

4.5 Power System Analysis

4.5.1 Purpose

A 370 MW combined cycle generating facility, which is scheduled to begin operation in 2008, is to be added to the Tashkent Thermal Power Plant. The purpose of the power system analysis is carrying out the calculation in order to examine the influence due to the introduction of this facility under normal condition and emergency condition. The power system analysis will be examined issues such as power flow, short-circuit current, stability, and frequency fluctuation.

4.5.2 Examined Case

Ideally, the power system of year 2008 would be simulated for the calculations, but accurate data is not available with regard to demand forecast, generation development plan, and power transmission system development plan for future years. Therefore, the analysis will be carried out based on the actual year 2002 data for the power system to which the new 370MW generator of the Tashkent Thermal Power Plant will be connected.

The calculations are carried out about the two cases that are the summer peak and winter peak representing the different aspects of the power flow.

4.5.3 Simulated System

Because the electrical power system in Uzbekistan retains the transmission system that was constructed during the time of the former Soviet Union, there are international connection lines between Uzbekistan and four other countries (Kazakhstan, Kyrgyzstan, Tajikistan and Turkmenistan). The five countries including Uzbekistan make up the Central Asia Power System. The trunk transmission lines of the Central Asia Power System are 500 kV and 220 kV lines. For the purposes of these calculations, almost all of the 500 kV and 220 kV transmission lines and substations of the system were simulated except some radial power system. Major power plants with capacities of 600 MW or more were simulated accurately unit by unit. Namely, the simulated 8 power plants are as follows.

Uzbekistan	Syrdariya	3000 MW	Thermal power plant
	Novo Angren	2100 MW	Thermal power plant

	Tashkent	1860 MW	Thermal power plant
	Navoi	1250 MW	Thermal power plant
	Charvac	620 MW	Hydro power plant
Kyrgyzstan	Toktogul	1200 MW	Hydro power plant
	Kurpsai	800 MW	Hydro power plant
Tajikistan	Nurek	3000 MW	Hydro power plant

The 500 kV bus of the Almaty substation in Kazakhstan was taken as the slack bus. (Figure 4.5-1)

4.5.4 Calculation Software

Calculations were carried out by using "CRIEPI's Power System Analysis Tools" developed by the Central Research Institute of the Electric Power Industry (CRIEPI) in Japan. This software is currently used by all the electric power companies in Japan. SJSC "Uzbekenergo" is using the calculation software named "Mustang" which was made in former Soviet Union.

4.5.5 Winter Peak Calculation Results

(1) Power Flow

The results of the power flow calculation after the new 370 MW generator is connected to the Tashkent Thermal Power Plant are shown in Figure 4.5-2.

The power flow through each transmission line is as shown in Table 4.5-1. For all the transmission lines, the calculated flow was within the allowable current capacity.

The power flow calculations when one circuit of 500kV transmission line is tripped were also carried out and the result is as shown in Table 4.5-1. For all the 500 kV transmission lines and most 220kV transmission lines, the calculated flow was within the allowable current capacity.

(2) Voltage

For the purposes of maintaining the proper voltage, the static condensers with required capacity were inserted into the several substations.

The voltage values for the 500 kV and 220 kV buses at each substation were as shown in Figure 4.5-2 and Table 4.5-2. The 500kV bus voltage of each substations was within the

range of 535 kV (107.1 %) and 500 kV (100.0 %). And the 220 kV bus voltage of each substations was within the range of 229 kV (104.0 %) and 201 kV (91.4 %). In all cases, the voltage was found to fall within the target range of ± 10 %.

(3) Short-circuit Current

The 3-phase short-circuit current values for the 500 kV and 220 kV buses for each substation were as shown in Table 4.5-3. The maximum short-circuit current was 13.1 kA for a 500 kV bus and 27.5 kA for a 220 kV bus. In all cases, the current was within the rated current capacity for the equipment of 40 kA.

The influence of introduction of 370 MW combined cycle power plant on the network system was +0.4 kA for a 500kV bus and +2.8 kA for a 220kV bus of Tashkent Thermal Power Plant. However, in these calculations, only principal power plants were simulated, so the values were slightly lower than the actual short-circuit current values.

According to NDC (National Dispatch Center) calculations, the present 3-phase short-circuit current value of Tashkent Thermal Power Plant 220kV bus is close to 40kA and according to the kind of faults it may be over 40kA. Therefore when the power system development plan is decided, the more exact short-circuit current calculation should be carried out about 2008 year stage when the new 370 MW generator is put into operation. And if necessary, either of the countermeasures should be taken. Since it seems that it is sufficiently possible to replace 220kV circuit breakers from designing to installation for two years, it will be possible to carry out it after the detailed study by SJSC "Uzbekenergo".

- a. One more 500/220kV transformer is constructed and 220kV bus bar is operated separately.
- b. Next replaced generators are connected to 500kV bus directly.
- c. As the next replaced generator's step-up transformers, high impedance ones are adopted.
- d. All 220kV circuit breakers are replaced to the rated current capacity 50kA or 63kA.

(4) Static Stability

Static stability calculations were carried out for the purpose of assessing whether or not stability can be maintained in the power system when a slight disturbance such as a circuit-breaker opening occurs somewhere in the system. The result of this calculation, which is provided in Figure 4.5-3, indicates that the system is stable.

(5) Dynamic Stability

Dynamic stability calculations were performed assuming the case that a 2LG-O(Line Ground fault - Open) fault occurred at the nearest point of the 370 MW generator of the Tashkent Thermal Power Plant.

Failure sequence:

500kV Transmission line, Transformer:

Circuit breaker opens 120 ms after the failure occurs.

220kV Transmission line:

Circuit breaker opens 200 ms after the failure occurs.

Case 1: 500kV Tashkent GRES - Shimkent

Case 2: 500kV Tashkent GRES - TashkentSS

Case 3: 220kV Tashkent GRES - Uksak

Case 4: Tashkent GRES 500/220 kV main transformer

The results of the calculations for each case are as shown in Figures 4.5-4, 4.5-5, 4.5-6, and 4.5-7. The fluctuation in the phase angle of the power plant is converged, so power system stability is stable.

(6) Frequency Fluctuation

The unit with the largest capacity in the Central Asia Power System is the 800 MW generator at the Tarimaljan Power Plant (expected to begin operation in 2003). The frequency drop was calculated for the case when the Tarimaljan 800 MW generator dropped out of the system, and the frequency rise was calculated in the cases of 5 % and 10 % load reductions of the whole system. The results of the calculations are shown in Figures 4.5-8, 4.5-9, and 4.5-10. The frequency drop of the case of the Tarimaljan 800 MW generator dropped out is 0.1Hz, the frequency rise of the case of 5% load reduction is 0.05Hz and the frequency rise of the case of 10% load reduction is 0.1Hz. The range of permitted frequency is 48.5Hz - 51.5Hz in the electric power companies of Japan, so this frequency fluctuation values are within the range.

The standard gas turbine of a certain manufacturer for commercial use is designed so as to be able to continuously operate under load within the range of the network frequency of 47.5 Hz to 51.5 Hz. Such allowable range is specified to avoid that the natural frequencies of rotating blades of the turbine and compressor will be resonant with the harmonics of the rotating speed.

Therefore, if the network frequency exceeds the said range, the generator breaker shall be forced to open or the gas turbine shall be forced to trip with the time delayed frequency relay. In case of the gas turbine mentioned above, the time delayed frequency relays have such functions as shown below:

a. Under Frequency Relay

$47.0 \text{ Hz} < F \leq 47.5 \text{ Hz}$ The generator breaker opens after 15 seconds.

$F = 47.0 \text{ Hz}$ The gas turbine trips after 0.1 second.

$F < 47.0 \text{ Hz}$ The gas turbine immediately trips.

b. Over Frequency Relay

$F = 51.5 \text{ Hz}$ The gas turbine trips after 0.1 second.

$F > 51.5 \text{ Hz}$ The gas turbine immediately trips.

The allowable range where the gas turbine can be continuously operated under load is changeable depending upon the design concept of the gas turbine manufacturer. So that we will recommend that SJSC "Uzbekenergo" should discuss with the EPC contractor as to how to pre-set the frequency relays.

4.5.6 Summer Peak Calculation Results

(1) Power Flow

The results of the power flow calculation after the new 370 MW generator is connected to the Tashkent Thermal Power Plant are shown in Figure 4.5-11.

The power flow through each transmission line is as shown in Table 4.5-1. For all the transmission lines, the calculated flow was within the allowable current capacity.

(2) Voltage

For the purposes of maintaining the proper voltage, the static condensers with required capacity were inserted into the several substations.

The voltage values for the 500 kV and 220 kV buses at each substation were as shown in Figure 4.5-11 and Table 4.5-2. The 500kV bus voltage of each substations was within the range of 543 kV (108.7 %) and 500 kV (100.0 %). And the 220 kV bus voltage of each substations was within the range of 241 kV (109.6 %) and 210 KV (95.5 %). In all cases, the voltage was found to fall within the target range of ± 10 %.

(3) Short-circuit Current

Same as winter peak calculation result.

(4) Static Stability

Static stability calculations were carried out for the purpose of assessing whether or not stability can be maintained in the power system when a slight disturbance such as a circuit-breaker opening occurs somewhere in the system. The results of these calculations, which are provided in Figure 4.5-12, indicate that the system is stable.

(5) Dynamic Stability

Dynamic stability calculations were performed assuming the case that a 2LG-O fault occurred at the nearest point of the 370 MW generator of the Tashkent Thermal Power Plant.

Failure sequence:

500kV Transmission line, Transformer:

Circuit breaker opens 120 ms after the failure occurs.

220kV Transmission line:

Circuit breaker opens 200 ms after the failure occurs.

Case 1: 500kV Tashkent GRES - Shimkent

Case 2: 500kV Tashkent GRES - TashkentSS

Case 3: 220kV Tashkent GRES - Uksak

Case 4: Tashkent GRES 500/220 kV main transformer

The results of the calculations for each case are as shown in Figures 4.5-13, 4.5-14, 4.5-15, and 4.5-16. The fluctuation in the phase angle of the power plant is converged, so power system stability is stable.

(6) Frequency Fluctuation

Same as winter peak calculation result.

4.5.7 Conclusion and Observations

(1) Conclusion

The analysis revealed that there will be no problems of power flow, voltage, short-circuit current, stability and frequency fluctuation caused by connecting the new 370 MW

generator of the Tashkent Thermal Power Plant to the existing power system.

This analysis study was carried out using the data in 2002 not 2008 when the new C/C will be putting into operation. For the exact power system development plan, it is necessary to carry out the analysis study at the stage of 2008 and of future year. Therefore it is necessary to clarify the problem of power system regarding power flow, voltage, short-circuit current, stability and frequency fluctuation based on more precise analysis study taking into account demand forecast, power generation development plan and power transmission development plan by SJSC "Uzbekenergo". It seems that SJSC "Uzbekenergo" holds the technical skill of power system analysis. NDC is mainly carrying out power system analysis in Uzbekistan system and UDC is mainly carrying out in whole Central Asia system.

(2) Observations

However, an examination of the system as a whole revealed a problem of dynamic stability. The power flow is heavy from the east side to the west side of the power system, making the system a very weak one in terms of system stability. In particular, the dynamic stability would become unstable if the faults were to occur on the 500 kV transmission lines between Tashkent and Syrdarinskaya, between Syrdarinskaya and Guzar, or from Frunzenskaya to Toktogulskaya to Lochin. Therefore the dynamic stability calculations were performed assuming the case that 3LG-O fault of these each 500kV transmission lines occurred.

* Tashkent - Syrdarinskaya

Unstable at 3LG-O (Figure 4.5-20)

Stable at 1LG-O-C (Figure 4.5-21)

When the 800 MW generator of the Tarimaljan Power Plant will be connected to the system, the westward power flow will be alleviated, and the level of dynamic stability will become stable (Figure 4.5-22).

* Syrdarinskaya - Guzar

When the 800 MW generator of the Tarimaljan Power Plant joins the system, the westward power flow will be alleviated, but the level of dynamic stability will be still unstable (Figure 4.5-23). It will be necessary to install the power system stabilizer to divide the system into east part and west part and the both system to be stable or the new 500kV transmission line from Syrdarinskaya to Guzar to keep the system stable when the transmission line is an accident.

* Frunzenskaya - Toktogulskaya - Lochin.
Stable at 3LG-O (Figure 4.5-24, 4.5-25)

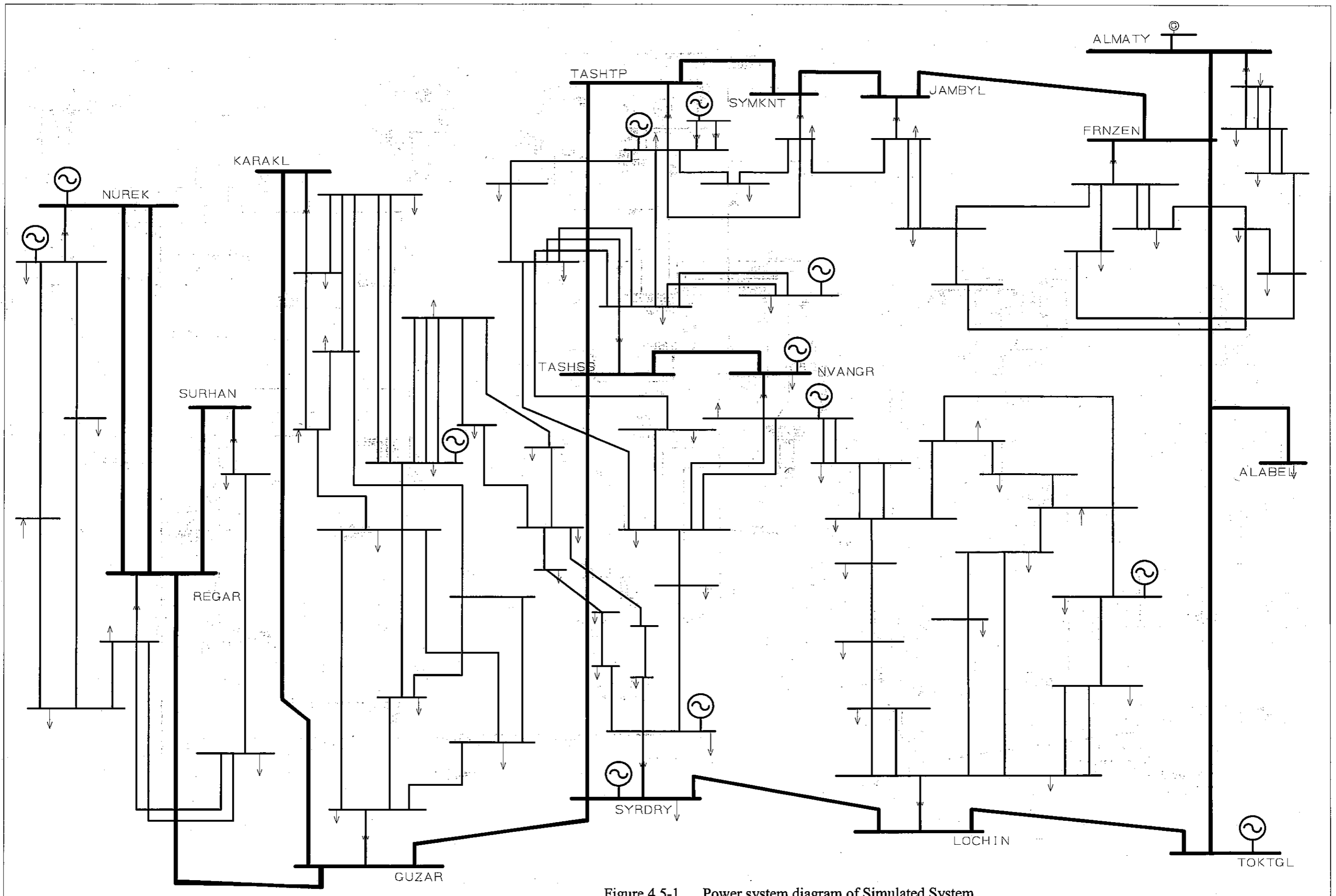
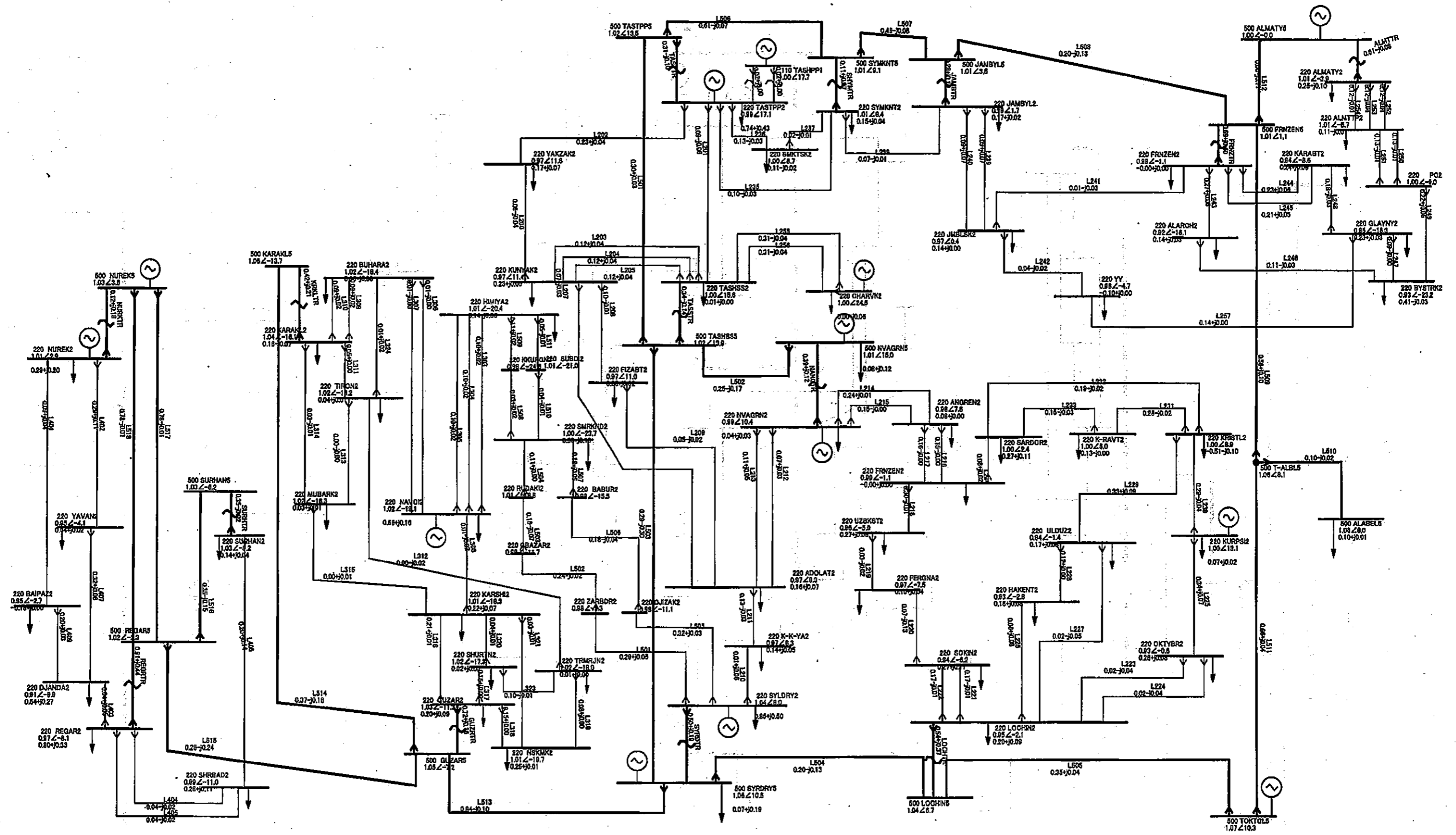


Figure 4.5-1 Power system diagram of Simulated System



注：母線電圧および線路潮流は p.u. 値
 (ベース電圧 500kV, 220kV ベース容量 1000MVA)

Figure 4.5-2 Power Flow Diagram of Winter Peak Demand

Table 4.5-2 Power Flow Calculation Result (Voltage value of each SS)

base_V	NAME	node voltage (normal condition)			
		summer		winter	
		(kV)	(%)	(kV)	(%)
500	TASTPP5	513.34	102.7%	507.90	101.6%
500	TASHSS5	513.34	102.7%	508.69	101.7%
500	NVAGRN5	507.66	101.5%	503.98	100.8%
500	SYDRY5	534.89	107.0%	529.03	105.8%
500	LOCHIN5	531.66	106.3%	520.58	104.1%
500	SYMKNT5	517.20	103.4%	507.22	101.4%
500	JAMBYL5	519.94	104.0%	505.42	101.1%
500	FRNZEN5	522.98	104.6%	506.58	101.3%
500	T-ALBL5	542.53	108.5%	531.79	106.4%
500	ALABEL5	543.01	108.6%	531.76	106.4%
500	TOKTGL5	542.24	108.4%	535.43	107.1%
500	ALMATY5	500.12	100.0%	500.10	100.0%
500	GUZAR5	542.84	108.6%	524.28	104.9%
500	KARAKL5	543.38	108.7%	528.33	105.7%
500	REGAR5	518.07	103.6%	508.56	101.7%
500	SURHAN5	519.67	103.9%	514.03	102.8%
500	NUREK5	519.76	104.0%	513.97	102.8%
220	TASTPP2	219.82	99.9%	218.54	99.3%
220	TASHSS2	222.12	101.0%	220.87	100.4%
220	KUNYAK2	214.32	97.4%	213.24	96.9%
220	YAKZAK2	213.15	96.9%	212.46	96.6%
220	NVAGRN2	216.82	98.6%	216.88	98.6%
220	ANGREN2	214.87	97.7%	215.59	98.0%
220	OBHYAT2	211.27	96.0%	212.04	96.4%
220	UZBKST2	213.80	97.2%	210.48	95.7%
220	FERGNA2	219.19	99.6%	213.23	96.9%
220	SOKIN2	213.41	97.0%	206.32	93.8%
220	LOCHIN2	218.67	99.4%	209.61	95.3%
220	OKTYBR2	214.55	97.5%	205.16	93.3%
220	HAKENT2	213.80	97.2%	204.89	93.1%
220	ULDUZ2	213.19	96.9%	205.74	93.5%
220	KRISTL2	213.08	96.9%	220.46	100.2%
220	K-RAVT2	210.73	95.8%	219.53	99.8%
220	SARDOR2	213.22	96.9%	219.56	99.8%
220	KURPSI2	219.58	99.8%	220.49	100.2%
220	SYLDRY2	234.01	106.4%	229.09	104.1%
220	K-K-YA2	212.83	96.7%	214.35	97.4%
220	ADOLAT2	213.80	97.2%	214.34	97.4%
220	FIZABT2	213.53	97.1%	213.04	96.8%
220	SYMKNT2	225.48	102.5%	221.62	100.7%
220	SMKTSK2	225.57	102.5%	221.03	100.5%
220	JAMBYL2	224.82	102.2%	218.59	99.4%
220	JMBLSK2	218.82	99.5%	213.46	97.0%
220	FRNZEN2	226.43	102.9%	218.31	99.2%
220	ALMATY2	220.18	100.1%	222.59	101.2%
220	ALARCH2	216.31	98.3%	201.88	91.8%
220	BYSTRK2	213.64	97.1%	205.20	93.3%
220	PC2	220.01	100.0%	220.56	100.3%
220	ALMTTP2	219.01	99.6%	221.84	100.8%
220	GLAYNY2	210.01	95.5%	208.53	94.8%
220	KARABT2	219.14	99.6%	207.43	94.3%
220	CHARVK2	220.33	100.2%	219.80	99.9%
220	YY	218.36	99.3%	215.14	97.8%
220	SMRKND2	234.20	106.5%	219.35	99.7%
220	HIMIYA2	225.83	102.7%	221.61	100.7%
220	NAVOI2	227.26	103.3%	223.70	101.7%
220	KARAKL2	237.70	108.0%	228.07	103.7%
220	BUHARA2	231.98	105.4%	223.62	101.6%
220	TIRON2	234.79	106.7%	225.37	102.4%
220	GUZAR2	237.79	108.1%	227.52	103.4%
220	KARSHI2	234.85	106.8%	222.64	101.2%
220	NSKMK2	236.44	107.5%	221.97	100.9%
220	TRMRJN2	236.27	107.4%	223.60	101.6%
220	SHURTN2	236.48	107.5%	224.13	101.9%
220	MUBARK2	235.95	107.3%	225.08	102.3%
220	ZARBDR2	232.08	105.5%	216.62	98.5%
220	CBAZAR2	234.64	106.7%	215.73	98.1%
220	RUDAKI2	241.06	109.6%	222.80	101.3%
220	DJZAK2	230.46	104.8%	216.04	98.2%
220	BABUR2	231.39	105.2%	216.46	98.4%
220	KKURGN2	226.30	102.9%	216.00	98.2%
220	SUEDI2	227.45	103.4%	221.55	100.7%
220	NUREK2	227.23	103.3%	221.97	100.9%
220	REGAR2	221.68	100.8%	214.36	97.4%
220	SURHAN2	228.25	103.8%	226.80	103.1%
220	SHRBAD2	219.86	99.9%	217.06	98.7%
220	DJANDA2	215.79	98.1%	201.08	91.4%
220	YAVAN2	220.95	100.4%	207.92	94.5%
220	BAIPAZ2	224.37	102.0%	208.91	95.0%

Table 4.5-3 Short Circuit Current Calculation Result

NAME	BASE Voltage (kV)	breaking capacity (kA)	FAULT CURRENT		FAULT CAPACITY	
			without CC (KA)	with CC (KA)	without CC (MVA)	with CC (MVA)
ALMATY5	500	40	40.0	40.0	34,823	34,629
TASTPP5	500	40	10.9	11.3	9,422	9,771
TASHSS5	500	40	11.8	12.2	10,243	10,599
NVAGRN5	500	40	8.9	9.0	7,677	7,831
SYDRY5	500	40	13.1	13.1	11,308	11,386
LOCHIN5	500	40	5.7	5.8	4,972	4,982
SYMKNT5	500	40	7.1	7.2	6,141	6,268
JAMBYL5	500	40	5.7	5.7	4,924	4,965
FRNZEN5	500	40	7.1	7.2	6,178	6,202
T-ALBL5	500	40	5.7	5.7	4,964	4,973
ALABEL5	500	40	4.8	4.9	4,196	4,203
TOKTGL5	500	40	6.2	6.2	5,358	5,367
GUZAR5	500	40	5.5	5.5	4,748	4,751
KARAKL5	500	40	3.1	3.1	2,717	2,718
REGAR5	500	40	6.4	6.4	5,538	5,539
SURHAN5	500	40	3.3	3.3	2,892	2,892
NUREK5	500	40	7.8	7.8	6,735	6,736
TASTPP2	220	40	24.7	27.5	9,400	10,469
TASHSS2	220	40	21.7	22.4	8,253	8,551
KUNYAK2	220	40	14.2	14.5	5,396	5,524
YAKZAK2	220	40	11.6	11.9	4,434	4,544
NVAGRN2	220	40	17.1	17.3	6,505	6,578
ANGREN2	220	40	10.8	10.8	4,098	4,124
OBHYAT2	220	40	6.1	6.1	2,328	2,334
UZBKST2	220	40	4.6	4.6	1,742	1,744
FERGNA2	220	40	4.7	4.7	1,784	1,786
SOKIN2	220	40	6.0	6.0	2,278	2,280
LOCHIN2	220	40	8.3	8.3	3,175	3,180
OKTYBR2	220	40	5.3	5.3	2,025	2,026
HAKENT2	220	40	6.1	6.1	2,326	2,328
ULDUZ2	220	40	6.2	6.2	2,378	2,380
KRISTL2	220	40	6.3	6.3	2,399	2,401
K-RAVT2	220	40	4.8	4.8	1,837	1,839
SARDOR2	220	40	4.9	4.9	1,853	1,855
KURPSI2	220	40	7.1	7.1	2,702	2,703
SYLDRY2	220	40	24.3	24.4	9,261	9,293
K-K-YA2	220	40	9.9	10.0	3,767	3,794
ADOLAT2	220	40	14.3	14.4	5,436	5,502
FIZABT2	220	40	11.3	11.5	4,295	4,370
SYMKNT2	220	40	11.8	12.0	4,483	4,564
SMKTSK2	220	40	6.9	7.0	2,615	2,650
JAMBYL2	220	40	9.4	9.5	3,589	3,612
JMBLSK2	220	40	7.0	7.0	2,651	2,662
FRNZEN2	220	40	12.7	12.8	4,857	4,871
ALMATY2	220	40	19.8	19.8	7,527	7,528
ALARCH2	220	40	3.5	3.5	1,350	1,351
BYSTRK2	220	40	4.1	4.1	1,550	1,551
PC2	220	40	6.9	6.9	2,634	2,634
ALMTP2	220	40	12.4	12.4	4,735	4,735
GLAYNY2	220	40	3.8	3.8	1,447	1,448
KARABT2	220	40	6.0	6.0	2,286	2,289
CHARVK2	220	40	11.5	11.6	4,398	4,438
YY	220	40	2.1	2.1	810	811
SMRKND2	220	40	4.5	4.5	1,729	1,729
HIMIYA2	220	40	8.7	8.7	3,298	3,298
NAVOI2	220	40	10.9	10.9	4,141	4,142
KARAKL2	220	40	7.0	7.0	2,672	2,673
BUHARA2	220	40	7.1	7.1	2,698	2,699
TIRON2	220	40	5.6	5.6	2,147	2,148
GUZAR2	220	40	9.1	9.1	3,479	3,481
KARSHI2	220	40	6.4	6.4	2,447	2,447
NSKMK2	220	40	4.7	4.8	1,810	1,810
TRMRJN2	220	40	5.6	5.6	2,116	2,116
SHURTN2	220	40	5.6	5.6	2,125	2,125
MUBARK2	220	40	4.6	4.6	1,764	1,764
ZARBDR2	220	40	3.7	3.7	1,403	1,403
OBAZAR2	220	40	3.0	3.0	1,156	1,156
RUDAKI2	220	40	3.0	3.0	1,139	1,140
DJZAK2	220	40	3.5	3.5	1,338	1,339
BABUR2	220	40	3.4	3.4	1,278	1,278
KKURGN2	220	40	4.1	4.1	1,549	1,549
SUBDI2	220	40	5.6	5.6	2,135	2,136
NUREK2	220	40	14.4	14.4	5,481	5,481
REGAR2	220	40	9.9	9.9	3,757	3,758
SURHAN2	220	40	6.4	6.4	2,437	2,437
SHRBAD2	220	40	5.4	5.4	2,053	2,053
DJANDA2	220	40	5.3	5.3	2,037	2,037
YAVAN2	220	40	6.2	6.2	2,360	2,360
BAIPAZ2	220	40	5.3	5.3	2,004	2,004

Winter Peak Calculation results

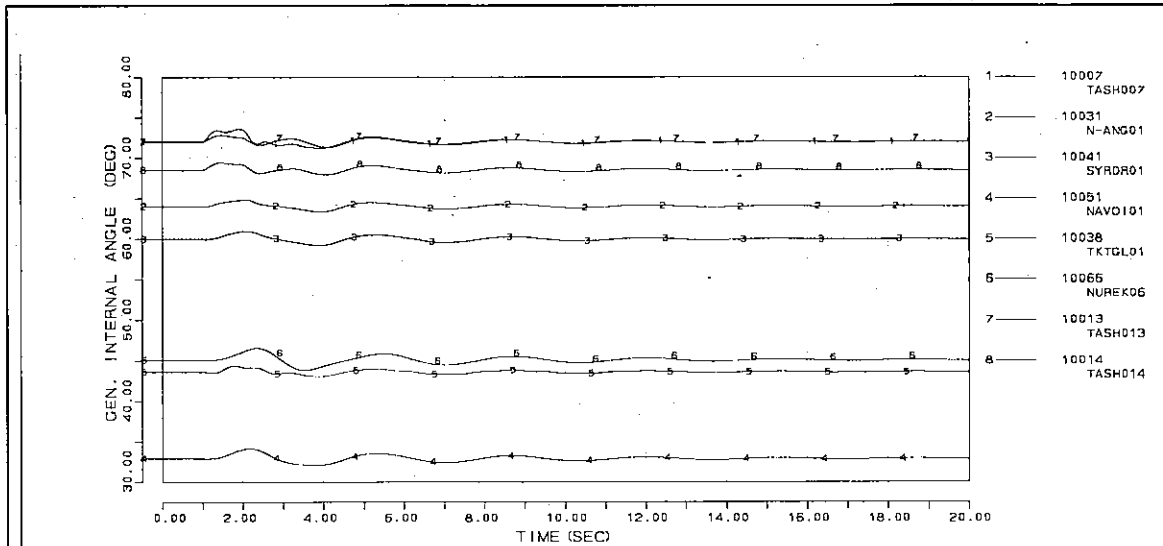


Figure 4.5-3 Static Stability

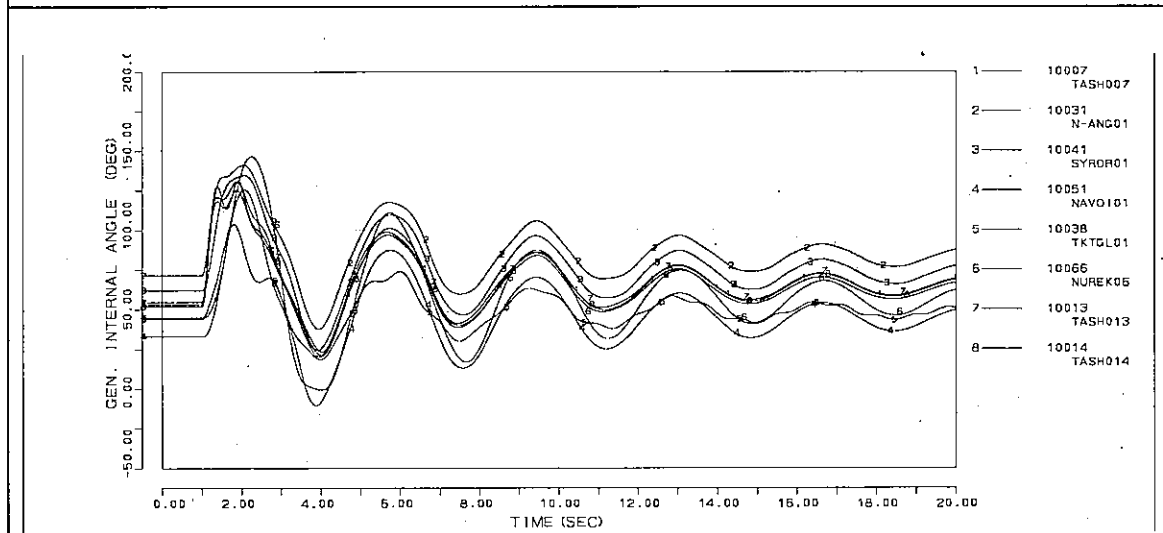


Figure 4.5-4 500kV TL Tashkent TPP-Symkent 2LGO

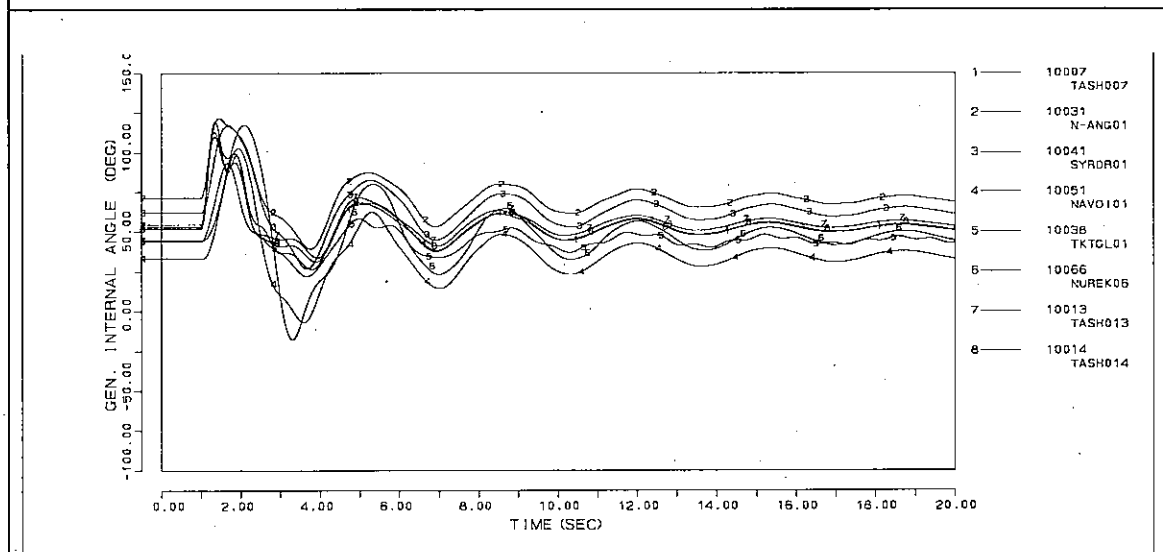


Figure 4.5-5 500kV TL Tashkent TPP-Tashkent SS 2LGO

Winter Peak Calculation results

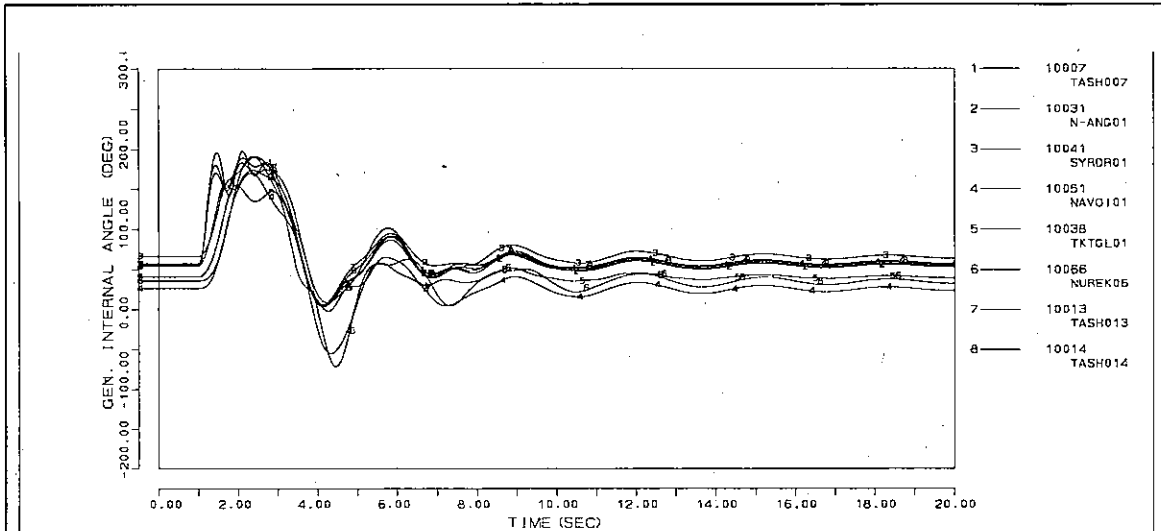


Figure 4.5-6 220kV TL Tashkent TPP-Uksak 2LGO

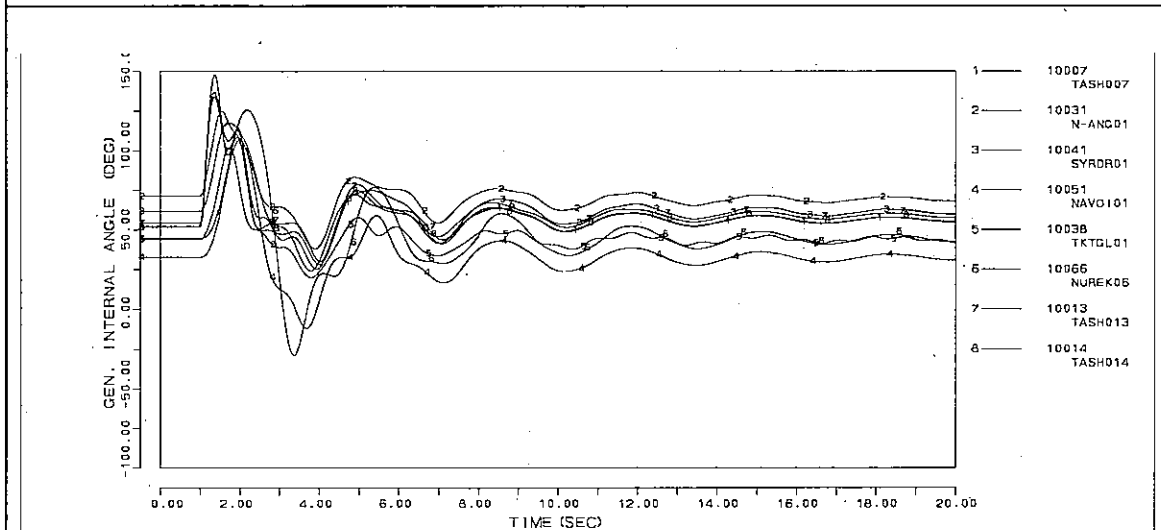


Figure 4.5-7 Tashkent TPP 500/220 Tr 2LGO

Winter Peak Calculation results

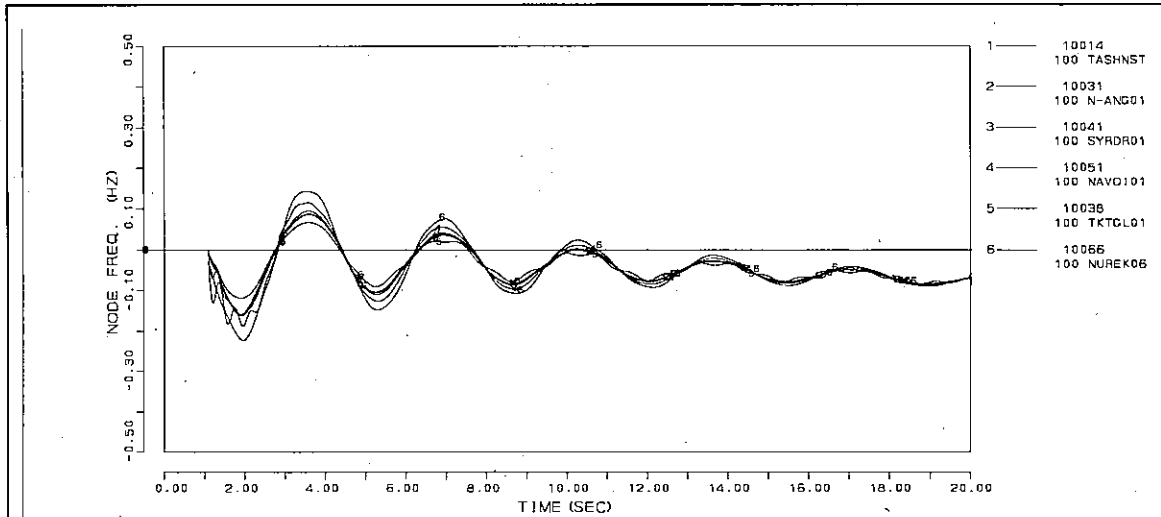


Figure 4.5-8 Tarimaljan 800MW generator drop out (frequency)

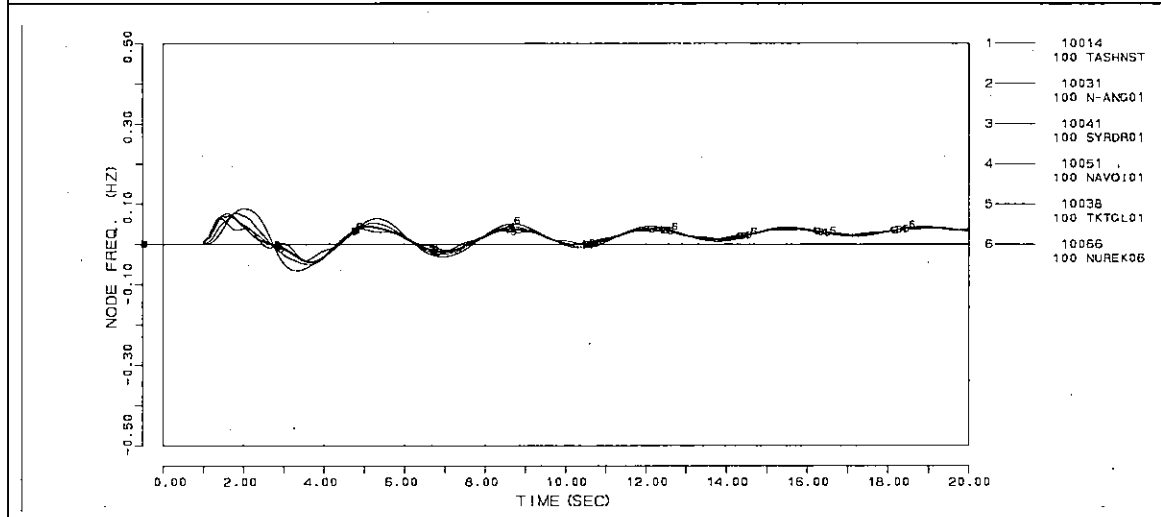


Figure 4.5-9 5% Load reduction (frequency)

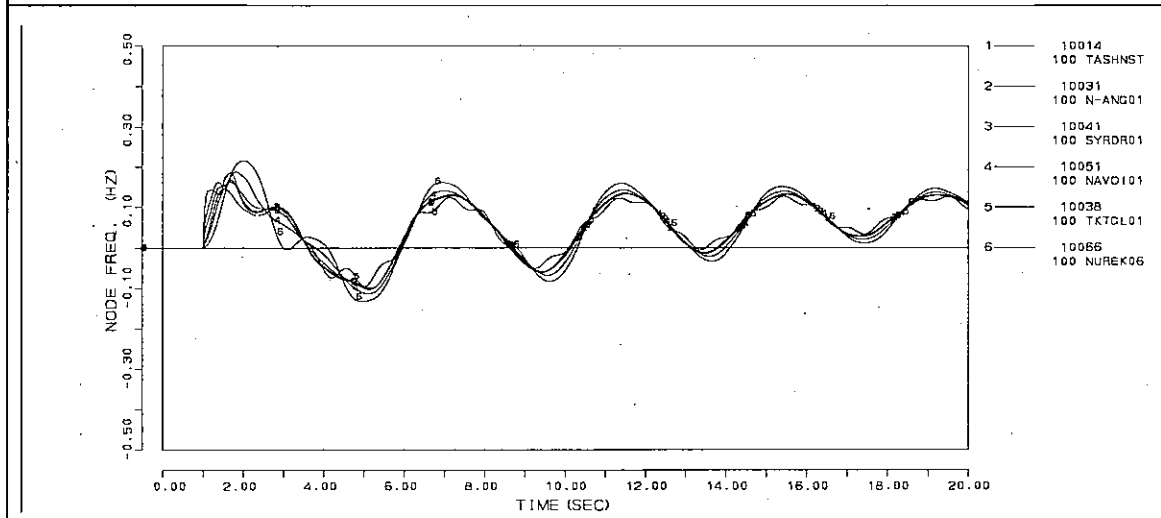
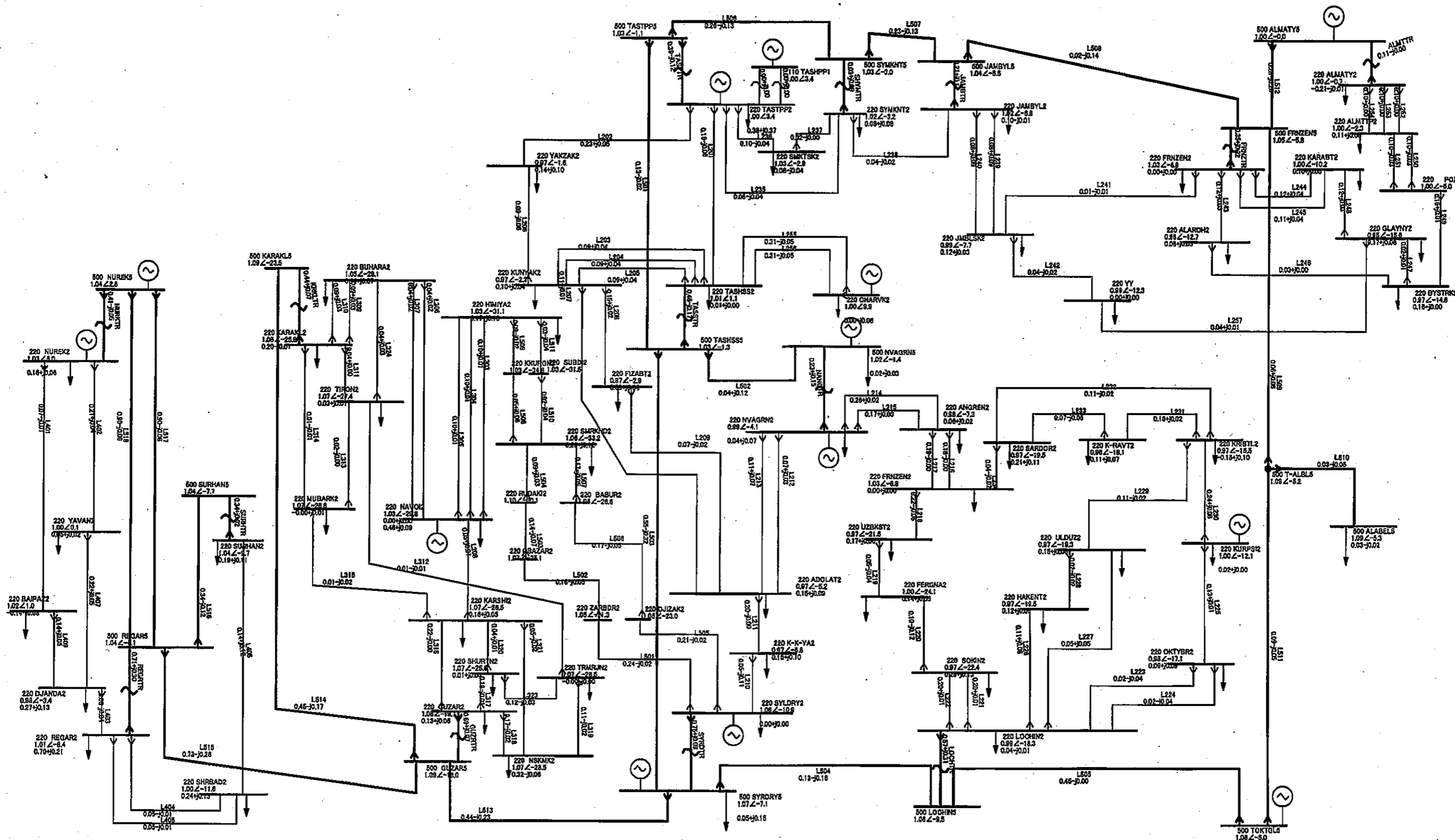


Figure 4.5-10 10% Load reduction (frequency)



注：母線電圧および線路潮流は p.u. 値
 (ベース電圧 500kV, 220kV ベース容量 1000MVA)

Figure 4.5-11 Power Flow Diagram of Summer Peak Demand

Summer Peak Calculation results

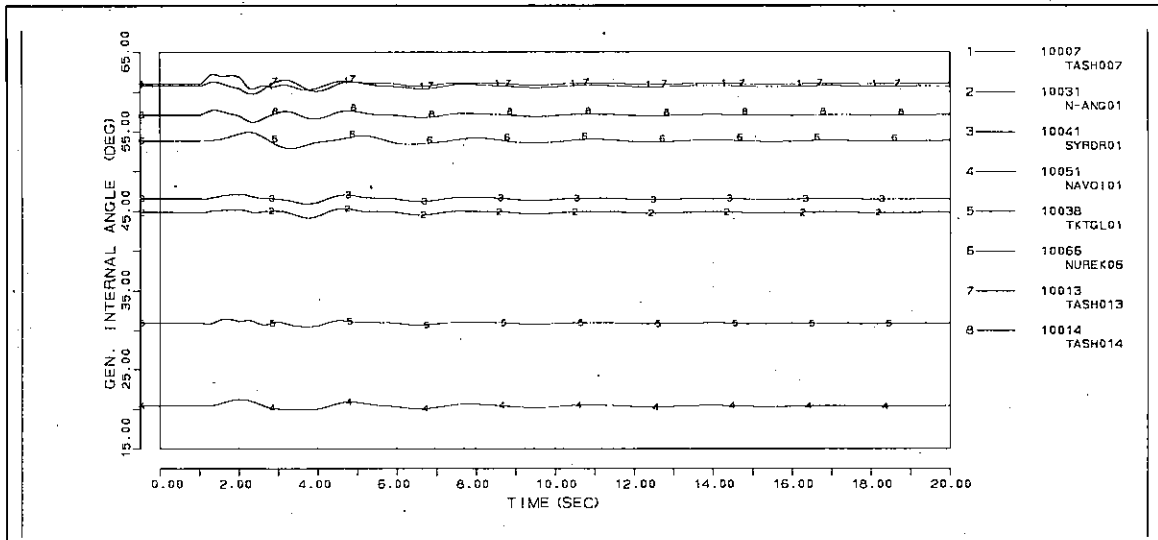


Figure 4.5-12 Static Stability

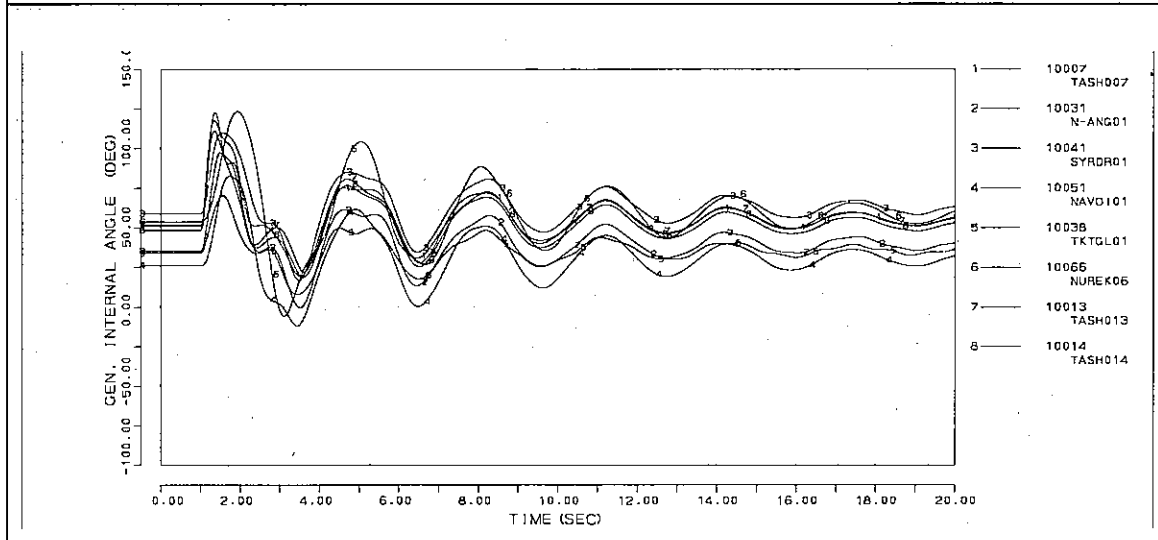


Figure 4.5-13 500kV TL Tashkent TPP-Symkent 2LGO

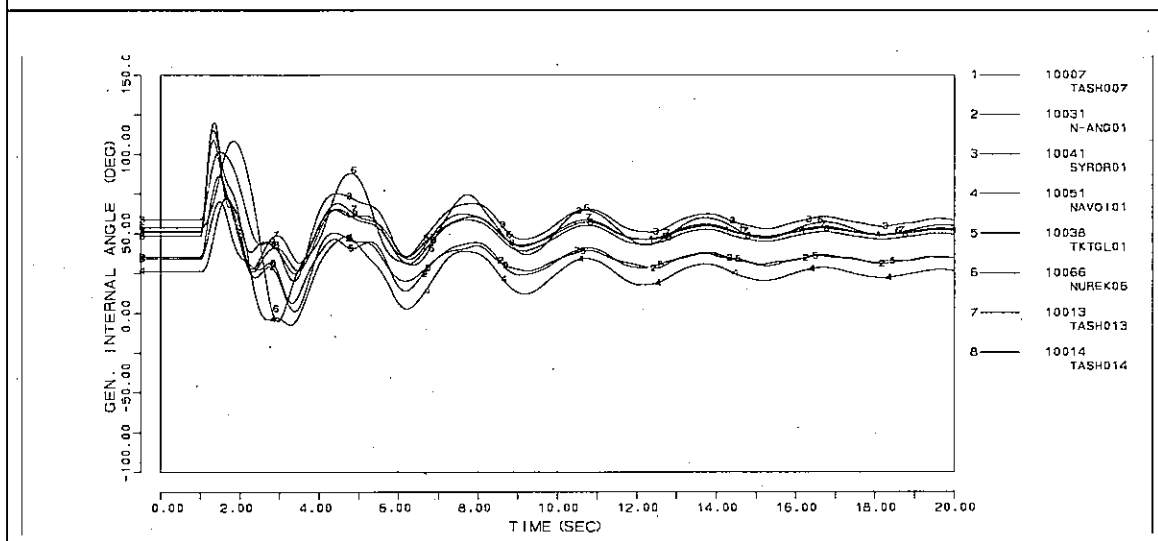


Figure 4.5-14 500kV TL Tashkent TPP-TashkentSS 2LGO

Summer Peak Calculation results

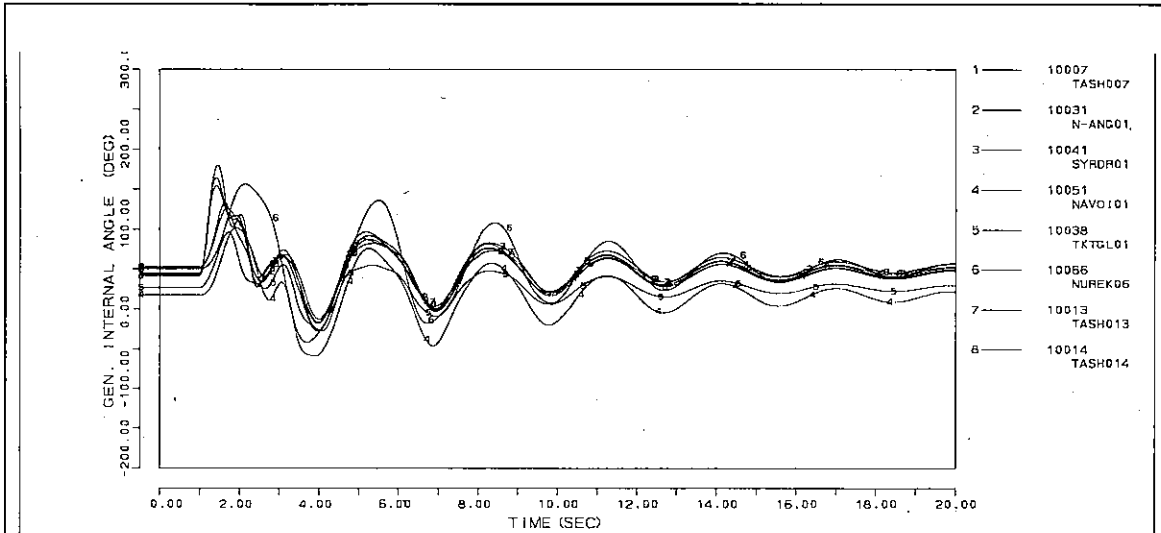


Figure 4.5-15 220kV TL Tashkent TPP-Uksak 2LGO

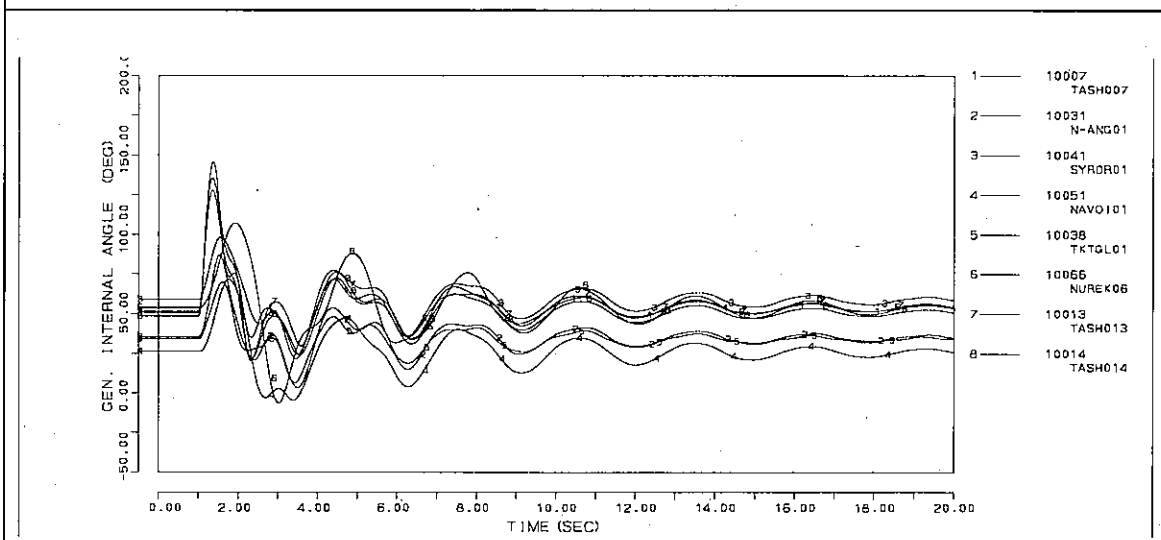


Figure 4.5-16 Tashkent TPP 500/220-Tr 2LGO

Summer Peak Calculation results

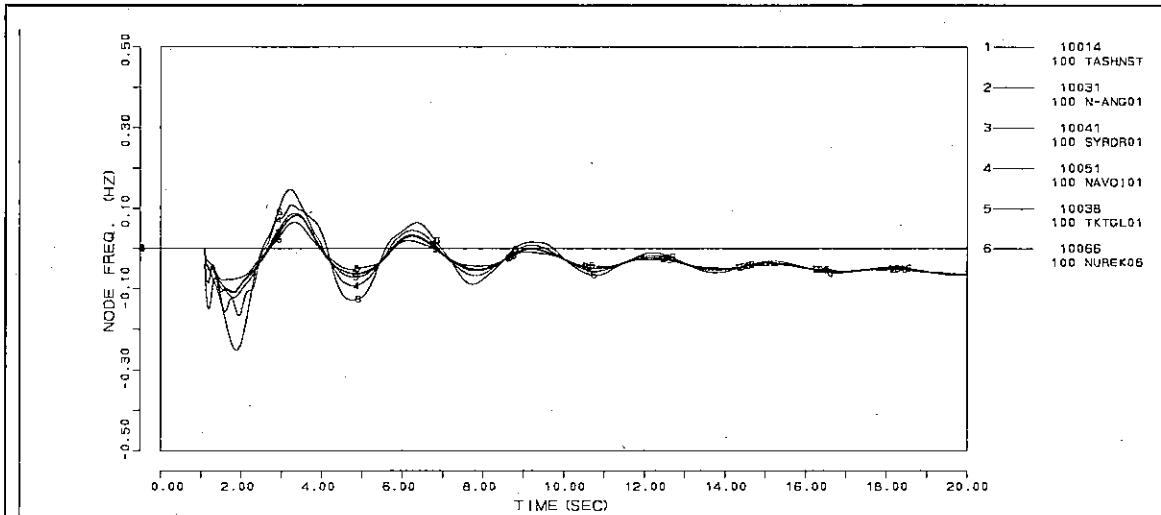


Figure 4.5-17 Tarimaljan 800MW generator drop out (frequency)

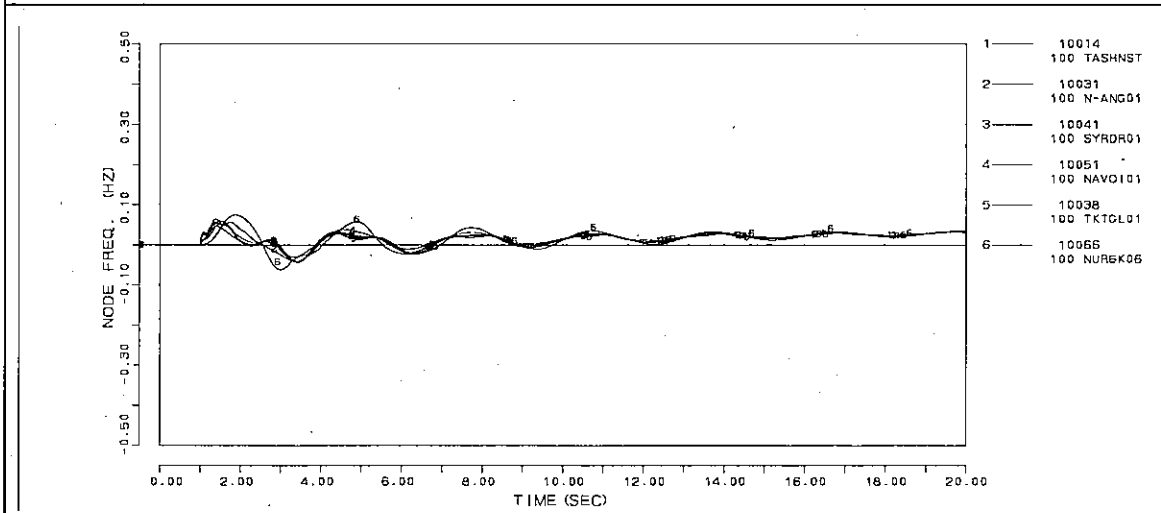


Figure 4.5-18 5% Load reduction (frequency)

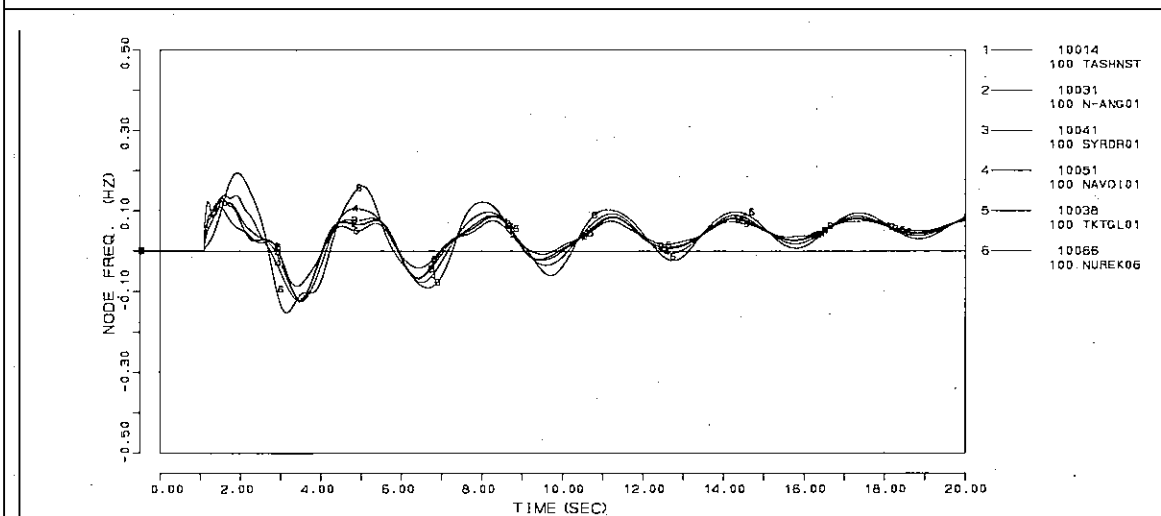


Figure 4.5-19 10% Load reduction (frequency)

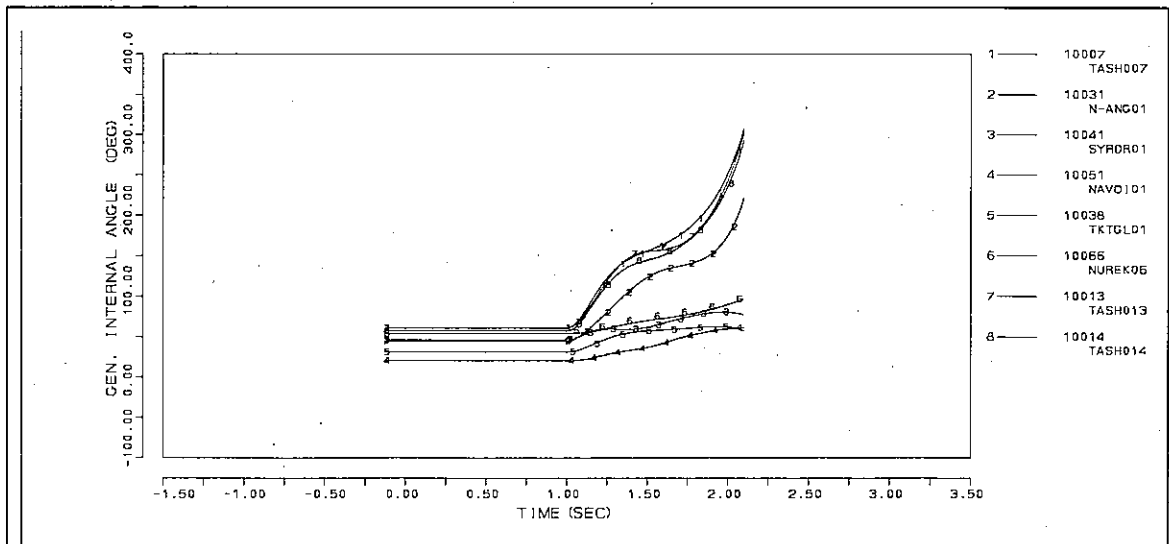


Figure 4.5-20 500kV TL TashkentSS-Syrdariya 3LGO

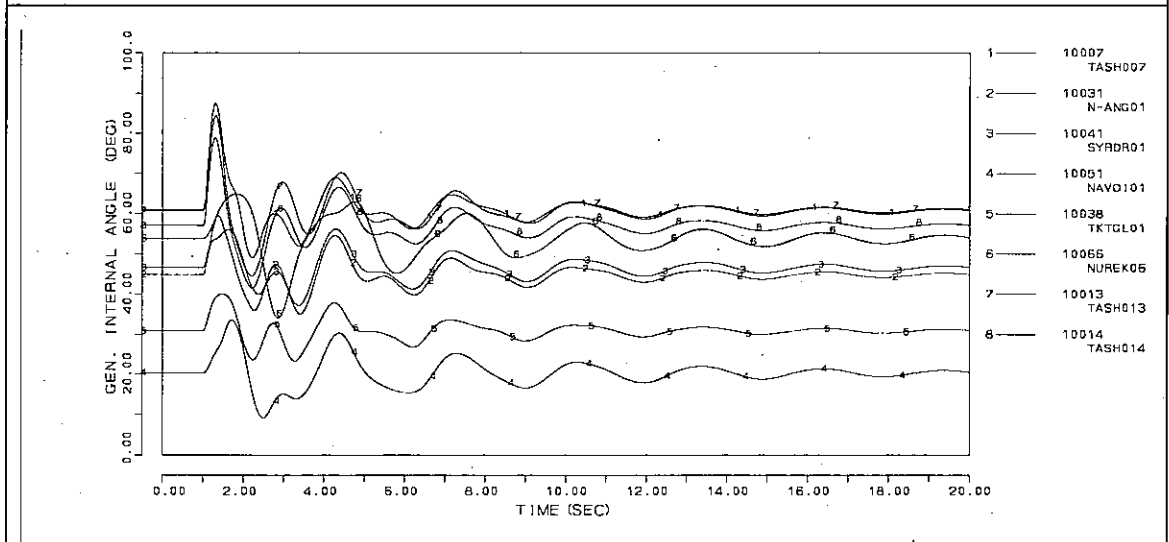


Figure 4.5-21 500kV TL TashkentSS-Syrdariya 1LGOC

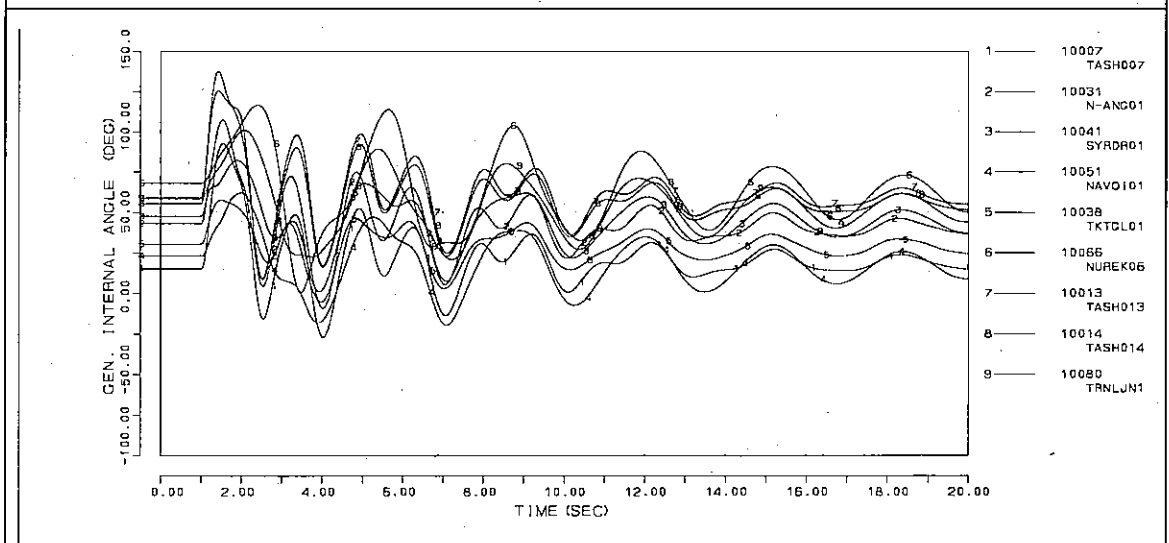


Figure 4.5-22 500kV TL TashkentSS-Syrdariya 3LGO with Tarimaljan

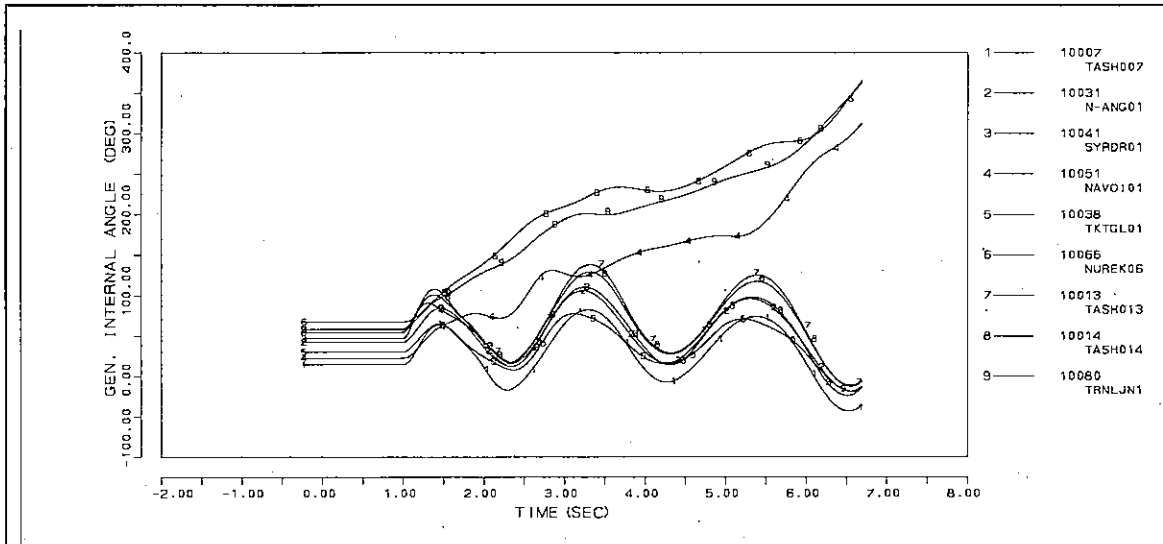


Figure 4.5-23 500kV TL Syrdarya-Guzar 3LGO with Tarimaljan

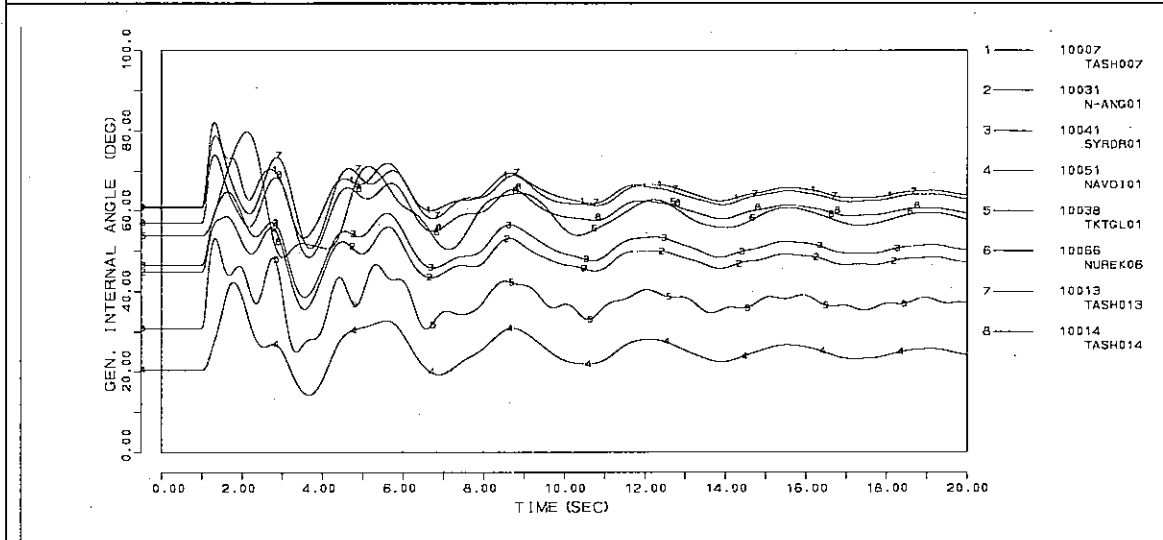


Figure 4.5-24 500kV TL Frunzen-Toktgul 3LGO

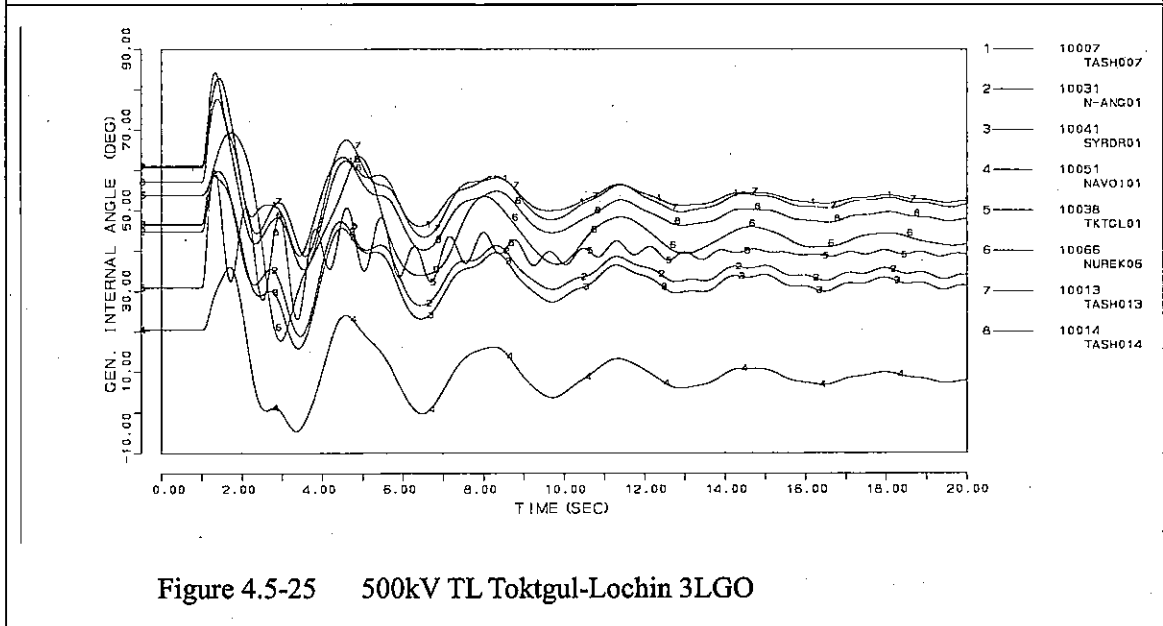


Figure 4.5-25 500kV TL Toktgul-Lochin 3LGO

**CHAPTER 5 IMPROVEMENT PLAN
FOR TASHKENT THERMAL
POWER PLANT
(DC “TASHTPP”)**

**THE DETAILED DESIGN STUDY FOR
MODERNIZATION OF TASHKENT THERMAL POWER PLANT
IN THE REPUBLIC OF UZBEKISTAN**

FINAL REPORT

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