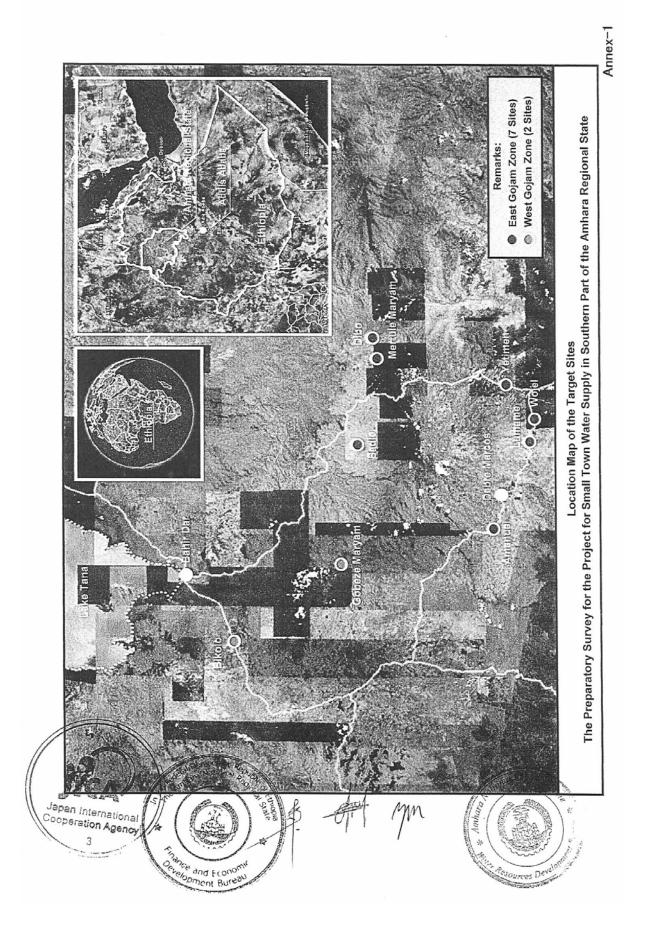
Annex:

- Annex-1 Project Sites
- Annex-2 Components of the Project
- Annex-3 Selected Sites
- Annex-4 Organization Chart of the Responsible Organization

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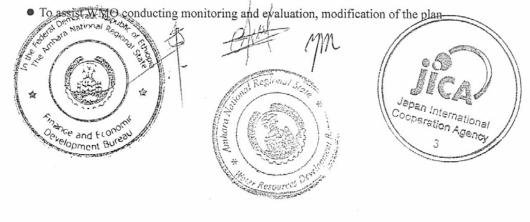
Annex-2

Components of the Project

No.	Town	Population (2016)	Water supply amount (2016)
9	Mertule Maryam	17,829	328.97 m ³ /day
10	Yetimen	3,877	74.33 m ³ /day
12	Lumame	13,451	255.17 m ³ /day
14	Wojel	3,758	121.22 m ³ /day
15	Sedie	3,947	87.99 m ³ /day
16	Dibo	2,510	89.22 m ³ /day
	Amanuel	12,694	86.40 m ³ /day
27	Gobeze Maryam	6,908	114.00 m ³ /day
	Bikolo	5,811	181.43 m ³ /day
	Total	70,786	1,338.73 m ³ /day

1. Construction of Water Supply Facilities: 9 towns as listed below

- 2. Technical Assistance consisting of:
 - To facilitate AWRDB and Woreda water office on the effective support system in proper management of Water Management Organization (WMO)
 - To institutionalize the operation and maintenance structures of WMO
 - To secure general understanding among the stakeholders on the operation and maintenance structures
 - To conduct technical trainings on the maintenance and repair of the facilities (implemented by EWTEC)
 - To conduct technical trainings on administrative tasks such as accountancy, book keeping and reporting

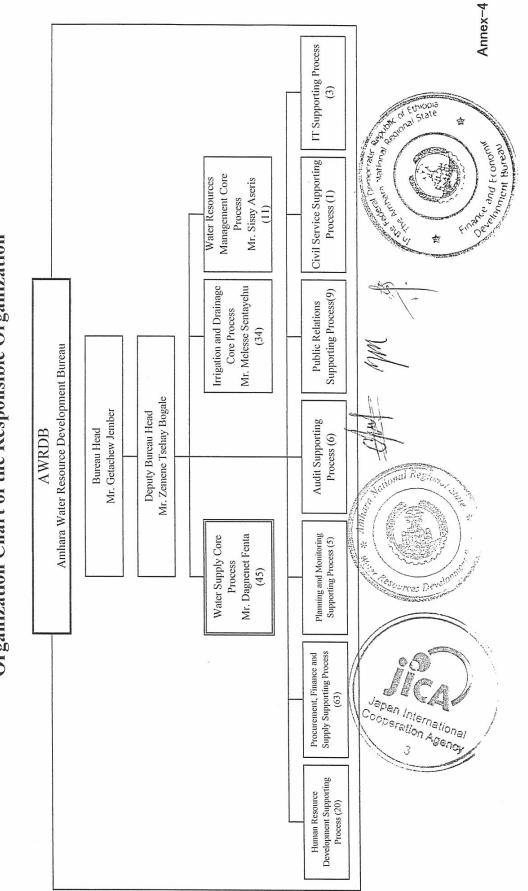


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Annex-3

			Selected Target Sites	
	No.	Zone	Woreda	Town
	9	East Gojam	Enebsie Sar Midir	Mertule Maryam
	10	East Gojam	Enemay	Yetimen
	12	East Gojam	Awabel	Lumame
	14	East Gojam	Awabel	Wojel
	15	East Gojam	Hulet Egu Enesie	Sedie
	16	East Gojam	Enebsie Sar Midir	Dibo
		East Gojam	Machakel	Amanuel
	27	West Gojam	Quarit	Gobeze Maryam
		West Gojam	Macha	Bikolo / /
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Organization Chart of the Responsible Organization

資料 5. ソフトコンポーネント計画書

アムハラ州南部地方小都市給水計画

ソフトコンポーネント計画書

(1) ソフトコンポーネントを計画する背景

1) 現状と課題

対象サイトにおいては、既存の水管理組織による運営・維持管理体制が整備されているが、管理 費用の積み立て計画を立案し、それを基に水料金を徴収・管理し、水道施設を運営していく能力に は乏しい。また、軽微な故障が発生しても、修繕せずに放置されている水道施設も散見される。他 方、施設の故障を防ぐための定期保守を担う Woreda 水事務所の役割分担が明確ではなく、それに かかる予算や人員も十分に配置されていないのが現状である。

以上から、水管理組織の運営・維持管理にかかる課題は、以下のとおりである。

- 運営・維持管理体制が確立されていない
- 機器操作や軽微な修理に対応できない
- 水料金(運営・維持管理費)の徴収・管理能力が低い

2) ソフトコンポーネントの必要性

前述のとおり、既存の水管理組織による運営・維持管理体制は整備されているが、管理費用の積 み立て計画を立案し、それを基に水料金を徴収・管理し、水道施設を運営していく能力には乏しい。 また、軽微な修繕に対する能力も不足している。本プロジェクトで整備される水道施設は、水管理 組織によって運営・維持管理が可能となる内容及び規模で計画するが、現状の水管理組織の体制及 び技術力では能力不足と判断される部分がある。

したがって、円滑なプロジェクトの立ち上がりを確実とするため、ソフトコンポーネントによる 技術支援を投入し、水管理組織及び Woreda 水事務所の運営・維持管理にかかる能力強化を支援す る。なお、対象サイトには、公共水栓式または各戸給水式水道施設が存在するため、住民の衛生理 念はある程度醸成されていると判断し、ソフトコンポーネント内での衛生教育は実施しない。

また、技術支援の内容としては、運営・維持管理能力の強化にかかるソフト面の支援に重点を置 くが、エチオピア国地下水開発・水供給訓練センター(Ethiopian Water Technology Centre、以下 「EWTEC」)と連携し、機械操作や軽微な修繕等のハード面についても技術支援を行なう。

(2) ソフトコンポーネントの目標

1) 目標

ソフトコンポーネントの目標は、「水管理組織が主体となって水道施設の運営・維持管理が適切 に実施されること」と定める。この上位目標は、「建設された水道施設がプロジェクト終了後も長期 間にわたって利用される」ことである。すなわち、ソフトコンポーネントの実施によって、本プロ ジェクト終了後の水道施設が、水管理組織主体で持続的に運営・維持管理されることを目指すもの である。なお、ソフトコンポーネントの PDM は、次表のとおりである。

PDM(ソフトコンポーネント)

	PDM(ソフトコン) 地描		以 如久供
プロジェクト要約 上位目標	指標	入手手段	外部条件
上位日標 建設された水道施設がプロジ ェクト終了後も長期間に亘って 利用される	住民の水因性疾病率の低下	・保健衛生の統計資料 ・住民アンケート	
ソフトコンポーネントの目標 水管理組織が主体となって、 水道施設の運営・維持管理が 適切に実行される	 ・全施設が年間を通して稼動している ・安全な水が得られる人口が 増加する 	 ・施設運転記録簿 ・施設利用登録簿 	AWRDB が水管理組織 主体の運営・維持管 理政策を変更しない
成果 1. 水道施設の運営・維持管 理に関わる実施体制が整う	 1.1 実施機関において、住民 主体の運営・維持管理に 対する連携意識が高ま り、水管理組織への支援 体制が形成される 1.2 各サイトにおいて水管理 組織が整備される 1.3 住民を含む関係者各自 が自分の役割を明確に認 識する 	 ・関係者へのヒアリング ・ワークショップ報告書 ・支援体制組織図 ・利用規約 ・水管理組織・組織図 ・運営・維持管理計画書 ・各担当者へのヒアリング 	住民が主体となること に関して、関係機関か らの異議がない
2. 運営・維持管理に必要な 技能や知識を習得する	 2.1 故障頻度が減少し、給水 施設の未使用期間が短 縮される 2.2 水管理組織での出納業 務を含む運営記録が作 成される 2.3 モニタリング・評価が計画 に応じて実施され、活動 に反映される 	 活動記録簿 施設運転記録簿 技術訓練報告書 故障時修理マニュアル 料金徴収出納帳 施設運転記録簿 ソフトコンポーネント 実施状況報告書 	
活動			前提条件
1.1 AWRDB 及び Woreda の 水管理組織への支援体 制を整える 12 水管理組織の運営・維持 管理体制を整備する 1.3 運営・維持管理体制に関 する理解を得る 2.1 水道施設の点検修理等 にかかる技術訓練(ハード 面)を実施する 2.2 会計、記録等のアドミニス トレーションにかかる技術 指導(ソフト面)を実施す る 2.3 活動のモニタリング・評価 を実施し、計画の修正を 行なう			関係者がプロジェクト実施に積極的である

2) 支援体制配慮事項

ソフトコンポーネントは、水道施設建設前に行なう「実施体制の確立」(フェーズ1)と建設中~ 後に行われる「運営・維持管理技術の習得」(フェーズ2)の2フェーズ体制を取り、サイト単位で 水管理組織を中心に啓蒙・教育活動を行なう。水道施設のハード面に関する維持管理に関しては、 EWTEC から2名の講師を各サイトに招き、関係者に対する合同の技術訓練を実施する。

(3) ソフトコンポーネントの成果

運営・維持管理にかかるソフトコンポーネントの成果(直接効果)は、以下のとおりである。

成果1:水道施設の運営・維持管理に関わる実施体制が整う

既存の水道施設は、サイト単位で水管理組織により運営されているが、故障や利用料金の支払い 困難等の様々な問題に対処できていないのが現状である。また、AWRDBや Woreda 水事務所による 支援体制はできているが、円滑に機能していない状態にある。

したがって、各機関における水管理組織への対応を見直したうえで、具体的な支援体制を整備する。また、利用規約を含む運営・維持管理計画を策定し、計画を具体的に推進させる。

成果2:運営・維持管理に必要な技能や知識を習得する

水管理組織による運営・維持管理を推進するためには、現在欠如している技術的能力に対する補 填が必要となる。実施機関による支援体制が整備されたうえで、具体的な問題に対応する能力を習 得するために、水管理組織及び Woreda 職員に対する技術訓練(ハード面及びソフト面)を行なう。 ハード面に対する技術訓練により、軽微な故障であれば水管理組織が修理し、複雑な修理が必要な 場合は Woreda 職員が対応することが可能となり、各機関による実施体制がより明確になる。

また、持続的な運営・維持管理とするためには、適切な利用料金の徴収と管理が重要であるため、 水管理組織及び Woreda 職員に対する会計管理に関する技術訓練を行なう。

さらに、水道施設の利用及び稼動状況を記録管理するため、記録作成にかかる訓練を実施する。 水管理組織で作成された記録簿は、Woreda水事務所から AWRDB に共有されることにより、故障に よる放置や水料金の徴収に関する問題が減少する。

(4) 成果達成度の確認方法

上記の成果を達成するための指標と成果達成度の確認方法は、以下のとおりである。

成果	達成度の確認項目	達成度の確認方法(案)
成果1	実施機関において、住民主体の運営・	・関係者へのヒアリング
水道施設の運営・維持管理	維持管理に対する連携意識が高まり、	・ワークショップ報告書
に関わる実施体制が整う	水管理組織への支援体制が形成され	·支援体制組織図
	たか	·利用規約
	各サイトにおいて、住民による水管理組	・水管理組織の組織図
	織が形成、または再編成されたか	·運営·維持管理計画書
	住民を含む関係者各自が自分の役割	・各担当者へのヒアリング
	を明確に認識しているか	·関係者全体組織図
成果 2	故障頻度が減少し、故障期間が短縮さ	・関係機関の活動記録
運営・維持管理に必要な技	れたか	·施設運転記録簿
能や知識を習得する		·技術訓練報告書
		・故障時修理マニュアル
	水管理組織での出納業務を含む運営	·料金徵収出納帳
	記録が作成される	·施設利用登録簿
	モニタリング・評価が計画に応じて実施	・モニタリング・評価記録
	され、活動に反映されたか	・ソフトコンポーネント実施報告書

成果達成度の確認方法

(5) ソフトコンポーネントの活動(投入計画)

1)活動区分

ソフトコンポーネントは、活動期間を「水道施設建設前」及び「施設建設中及び竣工後」の2フ ェーズに区分し、水管理組織を支援する実施機関である AWRDB 及び Woreda 水事務所の協力のも と、邦人コンサルタントがこれを統括する形で実施する。

また、水道施設の点検や修理等の技術訓練(ハード面)については、EWTEC の協力を仰ぐ。

2) 役割分担

本邦コンサルタント、Woreda 職員及び EWTEC 講師の役割分担は、以下のとおりである。

本邦コンサルタント

ソフトコンポーネント計画の統括者として以下を担当する。

- ソフトコンポーネント実施運営管理
- ワークショップ、セミナー等の立ち上げにかかる作業
- AWRDB との協議及び Woreda 職員に対するワークショップの実施
- 他ドナー、NGO との連携にかかる調整業務
- 水管理組織に対する AWRDB、Woreda 水事務所の支援体制の整備
- EWTEC 講師による施設維持管理にかかる技術訓練(ハード面)の運営実施
- アドミニストレーションにかかる技術指導(ソフト面)
- 運営・維持管理マニュアルの作成

- 各種規約の立案補助
- 各種記録簿作成補助
- 活動のモニタリング・評価に関するレビュー
- 各フェーズにおける活動結果のレビューとフィードバック
- 実施機関及び JICA への報告

Woreda 職員

本邦コンサルタントの指示のもと、作業計画遂行のための現地活動を統括し、継続的に計画に関 与する。本邦コンサルタントの不在時は、逐次活動の進捗状況確認を行なう。また、本邦コンサル タントが現地滞在中は、関係機関との調整を行ない、活動を補佐する。

- 住民による水管理組織の立ち上げ支援
- 各サイトでの住民集会開催における運営業務
- 各サイトでの運営・維持管理の状況確認と本邦コンサルタントへの報告
- EWTEC 講師による運営・施設維持管理にかかる技術研修(ハード面)調整
- 水管理組織の運営・維持管理に対する連携支援と定期監査
- 関係者によるモニタリング採集
- 邦人不在時における各関係機関との業務調整

EWTEC 講師

水管理組織職員及び Woreda 職員に対して、水道施設の運営・維持管理にかかる技術訓練(ハード面)を実施する。

- 新設水道施設に関する基礎知識の伝授
- 日常の点検方法
- 故障時の対応(軽微な故障の修理方法及び重度な故障の対応方法)
- スペアパーツの購入方法
- 施設の利用ルール
- 施設の清掃
- 3)活動計画

具体的な活動内容は、以下のとおりである。

<実施体制の確立(フェーズ1)>

活動 1-1: AWRDB 及び Woreda の水管理組織への支援体制を整える

プロジェクト開始に伴い、実施機関である AWRDB において、プロジェクトの目的、必要性、内 容、実施計画にかかる協議を行なう。その後、水管理組織による運営・維持管理を後方支援する Woreda の職員を対象に、既存の水道施設の使用状況、運営・維持管理にかかる現状把握及び住民主 体の運営・維持管理の必要性・重要性を理解するためワークショップを実施する。Woreda 職員はこ のワークショップを通じ、今後各サイトの水管理組織の職員及び住民を啓蒙指導するための住民参 加型手法を習得する。 邦人コンサルタントは、各 Woreda 職員に対するヒアリングにおいて、これまでの水管理組織との関わり方や問題点を明らかにしたうえで、支援体制の組織図を作成する。さらに Woreda 職員と 共に、活動 1-2 で選出される水管理組織の職員構成、役割、人選の方法、資金繰りを含めた運営体 制及び利用規約について具体案を捻出する。

対象者:	AWRDB 職員、Woreda 職員
投入:	邦人コンサルタント(10日)、車両(本邦コンサル及び先方機関投入)
成果品:	支援体制組織図、利用規約

活動 1-2:水管理組織の運営・維持管理体制を整備する

水道施設が整備される9サイトにおいて、既存の水管理組織を対象として、その在り方と問題点 を明らかにするためのワークショップを開催する。その結果を踏まえ、Woreda 職員主導の下で、今 後の運営・維持管理活動に適切と思われる職員構成、役割、人選方法を提示し、現職員の理解を得 る。

また、運営・維持管理の実施に際して水管理組織と住民との関わり方を再考し、次の住民集会での協議に先立ち、各水管理組織の連携による無理のない計画案を策定する。とりわけ、組織職員の 給与や運営資金、それらを捻出するための適切な水料金の設定と徴収方法に関しては、活動 1-3 で 行なわれる住民集会において提示できるよう本段階で策定する。

対象者:	水管理組織職員
投入:	邦人コンサルタント(9日)、Woreda 職員(9日)、車両
成果品:	水管理組織・組織図、運営・維持管理計画書案

活動 1-3:運営・維持管理体制に関する理解を得る

各サイトを統括する Woreda 職員により、運営・維持管理にかかる概略説明を行なった後、活動 1-1、1-2 で得られた成果をもとに、住民を対象にしたワークショップを開催する。ワークショップ では、安全な水の継続的確保のための水道施設の周囲環境整備、利用規約に従った施設の運営・維 持管理における住民参加の重要性、とりわけ水道施設の運営資金確保のための水料金徴収の必要性 に関して住民からの理解を得る。水管理組織職員は、活動 1-2 で策定された水管理組織による運営・ 維持管理計画案を住民に提示し、今後の連携と協力を求める。

対象者:	住民、村評議会
投入:	邦人コンサルタント(9日)、Woreda 職員(9日)、水管理組織職員(9日)、車両

<運営・維持管理技術の習得(フェーズ 2)>

活動 2-1:水道施設の点検、修理等にかかる技術訓練(ハード面)を実施する

Woreda 水事務所及び水管理組織の施設管理担当者に対し、EWTEC 講師による水道施設の運営・ 維持管理にかかる基礎知識と日常点検方法、故障時の対応、軽微な故障への修理技術の習得のため の技術訓練(ハード面)を、OJT 方式で実施する。プロジェクトの対象となる9サイトのうち、3 サイトが竣工した時点で第一回目の訓練を行う。引き続き3サイトが竣工する度に第二回目、第三 回目の訓練を実施する。訓練終了後においても、各担当者が習得した維持管理技術や知識を継続的 に実践できるよう、本邦コンサルタントは故障時修理マニュアル及び運転記録簿を作成し関係者に 配布する。

対象者:	Woreda 職員、水管理組織職員
投入:	EWTEC 講師(21 日×2 人)、邦人コンサルタント(15 日)、車両
成果品:	故障時修理マニュアル、活動記録簿、施設運転記録簿、技術訓練報告書

活動 2-2:会計、記録等のアドミニストレーションにかかる技術指導(ソフト面)を実施する

Woreda 及び水管理組織の職員、会計担当者に対し、施設の運営・維持管理におけるソフト面での 技術習得のため、本邦コンサルタント主導による OJT 研修を実施する。

本活動では、水使用料金の設定・徴収・管理方法のみに拘わらず、施設運営経費、職員の報酬、 修理に伴う部品代や修理費用の算出方法等の経理にかかる技能に加え、施設運転・稼動状況の記録 作成方法等のアドミニストレーションに関する技能訓練を実施する。

本活動は、本体工事の各工区竣工後の活動 2-1 の訓練の後に引き続いて行なわれる。また、活動 2-1 と同様、アドミニストレーションにかかるマニュアル、料金徴収出納帳は、邦人コンサルタン トが事前に作成し、変更があれば追記修正を行ない関係者に配布する。

対象者:	Woreda 職員、水管理組織職員
投入:	邦人コンサルタント(12日)、車両
成果品:	維持管理マニュアル、料金徴収出納帳、施設利用登録簿

活動 2-3:活動のモニタリング・評価を実施し、計画の修正を行なう

施設の運営・維持管理及びアドミニストレーションにかかる技術訓練の成果が活動に適切に反映 しているか否か、各関係者によるモニタリング・評価を実施する。邦人コンサルタントは、その結 果を次の工区の活動に生かすため、関係者に対する指導を行なう。

また、本プロジェクト終了後も、関係者自らが継続してモニタリング・評価を実施し、逐次運営・ 維持管理計画の修正を行なう。

対象者:	Woreda 職員、水管理組織職員、住民
投入:	邦人コンサルタント(10日)、水管理組織職員及び Woreda 職員(9日)、車両
成果品:	モニタリング計画書、モニタリング評価記録

活動	実施内容	形態	対象者(受講者)	実施主体者(投入者)=投入
	1.1 AWRDB 及び Woreda の水	協議	AWRDB 職員	邦人コンサルタント
中	管理組織への支援体制を	ワークショップ	Woreda 職員	
施	整える			
体	1.2 水管理組織の運営・維持	ワークショップ	水管理組織職員	邦人コンサルタント
前の	管理体制を整備する			Woreda 職員
実施体制の確立	1.3 運営・維持管理体制に関	住民集会	住民、村評議会	Woreda 職員
<u> </u>	する理解を得る	OJT		水管理組織職員
				邦人コンサルタント
谉	2.1 水道施設の点検、修理等	セミナー	Woreda 職員	EWTEC 講師
運 営	にかかる技術訓練(ハード	OJT	水管理組織職員	邦人コンサルタント
維	面)を実施する			
維持管理技術	2.2 会計、記録等のアドミニスト	セミナー	Woreda 職員	邦人コンサルタント
理	レーションにかかる技術指	OJT	水管理組織職員	
技	導(ソフト面)を実施する			
何の	2.3 活動のモニタリング・評価	モニタリング	Woreda 職員	邦人コンサルタント
の習得	を実施し、計画の修正を行	評価	水管理組織職員	
行	なう			

活動計画

(6) ソフトコンポーネントの実施リソースの調達方法

本ソフトコンポーネントは、本邦コンサルタントによる直接支援型とするが、投入計画における 水道施設の機械操作や故障時の対応、軽微な修繕等のハード面での技術移転に関しては、EWTEC と連携し、OJT 方式を用いて実施する。

(7) ソフトコンポーネントの実施工程

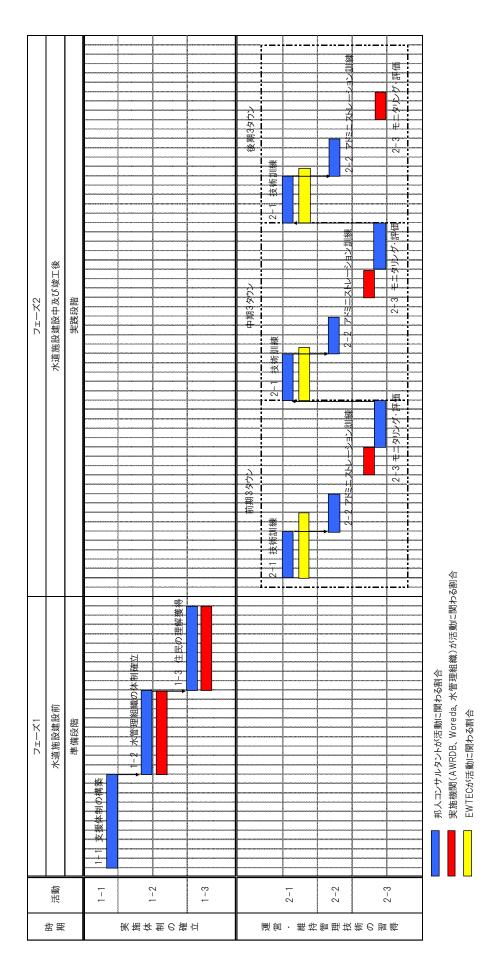
1) 実施内容

運営・維持管理にかかるソフトコンポーネントの実施計画概念及び必要作業日数の算出根拠は、 以下のとおりである。

ソフトコンポーネントは、フェーズ1(建設前:28日間)とフェーズ2(建設中~建設後:37日間)の2フェーズ体制とする。邦人コンサルタントの活動期間は、計65日を想定している。

邦人コンサルタントが現地で活動している期間は、水管理組織及び Woreda 職員が投入あるいは 享受によって活動に参加するため、邦人に対し常にローカルスタッフが同行することになる。

EWTEC による技術支援は、各工区 5 日間ずつとし、邦人コンサルタントはマニュアル作成のため訓練の全期間同行する。邦人コンサルタントの不在時に実施されるモニタリング・評価に関しては、Woreda 職員主導のもとで関係者により実施される。





	╞					実作業日数		移動	移動日数	合計	+
/		活動No.	活動內容	対象者	投入者	邦人(1人)	現地 (EWTEC:2人)	邦人(1人)	現地 (EWTEC:2人)	邦人(1人)	現地 (EWTEC:2人)
	平	1-1	AWRDB及びWoredaの水管理組織への支援体 制を整える	AWRDB職員 Woreda職員	邦人コンサルタント	10					
l%−ı	野の峙本	1-2	水管理組織の運営・維持管理体制を整備する	水管理組織職員	邦 人コンサルタント Woreda職員	o		4		32	
۲.	谢戴実	1-3	運営・維持管理体制に関する理解を得る	住民 村評議会	邦人コンサルタント Woreda職員 水管理組織職員	თ					
		2-1	水道施設の点検修理等にかかる技術訓練 (ハード面)を実施する		邦人コンサルタント EWTEC講師	م	5		2 2		14
		55 5-2	会計、記録等のアドミニストレーションにかかる技 術指導(ソフト面)を実施する	W oreda職員 水管理組織職員	ייע ייד יי ר ע≠	4		4		18	
		着	活動のモニタリング・評価を実施し、計画の修正 を行なう		オントリンシント	a					
ō	∮图(0)滑	2-1	水道施設の点検修理等にかかる技術訓練 (ハード面)を実施する		邦人コンサルタント EWTEC講師	5	5 5		2 2		14
ζχ—τι		55 万-5	会計、記録等のアドミニストレーションにかかる技 術指導(ソフト面)を実施する	Woreda職員 水管理組織職員	Υ.Υ. = ΤΙ.	4		4		18	
-		# 2-3	活動のモニタリング・評価を実施し、計画の修正 を行なう		おくよくりどうと	5					
		2-1	水道施設の点検修理等にかかる技術訓練 (ハード面)を実施する		邦人コンサルタント EWTEC講師	م	5	-	2 2	c .	14
		52 5-3	会計、記録等のアドミニストレーションにかかる技 術指導(ソフト面)を実施する	Woreda職員 水管理組織職員	邦 人コンサルタント	4		t		2	
		港 2-3	活動のモニタリング・評価を実施し、計画の修正 を行なう		Woreda職員						
						65	30	16	12	81	42

必要作業日数の算出根拠

2) 邦人コンサルタントの派遣期間及び回数の妥当性検討

運営・維持管理活動は、合計4回の本邦コンサルタントによる現地作業からなる。活動は実施内 容及び時期から、水道施設建設前に実施するフェーズ1(実施体制の確立)及び水道施設建設中及 び竣工後に実施するフェーズ2(運営・維持管理技術の習得)に区分される。

実施機関を対象とする活動は、邦人コンサルタントが100%関与する。

フェーズ1では関係者による合意形成が重要となるため、段階毎に邦人コンサルタントが確認す る必要がある。同様にフェーズ2においても、研修にかかる調整及びマニュアル、記録簿等の資料 作成業務のため、期間中の滞在が必須となる。

したがって、邦人コンサルタントの派遣期間及び回数は、妥当と判断する。

(8) ソフトコンポーネントの成果品

本ソフトコンポーネントにおける成果品は、以下のとおりである。

- 支援体制組織図(活動 1-1)
- 利用規約(活動 1-1)
- 水管理組織・組織図(活動 1-2)
- 運営・維持管理活動計画書(活動 1-2)
- 故障時修理マニュアル(活動 2-1)
- 活動記録簿(活動 2-1)
- 施設運転記録簿(活動 2-1)
- 技術訓練報告書(活動 2-1)
- 維持管理マニュアル(活動 2-2)
- 料金徴収出納帳(活動 2-2)
- 施設利用登録簿(活動 2-2)
- モニタリング計画書、評価記録(活動 2-3)
- ソフトコンポーネント実施状況報告書(邦人コンサルタント派遣毎)
- 完了報告書(終了時、相手国政府、日本側に対して)

(9) 相手国側の責務

実施機関(AWRDB 及び Woreda 水事務所)の分担事項は、以下のとおりである。

- 本邦コンサルタントとの提携によるプログラム全体の管理
- 各上層機関への報告
- プログラム実施にかかる他部署への協力要請
- 関係機関職員の提供及び現地活動費用、移動交通費、日当宿泊費等の経費負担
- EWTEC 講師による技術研修にかかる調整業務
- 合同協議会、ワークショップ開催にかかる会場準備、運営費用の負担

資料 6. 参考資料 6-1 収集資料リスト

番号	名称	形態(地図	1、報告書)	オリジナル・ コピー	発行機関	発行年
1	Hydrogeological Map of Northern Ethiopia, S=1/1,000,000	水理地質図	図面/ 電子ファイル	コピー	GSE	2002
2	Regional Hydrogeological Investigation of Northern Ethiopia	同解説書	電子ファイル	コピー	GSE	2003
3	Geological Map of the Bahir Dar Area (NC37-1), S=1/250,000	地質図	図面/ 電子ファイル	⊐ピ –	GSE	2010
4	Geology Geochemistry and Gravity Survey of the Bahir Dar Area	同解説書	電子ファイル	コピー	GSE	2010
5	Geological Map of the Debre Tabor Area (NC37-2), S=1/250,000	地質図	図面/ 電子ファイル	コピー	GSE	2010
6	Geology Geochemistry and Gravity Survey of the Debre Tabor Area	同解説書	電子ファイル	コピー	GSE	2010
7	Geological Map of the Bure (NC37-5), S=1/250,000	地質図	図面/ 電子ファイル	コピー	GSE	2007
8	Geology of Bure map Sheet (NC37-5)	同解説書	電子ファイル	コピー	GSE	2007
9	Geological Map of Debre Marcos Sheet (NC37-6), S=1/250,000	地質図	図面/ 電子ファイル	コピー	GSE	2009
10	Topografhic Map, S=1/250,000, EMA3, NC37-1, Bahir Dar	地形図	図面	コピー	EMA	1996
11	Topografhic Map, S=1/250,000, 1502, NC37-2, Debre Tabor	地形図	図面	コピー	EMA	1972
12	Topografhic Map, S=1/250,000, EMA3, NC37-5, Bure	地形図	図面	コピー	EMA	1995
13	Topografhic Map, S=1/250,000, EMA3, NC37-6, Debre Mark'os	地形図	図面	コピー	EMA	1995
14	Topografhic Map, S=1/50,000, ETH4, , Debre Mark'os	地形図	図面	コピー	EMA	1995
15	Topographic Map S=1/50,000, ETH 4 1037 A2 DABI (Gebez Maryam)	地形図	図面	コピー	EMA	1987
16	Topographic Map S=1/50,000, ETH 4 1037 A3 BURE (Mankusa, Kuchie)	地形図	図面	コピー	EMA	1987
17	Topographic Map S=1/50,000, ETH 4 1037 B2 KERANIYO (Keranyo, Sedie)	地形図	図面	コピー	EMA	1984
18	Topographic Map S=1/50,000, ETH 4 1037 C1 KUCH (Kuchie)	地形図	図面	コピー	EMA	1987
19	Topographic Map S=1/50,000, ETH 4 1037 D2 AMBER (Amberi, Lumamie)	地形図	図面	コピー	EMA	1984
20	Topographic Map S=1/50,000, ETH 4 1037 D4 LUMAME (Amberi, Lumamie)	地形図	図面	コピー	EMA	1984
21	Topographic Map S=1/50,000, ETH 4 1038 A2 MERTO LEMARYAM (Mertle Maryam, Dibo)	地形図	図面	コピー	EMA	1998
22	Topographic Map S=1/50,000, ETH 4 1038 C1 BICHENA (Bichena, Yetimen)	地形図	図面	コピー	EMA	1984
23	Topographic Map S=1/50,000, ETH 4 1038 C3 DEJEN (Wejele)	地形図	図面	コピー	EMA	1984
24	Topographic Map S=1/50,000, ETH 4 1137 A1 KUNZLA (Kunzila)	地形図	図面	コピー	EMA	1987
25	Topographic Map S=1/50,000, ETH 4 1137 C1 MER AWI (Mer-Awi)	地形図	図面	コピー	EMA	1987
26	Topographic Map S=1/50,000, ETH 4 1137 C4 ADAMA TERARA (Gebez Maryam)	地形図	図面	コピー	EMA	1987
27	Topographic Map S=1/50,000, ETH 4 1137 D3 GONJ (Gonji Kollela)	地形図	図面	コピー	EMA	1984

GSE:Geological Survey of Ethiopia EMA:Ethiopian Mapping Agency

資料7. その他の資料・情報 7-1 水理計算書

Hydraulic Calculation

1. Mertule Maryam

1.1. Basal Condition

Since the checked quantity of water intake is 424.01m3/day, and it is less than maximum daily supply and average daily supply, water facilities of Mertule Maryam are planed by total quantity of water intake.

1.2. Water Intake

There are two existing water sources in Mertule Maryam, both of two water sources are spring. One is transmitted to reservoir by gravity flow (139.35m3/day), and another is transmitted to the collection chamber by gravity flow (91.96m3/day) and then pumped up to reservoir.

The volume of existing collection chamber is 28.65m3 and another 28.83m3 of new collection chamber is designed, so totally 57.48m3 of volume of collection chambers are secured. Total volume of collection chamber is calculated 15 hours of volume of water intake (i.e. $91.96m3 \times 15$ hours / 24 hours = 57.48m3).

It was confirmed that another three springs are existing in Mertule Maryam. One is 42.59m3/day of volume, second one is 92.70m3/day and third one is 57.41m3/day. These three springs are transmitted by gravity flow, so at the end of this project, total 424.01m3/day of volume of water intake is secured.

The specification of pump at collection chamber is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from collection chamber to reservoir tank is 40m and flow volume is 3.19L/sec (91.96m3/day / 8 hours), so it is needed 3.7kw of capacity of pump.

1.3. Transmission Line

The specification of transmission lines is calculated by the conditions of each water intake. Diameter is decided by the calculation with Hazen-Williams formula. Each distance of each water intake to reservoir tank is from 440m to 3015m. Diameters of transmission line are almost 3", only one transmission line's diameter is 1"1/2.

1.4. Reservoir Tank

There are three existing reservoir tanks in Mertule Maryam. The volume is, first: 82.98m3, second: 50.36m3, third: 50.36m3. All the three reservoir tanks are not leaking water and it is useful, it is planed the new reservoir tank as additional. Required total capacity of reservoir tanks is 212.01m3, so short capacity is 28.31m3, it is planed 30m3 of reservoir tank by reinforced concrete.

1.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Mertule Maryam, but some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

1.6. Water Faucet

2. Yetimen

2.1. Basal Condition

In Yetimen, average daily supply is 102.98m3/day, maximum daily supply is 123.58m3/day and checked quantity of water intake is 250.56m3/day. Quantity of water intake is sufficient, so water facilities of Yetimen are planed by average and maximum daily supply.

2.2. Water Intake

There is one existing borehole as water sources in Yetimen, but new borehole was drilled and there is no problem about quality and quantity of that borehole, it is planed to use new borehole for this project.

From the borehole to reservoir tank, the water is pumped up, the specification of pump at borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from borehole to reservoir tank is 70m and flow volume is 4.29L/sec (123.58m3/day / 8 hours), so it is needed 5.5kw of capacity of pump.

2.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Distance from borehole to reservoir tank is 1250m. Diameter of transmission line is 3".

2.4. Reservoir Tank

There is an existing reservoir tank in Yetimen. The volume of reservoir tank is 60m3. Existing reservoir tank is now leaking, there is a option only to repair the existing reservoir tank, but preventing water leakage can not be guaranteed for the future because of the technical difficulty, new reservoir tank is planed in Yetimen.

Required capacity of reservoir tank is 64.36m3, so it is planed 70m3 of reservoir tank by reinforced concrete.

2.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Yetimen, but some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

2.6. Water Faucet

3. Lumame

3.1. Basal Condition

In Lumame, average daily supply is 342.64m3/day, maximum daily supply is 411.17m3/day and checked quantity of water intake is 399.17m3/day. Quantity of water intake is enough for average daily supply, so water facilities of Lumame are planed by average daily supply and quantity of water intake.

3.2. Water Intake

There are two existing boreholes as water sources in Lumame, but total quantity of those two boreholes is not enough for new water facilities (first: 57.60m3/day, second: 86.40m3/day, total: 144.00m3/day), so new borehole was drilled and it was confirmed the quantity of new borehole is 255.17m3/day. It is not enough for maximum daily supply but satisfied average daily supply, so it is planed to use all of three boreholes for this project.

From each borehole to reservoir tank, the water is pumped up, the specification of pump at borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Each total head from borehole to reservoir tank is 90m (first), 100m (second) and 110m (third). Flow volume is 2.00L/sec (57.60m3/day / 8 hours), 3.00L/sec (86.40m3/day / 8 hours) and 8.86L/sec (255.17m3/day / 8 hours), so each borehole need 5.5kw, 5.5kw and 15kw of capacity of pump.

3.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Existing transmission lines of existing two boreholes are combined on the line to reservoir tank. So, existing pumps do not function at the same time because of interfering with each other. It is planed to replace new transmission lines independently for existing transmission lines, and also planed to set new transmission line for new borehole.

Distance and diameter of each transmission line is 1927.22m (first: existing, 3"), 1475.14m (second: existing, 3"), 1208.09m (third: new, 4").

3.4. Reservoir Tank

There is an existing reservoir tank (elevated tank) in Lumame. The volume of existing reservoir tank is 50m3. Existing reservoir tank is functioning and new reservoir tank is planed to satisfy the total capacity of reservoir tank.

Required capacity of reservoir tank is 121.30m3, so it is planed 123m3 of reservoir tank by elevated type.

3.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Lumame, but some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

3.6. Water Faucet

4. Wojel

4.1. Basal Condition

In Wojel, average daily supply is 101.02m3/day, maximum daily supply is 121.22m3/day and checked quantity of water intake is 224.64m3/day. Quantity of water intake is sufficient, so water facilities of Wojel are planed by average and maximum daily supply.

4.2. Water Intake

There is one existing borehole as water sources in Wojel, but that borehole was abandoned and new borehole was drilled. There is no problem about quality and quantity of new borehole, it is planed to use new borehole for this project.

From the new borehole to reservoir tank, the water is pumped up, the specification of pump at borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from borehole to reservoir tank is 90m and flow volume is 4.21L/sec (121.22m3/day / 8 hours), so it is needed 7.5kw of capacity of pump.

4.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter of transmission line is decided by the calculation with Hazen-Williams formula. Distance from borehole to reservoir tank is 1000m. Diameter of transmission line is 3".

4.4. Reservoir Tank

There is an existing reservoir tank in Wojel. The volume of existing reservoir tank is 60m3 but that reservoir tank was deserted, so new reservoir tank is planed in Wojel.

Required capacity of reservoir tank is 63.14m3, so it is planed 70m3 of reservoir tank by reinforced concrete.

4.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Lumame, but every water facilities ware abandoned in wojel and it is difficult to confirm the condition of existing distribution line, so new distribution line is planed.

4.6. Water Faucet

5. Sedie

5.1. Basal Condition

In Sedie, average daily supply is 106.66m3/day, maximum daily supply is 127.99m3/day and checked quantity of water intake is 256.32m3/day. Quantity of water intake is sufficient, so water facilities of Yetimen are planed by average and maximum daily supply.

5.2. Water Intake

There is one existing borehole as water sources in Sedie, but new borehole was drilled and there is no problem about quality and quantity of that borehole, it is planed to use new borehole for this project.

From the borehole to reservoir tank, the water is pumped up, the specification of pump at borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from borehole to reservoir tank is 110m and flow volume is 4.44L/sec (127.99m3/day / 8 hours), so it is needed 7.5kw of capacity of pump.

5.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Distance from borehole to reservoir tank is 1455m. Diameter of transmission line is 3".

5.4. Reservoir Tank

There is an existing reservoir tank in Sedie. The volume of existing reservoir tank is 60m3. Existing reservoir tank is located low elevation, so new reservoir tank is planed in Sedie.

Required capacity of reservoir tank is 66.66m3, so it is planed 70m3 of reservoir tank by reinforced concrete.

5.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Sedie, but some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

5.6. Water Faucet

6. Dibo

6.1. Basal Condition

In Dibo, average daily supply is 74.35m3/day, maximum daily supply is 89.22m3/day and checked quantity of water intake is 256.32m3/day. Quantity of water intake is sufficient, so water facilities of Dibo are planed by average and maximum daily supply.

6.2. Water Intake

There is no existing borehole and any other water facility in Dibo except hand pump, so new borehole was drilled and there is no problem about quality and quantity of that borehole, it is planed to use new borehole for this project.

From the borehole to reservoir tank, the water is pumped up, the specification of pump at borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from borehole to reservoir tank is 90m and flow volume is 3.10L/sec (89.22m3/day / 8 hours), so it is needed 5.5kw of capacity of pump.

6.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Distance from borehole to reservoir tank is 2070m. Diameter of transmission line is 3".

6.4. Reservoir Tank

There is no existing reservoir tank in Dibo. Required capacity of reservoir tank is 46.47m3, so it is planed 50m3 of reservoir tank by elevated type.

6.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now there are no distribution lines in Dibo, so every pipeline for distribution is set as new.

6.6. Water Faucet

7. Amanuel

7.1. Basal Condition

In Amanuel, average daily supply is 326.76m3/day, maximum daily supply is 392.11m3/day and checked quantity of water intake is 230.40m3/day. Quantity of water intake is not enough for average and maximum daily supply, so water facilities of Amanuel are planed by quantity of water intake.

7.2. Water Intake

There are two existing boreholes as water sources in Amanuel, but one of existing boreholes is abandoned and quantity of another existing borehole is not enough (144.00m3/day) for new water facilities, so new borehole was drilled and it was confirmed the quantity of new borehole is 86.40m3/day. Total amount of water intake is not enough for average and maximum daily supply but it was not found another water intake as drilling, so it is planed to use two boreholes (existing and new) for this project.

From each borehole to reservoir tank, the water is pumped up, existing borehole and pump is functioning well, so at this project, only the pump for new borehole is set. The specification of pump at new borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from new borehole to reservoir tank is 100m. Flow volume is 3.00L/sec (86.40m3/day / 8 hours), so new borehole needs 5.5kw of capacity of pump.

7.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Existing transmission line is functioning, so only new transmission line from new borehole to reservoir tank.

Distance and diameter of new transmission line is 2386m. Diameter of transmission line is 3".

7.4. Reservoir Tank

There is two existing reservoir tanks (elevated tank) in Amanuel. Although the volume of existing reservoir tanks are 60m3 and 30m3, both reservoir tanks are leaking. So it is planed to construct new reservoir tank, required capacity of reservoir tank is 115.2m3, so it is planed 120m3 of reservoir tank by elevated type.

7.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Amanuel, but some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

7.6. Water Faucet

8. Gobeze Maryam

8.1. Basal Condition

Since the checked quantity of water intake is 164.00m3/day as a spring, and it is less than maximum daily supply and average daily supply, water facilities of Gobeze Maryam are planed by total quantity of water intake.

8.2. Water Intake

There is a existing water source in Gobeze Maryam as spring. The water is transmitted to the collection chamber by gravity flow and then pumped up to reservoir.

The volume of existing collection chamber is 19.87m3 and another 82.63m3 of new collection chamber is designed, so totally 102.50m3 of volume of collection chambers are secured. Total volume of collection chamber is calculated 15 hours of volume of water intake (i.e. $164.00m3 \times 15$ hours / 24 hours = 102.50m3).

The specification of pump at collection chamber is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from collection chamber to reservoir tank is 100m and flow volume is 5.69L/sec (164.00m3/day / 8 hours), so it is needed 11kw of capacity of pump.

8.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Distance from water intake to reservoir tank is 1300m. Diameters of transmission line are 3".

8.4. Reservoir Tank

There is a existing reservoir tank in Gobeze Maryam. The volume of existing reservoir tank is 50m3. But elevation of existing reservoir tank is not enough to distribute high area, existing reservoir tank will be abandoned and new reservoir tank is planed instead. Required capacity of reservoir tank is 102.50m3, so it is planed 105m3 of reservoir tank by reinforced concrete.

8.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Gobeze Maryam, but some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

8.6. Water Faucet

9. Bikolo

9.1. Basal Condition

In Bikolo, average daily supply is 151.19m3/day, maximum daily supply is 181.43m3/day and checked quantity of water intake is 403.20m3/day. Quantity of water intake is sufficient, so water facilities of Bikolo are planed by average and maximum daily supply.

9.2. Water Intake

There is one existing borehole as water sources in Bikolo, but new borehole was drilled and there is no problem about quality and quantity of that borehole, it is planed to use new borehole for this project.

From the borehole to reservoir tank, the water is pumped up, the specification of pump at borehole is calculated by 9 hours running per day (4 hours in the morning, 4 hours in the afternoon and 1 hour recess). Total head from borehole to reservoir tank is 110m and flow volume is 6.30L/sec (181.43m3/day / 8 hours), so it is needed 11kw of capacity of pump.

9.3. Transmission Line

The specification of transmission lines is calculated by the conditions of water intake. Diameter is decided by the calculation with Hazen-Williams formula. Distance from water intake to reservoir tank is 5533m. Diameters of transmission line are 4".

9.4. Reservoir Tank

There is an existing reservoir tank in Bikolo. The volume of existing reservoir tank is only 25m3. Moreover, the location of existing reservoir tank is centering of Bikolo town, water pressure for distribution is not enough. That is why existing reservoir tank will be abandoned and new reservoir tank is planed instead at high area of Bikolo town. Required capacity of reservoir tank is 94.49m3, so it is planed 105m3 of reservoir tank by reinforced concrete.

9.5. Distribution Line

Distribution lines are calculated by Hazen-Williams formula with peak hourly supply. Now distribution lines are already set in Bikolo, but new reservoir tank is designed to construct at high area, it is needed to extend the distribution line. And some lines are not in the ground, those lines crop out. So basically lines are replaced by the necessity of changing diameter, but also are changed at the lines that pipes are cropping out.

9.6. Water Faucet

Hydrologic Calculation

1. Basic Number

No.	Towns	Zone	Woreda	Existing Population 2012	Projection of pop. 2016	School number of students	Hospital, Clinic
9	Mertule Maryam	East Gojam	Enebsie Sar Midir	15,124	17,829	7,180	10
10	Yetimen	East Gojam	Enemay	3,289	3,877	2,346	11
12	Lumame	East Gojam	Awabel	11,410	13,451	5,735	10
14	Wojel	East Gojam	Awabel	3,188	3,758	2,486	10
15	Sedie	East Gojam	Hulet Egu Enesie	3,348	3,947	2,712	10
16	Dibo	East Gojam	Enebsie Sar Midir	2,129	2,510	2,839	10
	Amanuel	East Gojam	Machakel	10,768	12,694	6,002	10
27	Gobeze Maryam	West Gojam	Quarit	5,860	6,908	4,938	10
	Bikolo(Wetet Abay)	West Gojam	Mecha	4,929	5,811	3,000	10
	Tota	al		60,045	70,785	37,238	91

---- Annual Growth Rate of Population ----Growth Rate : 4.2 %

--- Number of students and beds ---It is based on the result of field study.

2. Water Demand

3. Volume of Water Intake

(AD : :	2012)								Jnit:m3/day	
No.	Towns	Dai General 20 l/c/day	School	emand(m3/d Hospital, Clinic 25 I/c/day	lay) Total	Ineffective water 15 %	Average Daily Supply	Maximum Daily Supply factor : 1.2	Peak Hourly Supply factor : 2.0	
9	Mertule Maryam	302.48	35.90	0.25	338.63	50.79	389.42	467.30	778.84	Unit of Water Demand :
10	Yetimen	65.78	11.73	0.28	77.79	11.67	89.46	107.35	178.92	
12	Lumame	228.20	28.68	0.25	257.13	38.57	295.70	354.84	591.40	
14	Wojel	63.76	12.43	0.25	76.44	11.47	87.91	105.49	175.82	
15	Sedie	66.96	13.56	0.25	80.77	12.12	92.89	111.47	185.78	Ineffective Water :
16	Dibo	42.58	14.20	0.25	57.03	8.55	65.58	78.70	131.16	
	Amanuel	215.36	30.01	0.25	245.62	36.84	282.46	338.95	564.92	Factor of Water Supply :
27	Gobeze Maryam	117.20	24.69	0.25	142.14	21.32	163.46	196.15	326.92	
	Bikolo(Wetet Abay)	98.58	15.00	0.25	113.83	17.07	130.90	157.08	261.80	
	Total	1,200.90	186.20	2.28	1,389.38	208.40	1,597.78	1,917.33	3,195.56	
(AD :	2016)							ι	Jnit∶m3⁄day	
		Dai	ily Water De	emand(m3/o	lay)	Ineffective	Average	Maximum Dailv	Peak Hourly	
No.	Towns	General	School	Hospital, Clinic Total		water	Daily	Supply Supply		
		20 l/c/day	5 l/c/day	25 l/c/day	Total	15 %	Supply		factor : 2.0	
9	Mertule Maryam	356.58	35.90	0.25	392.73	58.91	451.64	541.97	903.28	
10	Yetimen	77.54	11.73	0.28	89.55	13.43	102.98	123.58	205.96	
12	Lumame	269.02	28.68	0.25	297.95	44.69	342.64	411.17	685.28	
14	Wojel	75.16	12.43	0.25	87.84	13.18	101.02	121.22	202.04	
15	Sedie	78.94	13.56	0.25	92.75	13.91	106.66	127.99	213.32	
16	Dibo	50.20	14.20	0.25	64.65	9.70	74.35	89.22	148.70	
	Amanuel	253.88	30.01	0.25	284.14	42.62	326.76	392.11	653.52	
27	Gobeze Maryam	138.16	24.69	0.25	163.10	24.47	187.57	225.08	375.14	
	Bikolo(Wetet Abay)	116.22	15.00	0.25	131.47	19.72	151.19	181.43	302.38	
	Total	1,415.70	186.20	2.28	1,604.18	240.63	1,844.81	2,213.77	3,689.62	

- 20 I/c/day (Average Daily Demand)
 - l/c/day (School)
- 5 25 l/c/day (Hospital)

15 %

1.2 (Maximum Daily Supply)

Unit:m3/day

2.0 (Peak Hourly Supply)

		Maximum Daily	Volume of	Water Intak	(Existing)	Volume o	of Water Int	ake(New)	Volume o	of Water Int	ake(Total)	Design		
No.	Towns	Supply m3/day	Borehole	Spring	Total	Borehole	Spring	Total	Borehole	Spring	Total	Water Intake	Water Coverage	Remarks
			0.00	139.35	139.35	0.00	0.00	0.00						Existing use
			0.00	91.96	91.96	0.00	0.00	0.00						Existing use
9	Mertule Maryam	541.97	0.00	0.00	0.00	0.00	42.59	42.59	0.00	424.01	424.01	424.01	78.23%	New
			0.00	0.00	0.00	0.00	92.70	92.70						New
			0.00	0.00	0.00	0.00	57.41	57.41						New
10	Yetimen	123.58	0.00	0.00	0.00	0.00	0.00	0.00	250.56	0.00	250.56	123.58	100.00%	Abolishment
10	reamen	120.00	0.00	0.00	0.00	250.56	0.00	250.56	200.00	0.00	200.00	120.00	100.00%	New
			57.60	0.00	57.60	0.00	0.00	0.00						Existing use
12	Lumame	411.17	86.40	0.00	86.40	0.00	0.00	0.00	399.17	0.00	399.17	399.17	97.08%	Existing use
			0.00	0.00	0.00	255.17	0.00	255.17						New
14	Wojel	121.22	0.00	0.00	0.00	0.00	0.00	0.00	224.64	0.00	224.64	121.22	100.00%	Abolishment
	110,01	121.22	0.00	0.00	0.00	224.64	0.00	224.64	224.04	0.00	224.0	121.22	100.00%	New
15	Sedie	127.99	0.00	0.00	0.00	0.00	0.00	0.00	256.32	0.00	256.32	127.99	100.00%	Abolishment
		127.00	0.00	0.00	0.00	256.32	0.00	256.32	200.02	0.00	200.02	127.00	100.000	New
16	Dibo	89.22	0.00	0.00	0.00	256.32	0.00	256.32	256.32	0.00	256.32	89.22	100.00%	New
			144.00	0.00	144.00	0.00	0.00	0.00						Existing use
	Amanuel	392.11	0.00	0.00	0.00	0.00	0.00	0.00	230.40	0.00	230.40	230.40	58.76%	Abolishment
			0.00	0.00	0.00	86.40	0.00	86.40						New
27	Gobeze Maryam	225.08	0.00	164.00	164.00	0.00	0.00	0.00	0.00	164.00	164.00	164.00	72.86%	Existing use
	Bikolo(Wetet Abay)	181.43	0.00	0.00	0.00	0.00	0.00	0.00	403.20	0.00	403.20	181.43	100.00%	Abolishment
			0.00	0.00	0.00	403.20	0.00	403.20						New
	Total	2,213.77	288.00	395.31	683.31	1,732.61	192.70	1,925.31	2,020.61	588.01	2,608.62	1,861.02	84.07%	

4. Intake, Transmission Facilities

		Volume of V	Vater Intake	e(m3/day)		Elevat	ion(m)		Transmiss	ion Pipe, Inta	ake to the gr	und to Tank	Pump Plan(8h/day)			
No.	Towns	Spr Gravity	ing Pump	Borehole	Intake F Intake Point	acilities Ground	Tank	Vertical Drop	Length (m)	Diameter (mm)	Velocity (m/s)	Hydraulic Grade (‱)	Head loss (m)	Lifting Range (m)	Flow Volume (L/s)	Spec (kw)
		139.35	0.00	0.00	2,737.94	2,737.94	2,711.09	26.85	800.00	75	0.37	3.66	2.93			
		0.00	91.96	0.00	2,630.69	2,630.69	2,667.92	-37.23	440.00	75	0.72	1.70	0.75	40.00	3.19	3.7
9	Mertule Maryam	42.59	0.00	0.00	2,848.73	2,848.73	2,711.09	137.64	3,015.40	40	0.39	8.73	26.33			
		92.70	0.00	0.00	2,790.81	2,790.81	2,711.09	79.72	790.00	75	0.24	1.72	1.36			
		57.41	0.00	0.00	2,678.33	2,678.33	2,664.87	13.46	1,444.86	75	0.15	0.71	1.03			
10	Yetimen	0.00	0.00	123.58	2.382.83	2.405.63	2.445.78	-62.95	60.00	50	2.19	21.13	1.27	70.00	4.29	5.5
10	reamen	0.00	0.00	123.30	2,302.03	2,403.03	2,443.76	02.95	1,250.00	75	0.97	2.93	3.67	70.00	4.23	5.5
		0.00	0.00	57.60	2.418.84	2.464.13	2.505.77	-86.93	55.00	50	1.02	5.15	0.28	90.00	2.00	5.5
		0.00	0.00	57.00	2,410.04	2,404.13	2,303.77	80.93	1,927.22	75	0.45	0.71	1.38	50.00	2.00	5.5
12 Lu	Lumame	0.00	0.00	86.40	2.412.34	2.462.95	2.505.77	-93.43	55.00	50	1.53	10.90	0.60	100.00	3.00	5.5
		0.00	0.00	00.40	2,412.04	2,402.33	2,000.77	55.45	1,475.14	75	0.68	1.51	2.23	100.00	0.00	0.0
		0.00	0.00	255.17	2.407.00	2.424.95	2.505.77	5.77 -98.77	40.00	65	2.67	22.52	0.90	110.00	8.86	15.0
		0.00	0.00	255.17	2,407.00	2,424.55	2,303.77	50.77	1,208.09	100	1.13	2.76	3.34	110.00	0.00	13.0
14	Wojel	0.00	0.00	121.22	2.403.96	2.442.88	2.488.58	-84.62	55.00	50	2.14	20.39	1.12	90.00	4.21	7.5
14	110j01	0.00	0.00	121.22	2,400.00	2,442.00	2,400.00	04.02	1,000.00	75	0.95	2.83	2.83	50.00	7.21	7.5
15	Sedie	0.00	0.00	127.99	2.446.25	2.468.29	2.547.55	-101.30	60.00	50	2.26	22.55	1.35	110.00	4.44	7.5
10	oculo	0.00	0.00	127.55	2,440.23	2,400.29	2,347.33	101.30	1,455.27	75	1.01	3.13	4.56	110.00	4.44	7.5
16	Dibo	0.00	0.00	89.22	2.374.98	2.420.18	2.452.64	-77.66	55.00	50	1.58	11.57	0.64	90.00	3.10	5.5
10	0.00	0.00	0.00	03.22	2,074.00	2,420.10	2,452.04	77.00	2,071.06	75	0.70	1.61	3.33	50.00	0.10	0.0
		0.00	0.00	144.00	2.147.20	2.197.20	2.302.89	-155.69	100.00	50	2.55	28.05	2.80	170.00	5.00	13.0
		0.00	0.00	144.00	2,147.20	2,137.20	2,002.00	100.00	2,800.00	75	1.13	3.89	10.90	170.00	5.00	10.0
	Amanuel	0.00	0.00	144.00	2,302.89	2,302.89	2,397.78	-94.89	2,800.00		1.13	3.89	10.90	110.00	5.00	9.2
		0.00	0.00	86.40	2.306.14	2.336.49	2.397.78	-91.64	32.00	50	1.53	10.90	0.35	100.00	3.00	5.5
		0.00	0.00	00.40	2,000.14	2,000.40	2,007.70	51.04	2,386.25		0.68	1.51	3.61	100.00	0.00	0.0
27	Gobeze Maryam	0.00	164.00	0.00	2,156.40	2,156.40	2,243.37	-86.97	1,304.06	75	1.29	4.95	6.46	100.00	5.69	11.0
	Bikolo(Wetet Abay)	0.00	0.00		1.855.63	1,905.63	1.953.02	-97.39	50.00	65	1.90	11.98	0.60	110.00	.00 6.30	0 11.0
		0.00	0.00	101.43	1,000.00	1,000.00	1,000.02	57.35	5,533.39	100	0.80	1.47	8.14	110.00	0.30	11.0
	Total	332.05	255.96	1,417.01												

5. Transmission Facilities (Relay Tank)

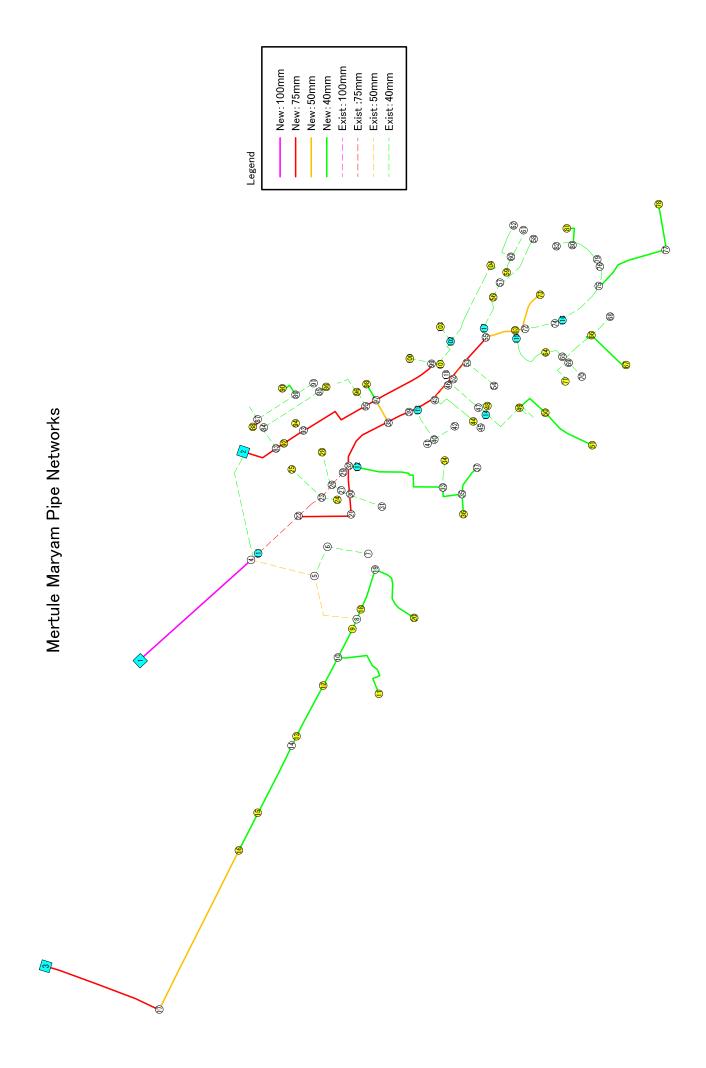
No.	Towns	Water Intake m3/day	Required Capacity of Tank (m3)	Vol. of Existing Tank (m3)	Additional capacity (m3)
9	Mertule Maryam	91.96	57.48	28.65	28.83
27	Gobeze Maryam	164.00	102.50	19.87	82.63

6. Distribution Facilities (Reservoir Tank)

		Average Dailv	Volume of Intake	Required		Existing	Existing	Short			Plan of Res	servoir Tank			
No.	Towns	Supply	Water	Reservo	irs (m3)	Reservoir	Use	Capacity	Width	Length	Net Depth	Number of	Volume	Category	Remarks
		(m3/day)	(m3/day)	12 hour	15 hour	(m3)	(m3)	(m3)	(m)	(m)	(m)	Tank	(m3)	Gategory	
						82.98	82.98		φ 6.20		2.75	1	82.98	RC	Existing use
9	Mertule Marvam	451.64	424.01	212.01		50.36	50.36	28.31	φ 5.40		2.20	1	50.36	Stone Masonry	Existing use
5	wertuie waryann	401.04	424.01	212.01		50.36	50.36	20.31	φ 5.40		2.20	1	50.36	Stone Masonry	Existing use
								-	3.00	4.00	2.50	1	30.00	RC	New
10	Yetimen	102.98	123.58		64.36	60.00	0.00	64.36						Stone Masonry	Abolishment
10	reamen	102.96	123.00		04.30		-	04.30	4.50	6.00	2.50	1	67.50	RC	New
12	Lumame	342.64	399.17	171.32		50.02	50.02	121.30	2.60	5.20	1.85	2	50.02	Elevated Tank	Existing use
12	Lumame	342.04	399.17	1/1.32				121.30	4.00	7.50	2.05	2	123.00	Elevated Tank	New
14	Wojel	101.02	121.22		63.14	60.00	0.00	63,14						Stone Masonry	Abolishment
14	wojei	101.02	121.22		03.14			03.14	4.50	6.00	2.50	1	67.50	RC	New
15	Sedie	106.66	127.99		66.66	60.00	0.00	66.66						Elevated Tank	Abolishment
15	Cedie	100.00	127.55		00.00			00.00	4.50	6.00	2.50	1	67.50	RC	New
16	Dibo	74.35	89.22		46.47	0.00	0.00	46.47	5.00	5.00	2.05	1	51.25	Elevated Tank	New
						60.00	0.00							Elevated Tank	Abolishment
	Amanuel	326.76	230.40	115.20		30.00	0.00	115.20						Elevated Tank	Abolishment
									4.00	7.50	2.05	2	123.00	Elevated Tank	New
27	Gobeze Maryam	187.57	164.00		102.50	50.00	0.00	102.50						Stone Masonry	Abolishment
21	CODEZE IVIALYAIII	107.07	104.00		102.50			102.50	3.00	7.00	2.50	2	105.00	RC	New
	Bikolo(Wetet Abav)	Bikolo(Wetet Abay) 151.19 181.43 94.49 25.0		25.00	0.00	94.49						Stone Masonry	Abolishment		
	bikolo(welet Abay)	131.19	101.43		94.49			94.49	3.00	7.00	2.50	2	105.00	RC	New
	Total	1,844.81	1,861.02	498.53	437.62	578.72	233.72	702.43					868.47		

7. Distribution Facilities (Pipeline)

Distribution pipelines of each site are determined by the hydraulic calculation.



			·							ط (ال	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $
·					,		·			围 但	$\begin{array}{c} 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. $
	、				ipe	Coefficient of Flow	f Flow Gradient	Ð		(%) I	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $
					Diameter Length of Pipe	Friction Coe Quantity of	Q .	Add Pressure		ү (ш/ s)	$\begin{array}{c} 0.000\\ 0.$
				•	<u>-</u>			E C		0 (1/s)	$\begin{array}{c} 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. $
	,					Pressur(Water				Coef C	
			Notes >>		Ground Level	ial Head Fr otion of Wa				」 目	$\begin{array}{c} 738. 592\\ 177. 672\\ 586. 845\\ 586. 845\\ 5532. 902\\ 5532. 902\\ 556. 867\\ 556. 867\\ 375. 927\\ 167. 427\\ 375. 927\\ 157. 427\\ 375. 927\\ 375. 927\\ 375. 927\\ 375. 927\\ 375. 927\\ 375. 927\\ 375. 927\\ 3858. 018\\ 375. 927\\ 375. 927\\ 3859. 018\\ 3858. 018\\ 3$
			Explanatory	н - -	Ground	El lec ti Consumi			LineData —	D (IIII)	100 750 750 750 750 750 750 750 750 750 7
		ļ	Expla	Node		с:: Сс:			- Line	Node	$\begin{array}{c} & & & & \\ & & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & & \\ & & & & \\ & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & &$
		 	\approx	I						ST	222298655433200988655547322
		Formula>>	(四)	(四)	(%)	(亚/ S)				Remarks	Reservoir Tank Reservoir Tank Protect Spring
		Hazen-Williams	69. 227	0.000	0.000	0.000				0c (1/s)	
			Maximum EHP	Minimum EHP	Maximum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0. & 000\\$
		ı ««Case.								EHP 1st (m)	
		Mertule Maryam	°3	109	113	6	0.00 (cm)	2 (times)	 	19	2, 611, 092 2, 667, 920 667, 920 678, 533 678, 548 678, 548 678, 548 678, 987 666, 099 667, 943 661, 574 661, 574 660, 943 660, 943 660, 943 660, 941 22, 660, 441 22, 660, 951 660, 951 22, 660, 951 22, 650, 905 674, 574 633, 156 777 756 757 757 756 757 75
· .		– – – – Me:	Tank	Node	Line	Pump, Decom	Convergence Gap	Calculation	NodeData	HF (a)	$\begin{array}{c} 2711. \ 092\\ 2667. \ 330\\ 26711. \ 092\\ 27711. \ 09$
		• •				3	Солvе	0	 	Node	232-00 232-08 20 232-0 232-0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

. .

	ط (۵	$\begin{array}{c} \begin{array}{c} & & & & & & & & & & & & & & & & & & &$
-	HL (II)	
	I (%)	
	V (面/ S)	
	0 (1/s)	
	Coef C	
	니 (j)	$\begin{array}{c} 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 76. \\ 77. \\ 76. \\$
LineData —	с (шш	333 50 50 50 50 50 50 50 50 50 50 50 50 50
- Line	Node T EN	$\begin{array}{c} 222\\ 223\\ 224\\ 225\\ 225\\ 225\\ 225\\ 225\\ 225\\ 225$
 	ST	300000111282233333322233332223333222233332222233333
	Remarks	
	0c (1/s)	
•	EHP 2nd (m)	$\begin{array}{c} 29, \ 723\\ 29, \ 723\\ 29, \ 723\\ 29, \ 723\\ 20, \ 777\\ 20, \ 781\ 20, \ 781\ 20, \ 781\ 20, $
	EHP 1st(m)	
 	」 15 19	$\begin{array}{c} 2, 648, 840\\ 2, 648, 840\\ 2, 638, 256\\ 2, 638, 256\\ 2, 638, 256\\ 2, 638, 256\\ 2, 638, 256\\ 2, 638, 356\\ 2, 638, 356\\ 2, 638, 356\\ 2, 638, 356\\ 2, 638, 356\\ 2, 638, 369\\ 2, 658, 369\\ 2, 658, 369\\ 2, 558, 299\\ 2, 558, 299\\ 2, 558, 299\\ 2, 558, 299\\ 2, 558, 152\\ 2, 558, 152\\ 2, 558, 152\\ 2, 558, 161\\ 2, 558, 161\\ 2, 558, 161\\ 2, 558, 161\\ 2, 558, 161\\ 2, 556, 153\\ 2, 556, 109\\ 2, 556, 109\\ 2, 556, 109\\ 2, 556, 109\\ 2, 556, 109\\ 2, 556, 109\\ 2, 556, 109\\ 2, 556, 109\\ 2, 556, 109\\ 2, 556, 203\\ 2, 556, 203\\ 2, 556, 109\\ 2, 556, 109\\ 2, 556, 203\\ 2, 556, 109\\ 2, 556, 203\\ 2, 556, 109\\ 2, 556, 203\\ 2, 556, 109\\ 2, 556, 203\\ 2, 556, 203\\ 2, 556, 203\\ 2, 556, 109\\ 2, 556, 203\\ 2, 556, 203\\ 2, 556, 203\\ 2, 556\\ 2$
- NodeData	日间	$\begin{array}{c} 2678. 563\\ 2678. 563\\ 2678. 563\\ 2678. 563\\ 2678. 563\\ 2678. 563\\ 2678. 563\\ 26578. 563\\ 26533. 840\\ 26533. 840\\ 26533. 840\\ 26533. 840\\ 26533. 840\\ 26533. 840\\ 26533. 546\\ 26233. 546\\ 26333. 840\\ 26333.$
 	Node	66666666666666666666666666666666666666

•

•

	년 (田	$\begin{array}{c} -64.78\\ -64.78\\ 0.000\\ $
	EL E	
	I (%)	
	V (m/s)	
	0 (1/s)	
	Coef C	
	」 (目)	$\begin{array}{c} 0 \\ 172.333 \\ 172.333 \\ 172.333 \\ 172.333 \\ 172.333 \\ 172.333 \\ 172.333 \\ 172.333 \\ 172.333 \\ 172.333 \\ 101.335.366 \\ 123.469 \\ 123.469 \\ 123.469 \\ 123.469 \\ 123.466 \\ 117.50 \\ 117.50 \\ 123.469 \\ 123.466 \\ 123.466 \\ 123.2$
LineData -	〔 〔 〕〕	21 32 32 32 32 32 32 32 32 32 32 32 32 32
- Line	Node T EN	$\begin{smallmatrix} 1116\\669\\1116\\669\\1116\\669\\110\\22\\96\\99\\96\\99\\96\\99\\96\\99\\96\\99\\90\\92\\92\\92\\92\\92\\92\\92\\92\\92\\92\\92\\92\\92\\$
1	ST	665 665 665 665 665 665 665 665 665 665
	Remarks	reak Pressure Val
	0c (1/s)	
	EHP 2nd (m)	37, 428 37, 428 37, 428 37, 428 37, 428 388 37, 428 37, 428 38, 445 57, 445
	EHP 1st(m)	75. 426 70. 991
بة ا ا	, [1] 19	$\begin{array}{c} 2, 576, 356\\ 2, 576, 356\\ 2, 570, 643\\ 2, 557, 570, 643\\ 2, 557, 570, 643\\ 570, 641, 121\\ 2, 567, 443\\ 566, 476\\ 567, 443\\ 567, 443\\ 567, 567, 567\\ 567, 443\\ 567, 566, 446\\ 557, 586, 446\\ 568, 446\\ 568, 446\\ 569, 337\\ 569, 255\\ 569, 255\\ 569, 255\\ 569, 236\\ 512, 593\\ 569, 365\\ 569, 365\\ 5612, 993\\ 5612, 993\\ 5612, 993\\ 568, 503\\ 572, 544\\ 512\\ 572, 544\\ 512\\ 572, 561\\ 572\\ 572\\ 572\\ 572\\ 572\\ 572\\ 572\\ 572$
— NodeData	en (ei	2613. 779 2613. 779 2619. 902 2619. 902 2619. 902 2619. 902 2619. 902 2619. 902 2619. 902 2619. 902 2618. 563 2678. 563 2678. 563 2678. 563 2678. 563 2678. 563 2678. 563 2678. 563 26678. 563 26677. 572 26677. 572
] [Node	00000000000000000000000000000000000000

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i I	- NodeData	la – – –					1	· LineData	lata ––	ļ						
Node	₽Ĵ	13 (II)	EHP 1st(m)	EHP 2nd (n)	Qc (1/s)	Remarks	Node ST EN	de ÉN	(III)	」 (目)	Coef C	0 (1/s)	۲ (۵/۵۱)	1 (‰)	王间	ط (E)
111	2678. 563	2, 678. 563	32. 528	0.000		sure	112	33	38		110	0.000				
112		633.		0.000		ure	113	40	38		110	0.000				
113		623.		0.000		ure	113	43	75	-	110	0.000				
114		598.		0.000		ure	114	49	38		110	0.000				
115	-	613.	-	0.000		reak Pressure Tan	115	64	38		110	0.000				
116		619.		0.000		алы	116	75	38		110	0.000				
117				0.000	0.000	ure	117	56	38	210.779	.110	0.000	0.000	0.000	0.000	0.000
- 118		611.		67.518			118	55	75		110	0.000				
							118	101	38		110	0.000				

——— NodeData ———

										ط (B	
			-							H H	$\begin{array}{c} 8.657\\ 2.192\\ 2.192\\ 2.192\\ 2.192\\ 0.000\\ 0.100\\ 0.000\\ 0.$
					Pipe	Coefficient of Flow	f Flow Gradient			I (‰)	$\begin{smallmatrix} & 1 \\ 1 \\ 1 \\ 1 \\ 2 \\ 2 \\ 1 \\ 2 \\ 2 \\ 1 \\ 2 \\ 2$
							ο	Head Loss Add Pressure		V (□/□)	$\begin{array}{c} 0.138\\ 0.138\\ 0.138\\ 0.138\\ 0.267\\ 0.267\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.204\\ 0.062\\ 0.000\\ 0.$
	·			•				HL: H P: A		0 (1/s)	$\begin{array}{c} \textbf{6.509}\\ \textbf{6.509}\\ \textbf{3.140}\\ \textbf{2.1242}\\ \textbf{2.1242}\\ \textbf{2.1196}\\ 2.119$
						Pressure Water				Coef C	
			Votes >>			Ξź			1	ц	$\begin{array}{c} 738 & 592 \\ 177 & 672 \\ 5386 & 845 \\ 5382 & 902 \\ 5332 & 902 \\ 55 & 672 \\ 55 & 672 \\ 55 & 619 \\ 55 & 619 \\ 388 & 912 \\ 388 & 912 \\ 388 & 912 \\ 375 & 927 \\ 375 & 927 \\ 375 & 997 \\ 375 & 997 \\ 375 & 997 \\ 375 & 997 \\ 375 & 901 \\ 858 & 018 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 334 & 669 \\ 335 & 677 \\ 333 & 917 \\ 333 & 917 \\ 333 & 917 \\ 334 & 669 \\ 346 & 676 \\ 335 & 677 \\ 346 & 669 \\ 347 & 669 \\ $
	•		Explanatory Notes		Head Pr Ground	Ellectual Hea Consumption ()ata —	D (回回)	100.0 75.0 75.0 75.0 75.0 87.5 87.5 87.5 87.5 87.5 87.5 87.5 87.5
	`	ļ	Explar			EHF: 0c:			. LineData	Node	$\begin{array}{c} 83\\ 83\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23\\ 2$
			\approx	I					l 	ST	2211386554448 22118865544443 221188655444483 221188655444483 221188655444483 221188655444483 221188655444483 221188655444483 221188655444483 221188655444483 221188655444483 221188655444483 221188655444483 22118865544483 221188655444848 22118865544483 221188655444848 221188655444848 2211886554484848 2211886554484848 22118865548 2211885554 2211885554 2211885554 2211885554 221187555 221187555 221187555 221187555 221187555 221187555 221187555 221187555 221187555 221187555 221187555 221187555 221187555 2211875555 2211875555 2211875555 22118755555 22118755555 221187555555 2211875555555555555555555555555555555555
·		Formula>>	(田)	(III)	(%)	(ш/s)		١		Remarks	Reservoir Tank Protect Spring
		Hazen-Williams	67.985 (0.000	64.767	1.125 (0c (1/s)	$\begin{array}{c} -6 \\ -6 \\ -6 \\ -6 \\ -6 \\ -6 \\ -6 \\ -6 $
		••	Maximum EHP	Minimum EHP	Maximum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0. \ 0.00\\ 0. \ 0.000\\ 0.000\\ 0. \ 0.000\ 0.000\\ 0.000\ 0.000\\ 0.000\ 0.000\\ 0.000\ 0.000\ 0.000\\ 0.000\$
		n < <case.2< td=""><td></td><td></td><td></td><td></td><td>÷</td><td></td><td></td><td>EHP 1st (m)</td><td></td></case.2<>					÷			EHP 1st (m)	
		-Mertule Maryam	60	109	113	6	0.88 (cm)	16 (times)	 	IJ.	$\begin{array}{c} 2,\ 711,\ 092\\ 2,\ 678,\ 330\\ 667,\ 330\\ 678,\ 568,\ 449\\ 678,\ 568,\ 449\\ 676,\ 987\\ 666,\ 099\\ 77\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 633\\ 661,\ 611\\ 633\\ 661,\ 611\\ 633\\ 661,\ 611\\ 633\\ 661,\ 611\\ 633\\ 661,\ 611\\ 633\\ 661,\ 611\\ 633\\ 661,\ 611\\ 633\\ 661,\ 611\\ 633\\ 661,\ 611\\ 633\\ 611\\ 611\\ 611\\ 612\\ 612\\ 612\\ 612\\ 612$
		Me	Tank	Node	Line	Pump, Decom	gence Gap	Calculation	— NodeData	£€€,	2711. 092 2667. 920 2667. 920 2672. 330 2697. 738 2697. 738 2697. 738 2675. 214 2672. 367 2672. 349 2672. 349 2677. 985 2677. 985 2674. 347 2677. 985 2677. 985 2672. 593 2672. 593 2672. 383 2672. 383 27672. 3772. 377272. 377
		 				d	Convergence	Ca]	Node	52525266844925 - 06849987998
											· ·

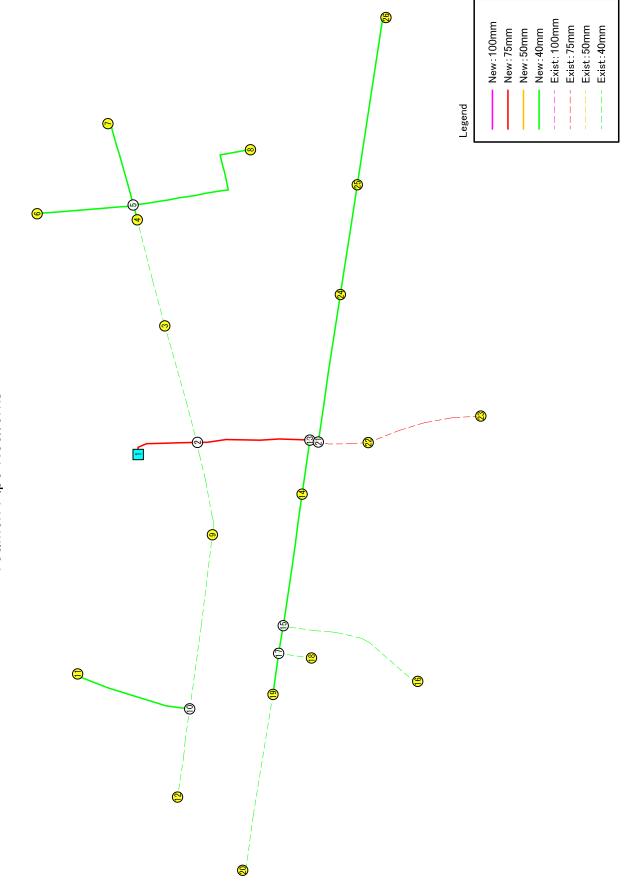
L.

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	d (E)	$\begin{array}{c} 0.000\\ 0.$
	H.	$\begin{array}{c} 0.000\\ 0.$
	I (%)	$\begin{array}{c} 2.2 \\ 2.46 \\ 2.57 \\ 2.5$
	V (四/S)	$\begin{smallmatrix} & 0.204 \\ $
	0 (1/s)	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $
-	Coef C	
	Ъ	$\begin{array}{c} 76. \ 626\\ 78. \ 843\\ 78. \ 843\\ 78. \ 843\\ 78. \ 843\\ 65. \ 855\\ 947\\ 155. \ 535\\ 739\\ 0. \ 100\\ 135. \ 739\\ 306. \ 663\\ 306. \ 663\\ 947\\ 135. \ 739\\ 135. \ 480\\ 96. \ 947\\ 135. \ 739\\ 135. \ 739\\ 135. \ 739\\ 126. \ 739\\ 127. \ 543\\ 100\\ 100\\ 100\\ 100\\ 100\\ 100\\ 100\\ 10$
LineData —	О (ШШ)	2327 5 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
- Line	Node T EN	$\begin{array}{c} 222\\ 252\\ 253\\ 253\\ 253\\ 253\\ 253\\ 253\\$
1 	ST	00000000000000000000000000000000000000
	Remarks	
,	0c (1/s)	
	EHP 2nd (m)	$\begin{array}{c} 23\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23\\ 23\\$
	EHP 1st(m)	
ן ן ש	(E) (E)	$\begin{array}{c} 2, 648, 840\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 648, 256\\ 2, 556, 258\\ 2, 556, 256\\ 2, 556, 256\\ 2, 556, 556\\ 2, 556, 556\\ 2, 556, 556\\ 2, 556, 556\\ 2, 556, 556\\ 2, 556, 556\\ 2, 556, 556\\ 2$
— NodeData	HÌ	2672 2672 591 2672 591 26572 591 26572 591 2657 591 26572 591 2655 730 26572 591 2655 730 26565 730 2655 657 26565 730 2655 657 26565 730 2652 651 26523 546 2652 538 26523 546 538 2652 26523 546 538 2652 26523 546 538 2652 26523 546 538 2652 26523 546 719 25591 26523 546 713 2653 26523 104 25591 389 26523 104 2653 104 26533 104 2653 104 26533 104 2653 104 26543 104 2653 104 26557 467 713 2651
 	Node	66666666666666666666666666666666666666

	۲ (۳)	$\begin{smallmatrix} & - & - & - \\ & 3.7. & 917 \\ 0.000$
	, H	$\begin{array}{c} 1.5 \\ 5.1 \\ 1.5 \\$
	(%) I	$\begin{array}{c} 23.\\ 23.\\ 23.\\ 23.\\ 23.\\ 23.\\ 23.\\ 23.\\$
	۲ (۱۳/۵)	$\begin{array}{c} 0.500\\ 0.204\\ 0.$
	0 (1/s)	$\begin{array}{c} 4 \\ 6 \\ 6 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7$
	Coef C	
1	」 〔目	$\begin{array}{c} 113.377\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 172.393\\ 107.395\\ 107.383\\ 107.3$
Data —		21 88 88 80 0 88 21 88 21 88 21 88 88 88 88 88 88 88 88 88 88 88 88 88
- LineData	Node T EN	$\begin{smallmatrix} 102\\ 102\\ 102\\ 102\\ 102\\ 102\\ 102\\ 102\\$
1	ST	$\begin{smallmatrix} & & & & & & & & & & & & & & & & & & &$
	Remarks	reak Pressure Val
	0c (1/S)	0. 225 0.
	EHP 2nd (m)	25 411 25. 411 25. 416 26. 166 37. 539 37. 939 37. 939 37. 939 37. 939 37. 539 37. 539 37. 539 37. 539 48. 566 48. 566 48. 566 48. 566 48. 566 48. 566 49. 128 37. 660 48. 566 48. 566 49. 128 36. 566 49. 128 37. 573 37. 573 37. 573 37. 573 37. 573 37. 573 37. 573 37. 576 49. 128 37. 576 49. 128 37. 576 49. 128 37. 577 37. 578 37. 578 3
	EHP 1st(m)	70. 088 51. 883
 	日 19	$\begin{array}{c} 2, 576, 356\\ 2, 573, 618\\ 2, 573, 618\\ 2, 553, 076\\ 2, 553, 076\\ 2, 553, 076\\ 2, 554, 186\\ 2, 561, 146\\ 2, 562, 186\\ 2, 561, 146\\ 2, 562, 038\\ 2, 561, 146\\ 2, 562, 038\\ 2, 556, 446\\ 2, 586, 446\\ 161\\ 2, 562, 038\\ 619, 902\\ 2, 561, 146\\ 2, 562, 038\\ 2, 561, 146\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 561, 121\\ 2, 562, 293\\ 2, 561, 121\\ 2, 561, 1$
— NodeData	Ê.	2601. 767 2601. 767 2600. 058 2600. 058 2600. 058 2601. 725 2601. 725 2601. 725 2601. 725 2601. 333 2661. 333 2661. 095 2661. 095 2661. 095 2661. 095 2661. 095 2661. 095 2662. 133 2661. 929 2661. 929 2661. 929 2661. 929 2661. 929 2661. 933 2661. 017 2661. 933 2661. 017 2661. 033 2661. 017 2661. 033 2661. 017 2661.
]]	Node	$\begin{array}{c} 666\\ 666\\ 667\\ 666\\ 666\\ 666\\ 666\\ 666$

		5. 184 0. 000 0. 183 5. 853 9. 631 2. 841 2. 089 -1. 491
	H(E)	
•	(%) I	$\begin{array}{c} 9. \ 913\\ 0. \ 000\\ 1. \ 849\\ 21. \ 003\\ 35. \ 780\\ 9. \ 913\\ 9. \ 913\\ 7. \ 963\\ -16. \ 074 \end{array}$
	V (面/ S)	$\begin{array}{c} 0.408\\ 0.408\\ 0.255\\ 0.817\\ 0.408\\ 0.408\\ 0.561\\ 0.530\end{array}$
-	Q (1/s)	$\begin{array}{c} 0.451\\ 0.000\\ 1.127\\ 0.676\\ 0.451\\ 0.451\\ 0.451\\ 0.451\\ 0.585\end{array}$
	Coef C	
	ц	522.930 174.553 98.768 278.695 269.183 286.580 286.580 286.580 286.580 286.53 280.779 281.653 92.744
)ata —	П	32333 323 323 323
—— LineData	de EN	33 440 55 55 55 101
1 	Node ST EN	112 113 115 116 117 118
	Remarks	reak Pressure Tan reak Pressure Tan reak Pressure Tan reak Pressure Tan reak Pressure Tan reak Pressure Tan reak Pressure Tan
	Qc (1/s)	0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.000000
	EHP 2nd (m)	$\begin{array}{c} 0. & 000 \\ -0. & 000 \\ 0. & 000 \\ -0. & 000 \\ 48. & 506 \\ 506 \end{array}$
	EHP 1st(m)	23. 771 31. 888 37. 105 17. 347 37. 917 28. 156 47. 281
9 	IJ.	2, 678, 563 2, 633, 840 2, 633, 840 2, 623, 546 2, 613, 779 2, 611, 779 2, 611, 902 2, 611, 045 2, 611, 045
· NodeData	H)	2678. 563 2633. 840 2623. 546 2523. 546 2513. 779 2619. 902 2610. 185 2659. 551 2659. 551
] [[Node	111 2 112 2 113 2 114 2 114 2 116 2 116 2 117 2 118 2



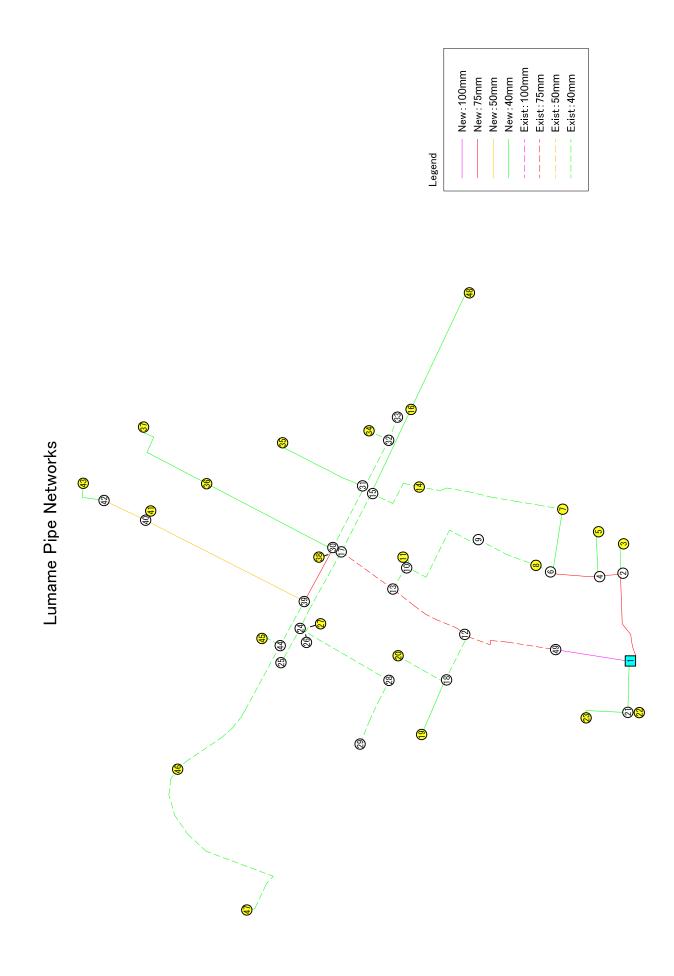
Yetimen Pipe Networks

)						Ч (Ш	
								ط ا	
			Pipe	Coefficient of Flow	f Flow Gradient			I (%)	0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.000000
			4	ᆸ	ంట	Head Loss Add Pressure		۲ (m/s)	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $
						HL: H P: A		0 (1/s)	$\begin{array}{c} 0.000\\ 0.$
				Fressure Water				Coef C	
	<< Explanatory Notes >>		-	bliectual Head Pr Consumption of Wa		·		ц	$\begin{array}{c} 122 \\ 233 \\ 233 \\ 233 \\ 233 \\ 211 \\ 233 \\ 211 \\ 233 \\ 211 \\ 233 \\ 211 \\ 233 \\ 234 \\ 333 \\ 333 \\ 333 \\ 334 \\ 344 \\ 333 \\ 334 \\ 333 \\ 334 \\ 334 \\ 334 \\ 349 \\ 357 \\ 349 \\ 349 \\ 349 \\ 349 \\ 357 \\ 349 \\ 349 \\ 357 \\ 349 \\ 349 \\ 357 \\ 349 \\ 340 \\$
	natory	- - 	Head Pressure Ground Level	EI I ectu Consump			LineData —	D (IIII)	22,22,22,22,22,22,22,22,22,22,22,22,22,
	K Expla	- Node		Uc:			- Line	Node T EN	2237520084202171084027 2337530084022171084022 2337530084022
ļ	\checkmark				-		 	ST	
<	(III)	(E)	(%)	(m/s)			·	Remarks	Reservoir Tank
is Formula	37.204	13.863	0.000	0.000				Qc (1/s)	0
Hazen-Williams Formula>>	Maximum EHP	Minimum EHP	Maximum I	Maximum V			•	EHP 2 nd (m)	$\begin{array}{c} 0. \\ 17. \\ 16. \\ 17. \\ 17. \\ 17. \\ 18. \\ 540 \\ 18. \\ 540 \\ 18. \\ 515 \\ 20. \\ 784 \\ 21. \\ 546 \\ 22. \\ 51. \\ 526 \\ 527 \\ 22. \\ 354 \\ 22. \\ 354 \\ 22. \\ 354 \\ 22. \\ 354 \\ 22. \\ 354 \\ 22. \\ 354 \\ 354 \\ 354 \\ 354 \\ 354 \\ 354 \\ 354 \\ 356 \\ $
< <case.1 :="" h<="" td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>EHP 1st (m)</td><td></td></case.1>								EHP 1st (m)	
Yetimen < <ca< td=""><td>-</td><td>25</td><td>25</td><td>0</td><td>0.00 (cm)</td><td>2 (times)</td><td> </td><td>」(旦 15</td><td>$\begin{array}{c} 2, 445. \\ 2, 445. \\ 2, 430. \\ 2, 430. \\ 2, 427. \\ 236. \\ 2, 427. \\ 235. \\ 2, 427. \\ 235. \\ 2, 428. \\ 21, 428. \\ 21, 428. \\ 22, 419. \\ 22, 419. \\ 2424. \\ 235. \\ 22, 419. \\ 22, 421. \\ 22, 421. \\ 22, 422. \\ 22, 419. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 23, 416. \\ 24, 416$</td></ca<>	-	25	25	0	0.00 (cm)	2 (times)	 	」(旦 15	$\begin{array}{c} 2, 445. \\ 2, 445. \\ 2, 430. \\ 2, 430. \\ 2, 427. \\ 236. \\ 2, 427. \\ 235. \\ 2, 427. \\ 235. \\ 2, 428. \\ 21, 428. \\ 21, 428. \\ 22, 419. \\ 22, 419. \\ 2424. \\ 235. \\ 22, 419. \\ 22, 421. \\ 22, 421. \\ 22, 422. \\ 22, 419. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 22, 416. \\ 23, 416. \\ 24, 416$
— — — Yei	Tank	Node	Line	Pump, Decom	gence Gap	Calculation	- NodeData	€ £	2445. 775 2445. 775 245. 775245. 775 245. 775
 				٠Pı	Convergence	Cal	 	Node	22222222222222222222222222222222222222

	d (町) 000		۰ ۲
	HL (III)		
	1 (%) 0 000		• • •
	ү (m/ s) 0. 000		
	0.000000000000000000000000000000000000	•	· · · · · · · · · · · · · · · · · · ·
	Coe f C 110		
	ц (п) 333. 357		
Data -	р (пп) 37.5		
LineData -	Node ST EN 25 26		
i	Remarks A ST 25		
	Qc 0. 000 0. 000		
	EHP 2nd (m) 29. 060 29. 060		·
	EHP 1st (m)	· · · · · · · · · · · · · · · · · · ·	
	GL (m) 2. 416. 328 2. 416. 715		
NodeData	H (m) 2445. 775 2 2445. 775 2		
	Node 25 26		• .

·								- - (Ш)	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $
				,			x	HL (ff)	$egin{array}{cccccccccccccccccccccccccccccccccccc$
			ipe	n coefficient ty of Flow	Flow radient	, ,		(%) I	5. 709 6. 721 6. 721 6. 721 6. 721 6. 722 0. 879 0. 8790 0. 8790 0. 879000000000000000000000000000000000000
			Diameter Length of Pi	Quantity of	Velocity of Hydraulic Gi	Head Loss Add Pressure		V (町/ S)	0. 469 0. 552 0. 552 0. 331 0. 110 0. 221 0.
•						HL: H P: A		0 (1/s)	$\begin{array}{c} 2. & 0.7\\ 0. & 365\\ 0. & 365\\ 0. & 365\\ 0. & 365\\ 0. & 365\\ 0. & 122\\$
			:	rressure Water				Coef C	
	Votes >>		neau rressure Ground Level					ц Ц	$\begin{array}{c} 122, 593\\ 233, 440\\ 181, 823\\ 218, 028\\ 218, 028\\ 211, 438\\ 229, 691\\ 168, 369\\ 334, 444\\ 168, 369\\ 3314, 448\\ 338, 976\\ 3314, 448\\ 338, 976\\ 3314, 448\\ 338, 976\\ 3314, 448\\ 336, 357\\ 799\\ 366, 666\\ 235, 331\\ 16, 799\\ 236, 666\\ 235, 331\\ 224, 857\\ 224, 857\\ 224, 857\\ 224, 222\\ 214, 222\\ 2$
	<< Explanatory Notes		Ground	Consumption			LineData —	и (шш)	75.0 337.5 75.0 337.5 75.0 75.7 75.7 75.7 75.7 75.7 75.7 7
	< Expla	- Node		Qc:			- Line	Node	22222038798792111087927 2334203879829 23342503879
I	Ÿ						1 1	ST	55555557722255 5555557722255 5555557722255 555555 55555 5555 5555 5555 5555 5555
	· (EI)	(四)	(%)	(m/s)				Remarks	Reservoir Tank
is Formula	33. 260	8.156 (17.312 (0.552 (0c (1/s)	-2.000 0.122 0.000 0.122 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000 0.122 0.000
Hazen-Williams Formula>>	Maximum EHP	Minimum EHP	Maximum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0. & 000\\ 1.45 & 828\\ 1.45 & 000\\ 1.1 & 378\\ 1.1$
 2	_		_			• ·		EHP 1st (m)	
-Yetimen < <case.< td=""><td></td><td>25</td><td>25</td><td>0</td><td>0.99 (cm)</td><td>12 (times)</td><td> </td><td>」 日 日</td><td>$\begin{array}{c} 2, \ 445, \ 775\\ 2, \ 445, \ 775\\ 2, \ 427, \ 269\\ 2, \ 427, \ 286\\ 2, \ 427, \ 286\\ 2, \ 427, \ 286\\ 2, \ 420, \ 286\\ 2, \ 420, \ 286\\ 2, \ 420, \ 286\\ 2, \ 420, \ 286\\ 2, \ 420, \ 291\\ 2, \ 419, \ 148\\ 2, \ 424, \ 991\\ 2, \ 416, \ 521\\ 2, \ 521\ 2, \ 521\\ 2, \ 521\ 2, \ 5$</td></case.<>		25	25	0	0.99 (cm)	12 (times)	 	」 日 日	$\begin{array}{c} 2, \ 445, \ 775\\ 2, \ 445, \ 775\\ 2, \ 427, \ 269\\ 2, \ 427, \ 286\\ 2, \ 427, \ 286\\ 2, \ 427, \ 286\\ 2, \ 420, \ 286\\ 2, \ 420, \ 286\\ 2, \ 420, \ 286\\ 2, \ 420, \ 286\\ 2, \ 420, \ 291\\ 2, \ 419, \ 148\\ 2, \ 424, \ 991\\ 2, \ 416, \ 521\\ 2, \ 521\ 2, \ 521\\ 2, \ 521\ 2, \ 5$
- — — Yet	Tank	Node	Line	Pump, Decom	Convergence Gap	Calculation 12	— NodeData	H (j)	2445. 775 2445. 775 2445. 075 2441. 034 2438. 613 2438. 813 2438. 250 2438. 250 2443. 853 2442. 577 2444. 692 2439. 568 2439. 932 2439. 932 2439. 932 2439. 932 2434. 682 2444. 682 2444. 682 2444. 682 2444. 682 2444. 682
 -					Conve	Ü,	 	Node	23321068462748321 5332108476657733 5332108476657733 5332108476657733 533210847665773 533210847665773 533210847665773 533210847665773 533210847665773 533210847665773 533210847665773 53321084767575757575757575757575757575757575757

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			879								
		I (%)	0. 879								
		_									
		ү (ш/s)	10								
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		5									
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		Q (1/S)	0.1								
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		coef c	110								
	•	ςΩ									
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	1	-5	333								
•	LineData		•••								
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	ata	□	37. 5								
	eDi										
	Lin	Node ST EN	26								
	, i	ode									
	i	ST N	25								
	I					•					
		Remarks									
		(BB)							•		
		Re									
			55								
		Qc (1/S)	0. 122 0. 122								
			00								
		_	<u></u>								
			. 74								
		EHP 2nd (m)	25. 743 25. 063								
		_									
								-			
		EHP 1st (m)									
			പറ								
		ප්ම	32								
		00	416. 116.		-		<u> </u>				
	 		2,4				<u>^</u> .				
	— NodeData —		2442. 071 2, 416. 328 2441. 778 2, 416. 715								
	deD	ÊÌ	17 77							•	
	No	нэ	42. 41.								
			24								
	-	de	25 26								
	1	Node									-



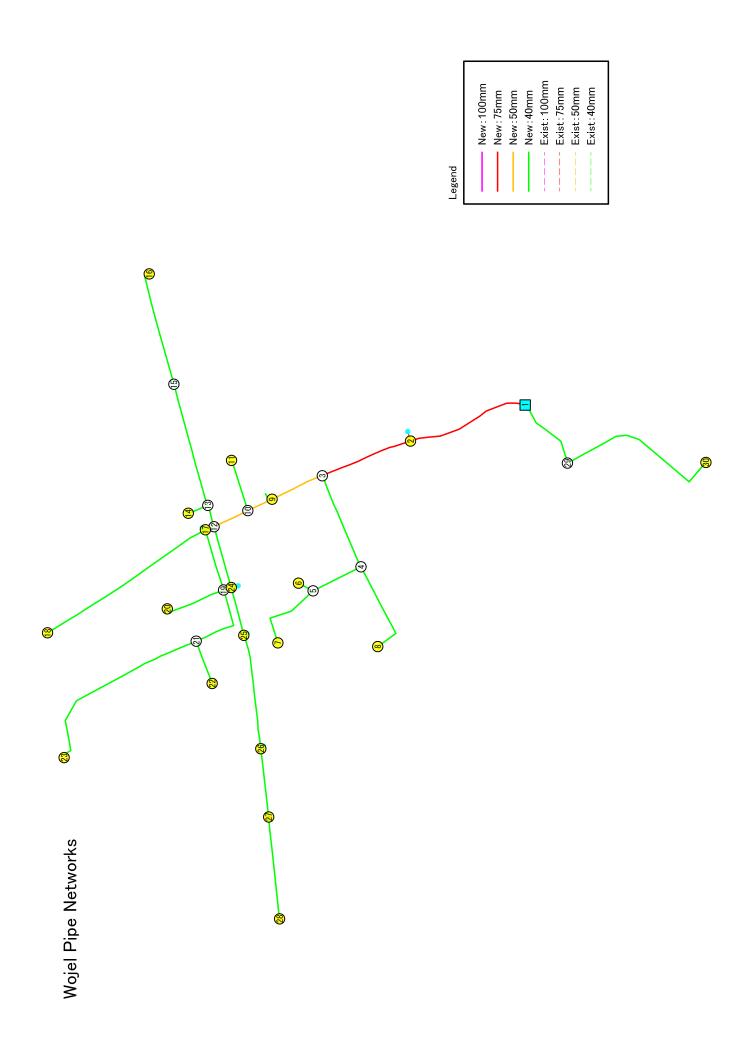
						ط (۳)	
						田间	0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.000000
		ipe 	Flow Flow	ı rıow Gradient Fe		I (%)	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $
,	I	- Diameter Length of Pipe	Priction to Quantity of	Hydraulic Gr Hydraulic Gr Head Loss Add Pressure		ү (ш∕ s)	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $
		- Line - D:] [:]	0: 0: 0: 0:			0 (1/s)	
			Fressure Water			Coef C	
	Notes >>	Pressure Id Level				(町 (目)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
· · ·	Explanatory Notes	- Head Pressur Ground Level			LineData —	(IIII)	75. 77. 77. 77. 77. 77. 77. 77.
		Node HP: GL: Fue			- Line	Node	1328261111109188765783876578 19082887111109188765183 1908288711110918876518
	∻	I			1 1 1	ST	844482555556849255555
	(III)	(m) (%)	(m/s)			Renarks	Reservoir Tank
Formula>>	52.343	12. 929 0. 000	0.000			Qc (1/s)	
Hazen-Williams	Maximum EHP	Minimum EHP Maximum I	Maximum V			EHP 2nd (m)	$\begin{array}{c} 8. & 050\\ 2.0. & 249\\ 2.0. & 249\\ 2.0. & 249\\ 3.0. & 541\\ 3.0. & 541\\ 3.0. & 542\\ 3.0. & 304\\ 3.0. & 304\\ 3.0. & 304\\ 3.0. & 304\\ 3.0. & 304\\ 3.0. & 304\\ 3.0. & 303\\ 3$
						EHP 1st (m)	
Lumame < <case.< td=""><td>-</td><td>48 50</td><td>0</td><td>0.00 (cm) 2 (times)</td><td>9 </td><td>13 13</td><td>2, 497. 769 2, 485. 570 2, 485. 570 2, 478. 572 478. 572 478. 572 478. 572 478. 002 478. 022 476. 975 2, 476. 975 2, 476. 975 2, 476. 975 2, 466. 395 2, 466. 395 2, 466. 395 2, 466. 203 2, 466. 203 2, 466. 203 2, 465. 203 2, 465. 203 2, 465. 203</td></case.<>	-	48 50	0	0.00 (cm) 2 (times)	9 	13 13	2, 497. 769 2, 485. 570 2, 485. 570 2, 478. 572 478. 572 478. 572 478. 572 478. 002 478. 022 476. 975 2, 476. 975 2, 476. 975 2, 476. 975 2, 466. 395 2, 466. 395 2, 466. 395 2, 466. 203 2, 466. 203 2, 466. 203 2, 465. 203 2, 465. 203 2, 465. 203
— — [n	Tank	Node Line	Pump, Decon	ergence Gap Calculation	- NodeData	日间	$\begin{array}{c} 2505 \\ 2505 \\ 2505 \\ 819 \\ 2505 \\ 819 \\ 2505 \\ 819 \\ 810 \\ $
			Ā	Convergence Calcula	 	Node	5322-068-1928-1968-1987-98-1987-98-1987-98-1987-98-1987-98-1987-98-1987-98-1987-98-1987-98-1987-98-1987-98-198 5335555555555555555555555555555555555

	ط (E	
	H.	
	I (%)	
	V (m/ S)	
	Q (1/s)	
	Coef C	
	IJ.	$\begin{smallmatrix} 133.816\\ 23.435\\ 97.004\\ 120.584\\ 120.584\\ 16.021\\ 12.562\\ 128.879\\ 174.023\\ 174.023\\ 174.023\\ 174.023\\ 174.023\\ 174.023\\ 174.023\\ 174.023\\ 174.023\\ 174.023\\ 124.093\\ 124.093\\ 124.093\\ 124.033\\ 124$
LineData —	۵ آ	3377 9 277 9
- Line	Node ST EN	$\begin{smallmatrix} & 22\\ & $
 	ST	$\begin{smallmatrix} & & & & & & \\ & & & & & & & \\ & & & & $
	Remarks	
	Qc (1/s)	
	EHP 2nd (m)	$\begin{array}{c} 43.570\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.777\\ 37.791\\ 37.791\\ 37.791\\ 37.791\\ 37.792\\ 37.792\\ 37.797\\ 37.792\\ 37.797\\ 37.792\\ 37.797\\$
	EHP 1st (m)	
] [日 日	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
NodeData	E E	2505.819 2505.819 2505.819 2505.819 2505.819 2505.819 2505.819 2505.819 2505.819 2505.819 2505.819 2505.819 2505.819 2505.819 2505.819 2505.819 2505.819 2505.819
- 	Node	, , , , , , , , , , , , , , , , , , ,

				ч (П	
	,			ĦĴ	$\begin{smallmatrix} & -1.557 \\ & 0.347 \\ & 0.347 \\ & 0.347 \\ & 0.347 \\ & 0.3449 \\ & 0.347 \\ $
	f Pipe Coefficient of Flow	Flow adient		I (‰)	$\begin{array}{c} 16. 590\\ 6. 483\\ 4. 596\\ 4. 596\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 3. 635\\ 1. 256\\ 1. 559$
	iameter ength o riction uantity	Velocity of Hydraulic Gr Head Loss Add Pressure		۲ (m/ s)	$^{-1}$
	- Line - D: D L: L Coef: F Q: Q			0 (1/s)	$\begin{array}{c} 2.5\\ -0.5\\ $
	Pressur6 Water			Coef C	
Notes >>	, py			ц	$\begin{array}{c} 2240 & 166 \\ 124 & 844 \\ 155 & 572 \\ 588 & 442 \\ 588 & 415 \\ 391 & 563 \\ 391 & 553 \\ 391 & 553 \\ 391 & 565 \\ 391 & 565 \\ 391 & 565 \\ 311 & 518 \\ 270 & 158 \\ 271 & 311 \\ 544 & 475 \\ 271 & 311 \\ 544 & 475 \\ 157 & 305 \\ 157 & 305 \\ 330 & 309 \\ 231 & 586 \\ 231 & 232 & 237 \\ 232 & 232 & 237 \\ 232 & 232 & 237 \\ 233 & 232 & 237 \\ 233 & 232 & 237 \\ 233 & 232 & 237 \\ 234 & 586 $
Explanatory 1	- Head Pressure Ground Level Effectual Hea Consumption o		Data -		75. 75. 75. 75. 75. 75. 75. 75.
<< Explai	- Node HP: GL: EHP: Qc:		LineData	Node ST EN	224 24 24 24 24 24 24 24 24 24 24 24 24
	(II) (%) (S/II)		I	Remarks	Reservoir Tank
5 Formula>	4.408 35.149 0.913			Qc (1/s)	-6.
Hazen-Williams Maximum EHP	Minimum EHP Maximum I Maximum V			EHP 2nd (m)	$\begin{array}{c} 8. & 050\\ 25. & 013\\ 26. & 050\\ 27. & 050\\ 27. & 050\\ 27. & 052\\ 29. & 290\\ 25. & 015\\ 29. & 290\\ 20. & 624\\ 29. & 290\\ 20. & 624\\ 29. & 029\\ 20. & 624\\ 20. & 629\\ 20. &$
	·			EHP 1st(m)	
Lumame < <case. nnk 1</case. 	48 50 0	0.97 (cm) 13 (times)	 !	B	$\begin{array}{c} 2, 497. \\ 2, 497. \\ 2, 485. \\ 2, 478. \\ 2, 478. \\ 002\\ 2, 478. \\ 002\\ 2, 476. \\ 002\\ 2, 476. \\ 002\\ 2, 476. \\ 002\\ 2, 476. \\ 002\\ 2, 479. \\ 003\\ 2, 480. \\ 005\\ 2, 480. \\ 005\\ 2, 480. \\ 005\\ 2, 482. \\ 005\\ 2, 482. \\ 005\\ 2, 487. \\ 005\\ 2, 4$
— Lur Tank	Node Line P, Decom	Convergence Gap Calculation	— NodeData	H)	2505.819 2505.819 2503.915 2503.915 2503.915 2503.915 2503.915 2503.915 2503.915 2503.915 2503.915 2503.915 2500.513 2497.139 2497.118 2493.918 2493.918 2493.918 2493.918 2493.918 2493.918 2493.918 2493.918 2493.918 2503.918 2503.918 2503.918 2503.918 2503.194 2503.194 2503.194 2503.194
	Pump,	178 1			

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Υ.	ط (آ	
	HI آ	$\begin{array}{c} 0.128\\ 0.128\\ 0.128\\ 0.128\\ 0.128\\ 0.128\\ 0.128\\ 0.128\\ 0.129\\ 0.$
	I (%)	19,5596 19,559
	, V (п/s)	$\begin{array}{c} 0.270\\ 0.$
	Q (1/s)	0. 298 0. 2988 0. 2988 0. 2988 00000000000000000000000000000000000
	Coef C	
-	ц Ц	$ \begin{smallmatrix} 133 \\ 23, 435 \\ 120, 584 \\ 97, 004 \\ 156, 021 \\ 16, 021 \\ 16, 021 \\ 12, 562 \\ 349, 479 \\ 174, 023 \\ 164, 023 \\ 164, 023 \\ 164, 023 \\ 164, 023 \\ 164, 023 \\ 164, 023 \\ 164, 023 \\ 124, 003 \\ 255, 273 \\ 124, 093 \\ 255, 273 \\ 124, 093 \\ 255, 273 \\ 124, 033 \\ 255, 375 \\ 246, 335 \\ 246, $
LineData —	(回) [1]	337.5 27.5 27.5 27.5 27.5 27.5 27.5 27.5 2
- Line	Node ST EN	$\begin{smallmatrix} 122\\ 122\\ 122\\ 122\\ 122\\ 122\\ 122\\ 122$
, 	ST	44444444444444444444444444444444444444
	Renarks	
	0c (1/s)	$\begin{array}{c} 0.00\\$
	EHP 2nd (m)	$\begin{array}{c} 31. \\ 32. \\ 25. \\ 752 \\ 25. \\ 753 \\ 753 \\ 753 \\ 753 \\ 753 \\ 753 \\ 753 \\ 763 \\ 733 \\ 763 \\ 763 \\ 733 \\ 763 \\ 763 \\ 763 \\ 764 \\ 770 \\ 733 \\ 764 \\ 770 \\ 733 \\ 764 \\ 770 \\ 733 \\ 764 \\ 770 \\ 786 \\$
	EHP 1st(回)	
 	19 19	$\begin{array}{c} 2,462,249\\ 2,467,756\\ 2,468,775\\ 2,468,775\\ 2,468,775\\ 2,466,103\\ 2,466,103\\ 2,466,266\\ 2,466,266\\ 2,466,243\\ 2,466,266\\ 2,466,273\\ 2,466,273\\ 2,467,287\\ 2,467,287\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,466,273\\ 2,287\\ 2,$
- NodeData	e e	 2493. 581 2493. 581 2493. 581 2493. 508 2493. 508 2491. 500 2490. 906 2490. 906 2491. 500 2491. 510 2491. 894 2492. 023 2492. 023 2493. 206 2493. 206 2493. 206 2493. 206 2493. 206 2493. 206 2493. 208 2493. 206 2493
1	Node	4 4 4 4 3



								ط (۳)	
								H E	
			pe	coefficient of Flow	f Flow Gradient			I (‰)	
					0	Head Loss Add Pressure		V (m/s)	
	,	,				HL: H P: A		0 (1/s)	
				rressure Water				Coef C	
	<< Explanatory Notes >>			of]	ц	$\begin{array}{c} 281. \ 892\\ 169. \ 070\\ 215. \ 938\\ 224. \ 731\\ 121. \ 741\\ 2224. \ 731\\ 121. \ 741\\ 2221. \ 458\\ 37. \ 460\\ 177. \ 094\\ 60. \ 825\\ 142. \ 825\\ 143. \ 358\\ 142. \ 724\\ 265. \ 710\\ 142. \ 724\\ 265. \ 724\\ 175. \ 749\\ 102. \ 786\\ 175. \ 786$
	natory	- Uood D.	Ground Level	Consumption			LineData —	C (IIII)	7377 755 7775 7775 7775 7775 7775 7775
	< Expla	- Node un.		Gc:			- Line	Node T EN	2221098611211076859433 2221098611121076859433 2321098611121076859433 23210986111121076859433 23210986111121076859433 232109861111177
	\sim						 [ST	21119221999555443332
	(田)	(11)	(%)	(S/ш) -				Remarks	Reservoir Tank
Formula>>	61.324	3. 995	0.000	0.000				0c (1/s)	
Hazen-₩illiams Formula>>	Maximum EHP	Minimum EHP	Maximum [.] I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0. & 000\\ 2.0. & 026\\ 3.0. & 026\\ 3.0. & 889\\ 3.4. & 224\\ 3$
 H	4	-	Α	~				EHP 1st(m)	
jel < <case.< td=""><td>1</td><td>29</td><td>29</td><td>0</td><td>0.00 (cm)</td><td>2 (times)</td><td> </td><td>E</td><td>$\begin{array}{c} 2,\ 488,\ 580\\ 2,\ 458,\ 580\\ 2,\ 456,\ 554\\ 2,\ 456,\ 554\\ 2,\ 456,\ 554\\ 2,\ 456,\ 556\\ 2,\ 449,\ 408\\ 557\\ 2,\ 449,\ 557\\ 2,\ 449,\ 556\\ 2,\ 449,\ 557\\ 2,\ 5,\ 557\\ 2,\ 557\ 2,\ 557\$</td></case.<>	1	29	29	0	0.00 (cm)	2 (times)	 	E	$\begin{array}{c} 2,\ 488,\ 580\\ 2,\ 458,\ 580\\ 2,\ 456,\ 554\\ 2,\ 456,\ 554\\ 2,\ 456,\ 554\\ 2,\ 456,\ 556\\ 2,\ 449,\ 408\\ 557\\ 2,\ 449,\ 557\\ 2,\ 449,\ 556\\ 2,\ 449,\ 557\\ 2,\ 5,\ 557\\ 2,\ 557\ 2,\ 557\$
⊶ —,— Wojel	Tank	Node	Line	Pump, Decom	gence Gap	Calculation	- NodeDaťa	H Û	$\begin{array}{c} 2488. 580\\ 2488$
1				P	Сопуегделсе	Ca		Node	-2°°4°°5°8°°°°°°4°°5°8°°°°°4°°°

		ط (أ	$\begin{array}{c} 0. & 0.0 \\ 0. &$						
pr.		(II)	0. 000 0. 000 0. 000 0. 000 0. 000						
		(%) 1	0. 000 0. 000 0. 000 0. 000 0. 000	,	·	×.		· .	ţ
		V (m/s)	0.000 0.000 0.000 0.000 0.000		·		·		
		0 (1/S)	0. 000 0. 000 0. 000 0. 000 0. 000						
		Coef C	110 110 110 110						
	1	ЪĴ	112. 254 261. 224 155. 753 233. 817 387. 175	•					
	Data —	(IIII)	37. 5 37. 5 37. 5 37. 5 37. 5					x	
·	- LineData	de EN	25 26 28 30 30						
	 ` 	Node ST EN	24 25 26 29						•
		Remarks							
		0c (1/s)	0.000					· · ·	
		EHP 2nd (m)	42. 214 51. 959 56. 242 61. 324 6. 261 3. 995					- -	
		EHP 1st(m)							
		(I) I)	2, 446, 366 2, 436, 621 2, 432, 338 2, 427, 256 2, 482, 319 2, 484, 585						
7	- NodeData	H (j	2488. 580 2488. 580 24888. 580 2488. 580 24880						
		Node	25 26 28 28 29 29 29 29						

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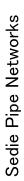
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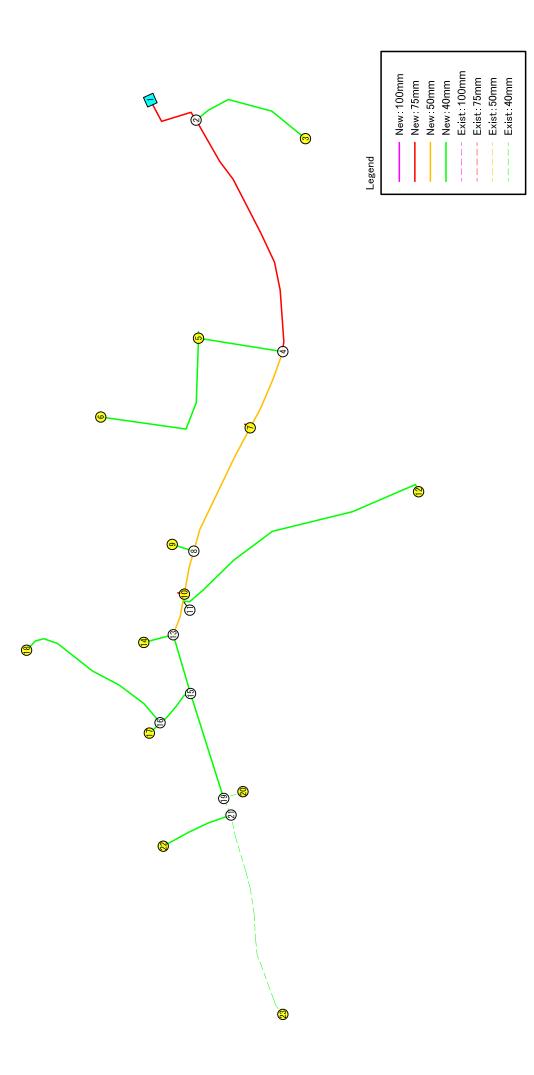
	•		·	-				년 (<u>태</u>	
								H)	$\begin{array}{c} 1.409\\ 0.117\\ 1.409\\ 0.971\\ 1.190\\ 0.153\\ 0.123\\ 0.$
			Pipe	Coefficient of Flow	f Flow Gradient			I (%)	
			·	Friction Coe Quantity of	o	Head Loss Add Pressure		V (лл∕s)	0.437 0.437 0.737 0.797 0.697 0.097 0
				•• ••		HL: H P: A		0 (1/s)	$\begin{array}{c} 1. & 928\\ 1. & 928\\ 1. & 821\\ 1. & 821\\ 1. & 821\\ 1. & 822\\ 1. & 823\\ 0. & 107\\ 1. & 392\\ 0. & 107\\$
	ų			Fressuré Water				Coef C	
	<< Explanatory Notes >>			of			1	л(Ш	$\begin{array}{c} 281:\ 892\\ 169:\ 070\\ 215:\ 938\\ 224,\ 731\\ 126:\ 041\\ 121:\ 741\\ 221:\ 741\\ 221:\ 458\\ 37.\ 460\\ 84.\ 910\\ 84.\ 910\\ 50.\ 613\\ 50.\ 613\\ 50.\ 613\\ 50.\ 613\\ 50.\ 613\\ 50.\ 613\\ 205.\ 724\\ 247.\ 965\\ 285.\ 724\\ 247.\ 965\\ 285.\ 724\\ 247.\ 965\\ 285.\ 724\\ 247.\ 965\\ 285.\ 724\\ 246.\ 829\\ 102.\ 781\\ 142.\ 782\\ 142.\ 782$ 142.\ 782 14
	natory 1	ي - ا ا	Head Fressure Ground Level	EIIECTUAL HE Consumption			LineData —	C (IIII)	75. 75. 75. 75. 75. 75. 75. 75. 75. 75.
	< Expla	- Node		ЕНГ: 0с:			- Line	Node	222009865144
	ॐ						i I	ST	22199999999999999999999999999999999999
	(田)	(II)	(%)	(m/s)				Remarks	Reservoir Tank
Formula>>	50.405	3.610	22.615	0. 764				Qc (1/s)	-2. 035 0. 107 0. 107 00000000000000000000000000000000000
Hazen-Williams	Maximum EHP	Mininum EHP	Maximum I	Махітит V		-	,	EHP 2nd (m)	$\begin{array}{c} 0. & 0.00\\ 28. & 617\\ 28. & 509\\ 25. & 553\\ 30. & 352\\ 30. & 352\\ 30. & 302\\ 30. & 302\\ 30. & 302\\ 30. & 302\\ 30. & 302\\ 30. & 302\\ 31. & 544\\ 32. & 030\\ 33. & 014\\ 33. $
 2								EHP 1st (m)	
Wojel < <case.< td=""><td></td><td>29</td><td>29</td><td>0</td><td>0.50 (сп)</td><td>14 (times)</td><td></td><td>GL EL</td><td>$\begin{array}{c} 2,\ 488,\ 580\\ 2,\ 468,\ 554\\ 2,\ 457,\ 591\\ 2,\ 457,\ 591\\ 2,\ 457,\ 591\\ 2,\ 455,\ 554\\ 2,\ 455,\ 554\\ 2,\ 445,\ 557\\ 2,\ 445,\ 576\\ 2,\ 445,\ 576\\ 2,\ 445,\ 576\\ 2,\ 445,\ 576\\ 2,\ 444,\ 528\\ 2,\ 444,$</td></case.<>		29	29	0	0.50 (с п)	14 (times)		GL EL	$\begin{array}{c} 2,\ 488,\ 580\\ 2,\ 468,\ 554\\ 2,\ 457,\ 591\\ 2,\ 457,\ 591\\ 2,\ 457,\ 591\\ 2,\ 455,\ 554\\ 2,\ 455,\ 554\\ 2,\ 445,\ 557\\ 2,\ 445,\ 576\\ 2,\ 445,\ 576\\ 2,\ 445,\ 576\\ 2,\ 445,\ 576\\ 2,\ 444,\ 528\\ 2,\ 444,$
°	Tank	Node	Line	Pump, Decom	ence Gap	Calculation 14	NodeData	副圓	$\begin{array}{c} 2488. 588\\ 2486. 500\\ 2486. 200\\ 2486. 200\\ 2485. 009\\ 2484. 679\\ 2484. 679\\ 2482. 150\\ 2482. 150\\ 2480. 547\\ 2480. 547\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2480. 382\\ 2479. 666\\ 2479. 666\\ 2479. 666\\ 2478. 917\\ 2478. 917\\ 2478. 751\\ 2478$
 				Pun	Convergence	Calc	 	Node	24 22 24 22 24 22 24 22 24 22 24 22 24 22 22

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i	- NodeData] []]	—— LineData	1	l						
Node	出间	IJ.	EHP 1st(m)	EHP - 2nd (m)	Qc (1/S)	Remarks	Node ST EN	EN	[] []	лÜ	coef C	0 (1/s)	ر» (III) (۱۱۷)	1 (%)	H)	」。 L
25 26 28 28 28 28 29 29	2477. 738 2 2476. 355 2 2475. 965 2 2475. 803 2 2488. 463 2 2488. 465 2	2, 446, 366 2, 436, 621 2, 432, 338 2, 427, 256 2, 482, 319		31. 372 39. 734 43. 627 6. 144 6. 144	0. 107 0. 107 0. 107 0. 107 0. 107		24 25 26 29	25 26 27 30 30	37. 5 37. 5 37. 5 37. 5 37. 5	112.254 261.224 155.753 233.817 387.175	110 110 110 110	0.428 0.321 0.214 0.107 0.107	0. 388 0. 291 0. 194 0. 097 0. 097	9. 023 5. 297 2. 500 0. 693 0. 693	1. 013 1. 384 0. 389 0. 162 0. 268	0.000

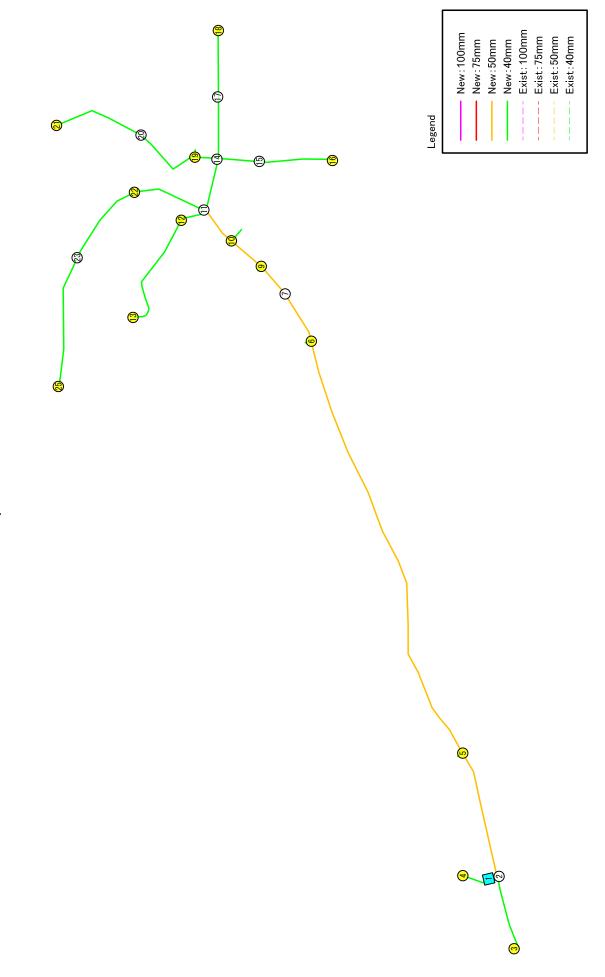
484. 585 3. 610 0. 107 3. 610 0. 107





<pre>>> - Line -</pre>	Coef Q V I HL C (1/s) (m/s) (‰) (m)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
- Line - D: D: L: L: Kater Coef: V: HL: P:	Q V (1/s) (m/s)	
- Line - D: Pressurt Coef: Water V: P: P:	Q (1/s)	
- Line - D: D: L: L: Tater 0: V: T: P:	1	
	coef C	'
otes essur level tion	ц П	$\begin{array}{c} 82.\ 469\\ 164.\ 065\\ 326.\ 205\\ 109.\ 160\\ 107.\ 358\\ 29.\ 107\\ 351.\ 117\\ 175.\ 117\\ 175.\ 117\\ 29.\ 160\\ 351.\ 88\\ 12\\ 351.\ 806\\ 141.\ 599\\ 152\\ 39.\ 102\\ 39.\ 102\\ 1$
Explanatory Notes >> Node - HP: Head Pressure GL: Ground Level EHP: Effectual Head Oc: Consumption of LineData	Q (間)	75. 37. 37. 37. 37. 37. 37. 37. 50. 37. 55. 57. 57. 57. 57. 57. 57. 57. 57. 5
Explanato Node - HP: Head GL: Grou EHP: Effe Qc: Cons LineData	de EN	22210 22200 22200 22200 22200 22200 22200 22200 22200 22200 22200 22200 22200 22200 22000 22000 22000 22000 22000 22000 22000 22000 22000 22000 2000000
	Node ST E	2219966555555511108823544222
(国) (国) (%) (%) (%)	Remarks	Reservoir Tank
53. 574 2. 501 0. 000 0. 000	Qc (1/s)	
Maximum EHP Minimum EHP Maximum V Maximum V	EHP 2nd (m)	$\begin{array}{c} 2. & 000\\ 2. & 2. \\$
•	EHP 1st (m)	· · · · · · · · · · · · · · · · · · ·
1 1 22 22 22 0 0 0 0 (cm) 2 (t ines) a	日 15	2, 547, 547 2, 547, 547 2, 547, 547 556, 064 558, 065 558, 065 558, 065 558, 065 558, 065 558, 065 558, 065 558, 065 551, 256 507, 050 2, 507, 060 2, 506, 727 2, 506, 331 2, 506, 331 2, 506, 639 2, 506, 031 2, 502, 041 2, 502, 041 2, 502, 041 2, 501, 727 2, 502, 041 2, 502, 041 2, 502, 041 2, 502, 041
	₽H.(E)	2549. 547 2549. 547 2549. 547 2549. 547 2549. 547 2549. 547 2549. 547 2549. 547 25549. 547 2555557. 547 255557. 547 255557. 547 255557. 547 25557. 5577. 5577. 5577. 5577. 5577. 55777. 5577. 5577. 55
Conve	Node	222200824008240082400 255500824000824000 255500824000 255500824000 255500824000 255500824000 255500824000 255500824000 255500824000 255500824000 255500824000 255500824000 2555008240000 2555008240000000000000000000000000000000

									P (E)	
·.,		•							H) E	0. 505 1. 721 1. 721
				pe íficient	of Flow	riow adient			I (‰)	$\begin{array}{c} 6. \\ 6. \\ 1. \\ 5. \\ 2. \\ 2. \\ 5. \\ 5. \\ 5. \\ 5. \\ 5$
			Diameter	Length of Pipe Friction Coeff	Quantity of	lic Gr	Add Pressure		ү (m/s)	0. 150 0.
			- Line - D: D		0:0		P: A		0 (1/S)	$\begin{array}{c} 2. & 150\\ 0. & 165\\ 1. & 985\\ 0. & 165\\ 1. & 654\\ 1. & 158\\ 0. & 165\\$
				Pressure	Hater				Coef . C	
		Votes >>	Pressure	ad	tion of Wat				」 〔 〔	$\begin{array}{c} 82.\ 469\\ 164.\ 100.\ 160\\ 109.\ 160\\ 107.\ 358\\ 231.\ 116\\ 107.\ 358\\ 231.\ 116\\ 107.\ 358\\ 231.\ 116\\ 107.\ 358\\ 231.\ 116\\ 107.\ 358\\ 231.\ 116\\ 102\\ 255\\ 262.\ 339\\ 152\\ 261.\ 699\\ 261.\ 699\\ 267.\ 690\\ 267.\ $
		Explanatory Notes	- Head Pr	Ground Effectu	Consumpt ion)ata — ·		75 77 77 77 77 77 77 77 77 77 77 77 77 7
		Explai	Node HP:	EIP:				- LineData	Node	255108440 255108440 255108440 255100 25500 255100 25500 2500000000
		\approx	1				,	 	No ST	551666655533311108832544222 22199666555333
		(II)	(田)	(%)	(回/S)			-	Remarks	Reservoir Tank
,	Formula>>-	39.862 (I	966		0.843 (1				0c (1/s)	-2. 150 0. 165 0. 165 0
	Hazen-Williams	Maximum EHP		Maximum I	Maximum V	·	•		EHP 2nd (m)	$\begin{array}{c} 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 $
	 73	W	X	-	Z				EHP 1st(m)	
	ie < <case< td=""><td>I</td><td>22</td><td>22</td><td>0</td><td>0. 85 (сп)</td><td>13 (times)</td><td>~ </td><td>1) E</td><td>547.547 528.065 528.065 528.065 528.827 528.827 507.050 500 500 500 500 500 500 500 500 500</td></case<>	I	22	22	0	0. 85 (сп)	13 (times)	~ 	1) E	547.547 528.065 528.065 528.065 528.827 528.827 507.050 500 500 500 500 500 500 500 500 500
	Sedie	Tank	Node	Line	Pump, Decom	gence Gap	Calculation 1	- NodeData		$\begin{array}{c} 2549 \\ 2549 \\ 547 \\ 2549 \\ 547 \\ 2549 \\ 547 \\ 321 \\ 321 \\ 321 \\ 321 \\ 321 \\ 321 \\ 321 \\ 321 \\ 321 \\ 321 \\ 323 \\ 331 \\ 335 \\ 3$
	 				2 .	Convergence	Ca	1	Node	- 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
				·						



Dibo Pipe Networks

٤								- d (目)	0. 000 0. 000									0.000				0.000
					,			H (B)	0.000 0.000			0. 000 0. 000						0.000				0.000
			pe	Coefficient of Flow	f Flow Gradient		-	[(‰)													0.000	
			44		city o aulic	Head Loss Add Pressure		V (ш/s)	0, 000 0, 000 0, 000		0.000			0, 000 0, 000				0.000				0. 000 0. 000
						HL : H P : A		ი (1/s)	0. 000 0. 000 0. 000		0.000							0,000			0. 000 0. 000	0. 000 0. 000
				Pressure Water				Coef C	110	110	110	110	110	110	110	110	110	110	110		110 110	110
	<< Explanatory Notes >>			of			1	」 [1]			861.812 104 105			75. 833 80. 550	51.921	143.415	235.909 81.991	120.299			<u></u> :	131. 438 255. 236
	natory	ء - ا ا	Head Pressur Ground Level	EIIectual He Consumption	,		Data —	C (IIII)	50.0 37.5 37.5													
	(Expla	- Node	55 10 10	CC:			- LineData	Nod <i>e</i> T EN	246	ഹ	9 6	- ∞	6	21	12	22	<u>1</u> 1 2	17	919	20	21 23	24 25
	⇒	•		•				ST		20	ഗഴ	- -	(- c	۹ 10	11	:=:	14	14	r o i	19	$20 \\ 22$	23
	(田)	(<u>I</u>)	(%o)	(町/ S)				Remarks	Reservoir Tank							•						
ormula>>-	52. 609	5.945	0.000	0.000	x			0c (1/s)	-0, 000 0, 000 0, 000		0,000							0,000			0.000	0.000
: Hazen-Williams Formula>>	Maximum EHP	Minimum EHP	Maximum I	Maximum V				EHP 2nd (m)	8. 000 8. 000 5. 945		11.515 33 453		34. 142	30. 043 38. 139	40.947 40.972	39.800	43.084	41.785 47.486			52.609 45.374	36. 085 50. 617
								EHP 1st(m)														
oo < <case.1< td=""><td>1</td><td>25</td><td>25</td><td>0</td><td>0.00 (cm)</td><td>2 (times)</td><td> </td><td>13 15</td><td>2, 452, 637 2, 452, 637 2, 454, 692</td><td>452.</td><td>449</td><td>425.</td><td>426.</td><td>420. 422.</td><td>419.</td><td>420.</td><td>410. 417.</td><td>418. 413.</td><td>410.</td><td>410. 411.</td><td>408. 415.</td><td>2, 424, 553 2, 410, 020</td></case.1<>	1	25	25	0	0.00 (cm)	2 (times)	 	13 15	2, 452, 637 2, 452, 637 2, 454, 692	452.	449	425.	426.	420. 422.	419.	420.	410. 417.	418. 413.	410.	410. 411.	408. 415.	2, 424, 553 2, 410, 020
Dibo	Tank	Node	Line	Pump, Decom	ence Gap	Calculation	NodeData	en (je)	2460. 637 2460. 637 2460. 637 2460. 637	637	637 637	637	637 c 9.7	637 637	637 637	637	637 637	2460. 637 2460. 637	637	637 637	$637 \\ 637 $	2460. 637 2460. 637
	-			Pu	Convergence	Cal	 	Node	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~													

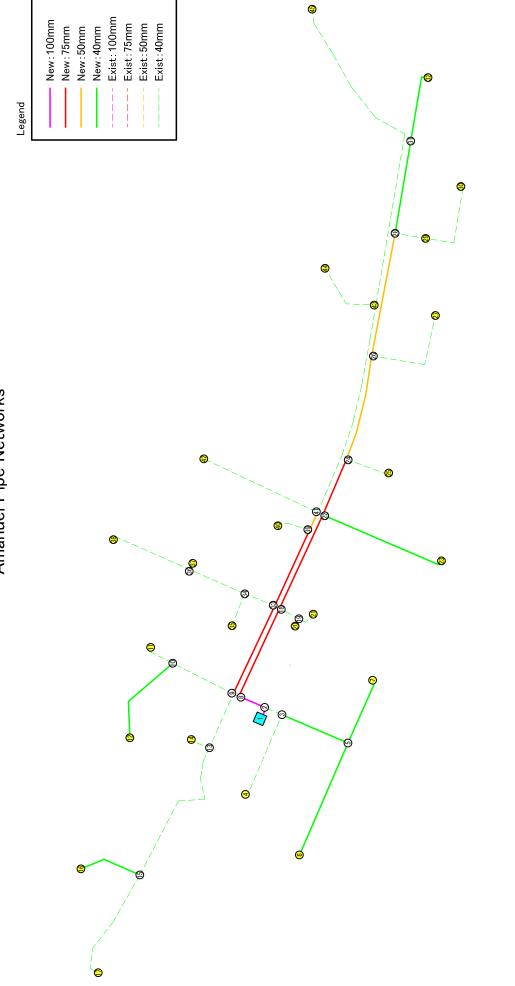
		d (ij	0. 000										
		日 日 日	0.000								•		
		1 (%)	0.000										
		V (п/s)	0.000										ı
		Q (1/S)	0. 000	, J									
		Coe f C	110										
	ł	-ц Ц	157. 144										
	Data —	(IIII)	26 37.5										
·	——— LineData	Node ST EN	25 26			1							
		Remarks						.'					
		Qc (1/S)	0. 000 0. 000										
-		EHP 2nd (m)	40.972 39.619										
		EHP 1st(m)										·	
	 	13 (E	2, 419, 665 2, 421, 018										
	- NodeData		2460. 637 .2 2460. 637 2					-		-			
		Node	25 26										

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						:		d (III)	
		;						H E	$\begin{array}{c} 0. & 341 \\ 0. & 341 \\ 0. & 056 \\ 0. & 141 \\ 1. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 102 \\ 0. & 103 \\ 0. & 103 \\ 0. & 113 \\ 0. & 103 \\ 0. & 103 \\ 0. & 113 \\ 0. & 102 \\ 0. & 103 \\ 0. & 102 \\ 0. &$
			pe	Coefficient of Flow	f Flow Gradient			1 (%)	$\begin{array}{c} 19. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ $
					city o aulic	Head Loss Add Pressure		V (加/S)	0. 115 0. 115 0. 115 0. 580 0. 580 0. 115 0. 387 0. 115 0.
			ä. 	Coel: F Q: Q		HL: H P: A		0 (1/s)	$\begin{array}{c} 1. & 392\\ 0. & 127\\ 0. & 127\\ 1. & 265\\ 1. & 128\\ 1. & 128\\ 1. & 128\\ 0. & 128\\ 0. & 128\\ 0. & 128\\ 0. & 127\\$
				Fressure Water				Coef C	
	<< Explanatory Notes >>		Pressure d Level	Ellectual Head Fr Consumption of Wa			1	ц ш	17. 292 59. 380 59. 380 59. 380 59. 380 59. 380 247. 922 861. 812 861. 812 861. 812 861. 812 861. 812 861. 812 104. 195 101. 411 101. 411 101. 411 101. 411 1120. 299 81. 999 121. 783 141. 846 170. 266 171. 836 171. 836 171. 836 171. 836 171. 836 171. 836 171. 836 171. 836 171. 836 171. 836
	natory]	;	Head Fressur Ground Level	El lec lu Consump			Data -		227.55 23
	(Expla	- Node		CC: 1			- LineData	Node	2253108669733275710 22531086697335757573757 227310877227577777777777777777777777777777777
i.	∻						 	ST	332209755555555555555555555555555555555555
	(田)	(II)	(%)	(II/S)				Remarks	Reservoir Tank
⁷ ormula>>-	32. 658	5. 463	19, 695	0.709				Qc (1/s)	$\begin{smallmatrix} -1 \\ -1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
: Hazen-Williams Formula>>	Maximum EHP	Minimum EHP	Maximum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 8. & 000\\ 7. & 944\\ 7. & 944\\ 7. & 944\\ 17. & 83\\ 15. & 659\\ 77. & 833\\ 16. & 764\\ 18. & 767\\ 19. & 777\\ 22. & 068\\ 23. & 390\\ 22. & 068\\ 23. & 390\\ 22. & 068\\ 23. & 390\\ 22. & 058\\ 23. & 390\\ 22. & 058\\ 23. & 390\\ 24. & 059\\ 25. & 658\\ 26. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 29. & 658\\ 20. & 598$
							·	EHP 1st (m)	
oo < <case.2< td=""><td>_</td><td>25</td><td>25</td><td>0</td><td>0.53 (cm)</td><td>14 (times)</td><td></td><td>13</td><td>$\begin{array}{c} 2, \ 452, \ 637\\ 2, \ 452, \ 637\\ 2, \ 454, \ 692\\ 2, \ 454, \ 692\\ 2, \ 452, \ 637\\ 2, \ 425, \ 637\\ 2, \ 425, \ 537\\ 2, \ 425, \ 537\\ 2, \ 425, \ 537\\ 2, \ 419, \ 560\\ 2, \ 418, \ 552\\ 2, \ 552\\ 2, \ 418, \ 552\\ 2, \ 552\ 2, \ 552\\ 2, \ 552\ 2, \ 55$</td></case.2<>	_	25	25	0	0.53 (cm)	14 (times)		13	$\begin{array}{c} 2, \ 452, \ 637\\ 2, \ 452, \ 637\\ 2, \ 454, \ 692\\ 2, \ 454, \ 692\\ 2, \ 452, \ 637\\ 2, \ 425, \ 637\\ 2, \ 425, \ 537\\ 2, \ 425, \ 537\\ 2, \ 425, \ 537\\ 2, \ 419, \ 560\\ 2, \ 418, \ 552\\ 2, \ 552\\ 2, \ 418, \ 552\\ 2, \ 552\ 2, \ 552\\ 2, \ 552\ 2, \ 55$
Dibo	Tank	Node	Line	Pump, Decom	ence Gap	Calculation 14	NodeData	出间	4460, 637 4460, 637 4460, 581 4460, 581 4460, 581 4460, 581 4444, 499 4441, 758 4441, 758 4441, 758 4440, 914 440, 914 440, 913 4440, 686 440, 1724 440, 172
	•			Pu	Convergence	Cal		Node	55555662555555555555555555555555555555

									,		м	
·	۲. ط	0. 000										
	H (B)	0. 000	, ,		•							
	I (‰)	0.000										
	V (m/s)	0. 000		÷	-			·		•		
	Q (1/S)	0. 000										
	Coef C	110	þ				. .					
l	」 (目	157. 144										
Data	Q (回)	37. 5										
LineData	Node ST EN	25 26	-									
	Remarks											
	0c (1/s)	0. 127 0. 000										
	EHP 2nd (m)	20. 234 18. 881										
	EHP 1st (m)											
 	19	2, 419. 665 2, 421. 018			-							
- NodeData -	E (II)	2439. 899 2 2439. 899 2				·					•	
	Node	25										



Amanuel Pipe Networks

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								王间	000 000 000 000 000 000 000 000 000 00
				ficient low	f Flow Gradient			I (%)	
			Diameter Length of Pipe	: Friction Coefficient Quantity of Flow	Velocity of H Hydraulic Gra	Head Loss Add Pressure		V (п/s)	
		•	<u> </u>	Coef: Fr Q: Qu		HL: Heac P: Add	-	0 (1/s)	
				Pressure Water				Coef C	
	otes >>		evel evel	tion of Wat			- · 	[田]	$\begin{array}{c} 28.598\\ 43.799\\ 64.943\\ 64.943\\ 64.943\\ 167.220\\ 167.220\\ 156.993\\ 136.127\\ 156.993\\ 136.127\\ 127\\ 225.047\\ 225.047\\ 225.047\\ 225.047\\ 225.047\\ 136.906\\ 148.405\\ 127\\ 225.047\\ 127\\ 127\\ 129\\ 127\\ 129\\ 127\\ 129\\ 127\\ 129\\ 129\\ 120\\ 129\\ 120\\ 129\\ 120\\ 129\\ 120\\ 120\\ 120\\ 120\\ 120\\ 120\\ 120\\ 120$
	<< Explanatory Notes >>		Head Pressure Ground Level	Ellectual H Consumption			LineData —-	(IIII)	100. 0 37. 5 37. 5 5 37. 5 5 37. 5 5 37. 5 5 37. 5 5 37. 5 5 37. 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
	(Expla	- Node		LHF: Qc:			- Line	Node T EN	5 31025551545111313084833555555555555555555555555555555555
1	⇒	,						ST	55566882227390066882237 55566882227900668882275
· · · · · · · · · · · · · · · · · · ·	(II)	(II)	(%)	(m/s)				Remarks	Reservoir Tank
Formula)	36. 735 (7.360 (0.000 (0. 000 (Qc (1/S)	
Hazen-₩illiam	faximum EHP	Minimum EHP	Maximum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 8\\ 2& 2& 0\\ 2& 2& 2& 0\\ 2& 2& 2& 2& 2& 2& 2& 2& 2& 2& 2& 2& 2& $
· ··	W	24	24	A				EHP 1st (m)	
Amanuel < <case.< td=""><td>1</td><td>44</td><td>44</td><td>0</td><td>0.00 (cm)</td><td>2 (times)</td><td>[</td><td>」 し じ じ</td><td>387. 780 388. 780 388. 858 388. 858 388. 858 388. 858 388. 858 388. 858 388. 858 388. 858 388. 858 388. 856 388. 856 388. 856 388. 856 388. 856 388. 856 388. 856 388. 870 388. 871 371. 777 388. 847 388. 847 388. 818 388. 819 370. 847 388. 810 373. 818 388. 817 388. 817 379. 847 388. 532 388. 532 373. 532</td></case.<>	1	44	44	0	0.00 (cm)	2 (times)	[」 し じ じ	387. 780 388. 780 388. 858 388. 858 388. 858 388. 858 388. 858 388. 858 388. 858 388. 858 388. 858 388. 856 388. 856 388. 856 388. 856 388. 856 388. 856 388. 856 388. 870 388. 871 371. 777 388. 847 388. 847 388. 818 388. 819 370. 847 388. 810 373. 818 388. 817 388. 817 379. 847 388. 532 388. 532 373. 532
— — Amaı	Tank	Node	Line	Pump, Decom	gence Gap	Calculation	- NodeData	HP (II)	23395, 780 23395, 780
i				P	Convergence	Ca		Node	

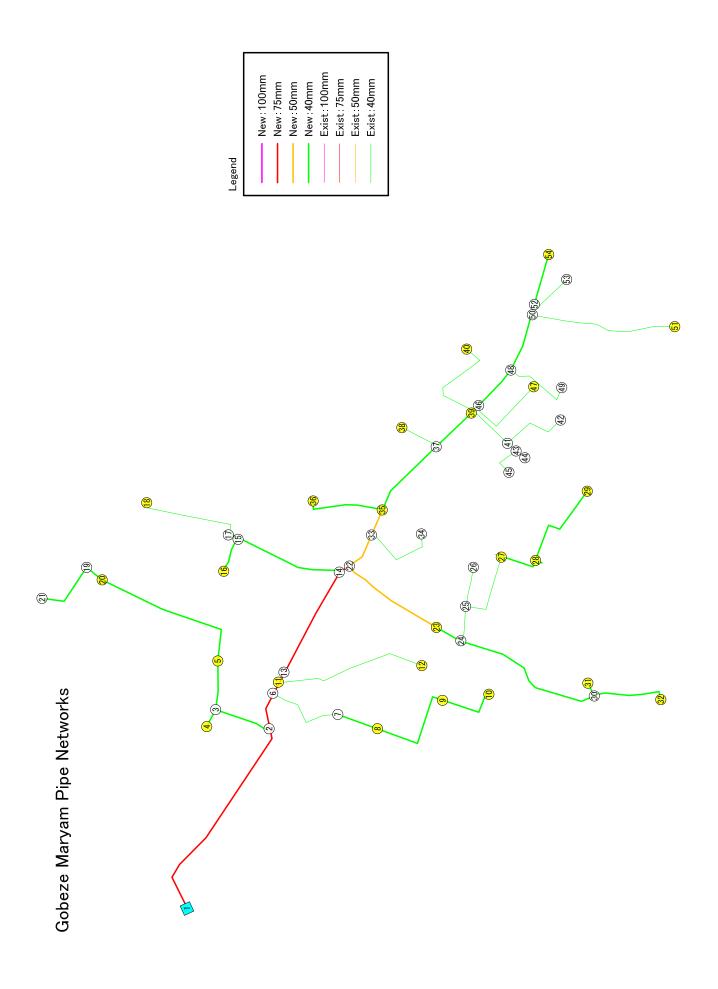
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	Р (п)			0.000																	
	HL E			0. 000									_	_	_	_	_	_	_	_	
	I (%)	0.000		0.000																	
	V (m∕s)	0.000	0.000	0. 000 0. 000	0.000	0.000	0.000	0.000	0.000	0. 000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
	Q (1/S)	0.000	0.000	0. UUU	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
	Coef C	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	
[.	-) (jj	105.811																			
LineData —	(I) (I)	$\frac{37.5}{2}$																			
- Line	Node ST EN	25	97 97	12	29	31	30	32	34	39	35	36	37	30	40	41	42	43	44	45	
	ST	24	24	07 96	28	28	29	31	ŝ	33	34	34	36	36	39	39	41	41	43	43	
	Remarks																				
	Qc (1/s)	0.000																			
	EHP 2nd (m)	13. 261																			
	EHP 1st (m)																				
	15 日 日	2, 382, 519	019. 281	378	381.	382.	380.	380.	382.	333.	383.	381.	381.	365.	382.	383.	382.	366.	382.	365.	375.
- NodeData	H)	2395. 780	780	780	780	780	780	780	780	780	180	180	08/	780	780	780	780	180	780	780	
 	Node	22	076	28	29	30	5	32	3	34		36	<u>0</u>	38	68	40	41	42	43	44	45

۰.								ط (ال														0. 000 0. 000 0. 000
							·	H H	0.338 1 307													0. 170 1. 181 0. 368
	pe fficient Flow adient							I (%)	11.820 29.844												3.003	3.902 3.902 2.628
		e - D: Diameter L: Length of Pipe f: Friction Coefficient 0: Quantity of Flow V: Velocity of Flow 1: Hydraulic Gradient L: Head Loss P: Add Pressure						ү (m/s)	0.833 0.740			0.247		0.494 0.404					0.247			$\begin{array}{c} 0. \ 247 \\ 0. \ 247 \\ 0. \ 308 \end{array}$
	- Line - D: Dia L: Len Coef: Friv Q: Quai V: Vel HL: Hea P: Add						0 (1/s)	6.538 0.817													0. 272 0. 272 1. 362	
	Pressur¢ Wåter					coef c	110	110	110	110	110	110	110	110	110	110	110	110	110	110		
	es >> ure Head n of					1	」 (回)	28.598 43.799					223.946 156 993							19. 150	43. 526 302. 739 139. 919	
	natory A	ب - ا =	Head Pressur Ground Level	Consumption			LineData —	C (IIII)	100. 0 37. 5	100.0 37 F		~ ~	<u>- ы</u>	75. 0 37. 5	- L		2					37. 5 37. 5 75. 0
	K Expla	- Node	Node HP: : GL: : Qc: :				- Line	Node T EN														23 24
ļ	\sim						1 [ST		25	ົ	un un	~~~	ω σ	000	л <u>С</u>	10	<u> </u>	15	18	<u>6</u>	$^{19}_{22}$
<	(8)	(日)	(%)	(II/S)				Remarks	Reservoir Tank													
ns Formula	32.118	3. 166	29.844	0.833				ც c (1/s)	-6.538 0.000			0.272 0.272		0.000	0. 272	0. 000	0.272 0.000	0. 272	0. 272 0. 000	0.000	0. 272	0. 000 0. 272 0. 000
Hazen-Williams Formula>>	Maxinum EHP	Minimum EHP						EHP 2nd (m)	8.000 7.022	10.277 10.016			8.842	9.501 16.612	18.010	4. 606	8. 536 6. 591	12.880	14. 645 11. 522	13.279	15. 704	10. 559 13. 560 9. 659
< <case. 2="" :="" ii<="" td=""><td>L</td><td>l</td><td></td><td></td><td></td><td></td><td></td><td>EHP 1st(m)</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></case.>	L	l						EHP 1st(m)														
Amanuel < <ca< td=""><td>1</td><td>44</td><td>44</td><td>0</td><td>0.89 (cm)</td><td>14 (times)</td><td>- </td><td>٦ ت</td><td>387. 388.</td><td></td><td>363.</td><td>361. 359.</td><td>386.</td><td>375</td><td>374. 366</td><td>385. 385.</td><td>2, 381. 832 2. 378. 646</td><td>371.</td><td>308. 381.</td><td></td><td>376.</td><td>2, 302, 000 2, 377, 818 2, 382, 532</td></ca<>	1	44	44	0	0.89 (cm)	14 (times)	- 	٦ ت	387. 388.		363.	361. 359.	386.	375	374. 366	385. 385.	2, 381. 832 2. 378. 646	371.	308. 381.		376.	2, 302, 000 2, 377, 818 2, 382, 532
— — — Ami	Tank	Node	Line	Pump, Decom	ence Gap	Calculation 14	· NodeData	E (II)	780 442	$135 \\ 324$	617	679 162	842	624 412	135 555	561	$368 \\ 236 $	657	u18 437	720 646		2392. 191 2392. 191
 				Ρu	Convergence	Cal		Node														57 57 57 57 57 57 57 57 57 57 57 57 57 5

	d (II)	
	۱ H	$\begin{array}{c} 0.413\\ 0.413\\ 0.940\\ 0.940\\ 0.792\\ 0.506\\ 0.778\\ 0.566\\ 0.297\\ 0.643\\ 0.643\\ 0.643\\ 0.643\\ 0.643\\ 0.643\\ 0.643\\ 0.643\\ 0.040\\ 0.778\\ 0.040\\ 0.778\\ 0.040\\ 0.778\\ 0.040\\ 0.778\\ 0.040\\ 0.$
	I (%)	$\begin{array}{c} 12.523\\ 12.523\\ $
	V . (m/s)	$\begin{array}{c} 0. & 247 \\ 0. & 547 \\ 0. & 247 \\ 0. &$
	0 (1/s)	$\begin{array}{c} 0. & 272 \\ 1. & 090 \\ 0. & 2172 \\ 0$
	coef C	
I [ц П	105. 811 246. 807 246. 807 240. 833 240. 833 71. 523 71. 523 75. 399 192. 406 75. 399 192. 406 137. 879 192. 446 137. 879 192. 446 76. 087 45. 179 291. 533 499. 885 164. 865 772. 496
LineData —	D (IIII)	37.5 50.0 57.5 57.5 57.5 57.5 57.5 57.5 5
– Line	Node ST EN	$\begin{smallmatrix} & & & & & & \\ & & & & & & \\ & & & & & $
Ì	ST	$\begin{array}{c} 228\\ 248\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238\\ 23$
	Remarks	
-	0c (1/s)	$\begin{array}{c} 0. & 272 \\ 0. &$
	EHP 2nd (m)	$\begin{array}{c} 9.\ 260\\ 6.\ 744\\ 6.\ 744\\ 7.\ 267\\ 7.\ 265\\ 7.\ 272\\ 9.\ 601\\ 9.\ 601\\ 10.\ 601\\ 10.\ 335\\ 10.\ 30\ 10.\ 30\\ 10.\ 30\ 10.\ 30\ 10\ 10\ 10\ 10\ 10\ 10\ 10\ 10\ 10\ 1$
	EHP 1st(m)	· · ·
 	Ē	 2, 382, 519 2, 379, 000 3, 379, 000 3, 379, 016 3, 378, 1417 3, 378, 1417 3, 381, 417 3, 381, 417 3, 381, 381, 417 3, 381, 382, 016 3, 382, 057 3, 382, 057 3, 382, 000 2, 382, 500 3, 375, 118
· NodeData	H)	2391. 778 23391. 778 23385. 974 23385. 974 23385. 974 23385. 974 23385. 138 23395. 138 23395. 149 52392. 140 23392. 140 23392. 140 23387. 824 23387. 824 23387. 824
 	Node	22222222222222222222222222222222222222



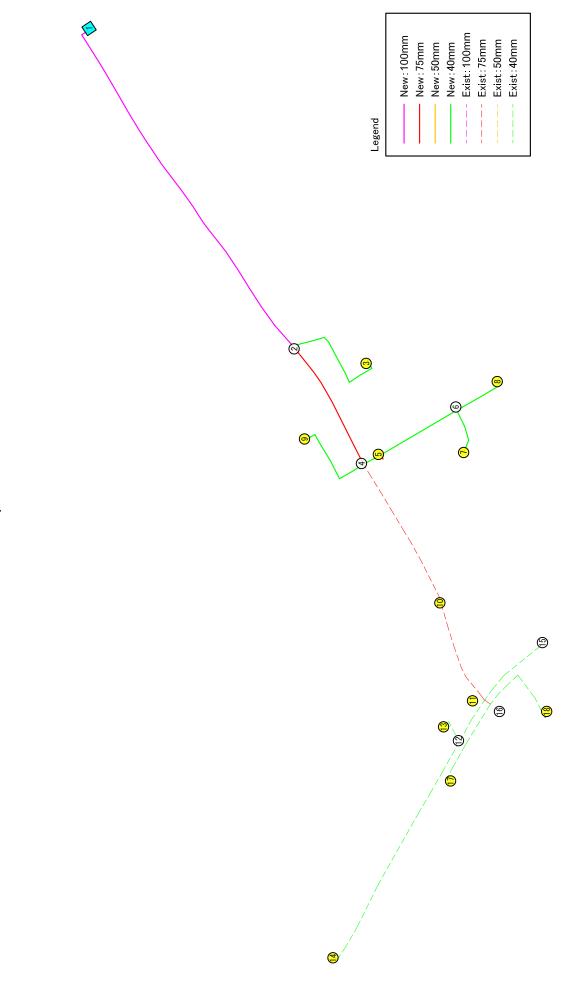
					·		-		ط (آل	$\begin{smallmatrix} & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & & \\ & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & & \\ & & & $
									H (II)	
				Pipe	efficient Flow	f Flow Gradient	, D		(%) I	
				Diameter Length of P		0	Head Loss Add Pressure		V (面/S)	
			1	<u>.</u>			HL: H P: A		Q (1/s)	
					Pressure Water				coef C	
		<< Explanatory Notes >>		Head Fressure Ground Level					」 日	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
		natory [.]	ء - ا ا	Ground	EITECTUAL H Consumption			LineData —	(Ium)	75. 77. 77. 77. 77. 77. 77. 77. 77. 77.
	I	(Expla	- Node HP: - GL: GL: Qc:				- Line	Node	23 23 23 23 23 23 23 23	
] 	⇒	ı					i I	ST	22229997155544 332229997155544 232229997155544
	Formula>>	(田)	(II)	(%)	(s/m)				Remarks	Reservoir Tank
	Hazen-Williams	58. 697	0.000	0.000	0.000				0c (1/s)	
	 ,	Maximum EHP	Minimum EHP	Maxinum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0 & 000 \\ 37. & 955 \\ 37. & 955 \\ 47. & 485 \\ 47. & 485 \\ 47. & 485 \\ 47. & 485 \\ 47. & 485 \\ 48. & 240 \\ 57. & 827 \\ 57. & 827 \\ 57. & 827 \\ 57. & 827 \\ 57. & 827 \\ 57. & 827 \\ 57. & 827 \\ 57. & 827 \\ 57. & 826 \\ 57. & 831 \\ 57. & 831 \\ 56. & 831 \\ 57. & 497 \\ 56. & 831 \\ 57. & 497 \\ 57. & 497 \\ 57. & 497 \\ 57. & 497 \\ 57. & 897 \\ 5$
	I < <case.< td=""><td>Æ</td><td>æ</td><td>Æ</td><td>ž</td><td></td><td></td><td></td><td>EHP 1st (m)</td><td>46. 493</td></case.<>	Æ	æ	Æ	ž				EHP 1st (m)	46. 493
	Gobeze Maryam	1	53	53	1	0.00 (cm)	2 (times)	 	٦) E	2 243 367 2 205 414 2 195 382 2 195 382 2 195 382 2 195 382 2 195 382 2 195 382 2 197 127 2 197 127 2 197 127 2 196 871 2 198 264 2 178 566 2 178 566 2 178 566 2 178 566 2 178 566 2 178 582 2 178 582 2 178 582 2 178 560 2 178 561 2 178 550 2 179 550 2 179 550 2 177 550 2
	Go	Tank	Node	Line	Рипр, Лесол	gence Gap	Calculation	- NodeData	H)	 22243. 367 2196. 874 2196. 874 2196. 874 2196. 874 2196. 874
	 				Pı	Convergence	Ca	 	Node	-222200846526284

	。 (田)	
	H (E	
	(%) I	
	V (四/S)	
	Q (1/S)	
	Coef C	
	, 」(副	78. 635 345. 446 95. 922 95. 922 95. 922 168. 380 89. 267 89. 267 70. 878 60. 878 60. 878 60. 878 171. 888 171. 888 88. 012 74. 456 75. 651 194. 022 116. 222 25. 812 25. 812
)ata —	U (IIII)	337.55 37.55 3
- LineData	Node ST EN	$\begin{smallmatrix} & & & & & & & & & & & & & & & & & & &$
 	ST Nc	$\begin{array}{c} 224\\ 225\\ 225\\ 225\\ 225\\ 225\\ 225\\ 225\\$
	Remarks	
	Qc (1/s)	
	EHP 2nd (m)	$\begin{array}{c} 23.82\\ 33.553\\ 33.553\\ 33.553\\ 33.553\\ 33.553\\ 33.553\\ 33.553\\ 33.553\\ 372\\ 11.2\\ 25.355\\ 590\\ 550\\ 550\\ 550\\ 550\\ 550\\ 550\\ 5$
	EHP 1st (m)	
NodeData	E (E	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	E E	$\begin{array}{c} 2196. \ 874\\ 374\\ 374\\ 374\\ 374\\ 374\\ 374\\ 374\\ 3$
 	Node	22222222222222222222222222222222222222

		,							۲ ا	$\begin{array}{c} \begin{array}{c} & & & \\ & & & & \\ & & & \\ & & & & \\ & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & $
									H)	$\begin{array}{c} \textbf{8.455}\\ \textbf{1.1220}\\ \textbf{1.1220}\\ \textbf{1.1330}\\ 1.1$
				ipe	efficient Flow	Flow radient	0		I (‰)	$\begin{smallmatrix} 17, 426\\ 18, 463\\ 12, 433\\ 12, 433\\ 10, 161\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 10, 838\\ 115\\ 11, 417\\ 115\\ 11, 417\\ 115\\ 12, 820\\ 11, 417\\ 12, 820\\ 12$
				: Diameter : Length of Pipe	Priction Coe Quantity of	Velocity of Hydraulic Gr	Head Loss Add Pressure		V (元/S)	$\begin{array}{c} 0.0000 \\ 0.000$
			- Line -	- - -	Coel: F				(s∕1) ∘	$^{-1}$ $^{-1$
					Fressure Water				Coef C	
		Votes >>		-	2 5			1	ц Ц	$\begin{array}{c} 485,\ 203\\ 128,\ 621\\ 84,\ 885\\ 43,\ 447\\ 109,\ 350\\ 178,\ 748\\ 333,\ 324\\ 337,\ 327\\ 16,\ 411\\ 178,\ 748\\ 337,\ 327\\ 179,\ 796\\ 11,\ 960\\ 129\\ 233,\ 157\\ 263\\ 377\\ 796\\ 11,\ 960\\ 129\\ 233,\ 157\\ 263\\ 377\\ 796\\ 11,\ 960\\ 129\\ 233,\ 157\\ 796\\ 11,\ 960\\ 129\\ 246,\ 241\\ 263\\ 232,\ 157\\ 263\\ 246,\ 241\\ 263\\ 246,\ 241\\ 263\\ 232,\ 157\\ 263\\ 246,\ 242\\ 263\\ 262\\ 262\\ 262\\ 262\\ 262\\ 262\\ 26$
	·	Explanatory Notes	- Decu	Ground Level	Ellectual Hee Consumption o			Data —		75. 75. 75. 75. 75. 75. 75. 75.
	t	Explai	Node					LineData	de EN	233325008110081149881 2333550887166332 2333550887166332
		\approx	I					 	Node	2222999577557444311198876663332221 222299995775574443
	Formula>>	(II)	(田)	(%)	(四/3)				Remarks	Reservoit Tank
۰	lliams	44.776	0.000	27.911	0.857				Qc (1/S)	-3.784 0.000 0.15800000000000000000000000000000000000
	.2 : Hazen-Wi	Maximum EHP	Minimum EHP	Maximum I	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0. \ 000\\ 29. \ 155\\ 29. \ 155\\ 36. \ 593\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 415\\ 37. \ 416\\ 38. \ 596\\ 38. \ 596\\ 38. \ 596\\ 13. \ 990\\ 10. \ 816\\ 10. \$
	< <case.< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>EHP 1st(m)</td><td>36. 556</td></case.<>								EHP 1st(m)	36. 556
	Gobeze Maryam	1	53	53	-	0.55 (cm)	16 (times)	3 	٦ <u>(</u>	f 2, 243. 367 f 2, 243. 367 f 2, 205. 414 f 2, 195. 382 f 2, 195. 337 f 2, 195. 337 f 2, 197. 337 f 2, 196. 470 f 2, 196. 626 f 1, 127 f 2, 196. 626 f 2, 177. 335 f 2, 176. 768 f 2, 176. 550 f 2, 179. 953 f 2, 179. 953 f 2, 179. 953 f 2, 179. 953
		Tank	Node	Line	Pump, Decom	gence Gap	Calculation	- NodeData	E C	$\begin{array}{c} 22243. \ 367\\ 22342. \ 367\\ 2232. \ 573\\ 2232. \ 573\\ 2232. \ 573\\ 2223. \ 575\\ 2223. \ 648\\ 22233. \ 556\\ 22233. \ 556\\ 22233. \ 556\\ 22233. \ 556\\ 22233. \ 556\\ 22233. \ 556\\ 22233. \ 566\\ $
					Ч	Convergence	Ca		Node	22222222222222222222222222222222222222

.

	d (E)	
	H H	0. 125 0. 233 0. 125 0. 238 0. 2388 0. 2388 0. 2388 0. 2388 0. 2388 0. 2388 0. 2388 0. 2388 0
	I (‰)	$\begin{array}{c} 10. \\ 5. 115 \\ 5. 115 \\ 5. 115 \\ 5. 115 \\ 5. 115 \\ 5. 115 \\ 1. 417 \\ 1. 417 \\ 1. 417 \\ 1. 417 \\ 1. 417 \\ 1. 417 \\ 1. 417 \\ 1. 417 \\ 1. 417 \\ 0. 000 \\$
	۲ (m/s)	$\begin{array}{c} 0. & 428\\ 0. & 286\\ 0. & 286\\ 0. & 000\\ 0. & 143\\ 0. & 000\\ 0. & 143\\ 0. & 000\\ 0. & 143\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 000\\ 0. & 143\\ 0. & 000\\$
	0 (1/s)	$\begin{array}{c} 0. \ 473\\ 0. \ 473\\ 0. \ 315\\$
	Coef C	
1	고(世	$\begin{array}{c} 78. \ 635\\ 345. \ 446\\ 95. \ 922\\ 168. \ 380\\ 168. \ 380\\ 168. \ 380\\ 168. \ 380\\ 171. \ 888\\ 171. \ 888\\ 171. \ 888\\ 174. \ 858\\ 174. \ 858\\ 174. \ 858\\ 174. \ 858\\ 174. \ 858\\ 122. \ 353\\ 162. \ 353\\ 25. \ 812\\ 25. \ 812\\ 25. \ 812\\ 25. \ 812\\ 25. \ 812\\ 25. \ 812\\ 25. \ 812\\ 25. \ 353\\ 162. \ 353\\ 25. \ 258\\ 330\\ 161. \ 267\ 161. \ 267\ 161. $
)ata —	(IIII)	
- LineData	Node ST EN	5222220668448758478 522220668448758479 5222206684487587583333355728322 5225206684487587575833333555728325 522520668448755757575757575757575757575757575757
 	No ST	222002844444444 222002844444444 25200888833333333333333337252544
	Remarks	
	Qc (1/s)	$\begin{array}{c} 0.000\\ 0.158\\ 0.158\\ 0.000\\ 0.000\\ 0.158\\ 0.158\\ 0.158\\ 0.158\\ 0.158\\ 0.158\\ 0.000\\ 0.158\\ 0.158\\ 0.000\\ 0.158\\ 0.000\\ 0.158\\ 0.000\\ 0.158\\ 0.000\\ 0.158\\ 0.000\\ 0.158\\ 0.000\\ 0.158\\ 0.000\\ 0.158\\ 0.000\\ 0.158\\ 0.000\\ 0.000\\ 0.158\\ 0.000\\ 0.000\\ 0.158\\ 0.000\\ 0.000\\ 0.158\\ 0.000\\ 0.$
	EHP 2nd (m)	$\begin{array}{c} 16. \\ 864 \\ 22. \\$
	EHP 1st(m)	
 	J)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
NodeData	E (E)	$\begin{array}{c} 2189. \ 917\\ 2189. \ 917\\ 2188. \ 092\\ 2187. \ 639\\ 2187. \ 635\\ 2187. \ 635\\ 2188. \ 692\\ 2188. \ 635\\ 2193. \ 694\\ 2193. \ 694\\ 2193. \ 694\\ 2193. \ 694\\ 2195. \ 657\\ 2195. \ 657\\ 2185. \ 657$
 [Node	22222222222222222222222222222222222222



Bikolo Pipe Networks

								ط (آ	
	•							H)	·
:				Coefficient of Flow	f Flow Gradient			(%) I	
			••	Friction Coe Quantity of	0	Head Loss Add Pressure		V (m/s)	
		- Line -				HL: H P: A		0 (1/s)	
				Pressure Vater				Coef C	
	<< Explanatory Notes >>	·	-	of			1	」 (単)	823. 886 257. 828 296. 953 44. 415 96. 106 117. 885 346. 203 346. 203 346. 203 104. 219 104. 219 104. 219 104. 219 110. 239 110.
	natory	ء - ا ا	Head Pressure Ground Level	Ellectual H Consumption			LineData —	(um)	100.0 37.5 37.5 37.5 37.5 37.5 37.5 37.5 37.5
	Expla		н.: С	EHL: Oc:			- Line	Node ST EN	84484352108446954332
	\approx	I						ST	166122111046665544222
<	(里)	· (U)	(‰)	(m/s)				Remarks	Reservoir Tank
s Formula	51, 220	16.200	0: 000	0. 000				Qc (1/S)	
Hazen-Williams Formula>>	Maximum EHP	Minimum EHP	Maximum I [,]	Maximum V				EHP 2nd (m)	$\begin{array}{c} 0. \ 000\\ 16. \ 200\\ 23. \ 590\\ 23. \ 590\\ 23. \ 590\\ 23. \ 590\\ 23. \ 590\\ 37. \ 570\\ 370\\ 37. \ 570\\ 370\\ 370\\ 370\\ 370\\ 370\\ 370\\ 370\\ 3$
••								EHP 1st (m)	· · ·
—Bikolo < <case.1< td=""><td>-</td><td>17</td><td>17</td><td>0</td><td>0.00 (cm)</td><td>2 (times)</td><td> </td><td>13 13</td><td>1, 953. 020 1, 953. 020 1, 936. 820 1, 932. 430 1, 923. 430 1, 923. 430 1, 923. 130 1, 932. 910 1, 932. 910 1, 932. 910 1, 932. 910 1, 932. 910 1, 932. 920 1, 917. 290 1, 915. 370 1, 915. 450 1, 915. 450 1, 915. 450</td></case.1<>	-	17	17	0	0.00 (cm)	2 (times)	 	13 13	1, 953. 020 1, 953. 020 1, 936. 820 1, 932. 430 1, 923. 430 1, 923. 430 1, 923. 130 1, 932. 910 1, 932. 910 1, 932. 910 1, 932. 910 1, 932. 910 1, 932. 920 1, 917. 290 1, 915. 370 1, 915. 450 1, 915. 450 1, 915. 450
— — — Bi	Tank	Node	Line	Pump, Decom	gence Gap	Calculation	— NodeData	E I	$\begin{array}{c} 1953.020\\ 1955.020\\$
I				е ц ,	Convergence	Ca		Node	846543210984654321

								ط (ال	
								HL.	$\begin{array}{c} 2. & 337\\ 1. & 024\\ 1. & 024\\ 1. & 024\\ 1. & 349\\ 0. & 741\\ 1. & 349\\ 0. & 741\\ 1. & 297\\ 0. & 606\\ 0. & 468\\ 0. & 249\\ 0. & 249\\ 0. & 249\\ 0. & 214\\ 0. & 204\\ 0. & 214\\ 0. & 804\\$
			pe	Coefficient of Flow	f Flow Gradient			I (%)	$\begin{array}{c} 2.836\\ 9.651\\ 3.970\\ 3.970\\ 3.970\\ 3.970\\ 3.970\\ 3.971\\ 3.$
·			Diameter Length of Pipe		city o aulic	Head Loss Add Pressure		V (国/ S)	$\begin{array}{c} 0. & 385\\ 0. & 249\\ 0. & 747\\ 0. & 249\\$
		E				HL: H P: A		Q (1/s)	3. 225 3. 225 0. 275 0. 275
· .		.		Pressure Water				Coef C	
-	<< Explanatory Notes >>			of			- 	」 (世	823, 886 257, 828 296, 953 44, 415 186, 654 96, 106 96, 106 117, 885 346, 203 346, 203 104, 219 104, 219 104, 219 104, 219 104, 219 104, 219 104, 219 104, 219 104, 219 105, 956 117, 885 203 203 202, 555
	natory 1	- E	Ground Level	LITECTUAL H Consumption			LineData —	C (IIII)	100 37.5 37.5 37.5 37.5 37.5 37.5 37.5 37.5
	Expla	- Node		Qc:			- Line	Node EN	846664935251108406954332
	∻	•					i I	ST	6612221104669744222
<	(四)	(II)	. (%)	(m/s)				Remarks	Reservoir Tank
Formula>	40.444	10, 502	30. 364	0. 747				Qc (1/s)	-3.025 0.275 0.
: Hazen-Williams Formula>>	Maximum EHP	Minimum EHP	Maximum I	Махітит V				EHP 2nd (m)	$\begin{array}{c} 0 & 000 \\ 13.863 \\ 17.230 \\ 11.206 \\ 11.206 \\ 12.23664 \\ 12.26681 \\ 12.26681 \\ 22.124 \\ 22.8674 \\ 22.8674 \\ 22.26.881 \\$
	,*							EHP 1st (m)	
colo < <case.2< td=""><td>1</td><td>17</td><td>17</td><td>0</td><td>0.72 (cm)</td><td>13 (times)</td><td></td><td>۳) (۱</td><td>1, 953. 020 1, 936. 820 1, 932. 430 1, 929. 940 1, 932. 130 1, 932. 940 1, 932. 910 1, 932. 120 1, 917. 240 1, 915. 370 1, 915. 450 1, 915. 450 1, 915. 450</td></case.2<>	1	17	17	0	0.72 (cm)	13 (times)		۳) (۱	1, 953. 020 1, 936. 820 1, 932. 430 1, 929. 940 1, 932. 130 1, 932. 940 1, 932. 910 1, 932. 120 1, 917. 240 1, 915. 370 1, 915. 450 1, 915. 450 1, 915. 450
Bikolo	Tank	Node	Line	Pump, Decom	Convergence Gap	Calculation 13	— NodeData	H)	$\begin{array}{c} 1953. \ 020\\ 1953. \ 020\\ 1949. \ 668\\ 1947. \ 817\\ 1947. \ 817\\ 1947. \ 817\\ 1943. \ 412\\ 1944. \ 420\\ 1944. \ 171\\ 1944. \ 925\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1944. \ 926\\ 1946. \ 926$
ł				-	Convei	Ű	i I	Node	1 1 1 1 1 1 1 1 1 1 1 1 1 1

資料 7. その他の資料・情報 7-2 試掘調査結果(柱状図)

[-

Test well drilling and existing water source survey for the second preparatory survey of the project for small towns water supply in southern part of the Amhara regional state

		Site No.	14 ductive well #1 (E	(H1)							
Well No.		ation	Coordinate		Altit	ude	Town	Zone East Goyam	State Anhara		Country Ethicae
Date: fron	n to 12/11/2011	Drilling :	Equipment Type 729-300	Method D774	Flor	W.	Depth GL -76.0	Depth	Depth		Final Depth GL -76.0m
sing Type :	Size	Inside Dia.		Joint Type Screw	Installation	depth:	+0.75-62	2			Total Length 63, 7m
reen Pipe :	6" Material	150.0mm Diameter	Silot Size	Open Rate	Joint T		Installatio	depth: -62.92 - 74.3	×		Total Length 33.477
PIC servation Pipe	6" Material	150.0mm Diameter	L.Onm Silot Size	Open Rate	Sore T sniot	ype	Installatio		0		Total Length 72.0m
avel Pakking	GS Ongin	Gravel Size	3/4" Location	Volume	Divelop		72.Cm	Method	Duration	SWL (m)	Discharge
bmersible pun	Basaite mp: 1	o 2-6mm nstallation Da	te:	2.0 M2				Å.r	5715		
lit Diameter (mm) and Hethod	P	osition of Pl Well Struc	pes and ture +0.70m			m Normal 0.5m No (ohyn-ny	innal	80 80 100	Well Column	Depth (m)	Lithology
тв				D	0 10 20	11				-1,07	Blak Clay
RM : 305mim	CG BS		- 6.0m	-10 -20							Weathered ⊤uff
		PC		-30					*****	-27 m	
HB DTH 254mm	OP			-40					X X X X X X X X X X X X X X X X X X X		Basalt:- Slightly fractured and slightly weathered. However between 61m ai 76m it is highly fractured and watehe and water bearing (Main aquifer)
				-50				<pre>{</pre>	<pre>cxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx</pre>		
		and a second	60.000	-20		11					
		100000000000	- 62.92m	-70		8		5	******		
	BP							/		-76m	
				-30							
				-90							
	_			-100							
MBOL: B = Hammer E B = Tricon Bit	BIt	CG = Ceme OP = obse G = Gravel	vation pipe	PC = PVC Ca S = Screen P = Pump Po						otary with rilled with	h mud water

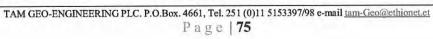
TAM GEO-ENGINEERING PLC. P.O.Box. 4661, Tel. 251 (0)11 5153397/98 e-mail tam-Geo@ethionet.et $P~a~g~e~\mid$ 73

		Site No. 1		1 /8411						
Well No.	Lo	cation	ductive well # Coordina	te (UTM)	Altitude	Town	Zone Fact Golam	State Amhara		Country Ethiopia
BH2 Date: from	to	Vetmen Drilling :	Equipment Type	Method	Flow	Depth Depth	East Gojam Depth	Depth		Final Depth GL +87.0m
sing Type :	Size	Inside Dia.	TOP-300 Outside Dia.	D7H Joint Type	Installation depth:	GL -87.0m				Total Length 69.4m
PVC reen Pipe :	Material	250.0mm Diameter	162. Sinn Silot Size	Open Rate	Joint Type	+0.75-65.64 Installation de	pth:			Total Length
PVC servation Pip	6" Material	150.0mm Dameter	2. Grom Silot Size	20% Open Rate	Joint Type	Installation de	-68.64 - 85.8 pth:		-	IR.2m Total Length
avel Pakking	Origin	Gravel Size	Location	Volume	Threaded Divelopment:	78.0m	Method	Duration	SWL (m)	78.0m Discharge
bmersible pun	Basa/bc	o 2-6mm Installation Date	:	2.0 m*			Air	57%		
iit Diameter (mm) and Method		Position of Pipe Well Structu	s and me+0.70			formal (ohnem) formal (ohnem) 200	300	Well Column	Depth (m)	Lithology
TB RM : 305mm			i.0m	D					-7m	Blak Clay
	BS	• • •	20m	-10 -20 -30					-36 m	Basalt:- Slightly fractured and slight weathered. However between 23m and 30m it is hard and not fractured
HB DTH 254mm	<u>OP</u>			-40 -60 -60						Volcanic Ash and Tuff:-volcar ash occurs from 36m to 40m, the remaining is tuff welded and weathered to variable digrees
	<u>8</u> P	- 66	3.64m	-70		>			-70 m	Basalt:- Highly to slightly fractured from 70m to 81m (Major aquifer)
	BP			-90					-87m	
IMBOL: IB = Hammer B IB = Tricon Bit	ĸ	CG = Cement OP = observa G = Gravel BS = Bentoni	tion pipe	PC = PVC Cas S = Screen P = Pump Po B.P.=Bottom	scion			R M = R DTH = D		n mud water Fair

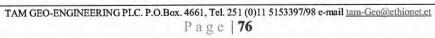
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D

Loc	cation Sede	tive well #1 (B) Coordinat		Altitude	Town	Zone	State		Country
		the second		and the second second second	Secle	East Cojam	Ampara		Ethiopia
to	Drilling :	Equipment Type	Method	Flow	Depth	Depth	Depth		Final Depth GL -SZ. Om
Size	Inside Dia.	Outside Dia.	Joint Type	Installation depth:	ALC: NO. OF CO.				Total Length
6" Material	Diameter	Silot Size	Open Rate	Jaint Type	10.75-68.69 Installation dep	th:			75.2m Total Length
5"	150. Centeri	s.Omm	10%	Screw Joint Type	Installation dep	-65.69 - 80.13			11.4m Total Length
65	3	14"		Threaded	77,0th		Duration	SVVI (m)	77.0m Descharge
Bese/tic	0 2-6mm		2.50 m*	precipinent)		Air	6Hs	arre und	
							1.2		
P	Well Structu			0.51	n Normal (ohm-m) n Normal (ohm-m) 600 800	1000	Well Column	Depth (m)	Lithology
<u>ca</u> ,	6	.0m	-10						Cl øy:- Reddish brown
<u>85</u>		20m	-20					-20m	Trachytet-Highly fractured & highly weathered trachyte
			-40					-38 m	Clay:- Reddish brown Clay
<u>0</u> P			-50		MM		*****************		Basalt:-highly Weathered
				N K	\leq		222	-60 m	
			-00		4			-62 m	Pyroclastic:- Highly weathered san
	1						*****		Basalt: - moderately waetherd and slightly fractured
	- 6	8.69m		1	-		XXXX	-69 m	
			-70	81				~70 m	Clay:- Red Clay
BP			-60			_	*****	-87m	Basalt:- Highly to moderately fractured and weathered from 70m 82m (Major aquifer)
	Conservation of the second sec		-90						
	6° Material 6° Material 65 Origin Researce Ip: CG BS	Size Inside Dia. Size Inside Dia. Size Communications of the second se	Size Inside Dia, Outside Dia, 6° 1280 Cmm 2582 Dmm 2582 Dmm 2582 Dmm 2582 Dmm 2582 Dmm 158 Star 9° 1282 Cmm 2 Johnn 3 Johnn 3 Starts Size Size Size Size Size Size Size Size	Size Inside Dia. Outstade Dia. Outstade Dia. Daint Type Misterial Daineter \$250 cmm \$250 cmm \$250 cmm Misterial Daineter \$301 Size Open Rate 65 \$250 cmm \$260 cmm \$260 cmm Misterial Daineter \$301 Size Open Rate 65 \$260 cmm \$260 cmm \$260 cmm 66 \$347 Open Rate \$260 cmm 67 \$200 cmm \$260 cmm \$260 cmm 68 \$247 Open Rate \$260 cmm 69 Gravel Size Location Volume 92: Installation Date : Installation \$260 cmm 92: Installation Date : Installed \$260 cmm 92: Installation Date : 100 cmm \$260 cmm 93: -20m -20 \$200 cmm 94: 510 cmm \$20 cmm \$20 cmm 95: -20m \$20 cmm \$20 cmm 96: -20m \$20 cmm \$20 cmm 97: -20m \$20 cmm \$20 cmm 98: -20m \$20 cmm \$20 cmm 99: -68.69m \$20 cmm \$20 cmm	Size Inside Dai. Outside Dai. Dain Type Instaliation depthy 6° 126,0mm 522,0mm Sec. Joint Type 8° 126,0mm 10% Sec. Joint Type 8° 126,0mm 10% Joint Type Joint Type 8° 126,0mm 10% Joint Type Joint Type 90% 0 10% Joint Type Joint Type 0 0 10% Joint Type Joint Type 0 10% 10% Joint Type Joint Type 0 10% 10% Joint Type Joint Type 0 10% 10% Joint Type Joint Type 0 2.00m 10% Joint Type Joint Type 0 2.00m 10% Joint Type Joint Type 0 2.00m 10% Joint Type Joint Type 0 10% 10% 10% Joint Type 0 -0.00 -0.00 -0.00 Joint Type 0 -0.00 -0.00 -0.00 Joint Type 0 -0.00 -0.00 -0.00 Joint Type 0 -0.00 -0.00 Joint Type Joint Type <td>Size B Trade Do. Docume Outside Do. Server Derivation of the Server Derivation of the ServerServerServer Derivation of</td> <td>Size B Tracke Dia, Distribution Genty Track Dial Distribution Genty Track Dial Distribution Genty Track Dial Distribution Genty Track Distribution Genty Track Distribution Genty Track Distribution Genty <thdistribution genty<="" th=""> <thdistribution genty<="" th=""></thdistribution></thdistribution></td> <td>See Trade Da Cuesto Da Abent Type Tradition Depty Tradition Depty Method 22.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Method 22.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Method 22.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Method 20.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Method 20.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Observed 20.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Observed 20.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Verification Dista resulted -1.0 cm -1.0 cm 0 20.0 cm Op -0.0 cm -0.0 cm -0.0 cm -0.0 cm 0 20.0 cm 0 -0.0 cm -0.0 cm -0.0 cm -0.0 cm 0 20.0 cm 0 -0.0 cm -0.0 cm -0.0 cm -0.0 cm 0 20.0 cm 0 -0.0 cm -0.0 cm -0.0 cm -0.0 cm 0 0 0 -0.0 cm -0.0 cm -0.0 cm 0 0 0 0</td> <td>Exam Desce Dos. Outloo de de construction destru Schull de construction de constructin de construction de construction de construction de construction</td>	Size B Trade Do. Docume Outside Do. Server Derivation of the Server Derivation of the ServerServerServer Derivation of	Size B Tracke Dia, Distribution Genty Track Dial Distribution Genty Track Dial Distribution Genty Track Dial Distribution Genty Track Distribution Genty Track Distribution Genty Track Distribution Genty Distribution Genty <thdistribution genty<="" th=""> <thdistribution genty<="" th=""></thdistribution></thdistribution>	See Trade Da Cuesto Da Abent Type Tradition Depty Tradition Depty Method 22.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Method 22.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Method 22.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Method 20.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Method 20.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Observed 20.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Observed 20.0 cm 20.0 cm 20.0 cm 20.0 cm 20.0 cm Verification Dista resulted -1.0 cm -1.0 cm 0 20.0 cm Op -0.0 cm -0.0 cm -0.0 cm -0.0 cm 0 20.0 cm 0 -0.0 cm -0.0 cm -0.0 cm -0.0 cm 0 20.0 cm 0 -0.0 cm -0.0 cm -0.0 cm -0.0 cm 0 20.0 cm 0 -0.0 cm -0.0 cm -0.0 cm -0.0 cm 0 0 0 -0.0 cm -0.0 cm -0.0 cm 0 0 0 0	Exam Desce Dos. Outloo de de construction destru Schull de construction de constructin de construction de construction de construction de construction



		Site No.	uctive well #1 (i	3H1)						
Well No. BHJ	L	ocation	Coordina	te (UTM)	Altitude	Town Dibo	Zone East Gojan	State Amhara		Country Ethiopia
Date: from	to 3 12 2011	Drilling :	Equipment Type 70P-300	Method D7H	Flow	Depth GL -80.0m	Depth	Depth		Final Depth GL -SG. Om
sing Type :	Size 6"	Inside Dia. 150.0mm		Joint Type Screw	Installation depth:	+0.75-83.95			1000	Total Length 6-7.1m
een Pipe :	Material 6*	Diameter	Silot Size	Open Rate	Joint Type Screw	Installation dep	th: -53.35 - 74.5	1		Total Length 73.4m
PVC servation Pip	Material	150.0mm Diameter	Silot Size	Open Rate	Joint Type Threaded	Installation dep 72.0m		1.00		Total Length 72.0m
vel Pakking	Origin	Gravel Size		Volume	Divelopment:	12.00	Method	Duration	SVVL (m)	Discharge
mersible pum	Basa/bc	0 2-cmm Installation Da	te :	1.50 m²			AF	SHS		
it Diameter (mm) ind Hethod		Position of Pi Well Struc	pes and ture +0.70	m		9m Normal (ohm-m 9m Normal (ohm-m 100 150	200	Well Column	Depth (m)	Lithology
TB				0 +					-2m	Blak Clay
RM : 305mm	<u>CG</u> <u>85</u> <u>OP</u>	-	- 6.0m	-10 -20 -20 -30 -40 -50 -50 -70					-75 m	Basalt:- Highly fractured and weathered from 70m to 75m (Majo aquifer)
					11				1	Pyroclastic:- Highly weathered pyriclastic material
				-80 -	11	-	-	1.00	-Būm	
				- 90 -						
MBOL:		CG = Came	nt Grout	-100 -	na			RM = R	cary with	i mud water
SIMBOL: NB = Hammer Bi TB = Tricon Bit	π	CG = Ceme OP = obser G = Gravel		PC = PVC Cass S = Screen P = Pump Pos					otary with	r mud water



5

		Site No.	oductive well #	3 (8H3)						a second s
Well No.		ation	Coordinat	te (UTM)	Altitude	Town	Zone East Gojam	State		Country Ethopia
Date: from	to 25 05 2012	Drilling :	Equipment Type 707-500	Method D7h	Flow	Depth GL -51.0m	Depth	Depth		Final Depth GL -61.0m
ing Type :	Size	Inside Dia.	Outside Dia.	Joint Type	Installation depth:	+0.75-42.34				Total Length <i>43, Im</i>
PVC ten Pipe :	Material	150. Cmm Diameter	369.0mm Slot Size	Sprew Open Rate	Joint Type	Installation dep	th: -+12.34 - 60			Total Length 17.2m
PVC ervation Pip	5" Material	150.0mm Diameter	I. Omm Silot Size	20% Open Rate	Joint Type	Installation dep				Total Length 45.0m
vel Pakking	Origin	Gravel Size	2/4" Location	Volume	Threaded Divelopment :	-15.0m	Method	Duration	SWL (m)	48.0m Discharge
mersible pur	Easa/tic	o 2-cener Installation Date	61	3.0 m*	Contract of Contract		Ar	51-15		
t Diameter (mm) nd Method	Pe	Well Struct		n o	0.5m N	ormal (ohmm) ormal (ohmm) 200	300	Well Column	Depth (m)	Lithology
TB RM : 305mm				0 -					-5m	Clay:-Brown silty clay
	<u>c</u> ,		6.0m	-10 -						Basalt:- Highly weathered
	BS ,		20m	-20				***********	-18m -26 m	Basalt:- Moderately weathered
HB DTH 254mm		PC		-20				**********	-39m	Basalt:- Fresh and massive
				-40 -					-42 m	Clay:- Brown clay
	OP			1				***	-46 m	Basalt:- Moderately weathered and slightly Fractured
				-50		_			-52 m	Basalt:- Fractured basalt (Water Bearing
	ВР		- 60.00m	-50				***********************	-61m	Basalt - Highly to slightly fractured from 70m to 81m (Major aquifer)
				-70						
				-80						
				-90-						
	8			-100 -						
Hammer B Tricon Bit	t (CG = Cemen OP = observ G = Gravel BS = Bentna	ation pipe	PC = PVC Case S = Screen P = Pump Posi B.P.=Bottom F	tion			R M = Ro DTH = D		i mud water air

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een Pipe : PiC PiC PiC	23 05 2012	Drilling :				Altitude	Ammenuel	Zone East Galaro	Amhere		Ethopia
een Pipe : PiC PiC PiC		Unling :	Equipment 7 DTH Rota			Flow	Depth 62 - 120.0m	Depth	Depth		Final Depth GL = 120,0m
een Pipe : Pitz	Size	Inside D	a. Outside D	a. Joint'	Type	Installation depth:					Total Length 39.3m
	Material 6"	Diamet 250.00	er Slot Size		Rate	Joint Type Screw	Installation dept	h: -58.56 - 50			Total Length 11,4n
servation Pip	Material	Diamet				Joint Type	Installation dept	h:			Total Length
evel Pakking	CS Origin	Gravel S	ze Location			Threaded Divelopment :	not installed	Method	Duration	SWL (m)	Discharge
mersible pur	Basaltic np: 1	nstallation		6.50	1m2			Ar	Bris		
	-				-			-	1	-	1
it Diameter (mm) ind Hethod	P	well St	Pipes and ucture	0.75m		0.5m	Normal (ohm-m) Normal (ohm-m) 200	300	Well Column	Depth (m)	Lithology
TB RM : 305mm					0		····	Ĩ		-Sm	Clay:-Brownsilty clay
	ca	•	- 6.0m		-10 -				*****	-16m	Basalt:- Highly weathered
	85		- 20m		-20				********	-28 m	Basalt:- Weathered & freactured
					-30		-	-	*****	-34m	Basalt:- Moderately weathered and fractured
		8.8.3.00	- 38.56m		-40						Basalt:- Highly fractured and weathered (main aquifer)
HB DTH 254mm	BP		- 50.00m	ŀ	- 60 - 60					-SDm	Basalt:- slightly weathered
		76			-70 -					-70 m	Basalt-Slightly weathered hard
					-100				***************************************	-98 m	Paralt technologies
					-110				*****	-120m	Basalt - Fresh Hard and massive
									1		
1BOL:			and from the	-					P.M - 21	tany unt	mud justar
- Hammer B		OP = obs	ervation pipe	PC = P S = Sc		ng			R M = Ro	organ with	n muid water

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		Site No.	29 ell #1 (BH1)							
Well No.		ation		ate (UTM)	Altitude	Town	Zone East Gojam	State Amhara		Country Ethiopie
BH1 Date: from	n to 25.01 2012	Kunzia Drilling :	Equipment Type 70P-300	Method DTH + Alud	Flow	Depth GL -66.0m	Depth	Depth		Final Depth GL -95.0m
ng Type :	Size	Inside Dia	Dutside Dia.	Joint Type	Installation dept	h:				Total Length
PVC en Pipe :	Material	150.0mm Diameter	162.5mm Silot Size	Screw Open Rate	+0.75-14.74 Joint Type	Installation de	-54.88 - 60.62	1.1.1.1.1.1.1	1.1	75.2m Total Length
PIC ervation Pipe		150.0mm Diameter	3.0mm Silot Size	Dpen Rate	Screw Joint Type	-14, 74 - 20, 44 Installation de	-#3,## - 54.88 oth:	50.62-66.3	*	11.4m Total Length
el Pakking	Origin	Gravel Size	8/4" Location	Volume	Divelopmen	77.0m	Method	Duration	SWL (m)	22.0m Discharge
mersible pur	Easa/bc	o 2-6mm nstallation Da		2.50 m2		_	Alt	6HIS		
Diameter (mm) id Method	P	Well Strue	pes and ture +0.7	om		1.0m Normal (ohmm 9.5m Normal (ohmm 00 600 600	ō	Well Column	Depth (m)	Lithology
TB RM:				D						Clay:- Reddish brown
Susanna			- 6.0m						-6m	
	CG ,	- 11						***		
	BS	*	10m	-10				****		
		10000						****		
			- 14.74m					XXXX		
		1			1			XXXX		
		1		-20	1			XXX X		
					S			*****		
					11			XXX		Desailer Highly whether a first state
		and			12			***		Basalt:- Highly weathered 6 to 16 m, water bearing; Highly weathered
		10			1		-	***		and fractured 29m to 52m water bearin (Major aquifer) and highly fractured
				-90	151			XXX		61m to 65 m water bearing
					K			***		The second
		PC		_				XXX		
				1.000				**********		
				-40	R			12XX		
	1.1.1		and a state		17			XXX		
нв	OP		- 43.44m		5	4	>	XXX		
DTH					(***		
254mm					2	5		*****		
				-50	1	T		XXXX		
		巖			1			****		
							_			
					S		_	****		
			- 60.62m	-50	5			****		
					1	4		****		
								IXXXX		
							_	***		
					1			XXXX XXXX		
				-70	8			XXXX		
					K			1222		
	BP				0			************		
					15			XXXX XXXX		
				-80	5			****		
					0			XXX		
					11			****	-86m	
		自由自由社)<			EXXX		1
				-90						
	0.00			-100						
				1						
IBOL:		CG = Ceme	ent Grout	PC - PVC C	sing E	R M = Rota	y with mud wa	ater	-	
Hammer B	310	OP = obset G = Gravel	vation pipe	S = Screen P = Pump P		DTH - Drile			-	DTH & Rotary with mud water
- INCON BC			once sealed	B.P.=Botton		1 0 111 - 0/100			A REAL PROPERTY.	The second s

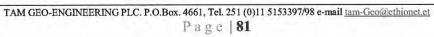
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		ite No. 2								
Well No.		unzila well ation	#2 (BH2) Coordinat	te (UTM)	Altitude	Town	Zone	State		Country
BH2 Date: from	n to ID	Kunzila rilling :	Equipment Type	Method	Flow	Kunzile Depth	East Gojam Depth	Amhara Depth	-	Ethopa Final Depth
2/2012	26/02/2012 Size	Inside Dia.	70P-900 Outside Dia.	DTH + Mud Joint Type	Installation depth:	GL -85.0m				GL -85.0m Total Length
ing Type : PIC	5*	150.0mm	162.5mm Silot Size	Screw Open Rate	+0.75-26.3 Joint Type	-32.02 - 49.28 Installation dept	-54.9 - 66.34	-77.8 - 83.5	5	62.4m Total Length
een Pipe : PVC	Material	Diameter 150.0mm	1.Crnm	10%	SCREW	-26.3 - 32.02	-49.18 - 54.9	-66.34 - 77.0	5	22.9m
servation Pipe	65	Diameter 3	Silot Size 1/4*	Open Rate	Joint Type Threaded	Installation dept 77.0m				Total Length 27.0m
vel Pakking	Origin Enseltic	Gravel Size	Location	Volume 2.50 m³	Divelopment		Method	Duration 6Hs	SWL (m)	Discharge
omersible pur		stallaton Date						_	_	
it Diameter (mm) nd Method	Po	sition of Pipe Well Structu		mo	0 700 20	.0m Normal (ohm m .5m Normal (ohm m 0 300 400		Well Column	Depth (m)	Lithology
TB RM : 305mm		- 6	.0m							Clay:- Reddish brown
HS&TB & RM DTH 254mm				-10 -20 -30 -40	And A M	N N A			-34m -34m	Basalt:- Highly weathered and vesicular (Sm to 20m), fractured and weathered (20m to 34m) water bearing Clay:- Reddish brown Basalt:- Highly weathered and disintegrated basalt with reddish brown clay (water bearing)
		- 6	6.34m	-50					-52m	Alluvial Deposit:- With Reddish brown clay Basalt- Highly weathered and
	БР			-80 -90 -100				****	-85m	Basalt - Highly weathered and disintegrated basalt with reddish brow

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		Site No.								
Well No.	Lo	Kunzila B cation	Coordinat	e (UTM)	Altitude	Town	Zone	State		Country
BH4 Date: from		Kanzia Drilling :	Equipment Type	Method	Flow	Kunzile Depth	East Gojam Depth	Amhara Depth		Ethopia Final Depth
06 2012 sing Type :	3/7/2012 Size	Inside Dia	TOP-300 Dutside Dia.	Jont Type	Installation depth:	GL -62.0m			-	GL ~62.0m Total Length
PIC reen Pipe :	6" Material	150.0mn Diameter	169.0mm	Screw Open Rate	+0.75-21.68 Joint Type	-27.4 - 33.12 Installation der	-38.84 - 44.55	-50.28 - 56		39.5m Total Length
PUC	6*	150.0mm	j. j.Crnm	10%	Screw	-23.67-27.4	-33.12 - 38.54	44.56 - 50.3	8	17.5m Total Length
bservation Pip	Material GS	Diameter	3/4"	Open Rate	Joint Type Threaded	Installation des 52.0m				52.8m
avel Pakking	Origin Sasa/bic	Gravel Siz		Volume 2.50 m *	Divelopment :		Method	Duration	SVVL (m)	Discharge
ibmersible pur	np :	Installation D	ate :							
Bit Diameter			and the second	-				Well	Depth	
(mm) and Hethod		Well Stru		n		9m Normal (ohm- 5m Normal (ohm-	n)	Column	(m)	Lithology
			1		0 100 200	300 40	0 500			
тв				0	1 mar 1					
RM : 305mm										Clay:- Reddish brown
			- 6.0m					S 2		
	CG								-Bm	
	BS		10m	-10				***	1.000	
			1000					1222		
								CXXX XXXX		6
								XXXX		Basalt:- weathered vescicular basalt (Sm to 17m), red ash(scoria) with vesicular
										basalt (17 to 20m) and fractured basalt
				-20				XXXX		(20m to 34m) water bearing
			- 21.7m					1222		
								222		
		臺麗	27.100					XXXX XXXX		
		G	- 27.4m					*****		
HB DTH 254mm		1000		-30				XXXX XXXX		
			- 33.12m					***	-34m	
								a a a	1	
		叢							1	Clay:- Reddish brown
1 11		PC	- 38.84m						++0 m	
1 1		1		-40						
1 11	OP	-	and and a second			1000000	1000 C	EXXX:	1000	Basalt Highly weathered and
1 1			- 44.56m					****	1.1.1	disintegrated basalt with reddish brown clay (little water)
		窶						888		
		: 3	- 49.16m	-50				1998		
			- 49.10111			120		XXX		
								XXXX XXX		
	BP							****		
No. of Concession, Name								1222		
				-50				XXXX		
								2222	-62m	
				-70						
				-80						
				-90						
				-100						
IMBOL:	4					1.1.1.2	-			
B = Hammer Bi		CG = Cem		PC = PVC Cas	ng	R M = Rota	y with mud wa	ter		
	C	OP = obse		S = Screen	ition	DTH = Drile				DTH & Rotary with mud water



Well No. BH2		ation	ell #2 (BH2) Coordina	te (UTH)	Altitude	Lomane	Zone East Gojam	State Amhara		Country Ethiopia
Date: from 01/2012	to 125 03 2032	eniling :	Equipment Type TOP-300	Method D77H	Flow	Depth GL -147.0m	Depth	Depth		Final Depth GL -147.0m
ing Type :	Size	Inside Dia.	Outside Dia.	Joint Type	Installation depth					Total Length
PIC ten Pipe :	5" Material	150.0mm Diameter	<i>169.0mm</i> Silot Size	Open Rate	+0.75-49.98 Joint Type	Installation de	pth:	-112.9 - 118.52		107.2m Total Length
FIC ervation Pipe	5* Moterial	150.0mm Diemeter	2.0mm Silot Size	J095 Open Rate	Screw Joint Type	-49.98 - 55.3 Installation de	-78.58 - 90	-107.18 - 112.5	-118.62 - 130	34.37 Totel Length
	GS		3/4"		Threaded	+0.75-107.2	5		make a h	109.0m
vel Pakking	Origin Basaloc	Gravel Size a 2-6mm	Location	J.O.m.	Divelopment :		Method	Duration 20Hs	SAVL (m)	Discharge
mersible pur		staliation Dat	e:							
t Diameter		S		-						
(mm) nd Hethod	P	Well Struc		m		Normal (ohm-m) Normal (ohm-m)		Well Column	Depth (m)	Lithology
a riculou			1		0 50 100	150 200	250 300	Internet		
TB	1000 B			0						
RM : 305mm										
JUJIM			6 0m	-10			1			Clay:-Black clay
	CG		- 6.0m						-11m	
								****	1-0-1	Basalt: - Moderately to slightly fractured
								***		and wathered between 11 and 23 m. Fresh
			2				-	***		and massive 28m to 35
					1			****		
1										
5	BS ,		- 20m	-30						

								XXXX	-35m	Clart Brown slav
		PC						000	-39m	Clay:- Brown clay
		10		-40				*******		
								222		
								XXX		
· · · · · · · · · · · · · · · · · · ·				-60				XXX	14	And a state of the state of the state
$(X) = \{$								XXX		Basalt:- slightly to highly fractured.
								222		Highly fractured and aquifer between 44m. and 55m
1				-50			-	XXX		
						0.000		XXX		
	DP							****		
1 3						al fait and		XXXX XXX		
				-70				***	-74m	
HB&TB						12.00		XXXX	-/-m	
& RM										
DTH				-80		-		2 3		
254mm		日本語						0		
1		1 金麗						2 11 3		
				-90	1	_				
								1.4		
				-100						
				-100				10 1		
								1		
				1.10				No. 1		Contraction of the second second
				-110						Tuff - weathered to different degrees
								1		
								1 2		
				-120						
		100 A		-130		-				
	1.									
	BP			-140		Sec. 1		19 19		
								to a		
					1				-148m	
-		1101012121212								
				-160	· · · · ·	1				1
BOL:		CG = Cemer		PC = PVC Cas	ang 🔄	R M - Rota	ary with mud w	vater		
			ration pipe	S = Screen						

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