Inspection Memo 3 Inspection of Hopin Small Hydropower Station in Hopin, Kachin

26.11.2002

3.1 Township Information

• Hopin, Kachin State

3.2 General Information of Hopin Power Station

• Access





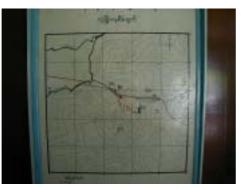
River crossing toward Hopin Station





11 kV Distribution Line crossing the river

• General layout





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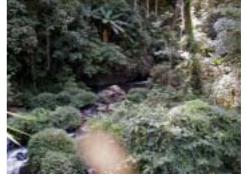
The Study on Introduction of Renewable Energies in Rural Areas in MYANMAR

• Intake



Looking intake weir from downstream





Water flowing into headtank

• Headrace



Steps on Siphon Pipes



Siphone







Outlet of Siphon



Side-overflow of headrace channel



Headrace channel





Trace of small slide upside the channel

Downside slope much eroded by water

• Headtank with regulating pond and desander





Excess water spillway





Inlet gate



A distant view of approach road and river

• Penstock







Hopin Power Station & penstock



A distant view of penstock

• Powerhouse





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• Tailrace



• Distribution lines



3.3 Particular Information of Hopin Power Station

- Unit 1 in automatic operation at guidevane opening of 63%
- Unit 2 in manual operation
- 55 Hz, 0.125 MW

Salient Features:

Name	: Hopin Ga Lang Chaung Hydropower Station	
Location	: 8 miles northeast of Hopin Township, Kachin State	
River Name	: Ga Lang Chaung	
Catchment area	: 9.0 sq.mile (23.3 km ²)	
Head	: Net head of 625 ft (190.5 m)	
Discharge	: 15 cusec x 2 units = 30 cusec (0.425 x 2 = $0.85 \text{ m}^3/\text{s}$)	
Output	: $630 \text{ kW x } 2 \text{ units} = 1,260 \text{ kW}$	
Weir	: 30 ft (L) x H 7 ft (9.1 m L x 2.1 m H)	
Siphon	: 550 ft (L) x \phi2 ft (167.6 m L x \phi0.61 m)	
Power Canal	: 2,300 ft (L) x 3 ft (B) x 2.5 ft (D) (701 m L x 0.91 m B x	
	0.76 m D)	
Head Tank	: 2,425 ft (L) x 50 ft (B) x 6.5 ft (D) (739 m L x 15.24 m B x	
	1.98 m D)	

Penstock Turbine Annual Energy	 108,000 cu ft (3,058 m³) 1,900 ft (L) x φ2 ft (579 m L x φ0.61 m) Pelton with 1 nozzle, made in Kunmin China 2.3 GWh 			
Distribution line	: 11kV line, 14km between Station and Hopin + 32km in Hopin,			
Nammar, and Moe Nyin = 46km in total				
Construction	: Feb 1990 – Sep 1991 Commissioning : 07-Sep-1991			
Project cost	: Public contribution 20.4 x 10^{6} Kyat MEPE LC 6.8 x 10^{6} Kyat FC 0.19 x 10^{6} US\$ (1.2 x 10^{6} Kyat) 28.4 x 10^{6} Kyat in total			
Supply Area	: Hopin, Monyin, and Namma			
Peak Load	: 1,300 kW. Load shedding is made at the peak time from 6 p.m. to 10 p.m.			
Consumer	: 3,147 in total (1,246 in Hopin, 1,223 in Monyin, and 678 in Namma)			
Operation	: 300 kW (1 unit) from March to May			
	: 1,100 kW (2 units) from Jun to Jan			
	: 900 kW (2 units) in Feb			

3.4 Issues

(1) Civil Structures

- It appears that the head tank has not been utilized for peak power generation. A water level gauge in the head tank needs to be installed for peak operation.
- 168 m long siphon consists of the waterway to cross the deep waterfall of Ga Lang Chaung. However, it appears that the debris and/or driftwoods have not been so significant to fill the inside of siphon or attack during floods, seeing from the sedimentation around the weir site.
- 100% of the river flow was taken at the Intake Weir, and led to the Head Tank on 26-Nov-2002. Some of the flow spilled out from the spillway of the Head Tank. The power output was 300 kW (unit-1) and 100 kW (unit-2) at that time.

Turbine discharge 400 / 1,260 x 0.85 $m^3/s = 0.27 m^3/s$ approx.

River discharge might be $0.4 \sim 0.5 \text{ m}^3/\text{s}$

• The state of flow from the siphon to the canal is of super-critical flow, and changes to sub-critical state.

Assuming slope=1/500, n=0.014 and b=0.90 m, uniform flow depths are as follows:

For $Q = 0.50 \text{ m}^3/\text{s}$ h = 0.49 m

For $Q = 0.85 \text{ m}^3/\text{s}$ (max. design discharge) h = 0.74 m (canal height 0.76 m)

- It was observed at the open canal that slope sliding above the waterway entered the canal once and dammed off the flow, of which overflow induced the slope failure below the canal.
- It appears that the Head Tank was designed to supply the maximum design discharge for just 1.0 hour only (0.85 m³/s x 3,600 = 3,060 m³)
- The water leakage was observed at 2 locations of expansion joints of Penstock.

3.5 Plates of Equipment

Automatic Speed Governor Type : XT-300 Standard No. GB 9652 No. 91-01 Governor Capacity : 3,000 J Rated Oil Pressure : 2.5 Mpa Date : 1991 Kunming Electrical Machinery Works Co., Ltd	Oil Pressure Unit Type : Hyz-01 Standard No. : GB9652 No.91-02 Rated Oil Pressure : 2.5 Mpa P. Tank Volume : 0.1 m ³
Electromagnetic Generator	Transformer to I.E.C 76
Type : TFY05-10 No.512-018	Type : SFW630-11/1180 No.691-06
Output : 0.5 kW	Capacity: 750 kVA Rated Frequency : 50 Hz
Main Sub	Type of Cooling : Onan
Voltage : 380, 220, 110V 190, 110 V	Rated Volt (No Load) : HV 11,000, LV 400 V
Current : 0.608, 1.09, 2.1 A 0.304, 0.525 A	Rated Current Load : HV 39.36, LV, 1982 A
Connection: , ,2 ,	Insulation Level : HV 75 kV _p LV 25 kV
Rotation : 600/1200 rpm Frequency : 50 Hz	Insulation liquid rise : 50
Raway Speed : 1050 rpm	Winding Resistance Rise : 60
Conn : Y cos : 0.3 Phase : 3	Year of Manufacture : 1981
Kunming Electrical Machinery Works	Connection Symbol : Dynll
	Untaking mass : 1190 kg, Total mass : 2,484 kg
	Transportation mass : 2136 kg

Mass of oil : 520 kg

Maker's serial No. : 65299/10

Oil : 609 L

Hawker Siddeley Brush Transformer Ltd., England

Turbine

 Type : J22-W-92/1x11

 Head : 190 m
 Flow : $0.424 \text{ m}^3/\text{s}$

 Output : 663 kW
 Speed : 600 rpm

 Weight : 6500 kg
 No. S91-007

 Kunming Electrical Wachinery Works Co., Ltd

Special Valve Cabinet

Oper V : 110V Cont P : 2.5 MPa No. 91-01 Date: 1991 Kunming Electrical Machinery Works Co., Ltd

Generator

Type : SFW630-11/1180 No.691-06 Output : 630 kW Sta Volt : 400 V Sta Curr 1137 A Rotation : 1500/1800 rpm Frequency : 50 Hz Raway Speed : 1050 rpm Conn : Y cos : 0.3 Phase : 3 Stator 6, Rotor F Rotation: Nil Date : 1991 03 Kunming Electrical Machinery Works Co., Ltd Inspection Memo 4 Inspection of Zi Chaung Power Station during De-Watering

23 to 29 May 2003



4.2 Lecture on Topographic Survey



Lecture on leveling to MEPE staff

Mapping by Total Station



4.1 Topographic Mapping of Intake Area

Mirror for distance measuring



4.3 Discharge Measurement Along Headrace Channel

4.4 Inspection of Headrace Channel

On 26 May 2003, the power station was shut down for inspection of turbine runner etc. On this occasion, the headrace channel was also dewatered and inspected from the intake down to the regulating pond.

The principal findings are:

- Sediment deposits had significant depth and volume on the channel floor with maximum thickness of about 35 cm.
- Most of the sediments entered the channel through the intake while the trashracks were left washed out while minor volume were from side slopes beside the channel.
- Sediment deposits are significant immediate downstream of the side spillway where water flow is violent and does not allow sediments to settle.
- Further downstream, much sediments are observed on the straight sections while less or almost nil on the curved sections.
- Joints between the floor slab and side walls received significant erosion probably by flowing sands and gravels.



Intake weir site being surveyed



Gravel deposits upstream of the intake



Gravel deposits in front of intake



Piers in front of intake trashracks



Intake trashrack and wreck of deck for operator to remove leaves etc.



Intake gates looked from upstream





Sand flushing gate

Sand flushing gate fully opened





Side overflow spillway section, bow being Blocked with concrete to avoid leakage Intake gates fully closed for inpsection Water leakage is marginal.



Side spillway section after intake gates fully closed.



Sediments deposits in the same section.

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Water remains undrained in the spillway section (left) due to the thick sediments in the downstream section (right) from where water has been mostly drained.



Sediments and test pit on the channel floor Hol

Hole depth so far dug is 32 cm.



Side wall height at 1.70 m.



Water pond seen in the curved section is created by dam up effect of the sediments downstream, looking downstream



Water depth at this curved section was at 35 cm. Sediments observed mostly in straight sections



Sediments are limited in curved section (left) or nil in some section (right)



Erosion of channel floor



Erosion of side wall foot





Channel floor in the leakage section right



Channel bridge over a tributary

Outside foundation of leakage section (it seemed the foundation has been eroded by leakage water.)



Rock from side slopes



Rock fallen in the channel.



Debris once entered into and removed outside beside the channel. These channel sections should be placed with concrete cover.



Debris on the channel cover, proving effectiveness of the cover.



Channel floor at one of the leakage points



Joint between floor slab and side wall



De-sanding basin



Eel found from the waterway for



A hole is made on side wall to divert water

flushing works in the Regulating Pond



Sediments in the upper part of Regulating Pond, mainly consisting of silt



Sloped pond floor towards penstock inlet looking upstream





Looking penstock inlet. Sediments were flushed in mid-May 2003

Sediment top covered with algae



Sediment surface in the Regulating Pond



4.5 Sand Flushing Tests

4.5.1 Testing of Flute Type Flushing Head (stationary, to be fixed to floor)



Flute made for testing purpose



Flute buried in the pond with sand



Water filled to the Pond



Flute under the water after sand flushing, part of horizontal pipe seen in the bottom of depression that was created by flushing sands around



 \overline{PVC} pipe connected to gain a higher head



Flushing by siphon action at a head of 0.8 m





Flushing at a head of 4 m

ditto



Flushing at a head of 5.5 m



Visitors from villages nearby

Witnesses

4.5.2 Testing of Saxophone Type Flushing Head (movable, to be operated from on raft)



Three suction head made for testing



Saxophone Type 2 (with larger slits)

Saxophone Type 3 (with horizontal slits)



Saxophone Type 1 (with smaller slits)



Saxophone Type 3 (with horizontal slits)



Test operation of Saxophone Type 3 (with horizontal slits)



Flushing at a head of 4 m

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Flushing at a head of 4 m Saxophone Type 1 (with smaller slits)



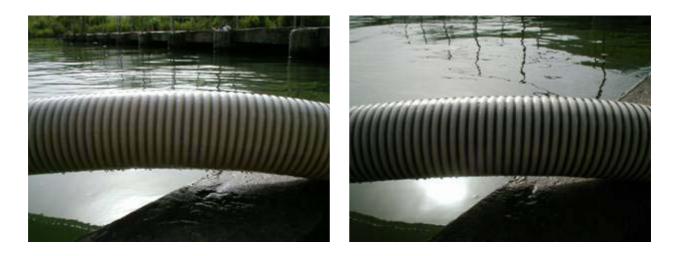
Test operation of Saxophone Type 1 (with smaller slits) from on a raft



Pipe connection to Flushing head and removing air from pipe



under flushing operation with Flushing head being moved



White color of the pipe shows less sacking of sand (left) while black full sacking (right)



Flushing at a head of 4 m



Flushing at a head of 1.8 m



Flushing at a head of 0.8 m