

*Appendix B-11*  
*Civil Structure Calculation*

## CONTENTS

<b>1. General</b>	.....	B-11- 2
<b>2. Grit Chamber</b>	.....	B-11- 3
<b>3. Temporary Influent Pump Station</b>	.....	B-11- 22
<b>4. Primary Sedimentation Tank</b>	.....	B-11- 31
<b>5. Secondary Sedimentation Tank</b>	.....	B-11- 37
<b>6. Blower Equipment RC Platform</b>	.....	B-11- 42
<b>7. Distribution Chamber for Secondary Sedimentation Tank</b>	.....	B-11- 51
<b>8. Temporary Discharge Pump Station</b>	.....	B-11- 58
<b>9. Manhole type pump station (4 types)</b>	.....	B-11- 67
<b>10. Pile foundation</b>	.....	B-11- 74

## 1. General

### 1.1 Structure character

- 1) 9 structures are dealt in this structure calculation.( Refer to the contents)
- 2) 9 structures are basically the water container except for the blower platform and pile foundation.
- 3) Structure element and finish specificaton.  
Refer to each sub-section.
- 4) The structures are in-situ reinforced concrete.

### 1.2 Design principle.

- 1) Limit state design.  
Two types of limit state analysis were conducted.
  - a. Ultimate strength analysis
  - b. Serviceability limit state analysis- crack width  
Crack width of 0.2mm was set as an allowable value for the condition.
- 2) Dead Load, Live Load shall be taken into consideration in the calculation.  
Snow Load (Sn.L)is assumed as 100 kgf/cm<sup>2</sup>, but this note dose not use (Sn.L), because  
Roof Live Load 100 kgf/cm<sup>2</sup> covers enough for (Sn.L).
- 3) Seismic force  
Seismic force is not included in the external forces because Astana city is located in the no seismic area.
- 4) Up-lift  
Upward thrust against the structure by ground water was examined.

**2. Grit Chamber**

**2.1 Material and Allowable stress**

**TABLE 2.1 Allowable Stress** (N/mm<sup>2</sup>, kg/cm<sup>2</sup>)

Item		Serviceability strength			Ultimate strength		
		Compression	Tension	Shear	Compression	Tension	Shear
Concrete	B30	10		0.8	30		1.2
		100	-----	8	300	-----	12
Steel Bar Round Bar	A- I	157.0	157.0	157.0	235.4	235.4	235.4
		1600	1600	1600	2400	2400	2400
Steel Bar Deformed Bar	A- II	196.2	196.2	196.2	358.1	358.1	358.1
		2000	2000	2000	3650	3650	3650

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

**TABLE 2.2 Allowable Bonding Stress of Steel Bar to Concrete**

(N/mm<sup>2</sup>, kg/cm<sup>2</sup>)

Item	Serviceability strength		Remarks
	Top bars	Other bars	
φ6,φ9,φ12	0.9	1.3	
	9	13.5	
D10,D13,D16 D19,D22,D25,D29	1.6	2.4	
	16.2	24.3	

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

**2.2 Load Table**

**TABLE 2.3 Dead Load**

Loc.	item	thickness	kg/m <sup>2</sup>	total kg/m <sup>2</sup>	Remarks
Roof	Mortar	4cm	80		
	Concrete slab	15cm	360		
	Ceiling		25	465	<----- MKS UNIT
				4562	<----- SI UNIT
Common slab	Leveling motar	-	-		
	Concrete slab	20cm	500	500	<----- MKS UNIT
				4905	<----- SI UNIT

**TABLE 2.4 Live Load and Floor Load**

kg/m<sup>2</sup> (Girder, Sub beam : Self weight not included)

Loc.	load type	slab	beam	girder	Remarks
Roof	Dead Load	465.0	465.0	465.0	
	Live Load	100.0	100.0	100.0	Including snow 25cm depth
	Total Load	565.0	565.0	565.0	
	SI unit	5543	5543	5543	<----- SI UNIT
Machin room	Dead Load	500.0	500.0	500.0	
	Live Load	500.0	400.0	400.0	** add Machine load
	Total Load	1000.0	900.0	900.0	
	SI unit	9810	8829	8829	<----- SI UNIT
Other floor	Dead Load	500.0	500.0	500.0	
	Live Load	300.0	250.0	200.0	
	Total Load	800.0	750.0	700.0	
	SI unit	7848	7358	6867	<----- SI UNIT

2.3 Facility weight

Table2.5 Grit Chamber Weight

Story	Load type	Unit w (kN/m <sup>2</sup> ,m)	width /height (m) or unit	Length (m)	Area or L (m <sup>2</sup> ), (m)	Weight (kN)	Small Total (t)	S Wi (t)	
1st story	Roof slab	5.54	8	11.50	92.00	509.92			
	Machine rm	8.83	8	11.50	92.00	812.27			
	Other floor 1	6.87	8	4.30	34.40	236.22			
	Other floor 2	6.87	4.4	6.00	26.40	181.29			
	Other floor 3	6.87	8	6.80	54.40	373.56			
	Girder 11.5m	3.92	4	11.50	46.00	180.50			
	Girder 8m	3.92	4	8.00	32.00	125.57			
	Machine	(Included in the floor load)							
	Brick wall 3.5m	8.65	3.5	39.00	136.50	1181.06			
	Wall.1 6.3m	9.81	6.3	23.00	144.90	1421.47			
	Wall 2 1.4m	9.81	1.4	18.00	25.20	247.21			
	Wall 3 3.8m	9.81	3.8	23.10	87.78	861.12			
	Circle 1 7.3m	9.81	2.5	45.87	114.68	1125.04			
	Circle 2 1.85m	9.81	2.2	11.63	25.58	250.90			
	Water 1	9.81	4.43	3.50	15.51	152.10			
	Water 2	9.81	0.72	3.40	2.45	24.01			
	Water 3	9.81	3.6		41.85	1478.11			
	Water 4	9.81	5		2.69	131.85			
	Water 5	9.81	3	6.80	20.40	200.12			
								9492.35	9492.35
Base	t300 Base 1	7.36	4.4	6.00	26.40	194.24			
	t300 Base 2	7.36	2	45.36	90.73	667.54			
	t500 Base 1	12.26	8.4	3.90	32.76	401.72			
	t500 Base 2	12.26	2	5.52	11.03	135.27			
	t500 Base 3	12.26	7	8.40	58.80	721.04			
				Σ	219.72 (m <sup>2</sup> )		2119.80	11612.15 (kN)	

Base Area 219.72 (m<sup>2</sup>)

Total W= 11,612.15

W-Base= 9,492.3

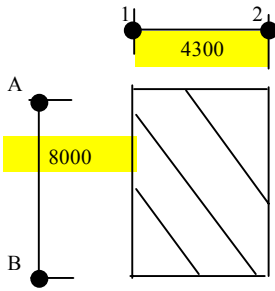
soil reaction =W/(Base area)= 52.850 (kN/m<sup>2</sup>)

Foundation's design force=	45.492 (kN/m <sup>2</sup> )
----------------------------	-----------------------------

2.4 FOUNDATION

1) Inlet chamber

Load condition



A = 34.4 m<sup>2</sup>

	Area	x	unit weight	kN
Floor slab=	34.40	x	7848.0=	269.97
Wall=	144.90	x	9.8=	1.42
			Σ =	271.4
	Soil reaction load=		7.89 kN/m <sup>2</sup>	
lx=	4.3 m			
ly=	8 m		t(cm)= 50	
λ =	1.86		d(cm)= 39	
			cover(cm)= 11	

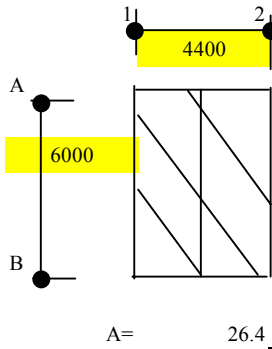
	a	wlx <sup>2</sup> (kNm <sup>2</sup> )	M(Nm)	Additional M from wall	Total M	at= M/(σ sjd)	re-bars	
Mx1=	0.078	145.87	11,378.1	194,680	206,058	30.776 cm <sup>2</sup>	bottom 9-D20-->D20@100	31.40cm <sup>2</sup>
Mx2=	0.052	145.87	7,585.4			0.982 cm <sup>2</sup>	upper 2-D10-->D10@200	3.93cm <sup>2</sup>
								0.9%
My1=	0.042	145.87	6,126.7	194,680	200,807	29.992 cm <sup>2</sup>	bottom 9-D20-->D20@100	31.40cm <sup>2</sup>
My2=	0.028	145.87	4,084.5			0.529 cm <sup>2</sup>	upper 2-D10-->D10@200	3.93cm <sup>2</sup>
		wlx	Q(N)			φ=Q/(τa jd)		0.9%
Qx =	0.52	33.92	17,640.5			2.17 cm <	62.8 ok	
Qy =	0.46	33.92	15,605.1			1.92 cm <	62.8 ok	

Suffix 1: end of span  
 Suffix 2: middle of span  
 From nomogram of two-way slab

Q cap  
 306,072 N > Q ok  
 306,072 N > Q ok

## 2) Water channel

### Load condition



Area		unit weight	kN
Floor slab=	26.40	x	7848.0= 207.19
Wall=	25.20	x	9.8= 0.25
			$\Sigma = 207.4$
Soil reaction load=			7.86 kN/m <sup>2</sup>
lx=	4.4	m	
ly=	6	m	t(cm)= 30
$\lambda =$	1.36		d(cm)= 19
			cover(cm)= 11

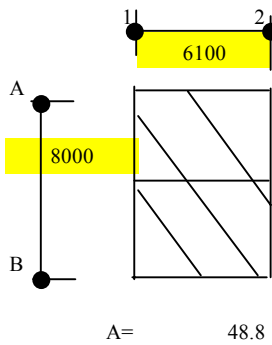
	a	wlx2(kNm <sup>2</sup> )	M(Nm)	Additional M from wall	Total M	at= M/( $\sigma$ sjd)	re-bars	
Mx1=	0.07	152.12	10,648.3		10,648	3.265 cm <sup>2</sup>	bottom 2-D10-->D10@200	3.93cm <sup>2</sup>
Mx2=	0.03	152.12	4,563.6			1.399 cm <sup>2</sup>	upper 2-D10-->D10@200	3.93cm <sup>2</sup>
								0.4%
My1=	0.042	152.12	6,389.0		6,389	1.959 cm <sup>2</sup>	bottom 2-D10-->D10@200	3.93cm <sup>2</sup>
My2=	0.028	152.12	4,259.3			1.306 cm <sup>2</sup>	upper 2-D10-->D10@200	3.93cm <sup>2</sup>
		wlx	Q(N)			$\phi=Q/(\tau a j d)$		0.4%
Qx =	0.51	34.57	17,631.9			4.45 cm <	15.7 ok	
Qy =	0.46	34.57	15,903.3			4.01 cm <	15.7 ok	

Suffix 1: end of span  
 Suffix 2: middle of span  
 From nomogram of two-way slab

Q cap  
 149,112 N > Q ok  
 149,112 N > Q ok

## 3) Outlet chamber

### Load condition



Area		unit weight	kN
Floor slab=	54.40	x	7848.0= 426.93
Wall=	87.78	x	9.8= 0.86
			$\Sigma = 427.8$
Soil reaction load=			8.77 kN/m <sup>2</sup>
lx=	6.1	m	
ly=	8	m	t(cm)= 50
$\lambda =$	1.31		d(cm)= 39
			cover(cm)= 11

	a	wlx2(kNm <sup>2</sup> )	M(Nm)	Additional M from wall	Total M	at= M/( $\sigma$ sjd)	re-bars	
Mx1=	0.068	326.19	22,181.0	62,784	84,965	12.690 cm <sup>2</sup>	bottom 5-D18-->D18@200	12.70cm <sup>2</sup>
Mx2=	0.028	326.19	9,133.4			1.364 cm <sup>2</sup>	upper 2-D10-->D10@200	3.93cm <sup>2</sup>
								0.4%
My1=	0.042	326.19	13,700.0	62,784	76,484	11.424 cm <sup>2</sup>	bottom 5-D18-->D18@200	12.70cm <sup>2</sup>
My2=	0.028	326.19	9,133.4			1.364 cm <sup>2</sup>	upper 2-D10-->D10@200	3.93cm <sup>2</sup>
		wlx	Q(N)			$\phi=Q/(\tau a j d)$		0.4%
Qx =	0.5	53.47	26,737.0			3.29 cm <	28.26 ok	
Qy =	0.46	53.47	24,598.1			3.02 cm <	28.26 ok	

Suffix 1: end of span  
 Suffix 2: middle of span  
 From nomogram of two-way slab

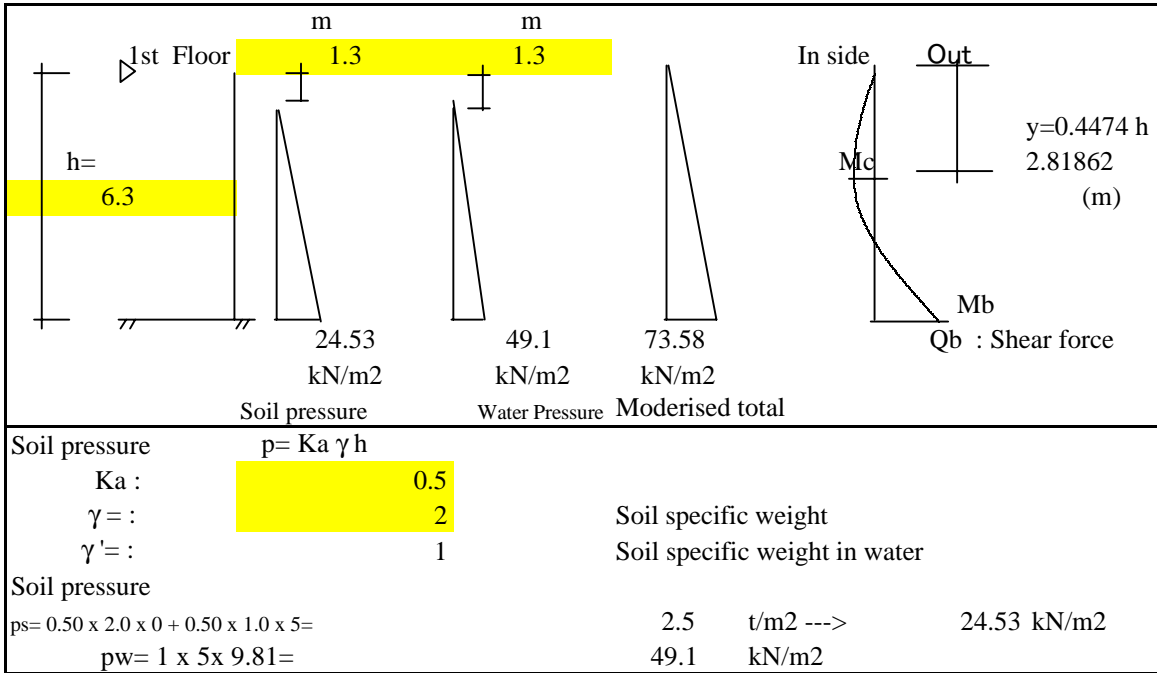
Q cap  
 306,072 N > Q ok  
 306,072 N > Q ok

2.5 Grit chamber wall W2-1

(1/4)

LOAD CONDITION

For wall's unit width (1m)



BENDING MOMENT and SHEAR FORCE

For wall's unit width			
$M_c = 0.06 W h =$	87.61 kNm	$W = 721.77 \times 6.3 / 2$	231.8 kN
$M_b = -2/15 W h =$	-194.68 kNm		
$Q_b = 4/5 W =$	185.41 kN		

Wall Profile

	external	inner
Wall thickness $t :$	40 cm	re-bar inside
$d :$	32 cm	35 cm
$j = 7/8 d :$	0.280 m	0.306 m
Re bar $f_t :$	200 N/mm <sup>2</sup> (196.2 $\approx$ 200)	200 N/mm <sup>2</sup>
$a_t = M_c / (f_t \times j) =$	14.30 cm <sup>2</sup> / (m w)	5 - D20
$a_t = M_b / (f_t \times j) =$	34.76 cm <sup>2</sup> / (m w)	10 - D25
		15.71 cm <sup>2</sup>
		49.09 cm <sup>2</sup>
		w $M_c = 0.49 \%$
		w $M_b = 1.53 \%$

Wall Shear Stress

Wall thickness $t :$	40 cm
$d :$	32 cm
$j = 7/8 d :$	0.280 m
Width $W_a :$	100 cm
$Q_b :$	185.41 kN
Shear stress $= Q_b / (W_a \times j) =$	0.66 N/mm <sup>2</sup> < 0.8 N/mm <sup>2</sup>

Bottom profile

slab thickness $t :$	50 cm	
$d :$	39 cm	
$j = 7/8 d :$	0.341 m	
Re bar $f_t :$	200 N/mm <sup>2</sup>	
$a_t = M_b / (f_t \times j) =$	28.52 cm <sup>2</sup> / (m w)	10 - D22
		38.01 cm <sup>2</sup>
		w $M_c = 0.97 \%$

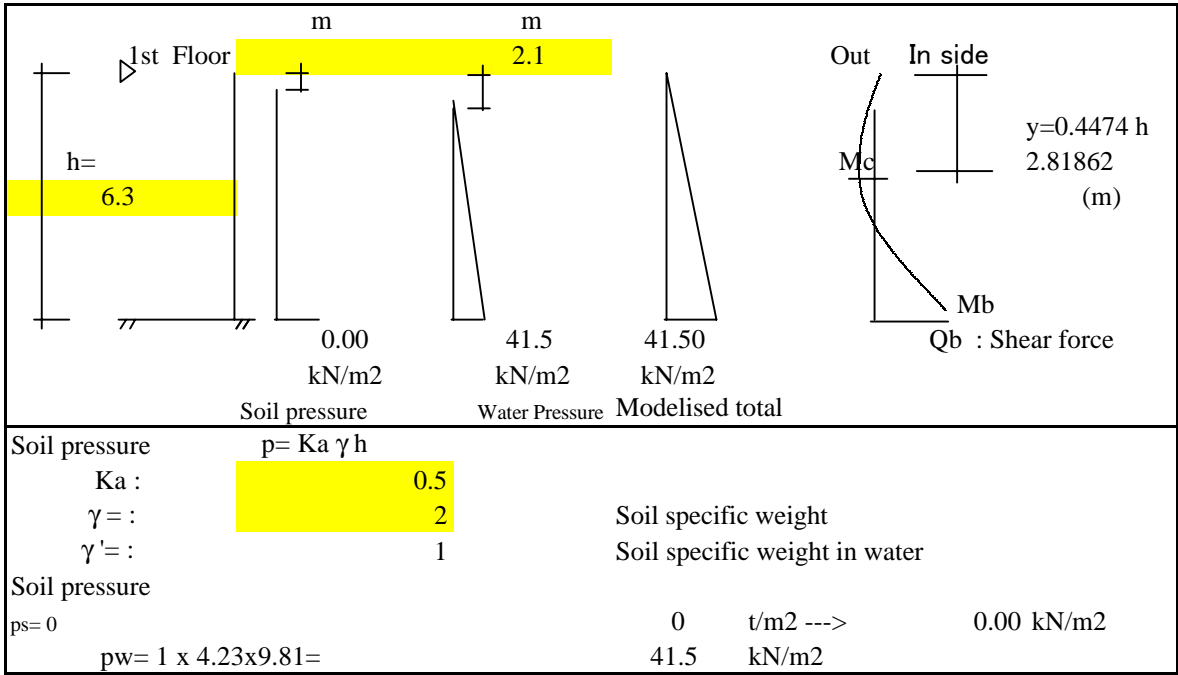


W2-2

(2/4)

**LOAD CONDITION**

For wall's unit width (1m)



**BENDING MOMENT and SHEAR FORCE**

For wall's unit width			
$M_c = 0.06 W h =$	49.41 kNm	$W = 6.3 \times 407.08/2$	130.7 kN
$M_b = -2/15 W h =$	-109.80 kNm		
$Q_b = 4/5 W =$	104.57 kN		

**Wall Profile**

	external	inner	
Wall thickness $t$ :	40 cm	re-bar inside	
$d$ :	32 cm	35	
$j = 7/8 d$ :	0.280 m	0.30625 m	
Re bar $f_t$ :	200 N/mm <sup>2</sup>	200 N/mm <sup>2</sup>	
$a_t = M_c / (f_t \times j) =$	8.07 cm <sup>2</sup> / (m w)	5 - D22	19.01 cm <sup>2</sup>
$a_t = M_b / (f_t \times j) =$	19.61 cm <sup>2</sup> / (m w)	10 - D20	31.42 cm <sup>2</sup>
		$w M_c =$	0.59 %
		$w M_b =$	0.98 %

**Wall Shear Stress**

Wall thickness $t$ :	40 cm
$d$ :	32 cm
$j = 7/8 d$ :	0.280 m
Width $W_a$ :	100 cm
$Q_b$ :	104.57 kN
Shear stress = $Q_b / (W_a \times j) =$	0.37 N/mm <sup>2</sup> < 0.8 N/mm <sup>2</sup>

**Bottom profile**

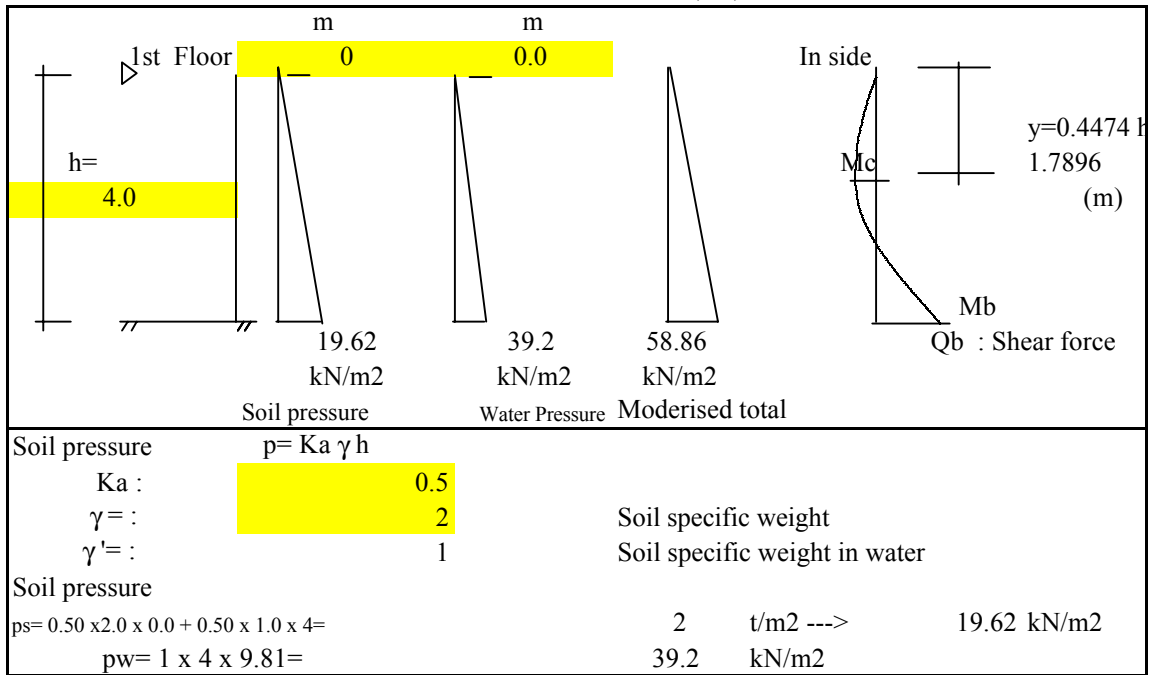
slab thickness $t$ :	50 cm		
$d$ :	39 cm		
$j = 7/8 d$ :	0.341 m		
Re bar $f_t$ :	200 N/mm <sup>2</sup>		
$a_t = M_b / (f_t \times j) =$	16.09 cm <sup>2</sup> / (m w)	10 - D22	38.01 cm <sup>2</sup>
		$w M_c =$	0.97 %

W2-3

(3/4)

**LOAD CONDITION**

For wall's unit width (1m)

**BENDING MOMENT and SHEAR FORCE**

For wall's unit width			
$M_c = 0.06 W h =$	28.25 kNm	$W = 4.0 \times 58.86 / 2 =$	117.7 kN
$M_b = -2/15 W h =$	-62.78 kNm		
$Q_b = 4/5 W =$	94.18 kN		

**Wall Profile**

	external	inner	
Wall thickness $t :$	40 cm	re-bar inside	
$d :$	32 cm	35	
$j = 7/8 d :$	0.280 m	0.30625 m	
Re bar $f_t :$	200 N/mm <sup>2</sup>	200 N/mm <sup>2</sup>	
$a_t = M_c / (f_t \times j) =$	4.61 cm <sup>2</sup> / (m w	5 - D14	7.70 cm <sup>2</sup>
$a_t = M_b / (f_t \times j) =$	11.21 cm <sup>2</sup> / (m w	10 - D14	15.39 cm <sup>2</sup>
		$w M_c =$	0.24 %
		$w M_b =$	0.48 %

**Wall Shear Stress**

Wall thickness $t :$	40 cm
$d :$	32 cm
$j = 7/8 d :$	0.280 m
Width $W_a :$	100 cm
$Q_b :$	94.18 kN
Shear stress $= Q_b / (W_a j) =$	0.34 N/mm <sup>2</sup> < 0.8 N/mm <sup>2</sup>

**Bottom profile**

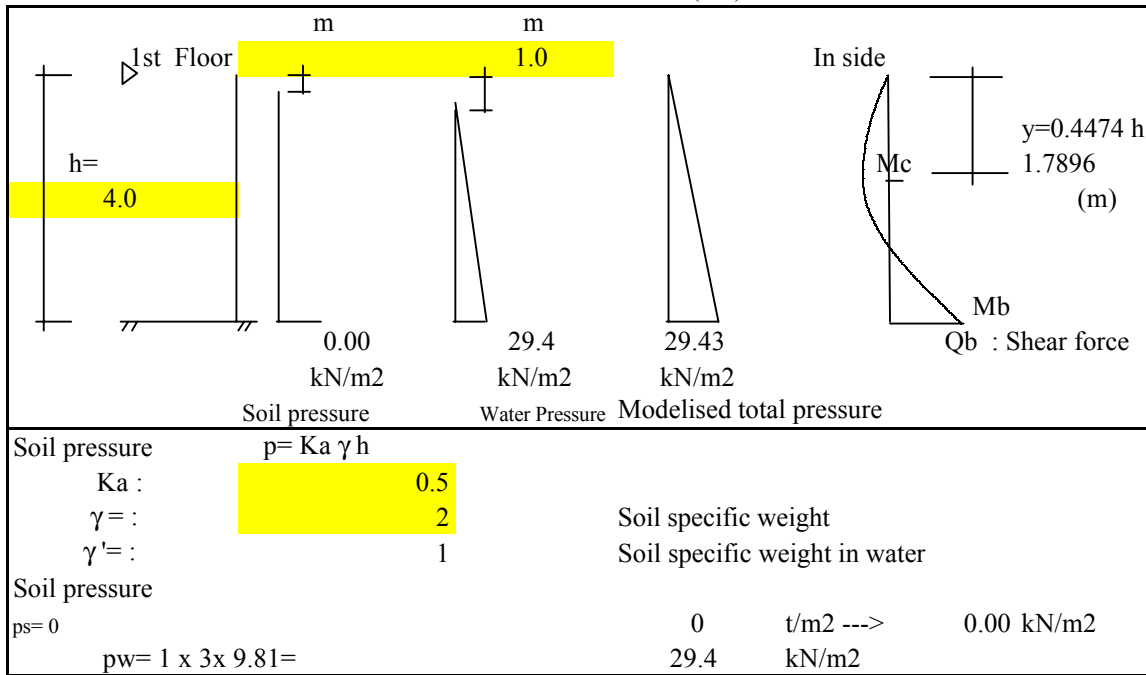
slab thickness $t :$	50 cm		
$d :$	39 cm		
$j = 7/8 d :$	0.341 m		
Re bar $f_t :$	200 N/mm <sup>2</sup>		
$a_t = M_b / (f_t \times j) =$	9.20 cm <sup>2</sup> / (m w	10 - D22	38.01 cm <sup>2</sup>
		$w M_c =$	0.97 %

W2-4

(4/4)

## LOAD CONDITION

For wall's unit width (1m)



## BENDING MOMENT and SHEAR FORCE

For wall's unit width			
$M_c = 0.06 W h =$	14.13 kNm	$W = 4.0 \times 29.43 / 2 =$	58.9 kN
$M_b = -2/15 W h =$	-31.39 kNm		
$Q_b = 4/5 W =$	47.09 kN		

## Wall Profile

	external	inner	
Wall thickness $t :$	40 cm	re-bar inside	
$d :$	32 cm	35	
$j = 7/8 d :$	0.280 m	0.30625 m	
Re bar $f_t :$	200 N/mm <sup>2</sup>	200 N/mm <sup>2</sup>	
$a_t = M_c / (f_t \times j) =$	2.31 cm <sup>2</sup> / (m width)	5 - D14	7.70 cm <sup>2</sup>
$a_t = M_b / (f_t \times j) =$	5.61 cm <sup>2</sup> / (m width)	10 - D14	15.39 cm <sup>2</sup>
		w $M_c :$	0.24 %
		w $M_b :$	0.48 %

## Wall Shear Stress

Wall thickness $t :$	40 cm
$d :$	32 cm
$j = 7/8 d :$	0.280 m
Width $W_a :$	100 cm
$Q_b :$	47.09 kN
Shear stress $= Q_b / (W_a \times j) =$	0.17 N/mm <sup>2</sup> < 0.8 N/mm <sup>2</sup>

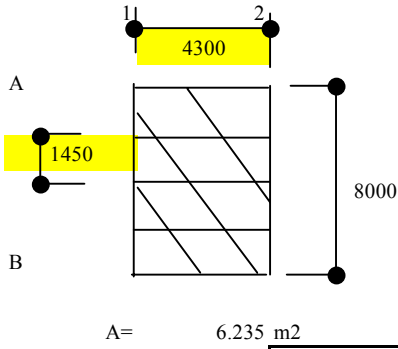
## Bottom profile

slab thickness $t :$	50 cm		
$d :$	39.0 cm		
$j = 7/8 d :$	0.341 m		
Re bar $f_t :$	200.00 N/mm <sup>2</sup>		
$a_t = M_b / (f_t \times j) =$	4.60 cm <sup>2</sup> / (m width)	10 - D14	15.39 cm <sup>2</sup>
		w $M_c :$	0.3947138 %

2.6 SLAB

1) Inlet chamber

Load condition



Floor slab=	6.24	x	7848.0=	48.93
Wall=	0.00	x	0.0=	0.00
			$\Sigma =$	48.9
lx=	4.3	m		
ly=	1.45	m	t(cm)=	20
$\lambda =$	2.97		d(cm)=	15
			cover(cm)=	5

	a	wlx2(kNm2)	M(Nm)	Additional M from wall	Total M	at= M/( $\sigma$ sjd)	re-bars	
Mx1=	0.083	16.50	1,369.5		1,370	0.532 cm2	upper 2-D10-->D10@200	3.93cm2
Mx2=	0.042	16.50	693.0			0.269 cm2	bottom 2-D10-->D10@200	3.93cm2
								0.5%
My1=	0.042	16.50	693.0	0	693	0.269 cm2	upper 2-D10-->D10@200	3.93cm2
My2=	0.028	16.50	462.0			0.179 cm2	bottom 2-D10-->D10@200	3.93cm2
		wlx	Q(N)			$\phi=Q/(\tau a jd)$		0.5%
Qx =	0.52	11.38	5,917.4			1.89 cm <	15.7 ok	
Qy =	0.46	11.38	5,234.6			1.67 cm <	15.7 ok	

Suffix 1: end of span

Suffix 2: middle of span

From nomogram of two-way slab

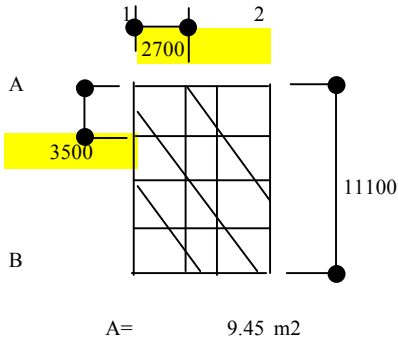
Q cap

117,720 N > Q ok

117,720 N > Q ok

2) Machine room

Load condition



Floor slab=	9.45	x	9810.0=	92.70
Wall=		x		
			$\Sigma =$	92.7
lx=	2.7	m		
ly=	3.5	m	t(cm)=	25
$\lambda =$	1.30		d(cm)=	20
			cover(cm)=	5

	a	wlx2(kNm2)	M(Nm)	Additional M from wall	Total M	at= M/( $\sigma$ sjd)	re-bars	
Mx1=	0.068	71.51	4,863.0		4,863	1.416 cm2	upper 2-D10-->D10@200	3.93cm2
Mx2=	0.028	71.51	2,002.4			0.583 cm2	bottom 2-D10-->D10@200	3.93cm2
								0.4%
My1=	0.042	71.51	3,003.6	0	3,004	0.875 cm2	upper 2-D10-->D10@200	3.93cm2
My2=	0.028	71.51	2,002.4			0.583 cm2	bottom 2-D10-->D10@200	3.93cm2
		wlx	Q(N)			$\phi=Q/(\tau a jd)$		0.4%
Qx =	0.5	26.49	13,243.5			3.17 cm <	15.7 ok	
Qy =	0.46	26.49	12,184.0			2.92 cm <	15.7 ok	

Suffix 1: end of span

Suffix 2: middle of span

From nomogram of two-way slab

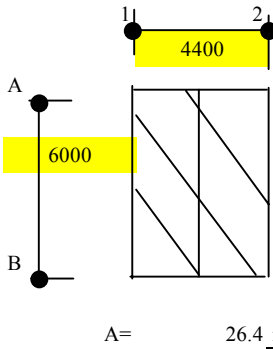
Q cap

156,960 N > Q ok

156,960 N > Q ok

### 3) Water channel

#### Load condition



Area		unit weight	kN
Floor slab=	13.20	x	7848.0= 103.59
Wall=		x	0.00
		$\Sigma$ =	103.6
$l_x$ =	2.2 m	$t(\text{cm})$ =	20
$l_y$ =	6 m	$d(\text{cm})$ =	15
$\lambda$ =	2.73	cover(cm)=	5

A= 26.4 m<sup>2</sup>

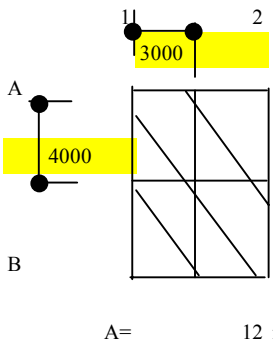
	a	wlx2(kNm <sup>2</sup> )	M(Nm)	Additional M from wall	Total M	at= M/( $\sigma$ sjd)	re-bars	
Mx1=	0.083	37.98	3,152.7		3,153	1.224 cm <sup>2</sup>	bottom 2-D10-->D10@200	3.93cm <sup>2</sup>
Mx2=	0.042	37.98	1,595.3			0.620 cm <sup>2</sup>	upper 2-D10-->D10@200	3.93cm <sup>2</sup>
My1=	0.042	37.98	1,595.3		1,595	0.620 cm <sup>2</sup>	bottom 2-D10-->D10@200	3.93cm <sup>2</sup>
My2=	0.028	37.98	1,063.6			0.413 cm <sup>2</sup>	upper 2-D10-->D10@200	3.93cm <sup>2</sup>
		wlx	Q(N)			$\phi=Q/(\tau a j d)$		0.5%
Qx =	0.51	17.27	8,805.5			2.81 cm <	15.7 ok	
Qy =	0.46	17.27	7,942.2			2.54 cm <	15.7 ok	

Suffix 1: end of span  
 Suffix 2: middle of span  
 From nomogram of two-way slab

Q cap  
 117,720 N > Q ok  
 117,720 N > Q ok

### 4) Outlet chamber

#### Load condition



Area		unit weight	kN
Floor slab=	12.00	x	7848.0= 94.18
Wall=		x	0.00
		$\Sigma$ =	94.2
$l_x$ =	3 m	$t(\text{cm})$ =	25
$l_y$ =	4 m	$d(\text{cm})$ =	20
$\lambda$ =	1.33	cover(cm)=	5

A= 12 m<sup>2</sup>

	a	wlx2(kNm <sup>2</sup> )	M(Nm)	Additional M from wall	Total M	at= M/( $\sigma$ sjd)	re-bars	
Mx1=	0.083	70.63	5,862.5		5,862	1.707 cm <sup>2</sup>	bottom 2-D10-->D10@200	3.93cm <sup>2</sup>
Mx2=	0.042	70.63	2,966.5			0.864 cm <sup>2</sup>	upper 2-D10-->D10@200	3.93cm <sup>2</sup>
My1=	0.042	70.63	2,966.5		2,967	0.864 cm <sup>2</sup>	bottom 2-D10-->D10@200	3.93cm <sup>2</sup>
My2=	0.028	70.63	1,977.7			0.576 cm <sup>2</sup>	upper 2-D10-->D10@200	3.93cm <sup>2</sup>
		wlx	Q(N)			$\phi=Q/(\tau a j d)$		0.4%
Qx =	0.51	23.54	12,007.4			2.88 cm <	15.7 ok	
Qy =	0.46	23.54	10,830.2			2.59 cm <	15.7 ok	


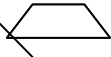
Suffix 1: end of span  
 Suffix 2: middle of span  
 From nomogram of two-way slab

Q cap  
 156,960 N > Q ok  
 156,960 N > Q ok

2.7 BEAMS

1) Grit chamber machine room **B1**

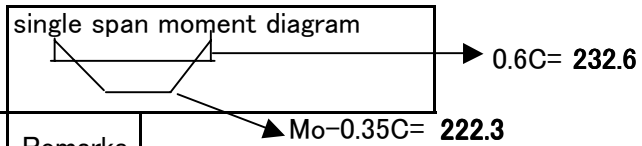
Typical example of the beam is the short side of rectangle beneath the wall.

B1	Load form	 (slab load)	 (slab load)	(girder load)+		Σ		
				other loads				
	Co	C/w 23.18	Co 204.72	Co/w 0.00	Co 0.00	w/l 47.46	Co 182.88	kNm 387.60
bxD 40x60	Mo	M/w 9.48	Mo 83.68	Mo/w 0.00	Mo 0.00	w/l 47.46	Mo 274.32	kNm 357.99
(cm)	Q	Q/w 10.45	Q 92.25	Q/w 0.00	Q 0.00	w/l 47.46	Q 161.36	kN 253.61
Slab load =		8.83 (kN/m <sup>2</sup> )		ly=	3.5 m			
Span =		6.8 (m)		lx=	2.27 m			λ= 1.54

1. Girder load 9.40 kN/m  
dead load

2. Line load = 0.00 kN/m + 38.06 kN/m = 38.06 kN/m  
roof wall

Total = 47.46 kN/m



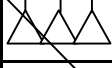
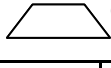
2) Determination of beam B1

Beam ID	B1			Remarks
Position	B end	Mid	C end	
D.L ] M(kNm) top	232.6		232.6	
+ ] bott.		222.3		
L.L ] Q (kN)	253.61		253.61	
] b x D (cm)	50	x	80	
Size ] d (cm)			75	
] j (cm)			65.625	
top	18.1		18.1	cm <sup>2</sup> at= M/(σ sjd)
	4D25		4D25	
bottom		17.3		cm <sup>2</sup>
		4D25		
τ=Q/bjd	0.77		0.77	N/mm <sup>2</sup>
top	0.52		0.52	min.0.4%
Pt (%) bott.		0.52		
top	19.64		19.64	
at (cm <sup>2</sup> ) bott.		19.64		
Main top	5	5	5	
Bars		D25		
bott	5	5	5	
φ (cm)	39.25		39.25	max 1.7
Q /fa.j (cm)	0.98		0.98	
judge	ok		ok	
fs.bj LT(ST)	252.7		252.7	kN
(t)	D10-250	D10-250	D10-250	
judge	ok		ok	

seismic force neglected

2) Grit chamber machine room

**B2**

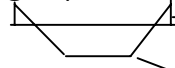
B1  bxD 40x60 (cm)	Load form	 (slab load)	 (slab load) x2	(girder load)+ other loads		Σ	
	Co	C/w 23.35	Co/w 23.24	Co 205.19	w/l 5.64	Co 5.76	kNm 210.94
	Mo	M/w 9.33	Mo/w 23.60	Mo 208.39	w/l 5.64	Mo 8.64	kNm 217.03
	Q	Q/w 10.28	Q/w 2.67	Q 23.59	w/l 5.64	Q 9.87	kN 33.46
Slab load =		8.83 (kN/m <sup>2</sup> )	ly=	3.5 m			
Span =		3.5 (m)	lx=	2.25 m			λ= 1.56

1. Girder load = 5.64 kN/m  
dead load

2. Line load = 0.00 kN/m + 0.00 kN/m = 0.00 kN/m  
roof wall

Total = 5.64 kN/m

single span moment diagram



0.6C = 126.6

Mo - 0.35C = 143.2

seismic force neglected

2) Determination of beam B1

Beam ID	B1			Remarks
Position	B end	Mid	C end	
D.L ] M(kNm) top	126.6		126.6	
+ ] bott.		143.2		
L.L ] Q (kN)	33.46		33.46	
] b x D (cm)	40	x	60	
Size ] d (cm)			55	
] j (cm)			48.125	
top	13.4		13.4	cm <sup>2</sup>
	3D25		3D25	at= M/(σ sjd)
bottom		15.2		cm <sup>2</sup>
		3D28		
τ=Q/bjd	0.10		0.10	N/mm <sup>2</sup>
top	0.43		0.43	min.0.4%
Pt (%) bott.		0.84		
top	9.42		9.42	
at (cm <sup>2</sup> ) bott.		18.48		
Main Bars	top	3	3	3
		D28		
		D28		
	bott	3	3	3
φ (cm)	23.55		23.55	
Q / fa.j (cm)	0.30		0.30	max
judge	ok		ok	1.7
fs.bj LT(ST)	148.2		148.2	kN
(t)	D10-250	D10-250	D10-250	
judge	ok		ok	

**1) Spec of Tank**

Diameter	d	<input type="text" value="7.3"/>	m	Unit Water load	DI	1.0 t/m <sup>3</sup> =	<input type="text" value="9.81"/>	kN/m <sup>3</sup>
Water Depth	h	<input type="text" value="1.8"/>	m	Supporting condition of bottom :		Rigid		
Wall Thickness	t	<input type="text" value="400"/>	mm			$\alpha e$ :	<input type="text" value="0"/>	
Wall height	h1	<input type="text" value="2.7"/>	m	f st =	<input type="text" value="120"/>	N/mm <sup>2</sup>		
				f ct =	<input type="text" value="2.00"/>	N/mm <sup>2</sup>	f cu=	<input type="text" value="30"/>
Unit concrete weight		<input type="text" value="23.544"/>	N/m <sup>3</sup>			permissible tensile stress		not used

**2) Employed Equation for analysis**

\*Max circumferential tension in wall due to internal pressure

$$N \max = 0.5 \cdot K3 \cdot D1 \cdot h \cdot d$$

K3: coefficient by Table 184 in "Reinforced Concrete Designer's Handbook"

DI: 9.81 kN/m<sup>3</sup>

h: Water Depth (m)

d: Diameter (m)

$$Re. As = 0.5 \cdot K3 \cdot D1 \cdot h \cdot d / f_{st}$$

f<sub>st</sub>: permissible rebar tensile stress

\*Vertical bending moment at the tank bottom

$$M \max = K1 \cdot DI \cdot h^3$$

K1: coefficient by Table 184 in "Reinforced Concrete Designer's Handbook"

\*Minimum thickness of Wall

$$T \min = DI \cdot h \cdot d / 2 \cdot [1 / f_{ct} - (\alpha e - 1) / f_{st}]$$

f<sub>ct</sub>: permissible concrete tensile stress

f<sub>st</sub>: permissible rebar tensile stress

$\alpha e$ : modular ratio

\*Direct compression in wall of empty underground tank

$$f_{cc} = 1/2 \cdot q_{ep} \cdot d / (t + (\alpha e - 1) \cdot As)$$

q<sub>ep</sub>: external pressure/m<sup>2</sup> at depth h1

t: wall thickness

**3) Forces and Bending Moment /Reinforcement**

$$0 \quad h^2/d/t = \boxed{1.1096} \quad \text{then} \quad K1 = \boxed{0.045} \quad K2 = \boxed{0.55} \quad K3 = \boxed{0.26}$$

By table 184, pp.405

1 BM at bottom =  kN/m

2 Position height of max tension =  m above the bottom

3 Max circumference tension =  kN/m around the position of the above

4 Required As =  cm<sup>2</sup>

5 Min. thickness of wall =  mm

6 Direct comp. =  kN/m<sup>2</sup>

=  N/mm<sup>2</sup>

Reinforcement

5	D10
5	D10

As =  cm<sup>2</sup>

pt =  %



#### 4) Foundation

**Effect of water pressure**

Ground Level = 348.0 m  
 Ground Water Level = 345 m  
 Bottom slab level = 347.0 m  
 Height of Bottom slab = 0.4 m  
 Soffit of bottom slab = (1.6) m

Upward thrust by water pressure

$$p = 9.81 \text{ kN/m}^3 \times (1.6) = -15.70 \text{ kN/m}^2$$

$$A = 62.21 \text{ m}^2 \text{ (including wall thickness)}$$

$$P = -976 \text{ kN}$$

#### Bottom slab depth

\*Basement including structure wall must be designed to prevent flotation

Weight

GL slab 585.9 kN (Slab thickness 0.4 m)

wall 615.1 kN

Total 1201 kN

$$\text{Required weight for bottom } (-976) - 1201 = -2177.455426 \text{ kN}$$

$$\text{Minimum dept } F_s=1.0 \quad t = -1.49 \text{ m}$$

\*No upward thrust will affect to this structure

The depth shall be decided by the structural-----:  $t = 0.5 \text{ m}$

Serviceability Check: by NJC

2.9 Limit state analysis

Rectangular section design and limited state analysis				( 1/3 )	
Concrete Permissible Strength		$f'_{ck} =$	17 N/mm <sup>2</sup>	by use of B30 30	
Direct tensile stress		$f_t =$	2.00 N/mm <sup>2</sup>		
Elasticity ratio		$n =$	15		
Elasticity		$E =$	200000 N/mm <sup>2</sup>		
Permissible strength		$\sigma_{sa} =$	250 N/mm <sup>2</sup>	round from BS	
		$\sigma_{sa} =$	140 N/mm <sup>2</sup>	deforme from BS	
Ultimate strength (characteristic strength)		$\sigma_s =$	365 N/mm <sup>2</sup>		
Check point				Foundation	Wall
Force	Bending Moment	Md	kN·m	206.1	194.7
	Shearing force	Sd	kN	17.6	185.4
Section Spec	Width	b	cm	100	100
	Height	h	cm	50	40
	Cover	dt	cm	5	5
	Effective Height	d	cm	45	35
Rebar Cross Section	Tension Rebar		cm <sup>2</sup>	10— D25	
				As= 49.09	
	Compression Rebar		cm <sup>2</sup>	5— D10	
				As= 3.93	
Stress	Concrete stress		N/mm <sup>2</sup>	5.2	
	Rebar stress		N/mm <sup>2</sup>	107.6	
	Shearing stress		N/mm <sup>2</sup>	0.046	
B.M value for crack		Mcr	kNm	72.12	46.76
Crack width	Rebar interval	cs	mm	100	100
	Rebar diameter	$\phi$	mm	25	25
	Cover depth	c	mm	40	40
	Rebar stress	$\sigma_{se}$	N/mm <sup>2</sup>	108.6	132.3
	<b>Crack width</b>	wcr	mm	0.147	0.172
<b>Judgement: wcr&lt;0.2: OK</b>				<b>OK</b>	<b>OK</b>
Examination with the Ultimate BM Strength					
Ultimate B.M Strength		Mud	kNm	729.75	558.79
$\gamma_i \cdot Md / Mud$				0.282	0.348
Judgement: $\gamma_i \cdot Md / Mud < 1.0$ : OK				OK	OK
Crack width shall be controled as follows:					
		1 normal condition	crack width < 0.3mm		
		2 severe condition	crack width < 0.2mm		
		3 very severe condition	crack width < 0.1mm		

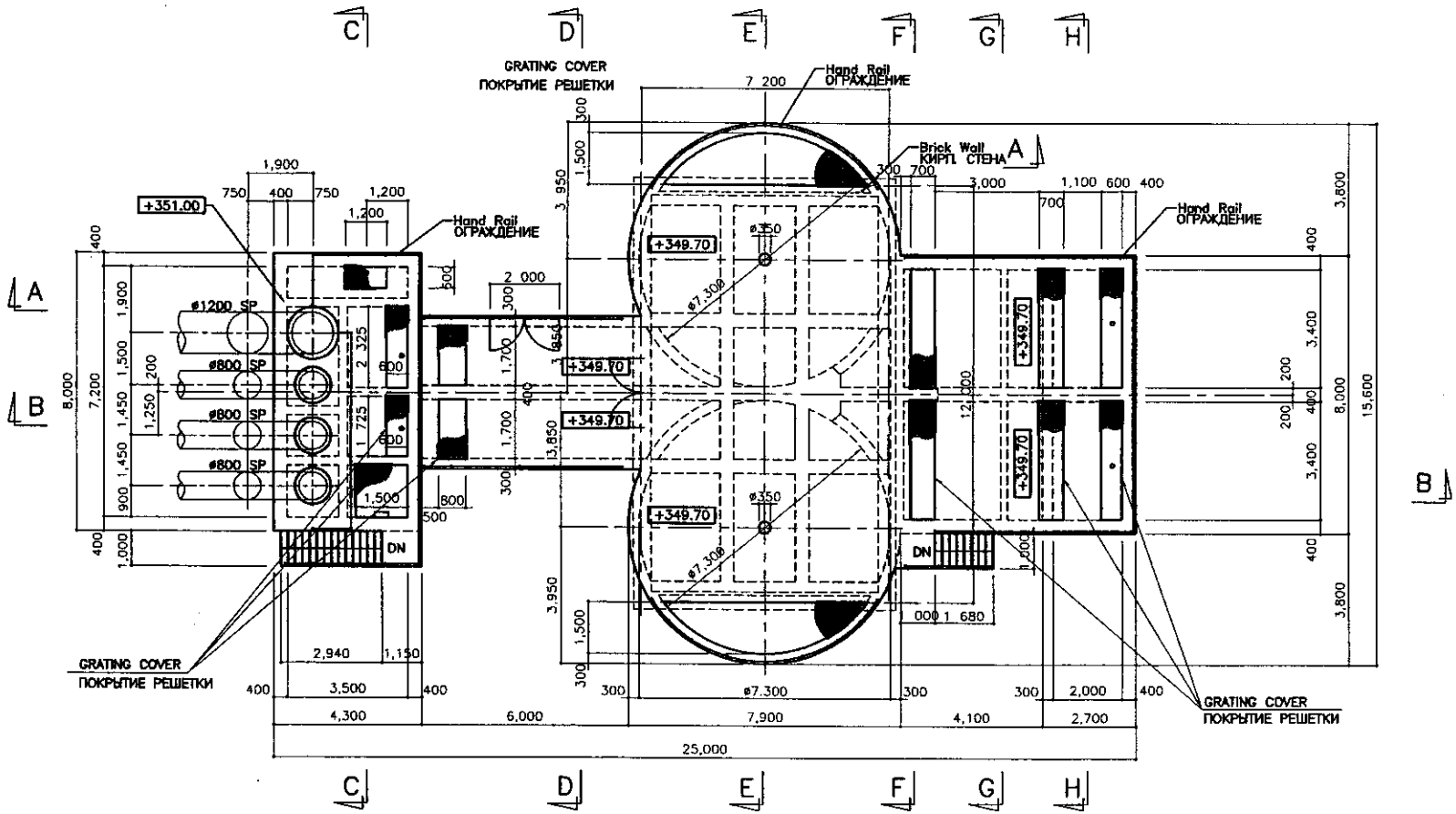
<b>Rectangular section design and limited state analysis</b>				( 2/3 )	
Concrete Permissible Strength		$f'_{ck} =$	17 N/mm <sup>2</sup>	by use of B30	30
Direct tensile stress		$f_t =$	2.00 N/mm <sup>2</sup>		
Elasticity ratio		$n =$	15		
Elasticity		$E =$	200000 N/mm <sup>2</sup>		
Permissible strength		$\sigma_{sa} =$	250 N/mm <sup>2</sup>	round from BS	
		$\sigma_{sa} =$	140 N/mm <sup>2</sup>	deforme from BS	
Ultimate strength (characteristic strength)		$\sigma_s =$	365 N/mm <sup>2</sup>		
Check point			Slab	Beam 1	
Force	Bending Moment	Md	kN·m	5.9	232.6
	Shearing force	Sd	kN	12.0	253.6
Section Spec	Width	b	cm	100	50
	Height	h	cm	25	80
	Cover	dt	cm	5	5
	Effective Height	d	cm	20	75
Rebar Cross Section	Tension Rebar		cm <sup>2</sup>	5— D10	
				As= 3.93	
	Compression Rebar		cm <sup>2</sup>	5— D10	
				As= 3.93	
Stress	Concrete stress		N/mm <sup>2</sup>	1.2	
	Rebar stress		N/mm <sup>2</sup>	78.6	
	Shearing stress		N/mm <sup>2</sup>	0.064	
B.M value for crack		Mcr	kNm	12.88	75.22
Crack width	Rebar interval	cs	mm	80	100
	Rebar diameter	$\phi$	mm	10	25
	Cover depth	c	mm	40	40
	Rebar stress	$\sigma_{se}$	N/mm <sup>2</sup>	79.7	139.9
	<b>Crack width</b>	wcr	mm	0.115	0.181
<b>Judgement: wcr&lt;0.2: OK</b>				<b>OK</b>	<b>OK</b>
Examination with the Ultimate BM Strength					
Ultimate B.M Strength		Mud	kNm	37.52	639.39
$\gamma_i \cdot Md / Mud$				0.156	0.364
Judgement: $\gamma_i \cdot Md / Mud < 1.0$ : OK				OK	OK
Crack width shall be controled as follows:					
		1 normal condition		crack width < 0.3mm	
		2 severe condition		crack width < 0.2mm	
		3 very severe condition		crack width < 0.1mm	

8.7 Limit state analysis

Rectangular section design and limited state analysis				( 3/3 )	
Concrete Permissible Strength	$f'_{ck} =$	17 N/mm <sup>2</sup>	by use of B30	30	
Direct tensile stress	$f_t =$	2.00 N/mm <sup>2</sup>			
Elasticity ratio	$n =$	15			
Elasticity	$E =$	200000 N/mm <sup>2</sup>			
Permissible strength	$\sigma_{sa} =$	250 N/mm <sup>2</sup>	round from BS		
	$\sigma_{sa} =$	140 N/mm <sup>2</sup>	deforme from BS		
Ultimate strength (characteristic strength)	$\sigma_s =$	365 N/mm <sup>2</sup>			

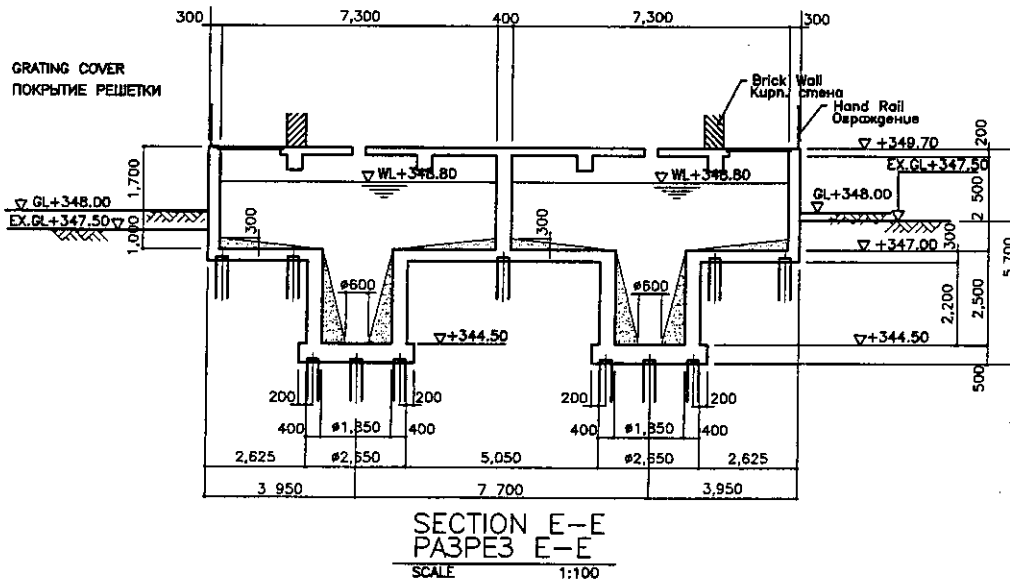
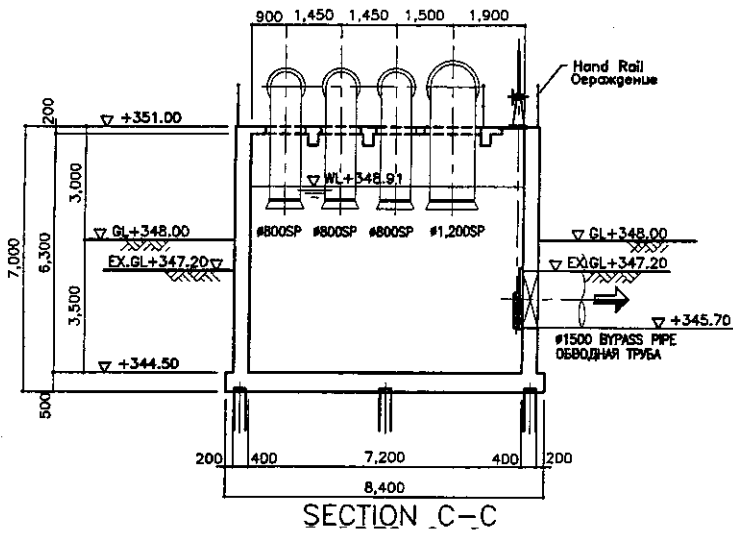
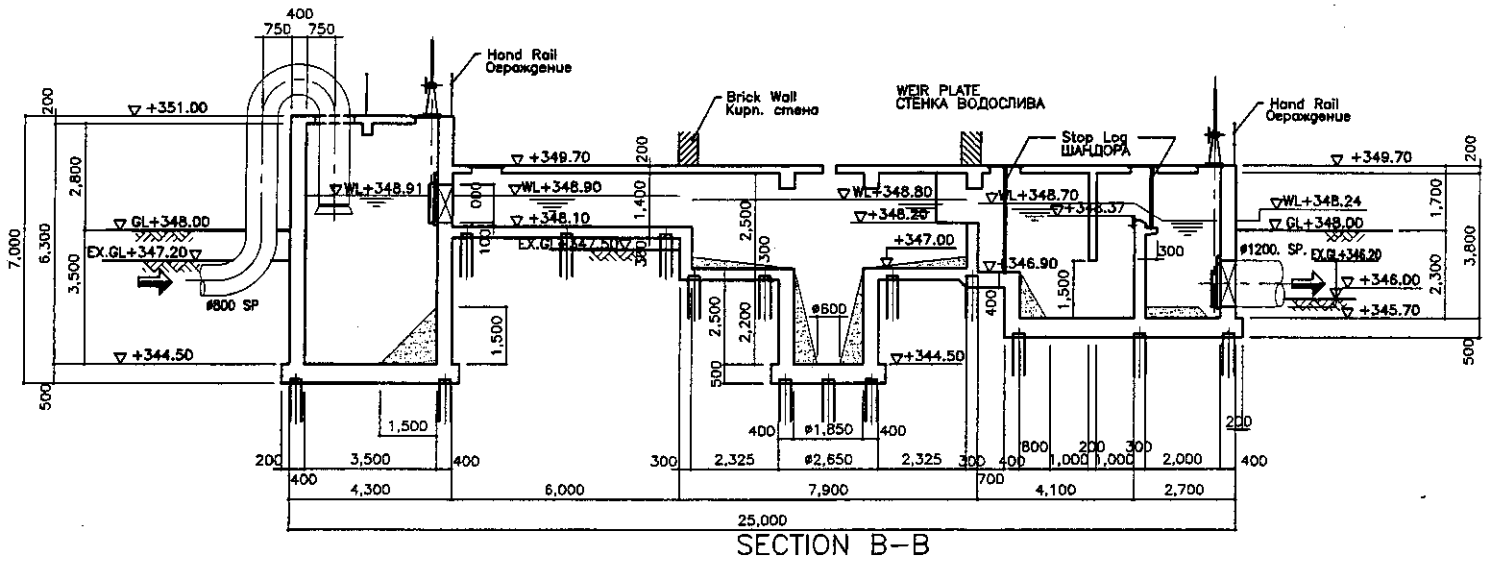
  

Check point				Beam 2 end	Beam 2 mid		
Force	Bending Moment	Md	kN·m	126.6	143.2		
	Shearing force	Sd	kN	33.5	0.0		
Section Spec	Width	b	cm	40	40		
	Height	h	cm	60	60		
	Cover	dt	cm	5	5		
	Effective Height	d	cm	55	55		
Rebar Cross Section	Tension Rebar		cm <sup>2</sup>	3— D28	3— D28		
				As = 18.47	As = 18.47		
	Compression Rebar		cm <sup>2</sup>	3— D28	3— D28		
				As = 18.47	As = 18.47		
Stress	Concrete stress		N/mm <sup>2</sup>	4.1	4.6		
	Rebar stress		N/mm <sup>2</sup>	133.5	151.0		
	Shearing stress		N/mm <sup>2</sup>	0.170	0.000		
B.M value for crack				Mcr	kNm	34.96	34.96
Crack width	Rebar interval	cs	mm	80	80		
	Rebar diameter	$\phi$	mm	28	28		
	Cover depth	c	mm	40	40		
	Rebar stress	$\sigma_{se}$	N/mm <sup>2</sup>	139.1	157.4		
	<b>Crack width</b>	wcr	mm	0.166	0.184		
<b>Judgement: wcr &lt; 0.2: OK</b>				<b>OK</b>	<b>OK</b>		
Examination with the Ultimate BM Strength							
Ultimate B.M Strength		Mud	kNm	346.96	346.96		
$\gamma_i \cdot Md / Mud$				0.365	0.413		
Judgement: $\gamma_i \cdot Md / Mud < 1.0$ : OK				OK	OK		
Crack width shall be controled as follows:							
		1 normal condition	crack width < 0.3mm				
		2 severe condition	crack width < 0.2mm				
		3 very severe condition	crack width < 0.1mm				



B-11-20

Grit chamber structure 2/2



### 3. Temprrary Influent Pumping Station

#### 3.1 Material and Allowable stress

**TABLE 3.1 Allowable Stress** (N/mm<sup>2</sup>, kg /cm<sup>2</sup>)

Item		Serviceability strength			Ultimate strength		
		Compression	Tension	Shear	Compression	Tension	Shear
Concrete	B30	10	0.8	30	1.2		
		100	8	300	12		
Steel Bar Round Bar	A- I	157.0	157.0	157.0	235.4	235.4	235.4
		1600	1600	1600	2400	2400	2400
Steel Bar Deformed Bar	A- II	196.2	196.2	196.2	358.1	358.1	358.1
		2000	2000	2000	3650	3650	3650

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

**TABLE 3.2 Allowable Bonding Stress of Steel Bar to Concrete**

(N/mm<sup>2</sup>, kg /cm<sup>2</sup>)

Item	Serviceability strength		Remarks
	Top bars	Other bars	
φ6,φ9,φ12	0.9	1.3	
	9	13.5	
D10,D13,D16 D19,D22,D25,D29	1.6	2.4	
	16.2	24.3	

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

#### 3.2 Load Table

**TABLE 3.3 Dead Load**

Loc.	item	thickness	kg/m <sup>2</sup>	total kg/m <sup>2</sup>	Remarks
Common slab	Leveling motar	-	-		
	Concrete slab	20cm	500	500	<----- MKS UNIT
				4905	<----- SI UNIT

**TABLE 3.4 Live Load and Floor Load**

kg/m<sup>2</sup> (Girder, Sub beam : Self weight not included)

Loc.	load type	slab	beam	girder	Remarks
Other floor	Dead Load	500.0	500.0	500.0	
	Live Load	1000.0	1000.0	1000.0	Load of heay equipment
	Total Load	1500.0	1500.0	1500.0	
	SI unit	14715	14715	14715	<----- SI UNIT

#### 3.3 Facility weight

**Table3.4 Temp. I.P.S Weight**

Story	Load type	Unit w (kN/m <sup>2</sup> ,m)	width /hight (m) or unit	Length (m)	Area or L (m <sup>2</sup> ), (m)	Weight (kN)	Small Total (kN)	S Wi (kN)
structure	slab	14.72	7	-	62.39	918.05		
	Beam 6m	2.94	1	6.00	6.00	17.66		
	Beam 3m*2	2.94	2	3.00	6.00	17.66		
	Machine	34.335	3	-	-	103.01		
	Wall.1 9.03m	12.263	9.03	20.42	184.40	2261.16		
	Water	9.81	9.03	28.27	255.32	2504.67		
							5822.20	5822.20
Base	t600 Base	14.72	1	28.27	28.27	416.06		
				Σ	28.27	(m <sup>2</sup> )	416.06	(kN)

Base Area 28.27 (m<sup>2</sup>)

Total W= 6,238.25

W-Base= 5,822.2

soil reaction =W/(Base area) 220.633 (kN/m<sup>2</sup>)

Foundation's design force= 205.918 (kN/m<sup>2</sup>)

3.3.Wall of cylindrical tanks for Temp IPS

( / )

1) Spec of Tank

Diameter	d	<input type="text" value="6"/>	m	Unit Water load	DI	1.0	t/m <sup>3</sup> =	<input type="text" value="9.81"/>	kN/m <sup>3</sup>
Water Depth	h	<input type="text" value="4.427"/>	m	Supporting condition of bottom :	Rigid				
Wall Thickness	t	<input type="text" value="500"/>	mm		$\alpha$ e:			<input type="text" value="15"/>	
Wall height	h1	<input type="text" value="9.027"/>	m	f st =	<input type="text" value="120"/>	N/mm <sup>2</sup>			
				f ct =	<input type="text" value="2.00"/>	N/mm <sup>2</sup>	f cu=	<input type="text" value="30"/>	
Unit concrete weight		<input type="text" value="23.544"/>	kN/m <sup>3</sup>	permissible tensile stress			not used		

2) Employed Equation for analysis

\*Same with the former section

3) Forces and Bending Moment /Reinforcement

0  $h^2/d/t = \text{input } 6.53$  then  $K1 = \text{input } 0.0175$   $K2 = \text{input } 0.42$   $K3 = \text{input } 0.54$   
 By table 184, pp.405

- 1 BM at bottom=  kN/m
- 2 Position height of max tension =  m above the bottom
- 3 Max circumference tension =  kN/m around the position of the above
- 4 Required As=  cm<sup>2</sup>

- 5 Min. thickness of wall =  mm
- 6 Direct comp.=  kN/m<sup>2</sup>  
 =  N/mm<sup>2</sup>

Reinforcement	
<input type="text" value="4-D16"/>	/m
<input type="text" value="4-D16"/>	/m
As =	<input type="text" value="16.085"/> cm <sup>2</sup>
pt =	<input type="text" value="0.3217"/> % > 0.3%
<input type="text" value="4-D14"/>	/m

7 Distribution Rebar 1 rank lower spec. of main rebar ----->

3.2. Foundation

1) Effect of water pressure

Ground Level =	<input type="text" value="345.0"/>	m
Ground Water Level =	<input type="text" value="343"/>	m
Bottom slab level=	<input type="text" value="336.0"/>	m
Height of Bottom slab=	<input type="text" value="0.6"/>	m
Soffit of bottom slab=	<input type="text" value="7.6"/>	m

Upward thrust by water pressure

p=  kN/m<sup>3</sup> ×  =  kN/m<sup>2</sup>  
 A=  m<sup>2</sup> (including wall thickness)  
 P=  kN

2) Bottom slab depth and reinforcement

\*Basement including structure wall must be designed to prevent flotation

Weight		
GL slab	<input type="text" value="236.7"/>	kN (Slab thickness <input type="text" value="0.2"/> m)
wall	<input type="text" value="2170"/>	kN
<b>Total</b>	<input type="text" value="2407"/>	<b>kN</b>

Cohesion Force  kN/m<sup>2</sup>  m<sup>2</sup> =

\*no cohesion Required weight for bottom  -  =  kN  
 Minimum depth  $F_s=1.0$   $t = \text{input } 1.14$  m

\*cohesion included  -  =  kN

When cohesion force between wall and soil included, additional depth for bottom slab is not necessary.

The depth shall be decided by the structural requirements. ----->  $t = \text{input } 0.6$  m

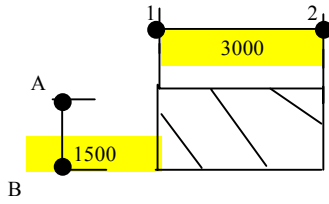
\*Reinforcement

Radial reinforcement



### 3.4 Slab

#### Load condition



	Area	unit weight	kN
Floor slab=	4.50	x	14,715.0
Wall=		x	0.00
			$\Sigma = 66.2$
	Soil reaction load=		14.72 kN/m2

lx=	1.5 m	t(cm)=	20
ly=	3 m	d(cm)=	15
$\lambda =$	2.00	cover(cm)=	5

A= 4.5 m2

	a	wlx2(kNm2)	M(Nm)	Additional M from wall	Total M	at= M/( $\sigma$ sjd)	re-bars	
Mx1=	0.078	33.11	2,582.5	0	2,582	1.003 cm2	bottom 2-D10-->D10@100	7.85cm2
Mx2=	0.052	33.11	1,721.7			0.669 cm2	upper 2-D10-->D10@100	7.85cm2
								1.0%
My1=	0.042	33.11	1,390.6	0	1,391	0.540 cm2	bottom 2-D10-->D10@100	7.85cm2
My2=	0.028	33.11	927.0			0.360 cm2	upper 2-D10-->D10@100	7.85cm2
		wlx	Q(N)			$\phi=Q/(\tau a j d)$		1.0%
Qx =	0.52	22.07	11,477.7			3.67 cm <	31.4 ok	
Qy =	0.46	22.07	10,153.4			3.24 cm <	31.4 ok	

Suffix 1: end of span  
 Suffix 2: middle of span  
 From nomogram of two-way slab

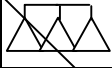
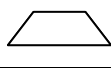
Q cap  
 117,720 N > Q ok  
 117,720 N > Q ok

### 3.4 FOUNDATION

3.5 BEAMS

1) Beam

**B1**

B1  bxD 40x60 (cm)	Load form	 (slab load)	 (slab load) *2	(girder load)+ other loads		Σ		
	Co	C/w 0.00	Co 0.00	Co/w 7.03	Co 103.42	w/l 4.11	Co 3.08	kNm 106.51
	Mo	M/w 0.00	Mo 0.00	Mo/w 7.22	Mo 106.25	w/l 4.11	Mo 4.63	kNm 110.87
	Q	Q/w 0.00	Q 0.00	Q/w 1.69	Q 24.83	w/l 4.11	Q 6.17	kN 31.00
	Slab load =	14.715 (kN/m <sup>2</sup> )		ly=	3 m		λ= 2.00	
Span =	3 (m)		lx=	1.50 m				

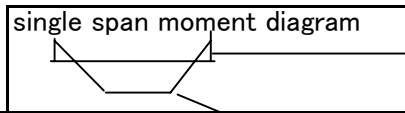
1.Girder load= 4.11 kN/m

dead load

2.Line load = 0.00 kN/m + 0.00 kN/m = 0.00 kN/m

roof wall

Total = 4.11 kN/m



0.6C= 63.9

▲ Mo-0.35C= 73.6


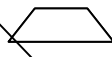
seismic force neglected

2) Determination of beam B1

Beam ID	B1			Remarks
Position	B end	Mid	C end	
D.L ] M(kNm)	63.9		63.9	
+ ] bott.		73.6		
L.L ] Q(kN)	31.00		31.00	
] b x D (cm)	35	x	50	
Size ] d (cm)			45	
] j(cm)			39.375	
top	8.3		8.3	cm <sup>2</sup> at= M/(σ sjd)
	3D22		3D22	
bottom		9.5		cm <sup>2</sup>
		3D22		
τ=Q/bjd	0.22		0.22	N/mm <sup>2</sup>
top	0.72		0.72	min.0.4%
Pt (%) bott.		0.72		
top	11.4		11.4	
at (cm <sup>2</sup> ) bott.		11.4		
Main Bars	3	D22	3	
	3	3	3	
φ (cm)	20.724		20.724	max 1.7
Q/fa.j (cm)	0.38		0.38	
judge	ok		ok	
fs.bj LT(ST)	106.1		106.1	kN
(t)	D10-250	D10-250	D10-250	
judge	ok		ok	

2) Girder

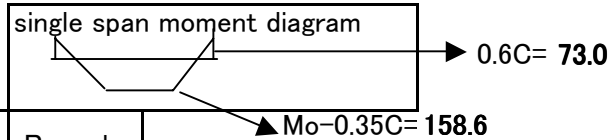
G1

	Load form	(slab load)		(slab load)		P (gider load)+		Σ
		 Co/w	Co	 Co/w	Co	w/l	Co	
2B2	Co	8.16	120.02	-	0.00	0.56	1.69	121.71
bxD 30x75	Mo	13.50	198.65	-	0.00	0.56	2.53	201.18
	Q	6.75	99.33	-	0.00	0.56	1.69	101.01
Slab load =		14.715 (kN/m <sup>2</sup> )		ly= 3.00 m				
Span =		6 (m)		lx= 3.00 m				λ= 1.00

1. Girder load = 5.64 kN/m  
 dead load

2. Line load = 0.00 kN/m + 0.00 kN/m = 0.00 kN/m  
 roof wall

Total = 5.64 kN/m



2) Determination of beam B1

Beam ID	B1			Remarks
Position	B end	Mid	C end	
D.L ] M (kNm)		73.0	73.0	
+ ] bott.		158.6		
L.L ] Q (kN)		101.01	101.01	
] b x D (cm)	40	x	60	
Size ] d (cm)			55	
] j (cm)			48.125	
top	7.7		7.7	cm <sup>2</sup> at= M/(σ sjd)
	3D20		3D20	
bottom		16.8		cm <sup>2</sup>
		4D25		
τ=Q/bjd	0.73		0.73	N/mm <sup>2</sup>
top	0.43		0.43	min.0.4%
Pt (%) bott.		0.89		
top	9.42		9.42	
at (cm <sup>2</sup> ) bott.		19.64		
Main Bars	top	3	3	3
		D20		
		D25		2
	bot	2	4	
φ (cm)	18.84		18.84	max
Q/fa.j (cm)	1.11		1.11	
judge	ok		ok	1.7
fs.bj LT(ST)	148.2		148.2	kN
(t)	D10-250	D10-250	D10-250	
judge	ok		ok	

seismic force neglected

3.6 Limit state analysis

Rectangular section design and limited state analysis				( 1/3 )	
Concrete Permissible Strength		$f_{ck} =$	17 N/mm <sup>2</sup>	by use of B30 30	
Direct tensile stress		$f_t =$	2.00 N/mm <sup>2</sup>		
Elasticity ratio		$n =$	15		
Elasticity		$E =$	200000 N/mm <sup>2</sup>		
Permissible strength		$\sigma_{sa} =$	250 N/mm <sup>2</sup>	round	from BS
		$\sigma_{sa} =$	140 N/mm <sup>2</sup>		deformed from BS
Ultimate strength (characteristic strength)		$\sigma_s =$	365 N/mm <sup>2</sup>		
Check point				Beam B1	Girder G1
Force	Bending Moment	Md	kN·m	63.9	73.0
	Shearing force	Sd	kN	31.0	101.0
Section Spec	Width	b	cm	35	40
	Height	h	cm	50	60
	Cover	dt	cm	5	5
	Effective Height	d	cm	45	55
Rebar Cross Section	Tension Rebar		cm <sup>2</sup>	3— D20	3— D20
				As = 9.42	As = 9.42
	Compression Rebar		cm <sup>2</sup>	2— D25	3— D20
				As = 9.82	As = 9.42
Stress	Concrete stress		N/mm <sup>2</sup>	4.2	3.4
	Rebar stress		N/mm <sup>2</sup>	160.6	149.8
	Shearing stress		N/mm <sup>2</sup>	0.217	0.502
B.M value for crack		Mcr	kNm	20.28	32.16
Crack width	Rebar interval	cs	mm	80	100
	Rebar diameter	$\phi$	mm	20	20
	Cover depth	c	mm	40	40
	Rebar stress	$\sigma_{se}$	N/mm <sup>2</sup>	166.2	153.9
	Crack width	wcr	mm	0.198	0.199
<b>Judgement: wcr &lt; 0.2: OK</b>				<b>OK</b>	<b>OK</b>
Examination with the Ultimate BM Strength					
Ultimate B.M Strength		Mud	kNm	146.02	181.55
		$\gamma_i \cdot Md / Mud$		0.438	0.402
		Judgement: $\gamma_i \cdot Md / Mud < 1.0$ : OK		OK	OK
Crack width shall be controled as follows:					
		1 normal condition		crack width < 0.3mm	
		2 severe condition		crack width < 0.2mm	
		3 very severe condition		crack width < 0.1mm	

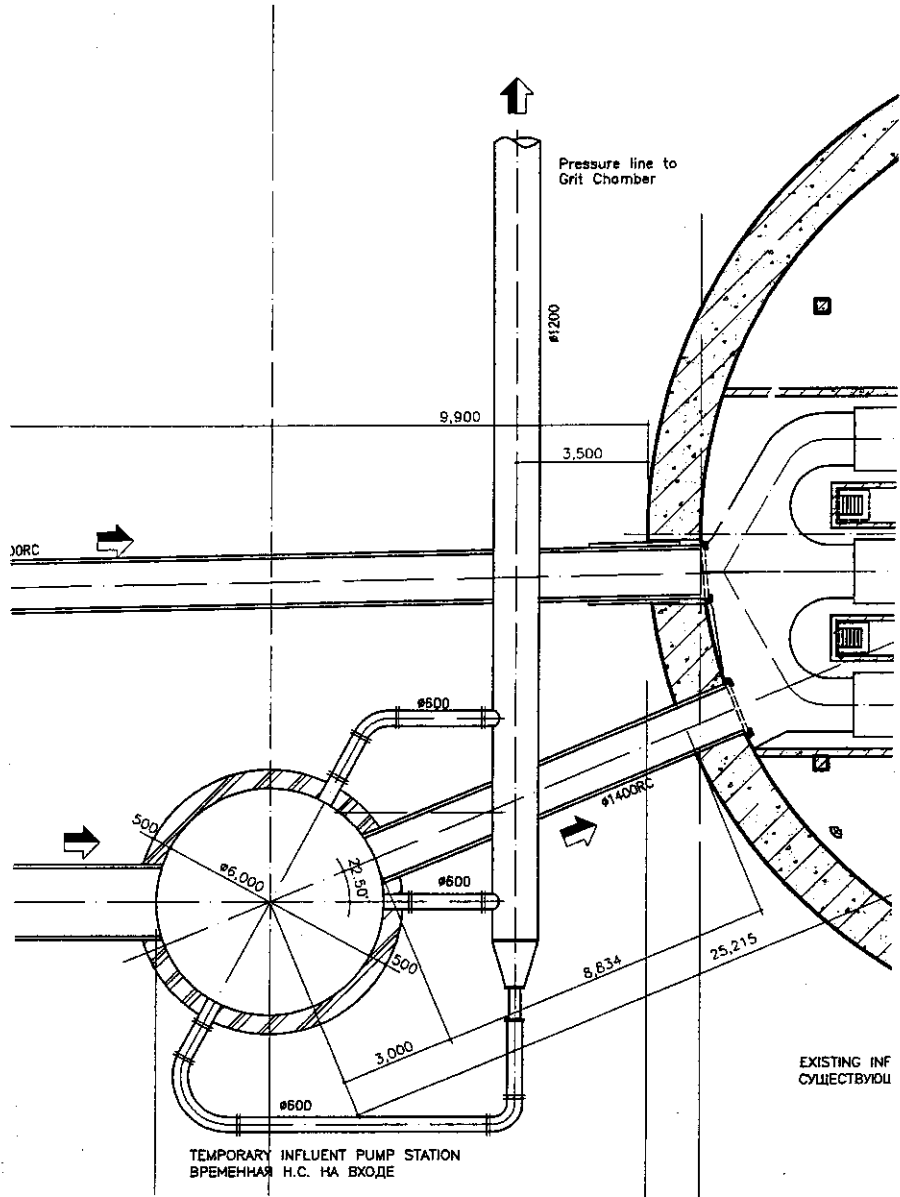
**Rectangular section design and limited state analysis**

( 2/3 )

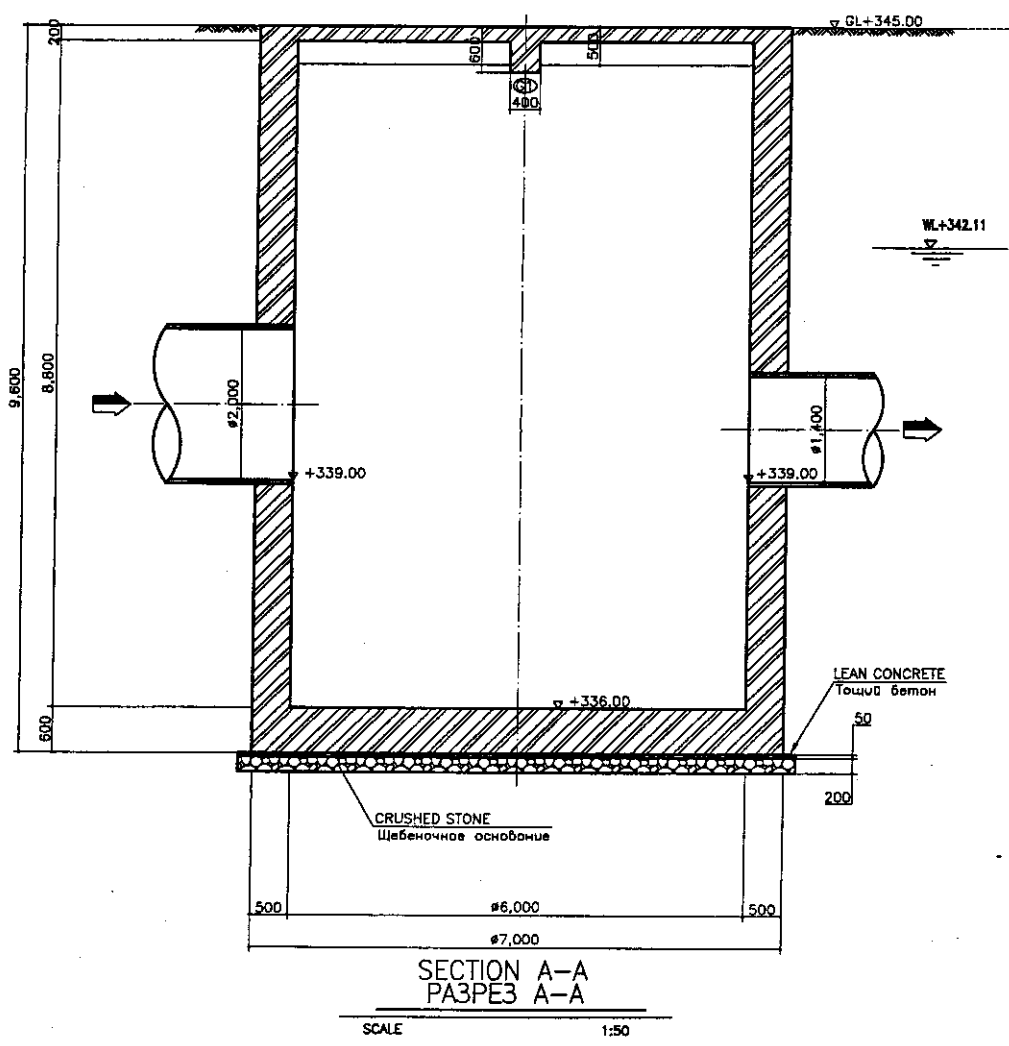
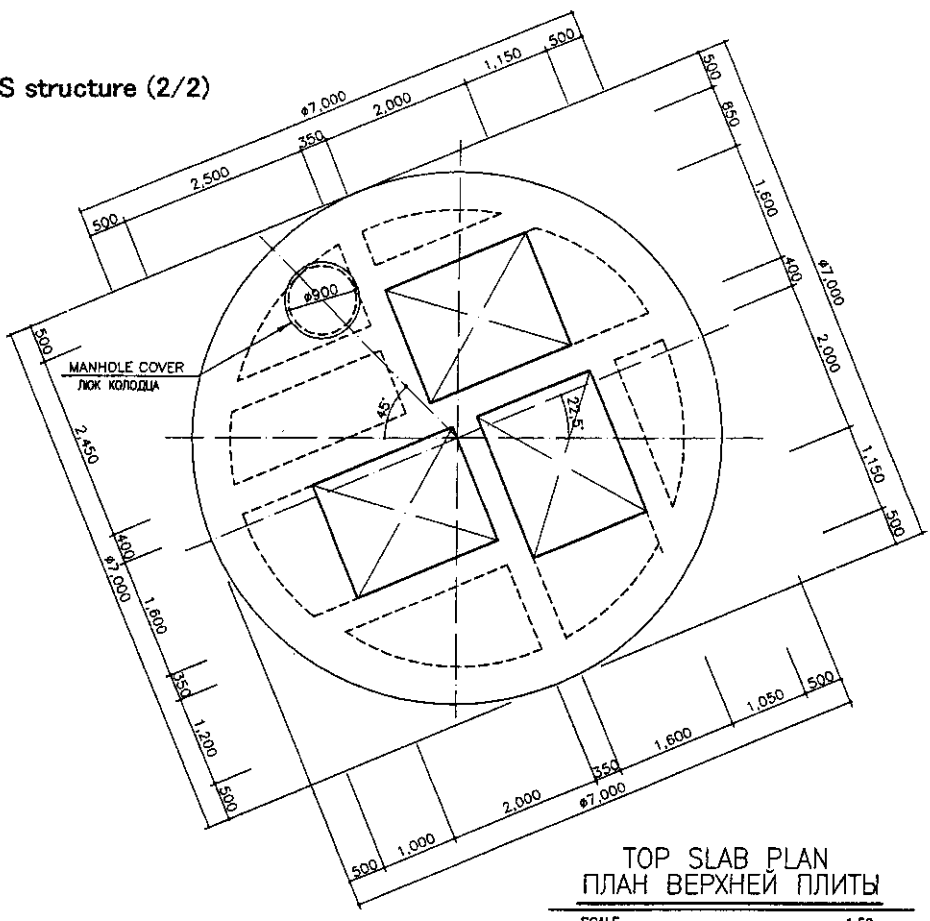
Concrete Permissible Strength	$f_{ck} =$	17 N/mm <sup>2</sup>	by use of B30	30
Direct tensile stress	$f_t =$	2.00 N/mm <sup>2</sup>		
Elasticity ratio	$n =$	15		
Elasticity	$E =$	200000 N/mm <sup>2</sup>		
Permissible strength	$\sigma_{sa} =$	250 N/mm <sup>2</sup>	round from BS	
	$\sigma_{sa} =$	140 N/mm <sup>2</sup>	deformed from BS	
Ultimate strength (characteristic strength)	$\sigma_s =$	365 N/mm <sup>2</sup>		

Check point				Slab			
Force	Bending Moment	Md	kN·m	2.6			
	Shearing force	Sd	kN	11.5			
Section Spec	Width	b	cm	100			
	Height	h	cm	20	#REF!		
	Cover	dt	cm	5	5		
	Effective Height	d	cm	15	#REF!		
Rebar Cross Section	Tension Rebar		cm <sup>2</sup>	10— D10	0— D0		
				As = 7.85			
	Compression Rebar		cm <sup>2</sup>	10— D10	0— D0		
				As = 7.85			
Stress	Concrete stress		N/mm <sup>2</sup>	0.6	#VALUE!		
	Rebar stress		N/mm <sup>2</sup>	23.4	#VALUE!		
	Shearing stress		N/mm <sup>2</sup>	0.084	#DIV/0!		
B.M value for crack				Mcr	kNm	9.15	#REF!
Crack width	Rebar interval	cs	mm	100	0		
	Rebar diameter	$\phi$	mm	10	0		
	Cover depth	c	mm	40	0		
	Rebar stress	$\sigma_{se}$	N/mm <sup>2</sup>	24.1	#VALUE!		
	<b>Crack width</b>	wcr	mm	0.060	#VALUE!		
<b>Judgement: wcr &lt; 0.2: OK</b>				<b>OK</b>	<b>0.00</b>		
Examination with the Ultimate BM Strength							
Ultimate B.M Strength		Mud	kNm	48.21	#DIV/0!		
$\gamma_i \cdot Md / Mud$				0.054	#DIV/0!		
Judgement: $\gamma_i \cdot Md / Mud < 1.0$ : OK				OK	0		
Crack width shall be controled as follows:							
		1 normal condition	crack width < 0.3mm				
		2 severe condition	crack width < 0.2mm				
		3 very severe condition	crack width < 0.1mm				

Temp IPS structure (1/2)



Temp IPS structure (2/2)



**4. Primary Sedimentation Tank**

**4.1 Material and Allowable stress**

**TABLE 4.1 Allowable Stress** (N/mm<sup>2</sup>, kg /cm<sup>2</sup>)

Item		Serviceability strength			Ultimate strength		
		Compression	Tension	Shear	Compression	Tension	Shear
Concrete	B30	10		0.8	30		1.2
		100	-----	8	300	-----	12
Steel Bar Round Bar	A- I	157.0	157.0	157.0	235.4	235.4	235.4
		1600	1600	1600	2400	2400	2400
Steel Bar Deformed Bar	A- II	196.2	196.2	196.2	358.1	358.1	358.1
		2000	2000	2000	3650	3650	3650

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

**TABLE 4.2 Allowable Bonding Stress of Steel Bar to Concrete** (N/mm<sup>2</sup>, kg /cm<sup>2</sup>)

Item	Serviceability strength		Remarks
	Top bars	Other bars	
φ6,φ9,φ12	0.9	1.3	
D10,D13,D16	9	13.5	
D19,D22,D25,D29	1.6	2.4	
	16.2	24.3	

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

**4.2 Load Table**

**TABLE 4.3 Dead Load**

Loc.	item	thickness	kg/m <sup>2</sup>	total kg/m <sup>2</sup>	Remarks
Foundation	Leveling motar	2.5	63		
	Concrete slab	60cm	1500		
				1563	<----- MKS UNIT
				15328	<----- SI UNIT

**TABLE 4.4 Live Load and Floor Load**

kg/m<sup>2</sup> (Girder, Sub beam : Self weight not included)

Loc.	load type	Foundation	beam	girder	Remarks
Mechanical eq.	Dead Load	-	-	-	
	Live Load	30000.0	-	-	Load of heay equipment
	Total Load	30000.0	-	-	
	SI unit	294300	-	-	<----- SI UNIT



### 4.3. Wall of cylindrical tanks for Primary Sedimentation Tanks

( / )

#### 1) Spec of Tank

Diameter	d	<b>28</b>	m	Unit Water load	DI	1.0 t/m <sup>3</sup> =	<b>9.81</b>	kN/m <sup>3</sup>
Water Depth	h	<b>3.5</b>	m	Supporting condition of bottom :		Rigid		
Wall Thickness	t	<b>600</b>	mm			$\alpha e$ :	<b>15</b>	
Wall height	h1	<b>3.8</b>	m	f <sub>st</sub> =	<b>120</b>	N/mm <sup>2</sup>		
				f <sub>ct</sub> =	<b>2.00</b>	N/mm <sup>2</sup>	<b>fcu=</b>	<b>30</b>
Unit concrete weight		<b>23.544</b>	kN/m <sup>3</sup>	permissible tensile stress			not used	

#### 2) Employed Equation for analysis

\*Same with the former section

#### 3) Forces and Bending Moment /Reinforcement

0  $h^2/d/t = \boxed{0.729}$  then  $K1 = \boxed{0.045}$   $K2 = \boxed{0.55}$   $K3 = \boxed{0.26}$   
 By table 184, pp.405

1 BM at bottom = **18.93** kNm/m

2 Position height of max tension = **1.925** m above the bottom

3 Max circumference tension = **124.98** kN/m around the position of the above

4 Required  $A_s = \boxed{40.1}$  cm<sup>2</sup> for tension

5 Min. thickness of wall = **184.26** mm

6 Direct comp. = **1293.87** kN/m<sup>2</sup>  
 = **1.294** N/mm<sup>2</sup>

#### Reinforcement

<b>5 - D25</b>	
<b>5 - D25</b>	
$A_s =$	<b>49.1</b> cm <sup>2</sup>
$p_t =$	<b>0.82</b> % > 0.3%

7 Shearing force  $V1 = F/PI/d$   
 = **24.50** kN

8 Distribution Rebar

**5 - D22**

### 4.2. Foundation

#### 1) Effect of water pressure

Ground Level =	<b>347.0</b>	m
Ground Water Level =	<b>342</b>	m
Bottom slab level =	<b>343.6</b>	m
Height of Bottom slab =	<b>0.6</b>	m
Soffit of bottom slab =	<b>(1.0)</b>	m

Upward thrust by water pressure

$p = 9.81$  kN/m<sup>3</sup> × **(1.0)** = **-9.81** kN/m<sup>2</sup>  
 $A = \boxed{824.5}$  m<sup>2</sup> (including wall thickness)  
 $P = \boxed{-8088.2}$  kN

#### 2) Bottom slab depth

\*Basement including structure wall must be designed to prevent flotation

Weight		
GL slab	<b>0</b>	kN (Slab thickness <b>0</b> m)
wall	<b>4823.164</b>	kN
Total	<b>4823.164</b>	kN

Required weight for bottom **-8088.16** - **4823** = **-12911** kN  
 Minimum depth  $F_s = 1.0$   $t = \boxed{-0.66513}$  m

\*No upward thrust will not affect to this structure.

\*Reinforcement

Radial reinforcement

**200 @ D25**

### |3) Weight of PST

\*Structure

	Diameter	height	thickness	unitweight	weight
Wall	28.6	3.8	0.6	23.544	4,823 kN
Base	30.2		0.6	23.544	10,119 kN
Water	28.0	3.5		9.81	21,142 kN
Total					<u>36,084 kN</u>

\*Equipoment

Sludge collector          design weight 30 t                  294 kN

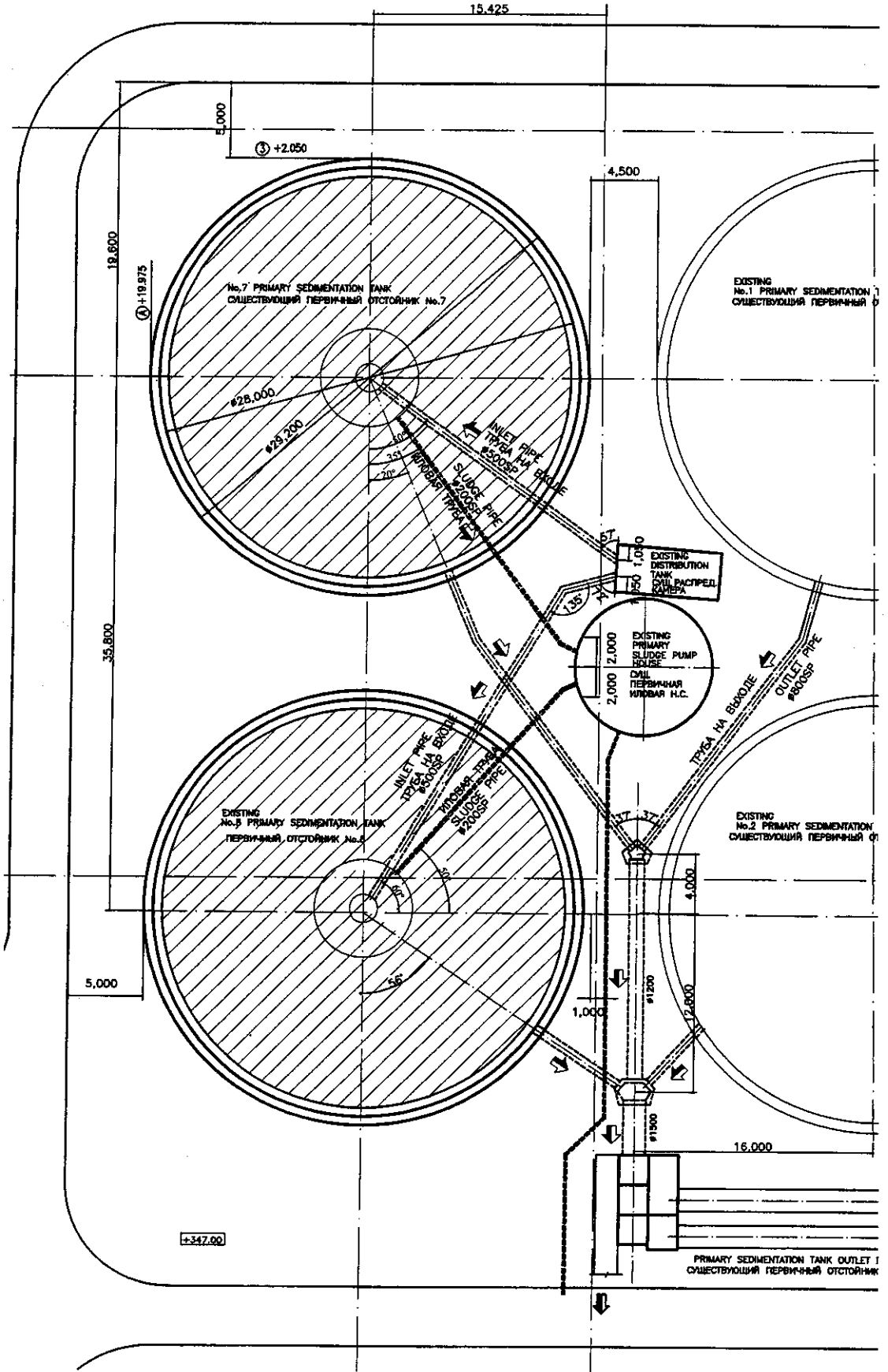
\*Grand total    36,378 kN

Unit load strength

$$\frac{36378.3 \text{ kN}}{\phantom{00000} \text{m}^2} = \frac{716.3}{\phantom{00000} \text{m}^2} = 50.8 \text{ kN/m}^2$$

3.6 Limit state analysis

Rectangular section design and limited state analysis				( 1/1 )
Concrete Permissible Strength		$f_{ck} =$	17 N/mm <sup>2</sup>	by use of B30
Direct tensile stress		$f_t =$	2.00 N/mm <sup>2</sup>	
Elasticity ratio		$n =$	15	
Elasticity		$E =$	200000 N/mm <sup>2</sup>	
Permissible strength		$\sigma_{sa} =$	250 N/mm <sup>2</sup>	round from BS
		$\sigma_{sa} =$	140 N/mm <sup>2</sup>	deformed from BS
Ultimate strength (characteristic strength)		$\sigma_s =$	365 N/mm <sup>2</sup>	
Check point				Wall
Force	Bending Moment	Md	kN·m	18.9
	Shearing force	Sd	kN	24.5
Section Spec	Width	b	cm	100
	Height	h	cm	60
	Cover	dt	cm	5
	Effective Height	d	cm	55
Rebar Cross Section	Tension Rebar		cm <sup>2</sup>	5 — D25
				As = 24.55
	Compression Rebar		cm <sup>2</sup>	5 — D25
				As = 24.55
Stress	Concrete stress		N/mm <sup>2</sup>	0.3
	Rebar stress		N/mm <sup>2</sup>	14.9
	Shearing stress		N/mm <sup>2</sup>	0.049
B.M value for crack		Mcr	kNm	80.79
Crack width	Rebar interval	cs	mm	200
	Rebar diameter	$\phi$	mm	25
	Cover depth	c	mm	70
	Rebar stress	$\sigma_{se}$	N/mm <sup>2</sup>	15.3
	Crack width	wcr	mm	0.091
Judgement: $w_{cr} < 0.2$ : OK				OK
Examination with the Ultimate BM Strength				
Ultimate B.M Strength		Mud	kNm	471.96
$\gamma_i \cdot Md / Mud$				0.040
Judgement: $\gamma_i \cdot Md / Mud < 1.0$ : OK				OK
Crack width shall be controled as follows:				
		1 normal condition	crack width < 0.3mm	
		2 severe condition	crack width < 0.2mm	
		3 very severe condition	crack width < 0.1mm	

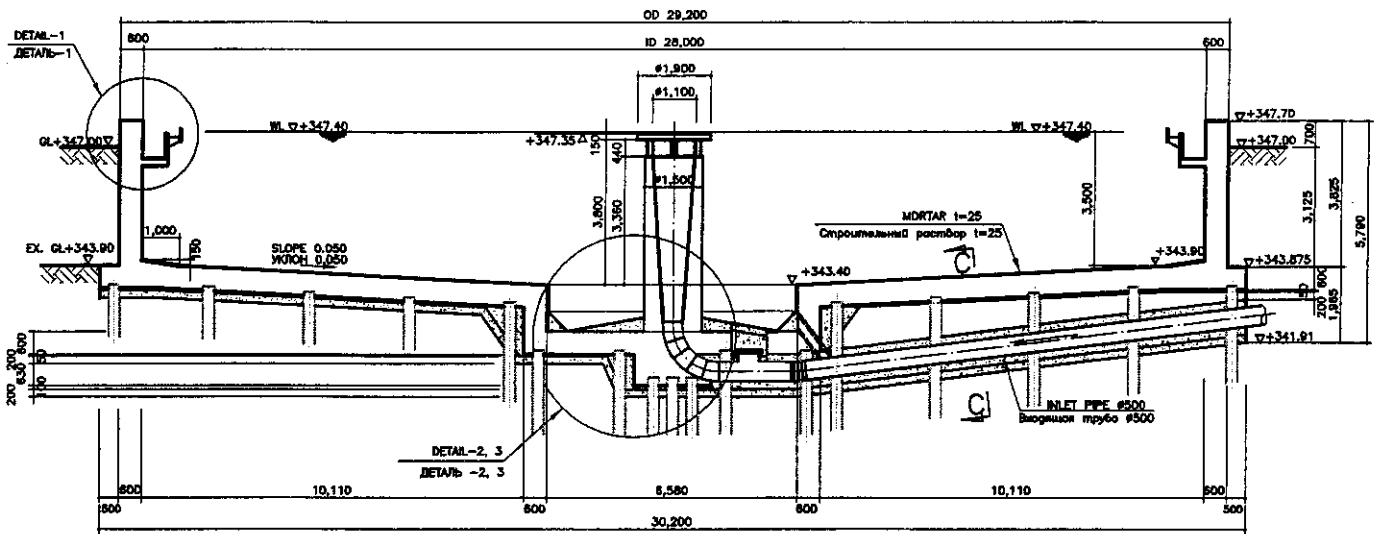


PRIMARY SEDIMENTATION TANK LAYOUT  
 РАСПОЛОЖЕНИЕ ПЕРВИЧНЫХ ОТСТОЙНИКОВ

SCALE

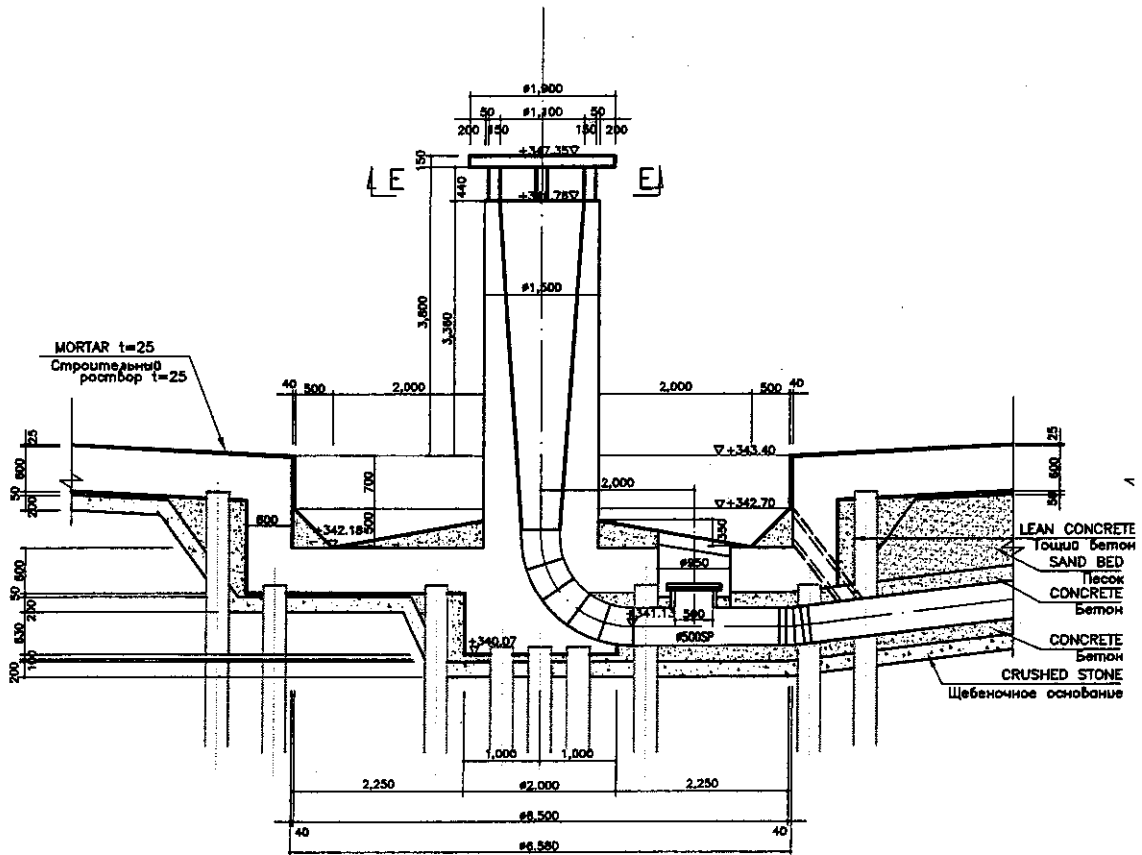
1:200

PST structure(2/2)



SECTION A-A  
РАЗРЕЗ A-A

SCALE 1:100



DETAIL-2  
ДЕТАЛЬ-2

SCALE 1:50

**5. Secondary Sedimentation Tank**

**5.1 Material and Allowable stress**

**TABLE 5.1 Allowable Stress** (N/mm<sup>2</sup>, kg /cm<sup>2</sup>)

Item		Serviceability strength			Ultimate strength		
		Compression	Tension	Shear	Compression	Tension	Shear
Concrete	B30	10		0.8	30		1.2
		100	-----	8	300	-----	12
Steel Bar Round Bar	A- I	157.0	157.0	157.0	235.4	235.4	235.4
		1600	1600	1600	2400	2400	2400
Steel Bar Deformed Bar	A- II	196.2	196.2	196.2	358.1	358.1	358.1
		2000	2000	2000	3650	3650	3650

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

**TABLE 5.2 Allowable Bonding Stress of Steel Bar to Concrete** (N/mm<sup>2</sup>, kg /cm<sup>2</sup>)

Item	Serviceability strength		Remarks
	Top bars	Other bars	
φ6,φ9,φ12	0.9	1.3	
	9	13.5	
D10,D13,D16 D19,D22,D25,D29	1.6	2.4	
	16.2	24.3	

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

**5.2 Load Table**

**TABLE 5.3 Dead Load**

Loc.	item	thickness	kg/m <sup>2</sup>	total kg/m <sup>2</sup>	Remarks
Foundation	Leveling motar	2.5	63		
	Concrete slab	60cm	1500		
				1563	<----- MKS UNIT
				15328	<----- SI UNIT

**TABLE 5.4 Live Load and Floor Load**

kg/m<sup>2</sup> (Girder, Sub beam : Self weight not included)

Loc.	load type	Foundation	beam	girder	Remarks
Mechanical eq.	Dead Load	-	-	-	
	Live Load	30000.0	-	-	Load of heay equipment
	Total Load	30000.0	-	-	
	SI unit	294300	-	-	<----- SI UNIT

**5.3.Wall of cylindrical tanks for Secondary Sedimentation Tanks**

( / )

**1) Spec of Tank**

Diameter	d	<input type="text" value="28"/>	m	Unit Water load	DI	1.0 t/m <sup>3</sup> =	<input type="text" value="9.81"/>	kN/m <sup>3</sup>
Water Depth	h	<input type="text" value="4"/>	m	Supporting condition of bottom :		Rigid		
Wall Thickness	t	<input type="text" value="600"/>	mm			$\alpha e$ :	<input type="text" value="15"/>	
Wall height	h <sub>1</sub>	<input type="text" value="4.2"/>	m	f <sub>st</sub> =	<input type="text" value="120"/>	N/mm <sup>2</sup>		
				f <sub>ct</sub> =	<input type="text" value="2.00"/>	N/mm <sup>2</sup>	<input type="text" value="30"/>	f <sub>cu</sub> =
Unit concrete weight		<input type="text" value="23.544"/>	kN/m <sup>3</sup>	permissible tensile stress				not used

**2) Employed Equation for analysis**

\*Same with the former section

**3) Forces and Bending Moment /Reinforcement**

0  $h^2/d/t = \text{input } 0.952$  then  $K1 = \text{input } 0.045$   $K2 = \text{input } 0.55$   $K3 = \text{input } 0.26$   
 By table 184, pp.405

1 BM at bottom =  kNm/m

2 Position height of max tension =  m above the bottom

3 Max circumference tension =  kN/m around the position of the above

4 Required A<sub>s</sub> =  cm<sup>2</sup> for tension

5 Min. thickness of wall =  mm

6 Direct comp. =  kN/m<sup>2</sup>  
 =  N/mm<sup>2</sup>

**Reinforcement**

5 -	D25
5 -	D25
A <sub>s</sub> =	49.1 cm <sup>2</sup>
pt =	0.82 % > 0.3%

7 Shearing force V<sub>1</sub> = F/PI/d  
 =  kN

8 Distribution Rebar

**5.4 Foundation**

**1) Effect of water pressure**

Ground Level =	<input type="text" value="345.0"/>	m
Ground Water Level =	<input type="text" value="343"/>	m
Bottom slab level =	<input type="text" value="341.3"/>	m
Height of Bottom slab =	<input type="text" value="0.7"/>	m
Soffit of bottom slab =	<input type="text" value="2.4"/>	m

Upward thrust by water pressure

$p = 9.81 \text{ kN/m}^3 \times \text{input } 2.4 = \text{input } 23.54 \text{ kN/m}^2$   
 $A = \text{input } 824.5 \text{ m}^2$  (including wall thickness)  
 $P = \text{input } 19411.6 \text{ kN}$

**2) Bottom slab depth**

\*Basement including structure wall must be designed to prevent flotation

Weight		
GL slab	<input type="text" value="0"/>	kN (Slab thickness <input type="text" value="0"/> m)
wall	<input type="text" value="5331"/>	kN
<b>Total</b>	<input type="text" value="5331"/>	<b>kN</b>

Required weight for bottom  -  =  kN  
 Minimum depth  $F_s = 1.0$   $t = \text{input } 0.725377$  m

\*No upward thrust will not affect to this structure.

\*Reinforcement

Radial reinforcement

### |3) Weight of SST

\*Structure

	Diameter	height	thickness	unitweight	weight
Wall	28.6	4.2	0.6	23.544	5,331 kN
Base	30.2		0.6	23.544	10,119 kN
Water	28.0	4		9.81	24,162 kN
<b>Total</b>					<b>39,612 kN</b>

\*Equipment

Sludge collector          design weight 30 t                          294 kN

\*Grand total    39,906 kN

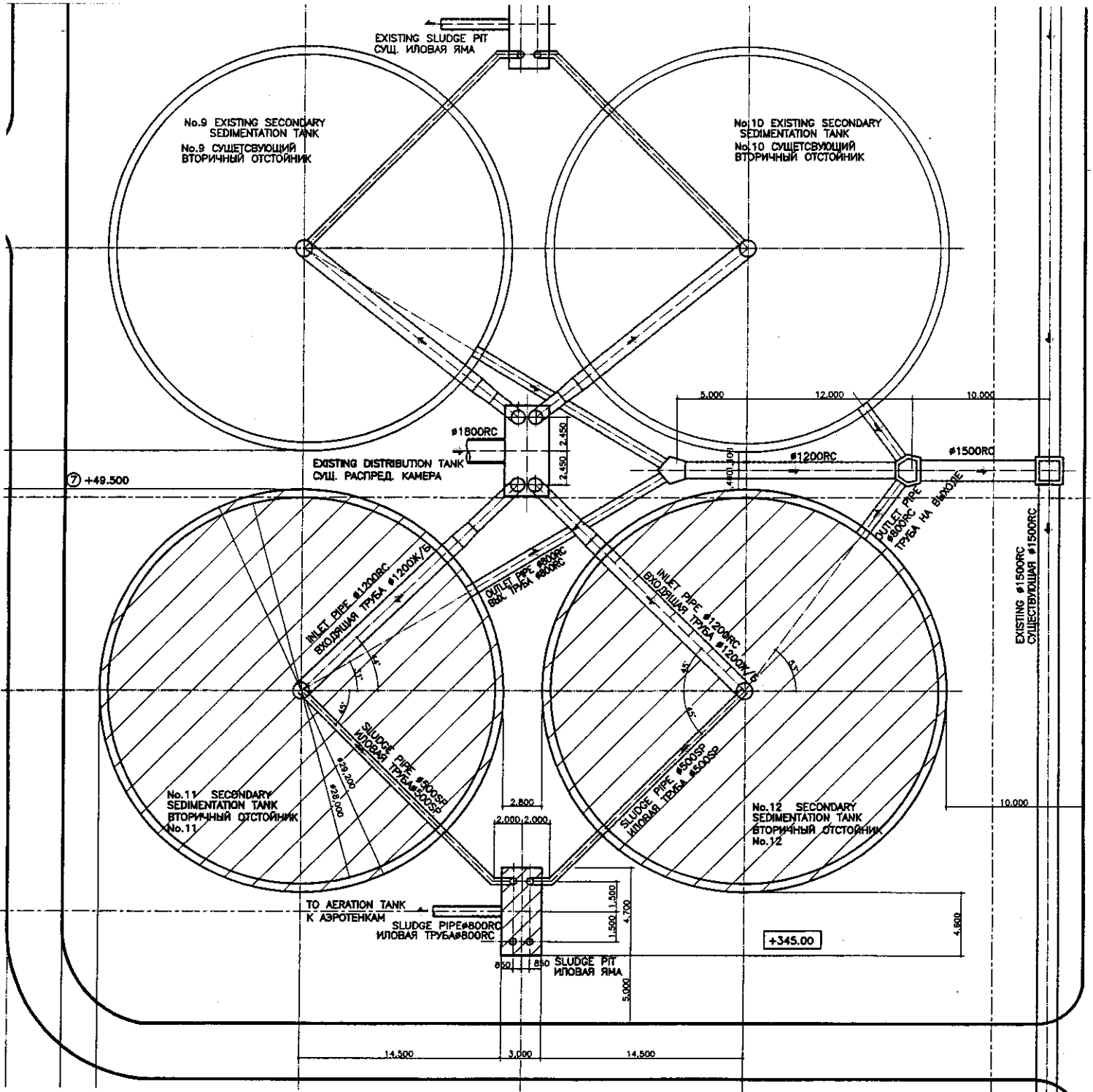
Unit load strength per m2

$$\frac{39906.3 \text{ kN}}{\text{m}^2} \div 716.3 = 55.7 \text{ kN/m}^2$$

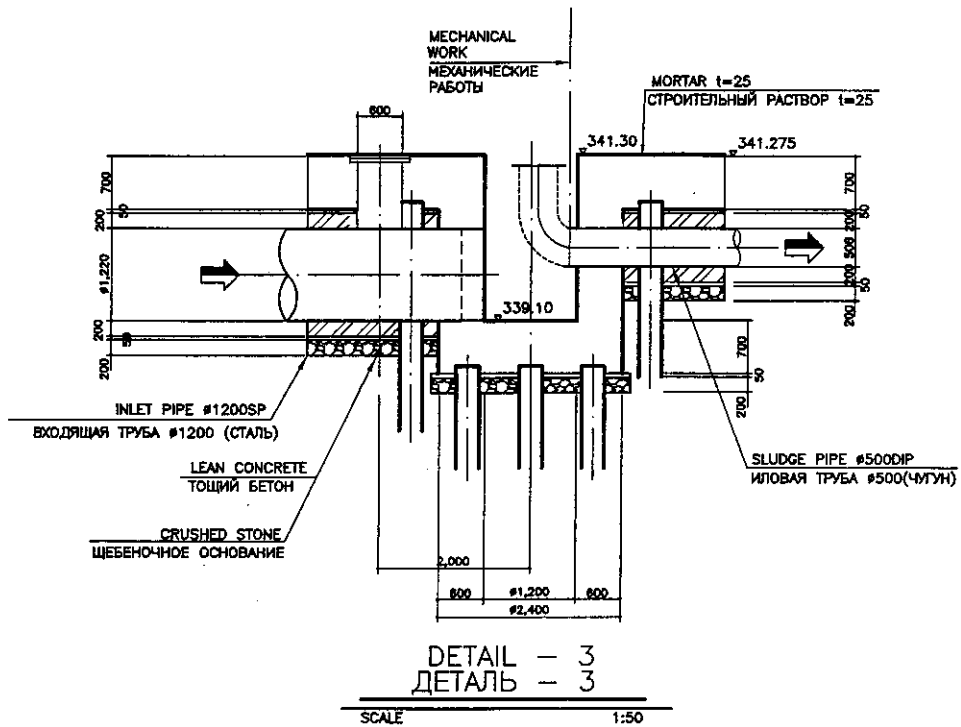
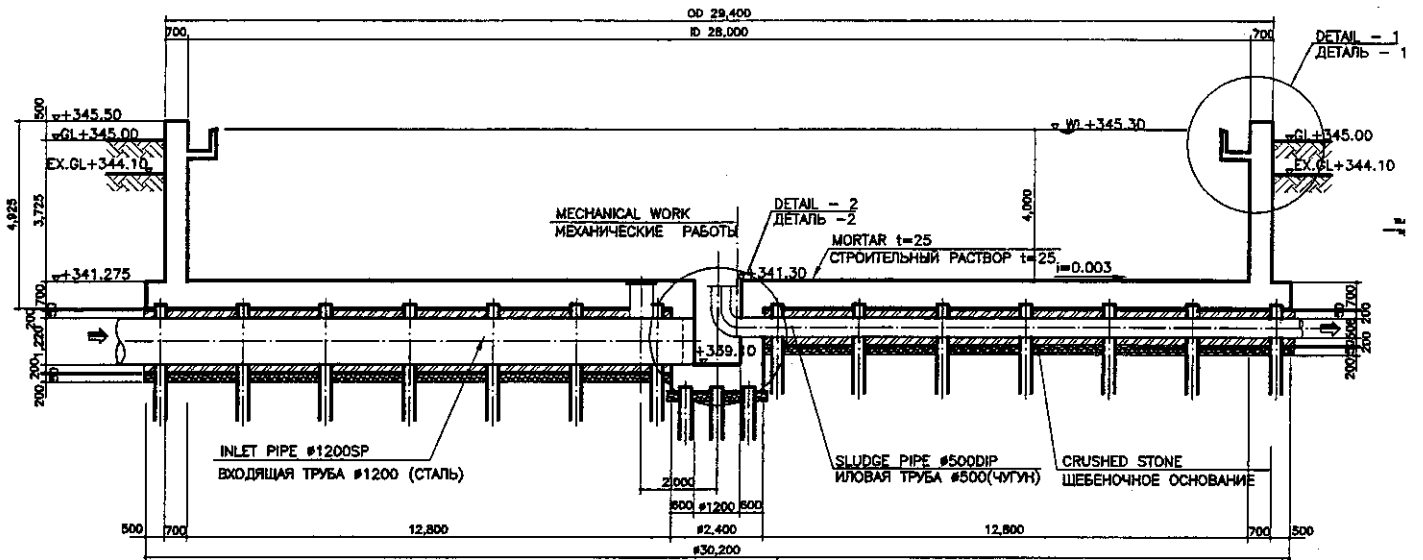


3.6 Limit state analysis

5.5 Rectangular section design and limited state analysis				( 1/1 )	
Concrete Permissible Strength		$f_{ck} =$	17 N/mm <sup>2</sup>	by use of B30 30	
Direct tensile stress		$f_t =$	2.00 N/mm <sup>2</sup>		
Elasticity ratio		$n =$	15		
Elasticity		$E =$	200000 N/mm <sup>2</sup>		
Permissible strength		$\sigma_{sa} =$	250 N/mm <sup>2</sup>	round from BS	
		$\sigma_{sa} =$	140 N/mm <sup>2</sup>	deformed from BS	
Ultimate strength (characteristic strength)		$\sigma_s =$	365 N/mm <sup>2</sup>		
Check point				Wall	
Force	Bending Moment	Md	kN·m	28.3	
	Shearing force	Sd	kN	24.5	
Section Spec	Width	b	cm	100	
	Height	h	cm	60	
	Cover	dt	cm	5	
	Effective Height	d	cm	55	
Rebar Cross Section	Tension Rebar		cm <sup>2</sup>	5 – D25	
				As = 30.80	
	Compression Rebar		cm <sup>2</sup>	5 – D25	
				As = 30.80	
Stress	Concrete stress		N/mm <sup>2</sup>	0.5	
	Rebar stress		N/mm <sup>2</sup>	17.8	
	Shearing stress		N/mm <sup>2</sup>	0.049	
B.M value for crack		Mcr	kNm	83.00	
Crack width	Rebar interval	cs	mm	200	
	Rebar diameter	$\phi$	mm	25	
	Cover depth	c	mm	70	
	Rebar stress	$\sigma_{se}$	N/mm <sup>2</sup>	18.4	
	<b>Crack width</b>	wcr	mm	0.097	
<b>Judgement: wcr &lt; 0.2: OK</b>				<b>OK</b>	
Examination with the Ultimate BM Strength					
Ultimate B.M Strength		Mud	kNm	586.39	
$\gamma_i \cdot Md / Mud$				0.048	
Judgement: $\gamma_i \cdot Md / Mud < 1.0$ : OK				OK	
Crack width shall be controlled as follows:					
		1 normal condition	crack width < 0.3mm		
		2 severe condition	crack width < 0.2mm		
		3 very severe condition	crack width < 0.1mm		



SST structure(2/2)



**6. Blower base**

**6.1 Material and Allowable stress**

**TABLE 6.1 Allowable Stress** (N/mm<sup>2</sup>, kg/cm<sup>2</sup>)

Item		Serviceability strength			Ultimate strength		
		Compression	Tension	Shear	Compression	Tension	Shear
Concrete	B30	10		0.8	30		1.2
		100	-----	8	300	-----	12
Steel Bar Round Bar	A- I	157.0	157.0	157.0	235.4	235.4	235.4
		1600	1600	1600	2400	2400	2400
Steel Bar Deformed Bar	A- II	196.2	196.2	196.2	358.1	358.1	358.1
		2000	2000	2000	3650	3650	3650

upper: SI units N/mm<sup>2</sup>  
lower: MKS units kg/cm<sup>2</sup>

**TABLE 6.2 Allowable Bonding Stress of Steel Bar to Concrete** (N/mm<sup>2</sup>, kg/cm<sup>2</sup>)

Item	Serviceability strength		Remarks
	Top bars	Other bars	
φ6,φ9,φ12	0.9	1.3	
	9	13.5	
D10,D13,D16 D19,D22,D25,D29	1.6	2.4	
	16.2	24.3	

upper: SI units N/mm<sup>2</sup>  
lower: MKS units kg/cm<sup>2</sup>

**6.2 Load Table**

**TABLE 6.3 Dead Load**

Loc.	item	thickness	kg/m <sup>2</sup>	total kg/m <sup>2</sup>	Remarks
slab	Mortar	-	-		
	Concrete slab	30cm	750		
				750	<----- MKS UNIT
				7358	<----- SI UNIT
Common slab	Leveling mortar	-	-		
	Concrete slab	20cm	500		
				500	<----- MKS UNIT
				4905	<----- SI UNIT

**TABLE 6.4 Live Load and Floor Load**

kg/m<sup>2</sup> (Girder, Sub beam : Self weight not included)

Loc.	load type	slab	beam	girder	Remarks
slab	Dead Load	750.0	750.0	750.0	
	Live Load	1421.6	1421.6	1421.6	**)
	Total Load	2171.6	2171.6	2171.6	
	SI unit	21303	21303	21303	<----- SI UNIT

\*\* ) Blower

Live load : 29ton = 284.49 kN  
 Base daimension 6.0 \* 3.4 = 20.4 m<sup>2</sup>  
 Average load 1,421.6 kg/m<sup>2</sup>  
 13.9 kN/m<sup>2</sup>  
 Frequency = 50 Hz

### 6.3 Facility weight

**Table6.5 Grit Chamber Weight**

Story	Load type	Unit w (kN/m <sup>2</sup> ,m)	width /height (m) or unit	Length (m)	Area or L (m <sup>2</sup> ), (m)	Weight (kN)	Small Total (t)	S Wi (t)
1st story	slab	7.36	3.4	6.00	20.40	150.09	530.89	530.89
	Machine	13.95	3.4	6.00	20.40	284.49		
	Girder 2.2m	8.09	2	2.20	4.40	35.61		
	Girder 1.2m	8.09	2	1.20	2.40	19.42		
	Girder 1.7m	8.09	3	1.70	5.10	41.28		
Column	800*800	7.36	4.4	6.00	26.40	194.24	594.49	1125.38
	h=4.25m	15.70	6	4.25	25.50	400.25		

**Base Area 20.40 (m<sup>2</sup>)**

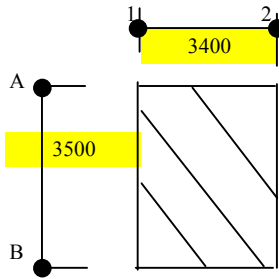
**Total W= 1,125.38**

**W-Base= 530.9**

reaction =W/(Base area)= **55.166 (kN/m<sup>2</sup>)**

6.4 SLAB

S1 Load condition



A= 11.9 m<sup>2</sup>

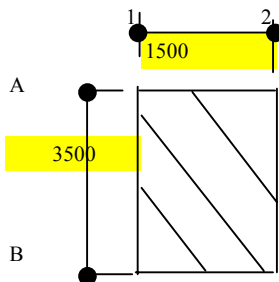
Area unit weight kN  
 Floor slab= 11.90 x 21.3= 253.51  
 Wall= x 0.00  
 Σ = 253.5  
 lx= 3.4 m  
 ly= 3.5 m t(cm)= 30  
 λ = 1.03 d(cm)= 25  
 cover(cm)= 5

	a	wlx2(kNm2)	M(Nm)	Additional M from wall	Total M	at= M/(σ sjd)	re-bars	
Mx1=	0	260.96	0.0		0	0.000 cm2	upper 4-D10-->D10@200	3.93cm2
Mx2=	0.035	260.96	9,133.7			2.128 cm2	bottom 4 -D10-->D10@200	3.93cm2
								0.3%
My1=	0	260.96	0.0	0	0	0.000 cm2	upper 4-D10-->D10@200	3.93cm2
My2=	0.042	260.96	10,960.4			2.554 cm2	bottom 4-D10-->D10@200	3.93cm2
		wlx	Q(N)			φ=Q/(τα jd)		0.3%
Qx =	0.44	74.56	32,806.8			6.29 cm <	15.7 ok	
Qy =	0.44	74.56	32,806.8			6.29 cm <	15.7 ok	

Suffix 1: end of span  
 Suffix 2: middle of span  
 From nomogram of two-way slab of free-support

Q cap  
 196,200 N > Q out  
 196,200 N > Q out  
 No adjustment, since beam width(60cm) covers the area of "out".

S2 Load condition



A= 5.25 m<sup>2</sup>

Area unit weight kN  
 Floor slab= 5.25 x 21.3= 111.84  
 Wall= x 0.00  
 Σ = 111.8  
 lx= 1.5 m  
 ly= 3.5 m t(cm)= 30  
 λ = 2.33 d(cm)= 25  
 cover(cm)= 5

	a	wlx2(kNm2)	M(Nm)	Additional M from wall	Total M	at= M/(σ sjd)	re-bars	
Mx1=			0.0		0	0.000 cm2	upper 2-D10-->D10@200	3.93cm2
Mx2=	0.105	47.93	5,032.9			1.173 cm2	bottom 2-D10-->D10@200	3.93cm2
								0.3%
My1=			0.0	0	0	0.000 cm2	upper 2-D10-->D10@200	3.93cm2
My2=	0.014	47.93	671.0			0.156 cm2	bottom 2-D10-->D10@200	3.93cm2
		wlx	Q(N)			φ=Q/(τα jd)		0.3%
Qx =	0.5	31.95	15,977.3			3.06 cm <	15.7 ok	
Qy =	0.46	31.95	14,699.1			2.82 cm <	15.7 ok	

Suffix 1: end of span  
 Suffix 2: middle of span  
 From nomogram of two-way slab

Q cap  
 196,200 N > Q ok  
 196,200 N > Q ok

6.5 BEAMS

1) **B1**

Typical example of the beam is the 2.2m length .

B1	Load form	(slab load)		(slab load)		(girder load)+ other loads		Σ
	Co	C/w	Co	Co/w	Co	w/l	Co	kNm
bxD 40x60 (cm)	Mo	M/w	Mo	Mo/w	Mo	w/l	Mo	kNm
	Q	Q/w	Q	Q/w	Q	w/l	Q	kN
Slab load =		21.3 (kN/m <sup>2</sup> )		ly= 3.5 m				
Span =		3.5 (m)		lx= 1.70 m				λ= 2.06

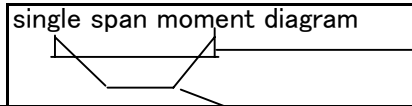
1.Girder load= 4.70 kN/m

dead load

2.Line load = 0.00 kN/m + kN/m = 0.00 kN/m

roof wall

Total = 4.70 kN/m



0.6C= 68.4

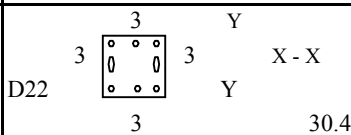
Mo-0.35C= 79.6

seismic force neglected

2) Determination of beam B1

Beam ID	B1			Remarks
Position	B end	Mid	C end	
D.L ] M(kNm) top		68.4	68.4	
+ ] bott.		79.6		
L.L ] Q (kN)		32.21	32.21	
] b x D (cm)	40	x	50	
Size ] d (cm)			45	
] j(cm)			39.375	
top	8.9		8.9	cm <sup>2</sup>
	3D25		3D25	at= M/(σ sjd)
bottom		10.3		cm <sup>2</sup>
		3D25		
τ=Q/bjd		0.20	0.20	N/mm <sup>2</sup>
top		1.03	1.03	min.0.4%
Pt (%) bott.		1.03		
top		18.48	18.48	
at (cm <sup>2</sup> ) bott.		18.48		
Main top	3	3	3	
Bars		28		
bott	3	3	3	
φ (cm)	23.55		23.55	max
Q /fa.j (cm)	0.35		0.35	
judge	ok		ok	1.7
fs.bj LT(ST)		121.3	121.3	kN
(t)	D10-250	D10-250	D10-250	
judge	ok		ok	

**6.6 Column Profile**

Column ID		Blower Base								Remarks
Direction		X		Y		X		Y		
Position		T	B	T	B	T	B	T	B	
LT	N (t)	4.83		4.83						
	M(tm)									
	Q(t)									
ET	N (t)									
	M(tm)									
	Q(t)									
ST	N (t)	4.83		4.83						
	M(tm)	0	0	0	0					
	Q(t)	0		0						
Size	b x d (cm), J(cm)	80	80	80	80					
	bD(x10 <sup>2</sup> ),bDD(x10 <sup>3</sup> )	6.4		5.12						
LT	N/ bD (kg/cm2)	0.76		0.75						
	M/bD2 (kg/cm2)	0.00		0.00						
	Pt(%)	0.20	0.20	0.20	0.20					
ST	N/ bD (kg/cm2)									
	M/bD2 (kg/cm2)									
	Pt(%)									
at (cm2)		12.8		12.8						
						25.6				
Main Bars D22 arrangement				30.4						
LT or ST	φ (cm)	28.26	28.26	28.26	28.26					
	Q/fa.j (cm) judge	0		0						
	QA=fs.bj (t) judge	40.425		40.425						
Pw (%) hoop		D10 - 150								



6.7 Limit state analysis

Rectangular section design and limited state analysis				( 1/1 )	
Concrete Permissible Strength	$f_{ck} =$	17 N/mm <sup>2</sup>	by use of B30	30	
Direct tensile stress	$f_t =$	2.00 N/mm <sup>2</sup>			
Elasticity ratio	$n =$	15			
Elasticity	$E =$	200000 N/mm <sup>2</sup>			
Permissible strength	$\sigma_{sa} =$	250 N/mm <sup>2</sup>	round	from BS	
	$\sigma_{sa} =$	140 N/mm <sup>2</sup>		deformer from BS	
Ultimate strength (characteristic strength)	$\sigma_s =$	365 N/mm <sup>2</sup>			
Check point			B1		
Force	Bending Moment	Md	kN·m	68.4	
	Shearing force	Sd	kN	32.2	
Section Spec	Width	b	cm	40	
	Height	h	cm	50	
	Cover	dt	cm	5	
	Effective Height	d	cm	45	
Rebar Cross Section	Tension Rebar		cm <sup>2</sup>	3 – D28	
				As = 18.48	
	Compression Rebar		cm <sup>2</sup>	3 – D28	
				As = 18.48	
Stress	Concrete stress		N/mm <sup>2</sup>	2.9	
	Rebar stress		N/mm <sup>2</sup>	88.3	
	Shearing stress		N/mm <sup>2</sup>	0.201	
B.M value for crack			Mcr	kNm	24.94
Crack width	Rebar interval	cs	mm	170	
	Rebar diameter	$\phi$	mm	28	
	Cover depth	c	mm	50	
	Rebar stress	$\sigma_{se}$	N/mm <sup>2</sup>	92.5	
	Crack width	wcr	mm	0.183	
Judgement: wcr < 0.2			OK		
Examination with the Ultimate BM Strength					
Ultimate B.M Strength		Mud	kNm	279.65	
$\gamma_i \cdot Md / Mud$			0.245		
Judgement: $\gamma_i \cdot Md / Mud < 1.0$			OK		
Crack width shall be controled as follows:					
1 normal condition		crack width < 0.3mm			
2 severe condition		crack width < 0.2mm			
3 very severe condition		crack width < 0.1mm			

6.8 Examination of vibration by equipment

$$\begin{array}{l}
 l_x = \boxed{3.5} \text{ m} \\
 l_y = \boxed{6} \text{ m} \\
 t = \boxed{30} \text{ cm} \\
 w = \boxed{2171} \text{ kg/m}^2
 \end{array}
 \quad
 \begin{array}{l}
 \text{Weight of Equipmen} \quad 29 \text{ t} \\
 = 29000 \text{ kg}
 \end{array}$$

$$\text{Concrete unit weight} = \frac{\boxed{2400} \text{ kg/m}^3}{1000} = 0.0024 \text{ kg/cm}^3$$

$$\text{Total mass} = \left( \text{volume} \times \text{unit weight} + \text{Equipment} \right) / 980 = 45.02 \text{ kg s}^2/\text{cm}$$

$$\text{Effective mass} = \frac{\boxed{0.234} \times 45.02}{11.4} = 0.91 \text{ kg s}^2/\text{cm}$$

$$\text{Slab Natural Frequency} = \frac{\boxed{129}}{11.2} \text{ Hz} \quad (E = 2.1 \times 10^5 \text{ kg/cm}^2)$$

$$\text{Blower Rotation} = \boxed{3000} \text{ r.p.m}$$

Therefore, Natural Frequency of slab is small enough compared with the vibration of Blower. Resonance phenomenon shall be avoided.

\* The following is a examination by K-value in "DIN 4025" on the assumption that impact value of jumping at upstairs is the same with the blower.

$$\text{Impact value } V_0 = \boxed{1.8} \text{ kg s at jumping on the upstairs by adult man}$$

$$\text{Impact time} = \boxed{0.0200000} \text{ s} = 0.02$$

$$\text{to } f_v = \frac{\boxed{0.02000000}}{\boxed{129}} = 0.000155 \text{ s} \Rightarrow k \delta = \boxed{0.145}$$

$$\text{Decay coefficient} = 0.05$$

$$\delta = 0.145 \times 1.8 / (2\pi \times 129 \times 10.53)$$

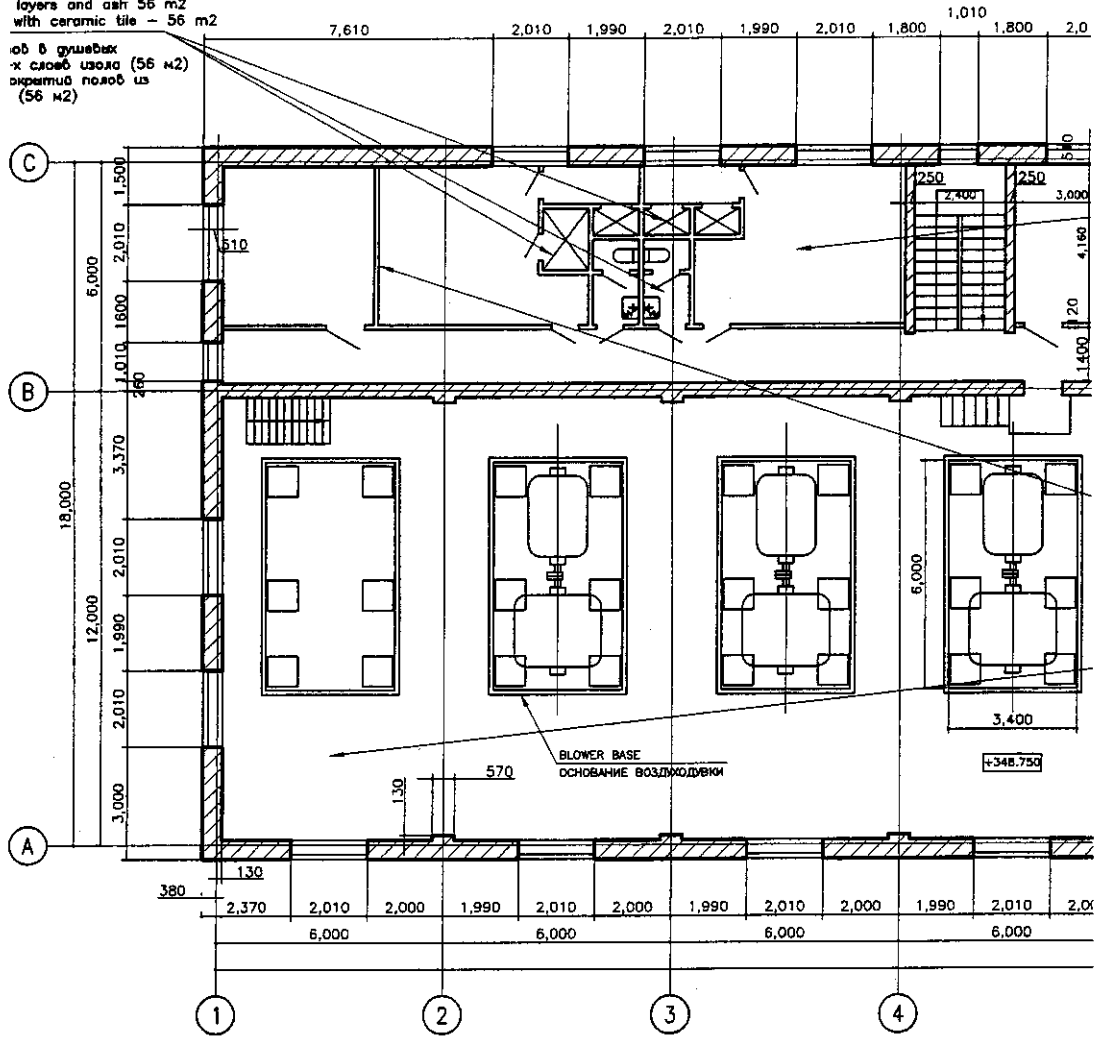
$$= 3.057 \times 10^{-5} = \boxed{0.3057} \mu$$

K value is from 0.1 to 0. from the figure

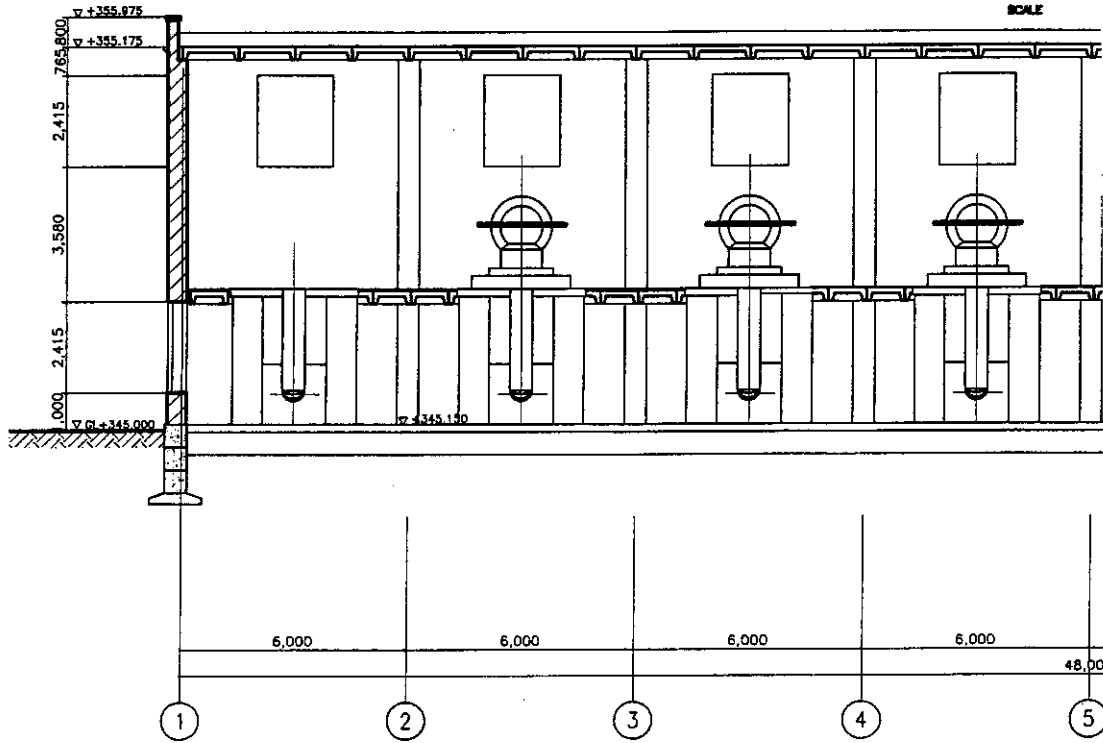
Vibration noticeable but able to withstand.  
No influence

# Blower base structure(1/2)

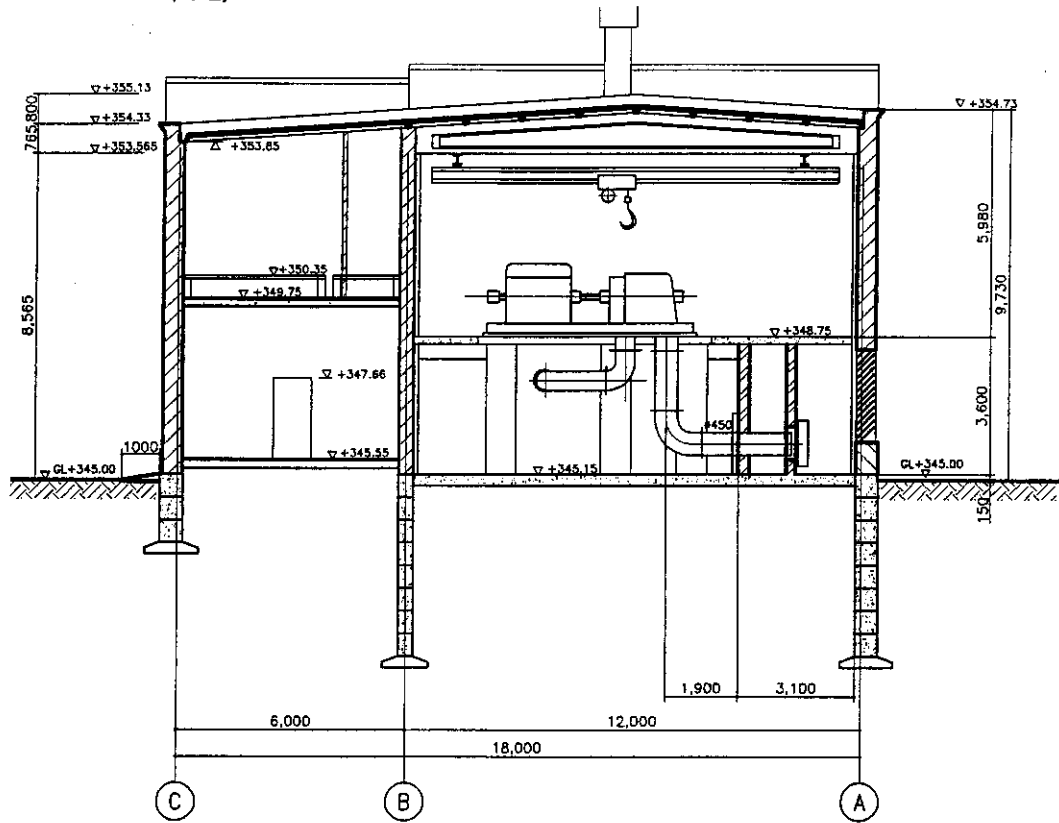
in shower rooms and water  
 layers and ash 56 m<sup>2</sup>  
 with ceramic tile - 56 m<sup>2</sup>  
 об в душевых  
 к слоев изоля (56 м<sup>2</sup>)  
 окрывает полов из  
 (56 м<sup>2</sup>)



2nd  
 ПЛАН В  
 SCALE

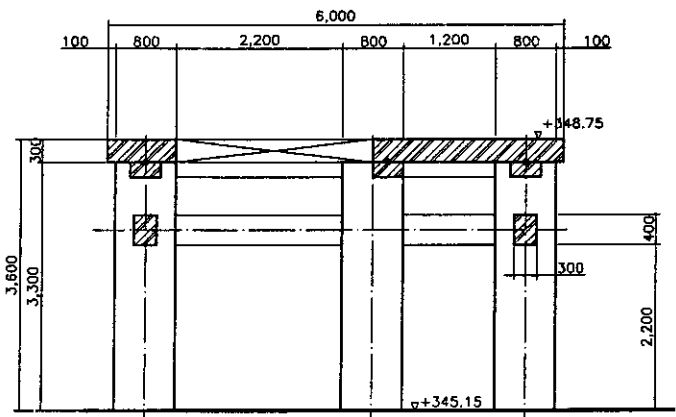
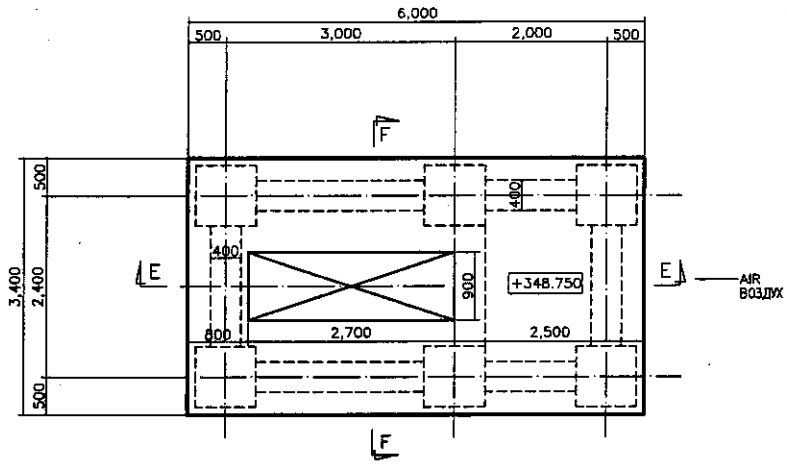


Blower base structure(2/2)



SECTION C-C  
PA3PE3 D-D

SCALE 1:100



**7.Distribution chamber**

**7.1Material and Allowable stress**

**TABLE 7.1 Allowable Stress** (N/mm<sup>2</sup>, kg /cm<sup>2</sup>)

Item		Serviceability strength			Ultimate strength		
		Compression	Tension	Shear	Compression	Tension	Shear
Concrete	B30	10		0.8	30		1.2
		100	-----	8	300	-----	12
Steel Bar Round Bar	A- I	157.0	157.0	157.0	235.4	235.4	235.4
		1600	1600	1600	2400	2400	2400
Steel Bar Deformed Bar	A- II	196.2	196.2	196.2	358.1	358.1	358.1
		2000	2000	2000	3650	3650	3650

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

**TABLE 7.2 Allowable Bonding Stress of Steel Bar to Concrete** (N/mm<sup>2</sup>, kg /cm<sup>2</sup>)

Item	Serviceability strength		Remarks
	Top bars	Other bars	
φ6,φ9,φ12	0.9	1.3	
	9	13.5	
D10,D13,D16 D19,D22,D25,D29	1.6	2.4	
	16.2	24.3	

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

**7.2 Load Table**

**TABLE 7.3 Dead Load**

Loc.	item	thickness	kg/m <sup>2</sup>	total kg/m <sup>2</sup>	Remarks
Slab	Concrete slab	20cm	500		
				500	<----- MKS UNIT
				4905	<----- SI UNIT
foundation	Leveling motar Concrete slab	50cm	1250		
				1250	<----- MKS UNIT
				12263	<----- SI UNIT

**TABLE 7.4 Live Load and Floor Load**

kg/m<sup>2</sup> (Girder, Sub beam : Self weight not included)

Loc.	load type	slab	Remarks
slab	Dead Load	360.0	
	Live Load	500.0	
	Total Load	860.0	
	SI unit	8437	<----- SI UNIT

7.3 Facility weight

Table 7.5 Tank Weight

Story	Load type	Unit w (kN/m <sup>2</sup> ,m)	width /hight (m) or unit	Length (m)	Area or L (m <sup>2</sup> ), (m)	Weight (kN)	Small Total (t)	S Wi (t)
Chamber	slab	4.91	2.5	7.00	17.50	85.84		
	Wall 1	4.91	12	5.60	67.20	329.62		
	Wall 2	4.91	14	5.60	78.40	384.55		
	Water 1	9.81	4.5	2.50	7.00	772.54		
							1572.54	1572.54
Base	1500 Base	12.26	7	8.40	58.80	721.04		
				Σ	58.80	(m <sup>2</sup> )	721.04	(kN) 2293.58

Base Area 58.80 (m<sup>2</sup>)

Total W= 2,293.58

W-Base= 1,572.5

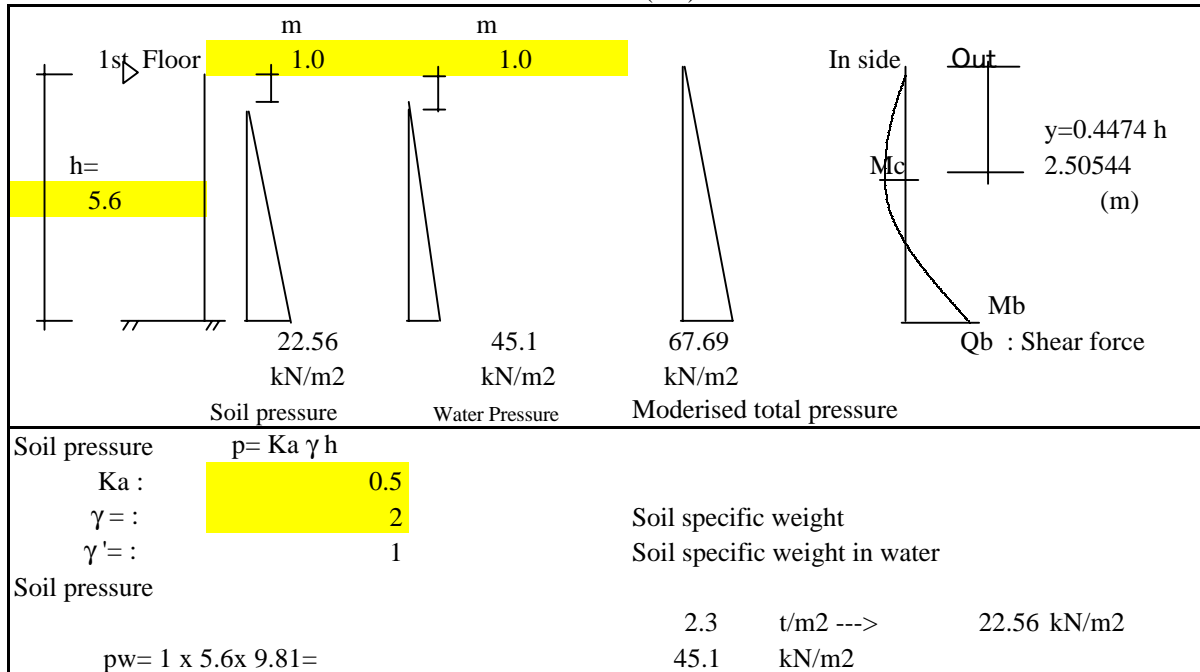
soil reaction =W/(Base area)= 39.006 (kN/m<sup>2</sup>)

## 7.5 Wall and Foundation

Wall 7-1

### LOAD CONDITION

For wall's unit width (1m)



### BENDING MOMENT and SHEAR FORCE

For wall's unit width			
$M_c = 0.06 W h =$	63.68 kNm	$W =$	189.5 kN
$M_b = -2/15 W h =$	-141.52 kNm		
$Q_b = 4/5 W =$	151.62 kN		

### Wall Profile

	external	inner	
Wall thickness $t :$	30 cm	re-bar inside	
$d :$	23 cm	26 cm	
$j = 7/8 d :$	0.201 m	0.2275 m	
Re bar ft :	200 N/mm <sup>2</sup> (196.2 $\approx$ 200)	200 N/mm <sup>2</sup>	
$a_t = M_c / (f_t \times j) =$	14.00 cm <sup>2</sup> / (m wi	5 - D20	15.71 cm <sup>2</sup>
$a_t = M_b / (f_t \times j) =$	35.16 cm <sup>2</sup> / (m wi	10 - D25	49.09 cm <sup>2</sup>
		$w M_c =$	0.68 %
		$w M_b =$	2.13 %

### Wall Shear Stress

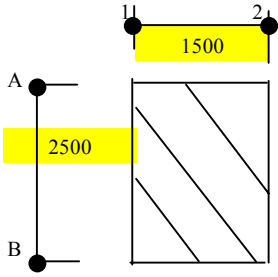
Wall thickness $t :$	30 cm
$d :$	23 cm
$j = 7/8 d :$	0.201 m
Width $W_a :$	100 cm
$Q_b :$	151.62 kN
Shear stress $= Q_b / (W_a j) =$	0.75 N/mm <sup>2</sup> < 0.80 N/mm <sup>2</sup>

### Bottom profile

slab thickness $t :$	50 cm		
$d :$	43 cm		
$j = 7/8 d :$	0.376 m		
Re bar ft :	200 N/mm <sup>2</sup>		
$a_t = M_b / (f_t \times j) =$	18.81 cm <sup>2</sup> / (m wi	10 - D22	38.01 cm <sup>2</sup>
		$w M_c =$	0.88 %

7.6 SLAB

Load condition



A= 3.75 m<sup>2</sup>

Area		unit weight	kN
Floor slab=	3.75	x	8436.6= 31.64
Wall=		x	0.00
			Σ = 31.6

lx=	1.5 m	t(cm)=	20
ly=	2.5 m	d(cm)=	15
λ =	1.67	cover(cm)=	5

	a	wlx2(kNm <sup>2</sup> )	M(Nm)	Additional M from wall	Total M	at= M/(σ sjd)	re-bars	
Mx1=	0.075	18.98	1,423.7		1,424	0.553 cm <sup>2</sup>	upper -->D10@200	3.93cm <sup>2</sup>
Mx2=	0.05	18.98	949.1			0.369 cm <sup>2</sup>	bottom -->D10@200	3.93cm <sup>2</sup>
								0.5%
My1=	0.042	18.98	797.3		797	0.310 cm <sup>2</sup>	upper -->D10@200	3.93cm <sup>2</sup>
My2=	0.028	18.98	531.5			0.206 cm <sup>2</sup>	bottom -->D10@200	3.93cm <sup>2</sup>
		wlx	Q(N)			φ=Q/(ra jd)		0.5%
Qx =	0.52	21.09	10,967.6			3.50 cm <	15.7 ok	
Qy =	0.46	21.09	9,702.1			3.10 cm <	15.7 ok	

Suffix 1: end of span  
 Suffix 2: middle of span  
 From nomogram of two-way slab

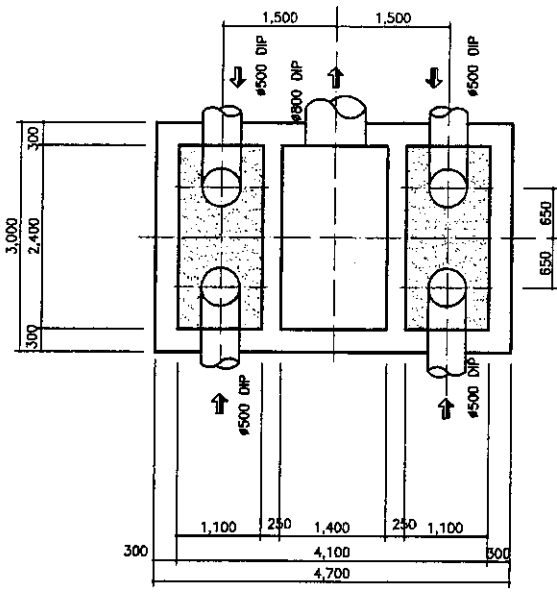
Q cap  
 117,720 N > Q ok  
 117,720 N > Q ok



7.7 Limit state analysis

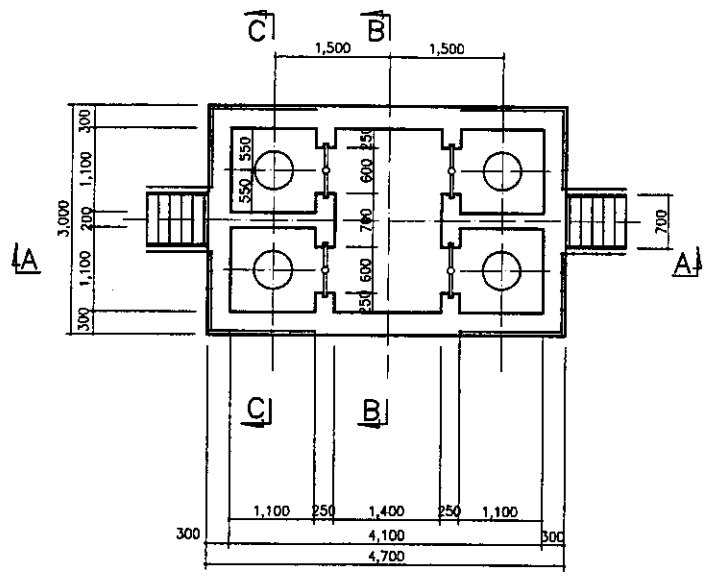
Rectangular section design and limited state analysis				( 1/2 )		
Concrete Permissible Strength		$f'_{ck} =$	17 N/mm <sup>2</sup>	by use of B30 30		
Direct tensile stress		$f_t =$	2.00 N/mm <sup>2</sup>			
Elasticity ratio		$n =$	15			
Elasticity		$E =$	200000 N/mm <sup>2</sup>			
Permissible strength		$\sigma_{sa} =$	250 N/mm <sup>2</sup>	round	from BS	
		$\sigma_{sa} =$	140 N/mm <sup>2</sup>	deformed	from BS	
Ultimate strength (characteristic strength)		$\sigma_s =$	365 N/mm <sup>2</sup>			
Check point				Wall	Slab	
Force	Bending Moment	Md	kN·m	141.5	1.4	
	Shearing force	Sd	kN	151.6	11.0	
Section Spec	Width	b	cm	100	100	
	Height	h	cm	30	20	
	Cover	dt	cm	5	5	
	Effective Height	d	cm	25	15	
Rebar Cross Section	Tension Rebar		cm <sup>2</sup>	10 – D25	5 – D10	
				As = 49.09	As = 3.93	
	Compression Rebar		cm <sup>2</sup>	5 – D20	5 – D10	
				As = 15.71	As = 3.93	
Stress	Concrete stress		N/mm <sup>2</sup>	7.9	0.5	
	Rebar stress		N/mm <sup>2</sup>	131.3	25.5	
	Shearing stress		N/mm <sup>2</sup>	0.720	0.079	
B.M value for crack			Mcr	kNm	28.54	8.47
Crack width	Rebar interval	cs	mm	100	200	
	Rebar diameter	$\phi$	mm	25	10	
	Cover depth	c	mm	40	40	
	Rebar stress	$\sigma_{se}$	N/mm <sup>2</sup>	137.0	26.0	
	Crack width	wcr	mm	0.177	0.082	
<b>Judgement: wcr &lt; 0.2: OK</b>				<b>OK</b>	<b>OK</b>	
Examination with the Ultimate BM Strength						
Ultimate B.M Strength		Mud	kNm	379.62	30.35	
$\gamma_i \cdot Md / Mud$				0.373	0.047	
<b>Judgement: <math>\gamma_i \cdot Md / Mud &lt; 1.0</math>: OK</b>				<b>OK</b>	<b>OK</b>	
Crack width shall be controled as follows:						
		1 normal condition	crack width < 0.3mm			
		2 severe condition	crack width < 0.2mm			
		3 very severe condition	crack width < 0.1mm			

DSTR structure(1/2)



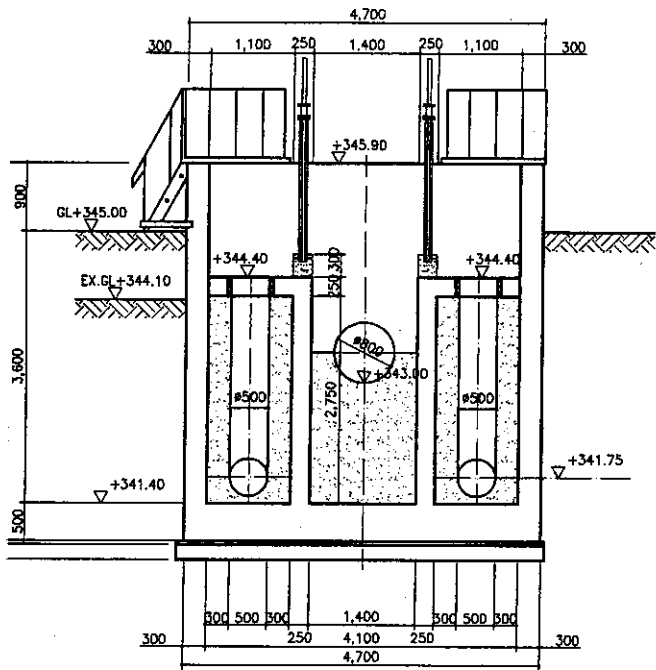
BASE PLAN  
ПЛАН ОСНОВАНИЯ

scale 1:50



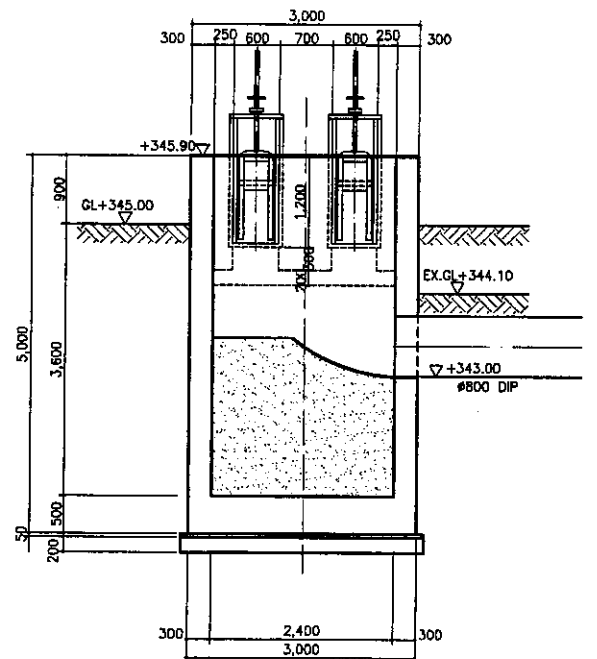
MIDDLE PLAN  
ПЛАН СРЕДНЕЙ ЧАСТИ

scale 1:50



SECTION A-A  
РАЗРЕЗ А-А

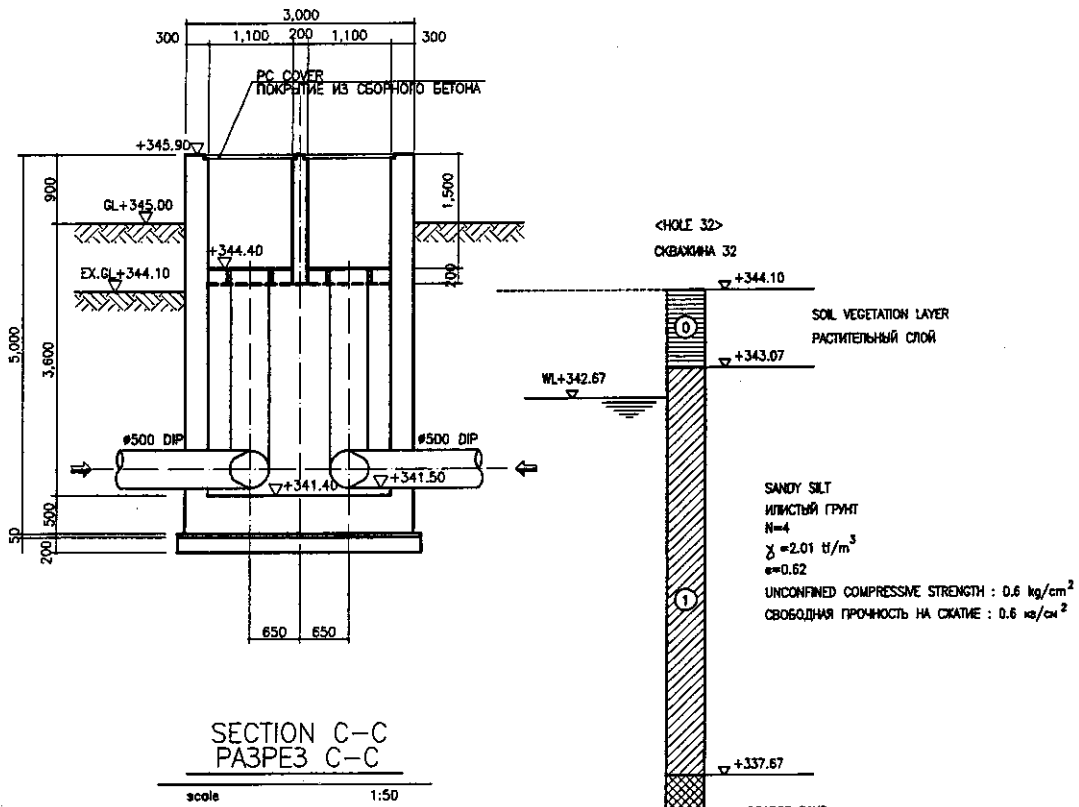
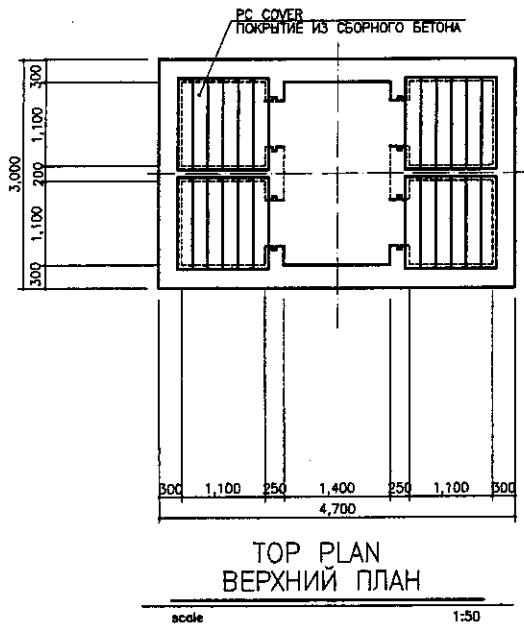
scale 1:50



SECTION B-B  
РАЗРЕЗ В-В

scale 1:50

DSTR structure(2/2)



## 8. Temporary Discharge Pumping Station

### 8.1 Material and Allowable stress

**TABLE 8.1 Allowable Stress** (N/mm<sup>2</sup>, kg/cm<sup>2</sup>)

Item		Serviceability strength			Ultimate strength		
		Compression	Tension	Shear	Compression	Tension	Shear
Concrete	B30	10		0.8	30		1.2
		100	-----	8	300	-----	12
Steel Bar Round Bar	A- I	157.0	157.0	157.0	235.4	235.4	235.4
		1600	1600	1600	2400	2400	2400
Steel Bar Deformed Bar	A- II	196.2	196.2	196.2	358.1	358.1	358.1
		2000	2000	2000	3650	3650	3650

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

**TABLE 8.2 Allowable Bonding Stress of Steel Bar to Concrete**

(N/mm<sup>2</sup>, kg/cm<sup>2</sup>)

Item	Serviceability strength		Remarks
	Top bars	Other bars	
φ6,φ9,φ12	0.9	1.3	
	9	13.5	
D10,D13,D16	1.6	2.4	
	16.2	24.3	

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

### 8.2 Load Table

**TABLE 8.3 Dead Load**

Loc.	item	thickness	kg/m <sup>2</sup>	total kg/m <sup>2</sup>	Remarks
Common slab	Leveling motar	-	-		
	Concrete slab	20cm	500		
				500	<----- MKS UNIT
				4905	<----- SI UNIT

**TABLE 8.4 Live Load and Floor Load**

kg/m<sup>2</sup> (Girder, Sub beam : Self weight not included)

Loc.	load type	slab	beam	girder	Remarks
Other floor	Dead Load	500.0	500.0	500.0	
	Live Load	1000.0	1000.0	1000.0	Load of heavy equipment
	Total Load	1500.0	1500.0	1500.0	
	SI unit	14715	14715	14715	<----- SI UNIT

### 8.3 Facility weight

**Table 8.4 Temp. I.P.S Weight**

Story	Load type	Unit w (kN/m <sup>2</sup> ,m)	width /hight (m) or unit	Length (m)	Area or L (m <sup>2</sup> ), (m)	Weight (kN)	Small Total (kN)	S Wi (kN)
structure	slab	14.72	7	-	62.39	918.05		
	Girder 6m	2.94	1	6.00	6.00	17.66		
	Beam 3m*2	2.94	2	3.00	6.00	17.66		
	Machine	34.335	3	-	-	103.01		
	Wall.1 6.415m	12.263	6.415	20.42	131.00	1606.35		
	Water	9.81	6.415	28.27	181.38	1779.34		
							4442.06	4442.06
Base	t600 Base	14.72	1	28.27	28.27	416.06		
				Σ	28.27 (m <sup>2</sup> )		416.06	(kN)

Base Area 28.27 (m<sup>2</sup>)

Total W= 4,858.12

W-Base= 4,442.1

soil reaction =W/(Base area) 171.820 (kN/m<sup>2</sup>)

Foundation's design force= 157.105 (kN/m<sup>2</sup>)

8.3.Wall of cylindrical tanks for Temp DPS

( / )

1) Spec of Tank

Diameter	d	<input type="text" value="6"/>	m	Unit Water load	DI	1.0 t/m <sup>3</sup> =	<input type="text" value="9.81"/>	kN/m <sup>3</sup>
Water Depth	h	<input type="text" value="4.1"/>	m	Supporting condition of bottom :		Rigid		
Wall Thickness	t	<input type="text" value="500"/>	mm			$\alpha e$ :	<input type="text" value="15"/>	
Wall height	h1	<input type="text" value="6.415"/>	m	$f_{st} =$	<input type="text" value="120"/>	N/mm <sup>2</sup>		
				$f_{ct} =$	<input type="text" value="2.00"/>	N/mm <sup>2</sup>	$f_{cu} =$	<input type="text" value="30"/>
Unit concrete weight		<input type="text" value="23.544"/>	kN/m <sup>3</sup>	permissible tensile stress		not used		

2) Employed Equation for analysis

\*Same with the former section

3) Forces and Bending Moment /Reinforcement

0  $h^2/d/t =$   then  $K1 =$    $K2 =$    $K3 =$

By table 184, pp.405

- 1 BM at bottom=  kN/m
- 2 Position height of max tension =  m above the bottom
- 3 Max circumference tension =  kN/m around the position of the above
- 4 Required  $A_s =$   cm<sup>2</sup>

- 5 Min. thickness of wall =  mm
- 6 Direct comp.=  kN/m<sup>2</sup>  
=  N/mm<sup>2</sup>

Reinforcement	
4- D16	/m
4- D16	/m
$A_s =$ 16.085	cm <sup>2</sup>
pt= 0.3217	% > 0.3%
4- D14	/m

- 7 Distribution Rebar 1 rank lower spec. of main rebar

8.4 Foundation

1) Effect of water pressure

Ground Level =	<input type="text" value="343.4"/>	m
Ground Water Level =	<input type="text" value="342"/>	m
Bottom slab level=	<input type="text" value="337.0"/>	m
Height of Bottom slab=	<input type="text" value="0.6"/>	m
Soffit of bottom slab=	<input type="text" value="5.6"/>	m

Upward thrust by water pressure

$p =$  9.81 kN/m<sup>3</sup>  $\times$   =  kN/m<sup>2</sup>

$A =$   m<sup>2</sup> (including wall thickness)

$P =$   kN

2) Bottom slab depth and reinforcement

\*Basement including structure wall must be designed to prevent flotation

Weight		
GL slab	<input type="text" value="236.7"/>	kN (Slab thickness <input type="text" value="0.2"/> m)
wall	<input type="text" value="1542"/>	kN
Total	<input type="text" value="1779"/>	kN

Cohesion Force  kN/m<sup>2</sup>  m<sup>2</sup> =

\*no cohesion Required weight for bottom  -  =  kN

Minimum depth  $F_s = 1.0$   $t =$   m

\*cohesion included  -  =  kN

When cohesion force between wall and soil included, additional depth for bottom slab is not necessary.

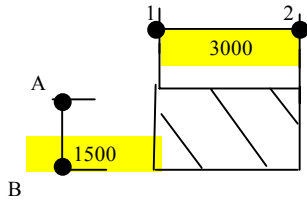
The depth shall be decided by the structural requirements.  $t =$   m

\*Reinforcement

Radial reinforcement

8.5 Slab

Load condition



Area unit weight kN  
 Floor slab= 4.50 x 14,715.0 66.22  
 Wall= x 0.00  
 Σ = 66.2  
 Soil reaction load= 14.72 kN/m²  
 lx= 1.5 m  
 ly= 3 m t(cm)= 20  
 λ = 2.00 d(cm)= 15  
 cover(cm)= 5

A= 4.5 m²


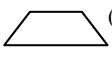

	a	wlx2(kNm²)	M(Nm)	Additional M from wall	Total M	at= M/(σ sjd)	re-bars	
Mx1=	0.078	33.11	2,582.5	0	2,582	1.003 cm²	bottom 2-D10-->D10@100	7.85cm²
Mx2=	0.052	33.11	1,721.7			0.669 cm²	upper 2-D10-->D10@100	7.85cm²
								1.0%
My1=	0.042	33.11	1,390.6	0	1,391	0.540 cm²	bottom 2-D10-->D10@100	7.85cm²
My2=	0.028	33.11	927.0			0.360 cm²	upper 2-D10-->D10@100	7.85cm²
		wlx	Q(N)			φ=Q/(τα jd)		1.0%
Qx =	0.52	22.07	11,477.7			3.67 cm <	31.4 ok	
Qy =	0.46	22.07	10,153.4			3.24 cm <	31.4 ok	

Suffix 1: end of span  
 Suffix 2: middle of span  
 From nomogram of two-way slab  
 Q cap  
 117,720 N > Q ok  
 117,720 N > Q ok

8.6 BEAMS

1) Beam

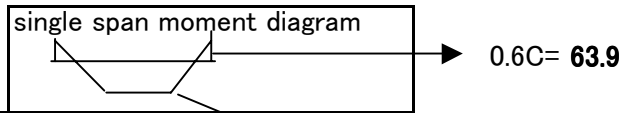
**B1**

B1  bxD 40x60 (cm)	Load form	 (slab load)	 (slab load) *2	 (girder load)+ other loads		Σ		
	Co	C/w 0.00	Co 0.00	Co/w 7.03	Co 103.42	w/1 4.11	Co 3.08	kNm 106.51
	Mo	M/w 0.00	Mo 0.00	Mo/w 7.22	Mo 106.25	w/1 4.11	Mo 4.63	kNm 110.87
	Q	Q/w 0.00	Q 0.00	Q/w 1.69	Q 24.83	w/1 4.11	Q 6.17	kN 31.00
	Slab load =	14.715 (kN/m <sup>2</sup> )		ly=	3 m		λ= 2.00	
Span =	3 (m)		lx=	1.50 m				

1. Girder load= 4.11 kN/m  
dead load

2. Line load = 0.00 kN/m + 0.00 kN/m = 0.00 kN/m  
roof wall

Total = 4.11 kN/m



2) Determination of beam B1

Beam ID	B1			Remarks
Position	B end	Mid	C end	
D.L ] M(kNm)	63.9		63.9	seismic force neglected
+ ] bott.		73.6		
L.L ] Q (kN)	31.00		31.00	
Size ] b x D (cm)	35	x	50	
] d (cm)			45	
] j (cm)			39.375	
top	8.3		8.3	cm <sup>2</sup>
	3D22		3D22	at= M/(σ sjd)
bottom		9.5		cm <sup>2</sup>
		3D22		
τ=Q/bjd	0.22		0.22	N/mm <sup>2</sup>
top	0.72		0.72	min.0.4%
Pt (%) bott.		0.72		
top	11.4		11.4	
at (cm <sup>2</sup> ) bott.		11.4		
Main Bars	3	3	3	
		D22		
	3	3	3	
φ (cm)	20.724		20.724	
Q/fa.j (cm)	0.38		0.38	max
judge	ok		ok	1.7
fs.bj LT(ST)	106.1		106.1	kN
(t)	D10-250	D10-250	D10-250	
judge	ok		ok	

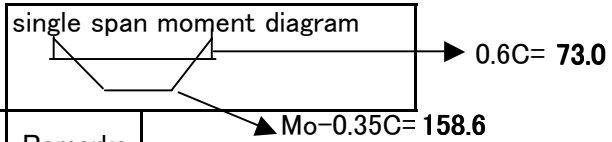
2) Girder

G1

	Load form	(slab load) *2		(slab load)		P (gider load)+		Σ
		Co/w	Co	Co/w	Co	w/1	Co	
2B2	Co	8.16	120.02	-	0.00	0.56	1.69	121.71
bxD 30x75	Mo	13.50	198.65	-	0.00	0.56	2.53	201.18
	Q	6.75	99.33	-	0.00	0.56	1.69	101.01
Slab load =		14.715 (kN/m <sup>2</sup> )		ly= 3.00 m				
Span =		6 (m)		lx= 3.00 m				λ= 1.00

1. Girder load = 5.64 kN/m  
 dead load  
 2. Line load = 0.00 kN/m + 0.00 kN/m = 0.00 kN/m  
 roof wall

Total = 5.64 kN/m



2) Determination of beam B1

Beam ID	B1			Remarks
Position	B end	Mid	C end	
D.L ] M(kNm)		73.0	73.0	
+ ] bott.		158.6		
L.L ] Q(kN)		101.01	101.01	
] b x D (cm)	40	x	60	
Size ] d (cm)			55	
] j (cm)			48.125	
top	7.7		7.7	cm <sup>2</sup> at= M/(σ s j d)
	3D20		3D20	
bottom		16.8		cm <sup>2</sup>
		4D25		
τ=Q/bjd	0.73		0.73	N/mm <sup>2</sup>
top	0.43		0.43	min.0.4%
Pt (%) bott.		0.89		
top	9.42		9.42	
at (cm <sup>2</sup> ) bott.		19.64		
Main Bars	top 3	D20	3	
		D25		
bot	2	4	2	
φ (cm)	18.84		18.84	max
Q/fa.j (cm)	1.11		1.11	
judge	ok		ok	1.7
fs.bj LT(ST)	148.2		148.2	kN
(t)	D10-250	D10-250	D10-250	
judge	ok		ok	

seismic force neglected



8.7 Limit state analysis

Rectangular section design and limited state analysis				( 1/2 )	
Concrete Permissible Strength		$f'_{ck} =$	17 N/mm <sup>2</sup>	by use of B30 30	
Direct tensile stress		$f_t =$	2.00 N/mm <sup>2</sup>		
Elasticity ratio		$n =$	15		
Elasticity		$E =$	200000 N/mm <sup>2</sup>		
Permissible strength		$\sigma_{sa} =$	250 N/mm <sup>2</sup>	round from BS	
		$\sigma_{sa} =$	140 N/mm <sup>2</sup>	deformed from BS	
Ultimate strength (characteristic strength)		$\sigma_s =$	365 N/mm <sup>2</sup>		
Check point				Beam B1	Girder G1
Force	Bending Moment	Md	kN·m	63.9	73.0
	Shearing force	Sd	kN	31.0	101.0
Section Spec	Width	b	cm	35	40
	Height	h	cm	50	60
	Cover	dt	cm	5	5
	Effective Height	d	cm	45	55
Rebar Cross Section	Tension Rebar		cm <sup>2</sup>	3— D20	
				As= 9.42	
	Compression Rebar		cm <sup>2</sup>	2— D25	
				As= 9.82	
Stress	Concrete stress		N/mm <sup>2</sup>	4.2	
	Rebar stress		N/mm <sup>2</sup>	160.6	
	Shearing stress		N/mm <sup>2</sup>	0.217	
B.M value for crack		Mcr	kNm	20.28	32.16
Crack width	Rebar interval	cs	mm	80	100
	Rebar diameter	$\phi$	mm	20	20
	Cover depth	c	mm	40	40
	Rebar stress	$\sigma_{se}$	N/mm <sup>2</sup>	166.2	153.9
	Crack width	wcr	mm	0.198	0.199
<b>Judgement: wcr&lt;0.2: OK</b>				<b>OK</b>	<b>OK</b>
Examination with the Ultimate BM Strength					
Ultimate B.M Strength		Mud	kNm	146.02	181.55
$\gamma_i \cdot Md / Mud$				0.438	0.402
Judgement: $\gamma_i \cdot Md / Mud < 1.0$ : OK				OK	OK
Crack width shall be controlled as follows:					
		1 normal condition	crack width < 0.3mm		
		2 severe condition	crack width < 0.2mm		
		3 very severe condition	crack width < 0.1mm		

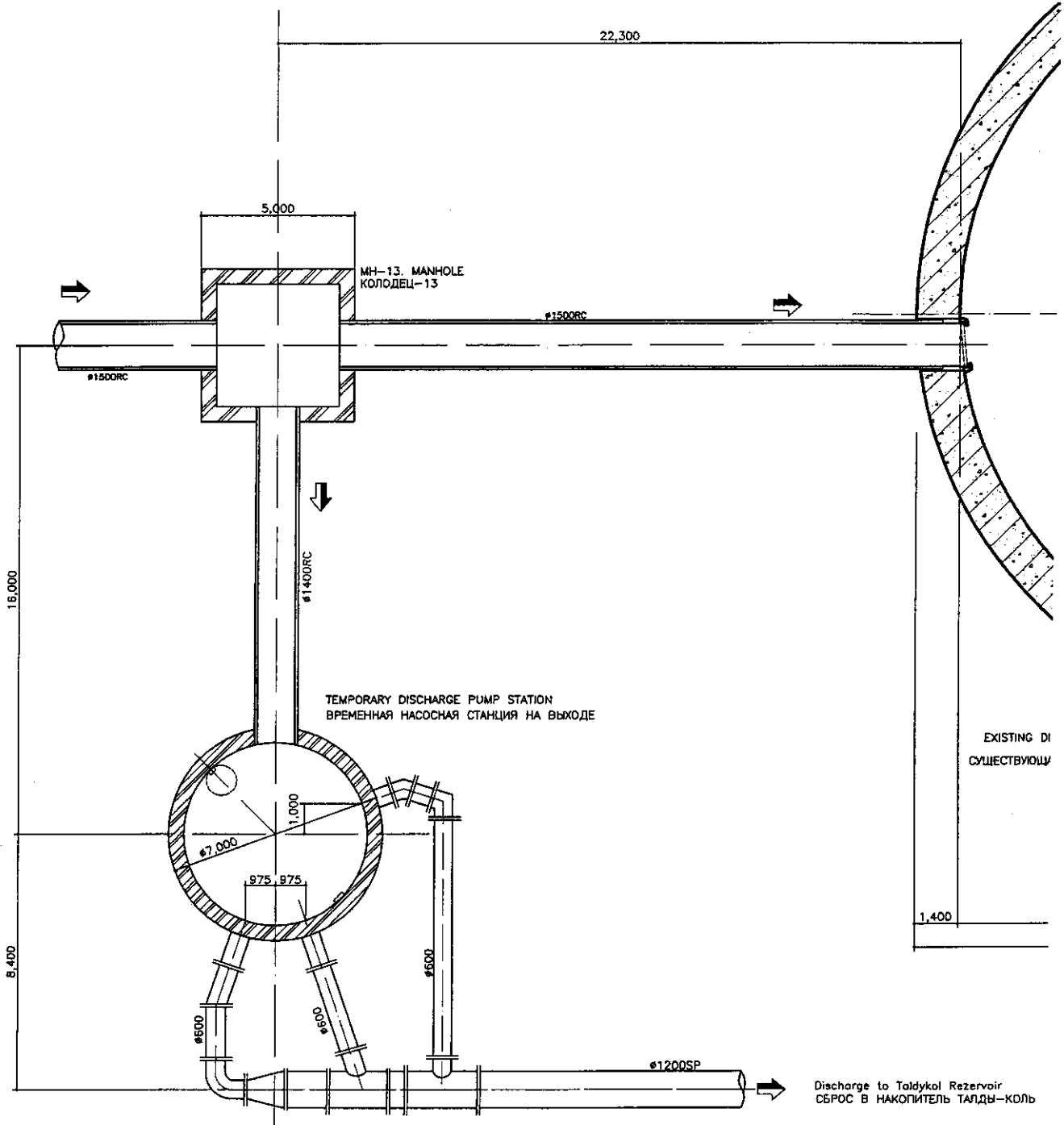
**Rectanglar section design and limited state analysis**

( 2/2 )

Concrete Permissible Strength	$f_{ck} =$	17 N/mm <sup>2</sup>	by use of B30	30
Direct tensile stress	$f_t =$	2.00 N/mm <sup>2</sup>		
Elasticity ratio	$n =$	15		
Elasticity	$E =$	200000 N/mm <sup>2</sup>		
Permissible strength	$\sigma_{sa} =$	250 N/mm <sup>2</sup>	round from BS	
	$\sigma_{sa} =$	140 N/mm <sup>2</sup>	deforme from BS	
Ultimate strength (characteristic strength)	$\sigma_s =$	365 N/mm <sup>2</sup>		

Check point				Slab			
Force	Bending Moment	Md	kN·m	2.6			
	Shearing force	Sd	kN	11.5			
Section Spec	Width	b	cm	100			
	Height	h	cm	20	#REF!		
	Cover	dt	cm	5	5		
	Effective Height	d	cm	15	#REF!		
Rebar Cross Section	Tension Rebar		cm <sup>2</sup>	10— D10	0— D0		
				As = 7.85			
	Compression Rebar		cm <sup>2</sup>	10— D10	0— D0		
				As = 7.85			
Stress	Concrete stress		N/mm <sup>2</sup>	0.6	#VALUE!		
	Rebar stress		N/mm <sup>2</sup>	23.4	#VALUE!		
	Shearing stress		N/mm <sup>2</sup>	0.084	#DIV/0!		
B.M value for crack				Mcr	kNm	9.15	#REF!
Crack width	Rebar interval	cs	mm	100	0		
	Rebar diameter	$\phi$	mm	10	0		
	Cover depth	c	mm	40	0		
	Rebar stress	$\sigma_{se}$	N/mm <sup>2</sup>	24.1	#VALUE!		
	<b>Crack width</b>	wcr	mm	0.060	#VALUE!		
<b>Judgement: wcr &lt; 0.2: OK</b>				<b>OK</b>	<b>0.00</b>		
Examination with the Ultimate BM Strength							
Ultimate B.M Strength		Mud	kNm	48.21	#DIV/0!		
$\gamma_i \cdot Md / Mud$				0.054	#DIV/0!		
Judgement: $\gamma_i \cdot Md / Mud < 1.0$ : OK				OK	0		
Crack width shall be controled as follows:							
		1 normal condition	crack width < 0.3mm				
		2 severe condition	crack width < 0.2mm				
		3 very severe condition	crack width < 0.1mm				

Temp Discharge PS structure(1/2)

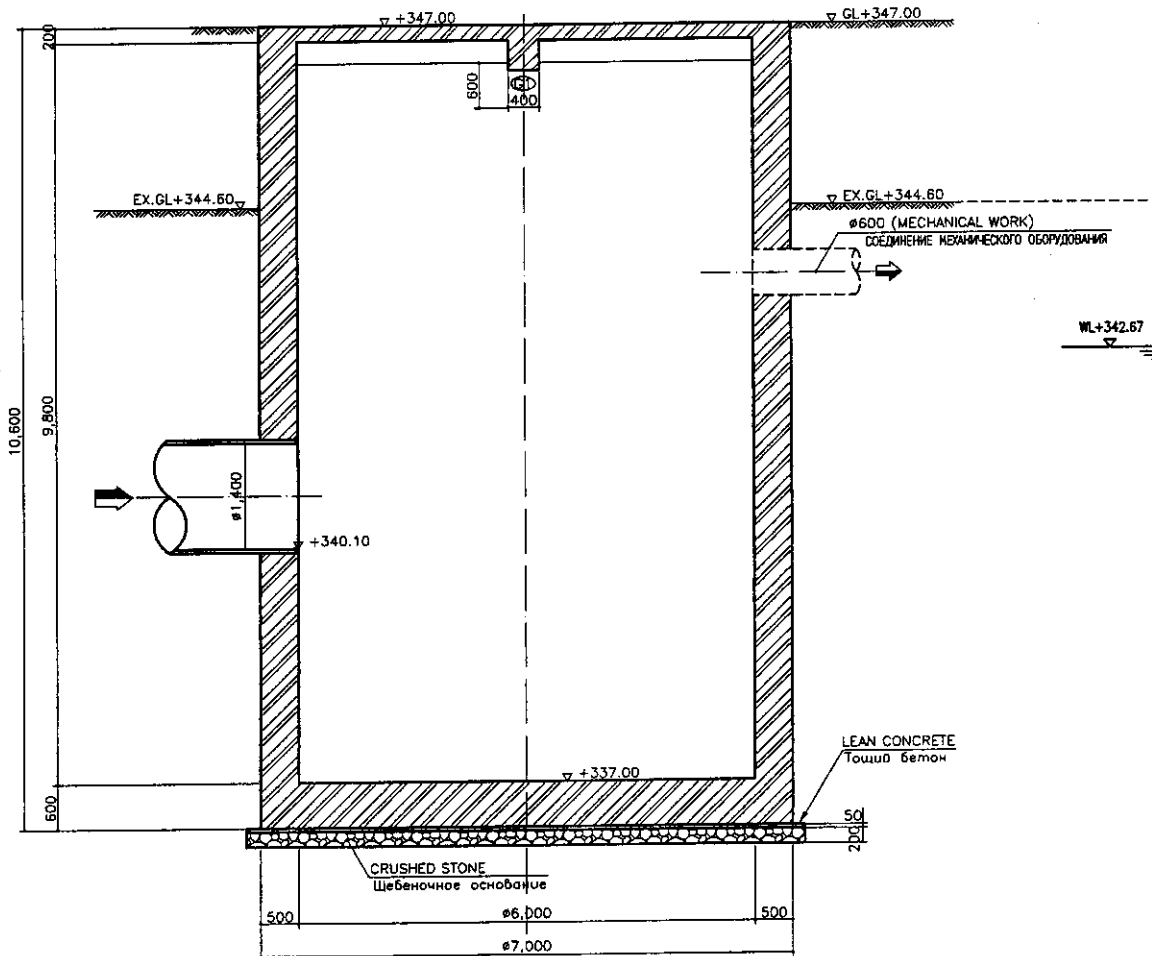
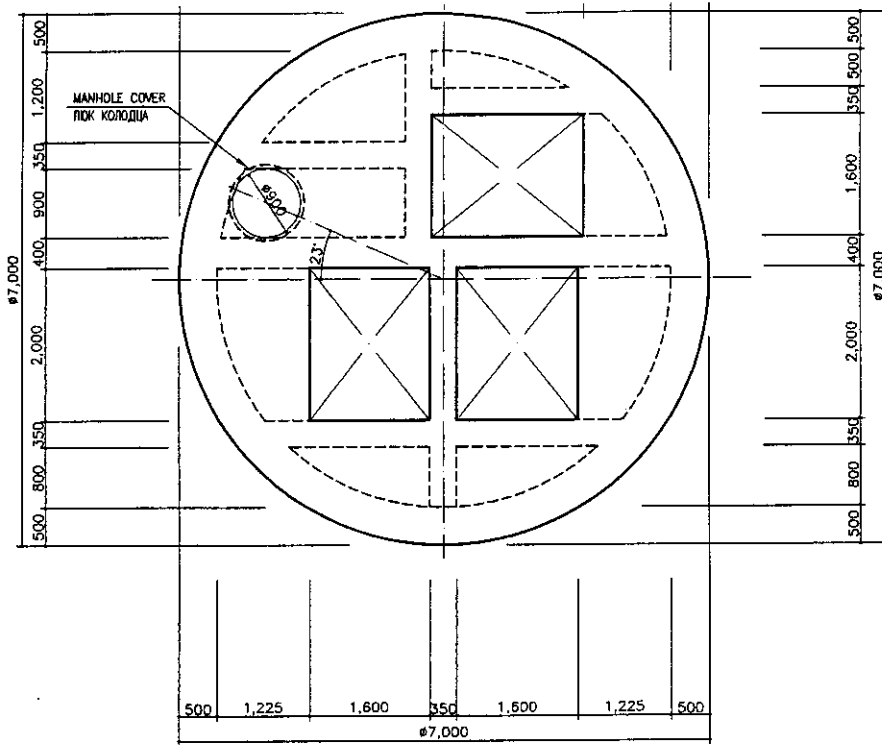


DISCHARGE PUMP FACILITY LAYOUT  
 ГЕН. ПЛАН СООРУЖЕНИЙ Н.С. НА ВЫХОДЕ

SCALE

11

Temp Discharge PS structure(2/2)



SECTION A-A  
РАЗРЕЗ A-A

SCALE 1:50

**9. Manhole pump station**

**9.1 Material and Allowable stress**

**TABLE 3.1 Allowable Stress** (N/mm<sup>2</sup>, kg /cm<sup>2</sup>)

Item		Serviceability strength			Ultimate strength		
		Compression	Tension	Shear	Compression	Tension	Shear
Concrete	B30	10		0.8	30		1.2
		100	-----	8	300	-----	12
Steel Bar Round Bar	A- I	157.0	157.0	157.0	235.4	235.4	235.4
		1600	1600	1600	2400	2400	2400
Steel Bar Deformed Bar	A- II	196.2	196.2	196.2	358.1	358.1	358.1
		2000	2000	2000	3650	3650	3650

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

**TABLE 3.2 Allowable Bonding Stress of Steel Bar to Concrete**

(N/mm<sup>2</sup>, kg /cm<sup>2</sup>)

Item	Serviceability strength		Remarks
	Top bars	Other bars	
φ6,φ9,φ12	0.9	1.3	
	9	13.5	
D10,D13,D16	1.6	2.4	
	16.2	24.3	

upper: SI units N/mm<sup>2</sup>

lower: MKS units kg/cm<sup>2</sup>

**9.2 Load Table**

**TABLE 3.3 Dead Load**

Loc.	item	thickness	kg/m <sup>2</sup>	total kg/m <sup>2</sup>	Remarks
Common slab	Leveling motar	-	-		
	Precast concrete cover	15cm	375		
				375	<----- MKS UNIT
				3679	<----- SI UNIT

**TABLE 3.4 Live Load and Floor Load**

kg/m<sup>2</sup> (Girder, Sub beam : Self weight not included)

Loc.	load type	slab	beam	girder	Remarks
Other floor	Dead Load	375.0	375.0	375.0	
	Live Load	360.0	360.0	360.0	Load of heay equipment
	Total Load	735.0	735.0	735.0	
	SI unit	7210	7210	7210	<----- SI UNIT

**3.3 Facility weight**

**Table3.4 Temp. I.P.S Weight**

Story	Load type	Unit w (kN/m <sup>2</sup> ,m)	width /hight (m) or unit	Length (m)	Area or L (m <sup>2</sup> ), (m)	Weight (kN)	Small Total (kN)	S Wi (kN)
structure	cover	7.21	2.5	-	7.96	57.38		
	Machine	3.5316	2	-	-	7.06		
	Wall.1 9.03m	12.263	9.03	20.42	184.40	2261.16		
	Water	9.81	9.03	28.27	255.32	2504.67		
							4830.27	4830.27
Base	t600 Base	14.72	1	28.27	28.27	416.06		
				Σ	28.27	(m <sup>2</sup> )	416.06	(kN)

Base Area 28.27 (m<sup>2</sup>)

Total W= 5,246.33

W-Base= 4,830.3

soil reaction =W/(Base area)= 185.550 (kN/m<sup>2</sup>)

Foundation's design force=	170.835 (kN/m <sup>2</sup> )
----------------------------	------------------------------

9.3.1 H=6.9(IH) and 7.0(28)

<b>1) Spec of Tank</b>			
Diameter	d	2.5 m	Unit Water load DI 1.0 t/m <sup>3</sup> = 9.81 kN/m <sup>3</sup>
Water Depth	h	2.15 m	Supporting condition of bottom : Rigid
Wall Thickness	t	400 mm	$\alpha e$ : 15
Wall height	h1	7.00 m	f <sub>st</sub> = 120 N/mm <sup>2</sup>
			f <sub>ct</sub> = 2.00 N/mm <sup>2</sup>
Unit concrete weight		23.544 kN/m <sup>3</sup>	f <sub>cu</sub> = 30
			permissible tensile stress not used

**2) Employed Equation for analysis**  
 \*Same with the former section

<b>3) Forces and Bending Moment /Reinforcement</b>			
0	$h^2/d/t=$	49.00	then K1= 0.002 K2= 0.195 K3= 0.83
			By table 184, pp.405
1	BM at bottom=	19.62 kN/m	
2	Position height of max tension =	0.419 m	above the bottom
3	Max circumference tension =	21.88 kN/m	around the position of the above
4	Required As=	1.82 cm <sup>2</sup>	
5	Min. thickness of wall =	10.11 mm	
6	Direct comp.=	112.3 kN/m <sup>2</sup>	
	=	0.112 N/mm <sup>2</sup>	
7	Shearing force $\sqrt{1}=F/PI/d$	1.34 kN	
8	Distribution Rebar	1 rank lower spec. of main rebar	4-D14 /m

<b>Reinforcement</b>	
4-D16	/m
4-D16	/m
As=	16.085 cm <sup>2</sup>
pt=	0.40212 % > 0.3%

**3.2. Foundation**

<b>1) Effect of water pressure</b>	
Ground Level =	360.4 m
Ground Water Level =	358.4 m
Bottom slab level=	353.4 m
Height of Bottom slab=	0.5 m
Soffit of bottom slab=	5.5 m
Upward thrust by water pressure	
$p=$	9.81 kN/m <sup>3</sup> × 5.5 = 53.96 kN/m <sup>2</sup>
A=	13.2 m <sup>2</sup> (including wall thickness)
P=	712.3 kN

<b>2) Bottom slab depth and reinforcement</b>			
*Basement including structure wall must be designed to prevent flotation			
Weight			
GL slab	46.63 kN	(Slab thickness	0.15 m)
wall	600.6 kN		
cutting edge	51.48 kN		
underwater concrete	33.71 kN		
Total	732.4 kN	>	712.3 OK
Cohesion Force	29.43 kN/m <sup>2</sup>	72.5 m <sup>2</sup>	= 2135
*no cohesion	Required weight for bottom	712.3	- 732.42 = -20.1 kN
Minimum depth	Fs=1.0	t= -0.06 m	
*cohesion included		712.3	- 2867.1 = -2154.7 kN

When cohesion force between wall and soil included, additional depth for bottom slab is not necessary. The depth shall be decided by the structural requirements. -----> t= 0.4 m

\*Reinforcement  
 Radial reinforcement 250@ D16

9.3.2 H=4.5(34) and 4.8(37)

<b>1) Spec of Tank</b>			
Diameter	d	2.5 m	Unit Water load DI 1.0 t/m <sup>3</sup> = 9.81 kN/m <sup>3</sup>
Water Depth	h	1.7 m	Supporting condition of bottom : Rigid
Wall Thickness	t	300 mm	α e: 15
Wall height	h1	4.80 m	f st = 120 N/mm <sup>2</sup>
			f ct = 2.00 N/mm <sup>2</sup>
			f <sub>cu</sub> = 30
Unit concrete weight		23.544 kN/m <sup>3</sup>	permissible tensile stress not used

**2) Employed Equation for analysis**  
 \*Same with the former section

<b>3) Forces and Bending Moment /Reinforcement</b>			
0	$h^2/d/t =$	30.72	then K1= 0.0045 K2= 0.25 K3= 0.78
			By table 184, pp.405
1	BM at bottom=	44.15 kN/m	
2	Position height of max tension =	0.425 m	above the bottom
3	Max circumference tension =	16.26 kN/m	around the position of the above
4	Required As=	1.36 cm <sup>2</sup>	
5	Min. thickness of wall =	7.99 mm	
6	Direct comp.=	118.3 kN/m <sup>2</sup>	
	=	0.118 N/mm <sup>2</sup>	
7	Shearing force $\sqrt{1}=F/PI/d$	1.06 kN	
8	Distribution Rebar	1 rank lower spec. of main rebar	4-D12 /m

Reinforcement

4-D14	/m
4-D14	/m
As = 12.3151	cm <sup>2</sup>
pt = 0.4105	% > 0.3%

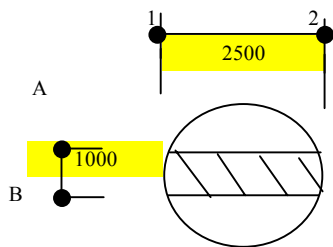
**3.2. Foundation**

<b>1) Effect of water pressure</b>		Ground Level =	346.7 m
		Ground Water Level =	344.7 m
		Bottom slab level=	341.9 m
		Height of Bottom slab=	0.5 m
		Soffit of bottom slab=	3.3 m
	Upward thrust by water pressure		
	p=	9.81 kN/m <sup>3</sup> × 3.3 =	32.37 kN/m <sup>2</sup>
	A=	10.8 m <sup>2</sup> (including wall thickness)	
	P=	348.1 kN	

<b>2) Bottom slab depth and reinforcement</b>			
*Basement including structure wall must be designed to prevent flotation			
Weight			
GL slab	37.97 kN	(Slab thickness	0.15 m)
wall	298.2 kN		
cutting edge	37.28 kN		
underwater concrete	33.71 kN	t=0.5m	
Total	407.2 kN	> 348.1	OK
Cohesion Force	29.43 kN/m <sup>2</sup>	46.7 m <sup>2</sup>	= 1375
*no cohesion	Required weight for bottom	348.1 - 407.19 =	-59.1 kN
	Minimum depth Fs=1.0	t=	-0.23 m
*cohesion included		348.1 - 1782.3 =	-1434.2 kN
When cohesion force between wall and soil included, additional depth for bottom slab is not necessary. The depth shall be decided by the structural requirements. -----> t= 0.4 m			
*Reinforcement			
Radial reinforcement			250@ D14

9.4 Cover (Common for 4 MPS)

Load condition



Diameter 2500

A= 2.5 m<sup>2</sup>

	Area		unit weight	kN
Floor slab=	2.50	x	7,210.4	18.03
Wall=		x		0.00
			Σ =	18.0
	Soil reaction load=			7.21 kN/m <sup>2</sup>

lx=	1 m	t(cm)=	15
ly=	2.5 m	d(cm)=	10
λ =	2.50	cover(cm)=	5

	a	wlx2(kNm2)	M(Nm)	Additional M from wall	Total M	at= M/(σ sjd)	re-bars	
Mx1=	0.078	7.21	562.4	0	562	0.328 cm <sup>2</sup>	bottom 2-D10-->D10@100	7.85cm <sup>2</sup>
Mx2=	0.052	7.21	374.9			0.218 cm <sup>2</sup>	upper 2-D10-->D10@100	7.85cm <sup>2</sup>
								1.6%
My1=	0.042	7.21	302.8	0	303	0.176 cm <sup>2</sup>	bottom 2-D10-->D10@100	7.85cm <sup>2</sup>
My2=	0.028	7.21	201.9			0.118 cm <sup>2</sup>	upper 2-D10-->D10@100	7.85cm <sup>2</sup>
		wlx	Q(N)			φ=Q/(τa jd)		1.6%
Qx =	0.52	7.21	3,749.4			1.80 cm <	31.4 ok	
Qy =	0.46	7.21	3,316.8			1.59 cm <	31.4 ok	

Suffix 1: end of span

Suffix 2: middle of span

From nomogram of two-way slab

Q cap

78,480 N > Q ok

78,480 N > Q ok



9.4 Limit state analysis

Rectangular section design and limited state analysis				( 1/2 )	
Concrete Permissible Strength		$f_{ck} =$	17 N/mm <sup>2</sup>	by use of B30 30	
Direct tensile stress		$f_t =$	2.00 N/mm <sup>2</sup>		
Elasticity ratio		$n =$	15		
Elasticity		$E =$	200000 N/mm <sup>2</sup>		
Permissible strength		$\sigma_{sa} =$	250 N/mm <sup>2</sup>	round	from BS
		$\sigma_{sa} =$	140 N/mm <sup>2</sup>	deformed	from BS
Ultimate strength (characteristic strength)		$\sigma_s =$	365 N/mm <sup>2</sup>		
Check point			cover	Wall No.28 PS	
Force	Bending Moment	Md	kN·m	0.56	19.6
	Shearing force	Sd	kN	0.30	1.3
Section Spec	Width	b	cm	100	100
	Height	h	cm	15	40
	Cover	dt	cm	5	5
	Effective Height	d	cm	10	35
Rebar Cross Section	Tension Rebar		cm <sup>2</sup>	10— D10	4— D14
				As = 7.85	As = 6.16
	Compression Rebar		cm <sup>2</sup>	10— D10	4— D14
				As = 7.85	As = 6.16
Stress	Concrete stress		N/mm <sup>2</sup>	0.2	1.4
	Rebar stress		N/mm <sup>2</sup>	7.6	95.7
	Shearing stress		N/mm <sup>2</sup>	0.003	0.004
B.M value for crack			Mcr	kNm	5.41
Crack width	Rebar interval	cs	mm	80	125
	Rebar diameter	$\phi$	mm	10	14
	Cover depth	c	mm	40	40
	Rebar stress	$\sigma_{se}$	N/mm <sup>2</sup>	7.9	97.0
	Crack width	wcr	mm	0.040	0.151
Judgement: wcr < 0.2 : OK				OK	OK
Examination with the Ultimate BM Strength					
Ultimate B.M Strength		Mud	kNm	33.87	85.77
$\gamma_i \cdot Md / Mud$				0.017	0.229
Judgement: $\gamma_i \cdot Md / Mud < 1.0$ : OK				OK	OK
Crack width shall be controlled as follows:					
1 normal condition		crack width < 0.3mm			
2 severe condition		crack width < 0.2mm			
3 very severe condition		crack width < 0.1mm			

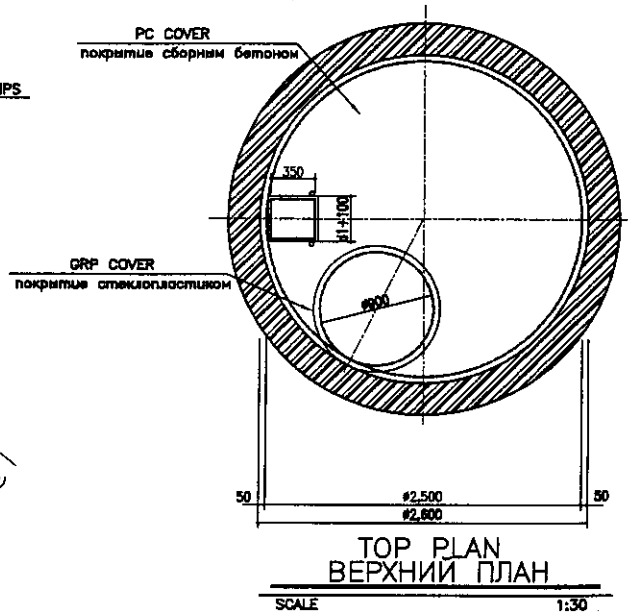
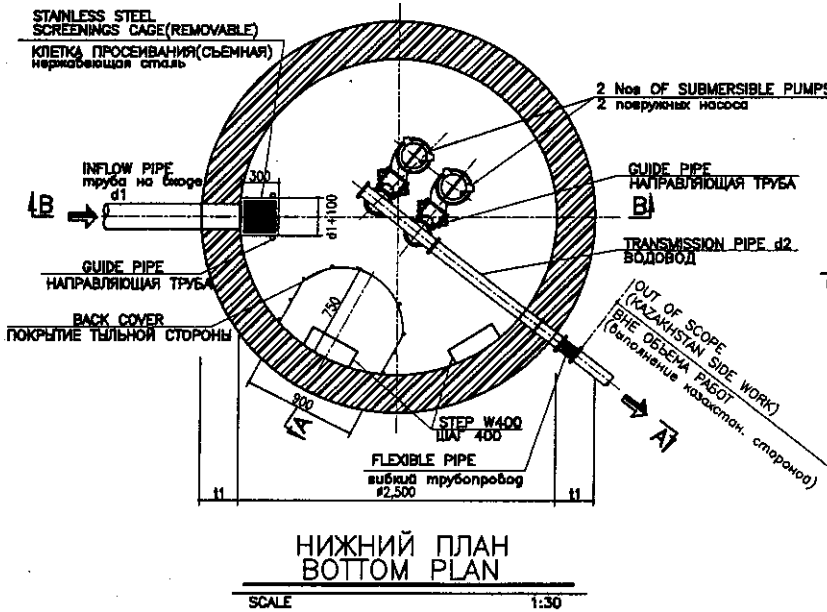
Dimensions of Manhole Type Pump Station

Размеры КНС колодезного типа

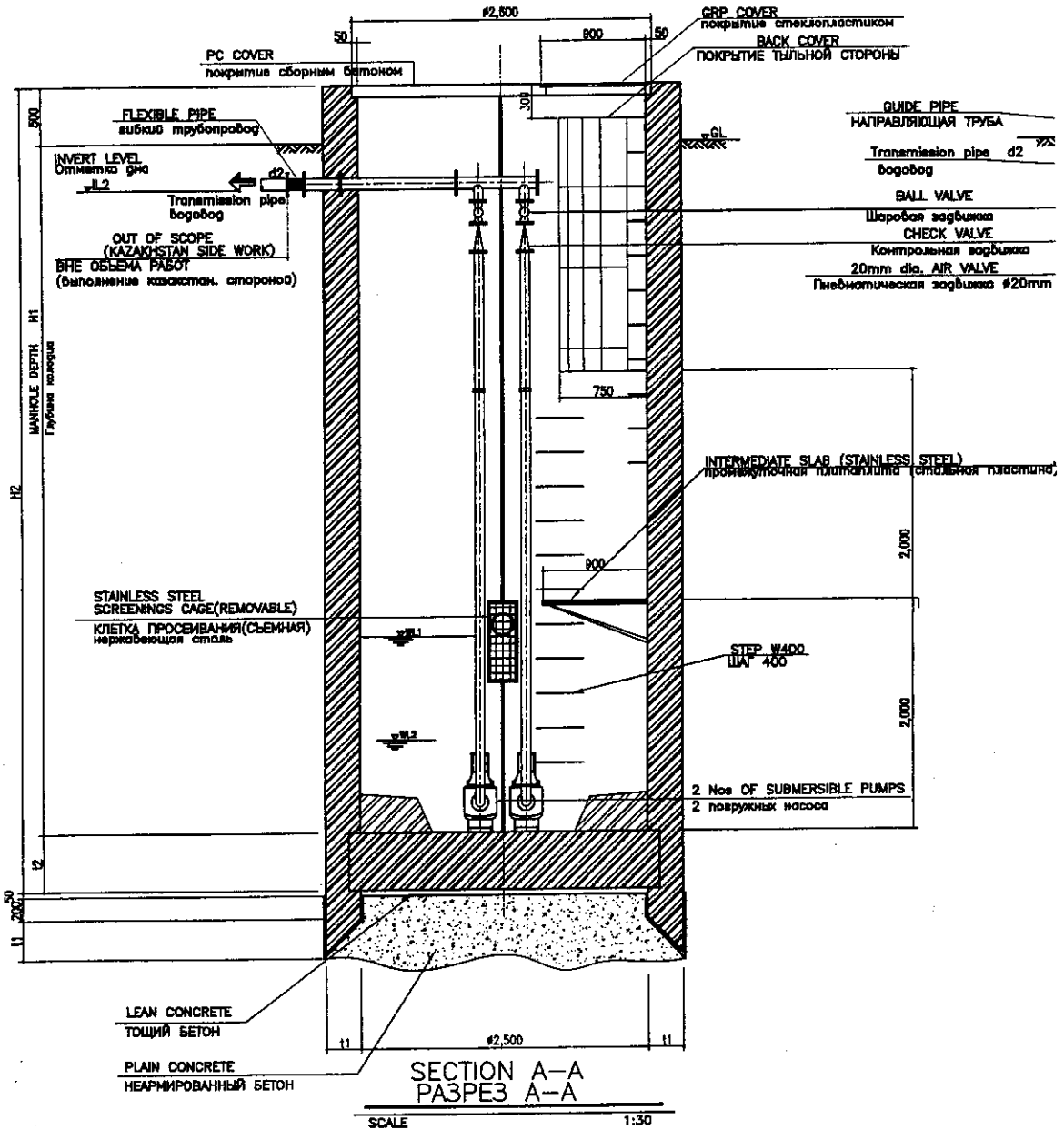
Symbol Символ	Item Наименование	PS No. 28 КНС-28	PS No. 34 КНС-34	PS No. 37 КНС-37	PS No. IH КНС-IH
GL	Ground Level Отметка земли	+380.35m	+345.30m	+348.70m	+356.78m
d1	Inflow Pipe Diameter Диаметр трубы на входе	#150CIP	#300CIP	#200CIP	#300CIP
IL1	Inflow Pipe Invert Level Отметка дна трубы на входе	+355.50m	+342.50m	+343.80m	+351.80m
d2	Transmission Pipe Diameter Диаметр водовода	#150SP	#300SP	#100SP	#100SP
IL2	Transmission Pipe Invert Level Отметка дна водовода	+357.70m	+342.50m	+344.80m	+353.80m
WL1	Pump Start Level Уровень включения насоса	+355.50m	+342.50m	+343.80m	+351.80m
WL2	Pump Stop Level Уровень останова насоса	+354.60m	+341.70m	+342.80m	+350.78m
BL	Manhole Bottom Level Отметка дна колодезя	+353.35m	+340.80m	+341.90m	+348.88m
H1	Manhole Depth Глубина колодезя	7.000	4.500	4.800	6.900
t1	Manhole Wall Thickness Толщина стен колодезя	400	300	300	400
t2	Manhole Wall Thickness Толщина стен колодезя	500	500	500	500
	Pump TAG No. НОМЕР НАСОСА	S64 IP 01/02	S65 IP 01/02	S66 IP 01/02	S67 IP 01/02
Qp	DISCHARGE CAPACITY производительность	1.3m <sup>3</sup> /min	0.84m <sup>3</sup> /min	0.84m <sup>3</sup> /min	0.84m <sup>3</sup> /min
H3	TOTAL HEAD общий напор	28.0m	4.0m	30.0m	15.0m
N	PUMP QUANTITY КОЛ-ВО НАСОСОВ	2 UNITS (1 STANDBY)	2 UNITS (1 STANDBY)	2 UNITS (1 STANDBY)	2 UNITS (1 STANDBY)
K	MOTOR OUTPUT мощность двигателя	22kW	3.7kW	18.5kW	7.5kW

Remarks:  
Примечание

PS No. 28: "Автоматика" Industrial Workshop  
КНС-28: Комбинат "Автоматика"  
PS No. 34: PDU Settlement - Astrakhanaky Settlement  
КНС-34: Поселок ПДУ, Астраханская трасса  
PS No. 37: Kotovsky St.  
КНС-37: Ул. Котовского  
PS No. IH: Isolation Hospital  
КНС-IH: Больничный комплекс



MHP structure (2/2)



10. Pile foundation calculation

Table 10.1 Pile numbers examination by static formulae of Terzaghi

note: Penetration into last strata shall be larger than 2\*size, that is 1m

Facility	Pile length (m)	Support strata	embedded length (m)	estimated mean N	pile cross-sectional area			Pile perimeter			strata for the frictional resistance		length in the strata (m)	frictional resistance C (t/m2)	safe load on the pile in kN			structure area (m <sup>2</sup> )	structure load (kN)	pile spec			judgement
					300	400	500	300	400	500	①	②			Size of pile(mm)					300	400	500	
					m2	m2	m2	m	m	m					Size of pile(mm)								
															300	400	500						
Grit Chamber	2.5	1st sandy silt	1	3	0.1	0.2	0.3	1.2	1.6	2	① 1st	2.5	3	55	86	122	220	11,612	nums.	212	136	96	unable to support
											②	0	0						area	1.04	1.62	2.29	
											③	0	0						ctr dist	1.01	1.27	1.51	
	3.5	2nd silty sandy	1	3	0.1	0.2	0.3	1.2	1.6	2	① 1st	2.5	3	61	94	132	220	11,612	nums.	191	124	88	unable to support
											② 2nd	1	1.5						area	1.15	1.77	2.50	
											③	0	0						ctr dist	1.07	1.33	1.58	
	7	4th coarse sand	2	26	0.1	0.2	0.3	1.2	1.6	2	① 1st	3	3	283	479	726	220	11,612	nums.	42	25	16	300 adopted
											② 2nd	3	1.5						area	5.23	8.79	13.73	
											③ 4th	1	0.2						ctr dist	2.28	2.96	3.70	
Sludge Cake House	4	1st	4	3	0.1	0.2	0.3	1.2	1.6	2	① 1st	4	3	73	109	151	344	24,696	nums.	339	227	164	unable to support
											②	0	0						area	1.01	1.52	2.10	
											③	0	0						ctr dist	1.00	1.23	1.44	
	7.5	4th	3	26	0.1	0.2	0.3	1.2	1.6	2	① 1st	4.5	3	283	479	727	344	24,696	nums.	88	52	34	300 adopted
											② 4th	3	0.1						area	3.91	6.62	10.12	
											③	0	0						ctr dist	1.97	2.57	3.18	
	11.5	6th clay silt	3	9	0.1	0.2	0.3	1.2	1.6	2	① 1st	4.5	3	161	250	357	344	24,696	nums.	154	99	70	not economical
											② 4th	6	0.1						area	2.23	3.47	4.91	
											③ 6th	1	6.9						ctr dist	1.49	1.86	2.21	
Primary Sedimentation Tank	4	2nd	1.5	3	0.1	0.2	0.3	1.2	1.6	2	① 1st	2.5	3	64	98	137	716	36,378	nums.	569	372	266	unable to support/arrange
											② 2nd	1.5	1.5						area	1.26	1.93	2.69	
											③	0	0						ctr dist	1.12	1.38	1.64	
	6	4th	3	26	0.1	0.2	0.3	1.2	1.6	2	① 1st	2.5	3	273	467	711	716	36,378	nums.	134	78	52	300 adopted
											② 2nd	2.5	1.5						area	5.35	9.18	13.78	
											③ 4th	1	0.1						ctr dist	2.31	3.03	3.71	
Secondary Sedimentation Tank	2	1st	-	3	0.1	0.2	0.3	1.2	1.6	2	① 1st	2	3	49	78	112	716	39,906	nums.	815	512	357	unable to support/arrange
											②	0	0						area	0.88	1.40	2.01	
											③	0	0						ctr dist	0.93	1.18	1.41	
	3.5	4th	1	26	0.1	0.2	0.3	1.2	1.6	2	① 1st	2.5	3	259	447	686	716	39,906	nums.	155	90	59	300 adopted
											② 4th	1	0.1						area	4.62	7.96	12.14	
											③	0	0						ctr dist	2.14	2.82	3.48	
Return Sludge Pump House	4	1st	-	3	0.1	0.2	0.3	1.2	1.6	2	① 1st	4	3	73	109	151	429	30,689	nums.	421	282	204	not adopted unable to support/arrange
											②	0	0						area	1.02	1.52	2.10	
											③	0	0						ctr dist	1.00	1.23	1.45	
	6	4th	3	26	0.1	0.2	0.3	1.2	1.6	2	① 1st	5	3	288	486	735	429	30,689	nums.	107	64	42	300 adopted
											② 4th	1	0.1						area	4.01	6.70	10.21	
											③	0	0						ctr dist	2.00	2.58	3.19	

B - 11.75