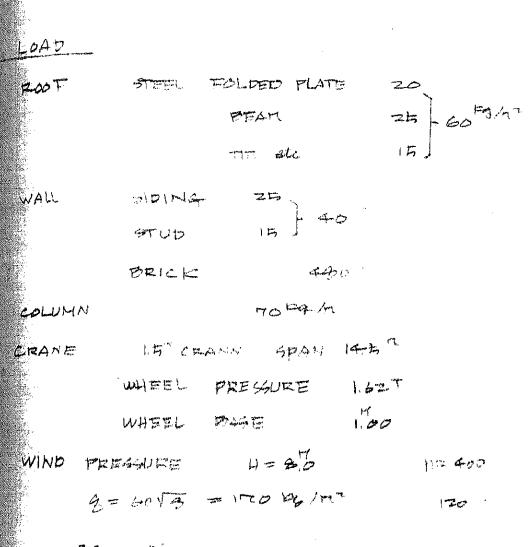
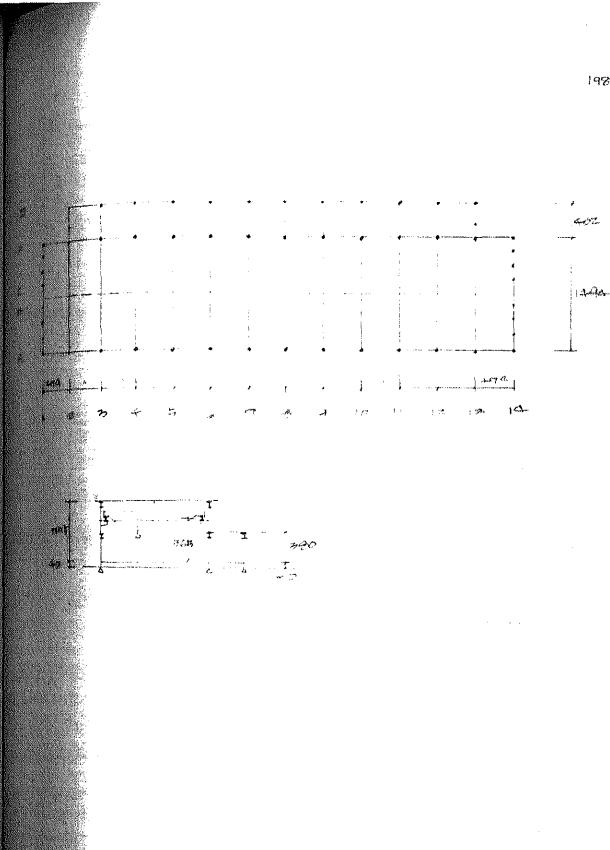


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TRAINING ROOM

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and the second second

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- CRAME GIRDER 1-1-0 p= 1.6= 1 - 100 mare M = 1.5= - (and - 100/2) / = + + 19 = 3.11 man Q = 1.6= (1 - 4-59-100) = = 290 GIRDER W = 50 + 22 - 9 - 80 12 14 Record . 4"A" 4 - 023 Q= i shad to = > 19 IMFACT LOAD XX = 0.15 P XY = 01P ZTX = 311 × 115 + 023 = 281 EQ. = 230. - 010 = 3,53 TY = #11 x 010 = 071 1-346 xind + 6x 2 Sb = ADD Lat 2 ~ Fird Ara and T tak 8- 8-6 - 3-31 / 6.5. - U HA - 2.04 5= 3500 - 40A" - 2000 × 11 100 00 0 34 = 41000 YAB = 31 /91 = 024 =1.60 The the loss and a alto a a go

WHE HEMBER

WIST #1 L= ATTA Was 40 Weller Who = sto state y = - at " & - and, " w= 45 (14 44 = 300 52/2 10=070 - 4.MA - 286 - M 46= 900 /409 - == /1040 # = 0.05 Fb = 36 / 1264 + 0417 = 0.00 J= 523 - CNA + ACT = 21 x10 - 11000 = 053 = 479/400 E Grand W = +0 < + + + + 0 × 765 = 2 30 2/4 to = 073 + +-4" 1 = 016 A = +++ A / = 055 H-298 x 149 x 5.5 x 2 10 = 900 sand wat 1 (10 1 - 1 = 0 125 Th= 64 /424 = 0.16 = 0.73 Pr l= +14 was しょ = チャンマッキ = 150 トラノー Wy + 100 - 0.4 × 0.175 /2 = = 520 Rx - 012 4 4 992/2 - 003 $M_{1} = o 5 i = 1.44$ THE THE YOR YAR 5bx = 100 200 × 30 / 15 20 = 0.344 Obx = 23/441 = 0.039

$$V_{M} = \frac{1 + 4}{2 + 6} \frac{1}{2 + 6} = \frac{1 + 7}{2 + 6} \frac{1}{2 + 6} = \frac{1 + 7}{2 + 6} \frac{1}{2 + 6} = \frac{1 + 7}{2 + 6} \frac{1}{2 + 6} = \frac{1 + 7}{2 + 6} = \frac{1 + 7}$$

- Wb

$$\frac{1}{12}$$

$$\frac{1}{12}\frac$$

4<u>6 II</u> George

6+ 4 **7** 4

allet Maria

204-1 = 100 W+40×(402/2+30)=200 -Ww = 120×20×40 = 1900 C= 070 × 3.0" /2 = 0.5% t3.40 6=070 × 7.0 = 0 bo 7.60

MUMN m = 753 × 40 = 141 T-411 Here 1+1+1+ 3× 2.6× 5.75+ (2.6-2×4.71)×10453/2×145 = -0.2ts +0.15 8= 3,53 × 40 / 196 = 0.13 1 = 0.45 100 = 120 - 0. A + 4 17 A = 650 100 /12 h= Mp= a.br x 7.9+ - 13.14 0- 0.K- x D.11:12 - 2.10.6 PW= 120 ×08 × 4,05/2 × 4,09 = 930 has 405 RAG 10 = 650 10/m W= DW XAAD == 53 H= x53 13 90 (21095 - 390) / 10× 17962 ローニマンラメ 60/010 + 013× 405/2010 = 1.91+047 = 230 an = 253+0.9% = = 3.09 = 1.09 「しんか」に見いなのし、 チカク l = 404 W= 120428 ×179 = 460 to 100 H= 120= 0.40 + 4 00 1/4 = 094 Q=046 x 40514 = 093 l=195 $w_1=355$ by h_2 $w_2=460$ by h_1 4 2.81 × 019 6 bb + 244 × 7.95 / 8 = 032+363 = 445 QT= 1.91 x 2.19/164 + 0.46 × 1945/2 = 046 +1.453 = 2.39 00=0.6=×014/00 + ... = 0.18 +1.83 = 2.01

AXIAL TOPES OF COLUMN

200=		WAUL	CRANE Sikder		P
** 7.F.× 台、二、	1.173	0.3.4.7.0.9.9. x 2.3.5 2.04 0.04 x 2.4 y 3.45 034		0156	9.46
*4-8 × 4-5-	2.45	000 × 4.90 × 3.14 1.14	0.7197	0.156	4.01
antit x aits	いいろ	= = = = = = = + + + + + + + + + + +	0.19	0.55	2.61
444×35	0.64 2.49	042234 × 7.200 400	o AA	0.56	A13
和分人 フ.0 白米赤白 ×ゆち	0 H) 2 A 5		0:7100	0.46	7.96
★年本日、□	1.62			0.70	1.072
6 * AB × 4.0	145			0.70	1 64

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HORIZONTAL LOAD

ARTHQUALE LOAD

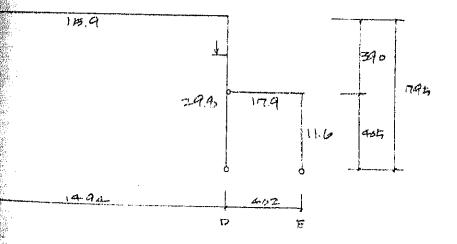
200 F 0.06 × 64 7 × 16 95	64,25
0.00 × 56.69 × 7.02	23.95)
WALL 0.4 AX (39.45 × 355 - 20× 1.45)	no. An
0.04 × (115,7 × 7) 50 + 52, 5 × 1.45)	30,44
CIEGNE GIRDER OOK / IZTE	9.96
COLUMN 007 + TA + 40	-7. 204-
0.0 bi x 1-2 x 2.0	1. 200
	, , , , , , , , , ,
	109.60-
$\Theta_{\rm E} = 199.64 \times 21 = 1996$	
WIND PRESSURE	
P.17 x 1, 7 x 15, 34 x 20/2 12, 572	
0.12×1.2: 2012 40/2 1.13	
xQy = 17.65	
0.11×1.2 × 62 +11 + 20 /2 50.47	
012 × 04 × 22 + 5 × + 4 6 20	
1-Gw = 36.47	
0.17×1.2×6= 1- 40/2 50.97	
P1/2 × 1/2 × 57 + + + + + + + + + + + + + + = + = 00	
4700 - 6=.97	

ATTENESS RATIO

CLUMN CA CO H-4-00×200× 3×13 = x - 23 002 $T_{1} = 1740$ CH H-20×200 $\times 25 \times 12$ $T_{X} = 47720$ $T_{1} = 1600$ H-4-00 $\times 200 \times 25 \times 13$ $T_{X} = = 3700$ Grz H-300 $\times 150 \times 6.5 \times 9$

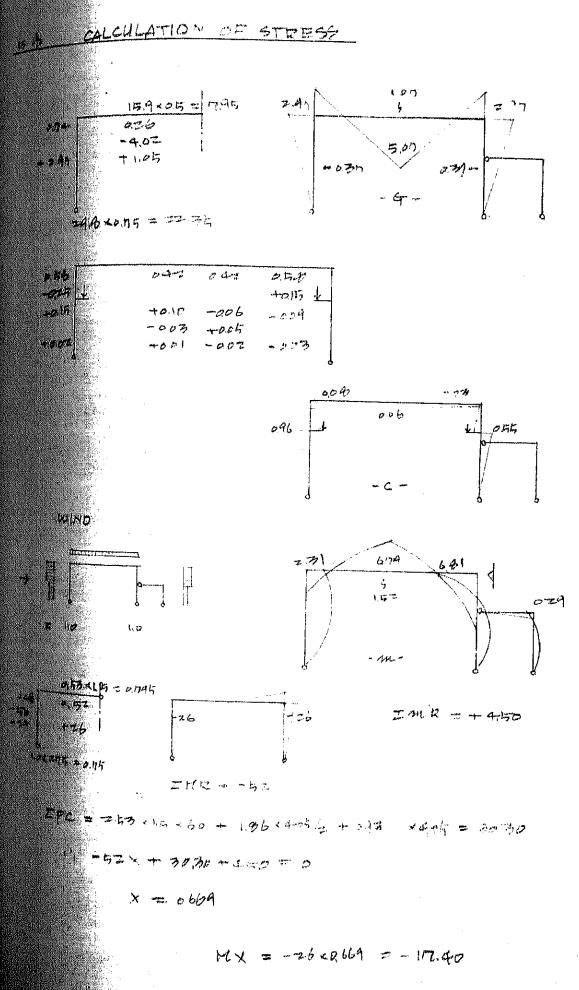
Ix = 17210

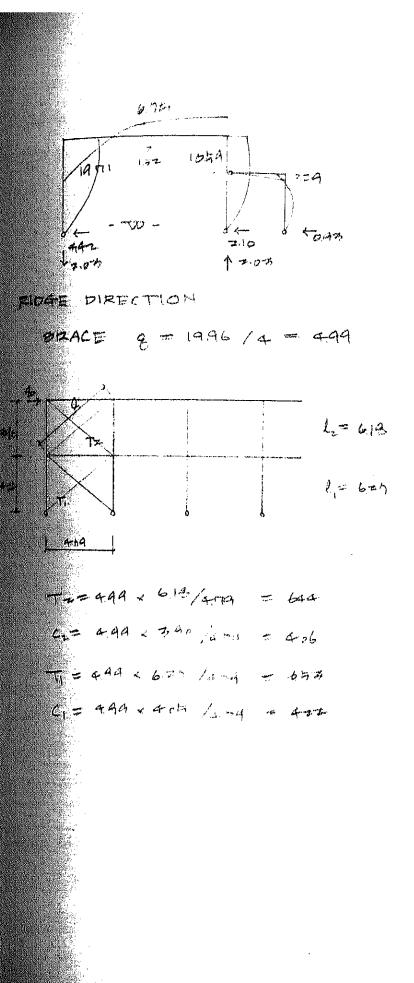
C. A.



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DESIGN OF SECTION

PEATL GAD THE PL PEE Q 1 -297 + 527 + 295 1.07 E +0,00 +2.26 - 0000 0 · [4,19] · 6075 · 12,15.4 1.5-5 +16,73 - 1 th + 17,56 = 2 4A H-40 100 × 8-13 lb= 1444 /1 = = = = = fr= APO / a gas a 40 / 20 - 1.3 4 1.156 10- 1673 /1190 - 121 < 156 × 1,5 = = 34 COLUNIN CA P M Q 4.07 + 19 0 3.0 C 743 grade or 7 2.63 19 (1) +4-2 A,63 1603 405 H- 400 x 300 - 1 / 12 diese that day = foto 7= 405/484 = 29-2 Se= 100

4b = 900 / 400 + 40 / 20 - 1.3 = 1.44Se = 9.63 / 24.12 = 0.114

 $f_{b} = \frac{16772}{1100} - \frac{141}{144} = \frac{141}{144} = \frac{114}{144} - \frac{109}{14} = \frac{1090}{16} = \frac{1090}{100} = 15$

21)

$$712$$

$$712 = 71.600 / 516 (716) = 6.63 + 37.607 = 555
m = 6.16 + 18 57 / 4 = 152.41
 $T = 16 + 5 + 12 - 19$
 $AB = -4 - 1919$
 $P = 16 + 5 + 12 - 19$
 $AB = -4 - 1919$
 $P = 16 + 5 + 12 + 12 + 12 + 13 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 200 + 100 +$$$

213 HE BEATL 35.90 1= 72.6 1=4799 w= 016 + 0.49 - 21 = 2.44 2.16 wo 44 + 12 + 12 - 12 - 143 6= 244×4.179 = 4:11 2.5 Man , 14 = 7.0 4-1 0= 1 × 47-1 = 5.0 フット 1000100 <u>0</u>. 「アートマレ = アー The = The abe = = = are 37 /07/6,20 = 22 2-019 Ac = = = 1 = 1 = 1 = 1 7 - 12.2 t no 043 OAN ON OF 7-0 øЬ 4.15 -70 +20 -20 -20 +19 + # 0 +1.2 +1.2 +1.2 +1.2 +0.4 A# = 50 / 0006 - 20 - 24 コーアンス AL = 4-5 -2-1-21-4 W=0.56 + 0.4.4 3 = 270 P= 441 2 × 585 1 = 320 C= 230 × 6 00 / 10 - 600 × 5,00 × 2/4 = 12.2 0.6 1 / + + × /a = 18.2 1.0 · Tanzo x Kubn /2 + 4an = 109 1.2-P4-1 1.d 93 0.45 67514 + 182 -06 131 -17.9 -91 a de la com

4-10	900 1	1 1999 by	1 1 1	10.6	,	
a.c =	17.1	1 0.726	1 12.0	1	4.0	A-DIA
UB =	10.7	1				あ- ロータ
a.c =	9,3	/	<i>P</i>	та ^{н.}	64	3-019

5 SOUTH CT

WALL	TIE REAN	CRAN	IP	n	L×L'
194 × 2.94 423 0/69 × 2.9 1.92	Fr 0	313	19-6	1	10 4.90
\$ 5 A × 4 3 7.473	みんら	西东西	14-1	2	90 × 210
1.44 x ZAA 4-23	常外的		12.2		ADXAD
144 × 2.4 4:23	A10	あっち	24:1	naraja Karan	90×210
164×24- 403	5,17	ついつ	20.9	-2-	17
MA . 3 4 10-	5,10	あたろ	105	7.	1)
1444 ×2 = 2.84	-20 -2001		9.5	١	A0 x 4 2
*#A×4.8 2.833	あい口		9.6	1	11
	1.44 × 2.94 4 23 0.49 × 2.94 4 23 0.49 × 2.94 4 23 1.44 × 2.94 4 23 1.45 × 2.94 4 20 1.55 × 2.94 1.55 2 3 1.55 × 2.95 1.55 2 3 1.55 × 2.95 1.55 2 3 1.55 × 2.55 2 3 1.55 × 2.5	WALL EFEAM. MALL EFEAM. MAL	WALL EMEAN CH2AN MAR × 2.94 4 2.3 4710 313 494×2.94 1.42 4710 3.13 494×2.94 1.42 4710 3.65 144×2.94 4723 3.45 144×2.94 4723 3.10 144×2.94 4723 5.177 144×2.94 4723 5.177 144×2.94 4723 5.177 5.177 $3.5.73$ 5.177 $3.5.73$ 5.177 $3.5.73$ 5.177 $3.5.73$ 5.177 $3.5.73$ 5.177 $3.5.73$	WALL ETEAN. CH2AN/ IP MA x 2 A4 4 2.3 42.3 510 3.13 1476 AGA x 2 A1 1.472 510 3.13 1476 AGA x 4 B 2.473 3.645 2.53 14.1 AGA x 4 B 2.473 3.645 2.53 14.1 AGA x 4 B 2.473 3.645 2.53 14.1 AGA x 2 A4 4.23 3.445 12.2 AGA x 2 A4 4.23 3.445 12.2 AGA x 2 A4 4.23 3.445 12.2 AGA x 2 A4 4.23 5.177 3.13 2.64 AGA x 2 A 14.2 5.177 3.573 $2.0.4$ AGA x 2 A 14.2 5.177 3.573 $2.0.4$ AGA x 2 A 14.2 7.573 10.5	WALL ETEAN $ETEAN$ $ETEAN$ ETP n MA × 2.A4 4.2.3 5710 3.13 1476 1 ASA×473 7710 3.13 1476 1 ASA×473 7473 3665 2.53 1471 2 ASA×473 7473 3665 2.53 1471 2 ASA×473 7473 3665 2.53 1471 2 ASA×473 7473 3655 1471 2 ASA×473 7473 3655 1471 2 ASA×2.44 4723 3475 12.2 1 ASA×2.44 4723 3475 2647 2 ASA×2.4 4737 5177 3.573 20.47 2 ASA×2.4 1472 3.573 10.57 2

47 364 = ----

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10 = 0.9×0.9×0.6×2.0 = 1.2

25-1=====

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$$\begin{aligned}
\begin{aligned}
A &= A - D & (6) \\
A &= A + A & (6) \\
A &= A & (6) \\
A &=$$