#### 9. The other inspection results

9-1 Visual inspection, Thickness measurement

Visual inspection results for boiler inside are shown in Table II -12

(Erosion of Water Wall tube around short soot blower)

- Erosion by soot blower were observed at a number of Water Wall tubes around short soot blower.
- ➤ The thickness measurement was carried out at the representative eroded portion (2<sup>nd</sup> short soot blower level) as shown in Table II-13~16.
- Min.thickness was 5.3mm at a rear wall tube around #1 short soot blower from right, that was less than the designed value tsr (thickness required) 6.1mm calculated with designed OD, pressure and allowable stress at the designed temperature.



Erosion of rear wall tube [extracted from Table II-12]

(Erosion of Water Wall tube around burner portion)

- Erosion by soot blower was observed at a number of Water Wall tubes around burner portion.
- The thickness measurement was carried out at the eroded portion as shown in Table II -17.
- Min.thickness was 4.7 mm, that was less than the tsr 6.1mm.



Erosion of Water Wall tube around burner portion [extracted from Table II-12]

(Erosion of Water Wall tube around corner portion)

- Erosion around corner portion at soot blower level was observed.
- ➤ The thickness measurement was carried out at the eroded portion as shown in Table II -18.
- Min.thickness was 4.2 mm, that was less than the tsr 6.1 mm.



Erosion of Water Wall tube around corner portion [extracted from Table II-12]

(Erosion of Platen SH tube at the highest level of soot blower)

- Slight erosion of Platen SH tube was observed at the highest level of soot blower.
- ➤ The thickness measurement was carried out at the eroded portion as shown in Table II -19.
- Min.thickness was 9.8mm, that was larger than the designed thickness 9.6 mm.



Erosion of Platen SH tube at the highest level of soot blower [extracted from Table II-18]

#### 9-2 OD measurement results

OD measurement results of residual life evaluated portion are shown in Table II  $-20 \sim 23$ .

• The increase in measured average OD to designed value was less than 1% for each portion, indicating no remarkable creep strain

Table II -24 OD measurement results of each portion (Increase in measured average OD to designed value)

Components	Location	Material	(Averaged measured value- Designed OD) /Designed OD(%)
Final SH Outlet Header	Circumferential weld at right side	SA335P22	0.74
De-Superheater-Left	Circumferential weld	SA335P12	0.44
De-Superheater-Right	Circumferential weld	SA335P12	0.46
	Circumferential weld at left side	SA335P22	0.20
RH Outlet Header	Circumferential weld at right side,top	SA335P22	0.57
	Circumferential weld at right side, front	SA335P22	0.57
Main Channa Dina Diale	Circumferential weld, intrados	SA335P22	
Main Steam Pipe-Right	Circumferential weld, near the stop valve	SA335P22	_
Hot Reheat Pipe-Right	Circumferential weld	SA335P22	0.01

OD measurement was not carried out for Main Steam Pipe-Right, because the OD of Main Steam Pipe was out of the measurement range of prepared outside micrometers.

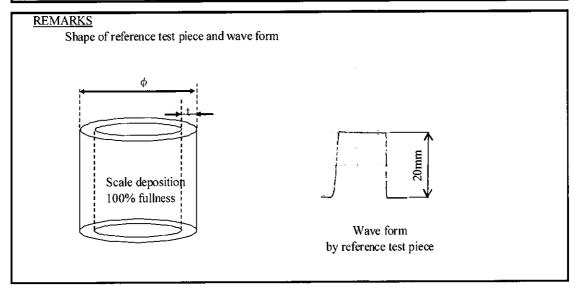
# 9-3 SUS scale deposition inspection

Applied equipment and inspection condition are shown in Table  $\,$  II -25.

Table II-25 Applied equipment and inspection condition

~	MAKER · TYPE	UNI-ELECTRONICS,Inc. · SSD-1
ŢŌ	I.D.№	34A3382 (64SCA02101)
ETECTOR	CHECK DATE PERSON	2009 June 5th · Shinichi Aizawa
DE	VAIDITY DATE	2010 June 4th
H.	MAKER • TYPE	HIOKI E. E. CORPORATION · 8205-10
	I.D.No.	041213164 (64SCZ05102)
RECORDER	CHECK DATE PERSON	2009 May 28th · Shinichi Aizawa
	VAIDITY DATE	2010 May 27th

INSPECTION METHOD	Magnetized scale deposition inspection of tube inside with scale detector
INSPECTION METHOD	Refer to next page
SENSITIVITY LEVEL	The sensitivity is adjusted at 20mm in amplitude of signal with the probe touching right to the reference test piece filled with the white magnetic particle 100% fullness.
SCANNING SPEED	Approx. 0.3m/sec
RECORDING RANGE	1V/cm
RECORDING SPEED	2.5mm/sec
REFERENCE TEST PIECE	Platen SH outermost tube bend portion, bottom tube straight portion $\phi$ 54.0×t9.5 (ID.No.50-21-1) $\phi$ 54.0×t5.6 (I.D. No : 50-20-1)



SUS scale deposition inspection was carried out at outer most tube bottom bend and horizontal portion of Platen-SH as shown in Fig. II -2.

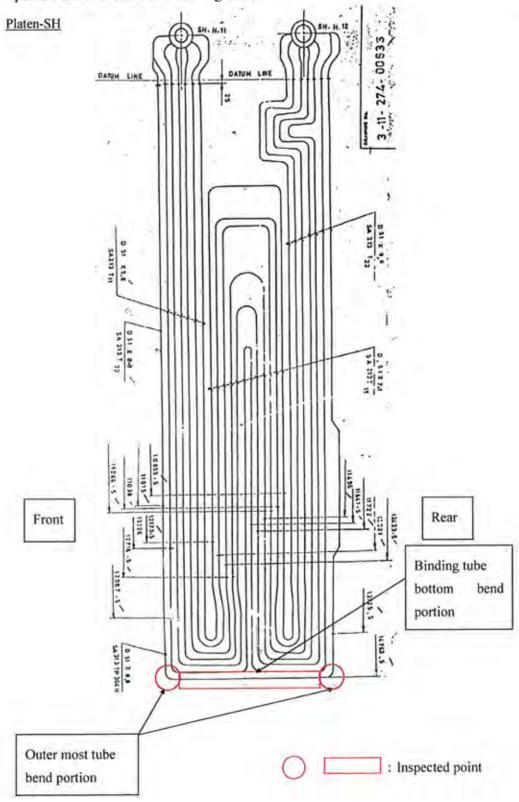


Fig. II -2 Inspection location

SUS scale deposition inspection results are shown in Table II -26.

SUS scale deposition was not significant with 15% fullness for 4 points, 10% fullness for 2 points and less than 10% fullness for the other portions.

Table II-26 SUS scale deposition inspection results

Platen Super Heater (Outermost tube bend portion)					
F	ront	R	ear		
Panel No.	Fullness (%)	Panel No.	Fullness (%)		
17	10	27	15		
18	15				
19	10				
20	15				
22	15				

#### (Remarks)

- Standard curve with  $\phi$  54.0×t9.5 was used for evaluation of fullness.
- The signal by magnetization of tube material with heat was recognized at front bend, rear bend and horizontal portion.

The representative deposition signal for this inspection is shown in Fig. II -3.

The standard curve used is shown in Fig. II -4.



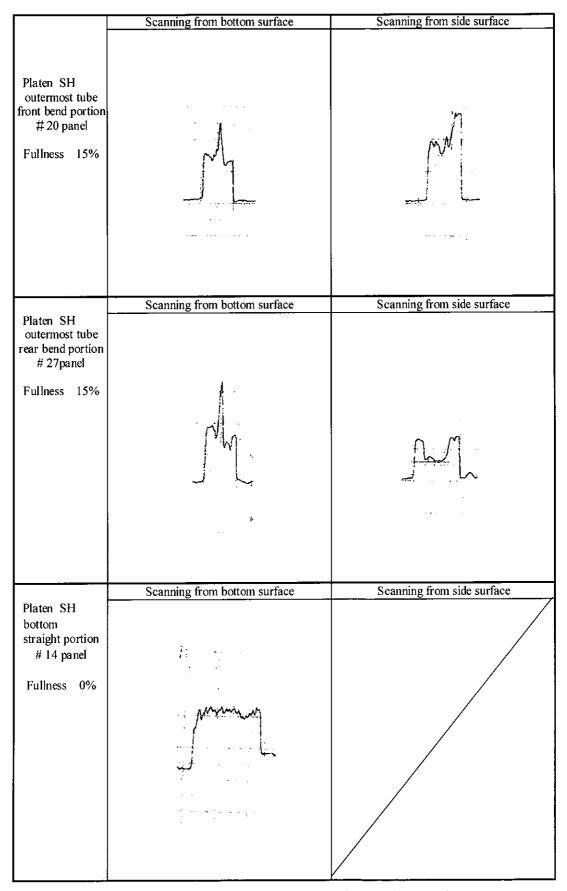
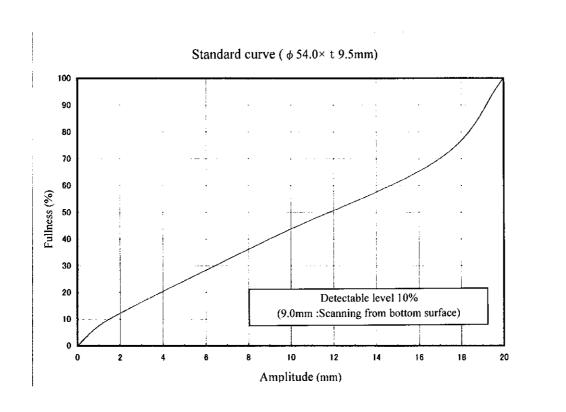


Fig. II-3 Representative deposition signal for this inspection



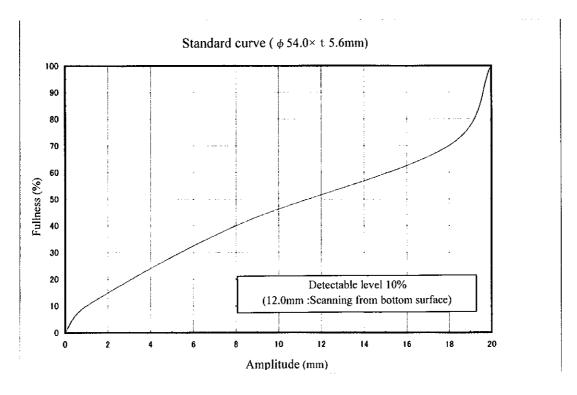


Fig. II -4 Standard curve used for evaluation

# 9-4 DPT

Applied material and examination condition are shown in Table II -27.

Table II -27 Applied material and examination condition

# APPLIED MATERIAL

AL	PENETRANT	BRAND	Eishin Kagaku Co., Ltd.
ERI		MAKER	R-1A(NT)
MATERIAI	REMOVER	BRAND	Eishin Kagaku Co., Ltd.
ED		MAKER	R-1S(NT)
APPLIED	DEVELOPER	BRAND	Eishin Kagaku Co., Ltd.
		MAKER	R-1M(NT)

### **EXAMINATION CONDITION**

EXAMINATION CONDITION	1.002-00-00
EXAMINATION METHOD	Liquid penetrant with removability for solvents - Drying development method
TIME TO EXAMINATION	at periodic inspection
TEMPERATURE OF EXAMINATION SURFACE	Normal temperature (10∼50°C)
EXAMINATION SURFACE CONDITION	As weld
PRE-TREATMENT	■Rinse with solvents □Others ( )
PENETRATION METHOD	■Spray □Brush painting □Dipping □Others ( )
PENETRATION TIME	10 minutes
REMOVING OF EXTRA PENETRANT	■ Wipe out with wes (using solvent) □Others ( )
DEVELOPMENT METHOD	■Spray □Brush painting □Dipping □Others ( )
DEVELOPMENT TIME	10 minutes
ILLUMINANCE OF EXAMINATION SURFACE/ILLUMINANCE OF ENVIRONMENT	500Lux or more

Inspected location of DPT is shown in Fig. II -5.

DPT inspection were carried out at 4 stub weld portions of #3 panel from right in Platen SH inlet header front side.

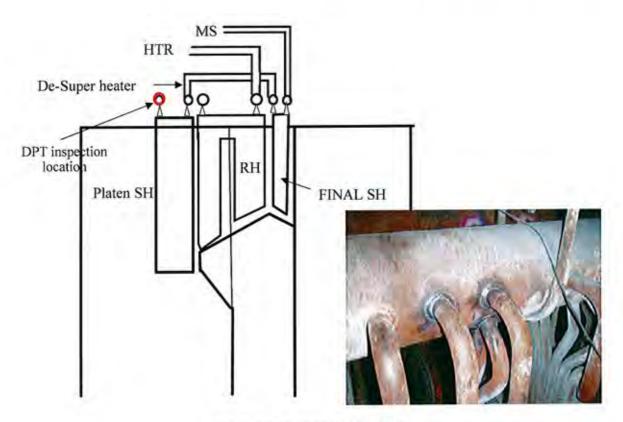


Fig. II -5 DPT inspection location

The indication pattern detected location is shown in Fig. II-6.

Two for each of  $\phi$  2mm and  $\phi$  1mm circular indication pattern were detected at 4th tube from front, although no indication pattern was judged as crack. After grinding off these indications, a new  $\phi$  2mm circular indication pattern appeared. The new indication has been left since it was not judged as crack.

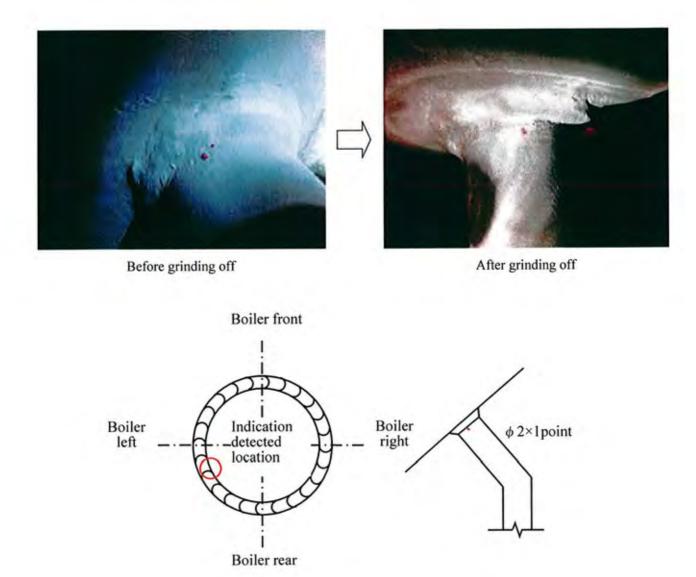


Fig. II-6 The indication pattern detected location

# 9-5 UT

Applied equipment and examination condition are shown in Table  $\, \, {\rm II}$  -28.

Table II -28 Applied equipment and examination condition

# APPLIED EQUIPMENT AND MATERIAL

	MAKER • TYPE	GE INSPECTIO	GE INSPECTION TECHNOLOGIES · USM35X				
8	SERIAL No.(I.D.№)	994a(61UAA06110)					
DETECTOR	AMPLITUDE LINEARITY	within ±3%	within ±3%				
	TIME SCALE LINEARITY	within ±1%					
FLAW	MARGIN OF DETECTION	40dB or more					
丘	CHECK DATE · PERSON	2008 November 2	20th · Hidekazu I	shihara(UT-2)			
	VAIDITY DATE	2009 November	19th				
	ТҮРЕ	angle beam probe	angle beam probe				
	DESIGNATION	2C14×14A45	2C14×14A60				
	MAKER	KGK	KGK				
	SERIAL No.	XA7426	18421				
	DEAD ZONE	7.5mm	8mm				
PROBE	STB ANGLE OF REFRACTION	45 degree	60 degree				
PR	ACCESIBLE LIMIT DISTANCE	14mm	15mm				
	FAR SURFACE RESOLUTION	7nun	7mm				
	CHECK DATE · PERSON	2009 August 26th Kawazu (UT-2)	2009 May 22th Kawazu (UT-2)				
	VAIDITY DATE	2010 February 25th	2010 February 25th				

# EXAMINATION CONDITION

EXAMINATION METHOD	Single angle beam probe technique
TIME TO EXAMINATION	at periodic inspection
SURFACE CONDITION	Grinded surface
COUPLANT	Sonicoat
SPECIFIED SENSITIVITY	RB-41 №2 φ 3.0mm side cylindrical hole: H-line
SENSITIVITY CORRECTION	Non
DISREGARD LEVEL	Regarded as flaw that echo hight is over DAC(H-line)
ACCEPTANCE CRITERIA	Crack length is 19mm or less
REFERENCE BLOCK OR CALIBRATION BLOCK	RB-41 №2 RB-41 №2
ANGLE OF REFRACTION IN TEST OBJECT	ANGLE OF REFRACTION: —  CALCULATION METHOD: □ Ratio of sound velocity of STB  □ V path technique

Inspected location of UT is shown in Fig. II -7.

UT inspection was carried out at circumferential weld of right side in Final-SH Outlet Header. As a result of UT inspection, no flaw echo exceeding the criteria was detected.

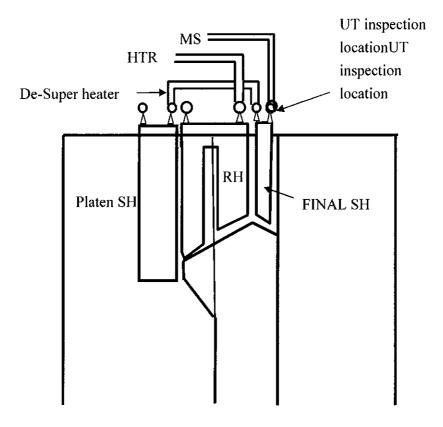


Fig. II -7 Inspected location of UT

#### 9-6 TOFD

Applied equipment and examination condition are shown in Table II -29.

TOFD inspection was carried out at the location identical to UT inspection location in Final-SH Outlet Header with three sets of detection in different depth of focal point from surface.

TOFD detection results are shown in Fig. II -8 $\sim$ 11.

No flaw echo judged as a crack was detected, although continuous subtle flaw echoes were detected at about 80mm in depth from surface.

Table II -29 Applied equipment and examination condition

#### APPLIED EQUIPMENT AND MATERIAL

FLAW TECTOR	MAKER · TYPE	OLYMPUS NDT $\mu$ -Tomoscan
FL, DETE	SERIAL No.(I.D.№)	23918-15(71UAA96105)
	DESIGNATION	5MHz、 φ 1/4inch
BE [	WEDGES	60°and 45°
PROBE	MAKER	GE INSPECTION TECHNOLOGIES
	SERIAL No.	00CP4M,00B25K

#### **EXAMINATION CONDITION**

EXAMINATION METHOD	TOFD technique
TIME TO EXAMINATION	at periodic inspection
SURFACE CONDITION	Grinded surface
COUPLANT	Sonicoat
SPECIFIED SENSITIVITY	φ 4.8mm side cylindrical hole ((d=40mm):80%+6dB
SENSITIVITY CORRECTION	Non
DISREGARD LEVEL	
ACCEPTANCE CRITERIA	
REFERENCE BLOCK OR CALIBRATION BLOCK	$\phi$ 4.8mm side cylindrical hole (d=20,40,60,80,100mm)

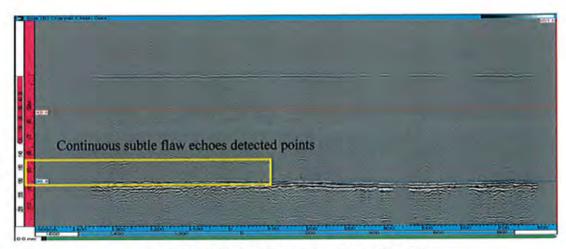


Fig. II -8 Set1 (Monitor range: 50mm~bottom)

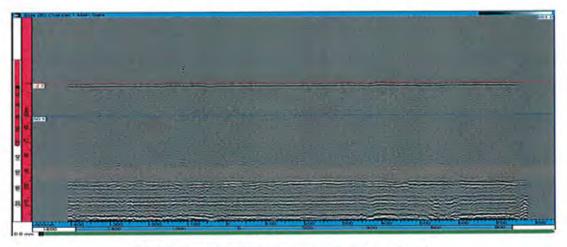


Fig. II -9 Set2 (Monitor range : Surface~50mm)

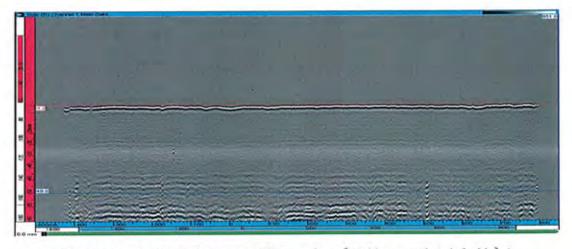


Fig. II -10 Set3 (Monitor range: Near surface [Weld toe portion, left side])

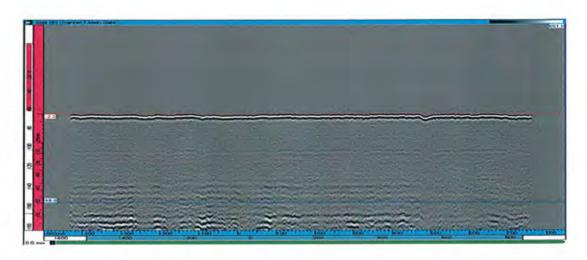
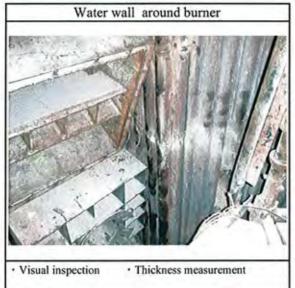
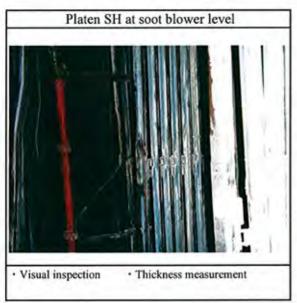
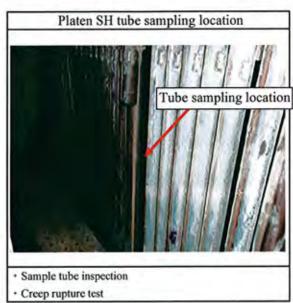


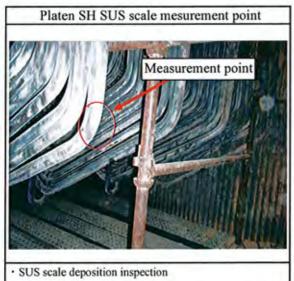
Fig. II -11 Set3 (Monitor range: Near surface [Weld toe portion, right side])

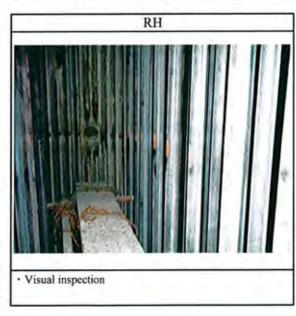


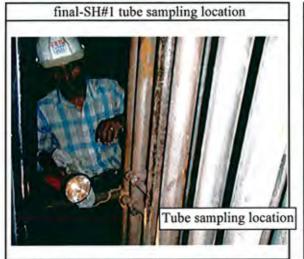




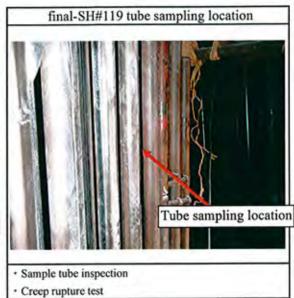


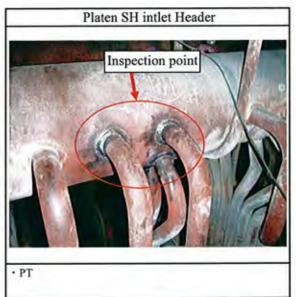


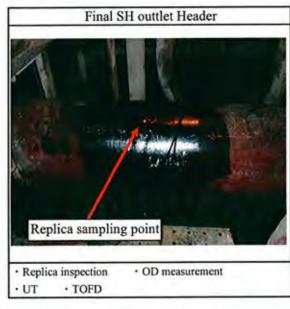


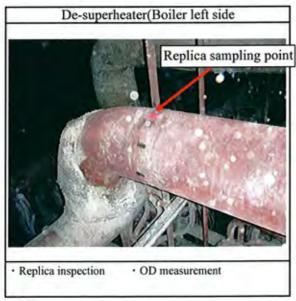


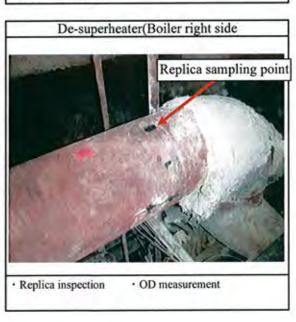
· Sample tube inspection



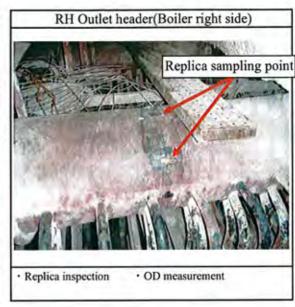




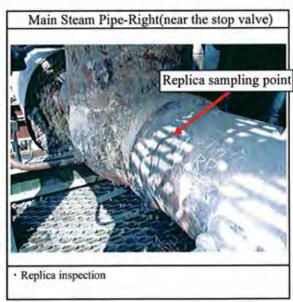












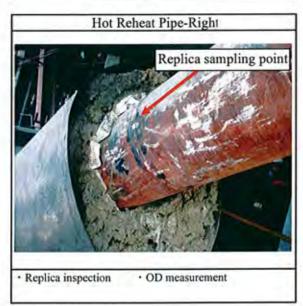


Table II -4 Microstructure observation resuluts

ا بر				OM (Optical microscope observation)							
Components		ficon	011	Microstructural features							
Comp		Location	Observed region	Precipitation at gain boundary	Precipitates free zone along grain boundary		Rod-shaped precipitates in ferrite grain	Granular precipitates	Coarse granular precipitates		
Final SH outlet header (SA 335 P22)		•	Base metal	Appeared	Not appeared						
	header	ntial	Intercritical zone	Not appeared	Not appeared						
SA 335 P22)	Rightside of header	Circumferential weld	Fine grain HAZ	Appeared							
nal Sh (SA	Rights	Ç	Coarse grain HAZ	Appeared							
選			Weld metal								
			Base metal	Appeared	Not appeared	Not appeared	Not appeared				
	icater	fia)	Intercritical zone	Appeared				Remaining	Not appeared		
	Left de superheater	Circumferential weld	Fine grain HAZ	Appeared					Not appeared		
ipe	Left de	2	Coarse grain HAZ	Not appeared					Not appeared		
De-Superheater pipe (SA 335 P12)			Weld metal					Appeared			
uperh			Base metal	Appeared	Not appeared	Not appeared	Not appeared				
De-S	heater	tial	Intercritical zone	Appeared				Remaining	Not appeared		
	e super	Circumferential weld	Fine grain HAZ	Appeared					Not appeared		
ŀ	Right de superheater	Circu	Coarse grain HAZ	Appeared					Not appeared		
	_		Weld metal					Appeared			
		_	Base metal	Appeared	Not appeared						
		Ę.	Intercritical zone	Appeared	Not appeared						
	Left	Circumferential weld	Fine grain HAZ	Appeared							
		Circur	Coarse grain HAZ	Not appeared							
			Weld metal								
_		Circumferential Circumferential wedd (Atnormal microstructure) wedd	Base metal	Appeared	Not appeared						
Reheater outlet header (SA 335 P22)			Intercritical zone	Appeared	Not appeared						
ater outlet he (SA 335 P22)			Fine grain HAZ	Appeared							
heater (SA			Coarse grain HAZ	Appeared							
Re	ä		Weld metal								
	Right		Base metal	Appeared	Not appeared						
			Intercritical zone	Appeared	Not appeared						
			Fine grain HAZ	Appeared							
			Coarse grain HAZ	Appeared							
ŀ			Weld metal								
				Base metal	Appeared	Not appeared					
	üghī	üghı	lial Pyalvo	Intercritical zone	Appeared	Not appeared					
			Figh.	Right	Circumferential weld (near the stop valve) intrados side	Fine grain HAZ	Appeared				
		Circit d (near intra	Coarse grain HAZ	Appeared							
m pip P22)		r.cl	Weld metal								
Main steam pipe (SA 335 P22)			Base metal	Appeared	Not appeared						
<sub>S</sub> S		tial p valve	Intercritical zone	Appeared	Not appeared						
	Right	Circumferential (near the stop v	Fine grain HAZ	Appeared							
	-	Circumforential weld (near the stop valve)	Coarse grain HAZ	Not appeared							
		wck	Weld metal								
$\dashv$			Base metal	Appeared	Not appeared						
3) je		ii i	Intercritical zone	Appeared	Not appeared						
ts P22	Right	Circumferential weld	Fine grain HAZ	Appeared							
ē m	Ź	R.	Righ	Circun	Coarse grain HAZ	Appeared					
Hot reh (SA 33	ı	]		1		and the same of th	ــــــــا	ا	1		
Hot reheat pipe (SA 335 P22)			Weld metal								

Table II -5 Creep void observation results

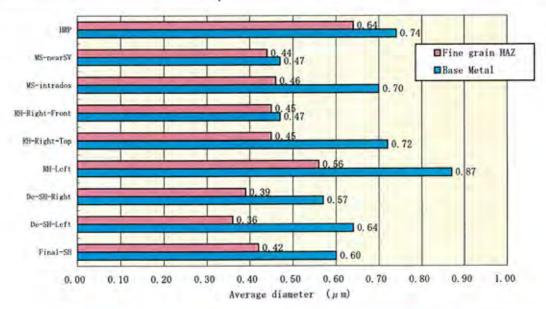
Components	Location		Observed region	SEM (Scanning Electron Microscope observation)	
	8	<u> </u>		Ceep void damage	
Final SH outlet h	Rightside of heade	rential	Fine grain HAZ	No void	
SH o	side o	Circumferential weld	Coarse grain HAZ	No void	
Fina		Ë	Weld metal	No void	
	rheater	ential	Fine grain HAZ	No void	
pipe (	e supe	Circumferential weld	Coarse grain HAZ	No void	
eater 5 P12	Left d	Circ	Weld metal	No void	
De-Superheater pipe (SA 335 P12)	Right de superheate Left de superheater	ntial	Fine grain HAZ	No void	
P P	de supe	Circumferential weld	Coarse grain HAZ	No void	
	Right	Ç	Weld metal	No void	
		ntial	Fine grain HAZ	No void	
	Left	Circumferential weld	Coarse grain HAZ	No void	
k		Circ	Weld metal	No void	
Reheater outlet header	· · · · · · · · · · · · · · · · · · ·	rtial	Fine grain HAZ	No void	
outle		Circumferential weld	Coarse grain HAZ	No void	
heater	Į.	Circu	Weld metal	No void	
Re	.gg	Right Circumferential weld (Abnormal microstructure)	Fine grain HAZ	No void	
			Coarse grain HAZ	No void	
			Weld metal	No void	
		ntial e stop is side	Fine grain HAZ	No void	
پ ا	Right	Circumferential weld (near the stop valve) intrados side	Coarse grain HAZ	No void	
steam pipe		Circu weld (r	Weld metal	No void	
Main stea		ial	Fine grain HAZ	No void	
Ma	Right	Circumferent reld (near the valve)	Coarse grain HAZ	No void	
;		Circumferent weld (near the valve)	Weld metal	No void	
, be			Fine grain HAZ	No void	
Hot reheat pipe	Right	Circumferential weld	Coarse grain HAZ	No void	
Hot re	1	Circu	Weld metal	No void	
				×500 (3 views)	
	V	iew nos.	for each area	×2000 (3 views)	

Table II-6 Precipitates distribution observation results

ম		_		TEM (Transmission Electron Microscope observation)								
ents		E						es features Fine				
Components	Location		Observed region	Precipitates free zone along grain boundary	Featherlike precipitates	Fine needlelike and granular precipitates	Needlelike precipitates	needlelike and granular precipitates in bainite grain	Bainite structure disintegration	Attenuated plate-shaped precipitates	Rod-shaped precipitates spherodized precipitates	
Final SH outlet header (SA 335 P22)	Jer	ie .	Base metal	Appeared	Disappeared		No decrease in ferrite grain	Partially disappeared				
(SA 335 P22)	et heac	ferenti: eld	Fine grain HAZ				Remaining					
(SA 3	Left outlet header	Circumferential weld	Coarse grain HAZ			Remaining						
Fina	1		Weld metal			Remaining						
			Base metal	Not appeared		Remaining in ferrite grain			Disintegrated	Not appeared		
	rheater	ential	Fine grain HAZ			Remaining				Not appeared	Coexist	
De superheater pipe	Left de superheater	Circumferential weld	Coarse grain HAZ			Remaining					Derease of roo shaped precipitates at spherodized	
erheat			Weld metal			Remaining						
De sup	ater	le le	Base metal	Not appeared		Remaining in ferrite grain			Disintegrated	Not appeared		
	Right de superheater	ferentia eld	Fine grain HAZ			Remaining				Not appeared	Coexist	
		Circumferential weld	Coarse grain HAZ			Remaining					Coexist	
	Ris		Weld metal			Remaining						
		<u></u>	Base metal	Appeared	Disappeared		No decrease in ferrite grain	Partially disappeared				
	Left	Circumferential weld	Fine grain HAZ				Disappeared					
	1	Circum	Coarse grain HAZ			Disappeared						
			Weld metal			Remaining		2 511				
Reheater outlet header (SA 335 P22)	Right	tial	Base metal	Appeared	Disappeared		No decrease in ferrite grain	Partially disappeared				
(SA 335 P22)		Circumferential weld	Fine grain HAZ				Spherodized					
(SA 3	æ	Circun	Coarse grain HAZ			Remaining						
₹   ¥		_	Weld metal			Remaining	No decrease	Partially				
		tial mal re)	Base metal	Appeared	Disappeared		in ferrite grain	disappeared				
	Right	Circumferential weld (Abnormal microstructure)	Fine grain HAZ				Spherodized					
	4		Coarse grain HAZ			Remaining						
$\rightarrow$			Weld metal			Remaining	No decrease					
		Circumferential weld (near the stop valve) intrados side	Base metal	Appeared	Disappeared		in ferrite grain	Disappeared				
	Right		Fine grain HAZ				Disappeared					
23 E	1		Coarse grain HAZ			Disappeared						
335 P.			Weld metal			Disappeared	No decrease					
Main steam pipe (SA 335 P22)		Circumferential weld (near the stop valve)	Base metal	Appeared	Disappeared		in ferrite grain	Disappeared				
	Right	mferer the st	Fine grain HAZ				Spherodized					
		Circu d (nea	Coarse grain HAZ			Remaining						
$\longrightarrow$		wel	Weld metal			Remaining	No decrease	Partially				
23 pa		ntial	Base metal	Appeared	Disappeared		in ferrite grain					
35 P22	Right	Circumferential weld	Fine grain HAZ			<u> </u>	Disappeared					
335 I		Circui	Coarse grain HAZ			Disappeared						
Hot reheat pipe (SA 335 P22)		Cir	Weld metal			Disappeared						

Table II-7 Quantitative evaluation of grain boundary precipitates

	77177777		Average dian	neter (µm)	Volume fraction		
Component	Evaluated location	Material	Base Metal	Fine grain HAZ	Base Metal	Fine grain HAZ	
Final SH Outlet Header	Circumferential weld at right side	SA335P22	0.60	0.42	0.021	0.025	
De-Suerheater-Left	Circumferential weld	SA335P12	0.64	0.36	0.024	0.017	
De-Suerheater- Right	Circumferential weld	SA335P12	0.57	0.39	0.026	0.024	
	Circumferential weld at left side	SA335P22	0.87	0.56	0.056	0.054	
RH Outlet Header	Circumferential weld at right side,top	SA335P22	0.72	0.45	0.037	0.031	
	Circumferential weld at right side, front	SA335P22	0.47	0.45	0.016	0.032	
Main Steam Pipe-	Circumferential weld,intrados	SA335P22	0.70	0.46	0.044	0.028	
Right	Circumferential weld,near the stop valve	SA335P22	0.47	0.44	0.017	0.028	
Hot Reheat Pipe- Right	Circumferential weld	SA335P22	0.74	0.64	0.049	0.048	



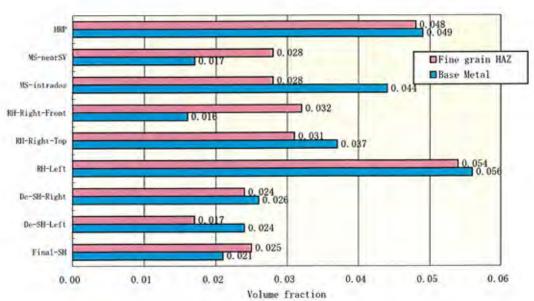


Table II-8 Precipitates free band width along grain boundary

Commissions	Evaluated location	Material	Precipitates free band width (µm) *1					
Component	Evaluated location	Material	Base Metal					
Final SH Outlet Header	Circumferential weld at right side	SA335P22	0.87					
	Circumferential weld at left side	SA335P22	0.85					
RH Outlet Header	Circumferential weld at right side,top	SA335P22	0.89					
	Circumferential weld at right side, front	SA335P22	1.04					
Main Steam Pipe-	Circumferential weld,intrados	SA335P22	0.81					
Right	Circumferential weld,near the stop valve	SA335P22	0.93					
Hot Reheat Pipe- Right	Circumferential weld	SA335P22	1.23					

※1 : Average value of 10 measured points

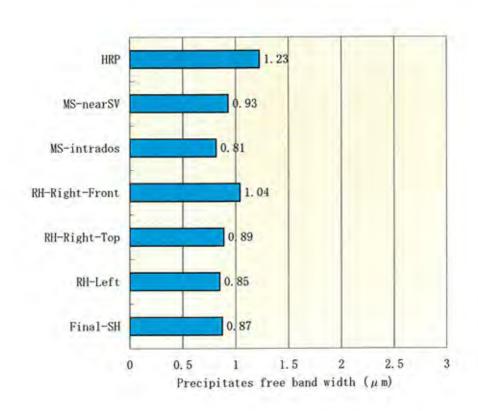
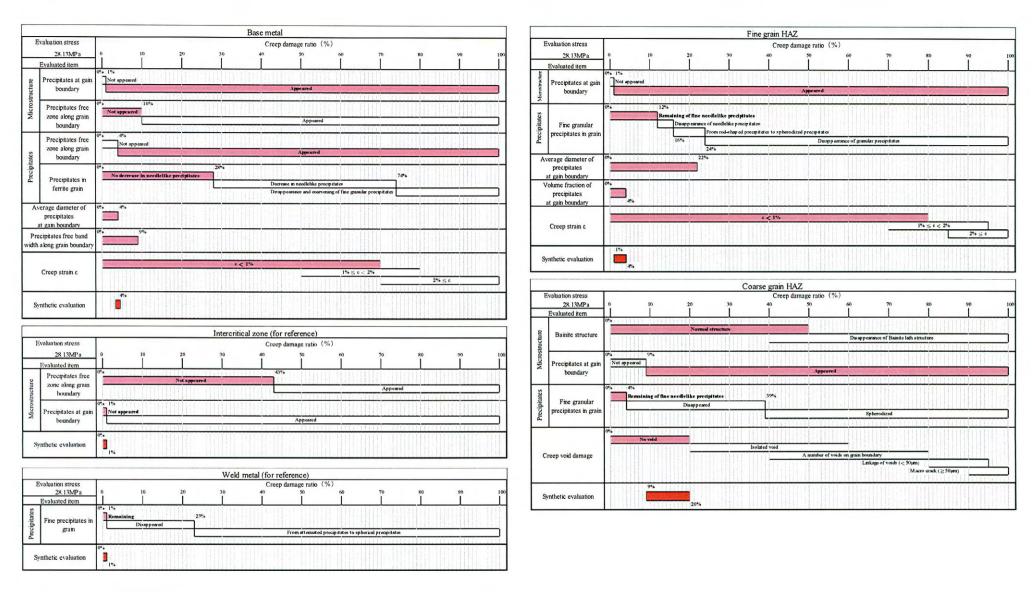
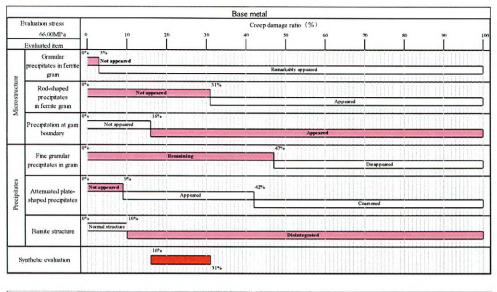


Table II -9 Operational condition of evaluated components(Unchahar)

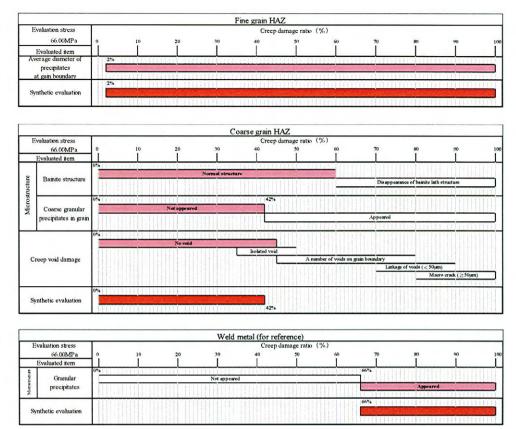
		Material			•	Hann Samon				
Component	Location	Mate	O.D.	t	Temperature	Рте	ssure	Hoop Stress		
		ASME	JIS	(mm)	(mm)	(°C)	(MPa)	(kg/cm <sup>2</sup> )	(MPa)	(kg/mm <sup>2</sup> )
Final SH Outlet Header	Circumferential weld at right side	SA335P22	STPA24	457.2	100.0	555	15.75	160.6	28.13	2.87
De-Suerheater-Left	Circumferential weld	SA335P12	STPA22	406.4	45.0	450	16.44	167.6	66.00	6.73
De-Suerheater-Right	Circumferential weld	SA335P12	STPA22	400.4	45.0	430				0.73
	Circumferential weld at left side	SA335P22	STPA24	558.8	45.0	555	4.32	44.1	24.69	
RH Outlet Header	Circumferential weld at right side,top	SA335P22	STPA24							2.52
	Circumferential weld at right side, front	SA335P22	STPA24							
Main Community District	Circumferential weld, intrados side	SA335P22	STPA24	255.6	50.3	540	1.5.54	160.5	47.77	4.87
Main Steam Pipe-Right	Circumferential weld,near the stop valve	SA335P22	STPA24	355.6	30.3	340	15.74			
Hot Reheat Pipe-Right	Circumferential weld	SA335P22	STPA24	508.0	28.0	540	3.69	37.6	31.61	3.22



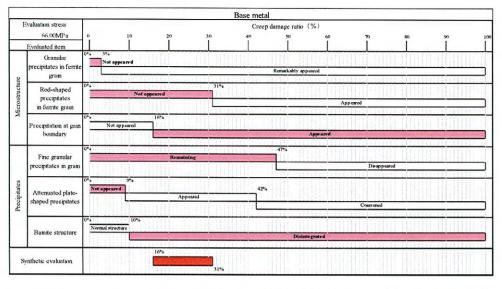




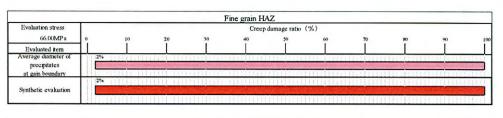
				Intercritic	cal zone (fo	r reference)								
Evaluation stress		Creep damage ratio (%)												
66.00MPa	0	10	20	30	40	50	60	70	80	90	10			
Evaluated item														
Synthetic evaluation														

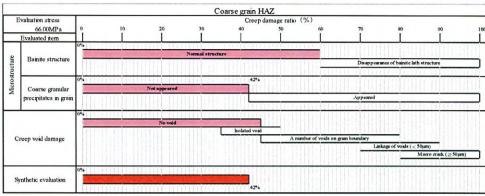






				Intercritic	cal zone (for	reference)					
Evaluation stress					Creep	damage ratio	(%)				
66.00MPa	0	10	20	30	40	50	60	70	80	90	100
Evaluated item	ed item					1					
Synthetic evaluation											





Eva	luation stress					Creep	damage ratio	(%)					
	66.00MPa	0	10	20	30	40	50	60		70	80	90	
Evaluated item		11								1	1	1	- 1
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		11111											



