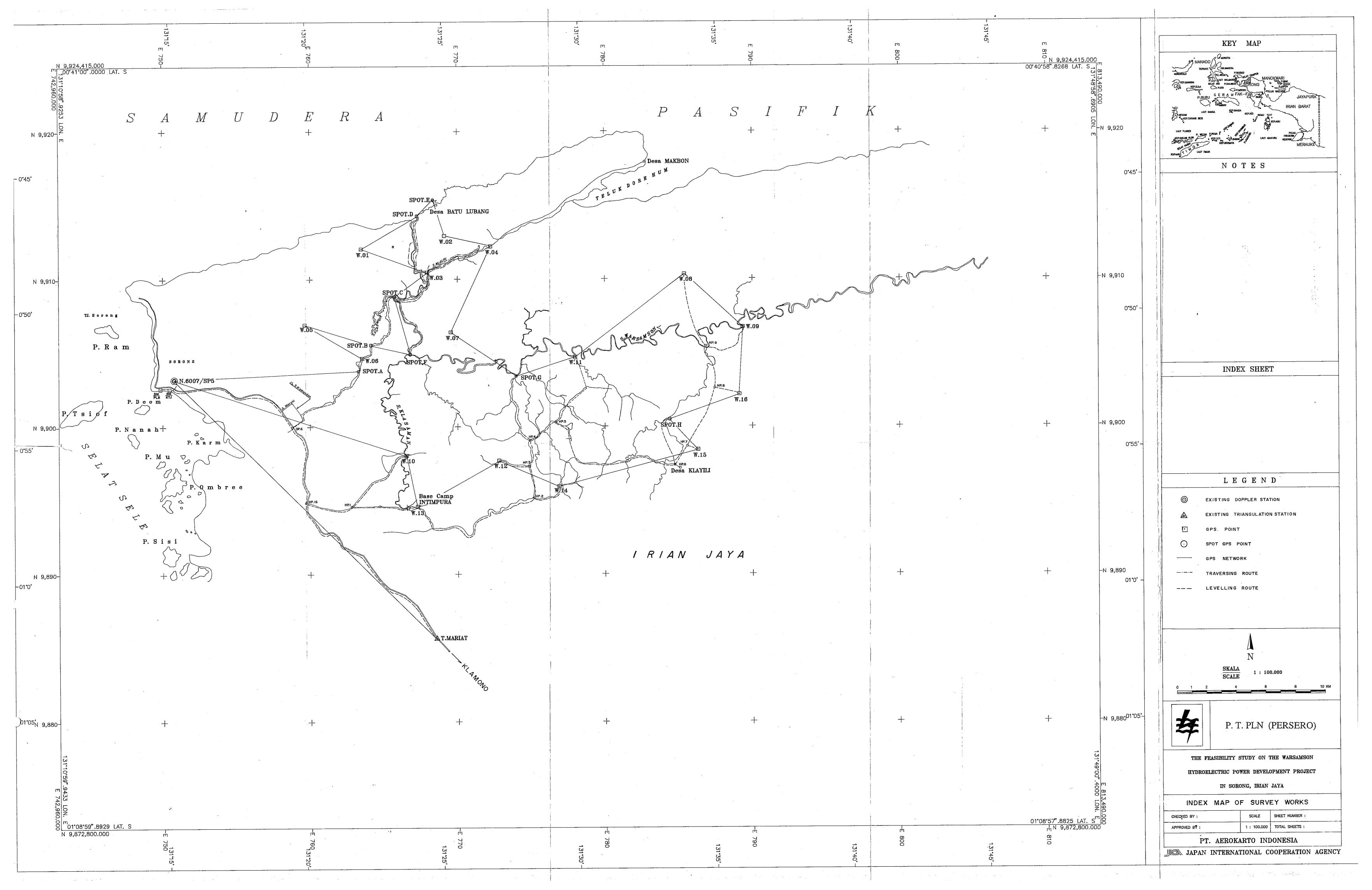
another transformation ? (Y/N)

APPENDIX 5.1 GEODETIC AND UTM COORDINATE IN ID '74

FINAL RESULT GOEDETIC AND UTM COORDINATE IN ID '74

| POINT ID | | LATITUDE | | | TON | LONGITUDE | EASTING | NORTHING | ELLIPSOID | MEAN SEA LEVEL |
|-------------|------|--------------|-------|-----|------|-------------|------------|-------------|----------------|----------------|
| | 0 | | | 0 | | | (METER) | (METER) | HEIGHT (METER) | (METER) |
| | , | | | | | | | | | |
| N.6007/SP.5 | 0 5 | 52 30.484873 | 73 8 | 131 | 15 | 11.809801 E | 750770.613 | 9903195.577 | 135.0122 | 65.924 |
| SPOT.A | 0 55 | 52 11.521678 | 78 S | 131 | 21 | 56.619315 E | 763292.357 | 9903770.590 | 175.4542 | 106.219 |
| SPOT.B | 0 | 51 14.330856 | 56 s | 131 | 22 | 23.966338 E | 764139.375 | 9905527.503 | 140.6619 | 71.308 |
| SPOT.C | 0 | 49 27.942737 | 37 8 | 131 | 23 | 15.458737 E | 765734.200 | 9908795.803 | 111.8788 | 42.568 |
| SPOT.D | 0 | 46 29.194036 | 36 8 | 131 | 24 | 5.140106 E | 767274.250 | 9914287.846 | 73.3456 | 4.237 |
| SPOT.E | 0 | 45 53.682857 | 57 s | 131 | 24 | 40.193206 E | 768359.216 | 9915378.500 | 103.9480 | 1 |
| SPOT.F | 0 | 51 34.578076 | 76 s | 131 | 23 | 50.090138 E | 766803.086 | 9904903.652 | 111.3999 | 42.051 |
| SPOT.G | 0 | 52 22.720677 | 77 S | 131 | 27 | 41.839936 E | 773971.154 | 9903419.594 | 142.0436 | 72.664 |
| SPOT. H | 0 | 53 58,620979 | 2 6 C | 131 | 33 | 18.570847 E | 784386.257 | 9900465.269 | 139.8071 | 70.277 |
| W.01 | 0 | 47 42.306675 | 75 S | 131 | 22 | 2.955983 E | 763493.337 | 9912043.270 | 440.5935 | ı |
| W.02 | 0 | 47 13,348256 | 26 S | 131 | 25 | 5.034047 E | 769126.261 | 9912929.911 | 258.9286 | 1 |
| W.03 | 0 | 48 34.165572 | 72 S | 131 | 24 2 | 27.726280 E | 767970.708 | 9910447.042 | 105.4277 | 36.416 |
| W.04 | 0 | 47 37.039582 | 82 S | 131 | 264 | 45.812070 E | 772243.397 | 9912200.031 | 86.5970 | 17.267 |
| W.05 | 0 | 50 29.096803 | 03.8 | 131 | 19 | 58.879759 E | 759652.299 | 9906920.231 | 138.0100 | , |
| W.06 | 0 51 | 1 43,431714 | 14 S | 131 | 22 | 4.843200 E | 763547.284 | 9904633.617 | 164.7633 | 95.478 |
| W.07 | 0 20 | 0 45,832418 | 18 S | 131 | 25 | 18.880571 E | 769550.663 | 9906399.900 | 140.5221 | • |
| W.08 | 0 48 | 8 38.302046 | 46 \$ | 131 | 35 | 50.92342 E | 785393.698 | 9910309.225 | 250.8584 | 181.623 |
| W.09 | 0 20 | 0 35.272855 | 55 8 | 131 | 33 | 58.653682 E | 789343.141 | 9906711.631 | 127.0826 | 57.664 |
| W.10 | 0 55 | 5 18.004726 | 26 S | 131 | 23 | 41.648464 E | 766537.491 | 9898037.920 | 145.9417 | 77.033 |
| W.11 | 0 51 | 1 40.851653 | 53 S | 131 | 29 | 52.060442 E | 778000.428 | 9904703.669 | 120.5015 | 51.116 |
| W.12 | 0 55 | 5 29.649308 | 08 S | 131 | 27 | 3.982401 瓦 | 772796.178 | 9897675.807 | 241.8427 | 172.561 |
| W.13 | 0 57 | 7 10.308663 | 63 S | 131 | 24 | 5.806582 E | 767282.409 | 9894586.301 | 162,5095 | 93.489 |
| W.14 | 95 0 | 6 26.392166 | g 99 | 131 | 29 | 16.621662 E | 776898.104 | 9898929.122 | 245.7648 | 176.449 |
| W.15 | 0 55 | 5 5.707576 | 76 s | 131 | 34 | 20.517556 E | 786301.245 | 9898402.073 | 198.1395 | 128.533 |
| W.16 | 0 53 | 3 3.584829 | 29 S | 131 | 35 | 51.172958 E | 789108.581 | 9902153.455 | 149.2650 | 79.663 |
| T. MARIAT | 1 02 | 2 1.494810 | 10 8 | 131 | 24 | 45.987847 E | 768518.802 | 9885637.166 | 250.3837 | 181.161 |

APPENDIX 6.1. MAP OF STATIC GPS NETWORK TRAVERSING AND LEVELLING ROUTE



APPENDIX 6.2. FINAL COORDINATE AND ELEVATION OF GPS SURVEY

FINAL COORDINATES AND ELEVATION GPS SURVEY OF WARSAMSON HEPDP

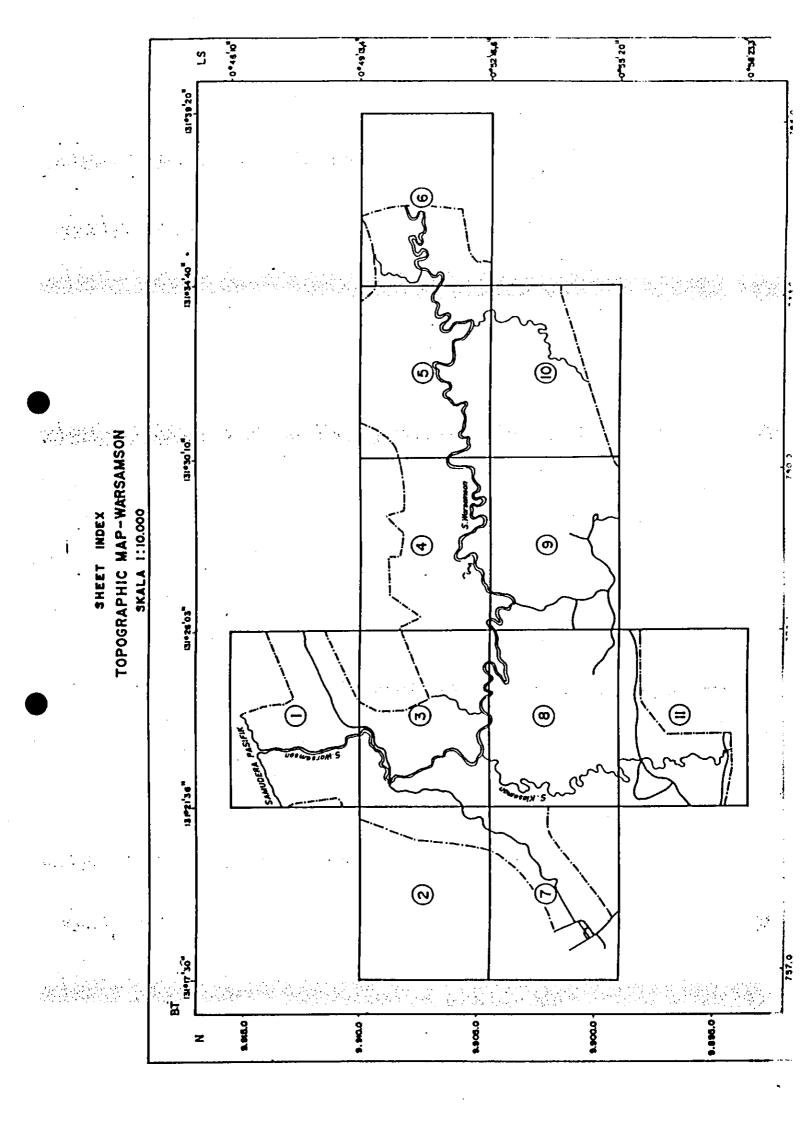
| STA. | E | N | Н | REMARKS |
|-------------|-------------|---------------|---------|----------------|
| N 6007/SP.5 | 750,770.613 | 9,903,195.577 | 65.924 | MASTER STATION |
| W.01 | 763,493.337 | | 372.860 | |
| W.02 | 769,126.261 | | 189.800 | |
| W.03 | 767,970.708 | 9,910,447.042 | 36.146 | |
| W.04 | 772,243.397 | 9,912,200.031 | 17.267 | |
| W.05 | 759,652.299 | 9,906,920.231 | 72.340 | *3 |
| W.06 | 763,547.284 | 9,904,633.617 | 95.478 | |
| W.07 | 769,550.663 | 9,906,399.900 | | |
| W.08 | 785,393.698 | 9,910,309.225 | 181.623 | |
| W.09 | 789,343.141 | 9,906,711.631 | 57.664 | |
| W.10 | 766,537.491 | 9,898,037.920 | 77.033 | |
| - W.11 | 778,000.428 | 9,904,703.669 | 51.116 | |
| W.12 | 772,796.178 | 9,897,675.807 | 172.561 | |
| W.13 | 767,282.409 | 9,894,586.301 | 93.489 | |
| W.14 | 776,898.104 | 9,895,929.122 | 176.449 | |
| W.15 | 786,301.245 | 9,898,402.073 | 128.533 | |
| W.16 | 789,108.581 | 9,902,153.455 | 79.663 | |
| SPOT-A | 763,292.357 | 9,903,770.590 | 106.219 | |
| SPOT-B | 764,139.375 | 9,905,527.503 | 71.308 | |
| SPOT-C | 765,734.200 | 9,908,795.803 | 42.568 | |
| SPOT-D | 767,274.250 | 9,914,287.846 | 4.237 | |
| SPOT-E | 768,359.216 | 9,915,378.500 | 35.120 | *4 |
| SPOT-F | 766,803.086 | 9,904,903.652 | 42.051 | |
| SPOT-G | 773,971.154 | 9,903,419.594 | 72.664 | |
| SPOT-H | 784,386.257 | 9,900,465.269 | 70.277 | |
| T. MARIAT, | 768,518.802 | 9,885,637.166 | 181.161 | |
| BM/KTJ | - | _ | 2.504 | |

NOTES

- 1) REFERENCE ELLIPSOID: ID74 (GRS 67)
 2) PROJECTION SYSTEM: UTM ZONE52
- 3) ELEVATION: SORONG PEIL MEAN SEA LEVEL OF SORONG BAY
 4) *1 ~ *3: ELEVATION BY "BLOCK ADJUSTMENT WITH BOUNDLES"
 - IN AERIAL TRIANGULATION
- 5) *4: ELEVATION BY EDM

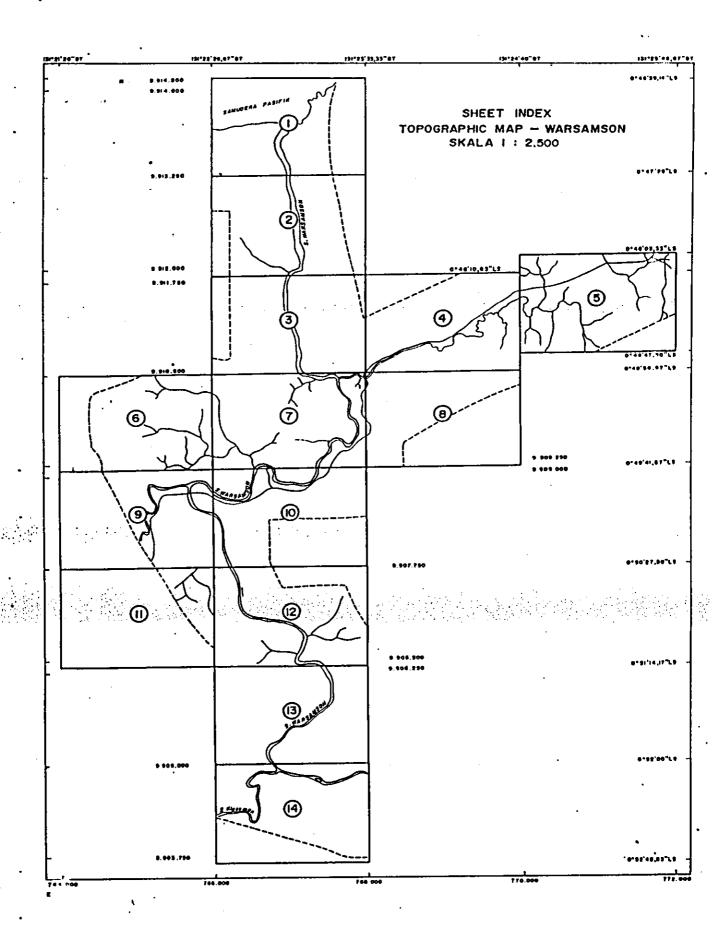
APPENDIX 9.1

INDEX SHEET FOR MAP OF SCALE 1: 10,000



APPENDIX 9.2

INDEX SHEET FOR MAP OF SCALE 1 : 2,500



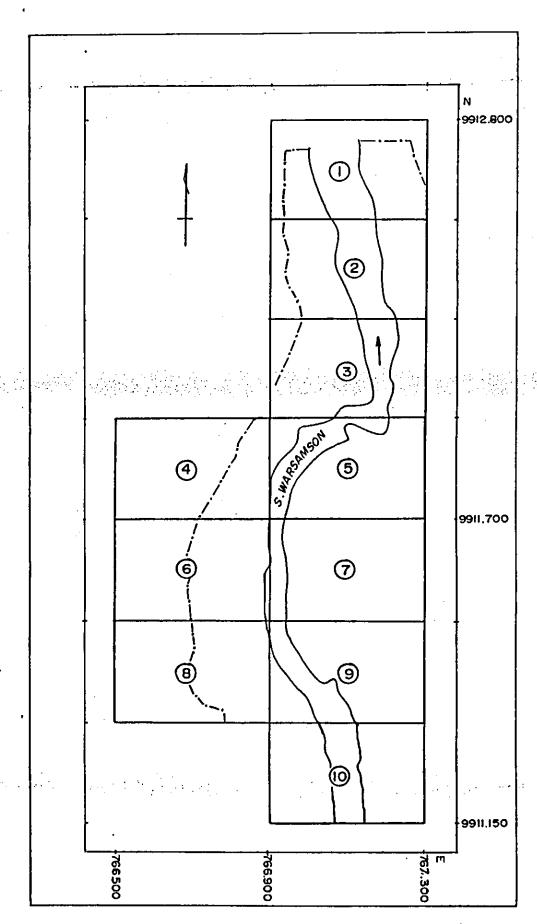
APPENDIX 9.3

INDEX SHEET FOR MAP OF SCALE 1 : 500

SHEET INDEX

TOPOGRAPHIC MAP WARSAMSON

SCALE 1:500



APPENDIX 11.1 FINAL COORDINATE AND ELEVATION OF MAIN TRAVERSE ROUTE

ROUTE: R

| NO. | E | N | H | REMARKS |
|--------|-------------|---------------|--------|--|
| SPOT-E | 768,359.216 | 9,915,378.500 | 35.12 | PVC |
| SPOT-D | 767,274.250 | 9,914,287.846 | 4.237 | PVC |
| AC.1 | 766,960,203 | 9,913,952.908 | 5.90 | PVC |
| 1 | 766,987.491 | 9,913,853.630 | 0.83 | |
| 2 | 766,974.487 | 9,913,817.184 | 2.00 | |
| 3 | 766,959.616 | 9,913,788.114 | 15,36 | |
| 4 | 766,941.081 | 9,913,744.940 | 1,65 | |
| 5 | 766,929,767 | 9,913,673.367 | 1.82 | <u>- </u> |
| 6 | 766,941.542 | 9,913,600.451 | 3.81 | |
| 7 | 766,977.238 | 9,913,540.246 | 7.51 | |
| 8 | 766,989.031 | 9,913,471.541 | 4.93 | |
| 9 | 767,002.401 | 9,913,445.955 | 1,78 | |
| 10 | 767,012,367 | 9,913,429.578 | . 6.88 | |
| 11 | 767,034.315 | 9,913,390.947 | 15.53 | |
| 12 | 767,042.623 | 9,913,367.653 | 12.21 | · |
| 13 | 767,051.055 | 9,913,305.986 | 0.85 | |
| 14 | 767,076.126 | 9,913,246.204 | 2.57 | |
| 15 | 767,063.884 | 9,913,187.450 | 9.69 | |
| 16 | 767,030.512 | 9,913,138.836 | 0.75 | |
| 17 | 767,027.788 | 9,913,099,735 | 0.96 | |
| D.10 | 767,036.418 | 9,913,071.654 | 3.49 | |
| 18 | 767,035.629 | 9,913,042.983 | 5.52 | |
| 19 | 767,037.198 | 9,912,993.394 | 2.73 | - |
| 20 | 767,042.720 | 9,912,962.349 | 0.76 | |
| 21 | 767,055,877 | 9,912,933.237 | 2.08 | |
| 22 | 767,064,169 | 9,912,880.875 | 0.95 | |
| 23 | 767,081.296 | 9,912,833.289 | 1.25 | |
| 24 | 767,106.812 | 9,912,790.872 | 2.49 | |
| R.1 | 767,112.066 | 9,912,717.774 | 3,45 | |
| R.2 | 767,143.928 | 9,912,693.236 | 12.12 | · · |
| R.3 | 767,159.025 | 9,912,659,951 | 37.57 | |
| D.8 | 767,158.635 | 9,912,649,966 | 42.61 | |
| R.4 | 767,159.273 | 9,912,604.820 | 22.94 | |
| D.7 | 767,159.529 | 9,912,580.912 | 8.57 | |
| R.5 | 767,156.756 | 9,912,533.108 | 3.68 | |
| R.6 | 767,166.516 | 9,912,479.561 | 7.05 | |
| R.7 | 767,191.034 | 9,912,383.076 | 17,13 | |
| R.8 | 767,182.188 | 9,912,356.578 | 5.29 | |
| R,9 | 767,179.463 | 9,912,337.512 | 5.14 | |
| AC.2 | 767,180.059 | 9,912,286.737 | 4.53 | PVC |

ROUTE: R

| NO. | E | N | H | REMARKS |
|--------|-------------|---------------|--------|----------|
| R.7 | 767,191.034 | 9,912,383.076 | 17.13 | |
| R.8 | 767,182.188 | 9,912,356.578 | 5.29 | · |
| R.9 | 767,179.463 | 9,912,337.512 | 5.14 | |
| AC.2 | 767,180.059 | 9,912,286.737 | 4.53 | PVC |
| PLN.10 | 767,212,272 | 9,912,268.121 | 9.11 | CONCRETE |
| R.10 | 767,226.602 | 9,912,216.791 | 8.21 | |
| R.11 | 767,218.447 | 9,912,159.751 | 6.15 | |
| R.12 | 767,211.261 | 9,912,123,600 | 8.22 | |
| AC.3 | 767,207.782 | 9,912,102.438 | 5.98 | PVC |
| R.13 | 767,209.029 | 9,912,087.999 | 9.16 | |
| R.14 | 767,220.609 | 9,912,025.468 | 15.66 | |
| R.15 | 767,211.206 | 9,911,988,817 | 19.33 | |
| D.6 | 767,179,446 | 9,911,934.087 | 6.88 | |
| R.16 | 767,188.492 | 9,911,878.819 | 22.93 | |
| R.17 | 767,210.613 | 9,911,852.055 | 43.20 | |
| R.18 | 767,227.191 | 9,911,767.770 | 60.15 | |
| R.19 | 767,232.785 | 9,911,706.531 | 71.82 | |
| D.5 | 767,237.487 | 9,911,680.416 | 74.88 | |
| R.20 | 767,193.300 | 9,911,627,954 | 126.25 | |
| R.21 | 767,184.672 | 9,911,603.995 | 141.20 | |
| R.22 | 767,169.865 | 9,911,582.829 | 153.85 | |
| D.4 | 767,147.008 | 9,911,563.077 | 153.66 | |
| R.23 | 767,146.226 | 9,911,511.418 | 149.18 | |
| R.24 | 767,144.984 | 9,911,457.897 | 142.83 | _ |
| R.25 | 767,147.489 | 9,911,417.937 | 132,55 | |
| R.26 | 767,155.630 | 9,911,378.980 | 133.83 | |
| R.27 | 767,151.332 | 9,911,360.544 | 134.51 | |
| R.28 | 767,147.844 | 9,911,330.793 | 126.62 | |
| R.29 | 767,142.801 | 9,911,296.001 | 113.03 | |
| R.30 | 767,151.349 | 9,911,253.164 | 90.03 | · |
| D.3 | 767,127.336 | 9,911,245.440 | 83.07 | |
| R.31 | 767,111.957 | 9,911,242.311 | 75.53 | |
| R.32 | 767,058.008 | 9,911,234.933 | 41.05 | |
| R.33 | 767,083.645 | 9,911,168.333 | 35.88 | |
| R.34 | 767,107.207 | 9,911,114.961 | 37.77 | |
| AC.4 | 767,116.160 | 9,911,076.024 | 42.11 | PVC |

ROUTE: R

| NO. | E | N | H | REMARKS |
|------|-------------|---------------|--------|----------|
| R.44 | 767,113.454 | 9,910,661.000 | 36.69 | |
| R.45 | 767,116.743 | 9,910,605.001 | 39.10 | <u> </u> |
| R.46 | 767,115.194 | 9,910,548.981 | 37.46 | ". |
| R.47 | 767,133.529 | 9,910,502.108 | 38.69 | |
| R.48 | 767,148.910 | 9,910,456.548 | 38.82 | |
| R.49 | 767,202.755 | 9,910,426.743 | 40.05 | |
| R.50 | 767,244.645 | 9,910,420.408 | 35.71 | *** |
| R.51 | 767,325.134 | 9,910,448.930 | 36.61 | *· *** |
| R.52 | 767,369.699 | 9,910,475.168 | 37.44 | |
| R,53 | 767,433.261 | 9,910,493.623 | 37.58 | |
| R,54 | 767,498.831 | 9,910,500,080 | 39.02 | |
| PB.1 | 767,533,750 | 9,910,500.601 | 37.31 | CONCRETE |
| R.55 | 767,594.362 | 9,910,494.765 | 35.31 | |
| R.56 | 767,641.403 | 9,910,477.115 | 36.78 | |
| R.57 | 767,681.913 | 9,910,491.490 | 36.86 | |
| R.58 | 767,739.952 | 9,910,510.236 | 31.51 | *** |
| R.59 | 767,796.245 | 9,910,492.034 | 34.57 | **** |
| R.60 | 767,843.851 | 9,910,465.915 | 37.96 | |
| R.61 | 767,907.064 | 9,910,455.691 | 39.03 | |
| W.03 | 767,970,708 | 9,910,447.042 | 36.146 | CONCRETE |

WARSAMSON PROJECT

ROUTE: L

| NO. | E | N | H | REMARKS |
|-------|-------------|---------------|--------|---------------------------------------|
| R2 | 767,143.928 | 9,912,693.236 | 12.12 | |
| R1 | 767,112.066 | 9,912,717.774 | 3.45 | |
| L1 | 767,020.033 | 9,912,712.193 | 1.66 | |
| L2 | 767,024.080 | 9,912,664.835 | 3.00 | |
| L3 | 767,047.487 | 9,912,600.265 | 3.15 | |
| PB.10 | 767,062.333 | 9,912,570.713 | 2.95 | CONCRETE |
| L4 | 767,048.872 | 9,912,516.901 | 17,52 | |
| L5 | 767,025.779 | 9,912,435.469 | 32.99 | |
| L6 | 767,020.581 | 9,912,377.279 | 45,48 | |
| L7 | 767,002.085 | 9,912,351.667 | 62.05 | |
| L8 | 766,992.661 | 9,912,302.142 | 84.17 | |
| L9 | 766,981.709 | 9,912,267.399 | 104,51 | |
| L10 | 766,966.878 | 9,912,214.832 | 130.11 | |
| Lli | 766,962.997 | 9,912,197.233 | 130,78 | |
| L12 | 766,938.482 | 9,912,107.702 | 141.13 | · · · · · · · · · · · · · · · · · · · |
| L13 | 766,938.491 | 9,912,085.019 | 138.48 | |
| L14 | 766,931.687 | 9,912,071.829 | 134.01 | |
| L15 | 766,927.294 | 9,912,065.107 | 128,34 | |
| L16 | 766,919.304 | 9,912,039,451 | 101.21 | |
| L17 | 766,918.160 | 9,912,026.135 | 87,30 | |
| L18 | 766,900.971 | 9,911,981.914 | 51.92 | |
| L19 | 766,914.925 | 9,911,950.646 | 59.52 | |
| L20 | 766,928.681 | 9,911,922.278 | 60.54 | |
| L21 | 766,898.128 | 9,911,886.587 | 63.99 | |
| L22 | 766,876,992 | 9,911,856.810 | 67.72 | |
| L23 | 766,852.145 | 9,911,822.152 | 70.83 | |
| L24 | 766,836,536 | 9,911,760.447 | 81.45 | |
| L25 | 766,823,045 | 9,911,701.959 | 88,99 | |
| L26 | 766,822.822 | 9,911,667.717 | 102.66 | |
| L27 | 766,819,144 | 9,911,609.858 | 95.89 | |
| L28 | 766,820.634 | 9,911,551.793 | 83.77 | |
| L29 | 766,812.130 | 9,911,492.266 | 89.15 | ** |
| L30 | 766,814.224 | 9,911,480.513 | 92.43 | |
| L31 | 766,814.619 | 9,911,435.438 | 84.08 | |
| L32 | 766,810.558 | 9,911,364.665 | 99.05 | |
| L33 | 766,815.137 | 9,911,315.764 | 117.08 | |
| L34 | 766,814.536 | 9,911,290,933 | 121.66 | |

ROUTE : L

| NO. | E | N | H | REMARKS |
|------|-------------|---------------|--------|---------|
| L35 | 766,817.648 | 9,911,268.046 | 103.14 | |
| L36 | 766,836.860 | 9,911,236.325 | 73.07 | |
| L37 | 766,862.715 | 9,911,204.397 | 61.02 | |
| L38 | 766,929.806 | 9,911,163.637 | 85.68 | • |
| L39 | 766,978.683 | 9,911,166.137 | 65.98 | |
| L40 | 767,018.888 | 9,911,148.412 | 45,30 | |
| L41 | 767,045.368 | 9,911,106.388 | 37.44 | |
| L42 | 767,071.183 | 9,910,999.158 | 44.83 | |
| L43 | 767,071.376 | 9,910,931.377 | 48.12 | |
| L44 | 767,064.976 | 9,910,870.383 | 48.83 | |
| L45 | 767,075.236 | 9,910,842.916 | 46.69 | |
| L46 | 767,070.235 | 9,910,790.543 | 42.02 | |
| L46' | 767,122.131 | 9,910,772.132 | 34.06 | |
| R42 | 767,128.830 | 9,910,776.943 | 38.05 | |
| R41 | 767,133.661 | 9,910,831,218 | 37.06 | |

ROUTE: C

| POINTS | E | N | Н | REMARKS |
|--------|-------------|---------------|-------|----------|
| R54 | 767,498.831 | 9,910,500.080 | 39.02 | |
| PB.1 | 767,533.750 | 9,910,500.601 | 37.31 | CONCRETE |
| C.1 | 767,558.938 | 9,910,463.153 | 35.58 | |
| C.2 | 767,568.592 | 9,910,405.814 | 34.57 | |
| C.3 | 767,562.181 | 9,910,396.301 | 34.71 | |
| C.4 | 767,572.842 | 9,910,373.224 | 34.18 | |
| C.5 | 767,567.065 | 9,910,347.629 | 34.63 | |
| C.6 | 767,573.029 | 9,910,302.375 | 39.97 | |
| C.7 | 767,556.956 | 9,910,260.751 | 34.01 | |
| C.8 | 767,557.658 | 9,910,214.379 | 35.49 | |
| C.9 | 767,595.256 | 9,910,130.652 | 35.17 | |
| C.10 | 767,646.649 | 9,910,079.297 | 35,63 | |
| C.11 | 767,674.449 | 9,910,041.888 | 36.43 | |
| C.12 | 767,713.629 | 9,909,998.741 | 36.89 | |
| C.13 | 767,723.686 | 9,909,969.089 | 38.38 | |
| C.14 | 767,739.161 | 9,909,931.633 | 38.84 | |
| C.15 | 767,756.850 | 9,909,859.914 | 37.67 | |
| C.16 | 767,793.906 | 9,909,845.593 | 39.62 | |
| C.17 | 767,831.320 | 9,909,840.185 | 38.86 | |
| C.18 | 767,899.282 | 9,909,818.493 | 36.71 | |
| C.19 | 768,001.718 | 9,909,588.458 | 39.62 | |
| C.20 | 767,972.966 | 9,909,515.478 | 39.31 | • |
| C.21 | 767,699.767 | 9,909,423.408 | 36,87 | |
| C.22 | 767,655.431 | 9,909,439.010 | 42.94 | |
| C.23 | 767,640.460 | 9,909,480.598 | 36.54 | |
| C.24 | 767,617.870 | 9,909,521.030 | 36.96 | |
| C.25 | 767,613,680 | 9,909,577.286 | 36.87 | |
| C.26 | 767,586.884 | 9,909,581.375 | 36.98 | |
| C.27 | 767,561.805 | 9,909,569.102 | 36.90 | |
| C.28 | 767,529.045 | 9,909,540.951 | 37.39 | |
| C.29 | 767,503.198 | 9,909,511.182 | 37.89 | |
| C.30 | 767,489.635 | 9,909,495.818 | 37.07 | |
| C.31 | 767,474.440 | 9,909,462.978 | 37.61 | |
| C.32 | 767,456.931 | 9,909,378,566 | 37.81 | |
| C.33 | 767,462.373 | 9,909,329.008 | 38.89 | |
| C.34 | 767,455.278 | 9,909,308.280 | 39.43 | |
| C.35 | 767,434.839 | 9,909,265.858 | 37.33 | |
| C.36 | 767,414.397 | 9,909,232.368 | 38.20 | |
| C.37 | 767,401.522 | 9,909,188.314 | 38.93 | |
| C.38 | 767,403.936 | 9,909,154.852 | 39.51 | |

ROUTE: C

| POINTS | E | N | Н | REMARKS |
|--------|-------------|---------------|---------|----------|
| C.39 | 767,411.013 | 9,909,104.758 | 38.22 | |
| C.40 | 767,415.690 | 9,908,994.616 | 39.38 | |
| C.41 | 767,157.842 | 9,908,802.416 | 36.52 | |
| C.42 | 767,119.456 | 9,908,808.898 | 38.05 | |
| C.43 | 767,091.631 | 9,908,826.233 | 38.49 | |
| C.44 | 767,032.149 | 9,908,840.644 | 39.96 | <u> </u> |
| C.45 | 767,003.008 | 9,908,841.071 | 38.86 | |
| C.46 | 766,988.693 | 9,908,836.415 | 38.85 | |
| C.47 | 766,962.576 | 9,908,828.936 | 38.10 | |
| C.48 | 766,932.006 | 9,908,822.961 | . 38.35 | |
| C.49 | 766,908.113 | 9,908,830.578 | 37.51 | |
| C.50 | 766,856.421 | 9,908,843.842 | 38.10 | |
| C.51 | 766,824.794 | 9,908,865.340 | 38.21 | |
| C.52 | 766,788.805 | 9,908,907.598 | 38.51 | |
| C.53 | 766,784.196 | 9,908,948.712 | 37.60 | |
| C.54 | 766,774.194 | 9,908,993.676 | 38.14 | |
| C.55 | 766,775.982 | 9,909,044.491 | 38.39 | , |
| C.56 | 766,777.883 | 9,909,096.638 | 38.22 | |
| C.57 | 766,730.017 | 9,909,163.481 | 38.47 | |
| C.58 | 766,697.563 | 9,909,194.178 | 38.13 | |
| C.59 | 766,652.687 | 9,909,167.779 | 37.92 | |
| C.60 | 766,645.805 | 9,909,135.233 | 38.35 | |
| C.61 | 766,615.283 | 9,909,082.010 | 38.35 | |
| C.62 | 766,594.997 | 9,909,040.020 | 37.92 | |
| C.63 | 766,589.882 | 9,908,996,809 | 38.56 | |
| C.64 | 766,599.474 | 9,908,978.830 | 40.24 | |
| C.65 | 766,602.317 | 9,908,958.485 | 50,14 | |
| C.66 | 766,585,869 | 9,908,926.510 | 41.82 | |
| C.67 | 766,569.681 | 9,908,888.203 | 45.87 | |
| C.68 | 766,573.828 | 9,908,847.767 | 42.49 | |
| C.69 | 766,563.253 | 9,908,784.048 | 41.97 | |
| C.70 | 766,555.676 | 9,908,773.627 | 37.63 | |
| C.71 | 766,350.797 | 9,908,652.731 | 36.59 | |
| C.72 | 766,331.856 | 9,908,645.677 | 38.81 | |
| C.73 | 766,299.133 | 9,908,656.478 | 38.58 | |
| C.74 | 766,257.920 | 9,908,655.694 | 39.65 | |
| C.75 | 766,209.327 | 9,908,674.578 | 39.04 | |
| C.76 | 765,988.225 | 9,908,789.899 | 36.72 | |
| C.77 | 765,972.675 | 9,908,808.030 | 38,11 | |
| C.78 | 765,951.280 | 9,908,856.821 | 38.66 | |

WARSAMSON

PROJECT

ROUTE: C

| POINTS | E | N | Н | REMARKS |
|--------|-------------|---------------|--------|----------|
| C.79 | 765,922.569 | 9,908,892.713 | 38.64 | |
| C.80 | 765,875,556 | 9,908,909.908 | 39.02 | |
| C.81 | 765,841.584 | 9,908,910.098 | 39.24 | |
| C.82 | 765,776,564 | 9,908,888,953 | 38.72 | |
| C.83 | 765,752.393 | 9,908,867.345 | 39.33 | |
| SPOT-C | 765,734.200 | 9,908,795,803 | 42.568 | CONCRETE |

WARSAMSON PROJECT

ROUTE: F

| NO. | E | N | H | REMARKS |
|------|-------------|---------------|-------|-------------|
| F.1 | 765,763.321 | 9,908,693.905 | 39.85 | |
| F.2 | 765,755.132 | 9,908,621.016 | 38.95 | |
| F.3 | 765,770.501 | 9,908,597.285 | 38.93 | |
| F.4 | 765,801.690 | 9,908,576.984 | 39.44 | |
| F.5 | 765,832.596 | 9,908,566.733 | 39.55 | |
| F.6 | 765,858.581 | 9,908,546.490 | 38.97 | · · |
| F.7 | 765,892.518 | 9,908,539.618 | 40.81 | |
| F.8 | 765,947.664 | 9,908,513.763 | 42,21 | |
| F.9 | 765,993.436 | 9,908,496.587 | 40.36 | |
| F.10 | 766,139.114 | 9,908,353.090 | 38.96 | |
| F.11 | 766,151.974 | 9,908,313.239 | 40.64 | |
| F.12 | 766,161.124 | 9,908,278.389 | 39.99 | *** |
| F.13 | 766,170.150 | 9,908,195.265 | 40.33 | |
| F.14 | 766,159.885 | 9,908,142.733 | 40.11 | |
| F.15 | 766,148.159 | 9,908,101.969 | 38.62 | <u> </u> |
| F.16 | 766,155.885 | 9,908,035.094 | 39.30 | |
| F.17 | 766,180.945 | 9,907,947.871 | 40.30 | |
| F.18 | 766,188.689 | 9,907,920.397 | 39.46 | |
| F.19 | 766,227.933 | 9,907,826.901 | 39.40 | |
| F.20 | 766,252.050 | 9,907,774.881 | 39.80 | |
| F.21 | 766,273.531 | 9,907,711.093 | 39.60 | |
| F.22 | 766,293.097 | 9,907,694.087 | 41.98 | |
| F.23 | 766,299.774 | 9,907,645.969 | 39.41 | |
| F.24 | 766,315.889 | 9,907,593.395 | 41.44 | ·• |
| F.25 | 766,317.034 | 9,907,563.935 | 40.31 | |
| F.26 | 766,331.122 | 9,907,538.049 | 39.29 | |
| F.27 | 766,353.395 | 9,907,487.341 | 39.78 | |
| F.28 | 766,361.086 | 9,907,463.339 | 42.14 | |
| F.29 | 766,366.919 | 9,907,423.893 | 41.28 | |
| F.30 | 766,399.311 | 9,907,368.484 | 43.36 | |
| F.31 | 766,400.498 | 9,907,348.916 | 40.89 | |
| F.32 | 766,422.570 | 9,907,297.346 | 43.13 | |
| F.33 | 766,440.275 | 9,907,254.161 | 39.74 | |
| F.34 | 766,467.227 | 9,907,198.011 | 39.41 | |
| F.35 | 766,502.759 | 9,907,152.694 | 39.66 | ··· |
| F.36 | 766,537.893 | 9,907,130.523 | 39.18 | |
| F.37 | 766,578.225 | 9,907,118.959 | 40.93 | |
| F.38 | 766,618.101 | 9,907,093.713 | 39.92 | |
| F.39 | 766,654.839 | 9,907,074.317 | 39.58 | |

ROUTE: F

| NO. | E | N | н | REMARKS |
|-------|-------------|---------------|-------|---------|
| F.40 | 766,719.544 | 9,907,059.744 | 39.35 | |
| F.41 | 766,796.404 | 9,907,046.606 | 39.82 | |
| F.42 | 766,842.524 | 9,907,036.371 | 40.71 | |
| F.43 | 766,959.813 | 9,907,022.524 | 40.80 | |
| F.44 | 767,004.927 | 9,907,000.844 | 40.35 | |
| F.45 | 767,038.742 | 9,906,963.204 | 39.51 | |
| F.46 | 767,062.894 | 9,906,946.165 | 44.80 | |
| F.47 | 767,115.163 | 9,906,910.584 | 40.21 | |
| F.48 | 767,151.660 | 9,906,892.118 | 40.07 | |
| F.49 | 767,197.818 | 9,906,670.375 | 39.35 | |
| F.50 | 767,201.736 | 9,906,639.724 | 40.97 | |
| F.51 | 767,166.095 | 9,906,561.541 | 40.72 | • |
| F.52 | 767,117.560 | 9,906,474.006 | 42.09 | |
| F.53 | 767,164.278 | 9,906,456.266 | 42.81 | |
| F.54 | 767,207.879 | 9,906,448.230 | 41.99 | |
| F.55 | 767,241.061 | 9,906,450.080 | 44.16 | |
| F.56 | 767,303.887 | 9,906,450.066 | 43.30 | |
| F.57 | 767,329.856 | 9,906,455.390 | 46.49 | |
| F.58 | 767,387.196 | 9,906,438.193 | 48.20 | |
| F.59 | 767,581.742 | 9,906,081.856 | 39.93 | |
| F.60_ | 767,603.857 | 9,906,045.861 | 42.66 | |
| F.61 | 767,604.372 | 9,906,008.041 | 42.80 | |
| F.62 | 767,615.051 | 9,905,974.455 | 41.40 | |
| F.63 | 767,615.684 | 9,905,908.752 | 40.26 | |
| F.64 | 767,588.489 | 9,905,876.352 | 42.07 | |
| F.65 | 767,583.901 | 9,905,838.000 | 41,23 | |
| F.66 | 767,565.011 | 9,905,791.941 | 41.69 | |
| F.67 | 767,519.201 | 9,905,774.766 | 41.32 | |
| F.68 | 767,485.642 | 9,905,753.098 | 40.65 | |
| F.69 | 767,437.558 | 9,905,739.162 | 40.71 | |
| F.70 | 767,407.342 | 9,905,688.259 | 41.11 | |
| F.71 | 767,319.509 | 9,905,632.931 | 41.76 | |
| F.72 | 767,260.506 | 9,905,579.550 | 44.99 | |
| F.73 | 767,222.132 | 9,905,564.008 | 41.86 | |
| F.74 | 767,188.403 | 9,905,532.438 | 42.15 | |
| F.75 | 767,086.656 | 9,905,527.406 | 43.09 | |
| F.76 | 767,035.632 | 9,905,514.034 | 48.28 | |
| F.77 | 766,992.697 | 9,905,486.507 | 47.59 | |
| F.78 | 766,963.673 | 9,905,459.676 | 43.28 | |

ROUTE: F

| NO. | E | N | H | REMARKS |
|--------|-------------|---------------|--------|---------|
| F.79 | 766,944.377 | 9,905,437.586 | 46.19 | |
| F.80 | 766,913.218 | 9,905,404.129 | 40.99 | |
| F.81 | 766,881.742 | 9,905,353.516 | 41.28 | |
| F.82 | 766,873.560 | 9,905,318.240 | 42.76 | |
| F.83 | 766,846.794 | 9,905,290.846 | 41.94 | |
| F.84 | 766,820.544 | 9,905,270.464 | 40.60 | |
| F.85 | 766,781.139 | 9,905,251.171 | 40.56 | _ |
| F.86 | 766,720.028 | 9,905,222.565 | 42.15 | |
| F.87 | 766,721.036 | 9,905,148.962 | 43.37 | |
| F.88 | 766,754.660 | 9,905,099.055 | 46.66 | |
| F.89 | 766,786.025 | 9,905,075.426 | 44.10 | |
| F.90 | 766,803.758 | 9,905,048.804 | 44.34 | |
| SPOT-F | 766,803.086 | 9,904,903.652 | 42.051 | PVC |

APPENDIX 11.2

PERMANENT AZIMUTH AND DISTANCE FOR FOLLOWING SURVEY

Permanent Azimuth and Distance For Following Survey

| Point Number | Easting (meter) | Northing (meter) | Elevation (meter) | Azimuth (D M S) | Distance (meter) |
|-----------------|--------------------|---------------------|-------------------|-----------------|---------------------|
| Spot E | 768,359.216 | 9,915,378.500 | 35.120 | | |
| Spot D | 767,274.250 | 9,914,287.846 | 4.237 | | 1,538.401 |
| AC.1 | 766,960.203 | 9,913,952.908 | 5.900 | 223 09 22.57 | 459.139 |
| AC.2 | 767,180.059 | 9,912,286.737 | 4.530 | | |
| PLN.10 | 767,212.272 | 9,912,268.121 | 9.109 | 120 01 25.54 | 37.205 |
| Spot C | 765,734.200 | 9,908,795.803 | 42.568 | • | |
| AB.1 | 765,649.333 | 9,908,798.566 | 42.848 | 271 51 52.96 | 84.912 |