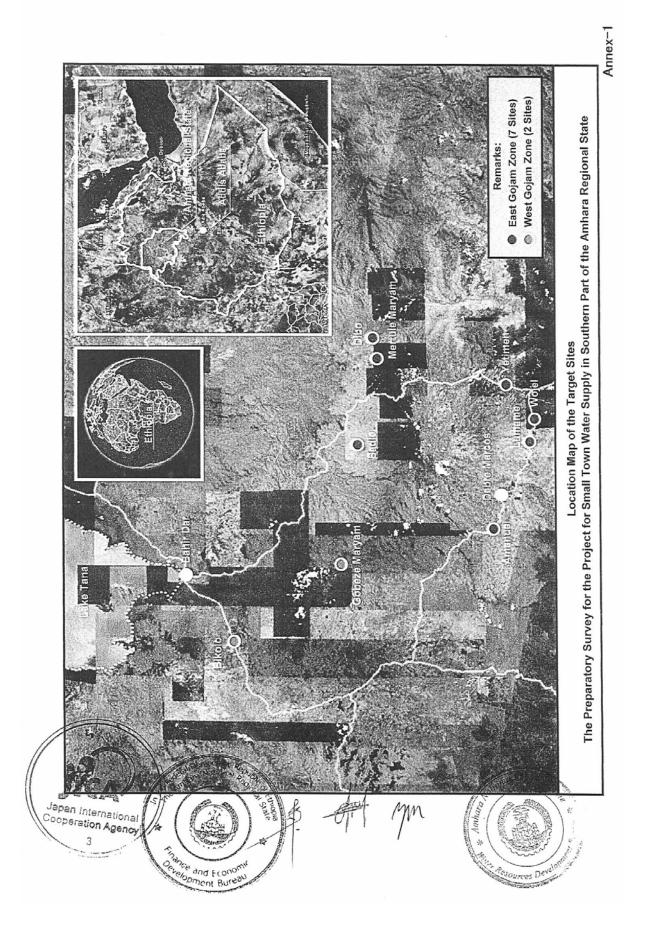
#### Annex:

- Annex-1 Project Sites
- Annex-2 Components of the Project
- Annex-3 Selected Sites
- Annex-4 Organization Chart of the Responsible Organization

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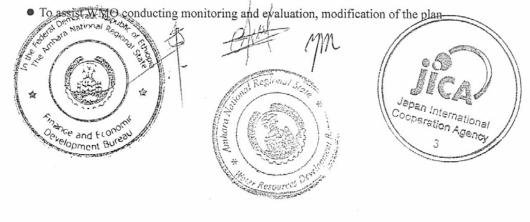
# Annex-2

# Components of the Project

No.	Town	Population (2016)	Water supply amount (2016) 328.97 m <sup>3</sup> /day		
9	Mertule Maryam	17,829			
10	Yetimen	3,877	74.33 m <sup>3</sup> /day		
12	Lumame	13,451	255.17 m <sup>3</sup> /day		
14	Wojel	3,758	121.22 m <sup>3</sup> /day		
15	Sedie	3,947	87.99 m <sup>3</sup> /day		
16	Dibo	2,510	89.22 m <sup>3</sup> /day		
	Amanuel	12,694	86.40 m <sup>3</sup> /day		
27	Gobeze Maryam	6,908	114.00 m <sup>3</sup> /day		
	Bikolo	5,811	181.43 m <sup>3</sup> /day		
	Total	70,786	1,338.73 m <sup>3</sup> /day		

1. Construction of Water Supply Facilities: 9 towns as listed below

- 2. Technical Assistance consisting of:
  - To facilitate AWRDB and Woreda water office on the effective support system in proper management of Water Management Organization (WMO)
  - To institutionalize the operation and maintenance structures of WMO
  - To secure general understanding among the stakeholders on the operation and maintenance structures
  - To conduct technical trainings on the maintenance and repair of the facilities (implemented by EWTEC)
  - To conduct technical trainings on administrative tasks such as accountancy, book keeping and reporting

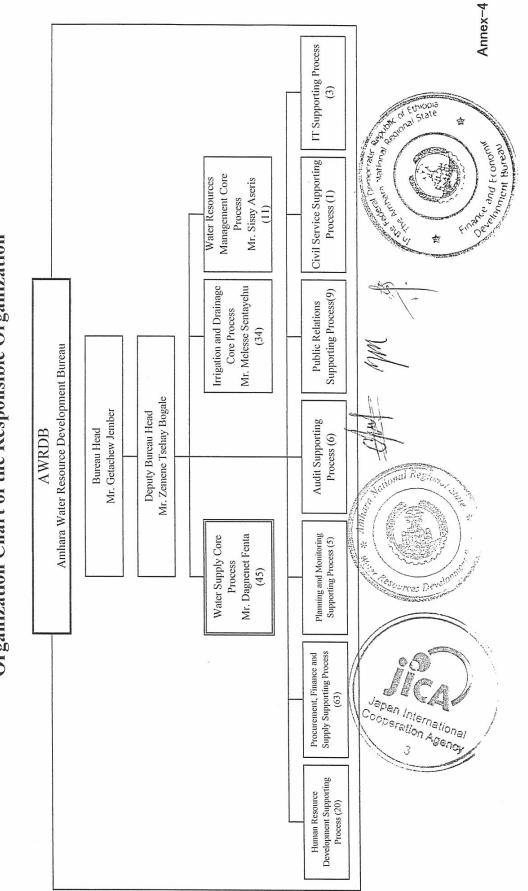


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# Annex-3

			Selected Target Sites			
	No.	Zone	Woreda	Town		
	9	East Gojam	Enebsie Sar Midir	Mertule Maryam		
	10	East Gojam	Enemay	Yetimen		
	12	East Gojam	Awabel	Lumame		
	14	East Gojam	Awabel	Wojel		
	15	East Gojam	Hulet Egu Enesie	Sedie		
	16	East Gojam	Enebsie Sar Midir	Dibo		
		East Gojam	Machakel	Amanuel		
	27	West Gojam	Quarit	Gobeze Maryam		
		West Gojam	Macha	Bikolo / /		
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- 2 -



**Organization Chart of the Responsible Organization** 

Appendix 5 Soft Component (Technical Cooperation) Plan

# The Project for Small Town Water Supply in Southern Part of the Amhara Regional State Soft Component (Technical Assistance) Plan

#### (1) Background of Planning the Soft Component

1) Present Situation and the Problem

In the target sites, the structure of operation and maintenance (O&M) for water supply facilities by existing Water Management Organization (WMO). However, the capability of planning to reserve O&M fee, collecting and managing water fee, and operating the water supply facilities are poor. The water supply facilities are left unrepaired and unattended, causing minor accidents. In the meantime, the role of Woreda water office of regular maintenance in order to avoid the accidents before they happen is not clear, and the budget and manpower are also insufficient. Therefore, the current problems of O&M by WMO are as follows:

- The structure of O&M is not secured.
- WMO cannot correspond to equipment operation and minor repairs.
- The capability of collecting and managing water fee (O&M cost) is poor by WMO.
- 2) Necessity of Soft Component

As mentioned above, there is the structure of O&M by existing WMO, however the capability of planning to reserve O&M fee, collecting and managing water fee, and operating the water supply facilities are poor. And the capability of minor repairs is also poor. The water supply facilities in the Project are planned as the composition and scale in order to conduct O&M by WMO, however, the structure of O&M and technique of existing WMO are poor. Therefore, in order to secure the commencement of the Project smoothly, technical assistance is given in the soft component, and supports to strengthen of the capability of O&M of WMO and Woreda water office. In the target sites, water supply facilities exist, hygiene philosophy is already made in the habitants; therefore hygiene education is not conducted in the soft component. The contents of technical support is placed priority on strengthening the capability of O&M (soft side); however, technical support of equipment operation and minor repairs (hard side) is also conducted in cooperation with the Ethiopian Water Technology Centre (EWTEC).

- (2) Objective of Soft Component
- 1) Objective

The objective of soft component is for O&M to be properly conducted by WMO. Moreover, the overall goal is defined as: long-term utilization of the constructed facilities after completion of the Project. In other words, the target is that the facilities will be utilized sustainably by O&M of the WMO after the completion of the Project. Project Design Matrix (PDM) of soft component is shown below.

# PDM (Soft component)

Summary of the Project	Indicator	Measurement	External condition
Overall goal			
Long-term utilization of facilities	Decline of percentage of the	* Statistical report about health	
after completion of the Project.	water-born disease rate of residents.	hygiene.	
		* Result of the questionnaire to	
		residents	
Target of the Soft Component			
Operation and maintenance are	* All facilities in Project area work	* Operation records of the	AWRDB does not
properly conducted by WMO	throughout the year	facilities	change the policy of
	* Increase safe water supply	* Log of facility users	O&M by WMO
	population in Project area.		
<u>Output</u>		* Overtionneire te nersone	
1. Executive system of the operation and maintenance of the facilities	1.1 The consciousness of the	* Questionnaire to persons concerned	Organization concerned
will be established.	implementing agency of the need	* Workshop Report	have no objection
will be established.	for citizen participation in O&M	* Chart of support system for	against the fact facilities
	is increased and a concrete	O&M	are operated by
	support system for the VWC is	* User rules	residents.
	developed.		
	1.2 The VWC of residents is formed	* Organization Chart for WMO	
	or reorganized in each village.	* O&M plan	
	1.3 Each organization and all	* Questionnaire to persons	
	residents concerned have a clear	concerned	
	understanding of their roles.	* Organization Chart for all concerned	
2. The concerned organizations	2.1 The period of breakdown is	* Records of the activities of the	
acquire the necessary skills and	shortened and the frequency of	organization concerned	
knowledge for operation and	breakdown is reduced.	* Operation records of the	
maintenance.		facilities	
		* Report of the technical	
		training	
		* Maintenance and repair	
		regulations	
	2.2 The records of administration	* Log of fee collection	
	containing the fee collection are	* Log of facility users	
	<ul><li>prepared in the WMO.</li><li>2.3 The monitoring and evaluation</li></ul>	* Implement report of soft	
	for the activities are carried out	* Implement report of soft component	
	and reflected in the activities of	component	
	the soft component		
Activities	*		Precondition
1.1 Formulate a support system of			All organizations
AWRDB and Woreda			concerned take an active
1.2 Formulate the O&M activities			part in the Project.
1.3 Obtain an understanding of the			part in the roject.
O&M activities			
2.1 Conduct the technical training			
(hard side) for the maintenance			
and repair of the facilities			
2.2 Conduct the technical training			
(soft side) of administrative			
tasks such as accountancy,			
record keeping and reporting			
2.3 Conduct monitoring, evaluation			
and modification of the plan			

#### 2) Considerations for the Support System

In the Project, O&M by the WMOs will be conducted for each site in two (2) phases: "Phase 1: Establishment of executive system," which is to be undertaken before the construction of facilities", and "Phase 2: Acquisition of O&M skills" during the construction. Concerning the technical O&M of the facilities, two (2) instructors from the Ethiopian Water Technology Centre (EWTEC) conducted the technical training for all persons concerned.

#### (3) Output of Soft Component

The expected outputs of the Soft Component are summarized as follows:

#### Output 1: Executive system of the O&M of the facilities will be established

The existing facilities are operated by the WMO of each site. But they cannot cope with various problems like repairs of malfunctions or inability of users to pay water rates. Other organizations such as AWRDB and Woreda water offices are in a position to fulfill this role, but their concrete support system also has not functioned smoothly.

With the soft component, the concrete support system will be established after reviewing the function of each organization with regard to WMO. In addition, concrete outcomes of the soft component will be ensured by establishing a plan of O&M which includes specific rules for the use of facilities.

#### Output 2: The concerned organizations acquire the necessary skills and knowledge for O&M

In order to conduct O&M by the WMO, it is necessary to compensate for the current lack of technical skills. After establishing a support system by administrative agency, the technical training (on hard and soft sides) for the persons in charge at the WMO and Woreda is executed to ensure they acquire the capacity to cope with concrete problems. With the technical training on hard side, the WMO will have the ability to repair slight troubles and if WMO is unable to handle a repair, the Woreda will be given the capacity to repair complicated problems. Consequently, the role of each organization will be clearly defined under the executive system of O&M. In addition, for O&M to be truly sustainable, it is paramount that the facility utilization fees are collected and managed properly. Therefore the chairman and accountants of WMO and Woreda will receive technical training on methods of accounting management (soft side).

Furthermore, in order to keep records of facilities usage and work done, the persons in charge at WMO and Woreda are given training on this and how to produce the records. The records made by WMO are presented to AWRDB through Woreda. With this joint information, the problems of fee collection or leaving facilities broken down will decrease.

#### (4) Indicator of Output Achievement

The indicator and measurement used to confirm the achievement of the two (2) output items are given in the table below.

0.45.4		Management
Output	Indicator	Measurement
Executive system of the O&M of the facilities will be established.	<ol> <li>The consciousness of the implementing agency of the need for citizen participation in O&amp;M is increased and a concrete support system for the WMO is developed.</li> <li>The WMO of residents is formed or reorganized in each willows</li> </ol>	<ul> <li>Questionnaire to person concerned</li> <li>Workshop Report</li> <li>Organization Chart for O&amp;M</li> <li>User rules</li> <li>Organization Chart for WMO</li> <li>O&amp;M plan</li> </ul>
	<ul> <li>village.</li> <li>3. Each organization and all residents concerned have a clear understanding of their roles.</li> </ul>	<ul> <li>Questionnaire to person concerned</li> <li>Organization Chart of all concerned</li> </ul>
The concerned organizations acquire the necessary skills and knowledge for O&M.	<ol> <li>The period of breakdown is shortened and the frequency of breakdowns is reduced.</li> </ol>	<ul> <li>Records of the agency concerned</li> <li>Operation records of the facilities</li> <li>Technical training report</li> <li>Maintenance and repair regulations</li> </ul>
	2. The records of administration containing the fee collection are prepared by the WMO.	<ul><li>Log of fee collection</li><li>Log of utilization</li></ul>
	3. The monitoring and evaluation for the activities are carried out and reflected in the activities of the soft component	<ul> <li>Monitoring/evaluation records</li> <li>Soft component report</li> </ul>

#### Indicator of output achievement

# (5) Plan of Soft Component Activities (Input Plan)

# 1) Division of the Activities

The Soft Component activities are categorized into two (2) phases: 1-Before construction and 2-During construction and after completion of main facilities. The activities will be carried out by the Japanese consultant with the cooperation of regional government staff such as AWRDB and Woreda. As to the technical training like inspection and repair of the facilities, it will be implemented with the cooperation of EWTEC.

# 2) Division of Roles

The role of the Japanese consultant and Woreda staff and EWTEC instructors are summarized as follows:

# Japanese Consultant

Overall responsibility for the Soft Component, and is in charge of:

- Supervision and implementation of this Project.
- Activities for commencing a workshop and a seminar.
- Meetings with AWRDB and implementation of workshops for Woreda staff.
- Cooperating and communicating with other donors and NGOs.
- Preparation of the support system for WMO of AWRDB and Woreda.

- Conduct a technical training (hard side) for the maintenance and repair of the facilities by EWTEC instructors.
- Technical training (soft side) for the administration.
- Preparation of O&M manual.
- Assistance for the drafting of all rules.
- Assistance for a preparation of all records.
- Monitoring of the activities and review of the evaluation.
- Review and the feedback of the results of each activity in each phase.
- Report to the AWRDB and JICA.

# Woreda Staff

Woreda staff will take part continuously in the entire Project, taking charge of activities to execute the work plan. During the Japanese consultant's absence, Woreda staff will keep a constant check on the progress of each activity. And also when the Japanese consultant is on site, they will arrange with the organization concerned and assist the activities.

- Support the establishment of WMOs by citizens in villages with water facilities.
- Organize resident meetings in each village.
- Confirm the situation of O&M in each site and report to the Japanese consultant.
- Organize the technical training (hard side) by EWTEC instructors.
- Cooperative support and regular inspection for the O&M of WMO.
- Assist the monitoring to the persons concerned.
- Adjustment with the organization concerned in absence of the Japanese consultant.

# EWTEC instructors

EWTEC instructors, as part of technical training (hard side) for the Woreda staff and WMO staff, are to teach:

- Basic knowledge about the new facilities.
- Method of the daily inspection.
- Method in case of failure (in case of slight damage and serious damage).
- Purchase of spare parts of the facilities.
- Rules of the facilities user.
- Cleaning of the facilities.

#### (6) Plan of the activities

The concrete content of the activities is as follows.

<Before the construction of main facilities - Establishment of executive system> Activity 1-1: Formulate a Support System of AWRDB and Woreda for the WMO

At the beginning of the Project, discussions will be held with the implementing agency, AWRDB concerning the objective, necessity and content of the Project, as well as the implementation plan.

Then a workshop will be held targeting the Woreda staff directly responsible for O&M activities in order to understand the condition of usage for the existing facilities, and the necessity and importance of O&M by the residents.

Through this workshop, Woreda staff will acquire the techniques needed to encourage resident participation by staff of WMO and the residents. Japanese consultants produce the organization chart after considering the relation with the WMO and the clarification of the problem at the hearing for Woreda staff. Additionally, the concrete plan for the management system including the membership which is selected in Activity 1-2, their role, the method of member selection, the management resources, and the user regulation will be formulated by the Japanese consultant and Woreda staff.

Target participants:	AWRDB staff and Woreda staff
Implementer:	Japanese consultant (10 days), Vehicle
Output:	Organization chart for the support system

#### Activity 1-2: Formulate the O&M activities of WMO

A workshop will be held in order to make sure of the function and clarify the problems of the nine (9) sites in which the new facilities will be constructed. Considering the results, under the leadership of Woreda staff, the appropriate membership for the future O&M, its role, and the method of member selection should be presented to get the understanding for the current staff.

With regard to the implementation of O&M, the relation between WMO and residents will be reconsidered, and a plan that is appropriate to the level of cooperation and capacity of each WMO will be drafted prior to the next resident committee meeting. Especially regarding the remuneration of organization staff and the resources of management, the appropriate water fee, the method of collection, should be determined at this Stage 1-2 to submit to the resident committee at the Activity 1-3.

Target participants:	WMO Staff
Implementer:	Japanese consultant (9 days), Woreda staff (9 days), Vehicle
Outputs:	Organization chart for WMO, Draft of O&M activities

#### Activities 1-3: Obtain an understanding of the O&M activities

A workshop will be held targeting the residents based on the results of 1-1, 1-2 activities after explaining the short summary of O&M by Woreda staff who control each site. Through this workshop, it is necessary for the residents to understand the environmental management of the facilities for the sustainable water supply services, the importance of the participation in O&M for facilities according to the user rules, especially the necessity for the collection of the water fee. WMO staff will provide the draft of O&M that they compiled in Activity 1-2, and ask the residents for their cooperation.

Target participants:	Residents, Village council
Implementer:	Japanese consultant (9 days), Woreda staff (9 days), WMO staff (9 days),
	Vehicle

<During construction to after completion of main facilities - Acquirement of skills of the O&M> Activity 2-1: Conduct technical training for the maintenance and repair of the facilities

EWTEC instructors are to teach through on-the-job training (OJT) the Woreda staff and the WMO member in charge of management of the facilities: basic knowledge for technical training, the method of O&M, the method of daily maintenance, how to deal with breakdowns and techniques for minor repairs. This technical training will be conducted three (3) times, after construction is completed at the third, sixth and ninth (and final) site.

At the end of training, the repair manual for the malfunctions and operation record produced by the consultants shall be distributed to the related personnel so that they can practice the regular O&M measures by using the techniques and knowledge of O&M.

Target participants:	Woreda staff, WMO staff	
Implementer:	EWTEC instructors (21 days x 2 persons), Japanese consultant (15 days),	
	Vehicle	
Outputs:	Repair manual for the malfunctions, Activity record, Facility's operation	
	record, Technical training report	
Outputs:	Repair manual for the malfunctions, Activity record, Facility's operation	

# Activity 2-2: Conduct technical training of administrative tasks such as accountancy, record keeping and reporting

In order to acquire the techniques of O&M for facilities, Woreda staff, WMO staff and accountants receive OJT from consultants who are expert in the abovementioned fields. In the OJT, technical training concerning the administrative task as described below will be conducted.

- Setting a water facility utilization fee
- Fee collection management methods
- Expense of facility management
- Remuneration for staff

- Cost of spare parts in case of repair
- Method of calculation for repair fee
- Operation of facility, and
- Method of recording for operation.

Same as the Activity 2-1, manual concerning the administrative task, financial records for the collection fee would be formulated beforehand by the consultants. In case of any changes in the manual, modification should be done and distributed to the related persons.

Target participants:	Woreda staff, WMO staff, Residents
Implementer:	Japanese consultant (12 days), Vehicle
Outputs:	Manual for O&M, Financial records for the collection fee, Log of
	utilization

# Activity 2-3: Conduct monitoring and evaluation, modification of the plan

Monitoring and evaluation will be conducted by the related persons in order to confirm if the result of technical training regarding O&M facilities and administrative tasks is reflected in the activity faithfully. Japanese consultant provides the related person some guidance so that they can use the result for the activity of next site. Additionally after the completion of the Project, the related persons themselves will continue the monitoring and evaluation, and modify the plan of O&M on each occasion, as necessary.

Target participants:	Woreda staff, WMO staff, Residents
Implementer:	Japanese consultant (10 days), Vehicle
Outputs:	Monitoring plan

	Activity Items	Feature	Target Audience	Implementer
xecutive	1.1 Formulate a support system of AWRDB and Woreda for the WMO	Meeting Workshop	AWRDB Woreda	Japanese consultant
on of E system	1.2 Formulate the O&M activities of WMO	Workshop	WMO	Japanese consultant Woreda staff
Preparation of Executive system	1.3 Obtain an understanding of the O&M activities.	Resident meeting OJT	Inhabitants	Japanese consultant Woreda staff WMO staff
ills for	2.1 Conduct technical training for the maintenance and repair of the facilities	Seminar OJT	Woreda WMO	Japanese consultant EWTEC staff
Acquisition of the skills for O&M	2.2 Conduct technical training of administrative tasks such as accountancy, record keeping and reporting	Seminar OJT	Woreda WMO	Japanese consultant
Acquis	2.3 Conduct monitoring, evaluation, and modification of the plan	Monitoring/ Evaluation	Woreda WMO	Japanese consultant

Contents of soft component activity

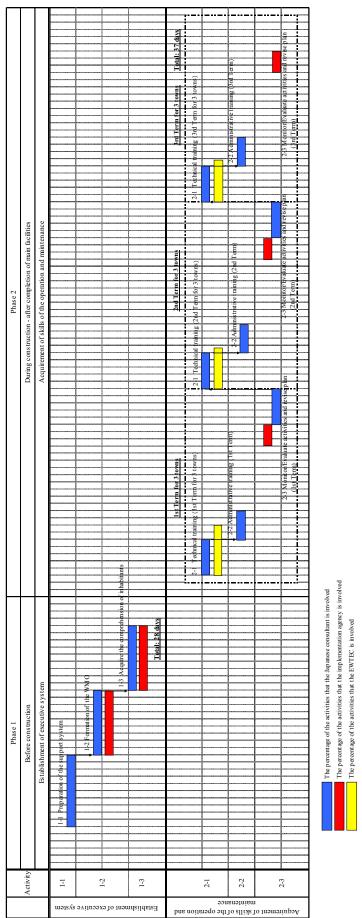
# (7) Supply a human resources for the Soft Component

The Project will be under the supervision of the Japanese consultant, however the technical training (on-the-job training) on various O&M and repair tasks will be conducted with the cooperation of EWTEC; meanwhile the persons in charge at Woreda and WMO will support training in each activity.

- (8) Implementation Schedule
- 1) Implementation Content

It is proper that some activities shall be implemented before commencement of construction, therefore the activities to be implemented in the soft component are divided into the following two (2) phases: "Phase 1: Before construction (28 days)" and "Phase 2: During construction (37 days)". The period of activity of the Japanese consultant will be assumed 65 days. Either the persons in charge at the WMO or in the Woreda office will accompany the Japanese consultants to participate in each activity at the various sites.

The technical training by EWTEC will be implemented over five days, and the Japanese consultant will accompany all this period to prepare a manual of technical maintenance. In addition, the monitoring and evaluation will be implemented by the persons concerned under the supervision of the Woreda staff.





Instructional control (control) (control)         Instructional control (control) (control)         Instructional control (contro)	<b></b>					n			-			-	1		
		Local staff (EWTEC×2)				14			14			14			42
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Autoristics National Systems         Autoristics National Systems         Number of security value         Number of value <th< td=""><td>ys to transfer</td><td>Local staff (EWTEC×2)</td><td></td><td></td><td></td><td>2 2</td><td></td><td></td><td>2 2</td><td></td><td></td><td>2</td><td></td><td></td><td>12</td></th<>	ys to transfer	Local staff (EWTEC×2)				2 2			2 2			2			12
Activity isens         Activit	Number of da	Japanese consultant (1)		4			4			4			t		16
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Activities No.         Activity items           1         Activities No.         Activity items           1         Formulate a support system of AWRDB and Woredu for the WMO         WMBB and Woredu for the WMO           1         Pormulate a support system of AWRDB and Woredu for the WMO         WMBB and Woredu for the WMO           1         Obtain an understanding of the O&M activities of WMO         WMO and the technical maining (hard side) for the mintenance and treporting.         WMO and the facilities.           2         Obtain an understanding of the O&M activities.         Dotain an understanding of the facilities.         WMO and the technical maining (hard side) for the mintenance and treporting.         WMO and the technical maining (hard side) for the mintenance and treporting.           3         Conduct the technical maining (hard side) for the mintenance and treporting.         WMO and the technical maining (hard side) for the mintenance and treporting.         WMO and the technical maining (hard side) for the mintenance and treporting.           3         Conduct the technical maining (hard side) for the mintenance and treporting.         WOO and the technical maining (hard side) for the mintenance and treporting.         Woredu suff           3         Conduct the technical maining (hard side) for the mintenance and treporting.         Woredu suff         Woredu suff           3         2         Conduct the technical maining (hard side) for the mintenance and treporting.         Woredu suff         W	Numbers of day	Jap anese consultant (1)	10	6	6	Ś	4	S	co.	4	S	v	4		65
Activity items         Activity items           1: 1: Formulate a support system of AVRDB and Woreda for the WMO         1: 1.           1: 1: 1         Formulate a support system of AVRDB and Woreda for the WMO         1: 1.           1: 1: 1         Formulate the O&M activities of WMO         1: 1.           1: 2         Formulate the O&M activities of WMO         1: 3.           1: 3         Obtain an understanding of the O&M activities of WMO         1: 3.           1: 3         Obtain an understanding of the fold it is:         2: 1.           2: 4         Conduct the technical training (hard side) for the maintenance and repair of the field it:         2: 2.           3: 4         Conduct the technical training of administrative tasks such as a diministrative tasks such as a diministrative tasks such as a diministration.         2: 3.           3: 4         Conduct the technical training of administration of the plin.         2: 3.           3: 4         Conduct the technical training of activities of administrative tasks such as a diministration.         2: 4.           3: 5         Conduct the technical training of activities of administration.         2: 4.           3: 5         Conduct the technical training of activities of administrative tasks such as a distribing of the plin.         2: 4.           3: 6         2: 7         Conduct the technical training of actonthance and repair of the plin.         2:		Implementer	Japanese consultant	Japanese consultant Woreda staff	Woreda staff WM O staff Japanese consultant	EWTEC instructors Japanese consultant	Tanan ana ana manakana	Japanese consultant	EWTEC instructors Japanese consultant	Tanan as a southing		EWTEC instructor Japanese consultant	Japanese consultant	Woreda staff	
2. Acquirement of skills of the operation and maintenance     1. Establishment of executive system       3. Acquirement of skills of the operation and maintenance     1. Establishment of executive system       3. Activities     1. Establishment of skills of the operation and maintenance       3. Activities     1. Establishment of skills of the operation and maintenance	t	l arget Audience	AWRDB staff Woreda staff	WM O staff	Residents Village council		WM O staff Woreda staff			WM O staff Woreda staff			WM O staff Woreda staff		
2. Acquirement of skills of the operation and maintenance system	4	Activity items	Formulate a support system of AWRDB and Woreda for the WMO	Formulate the O&M activities of WMO	Obtain an understanding of the O&M activities.	Conduct the technical training (hard side) for the maintenance and repair of the facilities	Conduct the technical training of administrative tasks such as accountancy, record keeping and reporting	Conduct monitoring and evaluation, modification of the plan.	Conduct the technical training (hard side) for the maintenance and repair for the facilities	Conduct the technical training of accountant, record, report concerning administration.	Conduct monitoring and evaluation, modification of the plan.	Conduct the technical training (hard side) for the maintenance and repair for the facilities	Conduct the technical training of administrative tasks such as accountancy, record keeping and reporting	Conduct monitoring and evaluation, modification of the plan.	
2. Acquirement of skills of the operation and maintenance system		stivities No.	ŀI	1-2	1-3										
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Basis for calculating the necessary number of days for the soft component

#### 2) Examination of validity of the number of and term of dispatches of the Japanese consultant

Japanese consultants will be dispatched four times into the field for O&M activities, and after considering the contents and the timing of execution, the activities will be conducted in two (2) phases; "Preparation of executive system" and "Acquisition of the skills for O&M".

The Japanese consultant will participate in all of the activities intended for the implementation organization. In the first phase, it is important to make an agreement with the persons concerned, and so it is necessary to confirm the activities in each period by the Japanese consultant. Similarly in phase 2, the Japanese consultant should stay at the site for the entire time during each activity to prepare a manual and records, and to give advice on the running of the OJT. Therefore, the dispatch term and the number of times of dispatches of the Japanese consultant are considered appropriate for the Project.

#### (9) Outputs of the soft component activities

The documents as outputs of the Project are as follows:

- Organizational framework of support system (Activity 1-1)
- User rules (Activity 1-1)
- Organizational framework of WMO (Activity 1-2)
- O&M plan (Activity 1-2)
- Repairing manual (Activity 2-1)
- Activity records (Activity 2-1)
- Operating records of facilities (Activity 2-1)
- Technical training report (Activity 2-1)
- O&M manual (Activity 2-2)
- Account book of water rates (Activity 2-2)
- Log of utilization (Activity 2-2)
- Monitoring plan (Activity 2-3
- Implementation report of soft component (for each dispatch period of Japanese consultants)
- Final report (to be submitted to Ethiopian and Japanese sides after Project completion)

# (10) Obligation of Recipient Country

In the implementation of the soft component, the concerned organization of recipient country is required to undertake certain measures, as follows:

- Supervision during the entire program in cooperation with the Japanese consultant.
- Reports to the upper level organizations concerned.
- Request for cooperation to other organizations concerned in carrying out the soft component.
- Provide staff of the organization concerned and cover their expense for the activities in the field, transportation, their daily allowance and accommodation charge.
- Coordination of lectures of technical training by the instructor of EWTEC.
- Burden of the working expenses for the preparation of the workshop space and for the joint committee meeting.

# Appendix 6 Other Relevant Data 6-1 Collected Data List

No.	Item	Config	juration	Original / Copy	Issuing Institution	Year
1	Hydrogeological Map of Northern Ethiopia, S=1/1,000,000	Hydrogeologic al Map	Drawing / Electronic File	Сору	GSE	2002
2	Regional Hydrogeological Investigation of Northern Ethiopia	Instruction Manual	Electronic File	Сору	GSE	2003
3	Geological Map of the Bahir Dar Area (NC37-1), S=1/250,000	Geological Map	Drawing / Electronic File	Сору	GSE	2010
4	Geology Geochemistry and Gravity Survey of the Bahir Dar Area	Instruction Manual	Electronic File	Сору	GSE	2010
5	Geological Map of the Debre Tabor Area (NC37- 2), S=1/250,000	Geological Map	Drawing / Electronic File	Сору	GSE	2010
6	Geology Geochemistry and Gravity Survey of the Debre Tabor Area	Instruction Manual	Electronic File	Сору	GSE	2010
7	Geological Map of the Bure (NC37-5), S=1/250,000	Geological Map	Drawing / Electronic File	Сору	GSE	2007
8	Geology of Bure map Sheet (NC37-5)	Instruction Manual	Electronic File	Сору	GSE	2007
9	Geological Map of Debre Marcos Sheet (NC37-6), S=1/250,000	Geological Map	Drawing / Electronic File	Сору	GSE	2009
10	Topografhic Map, S=1/250,000, EMA3, NC37-1, Bahir Dar	Topographical Map	Drawing	Сору	EMA	1996
11	Topografhic Map, S=1/250,000, 1502, NC37-2, Debre Tabor	Topographical Map	Drawing	Сору	EMA	1972
12	Topografhic Map, S=1/250,000, EMA3, NC37-5, Bure	Topographical Map	Drawing	Сору	EMA	1995
13	Topografhic Map, S=1/250,000, EMA3, NC37-6, Debre Mark'os	Topographical Map	Drawing	Сору	EMA	1995
14	Topografhic Map, S=1/50,000, ETH4, , Debre Mark'os	Topographical Map	Drawing	Сору	EMA	1995
15	Topographic Map S=1/50,000, ETH 4 1037 A2 DABI (Gebez Maryam)	Topographical Map	Drawing	Сору	EMA	1987
16	Topographic Map S=1/50,000, ETH 4 1037 A3 BURE (Mankusa, Kuchie)	Topographical Map	Drawing	Сору	EMA	1987
17	Topographic Map S=1/50,000, ETH 4 1037 B2 KERANIYO (Keranyo, Sedie)	Topographical Map	Drawing	Сору	EMA	1984
18	Topographic Map S=1/50,000, ETH 4 1037 C1 KUCH (Kuchie)	Topographical Map	Drawing	Сору	EMA	1987
19	Topographic Map S=1/50,000, ETH 4 1037 D2 AMBER (Amberi, Lumamie)	Topographical Map	Drawing	Сору	EMA	1984
20	Topographic Map S=1/50,000, ETH 4 1037 D4 LUMAME (Amberi, Lumamie)	Topographical Map	Drawing	Сору	EMA	1984
21	Topographic Map S=1/50,000, ETH 4 1038 A2 MERTO LEMARYAM (Mertle Maryam, Dibo)	Topographical Map	Drawing	Сору	EMA	1998
22	Topographic Map S=1/50,000, ETH 4 1038 C1 BICHENA (Bichena, Yetimen)	Topographical Map	Drawing	Сору	EMA	1984
23	Topographic Map S=1/50,000, ETH 4 1038 C3 DEJEN (Wejele)	Topographical Map	Drawing	Сору	EMA	1984
24	Topographic Map S=1/50,000, ETH 4 1137 A1 KUNZLA (Kunzila)	Topographical Map	Drawing	Сору	EMA	1987
25	Topographic Map S=1/50,000, ETH 4 1137 C1 MER AWI (Mer-Awi)	Topographical Map	Drawing	Сору	EMA	1987
26	Topographic Map S=1/50,000, ETH 4 1137 C4 ADAMA TERARA (Gebez Maryam)	Topographical Map	Drawing	Сору	EMA	1987
27	Topographic Map S=1/50,000, ETH 4 1137 D3 GONJ (Gonji Kollela)	Topographical Map	Drawing	Сору	EMA	1984

GSE: Geological Survey of Ethiopia EMA: Ethiopian Mapping Agency

# Appendix 7 References 7-1 Hydraulic Calculation

**Hydraulic Calculation** 

# 1. Mertule Maryam

#### 1.1. Basal Condition

Since the checked quantity of water intake is 424.01m3/day, and it is less than maximum daily supply and average daily supply, water facilities of Mertule Maryam are planed by total quantity of water intake.

# 1.2. Water Intake

There are two existing water sources in Mertule Maryam, both of two water sources are spring. One is transmitted to reservoir by gravity flow (139.35m3/day), and another is transmitted to the collection chamber by gravity flow (91.96m3/day) and then pumped up to reservoir.

The volume of existing collection chamber is 28.65m3 and another 28.83m3 of new collection chamber is designed, so totally 57.48m3 of volume of collection chambers are secured. Total volume of collection chamber is calculated 15 hours of volume of water intake (i.e.  $91.96m3 \times 15$  hours / 24 hours = 57.48m3).

It was confirmed that another three springs are existing in Mertule Maryam. One is 42.59m3/day of volume, second one is 92.70m3/day and third one is 57.41m3/day. These three springs are transmitted by gravity flow, so at the end of this project, total 424.01m3/day of volume of water intake is secured.

The specification of pump at collection chamber is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from collection chamber to reservoir tank is 40m and flow volume is 3.19L/sec (91.96m3/day / 8 hours), so it is needed 3.7kw of capacity of pump.

# 1.3. Transmission Line

The specification of transmission lines is calculated by the conditions of each water intake. Diameter is decided by the calculation with Hazen-Williams formula. Each distance of each water intake to reservoir tank is from 440m to 3015m. Diameters of transmission line are almost 3", only one transmission line's diameter is 1"1/2.

#### 1.4. Reservoir Tank

There are three existing reservoir tanks in Mertule Maryam. The volume is, first: 82.98m3, second: 50.36m3, third: 50.36m3. All the three reservoir tanks are not leaking water and it is useful, it is planed the new reservoir tank as additional. Required total capacity of reservoir tanks is 212.01m3, so short capacity is 28.31m3, it is planed 30m3 of reservoir tank by reinforced concrete.

#### 1.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Mertule Maryam, but some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

#### 1.6. Water Faucet

# 2. Yetimen

#### 2.1. Basal Condition

In Yetimen, average daily supply is 102.98m3/day, maximum daily supply is 123.58m3/day and checked quantity of water intake is 250.56m3/day. Quantity of water intake is sufficient, so water facilities of Yetimen are planed by average and maximum daily supply.

#### 2.2. Water Intake

There is one existing borehole as water sources in Yetimen, but new borehole was drilled and there is no problem about quality and quantity of that borehole, it is planed to use new borehole for this project.

From the borehole to reservoir tank, the water is pumped up, the specification of pump at borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from borehole to reservoir tank is 70m and flow volume is 4.29L/sec (123.58m3/day / 8 hours), so it is needed 5.5kw of capacity of pump.

#### 2.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Distance from borehole to reservoir tank is 1250m. Diameter of transmission line is 3".

#### 2.4. Reservoir Tank

There is an existing reservoir tank in Yetimen. The volume of reservoir tank is 60m3. Existing reservoir tank is now leaking, there is a option only to repair the existing reservoir tank, but preventing water leakage can not be guaranteed for the future because of the technical difficulty, new reservoir tank is planed in Yetimen.

Required capacity of reservoir tank is 64.36m3, so it is planed 70m3 of reservoir tank by reinforced concrete.

#### 2.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Yetimen, but some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

#### 2.6. Water Faucet

# 3. Lumame

#### 3.1. Basal Condition

In Lumame, average daily supply is 342.64m3/day, maximum daily supply is 411.17m3/day and checked quantity of water intake is 399.17m3/day. Quantity of water intake is enough for average daily supply, so water facilities of Lumame are planed by average daily supply and quantity of water intake.

#### 3.2. Water Intake

There are two existing boreholes as water sources in Lumame, but total quantity of those two boreholes is not enough for new water facilities (first: 57.60m3/day, second: 86.40m3/day, total: 144.00m3/day), so new borehole was drilled and it was confirmed the quantity of new borehole is 255.17m3/day. It is not enough for maximum daily supply but satisfied average daily supply, so it is planed to use all of three boreholes for this project.

From each borehole to reservoir tank, the water is pumped up, the specification of pump at borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Each total head from borehole to reservoir tank is 90m (first), 100m (second) and 110m (third). Flow volume is 2.00L/sec (57.60m3/day / 8 hours), 3.00L/sec (86.40m3/day / 8 hours) and 8.86L/sec (255.17m3/day / 8 hours), so each borehole need 5.5kw, 5.5kw and 15kw of capacity of pump.

# 3.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Existing transmission lines of existing two boreholes are combined on the line to reservoir tank. So, existing pumps do not function at the same time because of interfering with each other. It is planed to replace new transmission lines independently for existing transmission lines, and also planed to set new transmission line for new borehole.

Distance and diameter of each transmission line is 1927.22m (first: existing, 3"), 1475.14m (second: existing, 3"), 1208.09m (third: new, 4").

# 3.4. Reservoir Tank

There is an existing reservoir tank (elevated tank) in Lumame. The volume of existing reservoir tank is 50m3. Existing reservoir tank is functioning and new reservoir tank is planed to satisfy the total capacity of reservoir tank.

Required capacity of reservoir tank is 121.30m3, so it is planed 123m3 of reservoir tank by elevated type.

#### 3.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Lumame, but some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

#### 3.6. Water Faucet

# 4. Wojel

#### 4.1. Basal Condition

In Wojel, average daily supply is 101.02m3/day, maximum daily supply is 121.22m3/day and checked quantity of water intake is 224.64m3/day. Quantity of water intake is sufficient, so water facilities of Wojel are planed by average and maximum daily supply.

#### 4.2. Water Intake

There is one existing borehole as water sources in Wojel, but that borehole was abandoned and new borehole was drilled. There is no problem about quality and quantity of new borehole, it is planed to use new borehole for this project.

From the new borehole to reservoir tank, the water is pumped up, the specification of pump at borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from borehole to reservoir tank is 90m and flow volume is 4.21L/sec (121.22m3/day / 8 hours), so it is needed 7.5kw of capacity of pump.

# 4.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter of transmission line is decided by the calculation with Hazen-Williams formula. Distance from borehole to reservoir tank is 1000m. Diameter of transmission line is 3".

# 4.4. Reservoir Tank

There is an existing reservoir tank in Wojel. The volume of existing reservoir tank is 60m3 but that reservoir tank was deserted, so new reservoir tank is planed in Wojel.

Required capacity of reservoir tank is 63.14m3, so it is planed 70m3 of reservoir tank by reinforced concrete.

# 4.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Lumame, but every water facilities ware abandoned in wojel and it is difficult to confirm the condition of existing distribution line, so new distribution line is planed.

#### 4.6. Water Faucet

# 5. Sedie

#### 5.1. Basal Condition

In Sedie, average daily supply is 106.66m3/day, maximum daily supply is 127.99m3/day and checked quantity of water intake is 256.32m3/day. Quantity of water intake is sufficient, so water facilities of Yetimen are planed by average and maximum daily supply.

# 5.2. Water Intake

There is one existing borehole as water sources in Sedie, but new borehole was drilled and there is no problem about quality and quantity of that borehole, it is planed to use new borehole for this project.

From the borehole to reservoir tank, the water is pumped up, the specification of pump at borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from borehole to reservoir tank is 110m and flow volume is 4.44L/sec (127.99m3/day / 8 hours), so it is needed 7.5kw of capacity of pump.

# 5.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Distance from borehole to reservoir tank is 1455m. Diameter of transmission line is 3".

# 5.4. Reservoir Tank

There is an existing reservoir tank in Sedie. The volume of existing reservoir tank is 60m3. Existing reservoir tank is located low elevation, so new reservoir tank is planed in Sedie.

Required capacity of reservoir tank is 66.66m3, so it is planed 70m3 of reservoir tank by reinforced concrete.

# 5.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Sedie, but some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

#### 5.6. Water Faucet

# 6. Dibo

#### 6.1. Basal Condition

In Dibo, average daily supply is 74.35m3/day, maximum daily supply is 89.22m3/day and checked quantity of water intake is 256.32m3/day. Quantity of water intake is sufficient, so water facilities of Dibo are planed by average and maximum daily supply.

#### 6.2. Water Intake

There is no existing borehole and any other water facility in Dibo except hand pump, so new borehole was drilled and there is no problem about quality and quantity of that borehole, it is planed to use new borehole for this project.

From the borehole to reservoir tank, the water is pumped up, the specification of pump at borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from borehole to reservoir tank is 90m and flow volume is 3.10L/sec (89.22m3/day / 8 hours), so it is needed 5.5kw of capacity of pump.

#### 6.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Distance from borehole to reservoir tank is 2070m. Diameter of transmission line is 3".

#### 6.4. Reservoir Tank

There is no existing reservoir tank in Dibo. Required capacity of reservoir tank is 46.47m3, so it is planed 50m3 of reservoir tank by elevated type.

#### 6.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now there are no distribution lines in Dibo, so every pipeline for distribution is set as new.

#### 6.6. Water Faucet

# 7. Amanuel

#### 7.1. Basal Condition

In Amanuel, average daily supply is 326.76m3/day, maximum daily supply is 392.11m3/day and checked quantity of water intake is 230.40m3/day. Quantity of water intake is not enough for average and maximum daily supply, so water facilities of Amanuel are planed by quantity of water intake.

# 7.2. Water Intake

There are two existing boreholes as water sources in Amanuel, but one of existing boreholes is abandoned and quantity of another existing borehole is not enough (144.00m3/day) for new water facilities, so new borehole was drilled and it was confirmed the quantity of new borehole is 86.40m3/day. Total amount of water intake is not enough for average and maximum daily supply but it was not found another water intake as drilling, so it is planed to use two boreholes (existing and new) for this project.

From each borehole to reservoir tank, the water is pumped up, existing borehole and pump is functioning well, so at this project, only the pump for new borehole is set. The specification of pump at new borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from new borehole to reservoir tank is 100m. Flow volume is 3.00L/sec (86.40m3/day / 8 hours), so new borehole needs 5.5kw of capacity of pump.

# 7.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Existing transmission line is functioning, so only new transmission line from new borehole to reservoir tank.

Distance and diameter of new transmission line is 2386m. Diameter of transmission line is 3".

#### 7.4. Reservoir Tank

There is two existing reservoir tanks (elevated tank) in Amanuel. Although the volume of existing reservoir tanks are 60m3 and 30m3, both reservoir tanks are leaking. So it is planed to construct new reservoir tank, required capacity of reservoir tank is 115.2m3, so it is planed 120m3 of reservoir tank by elevated type.

#### 7.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Amanuel, but some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

#### 7.6. Water Faucet

# 8. Gobeze Maryam

#### 8.1. Basal Condition

Since the checked quantity of water intake is 164.00m3/day as a spring, and it is less than maximum daily supply and average daily supply, water facilities of Gobeze Maryam are planed by total quantity of water intake.

#### 8.2. Water Intake

There is a existing water source in Gobeze Maryam as spring. The water is transmitted to the collection chamber by gravity flow and then pumped up to reservoir.

The volume of existing collection chamber is 19.87m3 and another 82.63m3 of new collection chamber is designed, so totally 102.50m3 of volume of collection chambers are secured. Total volume of collection chamber is calculated 15 hours of volume of water intake (i.e.  $164.00m3 \times 15$  hours / 24 hours = 102.50m3).

The specification of pump at collection chamber is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from collection chamber to reservoir tank is 100m and flow volume is 5.69L/sec (164.00m3/day / 8 hours), so it is needed 11kw of capacity of pump.

#### 8.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Distance from water intake to reservoir tank is 1300m. Diameters of transmission line are 3".

#### 8.4. Reservoir Tank

There is a existing reservoir tank in Gobeze Maryam. The volume of existing reservoir tank is 50m3. But elevation of existing reservoir tank is not enough to distribute high area, existing reservoir tank will be abandoned and new reservoir tank is planed instead. Required capacity of reservoir tank is 102.50m3, so it is planed 105m3 of reservoir tank by reinforced concrete.

#### 8.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Gobeze Maryam, but some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

# 8.6. Water Faucet

# 9. Bikolo

#### 9.1. Basal Condition

In Bikolo, average daily supply is 151.19m3/day, maximum daily supply is 181.43m3/day and checked quantity of water intake is 403.20m3/day. Quantity of water intake is sufficient, so water facilities of Bikolo are planed by average and maximum daily supply.

#### 9.2. Water Intake

There is one existing borehole as water sources in Bikolo, but new borehole was drilled and there is no problem about quality and quantity of that borehole, it is planed to use new borehole for this project.

From the borehole to reservoir tank, the water is pumped up, the specification of pump at borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from borehole to reservoir tank is 110m and flow volume is 6.30L/sec (181.43m3/day / 8 hours), so it is needed 11kw of capacity of pump.

#### 9.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Distance from water intake to reservoir tank is 5533m. Diameters of transmission line are 4".

#### 9.4. Reservoir Tank

There is an existing reservoir tank in Bikolo. The volume of existing reservoir tank is only 25m3. Moreover, the location of existing reservoir tank is centering of Bikolo town, water pressure for distribution is not enough. That is why existing reservoir tank will be abandoned and new reservoir tank is planed instead at high area of Bikolo town. Required capacity of reservoir tank is 94.49m3, so it is planed 105m3 of reservoir tank by reinforced concrete.

#### 9.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Bikolo, but new reservoir tank is designed to construct at high area, it is needed to extend the distribution line. And some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

#### 9.6. Water Faucet

# Hydrologic Calculation

#### 1. Basic Number

No.	Towns	Zone	Woreda	Existing Population 2012	Projection of pop. 2016	School number of students	Hospital, Clinic
9	Mertule Maryam	East Gojam	Enebsie Sar Midir	15,124	17,829	7,180	10
10	Yetimen	East Gojam	Enemay	3,289	3,877	2,346	11
12	Lumame	East Gojam	Awabel	11,410	13,451	5,735	10
14	Wojel	East Gojam	Awabel	3,188	3,758	2,486	10
15	Sedie	East Gojam	Hulet Egu Enesie	3,348	3,947	2,712	10
16	Dibo	East Gojam	Enebsie Sar Midir	2,129	2,510	2,839	10
	Amanuel	East Gojam	Machakel	10,768	12,694	6,002	10
27	Gobeze Maryam	West Gojam	Quarit	5,860	6,908	4,938	10
	Bikolo(Wetet Abay)	West Gojam	Mecha	4,929	5,811	3,000	10
	Tota	al		60,045	70,785	37,238	91

---- Annual Growth Rate of Population ----Growth Rate : 4.2 %

--- Number of students and beds ---It is based on the result of field study.

#### 2. Water Demand

3. Volume of Water Intake

(AD : :	2012)								Jnit:m3/day	
No.	Towns	Dai General 20 l/c/day	School	emand(m3/d Hospital, Clinic 25 I/c/day	lay) Total	Ineffective water 15 %	Average Daily Supply	Maximum Daily Supply factor : 1.2	Peak Hourly Supply factor : 2.0	
9	Mertule Maryam	302.48	35.90	0.25	338.63	50.79	389.42	467.30	778.84	Unit of Water Demand :
10	Yetimen	65.78	11.73	0.28	77.79	11.67	89.46	107.35	178.92	
12	Lumame	228.20	28.68	0.25	257.13	38.57	295.70	354.84	591.40	
14	Wojel	63.76	12.43	0.25	76.44	11.47	87.91	105.49	175.82	
15	Sedie	66.96	13.56	0.25	80.77	12.12	92.89	111.47	185.78	Ineffective Water :
16	Dibo	42.58	14.20	0.25	57.03	8.55	65.58	78.70	131.16	
	Amanuel	215.36	30.01	0.25	245.62	36.84	282.46	338.95	564.92	Factor of Water Supply :
27	Gobeze Maryam	117.20	24.69	0.25	142.14	21.32	163.46	196.15	326.92	
	Bikolo(Wetet Abay)	98.58	15.00	0.25	113.83	17.07	130.90	157.08	261.80	
	Total	1,200.90	186.20	2.28	1,389.38	208.40	1,597.78	1,917.33	3,195.56	
(AD :	2016)							ι	Jnit∶m3⁄day	
		Dai	ily Water De	emand(m3/o	lay)	Ineffective	Average	Maximum Dailv	Peak Hourly	
No.	Towns	General	al School Hospital, Clinic		Total	water	Daily	Supply	Supply	
		20 l/c/day	5 l/c/day	25 l/c/day	Total	15 %	Supply		factor : 2.0	
9	Mertule Maryam	356.58	35.90	0.25	392.73	58.91	451.64	541.97	903.28	
10	Yetimen	77.54	11.73	0.28	89.55	13.43	102.98	123.58	205.96	
12	Lumame	269.02	28.68	0.25	297.95	44.69	342.64	411.17	685.28	
14	Wojel	75.16	12.43	0.25	87.84	13.18	101.02	121.22	202.04	
15	Sedie	78.94	13.56	0.25	92.75	13.91	106.66	127.99	213.32	
16	Dibo	50.20	14.20	0.25	64.65	9.70	74.35	89.22	148.70	
	Amanuel	253.88	30.01	0.25	284.14	42.62	326.76	392.11	653.52	
27	Gobeze Maryam	138.16	24.69	0.25	163.10	24.47	187.57	225.08	375.14	
	Bikolo(Wetet Abay)	116.22	15.00	0.25	131.47	19.72	151.19	181.43	302.38	
	Total	1,415.70	186.20	2.28	1,604.18	240.63	1,844.81	2,213.77	3,689.62	

- 20 I/c/day (Average Daily Demand)
  - l/c/day (School)
- 5 25 l/c/day (Hospital)

15 %

1.2 (Maximum Daily Supply)

Unit:m3/day

2.0 (Peak Hourly Supply)

		Maximum Daily	Volume of	Water Intak	(Existing)	Volume o	of Water Int	ake(New)	Volume o	of Water Int	ake(Total)	Design Volume		
No.	Towns	Supply m3/day	Borehole	Spring	Total	Borehole	Spring	Total	Borehole	Spring	Total	Water Intake	Water Coverage	Remarks
			0.00	139.35	139.35	0.00	0.00	0.00						Existing use
			0.00	91.96	91.96	0.00	0.00	0.00						Existing use
9	Mertule Maryam	541.97	0.00	0.00	0.00	0.00	42.59	42.59	0.00	424.01	424.01	424.01	78.23%	New
			0.00	0.00	0.00	0.00	92.70	92.70						New
			0.00	0.00	0.00	0.00	57.41	57.41						New
10	Yetimen	123.58	0.00	0.00	0.00	0.00	0.00	0.00	250.56	0.00	250.56	123.58	100.00%	Abolishment
10	reamen	120.00	0.00	0.00	0.00	250.56	0.00	250.56	200.00	0.00	200.00	120.00	100.00%	New
			57.60	0.00	57.60	0.00	0.00	0.00		0.00		399.17		Existing use
12	Lumame	411.17	86.40	0.00	86.40	0.00	0.00	0.00	399.17		399.17		97.08%	Existing use
			0.00	0.00	0.00	255.17	0.00	255.17						New
14	Wojel	121.22	0.00	0.00	0.00	0.00	0.00	0.00	224.64	0.00	224.64	121.22	100.00%	Abolishment
	110,01	121.22	0.00	0.00	0.00	224.64	0.00	224.64		0.00	224.04	121.22	100.00%	New
15	Sedie	127.99	0.00	0.00	0.00	0.00	0.00	0.00	256.32	0.00	256.32	127.99	100.00%	Abolishment
		127.00	0.00	0.00	0.00	256.32	0.00	256.32	200.02	0.00	200.02	127.00	100.000	New
16	Dibo	89.22	0.00	0.00	0.00	256.32	0.00	256.32	256.32	0.00	256.32	89.22	100.00%	New
			144.00	0.00	144.00	0.00	0.00	0.00						Existing use
	Amanuel	392.11	0.00	0.00	0.00	0.00	0.00	0.00	230.40	0.00	230.40	230.40	58.76%	Abolishment
			0.00	0.00	0.00	86.40	0.00	86.40						New
27	Gobeze Maryam	225.08	0.00	164.00	164.00	0.00	0.00	0.00	0.00	164.00	164.00	164.00	72.86%	Existing use
	Bikolo(Wetet Abay)	181.43	0.00	0.00	0.00	0.00	0.00	0.00	403.20	0.00	403.20	181.43	100.00%	Abolishment
	bikoid(Wetet Abay)		0.00	0.00	0.00	403.20	0.00	403.20		0.00			.43 100.00%	New
	Total	2,213.77	288.00	395.31	683.31	1,732.61	192.70	1,925.31	2,020.61	588.01	2,608.62	1,861.02	84.07%	

#### 4. Intake, Transmission Facilities

		Volume of V	Vater Intake	e(m3/day)		Elevat	ion(m)		Transmiss	ion Pipe, Inta	ake to the gr		und to Tank	Pump Plan(8h/day)			
No.	Towns	Spring Gravity Pump		Borehole	Intake Facilities Intake Point Ground		Tank	Vertical Drop	Length (m)	Diameter (mm)	Velocity (m/s)	Hydraulic Grade (‱)	Head loss (m)	Lifting Range (m)	Flow Volume (L/s)	Spec (kw)	
		139.35	0.00	0.00	2,737.94	2,737.94	2,711.09	26.85	800.00	75	0.37	3.66	2.93				
		0.00	91.96	0.00	2,630.69	2,630.69	2,667.92	-37.23	440.00	75	0.72	1.70	0.75	40.00	3.19	3.7	
9	Mertule Maryam	42.59	0.00	0.00	2,848.73	2,848.73	2,711.09	137.64	3,015.40	40	0.39	8.73	26.33				
		92.70	0.00	0.00	2,790.81	2,790.81	2,711.09	79.72	790.00	75	0.24	1.72	1.36				
		57.41	0.00	0.00	2,678.33	2,678.33	2,664.87	13.46	1,444.86	75	0.15	0.71	1.03				
10	Yetimen	0.00	0.00	123.58	2.382.83	2.405.63	2.445.78	-62.95	60.00	50	2.19	21.13	1.27	70.00	4.29	5.5	
10	reamen	0.00	0.00	123.30	2,302.03	2,403.03	2,443.78	02.95	1,250.00	75	0.97	2.93	3.67	70.00	4.23	5.5	
		0.00	0.00	57.60	2.418.84	2.464.13	2.505.77	-86.93	55.00	50	1.02	5.15	0.28	90.00	2.00	5.5	
12 Lumai		0.00	0.00	57.00	2,410.04	2,404.13	2,303.77	80.93	1,927.22	75	0.45	0.71	1.38	50.00	2.00	5.5	
	Lumame	0.00	0.00	86.40	2.412.34	2.462.95	2.505.77	-93.43	55.00	50	1.53	10.90	0.60	100.00	3.00	5.5	
		0.00	0.00	00.40	2,412.34	2,402.33	2,000.77	55.45	1,475.14	75	0.68	1.51	2.23	100.00	0.00	0.0	
		0.00	0.00	255.17	2.407.00	2.424.95	2.505.77	5.77 -98.77	40.00	65	2.67	22.52	0.90	110.00	8.86	15.0	
		0.00	0.00	255.17	2,407.00	2,424.55	2,303.77	50.77	1,208.09	100	1.13	2.76	3.34	110.00	0.00	13.0	
14	Nojel	0.00	0.00	121.22	2.403.96	2.442.88	2.488.58	-84.62	55.00	50	2.14	20.39	1.12	90.00	4.21	7.5	
14	110j01	0.00	0.00	121.22	2,400.00	2,442.00	2,400.00	2,400.00	04.02	1,000.00	75	0.95	2.83	2.83	50.00	7.21	7.5
15	Sedie	0.00	0.00	127.99	2.446.25	2.468.29	2.547.55	-101.30	60.00	50	2.26	22.55	1.35	110.00	4.44	7.5	
10	oculo	0.00	0.00	127.55	2,440.23	2,400.29	2,347.33	101.30	1,455.27	75	1.01	3.13	4.56	110.00	4.44	7.5	
16	Dibo	0.00	0.00	89.22	2.374.98	2.420.18	2.452.64	-77.66	55.00	50	1.58	11.57	0.64	90.00	3.10	5.5	
10	0.00	0.00	0.00	03.22	2,074.00	2,420.10	2,452.04	77.00	2,071.06	75	0.70	1.61	3.33	50.00	0.10	0.0	
		0.00	0.00	144.00	2.147.20	2.197.20	2.302.89	-155.69	100.00	50	2.55	28.05	2.80	170.00	5.00	13.0	
		0.00	0.00	144.00	2,147.20	2,137.20	2,002.00	100.00	2,800.00	75	1.13	3.89	10.90	170.00	5.00	10.0	
	Amanuel	0.00	0.00	144.00	2,302.89	2,302.89	2,397.78	-94.89	2,800.00		1.13	3.89	10.90	110.00	5.00	9.2	
		0.00	0.00	86.40	2.306.14	2.336.49	2.397.78	-91.64	32.00	50	1.53	10.90	0.35	100.00	3.00	5.5	
		0.00	0.00	00.40	2,000.14	2,000.40	2,007.70	51.04	2,386.25		0.68	1.51	3.61	100.00	0.00	0.0	
27	Gobeze Maryam	0.00	164.00	0.00	2,156.40	2,156.40	2,243.37	-86.97	1,304.06	75	1.29	4.95	6.46	100.00	5.69	11.0	
	Bikolo(Wetet Abay)	0.00	0.00	181.43	1.855.63	1,905.63	1.953.02	-97.39	50.00	65	1.90	11.98	0.60	110.00	6.30	11.0	
		0.00	0.00	101.43	1,000.00	1,000.00	1,000.02	57.35	5,533.39	100	0.80	1.47	8.14	110.00	0.30	11.0	
	Total	332.05	255.96	1,417.01													

#### 5. Transmission Facilities (Relay Tank)

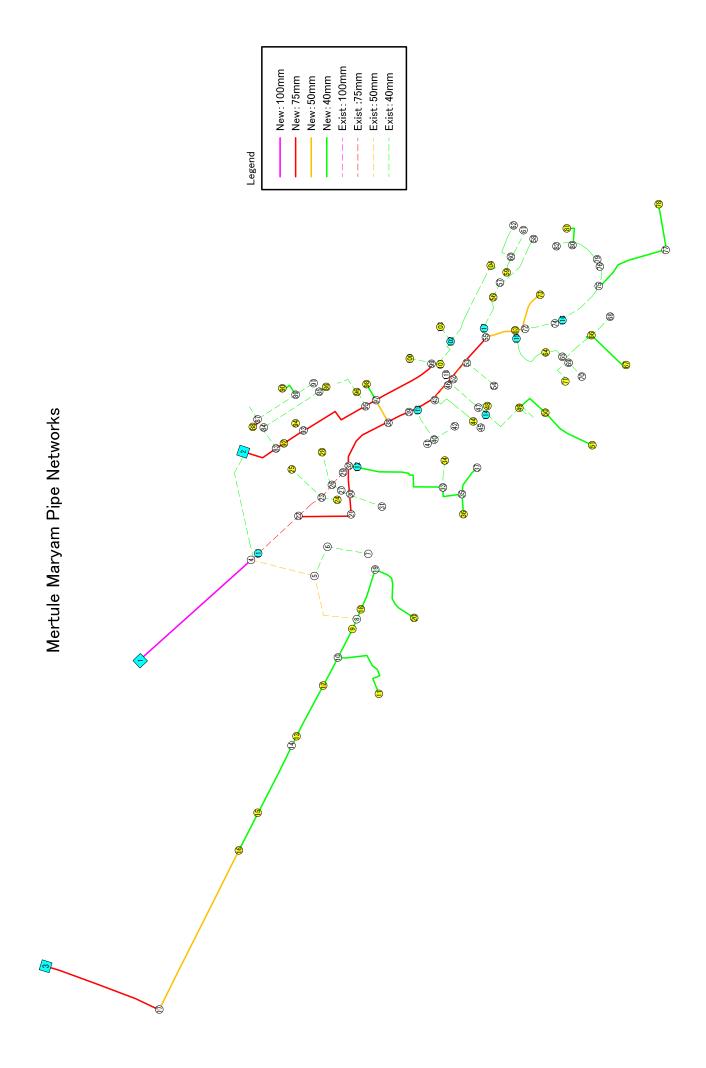
No.	Towns	Water Intake m3/day	Required Capacity of Tank (m3)	Vol. of Existing Tank (m3)	Additional capacity (m3)
9	Mertule Maryam	91.96	57.48	28.65	28.83
27	Gobeze Maryam	164.00	102.50	19.87	82.63

#### 6. Distribution Facilities (Reservoir Tank)

		Average Dailv	Volume of Intake	Required		Existing	Existing	Short			Plan of Res	servoir Tank			
No.	Towns	Supply	Water	Reservo	irs (m3)	Reservoir	Use	Capacity	Width	Length	Net Depth	Number of	Volume	Category	Remarks
		(m3/day)	(m3/day)	12 hour	15 hour	(m3)	(m3)	(m3)	(m)	(m)	(m)	Tank	(m3)	Gategory	
						82.98	82.98		φ 6.20		2.75	1	82.98	RC	Existing use
9	Mertule Marvam	451.64	424.01	212.01		50.36	50.36	28.31	φ 5.40		2.20	1	50.36	Stone Masonry	Existing use
5	wertuie waryam	401.04	424.01	212.01		50.36	50.36	20.31	φ 5.40		2.20	1	50.36	Stone Masonry	Existing use
									3.00	4.00	2.50	1	30.00	RC	New
10	Yetimen	102.98	123.58		64.36	60.00	0.00	64.36						Stone Masonry	Abolishment
10	reamen	102.96	123.00		04.30		-	04.30	4.50	6.00	2.50	1	67.50	RC	New
12	Lumame	Lumame 342.64 399.17 171.32			50.02	50.02	121.30	2.60	5.20	1.85	2	50.02	Elevated Tank	Existing use	
12	Lumame			1/1.32				121.30	4.00	7.50	2.05	2	123.00	Elevated Tank	New
14	Wojel	101.02	121.22		63.14	60.00	0.00	63,14						Stone Masonry	Abolishment
14	wojei	101.02	121.22		03.14			03.14	4.50	6.00	2.50	1	67.50	RC	New
15	Sedie	106.66	127.99		66.66	60.00	0.00	66.66~						Elevated Tank	Abolishment
15	Cedie	100.00	127.55		00.00			00.00	4.50	6.00	2.50	1	67.50	RC	New
16	Dibo	74.35	89.22		46.47	0.00	0.00	46.47	5.00	5.00	2.05	1	51.25	Elevated Tank	New
						60.00	0.00							Elevated Tank	Abolishment
	Amanuel	326.76	230.40	115.20		30.00	0.00	115.20						Elevated Tank	Abolishment
									4.00	7.50	2.05	2	123.00	Elevated Tank	New
27	Gobeze Maryam	187.57	164.00		102.50	50.00	0.00	102.50						Stone Masonry	Abolishment
21	CODEZE IVIALYAIII	107.07	104.00		102.50			102.50	3.00	7.00	2.50	2	105.00	RC	New
	Bikolo(Wetet Abav)	151.19	181.43	42 04.40 25.00 0		0.00	94.49						Stone Masonry	Abolishment	
	bikolo(welet Abay)	131.19	101.43		94.49			94.49	3.00	7.00	2.50	2	105.00	RC	New
	Total	1,844.81	1,861.02	498.53	437.62	578.72	233.72	702.43					868.47		

#### 7. Distribution Facilities (Pipeline)

Distribution pipelines of each site are determined by the hydraulic calculation.



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			Notes >>		Ground Level	ial Head Fr otion of Wa				」 目	$\begin{array}{c} 738. 592\\ 177. 672\\ 586. 845\\ 586. 845\\ 5532. 902\\ 5532. 902\\ 556. 867\\ 556. 867\\ 256. 867\\ 238. 912\\ 236. 847\\ 236. 847\\ 256. 997\\ 256. 997\\ 256. 997\\ 256. 997\\ 256. 997\\ 333. 917\\ 258. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 859. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 018\\ 858. 01$
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		ļ	Expla	Node		с:: Сс:			- Line	Node	$\begin{array}{c} & & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & & \\ & & & & \\ & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & &$
		   	$\approx$	I						ST	222298655433200988655547322
		Formula>>	(四)	(四)	(%)	(亚/ S)				Remarks	Reservoir Tank Reservoir Tank Protect Spring
		Hazen-Williams	69. 227	0.000	0.000	0.000				0c (1/s)	
			Maximum EHP	Minimum EHP	Maximum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\$
		ı ««Case.								EHP 1st (m)	
		Mertule Maryam	°3	109	113	6	0.00 (cm)	2 (times)	   	19	2, 611, 092 2, 667, 920 667, 920 678, 533 678, 548 678, 548 678, 548 678, 987 666, 099 667, 943 661, 574 661, 574 660, 943 660, 943 660, 943 660, 941 22, 660, 441 22, 660, 951 660, 951 22, 660, 951 22, 650, 905 674, 574 633, 156 777 756 757 757 756 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 757 75
· .		– – – – Me:	Tank	Node	Line	Pump, Decom	Convergence Gap	Calculation	NodeData	HF (a)	$\begin{array}{c} 2711. \ 092\\ 2667. \ 330\\ 26711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 092\\ 27711. \ 09$
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-	HL (II)	
	I (%)	
	V (面/ S)	
	0 (1/s)	
	Coef C	
	니 (j)	$\begin{array}{c} 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 77. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\$
LineData —	с (шш	333 50 50 50 50 50 50 50 50 50 50 50 50 50
- Line	Node T EN	$\begin{array}{c} 222\\ 223\\ 224\\ 225\\ 225\\ 225\\ 225\\ 225\\ 225\\ 225$
   	ST	300000111282233333322233332223333222233332222233333
	Remarks	
	0c (1/s)	
•	EHP 2nd (m)	$\begin{array}{c} 29, \ 723\\ 29, \ 723\\ 29, \ 723\\ 29, \ 723\\ 20, \ 777\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\\ 20, \ 781\ 20, \ 781\ 20, \ 781\ 20, \ 781\ 20, $
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112		633.		0.000		ure	113	40	38		110	0.000				
113		623.		0.000		ure	113	43	75	-	110	0.000				
114		598.		0.000		ure	114	49	38		110	0.000				
115	-	613.	-	0.000		reak Pressure Tan	115	64	38		110	0.000				
116		619.		0.000		алы	116	75	38		110	0.000				
117				0.000	0.000	ure	117	56	38	210.779	.110	0.000	0.000	0.000	0.000	0.000
- 118		611.		67.518			118	55	75		110	0.000				
							118	101	38		110	0.000				

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							ο	Head Loss Add Pressure		V (□/□)	$\begin{array}{c} 0.138\\ 0.138\\ 0.138\\ 0.138\\ 0.267\\ 0.267\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.$
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			Votes >>			Ξź			1	ц	$\begin{array}{c} 738 & 592 \\ 177 & 672 \\ 5386 & 845 \\ 5381 & 845 \\ 5332 & 902 \\ 5171 & 672 \\ 5172 & 845 \\ 5173 & 162 \\ 5173 & 162 \\ 388 & 912 \\ 388 & 912 \\ 388 & 912 \\ 375 & 927 \\ 375 & 927 \\ 375 & 997 \\ 375 & 997 \\ 375 & 997 \\ 375 & 997 \\ 375 & 901 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 334 & 166 \\ 336 & 186 \\ 336 & 186 \\ 337 & 166 \\ 337 & 166 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 & 100 \\ 338 $
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·		Formula>>	(田)	(III)	(%)	(ш/s)		١		Remarks	Reservoir Tank Protect Spring
		Hazen-Williams	67.985 (	0.000	64.767	1.125 (				0c (1/s)	$\begin{array}{c} -6 \\ -6 \\ -6 \\ -6 \\ -6 \\ -6 \\ -6 \\ -6 $
		••	Maximum EHP	Minimum EHP	Maximum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0. \ 0.00\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0. \ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\ 0.000\\ 0.000\ 0.000\\ 0.000\ 0.000\\ 0.000\ 0.000\ 0.000\\ 0.000\$
		n < <case.2< td=""><td></td><td></td><td></td><td></td><td>÷</td><td></td><td></td><td>EHP 1st (m)</td><td></td></case.2<>					÷			EHP 1st (m)	
		-Mertule Maryam	60	109	113	6	0.88 (cm)	16 (times)	   	IJ.	$\begin{array}{c} 2,\ 711,\ 092\\ 2,\ 678,\ 330\\ 667,\ 330\\ 678,\ 568,\ 449\\ 676,\ 987\\ 666,\ 092\\ 666,\ 092\\ 666,\ 092\\ 666,\ 092\\ 666,\ 093\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 611\\ 633\\ 660,\ 441\\ 633\\ 660,\ 441\\ 633\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 639,\ 156\\ 156\\ 156\\ 156\\ 156\\ 156\\ 156\\ 156\\$
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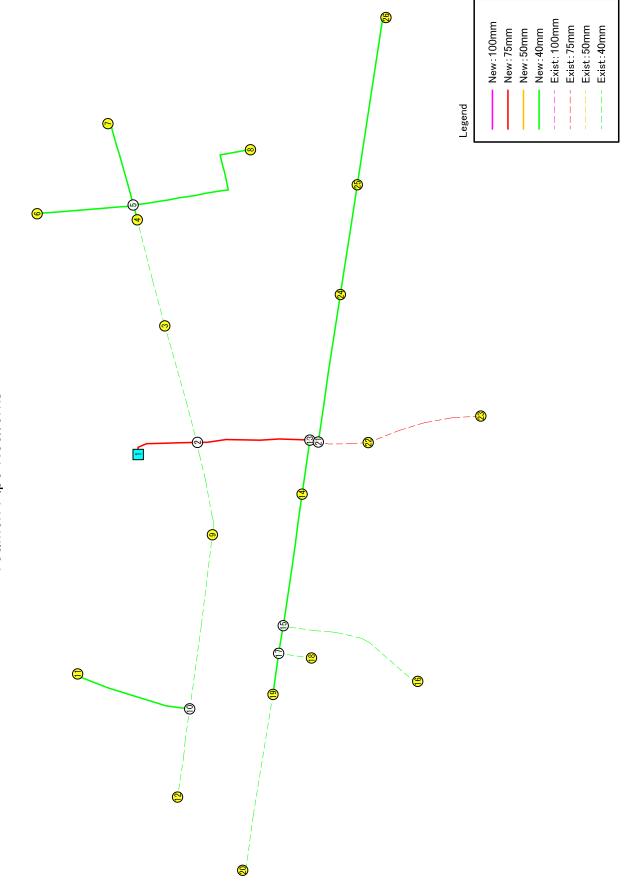
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	V (四/S)	$\begin{smallmatrix} & 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ 0.204 \\ $
	0 (1/s)	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $
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	Ъ	$\begin{array}{c} 76. \ 626\\ 78. \ 843\\ 78. \ 843\\ 78. \ 843\\ 78. \ 843\\ 65. \ 855\\ 947\\ 155. \ 535\\ 739\\ 0. \ 100\\ 135. \ 739\\ 306. \ 663\\ 306. \ 663\\ 947\\ 135. \ 739\\ 135. \ 480\\ 96. \ 947\\ 135. \ 739\\ 135. \ 739\\ 135. \ 739\\ 126. \ 739\\ 127. \ 543\\ 100\\ 100\\ 100\\ 100\\ 100\\ 100\\ 100\\ 10$
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ן ן ש	(E) (E)	$\begin{array}{c} 2, 648, 840\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 556, 258\\ 2, 556, 256\\ 2, 556, 256\\ 2, 556, 556\\ 2, 556, 556\\ 2, 556, 556\\ 2, 556, 556\\ 2, 556, 556\\ 2, 556, 556\\ 2, 556, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2, 556\\ 2$
— NodeData	HÌ	2672       2672       591         2672       591       26572       591         26572       591       2657       591         26572       591       2655       730         26572       591       2655       730         26565       730       2655       657         26565       730       2655       657         26565       730       2652       651         26523       546       2652       538         26523       546       538       2652         26523       546       538       2652         26523       546       538       2652         26523       546       538       2652         26523       546       719       25591         26523       546       713       2653         26523       104       25591       389         26523       104       2653       104         26533       104       2653       104         26533       104       2653       104         26543       104       2653       104         26557       467       713       2651
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	۲ (۳)	$\begin{smallmatrix} & - & - & - \\ & 3.7. & 917 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000 \\ 0.000$
	, H	$\begin{array}{c} 1.5 \\ 5.1 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.5 \\$
	(%) I	$\begin{array}{c} 23.\\ 23.\\ 23.\\ 23.\\ 23.\\ 23.\\ 23.\\ 23.\\$
	۲ (۱۳/۵)	$\begin{array}{c} 0.500\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.$
	0 (1/s)	$\begin{array}{c} 4 \\ 6 \\ 6 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7$
	Coef C	
1	」 〔目	$\begin{array}{c} 113.377\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 107.395\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.383\\ 107.3$
LineData -		21 88 88 80 0 88 21 88 21 88 21 88 88 88 88 88 88 88 88 88 88 88 88 88
- Line	Node T EN	$\begin{smallmatrix} 102\\ 102\\ 102\\ 102\\ 102\\ 102\\ 102\\ 102\\$
1	ST	$\begin{smallmatrix} & & & & & & & & & & & & & & & & & & &$
	Remarks	reak Pressure Val
	0c (1/S)	0. 225 0.
	EHP 2nd (m)	$^{25}$ 411 25. 411 25. 416 26. 166 37. 539 37. 939 37. 939 37. 939 37. 939 37. 539 37. 539 37. 539 37. 539 37. 539 48. 566 48. 566 48. 566 48. 566 48. 566 49. 128 37. 660 48. 566 48. 566 49. 128 36. 566 49. 128 37. 573 37. 573 37. 573 37. 573 37. 573 37. 573 37. 573 37. 576 49. 128 37. 576 49. 128 37. 576 49. 128 37. 577 49. 128 37. 578 37. 578 3
	EHP 1st(m)	70. 088 51. 883
   	日 19	$\begin{array}{c} 2, 576, 356\\ 2, 576, 356\\ 2, 573, 618\\ 2, 557, 618\\ 2, 557, 618\\ 2, 557, 618\\ 2, 557, 618\\ 2, 557, 618\\ 2, 567, 743\\ 2, 567, 743\\ 2, 567, 743\\ 2, 567, 743\\ 2, 567, 743\\ 2, 569, 337\\ 2, 569, 225\\ 619, 902\\ 2, 572, 614\\ 121\\ 2, 566, 446\\ 613, 128\\ 2, 569, 225\\ 613, 128\\ 2, 561, 695\\ 2, 561, 695\\ 2, 561, 695\\ 2, 561, 695\\ 2, 561, 695\\ 2, 561, 913\\ 2, 561, 913\\ 2, 561, 913\\ 2, 561, 913\\ 2, 561, 913\\ 2, 561, 913\\ 2, 561, 913\\ 2, 561, 913\\ 2, 561, 913\\ 2, 572, 561\\ 2, 572, 561\\ 2, 572, 561\\ 2, 572\\ 572\\ 572\\ 572\\ 572\\ 572\\ 572\\ 572\\$
— NodeData	Ê.	2601. 767           2600. 758           2600. 058           2600. 058           2600. 058           2600. 058           2601. 725           2601. 725           2601. 725           2601. 725           2601. 725           2601. 725           2601. 725           2601. 725           2601. 725           2601. 725           2601. 333           2601. 333           2601. 725           2601. 333           2601. 348           2605. 727           2605. 727           2605. 727           2605. 639           2661. 929           2662. 639           2661. 929           2661. 929           2665. 333           26661. 929           2665. 333           2665. 333           2665. 333           2665. 333           2665. 333           2665. 333           2665. 333           2665. 333           2665. 333           2665. 333           2665. 333           2665. 333           2665. 333 <t< td=""></t<>
] ]	Node	$\begin{array}{c} 666 \\ 666 \\ 667 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\ 666 \\$

		5. 184 0. 000 0. 183 5. 853 9. 631 2. 841 2. 089 -1. 491
	H(E)	
LineData	(%) I	$\begin{array}{c} 9. \ 913\\ 0. \ 000\\ 1. \ 849\\ 21. \ 003\\ 35. \ 780\\ 9. \ 913\\ 9. \ 913\\ 7. \ 963\\ -16. \ 074 \end{array}$
	V (五/ S)	$\begin{array}{c} 0.408\\ 0.408\\ 0.255\\ 0.817\\ 0.408\\ 0.408\\ 0.561\\ 0.530\end{array}$
	Q (1/s)	$\begin{array}{c} 0.451\\ 0.000\\ 1.127\\ 0.676\\ 0.451\\ 0.451\\ 0.451\\ 0.451\\ 0.585\end{array}$
	Coef C	
	ц	522.930 174.553 98.768 278.695 269.183 286.580 286.580 286.580 286.580 286.53 280.779 281.653 92.744
	П	32333 $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $323$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $3233$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $323$ $32$
	de EN	33 440 55 55 55 101
1   	Node ST EN	112 113 115 116 117 118
I	Remarks	reak Pressure Tan reak Pressure Tan reak Pressure Tan reak Pressure Tan reak Pressure Tan reak Pressure Tan reak Pressure Tan
	Qc (1/s)	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.000000
	EHP 2nd (m)	$\begin{array}{c} 0. & 000 \\ -0. & 000 \\ 0. & 000 \\ -0. & 000 \\ 48. & 506 \\ 506 \end{array}$
	EHP 1st(m)	23. 771 31. 888 37. 105 17. 347 37. 917 28. 156 47. 281
9   	IJ.	2, 678, 563 2, 633, 840 2, 633, 840 2, 623, 546 2, 613, 779 2, 611, 779 2, 611, 902 2, 611, 045 2, 611, 045
NodeData	H)	2678. 563 2633. 840 2623. 546 2523. 546 2513. 779 2619. 902 2619. 902 2659. 551 2659. 551
] [ [	Node	111 2 112 2 113 2 114 2 114 2 116 2 116 2 117 2 118 2



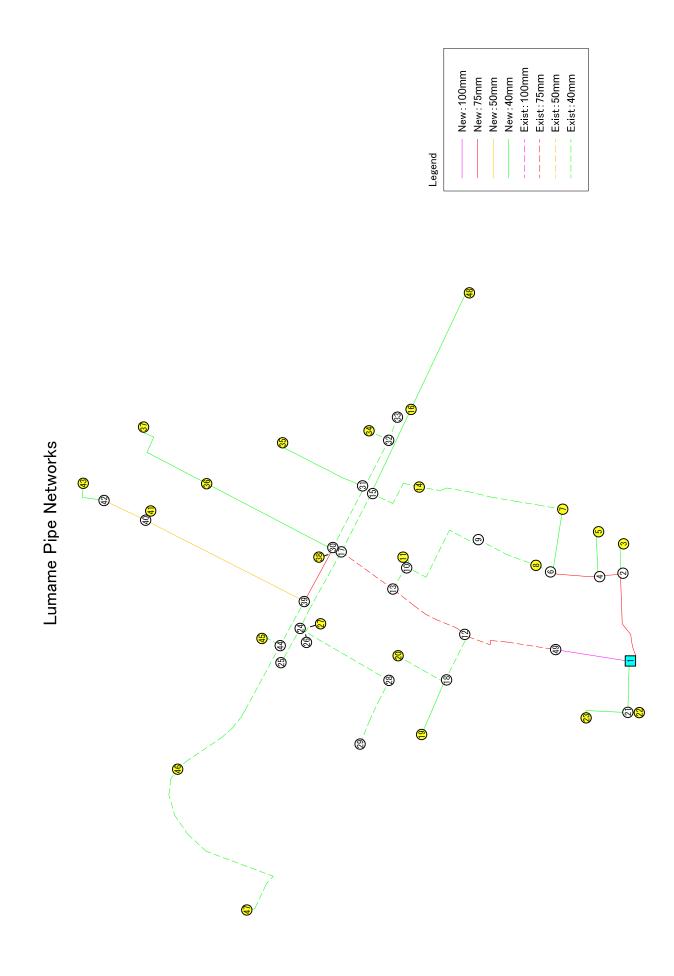
Yetimen Pipe Networks

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			Pipe	Coefficient of Flow	f Flow Gradient			I (%)	0.000 000 000 000 000 000 000 000 000 0
			4	ᆸ	ంట	Head Loss Add Pressure		۲ (m/s)	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $
						HL: H P: A		0 (1/s)	$\begin{array}{c} 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.$
				Fressure Water				Coef C	
	<< Explanatory Notes >>		-	bliectual Head Pr Consumption of Wa		·		ц	$\begin{array}{c} 122 \\ 233 \\ 233 \\ 233 \\ 233 \\ 211 \\ 233 \\ 211 \\ 233 \\ 211 \\ 233 \\ 211 \\ 233 \\ 234 \\ 333 \\ 333 \\ 333 \\ 334 \\ 344 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 333 \\ 334 \\ 333 \\ 333 \\ 334 \\ 334 \\ 334 \\ 349 \\ 357 \\ 349 \\ 349 \\ 357 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 349 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\ 340 \\$
	natory	- - 	Head Pressure Ground Level	EI I ectu Consump			LineData —	D (IIII)	22,22,22,22,22,22,22,22,22,22,22,22,22,
	K Expla	- Node		Uc:			- Line	Node T EN	2237520084202171084027 2337530084022171084022 2337530084022
ļ	$\checkmark$				-		<b> </b>   	ST	
<	(III)	(E)	(%)	(m/s)			·	Remarks	Reservoir Tank
is Formula	37.204	13.863	0.000	0.000				Qc (1/s)	0
Hazen-Williams Formula>>	Maximum EHP	Minimum EHP	Maximum I	Maximum V			•	EHP 2 nd (m)	$\begin{array}{c} 0. \\ 17. \\ 16. \\ 17. \\ 17. \\ 17. \\ 18. \\ 540 \\ 18. \\ 540 \\ 18. \\ 515 \\ 20. \\ 784 \\ 21. \\ 546 \\ 22. \\ 51. \\ 526 \\ 527 \\ 22. \\ 354 \\ 22. \\ 354 \\ 22. \\ 354 \\ 22. \\ 354 \\ 22. \\ 354 \\ 22. \\ 354 \\ 354 \\ 354 \\ 354 \\ 354 \\ 354 \\ 354 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ 356 \\ $
< <case.1 :="" h<="" td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>EHP 1st (m)</td><td></td></case.1>								EHP 1st (m)	
Yetimen < <ca< td=""><td>-</td><td>25</td><td>25</td><td>0</td><td>0.00 (cm)</td><td>2 (times)</td><td>       </td><td>」(旦 15</td><td><math display="block">\begin{array}{c} 2,  445. \\ 2,  445. \\ 2,  430. \\ 2,  430. \\ 2,  427. \\ 236. \\ 2,  427. \\ 235. \\ 2,  427. \\ 235. \\ 2,  428. \\ 21,  428. \\ 21,  428. \\ 22,  419. \\ 22,  419. \\ 2424. \\ 235. \\ 22,  419. \\ 22,  421. \\ 22,  421. \\ 22,  422. \\ 22,  419. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 23,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416</math></td></ca<>	-	25	25	0	0.00 (cm)	2 (times)	     	」(旦 15	$\begin{array}{c} 2,  445. \\ 2,  445. \\ 2,  430. \\ 2,  430. \\ 2,  427. \\ 236. \\ 2,  427. \\ 235. \\ 2,  427. \\ 235. \\ 2,  428. \\ 21,  428. \\ 21,  428. \\ 22,  419. \\ 22,  419. \\ 2424. \\ 235. \\ 22,  419. \\ 22,  421. \\ 22,  421. \\ 22,  422. \\ 22,  419. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 22,  416. \\ 23,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416. \\ 24,  416$
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LineData -	Node ST EN 25 26		
i	Remarks A ST 25		
	Qc 0. 000 0. 000		
	EHP 2nd (m) 29. 060 29. 060		·
	EHP 1st (m)	· · · · · · · · · · · · · · · · · · ·	
	GL (m) 2. 416. 328 2. 416. 715		
NodeData	H (m) 2445. 775 2 2445. 775 2		
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			ipe	n coefficient ty of Flow	Flow radient	, ,		(%) I	5. 709 6. 721 6. 721 6. 721 6. 721 6. 722 0. 879 0. 8790 0. 8790 0. 879000000000000000000000000000000000000
			Diameter Length of Pi	Quantity of	Velocity of Hydraulic Gi	Head Loss Add Pressure		V (町/ S)	0. 469 0. 552 0. 552 0. 331 0. 110 0. 221 0.
•						HL: H P: A		0 (1/s)	$\begin{array}{c} 2. & 0.7\\ 0. & 365\\ 0. & 365\\ 0. & 365\\ 0. & 365\\ 0. & 365\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\ 0. & 122\\$
			:	rressure Water				Coef C	
	Votes >>		neau rressure Ground Level					ц Ц	$\begin{array}{c} 122, 593\\ 233, 440\\ 181, 823\\ 218, 028\\ 218, 028\\ 211, 438\\ 229, 691\\ 168, 369\\ 334, 444\\ 168, 369\\ 3314, 448\\ 338, 976\\ 3314, 448\\ 338, 976\\ 3314, 448\\ 338, 976\\ 3314, 448\\ 336, 357\\ 799\\ 366, 666\\ 235, 331\\ 16, 799\\ 236, 666\\ 235, 331\\ 16, 799\\ 232, 787\\ 799\\ 232, 787\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 857\\ 234, 85$
	<< Explanatory Notes		Ground	Consumption			LineData —	и (ШШ)	75.0 337.5 75.0 337.5 75.0 75.7 75.7 75.7 75.7 75.7 75.7 7
	< Expla	- Node		Qc:			- Line	Node	22222038798792111087927 2334203879829 23342503879
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Hazen-Williams Formula>>	Maximum EHP	Minimum EHP	Maximum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0. & 000\\ 1.45 & 828\\ 1.45 & 000\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1 & 378\\ 1.1$
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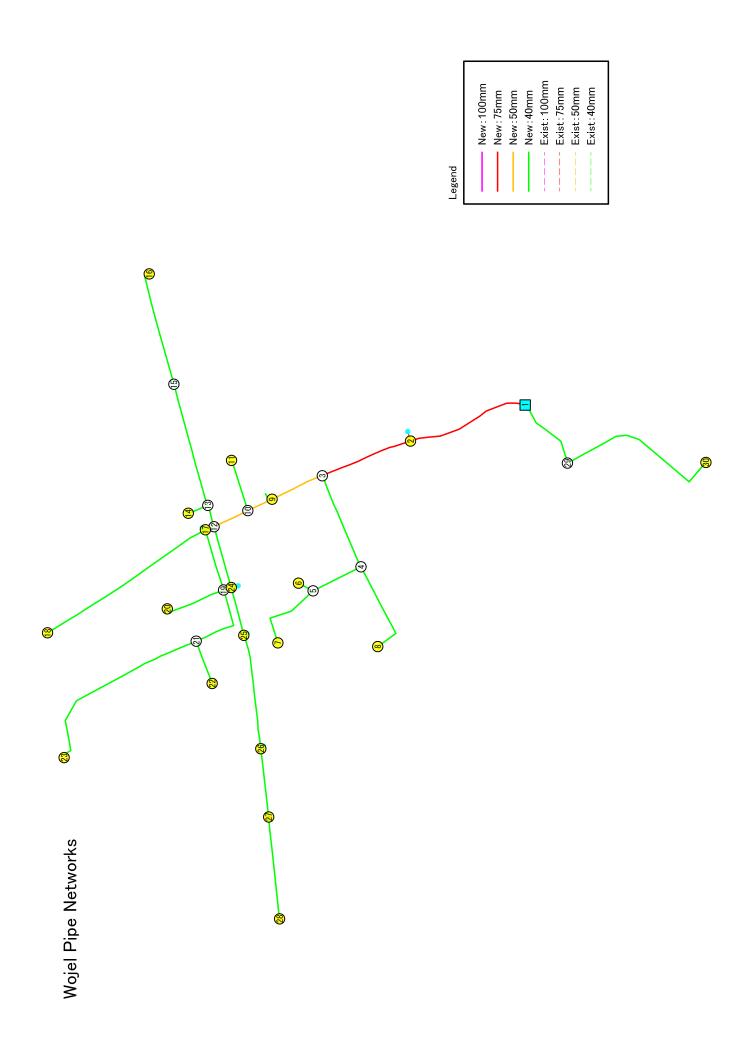
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· · ·	Explanatory Notes	- Head Pressur Ground Level			LineData —	(IIII)	75. 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 77.5 7
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Formula>>	52.343	12. 929 0. 000	0.000			Qc (1/s)	
Hazen-Williams	Maximum EHP	Minimum EHP Maximum I	Maximum V			EHP 2nd (m)	$\begin{array}{c} 8. & 050\\ 2.0. & 249\\ 2.0. & 249\\ 2.0. & 249\\ 3.0. & 541\\ 3.0. & 541\\ 3.0. & 542\\ 3.0. & 304\\ 3.0. & 304\\ 3.0. & 304\\ 3.0. & 304\\ 3.0. & 304\\ 3.0. & 304\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3.0. & 303\\ 3$
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			Ā	Convergence Calcula	   	Node	5322-068-1928-1968-1987-98-1987-98-1987-98-1987-98-1987-98-1987-98-1987-98-1987-98-1987-98-1987-98-1987-98-198 5335555555555555555555555555555555555

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   	ST	$\begin{smallmatrix} & & & & & & \\ & & & & & & & \\ & & & & $
	Remarks	
	Qc (1/s)	
	EHP 2nd (m)	$\begin{array}{c} 43.570\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.791\\ 37.791\\ 37.791\\ 37.791\\ 37.792\\ 37.792\\ 37.797\\ 37.792\\ 37.797\\ 37.792\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\ 37.797\\$
	EHP 1st (m)	
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	f Pipe Coefficient of Flow	Flow adient		I (‰)	$\begin{array}{c} 16. 590\\ 6. 483\\ 4. 596\\ 4. 596\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 1. 256\\ 1. 559\\ 1. 659\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559\\ 1. 559$
	iameter ength o riction uantity	Velocity of Hydraulic Gr Head Loss Add Pressure		۲ (m/ s)	$^{-1}$
	- Line - D: D L: L Coef: F Q: Q			0 (1/s)	$\begin{array}{c} 2.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ -0.5\\ $
	Pressur6 Water			Coef C	
Notes >>	, py			ц	$\begin{array}{c} 2240 & 166 \\ 124 & 844 \\ 155 & 572 \\ 588 & 442 \\ 588 & 415 \\ 391 & 563 \\ 391 & 553 \\ 391 & 553 \\ 391 & 565 \\ 391 & 565 \\ 391 & 565 \\ 311 & 518 \\ 270 & 158 \\ 271 & 311 \\ 544 & 475 \\ 271 & 311 \\ 544 & 475 \\ 157 & 305 \\ 157 & 305 \\ 330 & 309 \\ 231 & 586 \\ 231 & 232 & 237 \\ 232 & 232 & 237 \\ 232 & 232 & 237 \\ 233 & 232 & 237 \\ 233 & 232 & 237 \\ 233 & 232 & 237 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 \\ 234 & 586 $
Explanatory 1	- Head Pressure Ground Level Effectual Hea Consumption o		Data -		75. 75. 75. 75. 75. 75. 75. 75.
<< Explai	- Node HP: GL: EHP: Qc:		LineData	Node ST EN	224 24 24 24 24 24 24 24 24 24 24 24 24
	(II) (%) (S/II)		I	Remarks	Reservoir Tank
5 Formula>	4.408 35.149 0.913			Qc (1/s)	-6.
Hazen-Williams Maximum EHP	Minimum EHP Maximum I Maximum V			EHP 2nd (m)	$\begin{array}{c} 8. & 050\\ 25. & 013\\ 26. & 050\\ 27. & 050\\ 27. & 050\\ 27. & 052\\ 29. & 290\\ 26. & 029\\ 26. & 019\\ 26. & 029\\ 26. & 019\\ 26. & 019\\ 26. & 019\\ 26. & 019\\ 26. & 019\\ 26. & 019\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. & 009\\ 26. &$
	·			EHP 1st(m)	
Lumame < <case. nnk 1</case. 	48 50 0	0.97 (cm) 13 (times)	   !	B	$\begin{array}{c} 2, 497. \\ 2, 497. \\ 2, 485. \\ 2, 478. \\ 2, 478. \\ 002\\ 2, 478. \\ 002\\ 2, 476. \\ 002\\ 2, 476. \\ 002\\ 2, 476. \\ 002\\ 2, 476. \\ 002\\ 2, 479. \\ 003\\ 2, 480. \\ 005\\ 2, 480. \\ 005\\ 2, 480. \\ 005\\ 2, 482. \\ 005\\ 2, 482. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 487. \\ 005\\ 2, 4$
— Lur Tank	Node Line P, Decom	Convergence Gap Calculation	— NodeData	H)	2505.819           2505.819           2503.915           2503.915           2503.915           2503.915           2503.915           2503.915           2503.915           2503.915           2503.915           2503.915           2500.513           2497.139           2497.118           2493.918           2493.918           2493.918           2493.918           2493.918           2493.918           2493.918           2493.918           2493.918           2503.918           2503.918           2503.918           2503.918           2503.194           2503.194           2503.194           2503.194
	Pump,	178 1			

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	, V (п/s)	$\begin{array}{c} 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.270\\ 0.$
	Q (1/s)	0. 298 0. 2988 0. 2988 0. 2988 00000000000000000000000000000000000
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-	ц Ц	$ \begin{smallmatrix} 133 \\ 23, 435 \\ 120, 584 \\ 97, 004 \\ 156, 021 \\ 16, 021 \\ 16, 021 \\ 12, 562 \\ 349, 479 \\ 174, 023 \\ 164, 023 \\ 164, 023 \\ 164, 023 \\ 164, 023 \\ 164, 023 \\ 164, 023 \\ 164, 023 \\ 124, 003 \\ 255, 273 \\ 124, 093 \\ 255, 273 \\ 124, 093 \\ 255, 273 \\ 124, 033 \\ 255, 375 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, 335 \\ 246, $
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	0c (1/s)	$\begin{array}{c} 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\$
	EHP 2nd (m)	$\begin{array}{c} 31. \\ 32. \\ 25. \\ 752 \\ 25. \\ 753 \\ 753 \\ 753 \\ 753 \\ 753 \\ 753 \\ 753 \\ 763 \\ 733 \\ 763 \\ 763 \\ 733 \\ 764 \\ 733 \\ 764 \\ 733 \\ 766 \\ 733 \\ 766 \\ 733 \\ 766 \\ 733 \\ 766 \\ 733 \\ 766 \\ 733 \\ 766 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\ 786 \\$
	EHP 1st(回)	
   	19 15	$\begin{array}{c} 2,462,249\\ 2,467,756\\ 2,468,042\\ 2,468,042\\ 2,468,042\\ 2,466,028\\ 2,466,103\\ 2,466,103\\ 2,466,266\\ 2,466,243\\ 2,466,243\\ 2,466,243\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,287\\ 2,466,273\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,287\\ 2,2$
- NodeData	e e	<ul> <li>2493. 581</li> <li>2493. 581</li> <li>2493. 581</li> <li>2493. 508</li> <li>2493. 508</li> <li>2491. 500</li> <li>2490. 906</li> <li>2490. 906</li> <li>2491. 500</li> <li>2491. 510</li> <li>2491. 894</li> <li>2492. 023</li> <li>2492. 023</li> <li>2493. 206</li> <li>2493. 206</li> <li>2493. 206</li> <li>2493. 206</li> <li>2493. 206</li> <li>2493. 206</li> <li>2493. 208</li> <li>2493. 206</li> <li>2493</li></ul>
1	Node	4       4       4       4       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3



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					0	Head Loss Add Pressure		V (m/s)	
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				rressure Water				Coef C	
	<< Explanatory Notes >>			of			 ]	ц	$\begin{array}{c} 281. \ 892\\ 169. \ 070\\ 215. \ 938\\ 224. \ 731\\ 121. \ 741\\ 2224. \ 731\\ 121. \ 741\\ 2221. \ 458\\ 37. \ 460\\ 177. \ 094\\ 60. \ 825\\ 142. \ 825\\ 142. \ 724\\ 265. \ 710\\ 285. \ 724\\ 142. \ 729\\ 142. \ 729\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 175. \ 749\\ 102. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 175. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\ 185. \ 786\\$
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	$\sim$						<b> </b> [	ST	21119221999555443332 <b></b>
	(田)	(11)	(%)	(S/ш) -				Remarks	Reservoir Tank
Formula>>	61.324	3. 995	0.000	0.000				0c (1/s)	
Hazen-₩illiams Formula>>	Maximum EHP	Minimum EHP	Maximum <sup>.</sup> I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0. & 0.00\\ 2.0. & 0.026\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889\\ 3.0. & 889$
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jel < <case.< td=""><td>1</td><td>29</td><td>29</td><td>0</td><td>0.00 (cm)</td><td>2 (times)</td><td>     </td><td>E</td><td><math display="block">\begin{array}{c} 2, \ 488. \ 580\\ 2, \ 458. \ 580\\ 2, \ 456. \ 554\\ 2, \ 456. \ 554\\ 2, \ 456. \ 554\\ 2, \ 456. \ 556\\ 2, \ 449. \ 408\\ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 3, \ 557\\ 449. \ 557\\ 449. \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 5, \ 557\\ 5, \ 5, \ 5, \ 5, \ 5, \ 5, \ 5, \ 5, </math></td></case.<>	1	29	29	0	0.00 (cm)	2 (times)	   	E	$\begin{array}{c} 2, \ 488. \ 580\\ 2, \ 458. \ 580\\ 2, \ 456. \ 554\\ 2, \ 456. \ 554\\ 2, \ 456. \ 554\\ 2, \ 456. \ 556\\ 2, \ 449. \ 408\\ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 2, \ 449. \ 557\\ 3, \ 557\\ 449. \ 557\\ 449. \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 557\\ 5, \ 5, \ 557\\ 5, \ 5, \ 5, \ 5, \ 5, \ 5, \ 5, \ 5, $
⊶ —,— Wojel	Tank	Node	Line	Pump, Decom	gence Gap	Calculation	- NodeDaťa	H Û	$\begin{array}{c} 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488. 580\\ 2488$
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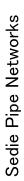
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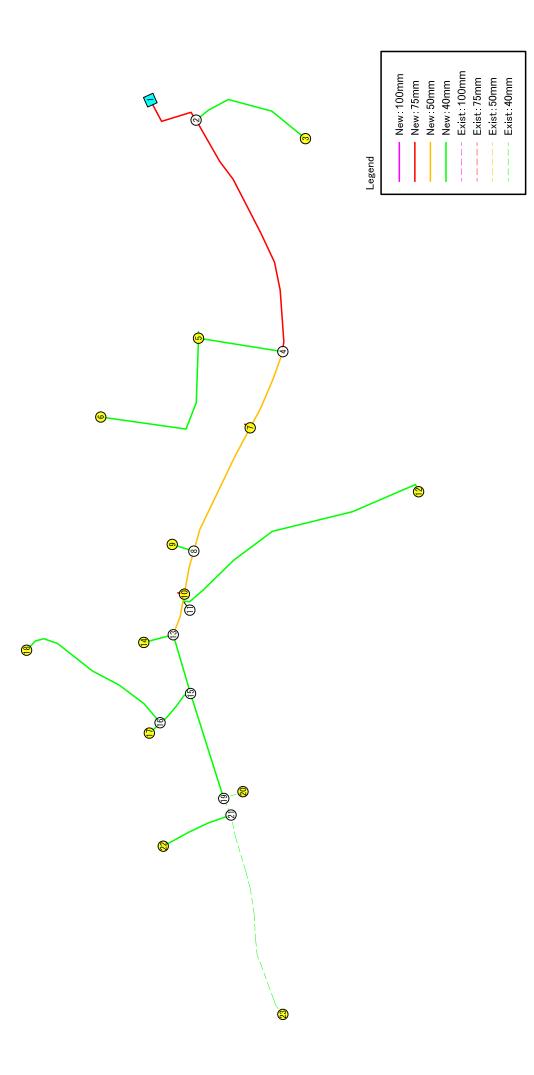
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	<< Explanatory Notes >>			of			1	л(Ш	$\begin{array}{c} 281:\ 892\\ 169:\ 070\\ 215:\ 938\\ 224,\ 731\\ 126:\ 041\\ 121:\ 741\\ 221:\ 741\\ 221:\ 458\\ 37.\ 460\\ 84.\ 910\\ 84.\ 910\\ 50.\ 613\\ 50.\ 613\\ 50.\ 613\\ 50.\ 613\\ 50.\ 613\\ 205.\ 724\\ 247.\ 965\\ 285.\ 724\\ 247.\ 965\\ 285.\ 724\\ 247.\ 965\\ 285.\ 724\\ 247.\ 965\\ 285.\ 724\\ 246.\ 829\\ 102.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 781\\ 142.\ 782\\ 162.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782\\ 142.\ 782$ 142.\ 782 1
	natory 1	ي - ا ا	Head Fressure Ground Level	EIIECTUAL HE Consumption			LineData —	C (IIII)	75. 75. 75. 75. 75. 75. 75. 75. 75. 75.
	< Expla	- Node		ЕНГ: 0с:			- Line	Node	222009865144
	ॐ						i I	ST	22199999999999999999999999999999999999
	(田)	(II)	(%)	(m/s)				Remarks	Reservoir Tank
Formula>>	50.405	3.610	22.615	0. 764				Qc (1/s)	-2. 035 0. 107 0. 107 00000000000000000000000000000000000
Hazen-Williams	Maximum EHP	Mininum EHP	Maximum I	Махітит V		-	,	EHP 2nd (m)	$\begin{array}{c} 0. & 0.00\\ 28. & 617\\ 28. & 509\\ 25. & 553\\ 30. & 352\\ 30. & 352\\ 30. & 302\\ 30. & 302\\ 30. & 302\\ 30. & 302\\ 30. & 302\\ 30. & 302\\ 31. & 544\\ 32. & 030\\ 31. & 544\\ 32. & 030\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. & 014\\ 33. $
 2								EHP 1st (m)	
Wojel < <case.< td=""><td></td><td>29</td><td>29</td><td>0</td><td>0.50 (с<b>п</b>)</td><td>14 (times)</td><td></td><td>GL EL</td><td><math display="block">\begin{array}{c} 2,\ 488,\ 580\\ 2,\ 468,\ 554\\ 2,\ 457,\ 591\\ 2,\ 457,\ 591\\ 2,\ 457,\ 591\\ 2,\ 455,\ 554\\ 2,\ 455,\ 554\\ 2,\ 445,\ 557\\ 2,\ 445,\ 576\\ 2,\ 445,\ 576\\ 2,\ 445,\ 576\\ 2,\ 445,\ 576\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,</math></td></case.<>		29	29	0	0.50 (с <b>п</b> )	14 (times)		GL EL	$\begin{array}{c} 2,\ 488,\ 580\\ 2,\ 468,\ 554\\ 2,\ 457,\ 591\\ 2,\ 457,\ 591\\ 2,\ 457,\ 591\\ 2,\ 455,\ 554\\ 2,\ 455,\ 554\\ 2,\ 445,\ 557\\ 2,\ 445,\ 576\\ 2,\ 445,\ 576\\ 2,\ 445,\ 576\\ 2,\ 445,\ 576\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 528\\ 2,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,\ 444,$
°	Tank	Node	Line	Pump, Decom	ence Gap	Calculation 14	NodeData	副圓	$\begin{array}{c} 2488. 588\\ 2486. 500\\ 2486. 200\\ 2486. 200\\ 2485. 009\\ 2484. 679\\ 2484. 679\\ 2482. 150\\ 2482. 150\\ 2480. 580\\ 2480. 580\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2479. 566\\ 2479. 566\\ 2478. 917\\ 2480. 382\\ 2478. 917\\ 2480. 382\\ 2478. 917\\ 2480. 382\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2480. 382\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2478. 917\\ 2480. 917\\ 2480. 917\\ 2480. 917\\ 2480. 917\\ 2480. 917\\ 2480. 917\\ 2480. 917\\ 2480. 917\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480. 912\\ 2480$
 				Pun	Convergence	Calc	<b> </b>   	Node	24 22 24 22 24 22 24 22 24 22 24 22 24 22 22

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i	- NodeData	] [					] ]	—— LineData	1	l						
Node	出间	IJ.	EHP 1st(m)	EHP - 2nd (m)	Qc (1/S)	Remarks	Node ST EN	EN	[] []	лÜ	coef C	0 (1/s)	ر» (III) (۱۳/۵)	1 (%)	H)	」。 L
25 26 28 28 28 28 29	2477. 738 2 2476. 355 2 2475. 965 2 2475. 803 2 2488. 463 2 2488. 465 2	2, 446, 366 2, 436, 621 2, 432, 338 2, 427, 256 2, 482, 319		31. 372 39. 734 43. 627 6. 144 6. 144	0. 107 0. 107 0. 107 0. 107 0. 107		24 25 26 29	25 26 27 30 30	37. 5 37. 5 37. 5 37. 5 37. 5	112.254 261.224 155.753 233.817 387.175	110 110 110 110	0.428 0.321 0.214 0.107 0.107	0. 388 0. 291 0. 194 0. 097 0. 097	9. 023 5. 297 2. 500 0. 693 0. 693	1. 013 1. 384 0. 389 0. 162 0. 268	0.000

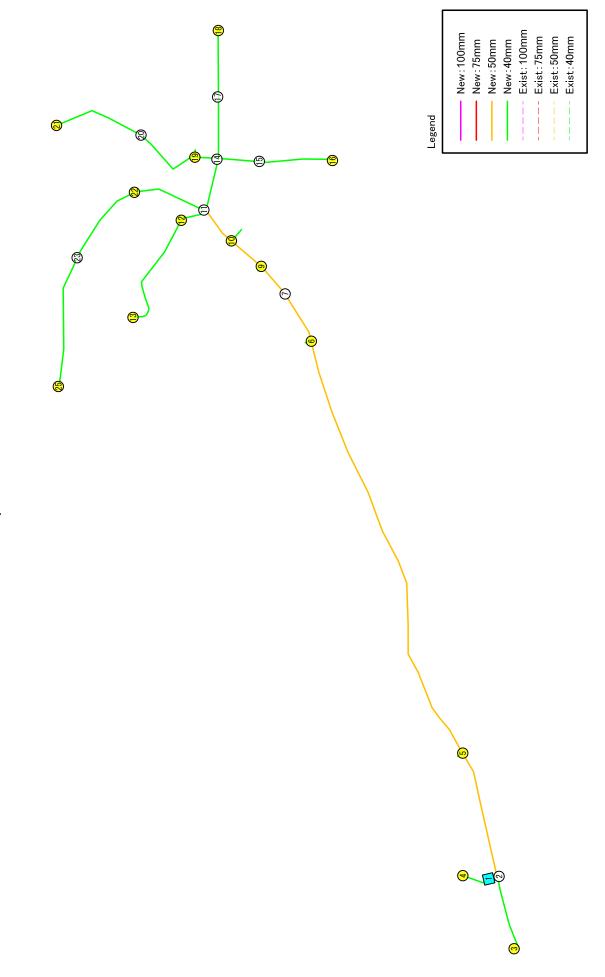
484. 585 3. 610 0. 107 3. 610 0. 107





<ul> <li>Line -         <ul> <li>Line -</li> <li>Diameter</li> <li>Diameter</li> <li>Diameter</li> <li>L: Length of Pipe</li> <li>L: Length of Fipe</li> <li>Q: Quantity of Flow</li> <li>Yelocity of Flow</li> <li>Hydraulic Gradient</li> <li>HL: Head Loss</li> <li>P: Add Pressure</li> </ul> </li> </ul>	Coef Q V I HL C (1/s) (m/s) (‰) (m)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
- Line - D: D: L: L: Kater Coef: V: HL: P:	Q V (1/s) (m/s)	
- Line - D: Pressurt Coef: Water V: P: P:	Q (1/s)	
- Line - D: D: L: L: Tater 0: V: T: P:	1	
	coef C	'
otes essur level 1 He tion	ц П	$\begin{array}{c} 82.\ 469\\ 164.\ 065\\ 326.\ 205\\ 109.\ 160\\ 107.\ 358\\ 29.\ 107\\ 351.\ 117\\ 175.\ 117\\ 175.\ 117\\ 29.\ 160\\ 351.\ 88\\ 12\\ 351.\ 806\\ 141.\ 599\\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 152\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 39.\ 102\\ 1$
Explanatory Notes >> Node - HP: Head Pressure GL: Ground Level EHP: Effectual Head Oc: Consumption of LineData	Q (間)	75. 37. 37. 37. 37. 37. 37. 37. 50. 37. 55. 57. 57. 57. 57. 57. 57. 57. 57. 5
Explanato Node - HP: Head GL: Grou EHP: Effe Qc: Cons LineData	de EN	22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22210 22200 22200 22200 22200 22200 22200 22200 22200 22200 22200 22200 22200 2200 22000 22000 22000 22000 22000 22000 22000 22000 22000 22000 22000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 2000000
	Node ST E	2219966555555511108823544222
(国) (国) (%) (%) (%)	Remarks	Reservoir Tank
53. 574 2. 501 0. 000 0. 000	Qc (1/s)	
Maximum EHP Minimum EHP Maximum V Maximum V	EHP 2nd (m)	$\begin{array}{c} 2. & 000\\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\ 2. & 2. \\$
•	EHP 1st (m)	· · · · · · · · · · · · · · · · · · ·
1 1 22 22 22 0 0 0 0 (cm) 2 (t ines) a	日 15	2, 547, 547         2, 547, 547         2, 547, 547         556, 064         558, 065         558, 065         558, 065         558, 065         558, 065         558, 065         558, 065         558, 065         551, 256         507, 050         2, 507, 060         2, 506, 727         2, 506, 331         2, 506, 331         2, 506, 639         2, 506, 031         2, 502, 041         2, 502, 041         2, 502, 041         2, 501, 727         2, 502, 041         2, 502, 041         2, 502, 041         2, 502, 041
	₽H.(E)	2549. 547 2549. 547 2549. 547 2549. 547 2549. 547 2549. 547 2549. 547 2549. 547 25549. 547 2555557. 547 255557. 547 2555757. 547 255575777777777777777777777777777777
Conve	Node	222200824008240082400 255500824000824000 255500824000 255500824000 255500824000 255500824000 255500824000 255500824000 255500824000 255500824000 255500824000 255500824000 2555008240000 2555008240000000000000000000000000000000

									P (E)	
·.,		•							H) E	0. 505 1. 721 1. 722 1. 723 1. 723
				pe íficient	of Flow	riow adient			I (‰)	$\begin{array}{c} 6. \\ 6. \\ 1. \\ 5. \\ 2. \\ 2. \\ 5. \\ 5. \\ 5. \\ 5. \\ 5$
			Diameter	Length of Pipe Friction Coeff	Quantity of	lic Gr	Add Pressure		ү (m/s)	0. 150 0.
			- Line - D: D		0:0		P: A		0 (1/S)	$\begin{array}{c} 2. & 150\\ 0. & 165\\ 1. & 985\\ 0. & 165\\ 1. & 654\\ 1. & 158\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\ 0. & 165\\$
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	ie < <case< td=""><td>I</td><td>22</td><td>22</td><td>0</td><td>0. 85 (сп)</td><td>13 (times)</td><td>~      </td><td>1) E</td><td>547.547 528.065 528.065 528.065 528.827 528.827 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 500 500 500 500 500 500 500 500 500</td></case<>	I	22	22	0	0. 85 (сп)	13 (times)	~     	1) E	547.547 528.065 528.065 528.065 528.827 528.827 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 507.050 500 500 500 500 500 500 500 500 500
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Dibo Pipe Networks

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	(田)	( <u>I</u> )	(%o)	(町/ S)				Remarks	Reservoir Tank							•						
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Dibo	Tank	Node	Line	Pump, Decom	ence Gap	Calculation	NodeData	en (je)	2460. 637 2460. 637 2460. 637 2460. 637	637	637 637	637	637 c 9.7	637 637	637 637	637	637 637	2460. 637 2460. 637	637	637 637	$637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 \\ 637 $	2460. 637 2460. 637
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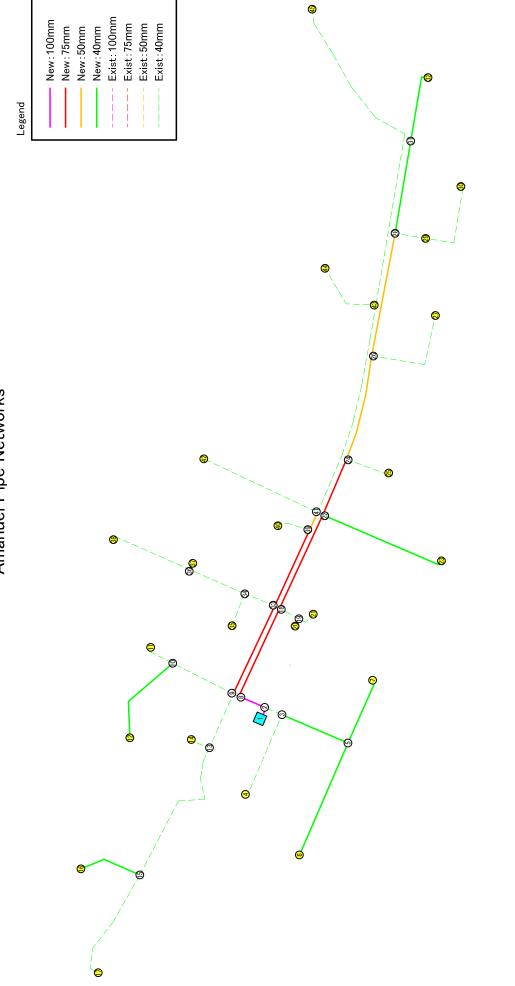
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		;						H E	$\begin{array}{c} 0. & 341 \\ 0. & 341 \\ 0. & 056 \\ 0. & 141 \\ 1. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 103 \\ 0. & 103 \\ 0. & 113 \\ 0. & 103 \\ 0. & 103 \\ 0. & 113 \\ 0. & 102 \\ 0. & 103 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. &$
			pe	Coefficient of Flow	f Flow Gradient			1 (%)	$\begin{array}{c} 19. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ $
					city o aulic	Head Loss Add Pressure		V (加/S)	0. 115 0. 115 0. 115 0. 580 0. 580 0. 115 0. 387 0. 115 0.
			ä. 	Coel: F Q: Q		HL: H P: A		0 (1/s)	$\begin{array}{c} 1. & 392\\ 0. & 127\\ 0. & 127\\ 1. & 265\\ 1. & 128\\ 1. & 128\\ 1. & 128\\ 0. & 128\\ 0. & 128\\ 0. & 128\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\ 0. & 127\\$
				Fressure Water				Coef C	
	<< Explanatory Notes >>		Pressure d Level	Ellectual Head Fr Consumption of Wa			1	ц ш	17.         292           59.         380           59.         380           59.         380           59.         380           59.         380           247.         922           861.         812           861.         812           861.         812           861.         812           861.         812           861.         812           104.         195           101.         411           101.         411           101.         411           101.         411           1120.         299           81.         999           121.         783           141.         846           170.         266           171.         836           171.         836           171.         836           171.         836           171.         836           171.         836           171.         836           171.         836           171.         836           171.         836
	natory ]	;	Head Fressur Ground Level	El lec lu Consump			Data -		227.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 237.55 23
	(Expla	- Node		CC: 1			- LineData	Node	2222228669733242 225310887923257573753 22531088792325777 225310887922 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 22531088792 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 225310 2253100000000000000000000000000000000000
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	(田)	(II)	(%)	(II/S)				Remarks	Reservoir Tank
<sup>7</sup> ormula>>-	32. 658	5. 463	19, 695	0.709				Qc (1/s)	$\begin{smallmatrix} -1 \\ -1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
: Hazen-Williams Formula>>	Maximum EHP	Minimum EHP	Maximum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 8. & 000\\ 7. & 944\\ 7. & 944\\ 7. & 944\\ 17. & 83\\ 15. & 659\\ 77. & 833\\ 16. & 764\\ 18. & 767\\ 19. & 777\\ 22. & 068\\ 23. & 390\\ 22. & 068\\ 23. & 390\\ 22. & 068\\ 23. & 390\\ 22. & 058\\ 23. & 390\\ 22. & 058\\ 23. & 390\\ 24. & 059\\ 25. & 658\\ 26. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598\\ 20. & 598$
							·	EHP 1st (m)	
oo < <case.2< td=""><td>_</td><td>25</td><td>25</td><td>0</td><td>0.53 (cm)</td><td>14 (times)</td><td></td><td>13</td><td><math display="block">\begin{array}{c} 2, \ 452, \ 637\\ 2, \ 452, \ 637\\ 2, \ 454, \ 692\\ 2, \ 454, \ 692\\ 2, \ 452, \ 637\\ 2, \ 425, \ 637\\ 2, \ 425, \ 537\\ 2, \ 425, \ 537\\ 2, \ 419, \ 560\\ 2, \ 419, \ 550\\ 2, \ 418, \ 852\\ 2, \ 418, \ 852\\ 2, \ 418, \ 852\\ 2, \ 418, \ 852\\ 2, \ 418, \ 852\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\ 2, \ 035\\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ </math></td></case.2<>	_	25	25	0	0.53 (cm)	14 (times)		13	$\begin{array}{c} 2, \ 452, \ 637\\ 2, \ 452, \ 637\\ 2, \ 454, \ 692\\ 2, \ 454, \ 692\\ 2, \ 452, \ 637\\ 2, \ 425, \ 637\\ 2, \ 425, \ 537\\ 2, \ 425, \ 537\\ 2, \ 419, \ 560\\ 2, \ 419, \ 550\\ 2, \ 418, \ 852\\ 2, \ 418, \ 852\\ 2, \ 418, \ 852\\ 2, \ 418, \ 852\\ 2, \ 418, \ 852\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 418, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\\ 2, \ 035\ 2, \ 035\\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ 035\ 2, \ $
Dibo	Tank	Node	Line	Pump, Decom	ence Gap	Calculation 14	NodeData	出间	4460, 637 4460, 637 4460, 581 4460, 581 4460, 581 4460, 581 4444, 499 4441, 758 4441, 758 4441, 758 4440, 914 440, 914 440, 913 4440, 686 440, 1724 440, 172
	•			Pu	Convergence	Cal		Node	55555662555555555555555555555555555555

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l	」 (目)	157. 144										
Data	Q (回)	37. 5										
LineData	Node ST EN	25 26	-									
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	0c (1/s)	0. 127 0. 000										
	EHP 2nd (m)	20. 234 18. 881										
	EHP 1st (m)											
   	19	2, 419. 665 2, 421. 018			-							
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Amanuel Pipe Networks

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			Je	ficient Now	f Flow Gradient			I (%)		
			neter sth of stion C ntity o ocity.o city.o raulic Pressu					V (п/s)		
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				Pressure Water				Coef C		
	otes >>		evel evel	tion of Wat			-  · 	[田]	$\begin{array}{c} 28.598\\ 43.799\\ 64.943\\ 64.943\\ 64.943\\ 167.220\\ 167.220\\ 156.993\\ 136.127\\ 156.993\\ 136.127\\ 127\\ 225.047\\ 225.047\\ 225.047\\ 225.047\\ 225.047\\ 136.906\\ 148.405\\ 127\\ 225.047\\ 127\\ 127\\ 129\\ 127\\ 129\\ 127\\ 129\\ 127\\ 129\\ 129\\ 120\\ 129\\ 120\\ 129\\ 120\\ 129\\ 120\\ 120\\ 120\\ 120\\ 120\\ 120\\ 120\\ 120$	
	<< Explanatory Notes >>		Head Pressure Ground Level	Ellectual H Consumption			LineData —-	(IIII)	100. 0 37. 5 37. 5 5 37. 5 5 37. 5 5 37. 5 5 37. 5 5 37. 5 5 37. 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	
	(Expla	- Node		LHF: Qc:			- Line	Node T EN	<b>5</b> 31025551545111313084833555555555555555555555555555555555	
1	⇒	,						ST	22299885555599999888558885555 522998855555999998885555555555	
· · · · · · · · · · · · · · · · · · ·	(II)	(II)	(%)	(m/s)				Remarks	Reservoir Tank	
Formula)	36. 735 (	7.360 (	0.000 (	0. 000 (				Qc (1/S)		
Hazen-₩illiam	faximum EHP	Minimum EHP	aximum I	Maximum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 8.\\ 2.360\\ 2.360\\ 2.325\\ 2.472\\ 2.472\\ 2.472\\ 2.472\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425\\ 2.425$
· ··	W	24	24	A				EHP 1st (m)		
Amanuel < <case.< td=""><td>1</td><td>44</td><td>44</td><td>0</td><td>0.00 (cm)</td><td>2 (times)</td><td>[    </td><td>」 し じ じ</td><td>387. 780         388. 780         388. 858         388. 858         388. 858         388. 858         388. 858         388. 858         388. 858         388. 858         388. 858         388. 856         388. 856         388. 856         388. 856         388. 856         388. 856         388. 856         388. 870         388. 871         371. 777         388. 847         388. 847         388. 818         388. 819         370. 847         388. 810         373. 818         388. 817         388. 817         379. 847         388. 532         388. 532         373. 532</td></case.<>	1	44	44	0	0.00 (cm)	2 (times)	[   	」 し じ じ	387. 780         388. 780         388. 858         388. 858         388. 858         388. 858         388. 858         388. 858         388. 858         388. 858         388. 858         388. 856         388. 856         388. 856         388. 856         388. 856         388. 856         388. 856         388. 870         388. 871         371. 777         388. 847         388. 847         388. 818         388. 819         370. 847         388. 810         373. 818         388. 817         388. 817         379. 847         388. 532         388. 532         373. 532	
— — — Amaı	Tank	Node	Line	Pump, Decom	gence Gap	Calculation	- NodeData	ÊH (Ē	23395, 780 23395, 780	
i				P	Convergence	Ca		Node		

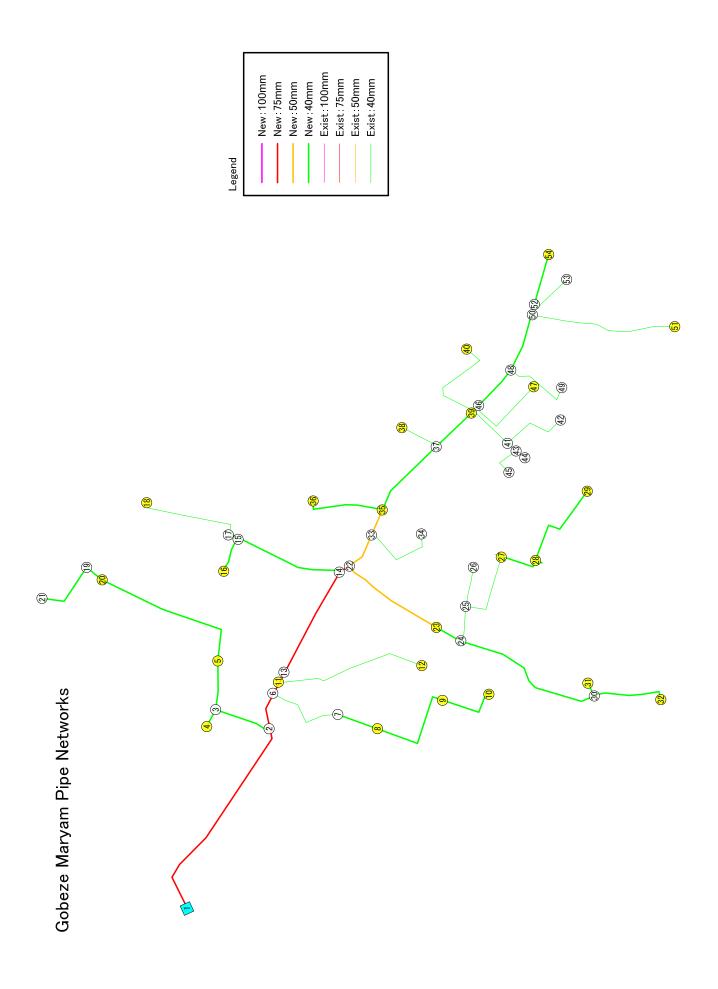
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	HL E			0. 000									_	_	_	_	_	_	_	_	
	I (%)	0.000		0.000																	
	V (m∕s)	0.000	0.000	U. UUU	0.000	0.000	0.000	0.000	0.000	0. 000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
	Q (1/S)	0.000	0.000	0. UUU	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
	Coef C	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	
[.	- <b>)</b> (jj	105.811																			
LineData —	(I) (I)	$\frac{37.5}{2}$																			
- Line	Node ST EN	25	97 97	12	29	31	30	32	34	39	35	36	37	30	40	41	42	43	44	45	
	ST	24	24	07 96	28	28	29	31	ŝ	33	34	34	36	36	39	39	41	41	43	43	
	Remarks																				
	Qc (1/s)	0.000																			
	EHP 2nd (m)	13. 261																			
	EHP 1st (m)																				
	15 日 日	2, 382, 519	019. 281	378	381.	382.	380.	380.	382.	333.	383.	381.	381.	365.	382.	383.	382.	366.	382.	365.	375.
- NodeData	H)	2395. 780	780	780	780	780	780	780	780	780	180	180	08/	780	780	780	780	180	780	780	
 	Node	22	076	28	29	30	5	32	3	34		36	<u>0</u>	38	68	40	41	42	43	44	45

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							·	H (B)	0.338 1 307													0. 170 1. 181 0. 368
	oe [ficient ?low idient							I (%)	11.820 29.844												3.003	3.902 3.902 2.628
	<ul> <li>Line –</li> <li>D: Diameter</li> <li>D: Length of Pipe</li> <li>L: Length of Fipe</li> <li>Coef: Friction Coefficient</li> <li>Q: Quantity of Flow</li> <li>V: Velocity of Flow</li> <li>V: Hudraulic Gradient</li> <li>HL: Head Loss</li> <li>P: Add Pressure</li> </ul>							ү (m/s)	0.833 0.740			0.247		0.494 0.404					0.247			$\begin{array}{c} 0. \ 247 \\ 0. \ 247 \\ 0. \ 308 \end{array}$
								0 (1/s)	6. 538 0. 817													0. 272 0. 272 1. 362
	y Notes >> Pressure d Level tual Head Pressure mption of Water							coef c	110	110	110	110	110	110	110	110	110	110	110	110	110	110
							I	口 (日)	28.598 $43.799$					223.946 156 993							19. 150	43. 526 302. 739 139. 919
	natory A	<pre>&lt;&lt; Explanatory Notes &gt;&gt; - Node - HP: Head Pressure GL: Ground Level EHP: Effectual Head Qc: Consumption of</pre>				LineData —	C (IIII)	100. 0 37. 5	100.0 37 F		~ ~	<u>- ы</u>	75. 0 37. 5	- L		2					37. 5 37. 5 75. 0	
	K Expla	- Node	문 문 문 문	CC:			- Line	Node T EN														23 24
ļ	$\sim$						1 [	ST		25	ົ	un un	~~~	ω σ	000	л <u>С</u>	10	<u> </u>	15	18	<u>6</u>	$^{19}_{22}$
<	(8)	(11)	(%)	(II/S)				Remarks	Reservoir Tank													
ns Formula	32.118	3. 166	29.844	0.833				<b>ც</b> c (1/s)	-6.538 0.000			0.272 0.272		0.000	0. 272	0. 000	0.272 0.000	0. 272	0. 272 0. 000	0.000	0. 272	0. 000 0. 272 0. 000
Hazen-Williams Formula>>	Maxinum EHP	Minimum EHP	Maximum I	Maximum V					EHP · 2nd (m)	8.000 7.022	10.277 10.016			8.842	9.501 16.612	18.010	4. 606	8. 536 6. 591	12.880	14. 645 11. 522	13.279	15. 704
< <case. 2="" :="" ii<="" td=""><td>L</td><td>l</td><td></td><td></td><td></td><td></td><td></td><td>EHP 1st(m)</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></case.>	L	l						EHP 1st(m)														
Amanuel < <ca< td=""><td>1</td><td>44</td><td>44</td><td>0</td><td>0.89 (cm)</td><td>14 (times)</td><td>-    </td><td>٦ ت</td><td>387. 388.</td><td></td><td>363.</td><td>361. 359.</td><td>386.</td><td>375</td><td>374. 366</td><td>385. 385.</td><td>2, 381. 832 2. 378. 646</td><td>371.</td><td>381. 381.</td><td></td><td>376.</td><td>2, 302, 000 2, 377, 818 2, 382, 532</td></ca<>	1	44	44	0	0.89 (cm)	14 (times)	-   	٦ ت	387. 388.		363.	361. 359.	386.	375	374. 366	385. 385.	2, 381. 832 2. 378. 646	371.	381. 381.		376.	2, 302, 000 2, 377, 818 2, 382, 532
— — — Ami	Tank	Node	Line	Pump, Decom	ence Gap	Calculation 14	· NodeData	E (II)	780 442	$135 \\ 324$	617	679 162	842	624 412	135 555	561	$368 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 \\ 236 $	657	u18 437	720 646		2392. 191 2392. 191
   				Ρu	Convergence	Cal		Node														57 57 57 57 57 57 57 57 57 57 57 57 57 5

	d (II)	
	le H	$\begin{array}{c} 0.413\\ 0.413\\ 0.940\\ 0.940\\ 0.942\\ 0.506\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.942\\ 0.$
	I (%)	$\begin{array}{c} 12.523\\ 12.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ 2.523\\ $
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	EHP 2nd (m)	$\begin{array}{c} 9.\ 260\\ 6.\ 744\\ 6.\ 744\\ 7.\ 267\\ 7.\ 267\\ 7.\ 265\\ 7.\ 274\\ 9.\ 601\\ 9.\ 601\\ 10.\ 601\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 335\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\\ 10.\ 30\ 10\ 10\ 10\ 10\ 10\ 10\ 10\ 10\ 10\ 1$
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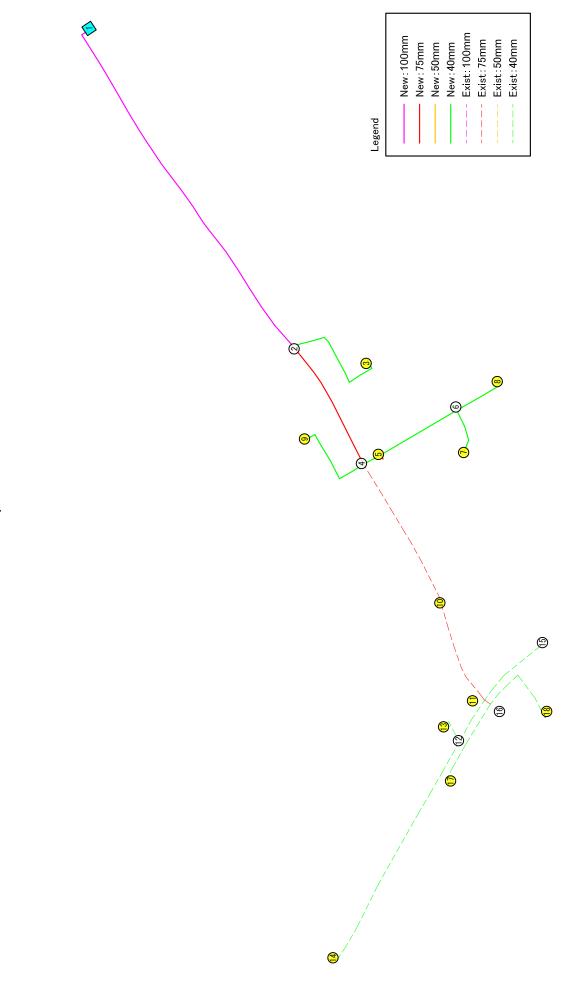
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	I	(Expla	- Node	GEN:			- Line	Node	23 $23$ $23$ $23$ $23$ $23$ $23$ $23$				
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	Formula>>	(田)	(II)	(%)	(s/m)				Remarks	Reservoir Tank			
	Hazen-Williams	58. 697	0.000	0.000	0.000				0c (1/s)				
	 ,	Maximum EHP	Minimum EHP	Maxinum I					EHP 2nd (m)	$\begin{array}{c} 0 \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 37. \\ 3$			
	I < <case.< td=""><td>Æ</td><td>æ</td><td>Æ</td><td>ž</td><td></td><td></td><td></td><td>EHP 1st (m)</td><td>46. 493</td></case.<>	Æ	æ	Æ	ž				EHP 1st (m)	46. 493			
	Gobeze Maryam	1	53	53	1	0.00 (cm)	2 (times)	   	٦) E	2       243       367         2       205       414         2       195       382         2       195       382         2       195       382         2       195       382         2       195       382         2       195       382         2       197       127         2       197       127         2       197       127         2       196       874         2       198       264         2       198       264         2       170       411         2       178       906         2       178       906         2       178       906         2       178       870         2       178       870         2       178       517         2       178       517         2       179       550         2       179       550         2       179       550         2       179       550			
	Go	Tank	Node	Line	Рипр, Лесол	gence Gap	Calculation	· NodeData	E (E)	<ul> <li>22243. 367</li> <li>2196. 874</li> <li>2196. 874</li> <li>2196. 874</li> <li>2196. 874</li> <li>2196. 874</li> </ul>			
	 				Pı	Convergence	Ca	   	Node	-222200846526284			

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- LineData	Node ST EN	$\begin{smallmatrix} & & & & & & & & & & & & & & & & & & &$
   	ST Nc	$\begin{array}{c} 224\\ 225\\ 225\\ 225\\ 225\\ 225\\ 225\\ 225\\$
	Remarks	
	Qc (1/s)	
	EHP 2nd (m)	$\begin{array}{c} 23.82\\ 23.82.553\\ 33.553\\ 33.556\\ 33.556\\ 33.556\\ 33.556\\ 33.556\\ 33.556\\ 33.556\\ 33.556\\ 590\\ 33.556\\ 590\\ 550\\ 550\\ 550\\ 556\\ 394\\ 44\\ 750\\ 550\\ 550\\ 556\\ 394\\ 44\\ 750\\ 550\\ 556\\ 394\\ 46\\ 750\\ 556\\ 392\\ 750\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 332\\ 556\\ 556\\ 332\\ 556\\ 556\\ 556\\ 556\\ 556\\ 556\\ 556\\ 55$
	EHP 1st(m)	· .
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- NodeData	E E	$\begin{array}{c} 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 2196.\ 874\\ 374\\ 374\\ 374\\ 374\\ 374\\ 374\\ 374\\ 3$
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									H(E)	$\begin{array}{c} \textbf{8.455}\\ \textbf{1.1220}\\ \textbf{1.1220}\\ \textbf{1.1330}\\ 1.1$
				ipe	efficient Flow	Flow radient	0		I (‰)	$\begin{smallmatrix} 17, 426\\ 18, 463\\ 12, 433\\ 12, 433\\ 10, 161\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 115\\ 11, 417\\ 115\\ 11, 417\\ 115\\ 12, 820\\ 11, 417\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12, 820\\ 12$
				: Diameter : Length of Pipe	Priction Coe Quantity of	Velocity of Hydraulic Gr	Head Loss Add Pressure		V (加/S)	$\begin{array}{c} 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.000$
			- Line -	- - -	Coel: F				(s∕1) ∘	$^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1}$ $^{-1$
					Fressure Water				Coef C	
		Votes >>		-	2 5			1	ц Ц	$\begin{array}{c} 485,\ 203\\ 128,\ 621\\ 84,\ 885\\ 43,\ 447\\ 109,\ 350\\ 178,\ 748\\ 333,\ 324\\ 337,\ 327\\ 16,\ 411\\ 178,\ 748\\ 337,\ 327\\ 179,\ 796\\ 11,\ 960\\ 129\\ 233,\ 157\\ 263\\ 377\\ 796\\ 11,\ 960\\ 129\\ 233,\ 157\\ 263\\ 377\\ 796\\ 11,\ 960\\ 129\\ 233,\ 157\\ 796\\ 11,\ 960\\ 129\\ 246,\ 241\\ 263\\ 232,\ 157\\ 263\\ 246,\ 241\\ 263\\ 246,\ 241\\ 263\\ 232,\ 157\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 246,\ 242\\ 263\\ 262\\ 262\\ 262\\ 262\\ 262\\ 262\\ 26$
	·	Explanatory Notes	- Decu	Ground Level	Ellectual Hee Consumption c			Data —		75. 75. 75. 75. 75. 75. 75. 75.
	t	Explai	Node					LineData	de EN	233325008110081149881 2333550887166332 2333550887166332
		$\approx$	I					    	Node	2222999577557444311198876663332221 222299995775574443
	Formula>>	(II)	(田)	(%)	(四/3)				Remarks	Reservoit Tank
۰	lliams	44.776	0.000	27.911	0.857				Qc (1/S)	-3.784 0.000 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.158 0.15800000000000000000000000000000000000
	.2 : Hazen-Wi	Maximum EHP	Minimum EHP	Maximum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0. \ 000\\ 29. \ 155\\ 29. \ 155\\ 36. \ 593\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 416\\ 38. \ 596\\ 38. \ 596\\ 38. \ 596\\ 13. \ 990\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \ 816\\ 10. \$
	< <case.< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>EHP 1st(m)</td><td>36. 556</td></case.<>								EHP 1st(m)	36. 556
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		Tank	Node	Line	Pump, Decom	gence Gap	Calculation	- NodeData	E C	$\begin{array}{c} 22243. \ 367\\ 22342. \ 367\\ 2232. \ 573\\ 2232. \ 573\\ 2232. \ 573\\ 2223. \ 575\\ 2223. \ 648\\ 22233. \ 556\\ 22233. \ 556\\ 22233. \ 556\\ 22233. \ 556\\ 22233. \ 556\\ 22233. \ 556\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ 22233. \ 566\\ $
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   	No ST	222002844444444 222002844444444 25200888833333333333333337252544
	Remarks	
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	EHP 2nd (m)	$\begin{array}{c} 16. \\ 864 \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\ 22. \\$
	EHP 1st(m)	
   	J.E	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
NodeData	E (E)	$\begin{array}{c} 2189. \ 917\\ 2189. \ 917\\ 2188. \ 092\\ 2187. \ 639\\ 2187. \ 635\\ 2187. \ 635\\ 2188. \ 692\\ 2188. \ 635\\ 2193. \ 694\\ 2193. \ 694\\ 2193. \ 694\\ 2193. \ 694\\ 2195. \ 657\\ 2195. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657\\ 2185. \ 657$
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**Bikolo Pipe Networks** 

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:				Coefficient of Flow	f Flow Gradient			(%) I	
			••	Friction Coe Quantity of	0	Head Loss Add Pressure		V (m/s)	
		- Line -				HL: H P: A		0 (1/s)	
				Pressure Vater				Coef C	
	<< Explanatory Notes >>	·	-	of			1	」 (単)	823. 886 257. 828 296. 953 44. 415 96. 106 117. 885 346. 203 346. 203 346. 203 104. 219 104. 219 104. 219 104. 219 110. 239 110.
	natory	ء - ا ا	Head Pressure Ground Level	Ellectual H Consumption			LineData —	(um)	100.0 37.5 37.5 37.5 37.5 37.5 37.5 37.5 37.5
	Expla		н.: 19	EHL: Oc:			- Line	Node ST EN	84484352108446954332
	$\approx$	I						ST	166122111046665544222
<	(里)	· (U)	(‰)	(m/s)				Remarks	Reservoir Tank
s Formula	51, 220	16.200	0: 000	0. 000				Qc (1/S)	
Hazen-Williams Formula>>	Maximum EHP	Minimum EHP	Maximum I <sup>,</sup>	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0. \ 000\\ 16. \ 200\\ 23. \ 590\\ 23. \ 590\\ 23. \ 590\\ 23. \ 590\\ 23. \ 590\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 37. \ 570\\ 370\\ 370\\ 370\\ 370\\ 370\\ 370\\ 370\\ 3$
••								EHP 1st (m)	· · ·
—Bikolo < <case.1< td=""><td>-</td><td>17</td><td>17</td><td>0</td><td>0.00 (cm)</td><td>2 (times)</td><td>     </td><td>13 13</td><td>1, 953. 020           1, 953. 020           1, 936. 820           1, 932. 430           1, 923. 430           1, 923. 430           1, 923. 130           1, 932. 910           1, 932. 910           1, 932. 910           1, 932. 910           1, 932. 910           1, 917. 240           1, 917. 290           1, 915. 370           1, 915. 450           1, 915. 450           1, 915. 450</td></case.1<>	-	17	17	0	0.00 (cm)	2 (times)	   	13 13	1, 953. 020           1, 953. 020           1, 936. 820           1, 932. 430           1, 923. 430           1, 923. 430           1, 923. 130           1, 932. 910           1, 932. 910           1, 932. 910           1, 932. 910           1, 932. 910           1, 917. 240           1, 917. 290           1, 915. 370           1, 915. 450           1, 915. 450           1, 915. 450
— — — Bi	Tank	Node	Line	Pump, Decom	gence Gap	Calculation	— NodeData	E I	$\begin{array}{c} 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1953.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\ 1955.020\\$
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								HL.	$\begin{array}{c} 2. & 337\\ 1. & 024\\ 1. & 024\\ 1. & 024\\ 1. & 349\\ 0. & 741\\ 1. & 349\\ 0. & 741\\ 1. & 297\\ 0. & 606\\ 0. & 468\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 214\\ 0. & 204\\ 0. & 214\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\ 0. & 804\\$
			pe	Coefficient of Flow	f Flow Gradient			I (%)	$\begin{array}{c} 2.836\\ 9.651\\ 3.970\\ 3.970\\ 3.970\\ 3.970\\ 3.970\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.971\\ 3.$
·			Diameter Length of Pipe		city o aulic	Head Loss Add Pressure		V (国/ S)	$\begin{array}{c} 0. & 385\\ 0. & 249\\ 0. & 747\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 249\\$
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	natory 1	- 4 - 1 - 1	Ground Level	LITECTUAL H Consumption			LineData —	C (IIII)	100 37.5 37.5 37.5 37.5 37.5 37.5 37.5 37.5
	Expla	- Node		Qc:			- Line	Node EN	8466649352510840054332
	∻	•					i I	ST	6612221104669744222
<	(四)	( <b>II</b> )	. (%)	(m/s)				Remarks	Reservoir Tank
Formula>	40.444	10, 502	30. 364	0. 747				Qc (1/s)	-3.025 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.275 0.
: Hazen-Williams Formula>>	Maximum EHP	Minimum EHP	Maximum I	Махітит V				EHP 2nd (m)	$\begin{array}{c} 0 & 000 \\ 13.863 \\ 17.230 \\ 11.206 \\ 11.206 \\ 12.23664 \\ 12.26681 \\ 12.26681 \\ 22.124 \\ 22.8674 \\ 22.8674 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\ 22.26.881 \\$
	,*							EHP 1st (m)	
colo < <case.2< td=""><td>1</td><td>17</td><td>17</td><td>0</td><td>0.72 (cm)</td><td>13 (times)</td><td></td><td>۳) (۱</td><td>1, 953. 020 1, 936. 820 1, 932. 430 1, 929. 940 1, 932. 130 1, 932. 940 1, 932. 910 1, 932. 120 1, 917. 240 1, 915. 370 1, 915. 450 1, 915. 450 1, 915. 450</td></case.2<>	1	17	17	0	0.72 (cm)	13 (times)		۳) (۱	1, 953. 020 1, 936. 820 1, 932. 430 1, 929. 940 1, 932. 130 1, 932. 940 1, 932. 910 1, 932. 120 1, 917. 240 1, 915. 370 1, 915. 450 1, 915. 450 1, 915. 450
Bikolo	Tank	Node	Line	Pump, Decom	Convergence Gap	Calculation 13	— NodeData	H)	$\begin{array}{c} 1953. \ 020\\ 1953. \ 020\\ 1947. \ 817\\ 1947. \ 817\\ 1947. \ 817\\ 1947. \ 817\\ 1943. \ 412\\ 1944. \ 420\\ 1944. \ 171\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 925\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926$ 1946. \ 926\\ 1946. \ 926\\ 1946. \ 926 1946. \ 926\\ 1946. \ 926
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## Appendix 7 References 7-2 Result of Test Well Drilling (Well Column Diagram)

## [ -

### Test well drilling and existing water source survey for the second preparatory survey of the project for small towns water supply in southern part of the Amhara regional state

		Site No.	14 ductive well #1 (E	(H1)							
Well No.		ation	Coordinate		Altit	ude	Town	Zone East Goyam	State Anhara		Country Ethicae
Date: fron	n to 12/11/2011	Drilling :	Equipment Type 729-300	Method D774	Flor	W.	Depth GL -76.0	Depth	Depth		Final Depth GL -76.0m
sing Type :	Size	Inside Dia.		Joint Type Screw	Installation	depth:	+0.75-62	2			Total Length 63, 7m
reen Pipe :	6" Material	150.0mm Diameter	Silot Size	Open Rate	Joint T		Installatio	depth: -62.92 - 74.3	×		Total Length 33.477
PIC servation Pipe	6" Material	150.0mm Diameter	L.Onm Silot Size	Open Rate	Sore T sniot	ype	Installatio		0		Total Length 72.0m
avel Pakking	GS Ongin	Gravel Size	3/4" Location	Volume	Divelop		72.Cm	Method	Duration	SWL (m)	Discharge
bmersible pun	Basaite mp: 1	o 2-6mm nstallation Da	te:	2.0 M2				Å.r	5715		
lit Diameter (mm) and Hethod	P	osition of Pl Well Struc	pes and ture +0.70m			m Normal 0.5m No (ohyn-ny	innal	80 80 100	Well Column	Depth (m)	Lithology
тв				D	0 10 20	11				-1,07	Blak Clay
RM : 305mim	CG BS		- 6.0m	-10 -20							Weathered ⊤uff
		PC		-30					*****	-27 m	
HB DTH 254mm	OP			-40					X X X X X X X X X X X X X X X X X X X		Basalt:- Slightly fractured and slightly weathered. However between 61m ai 76m it is highly fractured and watehe and water bearing (Main aquifer)
				-50				<pre>{</pre>	<pre>cxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx</pre>		
		and a second	60.000	-20		11					
		100000000000	- 62.92m	-70		8		5	******		
	BP							/		-76m	
				-30							
				-90							
	_			-100							
MBOL: B = Hammer E B = Tricon Bit	BIt	CG = Ceme OP = obse G = Gravel	vation pipe	PC = PVC Ca S = Screen P = Pump Po						otary with rilled with	h mud water

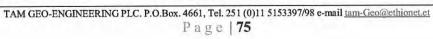
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		Site No. 1		1 /8411						
Well No.	Lo	cation	ductive well # Coordina	te (UTM)	Altitude	Town	Zone Fact Golam	State Amhara		Country Ethiopia
BH2 Date: from	to	Vetmen Drilling :	Equipment Type	Method	Flow	Depth	East Gojam Depth	Depth		Final Depth GL +87.0m
sing Type :	Size	Inside Dia.	TOP-300 Outside Dia.	D7H Joint Type	Installation depth:	GL -87.0m				Total Length 69.4m
PVC reen Pipe :	Material	250.0mm Diameter	162. Sinn Silot Size	Open Rate	Joint Type	+0.75-65.64 Installation de	pth:			Total Length
PVC servation Pip	6" Material	150.0mm Dameter	2. Grom Silot Size	20% Open Rate	Joint Type	Installation de	-68.64 - 85.8 pth:		-	IR.2m Total Length
avel Pakking	Origin	Gravel Size	Location	Volume	Threaded Divelopment:	78.0m	Method	Duration	SWL (m)	78.0m Discharge
bmersible pun	Basa/bc	o 2-6mm Installation Date	:	2.0 m*			Air	57%		
iit Diameter (mm) and Method		Position of Pipe Well Structu	s and me+0.70			formal (ohnem) formal (ohnem) 200	300	Well Column	Depth (m)	Lithology
TB RM : 305mm			i.0m	D					-7m	Blak Clay
	<u></u>	• • •	20m	-10 -20 -30					-36 m	Basalt:- Slightly fractured and slight weathered. However between 23m and 30m it is hard and not fractured
HB DTH 254mm	<u>OP</u>			-40 -60 -60						Volcanic Ash and Tuff:-volcar ash occurs from 36m to 40m, the remaining is tuff welded and weathered to variable digrees
	<u>8</u> P	- 66	3.64m	-70		>			-70 m	Basalt:- Highly to slightly fractured from 70m to 81m (Major aquifer)
	BP			-90					-87m	
IMBOL: IB = Hammer B IB = Tricon Bit	ĸ	CG = Cement OP = observa G = Gravel BS = Bentoni	tion pipe	PC = PVC Cas S = Screen P = Pump Po B.P.=Bottom	scion			R M = R DTH = D		n mud water Fair

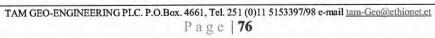
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# D

Loc	cation Sede	tive well #1 (B) Coordinat		Altitude	Town	Zone	State		Country
		the second		and the second second second	Secle	East Cojam	Ampara		Ethiopia
to	Drilling :	Equipment Type	Method	Flow	Depth	Depth	Depth		Final Depth GL -SZ. Om
Size	Inside Dia.	Outside Dia.	Joint Type	Installation depth:	N. C. 200 (1997)				Total Length
6" Material	Diameter	Silot Size	Open Rate	Jaint Type	10.75-68.69 Installation dep	th:			75.2m Total Length
5"	150. Centeri	s.Omm	10%6	Screw Joint Type	Installation dep	-65.69 - 80.13			11.4m Total Length
65	3	14"		Threaded	77,0th		Duration	SVVI (m)	77.0m Descharge
Bese/tic	0 2-6mm		2.50 m*	preciopinent'		Air	6Hs	arre und	
							1.2	1	
P	Well Structu			0.51	n Normal (ohm-m) n Normal (ohm-m) 600 800	1000	Well Column	Depth (m)	Lithology
<u>ca</u> ,	6	.0m	-10						Cl <b>øy:-</b> Reddish brown
<u>85</u>		20m	-20					-20m	Trachytet-Highly fractured & highly weathered trachyte
			-40					-38 m	Clay:- Reddish brown Clay
<u>0</u> P			-50		MM		*****************		Basalt:-highly Weathered
				N K	$\leq$		222	-60 m	
			-00		4			-62 m	Pyroclastic:- Highly weathered san
	1						*****		Basalt: - moderately waetherd and slightly fractured
	- 6	8.69m		1	-		XXXX	-69 m	
			-70	81				~70 m	Clay:- Red Clay
BP			-60			_	*****	-87m	Basalt:- Highly to moderately fractured and weathered from 70m 82m (Major aquifer)
	Conservation of the second sec		-90						
	6° Material 6° Material 65 Origin Researce Ip: CG BS	Size Inside Dia. Size Inside Dia. Size Communications of the second se	Size Inside Dia, Outside Dia, 6° 1280 Cmm 2582 Dmm 2582 Dmm 2582 Dmm 2582 Dmm 2582 Dmm 158 Star 9° 1282 Cmm 2 Johnn 3 Johnn 3 Johnn 2 Johnn	Size     Inside Dia.     Outstade Dia.     Outstade Dia.     Daint Type       Misterial     Daineter     \$250 cmm     \$250 cmm     \$250 cmm       Misterial     Daineter     \$301 Size     Open Rate       65     \$250 cmm     \$260 cmm     \$260 cmm       Misterial     Daineter     \$301 Size     Open Rate       65     \$260 cmm     \$260 cmm     \$260 cmm       66     \$247     Open Rate     \$260 cmm       67     \$200 cmm     \$260 cmm     \$260 cmm       68     \$247     Open Rate     \$260 cmm       69     Gravel Size     Location     Volume       92:     Installation Date :     Installation     \$260 cmm       92:     Installation Date :     Installed     \$260 cmm       92:     Installation Date :     100 cmm     \$260 cmm       93:     -20m     -20     \$200 cmm       94:     510 cmm     \$20 cmm     \$20 cmm       95:     -20m     \$20 cmm     \$20 cmm       96:     -20m     \$20 cmm     \$20 cmm       97:     -20m     \$20 cmm     \$20 cmm       98:     -20m     \$20 cmm     \$20 cmm       99:     -68.69m     \$20 cmm     \$20 cmm	Size     Inside Dai.     Outside Dai.     Dain Type     Instaliation depthy       6°     126,0mm     502,0mm     502,0mm     Social       8°     126,0mm     1000     5000     Social       8°     126,0mm     1000     1000     Donneting       8°     1260,0mm     1000     Donneting     1000       900     0     0     0     0       900     0     1000     0     0       900     0     1000     0     0       900     0     1000     0     0       900     0     1000     0     0       900     0     0     0     0       900     0     0     0     0       900     0     0     0     0       900     0     0     0     0       900     0     0     0     0       900     0     0     0     0       900     0     0     0     0       900     0     0     0     0       900     0     0     0     0       900     0     0     0     0       900     0     0     0 <td>Size B         Trade Do. Docume         Outside Do. Server         Derivation of the Server         Derivation of the ServerServerServer         Derivation of</td> <td>Size B         Tracke Dia, Distribution Genty         Track Dial Distribution Genty         Track Dial Distribution Genty         Track Dial Distribution Genty         Track Distribution Genty         Track Distribution Genty         Track Distribution Genty         <thdistribution genty<="" th=""> <thdistribution genty<="" th=""></thdistribution></thdistribution></td> <td>See     Trade Da     Cuesto Da     Abent Type     Tradition Depty     Tradition Depty       Method     22.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Method     22.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Method     22.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Method     20.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Method     20.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Observed     20.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Observed     20.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Verification Dista     resulted     -1.0 cm     -1.0 cm     0     20.0 cm       Op     -0.0 cm     -0.0 cm     -0.0 cm     -0.0 cm     0     20.0 cm       0     -0.0 cm     -0.0 cm     -0.0 cm     -0.0 cm     0     20.0 cm       0     -0.0 cm     -0.0 cm     -0.0 cm     -0.0 cm     0     20.0 cm       0     -0.0 cm     -0.0 cm     -0.0 cm     -0.0 cm     0     0       0     -0.0 cm     -0.0 cm     -0.0 cm     0     0     0       0</td> <td>Exam     Desce Dos.     Outloo de de construction destru     Schull de construction de constructin de construction de construction de construction de construction</td>	Size B         Trade Do. Docume         Outside Do. Server         Derivation of the Server         Derivation of the ServerServerServer         Derivation of	Size B         Tracke Dia, Distribution Genty         Track Dial Distribution Genty         Track Dial Distribution Genty         Track Dial Distribution Genty         Track Distribution Genty         Track Distribution Genty         Track Distribution Genty         Distribution Genty <thdistribution genty<="" th=""> <thdistribution genty<="" th=""></thdistribution></thdistribution>	See     Trade Da     Cuesto Da     Abent Type     Tradition Depty     Tradition Depty       Method     22.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Method     22.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Method     22.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Method     20.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Method     20.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Observed     20.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Observed     20.0 cm     20.0 cm     20.0 cm     20.0 cm     20.0 cm       Verification Dista     resulted     -1.0 cm     -1.0 cm     0     20.0 cm       Op     -0.0 cm     -0.0 cm     -0.0 cm     -0.0 cm     0     20.0 cm       0     -0.0 cm     -0.0 cm     -0.0 cm     -0.0 cm     0     20.0 cm       0     -0.0 cm     -0.0 cm     -0.0 cm     -0.0 cm     0     20.0 cm       0     -0.0 cm     -0.0 cm     -0.0 cm     -0.0 cm     0     0       0     -0.0 cm     -0.0 cm     -0.0 cm     0     0     0       0	Exam     Desce Dos.     Outloo de de construction destru     Schull de construction de constructin de construction de construction de construction de construction



		Site No.	uctive well #1 (i	3H1)						
Well No. BHJ	L	ocation	Coordina	te (UTM)	Altitude	Town Dibo	Zone East Gojan	State Amhara		Country Ethiopia
Date: from	to 3 12 2011	Drilling :	Equipment Type 70P-300	Method D7H	Flow	Depth GL -80.0m	Depth	Depth		Final Depth GL -SG. Om
sing Type :	Size 6"	Inside Dia. 150.0mm		Joint Type Screw	Installation depth:	+0.75-83.95			1000	Total Length 6-7.1m
een Pipe :	Material 6*	Diameter	Silot Size	Open Rate	Joint Type Screw	Installation dep	th: -53.35 - 74.5	1		Total Length 73.4m
PVC servation Pip	Material	150.0mm Diameter	Silot Size	Open Rate	Joint Type Threaded	Installation dep 72.0m		1.00		Total Length 72.0m
vel Pakking	Origin	Gravel Size		Volume	Divelopment:	12.00	Method	Duration	SVVL (m)	Discharge
mersible pum	Basa/bc	0 2-cmm Installation Da	te :	1.50 m²			AF	SHS		
it Diameter (mm) ind Hethod		Position of Pi Well Struc	pes and ture +0.70	m		9m Normal (ohm-m 9m Normal (ohm-m 100 150	200	Well Column	Depth (m)	Lithology
TB				0 +					-2m	Blak Clay
RM : 305mm	<u>CG</u> <u>85</u> <u>OP</u>		- 6.0m	-10 -20 -30 -40 -50 -50 -70					-75 m	Basalt:- Highly fractured and weathered from 70m to 75m (Majo aquifer)
					11				1	Pyroclastic:- Highly weathered pyriclastic material
				-80 -	11	-	-	1.00	-Būm	
				- 90 -						
MBOL:		CG = Came	nt Grout	-100 -	na			RM = R	cary with	i mud water
SIMBOL: NB = Hammer Bi TB = Tricon Bit	π	CG = Ceme OP = obser G = Gravel		PC = PVC Cass S = Screen P = Pump Pos					otary with	r mud water



5

		Site No.	oductive well #	3 (8H3)						a second s
Well No.		ation	Coordinat	te (UTM)	Altitude	Town	Zone East Gojam	State		Country Ethopia
Date: from	to 25 05 2012	Drilling :	Equipment Type 707-500	Method D7h	Flow	Depth GL -51.0m	Depth	Depth		Final Depth GL -61.0m
ing Type :	Size	Inside Dia.	Outside Dia.	Joint Type	Installation depth:	+0.75-42.34				Total Length <i>43, Im</i>
PVC ten Pipe :	Material	150. Cmm Diameter	369.0mm Slot Size	Sprew Open Rate	Joint Type	Installation dep	th: -+12.34 - 60			Total Length 17.2m
PVC ervation Pip	5" Material	150.0mm Diameter	I. Omm Silot Size	20% Open Rate	Joint Type	Installation dep				Total Length 45.0m
vel Pakking	Origin	Gravel Size	2/4" Location	Volume	Threaded Divelopment :	-15.0m	Method	Duration	SWL (m)	48.0m Discharge
mersible pur	Easa/tic	o 2-cener Installation Date	61	3.0 m*	Contract of Contract		Ar	515		
t Diameter (mm) nd Method	Pe	Well Struct		n o	0.5m N	ormal (ohmm) ormal (ohmm) 200	300	Well Column	Depth (m)	Lithology
TB RM : 305mm				0 <b>-</b>					-5m	Clay:-Brown silty clay
	<u>c</u> ,		6.0m	-10 -						Basalt:- Highly weathered
	BS ,	-	20m	-20				***********	-18m -26 m	Basalt:- Moderately weathered
HB DTH 254mm		PC		-20				**********	-39m	Basalt:- Fresh and massive
				-40 -					-42 m	Clay:- Brown clay
	OP			1				***	-46 m	Basalt:- Moderately weathered and slightly Fractured
				-50		_			-52 m	Basalt:- Fractured basalt (Water Bearing
	ВР		- 60.00m	-50				***********************	-61m	Basalt - Highly to slightly fractured from 70m to 81m (Major aquifer)
				-70						
				-80						
				-90-						
	8			-100 -						
Hammer B Tricon Bit	t (	CG = Cemen OP = observ G = Gravel BS = Bentna	ation pipe	PC = PVC Case S = Screen P = Pump Posi B.P.=Bottom F	tion			R M = Ro DTH = D		i mud water air

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een Pipe : PiC PiC PiC	23 05 2012	Drilling :				Altitude	Ammenuel	Zone East Galaro	Amhere		Ethopia
een Pipe : PiC PiC PiC		Unling:	Equipment 7 DTH Rota			Flow	Depth 62 - 120.0m	Depth	Depth		Final Depth GL = 120,0m
een Pipe : Pitz	Size	Inside D	a. Outside D	a. Joint'	Type	Installation depth:					Total Length 39.3m
	Material 6"	Diamet 250.00	er Slot Size		Rate	Joint Type Screw	Installation dept	h: -58.56 - 50			Total Length 11,4n
servation Pip	Material	Diamet				Joint Type	Installation dept	h:			Total Length
evel Pakking	CS Origin	Gravel S	ze Location			Threaded Divelopment :	not installed	Method	Duration	SWL (m)	Discharge
mersible pur	Basaltic np: 1	nstallation		6.50	1m2			Ar	Bris		
	-				-			-	1	-	1
it Diameter (mm) ind Hethod	P	well St	Pipes and ucture	0.75m		0.5m	Normal (ohm-m) Normal (ohm-m) 200	300	Well Column	Depth (m)	Lithology
TB RM : 305mm					0		····	Ĩ		-Sm	Clay:-Brownsilty clay
	ca	•	- 6.0m		-10 -				*****	-16m	Basalt:- Highly weathered
	85		- 20m		-20				********	-28 m	Basalt:- Weathered & freactured
					-30		-	-	*****	-34m	Basalt:- Moderately weathered and fractured
		8.8.3.00	- 38.56m		-40						Basalt:- Highly fractured and weathered (main aquifer)
HB DTH 254mm	BP		- 50.00m	ŀ	- 60 - 60					-SDm	Basalt:- slightly weathered
		76			-70 -					-70 m	Basalt-Slightly weathered hard
					-100				***************************************	-98 m	Paralt technologies
					-110				*****	-120m	Basalt - Fresh Hard and massive
									1		
1BOL:			and from the	-					P.M - 21	tany unt	mud justar
- Hammer B		OP = obs	ervation pipe	PC = P S = Sc		ng			R M = Ro	DEBTY WITH	n muid water

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		Site No.	29 ell #1 (BH1)							
Well No.		ation		ate (UTM)	Altitude	Town	Zone East Gojam	State Amhara		Country Ethiopie
BH1 Date: from	n to 25.01 2012	Kunzia Drilling :	Equipment Type 70P-300	Method DTH + Alud	Flow	Depth GL -66.0m	Depth	Depth		Final Depth GL -95.0m
ng Type :	Size	Inside Dia	Dutside Dia.	Joint Type	Installation dept	h:				Total Length
PVC en Pipe :	Material	150.0mm Diameter	162.5mm Silot Size	Screw Open Rate	+0.75-14.74 Joint Type	Installation de	-54.88 - 60.62	1.1.1.1.1.1	1.1	75.2m Total Length
PIC ervation Pipe		150.0mm Diameter	3.0mm Silot Size	Dpen Rate	Screw Joint Type	-14, 74 - 20, 44 Installation de	-#3,## - 54.88 oth:	50.62-66.3	*	11.4m Total Length
el Pakking	Origin	Gravel Size	8/4" Location	Volume	Divelopmen	77.0m	Method	Duration	SWL (m)	22.0m Discharge
mersible pur	Easa/bc	o 2-6mm nstallation Da		2.50 m2		_	Alt	6HIS		
Diameter (mm) id Method	P	Well Strue	pes and ture +0.7	om		1.0m Normal (ohmm 9.5m Normal (ohmm 00 600 600	ō	Well Column	Depth (m)	Lithology
TB RM: 305mm				D						Clay:- Reddish brown
Susanna			- 6.0m						-6m	
	CG ,	- 11						***		
	BS	*	10m	-10				****		
		10000						****		
			- 14.74m					XXXX		
		1			1			XXXX		
		1		-20	1			XXX X		
					S			******		
					11			XXX		Desailer Highly whether a first state
		and			12			***		Basalt:- Highly weathered 6 to 16 m, water bearing; Highly weathered
		10			1		-	***		and fractured 29m to 52m water bearin (Major aquifer) and highly fractured
				-90	151			XXX		61m to 65 m water bearing
					K			***		The second
		PC		_				XXX		
				1.000				**********		
				-40	R			12XX		
	1.1.1		and a state		17			XXX		
нв	OP		- 43.44m		5	4	>	XXX		
DTH					(			***		
254mm					2	5		*****		
				-50	1	T		XXXX		
		巖			1			****		
							_			
					S		_	****		
			- 60.62m	-50	5			****		
					1	4		****		
								IXXXX		
							_	***		
					1			XXXX XXXX		
				-70	8			XXXX		
					K			1222		
	BP				0			************		
					15			XXXX XXXX		
				-80	5			****		
					0			XXX		
					11			****	-86m	
		自由自由社			)<			EXXX		1
				-90						
	0.00			-100						
				1						
IBOL:		CG = Ceme	ent Grout	PC - PVC C	sing E	R M = Rota	y with mud wa	ater	-	
Hammer B	310	OP = obset G = Gravel	vation pipe	S = Screen P = Pump P		DTH - Drile			-	DTH & Rotary with mud water
- INCON BC			once sealed	B.P.=Botton		1 0 111 - 0/100			A REAL PROPERTY.	The second s

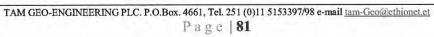
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Kunzila v Location Kunzila 12 Drilling: 12 Inside Di 250.0m d Diamete 350.0m d Diamete 350.0m Installation D Position of I Well Str	Equipment Type     TCP-300     a. Outside Dia. <i>TCP-300     TSlats State     TSlats State     τ     Slats State     T     Total     Tslats     T     Tslats     T     Tslats     T     Tslats     T     Tslats     T </i>	DTH + Aluć Joint Type Screw Open Rate 10% Open Rate Volume 2.50 m <sup>2</sup>	Altitude Flow Installation depth v6.7526.2 Joint Type Screy Joint Type Typeeded Divelopment : 0 v200 200	-22.02 - 49.39 Installation depth -26.3 - 92.02 Installation depth -27.0m	h: -49.38 - 54.9 h: Method Ar	State Ambara Depth -77,8 - 88,1 -66, 54 - 77,4 Duration 6HS Well Column	s SWL (m) Depth	Country Ethogum Final Depth GL-55.Cm Total Length 22.3m Total Length 22.3m Total Length 27.Cm Discharge
Drilling : Inside Dia 250.0mm Diamete 250.0mm d Diamete Gravel Si c a 2-6mm Installation D Position of f	TOP-500           b.         Outside Dia.           n         162.5mm           r         Slot Size           3/4"         Slot Size           2/4"         cettion           n         Location           n         Pipes and	DTh + Mud Joint Type Screw Open Rate 1055 Open Rate 2.50 m <sup>2</sup>	Installation depth: +0.75-25.3 Joint Type Sorew Joint Type Threaded Divelopment :	Depth GL -85.0m -82.02 - 49.18 Installation depth -26.3 - 82.02 Installation depth 27.0m -27.0m -27.0m	Depth -54.9-55.94 h: -49.35-54.9 h: Method Ar	Depth -77.8 - 83.1 -66.34 - 77.1 Duration 6Hs Well	s SWL (m) Depth	Final Depth GL -45.Cm Total Length GL -87 Total Length 22.9m Total Length 77.Cm Discharge
Inside Dia 250.0mm d Diamete 350.0mm d Diamete Gravel Si c a 2-6mm Installation D	b. Outside Dia. <u>1262.5mm</u> <u>1262.5mm</u> Silot Size <u>7.2.7mm     <u>7.477     Silot Size     <u>7.477     Silot Size     <u>7.477     Silot Size     <u>7.477     Silot Size     Pipes and     Pipes and  </u></u></u></u></u>	Joint Type Screw Open Rate 10% Open Rate Volume 2.50 m <sup>2</sup>	+0.75-25.3 Joint Type Screw Joint Type Divelopment :	-22.02 - 49.18 Installation depth -26.3 - 32.02 Installation depth 77.0m	h: -49.38 - 54.9 h: Method Ar	66.34 - 77.0 Duration 6hs Well	s SWL (m) Depth	Total Length 51-91 Total Length 22:91 Total Length 72:01 Discharge
250.0mm al Diamete 350.0mm d Diamete Gravel Sto c a 2-5mm Installation D Position of f	m 262.5mm r Silot Size m 2.0mm r Silot Size 3/4" ze Location m Nate: Pipes and	Screw Open Rate 1055 Open Rate Volume 2.50 m <sup>2</sup>	+0.75-25.3 Joint Type Screw Joint Type Divelopment :	-22.02 - 49.39 Installation depth -26.3 - 92.02 Installation depth -27.0m	h: -49.38 - 54.9 h: Method Ar	66.34 - 77.0 Duration 6hs Well	s SWL (m) Depth	Total Length 22.3m Total Length 77.2m Discharge
<u>350.0m</u> d Diamete Gravel St <i>c a 2-6m</i> Installator D Position of I	n <u>J.Crvm</u> r Silot Size 3/4" ze Location n Nate : Pipes and	1055 Open Rate Volume 2.50 m <sup>2</sup>	SCHEW Joint Type Threaded Divelopment :	-26.3 - 32.02 Installaton depth 77.0m	+9:28 - 5+.9 h: Method Ar	Duration 6Hs Well	SWL (m) Depth	22.9m Total Length 27.0m Discharge
Gravel Sto c <u>a 2-6m</u> Installation D Position of I	5/4" ze Location m vate : Pipes and	Volume 2.50 m²	Divelopment :	27.0m	Method Ar	6Hs Well	Depth	22.0m Discharge
E <u>p 2-6m</u> Installation D Position of I	n Date : Pipes and	2.50 m²				6Hs Well	Depth	
Position of I	Pipes and			.5m Normal (ohm-m)		Well		11
				.5m Normal (ohm-m)		Well		The second second
→			A CONTRACTOR OF A	0 300 400		column	(m)	Lithology
	- 6.0m							Clay:-Reddish brown
	- 10m	-10				*****	-8m	
	- 26.3m	-20		S N		***************************************		Basalt:- Highly weathered and vesicular (Sm to 20m), fractured and weathered (20m to 34m) water bearing
			F	5		****	-34m	Clay:- Reddish brown
PC		-40				21 proved	-40m	
	- 49.18m	-50		3,		*****	-52m	Basalt:- Highly weathered and disintegrated basalt with red dish brown clay (water bearing)
	- 66.34m	-50	D					Alluvial Deposit:- With Reddish brown clay
			R				• 78m	
		-80	ß			****	-85m	Basalt:- Highly weathered and disintegrated basalt with reddish brow
		PC - 49.18m	PC -49.18m -50 -66.34m -70	PC - 26.3m - 49.18m - 66.34m - 66.34m	-20 -20 -20 -20 -20 -20 -20 -20 -20 -20	- 26.3m	PC -49.18m -66.34m -66.34m	PC -49.18m -66.34m -66.34m -50 -66.34m -70 -78m

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		Site No.								
Well No.	Lo	Kunzila B cation	Coordinat	e (UTM)	Altitude	Town	Zone	State		Country
BH4 Date: from		Kanzia Drilling :	Equipment Type	Method	Flow	Kunzile Depth	East Gojam Depth	Amhara Depth		Ethopia Final Depth
06 2012 sing Type :	3/7/2012 Size	Inside Dia	TOP-300 Dutside Dia.	Jont Type	Installation depth:	GL -62.0m			-	GL -62.0m Total Length
PIC reen Pipe :	6" Material	150.0mn Diameter	169.0mm	Screw Open Rate	+0,75-21,68 Joint Type	-27.4 - 33.12 Installation der	-38.84 - 44.55	-50.28 - 56		39.5m Total Length
PUC	6*	150.0mm	j. j.Crnm	10%	Screw	-23.67-27.4	-33.12 - 38.54	44.56 - 50.3	8	17.5m Total Length
bservation Pip	Material GS	Diameter	3/4"	Open Rate	Joint Type Threaded	Installation des 52.0m				52.8m
avel Pakking	Origin Sasa/bic	Gravel Siz		Volume 2.50 m *	Divelopment :		Method	Duration	SVVL (m)	Discharge
ibmersible pur	np :	Installation D	ate :							
Bit Diameter			and the second	-				Well	Depth	
(mm) and Hethod		Well Stru		n		9m Normal (ohm- 5m Normal (ohm-	n)	Column	(m)	Lithology
			1		0 100 200	300 40	0 500			
тв				0	1 mar 1					
RM : 305mm										Clay:- Reddish brown
			- 6.0m					S 2		
	CG								-Bm	
	BS		10m	-10				***	1.00	
			1000					1222		
								CXXX XXXX		6
								XXXX		Basalt:- weathered vescicular basalt (Sm to 17m), red ash(scoria ) with vesicular
										basalt (17 to 20m) and fractured basalt
				-20				XXXX		(20m to 34m) water bearing
			- 21.7m					1222		
								2222		
		臺麗	27.100					XXXX XXXX		
		G	- 27.4m					*****		
HBDTH		1000		-30				XXXX XXXX		
254mm			- 33.12m					***	-34m	
								a a a	1	
1 11		叢							1	Clay:- Reddish brown
1 11		PC	- 38.84m						++0 m	
1 1		1		-40						
1 11	OP		and and a second			1000000	1000 C	EXXX:	1000	Basalt - Highly weathered and
1 1			- 44.56m					****	1.1.1	disintegrated basalt with reddish brown clay (little water)
		窶						888		
1 1		: <b>3</b>	- 49.16m	-50				1998		
			- 49.10111			120		XXX		
								XXXX XXX		
	BP							****		
No. of Concession, Name								1222		
				-50				XXXX		
								2222	-62m	
				-70						
				-80						
				-90						
				-100						
IMBOL:	4					1.1.1.2	-			
B = Hammer Bi		CG = Cem		PC = PVC Cas	ng	R M = Rota	y with mud wa	ter		
	C	OP = obse		S = Screen	ition	DTH = Drile				DTH & Rotary with mud water



Well No. BH2		ation Lumame	ell #2 (BH2) Coordina	te (UTH)	Altitude	Lomane	Zone East Gojam	State Amhara		Country Ethiopia
Date: from 01/2012	to 126 03 2032	eniling :	Equipment Type TOP-300	Method DTH	Flow	Depth GL -147.0m	Depth	Depth		Final Depth GL -147.0m
ing Type :	Size	Inside Dia.	Outside Dia.	Joint Type	Installation depth					Total Length
PIC ten Pipe :	5" Material	150.0mm Diameter	<i>169.0mm</i> Silot Size	Open Rate	+0.75-49.98 Joint Type	Installation de	epth:	-112.9 - 118.52		107.2m Total Length
FIC ervation Pipe	5* Material	150.0mm Diemeter	2.0mm Silot Size	10% Open Rate	Screw Joint Type	-49.98 - 55.3 Installation de	-78.58 - 90	-107.18 - 112.5	-118.62 - 130	34.37 Totel Length
	GS		3/4"	14 A A A A A A A A A A A A A A A A A A A	Threaded	+0.75-107.2	5		make a h	109.0m
vel Pakking	Origin Basaloc	Gravel Size a 2-6mm	Location	J.O.m.	Divelopment :		Method	Duration 20Hs	SWL (m)	Discharge
mersible pur		staliation Dat	e:						-	
Diameter		S		-						
(mm) nd Hethod	P	Well Struc		m		Normal (ohmm) Normal (ohmm)		Well Column	Depth (m)	Lithology
a riculou			1		0 50 100	150 200	250 300	Internet		
TB				0						
RM : 305mm										
Judinin			6.0m				1.0	1		Clay:-Black clay
	CG		6.011	-10					-11m	
	1.00							****	1-0-1	Basalt: - Moderately to slightly fractured
								***		and wathered between 11 and 23 m. Fresh
				-20			-	****		and massive 23m to 35
					1			*****		
1 8								***		
	BS		- 20m	-30				XXX		
				-35				1888		
								***	-35m	
		PC						000	-39m	Clay:- Brown clay
5				-40				***********		
								***		
					1			222		
		1		-60				***		and the second second second second
$(\lambda, \beta)$								888		Basalt:- slightly to highly fractured.
1 1								XXX		Highly fractured and aquifer between 44m. and 55m
- (								****		and SSM
				-50				222		
1	OP							XXX		
1 3	ur			1.1	1			XXXX		
				-70				***		
					1			****	-74m	
HB&TB		1						1		
& RM DTH				-80		-		12		
254mm								8		
1		医囊		1.1						
		1 <b>E</b>						1 1 1		
				-90		1		100 1		
								12 5		
				-100	+++		+-11			
					1			3		
				-110						Tuff - weathered to different degrees
				-120				And the second		
					1					
				-130						
	BP			-140						
		anna an						in a		
									-148m	
				-160						
				-160					-	1
IBOL:		_								
DUL.		CG = Cemer		PC = PVC Cas	sng 📃	R M - Rota	ary with mud w	vater		
- Hammer B		an = obtan	ation pipe	S = Screen						

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