

Figure 3.2.10 Slope > 20 Degree Area

Source: The JICA Study Team

DISTRITO CAPITAL CUADRO Nº 1: TOTAL DE VIVIENDAS POR CONDICIÓN DE OCUPACIÓN Y NÚMERO DE OCUPANTES, SEGÚN CLASE Y TIPO DE VIVIENDA CENSO 2001

01 - 0 5			(CONDICIÓN D	E OCUPACIÓN		
CLASE Y	TOTAL		OCUPADA				
TIPO DE VIVIENDA		N° DE VIVIENDAS	N° DE OCUPANTES	OCUPANTES POR VIVIENDA	DESCCUPADA	USO OCASIONAL	EN CONSTRUCCIÓN
TOTAL	491590	446226	1836286	4,1	28926	10603	5835
FAMILIARES	488827	443463	1808982 50383	4,1	28926 638	10603	5835 293
CASA	226772	209610	939113	4,5	11148	2842	3172
APARTAMENTO EN EDIFICIO	217608	193565	700546	3,6	15576	6225	2242
CASAQUINTA O CASA	13029	11947	46101	3,9	762	192	128
CASA DE VECINDAD	39	39	799	20,5	-	-	-
RANCHO	16501	15496	69697	4,5	802	203	-
OTRA CLASE 2/	687	687	2343	3,4	-	-	-

			C	ONDICIÓN DI	E OCUPACIÓN		
CLASE Y	TOTAL		OCUPADA				
TIPO DE VIVIENDA		N° DE VIVIENDAS	N° DE OCUPANTES	OCUPANTES POR VIVIENDA	DESOCUPADA	USO OCASIONAL	EN CONSTRUCCIÓN
Municipio SUCRE	153424	134346	546766	4,1	12217	3248	3613
FAMILIARES	153285	134207	545339	4,1	12217	3248	3613
OUINTA O CASAOUINTA 1/	10906	9266	38641	4,2	550	579	511
CASA	74663	68033	302620	4,4	4592	514	1524
APARTAMENTO EN EDIFICIO	55678	45786	157288	3,4	6353	2001	1538
CASAQUINTA O CASA	5196	4811	18749	3,9	280	65	40
CASA DE VECINDAD	13	13	285	21,9	-	-	-
RANCHO	6597	6066	27010	4,5	442	89	-
OTRA CLASE 2/	232	232	746	3,2	-	-	-
COLECTIVAS	139	139	1427	10,3	-	-	-
1/ INCLUYE LAS VIVIENDAS CLASIFICAD	AS COMO MAN	ISIÓN				-	r
Municipio CHACAO	27191	20099	64629	3,2	4388	1587	1117
FAMILIARES	27090	19998	63693	3,2	4388	1587	1117
OUINTA O CASAOUINTA 1/	2353	1899	8148	4,3	221	99	134
CASA	1686	1268	6249	4,9	380	18	20
APARTAMENTO EN EDIFICIO	22638	16504	48219	2,9	3714	1459	961
CASAQUINTA O CASA	367	281	932	3,3	73	11	2
CASA DE VECINDAD	-	-	-	-	-		-
RANCHO	9	9	39	4,3	-		-
OTRA CLASE 2/	37	37	106	2,9	-	-	-
COLECTIVAS	101	101	936	9,3	-	-	-

1/ INCLUYE LAS VIVIENDAS CLASIFICADAS COMO MANSIÓN

Source: Census 2001, INA

Figure 3.2.11	Census	Data of	Person /	Family
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Figure 3.2.12 The Damage Function for Damage Level 4 / EMS-98

	Type of Structure	Vı A	ılne B	rab: C	ility D	Cla E	ass F
	rubble stone, fieldstone	0					
	adobe (earth brick)	Ó	H				
4RY	simple stone	 -	0				
4SO1	massive stone		⊢	О	1		
M	unreinforced, with manufactured stone units	┢┅	0	1			
	unreinforced, with RC floors		╞┝	О			
	reinforced or confined			╞	О	H	
: (RC)	frame without earthquake-resistant design (ERD)	ŀ		0	1		
RETE	frame with moderate level of ERD		╞		ю	Η	
CONCE	frame with high level of ERD			ŀ		O	-1
ED (walls without ERD			О	H		
FORC	walls with moderate level of ERD			┝	Ь	H	
REIN	walls with high level of ERD				╞┅	О	-
3T EEL	steel structures			ŀ		0	-1
MOOD	timber structures		ŀ		0	-1	

Omost likely vulnerability class; — probable range; ----range of less probable, exceptional cases

Figure 3.2.13 Vulnerability Classes in EMS-98

	Classification of Damag	ge
	Masonry	RC Building
Grade 1:	Hair-line cracks in very few walls. Fall of small pieces of plaster only.	Fine cracks in plaster over frame members or in walls at the base.
Negligible to slight	Fall of loose stones from upper parts of buildings in very few cases.	Fine cracks in partitions and infills
damage	1 The second	
(no structural damage,		
slight non-structural		
damage)		
Grade 2:	Cracks in many walls. Fall of fairly large pieces of plaster.	Cracks in columns and beams of frames and in structural walls.
Moderate damage	Partial collapse of chimneys.	Cracks in partition and infill walls; fall of brittle cladding and plaster. Falling mortar from the
(slight structural damage,		joints of wall panels.
moderate		
non-structural damage)		
Grade 3:	Roof tiles detach. Chimneys fracture at the	frames at the base and at joints of coupled walls.
Substantial to heavy	roof line; failure of individual non-structural elements (partitions, gable	Spalling of concrete cover, buckling of reinforced rods.
damage	walls).	Large cracks in partition and infill walls, failure of individual infill papels
(moderate structural		
damage,		
heavy non-structural		
damage)		
Grade 4: Very heavy	Serious failure of walls; partial structural failure of roofs and floors	Large cracks in structural elements with compression failure of concrete and fracture of
damage		rebars; bond failure of beam reinforced bars; tilting of columns, Collapse of a few columns or
(heavy structural damage,	WINY'S BAR	of a single upper floor.
very heavy non-structural		
damage)		
Grade 5: Destruction	Total or near total collapse	Collapse of ground floor or parts (e. g. wings) of buildings.
(very heavy structural		
damage)		







Safina, 2003



Source: JICA Study Team

Figure 3.2.16 Flowchart of Human Casualties' Estimation



Source: Cronicas de Desasteres Terremoto de Cariaco, Venezuela, 1997, PAHO

Figure 3.2.17 Relation Between Number of Heavily Damaged Building and Number of Death of Cariaco Earthquake (1997)



Source: Social and Economic Dimensions of the Effects of the Earthquake in the Eje Cafetero. Diagnosis for the reconstruction, 1999, DANE, National Administrative Department of Statistics, Colombia and the JICA Study Team

Figure 3.2.18 Relation Between Heavily Damaged Building and Death Toll of Quindio Earthquake (1999, Colombia)



Source: The JICA Study Team





Source: Social and Economic Dimensions of the Effects of the Earthquake in the Eje Cafetero. Diagnosis for the reconstruction, 1999, DANE, National Administrative Department of Statistics, Colombia and the JICA Study Team

Figure 3.2.20 Relationship Between Death and Injured of Quindio Earthquake (1999, Colombia)

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 | S3 S4 (LM) (RC SW) 0 5.5 3.5 0 NA -1.0 5 -0.5 -0.5 6 -0.5 -0.5 6 -0.5 -0.5 5 -0.5 -0.5 5 -0.5 -0.5 5 N/A -1.0 5 N/A -0.5 5 N/A N/A A N/A N/A 0 +2.0 +2.0 | C1 C2 C
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+2.0 +2.0 | 3/85 PC1 PC 1.5 2.0 1 -0.5 NA -0 -0.5 -0.5 -0 -0.5 -1.0 -1 -1.0 -1.0 -1 -0.5 -1.0 -1 -0.5 -1.0 -1 -1.0 -1.0 -1 -0.5 -1.0 -1 -0.5 -1.0 -1 -0.5 -1.0 -1 -0.5 -1.0 -1 -0.5 -1.0 -1 -0.5 -1.0 -1 -0.5 -1.0 -1 -0.5 -1.0 -1 WA N/A -1 WA WA -1 WA +2.0 +2 | 2 RM L
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 | S3 S4 (LM) (RC SW) 0 5.5 3.5 0 N/A -1.0 5 -0.5 -0.5 6 -0.5 -0.5 5 -0.5 -0.5 0 -1.0 -1.0 5 -0.5 -0.5 5 N/A -1.0 5 -0.5 -0.5 6 -0.5 -0.5 7 -0.5 -0.5 8 N/A N/A 0 +2.0 +2.0 3 -0.3 -0.3 8 -0.6 -0.6 | C1 C2 C
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 | S3 S4 (LM) (RC SW) 0 5.5 3.5 0 N/A -1.0 5 -0.5 -0.5 6 -0.5 -0.5 0 -1.0 -2.0 0 -1.0 -1.0 5 -0.5 -0.5 5 N/A -0.5 6 -0.5 -0.5 7 -0.5 -0.5 8 N/A N/A 0 +2.0 +2.0 3 -0.3 -0.3 8 -0.6 -0.6 | C1 C2 C
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(MRF) (SW) (U
2.0 3.0
-1.0 -1.0
-0.5 -0.5
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-1.0 -1.0
-0.5 -0.5
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-1.0 N/A
-1.0 -1.0
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-0.8 -0.8</td><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>2 RM L
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(MRF) (SW) (U
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-1.0 -1.0
-0.5 -0.5
-1.0 -0.6
-2.0 -2.0
-1.0 -1.0
-0.5 -0.5
-0.5 N/A
-1.0 N/A
-1.0 -1.0
+2.0 +2.0
-0.8 -0.8</td><td>C3/S5 PC1 PC
RM NF) (TU)
1.5 2.0 1
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1.5 2.0 1
1.5 2.0 1
1.0 -1.0 -1
-0.5 -0.5 -0
-0.5 -0.5 -0
-0.5 -1.0 -1
NA NA -0
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NA +2.0 +2
-0.3 -0.3 -0
-0.6 -0.6 -0
-0.8 NA -0</td><td>2 RM (
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A -0.5 -0.</td><td>C.M. (M.) (RC SW)
(LM) (RC SW)
0 5.5 3.5
0 NA -1.0
5 -0.5 -0.5
5 -0.5 -0.5
0 -1.0 -2.0
0 -1.0 -1.0
5 -0.5 -0.5
5 NA -0.5
5 NA -0.5
5 NA -0.5
5 NA -0.5
5 NA -0.5
8 -0.6 -0.6
8 NA -0.8
9 NA -0.8</td><td>C1 C2 C
(MRF) (SW) (U
2.0 3.0
-1.0 -1.0
-0.5 -0.5
-1.0 -0.6
-2.0 -2.0
-1.0 -1.0
-0.5 -0.5
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-1.0 NA
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-0.8 -0.8</td><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>2 RM (
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× -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8</td><td>(LM) (RC SW)
(LM) (RC SW)
(LM) (RC SW)
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(MRF) (SW) (U
2.0 3.0
-1.0 -1.0
-0.5 -0.5
-1.0 -0.6
-2.0 -2.0
-1.0 -1.0
-0.5 -0.5
-0.5 NA
-1.0 NA
-1.0 NA
-1.0 NA
-1.0 -1.0
+2.0 +2.0
-0.8 -0.8
-0.8 -0.8
-0.8 -0.8</td><td>23/55 PC1 PC
RM NF) (TU)
1.5 2.0 1
1.5 2.0 1
1.5 2.0 1
1.5 NA -0
-0.5 -0.5 -0
-0.5 -0.5 -0
-0.5 -1.0 -1
-1.0 -1.0 -1
-1.0 -1.0 -1
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NA NA -0
NA NA -0
NA NA -0
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-0.3 -0.3 -0
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Figure 4</td><td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td><td>(LM) (RC SW)
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5 -0.5 -0.5
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6 -0.5 -0.5
8 -0.6 -0.6
8 -0.8 -0.8
8 -0.8 -0.8
9 -0.8 -0.8 -0.8
9 -0.8 -0.8 -0.8 -0.8
9 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8</td><td>C1 C2 C
(MRF) (SW) (U
2.0 3.0
-1.0 -1.0
-0.5 -0.5
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-2.0 -2.0
-1.0 -1.0
-0.5 -0.5
-0.5 NA
-1.0 NA
-1.0 NA
-1.0 -1.0
+2.0 +2.0
-0.8 -0.8
-0.8 -0.8
-0.8 -0.8</td><td>$\begin{array}{c} 3/35 \text{PC1} \text{PC} \\ \text{RM} \ \text{NF} \ (\text{TU}) \\ 1.5 2.0 1 \\ -0.5 \text{VA} -0 \\ -0.5 -0.5 -0.5 \\ -0.6 -1.0 -1 \\ -1.0 -1.0 -1 \\ -1.0 -1.0 -1 \\ -1.0 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -0.6 -0.6 \\ -0.6 -0.8 \text{VA} -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0 \\ -0.8 -0 \\ -0 \\ -0.8 -0 \\ -0 \\ -0.8 -0 \\ -0 \\ -0 \\ -0 \\ -0 \\ -0 \\ -0 \\ -0$</td><td>2 RM (
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.8 -0.</td></tr></td></tr> | S3 S4 (LM) (RC SW) 0 5.5 3.5 0 N/A -1.0 5 -0.5 -0.5 6 -0.5 -0.5 0 -1.0 -2.0 0 -1.0 -1.0 5 -0.5 -0.5 5 N/A -0.5 6 -0.5 -0.5 7 -0.5 -0.5 8 N/A N/A 9 -2.0 +2.0 10 +2.0 +2.0 10 +2.0 +2.0 10 +2.0 +2.0 10 +2.0 +2.0 10 -0.8 -0.6 10 N/A -0.8 | C1 C2 C
(MRF) (SW) (U
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-0.5 -0.5
-2.0 -2.0
-1.0 -1.0
-0.5 -0.5
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-1.0 N/A
-1.0 -1.0
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-0.8 -0.8 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 2 RM L
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RE | (MRF) (BR) .5 4.5 3. .4.5 3. .5 -0.5 .5 -0.5 .0 -2.5 .0 -2.5 .0 -2.5 .0 -0.5 .0 -2.5 .0 -2.5 .0 -0.5 .0 -2.5 .0 -2.5 .0 -2.5 .0 -2.5 .0 -0.5 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 .0 -2.0 <tr t<="" td=""><td>S3 S4 (LM) (RC SW) 0 5.5 3.5 0 NA -1.0 5 -0.5 -0.5 0 -1.0 -1.0 5 -0.5 -0.5 0 -1.0 -1.0 5 -0.5 -0.5 5 NA -0.5 5 NA -0.5 5 NA NA A NA NA A NA NA 0 +2.0 +2.0 3 -0.3 -0.3 8 -0.6 -0.6 8 NA -0.8</td><td>C1 C2 C
(MRF) (SW) (U
2.0 3.0
-1.0 -1.0
-0.5 -0.5
-1.0 -0.6
-2.0 -2.0
-1.0 -1.0
-0.5 -0.5
-0.5 N/A
-1.0 N/A
-1.0 -1.0
+2.0 +2.0
-0.8 -0.8</td><td>C3/S5 PC1 PC
RM NF) (TU)
1.5 2.0 1
1.5 2.0 1
1.5 2.0 1
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RM NF) (TU)
1.5 2.0 1
1.5 2.0 1
1.5 2.0 1
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-1.0 N/A
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RM NF) (TU)
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(LM) (RC SW)
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(MRF) (SW) (U
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RM NF) (TU)
1.5 2.0 1
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-0.8 -0.8
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-0.8 -0.8 | $\begin{array}{c} 3/35 \text{PC1} \text{PC} \\ \text{RM} \ \text{NF} \ (\text{TU}) \\ 1.5 2.0 1 \\ -0.5 \text{VA} -0 \\ -0.5 -0.5 -0.5 \\ -0.6 -1.0 -1 \\ -1.0 -1.0 -1 \\ -1.0 -1.0 -1 \\ -1.0 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -0.6 -0.6 \\ -0.6 -0.8 \text{VA} -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0 \\ -0.8 -0 \\ -0 \\ -0.8 -0 \\ -0 \\ -0.8 -0 \\ -0 \\ -0 \\ -0 \\ -0 \\ -0 \\ -0 \\ -0$ | 2 RM (
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| S3 S4 (LM) (RC SW) 0 5.5 3.5 0 N/A -1.0 5 -0.5 -0.5 6 -0.5 -0.5 0 -1.0 -2.0 0 -1.0 -1.0 5 -0.5 -0.5 5 N/A -0.5 6 -0.5 -0.5 7 -0.5 -0.5 8 N/A N/A 9 -2.0 +2.0 10 +2.0 +2.0 10 +2.0 +2.0 10 +2.0 +2.0 10 +2.0 +2.0 10 -0.8 -0.6 10 N/A -0.8 | C1 C2 C
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RM NF) (TU)
1.5 2.0 1
1.5 2.0 1
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(C SV)</td><td>C1 C2 C
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RM NF) (TU)
1.5 2.0 1
1.5 2.0 1
1.5 2.0 1
1.5 NA -0
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(MRF) (SW) (U
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-0.5 -0.5
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 | S3 S4 (LM) (RC SW) 0 5.5 3.5 0 NA -1.0 5 -0.5 -0.5 0 -1.0 -1.0 5 -0.5 -0.5 0 -1.0 -1.0 5 -0.5 -0.5 5 NA -0.5 5 NA -0.5 5 NA NA A NA NA A NA NA 0 +2.0 +2.0 3 -0.3 -0.3 8 -0.6 -0.6 8 NA -0.8 | C1 C2 C
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 | C.M. (M.) (RC SW)
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RM NF) (TU)
1.5 2.0 1
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| S3 S4 (LM) (RC SW) 0 5.5 3.5 0 NA -1.0 5 -0.5 -0.5 0 -1.0 -1.0 5 -0.5 -0.5 0 -1.0 -1.0 5 -0.5 -0.5 5 NA -0.5 5 NA -0.5 5 NA NA A NA NA A NA NA 0 +2.0 +2.0 3 -0.3 -0.3 8 -0.6 -0.6 8 NA -0.8 | C1 C2 C
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RM NF) (TU)
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1.5 2.0 1
1.5 2.0 1
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 | C.M. (M.) (RC SW)
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-0.8 -0.8 | 23/55 PC1 PC
RM NF) (TU)
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1.5 2.0 1
1.5 2.0 1
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Figure 4 | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$

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9 -0.8 -0.8 -0.8 -0.8
9 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 | C1 C2 C
(MRF) (SW) (U
2.0 3.0
-1.0 -1.0
-0.5 -0.5
-1.0 -0.5
-2.0 -2.0
-1.0 -1.0
-0.5 -0.5
-0.5 NA
-1.0 NA
-1.0 NA
-1.0 -1.0
+2.0 +2.0
-0.8 -0.8
-0.8 -0.8
-0.8 -0.8 | $\begin{array}{c} 3/35 \text{PC1} \text{PC} \\ \text{RM} \ \text{NF} \ (\text{TU}) \\ 1.5 2.0 1 \\ -0.5 \text{VA} -0 \\ -0.5 -0.5 -0.5 \\ -0.6 -1.0 -1 \\ -1.0 -1.0 -1 \\ -1.0 -1.0 -1 \\ -1.0 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -1.0 -1 \\ -0.5 -0.6 -0.6 \\ -0.6 -0.8 \text{VA} -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0.8 -0 \\ -0 \\ -0.8 -0 \\ -0 \\ -0.8 -0 \\ -0 \\ -0.8 -0 \\ -0 \\ -0 \\ -0 \\ -0 \\ -0 \\ -0 \\ -0$ | 2 RM (
.5 3.0
.5 -1.0 -
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.0 -0.5 -
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.0 -0.8 -
.8 -0. | | | | | |

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Source: Rapid Visual Screening of Buildings for Potential Seismic Hazards: A Handbook FEMA 154 1968

Figure 3.3.1 The Scoring Sheet with Actual Record



Source: Rapid Visual Screening of Buildings for Potential Seismic Hazards: A Handbook FEMA 154

Figure 3.3.2 Work Flowchart for the Rapid Screening Procedure (RSP) Identification Procedure



Source: The JICA Study Team





Source: Evaluating The Seismic Resistance Of Existing Buildings; ATC 14 1987

Figure 3.3.4 Seismic Evaluation Procedure (Continued on Next Page)



Source: Evaluating The Seismic Resistance Of Existing Buildings; ATC 14 1987

Figure 3.3.5 Seismic Evaluation Procedure (Continued from Previous Page)



Figure 3.4.1 Procedure of Seismic Damage Estimation



Figure 3.4.2 Cut and Cover Type Tunnel



Figure 3.4.3 Water Supply System



Figure 3.4.4 Flow Chart of Damage Estimation for Water Supply



Figure 3.4.5 Standard Damage Ratio



Object for damage estimation

Figure 3.4.6 Natural Gas Pipeline Network



Figure 3.4.7 Standard Damage Ratio for Gas Pipeline



Figure 3.4.8 Electric Power Supply Network













Figure 3.4.14 PGA and No. of Gasoline Stations



Figure 3.4.15 PGA and No. of Gasoline Stations



Figure 3.5.1 Floor Detail of Models



Figure 3.5.2 Floor and Foundation Detail of Models



Figure 3.5.3 Framing Elevation of Model 1 (1)



Figure 3.5.4 Framing Elevation of Model 1 (2)



Figure 3.5.5 Horizontal Load Transfer Steel Frame



Figure 3.5.6 Framing Elevation of Model 2



Figure 3.5.7 Framing Elevation of Model 3



Figure 3.5.8 Framing Elevation of Model 4



Figure 3.5.9 Grade Beam Detail and a Frame for Measurement



Figure 3.5.10 Detail of a Frame for Measurement



Figure 3.5.11 Distribution of Concrete Strength by Cylinder Test, Tested by IMME





4 # 5 # 6 B A # 1 # 1 # 2 # 2 # 3







Figure 3.5.14 Side View A

Figure 3.5.15 Side View B



Figure 3.5.16 Load Deflection Curve



Source: Seismic Code of Venezuela 2001 "NORMA VENEZOLANA COVENIN 1756-98"

Figure 3.5.17 Basic Concept of Seismic Reinforcement



Source: JICA Study Team



where: CB15; Concrete block wall in thk. of 150mm w/ reinforcing bar of

Vertical; D10 @ 800mm, Horizontal; 10 Ø @ 600mm

SW8; RC shear wall in thk. of 80mm (Refer to Figure 3.2.7)

SW10; RC shear wall in thk. of 100mm (Refer to Figure 3.2.7)

- SW12; RC shear wall in thk. of 120mm w/ reinforcing bar of D10 @ 250mm e.w., Anchor bar of D16 @250 (Similar to Figure 3.2.7)
- SW15; RC shear wall in thk. of 150mm w/ reinforcing bar of D10 @ 200mm e.w., Anchor bar of D16 @250 (Similar to Figure 3.2.7)

Grade Beam; W200mm x D300mm w/4D13, Strr. 6@@200mm









Figure 3.5.19(2) Recommended Seismic Reinforcement Methods for a Single Family House