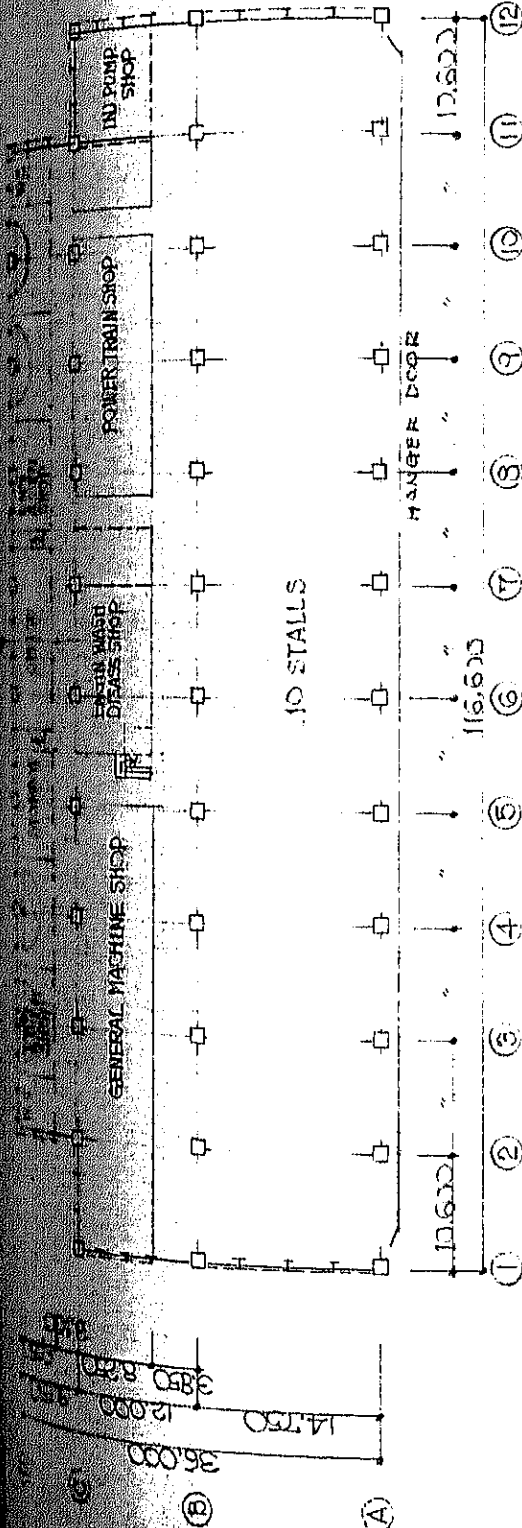


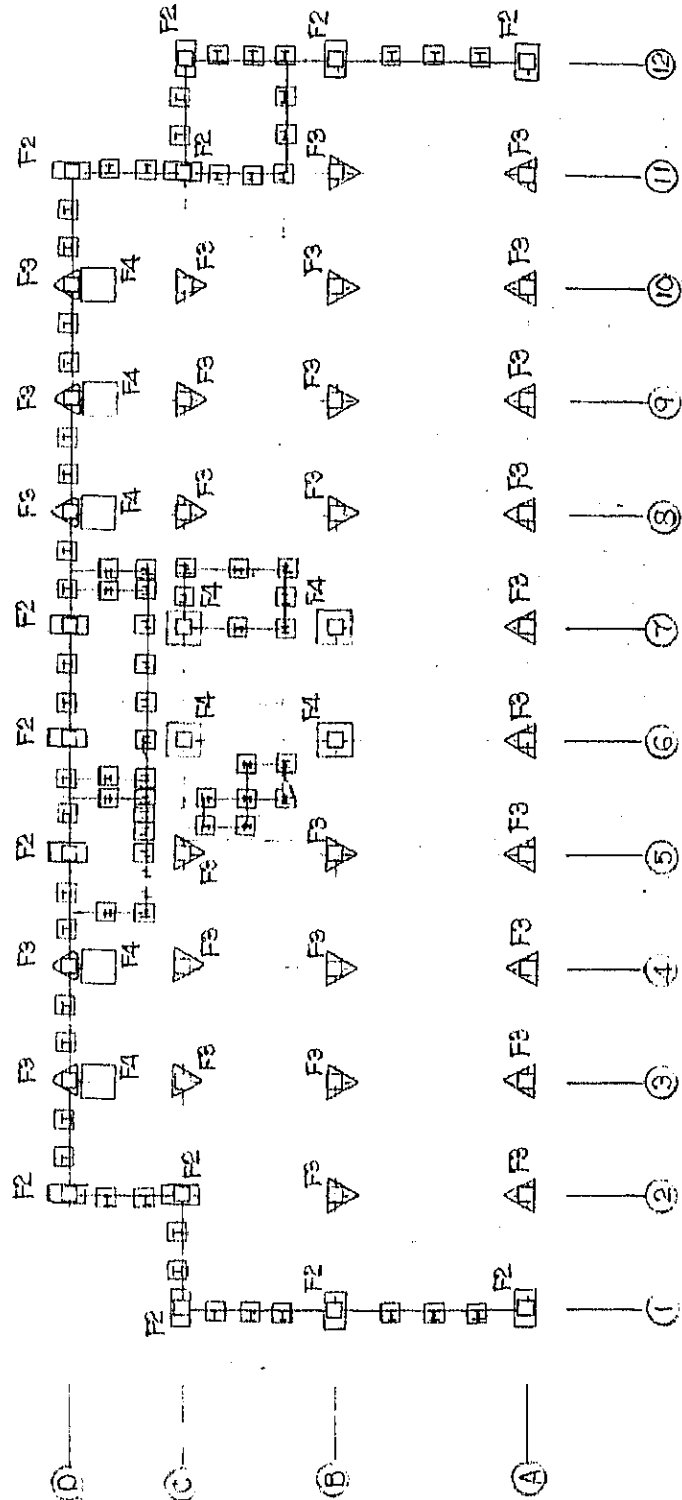
TO HEAVY REPAIR FACTORY

HEAVY REPAIR FACTORY

1F PLAN

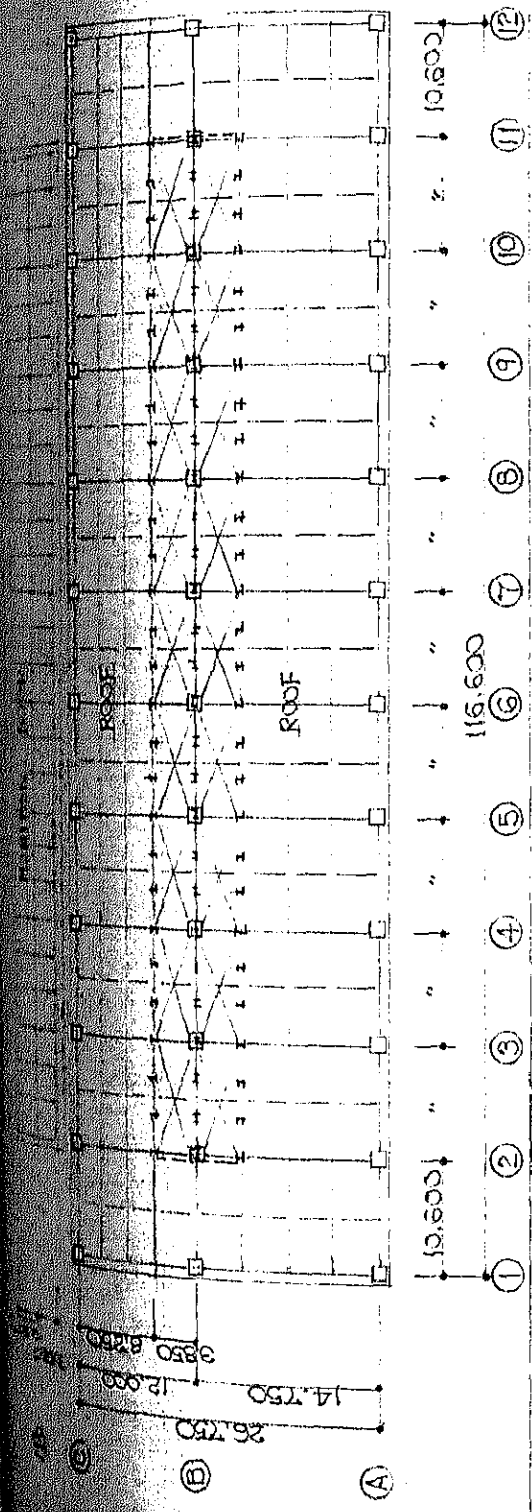


GF KEY PLAN

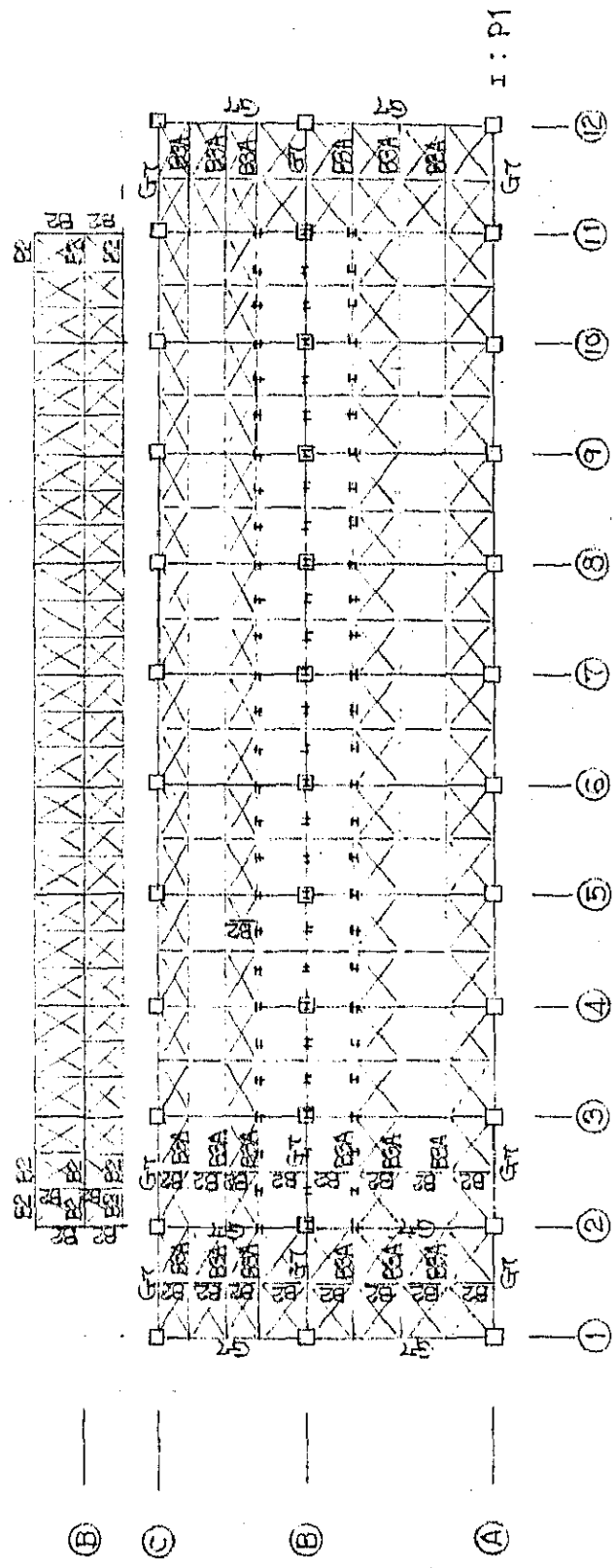


□ : F1
 — : F335

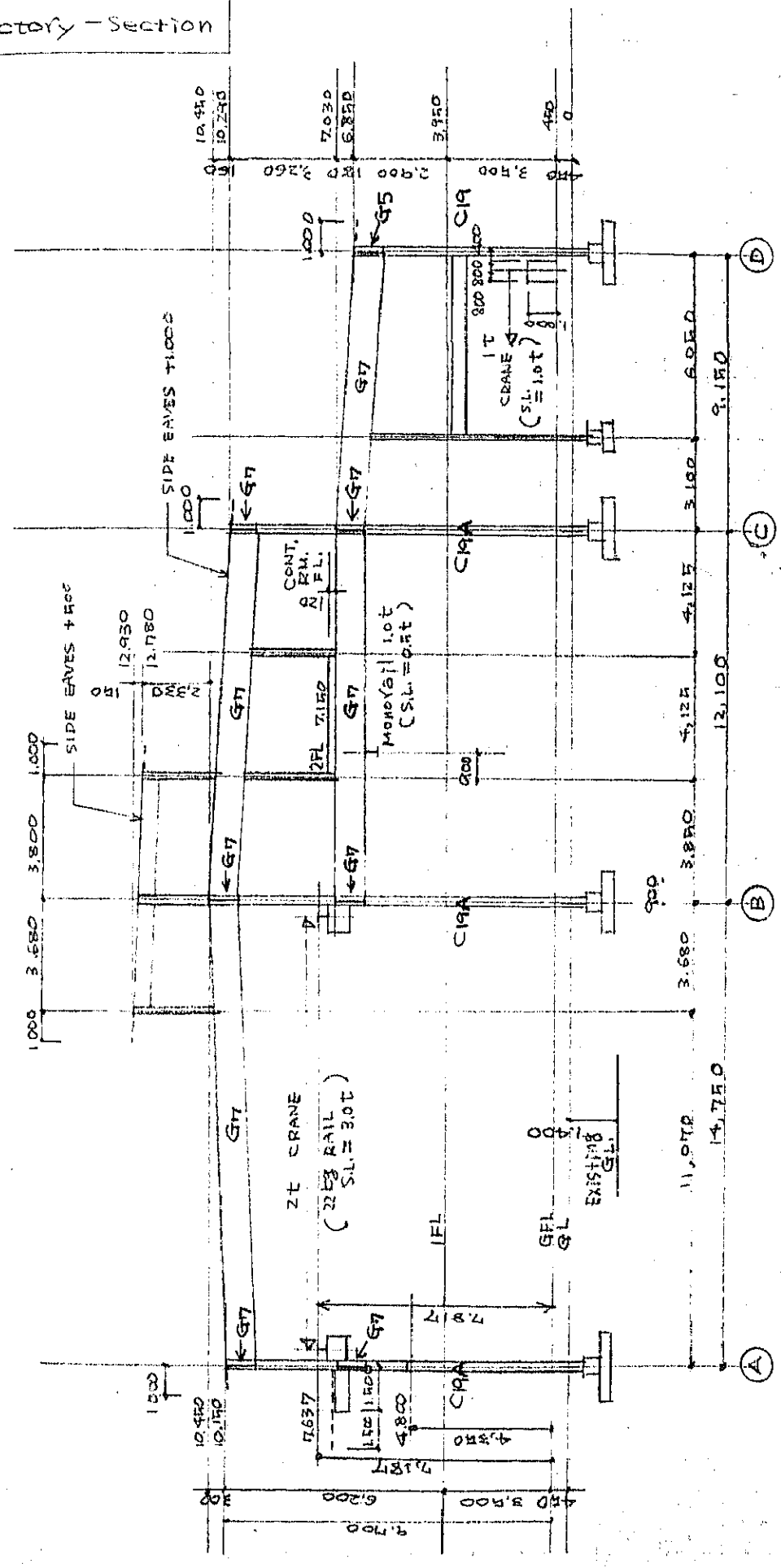
RF PLAN



RF KEYPLAN



Heavy Repair Factory - Section



Unit Load

Floor

		D. L.		L. L.		T. L.
Roof		Shell type roof	0.02	S, B	0.09	0.11 (0.15)
		Ceiling	(0.04)	G, C, F	0.07	0.09 (0.13)
			0.02 (0.06)	K	0.03	0.05 (0.09)
Floor		Finish Deck	0.13	S, B	0.30	0.51
		Ceiling	0.02	G, C, F	0.18	* 0.39
			0.21	K	0.08	0.29
					* With Above Ceiling	0.45
Step		Step	0.06	S, B	0.30	0.40
		String	0.04	G, C, F	0.18	0.28
			0.10	K	0.08	0.18

Beam

		t/m			Teach						
		Skeleton	Finish	Σ	l						
Beam	Gr	0.25	0	0.25							
	Gr	0.15	0	0.15							
	Beam	0.05	0	0.05							
	Beam	1.26	0	1.26							

Column

		t/m			Teach						
		Skeleton	Finish	Σ							
Column	Gr	0.20	0	0.20							
	Gr	0.15	0	0.15							
	Column	0.05	0	0.05							

Wall

		t/m ²			t/m						
		Skeleton	Finish	Σ							
Wall	Gr	0.01	0.01	0.02							
	Gr	0.01	0.07	0.08							
	Wall	0.01	0.04	0.05							
	Wall	0.49	0.11	0.60							

Wind Pressure

Velocity of Wind

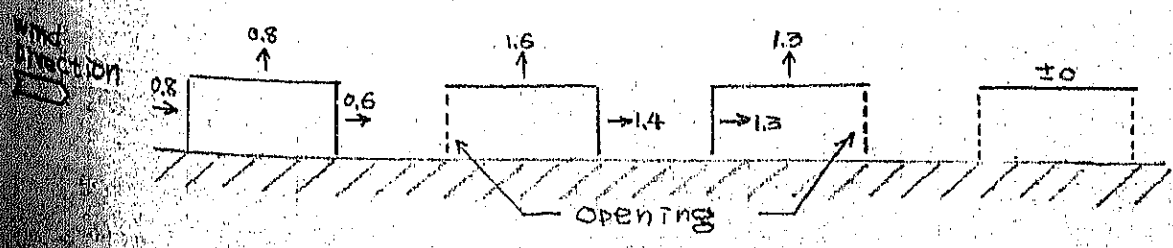
Cyclone $130 \text{ Miles/Hour} = 130 \times 1609.34 / 3,600$
 $= 58.1 \text{ m/sec}$
 $\rightarrow 60.0 \text{ m/sec } (C_h = 1.5 \text{ m})$

(In 1970, At Chittagong, recorded)
 $103 \text{ m.p.h.} = 46.0 \text{ m/sec}$

Velocity Pressure $q = \frac{1}{2} \rho V^2 = \frac{1}{2} \times \frac{1}{8} (60 \frac{\sqrt{h}}{15})^2$
 $= 60 \sqrt{h}$

Block	surface		[m]		[kg/m ²]	[lbs/ft ²]
			\bar{h}	$60\sqrt{h}$	q	Cp
Heavy repair Factory	Monitor Roof	Roof Wall	12.7	214	270	
		Roof Wall	10.5, 6.9	194, 158	200, 160	140, 120
Parts Storage	Monitor Roof	Roof Wall	9.39 - 9.29	184 - 183	180	
		Roof Wall	7.36 - 7.00	163	160	120
Inspection Factory	Monitor Roof	Roof Wall				
		Roof Wall	7.20 - 7.00	161	160	120
Periodical Repair Factory	Monitor Roof	Roof Wall	9.33 - 9.23	183	180	
		Roof Wall	7.23 - 7.00	161	160	120
Paint & Body Factory	Monitor Roof	Roof Wall	9.41 - 9.31	184	180	
		Roof Wall	7.31 - 7.00	162	160	120
Retreading & Metal Casting Factory	Monitor Roof	Roof Wall	9.45 - 9.30	184	180	
		Roof Wall	7.30 - 7.00	162	160	120

Coefficient of Wind Pressure



Axial Force

ct1 263

		D2		D3		D6			
A	S	/	/	/	/	/	/	/	/
	G,B								
	C								
B	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
C	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
D	C	/	/	/	/	/	/	/	/
	W								
	Z								
E	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
F	G,B	/	/	/	/	/	/	/	/
	C								
	W								
G	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
H	S	/	/	/	/	/	/	/	/
	G,B								
	C								
I	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
J	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
K	C	/	/	/	/	/	/	/	/
	W								
	Z								
L	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
M	G,B	/	/	/	/	/	/	/	/
	C								
	W								
N	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
O	S	/	/	/	/	/	/	/	/
	G,B								
	C								
P	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
Q	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
R	C	/	/	/	/	/	/	/	/
	W								
	Z								
S	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
T	G,B	/	/	/	/	/	/	/	/
	C								
	W								
U	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
V	S	/	/	/	/	/	/	/	/
	G,B								
	C								
W	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
X	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
Y	C	/	/	/	/	/	/	/	/
	W								
	Z								
Z	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
AA	G,B	/	/	/	/	/	/	/	/
	C								
	W								
AB	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
AC	S	/	/	/	/	/	/	/	/
	G,B								
	C								
AD	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
AE	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
AF	C	/	/	/	/	/	/	/	/
	W								
	Z								
AG	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
AH	G,B	/	/	/	/	/	/	/	/
	C								
	W								
AI	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
AJ	S	/	/	/	/	/	/	/	/
	G,B								
	C								
AK	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
AL	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
AM	C	/	/	/	/	/	/	/	/
	W								
	Z								
AN	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
AO	G,B	/	/	/	/	/	/	/	/
	C								
	W								
AP	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
AQ	S	/	/	/	/	/	/	/	/
	G,B								
	C								
AR	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
AS	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
AT	C	/	/	/	/	/	/	/	/
	W								
	Z								
AU	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
AV	G,B	/	/	/	/	/	/	/	/
	C								
	W								
AW	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
AX	S	/	/	/	/	/	/	/	/
	G,B								
	C								
AY	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
AZ	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
BA	C	/	/	/	/	/	/	/	/
	W								
	Z								
BB	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
BC	G,B	/	/	/	/	/	/	/	/
	C								
	W								
BD	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
BE	S	/	/	/	/	/	/	/	/
	G,B								
	C								
BF	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
BG	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
BH	C	/	/	/	/	/	/	/	/
	W								
	Z								
BI	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
BJ	G,B	/	/	/	/	/	/	/	/
	C								
	W								
BK	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
BL	S	/	/	/	/	/	/	/	/
	G,B								
	C								
BM	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
BN	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
BO	C	/	/	/	/	/	/	/	/
	W								
	Z								
BP	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
BQ	G,B	/	/	/	/	/	/	/	/
	C								
	W								
BR	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
BS	S	/	/	/	/	/	/	/	/
	G,B								
	C								
BT	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
BU	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
BV	C	/	/	/	/	/	/	/	/
	W								
	Z								
BW	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
BX	G,B	/	/	/	/	/	/	/	/
	C								
	W								
BY	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
BZ	S	/	/	/	/	/	/	/	/
	G,B								
	C								
CA	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
CB	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
CC	C	/	/	/	/	/	/	/	/
	W								
	Z								
CD	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
CE	G,B	/	/	/	/	/	/	/	/
	C								
	W								
CF	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
CG	S	/	/	/	/	/	/	/	/
	G,B								
	C								
CH	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
CI	Z'	/	/	/	/	/	/	/	/
	S								
	G,B								
CJ	C	/	/	/	/	/	/	/	/
	W								
	Z								
CK	W.L.	/	/	/	/	/	/	/	/
	Z'								
	S								
CL	G,B	/	/	/	/	/	/	/	/
	C								
	W								
CM	Z	/	/	/	/	/	/	/	/
	W.L.								
	Z'								
CN	S	/	/	/	/	/	/	/	/
	G,B								
	C								
CO	W	/	/	/	/	/	/	/	/
	Z								
	W.L.								
CP	Z'	/	/						





		B1		B2		B3		B6	
WF	S			0.04 X 55.3	5.0	X 101.1	9.1	X] =B3 12.7
	GB			0.05 X 31.0	1.6	X 46.9	2.3	X	
	C			0.05 X 2.3	0.1	X 2.3	0.1	X	
	W			0.02 X 0	0	X 0	0	X	
					0.08 X 17.4	1.4	X 0	0	
				0.09 X 12.2	0.6	X 24.4	1.2	X	
	Σ			(0.22 X 81.007) 8.7	8.7	12.7	12.7	12.7	12.7
	W.L.			-0.25 X 55.3	-13.8	X 101.1	-25.3	X	=B3 -25.3
	Σ'			-5.1	-5.1	-12.6	-12.6	-12.6	-12.6
RF	S	0.09 X 77.6	7.0	X 101.9	9.2	X 62.0	5.6	X] =B3
	GB	0.25 X 18.7	4.7	X 24.0	6.0	X 24.0	6.0	X	
		0.05 X 19.9	1.0	X 45.2	2.3	X 45.2	2.3	X	
	Σ	(0.22 X 81.007) 12.7	12.7	26.2	17.5	26.6	13.9	26.6	13.9
	W.L.	-0.23 X 77.6	-17.8	X 101.9	-23.4	X 62.0	-14.3	X	=B3 -14.3
	Σ'	-5.1	-5.1	-11.0	-5.9	-13.0	-0.4	-13.0	-0.4
IF	S	0.09 X 0	0	X 0	0	X 0	0	X] =B2 8.2
	GB	0.48 X 0	0	X 0	0	X 0	0	X	
		0.1 X 22.9	3.4	X 37.8	5.7	X 37.8	5.7	X	
		0.05 X 10.0	0.5	X 10.0	2.5	X 10.0	2.5	X	
		0.02 X 0	0	X 0	0	X 0	0	X	
		0.03 X 0	0	X 0	0	X 0	0	X	
		0.05 X 0	0	X 0	0	X 0	0	X	
		0.05 X 0	0	X 0	0	X 0	0	X	
		0.05 X 0	0	X 0	0	X 0	0	X	
		0.05 X 0	0	X 0	0	X 0	0	X	
	Σ	(0.26 X 81.007) 18.6	5.9	34.4	8.2	34.8	8.2	64.4	37.8
	W.L.	-0.20 X 0	0	X 0	0	X 0	0	X	0
	Σ'	0.8	5.9	-2.8	8.2	-4.8	8.2	24.8	37.8
		A1		A2					
WF	S								
	GB								
	C								
	W								
RF	S	0.09 X 48.6	4.4	X 88.8	8.0				
	GB	0.25 X 12.7	3.2	X 18.0	4.5				
		0.05 X 11.6	0.6	X 23.3	1.2				
	Σ	8.2	8.2	13.7	13.7				
	W.L.	-0.23 X 48.6	-11.2	X 88.8	-20.4				
	Σ'	-3.0	-3.0	-6.7	-6.7				
IF	S	0.05 X 17.4	1.6	X 31.8	2.9				
	GB	0.5 X 0	0	X 0	0				
		0.05 X 15.3	0.8	X 10.6	1.6				
		0.05 X 17.6	0.4	X 13.6	0.7				
		0.02 X 17.4	0.4	X 9.7	2.4				
		0.05 X 11.4	0.6	X 0	0				
		0.05 X 11.4	0.6	X 0	0				
		0.05 X 11.4	0.6	X 0	0				
		0.05 X 11.4	0.6	X 0	0				
		0.05 X 11.4	0.6	X 0	0				
	Σ	29.8	21.6	26.4	12.7				
	W.L.	-0.33 X 17.4	-5.7	X 31.8	-10.5				
	Σ'	12.9	15.9	-4.9	1.8				

Load of Beam

[t m, t]

Load		C	M ₀	Q
10.6 →	$(0.09 \times 3.77) + 0.20$	$\int 0.539 \times 10.6^2/12$ 5.0	$\times /8$ 7.6	$\times 10.6/2$ 2.9
10.6 →	$(-0.8 \times 0.20 - 0.07) \times 3.77$	$\int 0.857 \times 10.6^2/12$ -8.1	$\times /8$ -12.2	$\times 10.6/2$ -4.6
10.6 →	$(0.009 \times 1.57) + 0.20$ (0.02×3.26) MF (0.43×5.7) (0.08×10.0) (0.08×4.7) CRANE (1.09×0.38)	$\int 0.4019 \times 10.6^2/12$ 3.8 P 3.2 $\times 10.6/8$ 43 P' 1.2 $\times 10.6/8$ 1.6	$\times /8$ 5.7 $\times /4$ 8.8 $\times /4$ 3.2	$\times 10.6/2$ 2.1 $\times /2$ 4.6 $\times /2$ 0.6
10.6 →	$(-0.8 \times 0.16 - 0.07) \times 1.97$	$\int -0.307 \times 10.6^2/12$ -2.9	$\times /8$ -4.3	$\times 10.6/2$ -1.6
10.6 →	MF CRANE (3.09×0.62)	P 3.2 $\times 10.6/8$ 43 P' 1.9 $\times 10.6/8$ 2.5	$\times /4$ 8.5 $\times /4$ 5.0	$\times /2$ 1.6 $\times /2$ 1.0
10.6 →	$(0.09 \times 2.51) + 0.15$	$\int 0.376 \times 10.6^2/12$ 3.5	$\times /8$ 4.3	$\times 10.6/2$ 2.0
10.6 →	$(-0.8 \times 0.16 - 0.07) \times 3.77$	$\int 0.477 \times 10.6^2/12$ -4.7	$\times /8$ -7.0	$\times 10.6/2$ -2.6
Horizontal Axis		$\int 0.54$	H-700x300 $I_y = 10,300 \cong 0.F.$ $I_x = 0.54 \times 10.6^2 \times 100/8 \times 2.4 = 316.0$ $J_x = 5 \times 0.0054 \times 1060^3 \times 300 / 384 \times 2,100 = 11,963.0$	

[tm, t]

Load		C	M0	Q
	$(0.09 \times 10.6) + 0.20$	$1.154 \times 14.75^2 / 2$ 20.9	$\times / 8$ 31.4	$\times 14.75 / 2$ 8.5
	$(-0.8 \times 0.20 - 0.017) \times 10.6$ $(1.4 \times 0.22 \times 10.6 \times 2.5 / 2) \times 2.9 / 7.5 = 1.34$	$-7.438 \times 14.75^2 / 2$ $(1.0 \times 3.68) \times \frac{0.75}{0.25} \pm 2.8$ ± 8.9	$\times / 8$ -16.3 $0.3 \times 14.75 / 2$ ±2.2	$\times 14.75 / 2$ -18.0 $1.3 \times \frac{0.75}{0.25}$ +1.0 -0.3
		↑ B 47.0 A 75.1	↓ 41.4 48.8	↑ B 19.0 A 18.8
			↑ 68.5 60.9	↓ 17.0 17.7
	$(0.09 \times 10.6) + 0.20$	$1.154 \times 12.0^2 / 2$ 13.8	$\times / 8$ 20.8	$\times 12.0 / 2$ 6.9
	$(-0.8 \times 0.20 - 0.017) \times 10.6$	$-2.438 \times 12.0^2 / 2$ $(0.9 \times 6.0) \times \frac{0.31}{0.69} \pm 1.7$ ± 3.4	$\times / 8$ -43.9 $0.4 \times 12.0 / 2$ ±2.4	$\times 12.0 / 2$ -14.6 $1.3 \times \frac{0.31}{0.69}$ ±0.4 10.9
		↑ C 29.6 B 25.9	↓ 31.0 32.7	↑ C 14.2 B 13.7
			↑ 41.5 40.3	↓ 17.0 16.5
	$(0.43 \times 16.4) \times 10.6$ $(0.04 \times 11.9) \times 10.6$ $(0.08 \times 8.0) \times 10.6$	$8.3 \times \frac{6.0}{7.5}$ 10.7	$\times 6.0 / 3$ 16.0	$\times 1.0$ 8.5
	CRANE	$(2.1 \times 4.0) \times \frac{0.33}{0.67}$ 2.8 8.6	1.0×6.0 6.0	$\times 0.33$ 0.617 1.0 2.1
		C 13.5 B 16.3		9.3 10.4
			22.0	
	$(0.09 \times 32.3) \times 10.6$	$3.43 \times \frac{9.15}{4.5}$ 7.0	$\times / 3$ 10.5	$\times 1.0$ 3.4
	$(-0.8 \times 0.20 - 0.017) \times 32.3$	$0.15 \times \frac{9.15}{12}$ 1.0	$\times / 8$ 1.5	$\times 9.15 / 2$ 0.7
		8.0	12.0	4.1
		$-7.43 \times \frac{9.15}{4.5}$ 15.1	$\times / 3$ 22.7	$\times 1.0$ 7.4
		15.1	22.7	7.4

Load of Column

[t.m., t.]

Diagram	Load		C		Mo		Q
	C 0.8x0.6 q 0.14 @ 3.97	q	$0.422 \times 3.42^2 / 12$ 0.517	0.4 0.3	x / 8	0.6 0.5	x 3.42/2 0.7 0.5
			0 0	0.4 0.3		0.6 0.5	0.7 0.5
	C 0.8x0.6 q 0.14 @ 3.117	q	$0.422 \times 6.98^2 / 8$ 0.317	2.6 1.9	x / 8	2.6 1.9	x 6.98/2 1.5 1.1
			0 0	2.6 1.9		2.6 1.9	1.5 1.1
	C 0.8x0.6 q 0.12 @ 1.63	q	$0.156 \times 6.90^2 / 8$ 0.117	0.9 0.7	x / 8	0.9 0.7	x 6.90/2 0.5 0.4
			0 0	0.9 0.7		0.9 0.7	0.5 0.4
	M (CRANE) 2.7	M	$\frac{2.7}{2} (3 \frac{7.48^2}{10.1^2} - 1)$	0.4 0	x		$\frac{3 \times 2.7}{2 \times 10.1} (1 - \frac{7.48^2}{10.1^2})$ 0.2
	$\frac{0.9}{0.6} \times 0.14 \times 10.6 \times 2.6$ P1 $\frac{0.9}{0.6} \times 3.6$ P2	P1 P2	$\frac{0.9}{4.7} \times 0.85$ $\frac{12.2}{8.9} \times 0.75$	0.2 0.2 0.2	x 5.55 x 5.55	0.9 3.9 12.2 8.4	x 0.7, 0.3 x 0.5 2.2, 0.9 1.6, 0.7 TOP BTM 2.4, 3.1 2.2, 2.3
	$\frac{0.9}{0.6} \times 0.14 \times 3.53$	q	$\frac{0.394}{0.296} \times 3.26^2 / 12$	0.4 0.3	x / 8	0.6 0.4	x 3.26/2 0.6 0.5
			0 0	0.4 0.3		0.6 0.4	0.6 0.5
	$\frac{0.9}{0.6} \times 0.12 \times 3.53$	q	$\frac{0.394}{0.254} \times 6.9^2 / 8$	2.0 1.5	x / 8	2.0 1.5	x 6.9/2 1.2 0.8
			0 0	2.0 1.5		2.0 1.5	1.2 0.8

SEISMIC FORCE

		W	K	KW	Q
S	$0.05 \times 10.6 \times 9.54$	5.1			
B	$0.05 \times (31.8 + 22.6)$	2.7			
F	$0.05 \times 2.48 \times 9$	1.1			
V	$0.05 \times 21.2 \times 2.48$	2.6			
Σ	$\bar{W} = 11.5 / (10.6 \times 9.54) = 0.11 [t/m]$	11.5	0.10	1.2	1.2
S	$0.05 \times 10.6 \times 22.01$	11.7			
B	$0.20 \times (42.4 + 26.85)$	13.9			
D	$0.05 \times (10.6 \times 6) + 31.8 \times 0.15 \times 10.6$	6.4			
C	$(0.15 \times 5.38 \times 1) + (0.25 \times 1.71 \times 2)$	2.2			
F	$0.05 \times (6.4 \times 3) + (1.7 \times 4)$	1.2			
V	$0.05 \times (0.6 \times 5.38) + (10.6 \times 1.71) + (0.08 \times 21.2 \times 1.71)$	6.7			
Σ	$\bar{W} = 42.1 / (10.6 \times 29.59) = 0.13$	42.1	//	4.3	5.9
S	$(0.05 \times 10.6 \times 10.69) + (0.29 \times 10.6 \times 4.13)$	18.3			
B	$0.20 \times (21.2 + 21.3) + (0.15 \times 10.6)$	7.6			
D	$0.05 \times (9.0 + 13.3)$	10.1			
C	$(0.15 \times 5.38 \times 2) + (0.15 \times 3.58 \times 1)$	3.3			
F	$0.05 \times (1.7 \times 4) + (3.2 \times 4)$	3.2			
V	$0.05 \times (0.6 \times 1.71) + (10.6 \times 3.20) + (0.08 \times 21.2 \times 1.71)$	1.5			
Σ	$\bar{W} = 49.5 / (10.6 \times 14.78) = 0.32$	49.5	//	5.0	12.2
S	$0.24 \times 10.6 \times 6.05$	18.6			
B	$0.05 \times (31.8 + 24.2)$	2.8			
V	$0.08 \times 28.8 \times 4.65$	10.7			
Σ	$\bar{W} = 32.1 / (10.6 \times 6.05) = 0.50$	32.1	//	3.3	

CRANE
2.0+0.2+(1.5x2)
1.0+0.1+1.1



WIND FORCE

	C	q_z N/m ²		A m ²	H _t	Q _t	W	M
S	0.8 ~ 0.6	0.22	10.6 x 2.48	26.3	4.6 ~ 3.5	4.6 ~ 3.5	3.5 + 4.6 8.1	4.6 + 3.5 8.1
B	"	0.14	10.6 x 1.71	18.1	2.0 ~ 1.5	6.6 ~ 5.0	5.0 + 9.5 14.5	6.6 + 8.0 14.6
D	"	0.12	10.6 x 5.00	53.0	5.1 ~ 3.8	11.0 ~ 8.8	14.5 + 3.8 18.3	14.6 + 5.1 19.7
S	0.9 ~ 0.6	0.22	10.6 x 2.48	22.3	4.6 ~ 3.5	4.6 ~ 3.5		
B	"	0.14	10.6 x 5.00	53.0	5.1 ~ 4.5	7.5 ~ 8.0		

SEISMIC FORCE

		W	K	KW	Q
E	$0.05 \times 95.9 \times 9.48$	44.5			
K	$0.05 \times (848 + 67.8)$	7.6			
P	$0.05 \times 2.48 \times 27$	3.3			
M	$(0.05 \times 10.05 \times 2.48) + (0.05 \times 169.6 \times 2.98)$	23.0			
Z	$\bar{w} = 79.4 / (95.9 \times 9.48) = 0.09 \text{ [t/m}^2\text{]}$	79.4	0.10	8.0	8.0
S	$0.05 \times (117.1 \times 13.43) - (95.4 \times 7.73)$	42.7			
G	$0.20 \times (116.6 + 161.1)$	57.5			
B	$0.05 \times (116.6 \times 3) + (13.43 \times 12)$	25.5			
C	$0.15 \times 171 \times 12$	9.1			
F	$0.05 \times 9.38 \times 6$	1.6			
H	$0.05 \times 26.9 \times 5.0$	6.7			
Z	$\bar{w} = 137.1 / (117.1 \times 13.43) = 0.09$	137.1	1	13.8	21.8
E	$(0.05 \times 95.9 \times 4.58) + (0.29 \times 21.2 \times 3.1)$	22.0			
S	$0.20 \times (116.6 + 12.1 + 106.3)$	47.0			
B	$0.05 \times (95.4 + 41.2 + 46.9)$	9.2			
C	$0.15 \times 9.38 \times 12$	16.1			
F	$0.05 \times 3.42 \times 7$	1.2			
M	$(0.05 \times 117.1 \times 16.3) + (0.08 \times 25.3 \times 3.42)$	16.5			
Z	$\bar{w} = 112.0 / (439.2 + 44.5) = 0.23$	112.0	1	11.2	33.0

Wind Force (E)

	c	$q \text{ t/m}^2$	A _w m ²	H _f	Q _f
E	0.8 + 0.6	0.22	7.98×2.48	19.8	6.1
B	0	0.14	13.43×5.0	67.2	19.3

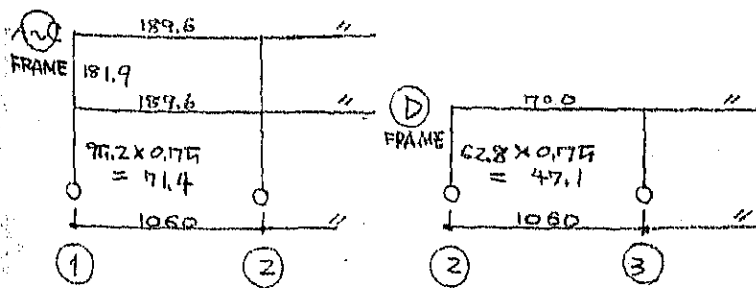
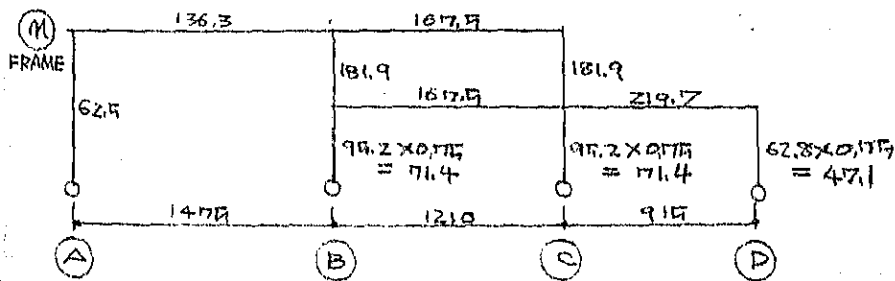
Stiffness Ratio

J	k						
	D/B	1475	1200	915	1060	623	326
201,000		136,3	167,5	219,7	189,6	—	94,9
71,000		—	—	—	70,0	—	—
63,100 54,600		—	—	—	—	95,2	181,9
40,700 35,300		—	—	—	—	60,8	62,8

$$\alpha = \frac{1}{J_{max}} = 0.20 + 0.80 \sqrt[3]{\left(\frac{J_{min}}{J_{max}}\right)^2} J_{max}$$

$$0.20 + 0.80 \sqrt[3]{\left(\frac{54,600}{63,100}\right)^2} = 0.94$$

$$0.20 + 0.80 \sqrt[3]{\left(\frac{35,300}{40,700}\right)^2} = 0.93$$

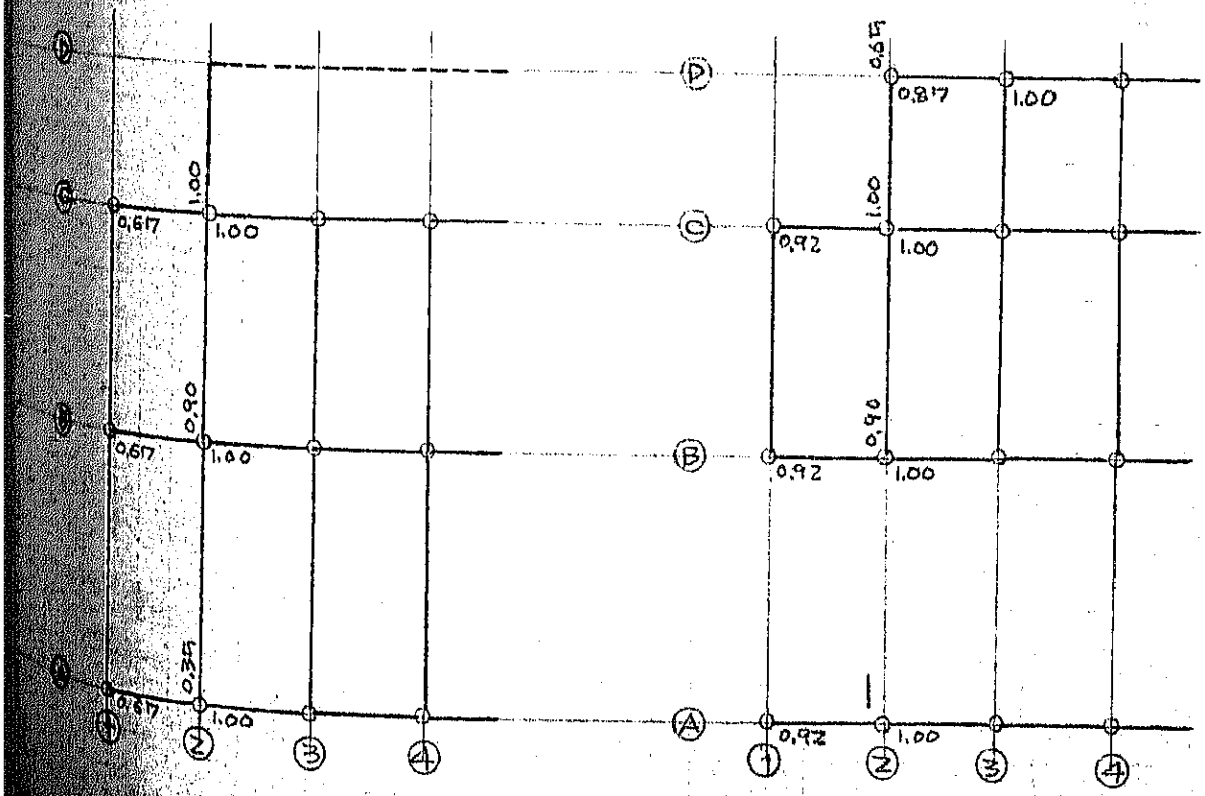


Distribution Factor & Inflection Point

No	D				D'	Y				D	K.L.			W.L.		
	K	E	α	D		Y ₀	Y ₁	Y _{2,3}	Z _Y		Q	MU	ML	Q	MU	ML
1	163	2.18	0.20	12.7	0.35	0		0	9.49				2.3	21.6	0	
				12.7												
2	113	1.30	0.39	17.5	0.90	0.40	-0.05	0.35	3.26				5.9	12.4	6.7	
				32.3												
3	147	1.52	0.43	18.7	1.00	0.45	0.05	0.50	3.26				6.9	10.6	10.6	
				35.8												
4	107	2.35	0.21	14.7	0.90	0		0	6.23				6.1	38.1	0	
5	172	5.42	0.23	16.3	1.00	0		0	"				6.8	42.4	0	
6	217	4.66	0.23	10.6	0.65	0		0	"				4.4	27.5	0	
7	172	1.04	0.34	62.3	0.67	0.40		0.40	3.26	1.3	1.4	2.9				
8	154	2.08	0.51	92.8	1.00	0.45		0.45	"	2.0	3.6	2.9				
9	196	2.66	0.21	15.0	0.92	0		0	6.23	2.6	16.0	0				
10	212	5.31	0.23	16.3	1.00	0		0	"	2.8	17.4	0				
11	100	1.49	0.19	8.8	0.87	0		0	6.23	1.2	7.6	0				
12	140	2.97	0.21	10.1	1.00	0		0	"	1.4	8.7	0				

$$\frac{1}{17.15} \left(\frac{326}{949} \right)^2 + \frac{1}{14.7} \left(\frac{623}{949} \right)^2 = \frac{1}{(1.65 \times 10^{-3}) + (2.93 \times 10^{-2})} = 32.3$$

$$\frac{1}{18.11} \left(\frac{326}{949} \right)^2 + \frac{1}{16.3} \left(\frac{623}{949} \right)^2 = \frac{1}{(1.50 \times 10^{-3}) + (2.64 \times 10^{-2})} = 35.8$$



UNIT: Stress

FL	K.L.			W.L.			
	Q	ΣD	$Q/\Sigma D$	Q	ΣD	$Q/\Sigma D$	
R	5.5	$0.35 + 0.90 + 1.00$	2.25	2.5	14.6	2.29	6.5
L	$\frac{(5.5 \times \frac{1.90}{2.29})}{5.0 + 1.7}$	$0.90 + 1.00 + 0.65$	2.55	4.5	$\frac{(14.6 \times \frac{1.90}{2.29})}{5.1}$	2.55	6.8
R	21.8	$(0.67 \times 2) + 10.0$	11.34	2.0	6.1	11.34	0.6
L	33.0	$(0.92 \times 2) + 10.0$	11.84	2.8	19.3	11.84	1.7
L	13.6	$(0.87 \times 2) + 8.00$	9.74	1.4	2.9	9.74	0.3

Deflection by Horizontal Force

FL	LOAD	Q	ΣP_{D_0}	$\frac{h_0^2}{12EK_0}$	δ	δ/h_0
R	K.L.	5.5	2.25 x 32.3	$\frac{623^2}{12 \times 2,100}$	1.17	$\frac{1}{532}$
	W.L.	14.6	"	"	3.09	$\frac{1}{201}$
I	K.L.	11.4	2.55 x 16.3	$\frac{326^2}{12 \times 2,100}$	1.16	$\frac{1}{282}$
	W.L.	17.4	"	"	1.77	$\frac{1}{185}$
R	K.L.	21.8	11.34 x 92.8	$\frac{623^2}{12 \times 2,100}$	3.19	$\frac{1}{95}$
	W.L.	6.1	"	"	0.09	$\frac{1}{698}$
I	K.L.	33.0	11.84 x 16.3	$\frac{326^2}{12 \times 2,100}$	0.772	$\frac{1}{452}$
	W.L.	19.3	"	"	0.43	$\frac{1}{772}$
I	K.L.	13.6	9.74 x 10.1	$\frac{326^2}{12 \times 2,100}$	0.558	$\frac{1}{454}$
	W.L.	2.9	"	"	0.12	$\frac{1}{2598}$