

付属資料

Modified Point of Transmission Lines and Transformers Data

PSSE Original DATA from CEB Red letters: Data should be changed to the standard value

Transmission Lines Data (100MVA base)

From	To	Target Data to be checked				Standard Value				
		X (pu/km)	B (pu/km)	capacity RateA	capacity RateB	Rate A (MVA)	Rate B	Rate C	X (pu)	B (pu)
1300 KELAN-1	1900 COL_C-1	0.00044	0.01401	180	180	160	160	0.000354	0.001654	0.016305
1430 COL-1	1435 COL_A-1	0.00112	0.06125	230	230	230	225	0.000621	0.004404	0.051482
1430 COL-1	1550 KOLON-1	0.00071	0.05288	255	255	255	255	0.000501	0.004245	0.054407
1435 COL_A-1	1990 DEHW-1	0.00151	0.09073	230	230	230	225	0.000951	0.006741	0.078900
1550 KOLON-1	1750 COL_E-1	0.00158	0.12119	120	120	120	120	0.001209	0.002285	0.094261
1550 KOLON-1	1920 COL_K132	0.00138	0.04378	180	180	180	160	0.001105	0.005168	0.050954
1550 KOLON-1	1940 COL_B_13	0.00116	0.03678	180	180	180	160	0.000928	0.004341	0.042601
1560 PANNI-1	1890 DEHW-1	0.00134	0.10346	255	255	255	255	0.000888	0.007518	0.096346
1690 HABAR-1	1705 NEWANU-1	0.02133	0.02543	165	165	140	225	0.021329	0.108611	0.025429
1840 JPURA	1920 COL_K132	0.00138	0.04378	180	180	180	160	0.001105	0.005168	0.050954
1900 COL_C-1	1940 COL_B_13	0.00065	0.01752	180	180	180	160	0.000442	0.002067	0.020382

Transformers Data (100MVA base)

From	To	Standard Value			Target Data to be checked			
		X	RateA	RateB	RateC	X	RateA	RateB
1220 KOTIMH-1	2220 KOTIMH-2	0.056	250	250	250	0.04	250	250

GENROU (Round Rotor Generator Model) Type

Type	Bus ID	Bus	Type	unit	T _{do}	T _{db}	T _{op}	T _{op}	Inertia	Seed Demand D	X _d	X _q	X _d	X _q	X _q '-X _d '-q	X _i	S(1,0)	S(1,2)	Remarks	
GT	1300	KELAN-1	'GENROU'	1	5.568	0.03	1.08	0.16	7.23	0.5	2.38	1.72	0.231	1.2	0.17	0.1	0.03	0.4	Decomposition to 16MWX 3	
GT	1300	KELAN-1	'GENROU'	1A	5.568	0.03	1.08	0.16	7.23	0.5	2.38	1.72	0.231	1.2	0.17	0.1	0.03	0.4		
GT	1300	KELAN-1	'GENROU'	1B	5.568	0.03	1.08	0.16	7.23	0.5	2.38	1.72	0.231	1.2	0.17	0.1	0.03	0.4		
GT	1300	KELAN-1	'GENROU'	1C	5.568	0.03	1.08	0.16	7.23	0.5	2.38	1.72	0.231	1.2	0.17	0.1	0.03	0.4		
ST(retired)	1300	KELAN-1	'GENROU'	2	6.97	0.036	1.08	0.19	4	0.5	1.79	1.72	0.23	1.2	0.12	0.1	0.03	0.4		steam turbine's data
GT	1300	KELAN-1	'GENROU'	3	6.64	0.049	1.18	0.066	8	0.5	1.81	1.77	0.259	0.344	0.179	0.1	0.125	0.589		No Existing
CC(GT)	2300	KELAN-2	'GENROU'	1	6.85	0.032	1	0.16	4	0.5	1.75	1.68	0.2262	0.437	0.163	0.0875	0.1	0.4		
CC(GT)	2300	KELAN-2	'GENROU'	2	6.85	0.032	1	0.16	4	0.5	1.75	1.68	0.2262	0.437	0.153	0.0875	0.1	0.4		
CC(GT)	2300	KELAN-2	'GENROU'	3	7.55	0.032	1	0.16	8	0.5	2.16	1.68	0.283	0.437	0.163	0.0875	0.1	0.4		
CC(GT)	2300	KELAN-2	'GENROU'	4	5.53	0.032	1	0.16	4	0.5	1.68	1.68	0.219	0.437	0.204	0.0875	0.1	0.4		
CC(2007)	2305	KERAWAL2	'GENROU'	1	6.85	0.032	1	0.16	4	0.5	1.75	1.68	0.2262	0.437	0.163	0.0875	0.1	0.4		
CC(2007)	2305	KERAWAL2	'GENROU'	2	6.85	0.032	1	0.16	4	0.5	1.75	1.68	0.2262	0.437	0.153	0.0875	0.1	0.4		
CC(2007)	2305	KERAWAL2	'GENROU'	3	6.85	0.032	1	0.16	4	0.5	1.75	1.68	0.2262	0.437	0.163	0.0875	0.1	0.4		
CC(2007)	2305	KERAWAL2	'GENROU'	4	6.85	0.032	1	0.16	4	0.5	1.75	1.68	0.2262	0.437	0.153	0.0875	0.1	0.4		
GT(2013)	2305	KERAWAL2	'GENROU'	5	6.85	0.032	1	0.16	4.5	0.5	1.75	1.72	0.27	1.31	0.163	0.1	0.03	0.4		
Coal(2008)	2815	PUTTA-2	'GENROU'	1	6.85	0.032	1	0.16	4	0.5	1.75	1.68	0.2262	0.437	0.16	0.0875	0.1	0.4		
Coal(2008)	2815	PUTTA-2	'GENROU'	2	6.85	0.032	1	0.16	4	0.5	1.75	1.68	0.2262	0.437	0.16	0.0875	0.1	0.4		
Coal(2008)	3301	KELAN-3A	'GENROU'	1	6.97	0.029	1.08	0.15	4.5	0.5	1.79	1.72	0.23	1.2	0.147	0.1	0.03	0.4	No existing	
Coal(2008)	3302	KELAN-3B	'GENROU'	1	6.97	0.029	1.08	0.15	4.5	0.5	1.79	1.72	0.23	1.2	0.149	0.1	0.03	0.4	No existing	
Typical Value presented by PTI																				
					6	0.05	1	0.05	3	0	1.4	1.35	0.3	0.6	0.2	0.1	0.03	0.4		

GENSAL (Salient Pole Generator Model) Type

Type	Bus ID	Bus	Type	unit	T _{do}	T _{dp}	T _{gp}	Inertia	Speed Damping D	X _d	X _q	X _{d'}	X _{q'}	X _{d''}	X _{q''}	X _l	S(1,0)	S(1,2)	Remarks
Hydro	1100 LAX-1	132.00	'GENSAL'	1	5.2	0.068	0.12	3	0.5	1.15	0.66	0.255	0.66	0.16	0.66	0.1	0.03	0.25	Decomposition to 1.2 MW×2
Hydro	1100 LAX-1	132.00	'GENSAL'	1A	5.2	0.068	0.12	3	0.5	1.15	0.66	0.255	0.66	0.16	0.66	0.1	0.03	0.25	
Hydro	1100 LAX-1	132.00	'GENSAL'	1B	5.2	0.068	0.12	3	0.5	1.15	0.66	0.255	0.66	0.16	0.66	0.1	0.03	0.25	
Hydro	1100 LAX-1	132.00	'GENSAL'	2	5.2	0.068	0.12	3	0.5	1.75	0.66	0.46	0.66	0.219	0.66	0.1	0.03	0.25	Decomposition to 8.33MW×3
Hydro	1110 LAX-1	132.00	'GENSAL'	2A	5.2	0.068	0.12	3	0.5	1.75	0.66	0.46	0.66	0.219	0.66	0.1	0.03	0.25	
Hydro	1110 LAX-1	132.00	'GENSAL'	2B	5.2	0.068	0.12	3	0.5	1.75	0.66	0.46	0.66	0.219	0.66	0.1	0.03	0.25	
Hydro	1110 LAX-1	132.00	'GENSAL'	2C	5.2	0.068	0.12	3	0.5	1.75	0.66	0.46	0.66	0.219	0.66	0.1	0.03	0.25	
Hydro	1110 N-LAX-1	132.00	'GENSAL'	1	8.6	0.066	0.12	3.32	0.5	0.9	0.55	0.23	0.55	0.15	0.55	0.1	0.03	0.25	
Hydro	1110 N-LAX-1	132.00	'GENSAL'	2	8.6	0.066	0.12	3.32	0.5	0.9	0.55	0.23	0.55	0.15	0.55	0.1	0.03	0.25	
Hydro	1120 MMAL-1	132.00	'GENSAL'	1	5.2	0.074	0.13	3	0.5	1.28	0.66	0.27	0.66	0.147	0.66	0.1	0.03	0.25	
Hydro	1120 MMAL-1	132.00	'GENSAL'	2	5.2	0.074	0.13	3	0.5	1.28	0.66	0.27	0.66	0.147	0.66	0.1	0.03	0.25	
Hydro	1130 POLPH-1	132.00	'GENSAL'	1	5.2	0.084	0.15	2.83	0.5	1.12	0.66	0.23	0.66	0.156	0.66	0.1	0.049	0.156	
Hydro	1130 POLPH-1	132.00	'GENSAL'	2	5.2	0.084	0.15	2.83	0.5	1.12	0.66	0.23	0.66	0.156	0.66	0.1	0.049	0.156	
Hydro	1140 CANYO-1	132.00	'GENSAL'	1	5.2	0.06	0.11	3.8	0.5	1.1	0.66	0.32	0.66	0.18	0.66	0.1	0.03	0.25	
Hydro	1140 CANYO-1	132.00	'GENSAL'	2	5.2	0.06	0.11	3.8	0.5	1.1	0.66	0.32	0.66	0.18	0.66	0.1	0.03	0.25	
Hydro	1170 SAMAN-1	132.00	'GENSAL'	1	7.58	0.07	0.15	3.18	0.5	1.03	0.57	0.288	0.57	0.19	0.57	0.1	0.057	0.256	
Hydro	1170 SAMAN-1	132.00	'GENSAL'	2	7.58	0.07	0.15	3.18	0.5	1.03	0.57	0.288	0.57	0.19	0.57	0.1	0.057	0.256	
Hydro	1200 UKUWE-1	132.00	'GENSAL'	1	8	0.055	0.08	3.2	0.5	1.1	0.58	0.28	0.58	0.22	0.58	0.08	0.179	0.5	
Hydro	1200 UKUWE-1	132.00	'GENSAL'	2	8	0.055	0.08	3.2	0.5	1.1	0.58	0.28	0.58	0.22	0.58	0.08	0.179	0.5	
Hydro	1210 BOWAT-1	132.00	'GENSAL'	1	5.2	0.073	0.13	4	0.5	0.87	0.66	0.157	0.66	0.148	0.66	0.1	0.259	0.625	
Hydro	1410 KUKULE-1	132.00	'GENSAL'	1	5	0.05	0.11	2.84	0	1.12	0.84	0.23	0.84	0.2	0.84	0.112	0.19	0.7	
Hydro	1410 KUKULE-1	132.00	'GENSAL'	2	5	0.05	0.11	2.84	0	1.12	0.84	0.23	0.84	0.2	0.84	0.112	0.19	0.7	
Hydro	2220 KOTMA-2	220.00	'GENSAL'	1	8	0.049	0.11	3.02	0.5	1	0.6	0.25	0.6	0.19	0.6	0.1	0.083	0.339	
Hydro	2220 KOTMA-2	220.00	'GENSAL'	2	8	0.049	0.11	3.02	0.5	1	0.6	0.25	0.6	0.19	0.6	0.1	0.083	0.339	
Hydro	2220 KOTMA-2	220.00	'GENSAL'	3	8	0.049	0.11	3.02	0.5	1	0.6	0.25	0.6	0.19	0.6	0.1	0.083	0.339	
Hydro	2225 UPKT-2	220.00	'GENSAL'	1	6.7	0.048	0.1	4.3	0.5	1.03	0.63	0.29	0.63	0.21	0.63	0.1	0.03	0.25	Decomposition to 7.0MW×3
Hydro	2225 UPKT-2	220.00	'GENSAL'	2	6.7	0.048	0.1	4.3	0.5	1.03	0.63	0.29	0.63	0.21	0.63	0.1	0.03	0.25	
Hydro	2230 VICTO-2	220.00	'GENSAL'	1	7.57	0.061	0.08	3.44	0.5	0.952	0.6	0.239	0.6	0.186	0.6	0.127	0.075	0.219	
Hydro	2230 VICTO-2	220.00	'GENSAL'	1A	7.57	0.061	0.08	3.44	0.5	0.952	0.6	0.239	0.6	0.186	0.6	0.127	0.075	0.219	
Hydro	2230 VICTO-2	220.00	'GENSAL'	1B	7.57	0.061	0.08	3.44	0.5	0.952	0.6	0.239	0.6	0.186	0.6	0.127	0.075	0.219	
Hydro	2230 VICTO-2	220.00	'GENSAL'	1C	7.57	0.061	0.08	3.44	0.5	0.952	0.6	0.239	0.6	0.186	0.6	0.127	0.075	0.219	
Hydro	2240 RANDE-2	220.00	'GENSAL'	1	6.2	0.04	0.09	3.65	0.5	1	0.63	0.32	0.63	0.21	0.63	0.153	0.064	0.211	Decomposition to 5.8MW×4
Hydro	2240 RANDE-2	220.00	'GENSAL'	2	6.2	0.04	0.09	3.65	0.5	1	0.63	0.32	0.63	0.21	0.63	0.153	0.064	0.211	
Hydro	3590 SAPUG-3A	33 000	'GENSAL'	1	3.6	0.021	0.09	0.53	0.5	2.2	1.06	0.358	1.06	0.241	1.06	0.173	0.075	0.26	
Hydro	3590 SAPUG-3A	33 000	'GENSAL'	1A	3.6	0.021	0.09	0.53	0.5	2.2	1.06	0.358	1.06	0.241	1.06	0.173	0.075	0.26	
Hydro	3590 SAPUG-3A	33 000	'GENSAL'	1B	3.6	0.021	0.09	0.53	0.5	2.2	1.06	0.358	1.06	0.241	1.06	0.173	0.075	0.26	
Hydro	3590 SAPUG-3A	33 000	'GENSAL'	1C	3.6	0.021	0.09	0.53	0.5	2.2	1.06	0.358	1.06	0.241	1.06	0.173	0.075	0.26	
Hydro	3590 SAPUG-3A	33 000	'GENSAL'	1D	3.6	0.021	0.09	0.53	0.5	2.2	1.06	0.358	1.06	0.241	1.06	0.173	0.075	0.26	
Hydro	3670 MATARA-3	33 000	'GENSAL'	1	3.8	0.027	0.09	0.83	0.5	2.34	1.13	0.381	1.13	0.258	1.13	0.093	0.242	0.242	Decomposition to 3MW×4
Hydro	3670 MATARA-3	33 000	'GENSAL'	1A	3.8	0.027	0.09	0.83	0.5	2.34	1.13	0.381	1.13	0.258	1.13	0.093	0.242	0.242	
Hydro	3670 MATARA-3	33 000	'GENSAL'	1B	3.8	0.027	0.09	0.83	0.5	2.34	1.13	0.381	1.13	0.258	1.13	0.093	0.242	0.242	
Hydro	3670 MATARA-3	33 000	'GENSAL'	1C	3.8	0.027	0.09	0.83	0.5	2.34	1.13	0.381	1.13	0.258	1.13	0.093	0.242	0.242	
Hydro	3670 MATARA-3	33 000	'GENSAL'	1D	3.8	0.027	0.09	0.83	0.5	2.34	1.13	0.381	1.13	0.258	1.13	0.093	0.242	0.242	
Hydro	4420 HORANA-G	11 000	'GENSAL'	1	3.8	0.027	0.09	0.83	0.5	2.34	1.13	0.381	1.13	0.258	1.13	0.093	0.242	0.242	Decomposition to 3MW×4
Hydro	4420 HORANA-G	11 000	'GENSAL'	1A	3.8	0.027	0.09	0.83	0.5	2.34	1.13	0.381	1.13	0.258	1.13	0.093	0.242	0.242	
Hydro	4420 HORANA-G	11 000	'GENSAL'	1B	3.8	0.027	0.09	0.83	0.5	2.34	1.13	0.381	1.13	0.258	1.13	0.093	0.242	0.242	
Hydro	4420 HORANA-G	11 000	'GENSAL'	1C	3.8	0.027	0.09	0.83	0.5	2.34	1.13	0.381	1.13	0.258	1.13	0.093	0.242	0.242	
Hydro	4420 HORANA-G	11 000	'GENSAL'	1D	3.8	0.027	0.09	0.83	0.5	2.34	1.13	0.381	1.13	0.258	1.13	0.093	0.242	0.242	
Hydro	4251 RANITE-G1	12 500	'GENSAL'	1	5.1	0.059	0.1	2.62	0.5	1.16	0.66	0.32	0.66	0.185	0.66	0.147	0.106	0.463	
Hydro	4252 RANITE-G2	12 500	'GENSAL'	1	5.1	0.059	0.1	2.62	0.5	1.16	0.66	0.32	0.66	0.185	0.66	0.147	0.106	0.463	
Hydro	1310 SAPUG-1P	132.00	'GENSAL'	1	3.92	0.05	0.19	3.2	0.5	2.4	1.9	0.42	1.9	0.42	1.9	0.42	0.089	0.1	0.246
Diesel	1310 SAPUG-1P	132.00	'GENSAL'	2	3.92	0.05	0.19	3.2	0.5	2.4	1.9	0.42	1.9	0.42	1.9	0.42	0.089	0.1	0.246
Typical Value presented by PTI																			
					5	0.05	0.06	5.084	1	1.5	1.2	0.4	1.2	0.4	1.2	0.12	0.03	0.25	

GENSAL (Salient Pole Generator Model) Type

Type	Bus ID	Bus	Type	unit	T _{do}	T _{do}	T _{do}	T _{op}	Inertia	Speed Damping D	X _d	X _q	X _d	X _d	X _l	S(1.0)	S(1.2)	Remarks
Diesel(2013refred)	1310	ISAPUG-1P	'GENSAL'	3	3.92	0.05	0.19	3.2	0.5	2.2	1.9	0.37	0.25	0.089	0.1	0.246	Decomposition to 18MW×4	
Diesel(2013refred)	1310	ISAPUG-1P	'GENSAL'	3A	3.92	0.05	0.19	3.2	0.5	2.2	1.9	0.37	0.25	0.089	0.1	0.246		
Diesel(2013refred)	1310	ISAPUG-1P	'GENSAL'	3B	3.92	0.05	0.19	3.2	0.5	2.2	1.9	0.37	0.25	0.089	0.1	0.246		
Diesel(2013refred)	1310	ISAPUG-1P	'GENSAL'	3C	3.92	0.05	0.19	3.2	0.5	2.2	1.9	0.37	0.25	0.089	0.1	0.246		
Diesel(2013refred)	1310	ISAPUG-1P	'GENSAL'	3D	3.92	0.05	0.19	3.2	0.5	2.2	1.9	0.37	0.25	0.089	0.1	0.246		
Diesel	1310	ISAPUG-1P	'GENSAL'	4	4.3	0.05	0.19	3.2	0.5	1.98	1.9	0.31	0.21	0.089	0.1	0.3	No existing	
Diesel	4595	KHD-G	'GENSAL'	1	5.5	0.049	0.14	1	0.5	2.38	1.51	0.44	0.23	0.1	0.03	0.25	Decomposition to 6.375MW×8	
Diesel	4595	KHD-G	'GENSAL'	1A	5.5	0.049	0.14	1	0.5	2.38	1.51	0.44	0.23	0.1	0.03	0.25		
Diesel	4595	KHD-G	'GENSAL'	1B	5.5	0.049	0.14	1	0.5	2.38	1.51	0.44	0.23	0.1	0.03	0.25		
Diesel	4595	KHD-G	'GENSAL'	1C	5.5	0.049	0.14	1	0.5	2.38	1.51	0.44	0.23	0.1	0.03	0.25		
Diesel	4595	KHD-G	'GENSAL'	1D	5.5	0.049	0.14	1	0.5	2.38	1.51	0.44	0.23	0.1	0.03	0.25		
Diesel	4595	KHD-G	'GENSAL'	1E	5.5	0.049	0.14	1	0.5	2.38	1.51	0.44	0.23	0.1	0.03	0.25		
Diesel	4595	KHD-G	'GENSAL'	1F	5.5	0.049	0.14	1	0.5	2.38	1.51	0.44	0.23	0.1	0.03	0.25		
Diesel	4595	KHD-G	'GENSAL'	1G	5.5	0.049	0.14	1	0.5	2.38	1.51	0.44	0.23	0.1	0.03	0.25		
Diesel	4595	KHD-G	'GENSAL'	1H	5.5	0.049	0.14	1	0.5	2.38	1.51	0.44	0.23	0.1	0.03	0.25		
Diesel	4444	BARGE-G1	'GENSAL'	1	4.9	0.056	0.1	1.62	0.1	1.35	0.77	0.39	0.29	0.18	0.111	0.436		
Diesel(2007)	3730	CHUNNA-3	'GENSAL'	1	4.3	0.05	0.06	3.2	0.5	1.98	1.9	0.31	0.21	0.089	0.1	0.3		
DG(2005)	1660	Embilpithya	'GENSAL'	1	3.6	0.033	0.06	7.704	0.5	1.77	0.88	0.48	0.16	0.15	0.1	0.3	should be added	
DG(2005)	1810	Ladanavi Puttlam	'GENSAL'	1	5.8	0.033	0.13	1.29	0.5	2.03	1.02	0.352	0.237	0.176	0.1	0.3	should be added	
Typical Value presented by PTI					5	0.05	0.06	5.084	1	1.5	1.2	0.4	0.25	0.12	0.03	0.25		

Checked Dynamic Data												
Exciters	Type	Node	Name	Type	I	TA/TB	TB	K	TE	Emin	Emax	Remarks
To 12.5MW×2	Hydro	1100	LAX-1	132.00	1	0.1	10	300	0.05	0	3	
To 8.33MW×3	Hydro	1100	LAX-1	132.00	2	0.1	10	300	0.05	0	3	
OK	Hydro	1110	N-LAX-1	132.00	1	0.1	10	300	0.05	0	3	
OK	Hydro	1110	N-LAX-1	132.00	2	0.1	10	300	0.05	0	3	
OK	Hydro	1120	MIMAL-1	132.00	1	0.1	10	300	0.05	0	3	
OK	Hydro	1120	MIMAL-1	132.00	2	0.1	10	300	0.05	0	3	
OK	Hydro	1130	POLPI-1	132.00	1	0.1	10	300	0.05	0	3	
OK	Hydro	1130	POLPI-1	132.00	2	0.1	10	300	0.05	0	3	
OK	Hydro	1140	CANYO-1	132.00	1	0.1	10	300	0.05	0	3	
OK	Hydro	1140	CANYO-1	132.00	2	0.1	10	300	0.05	0	3	
To 16MW×3	GT	1300	KELAN-1	132.00	1	0.1	10	300	0.05	0	3.5	partial conditions
should be removed	ST (retired)	1300	KELAN-1	132.00	2	0.1	10	300	0.05	0	3	
OK	GT	1300	KELAN-1	132.00	3	0.1	10	300	0.05	0	3.5	partial conditions
OK	Hydro	2220	KOTMA-2	220.00	1	0.1	10	300	0.05	0	3	
OK	Hydro	2220	KOTMA-2	220.00	2	0.1	10	300	0.05	0	3	
OK	Hydro	2220	KOTMA-2	220.00	3	0.1	10	300	0.05	0	3	
OK	Hydro	2225	UPKT-2	220.00	1	0.1	10	300	0.05	0	3	
OK	Hydro	2225	UPKT-2	220.00	2	0.1	10	300	0.05	0	3	
To 70MW×3	Hydro	2230	VCTO-2	220.00	1	0.1	10	300	0.05	0	3	
OK	Hydro	2240	RANDE-2	220.00	1	0.1	10	300	0.05	0	3	
OK	Hydro	2240	RANDE-2	220.00	2	0.1	10	300	0.05	0	3	
OK	CC	2300	KELAN-2	220.00	1	0.1	10	200	0.05	0	3	
OK	CC	2300	KELAN-2	220.00	2	0.1	10	200	0.05	0	4	
OK	CC	2300	KELAN-2	220.00	3	0.1	10	200	0.05	0	3.5	partial conditions
OK	CC	2300	KELAN-2	220.00	4	0.1	10	200	0.05	0	4	
To 5.6MW×4	Diesel (2 or 3 retired)	3590	SAPUG-3A	33.000	1	0.1	10	300	0.05	0	6	
OK	Hydro	4251	RANTE-G1	12.500	1	0.1	10	300	0.05	0	3	
OK	Hydro	4252	RANTE-G2	12.500	1	0.1	10	300	0.05	0	3	
OK	Diesel	1310	SAPUG-1P	132.00	1	0.1	10	300	0.05	0	5	
OK	Diesel	1310	SAPUG-1P	132.00	2	0.1	10	300	0.05	0	6	Out of PTH range
To 18MW×4	Diesel (2 or 3 retired)	1310	SAPUG-1P	132.00	3	0.1	10	300	0.05	0	6	Out of PTH range
No existing		1310	SAPUG-1P	132.00	4	0.1	10	300	0.05	0	5	
OK	Diesel (2007)	3730	CHUNNA-3	33.000	1	0.1	10	200	0.05	0	6	Out of PTH range
OK	CC (2007)	2305	KERAWAL2	220.00	1	0.1	10	200	0.05	0	3	
OK	CC (2007)	2305	KERAWAL2	220.00	2	0.1	10	200	0.05	0	3	
OK	CC (2007)	2305	KERAWAL2	220.00	3	0.1	10	200	0.05	0	3	
OK	CC (2007)	2305	KERAWAL2	220.00	4	0.1	10	200	0.05	0	3	
OK	GT (2013)	2305	KERAWAL2	220.00	5	0.1	10	200	0.05	0	3	
OK	Coal (2008)	2815	PUTT A-2	220.00	1	0.1	10	200	0.05	0	3	
OK	Coal (2008)	2815	PUTT A-2	220.00	2	0.1	10	200	0.05	0	3	
OK	Diesel	4444	BARGE-G1	11.000	1	0.1	10	200	0.05	0	3	
OK	Hydro	1210	BOWAT-1	132.00	1	0.1	10	300	0.05	0	3	
should be added	DG (2005)	1660	Embilipitiya		1	0.1	10	300	0.05	0	6	
should be added	DG (2005)	1810	Ladanavi Puttalam		1	0.1	10	300	0.05	0	6	

Checked Dynamic Data												
Exciters	Type	Node	Name	Type	I	TA/TB	TB	K	TE	Emin	Emax	Remarks
OK	Hydro	1410	KUKULE-1	132.00	1	0.1	10	200	0.05	0	4.5	0 10
OK	Hydro	1410	KUKULE-1	132.00	2	0.1	10	200	0.05	0	4.5	0 10

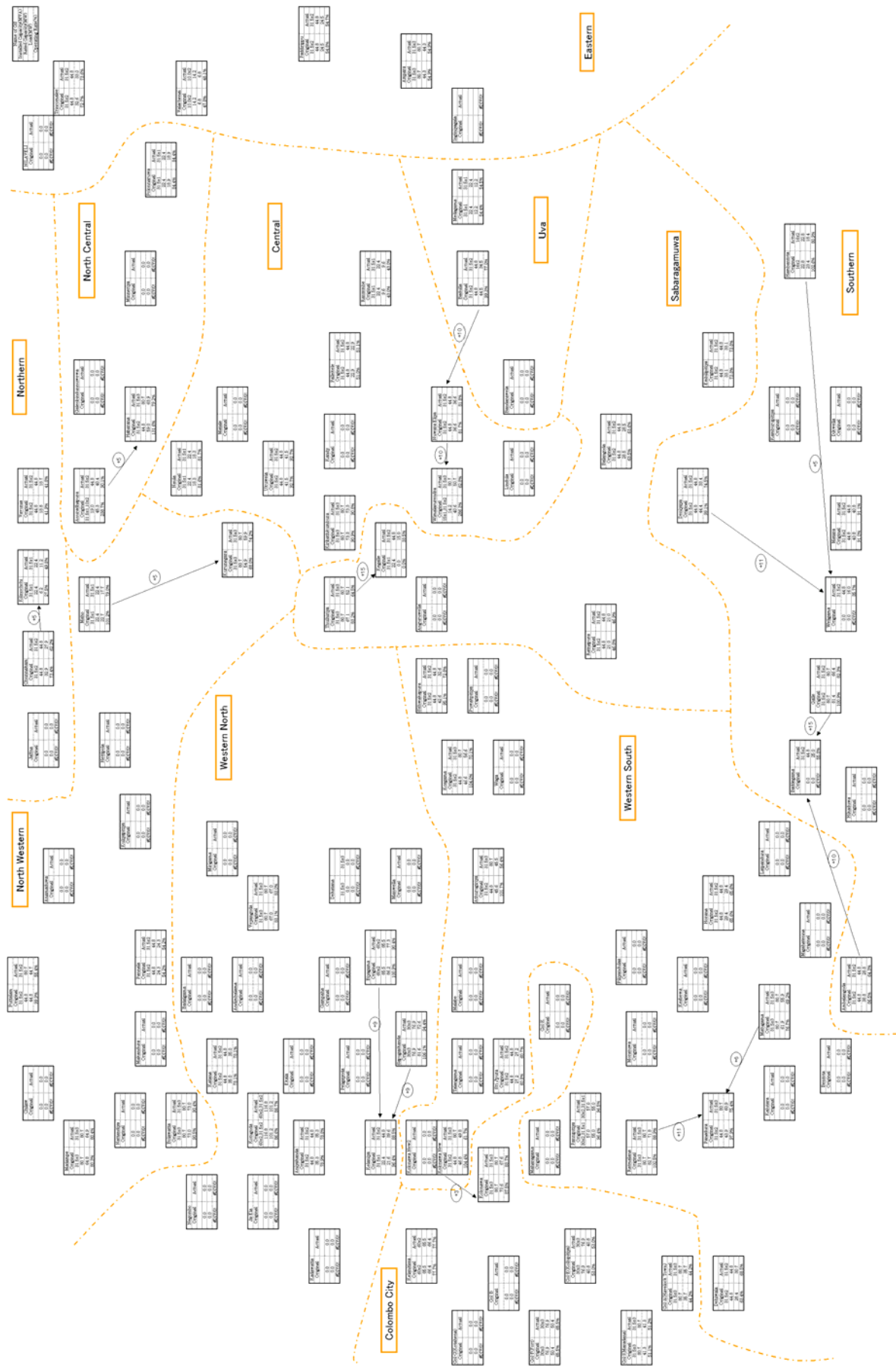
Checked Dynamic Data																
Type	Node	Name	TA	VRMAX	VRMIN	KE	TE	KF	TF	E1	SE(E1)	E2	SE(E2)	Remarks		
To 6.375MW×8	Diesel	4595 KHHD-G	11,000	40	0.001	4.5	0	1	0.35	0.04	0.32	0	3.38	0.01	4.5	0.05

Checked Dynamic Data														
Type	Node	Name	r	Tr	Tf	Tg	VELM	Gmax	Gmin	TW	At	Dturb	Q/NL	Remarks
To 12.5MW×2	Hydro	1100 LAX-1	0.3	5.2	0.05	0.5	0.2	0.95	0	1.3	1.1	0.5	0.08	
To 8.83MW×3	Hydro	1100 LAX-1	0.3	5.2	0.05	0.5	0.2	0.95	0	1.3	1.1	0.5	0.08	
OK	Hydro	1110 N-LAX-1	0.05	0.3	0.05	0.5	0.2	0.95	0	1.3	1.1	0.5	0.08	
OK	Hydro	1110 N-LAX-1	0.05	0.3	0.05	0.5	0.2	0.95	0	1.3	1.1	0.5	0.08	
OK	Hydro	1120 WIMAL-1	0.05	0.43	0.05	0.5	0.2	1	0	1.3	1.1	0.5	0.08	
OK	Hydro	1120 WIMAL-1	0.05	0.43	0.05	0.5	0.2	1	0	1.3	1.1	0.5	0.08	
OK	Hydro	1130 POLPT-1	0.05	0.43	0.05	0.5	0.2	0.85	0	1.3	1.1	0.5	0.08	
OK	Hydro	1130 POLPT-1	0.05	0.43	0.05	0.5	0.2	0.85	0	1.3	1.1	0.5	0.08	
OK	Hydro	1140 CANYO-1	0.05	0.43	0.05	0.5	0.2	0.85	0	1.3	1.1	0.5	0.08	
OK	Hydro	1140 CANYO-1	0.05	0.43	0.05	0.5	0.2	0.85	0	1.3	1.1	0.5	0.08	
OK	Hydro	1210 BOWAT-1	0.05	0.43	0.05	0.5	0.2	0.81	0	1.3	1.1	0.5	0.08	
OK	Hydro	1210 BOWAT-1	0.05	0.43	0.05	0.5	0.2	0.81	0	1.3	1.1	0.5	0.08	
OK	Hydro	1410 KUKULE-1	0.05	0.46	0.05	0.5	0.2	0.86	0	1.3	1.1	0.5	0.08	
OK	Hydro	1410 KUKULE-1	0.05	0.46	0.05	0.5	0.2	0.86	0	1.3	1.1	0.5	0.08	
OK	Hydro	2220 KOTMA-2	0.05	0.3	0.05	0.5	0.2	0.85	0	1.3	1.1	0.5	0.08	
OK	Hydro	2220 KOTMA-2	0.05	0.3	0.05	0.5	0.2	0.85	0	1.3	1.1	0.5	0.08	
OK	Hydro	2220 KOTMA-2	0.05	0.3	0.05	0.5	0.2	0.85	0	1.3	1.1	0.5	0.08	
OK	Hydro	2225 UPKT-2	0.05	0.3	0.05	0.5	0.2	0.95	0	1.3	1.1	0.5	0.08	
OK	Hydro	2225 UPKT-2	0.05	0.3	0.05	0.5	0.2	0.95	0	1.3	1.1	0.5	0.08	
To 70MW×3	Hydro	2230 VCTO-2	0.05	0.3	0.05	0.5	0.2	0.85	0	1.3	1.1	0.5	0.08	
OK	Hydro	2240 RANDE-2	0.05	0.3	0.05	0.5	0.2	0.85	0	1.3	1.1	0.5	0.08	
OK	Hydro	2240 RANDE-2	0.05	0.3	0.05	0.5	0.2	0.85	0	1.3	1.1	0.5	0.08	
OK	Hydro	4251 RANITE-G1	0.05	0.43	0.05	0.5	0.2	0.8	0	1.3	1.1	0.5	0.08	
OK	Hydro	4251 RANITE-G1	0.05	0.43	0.05	0.5	0.2	0.8	0	1.3	1.1	0.5	0.08	
OK	Hydro	4252 RANITE-G2	0.05	0.43	0.05	0.5	0.2	0.8	0	1.3	1.1	0.5	0.08	

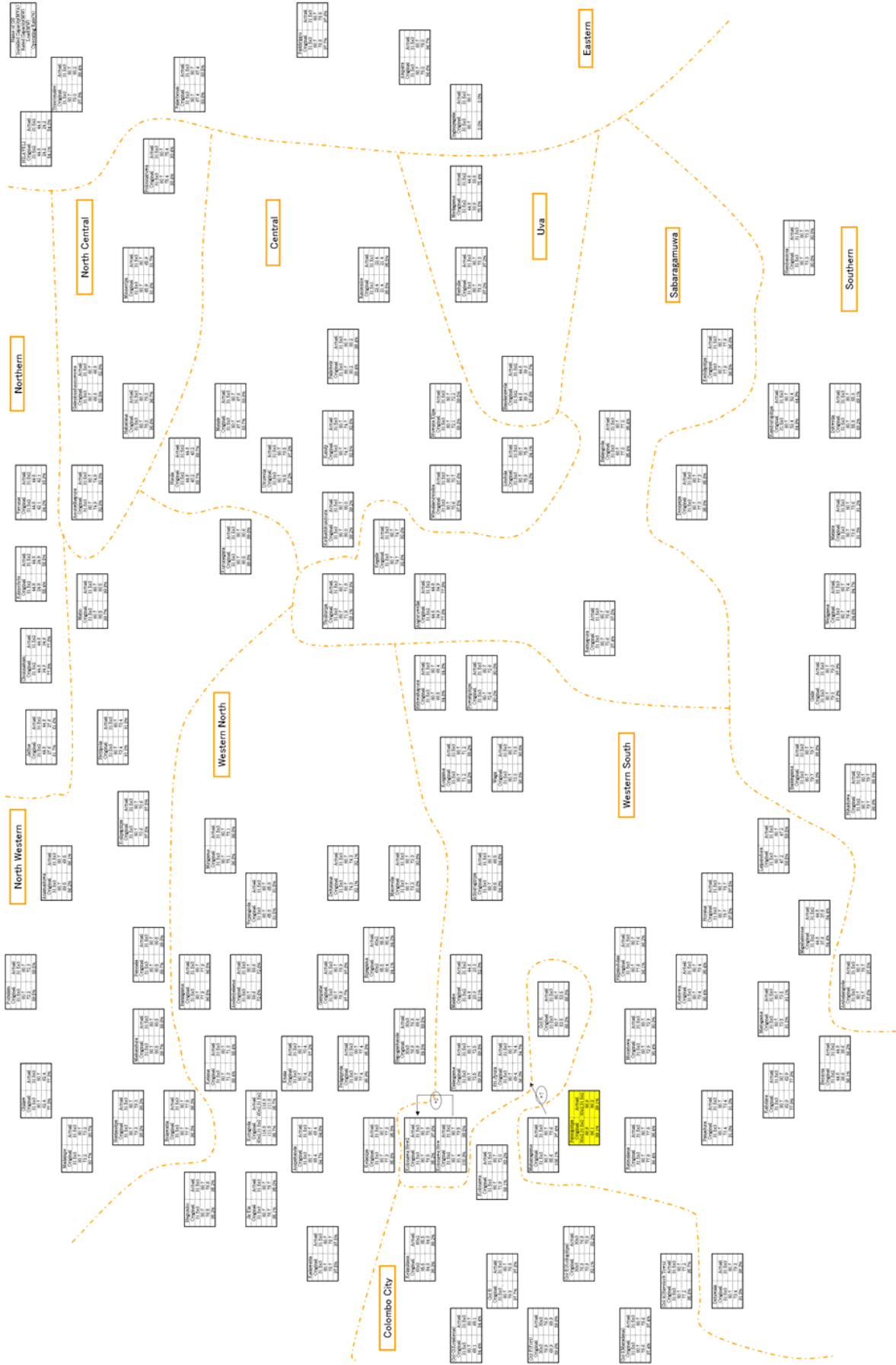
Checked Dynamic Data													
Type	Node	Name	T1	T2	T3	AT	KT	Vmax	Vmin	Dturb	Remarks		
To 16MW×3	GT	1300 KELAN-1	0.05	0.4	0.1	3	1	0.95	-0.05	0	0 (line controlled)		
OK	GT	1300 KELAN-1	0.05	0.4	0.1	3	1	0.95	-0.05	0			
OK	CC(2007)	2305 KERAWAL2	0.05	0.4	0.1	3	1	0.95	-0.05	0			
OK	CC(2007)	2305 KERAWAL2	0.05	0.4	0.1	3	1	0.95	-0.05	0			
OK	CC(2007)	2305 KERAWAL2	0.05	0.4	0.1	3	1	0.95	-0.05	0			
OK	CC	2300 KELAN-2	0.05	0.4	0.1	3	1	0.95	-0.05	0			
OK	CC	2300 KELAN-2	0.05	0.4	0.1	3	1	0.95	-0.05	0			

Checked Dynamic Data													
Type	Node	Name	T1	T2	T3	Vmin	Dt	Remarks					
To 5.6MW×4	ST (retired)	1300 KELAN-1	0.05	0.1	0.95	0	1.8	6	0				
should be removed	Diesel(2012retired)	3590 SAPUG-3A	0.05	0.5	0.85	0.3	1.8	6	0				
OK	Diesel(2007)	3730 CHUNNA-3	0.05	0.5	1.08	0.3	1.8	6	0				
OK	CC(2007)	2305 KERAWAL2	0.05	0.1	0.95	0	1.8	6	0				
OK	CC(2007)	2305 KERAWAL2	0.05	0.1	0.95	0	1.8	6	0				
OK	CC	2300 KELAN-2	0.05	0.1	0.95	0	1.8	6	0				
OK	CC	2300 KELAN-2	0.05	0.1	0.95	0	1.8	6	0				
should be added	DG(2005)	1660 Embilipitya	0.05	0.5	1.08	0.3	1.8	6	0				
should be added	DG(2005)	1810 Lalanavi.Puttiam	0.05	0.5	1.08	0.3	1.8	6	0				

Load Transfer Forecast for Each Grid Substation (2010)



Load Transfer Forecast for Each Grid Substation (2025)



Outline for Power Concentration Case Study

Single Line Diagram	Base Case	Power Concentration in Southern Area	Power Concentration in Northern Area	Items	Volume	Cost (MLKR)	
Lines	Chi - Vey Put - Chi Ham - Mat Thi - Hab Ban - Ham Vey - Kir Kir - Amb Ara - Amb Amb - Mat	45 km 140 km 135.6km 95 km 105 km 14.4km 22.2km 11.4km 58.2km	45 km 140 km 135.6km 95 km 105 km 14.4km 22.2km 11.4km 58.2km	Chi - Vey Put - Chi Ham - Mat Thi - Hab Ban - Ham Vey - Kir Kir - Amb Ara - Amb Amb - Mat	45 km 140 km 135.6km 95 km 105 km 14.4km 22.2km 11.4km 58.2km	Zebra_4 2cct 16,494.7	
	Ham - Vey Kot - U Kot U Kot - Ban Koru - Ker Ker - Kel	145 km 18.5km 46 km 18 km 14.4km	145 km 18.5km 46 km 18 km 14.4km	145 km 18.5km 46 km 18 km 14.4km	Ham - Vey Kot - U Kot U Kot - Ban Koru - Ker Ker - Kel	Zebra_2 2cct 4,720.6 CV_160mm2 2cct 2,117.6	
Transformers	220 - 132 - 33 250MVA (Manu: 1 units included) 220 - 132 - 33 150MVA	31 units 1 units	31 units 1 units	220 - 132 - 33 250MVA (Manu: 1 units included) 220 - 132 - 33 150MVA	6,904.6 181.4		
GIS	220kV	11places	11places	220kV	4,166.0		
SIS	220kV	1places	1places	SIS	369.8		
Phase Modifying Equipment (Trunk System)	SC (20MVR) Chi-210, Hab-80, Ban-100, Amb-150, Ara-150, Kel-100, Mat-150, Pen-50, Mat-200(SC)	59.5units	59.5units	SC (20MVR) Chi-210, Hab-80, Ban-100, Amb-150, Ara-150, Kel-100, Mat-150, Pen-50, Mat-200(SC)	1,190.0		
Others							
Total Cost						36,687.0	
Remarks	A						

Best Allocation Checking for Generators

	Alternative A	Alternative B	Base Case from Generation View Point				
Single Line Diagram							
Items	Cost (MLFR)	Volume	Items	Cost (MLFR)	Volume	Items	Cost (MLFR)
Base Cost	36,687.0		Base Cost	36,687.0		Base Cost	36,687.0
Transformers	220 · 132 · 33 250MVA units	1 units	220 · 132 · 33 250MVA (Mat - 1unit)	0.0	-222.7		
G/S	units	units					
S/S	places	places	220KV				
Phase							
Modifying Equipment	SC (20MVR)	units	SC (20MVR)		-200.0		
Others			Mat_200MVAR				
Total Cost				36,687.0			36,687.0
Technical Assessment	OK	OK	OK	OK	OK	OK	OK
N=0	OK	OK	OK	OK	OK	OK	OK
N=1	OK	OK	OK	OK	OK	OK	OK
(SS is not considered)	OK	OK	OK	OK	OK	OK	OK
Dynamic Stability	Ham - Mat	Ham - Mat	Put - Chi	Ham - Mat	Ham - Ban	Put - Chi	Ham - Mat
Effect of S/S	OK	OK	OK	OK	OK	OK	OK
Short Circuit	OK (Under 40kA)	OK (Under 40kA)	OK (Under 40kA)	OK (Under 40kA)	OK (Under 40kA)	OK (Under 40kA)	OK (Under 40kA)
Assessment	A	S (in case that 6 units in South are operated at any time)	S (in case that 6 units in South are operated at any time)	A	A	A	A
Remarks		SC and Transformer for SC can be reduced					
Total Remarks	The maximum number of generators in Northern area is 7. The number is can be 8 with extra high expence. The maximum number of generators in Southern area is 8. The number is can be 9 with extra high expence.						
	Red letters represent the difference between base case and the other's case						

Case that Power Stations are Concentrated in North Area

	Alternative A-1	Alternative A-2	Alternative A-3	
Single Line Diagram				
Cost	Items	Volume	Cost (MLKR)	Cost (MLKR)
	Base Cost		36,687.0	36,687.0
	Transformers	1 units	0.0	0.0
	GIS	units	222.7	445.5
	SIS	places	0.0	0.0
	Phase Modifying Equipment	2places	739.7	739.7
	Others	units	0.0	100.0
	Total Cost			37,649.4
Technical Assessment	OK		OK	OK
N-1	OK		OK	OK
(SS is not considered)			N.G. (In case of one line failure between Veyangoda and N.Chilaw, the other line is overrated or transformers at N.Chilaw are overrated with system configuration change.)	
Dynamic Stability	Put220 - Chi	Chi220 - Vey		Put220 - Chi
Effect of SIS	OK	OK		N.G.
Short Circuit	OK	OK		N.G.
				OK (Under 40kA)
Assessment	B		N.G.	N.G.
Remarks	One unit can be added with two SISs, however it costs a lot of money and is not so effective. Red letters represent the difference between base case and the other's case			

Case that Power Stations are Concentrated in North Area

	Alternative B-1	Alternative B-2 (Just Confirmation)	Alternative B-3																																																																																																												
Single Line Diagram																																																																																																															
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Red letters represent the difference between base case and the other's case

Case that Power Stations are Concentrated in North Area

Alternative C-1 (Bus Split)		Detailed Single Diagram at Puttalam		Matugama	
Items	Volume	Cost (MLFR)	Items	Volume	Cost (MLFR)
Lines					
Base Cost					
Put - Chi	70 km	36,687.0	Zebra_4 2cort		
Chi - Vey	45 km	1,895.4	Zebra_4 2cort		
Put - Chi	70 km	1,179.9	Zebra_4 2cort(400kV)		
Chi - Vey	45 km	7,855.7			
Transformers					
230 / 132 / 33kV MVA	1 units	222.7			
440 / 220/60MVA	6 units	5,874.0			
GIS	places	0.0			
SIS	places	0.0			
Phase Modifying Equipment	units	0.0			
Others					
Total Cost		47,624.1			
Technical Assessment					
N=0					
N=1					
(SS is not considered)					
Dynamic Stability	Put400 - Chi				
Effect of SIS	OK				
Short Circuit	-				
Assessment	OK (Under 40kA)				
Remarks	C				
Red letters represent the difference between base case and the other's case					

Case that Power Stations are Concentrated in North Area

	Alternative C-2 (Bus Split)	Alternative C-3 (Bus Split)						
Single Line Diagram								
Cost			Items	Volume	Cost (MLKR)	Items	Volume	Cost (MLKR)
Libres			Base Cost		36,687.0			
			Put - Chi	70 km	Zebra_4 2crt -1835.4			
			Chi - Vey	45 km	Zebra_4 2crt -1,179.9			
			Put - Chi	70 km	Zebra_4 2crt(400KV)			
			Chi - Vey	45 km	Zebra_4 2crt(400KV)			
			20 - 13 - S20MVA	2units	445.5			
			(Gal. Inst. Vc, 2crt Mat. Inst.)					
			440 - 220 600MVA	6units	5,874.0			
			places		0.0			
			places		1,240.7			
			400KV					
			SC (20MVR)	5 units	100.0			
			Vey_300, Mat_200					
Total Cost					49,316.6			49,187.5
Technical Assessment								
N-0			OK		OK			
N-1			OK		OK			
(SS is not considered)								
Dynamic Stability			Put220 - Chi	Put400 - Chi				
			N/G	OK				
Effort of S/S			OK					
Short Circuit				OK (Under 40kA)				
Assessment				OK (Under 40kA)				
Remarks			Very High Cost					

Red letters represent the difference between base case and the other's case

Case that Power Stations are Concentrated in South Area

	Alternative A-1	Alternative B-1	Alternative C
Single Line Diagram			
Items	Base Cost	Base Cost	Base Cost
Volume	Volume	Volume	Volume
Cost (MLKR)	36,687.0	36,687.0	36,687.0
Cost	37,849.4	49,287.9	36,687.0
Technical Assessment	OK	OK	N.G.
N-0	OK	OK	N.G.
N-1	OK	OK	N.G.
(SS is not considered)	OK	OK	N.G.
Dynamic Stability	Mat - Ham	Ham - Ban	Ham Tr
Effect of S/S	N.G	N.G	OK
Short Circuit	OK	OK	OK
Assessment	B	C	N.G.
Remarks	One unit can be added with two SSS, however it costs a lot of money and is not so effective.	Very High Cost	1 route is not enough to supply power even if total power in Hambantota is 240MW(8 units)

Red letters represent the difference between base case and the other's case

Case that Power Stations are Concentrated in South Area

	Alternative A-2	Alternative B-2						
Single Line Diagram								
Cost			Items	Volume	Cost (MLKR)	Items	Volume	Cost (MLKR)
Lines			Base Cost		36,687.0			
Transformers			220 - 132 - 33.250MVA (Mar-tunbs)	1 units	222.7	Ham - Mat(20 Z.4)	135.6km	36,687.0
GIS				units	0.0	Ham - Mat(400 Z.4)	135.6km	9,252.8
SIS			220KV	2places	739.7	220 - 132 - 33.250MVA (Mar-tunbs)	1units	222.7
Phase Modifying Equipment			SC (20MVR)	15 units	300.0	440 - 220.600MVA places	6units	5,874.0
Others			Mar-300			220KV	1places	369.8
Total Cost						SC (20MVR) Mar-100	5 units	100.0
Technical Assessment					37,949.4	Line Swith 400KV	4units	649.8
N-0								49,610.6
N-1 (SS is not considered)								
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Effect of SIS								
Short Circuit								
Assessment								
Remarks								

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N.G.

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Case that Power Stations are Concentrated in South Area

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Remarks	Very High Cost																																																																																												

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Case that Power Stations are Concentrated in North Area (Fault Clearance: 100ms)

	Alternative A-1	Alternative A-2	Alternative B-1																																																																																							
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Technical Assessment	<p>N-0 OK</p> <p>N-1 OK</p> <p>(SS is not considered)</p> <p>Dynamic Stability Put220 - Chi OK</p> <p>Effect of SIS OK</p> <p>Short Circuit OK (Under 40kA)</p>	<p>OK</p> <p>OK</p> <p>Put220 - Chi OK</p> <p>OK</p> <p>OK (Under 40kA)</p>	<p>OK</p> <p>OK</p> <p>Put220 - Chi OK</p> <p>OK</p> <p>OK (Under 40kA)</p>																																																																																							
Assessment	A	N.G	B																																																																																							
Remarks	100 msec of the clearance time is effective. 8 is the marginal number of unit in the Northern area.	100 msec of the clearance time is effective. One unit can be added with Parrot.	100 msec of the clearance time is effective. One unit can be added with Parrot.																																																																																							
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Case that Power Stations are Concentrated in South Area (Fault Clearance: 100ms)

Alternative A-1		Alternative A-2								
Single Line Diagram										
Items	Volume	Items	Volume	Items	Volume	Items	Volume	Cost (MLKR)	Cost (MLKR)	
Base Cost				Base Cost				36,687.0	36,687.0	
220 - 132 - 33.250MVA (Mat_1unit)	1 units			220 - 132 - 33.250MVA (Mat_1unit)	1 units			0.0	0.0	
G/S	units				units			222.7	222.7	
S/S	places				places			0.0	0.0	
Phase Modifying Equipment	places			220KV	places			0.0	0.0	
Others				SC (20MVR) Mat_200	10 units			200.0	200.0	
Total Cost								37,108.7	37,208.7	
Technical Assessment										
N-0	OK							OK	OK	
N-1	OK							OK	OK	
Dynamic Stability	Mat - Ham	Ham - Ban		Mat - Ham	Ham - Ban			OK	OK	
Effect of S/S	OK	OK		OK	OK			OK	OK	
Short Circuit	OK (Under 40kA)	OK (Under 40kA)		OK	NG (Over 40kA)			NG 41.7kA (Over 40kA)		
Assessment	A			N.G.(A)						
Remarks	100 msec of the clearance time is effective. 9 is the marginal number of unit in the Southern area.			10 units is acceptable with 50kA-Line switch.						
Red letters represent the difference between base case and the other's case										

Result on Countermeasure for Power Supply to Northern Area Interconnection Case

	Year	Construction Cost (M US\$)	O&M of IPP (M US\$)	O&M of CEB in Main Grid (M US\$)	Cost for Producing Loss Energy (M US\$)	Total (M US\$)	P.V (M US\$)	Remarks
0	2004		15.3			15.3	15.3	Present Year
1	2005		16.1			16.1	14.7	
2	2006		17.0			17.0	14.1	
3	2007	22.93	0.0	6.1	0.06	29.1	24.0	LTIDS 2004
4	2008		0.0	6.4	0.07	6.5	4.9	
5	2009		0.0	6.8	0.08	6.9	4.7	
6	2010		0.0	7.2	0.08	7.2	4.5	
7	2011		0.0	7.5	0.09	7.6	4.3	
8	2012		0.0	8.0	0.10	8.1	4.1	
9	2013		0.0	8.4	0.12	8.5	4.0	
10	2014		0.0	8.9	0.13	9.0	3.8	
11	2015		0.0	9.4	0.14	9.5	3.7	
12	2016		0.0	9.9	0.16	10.0	3.5	
13	2017		0.0	10.4	0.18	10.6	3.4	
14	2018		0.0	11.0	0.20	11.2	3.2	
15	2019		0.0	11.6	0.22	11.8	3.1	
16	2020		0.0	12.2	0.24	12.5	3.0	
17	2021		0.0	12.9	0.27	13.2	2.9	
18	2022		0.0	13.6	0.30	13.9	2.8	
19	2023		0.0	14.4	0.34	14.7	2.6	
20	2024		0.0	15.2	0.38	15.6	2.5	
20	2025		0.0	16.0	0.42	16.4	2.4	
Total Present Value							117.5	

After interconnection is installed, 100% of Total consumption in Jaffna area is supplied from CEB

Discount Rate =

10% Source: LTGEP2003

Generation Expantion Plan (CEB Only)

	Year	Power Plant Construction Cost (M US\$)	O&M of IPP (M US\$)	O&M of CEB in Jaffna (M US\$)	Total (M US\$)	P.V (M US\$)	Remarks
0	2004						
0	2005		15.3		15.3	15.3	Present Year
1	2006		16.1		16.1	14.7	
2	2007		17.0		17.0	14.1	
3	2008		18.0		18.0	13.5	
4	2009	44.8	0.0	14.9	59.7	40.8	
5	2010		0.0	15.8	15.8	9.8	
6	2011		0.0	16.6	16.6	9.4	
7	2012	22.4	0.0	17.6	40.0	20.5	
8	2013		0.0	18.5	18.5	8.6	
9	2014		0.0	19.6	19.6	8.3	
10	2015		0.0	20.6	20.6	8.0	
11	2016		0.0	21.8	21.8	7.6	
12	2017		0.0	23.0	23.0	7.3	
13	2018		0.0	24.2	24.2	7.0	
14	2019		0.0	25.6	25.6	6.7	
15	2020		0.0	27.0	27.0	6.5	
16	2021		0.0	28.5	28.5	6.2	
17	2022		0.0	30.1	30.1	5.9	
18	2023		0.0	31.7	31.7	5.7	
19	2024		0.0	33.5	33.5	5.5	
20	2025	22.4	0.0	35.3	57.7	8.6	
Total Present Value						230.0	

Considering N-1 condition, the number of units includes back-up.

Discount Rate =

10% Source: LTGEP2003

Generation Expantion Plan (CEB and IPP as Back-up)

	Year	Power Plant Construction Cost (M US\$)	O&M of IPP (M US\$)	O&M of CEB in Jaffna (M US\$)	Total (M US\$)	P.V (M US\$)	Remarks
0	2004						
0	2005		15.3		15.3	15.3	Present Year
1	2006		16.1		16.1	14.7	
2	2007		17.0		17.0	14.1	
3	2008		18.0		18.0	13.5	
4	2009	22.4	3.8	12.0	38.1	26.1	
5	2010		4.0	12.6	16.6	10.3	
6	2011		4.2	13.3	17.5	9.9	
7	2012	22.4	4.5	14.0	40.9	21.0	
8	2013		4.7	14.8	19.5	9.1	
9	2014		5.0	15.6	20.6	8.7	
10	2015		5.2	16.5	21.7	8.4	
11	2016		5.5	17.4	22.9	8.0	
12	2017		5.8	18.4	24.2	7.7	
13	2018		6.1	19.4	25.5	7.4	
14	2019		6.5	20.5	27.0	7.1	
15	2020		6.8	21.6	28.4	6.8	
16	2021		7.2	22.8	30.0	6.5	
17	2022		7.6	24.0	31.7	6.3	
18	2023		8.0	25.4	33.4	6.0	
19	2024		8.5	26.8	35.3	5.8	
20	2025	22.4	9.0	28.2	59.6	8.9	
Total Present Value						221.5	

80% of Total consumption in Jaffna area is supplied from CEB

Discount Rate =

10% Source: LTGEP2003

Interconnection between North Area and Main Grid (Generator is installed from the beginning)

Base Data: 2010 Night Peak (New Demand and Generators are considered)

	Alternative A	Alternative B	Alternative C	
Single Line Diagram				
Cost	Items	Vav - Kil (Lynx 74.1km) Kil - Chu(Lynx 67.2km) Vav- Chu(Lynx 141.3km)	Vav - Kil (Lynx 74.1km) Kil - Chu(Lynx 67.2km) Vav- Chu(Lynx 141.3km)	
	Volume	Lynx 2cct 141.3km	Lynx 2cct 141.3km	
	Cost (MLKR)	1,268.9	1,268.9	
	Phase Modifying Equipment	SC (Chunnakam) 5MVAR	SC (Chunnakam) 5MVAR	0
	Others	132kV line bay	132kV line bay	132kV line bay
Total Cost	Excluding Generator Construction Cost	1,378.7	1,342.1	1,415.3
Remarks				
Assessment on System Condition	B			C

Interconnection between North Area and Main Grid (Generator is installed from the beginning)

Base Data: 2015 Night Peak (New Demand and Generators are considered)

		Alternative A			Alternative B			
Single Line Diagram								
	Cost	Lines	Vav - Kil (Lynx 74.1km) Kil - Chu(Lynx 67.2km) Vav - Chu(Lynx 141.3km)	Volume Lynx 2cct 141.3km	Cost (MLKR) 1,268.9	Items Vav - Kil (Lynx 74.1km) Kil - Chu(Lynx 67.2km) Vav - Chu(Lynx 141.3km)	Volume Lynx 2cct 141.3km	Cost (MLKR) 1,268.9
		Phase Modifying Equipment	SC (Chunnakam) 5MVAR	units	0	SC (Chunnakam) 5MVAR	units	0
		Others	132kV line bay	4 units	73.2	132kV line bay	6 units	109.8
		Total Cost	Excluding Generator Construction Cost	1,342.1	Excluding Generator Construction Cost	1,378.7		
Remarks	If the line between Anuradhapura and Vavunia is failure, the system can not supply power to Vavunia. If the line between Anuradhapura and Kilinochchi is failure, the voltage at Kilinochchi is under 0.9 pu. (0.893)							
Assessment on System Condition	Not Good			A				

Interconnection between North Area and Main Grid (Generator is installed from the beginning)

Base Data: 2020 Night Peak (New Demand and Generators are considered)

		Alternative A			Alternative B			Alternative C		
Single Line Diagram										
	Cost	Items	Vav - Kil (Lynx 74.1km) Kil - Chu(Lynx 67.2km) Vav- Chu(Lynx 141.3km) Chu - Jaf(Lynx 10.8km)	Vav - Kil (Lynx 74.1km) Kil - Chu(Lynx 67.2km) Vav- Chu(Lynx 141.3km) Chu - Jaf(Lynx 10.8km)	Vav - Kil (Lynx 74.1km) Kil - Chu(Lynx 67.2km) Vav- Chu(Lynx 141.3km) Chu - Jaf(Lynx 10.8km)	Vav - Kil (Lynx 74.1km) Kil - Chu(Lynx 67.2km) Vav- Chu(Lynx 141.3km) Chu - Jaf(Lynx 10.8km)				
		Volume	Lynx 2ect 152.1km	Lynx 2ect 152.1km	Lynx 2ect 152.1km	Lynx 2ect 152.1km				
		Phase Modifying Equipment	SC (Chunnakam) 5MVAR	SC (Chunnakam) 5MVAR	SC (Chunnakam) 5MVAR	0				
		Others	132kV line bay	132kV line bay	132kV line bay	183.0				
Total Cost	Excluding Generator Construction Cost	1,451.9	Excluding Generator Construction Cost	1,555.5	Excluding Generator Construction Cost	1,451.9				
Remarks				Tower conversion cost (very small) is needed						
Assessment on System Condition	A			B			A-			

Interconnection between North Area and Main Grid (Generator is installed from the beginning)

Base Data: 2025 (New Demand and Generators are considered)

		Alternative A		Alternative B		Alternative C	
Cost	Single Line Diagram						
	Lines	Items	Volume	Cost (MLKR)	Items	Volume	Cost (MLKR)
	Phase Modifying Equipment	Items	Volume	Cost (MLKR)	Items	Volume	Cost (MLKR)
	Others	Items	Volume	Cost (MLKR)	Items	Volume	Cost (MLKR)
	Total Cost	Excluding Generator Construction Cost	1,451.9	Excluding Generator Construction Cost	1,585.5	Excluding Generator Construction Cost	1,451.9
Remarks	If the line between Anuradhapura and Vavunia is failure, the system, the voltage at Kilinochchi is under 0.9 pu. (0.889)						
Assessment on System Condition	Not Good		B		A		

Affect to the Main Grid by Mini-Hydro Interconnection

Base Data: 2005 Hydro Maximum Case (New Demand and Generators are considered)

Study A (N-0, N-1)		Study B (Frequency Drop)																		
<p style="text-align: center;">Single Line Diagram</p>	<p style="text-align: center;">How much Capacity will be able to be installed</p>	<p style="text-align: center;">Day</p>	<p style="text-align: center;">Drop</p>																	
<p style="text-align: center;">Pre Condition (Night)</p>	<p style="text-align: center;">How big impact does the system receive?</p> <p style="text-align: center;">dF = 1/4.75 x 100x (27.5 / 1700) = 0.34</p> <p style="text-align: center;">49.66Hz > 48.75 Hz → No Load Shedding</p> <p style="text-align: center;">49.66Hz > 49.5Hz (Grid Code) → No Problem</p>																			
<p style="text-align: center;">Result (Night)</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: left;">Bottle Neck</th> <th style="text-align: right;">Marginal Volume (Normal state) (MW)</th> </tr> </thead> <tbody> <tr><td>Wimalsurendura Tr</td><td style="text-align: right;">308.9</td></tr> <tr><td>Deniyaya Tr</td><td style="text-align: right;">329.1</td></tr> <tr><td>Sithawaka - Kolonnawa</td><td style="text-align: right;">459.9</td></tr> <tr><td>Ratnapura Tr</td><td style="text-align: right;">461.6</td></tr> <tr><td>Bottle Neck</td><td style="text-align: right;">198.7</td></tr> <tr><td>Wimalsurendura Tr</td><td style="text-align: right;">223.0</td></tr> <tr><td>N-Laxapana - Polpitiya</td><td style="text-align: right;">224.1</td></tr> <tr><td>Deniyaya Tr</td><td style="text-align: right;">241.1</td></tr> <tr><td>Ratnapura Tr</td><td style="text-align: right;">241.1</td></tr> </tbody> </table> <p style="text-align: center;">Causes (N-1) Wimalsurendura Tr 1 unit failure N-Laxapana - Polpitiya 1cct Open Deniyaya Tr 1 unit failure Ratnapura Tr 1 unit failure</p>	Bottle Neck	Marginal Volume (Normal state) (MW)	Wimalsurendura Tr	308.9	Deniyaya Tr	329.1	Sithawaka - Kolonnawa	459.9	Ratnapura Tr	461.6	Bottle Neck	198.7	Wimalsurendura Tr	223.0	N-Laxapana - Polpitiya	224.1	Deniyaya Tr	241.1	Ratnapura Tr	241.1
Bottle Neck	Marginal Volume (Normal state) (MW)																			
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Deniyaya Tr	241.1																			
Ratnapura Tr	241.1																			
<p style="text-align: center;">Pre Condition (Day)</p>	<p style="text-align: center;">During Off Peak</p> <p style="text-align: center;">Demand is 62% of Day Peak (Daily load curve as of Sep in 2004)</p> <p style="text-align: center;">dF = 1/4.75 x 100x (27.5 / 700) = 0.83</p> <p style="text-align: center;">49.17Hz > 48.75 Hz → No Load Shedding</p> <p style="text-align: center;">49.17Hz < 49.5Hz (Grid Code) → However, it can recover to the acceptable range after governor operating</p> <p style="text-align: center;">No Problem</p>																			
<p style="text-align: center;">Result (Day)</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: left;">Bottle Neck</th> <th style="text-align: right;">Marginal Volume (Normal state) (MW)</th> </tr> </thead> <tbody> <tr><td>Polpitiya - Kosgama</td><td style="text-align: right;">44.4</td></tr> <tr><td>Polpitiya - Thulhiriya</td><td style="text-align: right;">80.3</td></tr> <tr><td>Sithawaka - Kolonnawa</td><td style="text-align: right;">116.7</td></tr> <tr><td>N-Laxapana - Polpitiya</td><td style="text-align: right;">129.1</td></tr> <tr><td>Bottle Neck</td><td style="text-align: right;">0 (-42.6)</td></tr> <tr><td>Polpitiya - Thulhiriya</td><td style="text-align: right;">0 (-39.9)</td></tr> <tr><td>Polpitiya - Sithawaka</td><td style="text-align: right;">0 (-27.1)</td></tr> <tr><td>Polpitiya - Kosgama</td><td style="text-align: right;">17.2</td></tr> <tr><td>N-Laxapana - Polpitiya</td><td style="text-align: right;">17.2</td></tr> </tbody> </table> <p style="text-align: center;">Causes (N-1) Polpitiya - Thulhiriya 1cct Open Kosgama - Polpitiya 1cct Open Polpitiya - Sithawaka 1cct Open N-Laxapana - Polpitiya 1cct Open</p>	Bottle Neck	Marginal Volume (Normal state) (MW)	Polpitiya - Kosgama	44.4	Polpitiya - Thulhiriya	80.3	Sithawaka - Kolonnawa	116.7	N-Laxapana - Polpitiya	129.1	Bottle Neck	0 (-42.6)	Polpitiya - Thulhiriya	0 (-39.9)	Polpitiya - Sithawaka	0 (-27.1)	Polpitiya - Kosgama	17.2	N-Laxapana - Polpitiya	17.2
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<p style="text-align: center;">Summary</p> <p>Total around 20MW, 61MW as of existing working amount - 42.6 as of additional mini-hydro installed, is acceptable from the view point of thermal capacity.</p> <p>All mini-hydro power plants can not be connected during day peak.</p>																				

Affect to the Main Grid by Mini-Hydro Interconnection

Base Data: 2010 Hydro and Thermal Maximum Case (New Demand and Generators are considered)

Study A (N-0, N-1)		Study B (Frequency Drop)																					
<p>Single Line Diagram</p>			<p>Balangoda has the biggest Volume of mini-hydro at one site</p>																				
<p>Pre Condition (Night)</p>			<p>Out put of hydraulic power generation in central area declines, as compared with 2005. Because the excess capability of transmission lines in central area declines, as load increases. Out put of hydraulic power generation in central area is necessary to be reduced.</p>																				
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<p>Summary</p>	<p>Total around 0MW(-23.3MW), 61MW as of existing working amount - 84.3 as of additional mini-hydro installed, is acceptable from the view point of thermal capacity.</p> <p>Any mini-hydro power plants can not be connected during day peak.</p>																						

No Problem

During Off Peak
Demand is 62% of Day Peak (Daily load curve as of Sep in 2004)
dF = 1/4.75 x 100x (27.5 / 700) = 0.54
49.46Hz > 48.75 Hz → No Load Shedding
49.46Hz < 49.5Hz (Grid Code) → However, it can recover to the acceptable range after governor operating

Mini-Hydro Impact Analysis (Operating Condition of Mini Hydro)

2005

Night Peak Case

80% Operation for Hydro Maximum

			Pre P	Pre Q	Mini P	Mini P (80%)	Estimated P	Estimated Q
3770	KIRIB-3	33.000	69.1	37.3	9.65	7.72	61.38	33.1
3120	WIMAL-3	33.000	17	10.9	5.46	4.37	12.632	8.1
3520	NUWAR-3	33.000	38.2	17.4	4.41	3.53	34.672	15.8
3640	DENIY-3	33.000	22.1	14.8	6.35	5.08	17.02	11.4
3740	RATNAP-3	33.000	15	9.3	15.08	12.06	2.936	1.8
3510	SITHA-33	33.000	29	14.8	7.43	5.94	23.056	11.8
3630	BALAN-3	33.000	47.9	27	27.5	22.00	25.9	14.6
						75.88	60.70	

60% Operation for Thirmal Maximum

			Pre P	Pre Q	Mini P	Mini P (60%)	Estimated P	Estimated Q
3770	KIRIB-3	33.000	69.1	37.3	9.65	5.79	63.31	34.2
3120	WIMAL-3	33.000	17	10.9	5.46	3.28	13.724	8.8
3520	NUWAR-3	33.000	38.2	17.4	4.41	2.65	35.554	16.2
3640	DENIY-3	33.000	22.1	14.8	6.35	3.81	18.29	12.2
3740	RATNAP-3	33.000	15	9.3	15.08	9.05	5.952	3.7
3510	SITHA-33	33.000	29	14.8	7.43	4.46	24.542	12.5
3630	BALAN-3	33.000	47.9	27	27.5	16.50	31.4	17.7
						75.88	45.53	

Day Peak Case

80% Operation for Hydro Maximum

			Pre P	Pre Q	Mini P	Mini P (80%)	Estimated P	Estimated Q
3770	KIRIB-3	33.000	34.6	18.6	9.65	7.72	26.88	14.4
3120	WIMAL-3	33.000	7.7	5	5.46	4.37	3.332	2.2
3520	NUWAR-3	33.000	19.1	8.7	4.41	3.53	15.572	7.1
3640	DENIY-3	33.000	11.7	7.9	6.35	5.08	6.62	4.5
3740	RATNAP-3	33.000	7.5	4.6	15.08	12.06	-4.564	-2.8
3510	SITHA-33	33.000	21.1	10.8	7.43	5.94	15.156	7.8
3630	BALAN-3	33.000	37.7	21.3	27.5	22.00	15.7	8.9
						75.88	60.70	

60% Operation for Thirmal Maximum

			Pre P	Pre Q	Mini P	Mini P (60%)	Estimated P	Estimated Q
3770	KIRIB-3	33.000	34.6	18.6	9.65	5.79	28.81	15.5
3120	WIMAL-3	33.000	7.7	5	5.46	3.28	4.424	2.9
3520	NUWAR-3	33.000	19.1	8.7	4.41	2.65	16.454	7.5
3640	DENIY-3	33.000	11.7	7.9	6.35	3.81	7.89	5.3
3740	RATNAP-3	33.000	7.5	4.6	15.08	9.05	-1.548	-0.9
3510	SITHA-33	33.000	21.1	10.8	7.43	4.46	16.642	8.5
3630	BALAN-3	33.000	37.7	21.3	27.5	16.50	21.2	12.0
						75.88	45.53	

Mini-Hydro Impact Analysis (Operating Condition of Mini Hydro)

2010

Night Peak Case

80% Operation for Hydro_Maximum

			Pre P	Pre Q	Mini P	Mini P (80%)	Estimated P	Estimated Q
3770	KIRIB-3	33.000	73.3	39.6	9.65	7.72	65.58	35.4
3120	WIMAL-3	33.000	50.7	32.7	5.46	4.37	46.332	29.9
3520	NUWAR-3	33.000	36.6	16.7	4.41	3.53	33.072	15.1
3640	DENIY-3	33.000	33.4	24.6	6.35	5.08	28.32	20.9
3740	RATNAP-3	33.000	21	13	15.08	12.06	8.936	5.5
3510	SITHA-33	33.000	32.6	16.7	7.43	5.94	26.656	13.7
3630	BALAN-3	33.000	28.5	16.2	27.5	22.00	6.5	3.7
					75.88	60.70		

60% Operation for Thirmal Maximum

			Pre P	Pre Q	Mini P	Mini P (60%)	Estimated P	Estimated Q
3770	KIRIB-3	33.000	73.3	39.6	9.65	5.79	67.51	36.5
3120	WIMAL-3	33.000	50.7	32.7	5.46	3.28	47.424	30.6
3520	NUWAR-3	33.000	36.6	16.7	4.41	2.65	33.954	15.5
3640	DENIY-3	33.000	33.4	24.6	6.35	3.81	29.59	21.8
3740	RATNAP-3	33.000	21	13	15.08	9.05	11.952	7.4
3510	SITHA-33	33.000	32.6	16.7	7.43	4.46	28.142	14.4
3630	BALAN-3	33.000	28.5	16.2	27.5	16.50	12	6.8
					75.88	45.53		

Day Peak Case

80% Operation for Hydro_Maximum

			Pre P	Pre Q	Mini P	Mini P (80%)	Estimated P	Estimated Q
3770	KIRIB-3	33.000	36.6	19.8	9.65	7.72	28.88	15.6
3120	WIMAL-3	33.000	25.3	16.4	5.46	4.37	20.932	13.6
3520	NUWAR-3	33.000	18.3	8.3	4.41	3.53	14.772	6.7
3640	DENIY-3	33.000	17.7	11.9	6.35	5.08	12.62	8.5
3740	RATNAP-3	33.000	10.5	6.5	15.08	12.06	-1.564	-1.0
3510	SITHA-33	33.000	23.8	12.2	7.43	5.94	17.856	9.2
3630	BALAN-3	33.000	14.3	8.1	27.5	22.00	-7.7	-4.4
					75.88	60.70		

60% Operation for Thirmal Maximum

			Pre P	Pre Q	Mini P	Mini P (60%)	Estimated P	Estimated Q
3770	KIRIB-3	33.000	36.6	19.8	9.65	5.79	30.81	16.7
3120	WIMAL-3	33.000	25.3	16.4	5.46	3.28	22.024	14.3
3520	NUWAR-3	33.000	18.3	8.3	4.41	2.65	15.654	7.1
3640	DENIY-3	33.000	17.7	11.9	6.35	3.81	13.89	9.3
3740	RATNAP-3	33.000	10.5	6.5	15.08	9.05	1.452	0.9
3510	SITHA-33	33.000	23.8	12.2	7.43	4.46	19.342	9.9
3630	BALAN-3	33.000	14.3	8.1	27.5	16.50	-2.2	-1.2
					75.88	45.53		

高調波・電圧変動問題対策（CEBへ2次調査時に報告）

I. スリランカにおける小水力連系現状および問題

スリランカでは CEB への電力売電契約を結び系統へ接続している小水力 IPP が 2005 年 2 月現在 41 件存在している。その大半が Nuwala Eliya, Wimalasurendra, Balangoda といった中部の水力地点に集中しており、規模としては、0.07MW 程度から最大で 9.9MW であり、総計で 75.63MW である。またこれらの IPP はすべて 33kV 配電系統に接続されている。近年、こうした IPP が系統連系時また、系統離脱時において高調波・電圧低下の問題が発生している。

II. 小水力連系における問題

- CEB と小水力 IPP の間には電力規模についての契約はあるが、系統に連系する発電設備として具備すべき必要技術・制約等に関して取り決めがない。
- 系統への接続・離脱等を IPP 独自の意志で好きな時に行っている。なおその際 CEB への連絡がない。
- CEB の電力系統において SCADA が導入されている変電所は 70 のうち僅かに 17 である。さらに、IPP へも SCADA を導入したい意向はあるが、資金面の問題で進捗しておらず、IPP の発電状況連系状況等が把握しきれていない。

III. 制度面での対策

日本では、発電設備を商用電力系統に連系することを可能とするために必要となる技術要件が、分散型電源系統連系技術指針（JEAG 9701 (2001)）に取り纏められており、中部電力をはじめ日本のほとんどの電気事業者がこれに準じている。基本的に連系することによって生じる恐れのある高調波・電圧低下等の問題は、連系する IPP 側の問題として明示しており、こうした問題が発生しないよう IPP 側で対処していただくように指導している。

スリランカにおいても、早急に CEB として商用電力系統に連系する IPP に対して要求する技術的要件をまとめ、IPP と需給契約を結ぶ際確認すべきである。

以下に参考となるべく日本における、分散型電源系統連系技術指針について記載する。

1 背景・目的

小水力発電・ゴミ消却発電・燃料電池・太陽光発電等の分散型電源は、平成 7 年 10 月の電気事業法改正により、一般電気事業者の入札制度の創設、発電部門の自由化が実現したことから、電気事業に参入する事業者が増えるに伴い増加傾向にある。こうした発電設備が系統連系することにより、系統における電力品質・保守運用面での影響が懸念されるようになった。また系統を介して他の需要家へ影響を与えることがないように、系統へ連系する際は、系統連系に関わる情報の透明性および公平性が確保される必要があることが確認された。このため系統連系に必要な技術要件が本ガイドラインにとりまとめられている。

2 制約事項

2.1 高調波制約事項（全電圧階級）

電気共同研究会報告（第46巻第2号 電力系統における高調波とその対策）を参考として、**高調波流出電流を総合電流歪み率5%、各次電流歪み率3%以下**とすることが望ましい。

2.2 電圧フリッカ制約事項（全電圧階級）

電圧フリッカの対策要否判定基準は以下のとおり、

ΔV_{10} (発電設備設置者受電点における発電設備による単独の電圧フリッカ値) $\leq 0.23V$

風力発電設備の電圧フリッカとしては、風速の変化により並解列を繰り返し、突入電流等により電圧変動を生じる場合と風速の変化による出力変動により出力変動により生じる場合とがある。

2.2.1 頻繁な並解列による電圧フリッカによる電圧フリッカ

電圧フリッカは電圧変動値と変動頻度に左右されることから電圧変動値を抑制するか又は並解列頻度を低減する対策が必要。

電圧変動抑制対策としては、

- ▶ SVC（静止型無効電力補償装置）による無効電力の補償
 - ▶ サイリスタ等によるソフトスタートの採用
 - ▶ 配電線の太線化等による系統インピーダンスの採用
- 等があり、また並解列頻度低減対策としては、
- ▶ 並解列条件を瞬時風速から一定時間平均風速への変更
- 等がある。

2.2.2 出力変動による電圧フリッカ

この出力変動抑制対策としては、

- ▶ SVC（静止型無効電力補償装置）による無効電力の補償
 - ▶ 配電線の太線化等による系統インピーダンスの採用
- 等がある。

2.3 電圧変動制約事項(特別高圧：22kV以上)

2.3.1 発電設備の連系により、系統の電圧が適正值（**常時電圧の概ね1～2%以内**）を逸脱する恐れがあるときは、発電設備の設置者において自動的に電圧を調整するものとする。

2.3.2 同期発電機を用いる場合には、制動巻線付きのもの（制動巻線を有しているものと同等以上の乱調防止効果を有する制動巻線付きでない同期発電機を含む）とするとともに、自動同期検定装置を設置するものとする。誘導電動機を用いる場合であって、並列時の瞬時電圧低下により系統の電圧が適正值（**常時電圧の2%**を目安）を逸脱する恐れがあるときは、発電設備の設置者において源流リアクトル等を設置するものとする。なおこれにより対応できない場合は同期発電機を用いるものとする。

2.3.3 自励式の逆変換装置を用いる場合には、自動的に同期がとれる機能を有するもの

を用いるものとする。また他励式の逆変換装置を用いる場合であって、並列時の瞬時電圧低下により系統電圧が適正值（**常時電圧の2%**を目安）を逸脱する恐れがあるときは、発電設備の設置者において源流リアクトル等を設置するものとする。なおこれにより対応できない場合には自励式の逆変換装置を用いるものとする。

2.4 電圧変動制約事項(高圧：6.6kV以下)

2.4.1 一般配電線との連系であって、発電設備の脱落等により低圧需要家の電圧が適正值（ $101\pm 6V$ 、 $202\pm 20V$ ）を逸脱する恐れがある時には、発電設備の設置者において自動的に負荷を制限する対策を行うものとする。なお、これにより対応できない場合には配電線の増強を行うか、専用線による連系とするものとする。

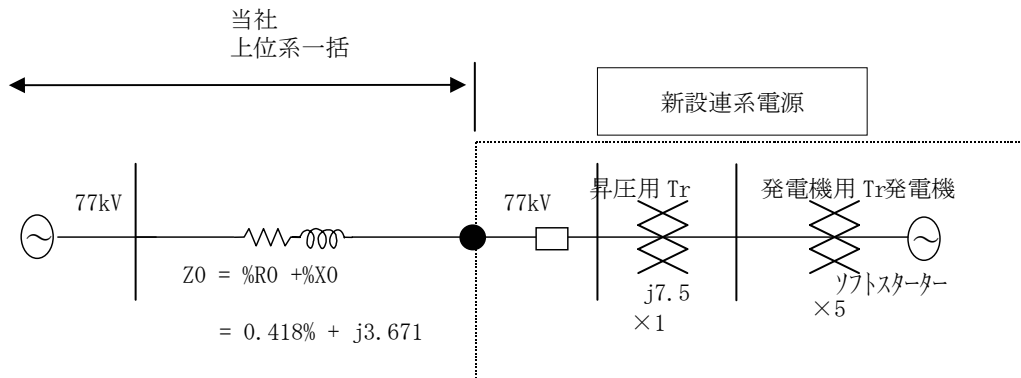
2.4.2 発電設備からの逆潮流により低圧需要家の電圧が適正值（ $101\pm 6V$ 、 $202\pm 20V$ ）を逸脱する恐れがある時には、発電設備の設置者において自動的に電圧を調整する対策を行うものとする。なお、これにより対応できない場合には配電線の増強を行うか、専用線による連系とするものとする。

2.4.3 同期発電機を用いる場合には、制動巻線付きのもの（制動巻線を有しているものと同等以上の乱調防止効果を有する制動巻線付きでない同期発電機を含む）とするとともに、自動同期検定装置を設置するものとする。誘導電動機を用いる場合であって、並列時の瞬時電圧低下により系統の電圧が適正值（**常時電圧の10%以内**）を逸脱する恐れがあるときは、発電設備の設置者において源流リアクトルや起動補償用コンデンサの設置、ソフトスターター機能付き発電機を設置するものとする。なおこれにより対応できない場合は同期発電機を用いるものとする。

2.4.4 自励式の逆変換装置を用いる場合には、自動的に同期がとれる機能を有するものを用いるものとする。また他励式の逆変換装置を用いる場合であって、並列時の瞬時電圧低下により系統電圧が適正值（**常時電圧の10%以内**）を逸脱する恐れがあるときは、発電設備の設置者において源流リアクトル等を設置するものとする。なおこれにより対応できない場合には自励式の逆変換装置を用いるものとする。

IV. 電圧変動対策検討（中部電力における実例）

1 供給概要



Step-up Transformers

定格容量	1,800kVA
リアクタンス	5.5%(自己容量ベース) 30.555%(10MVAベース)
台数	5台

Generators

種類	誘導機
定格容量	1,808kVA
定格出力	1,650kW
リアクタンス	17.6%(自己容量ベース) 97.245%(10MVAベース)
台数	5台

2 現システムでの検討結果

2.1 系統連系時の電圧変動検討

77kV 系統であるため、2%以下とする。しかしながら本ケースでは、ソフトスターター採用のため問題なし。参考値である。

$$\Delta V = \sqrt{\frac{R0^2 + X0^2}{R0^2 + (X0 + Xt + XG)^2}} \times 100$$

$$2.73\% = \sqrt{\frac{0.418^2 + 3.671^2}{0.418^2 + (3.671 + 7.5 + 30.555 + 97.245)^2}}$$

2.2 系統脱落時の電圧変動検討

$$\Delta V = \%R0 \times P(p.u) + \%X0 \times Q(p.u)$$

$$\pm 2 \geq 0.418 \times \frac{8.3}{10} + 3.671 \times \frac{Q}{10}$$

$$901k \text{ var} \leq Q \leq -1,277k \text{ var}$$

運転力率許容範囲

遅れ 87.8%～進み 79.1%で運用する必要がある。これを満たせない場合は力率改善コンデンサを投入するか、指定力率で運転可能な自動力率調整装置を設置する必要がある。

V. 高調波抑制対策

ここでは高調波抑制として有益で実際に採用されている対策について列記する。

1.1 電力変換器のパルス数を増加して低次高調波電流を抑制

1.1.1 多パルス化

電力変換器のパルス数を増加して低次高調波電流を抑制する方法である。低次高調波電流を抑制することは高調波を抑えることになる。ここで電力変換装置のパルス数と高調波電流の次数との関係は以下の通りとなる。

発生する高調波電流の次数 $n = k \times P \pm 1$

k : 1,2,3....

P : パルス数

このように、例えば 1 2 パルスの電力変換器の場合、理論的には 5 次及び 7 次の高調波電流を発生しないため（実際は回路の不均衡などにより若干の 5 次、7 次の高調波電流を発生する）、1 2 パルスの変換器を採用することは高調波抑制対策として大変効果的である。

1.2 高調波電流吸収

高調波電流を吸収して抑制する方法である。

1.2.1 受動フィルター

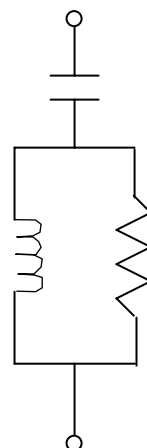
コンデンサ、リアクトルといった受動（Passive）素子を組み合わせることで特定の周波数あるいは周波数領域で低インピーダンスとなる分路を構成し、高調波電流を吸収するものである。受動フィルターには（単一）同調フィルターと高次フィルターの 2 種類がある。

同調フィルターとは、一つの高調波次数に共振した L-C-R 直列回路で構成され、同調周波数で低抵抗となり効果を発揮する。先鋭度・共振の鋭さである Q を大きくすることで更に効果を高めることができるが、逆に同調ずれが起りやすくなったり、フィルター過負荷を生じたりする可能性が高まる。

高次フィルターは広い周波数範囲で低抵抗となるので、高調波発生量の多い低次高調波を対象とした各次数の同調フィルターと組み合わせ高次高調波全体の吸収を分担するように構成される。



同調フィルター



高次フィルター

1.2.2 力率改善コンデンサ(需要家)

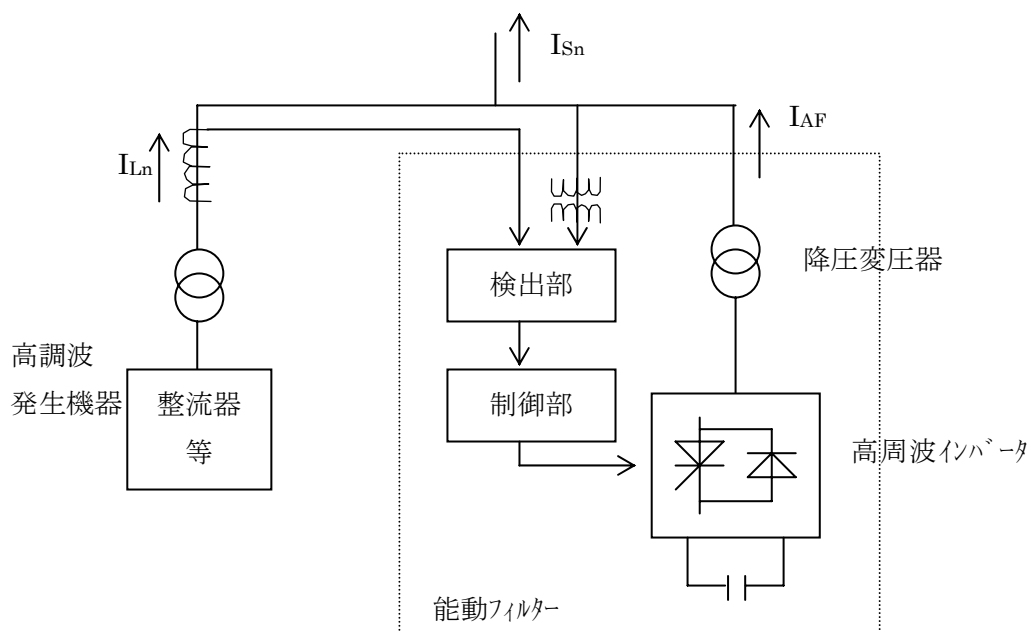
6%の直列リアクトル付き力率改善用コンデンサーは、高調波を吸収する効果があり、特に受電変圧器の抵圧側に設置すれば受電変圧器の漏れインダクタンスの大きさによっても異なるものの、第5高調波に対しては30～50%の流出電流を低減することができる。

1.3 高調波電流のキャンセル

高調波電流をキャンセルして抑制する方法である。

1.3.1 能動フィルター

発生する高調波電流を検出し、それを打ち消す極性の電流を能動的に(Active)に発生するものである。能動フィルターは下図のとおり、高周波インバータ、連系用変圧器、高周波検出部、電流制御部などからの基本構成されている。



1.3.2 Δ-Δ、Δ-Y巻線変圧器

一般に整流器などの電力変換装置には専用の変圧器が用いられる。三相変圧器の一次側と二次側巻線の結線方法にはΔ-Δ、Δ-Y、Y-Y、Y-Δの4方式がある。ここで同一母線に接続されたΔ-Δ、Δ-Y結線の2変圧器を組み合わせた方式により、一次側に流れる5, 7次高調波電流はお互いに180°の位相差となりキャンセルすることで高調波電流を低減できる。

Affect to the Main Grid by Wind-Power Interconnection

Base Data: 2005 Thermal Maximum Case (New Demand and Generators are considered)

N-1 Study		Frequency Drop Analysis
<p>Single Line Diagram</p>		
Result (Day)	Marginal Volume (MW)	Bottle Neck
N-1	<p>55MW (Puttalam - Madam_T - Bolaw_T - Kotugoda) 1cct is outage</p>	<p>Puttalam - Madam_T - Bolaw_T - Kotugoda</p>
Result (Night)	Marginal Volume (MW)	Bottle Neck
N-1	<p>210MW In case that (Puttalam - Madam_T - Bolaw_T - Kotugoda) 1cct is outage</p>	<p>Puttalam - Madam_T - Bolaw_T - Kotugoda</p>
Summary	Marginal Volume (MW)	Causes
Day	55MW	N-1 Problem
Night	100MW	Frequency Drop Problem
Off Peak	41MW	Frequency Drop Problem
Remarks		

$$dF = 1/4.75 \times 100 \times (55 / 1200) = 0.96$$

49.04Hz > 48.75 Hz → No Load Shedding

49.04Hz < 49.5Hz (Grid Code) → However, It can recover to the acceptable range after governor operating

$$dF = 1/4.75 \times 100 \times (210 / 1700) = 2.60$$

47.46Hz < 48.75 Hz → Load Shedding

$$dF = 1/4.75 \times 100 \times (100 / 1700) = 1.24$$

48.76Hz > 48.75 Hz → No Load Shedding

100MW is the marginal from the view point of no load shedding

During Off Peak

Demand is 62% of Day Peak (Daily load curve as of Sep in 2004)

$$dF = 1/4.75 \times 100 \times (41 / 700) = 1.23$$

48.77Hz > 48.75 Hz → No Load Shedding

41MW is the marginal from the view point of no load shedding

Result on Transmission Loss Reduction

Year	Power Flow (MW)	Zebra 4			Zebra LL 4			Parrrot 4			Remarks	
		Zebra_4 TL Cost (M US\$)	TL Loss (M US\$)	TL Incremental Cost	Reduced TL Loss (M US\$)	Total (M US\$)	P.V (M US\$)	TL Incremental Cost	Reduced TL Loss (M US\$)	Total (M US\$)		P.V (M US\$)
0 2011	600	19.712	2.523	-10.157	0.757	-9.400	-9.400	-7.901	1.211	-6.690	-6.690	Present Year
1 2012	600		2.523		0.757	0.757	0.688		1.211	1.211	1.101	
2 2013	600		2.523		0.757	0.757	0.626		1.211	1.211	1.001	
3 2014	600		2.523		0.757	0.757	0.569		1.211	1.211	0.910	
4 2015	600		2.523		0.757	0.757	0.517		1.211	1.211	0.827	
5 2016	600		2.523		0.757	0.757	0.470		1.211	1.211	0.752	
6 2017	600		2.523		0.757	0.757	0.427		1.211	1.211	0.684	
7 2018	600		2.523		0.757	0.757	0.388		1.211	1.211	0.621	
8 2019	600		2.523		0.757	0.757	0.353		1.211	1.211	0.565	
9 2020	900		1.388		0.404	0.404	0.171		0.656	0.656	0.278	2 route
10 2021	900		1.388		0.404	0.404	0.156		0.656	0.656	0.253	Break Even Point for Parrrot
11 2022	900		1.388		0.404	0.404	0.141		0.656	0.656	0.230	
12 2023	900		1.388		0.404	0.404	0.129		0.656	0.656	0.209	
13 2024	900		1.388		0.404	0.404	0.117		0.656	0.656	0.190	
14 2025	900		1.362		0.404	0.404	0.106		0.656	0.656	0.173	
15 2026	900		1.362		0.404	0.404	0.097		0.656	0.656	0.157	
16 2027	900		1.362		0.404	0.404	0.088		0.656	0.656	0.143	
17 2028	900		1.362		0.404	0.404	0.080		0.656	0.656	0.130	
18 2029	900		1.362		0.404	0.404	0.073		0.656	0.656	0.118	
19 2030	900		1.362		0.404	0.404	0.066		0.656	0.656	0.107	
20 2031	900		1.362		0.404	0.404	0.060		0.656	0.656	0.098	
Total Present Value											-4.079	1.855

Conversion Rate

10.74 USD/1000LKR

Source: LTGEP2003, 01st January 2002

Discount Rate =

10%

Source: LTGEP2003

Operation Cost

0.0000576 M US\$/MWh

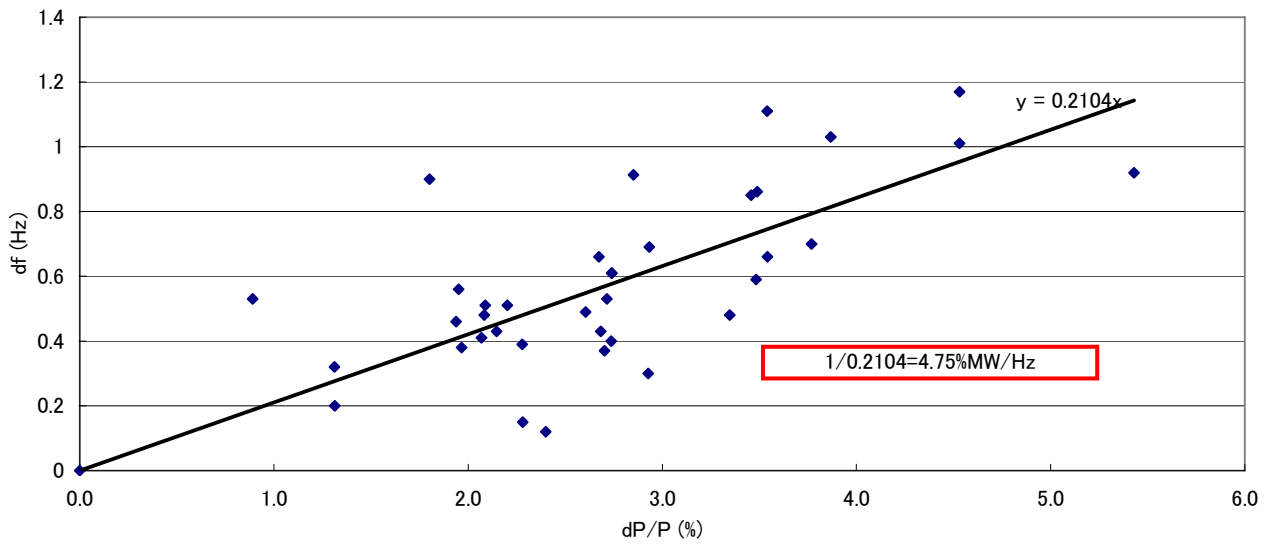
CEB Average Generation Cost Including Fuel and O/M Cost

Puttalam - Chilaw: 70km

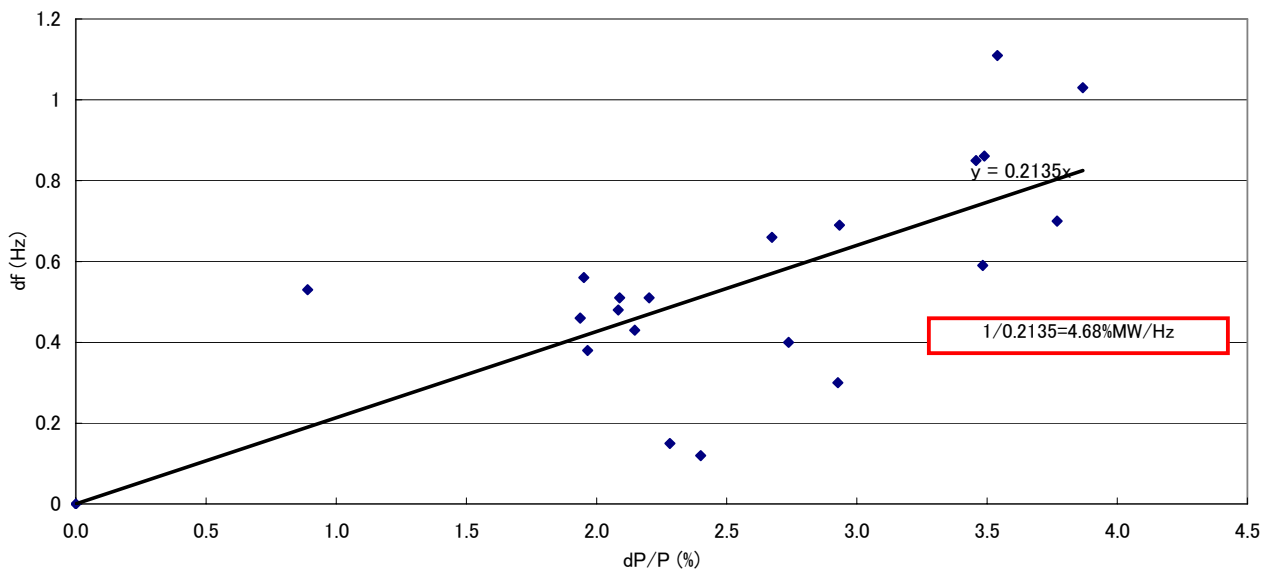
	Total	Only Conductor
Zebra 4 2cct	1835.4 MLKR	1.52MLKR/km
Parrrot 4 2cct	2571.1 MLKR	2.89MLKR/km
Zebra LL_4 2cct	2781.1 MLKR	3.265MLKR/km

Tower size is the same as that of the Zebra_4

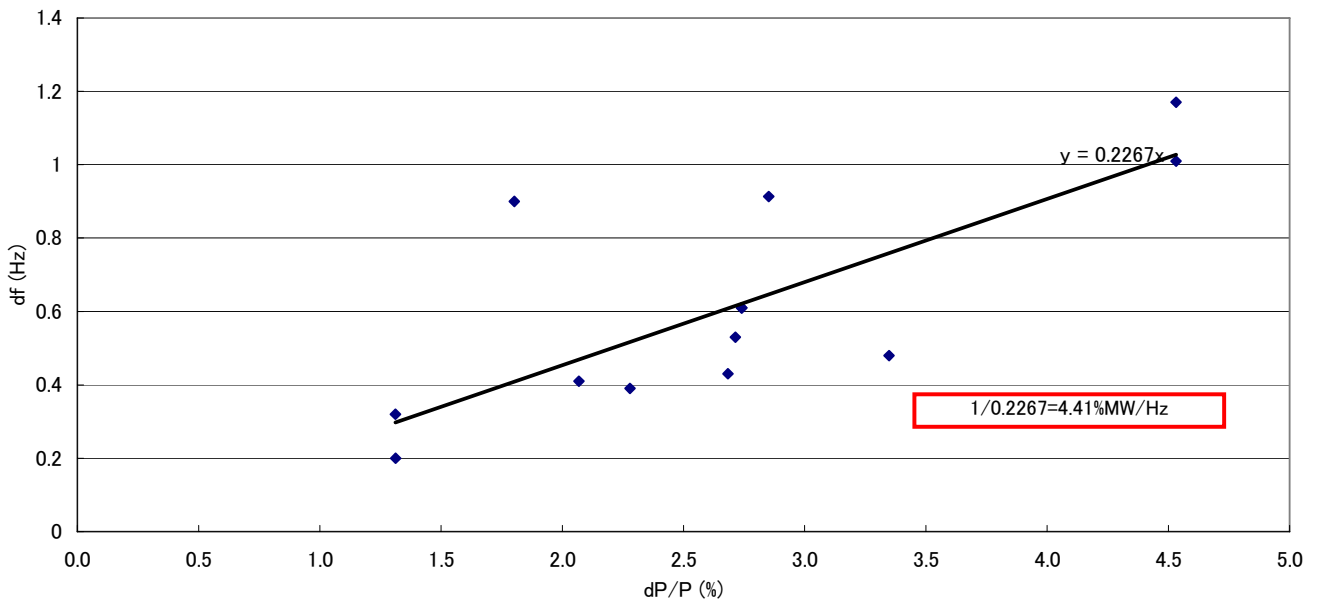
System Frequency Characteristic Constant (Whole Day)



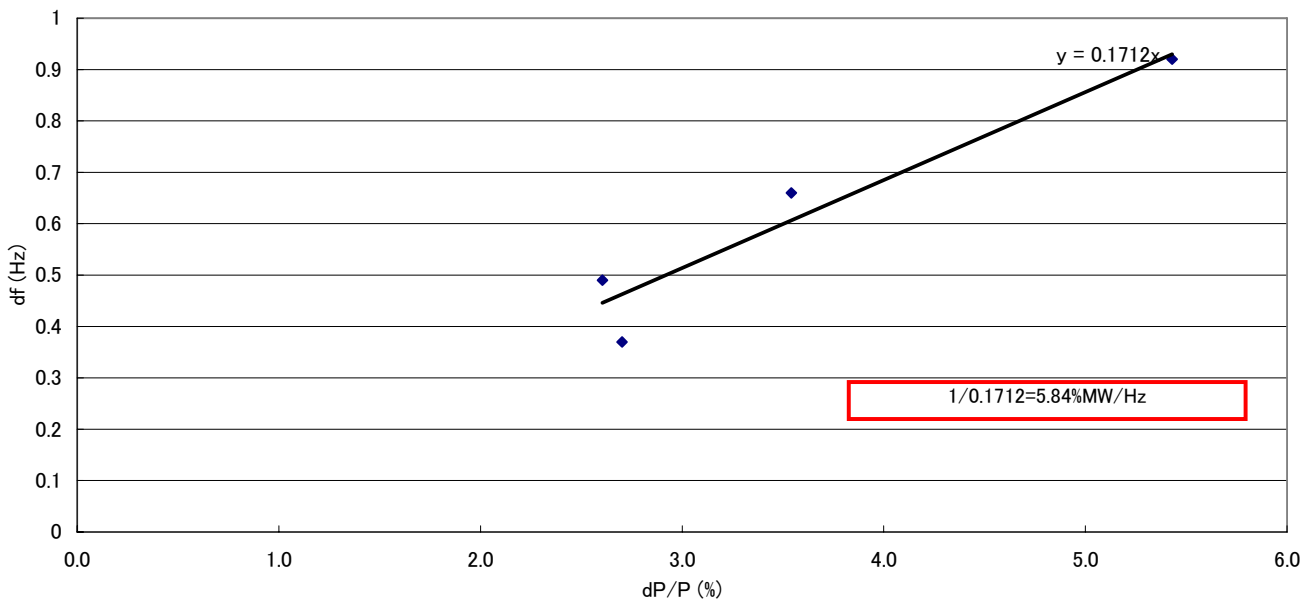
System Frequency Characteristic Constant (Day Peak)



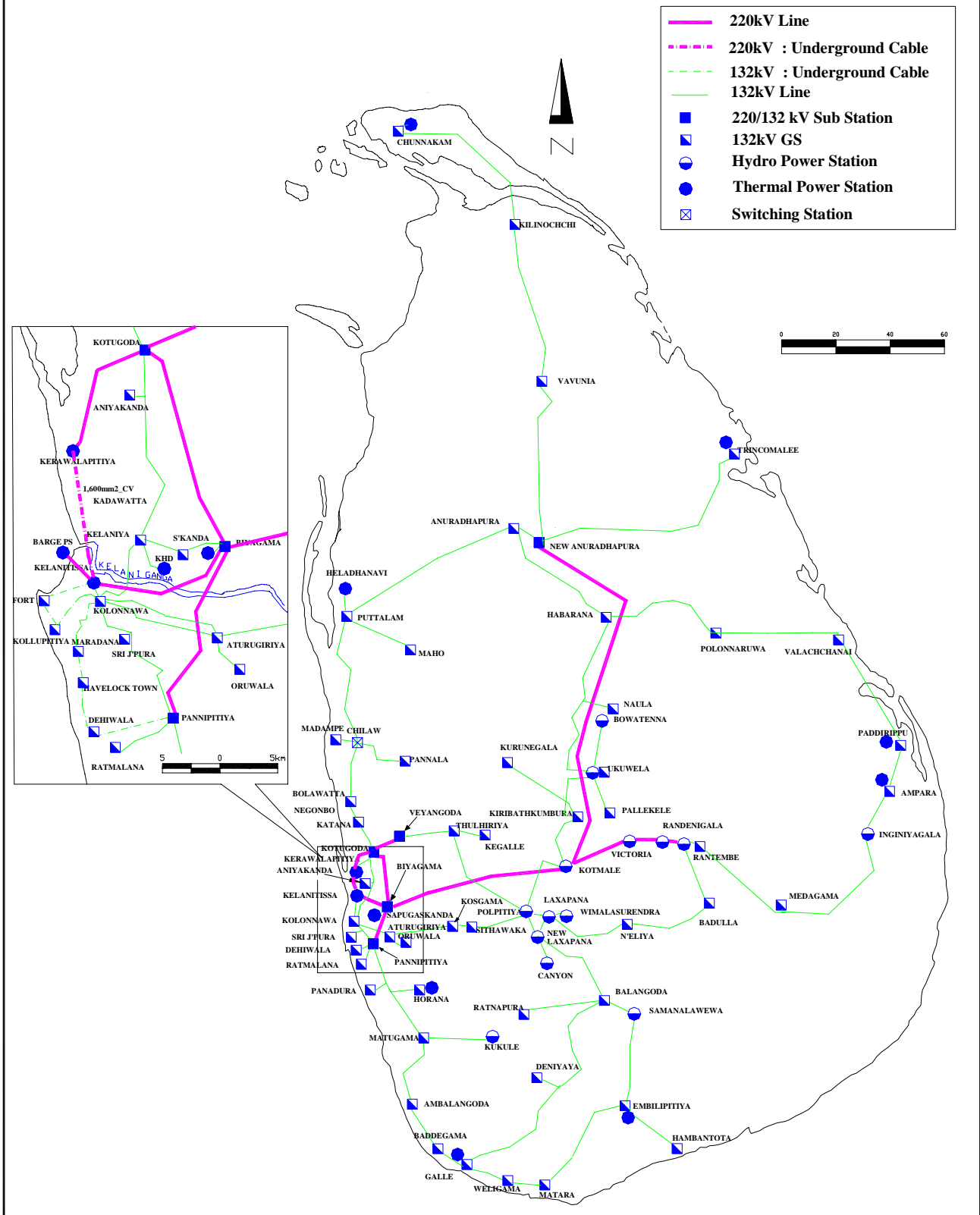
System Frequency Characteristic Constant (Night Peak)



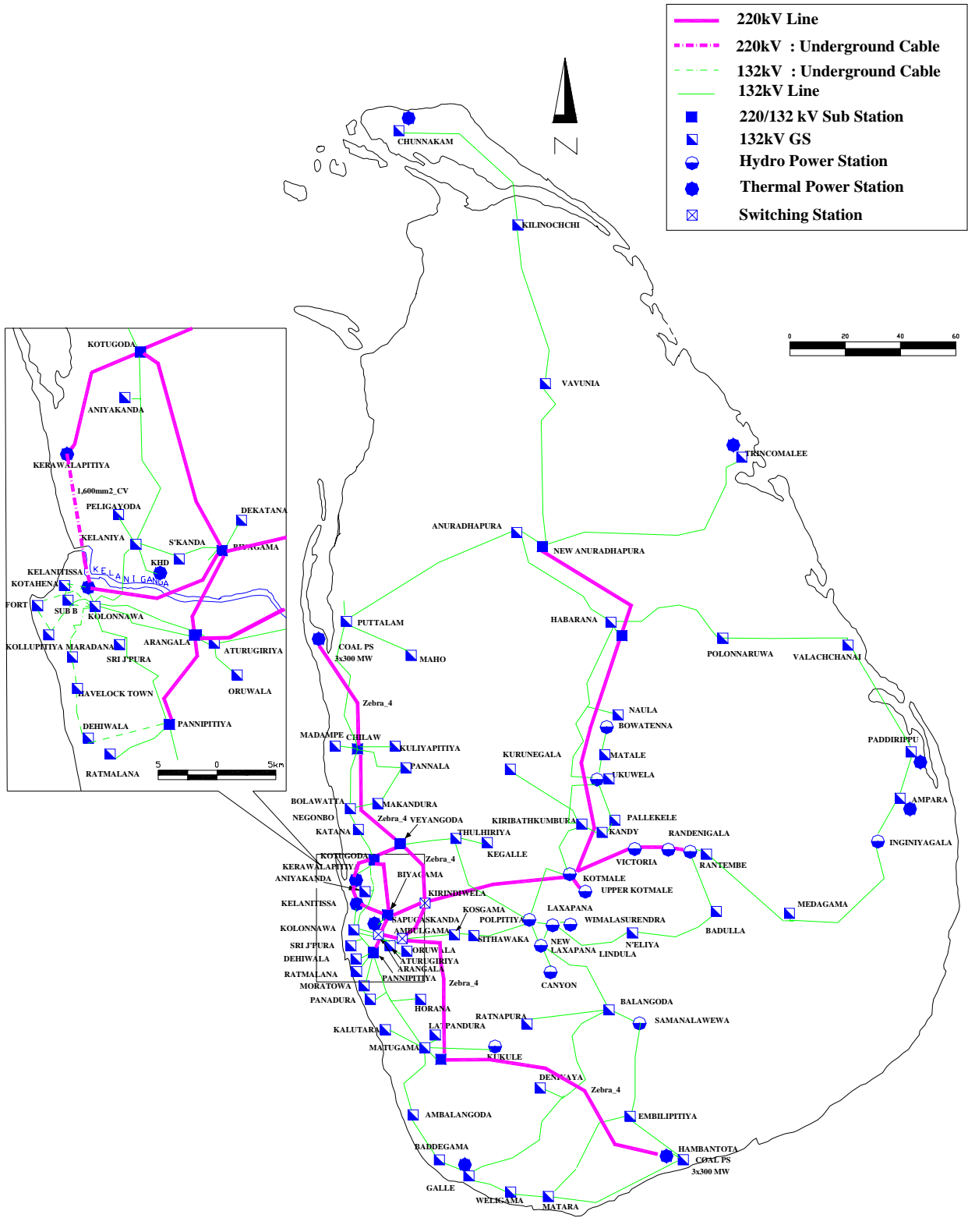
System Frequency Characteristic Constant (Off Peak)



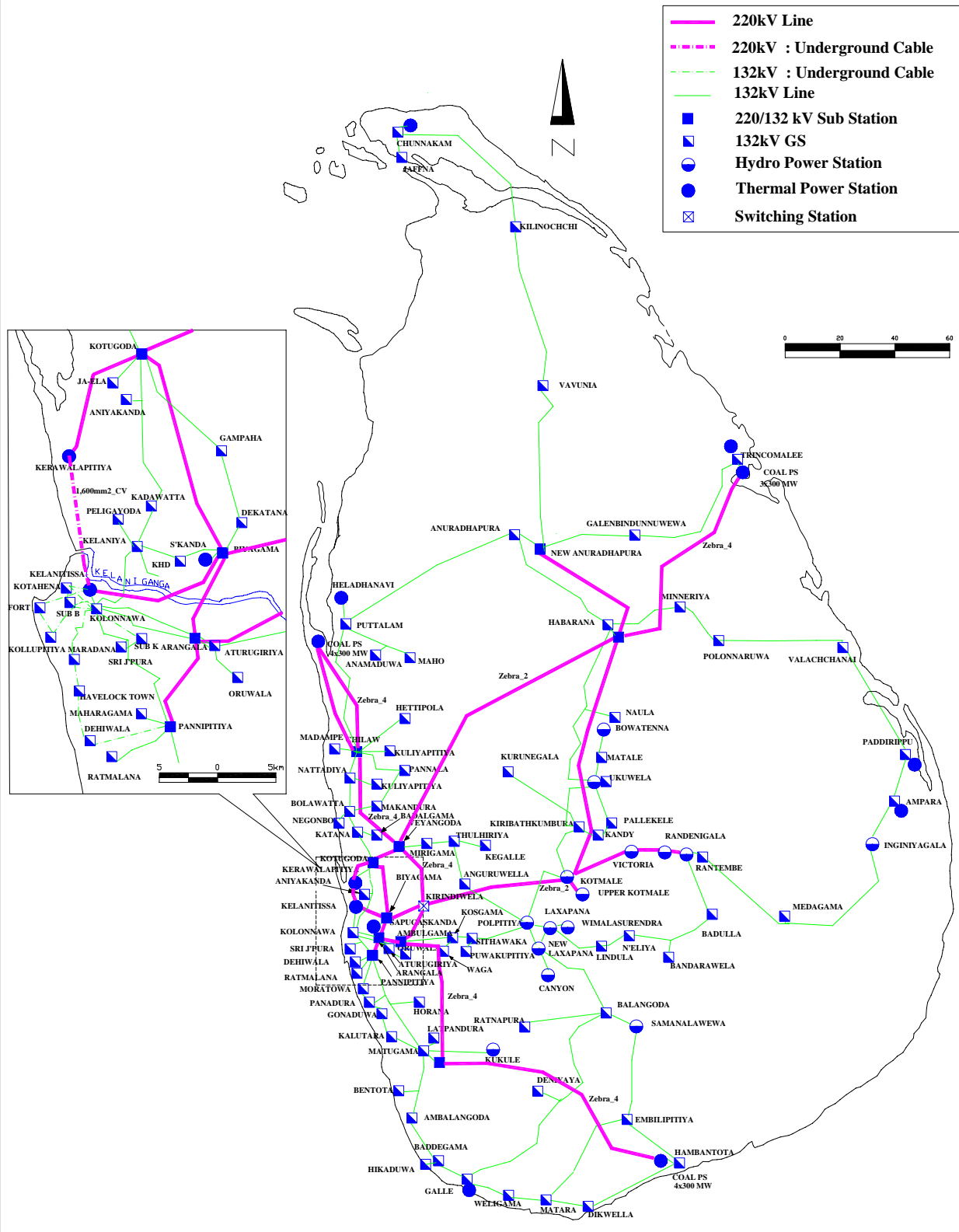
The Map of Sri Lanka Transmission System in Year 2010



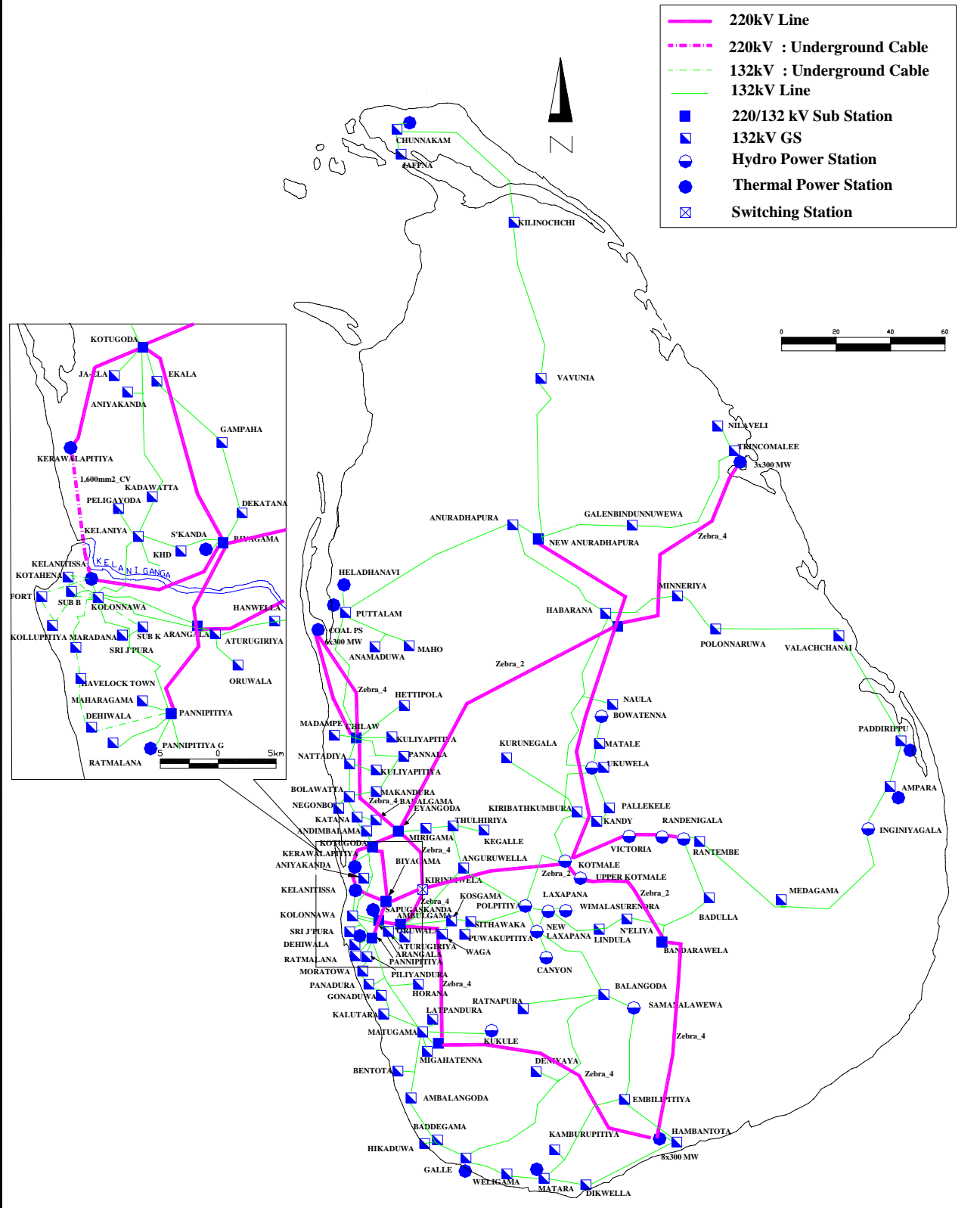
The Map of Sri Lanka Transmission System in Year 2015

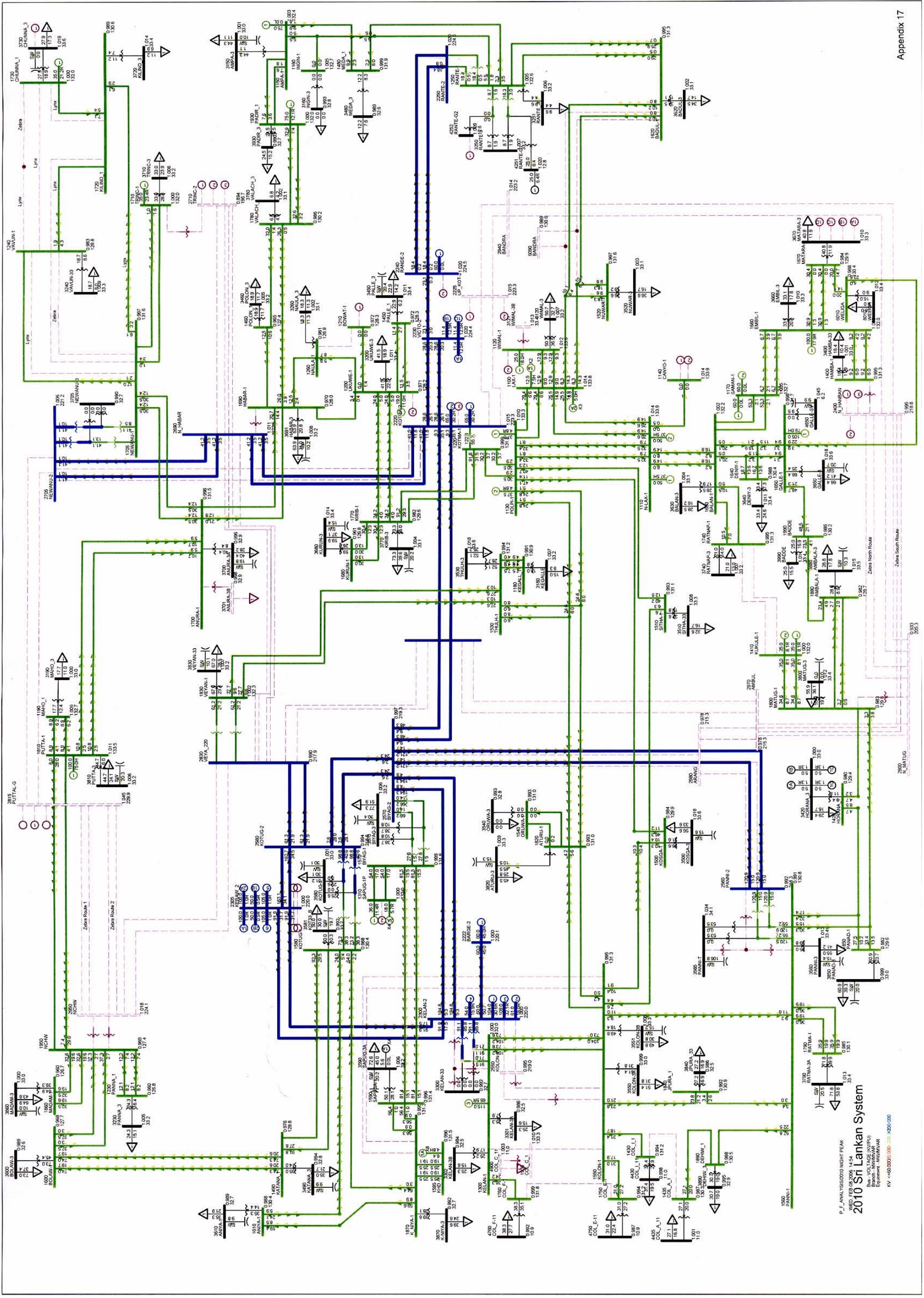


The Map of Sri Lanka Transmission System in Year 2020



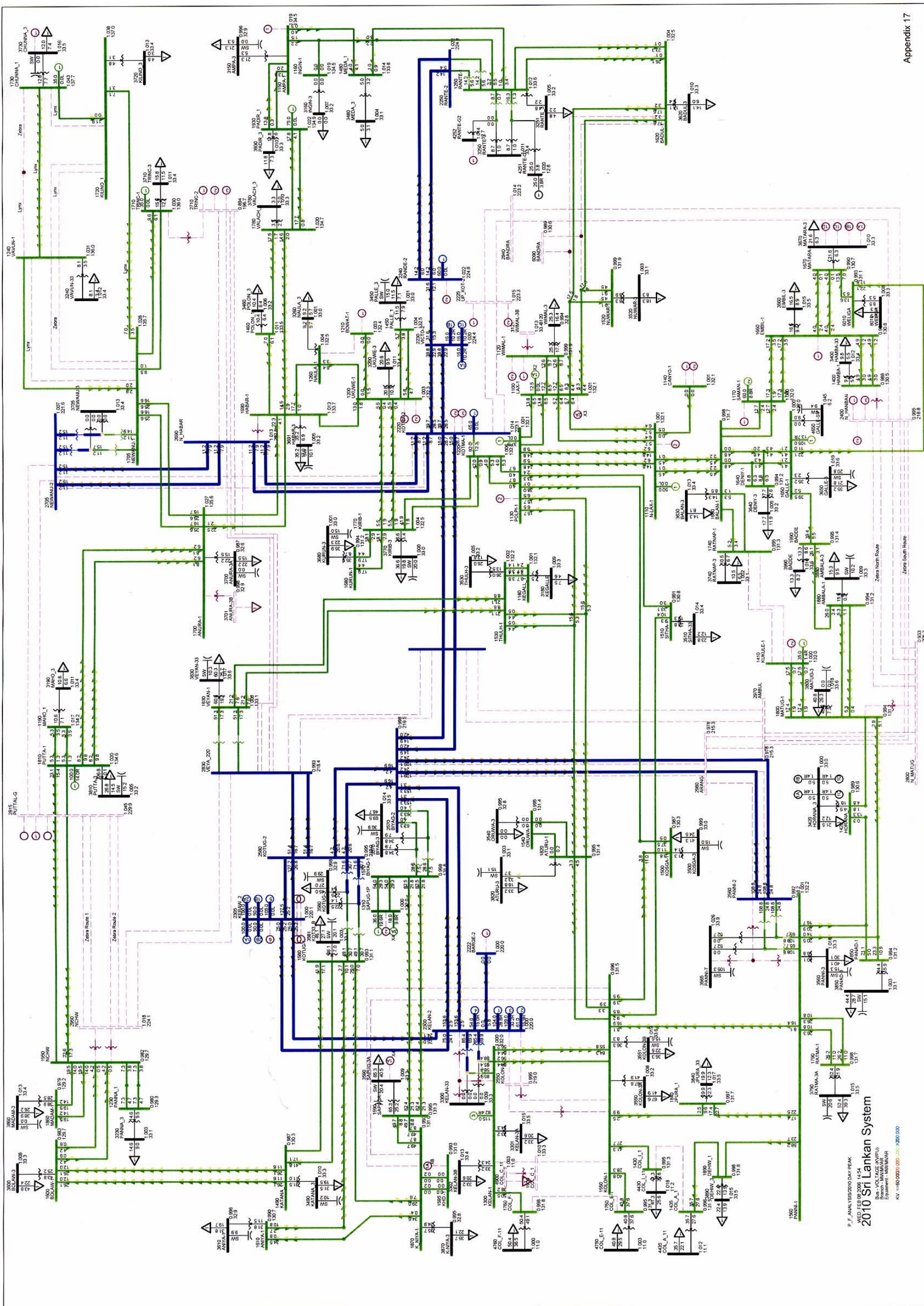
The Map of Sri Lanka Transmission System in Year 2025

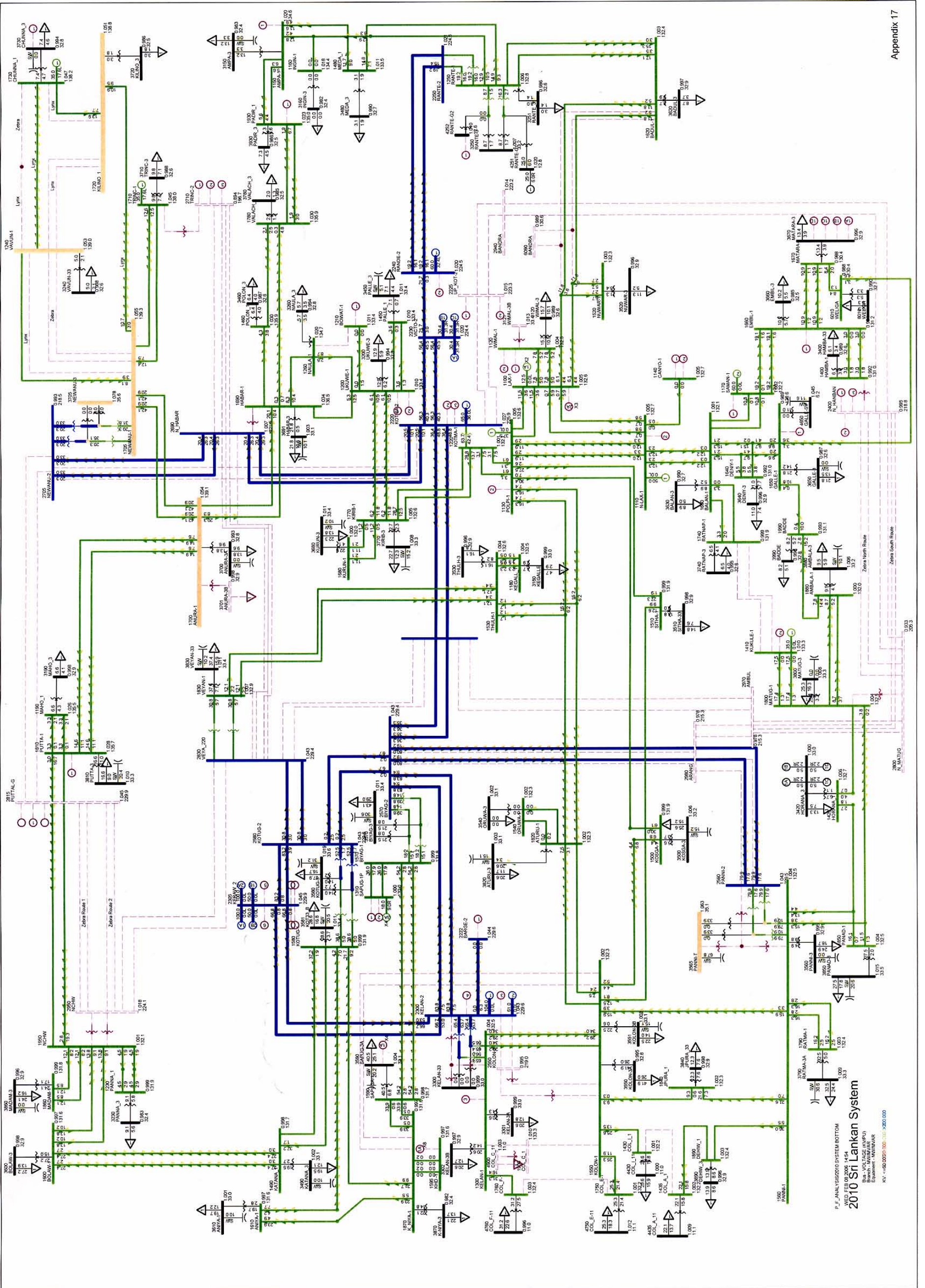




P.F. ANALYSIS@2010 NIGHT PEAK
WED, FEB 03, 2006 14:54
Bus VOLTAGE (KV/PU)
Element: WPT/RELAY/BRK
KV: 480.000/1000.000/250.000

2010 Sri Lankan System





P.F. ANALYSIS SYSTEM BOTTOM
WED FEB 09 2008 14:54
2010 Sri Lankan System
Branch: MW/MAR (P)
Equipment: MW/MAR
KV: 60000-330-230-000

N-1 Checking based on 2010_Night_Peak

1. Branches and Tie Lines

Monitored Elements	Base Flow	Maximum Flow	Impact Rate	%	Contingency	Countermeasures
Nothing						

2. Voltage
220kV

Bus	Voltage	Contingency	Countermeasures
Nothing			

132kV

Bus	Voltage	Contingency	Countermeasures
Nothing			

N-1 Checking based on 2010_Day_Peak

1. Branches and Tie Lines

Monitored Elements	Base Flow	Maximum Flow	Impact Rate	%	Contingency	Countermeasures
Nothing						

2. Voltage
220kV

Bus	Voltage	Contingency	Countermeasures
Nothing			

132kV

Bus	Voltage	Contingency	Countermeasures
Nothing			