# CHAPTER 5 WATER LEVEL FLUCTUATION IN LAGUNA LAKE DURING FLOOD IN PASIG-MARIKINA RIVER

In order to examine the water level fluctuation of Laguna Lake, and validity of the flood management measures, related data is collected and analyzed such as flow regime of the water fluctuation data of Laguna Lake and both Manggahan Floodway and Napindan Channel during the floods, and the water level fluctuation analysis model of Laguna Lake is built based on the water level fluctuation characteristic of Laguna Lake as follows.

# 5.1 Characteristics of Water Level Fluctuation of Laguna Lake

#### 5.1.1 Available Data

The available data regarding water level of Laguna Lake, rainfall in the basin, inflow discharge to Laguna Lake and flow regimes of Manggahan Floodway and Napindan Channel during floods (occurrence of reverse flow to/from Laguna Lake) are summarized in Table 5.1, Table 5.2, Figure 5.1 and Figure 5.2.

		1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012
	Science Garden	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	X	0	0	0	0	$\bigcirc$	$\bigcirc$	0	$\triangle$	$\times$	$\times$
	Napindan	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\bigcirc$	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\triangle$	$\times$	$\times$	$\times$	$\times$
	Mt.Campana	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\bigcirc$	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\triangle$	$\times$	$\times$	$\times$	$\times$
	Aries	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\bigcirc$	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\triangle$
Rainfall	Nangka	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigtriangleup$	$\triangle$	$\bigcirc$	$\triangle$
Naiman	BosoBoso	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\triangle$	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\triangle$	$\bigcirc$	$\triangle$
	Mt.Oro	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\triangle$	$\bigcirc$	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigtriangleup$	0	$\triangle$	0	$\triangle$
	Sulipan	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$
	Ipo dam	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$
	San Rafael	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$
	Rosario JS	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\triangle$	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\triangle$	$\bigtriangleup$	$\bigcirc$	$\bigcirc$	$\triangle$
	Rosario LS	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\triangle$	$\bigcirc$	$\times$	$\times$	$\times$	$\times$	$\times$
	Napindan JS	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\triangle$	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\times$	$\times$	$\triangle$	$\times$	$\times$
	Napindan LS	$\bigcirc$	$\bigcirc$	$\triangle$	$\triangle$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	0	$\triangle$	$\bigcirc$	$\times$	$\times$	$\times$	$\times$	$\times$
Waterlev	Nangka	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\triangle$	$\triangle$	$\bigcirc$	$\triangle$
el	San Juan	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\triangle$	$\triangle$	$\bigcirc$	$\triangle$
61	Montalban	$\bigcirc$	0	0	$\bigcirc$	$\bigcirc$	0	0	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\triangle$	$\triangle$	$\bigcirc$	0	$\triangle$
	Sto.Nino	$\bigcirc$	0	0	$\bigcirc$	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	0	0	$\bigcirc$	0	0	$\bigcirc$	$\bigcirc$	$\triangle$	$\triangle$	0	$\triangle$
	Pandacan	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\triangle$	$\triangle$	$\bigcirc$	$\bigcirc$	$\triangle$
	Fort Santiago	$\bigcirc$	0	0	0	$\bigcirc$	0	0	$\bigcirc$	0	0	0	0	0	$\bigcirc$	$\triangle$	$\triangle$	$\triangle$	0	$\triangle$
	Angono	$\triangle$	$\bigcirc$	0	0	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	0	0	0	0	0	0	$\triangle$	$\triangle$	$\bigcirc$	0	$\triangle$

Table5.1 Availability of Hourly Rainfall and Water Level Data (EFCOS)

Missing Data percentage : ≧90% ⇒× Missing Data percentage : ≧10% <90% ⇒△ Missing Data percentage : <10% ⇒○

Table 5	5.2 Availability	of Daily	Rainfall Dat	a (PAGASA)	

	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012
Pakil	$\bigcirc$	$\bigcirc$	0	0	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	$\bigcirc$	0	0
NAS	0	0	0	0	0	0	0	0	0	0	0	0	0
SanPedro	×	$\times$	×	×	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	×
NPP	×	$\times$	$\times$	×	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	×
PasigElem	0	0	0	0	0	0	0	0	0	$\times$	$\times$	0	0
Tipas	×	$\times$	×	×	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	$\times$	×
StaMaria	0	0	0	0	0	0	0	0	$\times$	$\times$	$\times$	0	0
StaCruz	0	0	0	0	0	0	0	0	$\bigtriangleup$	$\bigtriangleup$	0	0	0
Missing Data ner	contago	$\cdot > 90\%$	⇒× Mis	sing Dat	a norcon	tago · >	>10% < 9	$0\% \Rightarrow \land$	Missing	Data ner	contago	· < 10%	⇒∩

 $\text{Missing Data percentage} \ : \ \geqq 90\% \Rightarrow \times \ \text{Missing Data percentage} \ : \ \geqq 10\% < 90\% \Rightarrow \triangle \ \text{Missing Data percentage} \ : \ < 10\% \Rightarrow \bigcirc$ 

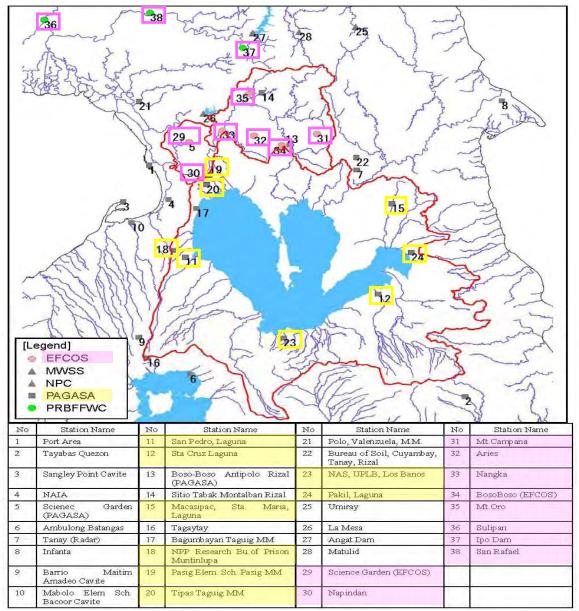


Figure 5.1 Locations of Rainfall Gauging Stations

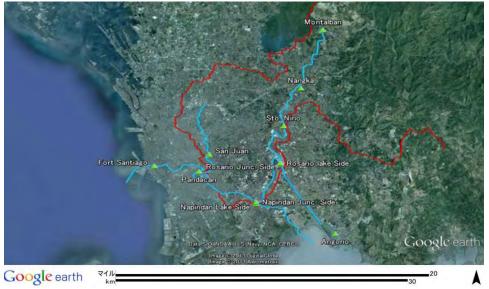


Figure 5.2 Locations of Water Level Gauging Stations

# 5.1.2 Monthly Fluctuation of Water Level

Secular change of monthly variation of water level at Anogono Station from 1994 to 2012 is summarized as follows.

- ➤ Water level of Laguna Lake becomes the lowest in the end of dry season in April or May and becomes the highest in late rainy season in September to January. (Refer to Figure 5.3) The average annual lowest and highest water levels are EL. 10.8m and EL. 12.4m, respectively.
- The average annual lowest water level is almost same as the mean sea level (MSL) of Manila Bay. It means that sea water intrusion to Laguna Lake occurs when high tide in the end of dry season.

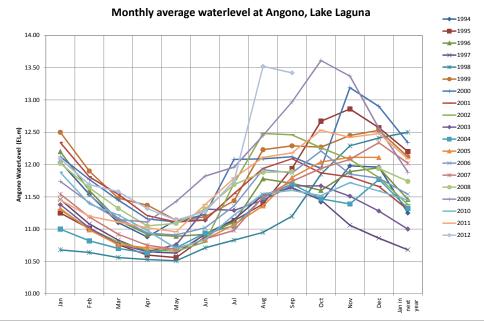


Figure 5.3 Monthly Variation of Water Level in Laguna Lake

# 5.1.3 Water Level Fluctuation during Floods

In order to identify flow regime of Manggahan Floodway and Napindan Channel during floods, difference of water levels of Rosario JS Station for Manggahan Floodway and Napindan JS Station for Napindan Channel against Angono Station are calculated. The hourly fluctuations are shown in Figure 5.4 and 5.5 and the fluctuations of daily mean water level is shown in Figure 5.6 and 5.7. It is noted that the positive number of difference means that water level of Angono is higher.

- Hourly hydrograph in 2004 in which two floods were occurred by the tropical cyclone Wennie in August and the typhoon Yoyong in December is analyzed. During flooding stage, water level of Rosario JS is more sensitive and always higher than Laguna Lake. It is expected that natural discharge to Laguna Lake through Manggahan Floodway always occurs during floods. On the other hand, clear correlation cannot be found between the water levels of Napindan JS and Laguna Lake. It is judged that natural diversion from Pasig River to Laguna Lake through Napindan Channel does not always occur. Using daily mean water level, this tendency is more emphasized.
- Since the hourly water level data of Typhoon Ondoy and Typhoon Pepeng are not available, calculation results using 2009 data is not utilized.

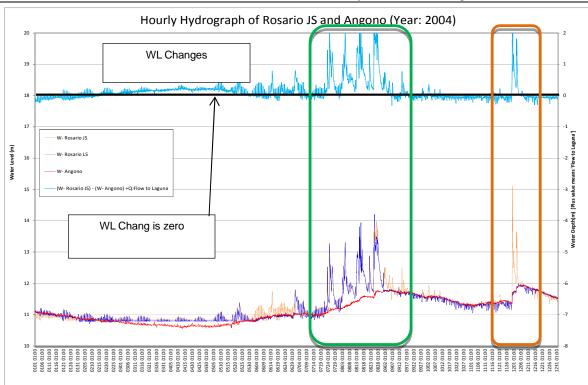


Figure 5.4 Hourly Hydrograph of Rosario JS and Angono (2004)

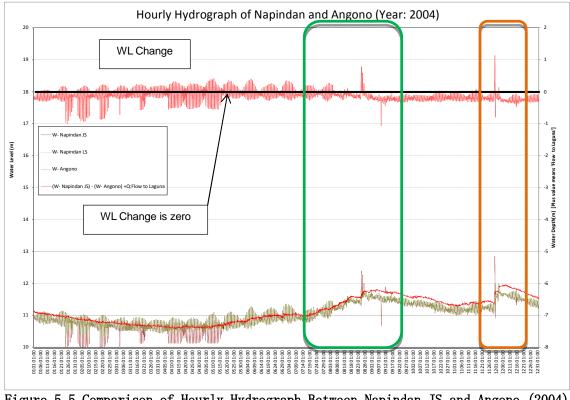


Figure 5.5 Comparison of Hourly Hydrograph Between Napindan JS and Angono (2004)

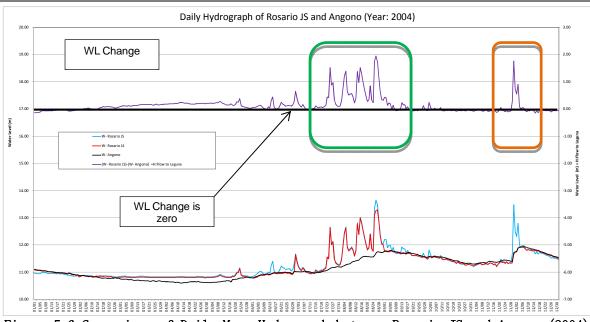
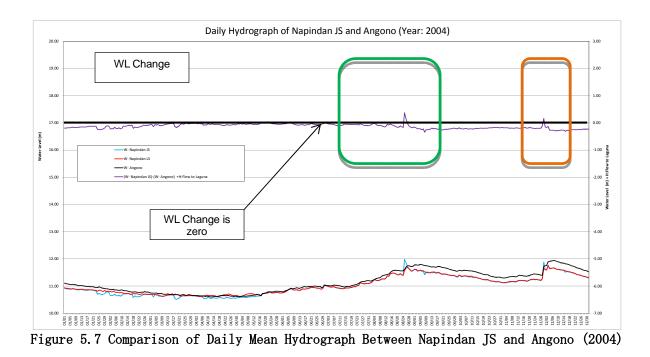


Figure 5.6 Comparison of Daily Mean Hydrograph between Rosario JS and Angono (2004)



## 5.2 Water Level Fluctuation Model

# 5.2.1 Establishment of Analysis Model

## (1) Objective of Modeling

The water level fluctuation model is established in order to analyze the followings.

- Validity regarding that reverse flow to Laguna Lake can be taken into account for flood management plan as proposed in the WB Study
- Effect of inflow from Manggahan Floodway to Laguna Lake to water level fluctuation of Laguna Lake
- Effect of Climate Change to water level fluctuation of Laguna Lake (Change of Evaporation and Rainfall)

# (2) Basic Concepts

- To establish the long-term one dimensional model correlating the water level at Angono, inflow discharge from other tributaries, inflow through Manggahan Floodway, inflow and outflow through Napindan Channel, and evaporation from Lake surface
- Hourly fluctuation of water level is affected by tide level, however, it is considered that daily average can explain the trend of water level fluctuation. Thus, day is applied as the calculation unit of model.
- Inflow discharge from other tributaries is estimated by the rational formula.
- Since the gate operation record during floods is uncertain for Rosario Weir, it is assumed that gate is full open.
- Water level at Napindan Gate has no correlation between the water level of Laguna Lake, and Napindan Gate has not closed since 2008. Thus, for calibration, Napindan Gate is always open.

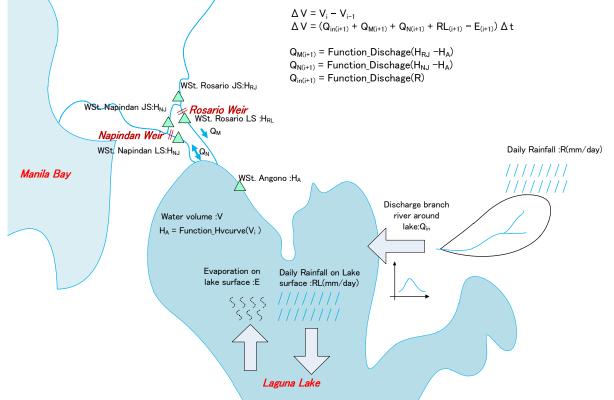


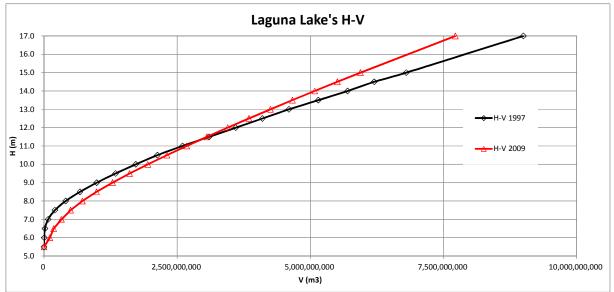
Figure 5.8 Conceptual Figure of Water Level Fluctuation Analysis Model in Laguna Lake

# (3) Model Verification

For verification of the model, 2004 observed data of which condition of data is good and 2009 in which Typhoon Ondoy occurred are used. The model parameters are evaluated and calibrated comparing observed and calculated water level of Laguna Lake.

# (4) Applied H-V Curves of Laguna Lake

Available H-V curves of Laguna Lake are made in 1997 and 2009. Considering the basin characteristics such as construction of lake shore dyke and sedimentation induced by Typhoon Ondoy and Pepeng, the 2009 H-V curve is applied for 2009 data and the 1997 H-V curve is applied for 2004 data. It is noted that the WB Study applied 1997 data for whole period probably since 2009 H-V was not verified at that time.



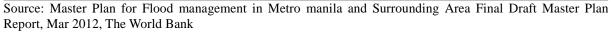
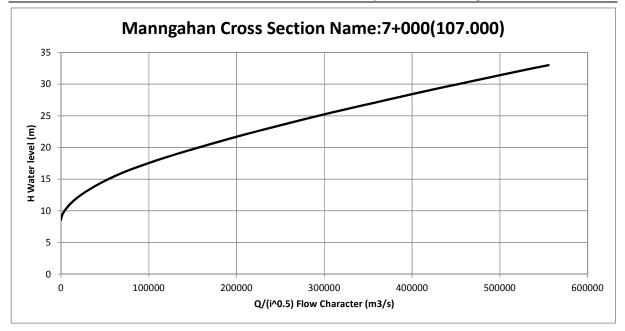


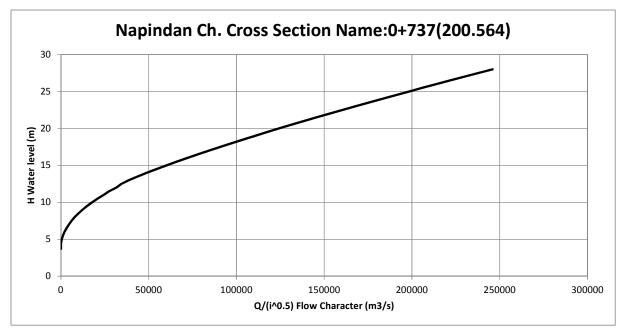
Figure 5.9 Laguna Lake H-V Curve

# (5) Cross Section Property of Manggahan Floodway and Napindan River

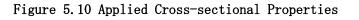
For long term flow regime of Manggahan Floodway and Napindan Channel, cross section property is an important factor to determine discharges as well as difference of water level between Laguna Lake and Pasig-Marikina River since riverbed slopes of both channel are gentle. It is more dominant than gate control of Rosario Weir and NHCS.

The cross section properties shown in Figure 5.10 are selected as typical cross section properties which fluctuation of discharge against fluctuation of water level is low.





Source: JICA Study



# (6) Inflow Rivers to Laguna Lake

Out of 38 sub basins of Pasig-Marikina River Basin which was set by the WB Study, the 23 sub-basins of which rivers directly flows into Laguna Lake are selected as shown in Table 5.3.

SB_ID	NAME	Area (km2)	Longest Flow Path L_r(km)	Elevetion Difference dH(m)	Time of Concentra tion TC(hr)	Lag Time (hr)	MajorRivers
SB - 00	Laguna Lake Surface	870.27	-	-	-	-	
SB - 01	Marikina	538.08	-	-	-	-	Marikina,Wawa
SB - 02	Mangahan	91. 02	4.8	55	1. 14	0. 68	Mangahan, Cainta (Baho), Buli, Mahaba
SB - 03	Angono	86.41	6. 1	74	1.08	0. 65	Angono
SB - 04	Morong	<i>98. 78</i>	23.1	124	<i>3. 25</i>	<i>1. 95</i>	Morong
SB - 05	Baras	22.71	<i>9.2</i>	127	1. 59	0. 95	Baras
SB - 06	Tanay	53.44	18.7	393	2.04	1. 22	Tanay
SB - 07	Pililla	41.19	<i>12.3</i>	162	1.66	1.00	Pililla
SB - 08	Jala - jala	73.12	3.5	57	0. 80	0.48	Jala-Jala
SB - 09	Sta.Maria	204.90	26.0	275	<i>3. 52</i>	<i>2.11</i>	Sta.Maria
SB - 10	Siniloan	74. 31	18.3	449	2.46	1. 48	Romero
SB - 11	Pangil	54.14	12.4	288	1. 77	1.06	Pangil
SB - 12	Caliraya	128.84	16.2	36	2.56	1. 54	
SB - 13	Pagsanjan	311.76	<b>54.</b> 1	581	5.88	3. 53	Pagsanjan
SB - 14	Sta. Cruz	148.35	32.2	675	3. 77	2.26	Sta. Cruz
SB - 15	Pila	90.55	13.1	92	2.08	1. 25	Bancabanca
SB - 16	Calauan	154.82	28.1	238	3. 40	2.04	Bay
SB - 17	LosBanos	102.83	7.0	358	1. 05	0. 63	Maulauen
SB - 18	SanJuan	191.77	39.1	393	4. 33	2.60	SanJuan
SB - 19	San Cristobal	140.66	33.4	511	3. 76	2.26	SanCristobal
SB - 20	Sta. Rosa	120.30	25.3	417	2.85	1. 71	Sta. Rosa
SB - 21	Binan	86.03	31.7	468	3. 38	2.03	Biñan
SB - 22	SanPedro	46.09	33.0	527	3. 21	1. 93	SanPedro
SB - 23	Muntinlupa	43.53	5.1	34	0. 98	0. 59	PasongDiablo
SB - 24	Taguig	45.29	2.4	8	0. 69	0. 41	NapindanChannel
SB - 31	Pasig	102.56	-	-	-	-	Pasig, SanJuan
SB - 32	CoreArea	73.46	-	-	-	-	
SB - 33	Paranaque – LasPinas	115.97	-	-	-	-	Parañaque, Zapote
SB - 34	Malabon – Tullahan	90.06	-	-	-	-	Tullahan
SB - 35	Meycauayan	171.23	-	-	-	-	Meycauayan,Marilao
SB - 36	Bulacan	390.89	51.0	211	6.52	3.91	Bulacan,Sta.Maria
SB - 37	BulacanCoastalArea	67.14	-	-	-	-	Meycauayan
B-103	Laguna Lake Model Catchment ster Plan for Flood manag	2, 410. 84					

#### Table 5.3 Summary of Inflow Rivers to Laguna Lake

Source: Master Plan for Flood management in Metro manila and Surrounding Area Final Draft Master Plan Report, Mar 2012, The World Bank

#### (7) Evaporation of a Laguna Lake

Since the area of Laguna Lake surface is wide as same as the catchment area of lake, rainfall and evaporation from the lake is large enough to be included in the simulation. The area scale of Laguna Lake surface and the area total of inflow river to Laguna Lake is almost equal, therefore, it is considered that the lake surface evaporation other than rain drops on the lake surface cannot be disregarded.

Reference to the WB Study, actual evaporation amount (E) modeled after the instrumental evaporation ( $E_0$ ) of Los Banoz is applied.

$$E = \alpha_1 E_0 \qquad P < 0.5mm/day$$
$$E = \alpha_1 \alpha_2 E_0 \qquad P \ge 0.5mm/day$$
Given  $\alpha_1 = 0.6, \alpha_2 = 0.5$ 

Table 5.4 Instrumental Evaporation ( <i>E</i> <sub>0</sub> ) and Monthly Mean Value (mm	/day)
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Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	0ct	Nov	Dec
4.38	5.70	6.72	7.90	7.31	5.66	4.66	4.50	4.48	4.38	4.19	3.80

Source: Master Plan for Flood management in Metro manila and Surrounding Area Final Draft Master Plan Report, Mar 2012, The World Bank

# (8) Rainfall Data

The applied rainfall stations are 6 stations consisting Pakil, NAS, PasigElem, StaMaria, and StaCruz which are continuously observed since 2000 under PAGASA, and Boso-Boso station under EFCOS to complement northern part of the basin.

Station	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012
Pakil	0	0	0	0	0	0	0	0	0	0	0	0	0
NAS	0	0	0	0	0	0	0	0	0	0	0	0	0
SanPedro	×	×	×	×	×	×	×	×	×	×	×	×	×
NPP	×	×	×	×	×	×	×	×	×	×	×	×	×
PasigElem	0	0	0	0	0	0	0	0	0	×	×	0	0
Tipas	×	×	×	×	×	×	×	×	×	×	×	×	×
StaMaria	0	0	0	0	0	0	0	0	×	×	×	0	0
StaCruz	0	0	0	0	0	0	0	0	Δ	Δ	0	0	0

Table 5.5 Data Availability of Adopted Rainfall Stations operated by PAGASA

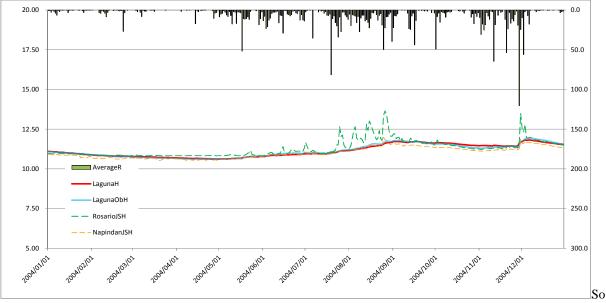
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# 5.2.2 Analysis Results of Laguna Lake Water Level

# (1) Result of Simulation

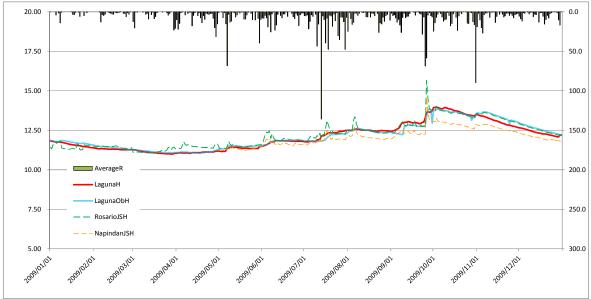
The numerical simulation was performed with the conditions mentioned above.

As shown in Figure 5.11, simulated water level of Laguna Lake well follows the observed water level showing good reproducibility of the model.

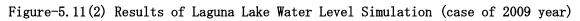


Source: JICA Study

Figure-5.11(1) Results of Laguna Lake Water Level Simulation (case of 2004 year)



Source: JICA Study



# (2) Water Level Fluctuation during Typhoon Ondoy and Pepeng Invasion

Typhoon Ondoy passed through the basin from the east to the west from September 25 to 26, 2009 and Typhoon Pepeng passed the northern part of Luzon Island from east to west with straying in October 3 to 10. The water level of Laguna Lake recorded 13.9m, which is the highest level after Manggahan Floodway construction.

The water levels of Laguna Lake, Rosario JS and Napindan JS during the two typhoons invasion are shown in Figure 5.14. As shown in the figure, water level of Laguna Lake remarkably rose during Typhoon Ondoy and rose again due to Typhoon Pepeng before the water level had fallen after Typhoon Ondoy. Total inflow to Laguna Lake was bigger by Typhoon Ondoy, and water levels of both Rosario JS and Napindan JS were higher than Laguna Lake resulting reverse flow to the lake through Napndan Channel. Based on the analysis of other floods, the situation that the water level of Napindan JS is higher than the lake during floods is very unique case while Rosario JS usually becomes higher than Laguna Lake.

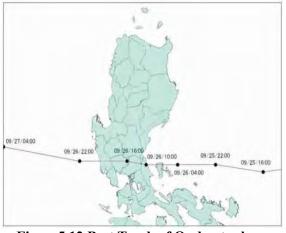
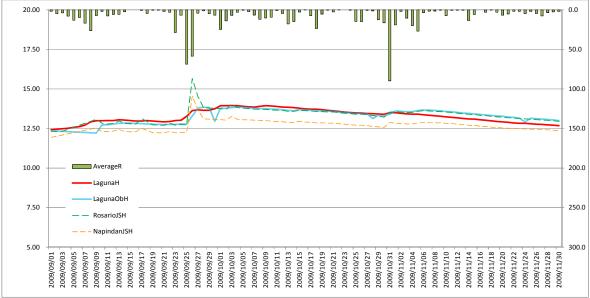


Figure 5.12 Best Track of Ondoy typhoon (T2009-16)



Figure 5.13 Best Track of Pepeng Typhoon (T2009-17)



#### Source: JICA Study

Figure 5.14 Water Level Fluctuation during Typhoon Ondoy Typhoon and Typhoon Pepeng

# 5.2.3 Validity of Including reverse flow (Napindan Waterway) of Laguna in Flood Measure Plan

Based on observed data in 2004 and analysis results in 2004 and 2009, water level of Rosario JS is always higher than Laguna Lake during floods. On the other hand, water level of Napindan JS is lower than Laguna Lake in many cases. Although it becomes higher than Laguna Lake occasionally depending of tidal level, its uncertainty is high to expect as flood control function and it is not recommended to include this phenomena as a flood control measure.

# 5.2.4 Influence of inflow from Pasig-Marikina River to Water Level Fluctuation of Laguna Lake

As discussed in section 4.3.1 (2), 82 % of inflow to Languna Lake during Typhoon Ondoy is came from Laguna Lake Basin, while only 10 % comes through Manggahan Flood way and 8 % comes through Napindan Channel. Based on this simulation results, it is judged that influence of inflow from Pasig-Marikina River is very small to water level fluctuation of Laguna Lake.

#### 5.2.5 Impact of Climate Change

Using the established model, water level of Laguna Lake in 2040 is estimated considering the effects of climate change.

#### (1) Model Parameter of Climate Change

In connection with the climate change currently explained by AR4 of IPCC, it is considered as temperature, rain, and a tide level as an influenced natural phenomena. Among them, although it is thought that it has the indirect influence of a tide level, it is not influenced directly in Laguna Lake. Temperature is also an indirect influence derived from meteorological influence. Change of precipitation and evaporation of the surface of the lake are the most significant impacts.

#### (2) Temperature Rise Influence on Rainfall

The increase ratio of precipitation in Manila and the emission scenario by IPCC is examined.

#### <Emission Scenario>

Out of the several scenarios which reported in the IPCC 4th Assessment Report in 2000, the A1B scenario which assumes realistic social and physical conditions is applied.

#### <Total Amount of Earth Temperature Rise>

The total amount of earth average temperature rises after 100 years (2000 standard) in this scenario is

estimated as 2.8K as optimal value as shown in Table 5.6.

If secular change of temperature rise is linier, temperature rise in 2040 will be set to 1.1K (=2.8K/100\*40). However, A1B scenario shown in Figure 5.15 is curvilinear form. Therefore, the total amount of earth average temperature rises in 2040 is set to 1.3K by direct reading of the graph.

Table 5.6	Rise Prediction of Global Average Ground Temperature and Sea Level Rise Prediction in End
	of the 21st Century

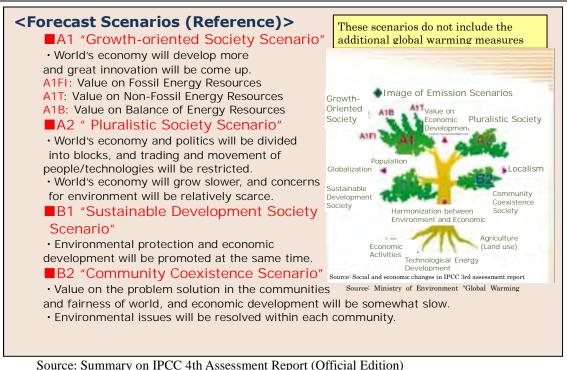
		of the 21st Century	
Scenarios <sup>a)</sup>	of year 2090-20	nperature (difference 199 based on the year 1999 ( $^{\circ}$ C)) <sup>C)</sup>	Sea Level Rise (difference of year 2090-2099 based on the year 1980-1999 (°C))
Scenarios	Best estimate value	Likely forecast range	Forecast range by models (exclusive of mechanical changes of rapid ice discharge)
Steady at the consistence of 2000 <sup>b)</sup>	0.6	0.3-0.9	No data
B1 scenario	1.8	1.1-2.9	0.18-0.38
A1T scenario	2.4	1.4-3.8	0.20-0.45
B2 scenario	2.4	1.4-3.8	0.20-0.43
A1B scenario	2.8	1.7-4.4	0.21-0.48
A2 scenario	3.4	2.0-5.4	0.23-0.51
A1FI scenario	4.0	2.4-6.4	0.26-0.59

Source: Summary on IPCC 4th Assessment Report (Official Edition)

Note: a) Scenarios are six SRES marker scenarios. CO2 conversion consistence (see p.823, 1<sup>st</sup> working group report of 3<sup>rd</sup> assessment report) corresponding to the radiative forcing by man-made greenhouse gas and aerosol are SRES marker scenarios of B1, A1T, B2, A1B, A2 and A1FI, and approximately 600, 700, 800, 850, 1250, 1550ppm respectively.

b) Composition of values of steady at the consistence of 2000 is obtained only by air-sea coupling system model (AOGCM).

c) Temperature is the best estimate value and forecast range of uncertainty obtained by models belonging to various hierarchies regarding constraints by observed values and composite degrees. Changes of temperature are presented as the differences between 1980-1999. To present the changes between 1850-1899,  $0.5^{\circ}$ C will be added.



Greenhouse Gas Emission Scenarios 2000-2100 (without Additional Climate

Policies) and Forecast of Surface Temperature

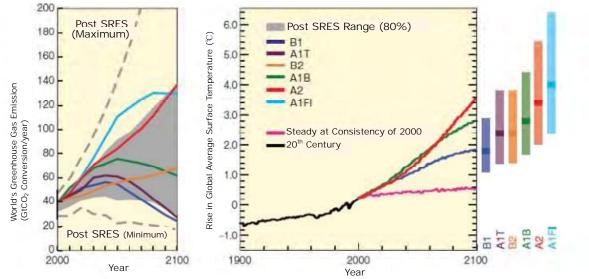


Figure SPM.5. Left Figure: amount of greenhouse emission (CO2 conversion) without additional climate policies: six SRES marker scenarios (colored lines), 80% tile of recent scenarios (post SRES) publicized after SRES (range with grey colored). Dot lines are overall range of results of post SRES scenario. CO2, CH4, N2O and CFC are included in emission amount. **Right Figure**: solid lines show rise in global average surface temperature continued from the condition of 20th century in models of A2, A1B, B1 scenarios. These forecasts are considered with the effects of short-lived greenhouse gas and aerosol. Pink line represents the simulation of air-sea coupling system model (AOGCM) which is sustained steadily at the atmospheric concentration of year 2000, but the scenario. Right belt of the figure indicates best estimation value (horizontal line of each belt) and forecast spread of high possibility from 2090-2099 of 6 SRES scenarios. All temperatures were comparison with 1980-1999.

Source: Summary on IPCC 4th Assessment Report (Official Edition) Figure 5.15 Forecast Scenarios in IPCC 4th Assessment Report

#### <Amount of Temperature Rises and Rate of Precipitation Increase in Manila>

Since the amounts of temperature rises by all the Earth climate change models are all the Earth surface average value, it is necessary to adjust to the area for examination by downscaling. The method of downscaling examines the relation between the amount of global temperature rises and the temperature rises of a local climate model by all the earth climate change models. There is the result of research which considered the relation with the amount of temperature rises in a local climate model according to the major cities until now. The same method also in this study. According to this method, it becomes the amount of rises of 0.883K in Manila to the amount 1.0K of temperature rises of all the earth climate change models. (Refer to Figure 5.16 Inclination of the regression line)

Furthermore, the amount of local temperature rises and the relation of the precipitation rate of increase are also shown. According to the relation, rainfall increases by 8.094% to the amount 1.0K of temperature rises. (Refer to Figure 5.17 inclination of the line)

The amount of temperature rises of Manila in 2040 was set to 1.15K from these relations, and the rainfall rate of increase became 9.3%. (Refer to Table 5.7).

	Value	Remarks
Global mean temperature increase	1.21/	A1B
$\Delta T_{global}[K]$	1.3K	2040 from 2000
$\Delta T_{\rm local} / \Delta T_{global}$	0.883	On Figure- 5.16
Local mean temperature change $\Delta T_{local}[K]$	1.15K	
$\frac{1}{\Delta P_{local}^{extreme}} \left[ \frac{\rho_{6}}{k} \right]$	8.094%/K	On Figure- 5.17
$\frac{\Delta T_{local}[K]}{\frac{1}{\Delta T_{local}} \frac{\Delta P_{local}^{extreme}}{P_{local}^{presentextreme}[\%/K]}$	(0.081)	
Change of precipitation $\Delta P_{local}^{extreme} / P_{local}^{present, extreme} [\%]$	9.3%	
mfuturepresent	· · ·	•

Table 5.7	<b>Rainfall Increment Volume</b>
1	Turning The chiefer of the second

 $\Delta T_{global} \equiv T_{global}^{future} - T_{global}^{present}$  $\Delta P \equiv P^{future} - P^{present}$ 

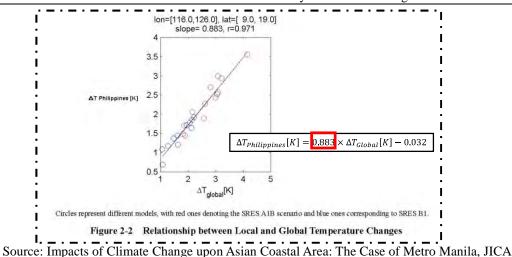
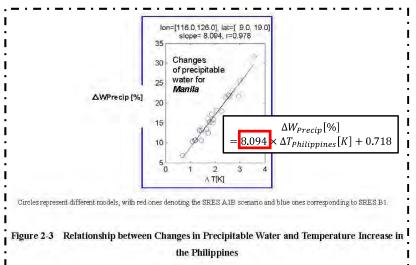


Figure 5. 16 Relation between Amount of Temperature Rises by Earth Models, and Amount of Temperature Rises in Philippines



Source: Impacts of Climate Change upon Asian Coastal Area: The Case of Metro Manila, JICA Figure 5.17 Amount of Temperature rises, and Relation of Rainfall Rate of Increase

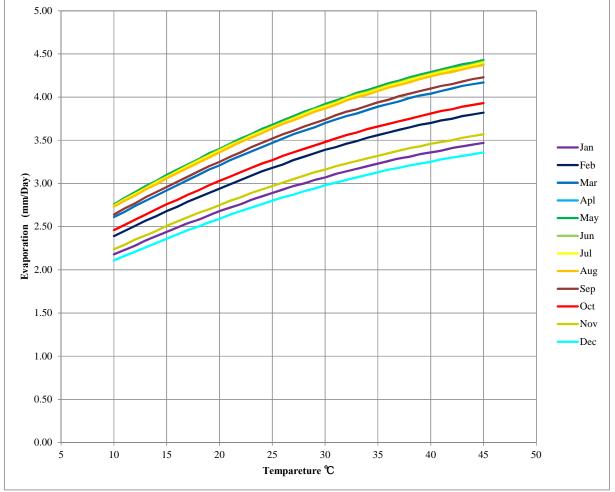
# (3) Influence on Lake Surface Evaporation

The relation between the temperature rise of Manila (N 14.533333") and the amount of evaporation was estimated. For estimation, Makkink Method is applied by which evaporation is estimated by temperature (evaporation of water) and sunshine (outer atmosphere amount of insolation by earth revolution and latitude). The relation between temperature and evaporation is as shown Figure 5.18 and amount of evaporation change per temperature change is summarized in Table 5.8.

Evaporation will increase by 7.1% per 1 degree at the maximum in March - August, and by 4.5% per 1 degree as annual average value. As the results, evaporation rate of increase becomes 5.2% in 2040 since the temperature rises is estimated as 1.15 degree.

Table	5.8 Amount	of Mon	thly E	vapor	ation	chang	ge to 1	°Cof	Temp	eratu	re Ris	es (M	anila)	
	Unit	EMAK Jan	Feb	Mar	Apl	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Anuualy Average
Eby Makkink Method														
Max	mm/day/1°C	0.06	0.06	0.07	0.07	0.07	0.07	0.07	0.07	0.07	0.06	0.06	0.05	0.07
Min	mm/day/1°C	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02
Ave	mm/day/1°C	0.04	0.04	0.04	0.05	0.05	0.05	0.05	0.05	0.05	0.04	0.04	0.04	0.05
Pan Evaporation at Los Banos														
Present	mm/day	4.38	5.70	6.72	7.90	7.31	5.66	4.66	4.50	4.48	4.38	4.19	3.80	5.31
Future(Max)	mm/day	4.64	6.04	7.19	8.45	7.82	6.06	4.99	4.82	4.79	4.64	4.44	3.99	5.66
Future(Min)	mm/day	4.47	5.81	6.85	8.06	7.46	5.77	4.75	4.59	4.57	4.47	4.27	3.88	5.41
Future(Average)	mm/day	4.56	5.93	6.99	8.30	7.68	5.94	4.89	4.73	4.70	4.56	4.36	3.95	5.55
Rate of Future and Present														
Max	%	5.9	6.0	7.0	7.0	7.0	7.1	7.1	7.1	6.9	5.9	6.0	5.0	6.5
Min	%	2.1	1.9	1.9	2.0	2.1	1.9	1.9	2.0	2.0	2.1	1.9	2.1	2.0
Ave	%	4.1	4.0	4.0	5.1	5.1	4.9	4.9	5.1	4.9	4.1	4.1	3.9	4.5

Source: JICA Study



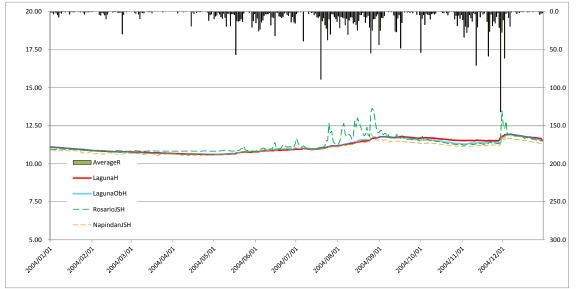
Source: JICA Study Figure 5. 18 Relation between the monthly temperature in Manila, and an amount of evaporation (Makkink method)

#### (4) Influence on Laguna Lake accompanying a climate change

Based on the aforementioned assumptions of rainfall and evaporation increases, water level of Laguna Lake is estimated for 2040.

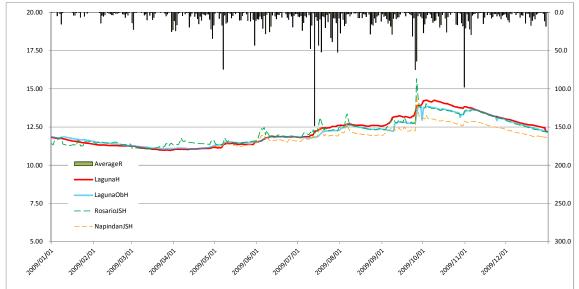
As a result, 11.82 m of simulated high water level in 2004 becomes 11.93 m (+0.11 m) and 13.96 m of simulated high water level during Typhoon Ondoy invasion in 2009 becomes 14.25 m (+0.29m).

At the observed water level base, 11.94m in 2004 becomes 12.05m and 13.85m in 2009 becomes 14.14m.



Source: JICA Study

Figure 5.19 (1) Result of Laguna Lake Water Level Analysis (2004 Year, Climate Condition in 2040 Year)



Source: JICA Study

Figure 5.19 (2) Result of Laguna Lake Water Level Analysis (2009 Year, Climate Condition in 2040 Year)

#### 5.3 Examination Validity of Flood Management Measures

Based on the aforementioned examination, validity of the proposed flood management measures in this Study which discussed in Chapter 4 is confirmed in the aspect of effect to the water level of Laguna Lake.

#### (1) Include reverse flow (Napindan Channel) to Laguna Lake in a flood measure plan.

➢ In Napindan JS, the water level may become higher than Laguna Lake in some cases. However, the uncertainty of the flood regulation from a relation with a tide level is high, and it is not recommended to consider as a flood management measure.

#### (2) Factor of a Laguna Lake water level rise

- The factor of a water level rise of Laguna Lake can be judged from the comparison result of amount of flood discharge. It is that the rainfall to the inflow river and the surface of Laguna Lake occupies about 80%.
- Balance of Marikina river catchment area: about 538 km2 and Laguna Lake surface of lake area: about 870km<sup>2</sup>, inflow river (excluding Pasig-Marikina River) catchment area about 2,410km<sup>2</sup>.
- > The influence of Pasig-Marikina River is small as a factor of a water level rise of Laguna Lake.

# 5.4 Remarks on Effect of Global Warming

Countermeasure against lake water rise is currently on-going. It is found that simulated highest water level of the lake becomes EL. 14.25m increasing 0.29m as an effect of global warming. It is recommended to take another countermeasures such as heightening by parapet wall and so on.

# **CHAPTER 6 CLIMATE CHANGE EFFECT**

# 6.1 Change of Flood Safety Degree

Increase of discharge and decline of flood safety degree are confirmed.

As discussed in Section 5.2.5, rainfall will increase about 10% in 2040 as a climate change impact, and rise of water level in Laguna Lake is expected to 29 cm as maximum. Besides, it is estimated based on the 4th IPCC report that tide level in Manila Bay rises about 22 cm.

Change of probable discharge is analyzed by simulation with inputting such increases as shown in Table 6.1. It is noted that river conditions as of Phase IV completion is applied for evaluation.

Simulation case	Temperature rise (°C)	Increased rate of rainfall(%)	Sea-level-rise (cm)	Laguna Lake- Water-level-rise(cm)
No Climate Change (Present conditon (2013))	0	-	-	-
After Climate Change* (2040)	1.3	9.3	22	29

Table 6.1 Boundary Conditions by Climate Change

Note:Climate Change Scenario:A1B

Sea-level-rise: 22cm = 48cm(2100)/2.8K(2100)×1.3K(2040)

Laguna Lake water-level-raise: from Chapter 5

Source: JICA Study Team

Probable peak discharges at Sto.Nino is shown in Table 6.2. Peak discharges increase about 17 % for 1/30 years flood and about 10 % for 1/100 years flood.

Therefore, safety degree of 1/30 years decline to 1/20 years and 1/100 years decline to 1/60 years.

Return Period	(A)No Climate Change (Present condition)	(B)After Climate Change	(C)=(B)-(A)	(B)/(A)
2	1,510	1,620	110	107%
5	2,090	2,300	210	110%
10	2,710	2,760	50	102%
20	2,900	3,110	210	107%
30	3,100	3,350	250	108%
50	3,370	3,550	180	105%
100	3,610	3,690	80	102%

 Table 6.2 Probable Peak Discharges at Sto.Nino Station

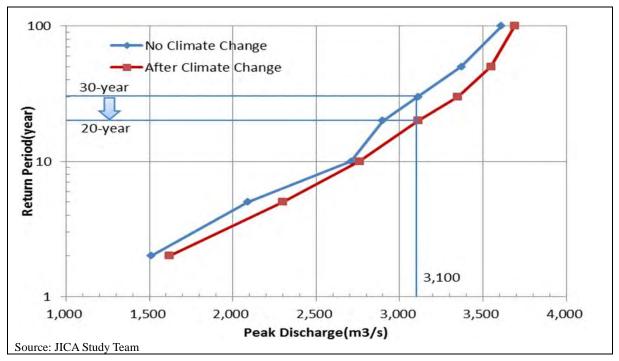


Figure 6.1 Relation between Probability and Peak Discharge

# 6.2 Change of Inundation by Climate Change after Phase IV Project Completion

Changes of inundation for 1/30 years flood and 1/100 years flood by the climate change under the conditions after Phase IV Project completion.

The simulation results are summarized in Table 6.3 and shown in Figure 6.2 to 6.5. Inundation areas increase about 1.26 times for 1/30 years flood and about 1.12 times for 1/100 years flood. On the other hand, inundation depths decrease about 15 cm for 1/30 years flood and about 9 cm for 1/100 years flood due to spread of inundation areas induced by increase of discharges.

Return Period (year)	Content	(A)No Climate Change (Present condition (2013))	(B)After Climate Change* (2040)	(B)-(A)	(B)/(A)
20	Inundation Area (km <sup>2</sup> )	10.38	15.03	4.65	1.45
30 (km) Average Inundat Depth(m)	Average Inundation Depth(m)	2.87	2.36	-0.51	0.82
100	Inundation Area (km <sup>2</sup> )	26.54	31.53	4.99	1.19
100	Average Inundation Depth(m)	1.69	1.62	-0.08	0.96

# Table 6.3 Impact of Climate Change

# [Phase IV Completed: 1/30 Years Flood]



Figure 6.2 Inundation Area by 1/30 Years Flood Without Climate Change Effect

[Phase IV Completed: 1/30 Years Flood with Climate Change]

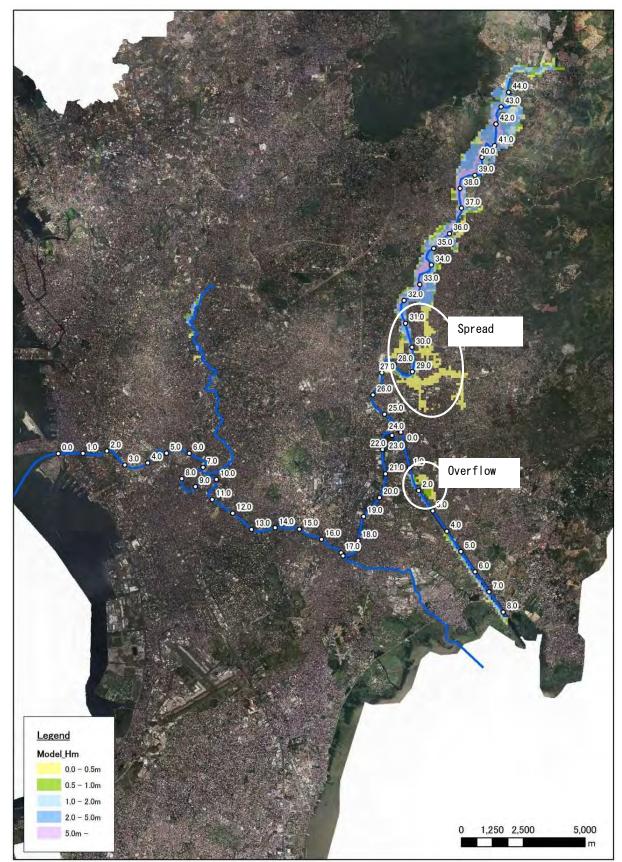


Figure 6.3 Inundation Area by 1/30 Years Flood With Climate Change Effect

# [Phase IV Completed: 1/100 Years Flood]

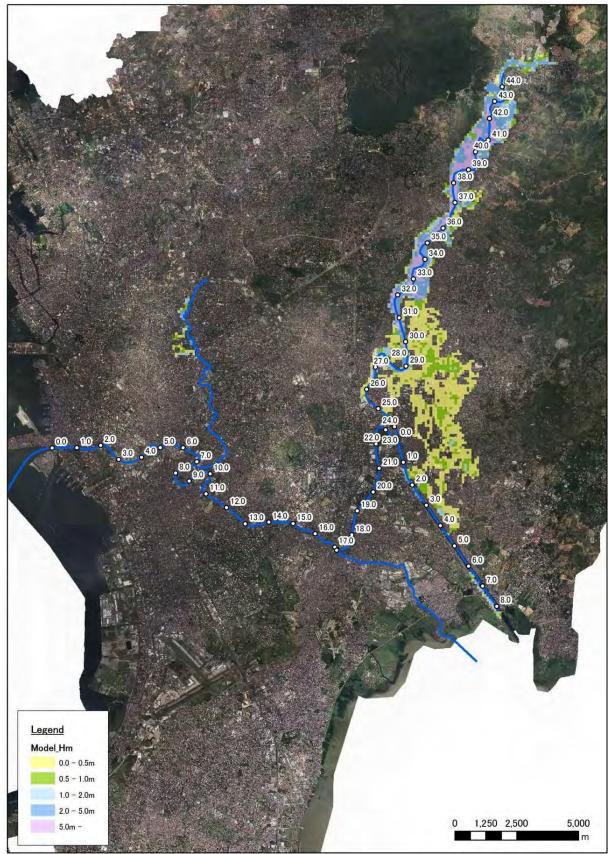


Figure 6.4 Inundation Area by 1/100 Years Flood Without Climate Change Effect

[Phase IV Completed: 1/100 Years Flood with Climate Change]

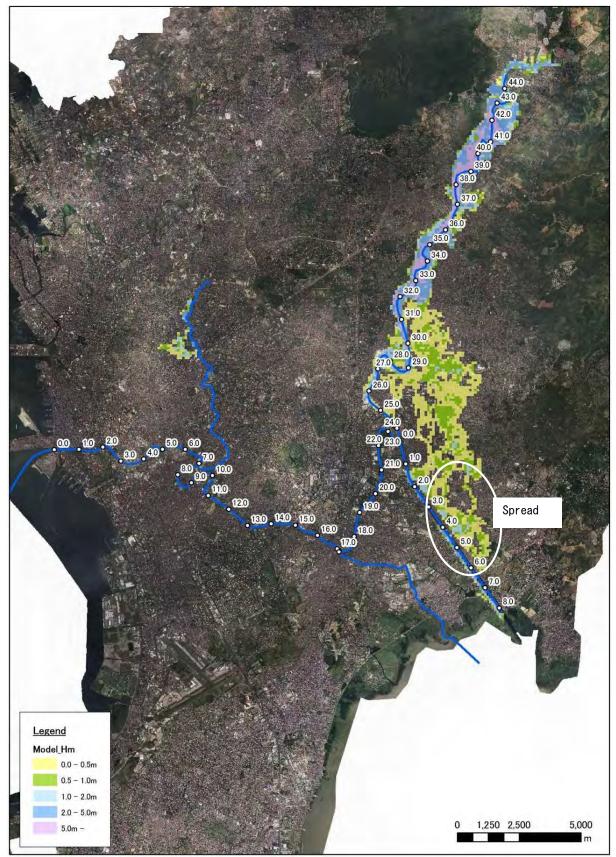


Figure 6.5 Inundation Area by 1/100 Years Flood With Climate Change Effect

#### 6.3 Adaptation Measures against Climate Change

It is expected that peak discharge at Sto.Nino increases about 10 %. Both structural and non-structural measures are required to adapt the climate change.

#### 6.3.1 Structural Measures

Possible structural adaptation measures for the alternatives of flood management measures are listed in Table 6.4 and 6.5.

The adaptation structural measures can be categorized into the measures upstream and downstream of MCGS. And the measures upstream of MCGS can be divided into the measures for flood control facilities upstream of Sto.Nino and increase of diversion discharge to Laguna Lake. As the measures upstream of Sto.Nino, increase of capacities of retarding basins, improvement of flood control function of dam and additional dam. The increase of diversion discharge can be achieved by increase of flow capacity of Manggahan Floodway such as dredging, and new floodway construction.

The adaptation measures downstream of MCGS is mainly the measures to reduce inflow discharge from San Juan River such as underground floodway, underground storage and runoff control facilities such as retarding storage, rainwater storage and infiltration facilities.

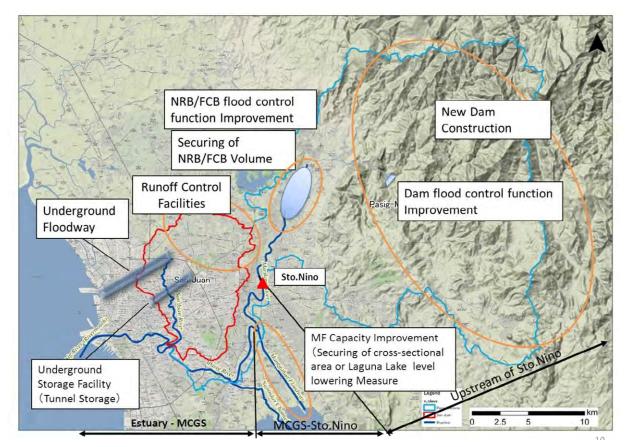


Figure 6.6Possible Structural Adaptation Measures

Alternative	A-1	A-2-1	A-3	A-2-2	
Upper Upper Marikina River	Dam + Natural Retarding Basin	Channel Improvement + Dam	Channel Improvement + Dam + Retarding Basin	Channel Improvement + Dam <sup>*</sup>	
(1)Upstream of Sto.Nino					
Heightening of Dam	0	0	0	0	
Improvement of Spillway	0	0	0	0	
New Dam Construction	0	0	0	0	
Secure of Capacity of Retarding Basin	0	-	0	_	
Improvement of Overflow Dyke	0	_	0	_	
(2)MCGS-Sto.Nino					
Improvement of Channel and Manggahan Floodway	0	0	0	0	
Reduce of WL of Laguna Lake	0	0	0	0	
(3)Downstream of MCGS					
Runoff Control Facilities	0	0	0	0	
Underground Floodway	0	0	0	0	
Underground Storage	0	0	0	0	

#### Table 6.4 Available Structural Adaptation Measures for Alternatives A-1 to A-3

\*: Improvement of Retarding Function is also conducted.

Source: JICA Study Team

#### Table 6.5 Available Structural Adaptation Measures for Alternatives O-1 to B-3

Alternative	<b>O</b> -1	O-2	B-1	B-2-1	B-3	B-2-2
Upper Upper Marikina River	Dam + Natural Retarding Basin	Channel Improveme nt + Dam	Dam + Retarding Basin	Channel Improveme nt + Dam <sup>*</sup>	Channel Improveme nt + Dam + Retarding Basin	Channel Improveme nt + Dam <sup>*</sup>
(1)Upstream of Sto.Nino						
Heightening of Dam	0	0	0	0	0	0
Improvement of Spillway	0	0	0	0	0	0
New Dam Construction	0	0	0	0	0	0
Secure of Capacity of Retarding Basin	0	-	0	-	0	_
Improvement of Overflow Dyke	0	-	0	-	0	_
(2)MCGS-Sto.Nino						
Improvement of Channel and Manggahan Floodway	0	0	0	0	0	0
Reduce of WL of Laguna Lake	0	0	0	0	0	0
(3)Downstream of MCGS						
Runoff Control Facilities	0	0	0	0	0	0
Underground Floodway	0	0	0	0	0	0
Underground Storage	0	0	0	0	0	0

\*: Improvement of Retarding Function is also conducted. Source: JICA Study Team

# 6.3.2 Non-Structural Measures

Change of inundation conditions based on comparisons of inundations with and without climate change for 1/30 years flood and 1/100 flood is summarized as follows.

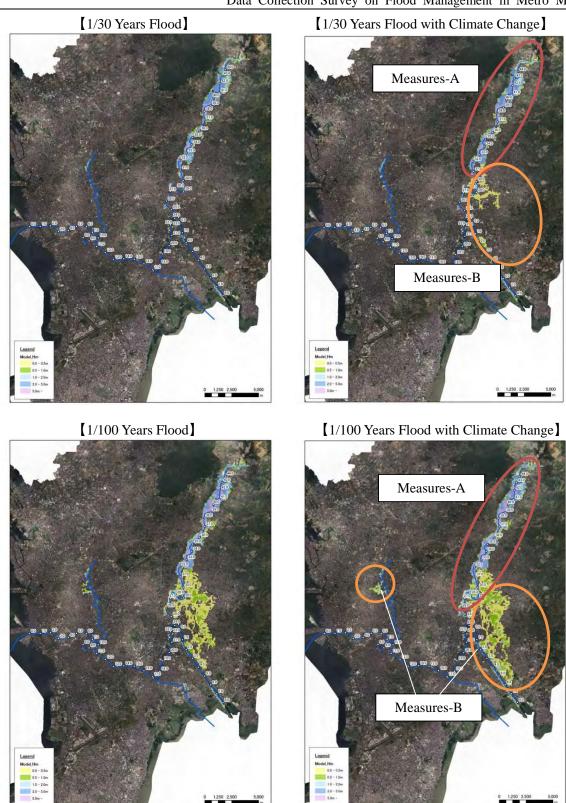
- > Inundation depth increase upstream area of confluence of Nangka River.
- > Inundation depth and inundation area increase between MCGS and confluence of Nangka River.
- > Inundation area increases in San Juan River Basin between the river mouth and MCGS.

As non-structural measures, evacuation system improvement, hazard map and landuse regulation, and conservation of retarding function of basins are considered. Non-structural adaptation measures are examined in the JICA Study as shown in Table 6.6.

Non-structural measures shall be implemented according to change of inundation conditions induced by the climate change. Proposed locations where the non-structural measures shall be implemented is shown in Figure 6.6.

	Adaj	Measures against Increase of Inundation Depth (A)	Measures against Increase of Inundation Area (B)	
		Improvement of Hazard Map and Dissemination	0	0
	Preparedness	Review of Evacuation Routs and Refugees	0	0
Evacuation		Review of Emergency Relief Goods	0	0
System and		Review of Warning Criteria	-	_
Preparedness	Information System	Improvement of Information System	-	0
		Improvement of Information Board	_	0
	Monitoring & Warning	Improvement of Warning Posts	-	0
		Installation of CCTV	-	0
		Installation of Simple Monitoring System	-	-
Landuse Regulation		Landuse Regulation by LGU	0	0
		Heightening of Road and Housing Area	0	0
		Regulations for conservation of retarding function	0	0

#### **Table 6.6 Proposed Non-Structural Adaptation Measures**



Source: JICA Study Team

Figure 6.7 Possible Non-Structural Adaptation Measures

# CHAPTER 7 CONCLUSION AND RECOMMENDATION

The works in this Study can be broadly categorized into the followings.

- (a) Establishment of hydrological and hydrodynamic flood simulation model with appropriately selected dataset in consideration of the future climate change
- (b) Reevaluation of technical validity of the proposed structural measures in Pasig-Marikina River Basin under the WB Study
- (c) Examination of flood management measures against 1/30 and 1/100 years probable floods and proposal of direction of flood management measures

The conclusion and recommendations of the Study are as follows.

#### 7.1 Conclusion

The results and conclusions of above mentioned work categories are summarized as follows.

#### 7.1.1 Establishment of Hydrological and Hydrodynamic Flood Simulation Model with Appropriately Selected Dataset in Consideration of Future Climate Change

Flood analysis model is established integrating runoff analysis model (WEB-DHM Model), river hydraulic model (one dimensional unsteady flow model) and inundation analysis model (two dimensional unsteady flow model). Since the detailed elevation data named LiDAR data, the latest river section survey, vegetation and landuse data, and timely and spatially varied hydrological data are utilized, accurate model against various types of flood including Typhoon Ondoy is established. Besides, H-Q equation is recalculated based on the detailed section data and discharges are estimated.

#### Flood Analysis Model

WEB-DHM Model is applied for runoff analysis since it can analyze hydrologic cycle among atmosphere, vegetation and soils with high accuracy reflecting the change of runoff pattern by changing of vegetation and landuse of a basin, and time and spatial variations of meteorology.

For river hydraulic model and inundation model, one-dimensional unsteady flow analysis model and two dimensional unsteady flow analysis model are applied, respectively, since effect of water level of Laguna Lake, effects of past and planned river improvement works, and effects of natural or artificial retarding basin can be properly reflected.

#### Verification of Model by Various Types of Floods

The river basin includes the center of Metro Manila in the downstream reach, and the river improvement works have been implemented to secure the safety against 1/30 years probable floods with assuming various types of floods. For examination of flood management measures against 1/100 years probable flood as the future target, various patterns of hyetographs such as high intensity with short period rainfall and long period rainfall including Typhoon Ondoy are utilized for calibration and verification of the model to improve the reproducibility of model.

# **Estimation of Discharge by New H-Q Equation**

Observed water level and discharge date is required for calibration of model parameters. However, there is no recent observed discharge data. H-Q equations have been formulated by previous studies, however, accuracy of high water level is uncertain because there is no observed discharge data. Thus, H-Q equation is re-formulated by non-uniform flow calculation based on the river section data combining LiDAR data and latest survey data, and detailed parameters.

#### 7.1.2 Reevaluation of Technical Validity of Proposed Structural Measures in Pasig-Marikina River Basin under the WB Study

Design discharges of PMRCIP based on the JICA Master Plan in 1990 and the WB Study are shown in Figure 7.1.

PMRCIP proposed diversion to Lower Marikina with 500m<sup>3</sup>/s controlling by MCGS and shut down of

NHCS during flood. On the other hand, the WB proposed that the diversion to Manggahan Floodway was controlled by Rosario Weir only without construction of MCGS, and natural diversion to Napindan Channel with NHCS open was expected.

Based on the analysis utilizing the established flood analysis model with referring the various types of design hyetographs estimated by "the Study of Water Security Master Plan for Metro Manila and its Adjoining Areas" and the results of water level fluctuation analysis of Laguna Lake by this Study, technical validity of these proposals are reevaluated as follows.

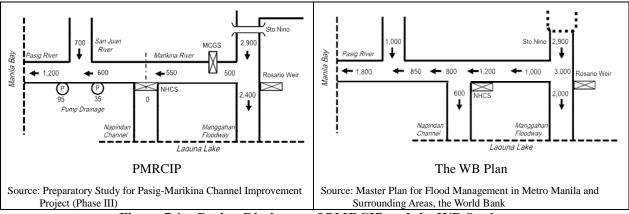


Figure 7.1 Design Discharge of PMRCIP and the WB Study

# (1) Necessity of MCGS Diversion Function

The Study concludes that the proposed flood management measures by the Study including the MCGS function based on the JICA Master Plan is more effective than flood management measures without MCGS, in aspects of reliability, feasibility and step-wise improvement of flood safety. The features of flood management measures with MCGS are as follows.

# <Reliability>

Various types of flood discharges can be securely diverted though Manggahan Flood way by the function of MCGS. As the results, Laguna Lake can be fully utilized as flood control facilities, and flood risk in lower reach can be reduced by controlling flood discharge to the downstream. This flood risk reduction in lower reach also works against excess floods or climate change impacts.

# <*Feasibility*>

The flood management measures with MCGS function is more feasible since it does not reinvestment to the river sections where the river improvement works has been already implemented such as re-improvement of PMRCIP, reconstruction of existing bridges and re-improvement of Napindan Channel.

# <Step-wise Improvement of Flood Safety>

With MCGS, the flood control works can be implemented separately by the upstream and downstream of MCGS since the discharge to downstream can be regulated by MCGS. Thus, improvement works can be implement in upstream sections with maintaining the safety against 1/30 years probable floods in the downstream of MCGS.

Besides, during the course of improvement of each section such as Lower Marikina and Upper-upper Marikina, flood safety can be improved step-wise without temporary decrease of flood safety of the Basin.

# (2) Operation of NHCS

The water level fluctuation analysis in Laguna Lake reveals that the water level at the inlet of Manggahan Floodway (Rosario Weir) is always higher than Laguna Lake while there is no clear correlation between the water levels at the confluence of Napindan Channel and Pasig River (NHCS) and Laguna Lake. It is also founded that impact of inflow discharge from Pasig-Marikina River to water level fluctuation in Laguna Lake is small. Thus, it is concluded that NHCS shall be closed during floods to mitigate increase of flood risk in Pasig-Lower Marikina Basin by preventing discharge from Laguna Lake to Pasig River.

- By closing NHCS, discharge from Laguna Lake to Pasig River is blocked in case the water level of lake is higher than the river, resulting uncertainty of flood management is eliminated.
- In case of natural diversion from Pasig River to Laguna Lake is expected in the flood management plan by opening NHCS, uncertainty of the plan remains since diversion will not occur if the water level of lake is higher than the river. Besides, there are many issues in this option such as a possibility to increase of flood risk in Pasig-Lower Marikina Basin against excess floods, necessity of reinvestment in PMRCIP (Phase II) section, large scale dredging and re-improvement of Napindan Channel which requires large scale land acquisition.

### (3) Dredging of Pasig River

Under the alternative "Without MCGS and NHCS opening", design discharge in Pasig River becomes 1,800m<sup>3</sup>/s which is about 1.5 times of the design discharge by PMRCIP of 1,200m<sup>3</sup>/s. To flow this discharge large scale dredging is required to deepen the riverbed about 2 to 3 m below the design riverbed in the master plan. Tremendous amount of maintenance cost is also required to maintain the riverbed.

In this Study, design discharge with 1/100 years return period becomes 1,400m<sup>3</sup>/s which is 200m<sup>3</sup>/s increase than the previous plan. However, it is within the flow capacity of channel if the riverbed is dredged until the design riverbed level. And scale of dredging works is also small which can be treated as a river maintenance works.

#### 7.1.3 Flood Management Measures for 1/30 and 1/100 Years Probable Floods

Review of hydrology with the latest data, 1/30 years probable flood discharge is estimated at 3,100m<sup>3</sup>/s at Sto.Nino which is larger than the design discharge of PMRCIP at 2,900m<sup>3</sup>/s. As alternatives for 1/30 years probable flood management, 2 alternatives are proposed as well as the PMRCIP plan (Alt-O: Phase IV only), one is enhancement of Manggahan Floodway (Alt-A: Phase IV + Manggahan Floodway) and the other is enhancement of retarding basin (Alt-B: Phase IV + Retarding Basin). And combining "dam" or "dam + retarding basin" options, 10 alternatives for 1/100 years probable flood management are also proposed with step-wise development scenarios from 1/30 probable flood management measures, consisting of 4 alternatives from Alt-A, 2 alternatives from Alt-O and 4 alternatives from Alt-B. (Refer to Figure 7.1) Economic feasibility is confirmed for all alternatives. By applying one of these alternatives, the flood management in Pasig-Marikina River can adapt to impacts of climate change with various options.

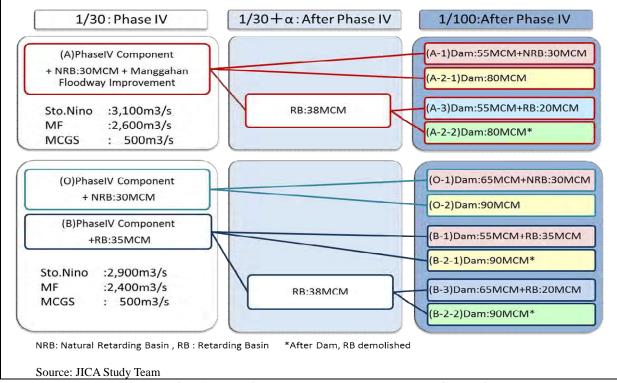


Figure 7.2 Alternatives and Phased Development Scenarios

# 7.2 Recommendations

# 7.2.1 Necessity of Further Studies

This Study is conducted using the various data and information from the previous studies. Thus, it is recommended to conduct further investigations, studies and designs such as follows.

- Optimal Location and Scale of Dam
- Scale and Capacity of Retarding Basin, Area of Natural Retarding Basin
- Design Flood Discharge in Phase IV Section and HWL
- Area of Channel Excavation of Manggahan Floodway

# 7.2.2 Restoration and Improvement of Manggahan Floodway

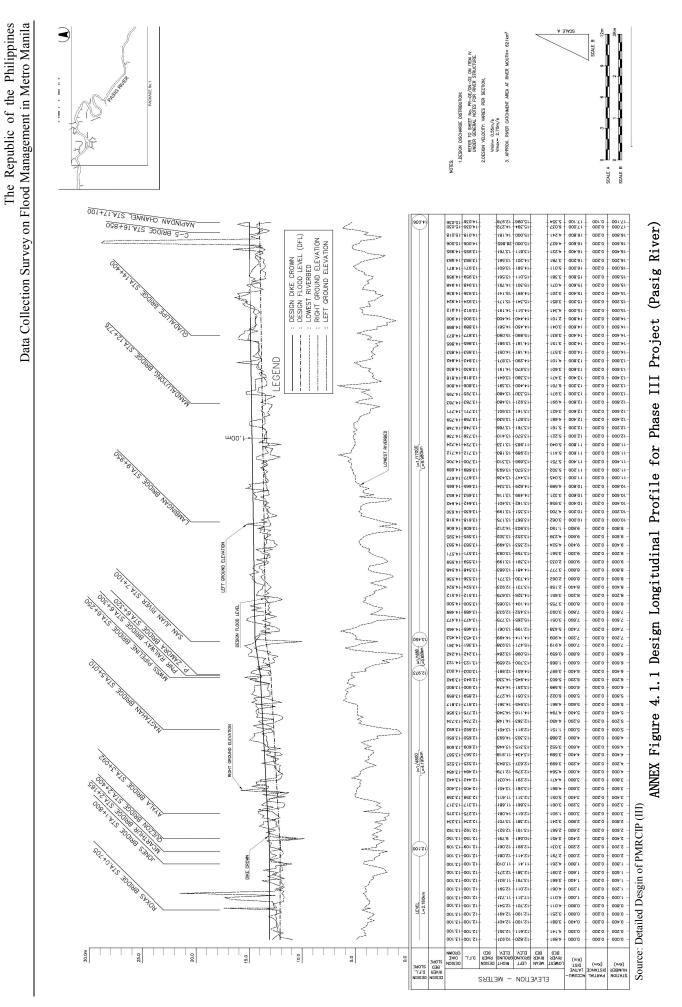
Manggahan Flood way was completed in 1988 with the design discharge of 2,400m<sup>3</sup>/s. However, flow area has been reduced mainly due to houses in river course and sedimentation. To divert flood discharge to Manggahan Floodway by MCGS, restoration of its function is a precondition. Resettlement and dredging shall be implemented to restore the original capacity.

In case of the design discharge at Sto.Nino is 3,100m<sup>3</sup>/s, flow capacity of Manggahan Floodway shall be increased to 2,600m<sup>3</sup>/s with additional 200m<sup>3</sup>/s. Considering excess floods and climate change impacts, capacity improvement of Manggahan Floodway is required. Enlargement of flow capacity of Manggahan Floodway by excavation is relatively easy since earth dyke is applied from Laguna Lake to 5km point.

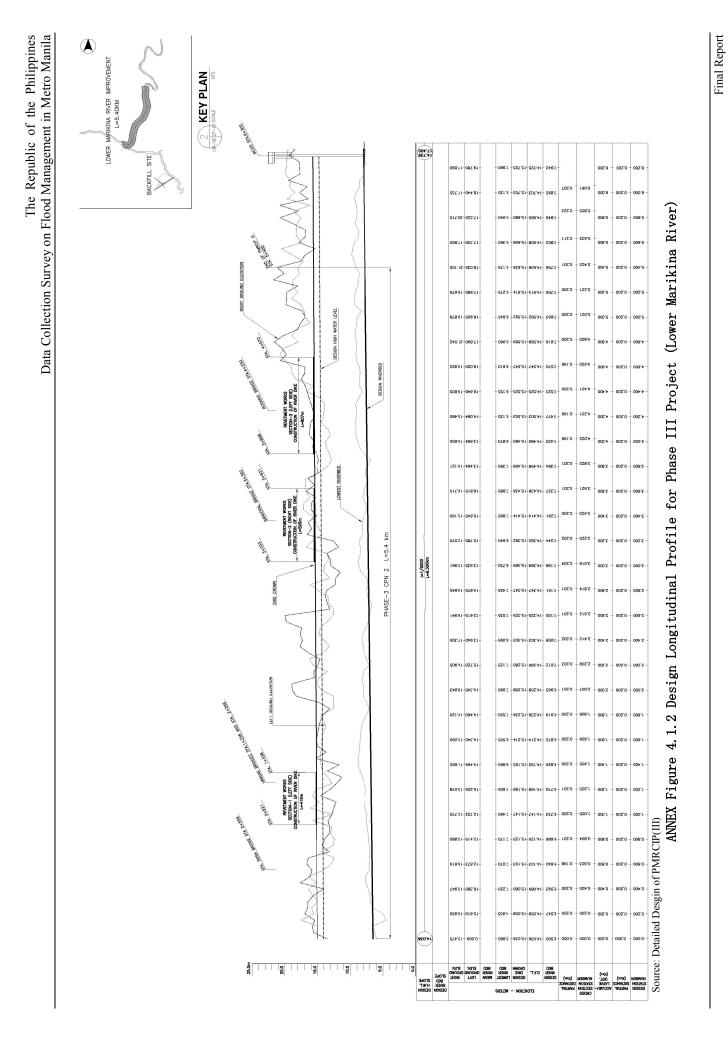
# 7.2.3 Retention of Natural Retarding Function and Necessity of Detailed Investigation of Retarding Basin

The alternatives for 1/100 years probable flood management measures can be divided into "dam" options and "dam + retarding basin" options. Even if a "dam" option is selected, the current natural retarding function shall be maintained since the dam project needs long time. It is needed to fix the area of natural retarding basin and to regulate land use to maintain the natural retarding function.

# APPENDIX I: Figure



Final Report



A-2

APPENDIX II: Table

### ANNEX Table 4.4.1 Breakdown of Project Costs for Each Alternative (2012 Price)

Toral		14,804.5	129.6	2,031.9	518.5	817.2	1,830.2	20,131.9
Dam		-	-	-	-	-	-	-
Upper Upper Marikina River	NRB	-	-	-	-	-	-	-
Upper Marikina River	Phase4	3,078.8	16.2	423.2	105.3	175.9	380.0	4,179.4
Mangahan Floodway	2,400m3/s	3,346.3	91.6	535.4	120.3	167.3	426.1	4,687.0
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0
Pasig River Dredging	1,200m3/s	-	-	-	-	-	-	-
Section	Contents	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Price contingency cost	Total
(O)Phase IV	(1/30(as of 2002))							unit:million peso

### (A)PhaseIV+Mangahan Floodway (1/30(as of 2013))

(A)PhaseIV+Mangahan Floodway	(1/30(as of 2013))							unit:million peso
Section	Contents	Direct construction cost	Compensat ion cost	Engineerin g service cost	Administrati on cost	Physical contingency cost	Price contingenc y cost	Total
Pasig River Dredging	1,300m3/s	993.0	-	158.9	34.8	49.7	123.7	1,360.1
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3
Mangahan Floodway	2,600m3/s	3,625.2	99.2	580.0	130.4	181.3	461.6	5,077.7
Upper Marikina River	3,100m3/s	3,291.1	17.2	452.4	112.6	188.0	406.2	4,467.5
Upper Upper Marikina River	NRB	-	-	-	-	-	-	-
Dam		-	-	-	-	-	-	-
Toral		16,288.7	138.2	2,264.6	570.7	893.0	2,015.6	22,170.8

(B)PhaseIV+Retarding Basin	(1/30(as of 2013))							unit:million peso
Section	Contents	Direct construction cost	Compensat ion cost	Engineerin g service cost	Administrati on cost	Physical contingency cost	Price contingenc y cost	Total
Pasig River Dredging	1,300m3/s	993.0	-	158.9	34.8	49.7	123.7	1,360.1
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3
Mangahan Floodway	2,400m3/s	3,346.3	91.6	535.4	120.3	167.3	426.1	4,687.0
Upper Marikina River	Phase4	3,078.8	16.2	423.2	105.3	175.9	380.0	4,179.4
Upper Upper Marikina River	NRB	-	-	-	-	-	-	-
	RB 5MCM	1,543.5	1,250.0	247.0	99.1	77.2	325.3	3,542.1
Dam		-	-	-	-	-	-	-
Toral		17,341.0	1,379.6	2,437.8	652.4	944.1	2,279.2	25,034.1

ANNEX Table 4.4.2 Breakdown of Project Costs for Each Alternative (2012 Price)

A-1:Dam&NRB	(1/100)							unit:million peso
Section	Contents	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Price contingency cost	Total
Pasig River Dredging	1,400m3/s	1,986.0	-	317.8	69.6	99.3	247.3	2,720.0
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3
Mangahan Floodway	2,600m3/s	3,625.2	99.2	580.0	130.4	181.3	461.6	5,077.7
Upper Marikina River	3,100m3/s	3,291.1	17.2	452.4	112.6	188.0	406.2	4,467.5
Upper Upper Marikina River	NRB	-	21,814.8	-	763.5	-	2,257.8	24,836.1
Dam	Dam 55MCM	8,396.6	-	1,343.5	293.9	419.8	1,045.4	11,499.2
Toral		25,678.3	21,953.0	3,767.0	1,662.9	1,362.4	5,442.4	59,866.0

A-2-1:Dam	(1/100)							unit:million peso
Section	Contents	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Price contingency cost	Total
Pasig River Dredging	1,400m3/s	1,986.0	-	317.8	69.6	99.3	247.3	2,720.0
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3
Mangahan Floodway	2,600m3/s	3,625.2	99.2	580.0	130.4	181.3	461.6	5,077.7
Upper Marikina River	3,100m3/s	3,291.1	17.2	452.4	112.6	188.0	406.2	4,467.5
Upper Upper Marikina River	CI 3,100m3/s	1,475.1	34.6	236.1	52.8	73.8	187.3	2,059.7
	NRB	-	21,780.2	-	763.5	-	2,257.8	24,801.5
Dam	Dam 80MCM	9,261.0	-	1,481.8	324.1	463.1	1,153.0	12,683.0
Toral		28,017.8	21,953.0	4,141.4	1,745.9	1,479.5	5,737.3	63,074.9

A-3:Dam&RB	(1/100)							unit:million peso
Section	Contents	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Price contingency cost	Total
Pasig River Dredging	1,400m3/s	1,986.0	-	317.8	69.6	99.3	247.3	2,720.0
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3
Mangahan Floodway	2,600m3/s	3,625.2	99.2	580.0	130.4	181.3	461.6	5,077.7
Upper Marikina River	3,100m3/s	3,291.1	17.2	452.4	112.6	188.0	406.2	4,467.5
Upper Upper Marikina River	RB 20MCM	2,873.0	2,000.0	459.7	172.6	143.6	570.7	6,219.6
	Cl 3100m3/s	1,475.1	34.6	236.1	52.8	73.8	187.3	2,059.7
	NRB	-	19,780.2	-	763.5	-	2,257.8	22,801.5
Dam	Dam 55MCM	8,396.6	-	1,343.5	293.9	419.8	1,045.4	11,499.2
Toral		30,026.4	21,953.0	4,462.8	1,888.3	1,579.8	6,200.4	66,110.7

A-2-2:Dam*	(1/100)							unit:million peso
Section	Contents	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Price contingency cost	Total
Pasig River Dredging	1,400m3/s	1,986.0	-	317.8	69.6	99.3	247.3	2,720.0
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3
Mangahan Floodway	2,600m3/s	3,625.2	99.2	580.0	130.4	181.3	461.6	5,077.7
Upper Marikina River	3,100m3/s	3,291.1	17.2	452.4	112.6	188.0	406.2	4,467.5
Upper Upper Marikina River	CI 3,100m3/s	1,475.1	34.6	236.1	52.8	73.8	187.3	2,059.7
	NBR	-	19,780.2	-	763.5	-	2,257.8	22,801.5
	RB 8MCM	2,469.6	2,000.0	395.1	158.5	123.5	520.5	5,667.2
Dam	Dam 80MCM	9,261.0	-	1,481.8	324.1	463.1	1,153.0	12,683.0
Toral		30,487.4	21,953.0	4,536.5	1,904.4	1,603.0	6,257.8	66,742.1

\*After Dam, RB demolished

### ANNEX Table 4.4.3 Breakdown of Project Costs for Each Alternative (2012 Price)

ANNEA TABLE 4.4.5 Dreakdown of Project Costs for Each Alternative (2012 Price)										
O-1:Dam&NRB	(1/100)							unit:million peso		
Section	Contents	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Price contingency cost	Total		
Pasig River Dredging	1,400m3/s	1,986.0	-	317.8	69.6	99.3	247.3	2,720.0		
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0		
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2		
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3		
Mangahan Floodway	2,400m3/s	3,346.3	91.6	535.4	120.3	167.3	426.1	4,687.0		
Upper Marikina River	Phase4	3,078.8	16.2	423.2	105.3	175.9	380.0	4,179.4		
Upper Upper Marikina River	NRB	-	21,814.8	-	763.5	-	2,257.8	24,836.1		
Dam	Dam 65MCM	8,767.1	-	1,402.7	306.8	438.4	1,091.5	12,006.5		
Toral		25,557.6	21,944.4	3,752.4	1,658.4	1,354.9	5,426.8	59,694.5		

O-2:Dam	(1/100)							unit:million peso
		Direct	Componention	Engineering	Administration	Physical	Price	
Section	Contents	construction	Compensation cost	Engineering service cost	cost	contingency	contingency	Total
		cost	COSI	Service COSt	COSI	cost	cost	Total 2,720.0 4,063.0 2,899.2 4,303.3 4,687.0 4,179.4 1,926.6 24,803.7
Pasig River Dredging	1,400m3/s	1,986.0	-	317.8	69.6	99.3	247.3	2,720.0
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3
Mangahan Floodway	2,400m3/s	3,346.3	91.6	535.4	120.3	167.3	426.1	4,687.0
Upper Marikina River	Phase4	3,078.8	16.2	423.2	105.3	175.9	380.0	4,179.4
Upper Upper Marikina River	Cl 2,900m3/s	1,379.9	32.4	220.8	49.4	69.0	175.1	1,926.6
	NBR	-	21,782.4	-	763.5	-	2,257.8	24,803.7
Dam	Dam 90MCM	9,631.4	-	1,541.0	337.1	481.6	1,199.1	13,190.2
Toral		27,801.8	21,944.4	4,111.5	1,738.1	1,467.1	5,709.5	62,772.4

ANNEX Table 4.4.4 Breakdown of Project Costs for Each Alternative (2012 Price)

B-1:Dam&RB	(1/100)							unit:million peso
Section	Contents	Direct construction cost	Compensati on cost	Engineering service cost	Administrati on cost	Physical contingency cost	Price contingency cost	Total
Pasig River Dredging	1,400m3/s	1,986.0	-	317.8	69.6	99.3	247.3	2,720.0
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3
Mangahan Floodway	2,400m3/s	3,346.3	91.6	535.4	120.3	167.3	426.1	4,687.0
Upper Marikina River	Phase4	3,078.8	16.2	423.2	105.3	175.9	380.0	4,179.4
Upper Upper Marikina River	NRB	-	20,564.8	-	763.5	-	2,257.8	23,586.1
	RB 5MCM	1,543.5	1,250.0	247.0	99.1	77.2	325.3	3,542.1
Dam	Dam 55MCM	8,396.6	-	1,343.5	293.9	419.8	1,045.4	11,499.2
Toral		26,730.6	21,944.4	3,940.2	1,744.6	1,413.5	5,706.0	61,479.3

B-2-1:Dam*	(1/100)							unit:million peso
Section	Contents	Direct construction cost	Compensati on cost	Engineering service cost	Administrati on cost	Physical contingency cost	Price contingency cost	Total
Pasig River Dredging	1,400m3/s	1,986.0	-	317.8	69.6	99.3	247.3	2,720.0
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3
Mangahan Floodway	2,400m3/s	3,346.3	91.6	535.4	120.3	167.3	426.1	4,687.0
Upper Marikina River	Phase4	3,078.8	16.2	423.2	105.3	175.9	380.0	4,179.4
Upper Upper Marikina River	Cl 2,900m3/s	1,379.9	32.4	220.8	49.4	69.0	175.1	1,926.6
	NBR	-	20,532.4	-	763.5	-	2,257.8	23,553.7
	RB 5MCM	1,543.5	1,250.0	247.0	99.1	77.2	325.3	3,542.1
Dam	Dam 90MCM	9,631.4	-	1,541.0	337.1	481.6	1,199.1	13,190.2
Toral		29,345.3	21,944.4	4,358.5	1,837.2	1,544.3	6,034.8	65,064.5

\*After Dam, RB demolished

B-3:Dam&RB	(1/100)							unit:million peso
Section	Contents	Direct construction cost	Compensati on cost	Engineering service cost	Administrati on cost	Physical contingency cost	Price contingency cost	Total
Pasig River Dredging	1,400m3/s	1,986.0	-	317.8	69.6	99.3	247.3	2,720.0
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3
Mangahan Floodway	2,400m3/s	3,346.3	91.6	535.4	120.3	167.3	426.1	4,687.0
Upper Marikina River	Phase4	3,078.8	16.2	423.2	105.3	175.9	380.0	4,179.4
Upper Upper Marikina River	RB 20MCM	2,873.0	2,000.0	459.7	172.6	143.6	570.7	6,219.6
	CI 2,900m3/s	1,379.9	32.4	220.8	49.4	69.0	175.1	1,926.6
	NBR	-	19,782.4	-	763.5	-	2,257.8	22,803.7
Dam	Dam 65MCM	8,767.1	-	1,402.7	306.8	438.4	1,091.5	12,006.5
Toral		29,810.5	21,944.4	4,432.9	1,880.4	1,567.5	6,172.6	65,808.3

B-2-2:Dam*	(1/100)							unit:million peso
Section	Contents	Direct construction cost	Compensati on cost	Engineering service cost	Administrati on cost	Physical contingency cost	Price contingency cost	Total
Pasig River Dredging	1,400m3/s	1,986.0	-	317.8	69.6	99.3	247.3	2,720.0
Pasig River Phase2	Phase2	3,033.2	10.9	371.2	107.5	170.8	369.4	4,063.0
Lower Marikina River	Phase3	2,164.4	7.7	264.9	76.7	122.0	263.5	2,899.2
MCGS	MCGS	3,181.8	3.2	437.2	108.7	181.2	391.2	4,303.3
Mangahan Floodway	2,400m3/s	3,346.3	91.6	535.4	120.3	167.3	426.1	4,687.0
Upper Marikina River	Phase4	3,078.8	16.2	423.2	105.3	175.9	380.0	4,179.4
Upper Upper Marikina River	CI 2,900m3/s	1,379.9	32.4	220.8	49.4	69.0	175.1	1,926.6
	NBR	-	19,782.4	-	763.5	-	2,257.8	22,803.7
	RB 8MCM	2,469.6	2,000.0	395.1	158.5	123.5	520.5	5,667.2
Dam	Dam 90MCM	9,631.4	-	1,541.0	337.1	481.6	1,199.1	13,190.2
Toral		30,271.4	21,944.4	4,506.6	1,896.6	1,590.6	6,230.0	66,439.6

\*After Dam, RB demolished

Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total
Pasig River Dredging			-	-	-	-
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7
Mangahan Floodway	2,643.6	52.2	637.1	116.7	155.6	3,605.2
Upper Marikina River	2,432.3	9.2	503.6	102.1	163.6	3,210.8
Upper Upper Marikina River	-	-	-	-	-	-
Dam	-	-	-	-	-	-
Total	11,695.6	73.9	2,418.0	502.9	760.0	15,450.3

# ANNEX Table 4.5.1 Result of Economic Evaluation (Case Alternative Plan O) (million pesos)

# ANNEX Table 4.5.2 Result of Economic Evaluation (Case<sup>(2)</sup>) Alternative Plan A)

(million pesc							
Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total	
Pasig River Dredging	784.5	-	189.1	33.8	46.2	1,053.5	
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3	
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4	
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7	
Mangahan Floodway	2,863.9	56.5	690.2	126.5	168.6	3,905.7	
Upper Marikina River	2,600.0	9.8	538.4	109.2	174.8	3,432.2	
Upper Upper Marikina River	-	-	-	-	-	-	
Dam	-	-	-	-	-	-	
Total	12,868.1	78.8	2,694.9	553.6	830.5	17,025.8	

### ANNEX Table 4.5.3 Result of Economic Evaluation (Case③ Alternative Plan B)

(million per						
Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total
Pasig River Dredging	784.5	-	189.1	33.8	46.2	1,053.5
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7
Mangahan Floodway	2,643.6	52.2	637.1	116.7	155.6	3,605.2
Upper Marikina River	2,432.3	9.2	503.6	102.1	163.6	3,210.8
Upper Upper Marikina River	-	-	-	-	-	-
	1,219.4	733.2	293.9	96.1	71.8	2,414.4
Dam	-	-	-	-	-	-
Total	13,699.4	807.1	2,901.0	632.8	878.0	18,918.3

					(m1110	on pesos)
Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total
Pasig River Dredging	1,568.9	-	378.2	67.5	92.3	2,107.0
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7
Mangahan Floodway	2,863.9	56.5	690.2	126.5	168.6	3,905.7
Upper Marikina River	2,600.0	9.8	538.4	109.2	174.8	3,432.2
Upper Upper Marikina River	-	12,434.4	-	740.6	-	13,175.0
Dam	6,633.3	-	1,598.8	285.1	390.4	8,907.6
Total	20,285.9	12,513.2	4,482.7	1,613.0	1,267.0	40,161.8

ANNEX Table 4.5.4 Result of Economic Evaluation (Case Alternative Plan A-1) (million posos)

ANNEX Table 4.5.5 Result of Economic Evaluation (Case<sup>5</sup>) Alternative Plan A-2-1)

(million pesos)							
Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total	
Pasig River Dredging	1,568.9	-	378.2	67.5	92.3	2,107.0	
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3	
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4	
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7	
Mangahan Floodway	2,863.9	56.5	690.2	126.5	168.6	3,905.7	
Upper Marikina River	2,600.0	9.8	538.4	109.2	174.8	3,432.2	
Upper Upper Marikina River	1,165.3	19.7	281.0	51.2	68.6	1,585.9	
	-	12,414.7	-	740.6	-	13,155.3	
Dam	7,316.2	-	1,763.3	314.4	430.7	9,824.6	
Total	22,134.1	<i>12,513.2</i>	4,928.3	1,693.5	1,375.9	42,645.0	

### ANNEX Table 4.5.6 Result of Economic Evaluation (Case<sup>6</sup>) Alternative Plan A-3)

(million pesos						
Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total
Pasig River Dredging	1,568.9	-	378.2	67.5	92.3	2,107.0
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7
Mangahan Floodway	2,863.9	56.5	690.2	126.5	168.6	3,905.7
Upper Marikina River	2,600.0	9.8	538.4	109.2	174.8	<i>3,432.2</i>
Upper Upper Marikina River	2,269.7	1,173.1	547.0	167.4	133.5	4,290.7
	1,165.3	19.7	281.0	51.2	68.6	1,585.9
	-	11,241.7	-	740.6	-	11,982.2
Dam	6,633.3	-	1,598.8	285.1	390.4	8,907.6
Total	23,720.9	12,513.2	5,310.7	1,831.7	1,469.2	44,845.7

					(millio	on pesos)
Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total
Pasig River Dredging	1,568.9	-	378.2	67.5	92.3	2,107.0
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7
Mangahan Floodway	2,863.9	56.5	690.2	126.5	168.6	3,905.7
Upper Marikina River	2,600.0	9.8	538.4	109.2	174.8	3,432.2
Upper Upper Marikina River	1,165.3	19.7	281.0	51.2	68.6	1,585.9
	-	11,241.7	-	740.6	-	11,982.2
	1,951.0	1,173.1	470.2	153.7	114.9	3,862.8
Dam	7,316.2	-	1,763.3	314.4	430.7	9,824.6
Total	24,085.0	12,513.2	5,398.4	1,847.3	1,490.8	45,334.7

# ANNEX Table 4.5.7 Result of Economic Evaluation (Case 7 Alternative Plan A-2-2)

# ANNEX Table 4.5.8 Result of Economic Evaluation (Case® Alternative Plan O-1)

	(million pesos							
Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total		
Pasig River Dredging	1,568.9	-	378.2	67.5	92.3	<i>2,107.0</i>		
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3		
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4		
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7		
Mangahan Floodway	2,643.6	52.2	637.1	116.7	155.6	3,605.2		
Upper Marikina River	2,432.3	9.2	503.6	102.1	163.6	<i>3,210.8</i>		
Upper Upper Marikina River	-	12,434.4	-	740.6	-	13,175.0		
Dam	6,926.0	-	1,669.2	297.6	407.7	9,300.5		
Total	20,190.5	12,508.3	4,465.4	1,608.6	1,260.1	40,032.9		

### ANNEX Table 4.5.9 Result of Economic Evaluation (Case<sup>(9)</sup>) Alternative Plan O-2)

(million pes						
Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total
Pasig River Dredging	1,568.9	-	378.2	67.5	92.3	2,107.0
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7
Mangahan Floodway	2,643.6	52.2	637.1	116.7	155.6	3,605.2
Upper Marikina River	2,432.3	9.2	503.6	102.1	163.6	3,210.8
Upper Upper Marikina River	1,090.1	18.5	262.8	47.9	64.2	1,483.4
	-	12,416.0	-	740.6	-	13,156.6
Dam	7,608.8	-	1,833.8	327.0	447.9	10,217.5
Total	21,963.4	12,508.3	4,892.7	1,686.0	1,364.4	42,414.8

					(millio	on pesos)
Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total
Pasig River Dredging	1,568.9	-	378.2	67.5	92.3	2,107.0
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7
Mangahan Floodway	2,643.6	52.2	637.1	116.7	155.6	3,605.2
Upper Marikina River	2,432.3	9.2	503.6	102.1	163.6	3,210.8
Upper Upper Marikina River	-	11,701.2	-	740.6	-	12,441.8
	1,219.4	733.2	293.9	96.1	71.8	2,414.4
Dam	6,633.3	-	1,598.8	285.1	390.4	8,907.6
Total	21,117.2	12,508.3	4,688.8	1,692.3	1,314.6	41,321.1

### ANNEX Table 4.5.10 Result of Economic Evaluation (Case<sup>®</sup> Alternative Plan B-1)

# ANNEX Table 4.5.11 Result of Economic Evaluation (Case<sup>①</sup> Alternative Plan B-2-1)

						on pesos)
Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total
Pasig River Dredging	1,568.9	-	378.2	67.5	92.3	2,107.0
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7
Mangahan Floodway	2,643.6	52.2	637.1	116.7	155.6	3,605.2
Upper Marikina River	2,432.3	9.2	503.6	102.1	163.6	3,210.8
Upper Upper Marikina River	1,090.1	18.5	262.8	47.9	64.2	1,483.4
	-	11,682.8	-	740.6	-	12,423.4
	1,219.4	733.2	293.9	96.1	71.8	2,414.4
Dam	7,608.8	-	1,833.8	327.0	447.9	10,217.5
Total	23,182.8	12,508.3	5,186.6	1,782.1	1,436.2	44,096.0

# ANNEX Table 4.5.12 Result of Economic Evaluation (Case<sup>(1)</sup>) Alternative Plan B-3)

					(milli	on pesos)
Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total
Pasig River Dredging	1,568.9	-	378.2	67.5	92.3	<i>2,107.0</i>
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7
Mangahan Floodway	2,643.6	52.2	637.1	116.7	155.6	3,605.2
Upper Marikina River	2,432.3	9.2	503.6	102.1	163.6	3,210.8
Upper Upper Marikina River	2,269.7	1,173.1	547.0	167.4	133.5	4,290.7
	1,090.1	18.5	262.8	47.9	64.2	1,483.4
	-	11,242.9	-	740.6	-	11,983.5
Dam	6,926.0	-	1,669.2	297.6	407.7	9,300.5
Total	23,550.3	12,508.3	<i>5,2</i> 75.2	1,824.0	1,457.8	44,615.5

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					(mill	lion pesos)
Section	Direct construction cost	Compensation cost	Engineering service cost	Administration cost	Physical contingency cost	Total
Pasig River Dredging	1,568.9	-	378.2	67.5	92.3	2,107.0
Pasig River Phase2	2,396.2	6.2	441.7	104.3	158.8	3,107.3
Lower Marikina River	1,709.9	4.4	315.2	74.4	113.5	2,217.4
MCGS	2,513.6	1.8	520.3	105.4	168.5	3,309.7
Mangahan Floodway	2,643.6	52.2	637.1	116.7	155.6	3,605.2
Upper Marikina River	2,432.3	9.2	503.6	102.1	163.6	3,210.8
Upper Upper Marikina River	1,090.1	18.5	262.8	47.9	64.2	1,483.4
	-	11,242.9	-	740.6	-	11,983.5
	1,951.0	1,173.1	470.2	153.7	114.9	3,862.8
Dam	7,608.8	-	1,833.8	327.0	447.9	10,217.5
Total	23,914.4	12,508.3	5,362.9	1,839.7	1,479.3	45,104.5

# ANNEX Table 4.5.13 Result of Economic Evaluation (Case<sup>1</sup> Alternative Plan B-2-2)

Image         Image         PRESENT VALLE         CODY         PRESENT VALLE         ODIT         PRESENT VALLE         ODIT         PRESENT VALLE           3014         -         -         3.66         3.46         11         1         1.3.72         3.67           3014         -         -         3.66         2.2.92         3.4         22         3.686         2.2.91           3014         1         2.3.16         11.9.07         -         4.4         22         4.6         2.2.92           3017         1         2.3.15         11.0.37         -         4.4         11         4.6         11           3017         1         2.3.15         5.13         5.73         -         -         4.4         11         4.6         11           3023         5         3.3.15         5.71         -         -         4.4         11         4.6         11           3023         5         3.3.15         5.71         -         -         4.4         11         4.6         11           3023         5         3.3.15         5.70         -         -         4.6         1.6         1.6         1.6         1.6     <	(10 <sup>6</sup> PESOS)											
Image         Image <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>NEFIT</td><td>BEI</td><td></td><td></td></t<>									NEFIT	BEI		
3916         1         1         1         2,163         3,165         3,175           3917         1         2,263         3,263         2,291         36         3,185         3,176           3917         1         2,245         3,663         2,256         46         36         3,185         2,166           3018         1         2,215         11,171         2,663         2,256         46         26         46         20         46         20         46         20         46         20         46         20         46         20         46         21         46         21         46         21         46         21         46         21         46         21         46         21         46         21         46         21         46         41         46	C B-c	B/C	8	Ø	6	5	4	3	2	1	_	Year
3916         1         1         1         2,163         3,165         3,175           3917         1         2,263         3,263         2,291         36         3,185         3,176           3917         1         2,245         3,663         2,256         46         36         3,185         2,166           3018         1         2,215         11,171         2,663         2,256         46         26         46         20         46         20         46         20         46         20         46         20         46         20         46         21         46         21         46         21         46         21         46         21         46         21         46         21         46         21         46         21         46         41         46		-									_	
3015         1         2         30         2.863         3.239         22         30         3.868         3.276           2017         1         2         3.461         2.540         46         30         3.908         2.546           2017         2         2.3151         11.349         46         30         3.908         2.546           2019         2         2.3151         11.349         46         12         46         10         46         11           2021         6         2.2151         6.366         46         13         46         15           2021         6         2.2151         6.366         46         16         46         16         16           2021         2.2156         6.436         46         16         46         10         46         10         46         10           2021         2.156         6.361         46         16         46         10         46         10           2021         13         2.316         5.440         46         46         46         46         46         46         46         46         46         46         46         4									PRESENT VALUE	BENEFIT		
Solie         D. 400         2.521         344         355         3.869         2.546           2011         1         32.115         13.472          6         30         3.000         2.546           2012         1         32.315         10.327          6         30         6         32           2020         2         32.315         10.337          6         10         64         10         64         10         64         10         64         11         64         11         64         11         64         11         64         11         64         11         64         11         64         11         64         11         64         11         64         11         64         11         64         11         64         11         64         11         64 <td>-3, 8</td> <td></td>	-3, 8											
Sh17         I         J <thj< th="">         J         <thj< th=""> <thj< th=""></thj<></thj<></thj<>	-3, 3											
1         1	-2, 9											
1919         2         23.915         11.80         46         22         46         22         46         22           1920         3         23.915         11.39         46         11         46         11         61         11           1922         5         23.915         7.81         46         13         46         13         46         13         46         13         46         13         46         13         46         13         46         11         46         11         46         11         46         11         46         11         46         11         46         11         46         11         46         10         45         66         46         67         72         72         72         45         72         45         72         45         72         45         72         45         72         45         46	-2, 5						2, 540					
3020         3         4         1         4         1         4         1         4         1         4         1         1         4         1         1         4         1         1         4         1         1         4         1         1         4         1         1         4         1         1         4         1         1         4         1         1         4         1         1         4         1         1         4         1	13, 6										_	
3202       4       23.9 15       8.9 1       46       17       46       17         2021       5       23.9 15       7.8 18       46       15       45       15         2024       7       23.9 15       6.7 18       46       11       45       11       45       11         2024       7       23.9 15       5.6 11       46       11       45       11       45       10         2025       8       23.9 15       5.8 10       45       10       45       6       45       6         2028       10       23.9 15       3.80       45       6       45       6	11, 8										_	
3222         5         323 95         7.818         7.818         645         15         45         15           3232         4         23 95         6.709         46         11         45         11           3232         4         23 95         6.709         46         11         45         11           3232         4         23 95         6.40         46         0         46         0         46         0           3242         10         3.915         3.80         46         6         45         6         46         6           3293         12         2.933         3.255         46         5         46         46         6         45         5           3203         16         23.915         1.92         46         46         46         4         45         4         45         3         4         23.915         1.92         46         46         2         46         2         46         2         46         2         45         2         45         2         2         2         2         2         45         2         45         2         2         2	10, 3											
1920         6         22.9 H5         6.780	8, 9										_	
1222       2       2.23,915       5.911	7,8											
1925         8         22.9 IS         5.140         Image: constraint of the second seco	6, 7										_	
3222         6         22.9 IS         4.470         6         8         8         8           2021         10         23.9 IS         3.80         46         7         46         7           2021         12         23.0 IS         2.39 IS         2.39 IS         46         6         46         6           2021         12         23.0 IS         2.39 IS         1.380         45         6         46         6           2031         14         23.9 IS         2.222         46         4         46         4           2031         15         2.2.9 IS         1.401         46         3         46         3         45         3           2031         16         2.3.9 IS         1.461         46         2         46         2         46         2           2031         10         23.9 IS         461         46         2         46         2         45         2           21         23.9 IS         463         46         1         46         1         46         1         1           22         23.9 IS         461         45         1         45         1	5, 9											
1922       10       22.3       15       3.887	5, 1											
11       22.0       11       22.0       3.30	4,4											
2929       12       23.3 15       2.9 39       44       6       45       6       6         2830       13       2.3 15       2.2 15       2.56       45       46       46       4         2931       16       2.3 15       1.92       45       4       45       4         2933       16       2.3 15       1.680       45       3       45       3         2935       18       2.3 15       1.461       45       3       45       2         2935       18       2.3 15       1.461       45       2       45       2         2935       19       2.3 15       1.461       45       2       45       2         2935       2       2.3 15       78       45       2       45       2         21       2.3 15       695       45       1       45       1       1         2335       2       2.3 15       786       46       1       45       1         22       2.3 15       778       46       45       1       45       1         24       2.3 15       316       46       46       1       45	3, 8											
2000       13       23.3 15       2.555       45       45       46       46       46         2031       14       23.9 15       2.222       45       44       45       44         2031       15       23.9 15       1.922       45       44       44       45       3         2031       15       23.9 15       1.920       45       2       45       2 <td< td=""><td>3, 3</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	3, 3											
233       14       23.3 fis       2.222       45       46       46       46       46         2032       15       2.3, 415       1, 432       45       3       445       3       445       3         2033       16       2.3, 415       1, 461       445       3       445       3       45       3         2034       17       2.3, 415       1, 105       445       2       45       2       2         2035       18       2.3, 415       1, 105       445       2       45       2       2         2036       12       2.3, 415       535       64       45       1       45       1       1       2         2037       22       2.3, 415       546       45       1       45       1<	2,9											
2022       15       23.3 f5       1.922       16       45       4       45       4         2033       16       23.9 f5       1.60       45       3       45       3         2035       18       23.3 f5       1.27       45       2       45       2         2035       19       23.9 f5       1.77       45       2       45       2         2037       20       23.4 f5       661       45       2       45       2       2         2038       19       23.4 f5       661       45       2       45       2       2         2038       21       23.2 f5       652       45       1       45       1       1         2040       22       23.2 f5       642       45       1       45       1       1         2041       24       23.2 f5       541       45       1       45       1       1         2042       25       23.9 f5       77       45       1       45       1       1         2042       27       23.9 f5       77       45       1       45       1       1         2043	2,5										_	
2033       16       23.915       1.600       45       3       45       3         2034       17       23.915       1.461       45       3       45       3         2035       18       23.915       1.105       45       2       45       2         2036       19       23.915       1.105       45       2       45       2         2037       20       23.915       1.065       45       2       45       2         2037       20       23.915       661       45       2       45       2         2038       21       23.915       760       23.915       760       45       1       45       1         2040       22       23.915       764       45       1       45       1       1       1         2041       24       23.915       740       45       1       45       1       1       1         2041       25       23.915       731       45       1       45       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1	2, 2											
2234       17       22.9 H5       1.4 H5       1.4 H5       1.4 H5       2       4.6       2         2035       16       22.3 H5       1.1 H5       1.4 H5       2       4.6       2         2037       20       23.2 H5       9.61       1.1 H5       1.4 H5       2       4.6       2         2038       21       23.3 H5       9.61       1.4 H5       1.4 H5       1.4 H5       1         2038       22       23.3 H5       726       4.65       1.4 H5       1.4 H5       1         2040       22       23.3 H5       6.52       1.4 H5       1.4 H5       1       1.4 H5       1         2041       24       25       23.3 H5       6.52       1.4 H5       1.4 H5       1       1.4 H5       1         2042       25       23.3 H5       4.4 H5       1.4 H5       1.4 H5       1       1.4 H5       1.4 H5       1       1.4 H5       1       1.4 H5       1       1.4 H5       1       1.4 H5       1.4 H5       1.4 H5       1.4 H5       1.4 H5	1, 9											
2005       16       23,915       1.271       45       2       46       2         2007       19       23,915       1.105       45       2       45       2       45       2         2008       21       23,915       995       455       2       455       2       455       2       455       2       455       2       455       2       455       2       455       1       445       1       1         2040       22       23,915       652       455       1       455       1       455       1       1       1         2041       24       23,915       549       455       455       1       455       1       455       1       1         2042       25       23,915       341       1       455       1       455       1       455       1       1       1       2047       23,915       351       1       1       2047       23,915       351       1       1       2047       30       23,915       351       1       1       2047       30       23,915       351       237       455       1       45       1       45	1, 6											
203         19         23         915         1,105         46         2         45         2           203         20         23,915         685         45         2         45         2           203         21         23,915         726         45         1         45         1         45         1           204         22         23,915         632         46         1         45         1         45         1           204         22         23,915         478         46         1         45         1         45         1           204         25         23,915         478         46         45         1         45         1         45         1           204         25         23,915         314         46         45         1         45         1         1           204         20         23,915         737         45         1         45         1         45         1           204         30         23,915         737         45         0         45         0         45         0           204         31         23,915 <t< td=""><td>1,4</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	1,4											
203         20         22, 915         961          645         2         455         2           2038         22         23, 915         725          455         1         455         1           2040         23         23, 915         725          455         1	1, 2										_	
203       21       22, 23, 915       383        465       2       465       1       465       1         204       23       23, 915       750       672       645       1       465       1       465       1         204       24       23, 915       754       0       645       1       465       1       465       1         204       24       23, 915       741       0       645       1       455       1       455       1         204       22       23, 915       741       0       645       1       455       1       455       1         204       23       23, 915       734       0       645       1       455       1       455       1         204       23       23, 915       734       0       645       0       455       0       455       0         204       33       23, 915       734       0       645       0       455       0       455       0         204       32       23, 915       736       0       645       0       455       0       455       0         20	1,1										-	
233       22       23.915       726       465       1       455       1         2040       24       23.915       632       455       1       455       1         2041       24       23.915       549       455       1       455       1       455       1         2042       25       23.915       478       465       1       455       1       455       1         2043       24       23.915       314       455       1       455       1       455       1         2044       27       23.915       314       455       1       455       1       455       1         2044       27       23.915       237       455       0       455       0       1         2047       30       23.915       207       455       0       455       0       1       0       0       204       32       3.915       186       0       455       0       455       0       1       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0	ç											
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204       24       23,915       549       45       1       45       1       45       1         2042       25       23,915       415       45       1       45       1       45       1         2044       27       23,915       415       45       1       45       1       45       1         2044       27       23,915       314       465       1       45       1       1         2046       29       23,915       273       45       0       45       0       1       1         2047       30       23,915       237       45       0       45       0       1       1       1       2049       32,915       156       6       0       45       0       1       0       1       1       1       2049       32,315       156       45       0       45       0       1       0       1       1       2049       32,315       136       45       0       45       0       1       1       2053       33       23,915       136       1       45       0       45       0       1       2053       36       23,915												
204       25       23,915       478       45       1       45       1       45       1         204       27       23,915       361       45       1       45       1       45       1         2044       27       23,915       361       45       1       45       1       45       1         2045       28       23,915       273       45       1       45       1       45       1         2047       30       23,915       273       45       0       45       0       1	6				-							
204       26       23.915       415       415       1       45       1       45       1         204       27       23.915       361       45       1       45       1       45       1         2046       28       23.915       273       45       1       45       1       45       1         2047       30       23.915       237       45       0       45       0       45       0         2048       32       23.915       237       45       0       45 </td <td>E</td> <td></td>	E											
2044       27       23.915       361       45       45       1       45       1         2045       28       23.915       273       45       1       45       1         2047       30       23.915       273       45       0       45       0         2048       31       23.915       207       45       0       45       0         2048       32       23.915       180       45       0       45       0         2049       32       23.915       180       45       0       45       0         2051       34       23.915       136       45       0       45       0         2052       35       23.915       118       45       0       45       0         2053       36       23.915       78       45       0       45       0         2054       38       23.915       78       45       0       45       0         2055       38       23.915       78       45       0       45       0         2056       41       23.915       59       45       0       45       0	4										-	
2045       28       23.915       314       45       1       45       1       45       1         2047       30       23.915       273       45       0       45       0       0         2048       31       23.915       207       45       0       45       0       45       0         2049       32       23.915       207       45       0       45       0       45       0         2050       33       23.915       180       45       0       45       0       45       0         2051       34       23.915       118       45       0	4										-	
2046       29       23,915       273        465       1       445       1       445       0         2047       30       23,915       237        455       0       455 </td <td>1</td> <td></td>	1											
2047       30       23,915       237       445       0       45       0       45       0         2048       31       23,915       207       445       0       45       0       45       0         2049       32       23,915       180       45       0       45       0       45       0         2050       33       23,915       118       45       0       45       0       45       0         2051       34       23,915       118       445       0       45       0       45       0         2052       35       23,915       118       445       0       45       0       45       0         2053       38       23,915       18       445       0       45       0       45       0         2054       37       23,915       88       23,915       88       23,915       18       45       0       45       0         2055       40       23,915       59       44       45       0       45       0       45       0         2056       41       23,915       51       44       45       0					1						_	
2048       31       23.915       207       445       6       455       6         2049       32       23.915       180       465       0       455       0         2050       33       23.915       116       465       0       455       0         2051       34       23.915       118       465       0       455       0       455       0         2052       35       23.915       118       445       0       455       0	2				1							
2249       32       23.915       180       4       45       0       45       0         2050       33       23.915       156        45       0	2											
205       33       2.3, 915       115        45        45        45         45         45 <td></td>												
2051       34       22,915       116       116       45       0	1											
2052       35       23,915       118       118       45       0       45       0         2053       36       23,915       103       45       0       45       0       45       0         2054       37       23,915       89       45       0       45       0       45       0         2056       38       23,915       78       45       0       45       0       45       0         2056       39       23,915       68       45       0       45       0       45       0         2057       40       23,915       59       45       0       45       0       45       0         2058       41       23,915       51       44       45       0       45       0         2060       43       23,915       39       45       0       45       0												
2053       36       23,915       100       45       0       45       0       45       0         2054       37       23,915       89       45       0       45       0       45       0         2055       38       23,915       78       45       0       45       0       45       0         2056       39       23,915       68       45       0       45       0       45       0         2057       40       23,915       59       45       0       45       0       45       0         2068       41       23,915       51       59       45       0       45       0       45       0         2060       43       23,915       39       44       39       45       0       45       0         2060       43       23,915       34       45       0       45       0	1	1									_	
2054       37       23,915       88 $=$											_	
2055       38 $23.915$ $68$ $100$ $45$ $00$ $45$ $00$ $45$ $00$ 2057       40 $23.915$ $68$ $100$ $45$ $00$ $45$ $00$ $45$ $00$ 2058       41 $23.915$ $55$ $100$ $100$ $45$ $00$ $45$ $00$ $45$ $00$ 2058       42 $23.915$ $55$ $100$ $100$ $45$ $00$ $45$ $00$ $45$ $00$ 2060       42 $23.915$ $33$ $100$ $100$ $45$ $00$ $45$ $00$ $45$ $00$ 2061       44 $23.915$ $33$ $100$ <td>1</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td></td>	1										_	
2056       39 $23,915$ $66$ $100$ $46$ $00$ $45$ $00$ $45$ $00$ $45$ $00$ 2057       40 $23,915$ $59$ $100$ $45$ $00$ $45$ $00$ $165$ $00$ 2058       41 $23,915$ $515$ $100$ $455$ $00$ $455$ $00$ $165$ $00$ 2058       42 $23,915$ $515$ $44$ $100$ $455$ $00$ $455$ $00$ $100$ 2060       43 $23,915$ $34$ $100$ $165$ $00$ $455$ $00$ $1000$ $100$ $100$												
2057       40       23.915       569       1       <												
2058       41       23,915       51 $add$ $addd$ $adddddddddddddddddddddddddddddddddddd$		1										
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$EIRR \qquad \Sigma (B - C) / \Sigma (1 + io)^{t-1} = 0 \qquad 0.635$ $NPV \qquad \Sigma (B - C) / \Sigma (1 + i)^{t-1} \qquad 91,769$	91, 7						12.682				- •	,
NPV $\Sigma (B - C) / \Sigma (1 + i)^{t-1}$ 91,769			,	, 511	200							
							0.035		_ (0 0)/ Z (T T		ľ	
							91 769	i) <sup>t-1</sup>	$\Sigma (B - C) / \Sigma (1 +$	NPV	,	
							51,105		_ (0 0)/2 (1 '		ľ	
B/C Σ (B/(1 + i) <sup>t-1</sup> )/Σ (C/(1 + i) <sup>t-1</sup> ) 8.1							Q 1	$(\Sigma (C/(1 + i))^{t-1})$	$\Sigma (B/(1 + i)^{t-1})$	R/C		

ANNEX Table 4.5.14 Cash Flow	(Case① Alternative Plan O)
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**Note :** Benefit of 1/20 is applied to this case owing to the design flood discharge of 2,900m<sup>3</sup>/s is reevaluated as 1/20 years flood as previously mentioned.

		DE									(10 <sup>6</sup> PESOS)
		(1) BEI	NEFIT ②	3	4	5	6	Ø	8		
Year		U	w.	9	æ	9	۲	W		B/C	B-c
		BENEFIT	PRESENT VALUE	COST	PRESENT VALUE	MAINTENANCE	PRESENT VALUE	COST	PRESENT VALUE		
2014				4, 256	4, 256	12	12	4, 269	4, 269		-4, 26
2015				4, 256	3, 701	25	22	4, 281	3, 723		-3, 72
2016				4, 256	3, 218	37	28	4, 294	3, 247		-3, 24
2017				4, 256	2, 799	50	33	4, 306	2, 831		-2,83
2018	1	25, 671	14,677			50	28	50			14, 64
2019	2	25,671	12, 763			50	25	50			12, 73
2020	3	25, 671	11,098			50	21	50			11,07
2021	4	25, 671	9,651			50	19	50			9,63
2022	5	25, 671	8, 392			50	16	50			8, 3
2023 2024	6	25, 671 25, 671	7, 297 6, 345			50 50	14	50 50	14		7, 2
2024	8	25, 671	5, 518			50	12	50			5, 5
2025	9	25, 671	4, 798			50	9	50	9		4, 7
2027	10	25, 671	4, 172			50	8	50	8		4, 1
2028	11	25, 671	3, 628			50	7	50	7		3, 62
2029	12	25, 671	3, 155			50	6	50	6		3, 14
2030	13	25, 671	2, 743			50	5	50	5		2, 7
2031	14	25, 671	2, 385			50	5	50	5		2, 3
2032	15	25, 671	2, 074			50	4	50	4		2, 0
2033	16	25,671	1, 804			50	3	50	3		1, 80
2034	17	25, 671	1,568			50	3	50	3		1, 5
2035	18	25, 671	1, 364			50	3	50	3		1, 3
2036	19	25, 671	1, 186			50	2	50	2		1, 1
2037	20	25,671	1, 031			50	2	50	2		1, 0
2038	21	25, 671	897			50	2	50	2		8
2039	22	25, 671	780			50	2	50			7
2040	23	25, 671	678			50	1	50			6
2041	24	25,671	590			50	1	50			58
2042	25	25,671	513			50	1	50			51
2043	26	25, 671	446			50	1	50			44
2044	27	25, 671	388			50	1	50			38
2045 2046	28 29	25, 671 25, 671	337 293			50 50	1	50 50			33
2046	30	25, 671	293			50	0	50			2
2047		25, 671	233			50	0	50			21
2049		25, 671	193			50	0	50			1
2050	33	25, 671	168			50	0	50			10
2051	34	25, 671	146			50	0	50			14
2052	35	25, 671	127			50	0	50	0		1:
2053	36	25, 671	110			50	0	50	0		1
2054	37	25, 671	96			50	0	50	0		9
2055	38	25, 671	83			50	0	50	0		
2056	39	25, 671	72			50	0	50			
2057	40	25, 671	63			50	0	50	0		(
2058		25, 671	55			50	0	50			1
2059		25,671	48			50	0	50			
2060		25, 671	41			50	0	50			
2061	44	25, 671	36			50	0	50			
2062		25, 671	31			50		50			
2063		25, 671	27			50		50		1	
2064 2065		25, 671 25, 671	24			50 50		50 50			
2065		25, 671				50		50			
2066						50		50			
2007		1, 283, 543			13, 975			19, 627			98, 1
		EIRR	$\Sigma (B - C) / \Sigma (1 +$		0. 626		312	13, 027	14, 200		30, 1
			∠ (D = V)/∠(I +	-0	0.020						
		NPV	$\Sigma (B - C) / \Sigma (1 +$	i) <sup>t-1</sup>	98, 136						
		B/C	$\Sigma (B/(1 + i)^{t-1})/$	$\Sigma (C/(1 + i)^{t-1})$	7.9						

### ANNEX Table 4.5.15 Cash Flow (Case<sup>2</sup>) Alternative Plan A)

		BE	NEFIT								(10 <sup>6</sup> PESOS)
Year		1	2	3	4	5	6	Ø	8	B/C	B-c
		BENEFIT	PRESENT VALUE	COST	PRESENT VALUE	MAINTENANCE	PRESENT VALUE	COST	PRESENT VALUE		
2014				4, 126	4, 126	12	12	4, 138	4, 138		-4, 13
2015				4, 126	3, 588	24	21	4, 150	3, 609		-3, 60
2016				4, 126	3, 120	36	27	4, 162	3, 147		-3, 14
2017 2018				4, 528 402	2, 977 230	49 50	32	4, 578 453	3, 010 259		-3, 01
2018				402	230	50	29	453	239		-23
2020				402	174	53	23	455	197		-19
2021				402	151	54	20	456	172		-17
2022				402	132	55	18	457	150		-15
2023	1	25, 671	7, 297			55	16	55			7, 28
2024	2	25, 671	6, 345			55	14	55			6, 33
2025	3	25, 671	5, 518			55 55	12	55			5, 50
2026 2027	4	25, 671 25, 671	4, 798 4, 172			55	9	55			4, 78
2027	6	25, 671	4, 172			55	8	55			3, 62
2029	7	25, 671	3, 155			55	7	55			3, 14
2030	8	25, 671	2, 743			55	6	55			2, 73
2031	9	25, 671	2, 385			55	5	55	5		2, 38
2032	10	25, 671	2, 074			55	4	55			2, 07
2033	11	25, 671	1, 804			55	4	55	4		1, 80
2034	12	25, 671	1,568			55	3	55	3		1, 56
2035 2036	13 14	25, 671 25, 671	1, 364 1, 186			55 55	3	55 55	3		1, 36
2036	14	25, 671	1, 186			55	2	55			1, 18
2037	16	25, 671	897			55	2	55	2		89
2039	17	25, 671	780			55	2	55	2		77
2040	18	25, 671	678			55	1	55	1		67
2041	19	25, 671	590			55	1	55	1		58
2042	20	25, 671	513			55	1	55	1		51
2043	21	25, 671	446			55	1	55	1		44
2044	22	25, 671	388			55	1	55	1		38
2045 2046	23 24	25, 671 25, 671	337 293			55	1	55	1		33
2040	24	25, 671	293			55	1	55	1		29
2047	26	25, 671	233			55	0	55	0		23
2049	27	25, 671	193			55	0	55	0		19
2050	28	25, 671	168			55	0	55	0		16
2051	29	25, 671	146			55	0	55	0		14
2052	30	25, 671	127			55	0	55			12
2053	31	25, 671	110			55	0	55			11
2054	32	25, 671	96			55 55	0	55 55	0		9
2055 2056	33 34	25, 671 25, 671	83			55	0	55	0		8
2056	35	25, 671	63			55	0	55			6
2058	_	25, 671	55			55	0	55			5
2059	37	25, 671	48			55	0	55			4
2060	38	25, 671	41			55	0	55	0		4
2061	39	25, 671	36			55	0	55			3
2062	40	25, 671	31			55	0	55			3
2063	41	25, 671	27			55	0	55			2
2064	42 43	25, 671	24			55 55	0	55			2
2065 2066	43	25, 671 25, 671	18			55	0	55			1
2066	44	25, 671	16			55	0	55			1
2068	46	25, 671	14			55	0	55			1
2069	47	25, 671	12			55	0	55			1
2070	48	25, 671	10			55	0	55	0		1
2071	49	25, 671	9			55	0	55			
2072	50	25, 671	8			55	0	55			
		1, 283, 543			14, 698	3, 137	328	22, 056	15, 026		40, 86
		EIRR	$\Sigma (B - C) / \Sigma (1 +$	io) "====0	0.280						
		NPV	$\Sigma (B - C) / \Sigma (1 +$	i) <sup>t-1</sup>	40, 868						
		INI V	∠ (D = V)/∠(I +	17	40, 008						
		B/C	Σ(B/(1 + i) <sup>t-1</sup> )/	$\Sigma (C/(1 + i)^{t-1})$	3.7						

### ANNEX Table 4.5.16 Cash Flow (Case<sup>3</sup>) Alternative Plan B)

1		BEN	IEFIT								
ear		1	2	3	4	5	6	Ø	8	B/C	B-c
		BENEFIT	PRESENT VALUE	COST	PRESENT VALUE	MAINTENANCE	PRESENT VALUE	COST	PRESENT VALUE		
2014				4, 520	4, 520	13	13	4, 533	4, 533		-4, 5
2015				4, 520	3,930	26	23	4, 546	3, 953		-3,
2016				4, 520	3, 418	39	30	4, 559	3, 447		-3,
2017				7,606	5,001	62	40	7,668	5,042		-5, (
2018 2019				3, 087 3, 087	1,765 1,535	71	40 40	3, 157 3, 166	1, 805 1, 574		-1, -1,
2019				3, 087	1, 335	80	38	3, 100	1, 374		-1,
2021				3, 087	1, 160	98	37	3, 184	1, 197		-1,
2022				3, 087	1,009	107	35	3, 193	1,044		-1,
2023				891	253	109	31	1,000	284		-
2024				891	220	112	28	1,002	248		-
2025				891	191	114	25	1,005	216		-
2026				891	166	117	22	1,008	188		-
2027	1	28,937	4, 703			117	19	117	19		4,
2028	2	28,937	4, 090			117	17	117	17		4,
2029	3	28,937	3, 556 3, 092			117	14	117	14		3,
2030 2031	4	28, 937 28, 937	3, 092 2, 689			117	12	117	12		3, 2,
2031	5	28,937	2, 089			117	9	117	9		2,
032	7	28,937	2, 338			117	8	117	9		2.
034	, 8	28,937	1, 768			117	7	117	7		1.
035	9	28,937	1, 537			117	6	117	6		1,
036	10	28,937	1, 337			117	5	117	5		1
037	11	28,937	1, 163			117	5	117	5		1
038	12	28, 937	1, 011			117	4	117	4		1
039	13	28,937	879			117	4	117	4		
040	14	28, 937	764			117	3	117	3		
041	15	28,937	665			117	3	117	3		
042	16	28,937	578			117	2	117	2		
043	17	28,937	503			117	2	117	2		-
044	18	28,937	437			117	2	117	2		-
045	19	28,937	380 330			117	2	117	2		
046 047	20 21	28, 937 28, 937	287			117	1	117	1		-
047	21	28,937	287			117	1	117	1		
049	23	28,937	217			117	1	117	1		
050	24	28, 937	189			117	1	117	1		
051	25	28,937	164			117	1	117	1		
052	26	28,937	143			117	1	117	1		
053	27	28,937	124			117	1	117	1		
054	28	28,937	108			117	0	117	0		_
055	29	28,937	94			117	0	117	0		-
056	30	28,937	82			117	0	117	0		
057	31	28,937	71			117	0	117	0		
058 059	32	28, 937 28, 937	62 54			11/	0	11/	0		-
060	33	28,937	47			117	0	117	0		
061	34	28, 937	47			117	0	117	0		+
062	36	28,937	35			117	0	117	0		1
063	37	28, 937	31			117	0	117	0		
064	38	28,937	27			117	0	117	0		
065	39	28,937	23			117	0	117	0		
066	40	28,937	20			117	0	117	0		
067	41	28,937	18			117	0	117	0		+
068 069	42	28, 937 28, 937	15			117	0	117	0		+
069 070	43 44	28,937 28,937	13			117	0	117	0		+
071	44	28,937	12			117	0	117	0		+
072	46	28,937	9			117	0	117	0		+
073	47	28,937	8			117	0	117	0		1
074	48	28,937	7			117	0	117	0		1
075	49	28,937	6			117	0	117	0		
076	50	28,937	5			117	0	117	0		
		1, 446, 833	36, 023	40, 162	24, 504	6,879	547	47, 041	25, 050		10
		EIRR	$\Sigma (B - C) / \Sigma (1 +$	io) <sup>t-1</sup> =0	0.176						
		NPV	$\Sigma (B - C) / \Sigma (1 +$	i) <sup>t-1</sup>	10, 973						

### ANNEX Table 4.5.17 Cash Flow (Case④ Alternative Plan A-1)

	_										(10 <sup>6</sup> PESOS)
		(1) BEI	VEFIT ②	3	4	5	6	Ø	8		
Year						•				B/C	В-с
0014		BENEFIT	PRESENT VALUE	COST	PRESENT VALUE	MAINTENANCE	PRESENT VALUE	COST	PRESENT VALUE		4.50
2014 2015				4, 520 4, 520	4, 520 3, 930	13 26	13	4, 533 4, 546	4, 533 3, 953		-4, 533
2016				4, 520	3, 418	39	30	4, 559	3, 447		-3, 44
2017				7, 959	5, 233	63	41	8, 022	5, 274		-5, 274
2018				3, 439	1,966	73	42	3, 512	2, 008		-2, 008
2019				3, 439	1, 710	83	41	3, 522	1, 751		-1, 75
2020				3, 439	1, 487	93	40	3, 532	1, 527		-1, 52
2021				3, 439	1, 293	103	39	3, 542	1, 332		-1, 33
2022				3, 439	1, 124	113	37	3, 552	1, 161		-1, 16
2023 2024				982 982	279 243	116	33	1,098	312		-31
2024				982	243	118	29	1, 101	212		-27
2026				982	184	124	23	1, 104	207		-20
2027	1	28, 937	4, 703			124	20	124	20		4, 68
2028	2	28, 937	4, 090			124	18	124	18		4, 07
2029	3	28, 937	3, 556			124	15	124	15		3, 54
2030	4	28, 937	3, 092			124	13	124	13		3, 07
2031	5		2, 689			124	12	124	12		2, 67
2032	6		2, 338			124	10		10		2, 32
2033	7	28, 937	2, 033			124	9		9		2, 02
2034	8		1, 768			124	8		8		1, 76
2035 2036	9 10		1, 537 1, 337			124	7	124	7		1, 53
2036	11	28, 937	1, 337			124	5		5		1, 33
2038	12		1, 103			124	4	124	4		1, 13
2039	13	28, 937	879			124	4	124	4		87
2040	14	28, 937	764			124	3	124	3		76
2041	15		665			124	3	124	3		66
2042	16	28, 937	578			124	2	124	2		57
2043	17	28, 937	503			124	2	124	2		50
2044	18	28, 937	437			124	2	124	2		43
2045	19	28, 937	380			124	2	124	2		37
2046	20	28, 937	330			124	1	124	1		32
2047	21	28, 937	287			124	1	124	1		28
2048 2049	22 23	28, 937 28, 937	250 217			124	1	124	1		24
2049	23	28, 937	189			124	1	124	1		18
2050	24	28, 937	169			124	1	124	1		16
2052	26	28, 937	143			124	1	124	1		14
2053	27	28, 937	124			124	1	124	1		12
2054	28	28, 937	108			124	0	124	0		10
2055	29	28, 937	94			124	0	124	0		9
2056	30	28, 937	82			124	0	124	0		8
2057	31	28, 937	71			124	0		0		7
2058	32		62			124	0		0		6
2059	33	28, 937	54			124	0		0		5
2060 2061	34 35	28, 937 28, 937	47			124	0		0		4
2061	36	28, 937	35			124	0		0		3
2062	37	28, 937	33			124	0	124	0		3
2064	38	28, 937	27			124	0	124	0		2
2065	39	28, 937	23			124	0	124	0		2
2066	40	28, 937	20			124	0	124	0		2
2067	41	28, 937	18			124	0	124	0		1
2068	42		15			124	0		0		1
2069	43		13			124	0		0		1
2070	44	28, 937	12			124	0		0		1
2071	45		10			124	0		0		1
2072 2073	46 47	28, 937 28, 937	9			124	0		0		
2073	47		7			124	0		0		
2074	40		6			124	0		0		
2076	50		5			124	0				
		1, 446, 833		42, 645	25, 598		571				9, 85
		EIRR	$\Sigma (B - C) / \Sigma (1 +$		0.173						
		NPV	$\Sigma (B - C) / \Sigma (1 +$	i) <sup>t-1</sup>	9,854						

### ANNEX Table 4.5.18 Cash Flow (Case<sup>5</sup>) Alternative Plan A-2-1)

											(10 <sup>6</sup> PESOS)
			NEFIT								
Year	ŀ	1	2	3	4	5	6	Ø	8	B/C	B-c
		BENEFIT	PRESENT VALUE	COST	PRESENT VALUE	MAINTENANCE	PRESENT VALUE	COST	PRESENT VALUE		
2014				4, 520	4, 520	13	13	4, 533	4, 533		-4, 533
2015 2016	_			4, 520 4, 520	3, 930 3, 418	26 39	23	4, 546 4, 559	3, 953 3, 447		-3, 953
2017				8, 387	5, 515	64	42	8, 451	5, 557		-5, 557
2018				3,867	2, 211	75	43	3, 942	2, 254		-2, 254
2019				3,867	1,923	86	43	3, 954	1,966		-1,966
2020 2021				3,867 3,867	1,672 1,454	98 109	42	3, 965 3, 976	1, 714 1, 495		-1, 714
2021	_			3,867	1, 434	109	39	3, 970	1, 493		-1, 303
2023				891	253	123	35	1,013	288		-288
2024				891	220	125	31	1, 016	251		-251
2025	_			891 891	191	128	27	1,019	219		-219
2026 2027	1	28, 937	4, 703	091	166	131	24	1, 021 131	21		-191 4, 682
2028	2	28, 937	4, 090			131	18	131	18		4, 071
2029	3	28, 937	3, 556			131	16	131	16		3, 540
2030	4	28, 937	3, 092			131	14	131	14		3, 078
2031 2032	5	28, 937 28, 937	2, 689 2, 338			131	12	131	12		2, 677 2, 328
2032	7	28, 937	2, 338			131	9	131	9		2, 328
2034	8	28, 937	1, 768			131	8	131	8		1, 760
2035	9	28, 937	1, 537			131	7	131	7		1, 530
2036	10 11	28, 937	1, 337			131	6	131	6		1, 331
2037 2038	12	28, 937 28, 937	1, 163			131	5	131	5		1, 157
2039	13	28, 937	879			131	4	131	4		875
2040	14	28, 937	764			131	3	131	3		761
2041	15	28, 937	665			131	3	131	3		662
2042 2043	16 17	28, 937 28, 937	578 503			131	3	131	3		575
2043	18	28, 937	437			131	2	131	2		435
2045	19	28, 937	380			131	2	131	2		378
2046	20	28, 937	330			131	1	131	1		329
2047 2048	21 22	28, 937 28, 937	287 250			131	1	131	1		286
2048	22	28, 937	230			131	1	131	1		249
2050	24	28, 937	189			131	1	131	1		188
2051	25	28, 937	164			131	1	131	1		164
2052	26	28, 937	143			131	1	131	1		142
2053 2054	27 28	28, 937 28, 937	124			131	1	131	1		124
2055	29	28, 937	94			131	0	131	0		94
2056	30	28, 937	82			131	0	131	0		81
2057	31	28, 937	71			131	0	131	0		71
2058 2059	32 33	28, 937	62 54			131	0	131	0		61
2059	34	28, 937 28, 937	47			131	0	131	0		53
2061	35	28, 937	41			131	0	131	0		40
2062	36	28, 937	35			131	0	131	0		35
2063	37	28,937	31			131	0	131	0		31
2064 2065	38 39	28, 937 28, 937	27			131	0	131	0		27
2066	40	28, 937	20			131	0	131	0		20
2067	41	28, 937	18			131	0	131	0		17
2068	42	28, 937	15			131	0	131	0		15
2069 2070	43 44	28, 937 28, 937	13			131	0	131	0		13
2070	45	28,937	10			131	0	131	0		10
2072	46	28, 937	9			131	0	131	0		g
2073	47	28, 937	8			131	0	131	0		8
2074 2075	48 49	28, 937 28, 937	7			131	0	131	0		7
2075	49 50	28, 937				131	0	131	0		
		1, 446, 833		44, 846	26, 737	7, 662	596	52, 508	27, 334		8, 689
		EIRR	$\Sigma$ (B - C) / $\Sigma$ (1 +	io) <sup>t-1</sup> =0	0.170						
				· t=1							
		NPV	$\Sigma$ (B - C) / $\Sigma$ (1 +	1)**	8, 689						
		B/C	Σ (B/(1 + i) <sup>t-1</sup> )/		1.3						

### ANNEX Table 4.5.19 Cash Flow (Case<sup>®</sup> Alternative Plan A-3)

perf         perf<												(10 <sup>6</sup> PESOS)
Norm         Parker Nuk         Open         Parker Nuk         Parker Nuk		ļ										
Set         N         6.339         6.439         10         10         6.439         6.439         4.439           206          4.439         3.40         0         2         6.466         3.40         -4.40           207           4.467         5.38         6         4.637         -4.50           208           3.468         5.29         5         6         5.461         -4.40           208           3.468         1.20         6         5.46         5.461         -4.40           208           3.468         1.168         0.46         3.46         1.161         2.164         -4.40           209           3.48         1.161         2.16         -4.40 <t< td=""><td>Year</td><td>╞</td><td>1</td><td>2</td><td>3</td><td>4</td><td>5</td><td>6</td><td>Ø</td><td>8</td><td>B/C</td><td>B-c</td></t<>	Year	╞	1	2	3	4	5	6	Ø	8	B/C	B-c
Set         N         6.339         6.439         10         10         6.439         6.439         4.439           206          4.439         3.40         0         2         6.466         3.40         -4.40           207           4.467         5.38         6         4.637         -4.50           208           3.468         5.29         5         6         5.461         -4.40           208           3.468         1.20         6         5.46         5.461         -4.40           208           3.468         1.168         0.46         3.46         1.161         2.164         -4.40           209           3.48         1.161         2.16         -4.40 <t< td=""><td></td><td>ŀ</td><td>RENEEIT</td><td>DRESENT VALUE</td><td>T200</td><td>DRESENT VALUE</td><td>MAINTENANCE</td><td>DRESENT VALUE</td><td>T200</td><td>DRESENT VALUE</td><td></td><td></td></t<>		ŀ	RENEEIT	DRESENT VALUE	T200	DRESENT VALUE	MAINTENANCE	DRESENT VALUE	T200	DRESENT VALUE		
2010         100 <td>2014</td> <td>-</td> <td>DENEFIT</td> <td>FRESENT VALUE</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-4 533</td>	2014	-	DENEFIT	FRESENT VALUE								-4 533
2000         1         4.101         3.4 tot         3.4 tot<												
2021         No.         No. <td></td> <td>-3, 447</td>												-3, 447
2010					8, 407		64					-5, 570
NBM         Image         I	2018				3, 888	2, 223	75	43	3,963	2, 266		-2, 266
2017	2019				3, 888	1, 933	87		3,974	1,976		-1,976
2022												-1, 723
BACE         BACE <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>-1, 503</td></th<>												-1, 503
2844		_										
909		_										
2088		_										
207     1     28.93     4.702		-										
2000         3         2000         3         2000         3         2000         4         400           2000         4         2000		1	28.937	4, 703								4, 682
2008         3         36.50          122         144         122         14         5.56           2011         5         3.500          122         14         122         14         5.20           2011         5         3.500          122         11         122         11         5.20           2011         3         3.500          122         11         122         11         5.20           2013         3         3.500          122         9         122         0         1.20         1.50           2014         1         3.500         1.50          1.50         1.50         1.50           2017         1         3.500         1.10          1.50         1.50         1.50         1.50           2017         1         3.500         1.10          1.50         1.50         1.50         1.50         1.50           2017         1.10          1.10         1.10         1.10         1.10         1.10         1.10         1.10         1.10         1.10         1.10         1.10         1.10		2										4, 071
201         5         28.07         2.09         2.09         2.20         112         1113 <th< td=""><td>2029</td><td>3</td><td>28, 937</td><td>3, 556</td><td></td><td></td><td>132</td><td>16</td><td>132</td><td>16</td><td></td><td>3, 540</td></th<>	2029	3	28, 937	3, 556			132	16	132	16		3, 540
2021         2         2         2         2         2         1         112         11         112         1         2.2.02           2031         2         2.8.91         2         0.000         112         0         0         2.2.02           2035         8         2.8.92         1.5.02         0         1132         0         1.5.32           2035         8         2.8.492         1.5.32         0         1.5.32         0         1.5.32           2037         11         2.8.492         1.1.61         0         1.5.22         0         1.5.33           2037         11         2.8.497         1.4.61         0         1.5.22         0         1.5.22         0         1.5.33           2037         12         2.6.97         7.46         0         1.5.22         0         1.5.22         0         0         1.5.2         0         1.5.33         1.5.2         0         1.5.2         0         1.5.2         0         1.5.2         1.5.2         0         1.5.2         1.5.2         0         1.5.2         0         1.5.2         1.5.2         1.5.2         1.5.2         1.5.2         1.5.2         1.5.2	2030	4	28, 937	3, 092			132	14	132	14		3, 078
2033         2         24.947         2.033         1122         9         1122         9         2.04           2055         8         2.84.927         1.537         2         1122         1132         0         1.17           2055         9         2.84.927         1.537         2         1122         1132         0         1.153           2055         12         2.84.927         1.161         1222         123         122         0         1.153           2056         12         2.84.927         1.161         1222         123         122         0         1.161           2061         12         2.84.927         1.011         1222         122         0         1.161         1.161         1.161         122         0         1.161         1	2031	5	28, 937									2,677
2804         9         94.947         1.788         1.788         1.732         1.732         1.732         1.732         1.733         1.		6										2, 328
2905         9         94.937         1.537         1 <th1< th="">         1         1         &lt;</th1<>		7										2, 024
2905         i         39.437         1.132         1         3937         11         28.637         1.135           2807         11         28.637         1.141         1.132         5         1.22         5         1.135           2807         11         28.637         1.141         1.23         5         1.22         1.24         1.141           2809         12         2.4.62         6.7.11         1.23         4         1.22         4         1.22         4         1.24         4         1.26           2804         15         2.8.437         7.66         1.23         3         1.22         3         1.26         1.27         2         1.26         1.26         1.27         2         1.27         2         1.27         2         1.27         2         1.27         2         1.27         2         1.27         2         1.27         2         1.27         2         1.27         2         1.27         2         1.27         2         1.27         2         1.27         2         1.27         2         1.27         2         1.28         1.27         2         1.27         2         2.27         2.27		-						8				1, 760
2037       1       23.8       1.9       1.9       1.92       5       1.92       5       1.9         2039       12       23.8       12       2.8       1.9       1.9       1.9         2039       12       24.807       7.97       1.9       1.12       1.22       1.22       1.2       1.9       1.9         2040       14       2.8.437       7.578       1.0       1.12       2.0       1.22       2.0       1.6       2.0       1.6       2.0       1.6       1.6       2.8.437       1.560       1.23       2.0       2.0       1.6       1.6       2.8.437       1.560       1.32       2.0       1.22       2.0								7				1, 530
2938         12         28.482         1.011         1.02         5         1.102         5         1.102         5         1.102         5         1.102         5         1.102         6         1.103           2838         13         2.8.437         0.764         1.322         4         1.322         4         1.322         4         1.322         3         1.422         3         0.668           2641         15         2.6.437         0.668         1.322         2         1.322         2         0.422         3         0.668         0.668         0.668         0.732         2         1.322         2         0.444         1.6         2.6.437         0.668         0.732 <td></td> <td></td> <td></td> <td></td> <td> </td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td>								-				
2595         13         28.423         899         (m)         132         4         1132         4         1132         3         1132         1												
2400         14         28.8.27         776         132         3         132         3         132         3         176           284         15         28.8.92         665         132         2         132         3         666           284         17         28.837         503         132         2         132         2         132         2         342         132         2         432           284         17         28.837         503         132         2         132         2         132         2         132         2         143         2         143         2         143         2         143         2         143         2         143         2         143         2         143         2         143         2         143         2         1         123         1         132         1         132         1         133         1         133         1         133         1         133         1         133         1         133         1         133         1         133         1         133         1         133         1         133         1         133         1								5				
2441         16         2.8.937         666           242         16         2.8.937         667           2442         16         2.8.937         6578          112         3         112         3         112         2         3          977           2444         18         2.8.937         6437          132         2         132         2         2         143           2445         18         2.8.937         6430          132         2         132         2         2          377           2446         24         2.8.937         6330           132         1         132         1          2         2         2         2         2         2         1          2         2         2         1          12         1          12         1          12         1          12         1         12         1         12         1         12         12         12         12         12         12         13         13         13         13								3		-		761
242         i6         28.8.97         777         model         112         3         122         132         23         53         577           246         17         28.8.97         653         663         112         2         112         2         122         2         122         2         122         2         132         2         133           246         18         28.837         330           132         2         132         2         333           244         2         28.937         256           132         1         132         1         23         2         3         23         2         333         2         2         333         2         1         333         2         1         333         2         1         333         2         1         132         1         132         1         133         1								3				662
2444         18         28.837         44.7         44.7         44.7         44.7         44.7           2485         18         28.837         34.00         112         2         112         2         112         2         112         2         112         2         112         2         1132         2         1132         2         1132         2         1132         2         1132         1         2         1132         1         113	2042	16	28, 937	578				3	132			575
2845       19       28,837       330       1132       2       132       2       32       2       333         2846       20       28,937       330       1132       2       132       2       2       2       2       2       2       2       2       2       2       2       2       2       2       330       1132       1132       1       2       2       2       2       2       2       2       2       2       330       1       132       1       132       1       2       1       2       2       2       2       2       2       330       1       1       1       2       1       1       2       1	2043	17	28, 937	503			132	2	132	2		500
2046       20       28,937       330        112       2       112       2       122       2       122       2       122       1        28       22       22       22       22       22       22       22       22       22       22       22       22       22       1       122       1       122       1       122       1       122       1       122       1       122       1       122       1       122       1       122       1       122       1       122       1       121       1       118       122       1       122       1       122       1       118       121       1       118       121       1       1111       111       111 <th< td=""><td>2044</td><td>18</td><td>28, 937</td><td>437</td><td></td><td></td><td>132</td><td>2</td><td>132</td><td>2</td><td></td><td>435</td></th<>	2044	18	28, 937	437			132	2	132	2		435
284       22       28,937       287       286       32       28,937       250       132       1       132       1       132       1       24         285       28,937       217       1       132       1       122       1       21       24         285       28       28,937       189       1       132       1       122       1       121       1       116         285       28       28,937       144       132       1       132       1       122       1       141       116         285       28       28,937       144       132       1       132       1       132       1       122       1       141       112         295       28       28,937       144       132       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       134       132 <td< td=""><td>2045</td><td>19</td><td>28, 937</td><td>380</td><td></td><td></td><td>132</td><td>2</td><td></td><td>2</td><td></td><td>378</td></td<>	2045	19	28, 937	380			132	2		2		378
286       22       28,937       250       112       112       112       1       122       1       121       1       121       1       121       1       121       1       121       1       121       1       121       1       121       1       121       1       121       1       121       1       121       1       121       1       1       121       1       1       121       1       1       121       1       1       111       1       1       111       1       1       111       1 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>2</td> <td></td> <td>2</td> <td></td> <td>329</td>								2		2		329
284       28       28.937       217       1132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       141       141         265       26       28.937       143       132       1       132       1       132       1       132       1       141         265       28       28.937       108       132       0       132       133								1				286
280       24       28,937       189       1132       1       122       1       122       1       132       1								1				
251       25       28, 937       164       112       1       132       1       132       1       14         2052       26       28, 937       144       132       1       122 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>												
282       28       28,937       143       112       112       1132       1132       1       14         2053       28       28,937       106       132       0       132       132												164
283       27       28, 93       124       1132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       1       132       0       144       206       35       25.937       41       112       112       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0       132       0												142
285       29       28.837       94       9       132       0       132								1		1		124
205       30       28.937       82       132       0       132       0       132       0       7         2051       31       28.937       62       132       0       132       0       66         2056       33       28.937       64       132       0       132       0       66         2066       34       28.937       64       132       0       132       0       66         2066       34       28.937       64       132       0       132       0       64         2061       34       28.937       47       6       132       0       132       0       44         2061       35       28.937       35       132       0       132       0       33         2063       37       28.937       31       1       132       0       132       0       133         2063       39       28.937       23       1       132       0       132       0       20       20       20       20       20       20       20       20       20       20       20       20       20       20       20       20	2054	28	28, 937	108			132	0	132	0		108
2057       31       28.937       71        132       0       133	2055	29	28, 937	94			132	0	132	0		94
205       32       28,937       62       112       0       132       0       132       0       132       0       132       0       152       0       55         206       34       28,937       44        132       0       132       0       132       0       14       4         2061       35       28,937       44        132       0       132       0       132       0       14         2061       36       28,937       44        132       0       132       0       133         2063       37       28,937       31         132       0       132       0       132       0       33         2065       36       28,937       27         132       0       132       0       132       0       20		_										81
2059       33       28.937       54       112       1132       <	2057	31	28, 937	71			132	0	132	0		71
2060       34       28.937       44       1132       0       132       0       144         2061       35       28.937       44       132       0       132       0       142       44         2062       36       28.937       35       1       132       0       132       0       132       0       33         2063       37       28.937       37       1       132       0       132       0       132       0       33         2063       38       28.937       27       1       132       0       132       0       122       0       20												61
206       35       28,937       44       44       132       0       132       0       33         2063       37       28,937       33       35       132       0       132       0       132       0       33         2063       37       28,937       31       1       132       0       132       0       132       0       33         2064       38       28,937       23       1       132       0       132       0       122       0       22         2065       39       28,937       23       132       0       132       0       122       0       22         2066       40       28,937       20       132       0       132       0       12       0       12         2067       41       28,937       13       132       132       0       132       0       11         2068       42       28,937       13       13       132       0       132       0       11         2064       43       28,937       13       14       132       0       132       0       11         2071       45												53
2062       36       28,937       35       112       112       112       112       1132												46
2063       37       28.937       31       1       132       0       132       0       33         2064       38       28.937       27       1       132       0       132       0       132       0       22         2065       39       28.937       23       1       132       0       132       0       132       0       22         2066       40       28.937       20       132       0       132       0       132       0       20												40
2064       38       28,837       27       1132												31
2065       39       28,837       23       1132       0       132       0		_						-				27
206       40       28.937       20       1       132       0       132       0       122       0       122         2067       41       28.937       18       1       132       0       132       0       131       0       131       131       131       131       131       0       131       0       132       0       131       0       131       131       0												23
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	2066	40	28, 937	20			132	0		0		20
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		_						-				17
$\begin{array}{c c c c c c c c c c c c c c c c c c c $												15
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												13
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		_						-				11
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												10
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												9
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $								-				7
$\begin{array}{c c c c c c c c c c c c c c c c c c c $												6
$\begin{array}{c c c c c c c c c c c c c c c c c c c $								0				5
NPV $\Sigma (B - C) / \Sigma (1 + i)^{t-1}$ 8,542				36, 023	45, 335	26, 881		600		27, 481		8, 542
NPV $\Sigma (B - C) / \Sigma (1 + i)^{t-1}$ 8,542			EIRR	$\Sigma$ (B - C) $/\Sigma$ (1 +	io) <sup>t-1</sup> =0	0.170						
$B/C \qquad \Sigma (B/(1+i)^{t-1})/\Sigma (C/(1+i)^{t-1}) \qquad 1.3$			NPV	$\Sigma$ (B - C) $/ \Sigma$ (1 +	i) <sup>t-1</sup>	8, 542						
B/C Σ (B/(1 + i) <sup>+</sup> )/Σ (C/(1 + i) <sup>+</sup> ) 1.3												
			B/C	$\Sigma (B/(1 + i)^{\tau-1})/$	$\Sigma (C/(1 + i)^{\tau-1})$	1.3						

### ANNEX Table 4.5.20 Cash Flow (Case⑦ Alternative Plan A-2-2)

		051									(10 <sup>6</sup> PESOS)
Year		(1)	vefit Ø	3	4	5	6	Ø	8	B/C	B-c
		BENEFIT	PRESENT VALUE	COST	PRESENT VALUE	MAINTENANCE	PRESENT VALUE	COST	PRESENT VALUE		
2014				4, 389	4, 389	13	13	4, 402	4, 402		-4, 402
2015				4, 389	3, 817	26	22	4, 415	3, 839		-3, 839
2016				4, 389	3, 319	38	29	4, 428	3, 348		-3, 348
2017				7, 515	4, 941	60	40	7, 575	4, 981		-4, 98
2018 2019				3, 126 3, 126	1, 787	69 78	40	3, 195 3, 204	1,827 1,593		-1,82
2019				3, 126	1, 554	87	39	3, 204	1, 593		-1, 38
2021				3, 126	1, 175	97	36	3, 222	1, 211		-1, 21
2022				3, 126	1,022	106	35	3, 232	1,056		-1,056
2023				930	264	108	31	1,038	295		-295
2024				930	230	111	27	1, 041	257		-25
2025				930	200	114	24	1,044	224		-224
2026			4 700	930	174	116	22	1,047	196		-196
2027 2028	2	28, 937 28, 937	4, 703 4, 090			116	19	116	19 16		4, 684
2028	2	28, 937	4, 090			116	16	116	14		3, 542
2023	4	28, 937	3, 092			116	14	116	14		3, 342
2000	5	28, 937	2, 689			116	11	116	11		2, 678
2032	6		2, 338			116	9	116	9		2, 329
2033	7	28, 937	2, 033			116	8	116	8		2, 025
2034	8	28, 937	1, 768			116	7	116	7		1, 76
2035	9	28, 937	1, 537			116	6	116	6		1,53
2036	10	28, 937	1, 337			116	5	116	5		1, 332
2037	11	28,937	1, 163			116	5	116	5		1, 158
2038 2039	12 13	28, 937 28, 937	1,011 879			116	4	116	4		1,00
2039	14	28, 937	764			116	4	116	3		76
2041	15	28, 937	665			116	3	116	3		662
2042	16	28, 937	578			116	2	116	2		576
2043	17	28, 937	503			116	2	116	2		50
2044	18	28, 937	437			116	2	116	2		435
2045	19	28, 937	380			116	2	116	2		378
2046	20	28, 937	330			116	1	116	1		329
2047	21	28, 937	287			116	1	116	1		280
2048 2049	22 23	28, 937 28, 937	250 217			116	1	116	1		249
2049	23	28, 937	189			110	1	116	1		188
2051	25	28, 937	164			116	1	116	1		164
2052	26	28, 937	143			116	1	116	1		142
2053	27	28, 937	124			116	1	116	1		124
2054	28	28, 937	108			116	0	116	0		108
2055	29	28, 937	94			116	0	116	0		94
2056	30	28, 937	82			116	0	116	0		8
2057	31	28,937	71			116	0	116	0		7
2058 2059	32 33	28, 937 28, 937	54			116 116	0	116	0		62 53
2055	34	28, 937	47			116	0	116	0		4
2000	35	28, 937	41			116	0	116	0		4(
2062	36		35		_	116	0	116	0		35
2063	37	28, 937	31			116	0	116	0		3
2064	38	28, 937	27			116	0	116	0		2
2065	39	28, 937	23			116	0	116	0		23
2066	40		20			116	0	116	0		20
2067 2068	41 42	28, 937 28, 937	18			116	0	116	0		11
2068	42	28, 937 28, 937	15			116	0	116	0		1:
2009		28, 937	13			110	0	116	0		1
2071	45	28, 937	10			116	0	116	0		1
2072	46		9			116	0	116	0		!
2073	47	28, 937	8			116	0	116	0		-
2074	48		7			116	0	116	0		
2075	49	28,937	6			116	0	116	0		-
2076	50		5			116	0	116	0		
		1, 446, 833			24, 224	6,849	540	46, 882	24, 765		11, 259
		EIRR	$\Sigma$ (B - C) / $\Sigma$ (1 +	io)' '=0	0.177						
		NPV	$\Sigma (B - C) / \Sigma (1 +$	i) <sup>t-1</sup>	11, 259						
		··· · ·	<u>~ (υ ' υ) / Ζ (Ι +</u>	17	11,209						

### ANNEX Table 4.5.21 Cash Flow (Case<sup>®</sup> Alternative Plan O-1)

	_										(10 <sup>6</sup> PESOS)
		BE ①	NEFIT ②	3	4	5	6	Ø	8		
Year										B/C	B-c
2014		BENEFIT	PRESENT VALUE	COST 4 200	PRESENT VALUE	MAINTENANCE	PRESENT VALUE	COST	PRESENT VALUE		
2014 2015				4, 389 4, 389	4, 389 3, 817	13 26	13	4, 402 4, 415	4, 402 3, 839		-4, 4
2016				4, 389	3, 319	38	29	4, 428	3, 348		-3, 3
2017				7, 851	5,162	61	40	7,912	5, 202		-5, 1
2018				3, 462	1,979	71	41	3, 533	2, 020		-2,0
2019				3, 462	1, 721	81	40	3, 543	1, 762		-1,3
2020				3, 462	1, 497	91	40	3, 553	1, 536		-1, 5
2021 2022				3, 462 3, 462	1, 301 1, 132	101	38	3, 563 3, 573	1, 340 1, 168		-1,3
2022				1, 022	290	112	33	1, 136	323		-:
2024				1, 022	253	117	29	1, 139	282		-2
2025				1,022	220	120	26	1, 142	246		-2
2026				1,022	191	123	23	1, 145	214		-2
2027	1	28, 937	4, 703			123	20	123	20		4, 6
2028	2	28, 937	4,090			123	17	123	17		4, (
2029 2030	3	28, 937 28, 937	3, 556 3, 092			123	13	123	13		3, 5
2031	5	28, 937	2, 689			123	11	123	11		2, 6
2032	6	28, 937	2, 338			123	10		10		2, 3
2033	7	28, 937	2, 033			123	9	123	9		2, 0
2034	8	28, 937	1, 768			123	8		8		1, 3
2035	9	28, 937	1, 537			123	7	123	7		1, 1
2036 2037	10 11	28, 937 28, 937	1, 337 1, 163			123	6		6		1,
2037	11	28, 937 28, 937	1, 163			123	4	123	5		1, 1
2030	13	28, 937	879			123	4	123	4		1,0
2040	14	28, 937	764			123	3		3		-
2041	15	28, 937	665			123	3		3		(
2042	16	28,937	578			123	2		2		ļ
2043	17	28, 937	503			123	2	123	2		
2044	18	28, 937	437			123	2		2		4
2045 2046	19 20	28, 937 28, 937	380 330			123	2	123	2		
2040	21	28, 937	287			123	1	123	1		2
2048	22	28, 937	250			123	1	123	1		2
2049	23	28, 937	217			123	1	123	1		2
2050	24	28, 937	189			123	1	123	1		1
2051	25	28, 937	164			123	1	123	1		1
2052 2053	26 27	28, 937 28, 937	143			123	1	123	1		1
2053	27	28, 937	124			123	0		0		1
2055	29	28, 937	94			123	0	123	0		
2056	30	28, 937	82			123	0	123	0		
2057	31	28, 937	71			123	0	123	0		
2058	-	28, 937	62			123	0		0		
2059	33	28, 937	54			123	0	123	0		-
2060 2061	34 35	28, 937 28, 937	47			123	0	123	0		-
2001	36	28, 937	35			123	0	123	0		
2063	37	28, 937	31			123	0	123	0		
2064	38	28, 937	27			123	0	123	0		
2065	39	28, 937	23			123	0	123	0		
2066	40	28, 937	20			123	0		0		
2067 2068	41 42	28, 937 28, 937	18			123	0		0		
2068	42	28, 937 28, 937	15			123	0	123	0		
2003	43	28, 937	13			123	0	123	0		
2071	45	28, 937	10			123	0	123	0		
2072	46	28, 937	9			123	0	123	0		
2073	47	28, 937	8			123	0	123	0		
2074	48	28, 937	7			123	0	123	0		_
2075	49	28, 937	6			123	0	123	0		-
2076	50	28, 937 1, 446, 833	5 36, 023	42, 415	25, 271	123 7, 242	564				10,
		1, 446, 833 EIRR	$\Sigma (B - C) / \Sigma (1 +$		0. 174		504	43,007	20, 030		10,
		LINN	<u>~ (v v)/ ~ (1 +</u>	10/ -0	0.174						
		NPV	$\Sigma$ (B - C) / $\Sigma$ (1 +	i) <sup>t-1</sup>	10, 189						

### ANNEX Table 4.5.22 Cash Flow (Case<sup>(9)</sup>) Alternative Plan O-2)

-	D D D D D D D D D D D D D D D D D D D	NEFIT ②	3	4						
-		(2)	3	(4)						
-	BENEFIT			-	5	6	Ø	8	B/C	B-c
		PRESENT VALUE	COST	PRESENT VALUE	MAINTENANCE	PRESENT VALUE	COST	PRESENT VALUE		
			4, 389	4, 389	13		4, 402	4, 402		-4, 40
			4, 389	3, 817	26	22	4, 415	3, 839		-3,83
			4, 389	3, 319	38	29	4, 428	3, 348		-3, 34
			7, 756 3, 367	5, 100	61 71	40 40	7,817	5, 140		-5, 14
			3, 367	1, 925 1, 674	80	40	3, 437 3, 447	1, 965 1, 714		-1,96
										-1, 49
					100	38				-1, 30
			3, 367	1, 101	110	36	3, 477	1, 137		-1, 13
			891	253	112	32	1,003	285		-28
			891	220	115	28	1,006	249		-24
										-21
_			891	166						-18
										4,6
										3, 54
										3, 07
5		2, 689				11		11		2,6
6	28, 937	2, 338			120					2, 32
7	28, 937	2, 033			120	8	120	8		2, 0
8	28, 937	1, 768			120	7	120	7		1, 76
9	28, 937	1, 537			120	6	120	6		1, 50
										1, 33
										1, 15
						4				1,00
						4				76
						3				66
16	28, 937	578			120	2	120	2		57
17	28, 937	503			120	2	120	2		50
18	28, 937	437			120	2	120	2		43
19	28, 937	380			120	2	120	2		37
20	28, 937					1	120	1		32
						1		1		28
						1		1		24
-						1		1		18
_						1		1		16
26	28, 937	143			120	1	120	1		14
27	28, 937	124			120	1	120	1		12
28	28, 937	108			120	0	120	0		1(
29	28, 937	94			120	0	120	0		9
										8
-										
										6
34										4
36	28, 937	35			120					
37	28, 937	31			120	0				:
38	28, 937	27			120	0	120	0		:
39	28, 937	23			120					:
40	28, 937	20			120					:
41										
-										
								0		
46	28, 937	9			120	0	120			1
47	28, 937	8			120	0	120	0		
48	28, 937	7			120	0	120	0		
49	28, 937	6			120	0	120	0		
50	28, 937	5			120	0	120	0		
				24, 877	7,067	555	48, 388	25, 432		10, 5
	EIRR	$\Sigma (B - C) / \Sigma (1 +$	io) <sup>t-1</sup> =0	0.175						
		F (D 0) (F ()	, t-1	10 501						
	WP V	∠ (B - U)/Σ(1 +	D.	10, 591						
	6         7           8         9           9         10           11         11           13         14           15         16           16         17           18         19           19         21           22         23           24         25           26         27           28         29           30         31           32         33           36         37           38         39           40         41           42         44           45         50	2         28.937           3         28.937           4         28.937           5         28.937           6         28.937           7         28.937           8         28.937           9         28.937           10         28.937           11         28.937           12         28.937           13         28.937           14         28.937           15         28.937           16         28.937           17         28.937           18         28.937           19         28.937           20         28.937           21         28.937           22         28.937           23         28.937           24         28.937           25         28.937           26         28.937           30         28.937           31         28.937           32         28.937           33         28.937           34         28.937           35         28.937           36         28.937           37	2         28.937         4.090           3         28.937         3.556           4         28.937         3.092           5         28.937         2.689           6         28.937         2.033           7         28.937         1.537           10         28.937         1.1758           11         28.937         1.1337           12         28.937         1.163           12         28.937         1.161           13         28.937         665           16         28.937         665           16         28.937         665           16         28.937         665           16         28.937         650           18         28.937         650           19         28.937         250           23         28.937         217           24         28.937         1164           25         28.937         1164           26         28.937         108           29         28.937         108           29         28.937         108           20         28.937         108	Image: state sta	Image: state of the state	Image: state in the	Image: state of the	Image: state in the	Image: state in the	Nome         3.307         1.488         90         32         3.457         1.468           1         1         3.307         1.228         100         38         4.07         1.137           1         1         1         100         38         3.407         1.137           1         1         100         100         100         220         1.000         220           1         2         1.001         100         100         220         1.001         200           1         2.80         7         4.000         100         100         101         100         101           1         2.80         7         4.000         100         100         101         100         101           1         2.80         2.000         100         100         100         101         100         101           1         2.80         1.101         100         100         101         100         101         101         100         101         101         101         101         101         101         101         101         101         101         101         101         101         101         <

### ANNEX Table 4.5.23 Cash Flow (Case<sup>®</sup> Alternative Plan B-1)

											(10 <sup>6</sup> PESOS)
Year	-	(1) BEI	Q	3	4	5	6	Ø	8	B/C	B-c
	F	BENEFIT	PRESENT VALUE	COST	PRESENT VALUE	MAINTENANCE	PRESENT VALUE	COST	PRESENT VALUE	ł	
2014				4, 389	4, 389	13	13	4, 402	4, 402		-4, 402
2015				4, 389	3,817	26	22	4, 415	3,839		-3, 83
2016 2017				4, 389	3, 319 5, 346	38	29 41	4, 428 8, 193	3, 348 5, 387		-3, 348
2017				8, 131 3, 742	2, 139	73	41	3, 815	2, 181		-5, 38
2010				3, 742	1, 860	84	42	3, 826	1, 902		-1, 902
2020				3, 742	1,618	95	41	3, 837	1,659		-1,659
2021				3, 742	1, 407	106	40	3, 847	1, 446		-1, 440
2022				3, 742	1, 223	116	38	3,858	1,261		-1, 26
2023 2024				1,022	290 253	119	34 30	1, 141	324 283		-324
2024				1, 022	233	122	27	1, 144	283		-24
2026				1, 022	191	128	24	1, 150	215		-21
2027	1	28, 937	4, 703			128	21	128	21		4, 682
2028	2	28, 937	4,090			128	18	128	18		4, 07
2029	3	28, 937	3, 556			128	16	128	16		3, 540
2030	4	28, 937	3,092			128	14	128	14		3, 07
2031 2032	5	28, 937 28, 937	2, 689 2, 338			128	12	128	12		2, 67
2032	7	28, 937	2, 338			128	9	128	9		2, 32
2034	8	28, 937	1, 768			128	8	128	8		1, 76
2035	9	28, 937	1,537			128	7	128	7		1, 53
2036	10	28,937	1,337			128	6	128	6		1, 33
2037	11	28, 937	1, 163			128	5	128	5		1, 15
2038 2039	12 13	28, 937 28, 937	1,011 879			128	4	128	4		1,00
2039	14	28, 937	764			128	3	128	4		76
2040	15	28, 937	665			128	3	128	3		66
2042	16	28, 937	578			128	3	128	3		57
2043	17	28, 937	503			128	2	128	2		50
2044	18	28,937	437			128	2	128	2		43
2045	19	28, 937	380			128	2	128	2		37
2046 2047	20 21	28, 937 28, 937	330 287			128	1	128	1		32
2047	21	28, 937	287			128	1	128	1		249
2049	23	28, 937	217			128	1	128	1		21
2050	24	28,937	189			128	1	128	1		18
2051	25	28, 937	164			128	1	128	1		164
2052	26	28, 937	143			128	1	128	1		143
2053 2054	27 28	28, 937 28, 937	124			128	1	128	1		124
2054	29	28, 937	94			120	0	120	0		94
2056	30	28, 937	82			128	0	128	0		8
2057	31	28, 937	71			128	0	128	0		7
2058		28, 937	62			128	0	128	0		6
2059	33	28, 937	54			128	0	128	0		5
2060 2061	34 35	28, 937 28, 937	47			128	0	128	0		40
2061	36	28, 937	35			128	0	128	0		3
2063	37	28, 937	31			128	0	128	0		3
2064	38	28,937	27			128	0	128	0		2
2065	39	28,937	23			128	0	128	0		2
2066	40 41	28, 937	20 18			128	0	128	0		2
2067 2068	41	28, 937 28, 937	18			128	0	128	0		1
2000	43	28, 937	13			120	0	128	0		1
2070	44	28, 937	12			128	0	128	0		1
2071	45	28, 937	10			128	0	128	0		1
2072	46	28, 937	9			128	0	128	0		
2073 2074	47 48	28, 937 28, 937	8			128	0	128	0		
2074	40	28, 937	6			128	0	128	0		
2076	50	28, 937	5			128	0	128	0		
		1, 446, 833	36,023	44, 096	26, 073	7,523	582	51,619	26,654		9,36
	E	IRR	$\Sigma$ (B - C) / $\Sigma$ (1 +	io) <sup>t-1</sup> =0	0.172						
				t-1							
	1	NPV	$\Sigma (B - C) / \Sigma (1 +$	i) * *	9, 369						

### ANNEX Table 4.5.24 Cash Flow (Case<sup>①</sup> Alternative Plan B-2-1)

	BEN	IEFIT								
	1	2	3	4	5	6	0	8	B/C	B-c
	BENEFIT	PRESENT VALUE	COST	PRESENT VALUE	MAINTENANCE	PRESENT VALUE	COST	PRESENT VALUE		
			4, 389	4, 389	13	13	4, 402	4, 402		-4, 4
			4, 389	3, 817	26	22	4, 415	3, 839		-3,
			4, 389	3, 319	38	29	4, 428	3, 348		-3,
			8, 279	5,444	62	41	8, 341	5,485		-5,
			3, 890	2, 224	74	42	3, 963	2, 266		-2,
			3, 890	1,934	85	42	3,975	1,976		-1,
			3, 890	1,682	96	42	3, 986	1, 723		-1,
			3, 890 3, 890	1,462	108	40 39	3, 997 4, 009	1, 503 1, 310		-1,
			930	264	113	35	1, 052	299		-
			930	230	124	31	1,054	261		-
			930	200	127	27	1,057	227		-
			930	174	130	24	1,060	198		-
1	28, 937	4, 703			130	21	130	21		4,
2	28, 937	4,090			130	18	130	18		4,
3	28, 937	3,556			130	16	130	16		3,
4		3,092			130	14	130	14		3,
5		2,689			130	12	130	12		2,
6		2,338			130	10	130	10		2
7		2,033			130	9	130	9		2
8		1, 768			130	8	130	8		1
9		1,537			130	7	130	7		1
0		1,337			130	6	130	6		1
1		1,163 1,011			130	5	130 130	5		1
2		879			130	5	130	5		1
1		764			130	3	130	4		+
<del>י</del> 5		665			130	3	130	3		+
6		578			130	3	130	3		+
7		503			130	2	130	2		-
8		437			130	2	130	2		1
9		380			130	2	130	2		+
0	28, 937	330			130	1	130	1		
1	28, 937	287			130	1	130	1		
2	28, 937	250			130	1	130	1		
3	28, 937	217			130	1	130	1		
4	28, 937	189			130	1	130	1		
5		164			130	1	130	1		
6		143			130	1	130	1		
7		124			130	1	130	1		
8		108			130	0	130	0		
9		94			130	0	130	0		
) 1		82			130	0	130	0		
2		62			130	0	130	0		+
3		54			130	0	130	0		-
4		47			130	0	130	0		+
5		47			130	0	130	0		+
6		35			130	0	130	0		+
7		31			130	0	130	0		1
3		27			130	0	130	0		1
9	28, 937	23			130	0	130	0		
)	28, 937	20			130	0	130	0		
1	28, 937	18			130	0	130	0		
2		15			130	0	130	0		
3		13			130	0	130	0		+
1		12			130	0	130	0		
5		10			130	0	130	0		
6		9			130	0	130	0		+
7		8			130	0	130	0		+
8		7			130	0	130	0		+
9 0		6			130	0	130	0		+
J	28, 937 1, 446, 833	36,023		26, 410	130 7, 616	0 589	130 52, 231	0 26, 999		9
		$\Sigma (B - C) / \Sigma (1 + C)$		0. 171	7,010	589	92, 231	20, 999		9
	NPV	$\Sigma$ (B - C) / $\Sigma$ (1 +	- x t-1	9,024						

### ANNEX Table 4.5.25 Cash Flow (Case<sup>(2)</sup>) Alternative Plan B-3)

	_	REN	NEFIT								(10 <sup>6</sup> PESOS)
Year		1	2	3	4	5	6	Ø	8	B/C	B-c
····		BENEFIT	PRESENT VALUE	COST	PRESENT VALUE	MAINTENANCE	PRESENT VALUE	COST	PRESENT VALUE	5, 0	
2014		DENELTI	TRESENT VALUE	4, 389	4, 389	13	13	4, 402			-4, 4
2015				4, 389	3, 817	26	22	4, 415			-3, 8
2016				4, 389	3, 319	38	29	4, 428	3, 348		-3, 3
2017				8, 299	5, 457	62	41	8, 362	5,498		-5,4
2018				3, 910	2, 236	74	42	3, 984	2, 278		-2,2
2019				3, 910	1,944	85	42	3,995	1,986		-1, 9
2020				3,910	1,690	97	42	4,007	1, 732		-1,
2021				3, 910	1,470	108	41	4, 018	1,511		-1,
2022 2023				3, 910 1, 022	1, 278 290	119	39 35	4, 029	1, 317 325		-1,
2023				1, 022	290	122	35	1, 144	284		-
2024				1, 022	233	123	28	1, 147	247		-
2026				1, 022	191	131	25	1, 153	216		-
2027	1	28, 937	4, 703			131	21	131	21		4,
2028	2	28, 937	4, 090			131	19	131	19		4,
2029	3	28, 937	3, 556			131	16	131	16		3,
2030	4	28, 937	3, 092			131	14	131	14		3,
2031	5	28, 937	2, 689			131	12	131	12		2,
2032	6	28, 937	2, 338			131	11	131	11		2,
2033	7	28, 937	2,033			131	9	131	9		2,
2034	8	28,937	1, 768			131	8	131	8		1,
2035 2036	9 10	28, 937 28, 937	1, 537			131		131			1,
2036	10	28, 937 28, 937	1, 337			131	6	131	6 5		1,
2037	12	28, 937	1, 103			131	5	131	5		1,
2039	13	28, 937	879			131	4	131	4		.,
2040	14	28, 937	764			131	3	131	3		
2041	15	28, 937	665			131	3	131	3		
2042	16	28, 937	578			131	3	131	3		
2043	17	28, 937	503			131	2	131	2		
2044	18	28, 937	437			131	2	131	2		
2045	19	28,937	380			131	2	131	2		
2046	20	28, 937	330			131	1	131	1		-
2047	21	28, 937	287			131	1	131	1		:
2048 2049	22 23	28, 937 28, 937	250 217			131	1	131	1		
2049	23	28, 937	189			131	1	131	1		
2051	25	28, 937	164			131	1	131	1		
2052	26	28, 937	143			131	1	131	1		
2053	27	28, 937	124			131	1	131	1		
2054	28	28, 937	108			131	0	131	0		
2055	29	28, 937	94			131	0	131	0		
2056	30	28, 937	82			131	0	131	0		
2057	31	28, 937	71			131	0	131	0		
2058		28, 937	62			131	0	131	0		
2059	33	28, 937	54			131	0	131	0		
2060 2061	34 35	28, 937 28, 937	47			131	0	131	0		+
2061	36	28, 937	41			131	0	131	0		+
2062	37	28, 937	33			131	0	131	0		+
2064	38	28, 937	27			131	0	131	0		1
2065	39	28, 937	23			131	0	131	0		1
2066	40	28, 937	20			131	0	131	0		
2067	41	28, 937	18			131	0	131	0		
2068	42	28, 937	15			131	0	131	0		
2069	43	28, 937	13			131	0	131	0		
2070	44	28,937	12			131	0	131	0		
2071	45	28, 937	10			131	0	131	0		
2072 2073	46 47	28, 937 28, 937	9			131	0	131	0		+
2073	47	28, 937	7			131	0	131	0		-
2074	40	28, 937	6			131	0	131	0		+
2076	50	28, 937	5			131	0	131	0		1
		1, 446, 833			26, 554	7,692	592	52, 797			8,
			$\Sigma (B - C) / \Sigma (1 +$		0.171						
		NPV	$\Sigma$ (B - C) / $\Sigma$ (1 +	i) <sup>t-1</sup>	8, 877						

### ANNEX Table 4.5.26 Cash Flow (Case<sup>(3)</sup>) Alternative Plan B-2-2)

APPENDIX III: Technical Working Group Material September 6, 2013 Japan International Cooperation Agency Department of Public Works and Highway (DPWH)

## DATA COLLECTION SURVEY ON FLOOD MANAGEMENT PLAN IN METRO MANILA

# **Summary of Draft Final Report**

September, 2013

Yachiyo Engineering Co., Ltd.

1

2

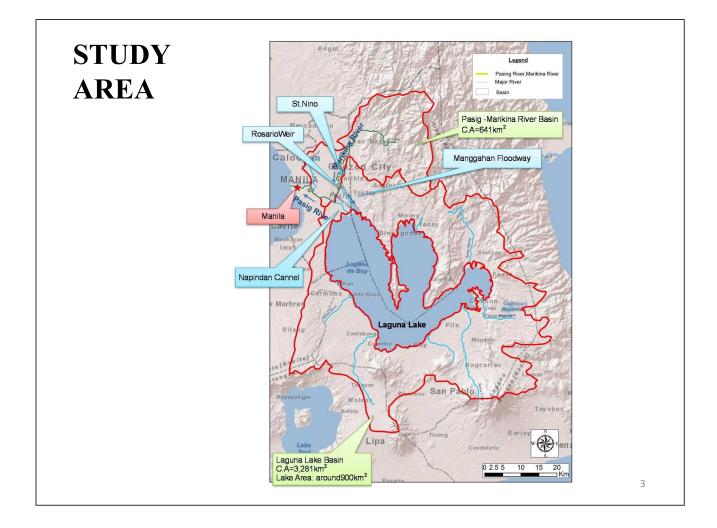
# **OBJECTIVE**

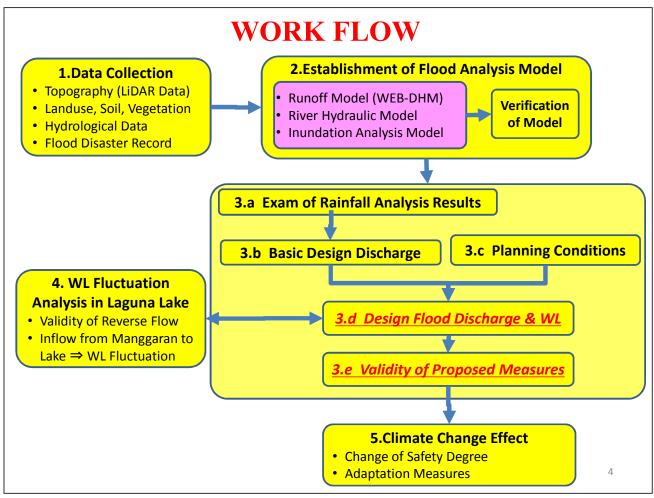
- To re-examine the technical validity of the proposed structural measures in Pasig-Marikina River Basin under the WB Study
- by utilizing the hydrological and hydrodynamic flood simulation model which is to be refined and updated with appropriately selected dataset
- in consideration of the future climate change;
- thereby bridging the concept planning and the actual implementation of projects.

# FRAMEWORK

• Counterpart in Philippines Side: DPWH

• Study Area: Pasig-Marikina River Basin & Laguna Lake Basin



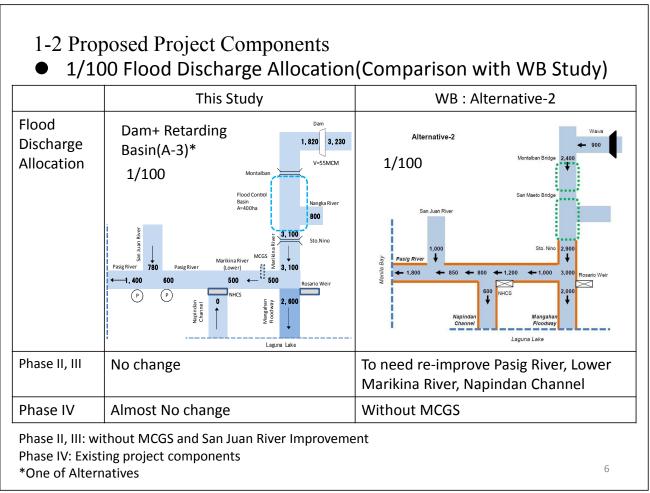


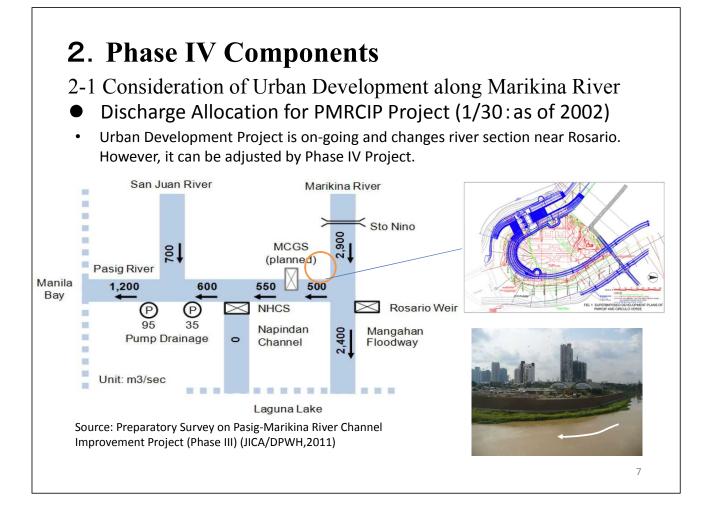
# **1.** Comparison with WB Study

# 1-1 Floods Utilized for Anlaysis

• In this Study, 7 observed floods including Typhoon Ondoy are selected while the WB selected only Typhoon Ondoy.

	This Study	WB
Design Hyetograph	7 Actual Hyetograph (including Ondoy) + Middle- peak Fictional Hyetograph	Ondoy +Middle-peak Fictional Hyetograph
Rainfall Duration	1day	2days
Design Rainfall	1/100:285.5mm/day	1/100:439mm/2days (Marikina Basin)
Period of Rainfall Analysis	1951-2012 (6 Stations)	1976-2010 (6 Stations)
		5



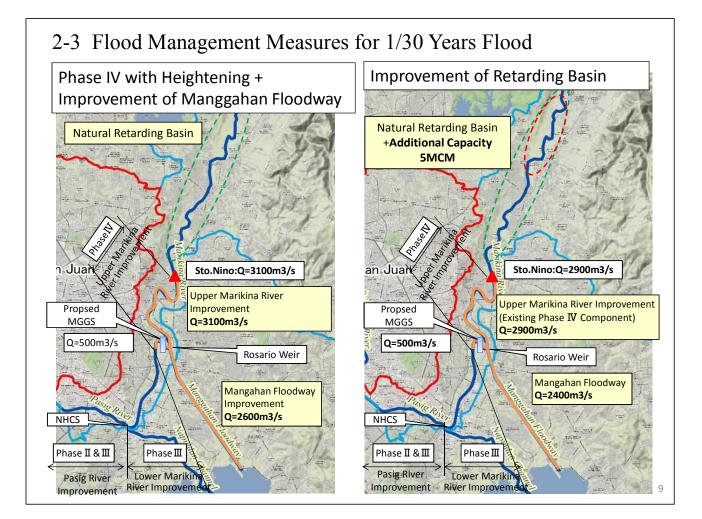


# 2. Phase IV Components

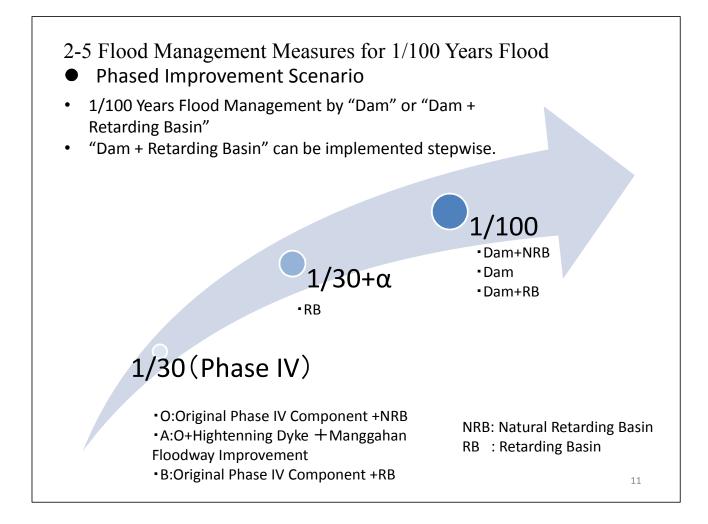
### 2-2 Basic Design Discharge of 1/30 Years Flood

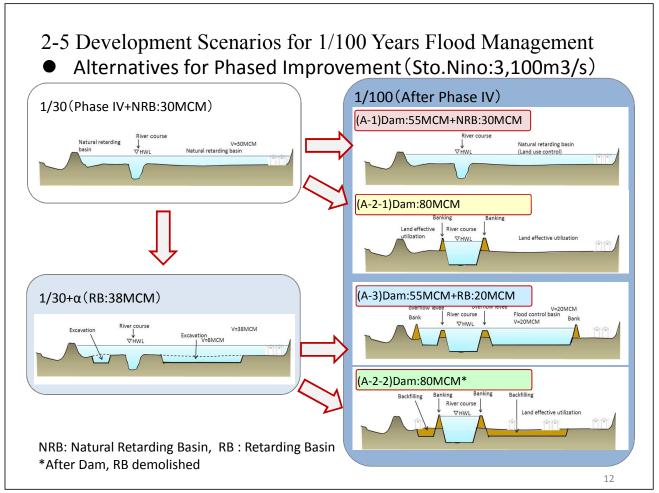
	D/D 2002(1/30 as of 2002)	This Study(1/30 as of 2013)
Design Hyetograph	Middle-peak Fictional Hyetograph	7 Actual Hyetograph (including Ondoy) + Middle-peak Fictional Hyetograph (Maximum:Ondoy)
Design Rainfall	1/30 :401mm/2days (Period of Rainfall Analysis:1903- 1999, 1 Station)	1/30:232.4mm/day (Period of Rainfall Analysis:1951- 2012,6 Stations)
Flood Analysis Model	Lumped System Model Storage Function Model Quasi-Linear Model	Distributed System Model River Basin :WEB-DHM Model River Course: 1-D Unsteady Flow Model Flood plain: 2-D Unsteady Flow Model
Basic Design Discharge	Sto.Nino:2,900m3/s	<b>Sto.Nino:3,100m3/s</b> (With Retarding Function)

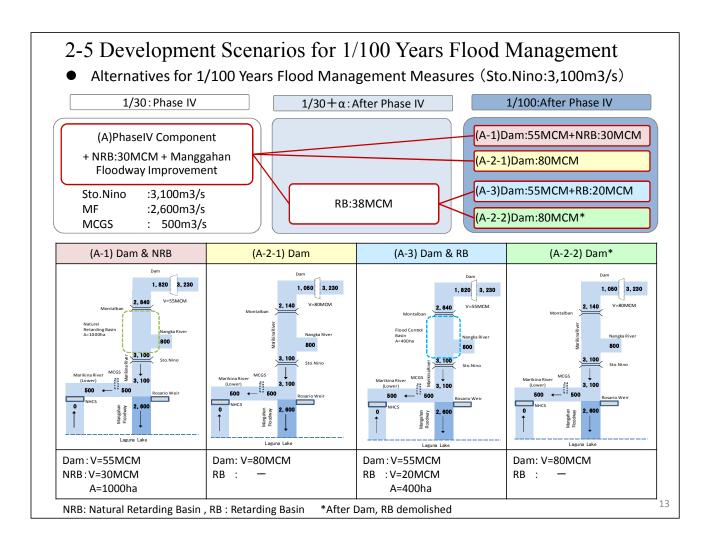
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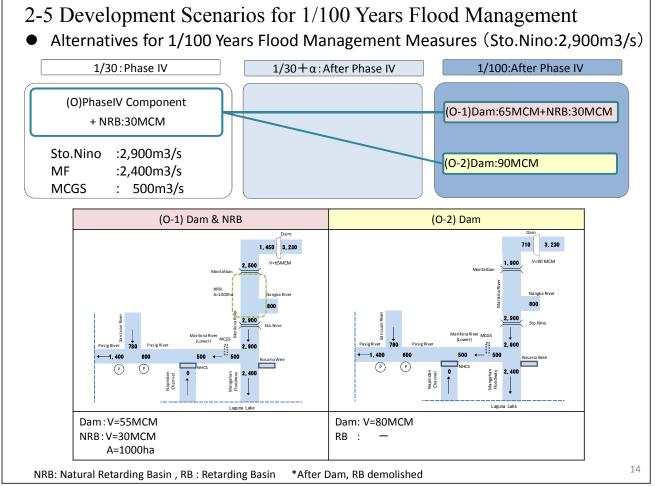


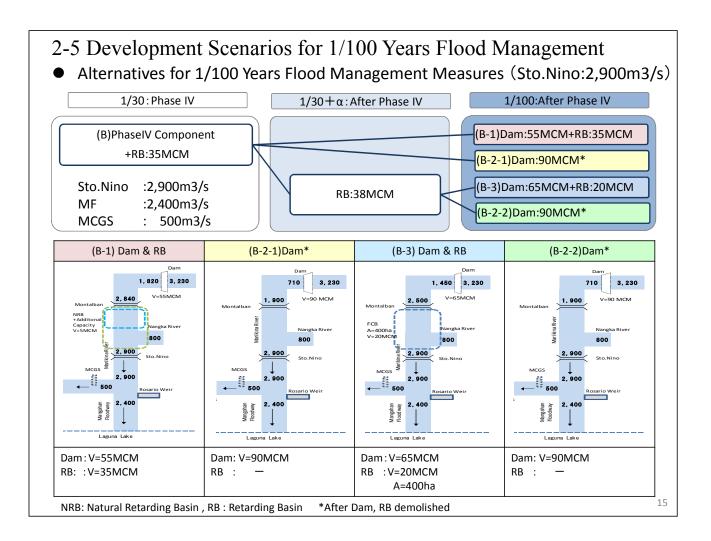
	ernatives Phase IV Control of the second sec	<u>A: Phase IV + Manggahan</u> FW	<u>B: Phase IV + Retarding</u> Basin
Sto.Nino	2900m3/s 1/30 (as of 2002)	3100m3/s 1/30(as of 2013)	2900m3/s 1/30(as of 2013)
Discharge Allocation	Montalban Natural Retarding Basin Marikina River (Lower) WCGS S00 S00 S00 S00 S00 S00 Kosario Weir Laguna Lake	Montalban Natural Retarding Basin MCGS Weight Univer (Lower) MCGS Sto. Nino MCGS Sto. Nino MCGS Sto. Nino MCGS Sto. Nino MCGS Sto. Nino MCGS Sto. Nino MCGS Sto. Nino MCGS Sto. Nino MCGS Sto. Nino Laguna Lake	Montalban Natural Retarding Basin +Additonal Capacity V=SMCM Marikina River (Lower) Usy by the standard standar
Phase IV Section	Original Components	Heightening of Dyke 0.5m + Improvement of Manggahan FW	Original Components
Upstream of Phase IV Section	Current Natural Ret. Basin	Current Natural Ret. Basin	Natural + Enhancement V=5MCM

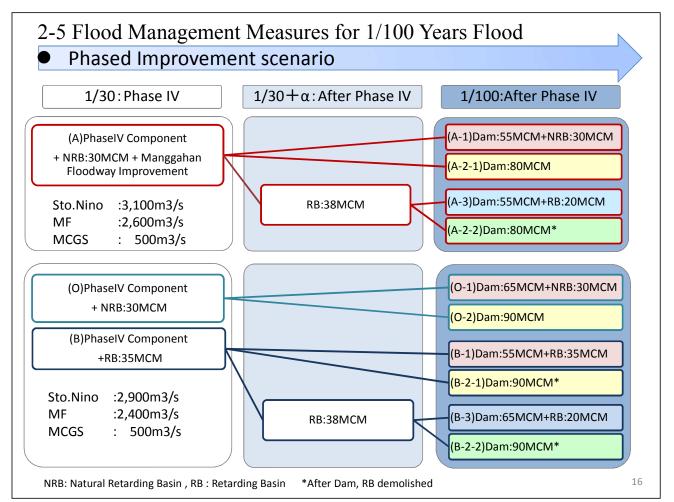


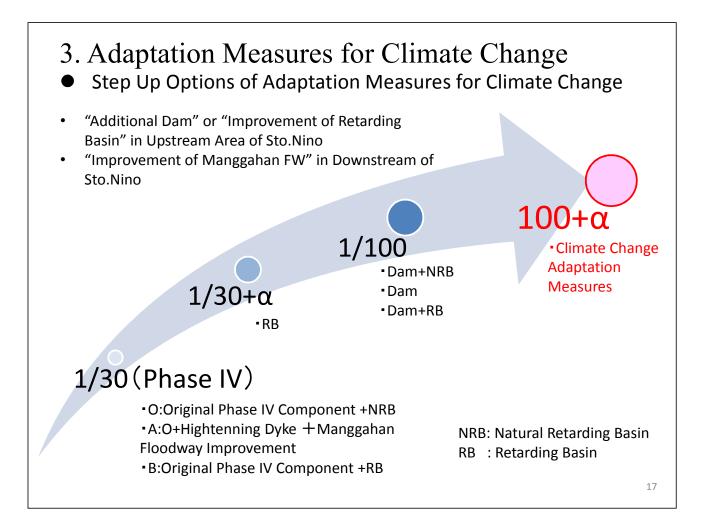


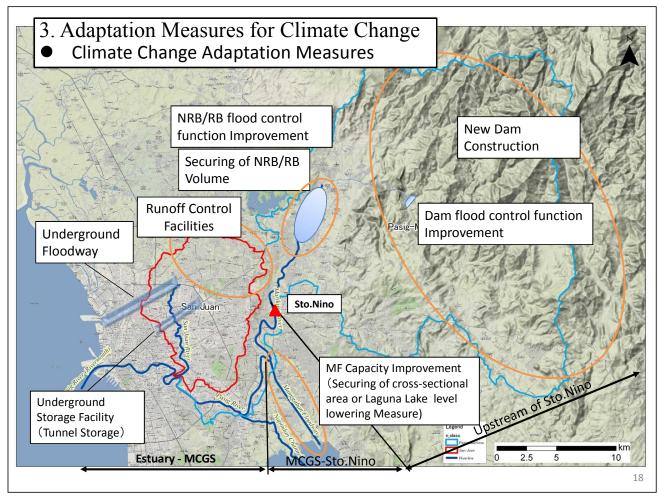


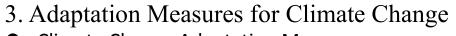




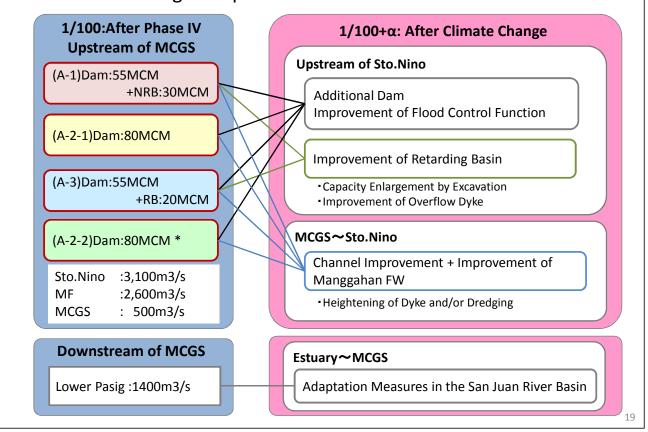








Climate Change Adaptation Measures



# 4. Points of The Study 4-1 Comparison with WB Study

# (1) Floods Utilized for Analysis

• This Study selects 7 observed floods including Typhoon Ondoy.

# (2) Proposed Project Components

- This Study confirmed that 1/100 years Flood Management is possible as Original Master Plan shows by putting countermeasures in Upper-Upper Marikina after completion of Phase-IV.
- This Study confirmed that large scale re-improvement in Phase I III sections is not necessary.

# 4-2 Phase IV Components

 This Study proposed various alternatives of the phased development scenario to 1/100 years flood management. These alternatives are useful for selection of final optimum components.

# 4-3 Adaptation Measures for Climate Change

 This Study proposed various step-up options of Adaptation Measures for Climate Change. These options are useful for selection of final adaptation measures. APPENDIX IV: Explanatory Material to Secretary February 13, 2014

# Minutes of Meeting between JICA & WB Both parties acknowledged the importance of proceeding with Phase IV including MCGS subject to: - Full timelines of processing of Phase IV and upstream measures will be prepared. - Subsequent studies (both Phase IV and upstream measures) will be conducted. The result of those studies will be commonly used for the best optimized flood management structures within the basin. Decision of DPWH taking into account parameters and ٠ aspects including but not limited to economic cost, time, benefit, social and environmental aspect, protection of asset and goods, strategic political choices etc. should be the most respected. 1

Japan International Cooperation Agency Department of Public Works and Highway (DPWH)

### DATA COLLECTION SURVEY ON FLOOD MANAGEMENT PLAN IN METRO MANILA

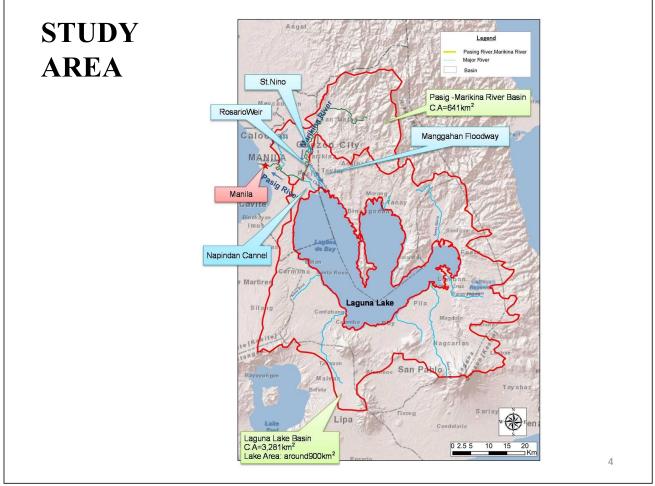
# **Summary of Draft Final Report**

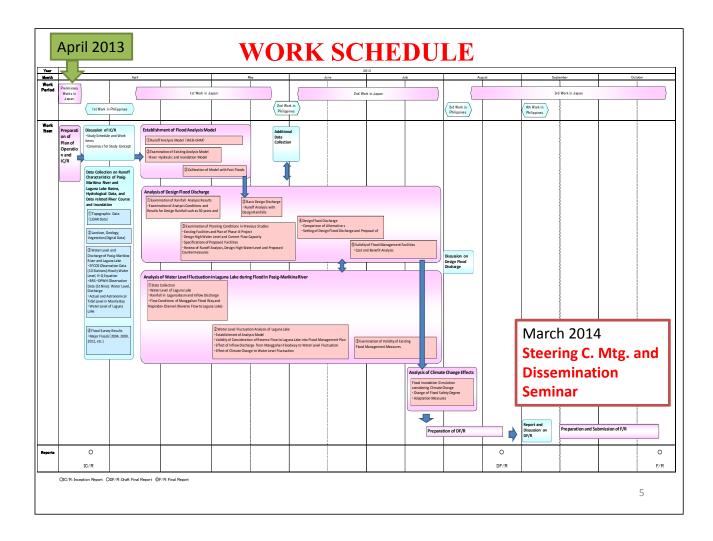
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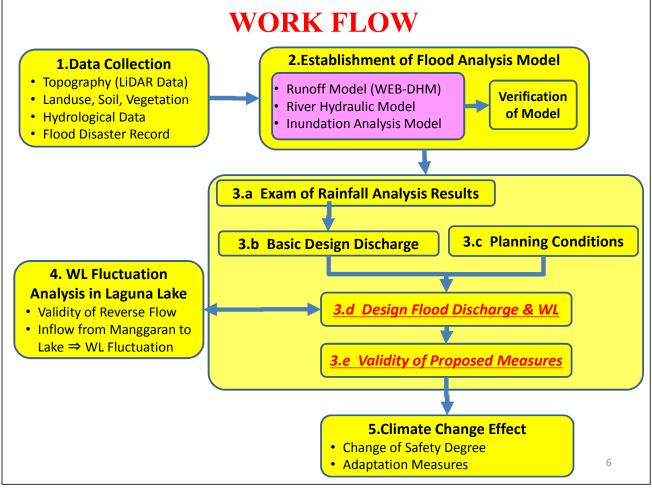
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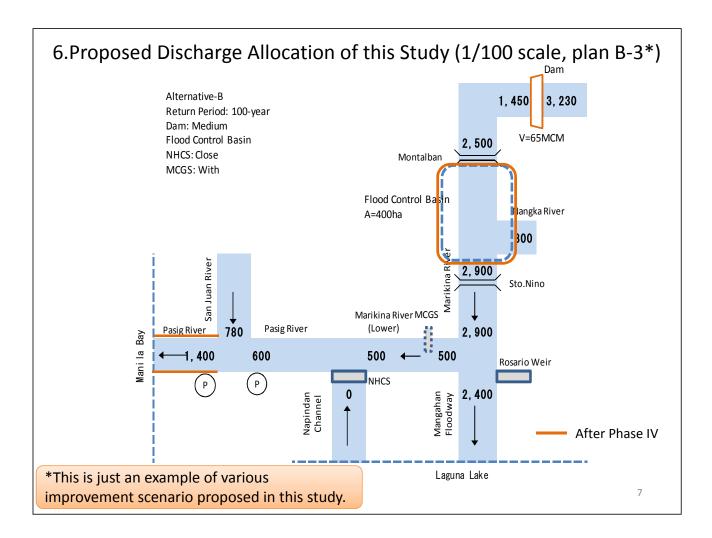
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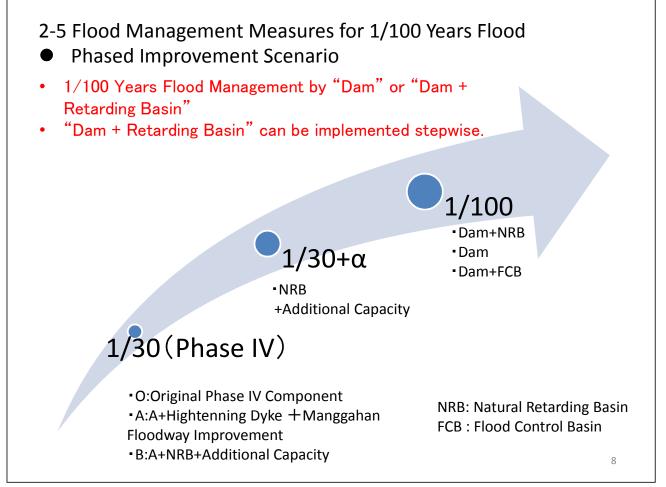
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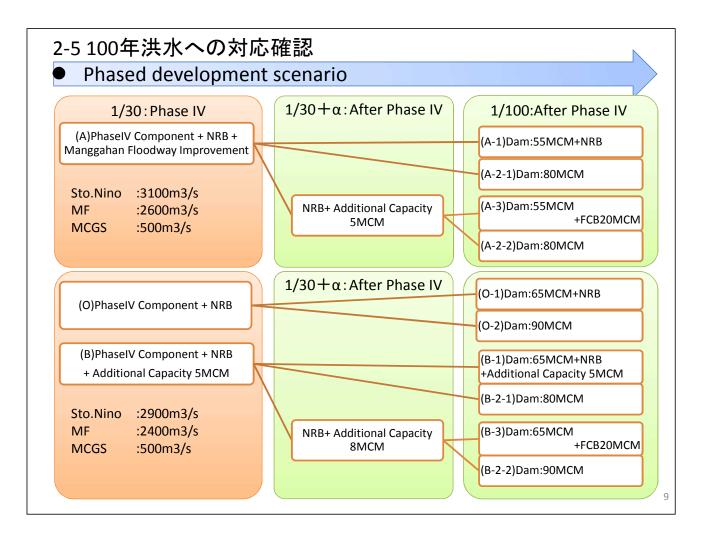


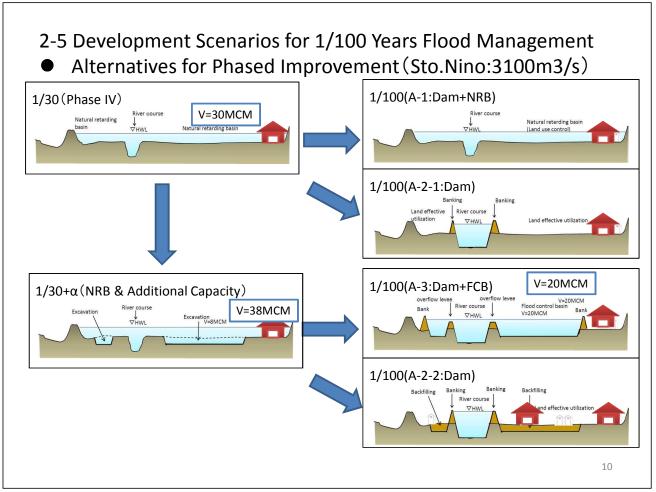


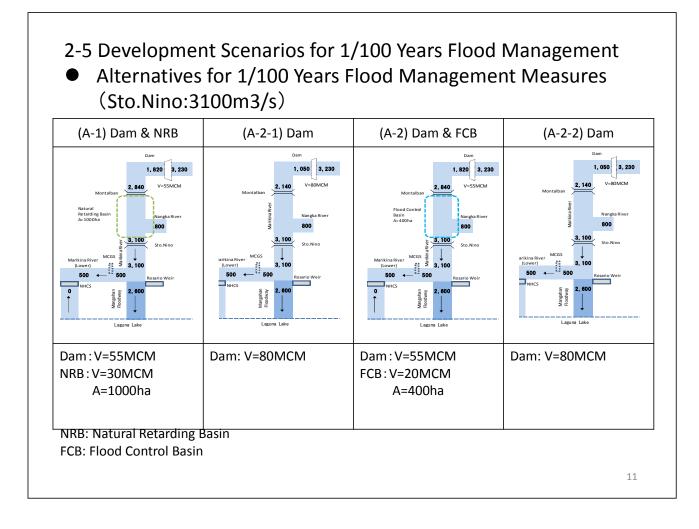




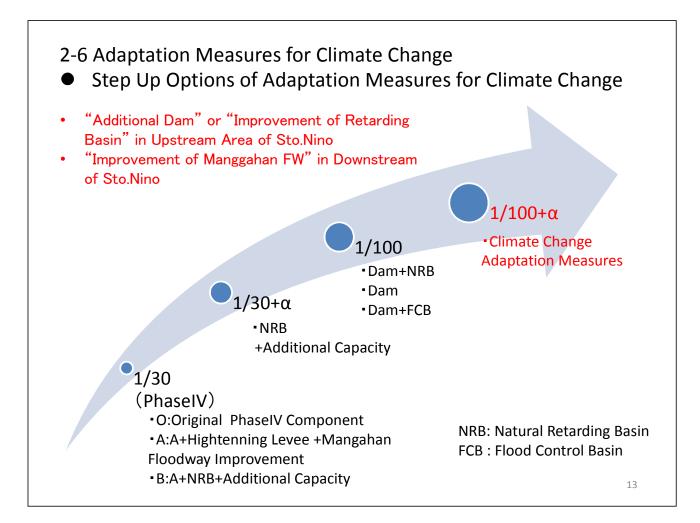


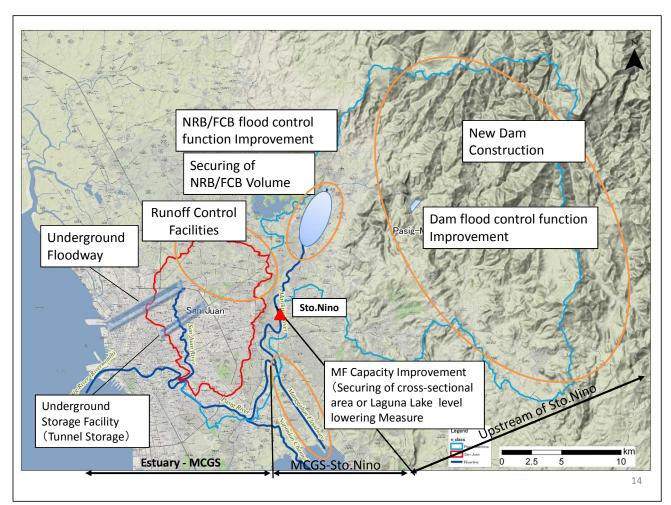


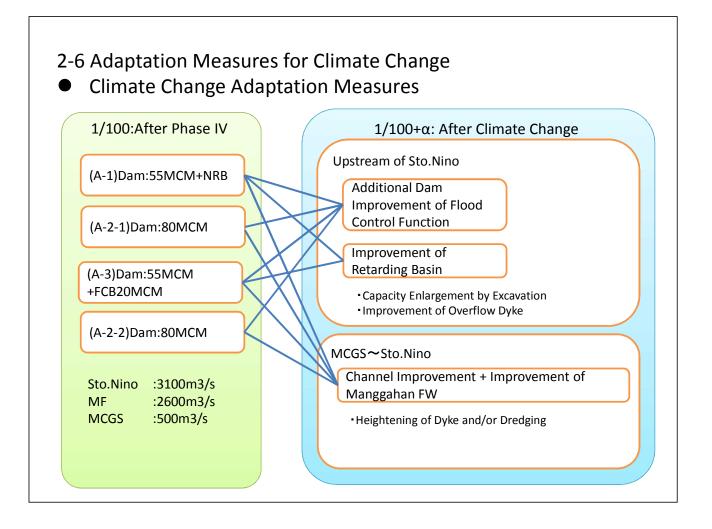


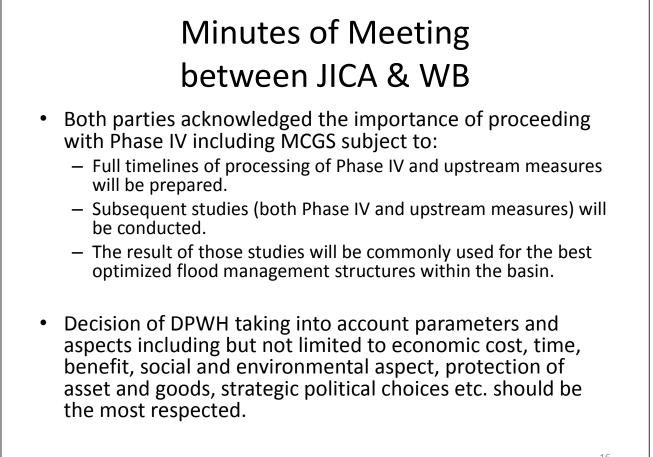


### 2-5 Development Scenarios for 1/100 Years Flood Management Alternatives for 1/100 Years Flood Management Measures (Sto.Nino:2900m3/s) (B-1)Dam & (O-1) Dam & (O-2) Dam NRB+Additional (B-2-1)Dam (B-3)Dam & FCB (B-2-2)Dam NRB Capapcity 3, 230 3, 230 3, 230 710 710 3, 230 Dam: V=90MCM Dam: V=90MCM Dam: V=65MCM Dam: V=90MCM Dam: V=65MCM Dam: V=65MCM NRB: V=30MCM NRB:V=35MCM FCB: V=20MCM A=1000ha Additional A=400ha Capacity: V=5MCM **NRB: Natural Retarding Basin** FCB: Flood Control Basin 12









# Recommendations

- Further flood management works in Pasig-Marikina River Basin shall be implemented based on the results of this study, including:
  - rainfall analysis,
  - hydrological model,
  - hydrodynamic model,
  - inundation model,
  - design flood discharge, and
  - component combination plans with different facility scale under step-wise approach.

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 Restoration works of Manggahan Floodway shall be proceeded as soon as possible.