






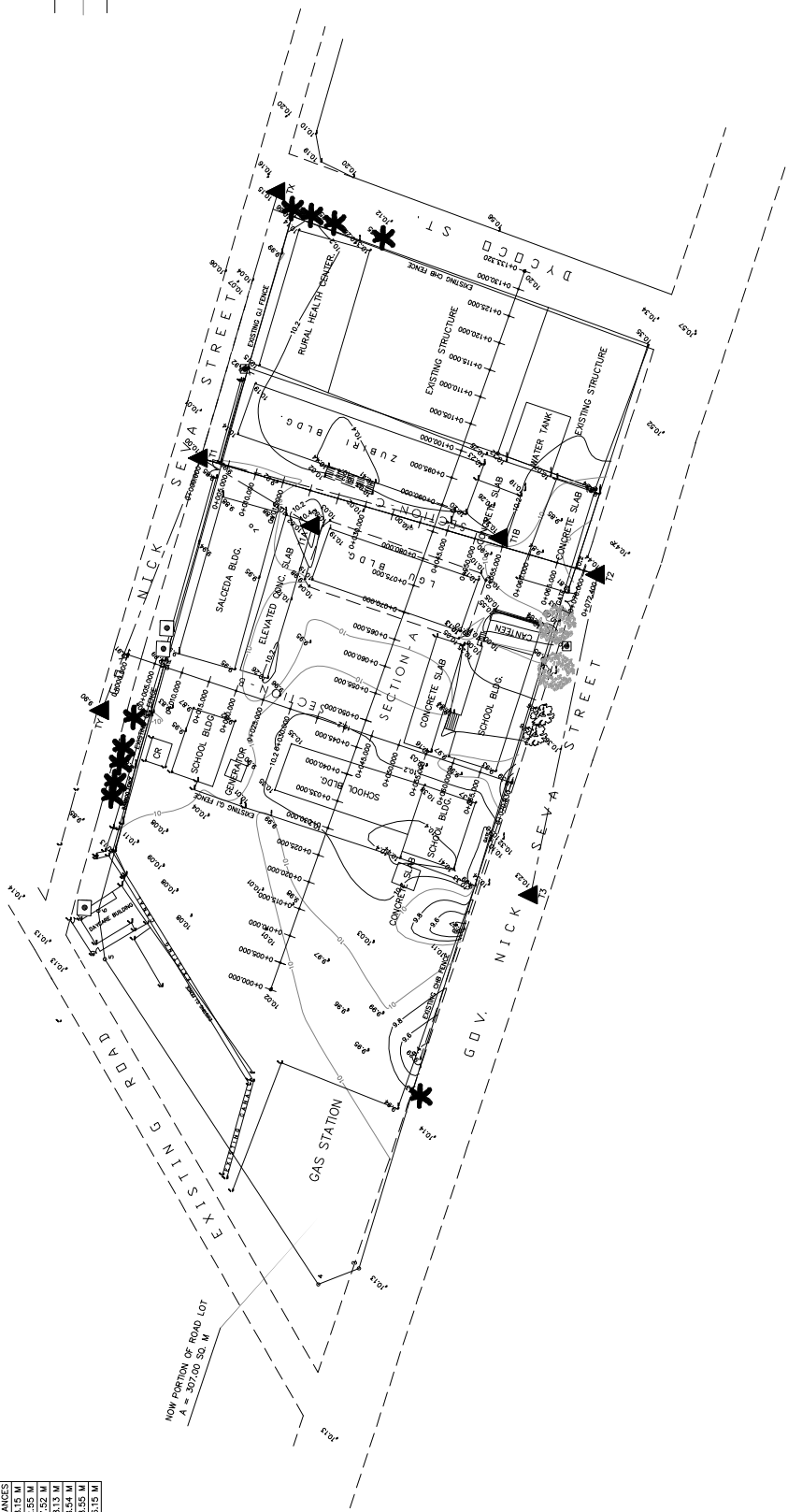


Ⅱ. 地形測量図／地質調査報告書




LEGEND:

-  COCO TREE
-  TALISAY TREE
-  MANGO TREE
-  TRAVERSE LINE
-  CONTOUR LINE
-  SECTION LINE
-  ELECTRIC POST



LOT 667		
THE LINE S84548°W	277.16 M	from BLM #1 Cad-1163, LIBON CADASTRE to corner 1
1-1	S7051°E	27.04 M
1-2	S7051°E	27.04 M
2-3	S2072°W	18.80 M
3-4	N89729°W	26.93 M
4-1	N1952°E	18.15 M
LOT 668		
THE LINE S84548°W	277.16 M	from BLM #1 Cad-1163, LIBON CADASTRE to corner 1
1-1	N1952°E	18.15 M
1-2	N1853°E	46.15 M
2-3	S7358°E	27.63 M
3-4	S1932°W	47.85 M
4-1	N7051°E	27.04 M
LOT 669		
THE LINE S84548°W	277.16 M	from BLM #1 Cad-1163, LIBON CADASTRE to corner 1
1-1	S7051°E	27.04 M
1-2	S7051°E	27.04 M
2-3	S1952°W	142.55 M
3-4	S1952°W	7.55 M
4-5	S1952°W	68.13 M
5-6	S1952°W	8.54 M
6-7	S1952°W	98.55 M
7-1	S1952°W	46.15 M

PREPARED BY:  RAINBOW GEO-SCIENTIFIC C O R P O R A T I O N <small>INCORPORATED IN THE PHILIPPINES</small>	CLIENT: MOHRI, ARCHITECT & ASSOCIATES, INC. 3rd Floor Cacho-Gonzales Bldg, 101 AGUIRRE CDR, TRASPIERA ST. LEGASPI VILLAGE, MAKATI CITY	PROJECT: TOPOGRAPHIC SURVEY OF LOT 669, Cacho-1163, LIBON CADASTRE AREA: 9,762.00 SQ. M. SCALE: 1" = 500 MTS	ENGINEER: BEDA C. MONPINBANUA GEODETIC ENGINEER REG. CERT. NO. 88382 LICENSE NO. 8738-3
SHEET No. 1/1		DATE SURVEYED: SEPTEMBER 16, 2010 DATE PREPARED: SEPTEMBER 24, 2010 CONTOUR INTERVAL: 0.20 M	

LINE	BEARING	DISTANCE
1-2	S 89° 58' 00" W	10.00 M
2-3	S 89° 58' 00" W	10.00 M
3-4	S 89° 58' 00" W	10.00 M
4-5	S 89° 58' 00" W	10.00 M
5-6	S 89° 58' 00" W	10.00 M
6-7	S 89° 58' 00" W	10.00 M
7-8	S 89° 58' 00" W	10.00 M
8-9	S 89° 58' 00" W	10.00 M
9-10	S 89° 58' 00" W	10.00 M
10-11	S 89° 58' 00" W	10.00 M
11-12	S 89° 58' 00" W	10.00 M
12-13	S 89° 58' 00" W	10.00 M
13-14	S 89° 58' 00" W	10.00 M
14-15	S 89° 58' 00" W	10.00 M
15-16	S 89° 58' 00" W	10.00 M
16-17	S 89° 58' 00" W	10.00 M
17-18	S 89° 58' 00" W	10.00 M
18-19	S 89° 58' 00" W	10.00 M
19-20	S 89° 58' 00" W	10.00 M
20-21	S 89° 58' 00" W	10.00 M
21-22	S 89° 58' 00" W	10.00 M
22-23	S 89° 58' 00" W	10.00 M
23-24	S 89° 58' 00" W	10.00 M
24-25	S 89° 58' 00" W	10.00 M
25-26	S 89° 58' 00" W	10.00 M
26-27	S 89° 58' 00" W	10.00 M
27-28	S 89° 58' 00" W	10.00 M
28-29	S 89° 58' 00" W	10.00 M
29-30	S 89° 58' 00" W	10.00 M
30-31	S 89° 58' 00" W	10.00 M
31-32	S 89° 58' 00" W	10.00 M
32-33	S 89° 58' 00" W	10.00 M
33-34	S 89° 58' 00" W	10.00 M
34-35	S 89° 58' 00" W	10.00 M
35-36	S 89° 58' 00" W	10.00 M
36-37	S 89° 58' 00" W	10.00 M
37-38	S 89° 58' 00" W	10.00 M
38-39	S 89° 58' 00" W	10.00 M
39-40	S 89° 58' 00" W	10.00 M
40-41	S 89° 58' 00" W	10.00 M
41-42	S 89° 58' 00" W	10.00 M
42-43	S 89° 58' 00" W	10.00 M
43-44	S 89° 58' 00" W	10.00 M
44-45	S 89° 58' 00" W	10.00 M
45-46	S 89° 58' 00" W	10.00 M
46-47	S 89° 58' 00" W	10.00 M
47-48	S 89° 58' 00" W	10.00 M
48-49	S 89° 58' 00" W	10.00 M
49-50	S 89° 58' 00" W	10.00 M
50-51	S 89° 58' 00" W	10.00 M
51-52	S 89° 58' 00" W	10.00 M
52-53	S 89° 58' 00" W	10.00 M
53-54	S 89° 58' 00" W	10.00 M
54-55	S 89° 58' 00" W	10.00 M
55-56	S 89° 58' 00" W	10.00 M
56-57	S 89° 58' 00" W	10.00 M
57-58	S 89° 58' 00" W	10.00 M
58-59	S 89° 58' 00" W	10.00 M
59-60	S 89° 58' 00" W	10.00 M
60-61	S 89° 58' 00" W	10.00 M
61-62	S 89° 58' 00" W	10.00 M
62-63	S 89° 58' 00" W	10.00 M
63-64	S 89° 58' 00" W	10.00 M
64-65	S 89° 58' 00" W	10.00 M
65-66	S 89° 58' 00" W	10.00 M
66-67	S 89° 58' 00" W	10.00 M
67-68	S 89° 58' 00" W	10.00 M
68-69	S 89° 58' 00" W	10.00 M
69-70	S 89° 58' 00" W	10.00 M
70-71	S 89° 58' 00" W	10.00 M
71-72	S 89° 58' 00" W	10.00 M
72-73	S 89° 58' 00" W	10.00 M
73-74	S 89° 58' 00" W	10.00 M
74-75	S 89° 58' 00" W	10.00 M
75-76	S 89° 58' 00" W	10.00 M
76-77	S 89° 58' 00" W	10.00 M
77-78	S 89° 58' 00" W	10.00 M
78-79	S 89° 58' 00" W	10.00 M
79-80	S 89° 58' 00" W	10.00 M
80-81	S 89° 58' 00" W	10.00 M
81-82	S 89° 58' 00" W	10.00 M
82-83	S 89° 58' 00" W	10.00 M
83-84	S 89° 58' 00" W	10.00 M
84-85	S 89° 58' 00" W	10.00 M
85-86	S 89° 58' 00" W	10.00 M
86-87	S 89° 58' 00" W	10.00 M
87-88	S 89° 58' 00" W	10.00 M
88-89	S 89° 58' 00" W	10.00 M
89-90	S 89° 58' 00" W	10.00 M
90-91	S 89° 58' 00" W	10.00 M
91-92	S 89° 58' 00" W	10.00 M
92-93	S 89° 58' 00" W	10.00 M
93-94	S 89° 58' 00" W	10.00 M
94-95	S 89° 58' 00" W	10.00 M
95-96	S 89° 58' 00" W	10.00 M
96-97	S 89° 58' 00" W	10.00 M
97-98	S 89° 58' 00" W	10.00 M
98-99	S 89° 58' 00" W	10.00 M
99-100	S 89° 58' 00" W	10.00 M

LEGEND:

- COCO TREE
- TREE
- MANGO TREE
- NARRA TREE
- WATER TANK
-
- TRAVERSE LINE
- CONTOUR LINE
- SECTION LINE



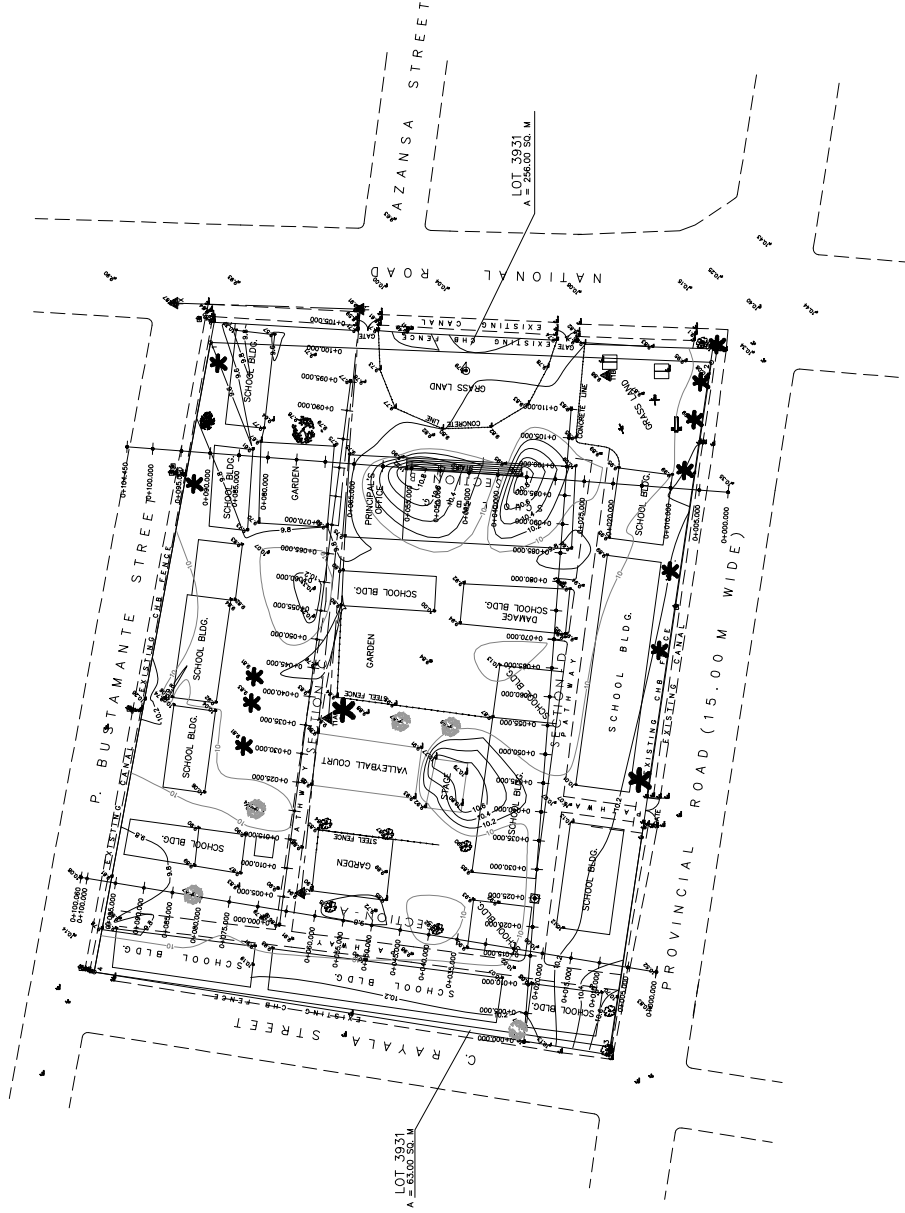
<p>PREPARED BY: G. S. & P. ENGINEERS <small>INCORPORATED IN THE PHILIPPINES</small></p>	<p>CLIENT: MOHRI ARCHITECT & ASSOCIATES, INC. <small>3rd Floor Cacho-Gonzales Bldg. 101 AGUIRRE CDR. TRASERRA ST. LEGASPI VILLAGE, MAHATI CITY</small></p>	<p>PROJECT: TOPOGRAPHIC SURVEY OF LOT 83, Cad-471-D, POLANGUI CADASTRE</p>	<p>ENGINEER: BEDIA C. MONFORANUA <small>REGISTERED PROFESSIONAL ENGINEER No. 10100 - 10101</small></p>
<p>DATE PREPARED: <u>SEPTEMBER 22, 2010</u> CONTOUR INTERVAL: <u>0.20 M</u></p>		<p>SHEET No. 1/1</p>	

THE LINE NUMBER	3465.72 M
1-1	807.80 M
1-2	807.80 M
2-1	807.80 M
2-2	807.80 M
2-3	807.80 M
2-4	807.80 M
3-1	807.80 M
3-2	807.80 M
3-3	807.80 M
3-4	807.80 M
4-1	807.80 M
4-2	807.80 M
4-3	807.80 M
4-4	807.80 M



LEGEND:

- COCO TREE
- TALISAY TREE
- ACACIA TREE
- TRAVERSE LINE
- CONTOUR LINE
- SECTION LINE
- WATER TANK
- NARRA TREE
- CONCRETE ELECTRIC POST / LAMP POST



PREPARED BY:

MOHRI, ARCHITECT & ASSOCIATES, INC.
 3rd Floor, Cocoyon-Gonzales Bldg. 101, AGUIRRE COR.
 TRASIERRA ST., LEGASPI VILLAGE, MAKATI CITY

CLIENT:
MOHRI, ARCHITECT & ASSOCIATES, INC.
 3rd Floor, Cocoyon-Gonzales Bldg. 101, AGUIRRE COR.
 TRASIERRA ST., LEGASPI VILLAGE, MAKATI CITY

PROJECT:
**TOPOGRAPHIC SURVEY
 OF LOT 03676, PSC-4604**

ENGINEER:
BEDA C. MONPINBANIA
 GEODETIC ENGINEER
 REG. OFF. NO. 30272
 BUREAU NO. 30272

DATE SURVEYED: SEPTEMBER 13 & 15, 2000
 DATE PREPARED: SEPTEMBER 24, 2000
 CONTOUR INTERVAL: 500 M

SHEET No.

1/1

IV.019

THE CURVE	LENGTH OF	AREA
LINE	BEARING	DISTANCES
1-2	107.718	10.7718
2-3	107.718	10.7718
3-4	107.718	10.7718
4-5	107.718	10.7718
5-6	107.718	10.7718
6-7	107.718	10.7718
7-8	107.718	10.7718
8-9	107.718	10.7718
9-10	107.718	10.7718
10-11	107.718	10.7718
11-12	107.718	10.7718
12-13	107.718	10.7718
13-14	107.718	10.7718
14-15	107.718	10.7718
15-16	107.718	10.7718
16-17	107.718	10.7718
17-18	107.718	10.7718
18-19	107.718	10.7718
19-20	107.718	10.7718
20-21	107.718	10.7718
21-22	107.718	10.7718
22-23	107.718	10.7718
23-24	107.718	10.7718
24-25	107.718	10.7718
25-26	107.718	10.7718
26-27	107.718	10.7718
27-28	107.718	10.7718
28-29	107.718	10.7718
29-30	107.718	10.7718
30-31	107.718	10.7718
31-32	107.718	10.7718
32-33	107.718	10.7718
33-34	107.718	10.7718
34-35	107.718	10.7718
35-36	107.718	10.7718
36-37	107.718	10.7718
37-38	107.718	10.7718
38-39	107.718	10.7718
39-40	107.718	10.7718
40-41	107.718	10.7718
41-42	107.718	10.7718
42-43	107.718	10.7718
43-44	107.718	10.7718
44-45	107.718	10.7718
45-46	107.718	10.7718
46-47	107.718	10.7718
47-48	107.718	10.7718
48-49	107.718	10.7718
49-50	107.718	10.7718
50-51	107.718	10.7718
51-52	107.718	10.7718
52-53	107.718	10.7718
53-54	107.718	10.7718
54-55	107.718	10.7718
55-56	107.718	10.7718
56-57	107.718	10.7718
57-58	107.718	10.7718
58-59	107.718	10.7718
59-60	107.718	10.7718
60-61	107.718	10.7718
61-62	107.718	10.7718
62-63	107.718	10.7718
63-64	107.718	10.7718
64-65	107.718	10.7718
65-66	107.718	10.7718
66-67	107.718	10.7718
67-68	107.718	10.7718
68-69	107.718	10.7718
69-70	107.718	10.7718
70-71	107.718	10.7718
71-72	107.718	10.7718
72-73	107.718	10.7718
73-74	107.718	10.7718
74-75	107.718	10.7718
75-76	107.718	10.7718
76-77	107.718	10.7718
77-78	107.718	10.7718
78-79	107.718	10.7718
79-80	107.718	10.7718
80-81	107.718	10.7718
81-82	107.718	10.7718
82-83	107.718	10.7718
83-84	107.718	10.7718
84-85	107.718	10.7718
85-86	107.718	10.7718
86-87	107.718	10.7718
87-88	107.718	10.7718
88-89	107.718	10.7718
89-90	107.718	10.7718
90-91	107.718	10.7718
91-92	107.718	10.7718
92-93	107.718	10.7718
93-94	107.718	10.7718
94-95	107.718	10.7718
95-96	107.718	10.7718
96-97	107.718	10.7718
97-98	107.718	10.7718
98-99	107.718	10.7718
99-100	107.718	10.7718

- LEGEND:
- BANANA TREE
 - TREE
 - ACACIA TREE
 - MANGSO TREE
 - COTTAGE / HUT
 - ELECTRIC POST
 - ELECTRIC WIRE LINE
 - TRANSVERSE LINE
 - CONTOUR LINE
 - SECTION LINE
 - ELECTRIC WIRE LINE
 - WATER LINE
 - BOUNDARY LINE

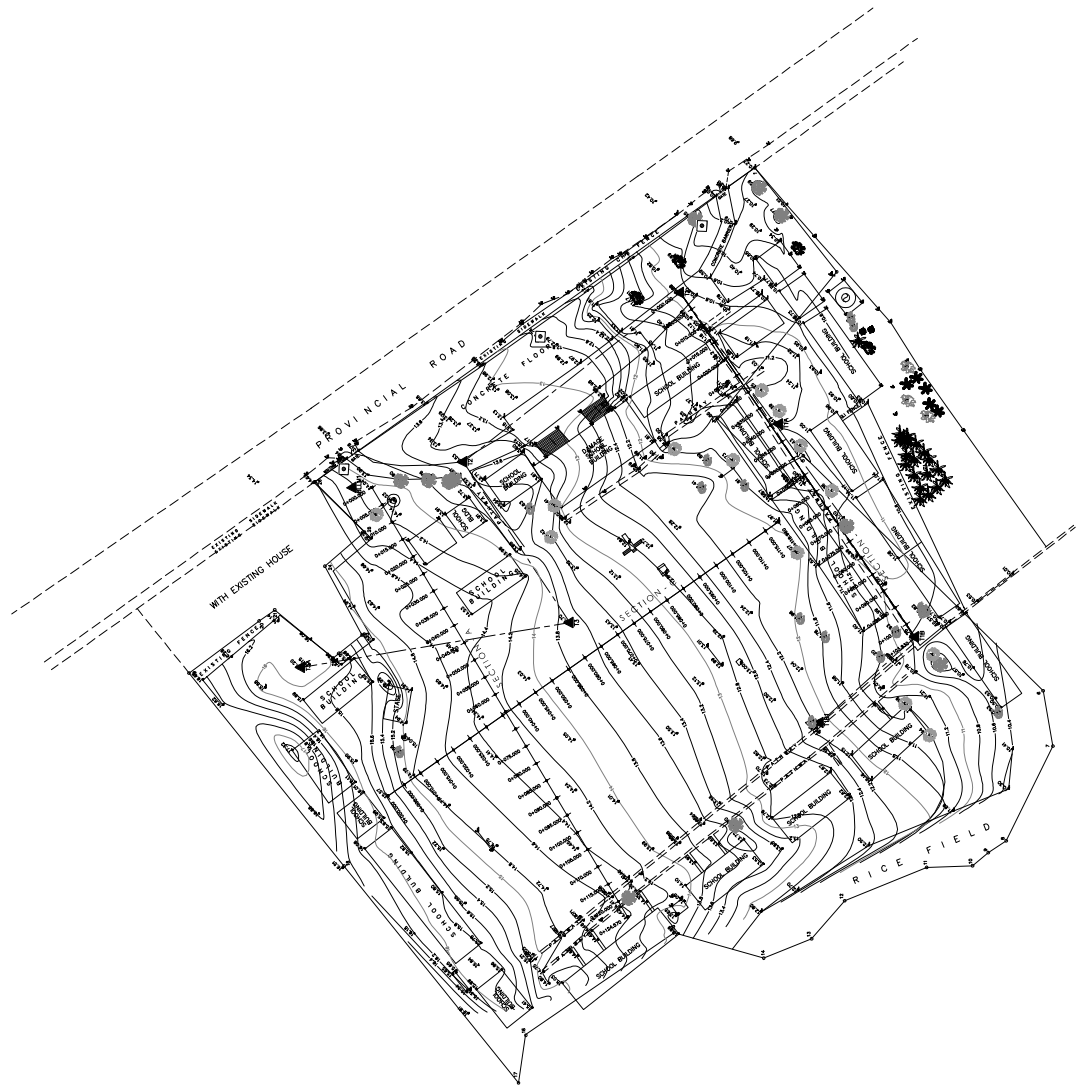


NOTE:
 -All corners are in accordance with the original survey.
 -The bearings and distances are as shown on the plan and are the existing ones.
 -The bearings and distances are as shown on the plan and are the existing ones.
 -The bearings and distances are as shown on the plan and are the existing ones.

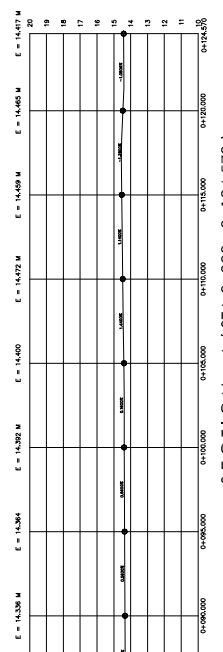
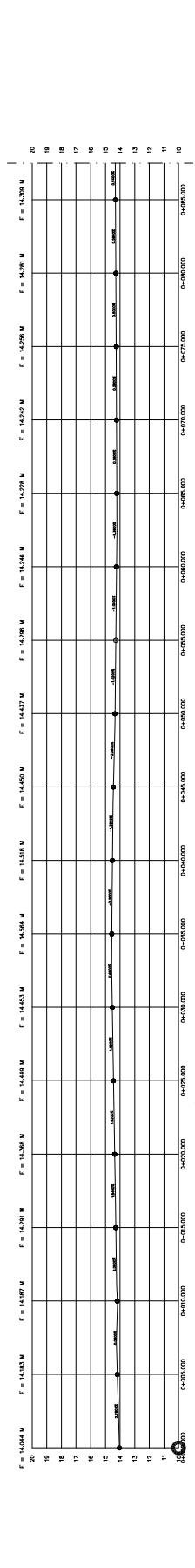
<p>PREPARED BY:</p> <p>G. O. P. & H. ARCHITECTS AND ENGINEERS 3rd Floor, Cacho-Gonzales Bldg., 101 Aguirre CDR. TRINERIA ST., LEGASPI VILLAGE, MAKATI CITY</p>	<p>CLIENT:</p> <p>MOHRI, ARCHITECT & ASSOCIATES, INC. 3rd Floor, Cacho-Gonzales Bldg., 101 Aguirre CDR. TRINERIA ST., LEGASPI VILLAGE, MAKATI CITY</p>	<p>PROJECT:</p> <p>TOPOGRAPHIC SURVEY OF LOT 166, MANITO CADASTRE</p> <p>AREA: 28,192.00 SQ. M SCALE: 1" = 500' H.T.S.</p>	<p>ENGINEER:</p> <p>BEA C. MONDAPANANIA REGISTERED PROFESSIONAL ENGINEER No. 10,000 - 10,000</p>	<p>SHEET No. 1/1</p> <p>DATE SURVEYED: SEPTEMBER 10-11-17 & 19, 2000. DATE PREPARED: SEPTEMBER 22-24, 2000 CONTOUR INTERVAL: 0.20 M</p>
--	---	---	---	---

LINE NO.	DESCRIPTION	DATE	BY	CHECKED
1	STATIONED	10/28/14
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60
61
62
63
64
65
66
67
68
69
70
71
72
73
74
75
76
77
78
79
80
81
82
83
84
85
86
87
88
89
90
91
92
93
94
95
96
97
98
99
100

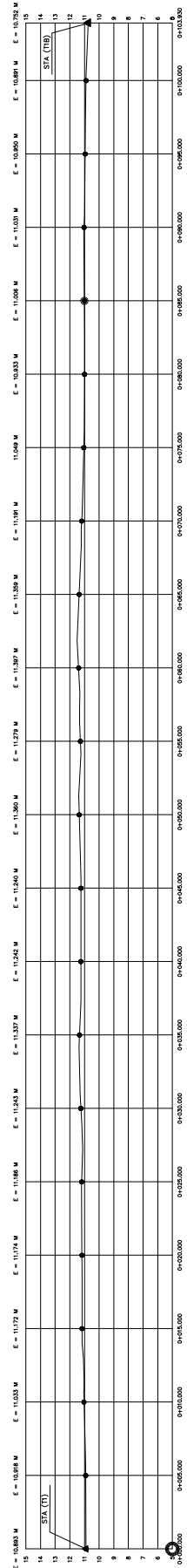
- LEGEND:
- ☉ WATER TANK
 - ☐ TREE
 - ◉ MANGO TREE
 - ◊ NARRA TREE
 - ◌ COCO TREE
 - ◌ CONCRETE ELECTRIC POST / LAMP POST
 - ◌ WATER TANK
 - ◌ KAMANS
 - ◌ BANANA TREE
 - ◌ JACKFRUIT TREE
 - TRAVERSE LINE
 - CONTOUR LINE
 - SECTION LINE



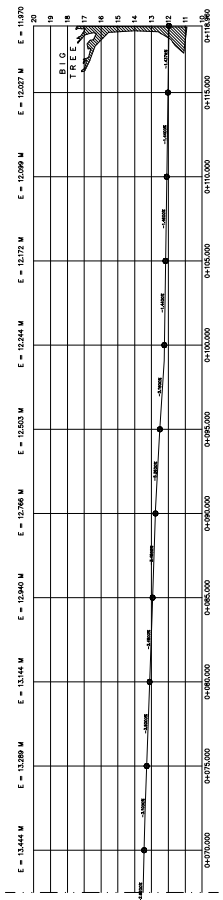
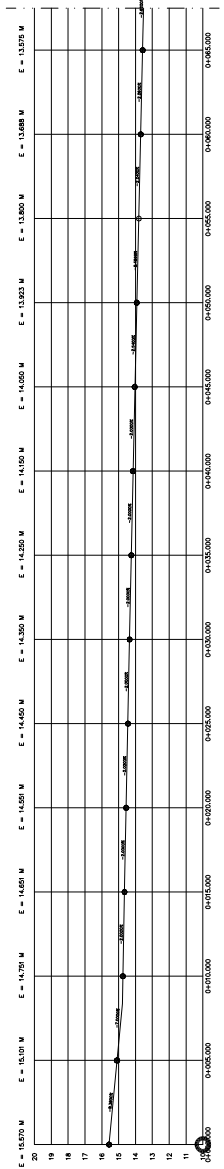
<p>PREPARED BY: RAINBOW GEO-SCIENTIFIC <small>INCORPORATED IN THE PHILIPPINES</small></p>	<p>CLIENT: MOHRI, ARCHITECT & ASSOCIATES, INC. <small>3rd Floor, Castro-Gonzales Bldg. 301, AGUIRRE CDR, TRINIDAD ST., LEGASPI VILLAGE, MARIKINA CITY</small></p>	<p>PROJECT: TOPOGRAPHIC SURVEY OF LOT 1651, Cad 488-D, STO. DOMINGO CADASTRE <small>AREA = 24,450.00 SQ. M SCALE = 1" = 500' MFS</small></p>	<p>ENGINEER: BEIDA C. MONTEPANDUA <small>REGISTERED PROFESSIONAL ENGINEER No. 16,994 - 1 - 1992 - 1993</small></p>	<p>SHEET No. <div style="text-align: center; border: 1px solid black; width: 30px; margin: 0 auto; padding: 5px;"> 1/1 </div> </p>
<p>DATE SURVEYED: <u>SEPTEMBER 14, 2010</u> DATE PREPARED: <u>SEPTEMBER 27-28, 2010</u> CONTOUR INTERVAL: <u>0.20 M</u></p>				



SECTION - A (STA 0+000 - 0+124.570)

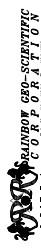


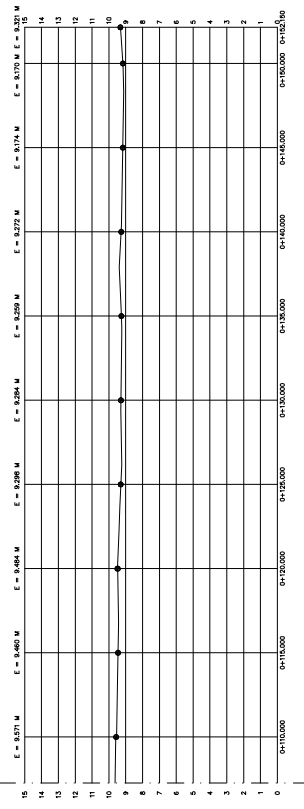
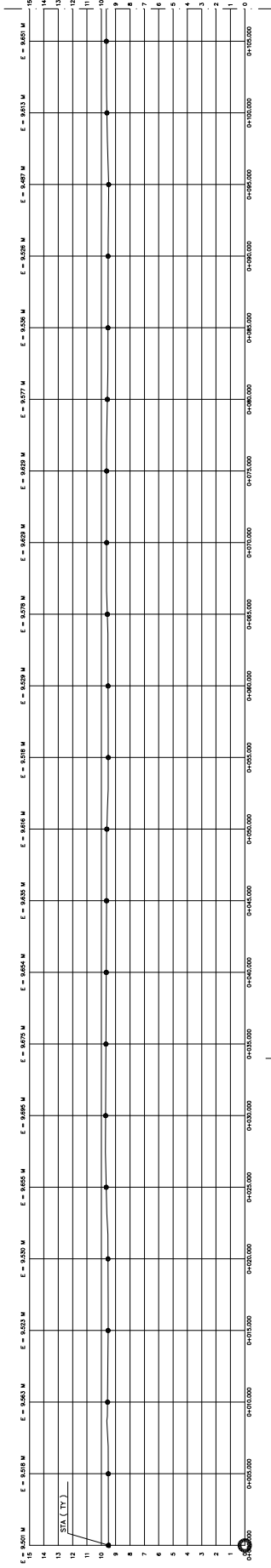
SECTION - B (STA 0+000 - 0+103.930)



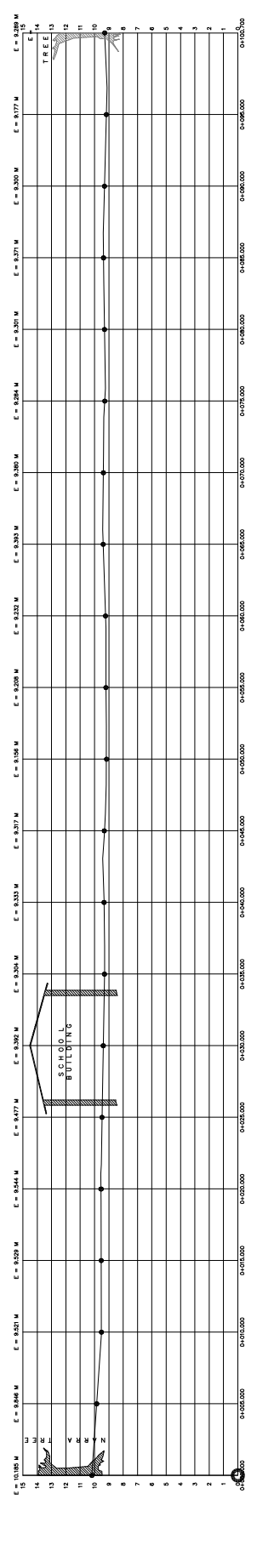
SECTION - C (STA 0+000 - 0+118.960)

PREPARED BY: MOHRRI ARCHITECT & ASSOCIATES INC. 3rd Floor, Dapco-Gonzales Bldg. 101, AGUIRRE CDR. TRASERRA ST. LEGASPI VILLAGE, MAKATI CITY	CLIENT: SECTIONS OF LOT 1651, Cad 488-D, STO. DOMINGO CADASTRE SCALED: 1 : 100 MTS	PROJECT: SECTIONS OF LOT 1651, Cad 488-D, STO. DOMINGO CADASTRE ENGINEER: BETA C. MONSERRANA REGISTERED PROFESSIONAL ENGINEER REG. NO. 101-101-101-101	SHEET NO. 1/1 DATE PREPARED: OCTOBER 7-8, 2010 SHEET CONTENT: SECTION A - C
--	--	---	--

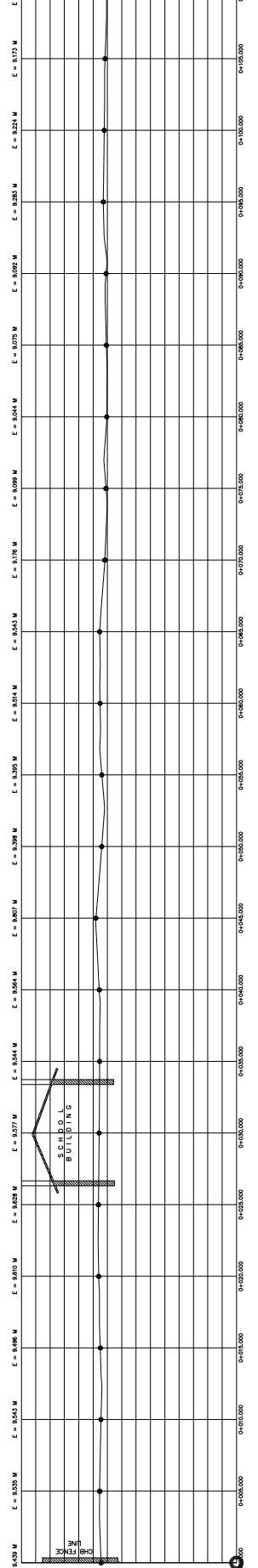




SECTION - A (STA 0+000 - 0+152.150)

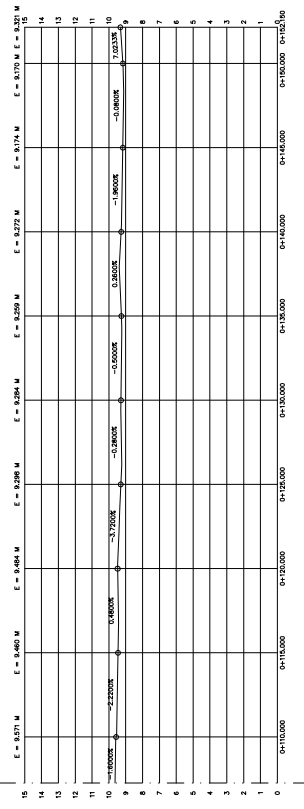
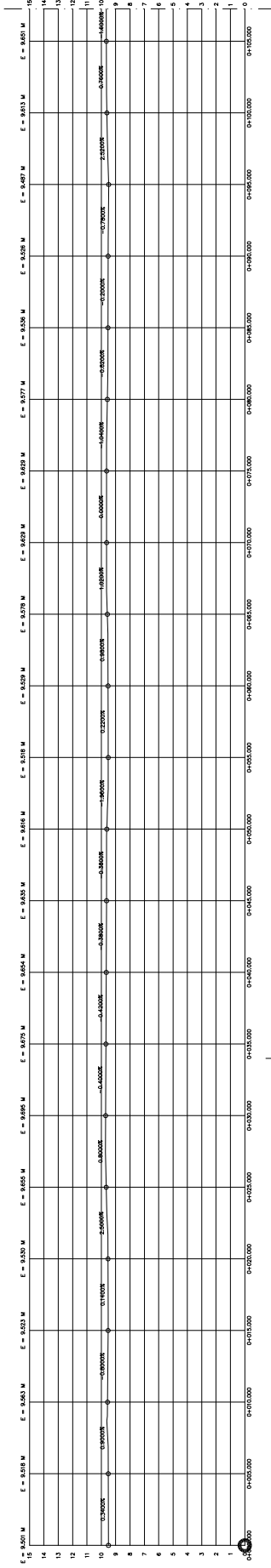


SECTION - B (STA 0+000 - 0+100.700)

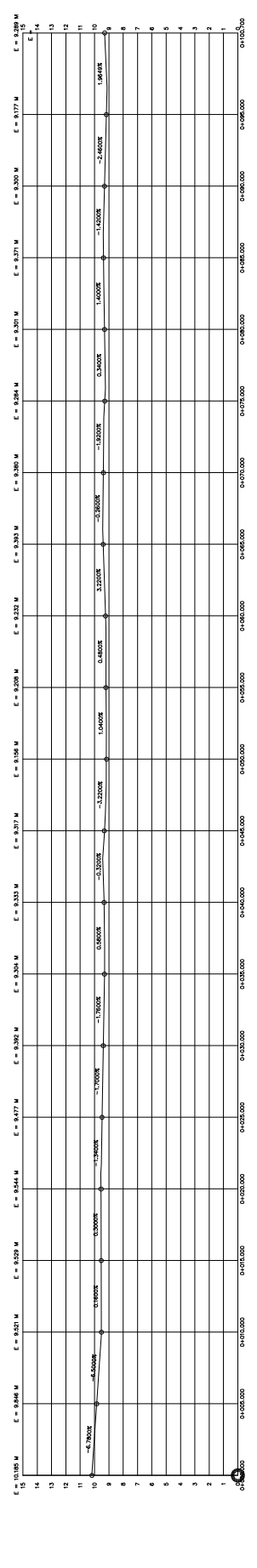


SECTION - C (STA 0+000 - 0+110.000)

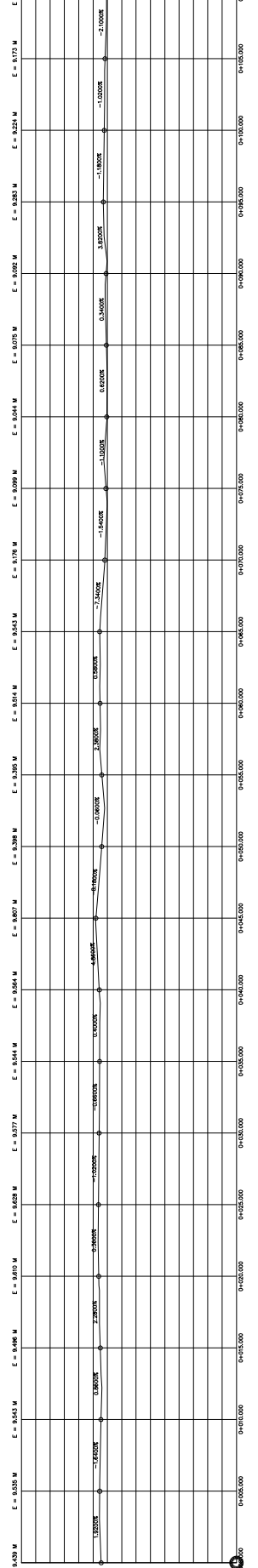
PREPARED BY: RAINBOW GEO-SCIENTIFIC CONSULTANTS 100, 101, 102, 103, 104, 105, 106, 107, 108, 109, 110, 111, 112, 113, 114, 115, 116, 117, 118, 119, 120, 121, 122, 123, 124, 125, 126, 127, 128, 129, 130, 131, 132, 133, 134, 135, 136, 137, 138, 139, 140, 141, 142, 143, 144, 145, 146, 147, 148, 149, 150, 151, 152, 153, 154, 155, 156, 157, 158, 159, 160, 161, 162, 163, 164, 165, 166, 167, 168, 169, 170, 171, 172, 173, 174, 175, 176, 177, 178, 179, 180, 181, 182, 183, 184, 185, 186, 187, 188, 189, 190, 191, 192, 193, 194, 195, 196, 197, 198, 199, 200, 201, 202, 203, 204, 205, 206, 207, 208, 209, 210, 211, 212, 213, 214, 215, 216, 217, 218, 219, 220, 221, 222, 223, 224, 225, 226, 227, 228, 229, 230, 231, 232, 233, 234, 235, 236, 237, 238, 239, 240, 241, 242, 243, 244, 245, 246, 247, 248, 249, 250, 251, 252, 253, 254, 255, 256, 257, 258, 259, 260, 261, 262, 263, 264, 265, 266, 267, 268, 269, 270, 271, 272, 273, 274, 275, 276, 277, 278, 279, 280, 281, 282, 283, 284, 285, 286, 287, 288, 289, 290, 291, 292, 293, 294, 295, 296, 297, 298, 299, 300, 301, 302, 303, 304, 305, 306, 307, 308, 309, 310, 311, 312, 313, 314, 315, 316, 317, 318, 319, 320, 321, 322, 323, 324, 325, 326, 327, 328, 329, 330, 331, 332, 333, 334, 335, 336, 337, 338, 339, 340, 341, 342, 343, 344, 345, 346, 347, 348, 349, 350, 351, 352, 353, 354, 355, 356, 357, 358, 359, 360, 361, 362, 363, 364, 365, 366, 367, 368, 369, 370, 371, 372, 373, 374, 375, 376, 377, 378, 379, 380, 381, 382, 383, 384, 385, 386, 387, 388, 389, 390, 391, 392, 393, 394, 395, 396, 397, 398, 399, 400, 401, 402, 403, 404, 405, 406, 407, 408, 409, 410, 411, 412, 413, 414, 415, 416, 417, 418, 419, 420, 421, 422, 423, 424, 425, 426, 427, 428, 429, 430, 431, 432, 433, 434, 435, 436, 437, 438, 439, 440, 441, 442, 443, 444, 445, 446, 447, 448, 449, 450, 451, 452, 453, 454, 455, 456, 457, 458, 459, 460, 461, 462, 463, 464, 465, 466, 467, 468, 469, 470, 471, 472, 473, 474, 475, 476, 477, 478, 479, 480, 481, 482, 483, 484, 485, 486, 487, 488, 489, 490, 491, 492, 493, 494, 495, 496, 497, 498, 499, 500, 501, 502, 503, 504, 505, 506, 507, 508, 509, 510, 511, 512, 513, 514, 515, 516, 517, 518, 519, 520, 521, 522, 523, 524, 525, 526, 527, 528, 529, 530, 531, 532, 533, 534, 535, 536, 537, 538, 539, 540, 541, 542, 543, 544, 545, 546, 547, 548, 549, 550, 551, 552, 553, 554, 555, 556, 557, 558, 559, 560, 561, 562, 563, 564, 565, 566, 567, 568, 569, 570, 571, 572, 573, 574, 575, 576, 577, 578, 579, 580, 581, 582, 583, 584, 585, 586, 587, 588, 589, 590, 591, 592, 593, 594, 595, 596, 597, 598, 599, 600, 601, 602, 603, 604, 605, 606, 607, 608, 609, 610, 611, 612, 613, 614, 615, 616, 617, 618, 619, 620, 621, 622, 623, 624, 625, 626, 627, 628, 629, 630, 631, 632, 633, 634, 635, 636, 637, 638, 639, 640, 641, 642, 643, 644, 645, 646, 647, 648, 649, 650, 651, 652, 653, 654, 655, 656, 657, 658, 659, 660, 661, 662, 663, 664, 665, 666, 667, 668, 669, 670, 671, 672, 673, 674, 675, 676, 677, 678, 679, 680, 681, 682, 683, 684, 685, 686, 687, 688, 689, 690, 691, 692, 693, 694, 695, 696, 697, 698, 699, 700, 701, 702, 703, 704, 705, 706, 707, 708, 709, 710, 711, 712, 713, 714, 715, 716, 717, 718, 719, 720, 721, 722, 723, 724, 725, 726, 727, 728, 729, 730, 731, 732, 733, 734, 735, 736, 737, 738, 739, 740, 741, 742, 743, 744, 745, 746, 747, 748, 749, 750, 751, 752, 753, 754, 755, 756, 757, 758, 759, 760, 761, 762, 763, 764, 765, 766, 767, 768, 769, 770, 771, 772, 773, 774, 775, 776, 777, 778, 779, 780, 781, 782, 783, 784, 785, 786, 787, 788, 789, 790, 791, 792, 793, 794, 795, 796, 797, 798, 799, 800, 801, 802, 803, 804, 805, 806, 807, 808, 809, 810, 811, 812, 813, 814, 815, 816, 817, 818, 819, 820, 821, 822, 823, 824, 825, 826, 827, 828, 829, 830, 831, 832, 833, 834, 835, 836, 837, 838, 839, 840, 841, 842, 843, 844, 845, 846, 847, 848, 849, 850, 851, 852, 853, 854, 855, 856, 857, 858, 859, 860, 861, 862, 863, 864, 865, 866, 867, 868, 869, 870, 871, 872, 873, 874, 875, 876, 877, 878, 879, 880, 881, 882, 883, 884, 885, 886, 887, 888, 889, 890, 891, 892, 893, 894, 895, 896, 897, 898, 899, 900, 901, 902, 903, 904, 905, 906, 907, 908, 909, 910, 911, 912, 913, 914, 915, 916, 917, 918, 919, 920, 921, 922, 923, 924, 925, 926, 927, 928, 929, 930, 931, 932, 933, 934, 935, 936, 937, 938, 939, 940, 941, 942, 943, 944, 945, 946, 947, 948, 949, 950, 951, 952, 953, 954, 955, 956, 957, 958, 959, 960, 961, 962, 963, 964, 965, 966, 967, 968, 969, 970, 971, 972, 973, 974, 975, 976, 977, 978, 979, 980, 981, 982, 983, 984, 985, 986, 987, 988, 989, 990, 991, 992, 993, 994, 995, 996, 997, 998, 999, 1000	CLIENT: MOHRI ARCHITECT & ASSOCIATES INC. 3rd Floor, Dacpo-Gonzales Bldg. 101 Aguirre CDR, TRASERRA ST. LEGASPI VILLAGE, MAKATI CITY	PROJECT: SECTIONS OF GOGON ELEMENTARY SCHOOL SCALE: 1 : 100 MTS	ENGINEER: BETA C. MONSERRA LICENSED PROFESSIONAL ENGINEER REG. NO. 100-100000-100000	DATE PREPARED: OCTOBER 4-5, 2010 SHEET CONTENT: SECTION A - C	SHEET NO. 1/1 MUDDO
--	---	---	---	--	-------------------------------



SECTION - A (STA 0+000 - 0+152.150)



SECTION - B (STA 0+000 - 0+100.700)



SECTION - C

PREPARED BY: RAINBOW GEO-SCIENTIFIC CONSULTANTS <small>INCORPORATED IN THE REPUBLIC OF SOUTH AFRICA</small>	CLIENT: MOHRI ARCHITECT & ASSOCIATES INC. <small>3rd Floor, Decho-Gonzales Bldg, 101 AGUIRRE CDR, TRASPERRA ST. LEGASPI VILLAGE, MAKATI CITY</small>	PROJECT: TOPOGRAPHIC SURVEY OF LOT 83, CAG-471-D <small>SCALE: 1 : 300 MTS AREA: 35,190.00 SQ. M</small>	ENGINEER: _____ DATE PREPARED: SEPTEMBER 22, 2010 CONTOUR INTERVAL: 0.50 M
<h1>SECTION - C</h1>			SHEET NO. 1/1

FINAL REPORT

SUBSURFACE INVESTIGATION
PROPOSED MAYON
EVACUATION CENTER
(3-STOREY)
LIBON COMMUNITY COLLEGE
BRGY. ZONE 4 LIBON, PROVINCE OF ALBAY

MOHRI, ARCHITECT & ASSOCIATES, INC.

OCTOBER 2010
JOB NO. 2209-10.R1



GEOTECHNICS PHILIPPINES, INC.
GEOTECHNICAL & FOUNDATION CONSULTANTS



DPWH-BRS Accredited

FINAL REPORT

TABLE OF CONTENTS

Contents	No. of Pages
1.0 INTRODUCTION.....	1
2.0 FIELD AND LABORATORY TEST PROCEDURES.....	2
3.0 SITE SOILS AND OBSERVATIONS.....	1
4.0 ENGINEERING ANALYSIS AND CONSIDERATIONS.....	2
5.0 CONSTRUCTION CONSIDERATIONS.....	1
6.0 CONCLUSIONS AND RECOMMENDATIONS.....	1
APPENDICES	
• Distribution of Active Faults and Trenches in the Philippines.....	1
• Photos.....	1
• Location Plan.....	1
• Soil Profile.....	1
• Final Boring Logs.....	2
• Summary of Test.....	1
• Natural Moisture Content/Atterberg Limit.....	4
• Atterberg Limit.....	1
• Grain Size Analysis.....	8





GEOTECHNICS PHILIPPINES, INC.
Geotechnical Contractor

119 Sauyo Road, Novaliches
Quezon City, Philippines

Business development : 9306555
Customer Service : 9382124/9353730
Fax : 4561140
Homepage : www.geophil.com
Email : jmcgpi@gmail.com

FINAL REPORT

**SUB-SURFACE INVESTIGATION FOR THE
PROPOSED MAYON EVACUATION CENTER (3-STOREY)
LOCATED AT BRGY. ZONE 4 LIBON, PROVINCE OF ALBAY**

1. INTRODUCTION

Geotechnics Philippines, Incorporated (GPI) completed the subsurface soil investigation for the proposed Mayon Evacuation Center. The proposed site explored is located at Brgy. Zone 4 Libon, Province of Albay.

Two (2) boreholes were drilled at the proposed site on October 16, 2010. Borings were undertaken down to 10m for both BH-1 and BH-2 below existing natural ground line. Borehole locations are as indicated on the accompanying Boring Plan and Soil Profile Sheets.

The subsurface soil exploration was undertaken upon the request of Mohri & PA Associates, Inc. in order to gain information on the subsurface conditions and bearing characteristics of the underlying soils at site.

The undersigned was tasked to evaluate the results of the completed subsurface soil exploration and to recommend a suitable foundation solution for the proposed structure.

This report embodies the undersigned's engineering analysis and recommendations based mainly on the results of the geotechnical soil borings and pertinent laboratory tests performed on extracted samples.

The results of geotechnical soil borings and laboratory tests can be referred to in the Attachments accompanying this report.

2. FIELD AND LABORATORY TEST PROCEDURES

Drilling Procedure

The boreholes were advanced by wash boring to the maximum boring depths. Standard Penetration Tests were conducted at every 1.5m interval or at change in soil formations. It consisted of driving a standard split spoon sampler of 5.08cm (2" O.D.) diameter in three (3) successive 15cm (6") intervals using a drop hammer of 64kg (140 lbs) weight from a height of 76cm (30"). The number of blows required to penetrate 15cm are recorded successively until the third interval is penetrated. The first interval blow count is called as the seating drive and is discarded. The last two blow counts are added to give the N-value, a measure of the density or consistency of the soil layer. SPT procedures are conducted in accordance with ASTM D-1586. Undisturbed soil samples were taken in soft to stiff soil deposits for Natural Moisture Content (NMC) testing and particle size analysis of soil.

f

2.2 LABORATORY TEST PROCEDURES

The following laboratory tests were performed on the soil samples taken from the site;

- | | |
|--|-------------|
| a. Classification of Soils (USCS) for Engineering Purposes | ASTM D 2487 |
| b. Particle Size Analysis of Soil | ASTM D 422 |
| c. Determination of Moisture Content of Soils | ASTM D 2216 |
| d. Liquid Limit of Soils | ASTM D 4318 |
| e. Plastic Limit of Soils | ASTM D 4318 |

3. SITE SOILS AND OBSERVATIONS

The soil profile indicating the completed two (2) boreholes is attached in this report. Standard Penetration Tests (SPT) indicate shallow layers of very loose poorly graded sand with silt (SP-SM) at depth 2.0m from the existing natural ground line. Drill intersections indicate deposition of fat clay (CH) with intervening layers and pockets of silty sand (SM) with traces of gravel down to a depth of 10m. A layer of silty clay (CH) may also be found within this depth. Trend of N-values generally shows increasing consistency and density with increasing depth. However, it is important to note the existence of relatively looser soils in deeper layers especially in BH-2.

Groundwater table (GWT) levels can be found at a depth of 0.75m for BH-1 and 1.57m for BH-2 reckoned from the existing natural ground line at the time of borings. Thus, excavation may possibly be in wet condition unless otherwise controlled as the detected GWT is fairly within the depths of excavation of proposed foundation elements.

4. ENGINEERING ANALYSIS AND CONSIDERATIONS

SPT N-values of 2 to 4 at a depth from 0 to 2.00 show very loose silty sand, thus shallow foundations to rest on the topmost loose formation (above 2-m) is not permitted. However, directly beneath is a layer of medium dense clayey and silty sand (SC-SM) with thickness ranging from 2m to 4m. Shallow foundations are possible to rest at 2.0m depth to bypass the relatively loose layers of poorly graded sand. This loose sand have to be removed and replaced with selected granular fill preferably well graded. An engineered fill has to be compacted at 95% of the soil's maximum dry density (95% MDD) in 300mm lift.

These shallow foundations shall be in the form of a isolated footing stiffened by a structural tie beam cast in place between column. The system will essentially function as an integrated foundation. The rigidity will assist in bridging across localized settlements and assuring uniform settlement of the structure.

The spread footing shall be proportioned and designed based on a net Allowable Bearing Capacity of 96 kPa (2000 psf). The effect of overburden shall be added to obtain the allowable gross bearing capacity. Where necessary, depending on the final design on the reactions of the building, and due to the low bearing capacity, a mat foundation may also be adopted as an alternate solution to spread footing to support the building foundation. The mat foundation should be made to maintain nearly uniform pressure to avoid differential settlements. For settlement analysis, a compression index of 0.54, modulus

of elasticity of 6 Mpa, and a Poisson's ratio of 0.35 may be used. Soil unit weight of 12 kN/m³ and an angle of internal friction of 28 degrees may be used for shallow foundation calculations.

The floor slabs should not be connected to more rigid elements of the structure such as walls and columns, and should be allowed to settle independently of the building.

This solution, however, is not without possible problems. The relatively poor deposits underlying the site are within the zone of influence of shallow foundations. These poor soil deposits together with the intervening pockets of loose to very loose sands pose a potentially liquefiable and therefore a risk during a significant seismic event. The nature of the soil formations, however, requires considerable earthquake magnitude and epicentral distance to cause soil liquefaction. Hence, settlements can be expected as well as the inherent danger of liquefaction.

5. CONSTRUCTION CONSIDERATIONS

The shallow water table poses a problem during foundation construction. Adequate number of dewatering equipment should be provided in order to allow excavation in almost dry condition. Likewise, concreting shall also be done in the dry condition by dewatering the foundations continuously.

Engineered fill shall be compacted using a vibratory plate compactor of adequate size. As previously noted, floor slabs should not be connected to more rigid elements of the structure such as walls and columns, and should be allowed to settle independently of the building.


6. CONCLUSIONS AND RECOMMENDATIONS

The spread footing or mat solution may be adopted, the foundation are subject to settlements and possibility of liquefaction due to poor soil deposits underneath. Although the mat will minimize the effect if the cited recommendations are followed by the engineer on record of the structure. The economics for using shallow foundations is considered in the design of the proposed 3-storey structure.

The recommendations submitted in this report are based in part upon the data obtained from a limited number of soil samples. The nature and extent of variations between explorations may not become evident until construction or further investigation. If the variations are of considerable magnitude, it will be necessary to reevaluate the recommendations in this report.

This report has been done by the undersigned in accordance with generally accepted Engineering Principles and Practices.

If you require additional comments or clarifications pertaining to the recommendations, the undersigned will be pleased to comply.



DIOSDADO A. URENA

CE Reg. No. 053884

PTR No. 3228274

Issued on January 8, 2010

Issued at Quezon City

APPENDICES



Distribution of Active Faults and Trenches in the Philippines

20 00'

18 00'

16 00'

14 00'

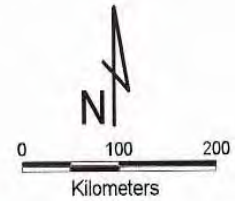
10 00'

8 00'

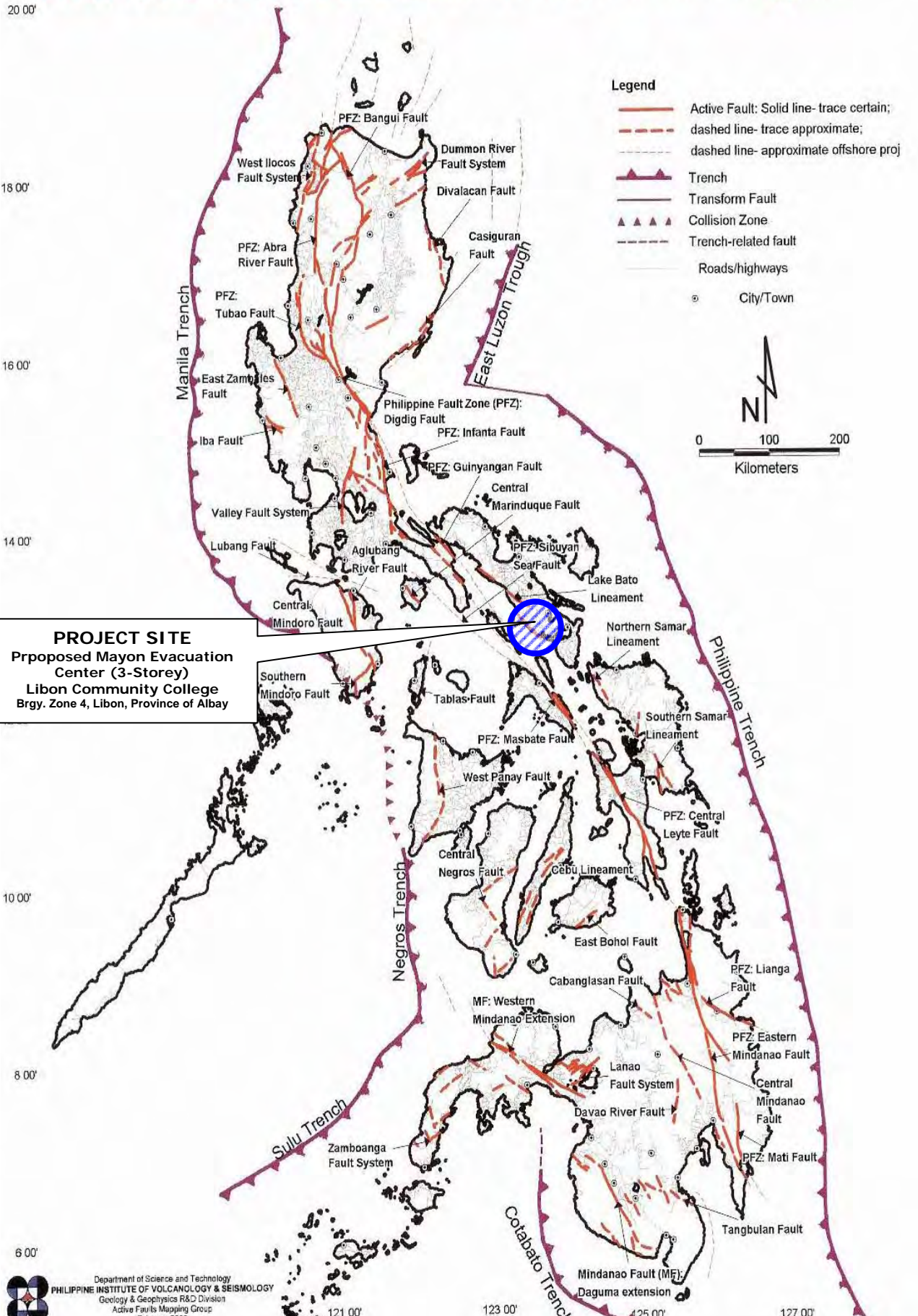
6 00'

Legend

- Active Fault: Solid line- trace certain;
- dashed line- trace approximate;
- dashed line- approximate offshore proj
- Trench
- Transform Fault
- Collision Zone
- Trench-related fault
- Roads/highways
- City/Town

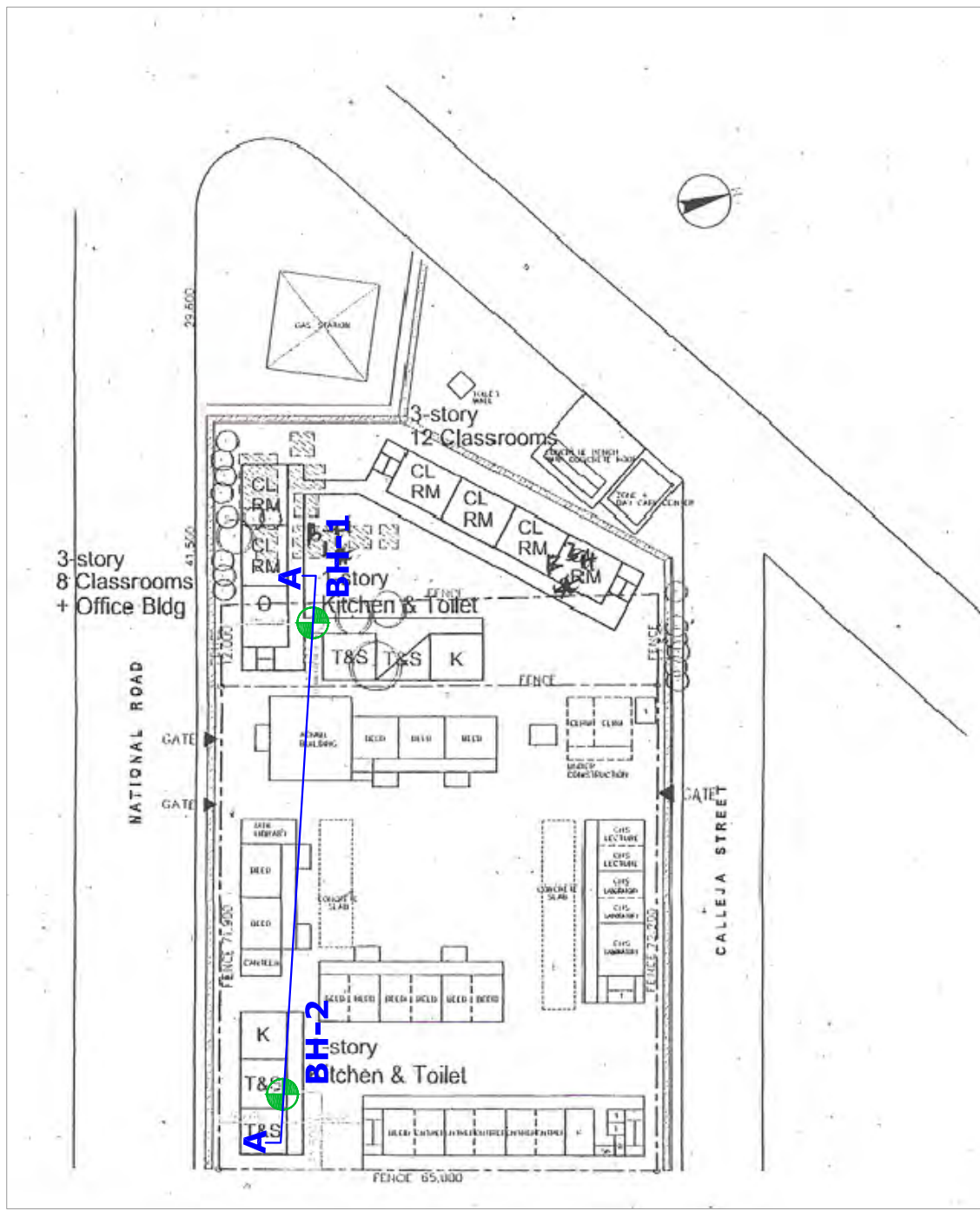


PROJECT SITE
 Proposed Mayon Evacuation
 Center (3-Storey)
 Libon Community College
 Brgy. Zone 4, Libon, Province of Albay





VICINITY MAP

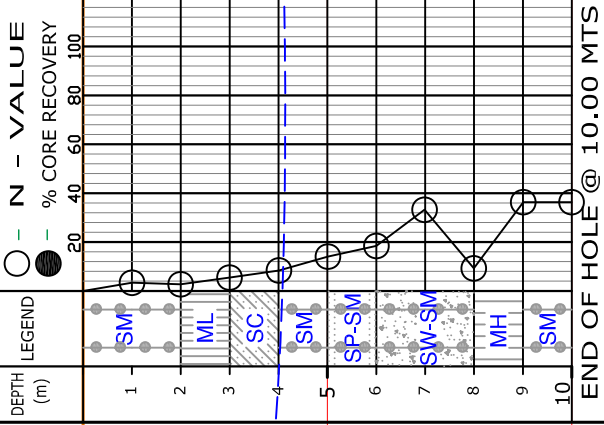
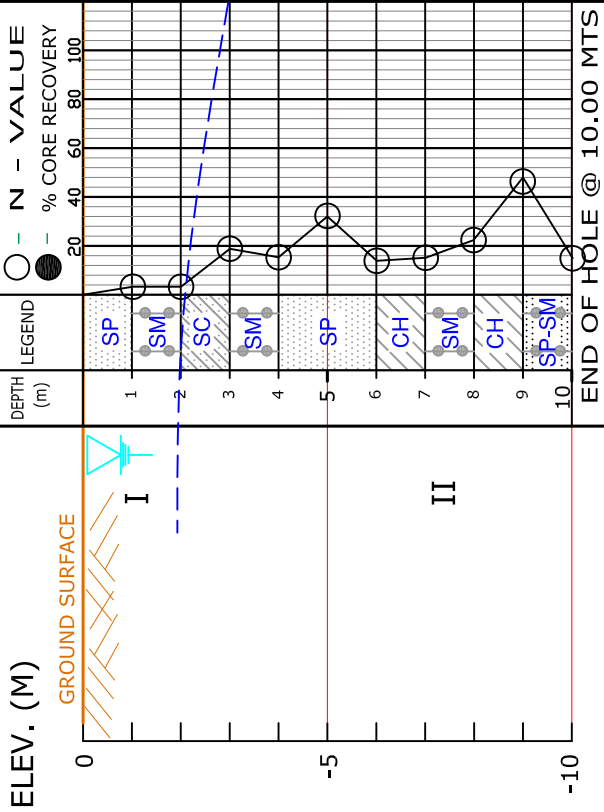


CONTRACTOR GEOTECHNICS PHILIPPINES, INC. 119 SAUYO ROAD, NOVALICHES, QUEZON CITY	PROJECT TITLE Proposed Mayon Evacuation Center (Libon Community College) Brgy. Zone 4 Libon, Province of Albay	SCALE NTS	SHEET CONTENTS LOCATION PLAN/VICINITY MAP	JOB NO. 2209-10-R1
				SHEET NO. 1/1



BOREHOLE NO. BH-1

BOREHOLE NO. BH-2



LEGEND :

- Silty CLAY
- Silty SAND
- Clayey SILT
- Silty SILT
- Clayey SAND
- Silty SAND
- Silty GRAVEL
- Clayey silty SAND

- Poorly graded SAND
- Well graded SAND
- Poorly graded SAND w/ silt
- Well graded SAND w/ silt

- Poorly graded GRAVEL
- Well graded GRAVEL
- Poorly graded GRAVEL w/ silt
- Well graded GRAVEL w/ silt

- SANDSTONE
- Clayey silty GRAVEL
- COBBLES
- GRAVEL
- SILTSTONE
- Silty TUFF
- Sandy TUFF
- SHALE

- I - N-VALUE < 10 (LIQUEFIABLE ZONE)
- II - N-VALUE > 10
- III - REFUSAL (WEATHERED ZONE)
- IV - CORING / HARD FORMATION

SECTION A - A

CONTRACTOR



GEOTECHNICS PHILIPPINES, INC.
119 SAUYO ROAD, NOVALICHES, QUEZON CITY

PROJECT TITLE :

**Proposed Mayon Evacuation Center
(Libon Community College)**
Brgy. Zone 4 Libon, Province of Albay

SHEET CONTENTS :

SOIL PROFILE
SCALE : N. T. S.

DRAWN BY :

MARIA ANTONIETTE P. CUNAHAP

CHECKED BY :

A. B. A. / M. R. R.

CERTIFIED BY :

AUTHORIZED SIGNATORY

JOB NO.

2209-10.R1

SHEET NO.

1/1