

REPUBLIC OF THE PHILIPPINES  
METROPOLITAN WATERWORKS AND SEWERAGE SYSTEM

STUDY FOR THE GROUNDWATER DEVELOPMENT  
IN  
METRO MANILA

MANUAL REPORT

JUNE 1992

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GROUNDWATER EXPLORATION MANUAL

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# 1. ELECTRIC RESISTIVITY SURVEY

## 1.1 GENERAL

The electric resistivity method is a major geophysical tool used in groundwater exploration efforts. Electric resistivity is undertaken to determine geology and geological structure based on resistivity,  $\sigma$ , the electrical property of geological formations. Each type of formation has an inherent resistivity value in unit cubic volume, and particular values in accordance with geological conditions. Unit of resistivity is  $\Omega - m$ . Electric resistivity may be measured by vertical electric sounding for the distribution of resistivity toward vertical direction, or by horizontal electric sounding for the distribution of resistivity toward horizontal direction. Both methods however, do not have substantial differences.

In measuring electric resistivity, four electrodes are used. These electrodes are arranged along a straight line as shown in Figure 1.1. The outer two electrodes ( $C_1, C_2$ ) are current electrodes and the inner two ( $P_1, P_2$ ) are potential electrodes to measure potential difference. If potential difference between  $P_1$  and  $P_2$  at the time of flow of electricity ( $I$ ) should be  $V$ , resistivity is calculated by the following equation:

$$\sigma_a = 2\pi \times 1/C \times V/I \text{ ----- (1)}$$

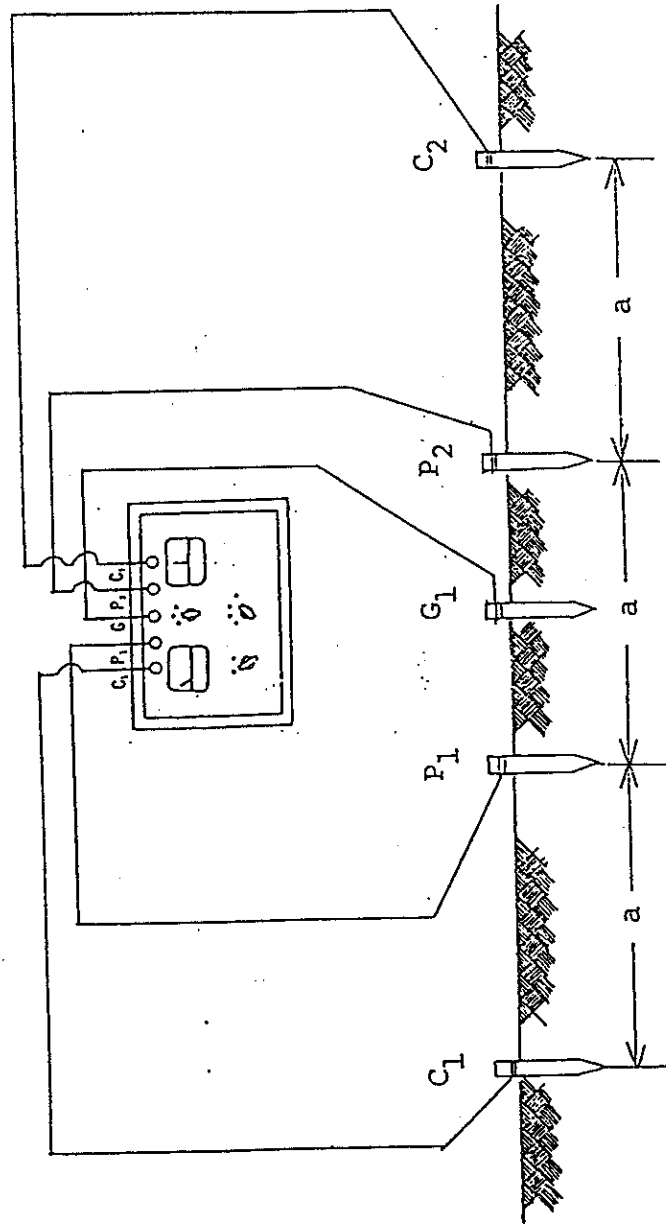
$$C = 1/C_1P_1 - 1/C_2P_1 - 1/C_1P_2 + 1/C_2P_2$$

Electrodes may be set in several ways based on electrode interval. The most common electrode setting is the Wenner's method, putting equal interval between each electrode.

In this condition,  $C_1P_1 = P_1P_2 = C_2P_2 = a$   
thus, equation (1) is converted as follows:

$$\sigma_a = 2\pi a \times V/I \text{ ----- (2)}$$

If geological formations are semi infinite and isotropic,  $\sigma_a$  would indicate the resistivity of the formation, and would become constant



$P_1, P_2$  : Potential Electrodes

$C_1, C_2$  : Current Electrodes

Figure 1.1. MEASURING METHOD OF ELECTRIC RESISTIVITY SURVEY ( WENNER METHOD )

notwithstanding electrode interval and electrode setting.

Actual formations have variable characteristics in vertical and horizontal directions, and are quite different from isotropic condition of geologic formation. As such, measured value  $\sigma_a$  is referred to as apparent resistivity, indicating resistivity in some range in accordance with electrode interval and geological structure.

If electrode interval is large, much electric current flows in deeper portions. As a result, apparent resistivity includes the influence of geological formations. Vertical electric sounding makes use of this phenomenon. In other words, the distribution of resistivity in the vertical direction is measured and estimated by the relation between a series of electrode intervals and apparent resistivity values. On the other hand, horizontal electric sounding estimates the variation of geological formation in horizontal direction based on horizontal distribution of apparent resistivity in a specified electrode interval.

## 1.2 MEASUREMENT

Resistivity is conducted by using the following materials and equipment:

Electric Resistivity Meter : 1 set

Electric Wire : 4 sets

(Length of the wire depends on maximum measuring depth)

(Color of the wire should be different from each other)

Electrode : 5 pieces

(Stainless, Large diameter)

Battery : 1 unit

(Type depends on electric resistivity meter type)

Tester : 1 unit

Measuring Tape : 1 lot

(Length of the tape depends on maximum measuring depth)

Hammer (1.0 - 1.5 kg)	:	6 pieces
Electrical Vinyl Tape (different colors)	:	1 lot
Hostel	:	1 piece
Transceiver	:	4 sets

Before the start of the survey, measuring tape shall be marked by electrical vinyl tape at every measuring point.

Measurement is generally conducted by flowing alternating current ranging from 5 to 40 Hz through the electric wire connecting the measuring equipment and electrodes as shown in Figure 1.1. The setting interval of electrodes in vertical sounding should be symmetrical on both sides, in the right and left sides of center point in horizontal direction. Thus, the direction of measurement is expected to extend along contour lines and in the direction of flow on river terraces or river beds.

After determining the area to be surveyed, lines connecting measuring points shall be checked. This distribution shall be determined considering surveying objective, topography, and geology. The interval of measuring points shall depend on the type of geological formations i.e., it will be longer if geological formations are simple and shorter if formations are complicated.

In vertical sounding, measurement is carried out step by step at a constant electrode interval. Data shall be recorded in a data sheet as shown in Table 1.1.

In order to detect the boundary between some formations and an underlayer, electrode interval(a) shall be expanded up to two or three times as long as the estimated depth of the boundary. On the other hand, horizontal sounding is carried out at constant electrode interval by using jointly two or three kinds of electrode intervals.

Measuring equipment indicates voltage and electric current in each measured point. Apparent resistivity  $\sigma_a$  is calculated by multiplying





$2\pi a$  by  $(R = V/I)$  in Table 1.1. In vertical sounding,  $\sigma - a$  curve is made by plotting  $\sigma_a$  and electrode interval  $a$  on log-log papers (Refer to Figure 1.3). In horizontal sounding, the relation between  $\sigma_a$  and horizontal distance of measuring points on semi-log and section papers shall be plotted.

### 1.3 ANALYSIS

The analysis of data is conducted by assuming that geology below ground surface would be stratified horizontal formations at any measuring point. In Wenner's electrode intervals, the standard curve of Sundberg (refer to Figure 1.2), the theoretical method is generally used. In case measured geological structures will be of two layers, the following analyzing procedures are used as shown in Figure 1.3.

- a. Determination of resistivity value and thickness in first layer: laying  $\sigma_a - a$  curve on top of standard curve, selecting standard curve matched and plotting a standard point (0) (in the condition of  $\sigma_a/\sigma_1 = 1$ ,  $a/d = 1$ ). In this case, 0 point in vertical coordinate on the log-log papers becomes the resistivity of first layer ( $\sigma_1$ ) and the horizontal coordinate indicates layer thickness ( $d$ ).
- b. Determination of resistivity in second layer:

If parameter of a standard curve matched with  $\sigma - a$ , curve shall be  $\sigma_2/\sigma_1 = \infty$ , the resistivity of second layer is calculated by the equation of  $\sigma_2 = \infty \times \sigma_1$ .

In case the geological structures are more than three layers, an auxiliary curve is necessary to replace the case of two layers. Therefore, the above treatment and procedures become complicated.

Draw the matching auxiliary curve starting from standard point (0) on the log-log paper (auxiliary curve I in Figure 1.3).

FIGURE 1.2-A

Sundberg's Standard Curve

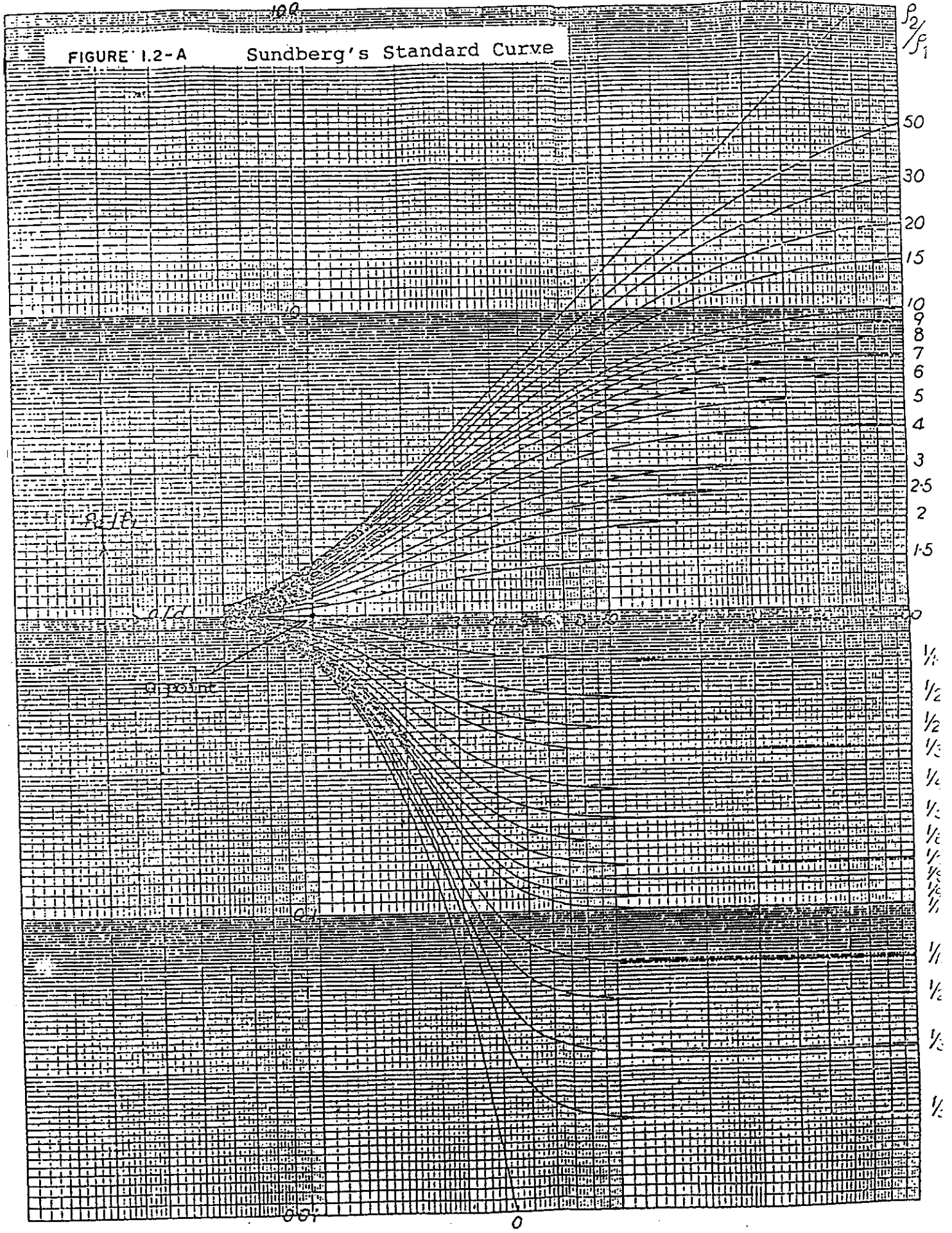
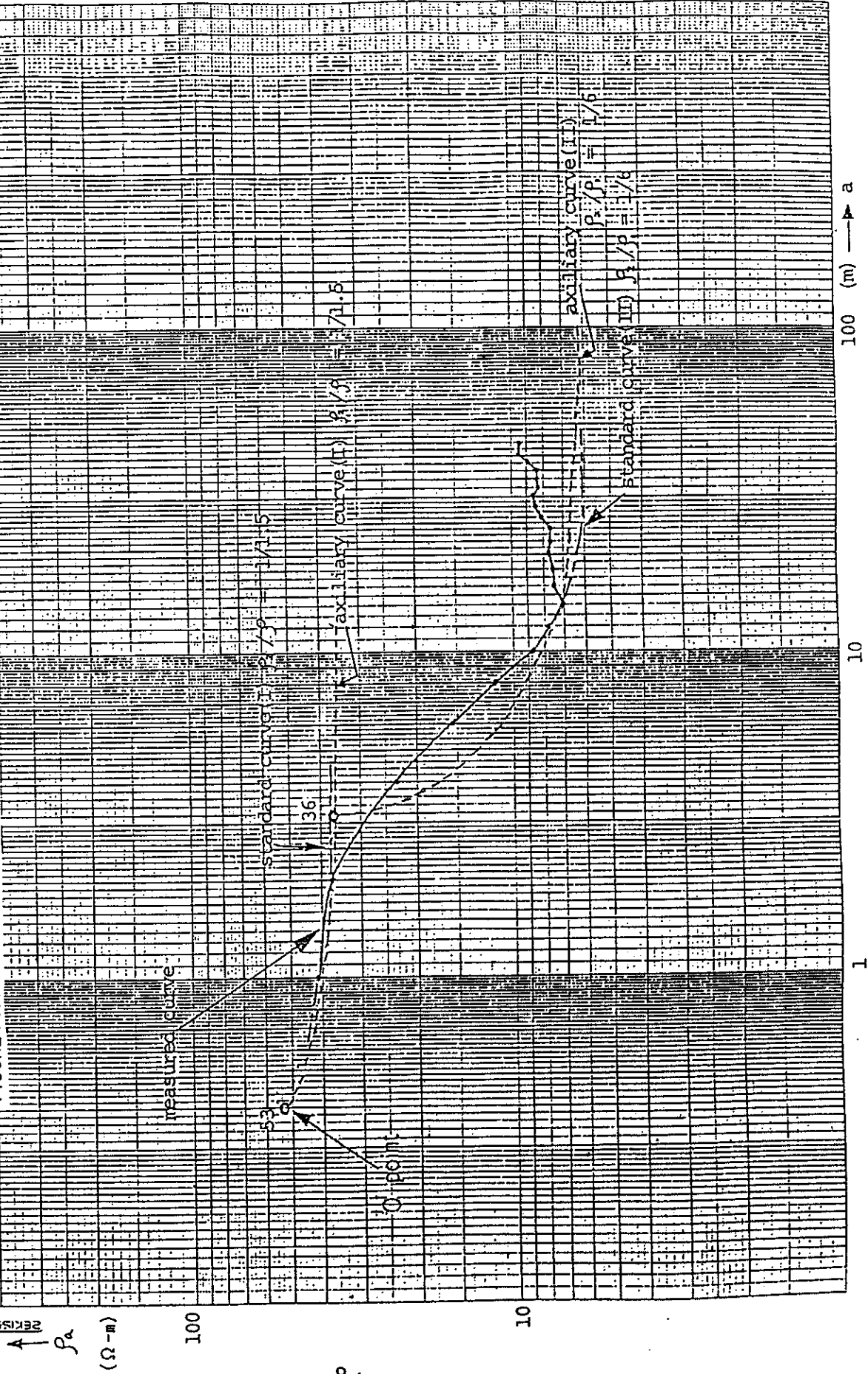




FIGURE 1.3 Analyzing Procedures of Electric Resistivity Survey



#### 1.4 INTERPRETATION

As the resistivity reflects formations, structures, porosity, percentage of clay, groundwater quality and moisture content, specific geological conditions cannot be easily and simply determined based on analyzed results, and the most probable geological condition is selected after considering several possibilities.

Resistivity values in geological formations are shown in Table 1.2 for reference in interpretation. In sand and gravel layer, resistivity is fairly high because groundwater has tendency to flow easily with few dissolved matter. The resistivity of igneous rock is generally high because of the influence of minute structure. Therefore, the identification of igneous rocks as a basement rock is comparatively easy, but for Tertiary formations is difficult.

In the interpretation of measured values, resistivity values are firstly classified into some blocks in each measuring point, and geological condition will be roughly estimated from every resistivity value. In addition, the results need to be examined and interpreted based on the detailed observation of survey area on geology and topography.

Table 1.2 Apparent Resistivity in Geological Structures of Two Layers (after Dobrin)

Geology		Apparent Resistivity ( $\Omega$ -m)
Alluvium	Clay	10 - 100
	Sand	100 - 600
	Sand/Gravel	100 - 1,000
Diluvium	Loam	100 - 250
	Sand/Gravel	300 - 1,000
Neogene	Sandstone	50 - 500
	Shale	20 - 200
	Conglomerate	100 - 500
Volcanics	Tuff	20 - 200
	Lava	500 - 10,000
	Andesite	100 - 2,000
	Granite	1,000 - 10,000

## 2. PHYSICAL LOGGING

### 2.1 ELECTRIC LOGGING

#### 2.1.1 General

Electric logging is undertaken to determine the character and thickness of the various strata at the well site. Electric logging in drilled holes measures the resistivity of the earth materials by recording the potential difference when current flows through the earth from one electrode to another.

The log can only be run in uncased holes filled with water or mud water to provide electrical connection between the logging tool and the formations. Current flow is generated between an electrode down the hole and one at the surface. Electrical potential is measured between these, or another pair of electrodes. Resistivity is measured in ohmmeters, a unit which allows for variations in the size of the flow path. The logging probe which will have one or more exposed electrodes is usually used. The sheave to support the logging cable will have to be rigged in the tripod and held so as to keep the cable in the center of the hole. The surface electrode is connected to any point of good ground contact preferably, the mud pit. The logging system is shown in Figure 2.1.

Electric logging measures resistivity around the drilled hole in a similar manner to electric resistivity survey. Two, three or four electrodes methods based on setting manners of electric current electrodes (A, B) and potential electrodes (M, N) may be used. Electrodes set in a drilled hole are dropped and lifted and are assembled in one probe with other electrodes set on ground surface fixed.

The two-electrodes method is generally used because identification with geological formation is comparatively easy. In the two electrode method, resistivity is calculated from the following equation:

$$\sigma = 4\pi a \times V/I$$

In the equation,  $a$  is equal to electrode interval,  $\sigma$  indicates not true resistivity of geological formation but its apparent resistivity for



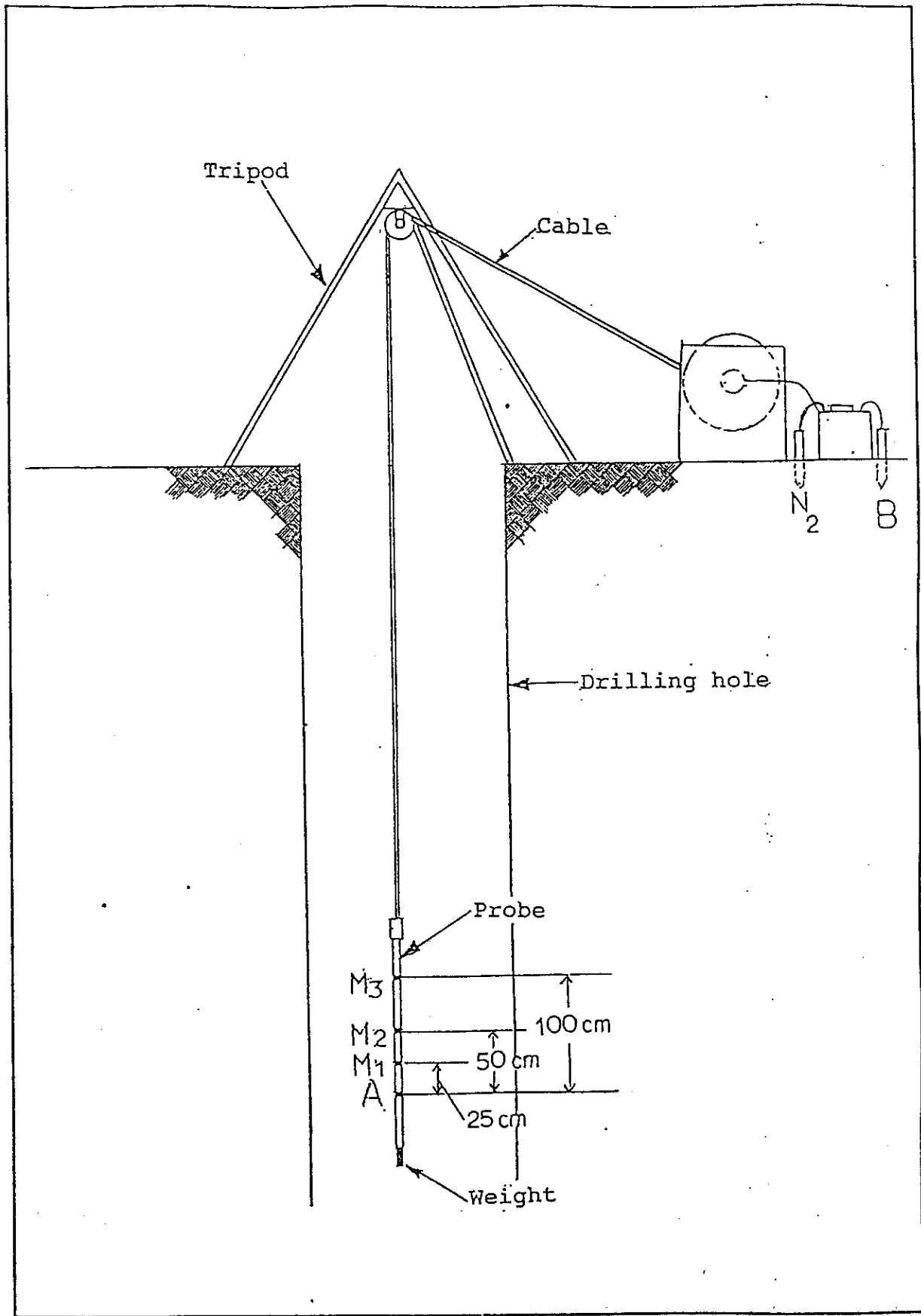


Figure 2.1 ELECTRIC LOGGING ( Normal )

including the influence of thickness of geological formation, the diameter of drilled hole and mud water.

### 2.1.2 Measurement

In electric logging, the following electric logging equipment or electric resistivity survey equipment are used:

Measuring equipment with recorder	:	1 unit
Normal resistivity-SP probe	:	1 unit
(and other probes based on measuring items)		
Weight for probe	:	1 unit
Tripod stand with pulley	:	1 unit
Cable with connector	:	1 set
(Length depends on measuring depth)		
Wrench	:	1 unit

Electrode interval is based on the thickness of geological formation or drilled hole diameter. In case electrode interval is small, detection capability of thinner layers shall increase influenced by mud water inside hole. If the interval is large, the equipment can measure resistivity in deeper portions in horizontal direction in drilled hole wall. Reversely, the thinner layers shall be difficult to detect. Therefore, in many cases, several electrode intervals shall be actually combined.

In combining electrode intervals in two electrodes method, the intervals of AM = 0.25, 0.5, 1.0 m or 0.5, 1.0, 1.5 m are generally used. The setting of electrodes is indicated in Figure 2.1. At measuring time, electrode interval is changed by a switch and is measured in different intervals. Fixed electrodes set on ground surface shall be at a distance from drilled hole. Potential electrode should be up to ten meters from each other and far more than 30 meters from a drilled hole for current electrodes.

After washing the inner side of drilled hole, probe is dropped to the well bottom and measurement is successively carried out with lifting of the equipment. Electric logging data are usually measured at intervals of one or two meters depth. The results of resistivity in a drilled hole with water shall be effective and useful in analysis and interpre-

tation.

### 2.1.3 Interpretation

The result of measurement will be influenced by drilled hole diameter and mud water. Apparent resistivity properly reflects the variation of geological formation, thus, the result of measurement has to be properly analyzed.

General interpretations shall be based on the following:

- a. Low resistivity is usually associated with saturated formations and saline water e.g. shales, clays.
- b. Medium resistivity indicates fresh water sand or porous rocks.
- c. High resistivity is exhibited by dense and impermeable rocks.

## 2.2 SPONTANEOUS POTENTIAL LOG

### 2.2.1 General

Spontaneous potential logs (S.P.) are records of the naturally occurring electrical potential at different depths along the bore hole. In the drilling hole, electrochemical potential is caused by the occurrence of the difference of chloride concentration between water inside drilled hole and groundwater, together with clay layer. In addition, electric flow occurs in case water inside the drilled hole intrudes in its peripheral formations.

Spontaneous potential comprise of electrochemical potential and potential of electric flow, and is affected by geological formation and chloride concentration in drilled hole.

Spontaneous potential is caused by a complex mixture of the different formations and the bore hole fluid. Mud water intrusion in the formation or an increase in bore hole diameter affects the measured values.

### 2.2.2 Measurement

To obtain the data required, it is only necessary to run a single electrode probe made of lead.

In general, spontaneous potential is measured with a pair of electrodes connected to a sensitive voltmeter used also for resistivity logging. An S.P. log is often and simultaneously run with the resistivity logs.

### 2.2.3 Interpretation

Spontaneous potential affects not only absolute values but also relative values. Standard value for the difference of relative values is generally electric potential. Spontaneous potential shall be interpreted with the result of resistivity logging, with both of them complementing the other. A sample of spontaneous potential log data is shown in Figure 2.2.

General conditions in the aquifer are as follows: Good aquifer including fresh water indicates high resistivity values and spontaneous potential moves to positive side. The resistivity values of aquifer with brackish or saline water is lower in comparison to that with fresh water, but is higher than resistivity values of adjacent clay layer and the values shift to negative side.

Considering the above, the evaluation of the occurrence of aquifers, the identification and comparison between the same formations, and alterations of groundwater quality are possible.

## 2.3 Gamma and Other Geophysical Log

A gamma ray log records the natural radiation of the formations. A gamma ray log can record in a dry hole and a cased hole; it will provide a log of an old hole when no other information about the hole is available. The gamma log usually distinguishes between aquifers (sand) and non water producing beds (clay and clayey sand) in unconsolidated formations. Difficulties in getting clear results from a gamma log arise from excessive clays in the mud layers in large diameter holes and high

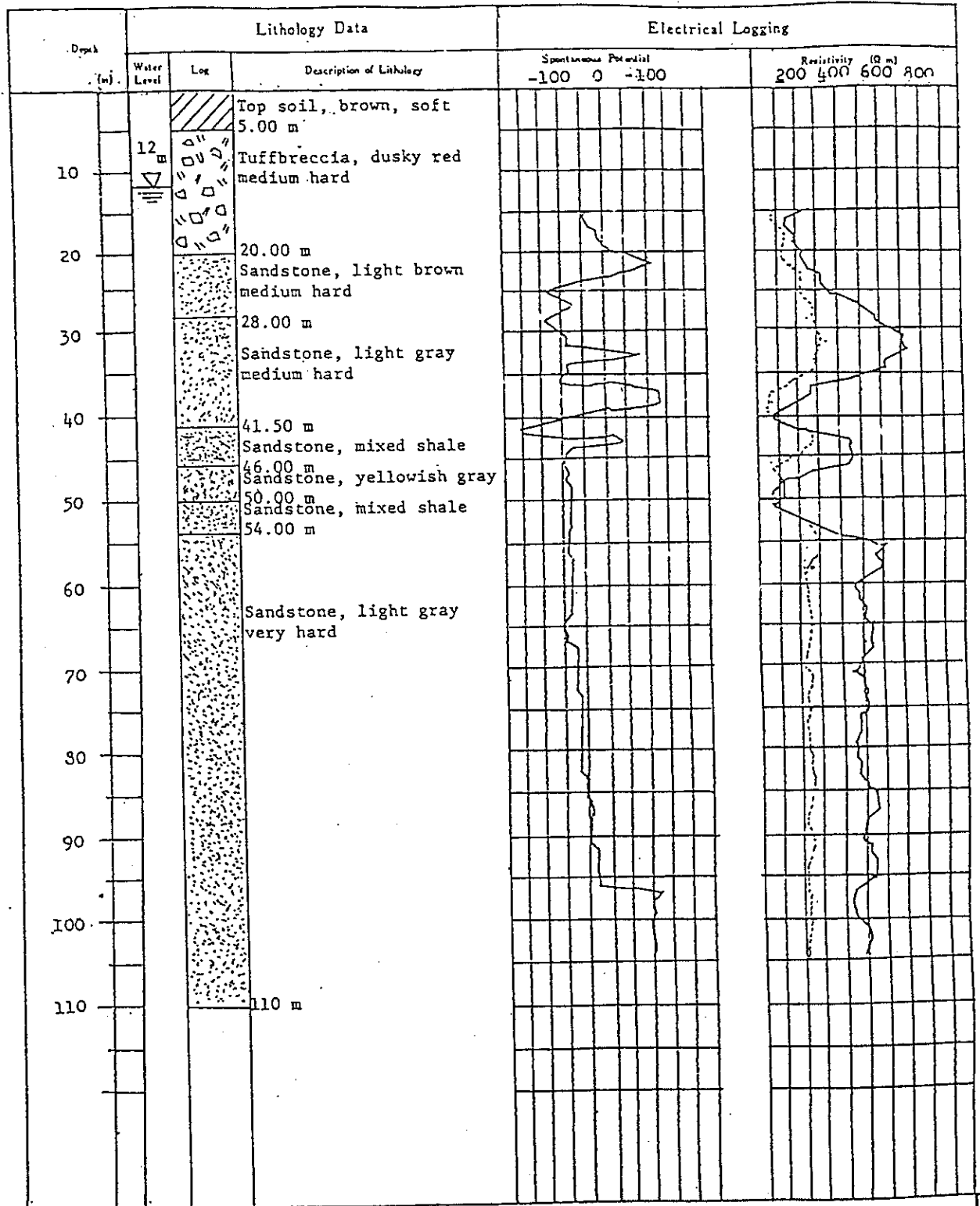


Figure 2.2 SAMPLE OF SPONTANEOUS POTENTIAL LOG DATA

radioactivity in some sand beds due to heavy minerals in the sand.

The gamma radiation from clays is usually much higher than that from sand. When the sand contains radio-active minerals, the relationship is reversed.

#### 2.4 Neutron Log

Neutron logs are used primarily as an indicator of total porosity under saturated conditions.

#### 2.5 Caliper Log

The caliper log measures the diameter of the bore hole. In some cases, it can detect casing couplings and reveal the position of screens in a cased hole. Most caliper tools contact the walls of the hole with three or more curved springs. Flexing of the springs to follow hole size is translated into diameter measurement and recorded as a graph of diameter against depth. Caliper measurement is recorded with the tool moving up the hole.

#### 2.6 Temperature Log

The temperature gradient and irregularities in the gradient measured in the borehole are an important factor in hydrogeological survey. A temperature log will indicate the location of water inflow zones.

### 3. PUMPING TEST

#### 3.1 GENERAL

Pumping test comprise of the step drawdown test, continuous drawdown test and recovery test. In general, pumping test is carried out to determine the safe yield of new wells, hydrogeological aquifer constant of transmissivity, storage coefficient and specific yield.

Step drawdown test involves five to seven steps with two pumping hours duration each step. Drawdown of dynamic water level in each step is continuously measured at specific time intervals. Results of step drawdown test reveal the safe yield, the constant aquifer loss and well loss. Safe yield of the well is necessary in the determination of pump capacity.

Continuous drawdown test, after completion of step drawdown, is carried out to obtain the transmissivity and storage coefficient. The test is generally undertaken by measuring drawdown under conditions of constant discharge for 24 hours pumping duration.

The aquifer constant, transmissivity and permeability and storage coefficient are used to determine the characteristics of the aquifer and to calculate radius of influence of cone of depression and other factors during pumping.

Transmissivity (T) is the multiplier coefficient of thickness of aquifer and permeability and is the product of thickness of saturated portion of aquifer. Storage coefficient (S) is defined as the volume of water released when the piezometric surface is lowered by one unit of its depth.

Recovery test is immediately executed after the continuous drawdown test. The recovery of lowered water level at specified time interval is determined by this test. The test also defines the constant of transmissivity.

### 3.2 Measurement

Pumping test involves preparation work, observation work and data analysis. The procedures and equipment required to carry out the pumping test are as follows:

#### a. Measurement of pumping rate

In the pumping test, the discharge must be measured continuously with the weir and orifice devices. Weirs are triangular or rectangular in shape. Considering discharge measurement, the triangular weir is more useful than the rectangular one. The completed or prefabricated weir is made of iron plates.

##### i) Triangular Weir

The cutting degrees of weir can be divided into two types, 60° and 90° according to the range of the measuring discharge. The weir plate section must be right angled between its inside and upper portions and the edge must be cut sharply. The width of upper portion of weir plate is about 2 mm. The cutting angle of weir plate shall be 60 or 90 degrees of which the bisection line must be located perpendicular to the center of the width of weir water channel as shown in Figure 3.1. Range of measuring discharge is 0.018 to 0.26 m<sup>3</sup> in 60° triangular weir and 0.110 to 1.5 m<sup>3</sup> in 90° triangular weir. Calculating equation for discharge is as follows:

60° triangular weir

$$Q = 0.577 k \times h^{5/2} \text{ ----- (3)}$$

$$K = 83 + 0.00624/B \times R^{3/4}$$

$$R = B \times 0.1 \times h \sqrt{\nu}$$

$\nu$  = kinematic viscosity of pumping  
solution = 10<sup>-6</sup> (m<sup>3</sup>/s)



90° triangular weir

$$Q = K \times h^{5/2} \text{ ----- (4)}$$

$$K = 81.2 + 0.24/h + (8.4 + 12/\phi D) \times (h/B - 0.09)^2$$

Q : discharge, h : water head in weir (m)  
 D : height of weir spill way (m)

The discharge is determined only by the width of weir and water head. Thus, the length of side direction (refer to Y sign in Figure 3.1) of weir box is not related to estimating factor of the discharge. However, the ample length shall be planned to make not a turbulent flow but laminate one in the box. Design plan of typical orifice and weir is also shown in Table 3.1 and Figure 3.1 and Figure 3.2. Discharge is pre-calculated as shown in Table 3.2 Relationship Between Height and Discharge in 90 Degree Triangular Weir.

Table 3.1 Design of Typical Weir

Type of Weir	X	Y	B	D
60° triangular	0.24	1.5	0.8	0.12
90° triangular	0.32	2.2	1.0	0.12

(Note) X, Y, B and D unit : m

ii) Orifice Weir

The orifice is a round hole with clean and square edges in the center of a circular steel plate and is set in the outlet of discharge pipe. A device called a piezometer (manometer) is installed in the discharge pipe. The piezometer consists of a clear plastic tube with 4 or 5 ft (1.2 or 1.5 m) length. The set-up of orifice weir is shown in Figure 3.2. Discharge is calculated as follows:

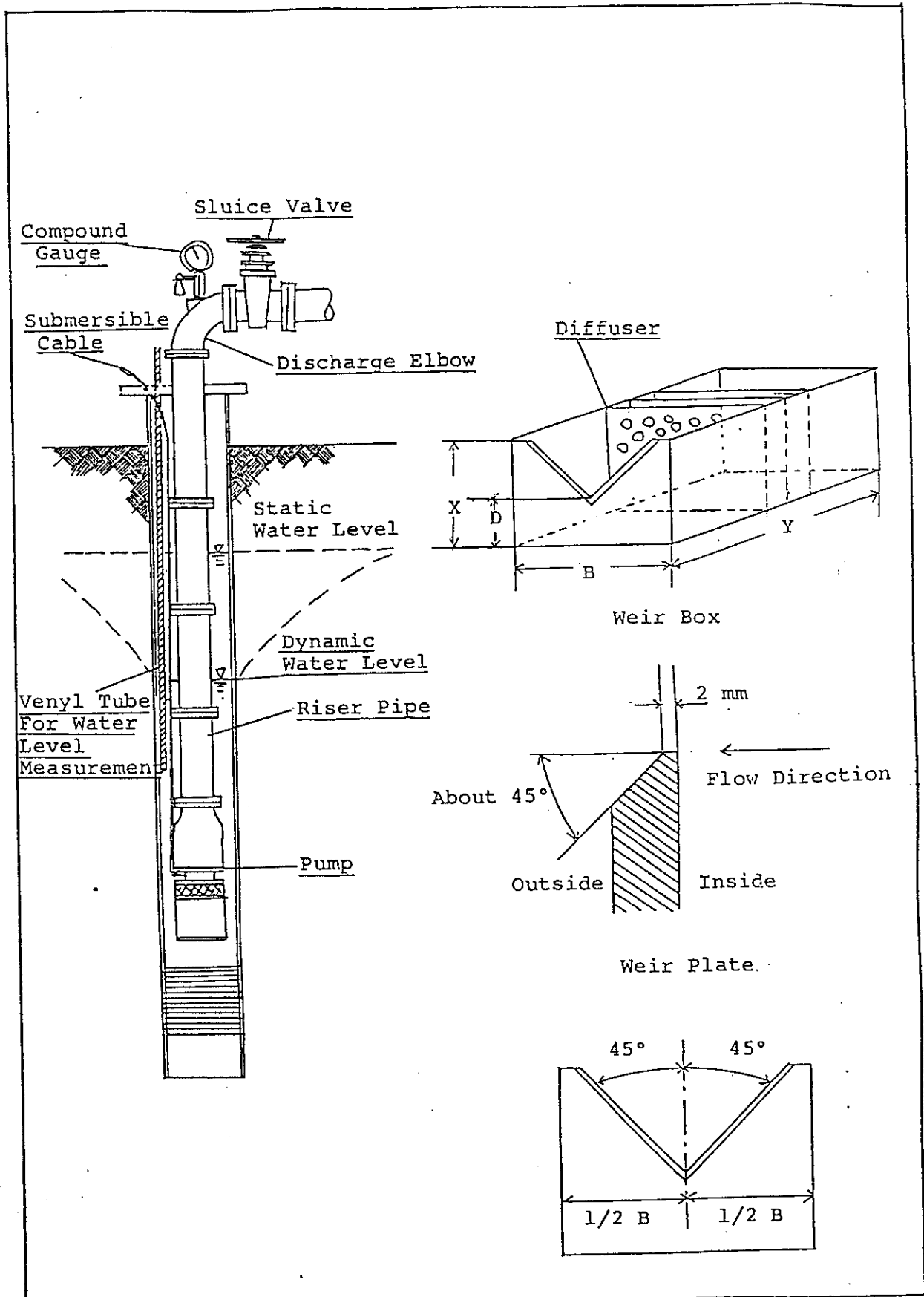


Figure 3.1 OUTLINE OF PUMP SETTING AND STRUCTURE OF TRIANGULAR WEIR

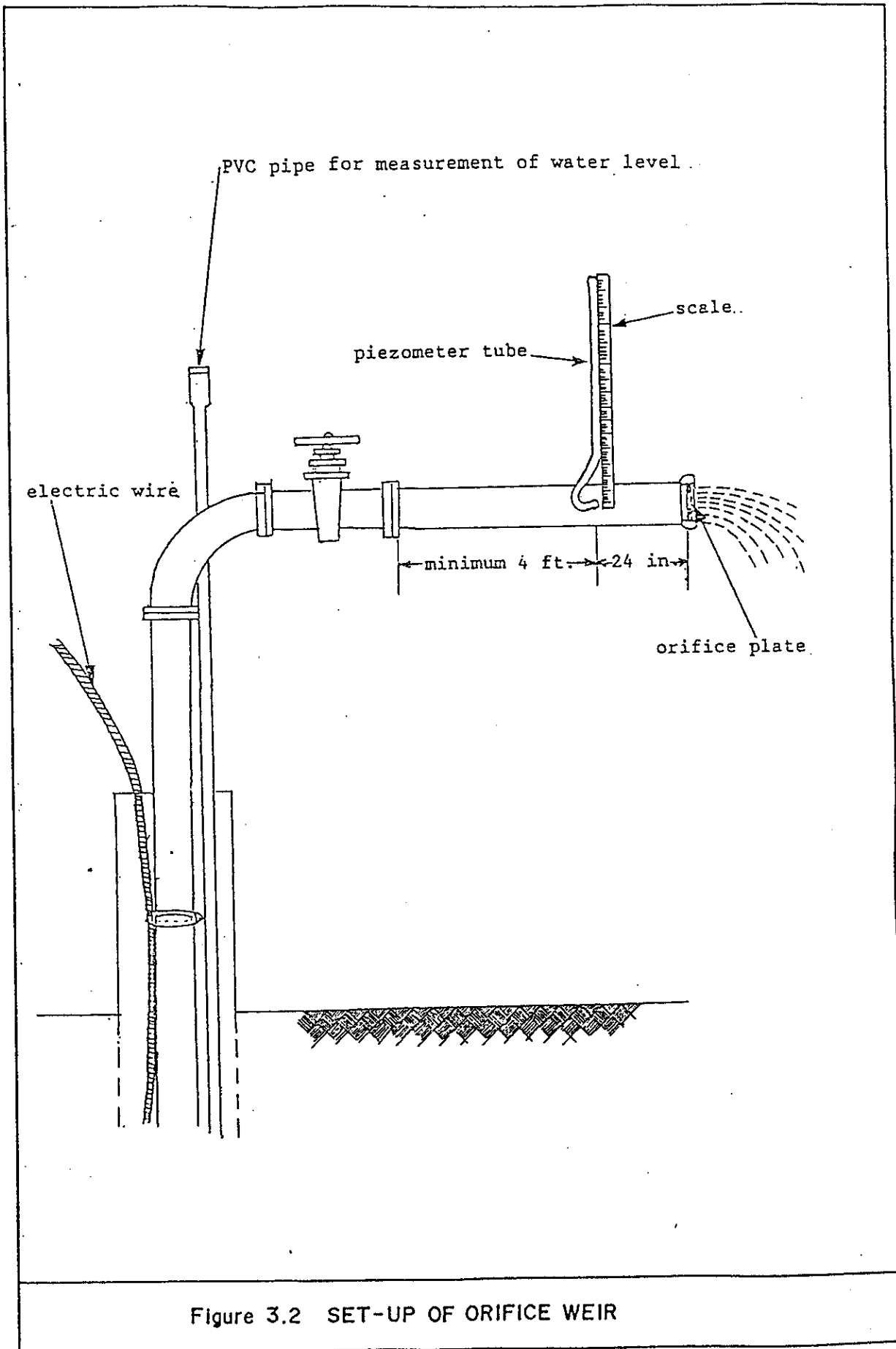


Figure 3.2 SET-UP OF ORIFICE WEIR

**Table 3.2 Relationship Between Height and Discharge  
in 90 Degree Triangular Weir**

**( After S. YAMAMOTO )**

Q = Discharge (l/sec), H = Height of Weir (cm)										
H	0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0	0	0.000045	0.00025	0.00069	0.0014	0.0025	0.0039	0.0057	0.0080	0.0114
1	0.014	0.018	0.022	0.027	0.032	0.039	0.045	0.053	0.061	0.070
2	0.079	0.089	0.1	0.112	0.125	0.138	0.153	0.166	0.184	0.200
3	0.22	0.24	0.26	0.28	0.30	0.32	0.34	0.37	0.39	0.42
4	0.45	0.48	0.51	0.54	0.57	0.60	0.64	0.67	0.71	0.74
5	0.78	0.82	0.86	0.91	0.95	0.99	1.04	1.09	1.13	1.18
6	1.23	1.29	1.34	1.39	1.45	1.51	1.57	1.63	1.69	1.75
7	1.8	1.9	2.0	2.1	2.2	2.3	2.4	2.5	2.6	2.7
8	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4
9	3.4	3.5	3.6	3.7	3.8	3.9	4.0	4.1	4.2	4.3
10	4.4	4.5	4.7	4.8	4.9	5.0	5.1	5.2	5.4	5.5
11	5.6	5.7	5.9	6.0	6.1	6.3	6.4	6.6	6.7	6.8
12	7.0	7.1	7.3	7.4	7.6	7.7	7.9	8.0	8.2	8.4
13	8.5	8.9	8.9	9.0	9.2	9.4	9.5	9.7	9.9	10.1
14	10.3	10.5	10.6	10.8	11.0	11.2	11.4	11.6	11.8	12.0
15	12.2	12.4	12.6	12.8	13.0	13.2	13.5	13.7	13.9	14.1
16	14.3	14.6	14.8	15.0	15.2	15.5	15.7	16.0	16.2	16.4
17	16.7	16.9	17.2	17.4	17.7	17.9	18.2	18.5	18.7	19.0
18	19.2	19.5	19.8	20.1	20.3	20.6	20.9	21.2	21.5	21.7
19	22.0	22.3	22.6	22.9	23.2	23.5	23.8	24.1	24.4	24.7
20	25.0	25.4	25.7	26.0	26.3	26.6	27.0	27.3	27.6	28.0
21	28.3	28.6	29.0	29.3	29.7	30.0	30.4	30.7	31.6	31.4
22	31.8	32.1	32.5	32.9	33.2	33.6	34.0	34.4	34.8	35.1
23	35.5	35.9	36.3	36.7	37.1	37.5	37.9	38.8	38.7	39.1
24	39.5	39.9	40.3	40.8	41.2	41.6	42.0	42.4	42.9	43.3
25	43.8	44.2	44.9	45.1	45.5	46.0	46.4	46.9	47.3	47.8
26	48.3	48.7	49.2	49.7	50.1	50.6	51.1	51.6	52.1	52.5
27	53.0	53.5	54.0	54.5	55.0	55.5	56.0	56.5	57.0	57.6
28	58.1	58.6	59.1	59.6	60.2	60.7	61.3	61.8	62.3	62.9
29	63.4	64.0	64.5	64.1	65.6	66.2	66.7	67.3	67.9	68.4
30	69.0	69.6	70.2	70.6	71.3	71.9	72.5	73.1	73.7	74.3

$$\begin{aligned}
Q &= CAV \text{ ----- (4)} \\
&= CA\sqrt{2gh} \\
&= 8.025CA\sqrt{h}
\end{aligned}$$

Q : pumping rate (gpm)

A : orifice area (square inch)

V : velocity of flow through the orifice

h : water level in the piezometer tube (inches)

C : coefficient of discharge for the orifice as shown in Figure 3.3

Coefficient of Discharge, C. (after Fletcher G. Driscoll, 1987, Groundwater and Wells)

### iii) Other Equipment

submersible pump	1 unit
generator	1 unit
drain hose	4 m
water level indicator	more than 2 sets
dia. 1" PVC pipe	less than 150 m
measuring tape	2 sets
transceiver	2 sets
cutting pliers	1 set
whistle	1 set
electric torch	2 sets
vinyl tape	4 pieces
transit	1 set
stopwatch	1 unit

#### 3.2.1 Preparation Work

The preparation work begins with the selection of source well. Generally, the construction of a new well is carried out as it is difficult to find appropriate observation wells and existing pumping wells which can be utilized and are of no use to the owner. The location of the wells must be selected considering the following:

- o There should be easy access to the site and large working area for well construction

- o The well should not be near canals, rivers, lakes, roads and embankments.
- o There are no existing wells close to the proposed well.
- o Preferably, the boundary of geological formation should be avoided.
- o There is access to electricity.

Observation wells shall be constructed based on the sectional groundwater contour map. The observation wells shall be set in the same aquifer as the existing pumping wells. In addition, screens of observation wells must be located in the aquifer portion corresponding to the center of pumping wells.

Discharge capacity could not be determined beforehand, but it can be estimated based on the pumping rate of existing wells. Drawdown is estimated to be 1 to 4 m in unconfined groundwater and 10 to 30 m in confined groundwater.

Furthermore, data required such as distance from pumping well to observation well, ground level of observation wells and pumping wells and other information shall be derived.

In newly constructed wells, submersible pumps shall be set at an interval of over several meters below the dynamic water level in maximum pumping rate and above the screen. If dynamic water level is below the pump setting near the screen, the pump impeller will be damaged by sand flowing through the screen slots at high velocity inflow of groundwater.

a. Measurement of static water level

Before the start of pumping tests particularly for new wells, static water level shall be measured at specific times.

b. Preliminary pumping test

Prior to the actual pumping test, a preliminary test shall be

carried out. The relation between drawdown and pumping rate shall be checked to determine pumping rate and the approximate length of water level sounding tube. In addition, the appropriate size of notch box is determined. The measuring depth of dynamic water level will be within 150 meters because of possible problems in the wire of water level measurement instrument. Pumping duration in preliminary test shall be approximately 30 minutes. Water level will be measured every ten minutes.

### 3.2.2 Pumping Test and Analysis

Pumping test data shall be taken at intervals as shown in sample pumping test records shown in Table 3.2. Measurement interval of water level during pumping tests shall be fairly short, i.e., every minute within the first 10 minutes from starting time. The interval shall be longer after 10 minutes as shown in the following:

starting time	interval
o from after 10 minutes to after 20 minutes	every 2 minutes
o from after 20 minutes to after 60 minutes	every 5 minutes
o from after 1 hour to after 2 hours	every 10 minutes
o from after 2 hours to after 3 hours	every 15 minutes
o from after 3 hours to after 6 hours	every 30 minutes
o from after 6 hours to after more than 10 hours	1 hour

This time interval shall be used for the step drawdown test, aquifer test and recovery test.





TABLE 3.3 (B) PUMPING TEST RECORD

PUMPING TEST  
(Continuous Drawdown Test)

WELL LOCATION : \_\_\_\_\_

SITE ELEVATION : \_\_\_\_\_

PUMPING EQUIPMENT : \_\_\_\_\_

WELL DEPTH : \_\_\_\_\_

EQUIPMENT CAPACITY : \_\_\_\_\_

CASING DIAMETER: \_\_\_\_\_

RISER PIPE: DIA. \_\_\_\_\_ L: \_\_\_\_\_

SWL : \_\_\_\_\_ PWL : \_\_\_\_\_

DATE CONDUCTED : \_\_\_\_\_

DATE COMPLETED : \_\_\_\_\_

TIME		INTERVAL		WATER LEVEL m (mbgl)	DRAWDOWN (m)	V-NOTCH 90 deg.	DISCHARGE (l/sec)	REMARKS
HOUR	M.	HOUR	M.					
	0		0					
	1		1					
	2		1					
	3		1					
	4		1					
	5		1					
	6		1					
	7		1					
	8		1					
	9		1					
	10		1					
	12		2					
	14		2					
	16		2					
	18		2					
	20		2					
	25		5					
	30		5					
	35		5					
	40		5					
	45		5					
	50		5					
	55		5					
1	00		5					
1	10		10					
1	20		10					
1	30		10					
1	40		10					
1	50		10					
2	00		10					
2	15		15					
2	30		15					
2	45		15					
3	00		15					
3	30		30					
4	00		30					
4	30		30					
5	00		30					

TABLE 3.3 (B) PUMPING TEST RECORD

TIME		INTERVAL		WATER LEVEL m (mbgl)	DRAWDOWN (m)	V-NOTCH 90 deg.	DISCHARGE (l/sec)	REMARKS
HOUR	M.	HOUR	M.					
6	00	1	00					
7	00	1	00					
8	00	1	00					
9	00	1	00					
10	00	1	00					
11	00	1	00					
12	00	1	00					
13	00	1	00					
14	00	1	00					
15	00	1	00					
16	00	1	00					
17	00	1	00					
18	00	1	00					
19	00	1	00					
20	00	1	00					
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37	00	1	00					
38	00	1	00					
39	00	1	00					
40	00	1	00					
41	00	1	00					
42	00	1	00					
43	00	1	00					
44	00	1	00					
45	00	1	00					
46	00	1	00					
47	00	1	00					
48	00	1	00					



1) Step Drawdown Test

The step drawdown test involves several steps. When dynamic water level becomes stable in the first step of the pumping test, the next step would be at a larger discharge rate. This generally consists of five or six steps with a duration of 1 to 2 hours each stage.

Analysis

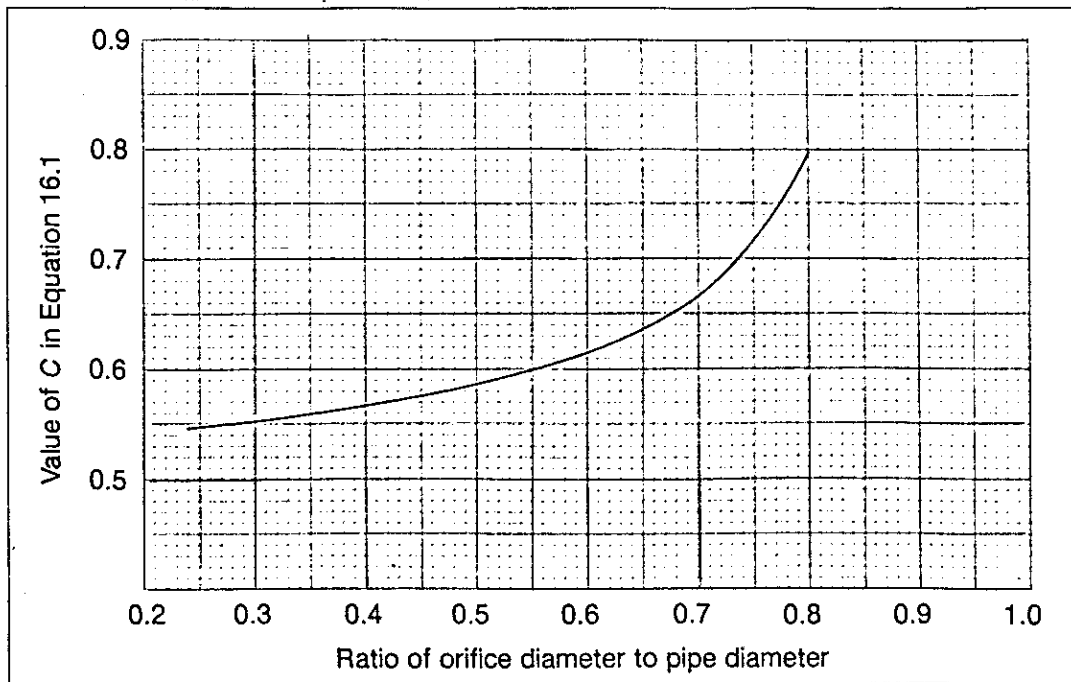
In the results measured by step drawdown test, if drawdown will be plotted in vertical axis and pumping rate will be plotted in horizontal axis, then both would be indicated in relation to a straight line. In case groundwater flow will be a laminate flow during pumping test, the inflow should be matched with Darcy equation and the slope in the straight line would be  $45^\circ$  in laminate flow and more than  $45^\circ$  in turbulent flow. In this case, variation of several degrees from the straight line in the results of step drawdown test indicates critical pumping rate. An actual analyzed sample is shown in Figure 3.3.

2) Continuous Drawdown Test

The continuous drawdown test is carried out by checking drawdown under constant pumping rate condition. Duration of pumping test is more than 24 hours. Pumping rate adopted shall be the rate before the last stage of step drawdown test. This is done to ensure that the pumping rate to be used is within the range capable of water level measurement while the pumping test was carried out at the pumping rate in the last stage of step drawdown test.

Analysis

To calculate aquifer constant from observation data, the equations of equilibrium and nonequilibrium may be used. Of the two equations, the nonequilibrium equation is generally used.



**Figure 3.3** COEFFICIENT OF DISCHARGE, C, IN THE ORIFICE-WEIR VARYING WITH THE RATIO OF ORIFICE DIAMETER TO PIPE DIAMETER (AFTER FLETCHER G. DRISCOLL, 1987, GROUNDWATER AND WELLS )

a) Theis' Nonequilibrium Equation

When constant rate is continuously pumped up through limitless aquifer from well, the influence of pumping, the cone of depression continuously and radially spreads around the well. The cone of depression spreads so as to equal multiplying drawdown speed and the coefficient of storage together, and is compensated with decrease of storage in aquifer. Nothing is at a steady state in this aquifer. Drawdown of water head will continue because of limitless sequence of aquifer. But the rate of drawdown continuously decreases while influence of depression of water level enlarges. In this standpoint, Theis' nonequilibrium equation was induced. When pumping rate in well and drawdown in observation wells (or recovery of drawdown) is known, transmissibility and coefficient of storage is calculated by this equation.

Theis' basic equation is as follows:

$$s = \frac{Q}{4\pi T} \int_{u}^{\infty} \frac{du}{u} \text{ ----- (6)}$$

$$u = \frac{r^2 S}{4 T t} \text{ ----- (7)}$$

s : drawdown, m

Q : pumping rate, M<sup>3</sup>/sec

T : transmissivity, m<sup>2</sup>/sec

(k = T/m, m : aquifer thickness, m)

r : distance from center of pumping well to measuring point

S : coefficient of storage

t : duration time for pumping, sec.

b) Theis' Standard Curve Analyzing Method

Replacing integral of exponent to well function W(u),

$$s = \frac{Q}{4\pi T} W(u) \text{ ----- (8)}$$

$$W(u) = -0.5772 - \ln u + u - \frac{u^2}{2.2} + \frac{u^3}{3.3} - \frac{u^4}{4.4}$$

The Wenzel (1942) analyzing method uses standard curve

plotted  $1/u$  in X axis  $W(u)$  in Y axis in log-log paper as shown in Figure 3.4 This is standard curve. The t-s curve is made by plotting duration time for pumping in X axis and drawdown  $s$  in Y axis from observation data in log-log paper with the same size. The t-s curve is reflected on standard curve, and read  $t$ ,  $s$ ,  $1/u$ ,  $W(u)$  at a point and then transmissibility (T) and coefficient of storage (S) can be calculated:

$$T = Q/4\pi T^*W(u) = 0.0796Q/s * W(u) \text{ ----- (9)}$$

$$S = 4Tt/r^2(1/u) = 4uTt/r^2 \text{ ----- (10)}$$

One analyzed sample is indicated by the pumping test data superimposed on the type curve as shown in Figure 3.5.

In the illustrated pumping test, discharge and radius are as follows:

$$Q = 4,500 \text{ cu.m/day}, \quad r = 15 \text{ m.}$$

On the diagram, match point is  $1/u = 10$ ,  $W(u) = 1.9$ ,  $s = 1.1 \text{ m}$  and  $t = 8 \text{ min}$  (0.0056 day).

Therefore

$$\begin{aligned} T &= 0.0796 Q/s * x W(u) \\ &= 0.0796 \times 4500 / 1.1 \times 1.9 \\ &= 618 \text{ sq.m/day} \end{aligned}$$

$$\begin{aligned} S &= 4uTt/r^2 \\ &= 4 \times 1 \times 618 \times 0.0056 / (10 \times 15^2) \\ &= 6.15 \times 10^{-3} \end{aligned}$$

This method requires much experience and individual difference is fairly large in choice of match point. As T-S curve can also and often be gotten, the following Stallman's manner may also be used.

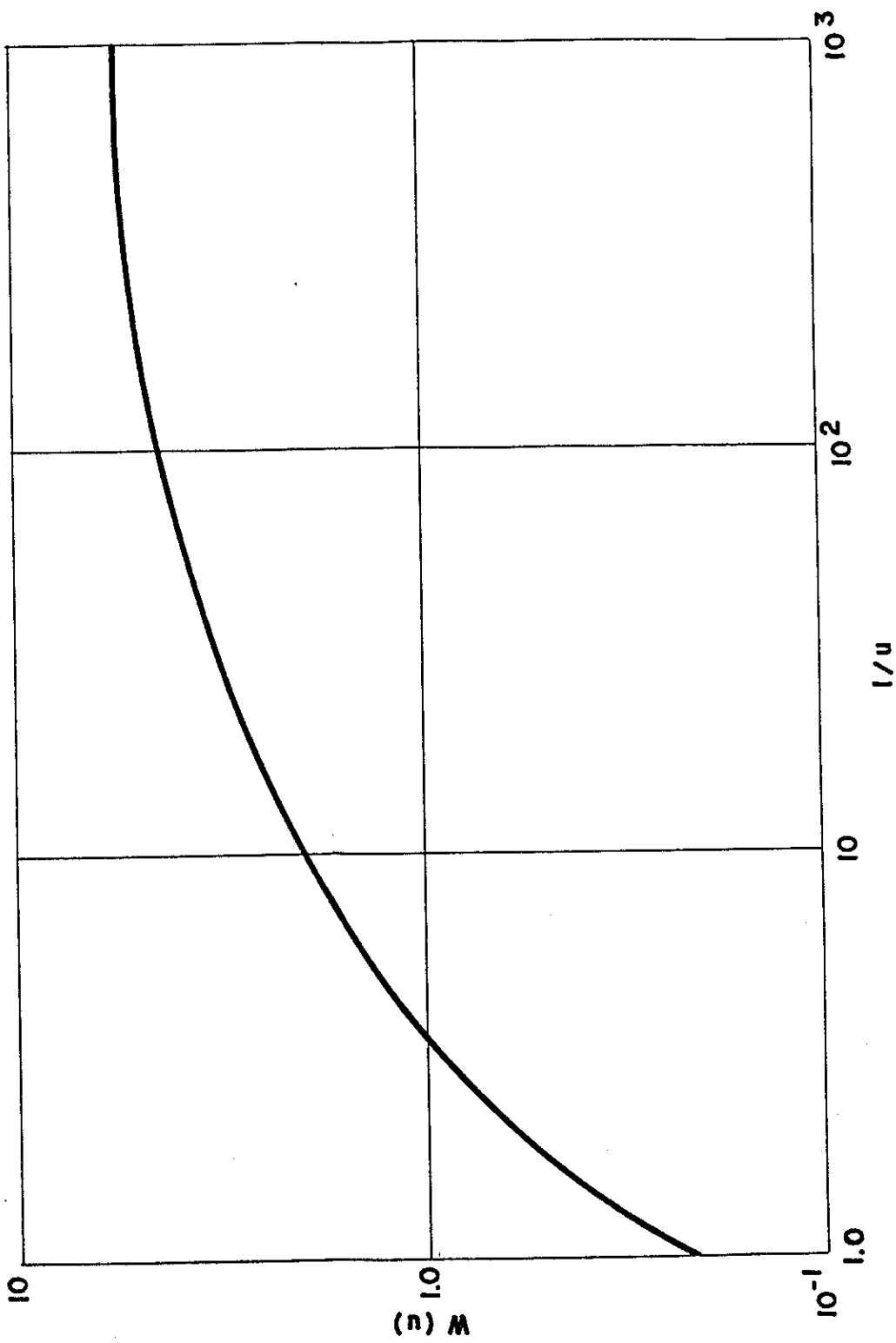
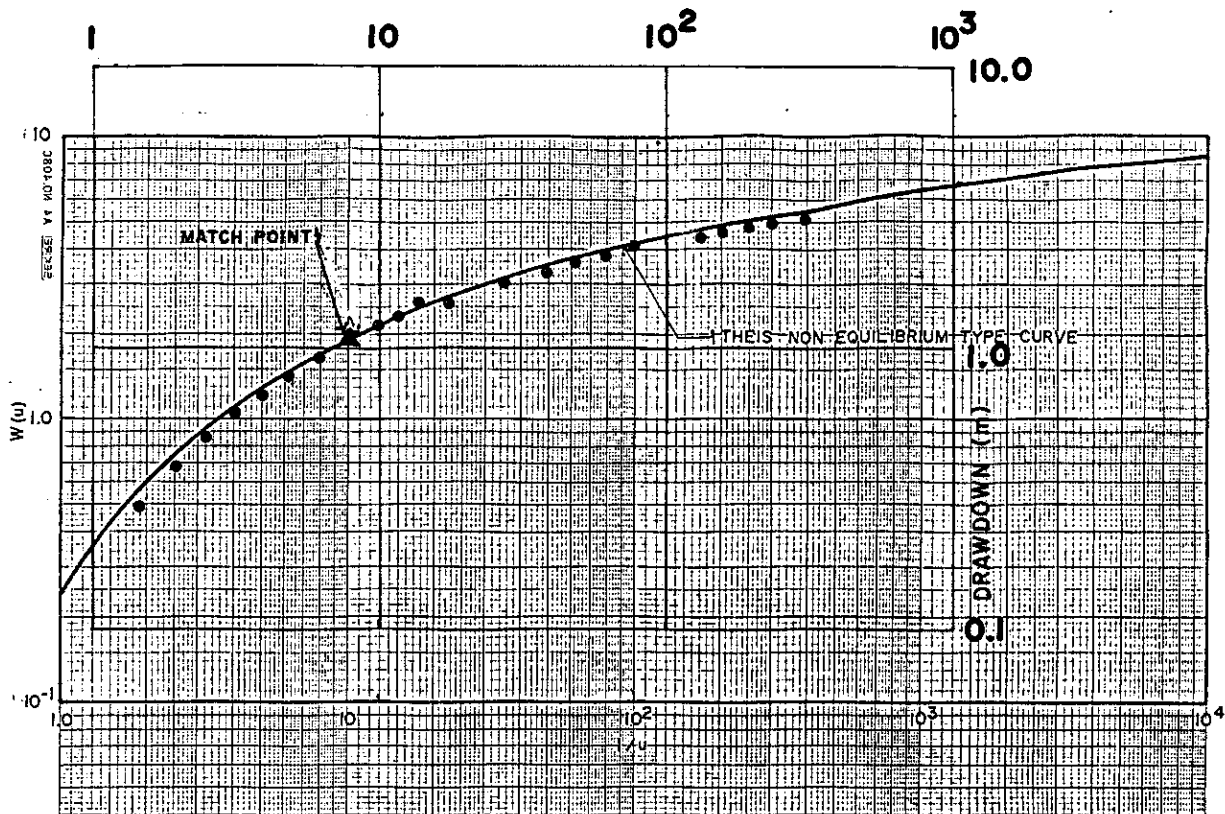


Figure 3.4 THEIS STANDARD CURVE ( NON EQUILIBRIUM TYPE CURVE )



TIME SINCE PUMP STARTED (Min.)



MATCH POINT,  $1/u = 10$ ,  $W(u) = 1.9$   
 $S = 1.1m.$ ,  $t = 8 \text{ min.}$

$$T = 0.0796 \frac{Q}{s} \times W(u)$$

$$= \frac{0.0796 \times 4500}{1.1} \times 1.9$$

$$= 618 \text{ Sq.m. / DAY}$$

$$S = 4uTt/r^2$$

$$= 6.15 \times 10^{-3}$$

Figure 3.5. DIAGRAM OF PLOTTED POINTS REPRESENTING PUMPING TEST DATA SUPERIMPOSED ON THE TYPE CURVE

c) Stallman's Analyzing Method

Stallman's analyzing method is as follows:

When one duplicates two curves and reads  $t_1$  and  $s_1$  in the point of  $W(u) = 1$  and  $1/u = 1$  in standard curve,  $T$  and  $S$  are simply calculated.

$$T = 0.0796Q/s_1 \text{ ----- (11)}$$

$$S = rTt_1/r^2 \text{ ----- (12)}$$

3) Recovery Test

The recovery test immediately measures the recovery from lowered dynamic water level after pumping stops at the instant that continuous drawdown test was performed. Measuring time interval is the same as that of step drawdown and constant discharge tests. Drawdown will be rapidly recovered in first several minutes, thus, measurement should be carried out immediately.

Analysis

The nonequilibrium equation may be used in the recovery of lowered groundwater level. Lowered groundwater level goes up when pumping stops after a certain duration. In this method, recovery discharge is assumed to be equal to the pumping rate.

Based on the nonequilibrium equation the following was derived:

$$T = 2.30Q/4\pi sr * \log (t/t') \text{ ----- (13)}$$

where:

$sr$  : residual recovery drawdown

$t'$  : duration time after pumping stops

In this diagram analyzing method,  $t/t'-sr$  curve on a semi log paper is done by plotting  $t/t'$  in log scale of X axis and  $sr$  in

regular scale of Y axis.

Supposing that residual recovery drawdown in one cycle of  $\log(t/t')$  is  $\Sigma s$ , the equation of  $\log(t/t') = 1$  is formed. Thus, equation (12) is converted as follows:

$$T = 0.183Q/\Sigma s_r \text{ -----(14)}$$

With the relation between  $Q$  and  $s_r$ ,  $T$  is calculated. Figure 3.5 shows an analyzed example based on the pumping test data. In this pumping test, discharge ( $Q$ ) was 691.2 cu.m/day. In the diagram,  $S_r = 0.27$

Therefore,

$$\begin{aligned} T &= 0.183 Q / S_r \\ &= 468.5 \text{ sq.m/day} \end{aligned}$$

RATIO: ( $t/t'$ )

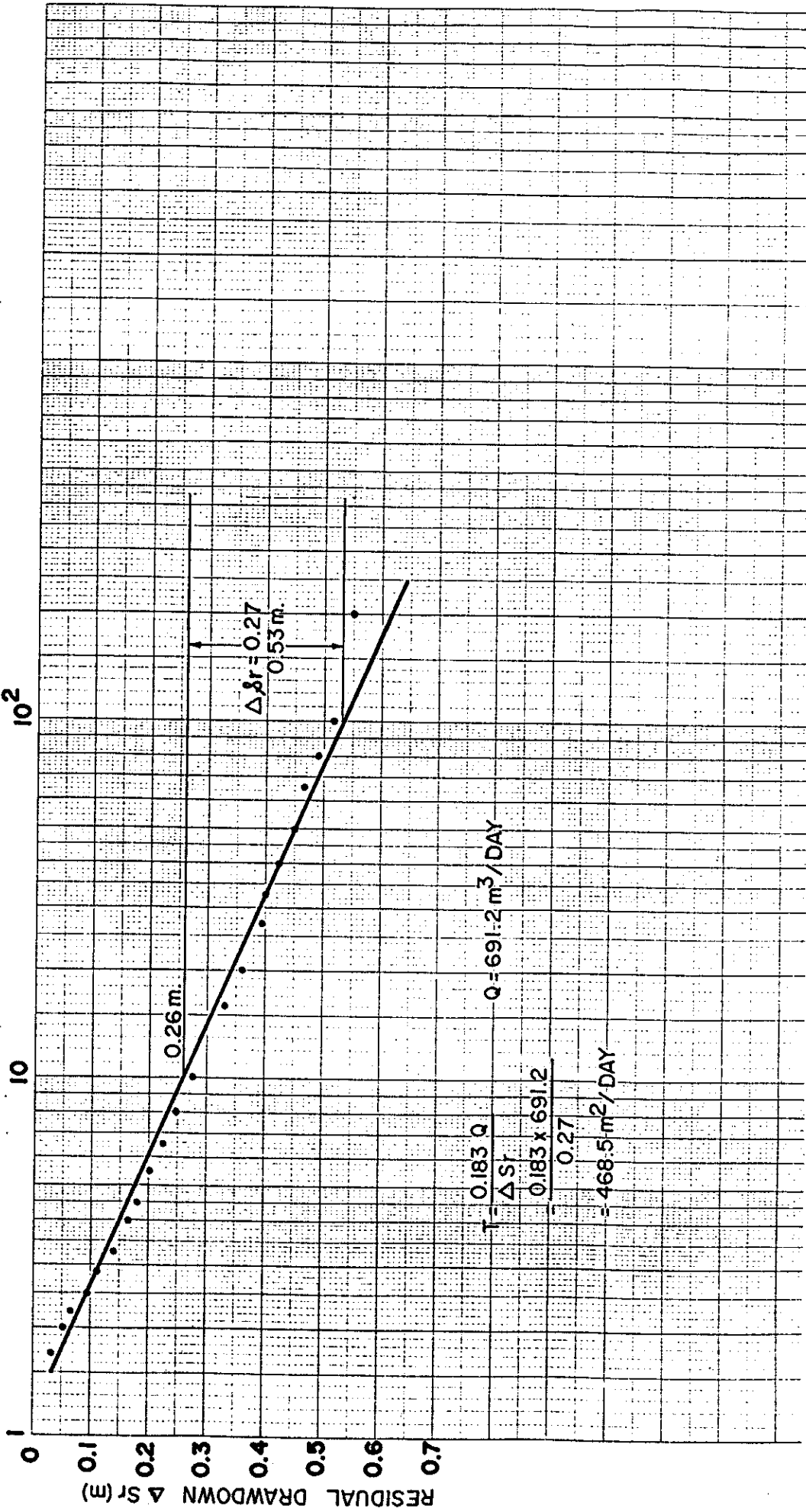


Figure 3.6 RESIDUAL DRAWDOWN PLOTTED AGAINST THE RATIO  $t/t'$  IN RECOVERY TEST

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REPUBLIC OF THE PHILIPPINES  
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# WELL CONSTRUCTION MANUAL

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## 1. WELL CONSTRUCTION

### 1.1 WELL DRILLING METHODS

Well drilling methods are classified into: (1) percussion, (2) rotary and (3) air drilling.

#### 1.1.1 Percussion Drilling Method

The percussion drilling method involves the repeated lifting and dropping of a heavy string of drilling tools into the borehole. The drill bit breaks or crushes consolidated rock into small fragments, whereas the bit primarily loosens the material when drilling in unconsolidated formations. The reciprocating action of the tools mixes the crushed or loosened particles with water to form a slurry or sludge at the bottom of the borehole. If little or no water is present in the penetrated formation, water is added to form a slurry. Slurry is removed at intervals from the borehole by a sand pump or bailer.

This method is appropriate for drilling unconsolidated formations such as alluvium and diluvium including gravel, cobble and boulders. It is not suitable for drilling granite, andesite and arkose sand since it will take a long time to drill and would be very costly. Figure 1.1 presents the percussion type drilling machine and Figure 1.2 the drilling bits, bailer pump and sand pump for percussion drilling.

#### 1.1.2 Rotary Drilling Method

The rotary drilling method was developed to increase drilling speeds and to reach greater depths in most formations. The borehole is drilled by rotating a bit and cuttings are removed by continuous circulation of a drilling fluid as the bit penetrates the formation. The bit is attached to the lower end of a string of drill pipe which transmits the rotation action from the rig to the bit. In the rotary drilling system, drilling fluid is pumped down through the ports or jets in the bit; the fluid then flows upward in the annular space between the hole and the drill pipe carrying the cuttings in suspension to the surface.

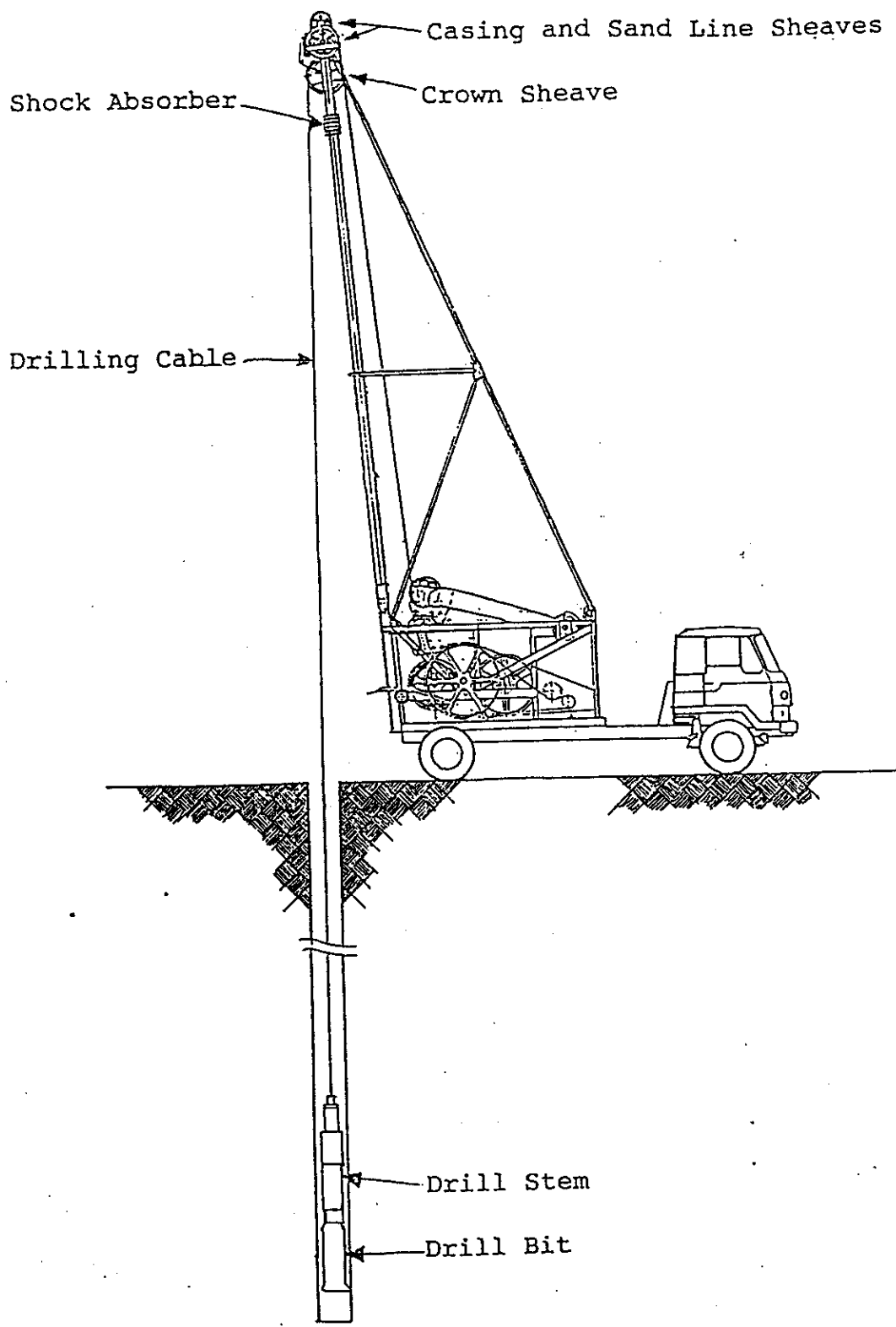


Figure 1.1 PERCUSSION TYPE DRILLING MACHINE

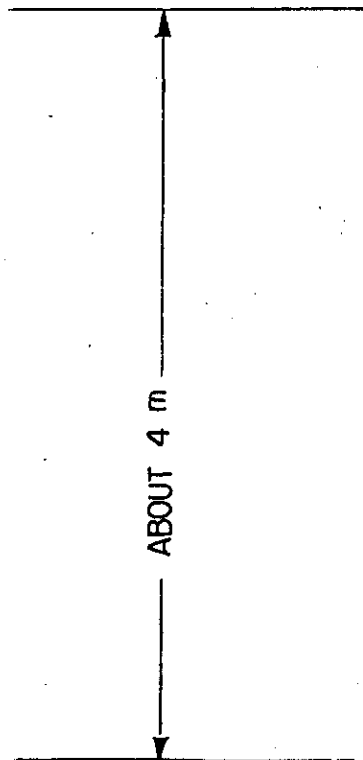
Percussion Drilling Bit



Sharp-pointed Bit

Straight Line Bit

Star Bit



Bailer

Sand Pump

Fig. 1.2 Drilling Bits And Bailer And Sand Pump For Percussion Drilling

(1) Spindle Type

The spindle type drilling machine is a small sized machine with a drilling capacity of less than 1,200 m.

With the spindle type, drilling work is carried out by rotation of the spindle with a pressure weight that is lifted and dropped through the rotation pipe fixed by the chuck of spindle. The typical spindle type drilling machine is shown in Figure 1.3.

(2) Rotary Table Type

The rotary table type is larger in size than the spindle type and can drill up to more than 2,000 m. It is usually of the truck-mounted type, therefore, drilling can be smoothly and quickly executed in a short time.

With the rotary table type, the drill stems connected to drill pipes are rotated by connecting with a square hole located in the center of rotating table. The pressure weight for the bit should be appropriately adjusted by the weight of drill stems, drill pipes, drill collars and bits.

Drilling machines of the rotary table type are fairly easier to maintain since these are mechanically operated. The typical rotary table type drilling machine is shown in Figure 1.4.

(3) Top-head Drive Type

The top-head drive type drilling machine is similar in size to the rotary table type, capable of drilling very deep below the ground and is of the truck-mounted type. Rotation of bit is by hydraulic mechanism with the water swivel with chuck hung in the upper portion of mast. This type is different from the rotary table type in that the full system is operated by hydraulic power while the rotary table type is operated mechanically.

Drilling machine of top-head drive type is easy to operate even with the connection of additional drill pipe during drilling time.

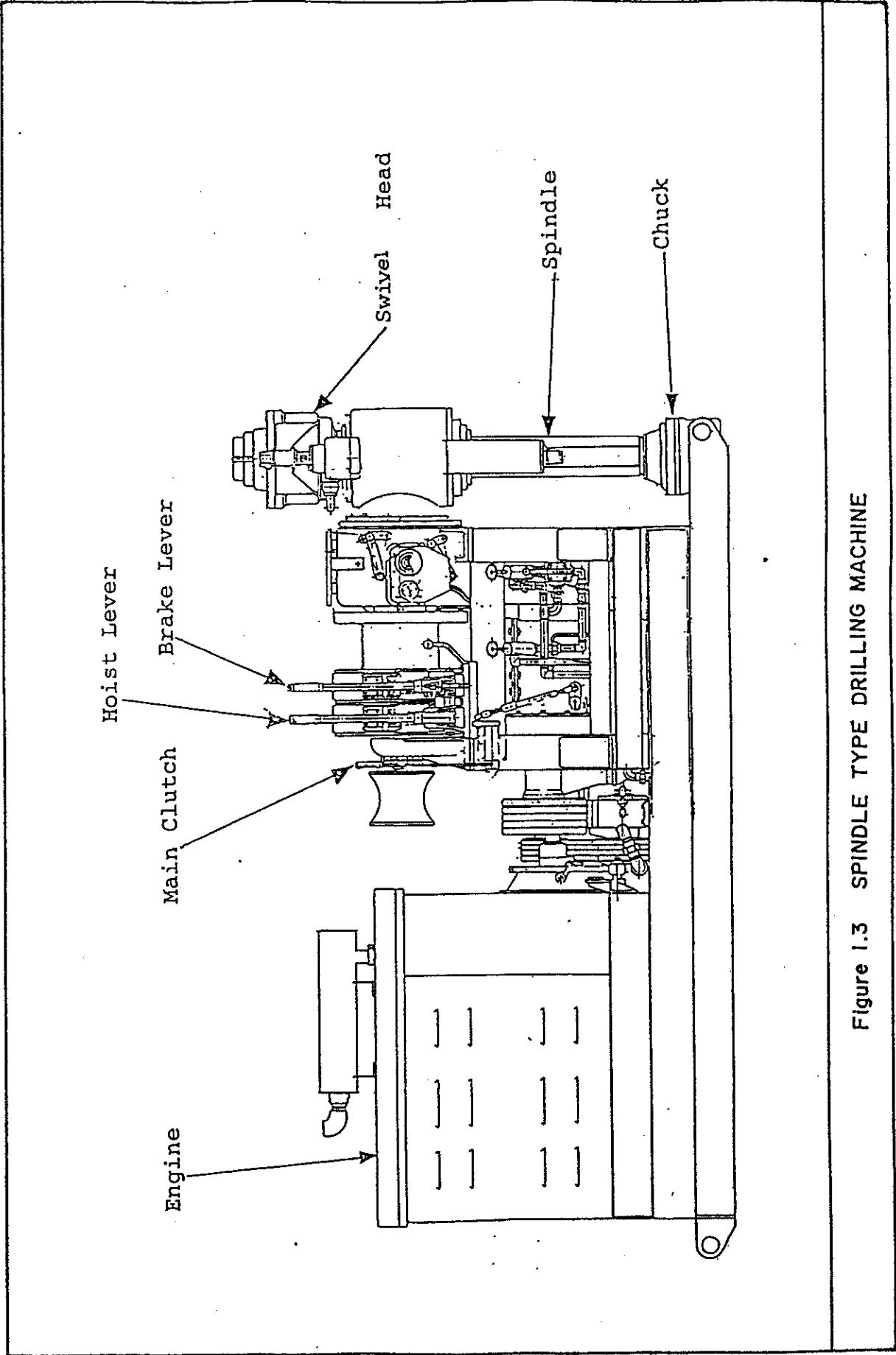


Figure 1.3 SPINDLE TYPE DRILLING MACHINE

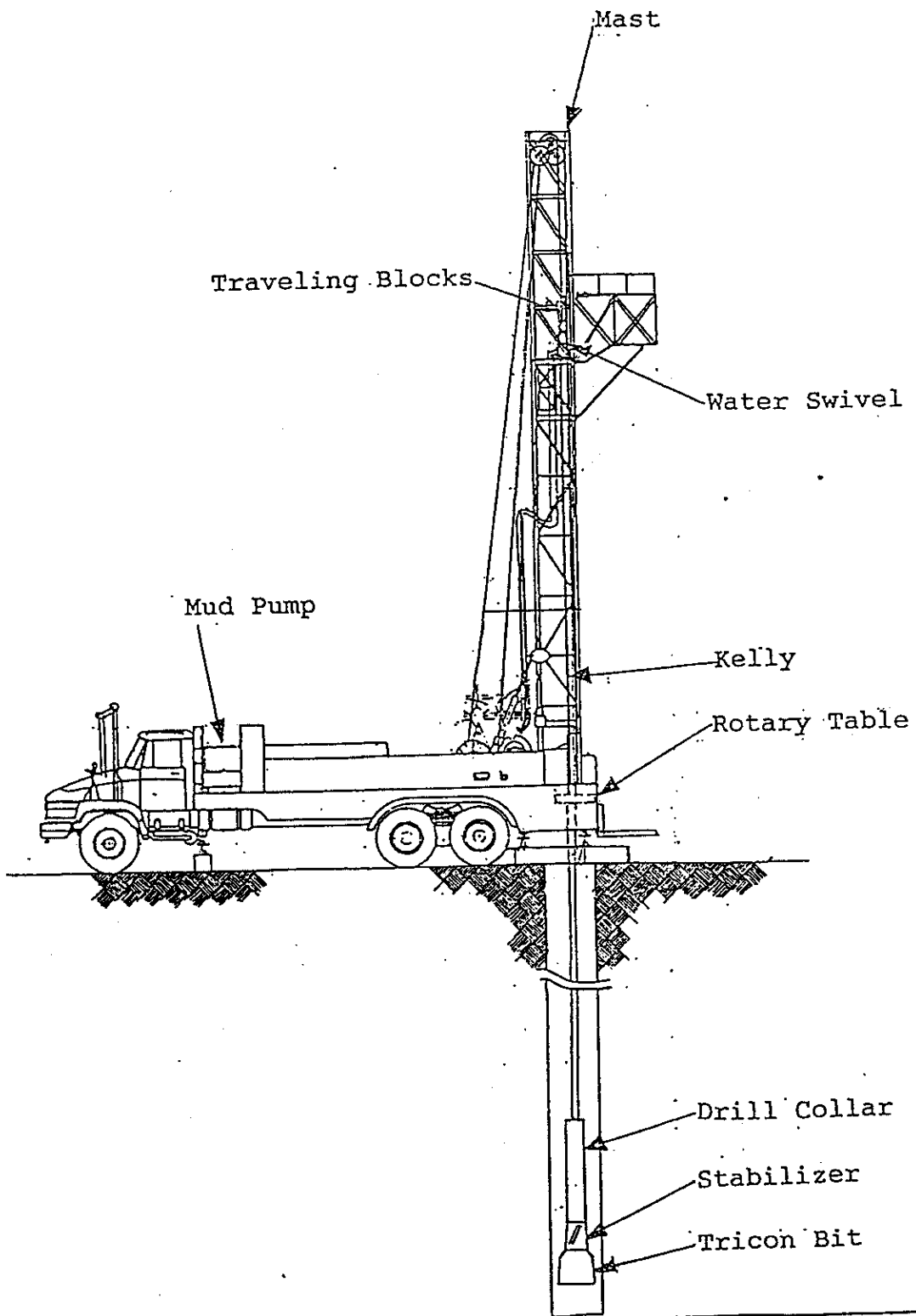


Figure 1.4 ROTARY TABLE TYPE DRILLING MACHINE

Maintenance, however, is very difficult because the whole system is hydraulically operated. The top head drive type of drilling machine is shown in Figure 1.5

### 1.1.3 Air Drilling (Down the Hole Drill)

Down the hole drilling is a method wherein the drilling bit hammer is moved by air pressure and crushes hard rock. Air necessary for air drilling is supplied through the boring rods by an air compressor, with rotation and driving done through boring rods connected between drilling bit hammer and rotary drilling machine. In down the hole drilling, air is used as percussion action of bit and as medium to convey drilling debris moving up between the drilled hole and boring rod up to outer hole.

Down the hole drilling is the most suitable drilling method for hard rock formation and drilling can be undertaken with the highest speed compared with other drilling methods. Hard rocks are crushed with the vibration of down the hole hammer operated by compressed air and pressure against the rotation of the hammer transmitted by rotary drilling machine of truck-mounted type, table rotary type or top-head drive type.

The down the hole drilling method has the following advantages:

- o A good natural drilling hole is maintained.
- o Drilling in fissured rocks may be done efficiently.
- o A straight hole can be attained with high speed drilling.
- o A longer life span of the rod is assured.

However, this method has the following disadvantages:

- o The equipment has to be regularly inspected, cleaned, lubricated and maintained to function effectively.
- o Circulating air speed has to be more than 20 m/second to convey drilling debris out of the drilling hole.



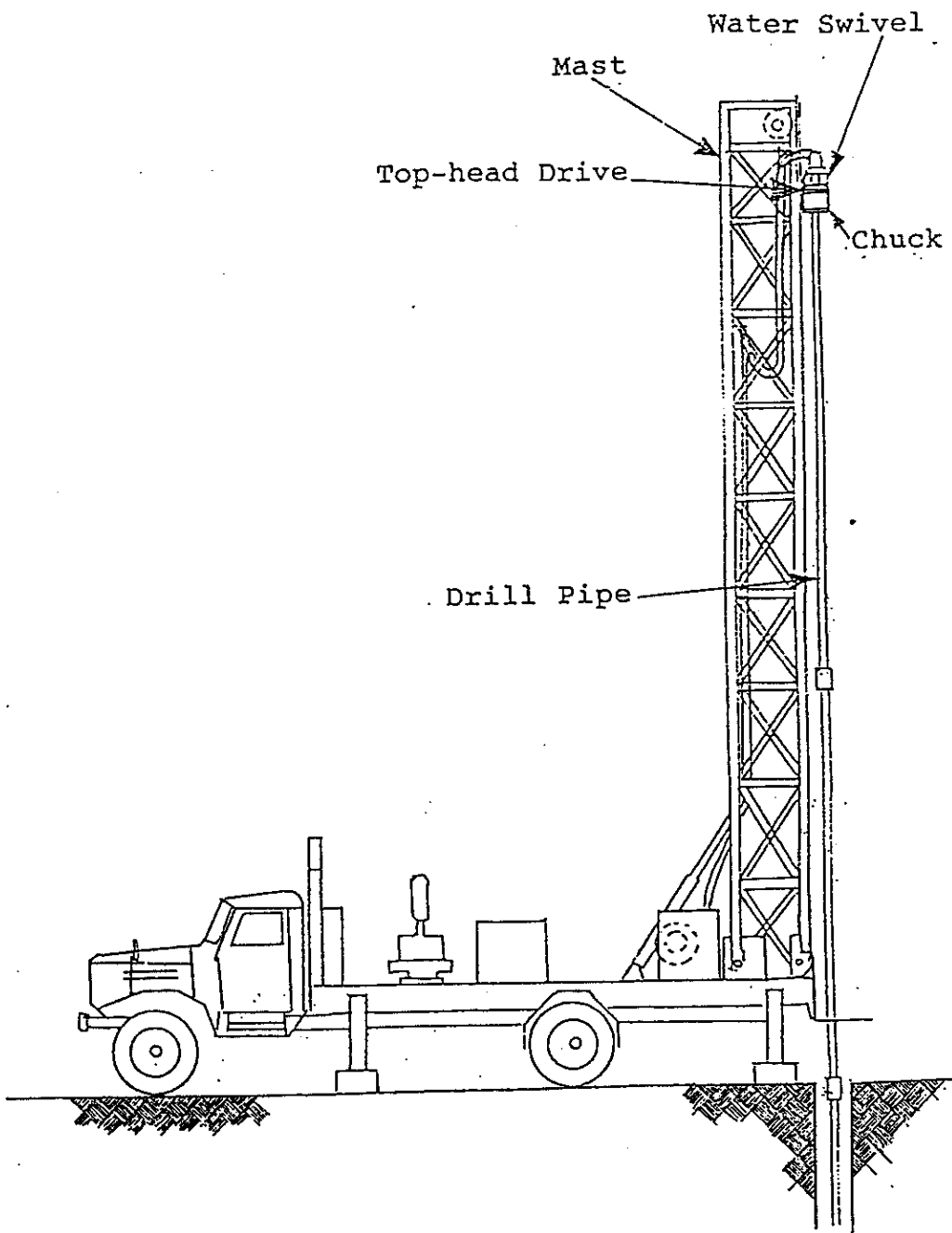


Figure I.5 TOP-HEAD DRIVE TYPE DRILLING MACHINE

- o To compensate the loss caused by back pressure due to water level in drilling hole, an air compressor with large capacity of air flow and pressure has to be used.

In the down the hole drilling, the following equipment and materials are required:

- o Drilling hammer (consisting of hammer, cylinder, chuck cylinder, bit and check valve and others),
- o Boring rods (normal rods more than 50 mm in diameter),
- o Base machine of rotary table type or top-drive type (normal type boring machine which supplies rotation and pressure to bit),
- o Air compressor (air pressure: 7-18 kg/cm<sup>2</sup>, air amount: 10-20 m<sup>3</sup>/min),
- o Generator to operate air compressor,
- o Foaming agent.

The air drilling method is shown in Figure 1.6.

## 1.2 HOLE CLEANING METHODS

With the rotary drilling method, boreholes may be cleaned either by normal circulation or by reverse circulation. Drilled cuttings must be completely removed from the hole and the wall of the hole be stabilized. Unless the hole is clean and open, drilling cannot be continued. The hole cleaning methods discussed below are illustrated in Figure 1.7.

### (1) Normal Circulation Method

Normal circulation is generally used when the circulation medium of either air, water or drilling mud is pumped under pressure down the drill rods through the bit and carries drill cuttings to the ground surface between the wall of the hole and the drill rods.

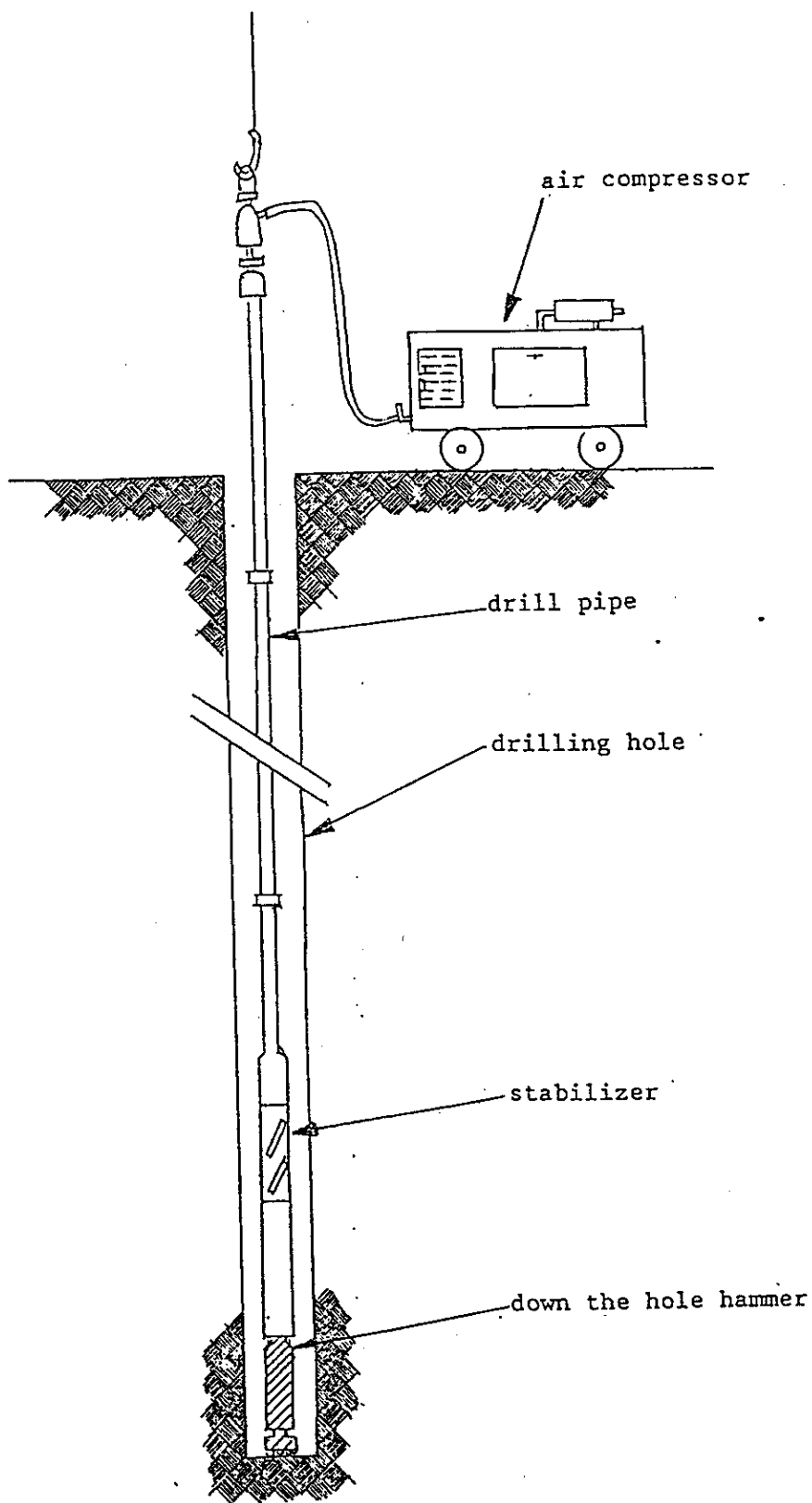
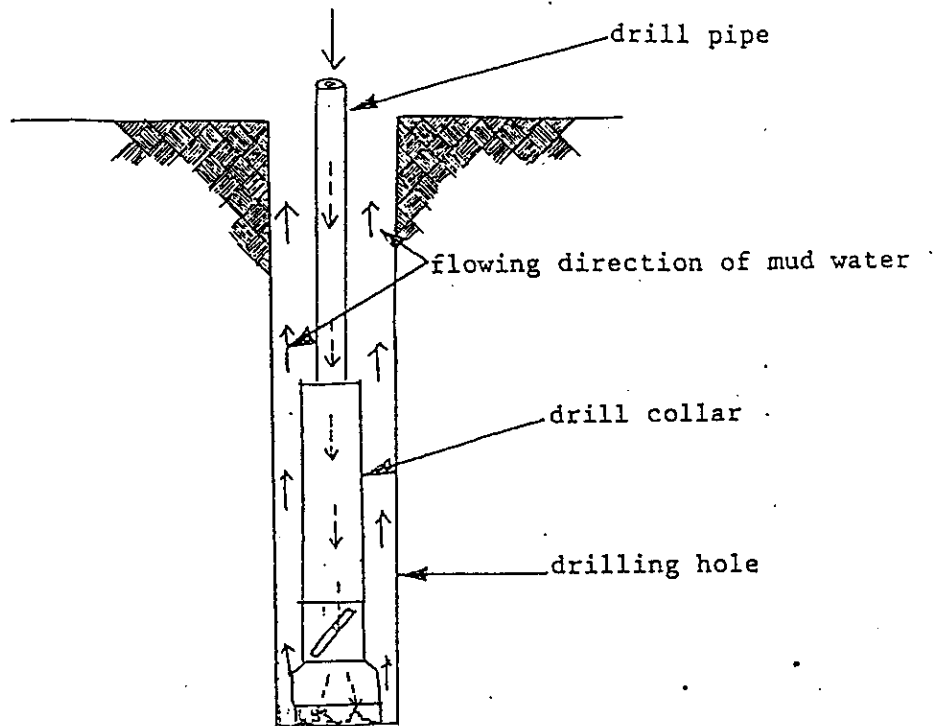


Figure I.6 AIR DRILLING METHOD

Normal Circulation Drilling



Reverse Circulation Drilling

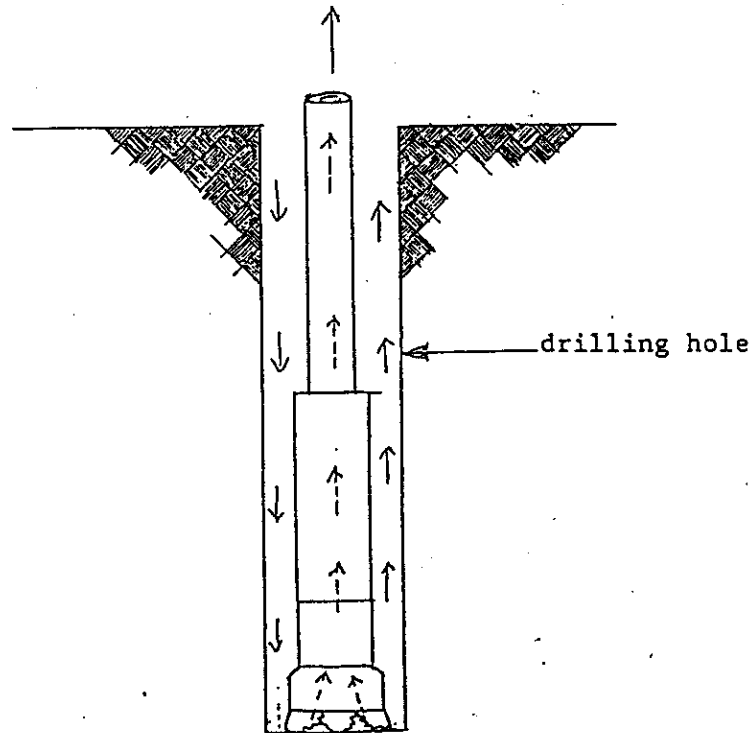


Figure I.7 HOLE CLEANING METHOD

Normal circulation method is most commonly used in the construction of deep water wells with casing diameters ranging from 4" to 16".

(2) Reverse Circulation Drilling Method

Reverse circulation drilling is the least expensive method for the drilling of large diameter holes in unconsolidated formations. When geologic conditions are favorable, the increasing diameter of the borehole does not necessarily increase the cost of the well. Therefore, most water wells 24 inches in diameter or larger (up to 60 in) are drilled using the reverse circulation method.

Reverse circulation drilling is most suitable to soft sedimentary rocks and unconsolidated sand and gravel where the static water level is 3 m or more below ground level. In case of high static water level, ramps are built above grade to support the drilling rig, or the specific gravity of the drilling fluid is increased to obtain the necessary hydrostatic pressure. The reverse circulation drilling method may not be satisfactory when the static water level is too high and adequate water supplies are not available. Reverse circulation has the flow circulating down the hole between the bit and up to the inside of the drill rods. Circulation is obtained by the following methods:

- (a) A suction lift pump is introduced between the drilling rig swivels and mud pit providing typically a 10 m suction lift to the fluid contained in the drill pipe. Circulation is then achieved by displacement.
- (b) Two air pipes are installed on the side of the drill pipes and are capable of being alternated to allow air to be introduced to the drilling fluid inside the drill pipe at typically 10-20 meters submergence.

The introduction of air makes the drilling fluid in the drill rods less dense than the fluid between the hole wall and rods. Circulation is achieved by displacement.

- (c) A stuffing box is installed on surface casing and the fluid is pumped under pressure down between the hole wall and drill rods, through the bit and up inside the drill rods.

In this system, the drill rods are attached with an inner and outer tube. Air passes between the inner and outer tube through the bit and returns with cutting debris up in the inner tube.

### 1.3 WELL DESIGN AND CONSTRUCTION

Generally, well construction is carried out in the following manner:

#### (1) Determination of Well Design

Prior to well drilling, well design shall be roughly determined based on geological and hydrogeological conditions and designed pumping rate. Well design comprise of well depth, well structure, length, size and material of screen and casing. After the survey and gathering of data on existing wells particularly static water level, dynamic water level, well depths, screen portion, columnar sections, geological formation and electric resistivity, groundwater development potential of the groundwater basin of the project area is analyzed and the final well design is determined.

#### (2) Selection of Drilling Method and Equipment

Based on the results of geological and hydrogeological studies, drilling methods and equipment suitable to geological condition, drilling depth and hole diameter will be determined.

#### (3) Determination of Drilling Point

Determination of drilling point is most important in drilling work. In low potential areas for groundwater development such as rocky and mountainous areas covered by hard rock on ground surface, selection of drilling point is very difficult and to get

groundwater and to encounter fault lines and fissure zone unlike alluvium and diluvium is fairly difficult in the area. Metro Manila area is underlain by fairly thick alluvium and diluvium formation in which high groundwater potential occurs except for the plateau like Antipolo. The determination of drilling points, it is considered, are not so difficult. In addition, drilling point shall be also determined under the consideration of groundwater quality.

Drilling points should be also selected in the point of view from the drilling work. The drilling sites must have good accessibility for drilling machine and vehicles to approach easily and afford an enough working space for drilling work.

**(4) Mobilization of Drilling Equipment and Materials**

Drilling equipment and materials will be mobilized, assembled and set up at the site. Work shall be done by skillful drillers and engineers and arrangements made to place each equipment and material in the drilling sites as required.

**(a) Setting of drilling machine**

Drilling machine shall be set up with care in the site. Unlike the assembly type of mast in the site, the drilling machine is generally very heavy weighing over several ten tons. The drilling machine shall be tightly set up using strong and solid timber and iron bars and the mast shall be held stable by tying between the four corners of the mast and fixed natural materials.

**(5) Drilling**

Drilling work is generally carried out by a team of one skilled driller and some laborers. The driller shall always check drilling condition by observing cutting debris and specific gravity of mud water and groundwater level in drilled hole and operating condition of equipment. Free flowing of mud water from drilled hole and/or the lowering of static groundwater level will imply the

encounter with aquifer on the way to well drilling.

(6) Electric Logging

After designed drilling depth is attained, electric logging tests shall be carried out in the drilled hole. The methodology is described in another manual on prospecting method for groundwater survey. In general, the electric logging tests shall be carried out by short normal and long normal methods at different intervals of each electrode. Based on the results of the electric logging test, the most suitable casing program particularly the screened portion in the well depth shall be established. The screen is generally located in the portion of fairly large difference between results of short normal and long normal because this area is identified as sand and gravel formations of good aquifers. On the contrary, low and similar values can be assumed to coincide with clay formation or aquiclude. An example of a casing program is shown in Figure 1.8.

(7) Installation of Casing

Casings and screens are to be installed in the drilled hole in accordance with the results of casing program. Casings and screens welded together are slowly lowered into the hole.

(8) Gravel Packing

Immediately after the installation of the casings and screens, gravel is packed in to ensure its stability. Since the final performance of the well is highly dependent on the correct construction of the intake, the installation of the gravel pack has to be carried out with all possible care. This takes the place of the graded zone of the permeable material that is produced by the natural development process. When properly constructed, the wells are efficient and stable. Size of gravel pack materials or particles is determined by the geological condition and type of screen. The thickness of gravel packing is a primary factor in the effectiveness of the development procedures taking place at the interface of the pack and formation. The minimum practical thickness



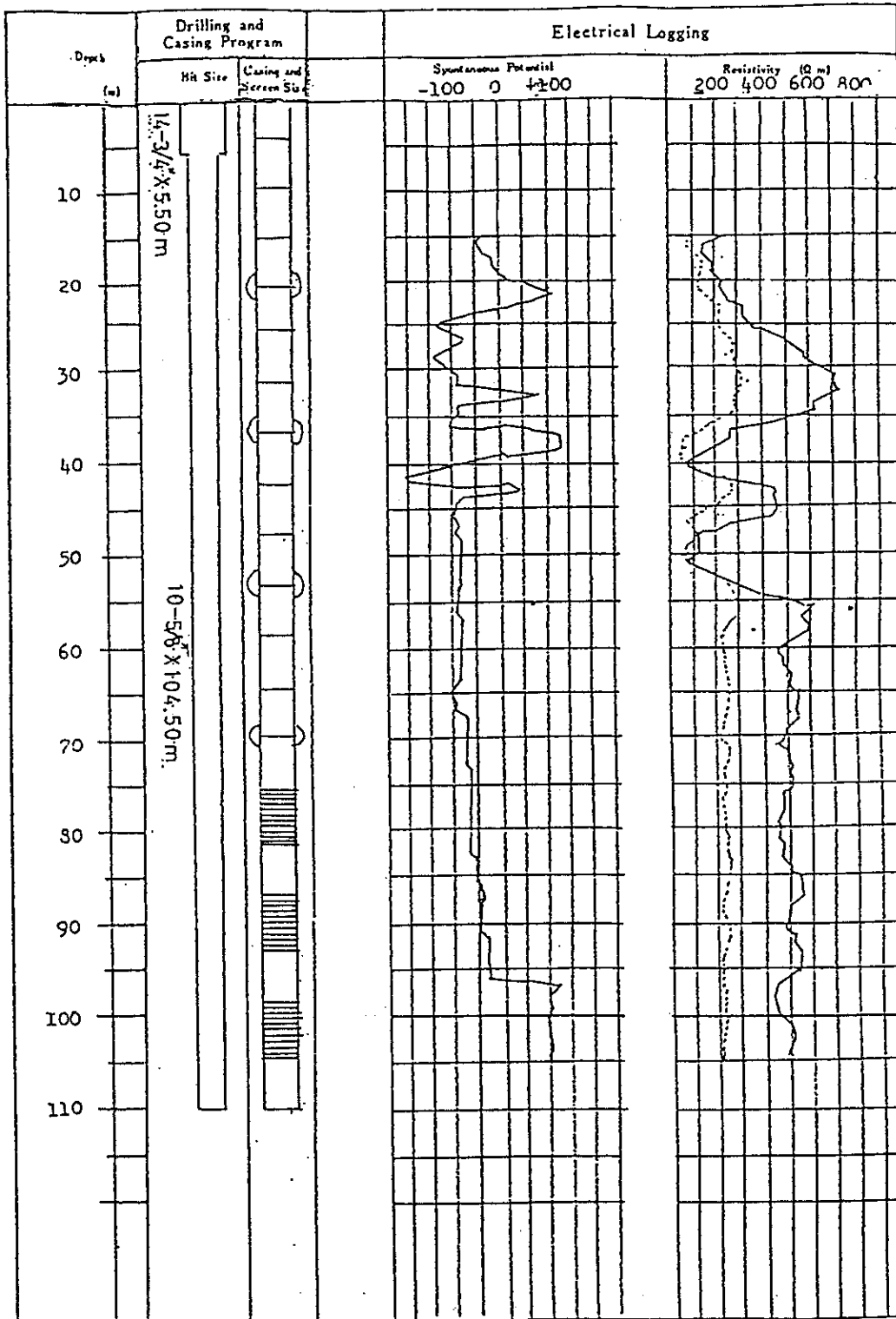


Figure I.8 CASING PROGRAM AND RESULTS OF ELECTRIC LOGGING

for the pack is 76 mm. Gravel packs thicker than 203 mm are not recommended because the effectiveness of the development procedures may be impaired.

(9) Well Development

The basic principle of well development involves the dislodgement and removal of any material hindering the free flow of water to or from the well. When deciding on the type of development which best suits the well and the situation existing in the zone to be developed, a driller must be sure that the undesirable material is dislodged or removed. Any method which dislodges the undesirable material but fails to remove it from the aquifer is not a suitable one. The method is particularly unsuitable if it tends to push clogging material further into the aquifer. This means that the most effective methods are those that continually draw water from the aquifer while intermittent surges or short reversals in the flow, serve to dislodge stubborn particles.

Where mud fluids or mud cake are in the aquifer, the mud is cleared from inside the screen and casing and the appropriate break or dispersing chemicals are introduced. Where a gap exists between the screen and the walls of a hole in an unconsolidated aquifer, the aquifers collapse against the screen. A gentle washing action is used, commencing at the lower end. The full screened interval is developed using a washing technique while the yield of the well and the movement of sand into the well is checked. Sluicing techniques may be required to complete development. These techniques are best applied to the screen, a short length at a time, commencing at the bottom. Open hole completions may be developed using shock methods. Sometimes shock development in the open hole is followed by casing and screening.

As development proceeds, the following shall be checked:

- 1) the net flow from the well,
- 2) the drawdown (below S.W.L.),
- 3) the quantity and size of the sand drawn into the well.

(a) Air lift development

Air lifting, when used for development has the following advantages:

- 1) the pump is not damaged by sand
- 2) the air lift column can be used to clean the bottom of the hole by suction
- 3) the intermittent nature of air lift pumping provides a gentle surging action
- 4) stronger agitation or surging can be achieved easily by lowering the air tube below the column, and closing the top of the casing with a tight head.

(b) Mechanical surging and high velocity jetting

Vigorous sluicing methods should not be used where the high energy action is likely to disperse thin clay or silt horizons through the more permeable parts of the aquifer. Aquifers of this type must be developed using washing techniques which draw water through the sand and gravel beds only.

The risk of damage to the aquifer during plunger surging or jetting operations, is reduced considerably if the material dislodged by the sluicing action is drawn into the well immediately. A continual flow of water from the aquifer into the well, will prevent the dislodged material moving back into the aquifer. The surge plunger equipment used for mechanical surging is shown in Figure 1.9.

1) Mechanical surging

For surging to be successful, the energy of the high velocity water must be directed to the material to be broken or dislodged. The effectiveness of the method is greatly reduced if there are insufficient openings in the screen or if a thick layer of pack material dissipates the energy of the water.

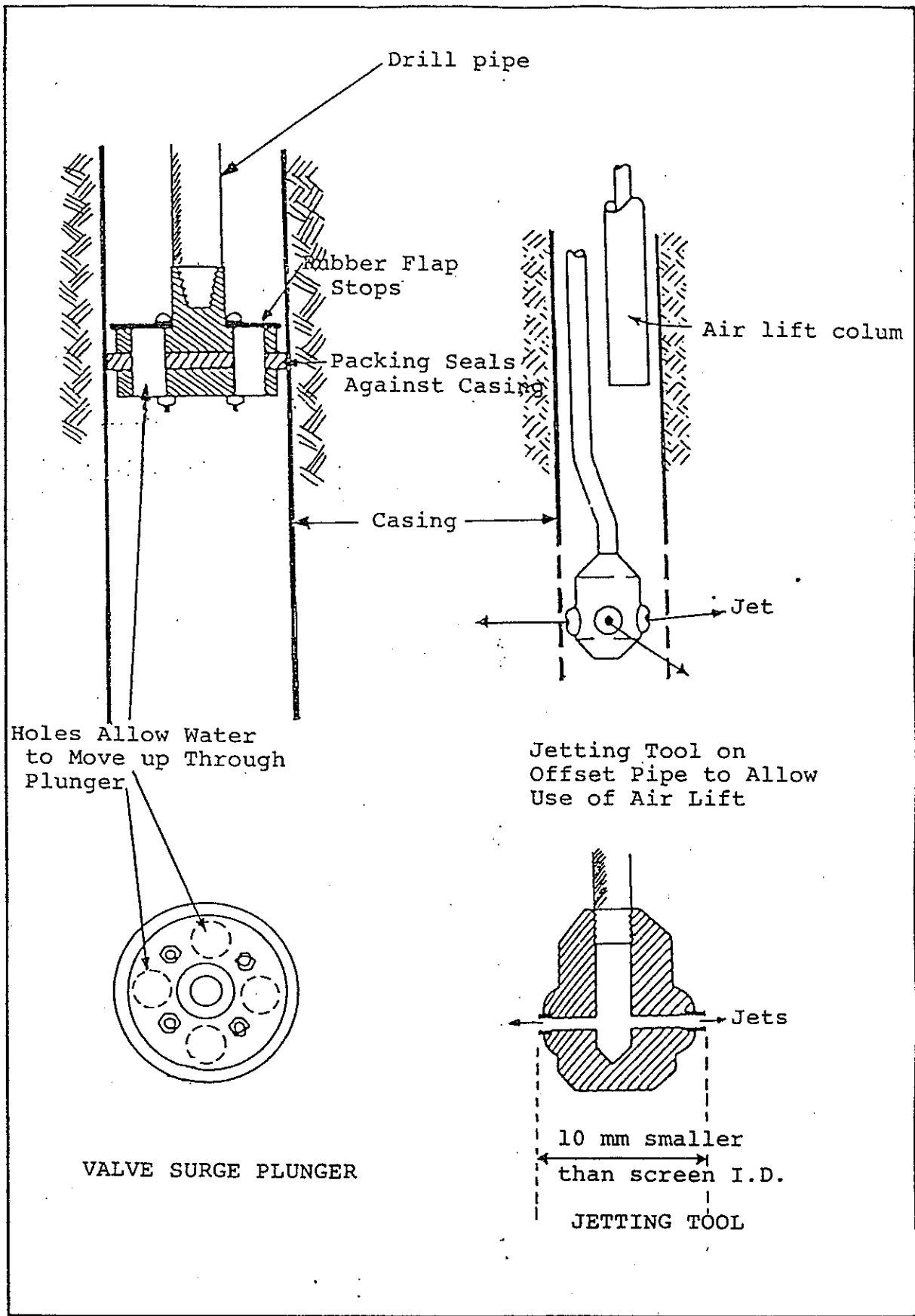


Figure 1.9 SURGE PLUNGER EQUIPMENT  
(for Mechanical Surging)

A surge plunger should be used only when the aquifer is free of clay or after initial bailing has produced a free flow of water into the well. The surge plunger packing must fit well in the casing. The plunger is made up on a drill stem (sinker bar) and run into the hole to a position about 5 m below the water level (but above the screen). With the rig on its longest stroke, the plunger spuds very slowly up and down for 10 minutes. The operation of the valve will cause the plunger to work as a pump and lift water and fine sand out of the hole. After ten (10) minutes, the plunger is withdrawn from the casing and a small bailer is used to clear sand from the screen. The plunger is then run again and the cycle repeated until no more sand is brought out. This process may be repeated with the spudded operating at a higher speed. It should be ensured that the rig action and the motion of the plunger remain smooth. Solid surge plungers (without the valve holes) are sometimes used to obtain a strong backwash flush but as the solid plunger does not move water out of the hole, it is more likely to damage the aquifer. Similarly, the operation of surge plunger inside the screen is not advisable. Surging with a plunger should not continue for more than an hour before conducting a short bailer test to check the specific capacity of the well.

## 2) Jetting method

Jetting is the ideal way of developing flowing wells. The jet is operated while the well is flowing. Before jetting commences, the hole should be cleared of mud by air lifting with the air lift operating at the bottom of the screen. Jetting must commence at the bottom of the screen. With the jets and the air lift (or well pump) operating, the tool is rotated slowly by hand and very slowly lifted (lifted at about 10 minutes per meter). When the jets have covered the full length of the screen, development by pumping

shall continue only until the well is clean.

For the products of development to be drawn out of the aquifer, jetting should be done simultaneous with pumping. Pumping must be at a rate above the rate of injection through the jets. In a large diameter hole, this is not a problem as the pump can be run alongside the jetting pipe. The jetting pipe may be offset for operation in smaller wells. The offset type tool can not be rotated but must be oscillated by hand, during jetting. Rig equipped with a dual pipe string may be developed by jetting while air lifting pumping operates between the string and the casing.

Jetting tools are easily fabricated. Special jetting nozzles are preferable and should be replaceable so that the jet size can be adjusted to suit the pump capacity. Nozzle diameters may vary from 4 mm to 10 mm. The pump capacity must be sufficient to provide a nozzle flow velocity of 50-70 meters per second. The jets should operate with the end of the nozzle about 5 mm clear of the inside of the screen.

### 3) Chemical method

Chemical methods are often used in conjunction with other techniques for development particularly where remedial development is required to break up mud cakes or flush out gelled mud.

Chemical methods, other than acidifying find their main application in unconsolidated sands and gravels. The following chemicals may be used:

- a) breakdown chemicals for polymer muds
- b) dispersant to break down clay smears, wall cakes, bentonite filter cakes or to assist in the removal of gelled bentonite

- c) chlorine or chlorine producing chemicals to assist in breaking colloids and to act on bacteria.

(10) Pumping test

Pumping test consist of step drawdown test, continuous drawdown test and recovery test.

prior to pumping test, trial test shall be conducted in order to check and determine the relation between pumping rate and drawdown. Trial test, often a short 15 minute test is run to confirm the specific capacity of the well and thus allow selection of the most suitable pumping rate for longer tests or to check that the pumping equipment and measuring equipment are operating satisfactorily.

(a) Step drawdown test

The step drawdown test is carried out to reveal the safety yield and the constant of aquifer loss and well loss. To check the safety yield is necessary for the decision of pump capacity, in a word, a pumping rate in newly drilled wells. The constant of aquifer loss and well loss is often used to calculate actual drawdown in wells. The test is executed by from five to seventh steps with two pumping duration hours in each step. The well loss is caused by a turbulent flow in the well which become a major factor in causing drawdown at high pumping rates. At lower rates, the aquifer losses in the formation are more significant. Pumping at a range of different rates allows these factors to be separated.

(b) Continuous drawdown test

Continuous drawdown test usually at the desired yield rate or at a rate within 20% of the capacity of the bore, are conducted with the pumping rate held constant (within 10%). This constant rate must be maintained for the full period of

the test. Wells for domestic or communal use may be tested for short periods (2 to 8 hours). Wells for high demand uses, such as irrigation or town supplies, are tested under the condition of constant discharge for periods of 24 to 48 hours.

The test is carried out to obtain the transmissibility and storage coefficient. The aquifer constant, transmissibility and permeability and storage coefficient are used to reveal the characteristics of aquifer and to calculate the radius of influence of cone of depression and others during pumping test. These data are effective to estimate the development potential of groundwater, especially.

(c) Recovery test

Recovery test is a measurement of residual drawdown during the recovery period. As pumping continues, groundwater gradient develops carrying water in to support the flow of the well. When the pump is turned off, the flow through the aquifer continues until the gradient is no longer present. The drawdown readings thus decrease in the same way they were established.

At the beginning of the pumping test, there is a need for accurate timing. Records of exactly when pumping starts and when the measurements are taken during the first 10 minutes, must be accurate to within a half minute. During the first minutes, the pump operator, who is a member of the drilling crew, must get the test pump engine to the correct speed and stabilize the pumping rate at the desired level. Flow measurements must be made every minute or so to check that the flow rate does not vary as the drawdown increases.

Accuracy of flow measurements must guarantee a reading within 10% of the true figure. This means that while orifice plates or weir boards are adequate for large flows, small flows are better measured by timing the filling of containers. The drawdown is best measured by reading the distance of the pumping level below the



static water level. The measurements must be accurate to within 5 mm of drawdown. Some tests may require even higher accuracy.

(11) Demobilization

Demobilization shall be started after completion of the drilling work. The site should be cleaned and restored to the original condition.

(12) Submission of drilling report

Drillers shall accomplish the daily progress report and submit it to the engineers. The drilling report shall include columnar section, the result of electric logging test, drilling speed and depth, water level in drilling hole, drilling work and performance. Sample format of daily progress report is shown in Figure 1.10.

Project Name:		
Site No.:		Date:
Site Name:		Location:
Drilling performance:		
Date/time	Drilling depth (m)	Items
		S.W.L(starting time, final time),Lithology Bit size and type and other performance
Remarks:		
Figure 1.10 SAMPLE FORMAT OF DAILY DRILLING REPORT		

## 2. CORE BORING

### 2.1 CORE BORING METHODS

Core boring methods were developed to directly investigate and check geological conditions below ground surface and to determine geological structure and the possibility of mining and ore development. The object of core boring is to take core samples which shall be subject to geological, lithologic and civil engineering inspections.

The most commonly used core boring methods are:

- 1) Single Core Tube method
- 2) Double core Tube method
- 3) Wire Line Core Barrel method

These methods have different characteristics mentioned below.

#### 2.1.1 Single Core Tube Method

The single core tube is a simple tool that is easy to operate and maintain at a fairly low cost. With this method, a larger core can be obtained and it has a larger drilling ratio compared to the large size double core boring bit tool. However, this method is only applicable to uniform hard formations and not on fault and fissure zones and nonuniform formations.

#### 2.1.2 Double Core Tube Method

The double core tube tool is of two types, namely the rigid and the swivel type.

The rigid type is a fairly simple tool. The inner and outer tube rotate simultaneously resulting in crushing of core samples. Operation cost is high due to the required wide cutting plane and large bit.

The swivel type is a more effective sampling tool and does not crush

core samples against every formation because the inner tube rotates independently from the outer tube.

### 2.1.3 Wire Line Core Barrel Method

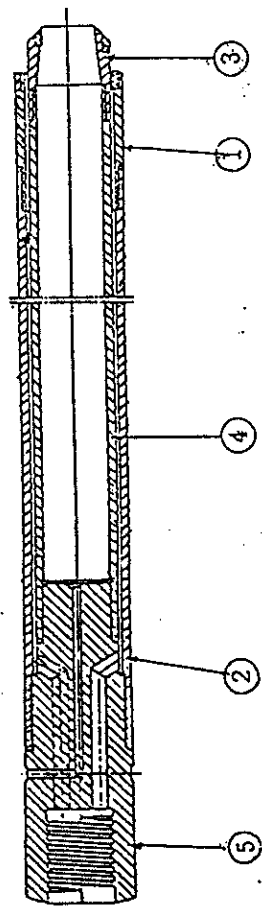
The wire line core barrel is a swivel type - double core tube. This equipment was used in the core boring survey of the Metro Manila Ground-water Development Project. This effective method is carried out at high drilling and core sampling speed in formations of every geological age. The wire line core barrel system is illustrated in Figure 2.1. In case the underground formation includes water, the inner tube goes down with the core tube. Otherwise, it overshoots the drilling bottom in the dried formation. If the inner tube is filled with the drilled formation during drilling, the inner tube is immediately lifted by wire rope. With this method, there is no need to bring up the entire system except for changing the bit, therefore, the working period is shortened. Wire line core barrel method comprise the following equipment:

- a) Outer tube assembly - reaming shell and diamond core bit are attached at the bottom of this tube and drill rod is connected to the upper rim of the tube.
- b) Inner tube assembly - after core samples have been taken, the tube is lifted to ground surface. The end of the tube is equipped with a core lifter to protect the dropping of core samples.
- c) Swivel assembly - outer tube and inner tube are connected by this swivel assembly to allow the outer tube to rotate without moving the inner tube.
- d) Overshot assembly - the tip is equipped with a lifting dog to grasp the inner tube and lift and drop it down the inner tube assembly.
- e) Wire line bit - the outer tube and inner tube diameters of the wire line bit differ largely due to the size of the connecting tube mechanism.

Wire line core boring has recently been applied in hard rock formations

DOUBLE CORE TUBE

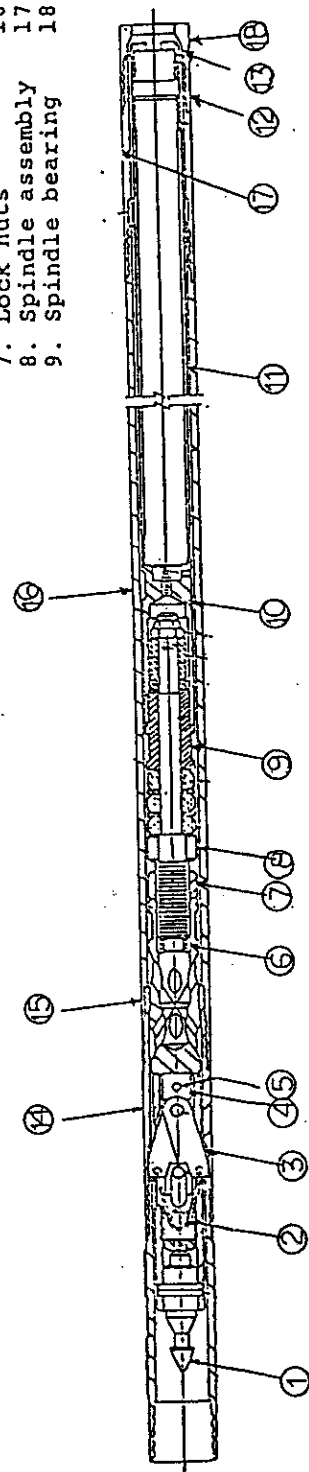
1. Outer metal crown
2. Outer tube
3. Inner metal crown
4. Inner tube
5. Core barrel head



DOUBLE CORE TUBE

WIRE LINE CORE BARREL COMPLETE

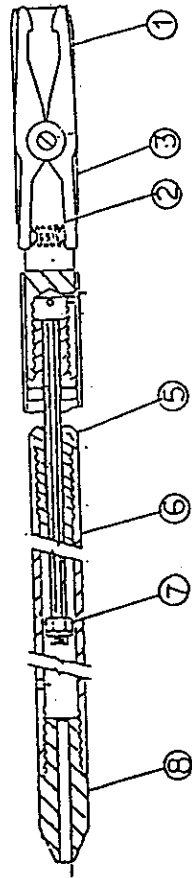
1. Spear head
2. Latch spring
3. Latch
4. Latch support
5. Spring pin
6. Latch body
7. Lock nuts
8. Spindle assembly
9. Spindle bearing
10. Inner tube cap
11. Inner tube
12. Core lifter case
13. Core lifter
14. Adapter capling
15. Landing ring
16. Outer tube
17. Reaming shell
18. Core bit



WIRE LINE CORE BARREL COMPLETE

OVERSHOT FOR WIRE LINE CORE BARREL

1. Lifting dog
2. Lifting dog spring
3. Overshot head
4. Jar head
5. Jar tube
6. Nut
7. Wire line socket



OVERSHOT FOR WIRE LINE CORE BARREL

Figure 2.1 WIRE LINE CORE BARREL SYSTEM

and fissure zones after different types of bits were developed, the shapes and types of which are shown in Table 2.1. For high efficiency, types and sorts of bits are selected based on drilling formation as follows:

<u>Formation</u>	<u>Type of Bit</u>
soft to hard rocks	taper bit
hard rocks	step type multi stage bit
fissure zone	combination reverse taper bit

## 2.2 EFFECTIVE CORE BORING

In case the inner tube of wire line core bore is clogged with the core samples, the core barrel shall be lifted up to ground surface. Core sampling work executed to check the groundwater and geological conditions often clogs inner tube because geological formation sometimes includes the clay. To avoid the clogging of barrel by the core samples, the special type bit (S crown type) and double core tube with mud water shall be used and care shall be taken to control mud water.

For effective drilling and smooth core boring, proper pressing weight should be applied to drilling bit, rotation of drilling bit is maintained and supply of water for bit is ensured. However, to ensure the above, ample experience is necessary.

### (1) Bit pressure and weight

Effective bit pressure and weight to crush and drill the rocks are different for every type of drilling formation, the number of bolts of bit and the rotation speed of bit.

### (2) Rotation speed of bit

Rotation speed of the bit depends on the cutting action of bit and on abrasion loss. Small bolts bit is ideally used with light weight and pressure which slightly exceed crushing drilling pres-

Table 2.1 Specifications of Wire Line Core Barrel

Type of Core	Q Series				TV Series			
	AD	BE	NO	HA	EX	AX	BX	NX
Dia. of Drilling Hole (mm)	48.0	60.0	75.8	96.0	37.7	48.0	60.0	75.7
Dia. of Core (mm)	27.0	36.5	47.6	63.5	20.0	27.0	36.4	47.6
Outer Dia. of reaming shell (mm)	48.0	60.0	75.8	96.0	37.72	48.01	59.94	75.69
Outer Dia. of outer tube (mm)	46.0	57.2	73.0	92.1	36.0	46.0	57.2	73.0
Outer dia of inner tube (mm)	32.5	42.9	55.6	73.0	24.5	32.5	42.9	55.6
Length of core barrel (ft)	5 10 -----	5 10 15	5 10 15	5 10 -----				
Weight of one set of core barrel (kg)	16.0 26.3	24.2 38.2 52.2	43.0 62.9 82.9	70.2 104.3				
Outer dia. of drilling rod	44.5	55.6	69.9	88.9	35	44.5	55.6	70
Inner dia. of drilling rod	34.9	46.0	60.3	77.8	26.5	35	46	60
Outer dia. of diamond core bit	47.6	59.5	74.6	95.6	37.34	47.64	59.56	75.31
Inner dia. of diamond core bit	27.0	36.5	47.6	63.5	20	26.97	36.40	47.63

sure and high rotation speed. Large bolts bit is used with heavy weight and slow rotation speed. In general, bolts abrasion becomes larger if rotation speed and bit weight operate effectively.

(3) Selection of diamond bit

Type of diamond bit shall correspond to the size of diamond and matrix of the drilling formation.



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## 1. THE CAUSES OF DAMAGES IN MWSS WELLS

The main causes of wells' low or no output of water are discussed as follows.

### 1.1 REGIONAL DECLINE OF GROUNDWATER LEVEL

Regional decline of water level occurs in the whole Metro Manila Area. The rate of decline is estimated at four (4) meters per year, as shown in Figure 1.1. Figure 1.1(A) shows the well condition immediately after its completion. Figure 1.1(B) shows the well condition 5 or 10 years later. Both the static and pumping water levels declined yearly, because of the overpumping of the well itself and/or its nearby wells. The declining water level has made the capacity of the submersible pump not fitted to the well condition: higher-head submersible pump is needed.

### 1.2 DEFECTIVE PUMPING UNIT

Pumping unit must be checked periodically, because it deteriorates and superannuates.

Defects in pumping unit are caused by: superannuation of pumping unit, regional decline of groundwater level, well cave-in, dirty water intrusion, drying up of well, etc.

#### 1.2.1 Superannuation of Pumping Unit

Pumping unit deteriorates and superannuates, because of bad quality of water, sand pumping, etc. Pumping unit must be checked and overhauled periodically.

#### 1.2.2 Regional Decline of Groundwater Level

Once the static water level declines, the discharge rate begins to drop, because the capacity of the pumping unit is not fitted anymore to the condition of the well. The pumping unit is now overloaded and required to have a higher head.

If the pumping water level almost reaches the pump setting position, tripping of pumping unit occurs frequently. The on and off operations will happen frequently, causing the pumping unit to deteriorate easily.

#### 1.2.3 Well Cave-in

Once well cave-in occurs, when the formation surrounding the well collapses, sand, gravel or clay enters the well. If the submersible pump is operated under this condition, sand, gravel or clay comes into the pump impeller, causing its vanes to wear and the well yield to decrease.

#### 1.2.4 Dirty Water Yields

Once surface water with iron bacteria enters the well, the iron bacteria produce accumulations of slimy gel-like material which causes plugging of openings in well screens, riser pipes and impeller of submersible pump. This material is soft at first and hardens gradually, because it dries especially when inside the riser pipes and submersible pump.

In this case, the submersible pump is operated under overload condition. When it is operated for a long time under this condition, the pump will deteriorate easily.

#### 1.2.5 Drying Up of Wells

Once well dries up, pumping water level will subsequently reach the pump setting position and make the pumping unit to trip frequently. The submersible pump will deteriorate easily because of the on and off operations of the pump when tripping happens, and also because of the intrusion of sand, gravel, clay or rust that have accumulated at the bottom of the well into the pump.

### 1.3 SALT WATER INTRUSION

Salty water were observed in wells along the coastal areas of Manila Bay and Laguna de Bay. Figure 1.2(A) shows the condition of the well immediately after its completion; this well yielded fresh water. Salt and fresh water zones were balanced at that time, because the fresh



water piezometric head was so high that salt water could not intrude into its zone.

Figure 1.2(B) shows the well condition 5 or 10 years later. Well has yielded salt water. The fresh water level has lowered because of over-pumping of the surrounding wells and also due to regional decline of groundwater level. The fresh water level has declined so much that salt water from marine ponds, Manila Bay or Laguna de Bay easily intruded the fresh water zone.

#### 1.4 WELL CAVE-IN

Well cave-in was observed in eight (8) municipalities: Caloocan City, San Mateo, Manila, Pasig, Cavite, Imus and Kawit. Figure 1.3(A) shows the condition of the well immediately after the completion of drilling. This well operated very well. Figure 1.3(B) shows its condition after well cave-in occurred. "Well cave-in" means that some formation surrounding the well collapsed, and the material consisting the formation, such as gravel, sand or clay, enters the well. The Study Team observed some fragile formations consisting of tuff when it carried out core borings at Las Piñas in 1990. The tuff formations could easily collapsed by overpumping, because the mass were not that firm or strong. Once well cave-in occurred, the submersible pump could easily become defective due to sand-pumping or low well yields: gravel, sand or clay that accumulated at the bottom of the well could block openings and prevent groundwater from passing through.

#### 1.5 DIRTY WATER INTRUSION

Dirty well yields were observed in five (5) municipalities along Marikina Fault: San Mateo, Quezon City, Cainta, Makati and Muntinglupa. Figure 1.4(A) shows the wells' conditions immediately after the completion of drilling. Fresh water was pumped up from these wells. Figure 1.4(B) shows the wells' conditions after dirt water has intruded. Dirty surface water which is sometimes contaminated with iron bacteria has intruded the wells because the well design was not proper that surface water could easily enter the well.

## 1.6 DRYING UP OF WELLS

Drying up of wells was observed in Cavite: Cavite City, Imus and Bacoor. Figure 1.5(a) shows the well condition immediately after its completion. These wells operated very well. Figure 1.5(b) shows the wells' operating conditions after well cave-in has occurred.

Drying up of a well seems to occur when the well depth is shallow, when the well did not penetrate a confined aquifer, or when well cave-in occurs. In the first case, the water level has reached the bottom of the well due to its continuous decline. In the case of well cave-in, the groundwater could hardly enter the well due to the accumulation of gravel, sand or clay at the well bottom.

## 2. THE PROCEDURE AND METHOD FOR REHABILITATION

### 2.1 THE STANDARD PROCEDURE AND METHOD FOR REHABILITATION

#### 2.1.1 Scope

The experimental work for rehabilitation was drawn up for five (5) MWSS deepwells in Metro Manila. In accordance with the results of the work, the following standard procedure and method for rehabilitation are recommended.

The standard work for rehabilitation involves the following activities:

- 1) Preparation and mobilization
- 2) Pulling out of existing pumping unit
- 3) Measuring of well depth and water level
- 4) Inspection of existing pumping unit
- 5) Installation of test pumping unit
- 6) First pumping test
- 7) Surging, bailing and airlifting
- 8) Second pumping test
- 9) Installation of new pumping unit
- 10) Demobilization

## 2.1.2 Preparation and Mobilization

### (1) Preparation of Equipment and Materials

The Contractor should prepare and provide equipment and materials necessary to complete the work within the contract period.

### (2) Mobilization

The contractor should mobilize equipment and materials and conduct preparatory work under the direction of the Consultant.

### (3) Pulling out of existing pumping unit

The Contractor should pull out the existing pumping unit (riser pipes, submersible cables and submersible pump) carefully.

### (4) Measuring of well depth and water level

#### Measurement

The Contractor should measure the well depth and static water level after pulling out the existing pumping unit. The accumulation of sand, mud, rust and other materials at the bottom of the well shall be investigated throughout the measurement.

### (5) Inspection of existing pumping unit

The Contractor should check the existing pumping unit that includes submersible pump and motor, submersible cable, riser pipes and control panel. Slight damage should be repaired. The scales adhering to the units should be removed and the units should be cleaned up.

### (6) Installation of test pumping unit

The Contractor should provide, install and operate a test pumping unit to carry out the following pumping test.

- Step drawdown test

- Constant discharge test
- Recovery test

The Contractor should provide the test pumping unit that will be able to deliver a discharge rate which will be the expected yield of the well where gate valve will be suitably throttled.

The Contractor should set the test pumping unit with accessories into the well under the direction of the Consultant.

The Contractor should install a temporary sounding tube of 3/4 inch diameter from top of the well to pump bowl assembly to sound water level easily.

#### (7) First pumping test

One of the following types of pumping test should be carried out at each well under the direction of the Consultant. Pumping water level should be observed and measured continuously by the use of notched weir and electrical sounding wire.

##### Step drawdown test

The step drawdown test should be conducted at five (5) steps with duration of two (2) hours for each step. The pumping rate should be decided at the site by the Consultant.

#### (8) Surging and bailing

After the first pumping test, the wells should be surged throughout the screen section. The wells should be bailed when any accumulation are observed. Surging and bailing should be performed more than two (2) days, at eight (8) hours per day.

(9) Airlifting

Upon completion of surging and bailing, the wells should be discharged by airlifting for more than two (2) days, also at eight (8) hours per day. The compressor used for pumping by airlifting should have a developing pressure of 8 kilograms per square centimeter (114 psi), and the delivery rate should be 17 cubic meter of air per minute. From time to time, the air blow should be stopped to facilitate the loosening of trapped materials.

Airlifting should be completed with the eductor pipes almost at the bottom of the well to ensure that all materials are cleaned out of the pipe.

(10) Second pumping test

After airlifting, three (3) types of second pumping test should be conducted as follows.

Step drawdown test

Step drawdown test should be conducted in the same manner as already described.

Continuous Pumping Test

This test should be conducted for 24 hours continuously.

The pumping rates should be directed by the Consultant.

Recovery test

After constant discharge test, the recovery of water level should be measured for eight (8) hours.

(11) Installation of new pumping unit

The Contractor should install a new pumping unit into the well after completion of the second pumping test under the direction of the Consultant. Sounding tubes of 3/4 inch diameter should be installed with the new pumping unit to facilitate measurement of water level.

## (12) Demobilization

Upon completion of the rehabilitation work, the Contractor should provide and operate all equipment and materials necessary to restore the well site as neat as possible to its condition before the commencement of the rehabilitation work. This work includes, but not limited to, restoration of structures, removal of sand, mud and other materials. After restoration work, all the equipment and materials used for the rehabilitation work should be demobilized by the Contractor.

## 2.2 COUNTERMEASURES FOR REHABILITATION OF MWSS DEEPWELLS

Of the 258 MWSS deep wells, 70 were identified as damaged wells with defective pumping unit, salty well yields, well cave-in, dirty well yields and drying up.

### 2.2.1 Regional Decline of Groundwater Level

Pull out of the submersible pump is recommended. The new pump which replaces the pulled-out one must be checked periodically.

Rehabilitation work shall be carried out at the same time, and after that, a more suitable pump should be selected and installed at a suitable setting position determined according to the result of pumping test. It is better to re-install and use the existing submersible pump with some additional pump bowls attached to increase the head.

Wells having water level reaching almost the bottom of the well and yielding little amount of water should be abandoned after plugging with cement.

If a well is intended for rehabilitation, then in case of regional decline of groundwater level, the existing pumping unit shall be pulled out at first, and then the well shall be drilled deeper to penetrate a confined aquifer. Some wells have iron plate attached to the bottom of casing pipes or have reduced casing pipe diameter at the bottom. In these cases, the well cannot be drilled any more.

If wells can still be drilled deeper, casing pipes with screens shall be installed at the deeper drilled position, gravel shall be placed surrounding the well screens, and cement grouting shall be carried out at the upper formation to protect the well from sand, gravel or clay intrusion. But this work is very difficult, and it is costly to drill deeper and to shut off completely the upper formation by cement grouting, so that the wells, where the water level has reached almost the bottom of the well, shall be recommended for abandonment. Drilling of a new well with a proper design is recommended instead.

#### 2.2.2 Defective Pumping Unit

If a pumping unit is defective, it shall be pulled out from the well as soon as possible. The well shall be rehabilitated in the same manner as described in Section 2.1 and then a suitable submersible pump shall be installed at a suitable setting position in accordance to the pumping test result.

#### 2.2.3 Salty Water Yields

If a well yields salty water, it shall be abandoned after plugging with cement.

If wells yielding salty water is intended for rehabilitation, at first, the existing pump shall be pulled out, and then electric conductivity logging shall be carried out in order to detect the formation with salt water intrusion. Fine sand shall be charged into the well beneath the formation with salt water intrusion by using triplex mud pump and drilling pipes. After that, cement milk shall be charged from top of the sand to ground level with the use of drilling equipment, such as triplex pump and drilling pipes, in order to shut off or plug the salt water intrusion zone. One day later, the cement milk hardens, and the cementation remaining inside the well shall be cut by using tricone bit. The sand shall also be removed by the tricone bit and drilling mud. But this work is very difficult, and it is costly to shut off the salt water intrusion zone completely, so that wells yielding salt water shall be recommended for abandonment. Drilling a new well with a proper design is recommended instead.

#### 2.2.4 Well Cave-In

If well cave-in occurs, the well shall be abandoned after plugging with cement.

If the well is intended for rehabilitation, at first, the existing pump shall be pulled out, and then the well depth shall be measured in order to detect the position of the collapsed formation. Gravel, sand or clay from the collapsed formation shall be removed out of the well by using triplex mud pump, tricone bit and drilling pipes. The removal shall be up to the original bottom of the well and done in the same manner as in drilling a new well. After that, new casing pipes which have smaller diameters than the existing ones shall be installed inside the well from ground level to the bottom of the collapsed formation. Then, overhauled and repaired submersible pump shall be installed into the well. If the existing submersible pump cannot be installed because of the new smaller casing pipes, it shall be replaced by a smaller one. This smaller pump shall reduce the discharge rate after rehabilitation. This work is very difficult, and it is costly to remove the collapsed materials inside the well and to install new casing pipes, so that in the case of well cave-in, the well shall be recommended for abandonment. Drilling a new well with a proper design is recommended instead.

#### 2.2.5 Dirty Water Yields

If well yield is dirty, the well shall be abandoned after plugging with cement.

If the well is intended for rehabilitation, at first, the existing pumping unit shall be pulled out, and then TV camera shall be lowered into the well in order to detect the formation with dirty water intrusion. Fine sand shall be charged into the well beneath the formation by using triplex mud pump and drilling pipes. After that, cement milk shall be charged from top of the sand to ground level with the use of drilling equipment, such as triplex pump and drilling pipes, in order to shut off or plug the dirty water intrusion zone. One day later, the cement milk shall harden, and the cementation remaining inside the well shall be cut by using tricone bit. The sand shall also be removed by the tricone bit and drilling mud. But this work is very difficult, and



it is costly to shut off the dirty water intrusion zone completely, so that wells yielding dirty water shall be recommended for abandonment. Drilling a new well with a proper design is recommended instead.

#### 2.2.6 Drying Up of Wells

If a well dries up and yields little amount of water, the well shall be abandoned after plugging with cement.

If the well is intended for rehabilitation, at first, the existing pumping unit shall be pulled out, and the well shall be drilled deeper in order to penetrate a confined aquifer. Some wells have iron plate attached to the bottom of casing pipes or have reduced casing pipe diameter at the bottom. In these cases, the well shall not be drilled any more.

If wells can still be drilled deeper, casing pipes with screens shall be installed at the deeper drilled position, gravel shall be placed surrounding the well screens, and cement grouting shall be carried out at the upper formation to protect the well from sand, gravel or clay intrusion or dirty water intrusion. But this work is very difficult, and it is costly to drill deeper and to shut off completely the upper formation by cement grouting, so that the wells, where the water level has reached almost the bottom of the well, shall be recommended for abandonment. Drilling of a new well with a proper design is recommended instead.

### 3. MAINTENANCE OF WATER WELLS AND SUBMERSIBLE PUMPS

#### 3.1 WATER WELLS

##### 3.1.1 Scope

A number of factors, including hydrogeologic conditions, well design and construction, and operational procedures, combine to determine the necessity, frequency and success of well maintenance. Any viable program of well maintenance must be founded on an understanding of these factors.

Aquifer characteristics and water quality parameters play a major role in determining maintenance requirements. If these basic hydrogeologic considerations are not considered during well design, or if actual well construction is faulty or inadequate, well failure is likely to result, giving rise to the need for frequent, costly and often extreme well maintenance measures.

Effective well maintenance programs rely on accurate, detailed record keeping. Records should contain up-to-date information on well conditions such as yields, drawdown and specific capacity. These data are derived through various well testing procedures.

The results of well testing provide essential information that can be used to determine if and when maintenance is needed. Test results additionally suggest the nature and extent of maintenance required.

### 3.1.2 Manual of Well Maintenance

#### (1) Keeping of Construction Records

Like water well drilling, well maintenance procedures have, until now, been considered a well driller's "art". Very little has been published about the nature of maintenance problems encountered by drillers, and even less about the techniques they use to solve these problems.

More has been published about the operation, inspection and maintenance of pumps because pump failure is much more common and is more likely to occur. Well failure, on the other hand, occurs much less frequently, and when it does, the decline is gradual-usually over a period of years. Sometimes well failure suddenly and unpredictably occur. An understanding of well maintenance problems and treatment techniques make this subject less of an art and more of a science.

It is important that only necessary work be performed on a well. Proper preventive maintenance of well will prevent expensive, unneeded work.

A comprehensive well maintenance program begins with proper record keeping at the time of well construction. The water well driller should provide the well owner with a copy of the well design, a geologic log,

and information regarding water quality, static water level, yield of the well, and pumping level. In addition, the contractor should keep a copy of this information for his own records. Too often such records are not kept by the contractor or by the well owner. Without such information, it is often difficult to recognize problems that can cause a reduction in well yield.

Well logging techniques are also useful in evaluating well maintenance needs. The information gathered from a geophysical survey or other logging technique can be compared to subsequent surveys to evaluate changes in formation porosity and permeability or damage to the well casing. Without preliminary well records and logging of a well that is performing poorly may require more time and more elaborate tests.

Well testing is also important to a timely and accurate evaluation of well maintenance needs. Measurements of well yield and specific capacity, in conjunction with logging techniques and accurate record keeping, will help ensure proper interpretation of a well's maintenance and rehabilitation requirements.

Many variables can cause a reduction in well performance. These include: pump damage or wear, well screen and casing corrosion or incrustation, incrustation of the producing formation, and structural failure of the well itself. These problems can often be traced to factors such as poor well design or construction or improper selection of pump materials.

There are, however, times when reduced well yield is not related to the well or the pump, but is instead the result of hydrogeologic conditions. These conditions may include reduced aquifer recharge, local overpumping of the aquifer, or interference from nearby wells. In addition, ambient groundwater quality is often a significant factor in well performance decline.

## (2) Record evaluation

No set of rules exist for determining when a well or pump will require major rehabilitation work. Such rehabilitation may be required every six months or every 10 years. But, rehabilitation work should be car-

ried out when the submersible pump will be pulled out of the well at the time of checking periodically or troubleshooting.

Many variables affect well performance, including well design and construction, pumping demand, and local hydrogeologic conditions.

As a result of these variables, operational records must be maintained in order to determine whether changes in well performance are due to problems in the power supply or pumping equipment, troubles within or adjacent to the well bore, or conditions within the aquifer surrounding the well. The frequency with which observations should be recorded varies according to the history of operation for a given well or areas. For high capacity units, the recording of different types of information is usually required on a daily, monthly or annual basis.

### (3) Daily records

Daily observations should be made of the quantity of water discharged and/or the discharge pressure.

Documentation of daily observations can often identify problems at an early stage, thus leading to relatively inexpensive solutions.

Variations in the turbidity, color and sand content of the water should be recorded daily. Turbidity and color indicate the presence of foreign substances, generally organic compounds and certain metallic ions. Sand should not be present in a properly constructed and developed well, but small amounts are often found in wells completed in sand and gravel aquifers. Large amounts of sand can fill the well screen, reduce well yield and cause excessive pump wear. Actual physical tests for these traits are preferred, but simple visual observations can be very helpful. By recording these observations, variations once thought to arise from normal operation can be linked to external sources such as rainfall, streamflow, or nearby pollutant discharge, and future problems can often be rapidly identified.

### (4) Monthly records

Pumping water level, discharge rate at the time of measurement and

static water level should be recorded monthly. It is preferable to measure the pumping water level in the production well with steel tape, electric sounder, or device of similar sensitivity. MWSS deepwells have no sounding tubes attached with riser pipes, water level can be measured hardly, because sounding wire sometimes trapped with the submersible cables. Sounding tube of 3/4 inch diameter should be installed inside the well when the submersible pump will be pulled out of the well at the time of checking the pump periodically or trouble shooting.

Discharge, or pumping rate, should be determined by metering equipment if possible. The importance of accurate metering cannot be over emphasized; without it, there are no reliable ways to make value judgments concerning production costs and operating efficiency.

Static water levels should be measured monthly. Changes in static water level may be the result of water storage depletion, seasonal fluctuations in water level, or changes in recharge conditions. These changes may be temporary or permanent, of regional or local extent. In many instances, problems thought to emanate from a production well have actually resulted from regional changes in static level; hence, maintenance would be completely ineffective. In this case, the setting of the existing submersible pump changed to a more deeper position.

If local water levels are controlled by a nearby surface recharge source such as river, the elevation of the source's surface should be measured and recorded with the discharge and drawdown measurements.

Measurements of drawdown should be taken monthly. As a rule, drawdown increases in all wells with continued production and advancing age. If the well is properly designed and pumped in proper relationship to its design, the drawdown should increase very slowly.

Aside from continued use and age, an increase in drawdown may result from well inefficiency or aquifer depletion. Well inefficiency may arise within the borehole, screen, or well due to particulate plugging, chemical corrosion, chemical incrustation, biological fouling or a combination of these conditions.

Aquifer depletion may caused by seasonal variations in water level or

when water withdrawals exceed recharge to the aquifer.

Determining whether increase drawdown is a function of well inefficiency or aquifer depletion is very important-well maintenance is only successful in the former case. Such a determination can be made by installing one or more observation wells in the aquifer outside the influence of the pumping well or wells. The comparison of changes in water levels of the pumping and nonpumping wells over a period of time will usually differentiate between lost well efficiency and aquifer depletion. Complete shutdown of production to allow the water level to return to its nonpumping or static state can provide comparable information.

#### (5) Yearly records

Water quality variations in alkalinity and hardness should be monitored on a yearly basis. Water can be aggressive, incrusting or both within a very small area. Hence, proper maintenance requires the identification of all water quality variations and the manner in which they may affect the well. The behavior of the well: static water level, pumping water level, discharge rate and etc. should be recorded monthly and analyzed on a yearly basis.

### 3.1.3 Establishment of Proper Well Design

Proper well design should be established to avoid well failure such as salty water intrusion, dirty water intrusion, well caved-in and drying up of well. Fig 4.1 and 4.2 shows samples of proper well design.

#### (1) Proper Well Design Along Coastal Area

Fig. 3.1 shows a sample of proper well design at coastal area to prevent salty water intrusion or "Well caved-in". A 22" diameter surface casing should be installed from 0.5-1 meter above ground level to 5-10 meters below ground level in order to protect from destroyed surface formation. Cement grout should be carried out in the clearance between 25" borehole and 22" surface casing pipe. 16" conductor pipe should be installed from 0.5-1 meter above ground level to 100-200 meters below ground level in order to prevent salty water intrusion or "well caved-in". The actual length of 16" casing pipes should determine the surrounding condi-

tions: lithology log, electric log and conductivity log.

Cement grout should be carried out in the clearance between 20" borehole and 16 "casing pipe.

8" casing pipe should be installed from 0.5-1 meter above ground level to 300 meters below ground level with wire wounded screen. Emplacement of gravel in the annular space between the 14" 1/4 diameter borehole and 8" diameter casing pipe from 10 meters above the top of the screen to the bottom of the well. Emplacement of sealing clay follows for about 20 meters from the top of the gravel packing followed by sand packing or cement grout from 5 to 10 meters below the ground level to the top of the clay seal. Cement should be poured from 0.5-1 meter above the ground level to the top of the sand packing or cement grout.

## (2) Proper Well Design for Another Area

Figure 4.2 shows a sample of proper well design for another area to prevent dirty water intrusion or "Dry up of well". A 22" diameter casing should be installed from 0.5-1 meter above ground level to 5-10 meters below ground level in order to protect from destroyed surface formation. Cement grout should be carried out in the clearance between 25" borehole and 22" surface casing pipe. A 16" diameter conductor pipe should be installed from 0.5-1 meter above ground level to 30-70 meters below ground level in order to prevent dirty water intrusion. The actual length of 16" casing pipes should determine the surrounding conditions.

Cement grout should be carried out in the clearance between 20" borehole and 16 " casing pipe.

8" casing pipe should be installed from 0.5-1 meter above ground level to 300 meters below ground level with wire wounded screen. Emplacement of gravel in the annular space between the 14" 1/4 diameter borehole and 8" diameter casing pipe from 10 meters above the top of the screen to the bottom of the well. Emplacement of sealing clay follows for about 20 meters from the top of the gravel packing followed by sand packing or cement grout from 5 to 10 meters below the ground level to the top of the clay seal. Cement should be poured from 0.5-1 meter above the ground level to the top of the sand packing or cement grout.

## 3.2 SUBMERSIBLE PUMPS

### 3.2.1 Product Specifications

See the name plate for the performance of the pump such as head (HEAD), discharge capacity (CAP), rotational speed (SPEED), voltage of the motor, current and the like.

Refer to the specifications. Do not use the pump beyond the limits of the specifications.

### 3.2.2 Installation

#### (1) Items To Be Checked Before Installation

- o Sealing liquid inside the motor: it is filled up when delivered from the factory. Check for any leak removing the pouring plug. If the solution should be short, replenish with clean water (equivalent to drinking water). Even when the solution was fully filled, shake a few times to assure there remains no air inside. Replace the plug securely after checking.
- o Measurement of insulation resistance: measure the insulation resistance between the ground and the motor cable (except power supply connected part) with the motor and the cable immersed in water. If the respective insulation resistance are 20 Mohm or more, there is no problem. When measuring, the core wire of the cable should be off the ground.

#### (2) Installation

Install the pump after completing the pumping test and the cleaning of the well.

##### 1) Position of the well strainer and the pump

Install the pump at the upper part of the well strainer without fail. If the well strainer is plural and the pump is to be installed between them, set the pump slightly lower from the middle



position. If the pump should be installed at the same position as the well strainer, it will suck a larger amount of sand leading to wear of the pump. On the contrary, if the pump is installed at the lower part than the lowest-positioned strainer, the area of dead water is generated around the outer periphery of the motor, and the motor might be damaged due to overheating, which should be noted. Sand and mud will be deposited gradually at the bottom of the well. Install the pump 20m or more from the bottom of the well so that the pump may not be buried.

## 2) Depth of submergence for the pump

The pump may be subject to failure when the external water pressure is 100m or more. Therefore set the position for installation so that the pump may not be submerged exceeding the specified value from the natural water level. The pump may be also damaged due to generated cavitation if the depth for submergence is not enough. Determine the fitting position of the electrode for low water level to provide the value more than the specified one in the outline drawing for pump in the gap between the lowest water level for operation and the upper end of the pump.

## 3) Caution during installation work

- o Handle the pump not to apply the bending moment to it when it transported and installed.
- o When the pump is lowered into the well, take care not to damage the cable by pinching it between the inner face of the casing for well and the flange for the drawing-out pipe.
- o The cable should be retained with the cable band and the like on the drawing-out pipe to avoid sliding down.
- o When the well is not straight and the pump may not be placed at the specified position, take an appropriate step such as changing the model of the pump not forcing to install.

#### 4) Piping on ground

- o The foundation area should not be thoroughly sealed but provided with smaller holes or gaps to remove the air.
- o The well cover must be mounted correctly and horizontally and secured with the anchor bolts.
- o Mount the check valve and the gate valve to the end of the discharge bend in this sequence.
- o Fit the automatic air vent valve and the coupling gauge to the discharge bend. The hose for the automatic air vent valve should be fixed by putting it into the hole of the well cover to avoid moving.
- o Tilt the coupling gauge to assure easy reading.

#### 5) Treatment of cable

Install the cable not to be exposed to sunshine in a windy state in order to avoid overheating of the cable taken out of the hole provided in the well cover. Take care that any longer cable kept bundled will cause overheating. In case two or more cables for electrode for low water level are mounted, wrapping color tapes for identification to the ends will be helpful.

### (3) Electrical Wiring

Concerning the power source unit for the motor and wiring work, they should be conducted correctly in accordance with the technical standard for electrical facilities and provisions for internal wiring. Any incomplete wiring, grounding (earth) and the like by unqualified person are not only very dangerous but constituting a breach of law, which should not be done absolutely.

If the submersible cable is connected, do contact the service men of the pump maker, for it is required to carry out the predetermined work with specified connecting kit.

For a single-phase model refer to the wiring diagram on the reverse side of the door for the control panel.

#### (4) Grounding

The grounding shall be arranged in accordance with such regulations as "Grounding work of the 3rd class" or "Special grounding work of 3rd class" for safety using tightening bolts for piping on ground or anchor bolts.

#### (5) Circuit Breaker

The user is required to mount the circuit breaker by law to prevent the worst case of electrification accident.

#### (6) Motor Protective Device

For the use of the control panel of the pump maker, the motor protective device (detection and protection of overcurrent, open-phase, and chattering) is adjusted beforehand.

When any control panel is provided by user, adjust the sensitivity of overcurrent and open-phase etc. conforming to the pump.

### 3.2.3 Operation

#### (1) Before starting the pump

- (a) Measure the insulation resistance again after the installation work as been completed. If the reading is 20 Mohm or more immediately after the installation, there is no problem.
- (b) Check whether the water level in the well is sufficient. Never operate the pump dry, for it may cause the pump to burn out.
- (c) Check the state of the primary power source, the electrical wiring, capacity of the breaker and the present value for the over-current protective relay.

**(2) Test Operation**

- (a) Open the gate valve fully before turning on the switch.
- (b) Turn the switch on and off one or two times to check its normal start (provided however once the switch has been turned off, interval of three minutes or more should be kept before the next start).
- (c) Check the rotational direction of the pump when no abnormal start has been found. Higher shutoff pressure and lower current represent the correct direction when the pump is operated.

The reverse rotation will show not only lower shutoff pressure but also generate sudden rise in current as the gate valve is gradually opened. Change the wiring to provide the correct rotation when it is reverse. (in this case the shutoff operation time shall be ten minutes as maximum).

- (d) Open the gate valve one-half to one full turn under the correct rotation and operate for a while. Open the gate valve gradually when the water discharged becomes clear. If it is opened too quickly, the pump may clog with sand.
- (e) When the discharge amount reaches the specified valve, check the pump whether the total head (water level in the well + pressure on ground + piping loss) and current value are closely near those in test results. If any imbalance of current is found in each phase, there is no problem when the maximum value is within + 5% of the current value stated on the nameplate. Also check any abnormal vibration and/or noise.
- (f) The test operation will be completed when no abnormality is found. But check no severe water hammer is generated in this case.

**(3) Regular Operation**

Regular operation can be started as soon as the test operation has been completed.

- (a) Be sure to operate the pump (discharge volume) within the "suitable operation range". In case it is operated beyond the range, adjust the gate valve.
- (b) Do not open and close valves once they have been adjusted. Establishment of the pumped water volume will prolong the well life.
- (c) Keep the cock of the coupling gauge closed other than the measuring time. If this is kept open, it may cause frequent failure.
- (d) Suitable operation range of pump

Set the discharge volume so that it may be between the first main point and the second main point in the right figure. Too smaller discharge volume will cause overheating of motor and may lead to burning out, while too larger discharge volume may be cause for vibration and troubles such as failure of bearings.

- (e) Number of starting of pump operation per hour were shown below.

Output of motor (kW)	Number of start per hour
-----	-----
7.5 or less	Within 12 times
11 - 22	Within 6 times
26 - 45	Within 4 times
Starting time	3 minutes or more after stop

#### 3.2.4 Maintenance

Check pressure, discharge volume, voltage, current, insulation resistance and others. If these are found to be different from normal ones, it will represent the sign of troubles. Take earlier action referring to the cause and remedy for troubles in the troubleshooting section

3.2.5. Preparation for a spare pump is recommendable for the worst case.

(1) Daily Inspections

Daily inspection shall be made as follows. Recording the data measured at inspection in "Records for Operation Management" will serve as the reference data in prediction of life of the pump and catching the state of the well.

If the facilities are critical ones, inspect more often than this.

(a) Check of current value: once a day

Measure the current value and check whether it is closely near the value shown during the test operation. Also check fluctuation of current, imbalance of three-phase and voltage simultaneously.

(b) Check of discharge volume: once a week

Where any flow meter is mounted, check if the discharge volume is very near the value shown during the test operation for total head.

In case of flow meter is provided, measure the total head during the shutoff operation as necessary (once a month approximately) and check whether the value is closely similar to that seen during the test operation.

(c) Check of vibration resistance: once a month

Check whether any abnormal vibration and/or noise are produced in pump.

(d) Check of insulation resistance: once a month

Pump can be operated when the insulation resistance shows 1 Mohm or more. If the value shows sudden decrease, take every care such as by shortening interval of measurement and taking other steps.

(e) Check of water level in well:

Measurement and recording of the water level in the well will form the data for state of well and serve as reference data to predict the well life.

(2) Records for Operation Management

Recording the data measured at daily inspection in the records for operation management as the table shown below will serve as a reference data to predict the life of the pump and catch the state of the well.

Pump for deep wells		:Mfg. No. of pump:	
Records for operation management		: Model of pump:	
Well dia:	mm	:Water level for	:
:	:	operation	m:Main spec. of pump:
Well depth:	m	:Installed position	:
:	:	:of pump	m:Rated current:
Date/	:Pumping	:Discharge:Discharge:	:Insulation:
Time	:water level:	pressure : volume	:Voltage:Current:resistance: Note
:	(m)	(kg/cm) : (m/min)	(V) : (A) : (Mohm) :
:	:	:	:
:	:	:	:
:	:	:	:

(3) Overhaul

(a) The first overhaul is recommended to be done one to two years later after starting the operation. The time of the second overhaul should be determined upon the inspection results of the first overhaul. The same procedure shall be applied to the third overhaul and hereafter. The time of the first overhaul shall be

judged depending on importance of the facilities, hardness of the operation, the water quality and other factors.

#### Installation and start of operation

The first overhaul     one to two years later

The second overhaul    To decide on results of the first overhaul  
                          (five years as max.)

The third overhaul     To decide on results of the second overhaul  
                          (five years as max.)

- (b) Another opportunity to overhaul is provided by finding out any sign of troubles through assuming the deterioration progress of the pump from the water level of pump, discharge pressure, discharge volume, current value, insulation resistance and others measured at daily inspections. In this case, the data shall be provided from the continuous measurement as possible to catch the deterioration progress easily.
- (c) When the damaged pump is taken out to repair without overhauling in management, it is advisable to prepare a spare pump, by which the spare pump can be installed without any delay after the pump was damaged to minimize the influence over the pumped water plan. The damaged pump can be stored as a spare pump after repair and inspection.

#### (4) When Operation is suspended

When the operation is suspended for a long time or the pump is installed as a spare pump, operate it for about ten minutes once a month. The operation should be started in accordance with the section 3.2.3.

#### (5) Storage of Pump

The following point should be taken care when the pump is stored for a long time without installation. If the use is required after storage. Follow the section 3.2.2 for installation and then the section 3.2.3 to



start the operation.

- (a) Store the pump where there is no direct sunshine and no higher temperature and humidity.
- (b) Remove any water inside the pump and dry it thoroughly, but, do not remove the water inside the motor.
- (c) Apply taping to the ends of cable to avoid water.
- (d) Put a cover on the pump not to cause any failure to the motor and the cable.

### 3.2.5 Trouble Shooting

Trouble	Cause	Remedy
Does not start.	:Wiring disconnected or cut.	:Repair or replace.
Start, but immediately stops.	:No power. :Dry operation prevention : electrode or pressure : switch etc. damaged. :Not connected well. :Voltage drops (10% or more). :Circuit breaker functioning. : :Pump or motor locked. :Magnet switch flutters. :Motor burned out. :	:Contact power company. :Replace. : : :Connect correctly. :Contact power company. :Repair or replace point : of short circuit. :Remove pump and repair. :Replace. :Remove pump and repair :or replace
Overcurrent during operation.	:No connected well. :Voltage drops (10% or more). :Pump clogged with sand. :Pump or motor shaft worn.	:Connect correctly. :Contact power company. :Clean the well. :Remove and repair.
No water.	:Pump exposed.	:Lower pump position.

	:Faulty connection.	:Connect correctly.
-----		
Rated flow not provided.	:Inside of pump worn. :Hole in piping.	:Replace worn parts. :Repair.
Not enough discharge.	:Hole in piping. :Scales inside piping. :Foreign matter clogged in : impeller or casing. :Foreign matter clogged in : pump strainer. :Gate valve damaged. :Water level extremely low. : :Not connected well.	:Replace. :Remove scales and clean. :Remove, disassemble and : clean. :Remove, disassemble and : clean. :Repair or replace. :Replace with a pump hav- : ing higher total head :Connect correctly.
-----		
Low Insulation resistance	:Motor deteriorated. :Motor burned out. :Submersible cable damaged. :Water leaking into : connection of cable under : water.	:Replace motor. :Replace motor. :Remove and repair. :Remove and repair. : :
-----		
Vibration & Noise	:Water hammer in piping : above ground. :Gate valve closed too far. : :Built-in check valve damaged. :Pump worn.	:Take countermeasure to : prevent water hammer. :Increase opening of : gate valve. :Remove and repair. :Remove and repair.
-----		

Figure 1.1 REGIONAL DECLINING OF WATER LEVEL

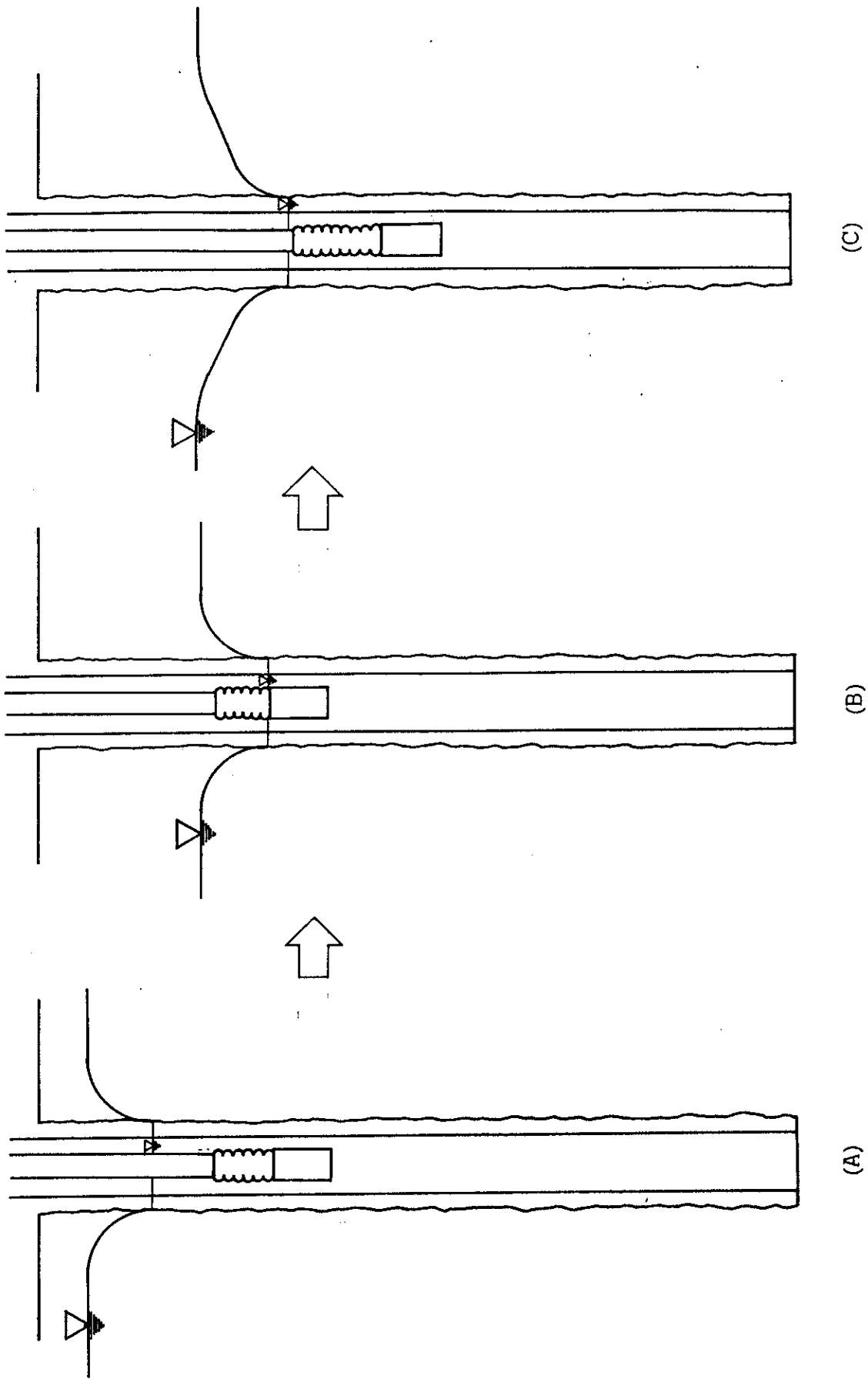


Figure 1.2 SALTY WATER INTRUSION

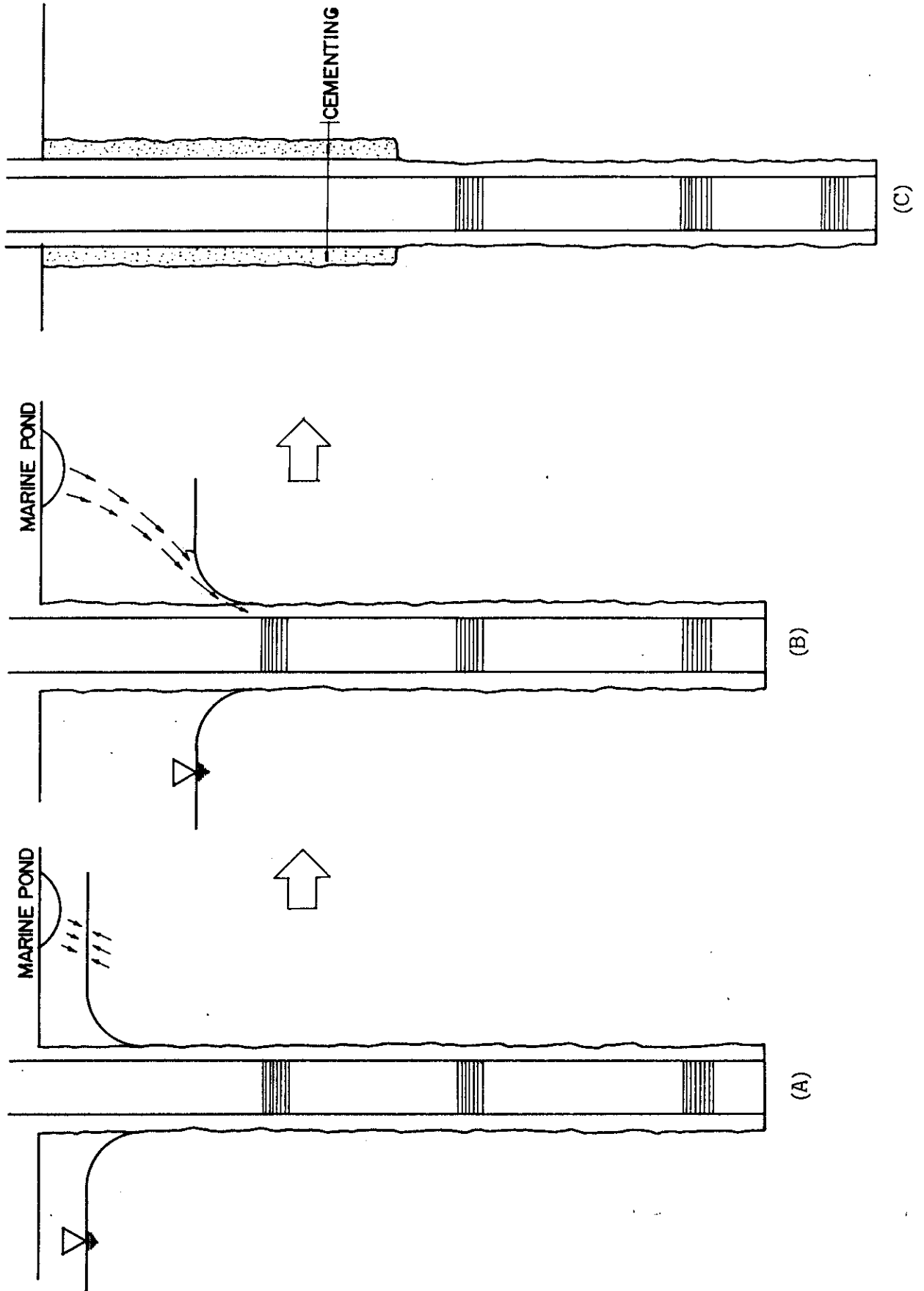


Figure 1.3 WELL CAVED-IN

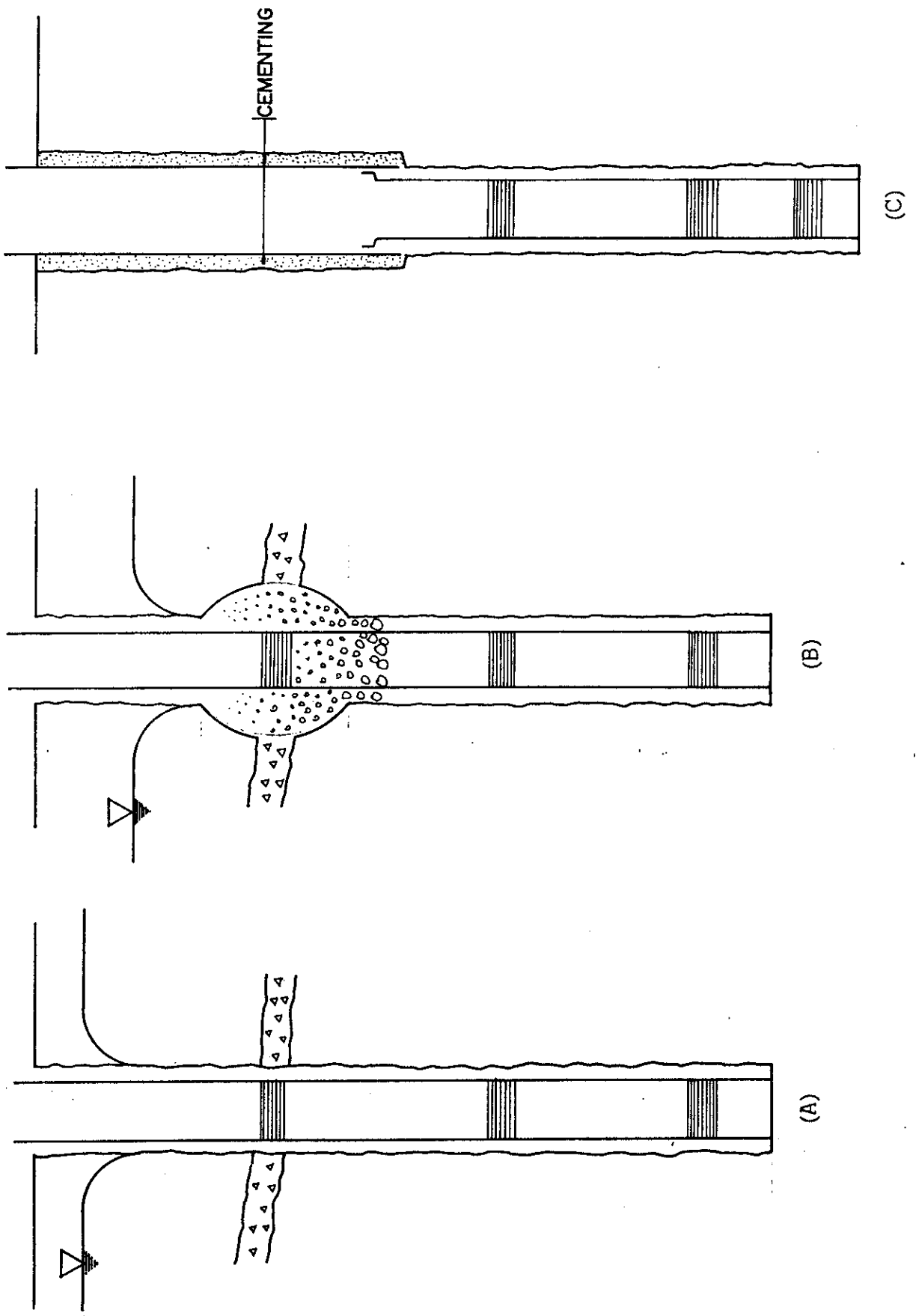


Figure 1.4 DIRTY WATER INTRUSION

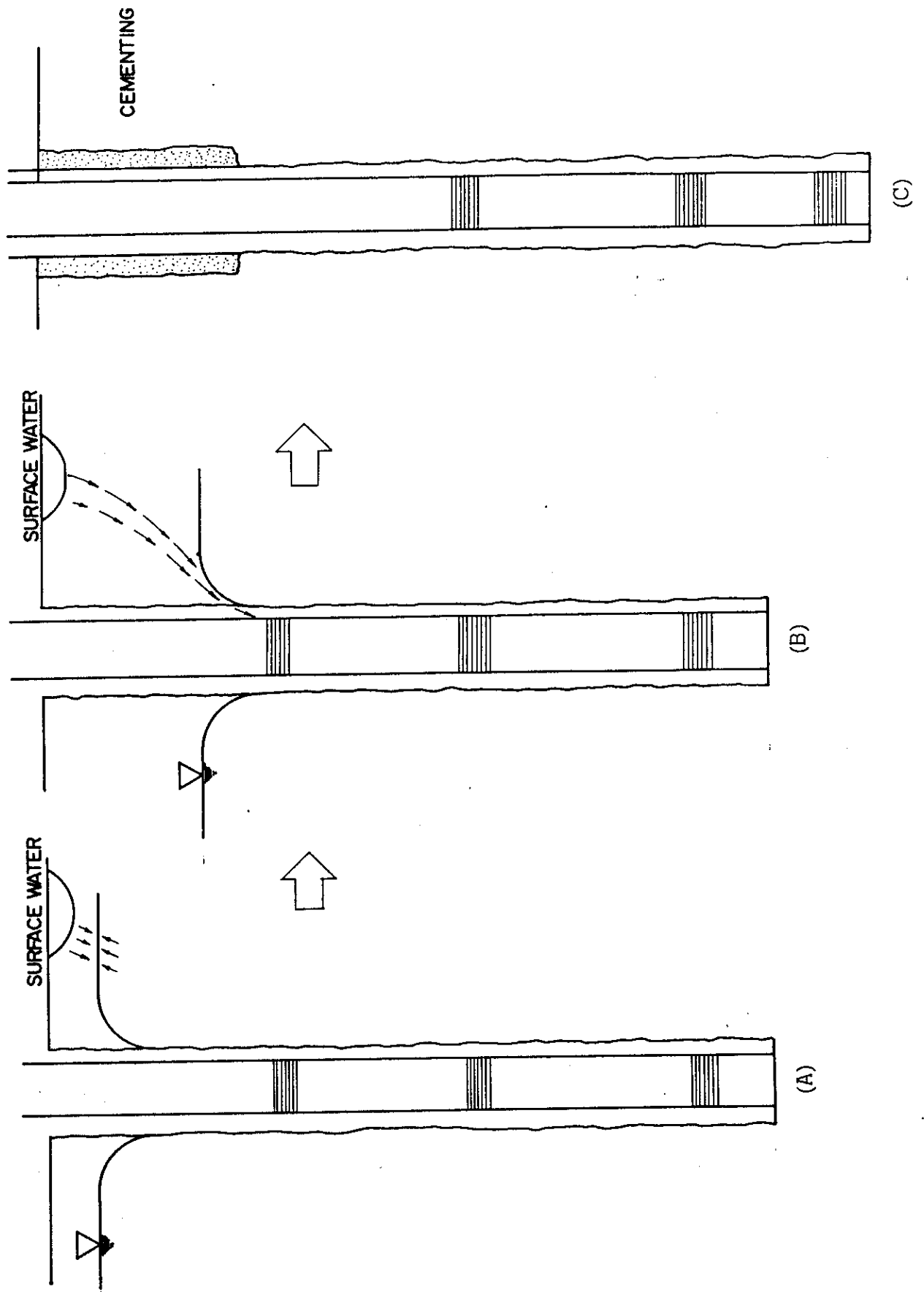
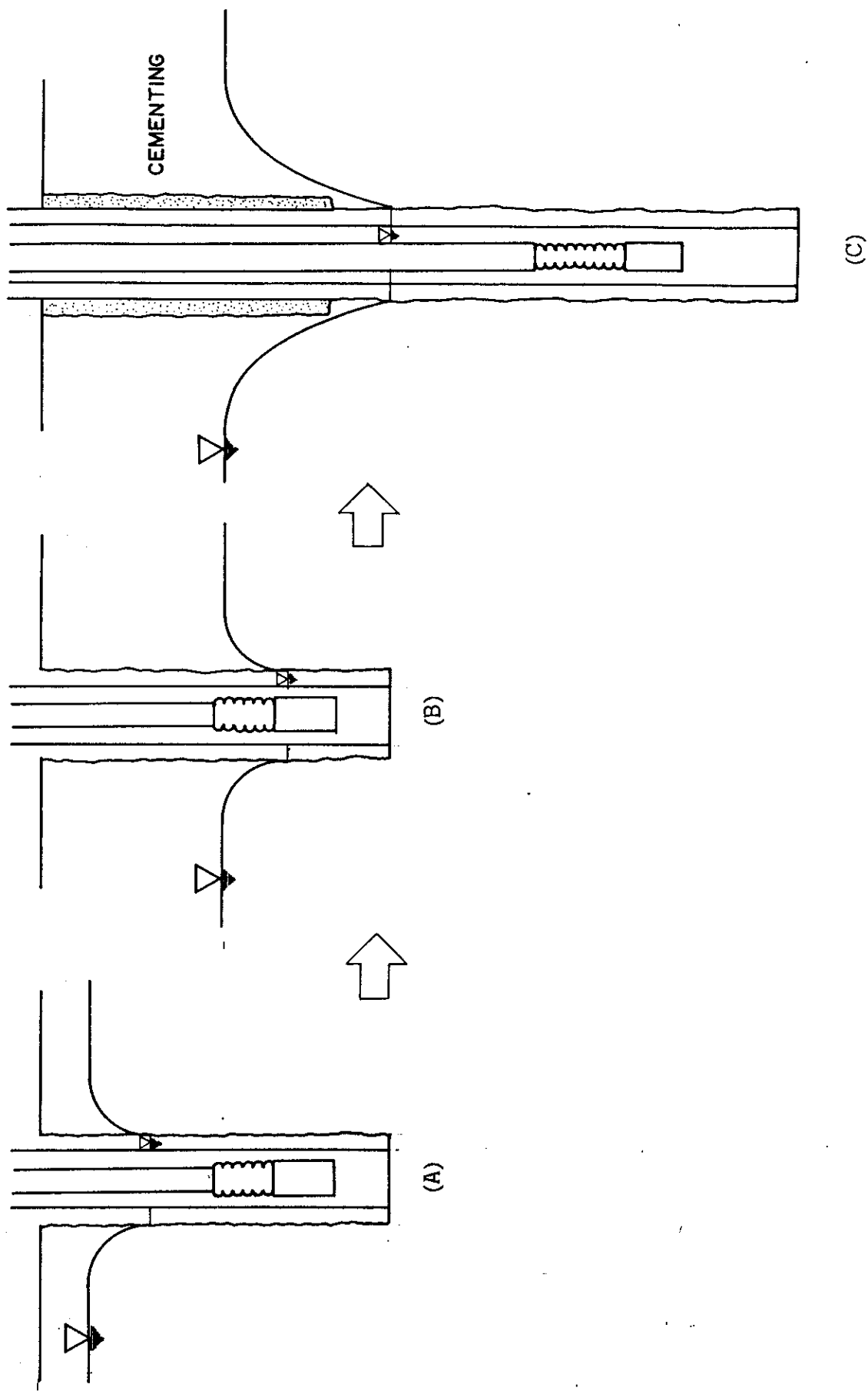


Figure 1.5 WELL IS ALMOST DRY



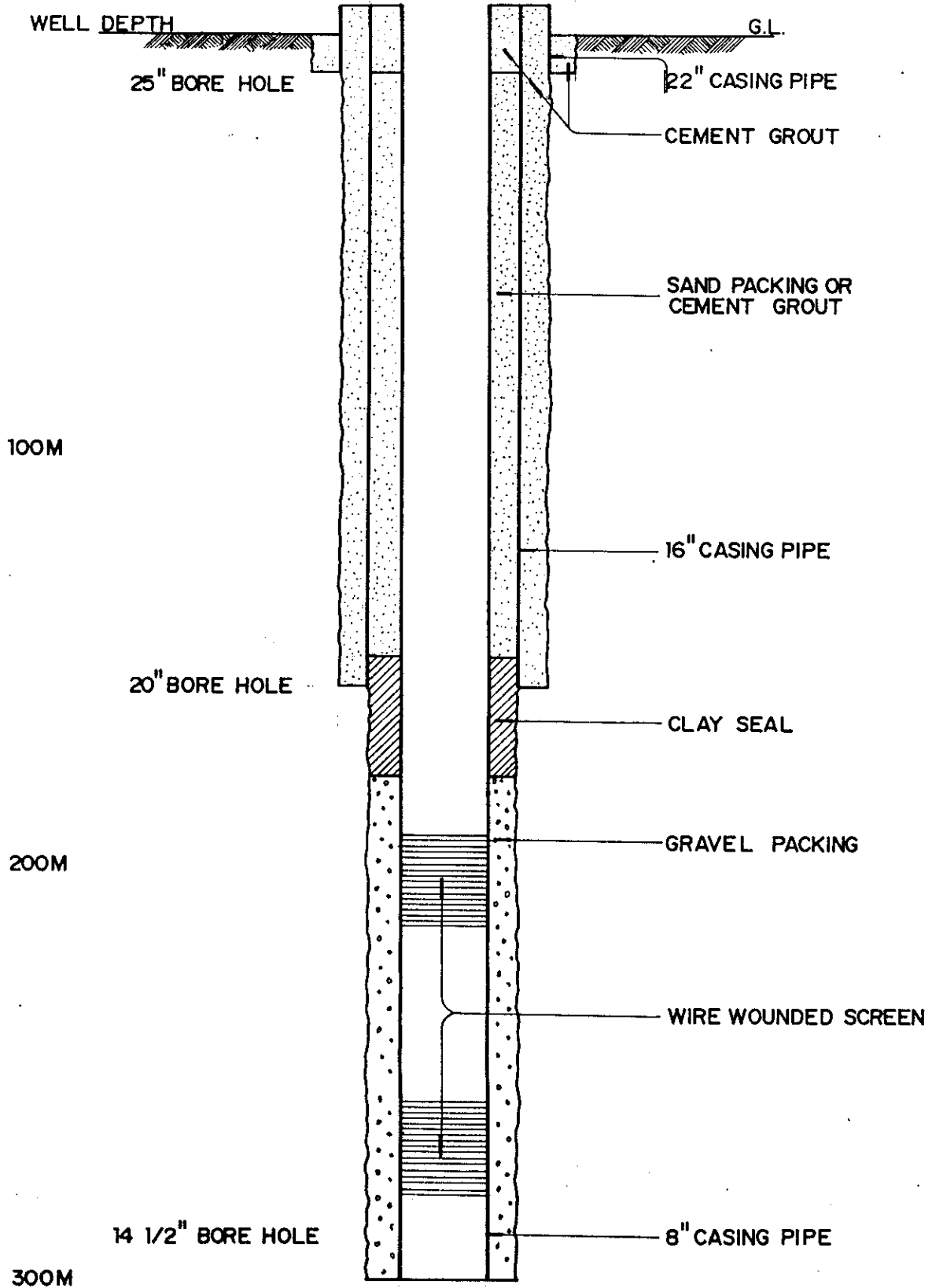


Figure 3.1 PROPER WELL DESIGN I



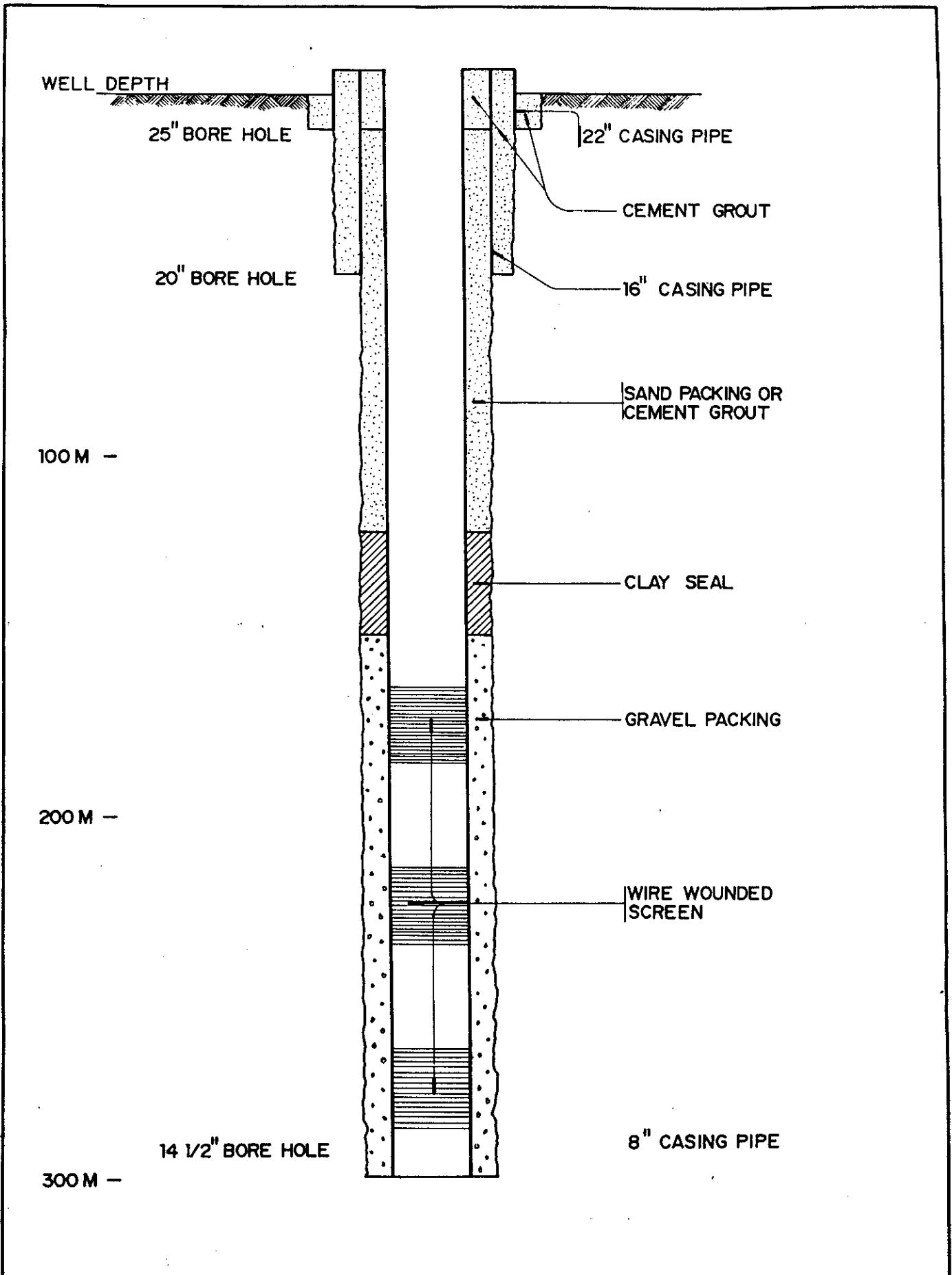


Figure 3.2 PROPER WELL DESIGN II

JICA

REPUBLIC OF THE PHILIPPINES  
METROPOLITAN WATERWORKS AND SEWERAGE SYSTEM

STUDY FOR THE GROUNDWATER DEVELOPMENT  
IN  
METRO MANILA

GROUNDWATER DATABASE SYSTEM  
USER'S MANUAL

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# GROUNDWATER DATABASE SYSTEM

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## GROUNDWATER DATABASE SYSTEM

The Groundwater Database System aims to support the groundwater development and conservation program of the Metropolitan Waterworks and Sewerage System (MWSS). The system was designed to facilitate the retrieval of necessary information from the database as well as the inputting of data directly (from the source document) into the computer.

The system is composed of five databases containing the following information:

- o well inventory data
- o meteorological data
- o hydrological data
- o hydrogeological data
- o related literature records.

## HARDWARE REQUIREMENT

The system runs on IBM PC/AT or any similar compatible micro-computer system whose configuration is characterized by the following:

1. A memory size of at least two megabyte (MB) -- without the graph, the system needs only at least one megabyte
2. With at least one 3.5" (and 5.25") floppy disk drive
3. With hard disk of at least 40 megabytes storage capacity
4. With DOS 3.3 or higher
5. A printer similar to Epson FX-1000.

## SOFTWARE REQUIREMENT

The system was designed to be user-friendly and has a program named WELL. It was developed specifically for the system to hide the complexity of the database internal structures and procedures.

The system utilizes Lotus-123 (Release 2) software for the graphs.

```

+-----+
| IMPORTANT:                                     |
|                                               |
| CONFIG.SYS installed in the computer must   |
| contain FILES=100 (or more); otherwise the  |
| Groundwater Database System will not run.   |
+-----+

```

## LOADING THE SYSTEM

1. From the root directory, create sub-directory MWSS

C:\>MD MWSS                      and press the <Enter> key

2. Enter sub-directory MWSS

C:\>CD MWSS                      and press the <Enter> key

3. Copy the programs, data file structures and other support files stored in three 3.5" diskettes. Diskettes #1, #2, #3 are program diskettes. Diskette #4 contains the data file structures (Appendices A.1 to A.5).

- Insert Diskette #1 in Drive B and copy all the contents.

C:\MWSS>[path]XCOPY B:/s            and press the <Enter> key

XCOPY is a DOS 3.3 command. [path] indicates the drive and/or sub-directory where the DOS commands are stored or where the command XCOPY is to be called.

- After copying Diskette # 1, insert Diskette # 2, copy the contents, and so on until all diskettes have been copied.

## STARTING THE SYSTEM

After the successful loading of the program WELL and the data file

structures, the user can gain access to WELL by following the instructions below:

1. Activate the WELL program from sub-directory MWSS.  
C:\MWSS>WELL and press the <Enter> key
  - Screen 1 is displayed.
2. Press any key to continue.
  - The Main Menu appears on the screen. The user can choose from any of the five modules comprising the system (Screen 2).
3. Type the letter corresponding to the module to be chosen and press the <Enter> key to activate the selected module.
  - W for well inventory data, M for meteorological data, H for hydrological data, G for hydrogeological data, and L for literature records.
  - A message "Please wait... setting up the files" is displayed onscreen.

#### ENDING THE SYSTEM

Pressing the Esc key allows the user to go back to the previous screen. When Screen 2 appears, no module is active.

#### WELL INVENTORY DATABASE

Well inventory includes MWSS-supervised wells and turned-over deep wells, private wells applying for water rights from NWRB, wells inventoried during the Electrowatt project, wells from MGB (NWRB's countrywide inventory of existing wells), wells visited during the groundwater use survey and groundwater levelling, test wells drilled during the JICA study, wells inventoried in NWRB's Philippine Groundwater Summary, and



wells from drilling companies.

The data file structures and coding instructions for well inventory are described in Appendix A.1.

When this module is activated, Screen W1 is displayed onscreen and the list of wells is shown. The user can browse through the list and select the desired well for more detailed information. In the Edit mode, the user can make changes on the data shown in Screen W1.

A. To browse data in Screen W1.

The user can browse through the list of wells by using the command keys described in Appendix B. In this "display" mode, the user can also print the data by location.

To print, press F4.

The system will prompt:

SET THE PRINTER ON (in condensed mode)... Press any key when ready

Pressing any key except Esc key (cancels the print option), readies the user for printing. The system prompts for the location code.

LOCATION CODE: \_\_\_

The user responds by typing the location code (See Appendix A.1). If valid, the location name appears beside the code. If not, a message appears onscreen:

"INVALID CODE... Please try again"

Pressing the Esc key aborts this option.

B. To edit data in Screen W1.

- Press F5.

The screen changes to the Edit mode and some of the data previously displayed are changed to codes. In this mode, the user can select the data item to be edited, add new record(s), delete record(s), print information displayed on the screen and/or extract data from the database for further processing (see Appendix B).

C. To obtain more detailed information about the selected well:

1. Be sure Screen W1 is in the "display" or "browse" mode.
2. Select the desired well.

There are two ways of selecting the desired well:

- a. By positioning the highlighted bar to the desired well.
- b. Pressing Shift-F2 (Shift key + F2 key simultaneously).

When Shift-F2 is pressed, the system prompts:

```
WELL CODE ==> _____
```

The user responds by typing the code of the desired well. (Pressing the Esc key aborts this option.) If the code is mistyped or not available, the message below appears onscreen:

```
" << WELL CODE not found... Please try again >> "
```

After the code has been accepted, the highlighted bar immediately goes to the record of the selected well.

3. Press F3.

Screen W2 appears and displays the basic information about the well. At the bottom, there are command options to choose from.

- Press the left or right arrow key to move from one option to another. The active option is the one with the highlighted bar.
- Press the <Enter> key to activate the command.

Command options:

    Edit - allows the user to modify the data items displayed on the screen. Data items that are selected for editing are highlighted. The user can traverse through these fields and make some modifications. The <Esc> key returns the cursor to the command mode.

    Print - allows the user to get a hardcopy of the displayed information.

    Quit - exits the user to the previous screen.

The box at the right-hand bottom corner of Screen W2 contains more information about the well -- Well Design, Log Record, Pumping Test and Well Production (for MWSS wells only). To enter this section,

- Press the right arrow key until the highlighted bar reaches the desired information inside the box.

    Design - allows the user to enter Screen W3  
    Log Record - allows the user to enter Screen W4  
    Pumping Test - allows the user to enter Screen W5  
    Production - allows the user to enter Screen W6.

- Press the <Enter> key to select.

## Well Design

Screen W3 displays the Well Design. There are command options (Edit, Print, Quit) at the bottom of the screen whose functions are similar to Screen W2.

Information on the casing schedule or well screen section can be displayed by choosing any of the two options located at the bottom right-hand corner of the screen.

1. Press the right arrow key until it reaches the box at the bottom right-hand corner of the screen.

Screen Section - allows the user to enter Screen W3.1.

This contains information about the well screen section.

Casing Schedule - allows the user to enter Screen W3.2.

This contains information about the well casing.

2. Press the <Enter> key to select.

When in Screen W3.1 or Screen W3.2, the user can either browse through the list, add new record(s), delete record(s), edit, print information displayed or extract data using the command keys described in Appendix B.

## Well Log Record

The Well Log Record describes the well strata (Screen W4). The user can either browse through the records, add new record(s), delete record(s), edit, print information displayed or extract data using the command keys described in Appendix B.

## Pumping Test

Screen W5 gives the result of the pumping test. There are command options at the bottom of the screen whose functions are similar to that of Screen W2.

## Production

Well production data are available only for MWSS wells. Monthly pumpage is measured in cubic meters and yearly data are automatically generated by the system.

To choose from monthly and yearly data, press the right or left arrow key to move the highlighted bar to the desired data and then press <Enter> key to select.

Screen W6.1 displays the monthly data while Screen W6.2, that of the yearly data.

## Editing and Extracting Data

-----

Editing is accepted only when monthly data is requested. User can add, modify or delete records. Command and function keys available for editing as well as extracting data are described in Appendix B.

## Updating

-----

To update yearly data:

- Press F8.

A message appears onscreen: **\*\*\* UPDATING \*\*\***

The system (re)computes the annual data.

## Mean and Standard Deviation

-----

To request for the mean and standard deviation:

1. Be sure the screen is in Screen W6.1 or W6.2.
2. Press F9.

The system prompts for the years (e.g. 1980) covered (Screen W6.1.1).

3. After supplying the years, press the <Enter> key.

A message "\*\*\* COMPUTING \*\*\*" appears at the bottom left corner of the screen.

After a while, the mean and standard deviation, will be displayed.

4. To print the mean and standard deviation, press F4.

## Graph

-----

Graph can be requested while in Screen W6.1 or Screen W6.2. This option makes use of Lotus' graphing capability.

1. To activate the graph, press F10.
2. Type-in the years (e.g. 1980) to be graphed and press the <Enter> key.

The system activates Lotus 123.

Within Lotus 123:

- Select the type of graph -- Linear or Bar graph.
- Select End to quit.

The system returns to Screen W2.

## METEOROLOGICAL DATABASE

The meteorological database contains the daily, monthly, and annual records of rainfall, temperature (mean, minimum and maximum), evaporation, humidity, wind velocity and sunshine duration measured from meteorological stations. The codes and the data file structures used in this database are described in Appendix A.2.

When this module is activated, Screen M1 is displayed onscreen and the list of meteorological stations is shown. As in Screen W1, the user can browse through the list, print, and select the desired station for more detailed information. In the Edit mode, the user can make changes on the data. The user can also extract data from the database.

Command options and function keys necessary for selecting, editing, adding, deleting, printing and extracting of data are similar to those in well inventory database.

Screen M2 displays the basic information about the selected station. Data being observed -- rainfall, temperature, evaporation, humidity, sunshine duration and wind velocity -- are listed at the bottom right-hand corner of the screen. Choosing any of these data items, brings the user to Screen M2.1 for daily data, Screen M2.2 for monthly data, or Screen M2.3 for yearly data.

The user can input and/or modify existing data for daily observations only. To display the data, the user has to move the highlighted bar from any of the desired frequency of measurement -- Daily, Monthly, and Annual -- and press the <Enter> key to select.

If Daily data is requested, the system prompts for the desired YEAR (e.g. 1989). If the desired YEAR is not available, the system displays message onscreen:

YEAR is not available... Want to input data (Y/N)?

If Y(es), the system automatically generates blank fields for the YEAR and DAY. Command and function keys for editing, adding, deleting, printing and extracting data are described in Appendix B. YEAR and DAY cannot be altered.

Monthly and yearly data are automatically computed by the system. No editing can be done when these data are requested.

Function keys for updating data, requesting for mean, standard deviation and graph are similar to those described in well inventory database (well production section).

#### HYDROLOGICAL DATABASE

The hydrological database provides information about the hydrological gaging stations as well as the daily, monthly, and annual continuous observations on the river discharge and gage height measured from the said station. It also contains the simultaneous observations on spring discharge and streamflow in the Antipolo area. The data file structures and codes used in this database are described in Appendix A.3.

The first screen (Screen H1) of the database provides the user with two options for hydrological observations -- Simultaneous and Continuous.

To select the desired observation:

- Move the highlighted bar to the desired observation -- Simultaneous or Continuous.
- Press the <Enter> key.

Either Screen H2 (simultaneous observation) or Screen H3 (continuous observation) appears on the screen with the list of hydrological stations. The user can either browse through the list, print or extract data.

To obtain detailed information:



- Press F3.

Screen H2.1 or H3.1 is displayed showing the basic information about the hydrological station and the data being observed for each station.

- Move the highlighted bar to the desired data -- spring and streamflow discharge or river discharge and gage height -- located at the bottom right-hand corner of the screen and press the <Enter> key.

Either screen for simultaneous observation -- Spring Discharge (Screen H2.1.1) and Streamflow Discharge (Screen H2.1.2) -- or, for continuous observation -- River Discharge (Screens H3.1.1 to Screens H3.1.3) and Gage Height (Screens H3.1.4 to H3.1.6) -- is displayed.

Command keys and function keys for selecting, modifying, printing and extracting of data are similar to those in well inventory database.

Graph as well as mean and standard deviation are provided for data on hydrological continuous observation. Function keys are similar to those in Meteorological Database.

#### HYDROGEOLOGICAL DATABASE

The hydrogeological database contains data only of those wells tested and measured during the actual test drillings, rehabilitation studies, pumping test and groundwater quality investigations of wells. The data file structures and codes used for the database are described in Appendix A.4.

When activated, the list of wells is displayed (Screen G1). Like Screen W1 and Screen M1, the user can browse through the list and select the desired well for more detailed information.

After the desired well is selected, Screen G2 appears with five options for the user to choose from -- pumping test data, groundwater level

(continuous and simultaneous observation), chemical and physical quality of water. The option Pumping Test brings the user to Screen G3, Groundwater Level (continuous) to Screen G4.1 to G4.3, Groundwater Level (simultaneous) to Screen G5, Chemical Quality of Water, to Screen G6 and Physical Quality of Water to Screen G7.

Command options and function keys for selecting, modifying, printing and extracting of data are similar to those in the well inventory database.

Graph as well as mean and standard deviation are provided for the Groundwater Level Continuous observation data. The function keys are similar to Meteorological database.

#### LITERATURE DATABASE

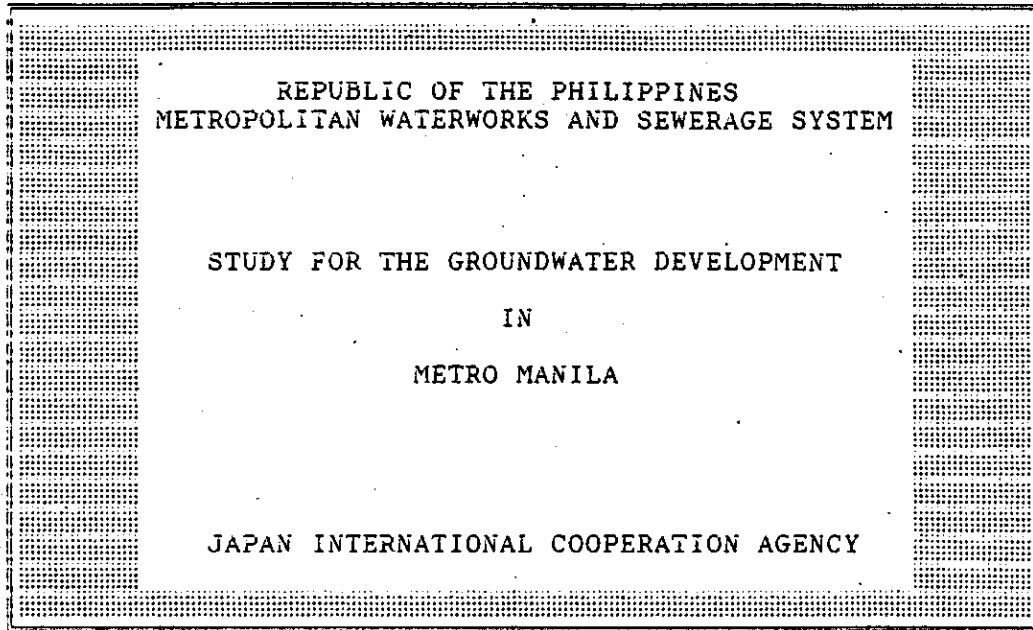
The literature database provides literature records relevant to the groundwater development study. The data file structures and codes used are described in Appendix A.5.

When this module is activated, Screen L1 is displayed. There are command options at the bottom of this screen whose functions are the following:

- Edit - allows the user to modify the data items displayed on the screen. Data items that are selected for editing are highlighted. The user can traverse through these fields and make some modifications. The <Esc> key returns the cursor to the command mode.
- Previous - displays the record preceding the record currently displayed.
- Next - displays the next record.
- Print - allows the user to get a hardcopy of the displayed information.
- Quit - exits from the database.

**SYSTEM SCREEN DESIGNS**

Screen 1



Press any key to continue...

Screen 2

REPUBLIC OF THE PHILIPPINES  
METROPOLITAN WATERWORKS AND SEWERAGE SYSTEM

Date: 08/27/91

DATABASE ==>

- W ...well inventory data
- M ...meteorological data
- H ...hydrological data
- G ...hydrogeological data
- L ...literature records

Choose...

C:\MWSS>

Screen W1

\*\*\* WELL INVENTORY DATA \*\*\*

Wcode	Location	Type	Well Name	Status

Screen W2

Well Code	Location	Type	Status
Well Name			
Well No. New	Old		
Owner: Present			
Former			
Well Address			
Ground Elevation		meters	
Map Sheet No.			
Coordinates:			
Latitude	° ' "		
Longitude	° ' "		
Driller			
Date of Completion	/ /	(mm/dd/yy)	
Groundwater Use			
Source of Data			

- Design
- Log Record
- Pumping Test

.. Edit... Print... Quit... ..

Screen W3

Well Code	Location	Type	Status
Well Name			

\*\*\* WELL DESIGN \*\*\*

Well Depth		meters
Diameter of Riser Pipe		centimeters
Rated Pump Capacity:	Old	LPS
	New	LPS
Total Dynamic Head:	Old	meters
	New	meters
Pump Setting:	Old	meters
	New	meters
Motor HP Rating:	Old	
	New	
Aquifer Type		

▪ Casing Schedule
▪ Screen Section

.. Edit... Print... Quit... ..



Screen W3.1

Well Code ■	Location ■	Type ■	Status ■
Well Name ■			

\*\*\* WELL SCREEN SECTION \*\*\*

Screen	Type	Diameter, in centimeters	Depth, in meters	
			From	To

Screen W3.2

Well Code ■	Location ■	Type ■	Status ■
Well Name ■			

\*\*\* WELL CASING SCHEDULE \*\*\*

Casing No.	Diameter, in centimeters	Depth, in meters	
		From	To



Screen W5

Well Code ■	Location ■	Type ■	Status ■
Well Name ■			

\*\*\* PUMPING TEST DATA \*\*\*

Static Water Level.....	Date ■	(mm/dd/yy)
After Construction ■	meters	/ /
Recent Measurement ■	meters	/ /
Pumping Water Level.....	Date ■	
After Construction ■	meters	/ /
Recent Measurement ■	meters	/ /
Actual Discharge.....	Date ■	
After Construction ■	LPS	/ /
Recent Measurement ■	LPS	/ /
Specific Capacity ■	LPS/M	
Transmissibility ■	M <sup>2</sup> /day	
Storage Coefficient ■		
Pumping Duration ■	hours.	
Type of Pumping Test ■		

.. Edit... Print... Quit... ..

Screen M1

\*\*\* METEOROLOGICAL DATA \*\*\*

S-Code	Station Name	Type	Status

Screen M2

Station Code	Type	Status
Station Name		
Location		
Responsible Agency		
Elevation		meters above MSL
River Basin		
Map Sheet No.		
Map Sheet Quadrant		
Coordinates:		
Latitude	° ' "	"
Longitude	° ' "	"
Years of Record	From:	To:
Time of Measurement		
Remarks		

DATA BEING OBSERVED

Rainfall	Humidity
Temperature	Sunshine Duration
Evaporation	Wind Velocity

•• Edit ... Print... Quit... ••

Screen M2.1

Station Code	Type	Status
Station Name		
Location		

RAINFALL ==>>>>  
in millimeters

Daily

Monthly

Annual

YEAR: 1989

YEAR	DAY	JAN	FEB	MAR	APR	MAY	JUN	JUL
1989	1							
1989	2							
1989	3							
1989	4							
1989	5							
1989	6							
1989	7							

Screen M2.2

Station Code ■	Type ■	Status ■
Station Name ■		
Location ■		

RAINFALL ==>>>>  
in millimeters

Daily

Monthly

Annual

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL

-----



Screen M2.3

Station Code. ■	Type ■	Status ■
Station Name ■		
Location ■		

RAINFALL ==>>>  
in millimeters

Daily

Monthly

Annual

YEAR	RAINFALL

Station Code •	Type •	Status •
Station Name •		
Location •		

TEMPERATURE in °C    ==>     Mean    Minimum    Maximum     Daily    Monthly    Annual

YEAR:    1989

YEAR	DAY	JAN	FEB	MAR	APR	MAY	JUN	JUL
1989	1							
1989	2							
1989	3							
1989	4							
1989	5							
1989	6							
1989	7							

Station Code ■	Type ■	Status ■
Station Name ■		
Location ■		

TEMPERATURE in °C ==>

Mean    Minimum    Maximum    Daily    Monthly     Annual

YEAR	TEMPERATURE

-----

Station Code	Type	Status
Station Name		
Location		

TEMPERATURE in °C    =====>     Mean    Minimum    Maximum    Daily     Monthly    Annual

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL

Station Code	Type	Status
Station Name		
Location		

TEMPERATURE in °C    ==>    Mean    **Minimum**    Maximum    **Daily**    Monthly    Annual  
 YEAR:    1989

YEAR	DAY	JAN	FEB	MAR	APR	MAY	JUN	JUL
1989	1							
1989	2							
1989	3							
1989	4							
1989	5							
1989	6							
1989	7							

Station Code	Type	Status
Station Name		
Location		

TEMPERATURE in °C    ==>    Mean     Minimum    Maximum    Daily     Monthly    Annual

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL

Station Code ▪	Type ▪	Status ▪
Station Name ▪		
Location ▪		

TEMPERATURE in °C    =====>    Mean     Minimum    Maximum    Daily    Monthly     Annual

YEAR	TEMPERATURE

Station Code •	Type •	Status •
Station Name •		
Location •		

TEMPERATURE in °C    =====>    Mean    Minimum     Maximum     Daily    Monthly    Annual

YEAR:    1989

YEAR	DAY	JAN	FEB	MAR	APR	MAY	JUN	JUL
1989	1							
1989	2							
1989	3							
1989	4							
1989	5							
1989	6							
1989	7							



Station Code •	Type •	Status •
Station Name •		
Location •		

TEMPERATURE in °C    =====>    Mean    Minimum     Maximum    Daily     Monthly    Annual

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL

Station Code	Type	Status
Station Name		
Location		

TEMPERATURE  
in °C

====>

Mean

Minimum

Maximum

Daily

Monthly

Annual

YEAR	TEMPERATURE

-----

Station Code •	Type •	Status •
Station Name •		
Location •		

EVAPORATION ==>  
in millimeters

Daily

Monthly

Annual

YEAR: 1989

YEAR	DAY	JAN	FEB	MAR	APR	MAY	JUN	JUL
1989	1							
1989	2							
1989	3							
1989	4							
1989	5							
1989	6							
1989	7							

Station Code	Type	Status
Station Name		
Location		

EVAPORATION ---->  
in millimeters

Daily    **Monthly**    Annual

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL

Station Code ■	Type ■	Status ■
Station Name ■		
Location ■		

EVAPORATION ==>>>>  
in millimeters

Daily      Monthly       Annual

YEAR	EVAPORATION

-----

Station Code	Type	Status
Station Name		
Location		

HUMIDITY ==>  
in percent

Daily

Monthly

Annual

YEAR: 1989

YEAR	DAY	JAN	FEB	MAR	APR	MAY	JUN	JUL
1989	1							
1989	2							
1989	3							
1989	4							
1989	5							
1989	6							
1989	7							

-----

Station Code . .	Type .	Status .
Station Name .		
Location .		

HUMIDITY ====>  
in percent

Daily

Monthly

Annual

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL

Station Code ■	Type ■	Status ■
Station Name ■		
Location ■		

HUMIDITY ==>>>>  
in percent

Daily      Monthly

Annual

YEAR	HUMIDITY

-----



Station Code ■	Type ■	Status ■
Station Name ■		
Location ■		

SUNSHINE DURATION in hours      =====>       Daily       Monthly       Annual

YEAR: 1989

YEAR	DAY	JAN	FEB	MAR	APR	MAY	JUN	JUL
1989	1							
1989	2							
1989	3							
1989	4							
1989	5							
1989	6							
1989	7							

Station Code •	Type •	Status •
Station Name •		
Location •		

SUNSHINE DURATION    ---->  
in hours

Daily

Monthly

Annual

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL

Station Code ■	Type ■	Status ■
Station Name ■		
Location ■		

SUNSHINE DURATION  
in hours

====>

Daily

Monthly

Annual

YEAR	SUNSHINE DURATION

-----

Station Code	Type	Status
Station Name		
Location		

WIND VELOCITY      =====>  
in m/sec

Daily     Monthly     Annual

YEAR:    1989

YEAR	DAY	JAN	FEB	MAR	APR	MAY	JUN	JUL
1989	1							
1989	2							
1989	3							
1989	4							
1989	5							
1989	6							
1989	7							

Station Code	Type	Status
Station Name		
Location		

WIND VELOCITY      ===>      Daily      **Monthly**      Annual  
in m/sec

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL

Station Code ■	Type ■	Status ■
Station Name ■		
Location ■		

WIND VELOCITY    ---->  
in m/sec

Daily

Monthly

Annual

YEAR	WIND VELOCITY

-----

Screen H1

HYDROLOGICAL OBSERVATION ==>

Simultaneous
Continuous

\*\*\* HYDROLOGICAL SIMULTANEOUS OBSERVATION \*\*\*

H-Code	River Basin	River



Screen H2.1

Station Code	▪	
River Basin	▪	
River	▪	
Location	▪	
Station	▪	
Status	▪	
<hr/>		
Responsible Agency	▪	
Drainage Area	▪	square kilometers
Elevation	▪	meters
Map Sheet No.	▪	
Map Sheet Quadrant	▪	
Coordinates:		
Latitude	▪	° ' "
Longitude	▪	° ' "
Years of Record	▪	From: To:
Remarks	▪	

DATA BEING OBSERVED

Spring Discharge
Streamflow

•• Edit ... Print... Quit... ••

Screen H2.1.1

Station Code	▪
River Basin	▪
River	▪
Location	▪
Station	▪
Status	▪

\*\*\* SPRING DISCHARGE SIMULTANEOUS OBSERVATION \*\*\*

Discharge, in LPS	Date Measured	Time Measured	Remarks

-----

Screen H2.1.2

Station Code	▪
River Basin	▪
River	▪
Location	▪
Station	▪
Status	▪

\*\*\* STREAMFLOW DISCHARGE SIMULTANEOUS OBSERVATION \*\*\*

Discharge, in LPS	Date Measured	Time Measured	Remarks

Screen H3

\*\*\* HYDROLOGICAL CONTINUOUS OBSERVATION \*\*\*

H-Code	River Basin	River

-----

Screen H3.1

Station Code	▪	
River Basin	▪	
River	▪	
Location	▪	
Station	▪	
Status	▪	
Responsible Agency	▪	
Drainage Area	▪	square kilometers
Elevation	▪	meters
Map Sheet No.	▪	
Map Sheet Quadrant	▪	
Coordinates:		
Latitude	▪	° ' "
Longitude	▪	° ' "
Years of Record	▪	From: To:
Remarks	▪	

DATA BEING OBSERVED

River Discharge
Gage Height

.. Edit ... Print... Quit... ..

Screen H3.1.1

Station Code	▪
River Basin	▪
River	▪
Location	▪
Station	▪
Status	▪

RIVER DISCHARGE =====>  
in cms

Daily

Monthly

Annual

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG

Screen H3.1.2

Station Code	*
River Basin	*
River	*
Location	*
Station	*
Status	*

RIVER DISCHARGE ====>  
in cms

Daily

Monthly

Annual

YEAR: 1989

YEAR	DAY	JAN	FEB	MAR	APR	MAY	JUN	JUL
1989	1							
1989	2							
1989	3							
1989	4							
1989	5							

Screen H3.1.3

Station Code	▪
River Basin	▪
River	▪
Location	▪
Station	▪
Status	▪

RIVER DISCHARGE =====>  
in cms

Daily

Monthly

Annual

YEAR	RIVER DISCHARGE



Screen H3.1.4

Station Code	•
River Basin	•
River	•
Location	•
Station	•
Status	•

GAGE HEIGHT ==>>>>  
in meters

Daily

Monthly

Annual

YEAR: 1989

YEAR	DAY	JAN	FEB	MAR	APR	MAY	JUN	JUL
1989	1							
1989	2							
1989	3							
1989	4							
1989	5							

Screen H3.1.5

Station Code	▪
River Basin	▪
River	▪
Location	▪
Station	▪
Status	▪

GAGE HEIGHT ---->  
in meters

Daily

Monthly

Annual

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG

Screen H3.1.6

Station Code	▪
River Basin	▪
River	▪
Location	▪
Station	▪
Status	▪

GAGE HEIGHT ==>>>>  
in meters

Daily

Monthly

Annual

YEAR	GAGE HEIGHT

Screen G1

\*\*\* HYDROGEOLOGICAL DATA \*\*\*

Wcode	Location	Type	Well Name	Status

Screen G2

Well Code ■	Location ■	Type ■	Status ■
Well Name ■			

\*\*\* HYDROGEOLOGICAL INFORMATION \*\*\*

==> Choose...

- Pumping Test Data
- Groundwater Level:
  - Continuous Observation
  - Simultaneous Observation
- Chemical Quality of Water

Screen G3

Well Code ■	Location ■	Type ■	Status ■
Well Name ■			

\*\*\* PUMPING TEST DATA \*\*\*

Static Water Level.....	Date ■	(mm/dd/yy)
After Construction ■	meters	/ /
Recent Measurement ■	meters	/ /
Pumping Water Level.....	Date ■	
After Construction ■	meters	/ /
Recent Measurement ■	meters	/ /
Actual Discharge.....	Date ■	
After Construction ■	LPS	/ /
Recent Measurement ■	LPS	/ /
Specific Capacity ■	LPS/M	
Transmissibility ■	M <sup>2</sup> /day	
Storage Coefficient ■		
Pumping Duration ■	hours	
Type of Pumping Test ■		

.. Edit... Print... Quit... ..

Screen G4.1

Well Code •	Location •	Type •	Status •
Well Name •			

GROUNDWATER LEVEL  
CONTINUOUS OBSERVATION  
in meters

====>

Daily

Monthly

Annual

YEAR: 1989

YEAR	DAY	JAN	FEB	MAR	APR	MAY	JUN	JUL
1989	1							
1989	2							
1989	3							
1989	4							
1989	5							

Screen G4.2

Well Code ■	Location ■	Type ■	Status ■
Well Name ■			

GROUNDWATER LEVEL  
CONTINUOUS OBSERVATION  
in meters

====>

Daily

Monthly

Annual

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL



Screen G4.3

Well Code •	Location •	Type •	Status •
Well Name •			

GROUNDWATER LEVEL  
CONTINUOUS OBSERVATION  
in meters

====>

Daily

Monthly

Annua i

YEAR	WATER LEVEL

-----

Screen G5

Well Code ■	Location ■	Type ■	Status ■
Well Name ■			

\*\*\* GROUNDWATER LEVEL SIMULTANEOUS OBSERVATION \*\*\*

C-No.	C-Diam.	C-Top	H2O-Below C-Top	Water Level	Ground Elevation

C-Diam., in centimeters  
C-Top, in ma/bgs  
H2O-Below C-Top, in mbgs

Water Level, in mbgs  
Ground Elevation, in masl  
Piezo Level, in ma/bsi

Sheet 65

Well Code •	Location •	Type •	Status •
Well Name •			

\*\*\* GROUNDWATER LEVEL SIMULTANEOUS OBSERVATION \*\*\*

Piezo Level	Water Quality	Date Measured	Time Measured

C-Diam., in centimeters  
C-Top, in ma/bgs  
H2O-Below C-Top, in mbgs

Water Level, in mbgs  
Ground Elevation, in masl  
Piezo Level, in ma/bsl

Screen G6

Well Code ■	Location ■	Type ■	Status ■
Well Name ■			

\*\*\* CHEMICAL QUALITY OF WATER \*\*\*

Principal Ions	Concentration, in mg/l	Date of Sampling

\*\*\* LITERATURE RECORDS \*\*\*

Literature Code	▪
Title	▪
Author	▪
Subject Matter	▪

ABSTRACT ▪

--

•• Edit... Print... Previous... Next... Quit ••

Screen W6

Well Code ■	Location ■	Type ■	MWSS	Status ■
-------------	------------	--------	------	----------

PUMPAGE      =====>  
in cu. m.

Monthly      Annual

Screen W6.1

Well Code ■	Location ■	Type ■ MWSS	Status ■
Well Name ■			

PUMPAGE ==>>>>  
in cu. m.

Monthly

Annual

YEAR	JAN	FEB	MAR	APR	MAY

Screen W6.2

Well Code ■	Location ■	Type ■ MWSS	Status ■
Well Name ■			

PUMPAGE   =====>  
in cu. m.

Monthly

Annual

YEAR	PUMPAGE



Screen G7

Well Code ■ VLZ-1003 Location ■ Type ■ MWSS Status ■  
Well Name ■ MWSS

\*\*\* PHYSICAL QUALITY OF WATER \*\*\*

Temperature	■	°C
Turbidity	■	units
Color	■	units
Odor	■	
Total Solids	■	mg/l
Dissolved Solids	■	mg/l
pH	■	
Spe. Cond.	■	micromhos/cm
Alkalinity	■	mg/l, CaCO3
Hardness	■	mg/l, CaCO3
Residual Chlorine	■	mg/l
Acidity	■	mg/l, CaCO3

■ Edit... Print... Quit... ■

**APPENDIX A**

**DATA FILE STRUCTURE**

APPENDIX A.1

DATA FILE STRUCTURE  
WELL INVENTORY DATABASE

1. Filename: WELLDATA. DBF  
(contains Well Data; sorted by W\_CODE)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
W_CODE	Character	8		Well Code
W_LOC	Character	2		Location: 01 - Antipolo (ATP) 02 - Bacoor (BCR) 03 - Caloocan-A (CLA) 04 - Cainta (CTA) 05 - Cavite City (CVC) 06 - IMUS (IMS) 07 - Kawit (KWT) 08 - Las Pinas (LPS) 09 - Makati (MKT) 10 - Malabon (MLB) 11 - Mandaluyong (MDL) 12 - Manila (MNL) 13 - Marikina (MRK) 14 - Montalban (Rodriguez)(MTB) 15 - Muntinlupa (MTL) 16 - Navotas (NAV) 17 - Noveleta (NOV) 18 - Paranaque (PRN) 19 - Pasay City (PSC) 20 - Pasig (PSG) 21 - Pateros (PTR) 22 - Quezon City (QCT) 23 - Rosario (ROS) 24 - San Juan (SJN) 25 - San Mateo (SMT) 26 - Taguig (TGG) 27 - Taytay (TYT) 28 - Valenzuela (VLZ) 29 - Caloocan-B (CLB) 30 - Angono (AGN) 31 - Baras (BRS) 32 - Binangonan (BNG) 33 - Cardona (CDN) 34 - Jala-Jala (JLJ) 35 - Morong (MRN) 36 - Pilillia (PLL) 37 - Tanay (TNY) 38 - Teresa (TRS)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
=====	=====	=====	=====	=====
W_TYPE	Character	1		Well Type: 1 - MWSS 2 - Private
W_STATUS	Character	1		Well Status: 1 - Active 2 - Inactive 3 - Abandoned
W_NAME	Character	36		Well Name
W_ADDR1	Character	50		Well Address
W_ADDR2	Character	50		Well Address (continuation)
OWNER	Character	60		Owner of the well
F_OWNER	Character	60		Former Owner of the well
NEW_NO	Character	5		New No.
OLD_NO	Character	5		Old No.
MAP_NO	Character	5		Map Sheet No.
ELEVATION	Numeric	10		Ground Elevation, in meters
X	Character	2		X coordinate
Y	Character	2		Y coordinate
LAT_DEGR	Numeric	3		Latitude, in degrees
LAT_MIN	Numeric	3		Latitude, in minutes
LAT_SEC	Numeric	3		Latitude, in seconds
LONG_DEGR	Numeric	3		Longitude, in degrees
LONG_MIN	Numeric	3		Longitude, in minutes
LONG_SEC	Numeric	3		Longitude, in seconds
W_DEPTH	Numeric	10	2	Well Depth, in meters
RISER_PIPE	Numeric	10	2	Diameter of Riser Pipe, in centimeters
AQUI_TYPE	Character	1		Aquifer Type: 1 - Upper Guadalupe 2 - Lower Guadalupe 3 - Basement
DRILLER	Character	35		Well Driller
COMP_MM	Character	2		Completion Date: Month (1-12)
COMP_DD	Character	2		Day (1-31)
COMP_YY	Character	2		Year (1900-...)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
GW_USE	Character	1		Groundwater Use: 1 - Public: Domestic 2 - Public: Institution 3 - Commercial 4 - Industrial: Food/Beverages 5 - Industrial: Chemicals 6 - Industrial: Leather 7 - Industrial: Textile, Paper & Pulp 8 - Industrial: Others
RPC_OLD	Numeric	5	2	Rated Pump Capacity: Old, in LPS
RPC_NEW	Numeric	5	2	Rated Pump Capacity: New, in LPS
TDH_OLD	Numeric	6	2	Total Developed Head: Old, in m.
TDH_NEW	Numeric	6	2	Total Developed Head: New, in m.
MHP_OLD	Numeric	6	2	Motor HP Rating: Old
MHP_NEW	Numeric	6	2	Motor HP Rating: New
PSET_OLD	Numeric	10	2	Pump Setting: Old, in meters
PSET_NEW	Numeric	10	2	Pump Setting: New, in meters
SWL_AC	Numeric	10	2	Static water level - After construction
SWL_RM	Numeric	10	2	Static water level - Recent measurement
SWL_MM	Character	2		Month: SWL-AC (1-12)
SWL_DD	Character	2		Day: SWL-AC (1-31)
SWL_YY	Character	2		Year: SWL-AC (1900-...)
SWL1_MM	Character	2		Month: SWL-RM (1-12)
SWL1_DD	Character	2		Day: SWL-RM (1-31)
SWL1_YY	Character	2		Year: SWL-RM (1900-...)
PWL_AC	Numeric	10	2	Pumping Water Level: Old, in m.
PWL_RM	Numeric	10	2	Pumping Water Level: New, in m.
PWL_MM	Character	2		Month: PWL-AC (1-12)
PWL_DD	Character	2		Day: PWL-AC (1-31)
PWL_YY	Character	2		Year: PWL-AC (1900-...)
PWL1_MM	Character	2		Month: PWL-RM (1-12)
PWL1_DD	Character	2		Day: PWL-RM (1-31)
PWL1_YY	Character	2		Year: PWL-RM (1900-...)
YLD_AC	Numeric	10	2	Yield-After construction, in LPS
YLD_RM	Numeric	10	2	Yield-Recent Measurement, in LPS
YLD_MM	Character	2		Month: YLD-AC (1-12)
YLD_DD	Character	2		Day: YLD-AC (1-31)
YLD_YY	Character	2		Year: YLD-AC (1900-...)
YLD1_MM	Character	2		Month: YLD-RM (1-12)
YLD1_DD	Character	2		Day: YLD-RM (1-31)
YLD1_YY	Character	2		Year: YLD-RM (1900-...)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
ST_COEFF	Numeric	10	5	Storage Coefficient
TRANSMISS	Numeric	10	5	Transmissibility, in M <sup>2</sup> /D
P_DURATION	Numeric	5		Pumping Duration, in hours/day
SPCF_CPCTY	Numeric	10	5	Specific Capacity, in LPS/M
PTEST_TYPE	Character	1		Type of Pumping Test: 1 - Step Drawdown 2 - Constant Rate Discharge
DAT_SOURCE	Character	30		Source of Data

2. Filename: WCASING.DBF  
(contains Well Casing Schedule; sorted by W\_CODE)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
W_CODE	Character	8		Well Code (same as in WELLDATA.DBF)
CASING_NO	Numeric	2		Casing No.
DIAMETER	Numeric	8	2	Casing Diameter, in centimeters
DEPTH_FROM	Numeric	8	2	Casing Depth: From, in meters
DEPH_TO	Numeric	8	2	Casing Depth: To, in meters

3. Filename: WSCREEN.DBF  
(contains Well Screen Section; sorted by W\_CODE)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
W_CODE	Character	8		Well Code (same as in WELLDATA.DBF)
SCR_NO	Numeric	1		Screen No.
SCR_TYPE	Character	1		Type of Screen: 1 - Johnson (continuous-slot) 2 - Slotted 3 - Wedge Wire Wound 4 - Louvered 5 - Perforated
DIAMETER	Numeric	10	2	Screen Diameter, in centimeters
DEPTH_FROM	Numeric	10	2	Screen Depth Below Ground: From, in meters
DEPTH_TO	Numeric	10	2	Screen Depth Below Ground: To, in meters

4. Filename: WSTRATUM.DBF  
 (contains Well Log Record; sorted by W\_CODE)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
=====	=====	=====	=====	=====
W_CODE	Character	8		Well Code (same as in WELLDATA.DBF)
STR_NO	Numeric	2		Stratum No.
DEPTH_FROM	Numeric	8	2	Stratum Depth Below Ground: From, in meters
DEPTH_TO	Numeric	8	2	Stratum Depth Below Ground: To, in meters
STR_DESC1	Character	50		Description of Stratum
STR_DESC2	Character	25		Description of Stratum (continuation)

APPENDIX A.2

DATA FILE STRUCTURE  
METEOROLOGICAL DATABASE

1. Filename: MSTATION.DBF  
(contains data on Meteorological Stations)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
=====	=====	=====	=====	=====
M_CODE	Character	8		Meteorological Station Code
M_NAME	Character	40		Name of the Station
M_TYPE	Character	1		Type of Station: 1 - Official Rainfall 2 - Climatological/Cooperative Rainfall 3 - Agrometeorological 4 - Synoptic Station
M_STATUS	Character	1		Status of the Station: 1 - Operational 2 - Abandoned
M_LOC	Character	30		Location of the Station
M_AGENCY	Character	1		Responsible Agency: 1 - MWSS 2 - PAGASA 3 - BRS 4 - NWRB 5 - MGB 6 - EMB 7 - Private Drilling Company
M_ELEV	Numeric	10	2	Elevation, in meters above MSL
R_BASIN	Character	3		River Basin
M_MAPNO	Character	5		Map Sheet No.
M_MQUAD	Character	2		Map Sheet Quadrant: NE - North East NW - North West SW - South West SE - South East



FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
MLAT_DEGR	Numeric	3		Latitude, in degrees
MLAT_MIN	Numeric	2		Latitude, in minutes
MLAT_SEC	Numeric	2		Latitude, in seconds
MLONG_DEGR	Numeric	3		Longitude, in degrees
MLONG_MIN	Numeric	2		Longitude, in minutes
MLONG_SEC	Numeric	2		Longitude, in seconds
FROM_REC	Numeric	4		Year of Record: From
TO_REC	Numeric	4		Year of Record: To
TIME_REC	Character	30		Time Measurement
M_REMARKS	Character	45		Remarks

2. Filename:RAIN\_D.DBF (Daily Rainfall Data; sorted by M\_CODE)
3. TMAV\_D.DBF (Daily Mean Temperature; sorted by M\_CODE)
4. TMIN\_D.DBF (Daily Minimum Temperature; sorted by M\_CODE)
5. TMAX\_D.DBF (Daily Maximum Temperature; sorted by M\_CODE)
6. EVAP\_D.DBF (Daily Evaporation; sorted by M\_CODE)
7. HUMID\_D.DBF (Daily Humidity; sorted by M\_CODE)
8. SUN\_D.DBF (Daily Sunshine Duration; sorted by M\_CODE)
9. WIND\_D.DBF (Daily Wind Velocity; sorted by M\_CODE)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
M_CODE	Character	8		Meteorological Code (same as in MSTATION.DBF)
YEAR	Numeric	4		Year Observed (1900-...)
DAY	Numeric	2		Day Observed (1-31)
JAN	Numeric	9	4	Measurement: * 0.0000 - No Data * 0.0001 - Zero - Rainfall, in mm - Temperature, in °C - Evaporation, in mm - Humidity, in percent - Sunshine Duration, in hours - Wind Velocity, in m/sec for DAY and month JAN (January)
FEB	Numeric	9	4	..... (February)
MAR	Numeric	9	4	..... (March)
APR	Numeric	9	4	..... (April)
MAY	Numeric	9	4	..... (May)
JUN	Numeric	9	4	..... (June)
JUL	Numeric	9	4	..... (July)
AUG	Numeric	9	4	..... (August)
SEP	Numeric	9	4	..... (September)
OCT	Numeric	9	4	..... (October)
NOV	Numeric	9	4	..... (November)

DEC            Numeric        9        4        ..... (December)

- 10. Filename:RAIN\_M.DBF (Monthly Rainfall Data; sorted by M\_CODE)
- 11.            TMAV\_M.DBF (Monthly Mean Temperature; sorted by M\_CODE)
- 12.            TMIN\_M.DBF (Monthly Minimum Temperature;sorted by M\_CODE)
- 13.            TMAX\_M.DBF (Monthly Maximum Temperature;sorted by M\_CODE)
- 14.            EVAP\_M.DBF (Monthly Evaporation; sorted by M\_CODE)
- 15.            HUMID\_M.DBF (Monthly Humidity; sorted by M\_CODE)
- 16.            SUN\_M.DBF (Monthly Sunshine Duration; sorted by M\_CODE)
- 17.            WIND\_M.DBF (Monthly Wind Velocity; sorted by M\_CODE)

Note: Data are computed.

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
=====	=====	=====	=====	=====
M_CODE	Character	8		Meteorological Station Code (same as in MSTATION.DBF)
YEAR	Numeric	4		Year Observed (1900-...)
				Measurement (same as in daily data) for the month of:
JAN	Numeric	9	4	... January
FEB	Numeric	9	4	... February
MAR	Numeric	9	4	... March
APR	Numeric	9	4	... April
MAY	Numeric	9	4	... May
JUN	Numeric	9	4	... June
JUL	Numeric	9	4	... July
AUG	Numeric	9	4	... August
SEP	Numeric	9	4	... September
OCT	Numeric	9	4	... October
NOV	Numeric	9	4	... November
DEC	Numeric	9	4	... December
YDATA	Numeric	10	2	... Yearly data

APPENDIX A.3

DATA FILE STRUCTURE  
HYDROLOGICAL DATABASE

1. Filename: HSTATION.DBF  
(contains information on Hydrological Stations)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
=====	=====	=====	=====	=====
H_CODE	Character	8		Hydrological Station Code
H_STATION	Character	30		Name of the Station
H_OBS	Character	1		Type of Observation: 1 - Simultaneous 2 - Continuous
H_STAT	Character	15		Status of the Station: 1 - Operational 2 - Abandoned
H_LOC	Character	30		Location of the Station
R_BASIN	Character	30		River Basin
R_NAME	Character	30		River
H_AGENCY	Character	1		Responsible Agency: 1 - MWSS 2 - PAGASA 3 - BRS 4 - NWRB 5 - MGB 6 - EMB 7 - Private Drilling Company
H_DRAIN	Numeric	10	2	Drainage Area, in sq. kms.
H_ELEV	Numeric	10	2	Elevation, in meters above MSL
H_MAPNO	Character	5		Map Sheet No.

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
=====	=====	=====	=====	=====
H_MQUAD	Character	2		Map Sheet Quadrant: NE - North East NW - North West SW - South West SE - South East
				Coordinates:
HLAT_DEGR	Numeric	3		Latitude, in degrees
HLAT_MIN	Numeric	2		Latitude, in minutes
HLAT_SEC	Numeric	2		Latitude, in seconds
HLONG_DEGR	Numeric	3		Longitude, in degrees
HLONG_MIN	Numeric	2		Longitude, in minutes
HLONG_SEC	Numeric	2		Longitude, in seconds
FROM_REC	Numeric	4		Year of Record: From
TO_REC	Numeric	4		Year of Record: To
H_REMARKS	Character	45		Remarks

2. Filename: RDIS\_D.DBF (Daily River Discharge; sorted by H\_CODE)
3. GAGE\_D.DBF (Daily Gage Height; sorted by H\_CODE)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
=====	=====	=====	=====	=====
H_CODE	Character	8		Hydrological Code (same as in HSTATION.DBF)
YEAR	Numeric	4		Year Observed (1900-...)
DAY	Numeric	2		Day Observed (1-31)
JAN	Numeric	9	4	Measurement: *0.0000 - No Data *0.0001 - Zero - River Discharge, in m <sup>3</sup> - Gage Height, in meters for DAY and month JAN (January)
FEB	Numeric	9	4	..... (February)
MAR	Numeric	9	4	..... (March)
APR	Numeric	9	4	..... (April)
MAY	Numeric	9	4	..... (May)
JUN	Numeric	9	4	..... (June)
JUL	Numeric	9	4	..... (July)
AUG	Numeric	9	4	..... (August)
SEP	Numeric	9	4	..... (September)
OCT	Numeric	9	4	..... (October)
NOV	Numeric	9	4	..... (November)
DEC	Numeric	9	4	..... (December)

4. Filename: RDIS\_M.DBF (Monthly River Discharge; sorted by H\_CODE)  
 5. GAGE\_M.DBF (Monthly Gage Height; sorted by H\_CODE)

Note: Data are computed.

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
H_CODE	Character	8		Hydrological Station Code (same as in HSTATION.DBF)
YEAR	Numeric	4		Year Observed (1900-...)
				Measurement (same as in daily data) for the month of:
JAN	Numeric	9	4	... January
FEB	Numeric	9	4	... February
MAR	Numeric	9	4	... March
APR	Numeric	9	4	... April
MAY	Numeric	9	4	... May
JUN	Numeric	9	4	... June
JUL	Numeric	9	4	... July
AUG	Numeric	9	4	... August
SEP	Numeric	9	4	... September
OCT	Numeric	9	4	... October
NOV	Numeric	9	4	... November
DEC	Numeric	9	4	... December
YDATA	Numeric	10	2	... Yearly data

6. Filename: SPRING.DBF (Spring Discharge, sorted by H\_CODE)  
 7. STREAM.DBF (Streamflow, sorted by H\_CODE)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
H_CODE	Character	4		Hydrological Station Code (same as in HSTATION.DBF)
DISCHARGE	Numeric	8	2	Spring Discharge, in LPS/ Streamflow, in LPS
DATE_M	Character	8		Date Measured
TIME_M	Character	8		Time Measured
REMARKS	Character	45		Remarks

APPENDIX A.4

DATA FILE STRUCTURE  
HYDROGEOLOGICAL DATABASE

1. Filename: HGEO.DBF  
(contains Pumping Test data; sorted by W\_CODE)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
=====	=====	=====	=====	=====
W_CODE	Character	8		Well Code (Same as in WELLDATA.DBF)
W_LOC	Character	2		Location (Same as in WELLDATA.DBF)
W_TYPE	Character	1		Well Type (Same as in WELLDATA.DBF)
W_NAME	Character	36		Well Name (Same as in WELLDATA.DBF)
W_STATUS	Character	1		Well Status (Same as in WELLDATA.DBF)
SWL_AC	Numeric	10	2	Static Water level - After construction
SWL_RM	Numeric	10	2	Static Water level - Recent measurement
SWL_MM	Character	2		Month: SWL-AC (1-12)
SWL_DD	Character	2		Day: SWL-AC (1-31)
SWL_YY	Character	2		Year: SWL-AC (1900-...)
SWL1_MM	Character	2		Month: SWL-RM (1-12)
SWL1_DD	Character	2		Day: SWL-RM (1-31)
SWL1_YY	Character	2		Year: SWL-RM (1900-...)
PWL_AC	Numeric	10	2	Pumping Water Level: Old, in meters
PWL_RM	Numeric	10	2	Pumping Water Level: New, in meters
PWL_MM	Character	2		Month: PWL-AC (1-12)
PWL_DD	Character	2		Day: PWL-AC (1-31)
PWL_YY	Character	2		Year: PWL-AC (1900-...)
PWL1_MM	Character	2		Month: PWL-RM (1-12)
PWL1_DD	Character	2		Day: PWL-RM (1-31)
PWL1_YY	Character	2		Year: PWL-RM (1900-...)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
YLD_AC	Numeric	10	2	Yield - After Construction, in LPS
YLD_RM	Numeric	10	2	Yield - Recent Measurement, in LPS
YLD_MM	Character	2		Month: YLD-AC (1-12)
YLD_DD	Character	2		Day: YLD-AC (1-31)
YLD_YY	Character	2		Year: YLD-AC (1900-...)
YLD1_MM	Character	2		Month: YLD-RM (1-12)
YLD1_DD	Character	2		Day: YLD-RM (1-31)
YLD1_YY	Character	2		Year: YLD-RM (1900-...)
ST_COEFF	Numeric	10	5	Storage Coefficient
TRANSMISS	Numeric	10	5	Transmissibility, in M <sup>2</sup> /D
P_DURATION	Numeric	5		Pumping Duration, in hours/day
SPCF_CPCTY	Numeric	10	5	Specific Capacity, in LPS/M
PTEST_TYPE	Character	1		Type of Pumping Test 1 - Step Drawdown 2 - Constant Rate Discharge

2. Filename: WGWS.DBF

(contains Groundwater Level Simultaneous Observation;  
sorted by W\_CODE)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
W_CODE	Character	8		Well Code (Same as in WELLDATA.DBF)
CASING_NO	Character	2		Casing No.
CASING_D	Numeric	5	2	Casing Diameter, in centimeters
CASING_T	Numeric	5	2	Top of Casing, ma/bgs
WL_BT	Numeric	5	2	Water Below Casing Top, in mbgs
WL	Numeric	5	2	Water Level, in mbgs
GR_EL	Numeric	5	2	Ground Elevation, in masl
PIEZO	Numeric	5	2	Piezo Level, in ma/bsl
W_QUALITY	Character	30		Water Quality
DATE_M	Character	8		Date Measured
TIME_M	Character	8		Time Measured
REMARKS	Character	45		Remarks

3. Filename: WGWC\_D.DBF

(contains Daily Groundwater Level Continuous Observation;  
sorted by W\_CODE)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
W_CODE	Character	8		Well Code (same as in WELLDATA.DBF)
YEAR	Numeric	4		Year Observed (1900-...)
DAY	Numeric	2		Day Observed (1-31)
JAN	Numeric	9	4	Water Level Observation, in meters, for DAY and month JAN (January) *0.0000 - No Data *0.0001 - Zero
FEB	Numeric	9	4	..... (February)
MAR	Numeric	9	4	..... (March)
APR	Numeric	9	4	..... (April)
MAY	Numeric	9	4	..... (May)
JUN	Numeric	9	4	..... (June)
JUL	Numeric	9	4	..... (July)
AUG	Numeric	9	4	..... (August)
SEP	Numeric	9	4	..... (September)
OCT	Numeric	9	4	..... (October)
NOV	Numeric	9	4	..... (November)
DEC	Numeric	9	4	..... (December)

4. Filename: WGWC\_M.DBF

(contains Monthly Groundwater Level Continuous Observation;  
sorted by W\_CODE)

Note: Data are computed.

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
W_CODE	Character	8		Well Code (same as in WELLDATA.DBF)
YEAR	Numeric	4		Year Observed (1900-...)
				Water Level Observation for the Month of: (in meters)
JAN	Numeric	9	4	January
FEB	Numeric	9	4	February
MAR	Numeric	9	4	March
APR	Numeric	9	4	April
MAY	Numeric	9	4	May
JUN	Numeric	9	4	June
JUL	Numeric	9	4	July
AUG	Numeric	9	4	August
SEP	Numeric	9	4	September
OCT	Numeric	9	4	October
NOV	Numeric	9	4	November
DEC	Numeric	9	4	December
YDATA	Numeric	10	2	Yearly data



5. Filename: WCHEM.DBF

(contains the Chemical Quality of Water; sorted by W\_CODE)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
=====	=====	=====	=====	=====
W_CODE	Character	8		Well Code (same as in WELLDATA.DBF)
IONS	Character	2		Principal Ions 01 - Ca: Calcium (++) 02 - Na: Sodium (+) 03 - HCO3: Bicarbonate (-) 04 - Cl: Chloride (-) 05 - F: Flouride (-) 06 - Fe: Iron (++,+++) 07 - Mg: Magnesium (++) 08 - K: Potassium (+) 09 - SO4: Sulfate (--) 10 - NO3: Nitrate (-) 11 - TDS: Dissolved solids
CONCENT	Numeric	6	2	Concentration, in mg/l
DATE_S	Character	8		Date of Sampling

APPENDIX A.5

DATA FILE STRUCTURE  
LITERATURE DATABASE

1. Filename: LITR.DBF  
(contains Literature Records; sorted by LIT\_CODE)

FIELD NAME	TYPE	WIDTH	DECIMAL	DESCRIPTION
=====	=====	=====	=====	=====
LIT_CODE	Character	4		Literature Code
LIT_NAME1	Character	50		Literature Title
LIT_NAME2	Character	50		Literature Title (continuation)
AUTHOR1	Character	30		Author-1
AUTHOR2	Character	30		Author-2
AUTHOR3	Character	30		Author-3
SUBJ1	Character	2		Subject Matter: 01 - Hydrogeological Study 02 - Regional Deveelopment Study 03 - Test Drilling and/or Pumping Test 04 - Geographical Prospecting 05 - Chemical Quality Test 06 - Water Level Observation 07 - Discharge Observation 08 - Groundwater Potential 09 - Water Supply System Design
SUBJ2	Character	2		Subject Matter-2
SUBJ3	Character	2		Subject Matter-3
SUBJ4	Character	2		Subject Matter-4
SUBJ5	Character	2		Subject Matter-5
ABSTRACT				Literature Abstract

APPENDIX B

COMMAND AND FUNCTION KEYS

APPENDIX B  
COMMAND AND FUNCTION KEYS

Browsing

Browse keys:

- a. Right, left, up or down arrow key

Moves the highlighted bar from one record or from one data item to another on the screen. A record which is highlighted is called the active record.

- b. Home

Moves the highlighted bar to the first data item of the active record displayed on the screen.

- c. End

Moves the highlighted bar to the last data item of the active record displayed on the screen.

- d. Page-up

Scrolls the screen up.

- e. Page-down

Scrolls the screen down.

- f. Ctrl+Right arrow key

Scrolls one screen to the right.

- g. Ctrl+Left arrow key

Scrolls one screen to the left.

- h. Ctrl+Home

Moves the highlighted bar to the first data item of the active record.

- i. Ctrl+End

Moves the highlighted bar to the last data item of the active record.

- j. Ctrl+Page-up

Brings the user to the beginning of the list.

- k. Ctrl+Page-down

Brings the user to the end of the list.

#### Adding

To add new record(s), press the Ins-key or Ctrl+V. The cursor moves to the end of the list and the computer automatically generates blank space for data to be inputted.

#### Editing

To change the system to the edit mode, select the data item on the screen using the browse keys and press the Enter key. "EDIT" appears at the bottom left-corner of the screen. The system is now ready to accept information from the keyboard.

Note: Pressing Enter key a second time, changes the system to the browse mode and moves the cursor to the next data item to the right. Pressing the <Esc> key aborts the editing and brings the user back to the browse mode.

#### Edit keys:

- a. Del or Ctrl+G

Deletes the character where the cursor is.

- b. Ins or Ctrl+V

Inserts a character before the cursor.

- c. Ctrl+T

Deletes a word after the cursor.

- d. Backspace

Deletes a character before the cursor.

#### Deleting

To delete a record,

- a. Move the highlighted bar to the record to be deleted.

- b. Press Del key or Ctrl+G.

The "Delete" remark is displayed at the bottom right of the screen.

- c. To undo deletion, press F1 key.

- d. To save the file excluding all records marked "Delete", press Ctrl+Q.

Be careful. Deleted records can no longer be retrieved.

- e. To save the file including all records marked "Delete", press Esc key.

### Printing

To print data displayed on the screen,

- Press F4.

A message below appears at the bottom of the screen:

"SET THE PRINTER ON... Press any key when ready"

Pressing Esc key aborts the print option.

### Important:

- a. Turn the printer ON before pressing any key.
- b. Set your printer in condensed mode.

The image shows a highly textured, black and white surface, likely a book cover or endpaper. The texture is characterized by numerous fine, irregular lines and creases that create a complex, organic pattern. In the center of the image, there is a stylized logo consisting of the letters 'JICA' in a bold, sans-serif font. The logo is slightly darker than the surrounding texture, making it stand out. The overall appearance is that of a weathered or aged material with a prominent grain.

REPUBLIC OF THE PHILIPPINES  
METROPOLITAN WATERWORKS AND SEWERAGE SYSTEM

STUDY FOR THE GROUNDWATER DEVELOPMENT  
IN  
METRO MANILA

COMPUTER SIMULATION  
MANUAL

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# COMPUTER SIMULATION MANUAL

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## 1. INTRODUCTION

Computer simulation techniques were used to understand the dynamic behavior of groundwater flow and to evaluate the groundwater resources in the Metro Manila. The quasi three-dimensional flow model (Q3P model) was applied to the Antipolo groundwater basin and the Metro Manila groundwater basin. The two-dimensional solute transport model (MOC model) revealed the mechanism of saltwater intrusion in Las Pinas area. The model studies have helped design future groundwater use plans as well as prognose some remedial measures.

In recent years, digital computer models have gained wider acceptance as they foster more efficient groundwater resources management. For example, using a properly constructed groundwater model, it is possible to test various management schemes and to predict the effects of certain actions.

Of course, the validity of the model predictions will depend on how well the model approximates field conditions. Good field data are essential when using a model for predictive purposes. However, it is difficult to obtain adequate field data due to several constraints. Further, as natural aquifer systems are inherently complex and uncertain, construction of the model always requires the making of assumptions and simplifications. It is very important to keep this awareness about the model, even though sophisticated numerical techniques and high-speed computers have already been developed.

The instructions for using the computer models used in the study are described in detail in this manual. It is assumed that the user is familiar with the operation of the computer and its peripherals and understands the Disk Operating System manual supplied with the computer. The user is also expected to have a working knowledge of hydrogeology and have read books on groundwater hydrology and modeling.

## 2. SYSTEM REQUIREMENTS

### 2.1 HARDWARE

Followings are required hardware to run the computer models:

IBM Personal Computer or IBM Compatible Personal Computer.  
640K RAM.  
Intel 8087, 80287 or 80387 Numerical Co-processor  
Hard disk.  
Dot matrix printer with 132 column capability.

The Study Team used following hardware:

TOSHIBA J-3100SGX (with 100MB hard disk and 3.5" floppy disk drive).  
Additional memory cards (2MB x 2 = 4MB).  
Numerical co-processor (Intel 80387-20).  
TOSHIBA Dual Mode Printer 4.

### 2.2 SOFTWARE

Followings are required software to run the computer models:

PC-DOS or MS-DOS Version 3.0 or higher.  
FORTRAN 77 Compiler.  
BASIC Compiler or Interpreter (for graphics).  
LOTUS 123 or similar commercial program (for graphics).

The Study Team used following software:

MS-DOS Version 3.2.  
Pro FORTRAN-77 Compiler.  
Japanese MS-DOS Version 3.10 (for graphics).  
TOSHIBA BASIC Interpreter Version 3.2 (for graphics).  
LOTUS 123 (for graphics).

### 3. GROUNDWATER FLOW MODEL

#### 3.1 MODEL ABSTRACT

The computer model used for the study is a quasi three-dimensional groundwater flow model (Q3P model). The original Q3P model was constructed by Fujisaki (1982) and modified by KOKUSAI KOGYO Co., Ltd. Its basic concept is that the groundwater in the main confined aquifer is supplied by lateral flow through the aquifer and by a vertical flow through the aquitard from the overlying phreatic aquifer (Figure 3.1).

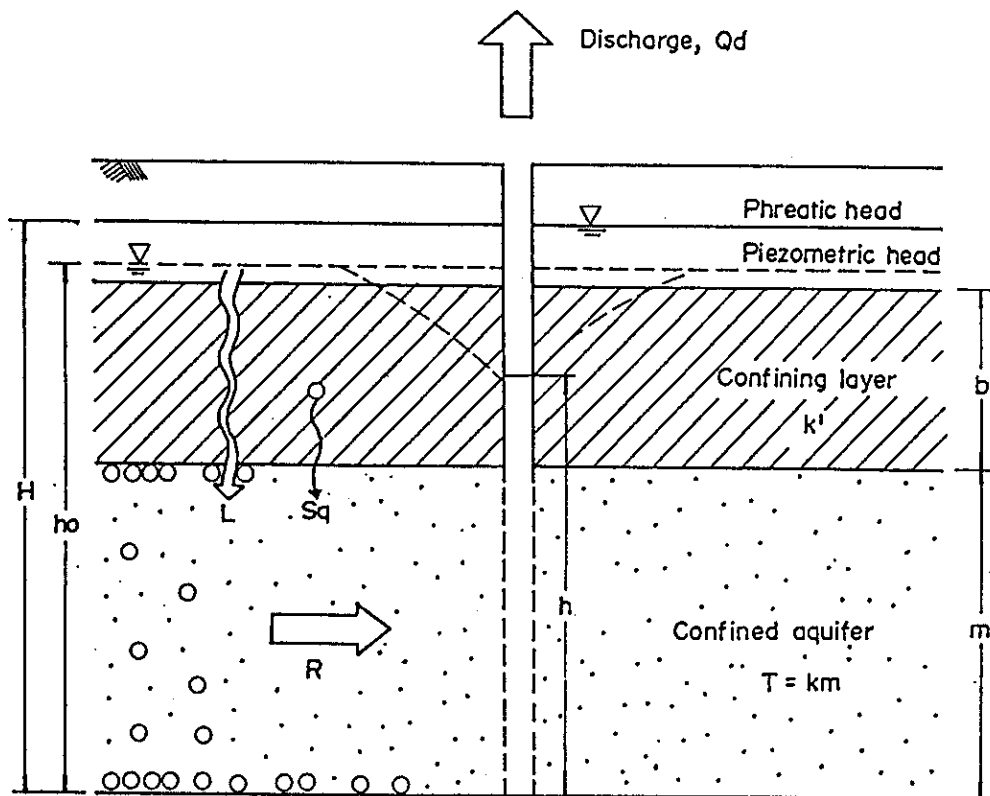
Q3P solves the groundwater flow equation using a finite-element approximation. The model is based on a rectangular finite-element grid. The model is applicable to two-dimensional or three-dimensional problems even in multi-aquifer systems involving steady-state or nonsteady-state flow.

The model computes changes in piezometric heads over time caused by changes in groundwater pumpage and groundwater recharge. If future plans of groundwater pumpage are inputted to the model, it can calculate future piezometric heads.

The model assumes that geohydrologic parameters such as transmissivity, storage coefficient and leakance are not affected by changes of piezometric heads. Also, the model needs to assume that those parameters and boundary conditions do not change over time. The phreatic water levels are assumed to be constant over time.

The model must be calibrated before starting actual calculations. The main procedure of model calibration is to specify boundary conditions and to identify some poor reliable hydrogeologic parameters. Generally the model is verified by the comparison of calculated piezometric heads with actual piezometric heads. Figure 3.2 shows the general flow of model calibration.

After all parameters and boundary conditions are fixed, the model can compute future piezometric heads based on future groundwater pumpage plans and future recharge estimates.



STUDY FOR THE GROUNDWATER DEVELOPMENT  
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Figure 3.1  
SCHEMATIC CROSS-SECTION OF  
THE QUASI 3-DIMENSIONAL MODEL

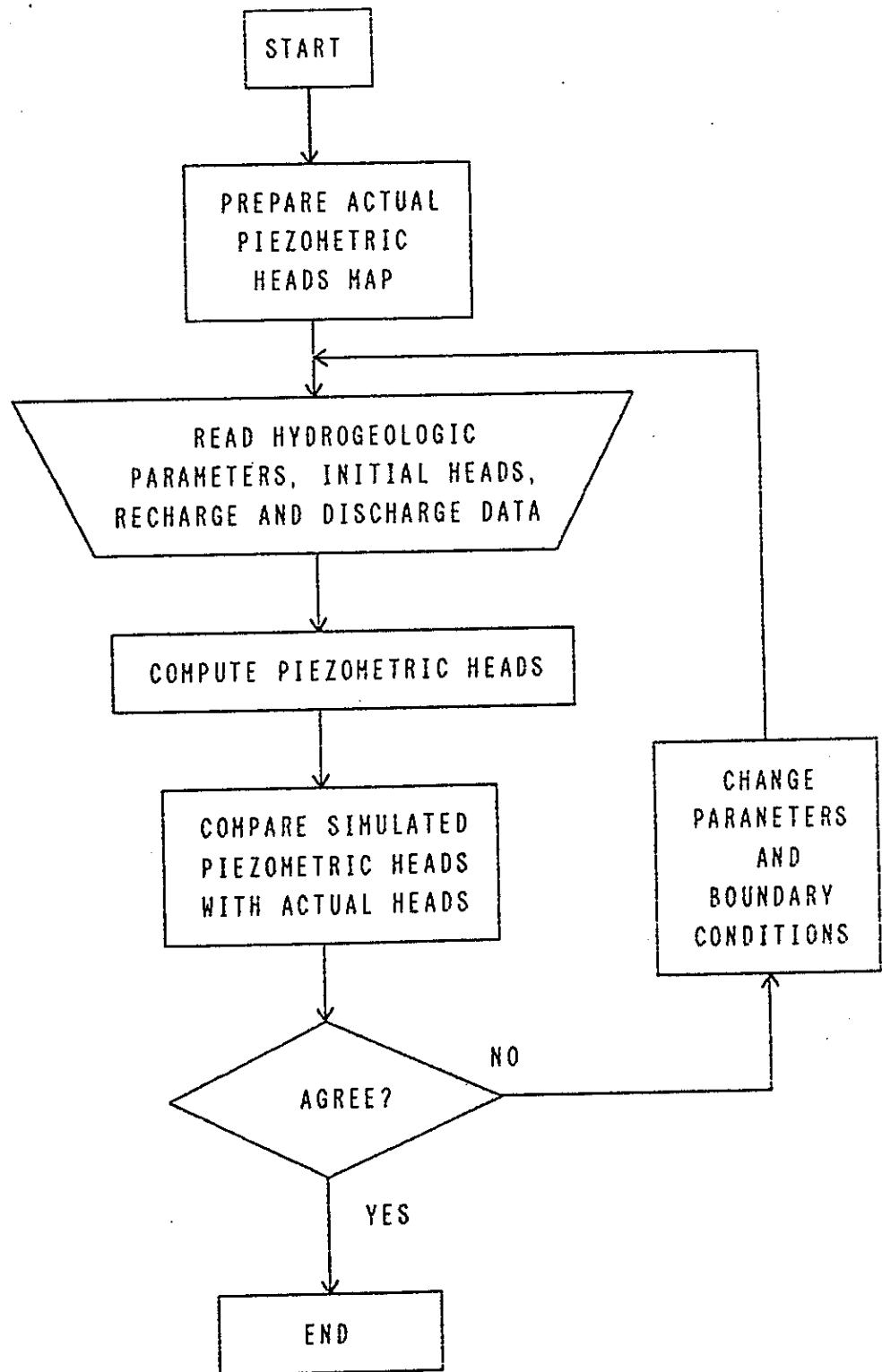


Figure 3.2 General Flow Chart of Model Calibration



This model can be applied to a wide variety of field problems. However, the user should first become aware of the assumptions and limitations inherent in the model. The computer program presented in this report is offered as a basic working tool that may have to be modified by the user for efficient application to specific field problems. The program is written in FORTRAN 77 and is compatible with most high-speed computers.

The groundwater flow model was applied to the Antipolo groundwater basin and the Metro Manila groundwater basin in the study.

### 3.2 MODEL FRAMEWORK

A rectangular finite-element grid should be constructed based on objectives of groundwater modeling, hydrogeological conditions and memory capacity of the computer. The grid spacing of each cell should be uniform. The original Q3P program presented here is written to allow a grid having up to 900 elements or 990 nodes.

Q3P model can be applied to two-dimensional single aquifer problem, quasi three-dimensional single aquifer problem and quasi three-dimensional double aquifer problem. All geohydrologic parameters should be prepared by the x- and y-coordinates.

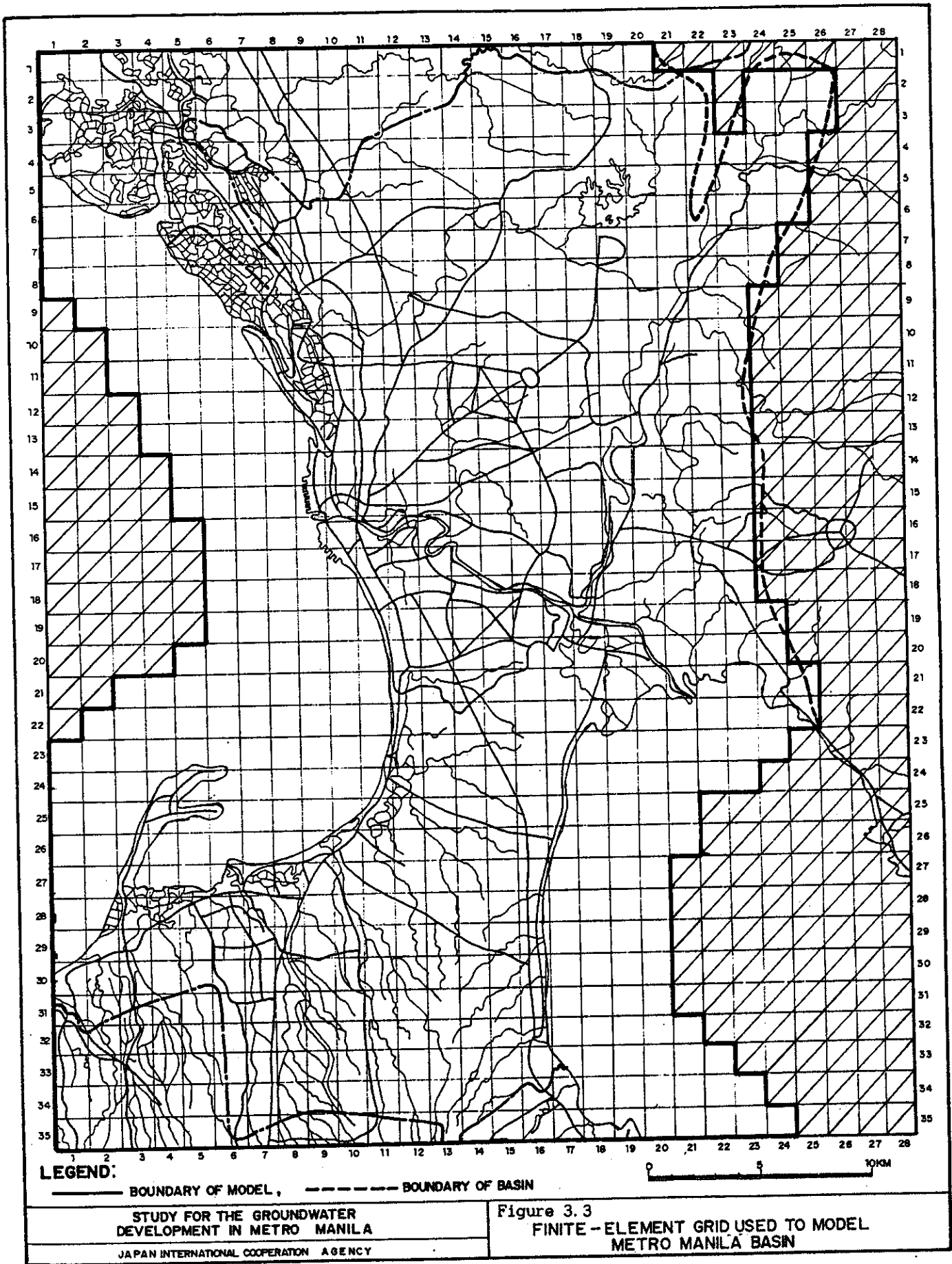
#### 3.2.1 Column Number and Row Number

Column numbers are given from left to right in x-direction and row numbers are given from top to bottom in y-direction. Figure 3.3 shows the finite-element grid used to model the Metro Manila groundwater basin. In the FORTRAN programs I and J represent the row number and the column number, respectively.

#### 3.2.2 Element Number

After fixing the finite element grid, element numbers should be given from the top left element to the bottom right element in the modeled domain in ascending order (see Figure 3.4). The number of the elements located out of the modeled domain should be assigned as 0.

#### 3.2.3 Nodal Number



Nodal numbers should be assigned at each node from the top left node to the bottom right node in the domain in ascending order (see Figure 3.5). The number of the nodes located out of the domain should be assigned as 0.

### 3.3 INPUT DATA

A simplified flow chart of Q3P model is given in Figure 3.6. Q3P needs following input data files.

ELE.DAT : element data.  
NOD.DAT : node data.  
NOP.DAT : data for element specification by nodes.  
HBOUND.DAT : constant-head boundary data.  
KYOKAI.LAB : labels of modeled domain, direct recharge and leakage recharge area.  
T\_03.IND : transmissivity.  
B.IND : thickness of confining layer.  
S.IND : storage coefficient.  
KD\_03.LAB : permeability of confining layer.  
PRM\_03.DAT : generated data file by PARAC (unformatted).  
INI\_03.DAT : initial piezometric heads (unformatted).  
H.IND : water levels of phreatic aquifer.  
QIN30.DAT : discharge data.  
RIN30.DAT : direct recharge data.  
OBSH63\_2.DAT: observation points.  
BLOCK.DAT : block data for water balance calculation.  
Q3PSIM2.PAR : model control card.

Each data file should be prepared as follows. The names of variables shown below are used in Q3P program or data generating program named PARAC. The formats are written in FORTRAN expression. The sample data given in figures were used in the simulation of Metro Manila groundwater basin.

(1) ELE.DAT

*Variables:* NR(I,J)

where I is the row number, J is the column number.

*Format:* (nI4)  
where n is the total number of columns in x-direction.

The element numbers should be given from the top left element to the bottom right element in the modeled domain in ascending order (see Figure 3.4). The element numbers located out of the modeled domain should be assigned as 0.

(2) NOD.DAT

*Variables:* NNO(I,J)  
where I is the grid line number in y-direction and J is the grid line number in x-direction.

*Format:* (nI4)  
where n is the total number of grid lines in x-direction.

The nodal numbers should be given from the top left node to the bottom right node in the modeled domain involving the perimeters in ascending order (see Figure 3.5). The nodal numbers located out of the modeled domain should be assigned as 0.

(3) NOP.DAT

*Variables:* (NOP(I,J), J=1,4)  
where I is the element number. J represents nodal identification number to the corresponding element.

*Format:* (8(4I4))

Each element has 4 (four) nodes. This data file defines each element number by corresponding 4 (four) nodal numbers from the lower left node counterclockwise shown as follows:

```

      4      3
      +---+
      I      I
      +---+
      1      2

```

Figure 3.7 shows the data sequence of NOP.DAT used in the Metro Manila model.

(4) HBOUND.DAT

*Variables:* NNC, (NOHC(I,1), I=1,NNC)  
 HC(I,J)

*Format:* (I4, nI4)  
 where n is the total number of constant-head nodes.  
 (10F8.2)

NNC is a total number of constant-head nodes. NOHC(I,J) is the nodal number assigned as constant-head boundary. HC(I,J) is constant piezometric head of confined aquifer J (J=1 or 2) at node I. The data sequence of HC(I,J) locates from the next line of NOHC(I,1) data sequence. If the model is applied to a quasi 3-D two-confined aquifer model, the boundary conditions of the second confined aquifer are the same with first aquifer (NOHC(I,2) = NOHC(I,1)). The data sequence of HBOUND.DAT is shown in Figure 3.8.

(5) KYOKAI.LAB

*Variables:* KY(I,J)  
 where I and J are the row number and the column number, respectively.

*Format:* (nI1)  
 where n is the total number of columns in x-direction.

KY(I,J) is the label for recharge type identification at element (I,J); 0 indicates leakage recharge, 1 indicates direct recharge, and 9 means out of the modeled domain (see Figure 3.9).

(6) T\_03.IND

*Variables:* IT(I,J)

where I and J are the row number and the column number, respectively.

*Format:* (nI4)

where n is the total number of columns in x-direction.

IT(I,J) is local value of transmissivity ( $m^2/d$ ) at element (I,J). 9999 should be assigned at elements located out of the modeled area (see Figure 3.10).

(7) B.IND

*Variables:* IB(I,J)

where I and J are the row number and the column number, respectively.

*Format:* (nI4)

where n is the total number of columns in x-direction.

IB(I,J) is thickness of the confining layer (m) overlying the first confined aquifer at element (I,J). 9999 should be assigned at elements located out of the modeled area (see Figure 3.11).

(8) S.IND

*Variables:* IS(I,J)

where I and J are the row number and the column number, respectively.

*Format:* (nI4)

where n is the total number of columns in x-direction.

Storage coefficient at element (I,J) can be computed as  $1 \times 10^{(-IS(I,J)/10)}$ . The unit of storage coefficient is dimensionless. 9999 should be assigned at elements located out of the modeled domain (see Figure 3.12).

(9) KD\_03.LAB

*Variables:* DK(I,L)

where I is the number of leakance label for confined aquifer L (L=1 or 2).

LK(I,J)

where I and J are the row number and the column number, respectively.

*Format:* (8F8.0)

(nA1)

where n is the total number of columns in x-direction.

DK(I,L) is permeability of confining layer (m/d) underlain by the confined aquifer L. As many as 16 (sixteen) different values of permeability can be assigned to the elements. There are 16 (sixteen) labels (LK(I,J)) to specify each element viz. 0,1,2,3,4,5,6,7,8,A,B,C,D,E, and F. The first line of DK(I,L) sequence corresponds to the labels from 0 to 7, and the second line corresponds to the labels from 8 to F, respectively (see Figure 3.13).

(10) PRM\_03.DAT

*Variables:* BD(I,J)

T(I,J)

S(I,J)

HF(I,J)

where I is the element number. J (J=1 or 2) is the aquifer number.

*Format:* Unformatted.

FORTTRAN program PARAC generates a geohydrologic parameters file (PRM\_03.DAT) from B.IND, KD\_03.LAB, T\_03.IND, S.IND and H.IND using ELE.DAT, NOD.DAT and KYOKAI.LAB. BD(I,J) is leakance (1/d) at each element which is computed by DK(I,L)/IB(I,J). The units of T(I,J), S(I,J) and HF(I,J) are m<sup>2</sup>/d, dimensionless and masl, respectively. In addition, PRL\_03.LST is also generated by PARAC to check input data.

(11) INI\_03.DAT

*Variables:* HN(I,J)

where I is the nodal number. J (J=1 or 2) is the aquifer number.

*Format:* Unformatted

HN(I,J) is an initial piezometric head at each node. INI\_03.DAT can be generated from INIH.IND using FORTTRAN program MINIH or obtained from the output file (INI\_30.DAT) of Q3P.

The variables and format of INIH.IND are as follows:

*Variables:* INIH(I,J)

where I is the grid line number in y-direction and J is the grid line number in x-direction, respectively.

*Format:* (nF5.0)

where n is the total number of grid lines in x-direction.

INIH(I,J) is a piezometric head (masl) at node (I,J). 9999. should be assigned at nodes located out of the modeled domain.

(12) H.IND

*Variables:* IH(I,J)



where I and J are the row number and the column number, respectively.

*Format:* (nI4)

where n is the total number of columns in x-direction.

IH(I,J) is water level of phreatic aquifer (masl) at element (I,J). 9999 should be assigned at elements located out of the modeled area (see Figure 3.14). H.IND is used to generate PRL\_03.DAT by FORTRAN program PARAC.

(13) QIN30.DAT

*Variables:* (Q(I,J), I=1,NE), J=1,IL

where I is the element number. NE is the total number of elements. J (J=1 or 2) is the aquifer number.

*Format:* (10F10.0)

Q(I,J) is discharge ( $m^3/d$ ) from element number I extracted from aquifer J. In case of nonsteady-state simulation, a sequence of discharge data in each time-step should be prepared and jointed in the same file.

(14) RIN30.DAT

*variables:* R(I), I=1,NE

where I is the element number. NE is the total number of elements.

*Format:* (10F10.0)

R(I) is direct recharge ( $m^3/d$ ) to element number I. In case of non-steady-state simulation, a sequence of direct recharge data in each time-step should be prepared and jointed in the same file.

(15) OBSH63\_2.DAT

*Variables:* NS(I), NW(I), (CN(I,N),N=1,3), SVAL(I), EVAL(I),  
NWOUT(I), OBS(I,J,K)  
where I is observation point number. J is aquifer  
number. K is time-step.

*Format:* (I4,I2,3A8,2F10.4,I1)  
(/8X,12F6.2)

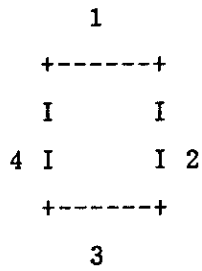
The data sequence of OBSH63\_2.DAT is shown in Figure 3.15. As many as 70 (seventy) observation points can be located in the modeled domain. Each observation point should be located at a particular node NS(I). Piezometric changes of aquifer NW(I) can be observed in each time-step. CN(I,N) is the name of an observation point. A hydrograph at each point can be drawn between minimum level SVAL(I) and maximum level EVAL(I). A hydrograph of the observation point I shall be printed if NWOUT(I) is 1. OBS(I,J,K) is actual piezometric head (masl) of aquifer J at observation point I in time-step K. Q3P can draw hydrographs of both actual and simulated piezometric changes.

(16) BLOCK.DAT

*Variables:* LBL(I)  
I is the element number.  
NL(I)  
I is the line number.  
NLE(I,K),NLP(I,K)  
I is the line number. K is the segment number of  
a line.

*Format:* (40I1)  
(20I4)  
(10(I4,I2))

BLOCK.DAT is a control data file for water balance quantification in each block. LBL(I) shows a block label of each element. NL(I) is the number of segments consisting line I. NLE(I,K) is the element number at which segment K of line I touches. NLP(I,K) indicates position of the side which is defined as follows.



(17) Q3PSIM2.PAR

*Variables:* TITLE

NP, NE, NBAND, IDENT, NSTEPS, IROW, JCOL  
 DT, X1, Y1  
 NC(1), NC(2)  
 KQIN, KHOUT, KHIN, IPP, KPRI  
 NWEL, IHO  
 VIND  
 NBK, NLL  
 NPRINT  
 RRR

*Format:* (A32)  
 (7I5)  
 (3F10.5)  
 (2I5)  
 (4I1,I5)  
 (2I5)  
 (F10.5)  
 (2I5)  
 (I4)  
 (F5.2)

Q3PSIM2.PAR has various parameters for the model control. Its data sequence is shown in Figure 3.16. Meanings of the variables are as follows:

- TITLE: Title of the simulation.
- NP : Number of nodes in the modeled domain.
- NE : Number of elements in the modeled domain.
- NBAND: Band width for finite-element matrix.

IDENT: Type of analysis  
       1: horizontal 2-D 1 aquifer  
       2: quasi 3-D 1 aquifer  
       3: quasi 3-D 2 aquifers

NSTEP: Number of time-steps.

IROW : Number of elements in y-direction.

JCOL : Number of elements in x-direction.

DT   : Duration of one time-step (day).

X1   : Grid spacing in x-direction (m).

Y1   : Grid spacing in y-direction (m).

NC(1): Number of constant-head nodes in 1st aquifer.

NC(2): Number of constant-head nodes in 2nd aquifer.

KQIN : Option for type of simulation  
       (1: steady-state, 2: nonsteady-state).

KHOUT: Option for generating a file of simulated piezometric heads  
       (1: last time-step, 2: every time-step).

KHIN : Option for file type of initial piezometric heads  
       (0: formatted, 1: unformatted).

IPP   : Option for printing input data list  
       (0: do not print, 1: print).

KPRI : Number of time-steps in which simulated piezometric maps to be  
       printed.

NWEL : Number of observation points.

IHO   : Option for printing actual piezometric changes  
       (0: data not available, 1: print).

VIND : Spacing for printing simulated piezometric changes.

NBK   : Number of blocks for quantifying water balance.

NLL   : Number of lines for quantifying water balance.

NPRI : The number of time-step in which simulated piezometric heads to  
       be printed.

RRR   : Magnification of recharge intensity.





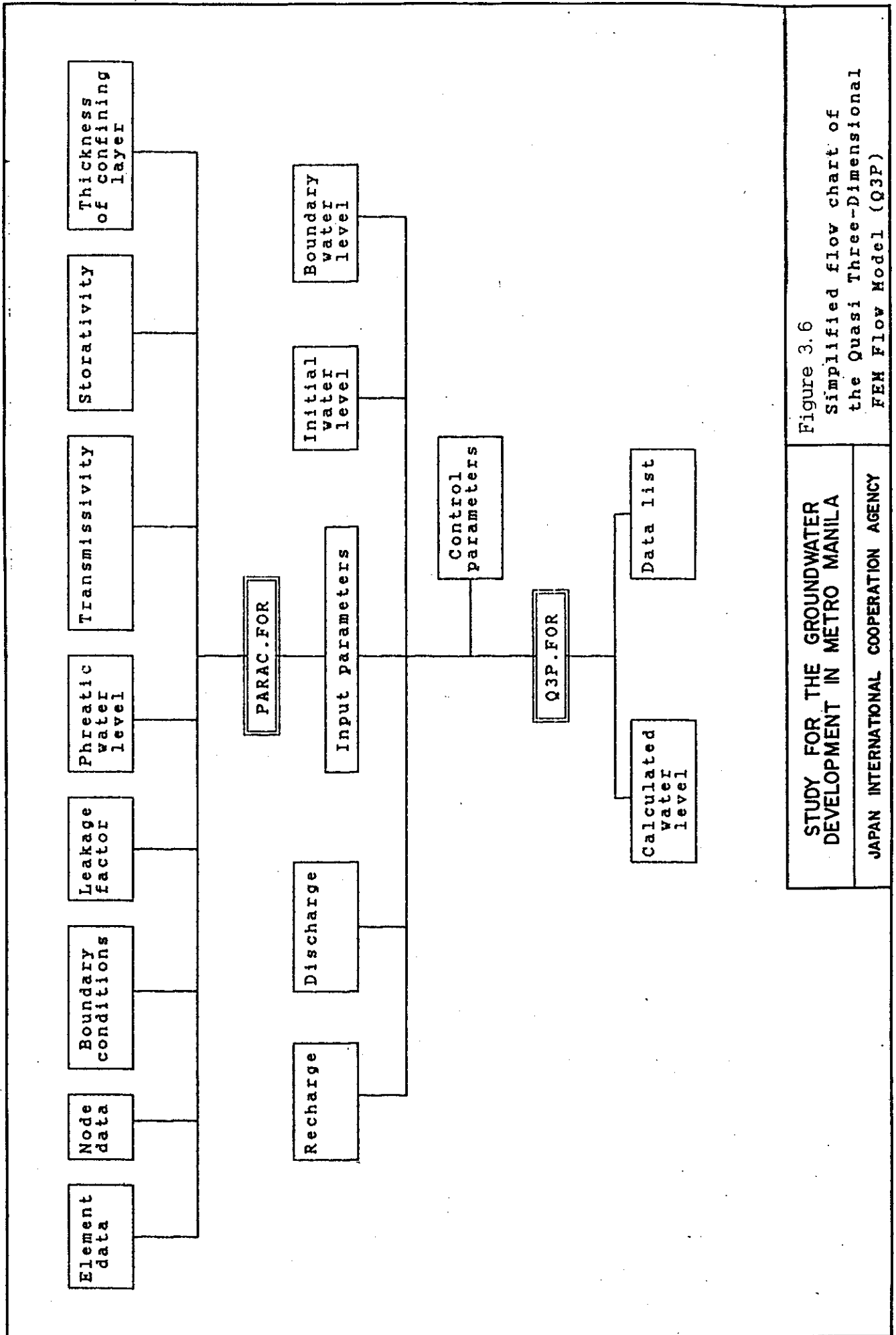


Figure 3.6  
Simplified flow chart of  
the Quasi Three-Dimensional  
FEM Flow Model (Q3P)

STUDY FOR THE GROUNDWATER  
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JAPAN INTERNATIONAL COOPERATION AGENCY

















	0	1	2	3	4	5	6		
	1234567890123456789012345678901234567890123456789012345678901234								
1	1.0E-1	5.0E-3	2.0E-3	1.0E-3	7.0E-4	5.0E-4	2.0E-4	1.0E-4	1
2	7.0E-5	5.0E-5	2.0E-5	1.0E-5	7.0E-6	5.0E-6	2.0E-6	1.0E-9	2
3	AAFFFFCCCCC311111122222222				1	KL1			3
4	AAFFFFFCCCC322111111111222				2				4
5	66FFFFFFFCCC422111111111222				3				5
6	66FFFFFFF5221111111111222				4				6
7	6FFFFFFF88522111111111222				5				7
8	666FFFFFF7363111111111222				6				8
9	66666FFFF33564211111111222				7				9
10	666555A76788543211111111222				8				10
11	F844444557B8655551111111222				9				11
12	FF6455A33666434AB21111222222				10				12
13	FF866F333766334AB2222222222				11				13
14	FFFAAA367873357BB54443222222				12				14
15	FFFAAA356776657643255222222				13				15
16	FFFFAA52224A8562223633222222				14				16
17	FFFFFAA865B76722565333222222				15				17
18	FFFFFFF55843C531122222222				16				18
19	FFFFFFF45421222222222222				17				19
20	FFFFFFF5325532332211222				18				20
21	FFFFFFF2247422388211222				19				21
22	FFFFFFF522277423488522222				20				22
23	FFFFFFF53334465345AAA55444				21				23
24	FFFFFFF54443456655AAA55444				22				24
25	FFAFFFF44444666865588884444				23				25
26	FF3147FF44444642213444444444				24				26
27	FFA857FF44423522112344444444				25				27
28	FF67775445622441112244444444				26				28
29	FFFFFF7577356642222444444444				27				29
30	FFFFFF46A722342223444444444				28				30
31	FF6333126CC11331112344444444				29				31
32	AAA1111121111880113444444444				30				32
33	AAA311111112321124444444444				31				33
34	AAA411111133222223444444444				32				34
35	4444444444566633334444444444				33				35
36	44444444445AAAAA66444444444				34				36
37	44444444444AAAAAA4444444444				35				37
	1234567890123456789012345678901234567890123456789012345678901234								
	0	1	2	3	4	5	6		

Figure 3.13 KD\_03.LAB for the Metro Manila Groundwater basin Model





	0	1	2	3	4	5	6	7	8
	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890
1	263	1CLC			-150.0		-50.01		
2	290	1QCT			-50.0		50.01		
3	412	1PSG			-100.0		0.01		
4	448	1MKT			-100.0		0.01		
5	564	1CVC			-100.0		0.01		
6	574	1PRN			-100.0		0.01		
7	615	1LPS			-50.0		50.01		
8	QCT								
9					999.99999		99999.99999		99999.99999
10					999.99999		99999.99999		99999.99999
11					999.99999		99999.99999		99999.99999
12	VLZ								
13					999.99999		99999.99999		99999.99999
14					999.99999		99999.99999		99999.99999
15					999.99999		99999.99999		99999.99999
16	TYY								
17					999.99999		99999.99999		99999.99999
18					999.99999		99999.99999		99999.99999
19					999.99999		99999.99999		99999.99999
20	MKT								
21					999.99999		99999.99999		99999.99999
22					999.99999		99999.99999		99999.99999
23					999.99999		99999.99999		99999.99999
23	CVC								
24					999.99999		99999.99999		99999.99999
25					999.99999		99999.99999		99999.99999
26					999.99999		99999.99999		99999.99999
27	LPS								
28					999.99999		99999.99999		99999.99999
29					999.99999		99999.99999		99999.99999
30					999.99999		99999.99999		99999.99999
31	MTL								
32					999.99999		99999.99999		99999.99999
33					999.99999		99999.99999		99999.99999
34					999.99999		99999.99999		99999.99999

Figure 3.15 OBSH63\_2.DAT for the Metro Manila Groundwater Basin Model

```

0          1          2          3          4
12345678901234567890123456789012345678901234567

1  MSA NONSTEADY-STATE, 30STEPS 1
2  829  754  30   1  30  35  28 2
3      365.    1350.    1380. 3
4    48  48 4
5 2211  1  ! TEI=1110  1  HITEI=2210  1 5
6    7  1 6
7      5.0 7
8    2  4  !!!NBK, NLL 8
9    30 9
10 0.30 10

1234567890123456789012345678901234567
0          1          2          3          4

```

Figure 3.16 Q3PSIM2.PAR for the Metro Manila Groundwater Basin Model

### 3.4 MODEL OPERATION

General flow of the model operation is shown in Figure 3.17. Data preparation and model calibration are the most important works for using the model.

Input data files mentioned above should be carefully prepared. Several FORTRAN programs are needed for data processing. The user should pay attention to data formats, units of values, miss-typing, file name, etc.

If the user creates/modified FORTRAN programs, the user must compile and link those programs using a FORTRAN Compiler to create executable (\*.EXE) files. Then the user can run those programs. If the user uses Pro FORTRAN-77 Compiler, source programs are compiled and linked in the following manner:

1. Specify source program name as '\*.FOR' ('\*' is the program name).
2. Confirm 'PATH=C:\PROFORT', where Pro FORTRAN-77 Compiler exists.
3. Create \*.OBJ file. Type 'F77 \*' and press <ENTER>.
4. Change directory to PROFORT. (Type 'CD C:\PROFORT' and press <ENTER>).
5. Create \*.EXE file. Type 'PROLINK C:\###\\*, F77LIB7B/S' and press <ENTER> (### is the subdirectory name where the source program exists).
6. Change directory to ### (Type 'CD C:\###' and press <ENTER>).
7. Find \*.EXE file and run the program (Type '\*' and press <ENTER>).

The study team prepared several FORTRAN programs to process and arrange data (see APPENDIX). All these programs can be run in Batch Files (\*.BAT). The user is recommended to use Batch Files so as to save time and avoid mistakes during complicated operation procedure.

Some of the less reliable geohydrologic parameters are modified/identified during model calibrations. The main procedure of the model calibration is to specify boundary conditions and to identify some poor reliable hydrogeologic parameters. Generally the model is verified by the comparison of calculated piezometric heads with actual piezometric heads. Sometimes this work is repeated more than 100 times until the computed heads show a good agreement with the actual heads.

After the calibration, the model can be used to predict future piezometric heads. Based on the future groundwater use plans and future recharge estimates, several discharge data and direct recharge data are prepared using same formats as QIN\_30.DAT and RIN\_30.DAT. The actual piezometric heads at present are generally used as the initial heads for future simulation.

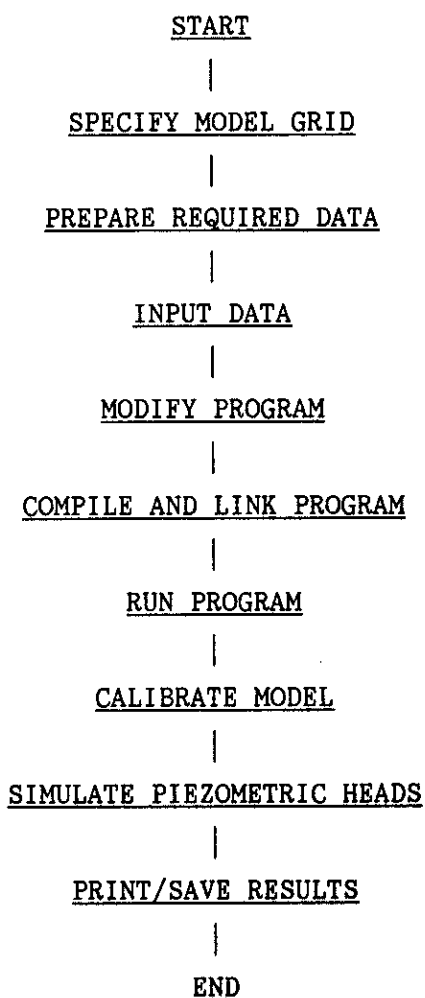


Figure 3.17 General Flow of Model Operation

### 3.5 OUTPUT DATA

Q3P generates several output files. Followings are essential output files involving results of calculation.

Q3P\_30.LST

INI\_30.DAT

BLOCK.OUT

Q3P\_30.LST is the most important output file. It involves simulated piezometric heads in each time-step and piezometric changes at observation points as well as those hydrographs. If IPP is 1, lists of input data are also generated in this file.

INI\_30.DAT is an unformatted file of piezometric heads in the last time-step of simulation. This file is useful when the calculated piezometric heads are employed as initial heads for subsequent simulation. For example, if the data of actual heads are not available at the beginning stage of nonsteady-state simulation, INI\_30.DAT obtained from the preceding steady-state simulation can be used as estimated initial piezometric heads for the nonsteady-state simulation.

Results of water balance computation in the fixed blocks are generated in BLOCK.OUT. The water balance components viz. direct recharge, leakage recharge, discharge, lateral inflow/outflow and change of storage in selected blocks are given in the output tables.

INI\_30.DAT and Q3P\_30.LST are used for graphics.

### 3.6 GRAPHICS

Computer graphic technique helps immediate graphical understanding of the results of simulation. Also the user can easily compare the results with other results obtained from different data input because the graphical representations are drawn in the same form.

Two types of graphic techniques are presented in this manual. One is the representation of piezometric changes at observation points. The other is the drawing of equipotential contours (or isolines) of piezometric

heads.

### 3.6.1 Piezometric Heads Changes

The output file Q3P\_30.LST contains the piezometric heads changes throughout the simulation period at the observation points selected in OBSH63\_2.DAT. Though this output file shows the simulated piezometric heads changes using simplified graphics, it is recommended to use other graphic software.

The study team used LOTUS-123 to draw simulated hydrographs at the observation points. LOTUS-123 is one of the most common and useful software of worksheet which involves graphic functions. It is assumed that the user has already understood basic operations of the LOTUS-123.

A FORTRAN program FOBS has been made to find computed piezometric heads data from Q3P\_30.LST. Q3P\_30.PRN is generated from the program. The sequences of piezometric heads values are arranged in the file. The LOTUS-123 can retrieve Q3P\_30.PRN as a text file. Then using the graphic commands of LOTUS-123, beautiful hydrographs can easily be drawn.

If the user defines necessary parameters of the graphic functions and saves this LOTUS data file, then the user can utilize this LOTUS data file and draw hydrographs in the same format from next time.

### 3.6.2 Contour Map

Two programs for drawing contours have been prepared. The programs are written in BASIC because the BASIC language has various graphic functions. The study teams executed the programs using TOSHIBA BASIC Interpreter Ver. 3.2 under Japanese MS-DOS Ver.3.1. The TOSHIBA BASIC is following the Microsoft BASIC so that user can easily modify the programs into other BASIC Interpreters/Compilers such as IBM PC BASIC or GWBASIC which can be run under the English MS-DOS.

Followings are the contour map programs used for the Metro Manila groundwater basin model.

MSAPLTS.BAS : draw small scale contour map.

MSAPLTL.BAS : draw large scale contour map.  
CONXYZ.MAP : draw contour map with locations of  
observation points.

The original program of MSAPLTS.BAS and MSPLTL.BAS is shown in Kinzelbach (1986) as SAMPLE PROGRAM 5. The original program of CONXYZ.MAP is shown in Shiono et al. (1988) as XYZCON.MAP. Those original programs were modified by the Study Team for the TOSHIBA BASIC Interpreter.

The programs can draw simulated piezometric contour maps in Metro Manila. The contour intervals, minimum and maximum values etc. can be specified from the keyboard.

The graphic programs require following input data files.

MSAPLTS.BAS : CALS.PLT  
MSAPLTL.BAS : CALD1.PLT (for northern map)  
CALD2.PLT (for southern map)  
CONXYZ.MAP : HDN.OUT (for northern map)  
HDS.OUT (for southern map)  
CONT.LOC (observation points data)

The input data files mentioned above except CONT.LOC are produced by the following data input programs written in FORTRAN. These programs produce the input data files from INI\_30.DAT, which are obtained from Q3P program.

MPRO5DS : Generate input data file for MSAPLTS.BAS  
MPRO5DL : Generate input data files for MSAPLTL.BAS  
MCONT : Generate input data files for CONXYZ.MAP

The user should modify dimension sizes and some parameters in the programs depending upon the user's problems.

## 4. SOLUTE TRANSPORT MODEL

### 4.1 MODEL ABSTRACT

The two-dimensional solute transport and dispersion model (MOC model) used in the study was originally devised by L. F. Konikow and J. D. Bredehoeft in 1978.

MOC is a two-dimensional model for the simulation of non-conservative solute transport in saturated groundwater systems. It computes changes in the spatial concentration distribution over time caused by convective transport, hydrodynamic dispersion, mixing or dilution from recharge, and chemical reactions.

The chemical reactions include first-order irreversible rate reaction (such as radioactive decay), reversible equilibrium-controlled absorption with linear, Freundlich or Langmuir isotherms, and reversible equilibrium-controlled ion exchange for monovalent or divalent ions.

The model assumes that fluid density variations, viscosity changes and temperature gradients do not affect the velocity distribution. MOC does allow modeling heterogeneous and/or anisotropic aquifers.

MOC couples the groundwater flow equation with the non-conservative solute transport equation. The computer program uses the Alternating Direction Implicit (ADI) procedure or Strongly Implicit Procedure (SIP) to solve the finite difference approximation of the groundwater flow equation. The SIP procedure for solving the groundwater equation is most useful when aerial discontinuities in transmissivity exist or when the ADI solution does not converge.

MOC uses the method of characteristics to solve the solute transport equation. It uses a particle tracking method to represent convective transport and a two-step explicit procedure to solve the finite difference equation that describes the effects of hydrodynamic dispersion, fluid sources or sinks, and divergence of velocity.

The explicit procedure is subject to stability criteria, but the program



automatically determines and implements the time-step limitations necessary to satisfy the stability criteria.

MOC uses a rectangular, block-centered, finite-difference grid for flow and transport calculations. The grid size for flow calculations is limited to 40 rows and 40 columns. The grid size for transport calculations is limited to 20 rows and 20 columns which can be assigned to any area of the flow grid.

The program allows spatially varying diffuse recharge or discharge, saturated thickness, transmissivity, boundary conditions, initial heads and initial concentrations and unlimited number of injection or withdrawal wells.

MOC model can be applied to one- or two-dimensional problems involving steady-state or transient flow. The solute transport model was originally developed for plain two-dimensional problem, but it was applied to the vertical two-dimensional multiple aquifer system in Las Pinas area to reveal the mechanism of saline water intrusion (see Figure 4.1).

#### 4.2 MODEL FRAMEWORK

A rectangular, block-centered, finite-difference grid should be constructed depending on the objectives of solute transport modeling, hydrogeological conditions and the limitations of grid size for both flow calculation and transport calculation. The original MOC program presented here is written to allow a flow grid having up to 40 rows and 40 columns in which a transport grid can be located up to the size of 20 rows and 20 columns.

If both the transport equation and the flow equation are solved on the same grid, the number of nodes in the x- and y-directions,  $NX$  and  $NY$ , respectively are restricted to 20.

The transport equation may be solved on a smaller grid than the grid on which the flow equation is solved. This may yield savings in computation time and storage for problems in which the hydraulic gradients within the area of interest for transport are influenced by hydraulic stresses and/or boundary conditions outside of the area in which solute transport

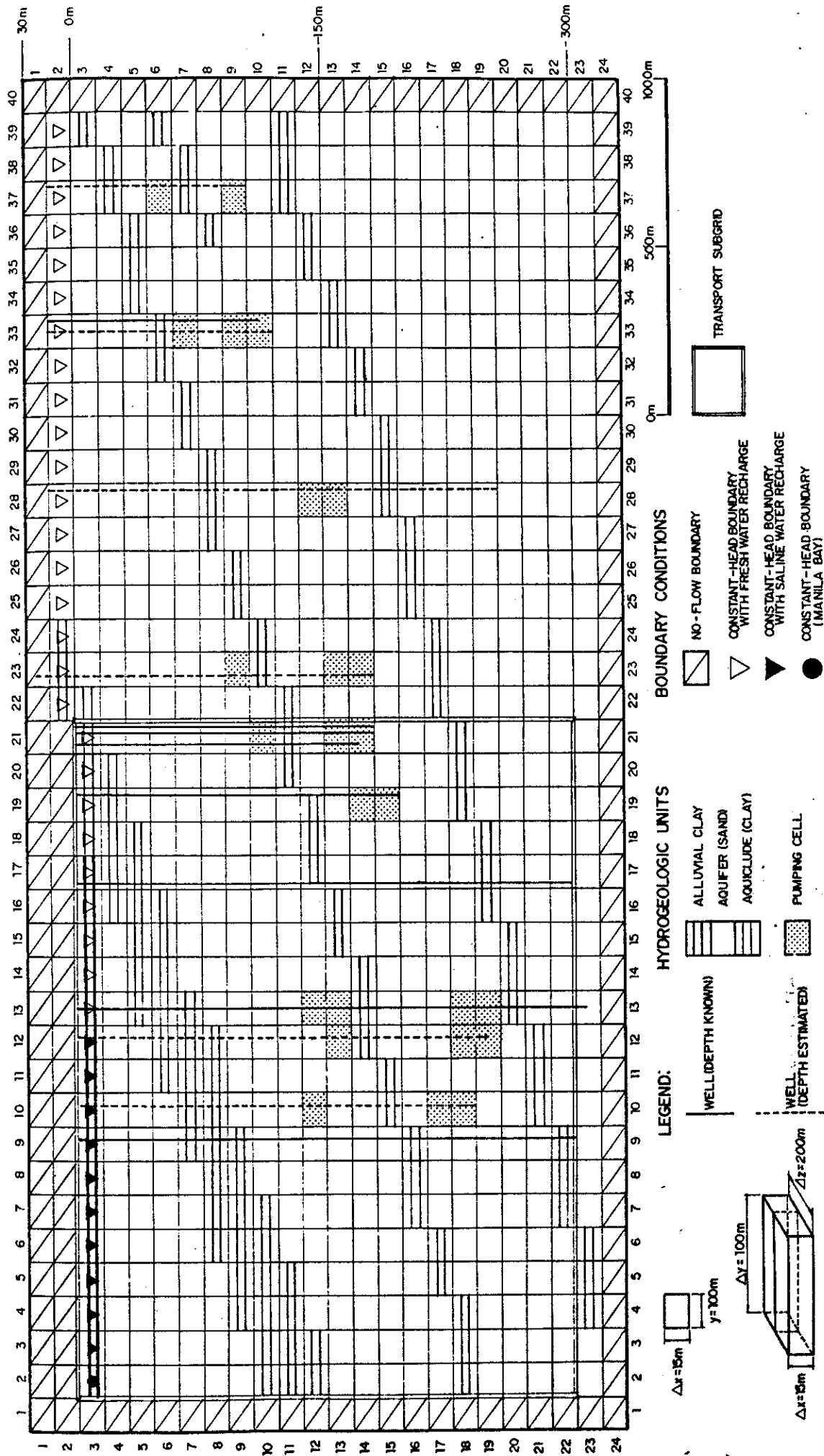


Figure 4.1  
 VERTICAL TWO-DIMENSIONAL GRID FOR THE SOLUTE  
 TRANSPORT AND DISPERSION MODEL IN LAS PINAS

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is occurring.

The approach is to define a primary finite-difference grid for the flow model. A smaller, secondary subgrid for transport is then defined within the coordinates of the primary grid.

To specify different grid size for the transport and flow grids, specify NX as a negative value greater than -40. Then enter a positive value for NY in the range (1 to 40). The program will then prompt for four additional inputs: MX, MY, MMX and MMY. MX and MY are, respectively, the x- and y-coordinates within the primary grid of the upper-left node of the transport subgrid. MMX and MMY are the respective grid coordinates of the lower-right node of the transport subgrid.

For example, if the primary grid is 20 by 20 (that is, NX = -20 and NY = 20) , and if the subgrid for transport was to be 10 by 10, with the upper-left node of the subgrid corresponding to node (3,4) of the primary grid, then the following specifications would be made: MX = 3, MY = 4, MMX = 12 and MMY = 13.

It is noted that the "window" for the transport subgrid can overlap all or any part of the primary grid, but cannot extend beyond it. Also note that unless the subgrid overlaps the first or last row or column of the primary grid, which are no-flow boundaries, then all nodes of the subgrid can be "active" nodes.

Finally, the subgrid should be located so that there will not be a significant amount of convective transport across the subgrid boundary, or else the accuracy of the solution will be adversely affected.

#### 4.3 DATA INPUT

An input processor MOCINP was provided in the MOC package. MOCINP is used to create or modify the data file required by MOCADI or MOCSIP.

The user should become familiar with the inputs required by MOC prior to using MOCINP. The USGS MOC reports and associated MOC Computer Program Updates Note (see Appendix) describes all inputs. MOCINP provides convenient means for producing the input data files required by MOC.

### 4.3.1 MOCINP and MOC

The preprocessor MOCINP is written to enable its user to prepare data set for the model USGS-2D-TRANSPORT/MOC. The functional relationship between the preprocessor and the model is illustrated in Figure 4.2. After preparing a data file using MOCINP, you will run MOC separately.

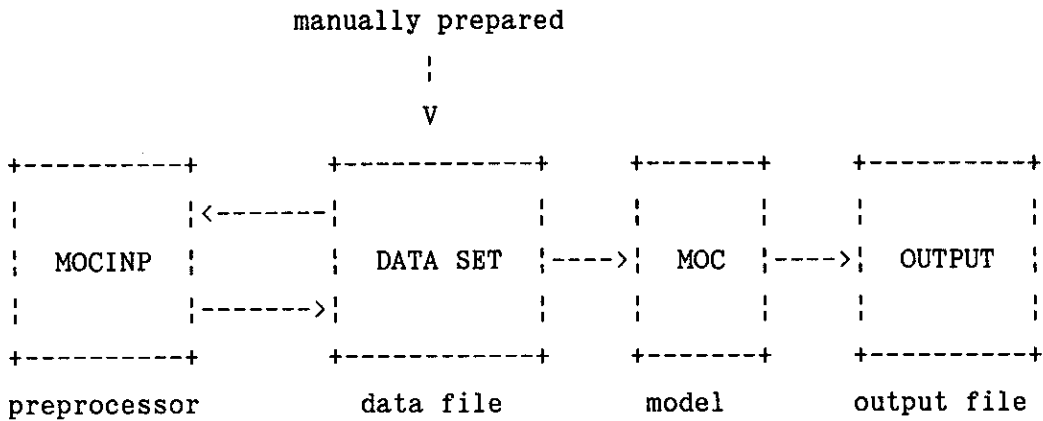


Figure 4.2 Relationship between MOCINP and MOC

The model will use the data file as if it were prepared manually. Thus the preprocessor remains transparent to the model.

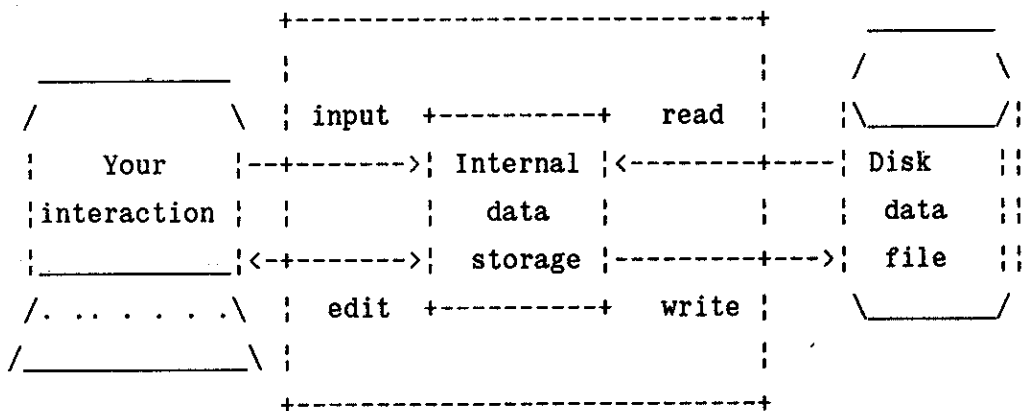


Figure 4.3 Functions of MOCINP

The preprocessor has four major functions. They are: 1. prepare a fresh data set; 2. modify current (internal) data; 3. read data from a disk file; and 4. write data to a file. As illustrated in Figure 4.3, an internal storage space is used to perform these functions.

#### 4.3.2 MOCINP Usage

MOCINP has following files:

MOCINP.EXE : MOC input processor  
MOCINPD.TXT : Text file containing MOC menus

The user can run MOCINP to create or modify the data file from TECSOFT menu. Then the user can input data as following procedure.

##### 1) Main Menu

Example uses of MOCINP are:

1. User prepares a data set (option 1), edits it (option 2) to correct any mistake, saves it on a disk file (option 4), and exits (option 6).
2. User reads an existing disk file (option 3), modifies the data using MOCINP editor (option 2), saves it on the same (or another) disk file (option 4), and exits (option 6).
3. User reads an existing file (option 3), views it using the editor (option 2) without making any corrections, and exits (option 6).
4. User reads a manually-prepared data file (option 3) just to see if the format is correct, and exits (option 6). Running MOCINP to check the format of data files, precludes the need to run the model to do the same.

MAIN MENU  
-----

1. Enter new data
2. Edit current data
3. Read data from a file
4. Write data to a file
5. See help modules
6. Exit MOCINP

Enter option number:

Figure 4.4 Main Menu of MOCINP

Sometimes, the user may inadvertently choose to exit MOCINP forgetting to save the current data set. This may result in a loss of your valuable time. To prevent such accidental termination of a session, MOCINP keeps track to see if the latest version of data has been saved on a disk file. If not, it issues a 'reminder' message at the time of termination. You may then ignore the message and choose option 6 to exit, or save the data (option 4) and then exit.

The four options, input, edit, read, and write are chosen from a MAIN MENU screen shown below. At the end of each option, you are brought back to the main menu.

## 2) Cards and Screen

The variables of MOCINP are grouped together in the same manner as it is done in the MOC input data instruction. Cards 1 through 3, and data

sets 1 through 10 are identical to their representation in the model documentation. These cards and data sets will be referred hereafter as just 'cards.'

During inputting, reading or writing options, the variables are handled in the same order as they appear in the MOC input data instruction. For editing, however, a card may be accessed at will.

While you are inputting or editing data, a single card is handled at any time. A separate screen is allotted for each card. For clarity, some cards are allotted more than one screen.

The general screen layout for the input and edit screens is shown in Figure 4.5. The cursor always stops at the location of each underline '\_' character prompting you for keyboard entry. In the space between top and bottom lines, User - MOCINP interaction is carried out in handling the data.

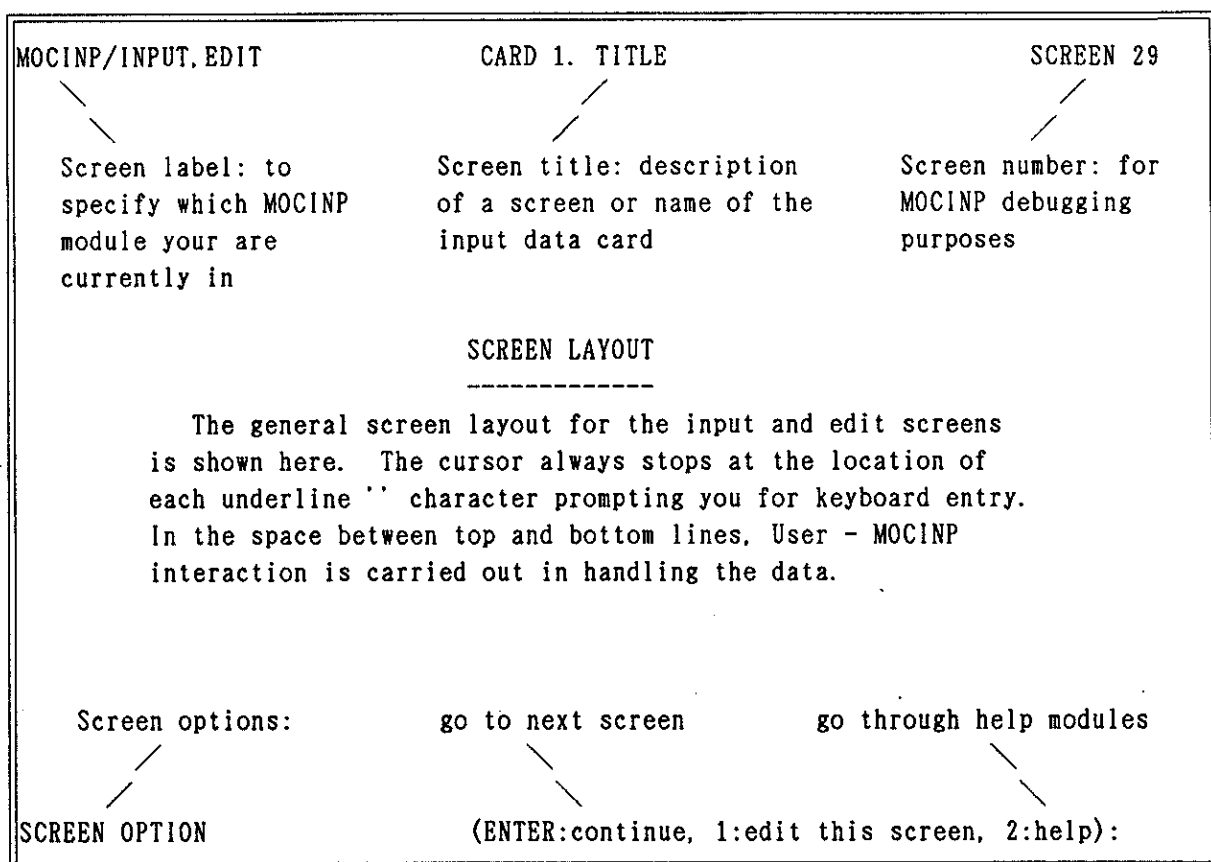


Figure 4.5 General Screen Layout of MOCINP

### 3) Input Procedure

A fresh data file for MOC can be prepared using MOCINP input option. Once this option is chosen, you are taken through all the input screens in sequence. Steps involved in preparing data for each card are:

step 1. The text screen corresponding to the card is shown.

step 2. Cursor stops at each inquiry and prompts for a value. You should type the value and hit <ENTER>. MOCINP checks this value against acceptable values. If invalid, the cursor prompts for another value. If valid, the cursor moves to the next inquiry. Acceptable values for the variables are tabulated in the help module, 'MOC Input Variables.'

step 3. At the bottom of the screen, you are given option to redo any variable's value on the screen. The help module, 'Screen Editing' describes this procedure. If the values entered are satisfactory, you should hit <ENTER> to go to next screen.

For assigning values to two-dimensional array variables, a special procedure is used. This procedure is described in the help module, 'Block Assignment for Arrays.'

The screens used during input option may also be accessed using the MOCINP editor. Therefore, any mistake in the input data can be corrected later using the edit option.

### 4) Edit Procedure

The MOCINP editor may be used to review, and modify if necessary, the data entered using input option or data read from a disk file.

The steps involved are:

step 1. A menu screen containing names of all the data cards are shown to you first (Figure 4.6). The cards are given identification numbers 1 through 13. Any of the cards may be accessed by



Select a screen you want to edit or review, and enter its number.

	cards	number
	-----	-----
card 1. Title . . . . .		1
cards 2, 2a & 3a. Control cards I, Ia & IIa. .		2
card 3. Control card II . . . . .		3
data set 1. Observation points. . . . .		4
data set 2. Wells . . . . .		5
data set 3. Transmissivity. . . . .		6
data set 4. Aquifer thickness . . . . .		7
data set 5. Recharge/discharge. . . . .		8
data set 6. Node identification matrix. .		9
data set 7. Instruction for node id's .		10
data set 8. Initial head. . . . .		11
data set 9. Initial concentration . . .		12
data set 10. Additional pumping periods.		13
All cards in sequence . . .		14

Selection (ENTER to exit):

Figure 4.6 Menu Screen for Screen Selection

entering the corresponding id number. Just hitting <ENTER> (equivalent to typing 0 and hitting <ENTER>) at this point will take you back to MOCINP main menu.

- step 2. For each card accessed, the corresponding text screen is shown first.
- step 3. The current values of variables on the screen are then displayed.
- step 4. At the bottom of the screen, you are given option to modify any value on the screen. This procedure is described in the help module, 'Screen Editing.' If the values on screen are satisfactory you should hit <ENTER> to go to editor menu.

Using the procedure described above, you can access only one card at a time. Sometimes, it may be necessary to review all the 13 cards. To do

this, an identification number of 14 is provided in the editor menu. By choosing this option you can go through all cards in sequence along with their current data, and modify any card if necessary.

As with the input option, array variables are edited using the special procedure which is described in the help module, 'Block Assignment for Arrays.'

## 5) Screen Editing

Screen editing procedure is used to modify the data currently on screen. The steps involved are:

1. Once this option is chosen, the cursor goes to the first data value and prompts.
2. If the value is OK, just hit <ENTER> key. This is equivalent to entering a zero. The cursor goes to next value and prompts.
3. If you want to modify the value, type the new value and hit <ENTER> key. MOCINP checks this value against acceptable values. If it is valid the new value is printed on screen, and the cursor goes to next value. If it is invalid cursor stays at the same location.

NOTE: If the new value you want to enter is 0, type a letter in the alphabet (ex: Z) first and hit <ENTER>. The cursor stays on. Now type 0 and hit <ENTER>.

The following example illustrates the procedure. The location of cursor at any point is shown by a '^' character under the location. Let us assume that the user wants to leave NX as it is and change NY to 18.

1. First cursor prompts at NX value.

```
NX                               No. of nodes in x-direction:   15
NY                               No. of nodes in y-direction:   20
```

2. NX value of 15 is OK; therefore user hits <ENTER>. Cursor goes to



3	15
-	-
-	-

To ADD an entry to the table:

The value of NVAR must be increased by 1. In general, NVAR is specified in a different card. Therefore, you must first access the screen containing NVAR, and modify its value to 4. When you come back to the screen containing table of VAR, it would look like this:

NVAR            Number of entries of VAR: 4

Serial No.	VAR
-----	-----
1	37
2	21
3	15
4	0
-	-

Notice that VAR(4) is assigned a value of 0. Now use screen editing procedure to change VAR(4) to the new value.

To DELETE an entry from the table:

Let us say you want to delete entry number 1. Using the screen editor modify value VAR(1) to that of VAR(2), and value of VAR(2) to that of VAR(3). Leave value of VAR(3) as it is. The table before and after this editing is shown below.

NVAR            Number of entries of VAR: 3

BEFORE EDITING

AFTER EDITING

Serial No.	VAR	Serial No.	VAR
-----	-----	-----	-----
1	37	1	21
2	21	2	15

Now go back to the control card specifying the value of NVAR and modify NVAR to 2.

If the aquifer is nonhomogeneous with respect to a parameter, such as transmissivity, aquifer thickness, etc., the value of the parameter must be specified at each node. If many nodes share a common value for the parameter, it will be easier to assign a single value to a block of nodes rather than assigning values to them individually.

In the illustration, box ABCD	col 1 . . .	NC
represents the aquifer and	row 1 A-----B	
box EFGH is a block of zone	.	
where nodal values of a parameter	.   E-----F	
are the same.		
AD is column 1; BC is column NC; AB	H-----G	
is row 1; and DC is row NR; where,		
NC and NR represent the number	NR D-----C	
of columns and rows in the aquifer,		
respectively.		

The block EFGH is bound by columns EH and FG, and rows EF and HG. To specify EFGH these two columns and rows must be given by the user.

Many possible block structures exist. A block may have only one column (eg. block AB), one row (eg. block CD), or one node (eg. X). Some blocks may overlap (eg. blocks EFGH and IJKL). If block IJKL is specified after EFGH, the value specified for IJKL will replace that for EFGH for nodes common between these two blocks. Therefore, the order in which the blocks are specified is important.



and value for block assignment, the following line is displayed on the screen.

```
COLUMNS (begin: _ ,end: _ ) ROWS (begin: _ ,end: _ ) VALUE: _
```

Choosing edit screen option, you may specify rows and columns of block and the parameter value in that block. Type -1 for a row or a column prompt to scroll to the next window.

The values you entered are checked then for possibility of forming a block. For 'line' blocks, either columns or rows will have the same beginning and ending values. If a block is possible, the value is assigned to nodes within the block, and the display is altered accordingly.

#### 7) Read Option

Using the read option you can read the contents of a data file for MOC. MOCINP reads the data file in the same manner as MOC does. If MOCINP and MOC are compiled using the same FORTRAN compiler, their interpretation of the input data format will be identical.

##### Procedure:

In the first read option screen, you will enter the name of the disk file to read. MOCINP checks to see if the file exists. If not, it prompts you for another file name.

A monitoring feature is provided in the next screen. The names of all data cards are displayed first. When a card is read successfully, a character 'X' appears next to the card name on this screen. The monitoring process is useful while reading data that was prepared using a text editor. If there is a format error on a card, MOCINP stops reading and displays an error message at the bottom of the screen. You should note down the erroneous card, exit MOCINP, and edit the data file using a text editor.

#### 8) Write Option

The write option is used to prepare an input data file for MOC with the current data in MOCINP.

**Procedure:**

If you have read a data file prior to using this option, you may choose to replace the same file with the modified data. Otherwise, you will be asked to enter a new file name. As in the read option, a monitor screen is then displayed to indicate the cards prepared in the disk file.

An important step in this procedure is specification of the file name. If the FORTRAN compiler used on this computer allows error trapping while opening disk files, this feature would have been incorporated in MOCINP. Otherwise, if error condition occurs while opening a disk file, it may result in loss of your data.

A brief discussion of file names is presented next.

#### 4.3.3 MOC Input Variables

The range of values an input variable can have is set at the time of programming MOCINP. It is based on one or more of the following:

1. Definition of the variable.
2. Allocation of storage space for the variable, especially if it is an array.
3. Format identifier used by MOC to read the value of the variable.
4. Format identifier used by MOCINP to write the value in a data file.

The ranges set for this version of MOCINP are given in Table 4.1. The variables are listed in alphabetical order. For clarity, the array variables are grouped together and are listed at the end of the table.



Table 4.1 MOC Input Variables

variable	type	range of values	output format
ANFCTR	real number	0.0 <= ANFCTR	F5.2
BETA	real number	0.0 <= BETA	F5.0
CELDIS	real number	1E-20 <= CELDIS <= 1.0	F5.0
CNRECH	real number	none	G8.2
DLTRAT	real number	0.0 <= DLTRAT <= 1.0	F5.2
FCTR1	real number	none	F10.2
FCTR2	real number	none	F10.2
FCTR3	real number	none	F10.2
ICLK	integer	0 <= ICHK <= 1	I1
ICODE	integer	1 <= ICODE <= 9	I2
INPUT	integer	0 <= INPUT <= 1	I1
IX	integer	2 <= IX <= NX-1	I2
IXOBS	integer	2 <= IXOBS <= NX-1	I2
IY	integer	2 <= IY <= NY-1	I2
IYOBS	integer	2 <= IYOBS <= NY-1	I2
ITMAX	integer	100 <= ITMAX <= 200	I4
NCODES	integer	0 <= NCODES <= 10	I4
NITP	integer	4 <= NITP <= 10	I4
NPDEL	integer	0 <= NPDEL <= 1	I4
NPMAX	integer	1 <= NPMAX <= 6400	I4
NPMP	integer	1 <= NPMP	I4
NPNCHV	integer	0 <= NPNCHV <= 2	I4
NPNT	integer	1 <= NPNT	I4
NPNTD	integer	0 <= NPNTD <= 2	I4
NPNTMV	integer	0 <= NPNTMV	I4
NPNTVL	integer	0 <= NPNTVL <= 2	I4
NPTPND	integer	1 <= NPTPND <= 16	I4
NREC	integer	0 <= NREC	I4
NTIM	integer	1 <= NTIM <= 100	I4
NUMOBS	integer	0 <= NUMOBS <= 5	I4
NX	integer	-40 <= NX <= 20	I4
NY	integer	3 <= NY <= 40	I4
OVERRD	integer	0 <= OVERRD <= 99	I2
PINT	real number	0.0 <= PINT	F5.1

POROS	real number	0.01 <= POROS <= 0.99	F5.2
REC	real number	none	G8.2
S	real number	.0001 <= S < 1.0 or S = 0.0	F5.4
TIMX	real number	1.0 <= TIMX <= 2.0	F5.2
TINIT	real number	0.0 <= TINIT	F5.0
TITLE	character array	maximum 80 characters	20A4
TOL	real number	1E-10 <= TOL <= 1.0	F5.4
XDEL	real number	1E-20 <= XDEL	F5.0
YDEL	real number	1E-20 <= YDEL	F5.0

---

### ARRAYS

Array variables are dimensioned as ARRAY(NX,NY) where NX=40, and NY=40. Because of the number of columns allocated in input FORMAT statements of MOC, the precision with which one can specify their values is limited. It is further restricted by the rules governing output FORMAT descriptors of MOCINP. In most cases these restrictions may be overcome by carefully choosing a multiplication factor FCTR (which does not have any FORMAT-based restriction on its range) for each array variable.

Table 4.2 specifies the range and precision of the each array. In terms of precision, a range of -99. to 999. does not include the values 1.23 or 0.4.

Table 4.2 MOC Input Arrays

variable.	type	range of values	output format
CONC	real array	-99. <= CONC <= 999.	20F4.0
NODEID	integer array	0 <= NODEID <= 9	20I1
RECH	real array	-99. <= RECH <= 999.	20F4.0
THCK	real array	-9. <= THCK <= 99.	20F3.0
VPRM	real array	-99. <= VPRM <= 999.	20F4.0
WT	real array	-99. <= WT <= 999.	20F4.0
NREACT	integer	-1 <= NREACT <= 7	I4
MX	integer	1 <= MX <= 40	FREE
MY	integer	1 <= MY <= 40	FREE

MMX	integer	1 <= MY <= 40	FREE
MMY	integer	1 <= MY <= 40	FREE
DK	real number	0 <= DK	FREE
RHOB	real number	0 <= RHOB	FREE
THALF	real number	0 <= THALF	FREE
CEC	real number	0 <= CEC	FREE
CTOT	real number	0 <= CTOT	FREE
EK	real number	0 <= EK	FREE
EKF	real number	0 <= EKF	FREE
EKL	real number	0 <= EKL	FREE

---

#### 4.3.4 MOCINP Screen

The user can input/modify data following the MOCINP Screens shown in Figures 4.7 to 4.24.

MOCINP/INPUT, EDIT	CARD 1. TITLE	SCREEN 09
<p>TITLE      Title of the problem (maximum 80 characters)</p> <p>#. ....</p>		
SCREEN OPTION	(ENTER:continue, 1:edit this screen, 2:help):	

Figure 4.7 MOCINP Screen for CARD 1. TITLE

MOCINP/INPUT, EDIT	CARD 2. CONTROL CARD I	SCREEN 10
NTIM	Maximum no. of time steps in a pumping period (limit 100):	
NPMP	No. of pumping periods:	
NX	No. of nodes in x-direction:	
NY	No. of nodes in y-direction:	
NPMAX	Maximum no. of particles (limit 6400):	
NPNT	No. of time steps between printouts:	
NITP	No. of iteration parameters (usually between 4 & 10):	
NUMOBS	No. of observation points (maximum 5):	
ITMAX	No. of iterations in ADIP (usually between 100 & 200):	
SCREEN OPTION	(ENTER:continue, 1:edit this screen, 2:help):	

Figure 4.8 MOCINP Screen for CARD 2. CONTROL CARD I(1)

MOCINP/INPUT, EDIT	CARD 2. CONTROL CARD I	SCREEN 11
NREC	No. of pumping or injection wells to be specified:	
NPTPND	Initial no. of particles per node (1, 4, 5, 8, 9, or 16):	
NCODES	No. of node identification codes (maximum 10):	
NPNTMV	Particle movement interval (IMOV) for printing chemical data (enter 0 for printing at the end of the simulation):	
NPNTVL	Option for printing computed velocities (0: do not print, -1: 1st time step, -2: last time step, n>0: nth tm step):	
NPNTD	Option for printing computed dispersion coefficients (0: do not print, 1: 1st time step, 2: last time step):	
NPDELC	Should changes in concentration be printed (1:yes, 0:no):	
NPNCHV	Option to write velocity, heads or concentrations to disk (0, -1, -2, n>0 - same as for NPNTVL above):	
SCREEN OPTION	(ENTER:continue, 1:edit this screen, 2:help):	

Figure 4.9 MOCINP Screen for CARD 2. CONTROL CARD I(2)

```

MOCINP/INPUT,EDIT          CARD 3. CONTROL CARD II          SCREEN 12

PINT          Pumping period in years:

TOL          Convergence criteria in ADIP (usually within 0.01):

POROS          Effective porosity:

BETA          Characteristic length (longitudinal dispersivity) in feet:

S          Storage coefficient (set 0 for steady flow problems):

TIMX          Time increment multiplier:

TINIT          Initial time in seconds:

SCREEN OPTION          (ENTER:continue, 1:edit this screen, 2:help):

```

Figure 4.10 MOCINP Screen for CARD 3. CONTROL CARD II(1)

```

MOCINP/INPUT,EDIT          CARD 3. CONTROL CARD II          SCREEN 13

XDEL          Width of finite-difference cell in x-direction, in feet:

YDEL          Width of finite-difference cell in y-direction, in feet:

DLTRAT          Ratio of transverse to longitudinal dispersivity:

CELDIS          Maximum cell distance per particle move (between 0 & 1):

ANFCTR          Ratio of  $T_{yy}$  to  $T_{xx}$  :

SCREEN OPTION          (ENTER:continue, 1:edit this screen, 2:help):

```

Figure 4.11 MOCINP Screen for CARD 2. CONTROL CARD II(2)

Number of points =

No.	x	y
I	IXOBS	IYOBS

SCREEN OPTION

(ENTER:continue, 1:edit this screen, 2:help):

Figure 4.12 MOCINP Screen for DATA 1. OBSERVATION POINTS

Number of wells =

number	coordinates		pumping(+) or injection(-)	concentration of injected water
I	IX	IY	rate REC	CNRECH

SCREEN OPTION

(ENTER:continue, 1:edit this screen, 2:help):

Figure 4.13 MOCINP Screen for DATA SET 2. WELLS

NCODES Number of node ID codes:

serial number	code ICODE	leakance FCTR1	concentration FCTR2	recharge FCTR3	factor OVERRD

SCREEN OPTION (ENTER:continue, 1:edit this screen, 2:help):

Figure 4.14 MOCINP Screen for DATA SET 7. INSTRUCTION FOR NODE ID'S

Pumping period:  
-----

- ICLK Should data be revised for this period(1:yes, 0:no):
- NTIM Maximum no. of time steps in a pumping period (limit 100):
- NPNT No. of time steps between printouts:
- NITP No. of iteration parameters (usually between 4 & 10):
- ITMAX No. of iterations in ADIP (usually between 100 & 200):
- NREC No. of pumping or injection wells to be specified:
- NPNTMV Particle movement interval (IMOV) for printing chemical data (enter 0 for printing at the end of the simulation):

SCREEN OPTION (ENTER:continue, 1:edit this screen, 2:help):

Figure 4.15 MOCINP Screen for DATA SET 10. ADDITIONAL PUMPING PERIOD(1)





```

MOCINP/INPUT,EDIT          CARD 2. CONTROL CARD I          SCREEN 59

NREACT    Reaction Specifier (-1 through 7):

          -1. Decay Only
           0. No Reaction
           1. Linear Sorption
           2. Freundlich Sorption
           3. Langmuir Sorption
           4. Monovalent Exchange
           5. Divalent Exchange
           6. Mono-Divalent Exchange
           7. Di-Monovalent Exchange

                                     Enter Selection:

SCREEN OPTION                (ENTER:continue, 1:edit this screen, 2:help):

```

Figure 4.18 MOCINP Screen for CARD 2. CONTROL CARD I

```

MOCINP/INPUT,EDIT          CARD 2a. CONTROL CARD Ia          SCREEN 60

MX        X coordinate, within the primary grid, of the UPPER-LEFT
          node of the transport subgrid:

MY        Y coordinate, within the primary grid, of the UPPER-LEFT
          node of the transport subgrid:

MMX       X coordinate of LOWER-RIGHT node of transport subgrid:

MMY       Y coordinate of LOWER-RIGHT node of transport subgrid:

SCREEN OPTION                (ENTER:continue, 1:edit this screen, 2:help):

```

Figure 4.19 MOCINP Screen for CARD 2a. CONTROL CARD Ia

```

MOCINP/INPUT,EDIT          CARD 3a. CONTROL CARD IIa          SCREEN 61

DK                          distribution coefficient:

RHOB                        bulk density of the solid:

THALF                      half-life of the solute (in seconds):

SCREEN OPTION                (ENTER:continue, 1:edit this screen, 2:help):

```

Figure 4.20 MOCINP Screen for CARD 3a. CONTROL CARD IIa(1)

```

MOCINP/INPUT,EDIT          CARD 3a. CONTROL CARD IIa          SCREEN 62

THALF                      Half-life of the solute (in seconds):

SCREEN OPTION                (ENTER:continue, 1:edit this screen, 2:help):

```

Figure 4.21 MOCINP Screen for CARD 3a. CONTROL CARD IIa(2)

MOCINP/INPUT, EDIT	CARD 3a. CONTROL CARD IIa	SCREEN 63
RHOB	bulk density of the solid:	
EKF	Freundlich sorption coefficient:	
XNF	Freundlich sorption exponent:	
THALF	half-life of the solute (in seconds):	
SCREEN OPTION	(ENTER:continue, 1:edit this screen, 2:help):	

Figure 4.22 MOCINP Screen for CARD 3a. CONTROL CARD IIa(3)

MOCINP/INPUT, EDIT	CARD 3a. CONTROL CARD IIa	SCREEN 64
RHOB	bulk density of the solid:	
EKL	Langmuir sorption coefficient:	
CEC	maximum sorption capacity :	
THALF	half-life of the solute (in seconds):	
SCREEN OPTION	(ENTER:continue, 1:edit this screen, 2:help):	

Figure 4.23 MOCINP Screen for CARD 3a. CONTROL CARD IIa(4)

```
RHOB                bulk density of the solid:
EK                  ion-exchange selectivity coefficient:
CEC                  ion-exchange capacity :
CTOT                total solution concentration of two exchanging ions:
THALF                half-life of the solute (in seconds):

SCREEN OPTION      (ENTER:continue, 1:edit this screen, 2:help):
```

Figure 4.24 MOCINP Screen for CARD 3a. CONTROL CARD IIa(5)

#### 4.4 MODEL OPERATION

MOC executes in a batch environment system designed by TECSOFT INC. In the response to the system prompt C:>TECSOFT, type TECSOFT and press <ENTER>, then the following TECSOFT ACCESS MENU will appear on the screen. Select MOC from the menu and press <ENTER>. Enter the default data drive where all data is read or written. If the user is using the hard disk, the drive name is C (or D).

MOCINP is selected when the user creates or modifies data files required by MOC as described in the previous chapter.

The batch processing environment is initiated by selecting MOC from the menu. The four (4) major functions within the batch shell are FILES, SELECT, EXECUTE and QUIT.

Help is available for most functions within the shell by pressing the <F1> function key while highlighting that function. Exit help by pressing the <ESC> key.

#### 4.4.1 FILES

FILES permits the creation (CREATE) or modification (MODIFY) of batch files necessary for execution. The default extension for the batch files is 'MCB'. Any number of MOC batch files may exist concurrently. Prior to execution, a batch file must be selected.

To execute, MOC requires various files:

1. A data file must be provided for each simulation. This file is created and/or modified using MOCINP.
2. The name of Hardcopy Output File must be specified. This file will contain all output generated during the simulation.
3. If Binary Concentration/Head/Drawdown data is to be saved, the name of the file in which it will be saved must be also be specified.

Rather than enter the file names manually during MOC execution, a batch file is selected prior to execution. The Batch File contains all file-names required for MOC execution. Batch Files may be created or modified by the program. It is noted that the Batch Files described are internal to the TECSOFT version of MOC and have no relation to DOS batch files.

##### (1) CREATE

In the Create Batch File process, the program prompts for two file types:

1. Specified Files (Hardcopy Output, Binary Concentration/Head/Velocity Vectors and Batch Files).
2. Selected File (MOC Data File).

The Specified Files are created during MOC execution. The default extensions for the Specified Files are:

OUT (Hardcopy Output File)  
BIN (Binary File - Concentration/Head/Velocity)

## MCB (MOC Batch File)

The MOC Data File was previously created using MOCINP and is selected from a picklist when creating the batch File. The default extension for the MOC Data File is .DAT. A group of files may also be selected by using a different mask.

For example, to select all files with a .NAM extension, enter \*.NAM for the mask. Wild card characters may be used. All files in current directory may be displayed by using the mask (\*.\*)).

To change the pick directory, select the entry at the top of the list. The desired directory may now be selected. To select a specific file, merely type the name (up to 63 characters).

### (2) MODIFY

In the Modify Batch File process, the Batch File to be modified is selected. The program sequentially displays the filenames read from the Batch File and modifications may be made. The name of the Batch Files containing the modifications is specified.

The Specified File names may be edited or overridden. The default extensions for the Specified Files are the same as mentioned above.

### (3) Specify File

Enter a pathname of up to 63 characters or a filename of up to 12 characters. The format is:

```
[C]:[\dirname][\dirname]...[\]filename[.ext]
```

A sophisticated line editor with Wordstar compatibility is included for use when entering the name of the file.

#### 4.4.2 SELECT

This option selects an existing MOC Batch File prior to MOC execution. MOC will not execute if a selection has not been made. The Batch File

may be created or modified prior to selection.

The Batch File may be selected by entering a specific file name or choosing from a picklist. If entering a specific file name, a pathname may consist of up to 63 characters. The filename itself may consist of up to 12 characters. The format is:

```
[c]:[\dirname][\dirname]...[\]filename[.ext]
```

After the Batch File is selected, Specified Files are checked for path existence and the data File is checked for existence prior to MOC execution.

#### 4.4.3 EXECUTE

Execute MOC using the Selected Batch File. The appropriate solver (MOCADI or MOCSIP) must be selected. MOCADI solves MOC using the Alternating Direction Implicit method. MOCSIP solves MOC using the Strongly Implicit Procedure method.

For most problems, MOCADI should be used. However, for steady-state cases when grid nodes have zero transmissivity and for cases in which the transmissivity is highly anisotropic, MOCSIP should be used.

If a Batch File was not selected prior to execution, an error message is reported.

MOC errors, which normally result in program abortion, are reported and appropriate action can be taken.

#### 4.4.4 QUIT

This option is to terminate the MOC program. It is recommended that the user should move the cursor to QUIT and press <ENTER> key immediately after Executing to avoid losing created data files.

#### 4.5 OUTPUT PROCESSOR

MOC generates a Hardcopy Output File and a Binary File which may contain

concentrations, heads and velocity vectors.

MOCREC was provided in the MOC package to remove carriage control characters and replace with appropriate ASCII control characters, if desired.

An output processor MOCOUT was also provided in the package. MOCOUT takes as input the binary file from MOCADI (or MOCSIP) and outputs an ASCII file. Binary data may have been saved for all simulation time steps (NPNCHV=1). Rather than process all of this data with MOCGRAF, when only a subset is required. MOCOUT gives the user an opportunity to thin out the data while converting to ASCII.

The four (4) major functions such as FILES, INPUTS, EXECUTE and QUIT are used in the MOCOUT program.

Help is available for most functions within the shell by pressing the <F1> function key while highlighting that function. Exit help by pressing the <ESC> key.

#### 4.5.1 FILES

Select all inputs and output files required by MOCOUT.

The input file is:

- The Binary File which may contain concentrations, heads and velocity vectors.

This is the only required input file for MOCOUT. If this file has not been specified prior to execution of MOCOUT, the execution will abort.

The Binary File may be selected by entering a specific filename or choosing from a picklist. The picklist default is \*.BIN for the Binary File.

The output files are:

- The ASCII MOCGRAF Data File
- The Hardcopy Output File



These are the required output files for MOCOUT. If either of these files has not been specified prior to execution of MOCOUT, the execution will abort.

The ASCII MOCGRAF data file is the file containing ASCII Concentration/Head/Velocity Vector data which will be input to MOCGRAF. This file may contain all or a subset of the data contained in the original binary file. This file will be used by MOCGRAF to produce contours of concentrations and heads and, optionally, velocity vectors. A pathname of up to 63 characters or a file name of up to 12 characters must be entered. The format is:

```
[C]:[\dirname][\dirname]...[\]filename[.ext]
```

The Default file extension is [.MCG]

#### 4.5.2 INPUTS

This option is used to select a required input other than a file name. The input which will be selected is:

- Output ASCII File Format

#### 4.5.3 EXECUTE

The MOCOUT program converts binary (Concentration/Heads/ Velocity Vector) files generated by MOC to ASCII files which may be read and contoured by MOCGRAF. Each binary file may contain numerous sets of data. Each set corresponds to a particular time step and pumping period from the MOC simulation.

In addition to converting from binary to ASCII, MOCOUT affords the opportunity to view the time step, pumping period and total elapsed time corresponding to each set of binary data read and to determine whether that set of data shall be converted to ASCII and saved in a file.

All or part of the original binary file may be converted and saved. The

original binary files are neither destroyed nor modified in the conversion process.

Three options exist for saving ASCII data:

- 1) Save all ASCII data in one file for use with MOCGRAF.
- 2) Save each set of ASCII data in TECKON format.
- 3) Save each set of ASCII data in general XYZ format.

#### (1) Option (1)

In addition to offering simplicity by using a single ASCII file, Option (1) (MOCGRAF option) is easiest to use. It eliminates the book-keeping and possible confusion associated with the use of multiple files and requires minimal intervention.

MOCGRAF is a graphic module designed specially for use with the MOC model. MOCGRAF requires relatively little user intervention and is extremely easy to use. It uses sophisticated algorithms to produce high resolution graphics on a variety of graphics devices.

#### (2) Option (2)

Although Option (2) requires the use of individual ASCII files, it permits the use of TKON2R and TKON3D, 2-D and 3-D contouring by TECISOFT. TKON2R and TKON3D are powerful modules offering a wide selection of contouring options and customizing capability.

#### (3) Option (3)

This option produces general XYZ ASCII files. The Binary File is a file created by MOC and may contain any or all of the following data types:

- Concentration
- Head
- Velocity Vector

Each set corresponds to a specific time step and pumping period of the MOC simulation. The Binary file is converted to one or more ASCII files

by MOCOUT.

As each set of binary data is read, the data may be written to an ASCII file or discarded. In any event, the binary file is not modified. Since ASCII files usually require much more disk space than binary files containing equivalent data, if disk space is concern, only the data of immediate interest need be saved as ASCII.

#### 4.5.4 QUIT

This option is to terminate the MOCOUT program. It is recommended that the user should move the cursor to QUIT and press Enter key immediately after Executing to avoid losing created data files.

#### 4.6 GRAPHICS

MOCGRAF is a program provided in the TECSOFT package. MOCGRAF is used to contour heads and concentrations and to generate velocity vectors which may be superimposed on the contours or drawdown stand-alone. MOCGRAF reads and processes the ASCII file from MOCOUT.

TECSOFT's TRANSLATE program is required to process the plot files generated by MOCGRAF and output the graphics.

##### 4.6.1 MOCGRAF

The batch processing environment is initiated by selecting MOCGRAF from the TECSOFT menu. The four (4) major functions within the batch shell are FILES, SELECT, EXECUTE and QUIT.

Help is available for most functions within the shell by pressing the <F1> function key while highlighting that function. Exit help by pressing the <ESC> key.

##### (1) FILES

To Execute, MOCGRAF requires a Batch File. The Batch File contains specific (numeric and text) inputs required to execute MOCGRAF, in addition to input/output files. The Batch Files may be created or modi-

fied by the package prior to MOCGRAF execution. The following filenames are contained in the Batch Files:

1. An ASCII Data File produced by MOCOUT which contains concentration, head and velocity vector data.
2. The name of the Plot File which will be created by MOCGRAF and which contains graphics information which will be input to TRANSLATE.
3. The name of a Hardcopy Output File which will contain all output generated during MOCGRAF execution. This file is optional.

It is noted that the Batch Files described above are internal to the MOCGRAF package and have no relation to DOS batch files.

The data associated with the creation of head and/or concentration contours and, optionally, the superposition of velocity vectors is entered through a series of seven (7) possible menus. The program scans the Input Data File and sequentially displays the appropriate set of menus for each set of data. <PgUp> key and <PgDn> key are used to select the various menus.

*a) Menu 1 -- Graphics Options*

This menu displays the ordinal number of the current data set and indicates whether head, concentration and velocity vector data are present. Also displayed are the Time Step, Pumping Period and Total Elapsed Time. The times are displayed in years.

The user may select this set of data for contouring. If both head and concentration data are present, the user may choose to contour either or both. If neither is to be contoured, the program skips to read the next set. If the head and/or concentration data is selected for contouring and if velocity vector data is present, the user is prompted to specify whether velocity vectors will be superimposed on the contours.

*b) Menu 2 -- Aspect Ratio*

The aspect ratio is defined as:

$$(\text{Length of Y-axis}) / (\text{Length of X-axis})$$

The program scans the current set of data, computes the aspect ratio and displays the computed value. The user is prompted to enter the aspect ratio and, thus, may override the computed value.

*c) Menu 3 -- Contour Section Types*

Contour levels may be selected in one of three (3) ways:

1. Computer Selects Contour Levels (Default)
2. User Selects Maximum, Minimum and Increment
3. User Selects Specific Contour Levels

If the computer (program) selects the contour levels, the data set is scanned and a set of pleasing, evenly spaced levels is chosen. If both head and concentration data are present in the current data set, contour levels may be selected in a different manner for each.

*d) Menu 4 -- Contour Increment and Bounds*

This menu is displayed only if the user selects the minimum and maximum contour levels and increment. The program scans the data set and computes the minimum and maximum values of the data to be contoured and computes an interval based on ten (10) contour levels. The data is then displayed. The user may override these computed values with his/her own selections.

*e) Menu 5 -- Selected Contour Levels*

This menu is displayed only if the user selects specific contour levels. The program scans the data and computes the minimum and maximum values of the data to be contoured. The data is displayed. The user specifies the number of contour levels which will be selected. The maximum allowable number is 50.

*f) Menu 6 -- Selected Contour Levels*

This menu is only displayed only if the user selects specific contour levels. The desired contour levels are entered through this menu.

*g) Menu 7 -- Title/Label Options*

Title, X-axis and Y-axis labels for heads and/or concentration data may be entered through this menu. Each may consist of a string of up to 40 alpha-numeric characters.

Menus 1 through Menu 7 repeat for each set of data processed.

**(2) SELECT**

This option selects an existing MOCGRAF Batch File prior to MOCGRAF execution. MOCGRAF will not execute if a selection has not been made. The Batch File may be created or modified prior to selection.

The batch File may be selected by entering a specific file name or choosing from a picklist. The picklist default is \*.GCB. If entering a specific file name, a pathname may consist of up to 63 characters. The filename itself may consist of up to 12 characters.

After the Batch File is selected, Specified Files are checked for path existence and Selected Files are checked for file existence prior to MOCGRAF execution.

**(3) EXECUTE**

Execute MOCGRAF using the Selected Batch File. If a Batch File was not selected prior to execution, an error message is reported. MOCGRAF errors, which normally result in program abortion, are reported and appropriate action can be taken.

**(4) QUIT**

This option is to terminate the MOCGRAF program.

#### 4.6.2 TRANSLATE

TRANSLATE produces high quality screen, dot matrix printer and vector plotter graphics on a wide variety of devices by translating a graphics metacode file (previously generated by a TECSOFT application program such as MOCGRAF). Among the devices supported are: CGA, EGA, Hercules, AT&T (normal & high resolution) screen graphics; IBM graphics printer, Epson and Comrex printers; Hewlett-Packard, Houston Instruments, IBM, Calcomp, Roland, Sweet Pea and other vector plotters.

The graphics files may contain up to 500 pictures (plots) stacked sequentially as pictures in camera. TRANSLATE permits selective slipping or plotting of specific pictures. Re-translation for another device is possible without exiting from the program. Paper size (A, B, C, D, E) may be selected through the program for applicable plotters. Serial port (plotters, printers), parallel port (printers) and baud rate (plotters) are also selected.

The procedure for running the program is to set the system to the drive and directory where the program resides. Type TECSOFT and press <ENTER>. Select TRANSLATE from the TECSOFT ACCESS MENU and press <ENTER>. Enter the default drive. This is the drive where all data is read or written. The TRANSLATE introductory menu appears. The user is prompted for program inputs through a series of menus. Press any key to invoke the Metacode Graphics File menu.

The usage of the program is mentioned below:

##### (1) METACODE PLOT FILE NAME

###### ENTER PLOT FILE NAME:

Enter the name of the metacode graphics file to be translated. This is a graphics file created by a TECSOFT program.

It is noted that the metacode graphics file name may consist of up to 61 characters (including optional path designation). A drive letter must never be appended to the file name since it is specified in the TECSOFT ACCESS MENU and is automatically concatenated to the name. If a path designation is used, the file name appears as:

\subdir1\subdir2\...\filename.

## (2) SELECT FUNCTION

- <1> TRANSLATE A FILE
- <2> CREATE Hewlett-Packard HPGL FILE(S)
- <3> CREATE AutoCAD (.DXF) FILE(S)
- <R> RETURN TO PREVIOUS MENU
- <E> EXIT TO TECSOFT ACCESS MENU.

Selection <1> reads a metacode graphics file and selectively produces plots on the selected device (plotter, printer or screen). No additional files are saved.

Selection <2> reads a metacode graphics file and selectively converts plots to HPGL (Hewlett-Packard Graphics Language), an ASCII graphics code, and saves the results in specified files. Once a plot has been converted to HPGL and saved, That file may later be incorporated directly into many popular word processors and desktop publishing packages to produce professional looking reports with graphics.

Selection <3> reads a metacode graphics file and selectively creates AutoCAD DXF files. DXF files are ASCII files written in a format recognizable to AutoCAD, ProDesign II and other CAD packages. Once input to a CAD package supporting the DXF convention, a file can be saved as a working drawing. This selection is available only with the DXF version of TRANSLATE.

### ENTER SELECTION:

Enter Selection 1,2,3,R or E.

## (3) SELECT GRAPHICS TYPE

- <1> VECTOR PLOTTER
- <2> SCREEN GRAPHICS
- <3> PRINTER GRAPHICS
- <4> RETURN TO PREVIOUS MENU
- <5> EXIT TO TECSOFT ACCESS MENU



This menu appears only if translating a file (Selection <1>) is selected.

ENTER GRAPHICS SELECTION

Enter selection (1,2 or 3).

(3.1) VECTOR PLOTTER

ENTER SERIAL PORT#(1,2):

Enter the serial port (1 or 2) to which the plotter is connected.

ENTER BAUD RATE 1 2 3 4 5 6:

Enter selection (1,2,3,4,5 or 6). These correspond to baud rates of 300, 600, 1200, 2400, 4800 and 9600, respectively.

The plotter currently supported are:

- HEWLETT PACKARD 7440 ColorPro, 7470, 7475, 7550 DraftPro, 7580, 7585, 7595 DraftMaster
- HOUSTON INSTRUMENTS DMP29, DMP40, DMP41, DMP42, DMP51, DMP52, 595, 695
- CALCOMP 945, 965, 1040, 1070
- IBM 7371, 7372
- ROLAND 880, 980
- SWEET PEA 100, 600
- FACIT 4550, 4551
- GOULD 6120, 6320, TAXAN 710
- WESTERN GRAPHTEC MP1000, MP2000

Select the brand of plotter, the specific model and paper size, if applicable. Choose an option by entering the appropriate character.

(3.2) SCREEN GRAPHICS

The Screen Graphics types currently supported include:

- CGA (640x200)
- EGA (640x350)

- Hercules (720x345)
- AT&T normal and high resolution (640x200, 640x400)

### (3.3) PRINTER GRAPHICS

#### ENTER PORT TYPE (SERIAL OR PARALLEL)(S/P):

A printer may be connected to either a serial or parallel port. Enter Selection (S or P).

If 'S' is selected, enter the serial port number (1 or 2).

If 'P' is selected, enter the parallel port number (1,2 or 3).

The Printer Graphics types currently supported include:

- IBM PC Graphics Printer
- EPSON FX, LX, RX, MX series (single or double density)
- EPSON LQ series (single or double density)
- COMREX 420
- HP LaserJet Series II

Select the brand of printer and specific model. Choose an option by selecting the appropriate character.

### (4) TRANSLATOR OPTIONS

- <P> PLOT THIS PICTURE
- <S> SKIP THIS PICTURE
- <R> RESELECT FUNCTION

If <P> is selected, the metacode file is read and the current picture is plotted on the selected plotter.

If <S> is selected, the metacode file is read and the current picture will be skipped.

Choosing <R> will return for selection of another device. The metacode graphics file is automatically rewound and another graphics device (screen, printer or vector plotter ) may be selected.

This menu appears only if translating a file (Selection <1>) is selected.

(5) HEWLETT PACKARD - HPGL

- <1> HP7470, HP7440 ColorPro
- <2> HP7475
- <3> HP7550
- <4> HP7570 DraftPro
- <5> HP7580
- <6> HP7585
- <7> HP7595 DraftMaster

ENTER SELECTION:

Enter selection (1,2,3,4,5,6 or 7).

A prompt for paper size (A,B,C,D or E) will also appear, if applicable. The HPGL files will vary slightly between plotter models. Although most HPGL commands apply to all HP plotters, a few commands do not apply to all of the plotter models.

This menu appears only if Creating HPGL Files (Selection <2>) is selected.

(6) HPGL OPTION MENU

- <W> WRITE HPGL FILE FOR THIS FRAME
- <S> SKIP THIS PICTURE
- <R> RETURN TO PREVIOUS MENU
- <E> EXIT TO TECSOFT ACCESS MENU

If Selection <W> is made, the metacode file is read, and an HPGL file will be written. The following prompt appears:

ENTER HPGL FILE NAME:

The HPGL file names may consist of up to 61 characters.

If Selection <F> is made, the metacode file will be read but an HPGL file will not be written.

<R> returns for selection of another function.

The HPGL OPTION MENU appears only if Creating HPGL Files (Selection <2>) is selected.

(7) AutoCAD OPTION MENU

<B> BUILD DXF FILE FOR THIS FRAME

<S> SKIP THIS FRAME

<R> RETURN TO PREVIOUS MENU

<E> EXIT TO TECSOFT ACCESS MENU

If Selection <B> is made, the metacode file is read, and a DXF file will be written. The following prompt appears:

ENTER DXF FILE NAME:

If Selection <B> is made, the metacode file is read, and a DXF file will be written. The following prompt appears:

ENTER DXF FILE NAME:

The DXF file names may be consist of up to 61 characters.

If Selection <S> is made, the metacode file will be read but a DXF file will not be written.

The AutoCAD OPTION MENU appears only if Creating DXF Files (Selection <3> is chosen.

APPENDIX A

COMPUTER PROGRAMS AND RELATED  
DATA FOR Q3P MODEL

```

C *****
C *
C * TWO-DIMANSIONAL/QUASI THREE DIMENSIONAL *
C * GROUNDWATER FLOW MODEL (QSP MODEL) *
C * FOR METRO MANILA GROUNDWATER BASIN *
C *****
C
C *** VARIABLES, ARRAY ***
C HN(I,1) = PHREATIC WATER LEVEL (M)
C HN(I,2) = HEAD OF CONFINED AQUIFER-1
C HN(I,3) = HEAD OF CONFINED AQUIFER-2
C IDENT = MODEL SPECIFICATION
C (0: PLAIN 2-D MODEL FOR SINGLE AQUIFER)
C (1: QUASI 3-D MODEL FOR SINGLE AQUIFER)
C (2: QUASI 3-D MODEL FOR DOUBLE AQUIFER)
C
C T = TRANSMISSIVITY(M**2/D)
C S = STORAGE COEFFICIENT
C X,Y = X- AND Y-COORDINATES
C BD = LEAKANCE(1/M)
C SS = SPECIFIC STORAGE(1/M) OF AQUICLUDE
C Q = DISCHARGE(M**3/D)
C DT = DURATION OF 1-TIME STEP (D)
C NSTEPS = NUMBER OF STEPS
C NINTER = NUMBER OF DIVIDE IN ONE CALCULATION STEP
C NP = NUMBER OF NODES
C NE = NUMBER OF ELEMENTS
C NBAND = WIDTH OF BAND
C NC(I) = NUMBER OF CONSTANT-HEAD NODEL IN AQUIFER-I
C KQIN = 1:STEADY-STATE 2:NONSTEADY-STATE
C KOUT = 1:OUTPUT ALL STEPS 2:OUTPUT FINAL STEP
C KHIN = INPUT INITIAL HEADS
C (0:FROM FILE-5)
C (1:FROM FILE-3)
C
C KPRI = NUMBER OF OUTPUT STEPS
C NPRINT(I) = STEP NUMBER FOR PRINT OUT
C DX,DY = SCALE FOR MAP PRINT OUT
C
C *** INPUT ***
C FILE-1 : DISCHARGE DATA
C FILE-3 : INITIAL HEADS
C FILE-5 : CONTROL DATA
C FILE-7 : AQUIFER PARAMETERS
C
C *** OUTPUT ***
C FILE-2 : COMPUTED HEADS
C FILE-6 : LIST OF RESULTS
C
COMMON TITLE(4),NBAND,NSTEPS,KQIN,KHOUT,IROW,JCOL,RRR
COMMON NP,X1,Y1,HF(900),NNO(38,29)
COMMON NE,NOP(900,4),T(900,2),S(900,2),Q(900,2)
COMMON SK(990,30,2),F(990),HN(990,2),BD(900,2)
COMMON NC(2),HC(30,2),NOHC(30,2),NPRINT(30)
COMMON /BK3/NWEL,EVAL(70),SVAL(70),VIND,CN(70,3),NWOUT(70),
* OBS(70,3,30),CAL(70,2,30),NW(70),NS(70),IHO
COMMON /BK4/R(900)
COMMON /BK8/LBL(900),NBK,NLL,NL(15),NLE(15,100),NLP(15,100),
* HO(990,2)
INTEGER*2 NOP,NOHC,NPRINT,NNO,NL,NLE,NLP,LBL
CHARACTER*8 TITLE,CN
C=====
C==FILE SPECIFICATION=====
OPEN(UNIT=1,FILE='MSA\DAT\QIN30.DAT',STATUS='OLD')
OPEN(UNIT=19,FILE='MSA\DAT\RIN30.DAT',STATUS='OLD')
OPEN(UNIT=5,FILE='MSA\DAT\Q3PSIM2.PAR',STATUS='OLD')
OPEN(UNIT=7,FILE='MSA\DAT\PRM_03.DAT',STATUS='OLD',
*FORM='UNFORMATTED')
OPEN(UNIT=4,FILE='MSA\DAT\NOP.DAT',STATUS='OLD')
OPEN(UNIT=13,FILE='MSA\DAT\NOD.DAT',STATUS='OLD')
OPEN(UNIT=3,FILE='MSA\DAT\INI_03.DAT',STATUS='OLD',
*FORM='UNFORMATTED')
OPEN(UNIT=8,FILE='MSA\DAT\HBOUND.DAT',STATUS='OLD')
OPEN(UNIT=14,FILE='MSA\DAT\OBSh63_2.DAT',STATUS='OLD')
OPEN(UNIT=15,FILE='MSA\DAT\BLOCK.DAT',STATUS='OLD',
*BLANK='ZERO')
C=====
C OPEN(UNIT=6,FILE='MSA\OUT\Q3P_30.LST',STATUS='NEW')
C OPEN(UNIT=2,FILE='MSA\OUT\CAL_30.DAT',STATUS='NEW',
C *FORM='UNFORMATTED')
C OPEN(UNIT=20,FILE='MSA\OUT\INI_30.DAT',STATUS='NEW',
C *FORM='UNFORMATTED')

```

```

C   OPEN(UNIT=22, FILE='MSA\OUT\HBU_30.DAT', STATUS='NEW',
C   *FORM='UNFORMATTED')
C   OPEN(UNIT=24, FILE='MSA\OUT\FORO24.DAT', STATUS='NEW',
C   *FORM='UNFORMATTED')
C   OPEN(UNIT=30, FILE='MSA\OUT\FORO30.DAT', STATUS='NEW')
C   OPEN(UNIT=28, FILE='MSA\OUT\BLOCK.OUT', STATUS='NEW')
C=====
C=====
C   ***** ZERO CLEAR *****
C   CALL CLEAR
C   ***** DATA INPUT *****
C   CALL GDATA(IL)
C   ***** ESTABLISH MATRIX *****
C   DO 10 ID=1, IL
C   CALL FORMK(ID)
C   10 CONTINUE
C   ***** START CALCULATION *****
C   IF(KQIN.EQ.1) READ(1,101) ((Q(I,J),I=1,NE),J=1,IL)
C   IF(KQIN.EQ.1) READ(19,101) (R(I),I=1,NE)
C   101 FORMAT(10F10.0)
C   KT=1
C   WRITE(*,192)
C   192 FORMAT(///19X,2X,'STEP')
C
C   DO 200 KY=1,NSTEPS
C   WRITE(*,191)KY
C   191 FORMAT(1H+,15X,I3)
C   IF(KQIN.EQ.2) READ(1,101) ((Q(I,J),I=1,NE),J=1,IL)
C   IF(KQIN.EQ.2) READ(19,101) (R(I),I=1,NE)
C   DO 20 J=1,IL
C   K=NC(J)
C   READ(8,102) (HC(I,J),I=1,K)
C   20 CONTINUE
C   102 FORMAT(10F8.2)
C
C   ***** CREATE BASIC VECTOR *****
C   CALL RIGHT(1)
C   GO TO (300,301),IL
C   301 CALL RIGHT(2)
C   CALL RIGHT(2)
C   CALL RIGHT(1)
C   ***** PRINT OUT RESULTS *****
C   300 IF(NWEL.NE.0) THEN
C   DO 30 I=1,NWEL
C   IW=NS(I)
C   DO 40 J=1,2
C   CAL(I,J,KY)=HN(IW,J)
C   40 CONTINUE
C   30 CONTINUE
C   ENDIF
C   IF(KHOUT.GE.2) WRITE(2) ((HN(I,J),I=1,NP),J=1,IL)
C   IF(NPRINT(KT).EQ.KY) THEN
C   CALL PRINT(KY)
C   CALL OUTPUT(1,KY)
C   IF(IL.EQ.2) CALL OUTPUT(2,KY)
C   WRITE(22)KY,((HN(I,J),I=1,NP),J=1,IL)
C   21 KT=KT+1
C   ENDIF
C   200 CONTINUE
C   IF(KHOUT.GE.1) WRITE(20) ((HN(I,J),I=1,NP),J=1,IL)
C   ***** OUTPUT OBSERVED HEADS ***
C   IF(NWEL.EQ.0) GO TO 900
C   DO 800 N=1,NWEL
C   WRITE(24)((CAL(N,J,KY),KY=1,NSTEPS),J=1,IL)
C   IF(NWOUT(N).NE.0)CALL WELPRI(N)
C   800 CONTINUE
C   900 STOP
C   END
C   SUBROUTINE CLEAR
C
C   *****
C   *
C   * ZERO CLEAR
C   *
C   *
C   *****
C
C   COMMON TITLE(4),NBAND,NSTEPS,KQIN,KHOUT,IROW,JCOL,RRR
C   COMMON NP,X1,Y1,HF(900),NNO(38,29)

```

```

COMMON NE,NOP(900,4),T(900,2),S(900,2),Q(900,2)
COMMON SK(990,30,2),F(990),HN(990,2),BD(900,2)
COMMON NC(2),HC(30,2),NOHC(30,2),NPRINT(30)
COMMON /BK3/NWEL,EVAL(70),SVAL(70),VIND,CN(70,3),NWOUT(70),
*   OBS(70,3,30),CAL(70,2,30),NW(70),NS(70),IHO
INTEGER*2  NOP,NOHC,NPRINT,NNO
CHARACTER*8 TITLE,CN
DO 20 ID=1,2
DO 10 I=1,990
DO 10 J=1,30
SK(I,J,ID)=0.0
10 CONTINUE
DO 15 I=1,900
T(I, ID) =0.0
S(I, ID) =0.0
15 BD(I, ID) =0.0
20 CONTINUE
RETURN
END
SUBROUTINE GDATA(IL)
C
C *****
C *
C * DATA INPUT
C *
C *****
C
COMMON TITLE(4),NBAND,NSTEPS,KQIN,KHOUT,IROW,JCOL,RRR
COMMON NP,X1,Y1,HF(900),NNO(38,29)
COMMON NE,NOP(900,4),T(900,2),S(900,2),Q(900,2)
COMMON SK(990,30,2),F(990),HN(990,2),BD(900,2)
COMMON NC(2),HC(30,2),NOHC(30,2),NPRINT(30)
COMMON /BK3/NWEL,EVAL(70),SVAL(70),VIND,CN(70,3),NWOUT(70),
*   OBS(70,3,30),CAL(70,2,30),NW(70),NS(70),IHO
COMMON /BK8/LBL(900),NBK,NLL,NL(15),NLE(15,100),NLP(15,100),
*   HO(990,2)
INTEGER*2  NOP,NOHC,NPRINT,NNO,NL,NLE,NLP,LBL
CHARACTER*8 TITLE,CN
COMMON /BK1/IDENT
C ***** INPUT DATA *****
C *** << TITLE & CONTROL DATA>> *****
READ(5,501) (TITLE(I),I=1,4),NP,NE,NBAND,IDENT,NSTEPS,IROW,JCOL,
*   DT,X1,Y1,(NC(I),I=1,2),KQIN,KHOUT,KHIN,IPP,
*   KPRI,NWEL,IHO,VIND,NBK,NLL
READ(5,511) (NPRINT(I),I=1,KPRI)
501 FORMAT(4A8/7I5/3F10.5/2I5/4I1,I5/2I5/F10.5/2I5)
511 FORMAT(20I4)
IL=2
IF(IDENT.LE.1) IL=1
C ***** ELEMENT NUMBERING *****
READ(4,503) ((NOP(I,J),J=1,4),I=1,NE)
503 FORMAT(32I4)
DO 10 I=1,IROW+1
READ(13,512) (NNO(I,J),J=1,JCOL+1)
10 CONTINUE
512 FORMAT(30I4)
C ***** ERROR CHECK *****
CALL ERCHK
C ***** BLOCK LABEL *****
IF(NBK.NE.0) READ(15,589) (LBL(I),I=1,NE)
IF(NLL.NE.0) THEN
READ(15,591) (NL(I),I=1,NLL)
DO 11 I=1,NLL
J=NL(I)
READ(15,590) (NLE(I,K),NLP(I,K),K=1,J)
11 CONTINUE
ENDIF
589 FORMAT(40I1)
590 FORMAT(10(I4,I2))
591 FORMAT(20I4)
C ***** LEAKANCE *****
IF(IDENT.EQ.0) GO TO 41
DO 20 J=1,IL
20 READ(7) (BD(I,J),I=1,NE)
C
WRITE(*,507) (BD(I,1),I=1,NE)
505 FORMAT(10F8.6)
C ***** TRANSMISSIVITY & STORAGE COEFFICIENT *****

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```

DO 51 J=1,IL
51 READ(7) (T(I,J),I=1,NE)
DO 50 J=1,IL
50 READ(7) (S(I,J),I=1,NE)
507 FORMAT(10F8.7)
C   *** << PHREATIC WATER LEVEL >> *****
IF(IDENT.GE.1) READ(7) (HF(I),I=1,NE)
C   *** << INITIAL HEADS >> *****
IF(KHIN.EQ.0) THEN
DO 55 J=1,IL
55 READ(7) (HN(I,J),I=1,NP)
510 FORMAT(10F8.2)
ELSE
READ(3) ((HN(I,J),I=1,NP),J=1,IL)
ENDIF
100 CONTINUE
508 FORMAT(10F8.0)
C   *** << CONSTANT-HEAD BOUNDARY >> *****
41 CONTINUE
READ(8,506)NNC, (NOHC(I,1),I=1,NNC)
NC(1)=NNC
NC(2)=NNC
DO 12 I=1,NNC
NOHC(I,2)=NOHC(I,1)
12 CONTINUE
506 FORMAT(20I4)
40 CONTINUE
READ(5,543)RRR
543 FORMAT(F5.2)
C   *** << OBSERVED HEADS >> *****
IF(NWEL.EQ.0) GO TO 90
DO 93 I=1,NWEL
93 READ(14,542) NS(I),NW(I),(CN(I,J),J=1,3),SVAL(I),EVAL(I),NWOUT(I)
542 FORMAT(I4,I2,3A8,2F10.4,I1)
IF(IHO.EQ.0) GO TO 90
DO 91 I=1,NWEL
N=NW(I)
DO 91 J=1,N
READ(14,541)
91 READ(14,541)(OBS(I,J,K),K=1,NSTEPS)
541 FORMAT(8X,12F6.2)
90 CONTINUE
C   ***** DATA PRINT OUT *****
IF(IPP.NE.0) CALL DPRINT(DT,KPRI)
IF(IL.EQ.2) DT=DT/2.0
DO 30 J=1,IL
DO 30 I=1,NE
S(I,J)=X1*Y1*S(I,J)/DT/36.0
BD(I,J)=X1*Y1*BD(I,J)/36.0
30 CONTINUE
DO 13 I=1,NP
DO 14 J=1,IDENT
HO(I,J)=HN(I,J)
14 CONTINUE
13 CONTINUE
RETURN
END
SUBROUTINE DPRINT(DT,KPRI)
C
C   *****
C   *
C   * DATA PRINT OUT
C   *
C   *****
C
COMMON TITLE(4),NBAND,NSTEPS,KQIN,KHOUT,IROW,JCOL,RRR
COMMON NP,X1,Y1,HF(900),NNO(38,29)
COMMON NE,NOP(900,4),T(900,2),S(900,2),Q(900,2)
COMMON SK(990,30,2),F(990),HN(990,2),BD(900,2)
COMMON NC(2),HC(30,2),NOHC(30,2),NPRINT(30)
COMMON /BK3/NWEL,EVAL(70),SVAL(70),VIND,CN(70,3),NWOUT(70),
* OBS(70,3,30),CAL(70,2,30),NW(70),NS(70),IHO
INTEGER*2 NOP,NOHC,NPRINT,NNO
CHARACTER*8 TITLE,CN
COMMON /BK1/IDENT
C
WRITE(6,601) (TITLE(I),I=1,4),NP,NE,NBAND,IDENT,NSTEPS,
* (NC(I),I=1,2),DT,X1,Y1,KQIN,KHOUT,KHIN,

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*          KPRI,NWEL,IHO,VIND,IROW,JCOL
601 FORMAT(1H1//10X,4A8//16X,'NP =',I5/16X,'NE =',
*I5/13X,'NBAND =',I5/13X,'IDENT =',I5/
*13X,'NSTEPS =',I5/13X,'NC(1) =',I5/
*13X,'NC(2) =',I5/16X,'DT =',F5.0/16X,'X1 =',
*F7.1/16X,'Y1 =',F7.1/14X,'KQIN =',
*I5/13X,'KHOUT =',I5/14X,'KHIN =',I5/14X,'KPRI =',I5/
*14X,'NWEL =',I5/15X,'IHO =',I5/
*13X,'VIND =',F10.4//14X,'IROW =',I5/14X,'JCOL =',I5//)
WRITE(6,608) (NPRINT(I),I=1,KPRI)
608 FORMAT(10X,' =22 3A@^< =C/L_/'/(10X,10I5))
C
DO 60 I=1,NE
IF(MOD(I,50).EQ.1) WRITE(6,604)
WRITE(6,605) I,(NOP(I,J),J=1,4),(T(I,J),J=1,2),(S(I,J),J=1,2),
*          (BD(I,J),J=1,2),HF(I),I
604 FORMAT(/10X,'NOP(I,J),TRANS.,STORAGE COFF.,LEAKANCE '//5X,
*          'I',9X,'NOP(I,J)',10X,'T(1)',4X,'T(2)',5X,'S(1)',5X,
*          'S(2)',5X,'K/B(1)',3X,'K/B(2)',7X,'HF',5X,'I'/)
605 FORMAT(3X,I4,1X,4I5,1X,2F8.1,1X,2F9.6,1X,2F9.6,1X,F9.2,2X,I4)
60 CONTINUE
C
CALL OUTPUT(1,KY)
IF(IDENT.EQ.2) CALL OUTPUT(2,KY)
200 CONTINUE
RETURN
END
SUBROUTINE ERCHK
C
C *****
C *          *
C * NOP, COORDINATES ERROR CHECK *
C *          *
C *****
COMMON TITLE(4),NBAND,NSTEPS,KQIN,KHOUT,IROW,JCOL,RRR
COMMON NP,X1,Y1,HF(900),NNO(38,29)
COMMON NE,NOP(900,4),T(900,2),S(900,2),Q(900,2)
COMMON SK(990,30,2),F(990),HN(990,2),BD(900,2)
COMMON NC(2),HC(30,2),NOHC(30,2),NPRINT(30)
COMMON /BK3/NWEL,EVAL(70),SVAL(70),VIND,CN(70,3),NWOUT(70),
*          OBS(70,3,30),CAL(70,2,30),NW(70),NS(70),IHO
INTEGER*2  NOP,NOHC,NPRINT,NNO
CHARACTER*8 TITLE,CN
C *** ERROR CHECK *****
DO 5 N=1,NE
I=NOP(N,1)
J=NOP(N,2)
K=NOP(N,3)
L=NOP(N,4)
MA=MAX0(I,J,K,L)
MI=MIN0(I,J,K,L)
NB=MA-MI+1
5 IF(NB.GT.NBAND) WRITE(6,610) N,I,J,K
610 FORMAT(/10X,'ERROR BAND WIDTH NO. =',4I4)
RETURN
END
SUBROUTINE FORMK(ID)
C
C *****
C *          *
C * ESTABLISH WHOLE MATRIX *
C *          *
C *****
COMMON TITLE(4),NBAND,NSTEPS,KQIN,KHOUT,IROW,JCOL,RRR
COMMON NP,X1,Y1,HF(900),NNO(38,29)
COMMON NE,NOP(900,4),T(900,2),S(900,2),Q(900,2)
COMMON SK(990,30,2),F(990),HN(990,2),BD(900,2)
COMMON NC(2),HC(30,2),NOHC(30,2),NPRINT(30)
COMMON /BK3/NWEL,EVAL(70),SVAL(70),VIND,CN(70,3),NWOUT(70),
*          OBS(70,3,30),CAL(70,2,30),NW(70),NS(70),IHO
INTEGER*2  NOP,NOHC,NPRINT,NNO
CHARACTER*8 TITLE,CN
COMMON /BK1/IDENT
DIMENSION E(4,4)
C ***** OVERLAP ELEMENT MATRIX TO WHOLE MATRIX****
DO 100 N=1,NE
P1=Y1*T(N,ID)/X1/6.0

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P2=X1*T(N, ID)/Y1/6.0
P3=BD(N, ID)
IF(ID.EQ.1) P3=P3+BD(N, ID+1)
P4=S(N, ID)
E(1,1)=2.0*P1+2.0*P2+4.0*P3+4.0*P4
E(2,2)=E(1,1)
E(3,3)=E(1,1)
E(4,4)=E(1,1)
E(1,2)=-2.0*P1+P2+2.0*P3+2.0*P4
E(3,4)=E(1,2)
E(2,1)=E(1,2)
E(4,3)=E(1,2)
E(1,3)=-P1-P2+P3+P4
E(2,4)=E(1,3)
E(3,1)=E(1,3)
E(4,2)=E(1,3)
E(1,4)=P1-2.0*P2+2.0*P3+2.0*P4
E(2,3)=E(1,4)
E(3,2)=E(1,4)
E(4,1)=E(1,4)
DO 300 I=1,4
  II=NOP(N, I)
DO 300 J=1,4
  JJ=NOP(N, J)
  LL=JJ-II+1
  IF(LL) 300,300,320
320 SK(II, LL, ID)=SK(II, LL, ID)+E(I, J)
300 CONTINUE
100 CONTINUE
C ***** CONSTANT-HEAD BOUNDARY *****
  NNC=NC(ID)
  IF(NNC.EQ.0) GO TO 20
  DO 10 N=1, NNC
    I=NOHC(N, ID)
    SK(I, 1, ID)=SK(I, 1, ID)*(10.**8.)
  10 CONTINUE
C ***** FORWARD ELIMINATION OF MATRIX *****
  20 CALL SOLVE1(ID)
  RETURN
  END
  SUBROUTINE RIGHT(NN)
C
C *****
C *
C * CREATE BASIC VECTOR *
C *
C *****
C
  COMMON TITLE(4), NBAND, NSTEPS, KQIN, KHOUT, IROW, JCOL, RRR
  COMMON NP, X1, Y1, HF(900), NNO(38, 29)
  COMMON NE, NOP(900, 4), T(900, 2), S(900, 2), Q(900, 2)
  COMMON SK(990, 30, 2), F(990), HN(990, 2), BD(900, 2)
  COMMON NC(2), HC(30, 2), NOHC(30, 2), NPRINT(30)
  COMMON /BK3/NWEL, EVAL(70), SVAL(70), VIND, CN(70, 3), NWOUT(70),
  * OBS(70, 3, 30), CAL(70, 2, 30), NW(70), NS(70), IHO
  COMMON /BK4/R(900)
  INTEGER*2 NOP, NOHC, NPRINT, NNO
  CHARACTER*8 TITLE, CN
  COMMON /BK1/IDENT
C ***** ZERO CLEAR *****
  DO 10 N=1, 990
10 F(N)=0.0
  N1=NN-1
  N2=NN+1
C ***** CREATE VECTOR *****
  DO 200 N=1, NE
  I=NOP(N, 1)
  J=NOP(N, 2)
  K=NOP(N, 3)
  L=NOP(N, 4)
  SS=S(N, NN)
C ***** COMPUTE STORAGE CHANGE *****
  F(I)=F(I)+SS*(HN(I, NN)*4.0+HN(J, NN)*2.0+HN(K, NN)
1 +HN(L, NN)*2.0)
  F(J)=F(J)+SS*(HN(I, NN)*2.0+HN(J, NN)*4.0+HN(K, NN)*2.0
1 +HN(L, NN) )
  F(K)=F(K)+SS*(HN(I, NN) +HN(J, NN)*2.0+HN(K, NN)*4.0
1 +HN(L, NN)*2.0)

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      F(L)=F(L)+SS*(HN(I,NN)*2.0+HN(J,NN)      +HN(K,NN)*2.0
1      +HN(L,NN)*4.0)
      FI1=F(I)
      FJ1=F(J)
      FK1=F(K)
      FL1=F(L)
C      ***** LEAKAGE FROM UPPER AQUIFER *****
      IF (IDENT.EQ.0)      GO TO 400
      GO TO (30,20),NN
20     IF (BD(N,NN).EQ.0.) GO TO 300
      BB=BD(N,NN)
C
      F(I)=F(I)+BB*(HN(I,N1)*4.0+HN(J,N1)*2.0+HN(K,N1)
1      +HN(L,N1)*2.0)
      F(J)=F(J)+BB*(HN(I,N1)*2.0+HN(J,N1)*4.0+HN(K,N1)*2.0
1      +HN(L,N1)      )
      F(K)=F(K)+BB*(HN(I,N1)      +HN(J,N1)*2.0+HN(K,N1)*4.0
1      +HN(L,N1)*2.0)
      F(L)=F(L)+BB*(HN(I,N1)*2.0+HN(J,N1)      +HN(K,N1)*2.0
1      +HN(L,N1)*4.0)
300    CONTINUE
      GO TO 400
C      ***** LEAKAGE FROM LOWER AQUIFER *****
30     IF (BD(N,N2).EQ.0)      GO TO 400
      BB=BD(N,N2)
      CC=HF(N)*BD(N,NN)*9.0
      F(I)=F(I)+BB*(HN(I,N2)*4.0+HN(J,N2)*2.0+HN(K,N2)
1      +HN(L,N2)*2.0)+CC
      F(J)=F(J)+BB*(HN(I,N2)*2.0+HN(J,N2)*4.0+HN(K,N2)*2.0
1      +HN(L,N2)      )+CC
      F(K)=F(K)+BB*(HN(I,N2)      +HN(J,N2)*2.0+HN(K,N2)*4.0
1      +HN(L,N2)*2.0)+CC
      F(L)=F(L)+BB*(HN(I,N2)*2.0+HN(J,N2)      +HN(K,N2)*2.0
1      +HN(L,N2)*4.0)+CC
400    CONTINUE
      FI2=F(I)-FI1
      FJ2=F(J)-FJ1
      FK2=F(K)-FK1
      FL2=F(L)-FL1
      FLEAK=FI2+FJ2+FK2+FL2
C      WRITE (28,777)FLEAK
777    FORMAT(10F15.0)
C      ***** DISCHARGE*****
      QQ=Q(N,NN)/4.0
      IF (NN.EQ.1) QQ=QQ-R(N)*RRR/4.0
      F(I)=F(I)-QQ
      F(J)=F(J)-QQ
      F(K)=F(K)-QQ
      F(L)=F(L)-QQ
500    CONTINUE
200    CONTINUE
C      ***** CONSTANT-HEAD NODE *****
      NNC=NC(NN)
      IF (NNC.NE.0) THEN
        DO 41 NO=1,NNC
          I=NOHC(NO,NN)
          F(I)=SK(I,1,NN)*HC(NO,NN)
41      CONTINUE
        ENDIF
C      ***** COMPUTE NEXT STEP *****
35     CALL SOLVE2(NN)
C      ***** CHANGE COMPUTED HEADS *****
      DO 40 I=1,NP
        HN(I,NN)=F(I)
40     CONTINUE
      RETURN
      END
      SUBROUTINE SOLVE1(ID)
C
C      *****
C      *
C      * FORWARD ELIMINATION PROGRAM
C      *
C      *****
C
COMMON TITLE(4),NBAND,NSTEPS,KQIN,KHOUT,IROW,JCOL,RRR
COMMON NP,X1,Y1,HF(900),NNO(38,29)
COMMON NE,NOP(900,4),T(900,2),S(900,2),Q(900,2)

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COMMON SK(990,30,2),F(990),HN(990,2),BD(900,2)
COMMON NC(2),HC(30,2),NOHC(30,2),NPRINT(30)
COMMON /BK3/NWEL,EVAL(70),SVAL(70),VIND,CN(70,3),NWOUT(70),
*   OBS(70,3,30),CAL(70,2,30),NW(70),NS(70),IHO
INTEGER*2   NOP,NOHC,NPRINT,NNO
CHARACTER*8 TITLE,CN
C
DO 300 N=1,NP
I=N
DO 290 L=2,NBAND
I=I+1
IF(I.GT.NP) GO TO 290
IF(SK(N,L,ID)) 240,290,240
240 C=SK(N,L,ID)/SK(N,1,ID)
J=0
DO 270 K=L,NBAND
J=J+1
IF(SK(N,K,ID)) 260,270,260
260 SK(I,J,ID)=SK(I,J,ID)-C*SK(N,K,ID)
270 CONTINUE
SK(N,L,ID)=C
290 CONTINUE
300 CONTINUE
RETURN
END
SUBROUTINE SOLVE2(ID)
C
C *****
C *
C * BACKWARD SUBSTITUTION
C *
C *****
C
COMMON TITLE(4),NBAND,NSTEPS,KQIN,KHOUT,IROW,JCOL,RRR
COMMON NP,X1,Y1,HF(900),NNO(38,29)
COMMON NE,NOP(900,4),T(900,2),S(900,2),Q(900,2)
COMMON SK(990,30,2),F(990),HN(990,2),BD(900,2)
COMMON NC(2),HC(30,2),NOHC(30,2),NPRINT(30)
COMMON /BK3/NWEL,EVAL(70),SVAL(70),VIND,CN(70,3),NWOUT(70),
*   OBS(70,3,30),CAL(70,2,30),NW(70),NS(70),IHO
INTEGER*2   NOP,NOHC,NPRINT,NNO
CHARACTER*8 TITLE,CN
C
DO 300 N=1,NP
I=N
DO 290 L=2,NBAND
I=I+1
IF(I.GT.NP) GO TO 290
F(I)=F(I)-SK(N,L,ID)*F(N)
290 CONTINUE
300 F(N)=F(N)/SK(N,1,ID)
C
N=NP
350 N=N-1
IF(N) 500,500,360
360 L=N
DO 400 K=2,NBAND
L=L+1
IF(L.GT.NP) GO TO 400
IF(SK(N,K,ID)) 370,400,370
370 F(N)=F(N)-SK(N,K,ID)*F(L)
400 CONTINUE
GO TO 350
500 RETURN
END
SUBROUTINE OUTPUT(KH,NS)
C
C *****
C *
C * PRINT OUT MAPS
C *
C *****
C
COMMON TITLE(4),NBAND,NSTEPS,KQIN,KHOUT,IROW,JCOL,RRR
COMMON NP,X1,Y1,HF(900),NNO(38,29)
COMMON NE,NOP(900,4),T(900,2),S(900,2),Q(900,2)
COMMON SK(990,30,2),F(990),HN(990,2),BD(900,2)
COMMON NC(2),HC(30,2),NOHC(30,2),NPRINT(30)

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      INTEGER*2  NOP,NOHC,NPRINT,NNO
      CHARACTER*8 TITLE,CN,HU
      CHARACTER*5 HP(38,30),BLK
      DATA BLK/'
      '/
      DATA HU/'KEISAN H'/
C
      DO 10 I=1,IROW+1
      DO 20 J=1,JCOL+1
      K=NNO(I,J)
      IF(K.NE.0) THEN
      REWIND 30
      WRITE(30,111)HN(K,KH)
      REWIND 30
      READ(30,191)HP(I,J)
191  FORMAT(A5)
      ELSE
      HP(I,J)=BLK
      ENDIF
      20  CONTINUE
      10  CONTINUE
      111 FORMAT(F5.1)
      M=1
C ***** PRINT OUT MAPS *****
      CALL OUT(HP,KH,NS,TITLE,HU,IROW+1,JCOL+1)
C      WRITE(6,601) (TITLE(I),I=1,4),NS,KH,M
601  FORMAT(1H1///10X,'***',4A8,'***',10X,I3,'STEP_',2X,'NO.',I1,
      * 'AQUIF.',20X,'PAGE',I1//)
      RETURN
      END
      SUBROUTINE WELPRI(IW)
C
C *****
C *
C * PRINT OUT SIMULATED HEADS *
C * AND LAND SUBSIDENCE *
C *
C *****
C
      COMMON TITLE(4),NBAND,NSTEPS,KQIN,KHOUT,IROW,JCOL,RRR
      COMMON NP,X1,Y1,HF(900),NNO(38,29)
      COMMON NE,NOP(900,4),T(900,2),S(900,2),Q(900,2)
      COMMON SK(990,30,2),F(990),HN(990,2),BD(900,2)
      COMMON NC(2),HC(30,2),NOHC(30,2),NPRINT(30)
      COMMON /BK3/NWEL,EVAL(70),SVAL(70),VIND,CN(70,3),NWOUT(70),
      * OBS(70,3,30),CAL(70,2,30),NW(70),NS(70),IHO
      INTEGER*2  NOP,NOHC,NPRINT,NNO
      CHARACTER*8 TITLE,CN
      COMMON /BK1/IDENT
      CHARACTER*1 CO(3),CC(3),BLNK,IBND,PLUS,MINS,AP(101),BP(101)
      DATA CO,CC,BLNK,IBND,PLUS/'A','B','C','+', 'X','*', ' ', 'I','+' /
      DATA MINS/'-' /
      ETRC=.4999999
      VINT=(EVAL(IW)-SVAL(IW))*0.01
      DO 100 I=2,100
100  BP(I) =MINS
      BP(1) =PLUS
      BP(101)=PLUS
      VVVV=VIND/VINT
      PPT=1.0+VVVV
      IPPT=INT(PPT)
110  BP(IPPT)=PLUS
      PPT=PPT+VVVV
      IPPT=INT(PPT)
      IF(IPPT.LT.101) GO TO 110
      NNW=NW(IW)
      IF(NSTEPS.GT.60)WRITE(6,600)
600  FORMAT(1H1/)
      DO 120 N=1,NNW
120  WRITE(6,601) CO(N),CN(IW,N)
      DO 125 N=1,2
125  WRITE(6,621) CC(N),N
      WRITE(6,604) SVAL(IW),EVAL(IW)
      WRITE(6,607) (BP(I),I=1,101)
      DO 200 N=1,NSTEPS
      DO 205 I=2,100
205  AP(I) =BLNK
      AP(1) =IBND
      AP(101)=IBND

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DO 206 J=1,2
IPPT=1+INT((CAL(IW,J,N)-SVAL(IW))/VINT+ETRC)
IF(IPPT.LT.1) IPPT=1
IF(IPPT.GT.101) IPPT=101
206 AP(IPPT)=CC(J)
C   WRITE(6,605) N,(CAL(IW,J,N),J=1,2),(OBS(IW,J,N),J=1,3),
C   *   (AP(I),I=1,101)
C   IF(IHO.EQ.0) GO TO 203
C   DO 201 I=1,101
C 201 AP(I)=BLNK
DO 202 M=1,NNW
IPPT=1+INT((OBS(IW,M,N)-SVAL(IW))/VINT+ETRC)
IF(IPPT.LT.1) IPPT=1
IF(IPPT.GT.101) IPPT=101
202 AP(IPPT)=CO(M)
WRITE(6,605) N,(CAL(IW,J,N),J=1,2),(OBS(IW,J,N),J=1,3),
*   (AP(I),I=1,101)
C   WRITE(6,606) (AP(I),I=1,101)
203 CONTINUE
200 CONTINUE
WRITE(6,607) (BP(I),I=1,101)
WRITE(6,608) SVAL(IW),EVAL(IW)
601 FORMAT(30X,'OBSVAL',A1,2X,A8)
604 FORMAT(/2X,'N',2X,'CA1',2X,'CA2',2X,
*   'OB1',2X,'OB2',2X,'OB3',1X,F5.1,91X,F5.1)
621 FORMAT(30X,'CMPVAL',A1,' NO.',I1,'AQUIFER')
607 FORMAT(31X,101A1)
605 FORMAT(1X,I3,F6.1,4F5.1,2X,101A1)
606 FORMAT(1H+,31X,101A1)
608 FORMAT(31X,F5.0,91X,F5.0)
RETURN
END
SUBROUTINE PRINT(NT)
C
C *****
C *
C * COMPUTE FLUX
C *
C *****
C
COMMON TITLE(4),NBAND,NSTEPS,KQIN,KHOUT,IROW,JCOL,RRR
COMMON NP,X1,Y1,HF(900),NNO(38,29)
COMMON NE,NOP(900,4),T(900,2),S(900,2),Q(900,2)
COMMON SK(990,30,2),F(990),HN(990,2),BD(900,2)
COMMON NC(2),HC(30,2),NOHC(30,2),NPRINT(30)
COMMON /BK3/NWEL,EVAL(70),SVAL(70),VIND,CN(70,3),NWOUT(70),
*   OBS(70,3,30),CAL(70,2,30),NW(70),NS(70),IHO
COMMON /BK4/R(900)
COMMON /BK8/LBL(900),NBK,NLL,NL(15),NLE(15,100),NLP(15,100),
*   HO(990,2)
INTEGER*2 NOP,NOHC,NPRINT,NNO,NL,NLE,NLP,LBL
CHARACTER*8 TITLE,CN
COMMON /BK1/IDENT
DIMENSION QB(10,2),DD(10,2),RB(10,2),FB(15,2),DRB(10,2)
C
1000 IF(NBK.EQ.0) GO TO 900
DO 10 I=1,2
DO 11 J=1,10
QB(J,I)=0.0
RB(J,I)=0.0
DRB(J,I)=0.0
11 DD(J,I)=0.0
DO 12 J=1,15
12 FB(J,I)=0.0
10 CONTINUE
C
DO 500 N=1,NE
I=NOP(N,1)
J=NOP(N,2)
K=NOP(N,3)
L=NOP(N,4)
J1=LBL(N)
IF(J1) 500,500,501
501 CONTINUE
DO 510 M=1,IDENT
QB(J1,M)=QB(J1,M)-Q(N,M)
HH=S(N,M)*(HO(I,M)+HO(J,M)+HO(K,M)+HO(L,M)-HN(I,M)
*   -HN(J,M)-HN(K,M)-HN(L,M))*4.5

```





```

670 WRITE(28,112) I,(FB(J,I),J=11,NLL)
900 CONTINUE
    DO 100 I=1,IDENT
    DO 100 J=1,NP
100 HO(J,I)=HN(J,I)
    RETURN
    END
    SUBROUTINE OUT(NQ,KH,NS,TITLE,HU,IRR,JCC)
    CHARACTER*8 TITLE(4),HU
C
    CHARACTER*5 NQ(38,30),IA(22)
C
    IPAGE=(JCC-1)/20+1
    DO 10 IP=1,IPAGE
    LS=20*(IP-1)+1
    LE=20*IP
    IF(IP.LT.IPAGE)GO TO 15
    IF(JCC.LT.20) GO TO 11
    LS=JCC-20+1
11  LE=JCC
C
15  WRITE(6,600) TITLE,NS,HU,KH,IP,(J,J=LS,LE)
600  FORMAT(1H1//30X,4A8,30X,'STEP=',I3,2X,A8,
*      I1,'AQUIF.',8X,'PAGE=',I3//4X,20I6/)
    DO 70 I=1,IRR
    DO 75 J=LS,LE
    JJ=J-LS+1
    IA(JJ)=NQ(I,J)
75  CONTINUE
    LE1=LE-LS+2
    REWIND 30
    WRITE(30,103)I
103  FORMAT(I5)
    REWIND 30
    READ(30,193)IA(LE1)
193  FORMAT(A5)
C    WRITE (6,610)
C    2  WRITE(6,610)I,(IA(J),J=1,LE1)
C    WRITE(6,610)I
610  FORMAT(2X,I2,21(1X,A5))
C
C    70  CONTINUE
C
C    WRITE(6,620)(J,J=LS,LE)
620  FORMAT(/4X,20I6)
10  CONTINUE
    RETURN
    END

```

```

C          PROGRAM                      PARAC
C
C          ** DATA FORM CHANGE **
C
C          CHARACTER CHA*16,C1*1,LK(40,30)
C          DIMENSION H(40,30),DD(1000),DK(16,2),ND(30)
C          INTEGER*2 NR(40,30),NP(40,30),KY(40,30)
C
C          DATA    CHA/'0123456789ABCDEF'/
C
C          OPEN(UNIT=1,FILE='MSA\DAT\PRM_03.DAT',STATUS='NEW',
*          FORM='UNFORMATTED')
C          OPEN(UNIT=2,FILE='MSA\DAT\ELE.DAT',STATUS='OLD',BLANK='ZERO')
C          OPEN(UNIT=3,FILE='MSA\DAT\NOD.DAT',STATUS='OLD',BLANK='ZERO')
C          OPEN(UNIT=4,FILE='MSA\DAT\KD_03.LAB',STATUS='OLD',BLANK='ZERO')
C          OPEN(UNIT=5,FILE='MSA\DAT\KYOKAI.LAB',STATUS='OLD',
*          BLANK='ZERO')
C          OPEN(UNIT=11,FILE='MSA\DAT\H.IND',STATUS='OLD',BLANK='ZERO')
C          OPEN(UNIT=12,FILE='MSA\DAT\T_03.IND',STATUS='OLD',BLANK='ZERO')
C          OPEN(UNIT=13,FILE='MSA\DAT\B.IND',STATUS='OLD',BLANK='ZERO')
C          OPEN(UNIT=14,FILE='MSA\DAT\S.IND',STATUS='OLD',BLANK='ZERO')
C          OPEN(UNIT=6,FILE='MSA\DAT\PRL_03.LST',STATUS='NEW')
C
C          IR=35
C          JC=28
C          NNE=754
C          NNP=829
C
C          DO 10 I=1,IR
C          READ(2,200)(NR(I,J),J=1,JC)
C          READ(5,210)(KY(I,J),J=1,JC)
C          READ(3,200)(NP(I,J),J=1,JC+1)
10      CONTINUE
200     READ(3,200)(NP(IR+1,J),J=1,JC+1)
210     FORMAT(30I4)
210     FORMAT(40I1)
C
C          LEAK
C
C          DO 11 L=1,2
C          L=1
C          READ(4,220)(DK(I,L),I=1,16)
220     FORMAT(8F8.0)
C          11 CONTINUE
C
C          DO 12 L=1,2
C          L=1
C
C          DO 13 K=1,NNE
C          DD(K)=0.
13      CONTINUE
C
C          WRITE(6,610)(J,J=1,28)
610     FORMAT(1H1//4X,30I4)
C          DO 14 I=1,IR
C          READ(4,500)(LK(I,J),J=1,JC)
14      CONTINUE
C
C          500 FORMAT (28A1)
C
C          DO 15 I=1,IR
C          READ(13,100)(H(I,J),J=1,JC)
100     FORMAT(30F4.0)
C
C          DO 16 J=1,JC
C          K=NR(I,J)
C          IF (K.GT.0) THEN
C          C1=LK(I,J)
C          LL=INDEX(CHA,C1)
C          IF (LL.EQ.0) LL=1
C          DD(K)=DK(LL,L)
C          IF (H(I,J).GT.0) DD(K)=DK(LL,L)/H(I,J)
C          ND(J)=INT(DD(K)*1000000.)+1
C          IF (L.EQ.1.AND.KY(I,J).EQ.1) THEN
C          DD(K)=0.
C          ND(J)=-1
C          END IF
C          ELSE

```

```

        ND(J)=9999
        END IF
16    CONTINUE
C
    WRITE(6,600)I,(ND(J),J=1,JC),I
600   FORMAT(2X,30I4)
15    CONTINUE
C
    WRITE(1)(DD(K),K=1,NNE)
    WRITE(*,300)(DD(K),K=1,NNE)
300   FORMAT(8F10.8)
C    12    CONTINUE
C
C
C    T
C
C    DO 17 L=1,2
        L=1
        DO 18 K=1,NNE
            DD(K)=0.
18    CONTINUE
C
    WRITE(6,610)(J,J=1,28)
    DO 19 I=1,IR
        READ(12,100)(H(I,J),J=1,JC)
C
        DO 20 J=1,JC
            K=NR(I,J)
            ND(J)=9999
            IF(K.GT.0)THEN
                DD(K)=H(I,J)
                ND(J)=H(I,J)
            END IF
20    CONTINUE
        WRITE(6,600)I,(ND(J),J=1,JC),I
19    CONTINUE
C
    WRITE(1)(DD(K),K=1,NNE)
310   FORMAT(10F8.0)
C    17    CONTINUE
C
C
C    S
C
C    DO 21 L=1,2
        L=1
        DO 22 K=1,NNE
            DD(K)=0.
22    CONTINUE
C
    WRITE(6,610)(J,J=1,28)
    DO 23 I=1,IR
        READ(14,100)(H(I,J),J=1,JC)
C
        DO 24 J=1,JC
            K=NR(I,J)
            ND(J)=9999
            IF(K.GT.0)THEN
                R=-H(I,J)*0.1
                DD(K)=10**R
                ND(J)=H(I,J)
            END IF
24    CONTINUE
        WRITE(6,600)I,(ND(J),J=1,JC),I
23    CONTINUE
C
    WRITE(1)(DD(K),K=1,NNE)
340   FORMAT(10F8.6)
C    21    CONTINUE
C
C
C    H
C
C    DO 25 K=1,NNE
        DD(K)=0.
25    CONTINUE
C
    DO 26 I=1,IR
        READ(11,110)(H(I,J),J=1,JC)
110   FORMAT(30F4.0)
C

```

```
DO 27 J=1,JC
K=NR(I,J)
IF(K.GT.0)DD(K)=H(I,J)
27 CONTINUE
26 CONTINUE
C
WRITE(1)(DD(K),K=1,NNE)
L=1
C DO 28 L=1,2
WRITE(1)(DD(K),K=1,NNP)
360 FORMAT(10F8.2)
C 28 CONTINUE
C
STOP
END
```

AN EXAMPLE BATCH FILE (Q3PSCN1.BAT)  
USED FOR THE METRO MANILA MODEL

```
ECHO ON
CD C:\MSA\DAT
DIR PR*.*
PAUSE Delete these files?
DEL PR*.*
DEL RIN30.DAT
TYPE T_03.IND
PAUSE Confirmed?
TYPE S.IND
PAUSE Confirmed?
TYPE KD_03.LAB
PAUSE Confirmed?
CD C:\MSA\OUT
DIR
PAUSE Delete these files?
DEL *.*
CD C:\MSA\EXE
MR30IN
PARAC
COPY C:\MSA\DAT\INI_81AV.DAT C:\MSA\DAT\INI_03.DAT
COPY C:\MSA\DAT\Q3PSIM2.NSS C:\MSA\DAT\Q3PSIM2.PAR
COPY C:\MSA\DIS\CASE\SCNRO1\QIN30.DAT C:\MSA\DAT\QIN30.DAT
TYPE C:\MSA\DAT\Q3PSIM2.PAR
Q3PF
MPRO5DS
MPRO5DL
FOBS
HELE
HN10C90C
MCONT
HDCONT
cd c:\MSA\OUT
dir
COPY *.* C:\MSA\OUT\SCN1
TYPE Q3P_30.PRN
```

PROGRAM LIST OF CONXYZ.MAP TO DRAW CONTOURS

```

10 '*****PROGRAM CONXYZ.MAP*****
20 '
30 '
40 '
50 KEY OFF
60 DEFINT I-N
70 MXGR=100
80 DIM XG(MXGR) , YG(MXGR) , F(MXGR,MXGR)
90 MXDT=250
100 DIM XD(MXDT),YD(MXDT),ZD(MXDT)
110 'CONSOL ,,0
120 SCREEN 3 : CLS
130 COLF=1
140 VNULL=1E+09
150 '
160 '------(1) READ GRID DATA-----
170 '
180 GOSUB 3040 'GOSUB *GRID.IN
190 IF IFLG<>0 THEN 400
200 FOR I=1 TO NX : XG(I)=XMIN+(I-1)*DX : NEXT
210 FOR J=1 TO NY : YG(J)=YMIN+(J-1)*DY : NEXT
220 GOSUB 3340 'GOSUB *OBSDAT.IN
230 IF IFLG<>0 THEN 400
240 '
250 '------(2)DISPLAY AND AXES-----
260 '
270 COMMENT$="GRID DATA="+NFGI$+" ["+CMNTG$+]"
280 GOSUB 1560 'GOSUB *SCREEN.FULL
290 '
300 GOSUB 3620 'GOSUB XYZ.PAR
310 GOSUB 3850 'GOSUB XYZ.DRW
320 '------(3)CONTOR MAP-----
330 'CLS
340 GOSUB 490 'GOSUB *CONTOUR
350 GOSUB 2290 'GOSUB *LABEL.DRAW
360 GOSUB 3850
370 LCOPY
380 '------(4)NEXT OPERATION-----
390 'LOCATE 10,60
400 PRINT
410 PRINT "-----NEXT OPERATION-----"
420 PRINT " ADD MORE CONTOR -->1"
430 PRINT " REWRITE USING SAME DATA -->2"
440 PRINT " INPUT NEW DATA -->3"
450 PRINT " END"
460 INPUT " PLEASE SELECT? --> ",NW
470 ON NW GOTO 340,270,180
480 END
490 '
500 '-----SUBROUTINE *CONTOUR-----
510 ' DRAWING CONTOUR LINES
520 ' NULL VALUES NOT BE DRAWN
530 ' [REQUIRED DATA] GRID POINTS : XG(I),YG(I)
540 ' VALUES : F(I,J) (I=1-NX,J=1-NY)
550 ' [REQUIRED SUBROUTINE] *STATG.F *DRAW.CONT
560 '-----
570 '
580 '*CONTOUR
590 ' [MAX. AND MIN. OF F(I,J)]
600 GOSUB 1420 'GOSUB *STATG.F
610 DELTAF=(FMX-FMN)*.000001
620 ' [PARAMETERS OF CONTOUR]
630 PRINT "-----"
640 PRINT " MIN. VALUE Fmin =";FMN
650 PRINT " MAX. VALUE Fmax =";FMX
660 PRINT " ***SPECIFICATION****"
670 INPUT " START VALUE =",CST
680 INPUT " END VALUE =",CEN
690 IF CST>CEN THEN SWAP CST ,CEN
700 IF CST>FMX OR CEN<FMN THEN RETURN : RETURN
710 INPUT " INTERVAL =",CIN
720 CIN=ABS(CIN)

```

```

730         IF CIN<(FMX-FMN)/1000 THEN 630
740 INPUT "          COLOUR          =",COL
750 IF COL>0 THEN LN=&HFFFF ELSE LN=&H5555
760 COL=ABS(COL)
770 GOSUB 790          'GOUSUB *DRAW.CONT
780 RETURN          'GOTO 630
790 CLS
800 '-----SUBROUTINE *DRAW.CONT-----
810 '*DRAW.CONT
820 FOR I=1 TO NX-1
830     I1=I+1
840     XP(1)=XG(I) : XP(2)=XG(I1) : XP(3)=XG(I1) : XP(4)=XG(I)
850     FOR J=1 TO NY-1
860         J1=J+1
870         YP(1)=YG(J) : YP(2)=YG(J) : YP(3)=YG(J1) : YP(4)=YG(J1)
880         FP(1)=F(I,J) : FP(2)=F(I1,J) : FP(3)=F(I1,J1) : FP(4)=F(I,J1)
890     '
900     '          [CONTORS OF ICS TO ICE PASS IN THE CELL]
910     FBOT=FP(1) : FTOP=FP(1)
920     FOR K=2 TO 4
930         IF FP(K)<FBOT THEN FBOT=FP(K)
940         IF FP(K)>FTOP THEN FTOP=FP(K)
950     NEXT
960     IF FTOP>VNULL THEN 1390          :' [SKIP AT NULL]
970     IF FBOT<CST THEN FLBT=CST ELSE FLBT=FBOT
980     ICS=INT((FLBT-CST)/CIN+.9999)
990     IF FTOP>CEN THEN FLTP=CEN ELSE FLTP=FTOP
1000    ICE=INT((FLTP-CST)/CIN+.0001)
1010    IF ICS>ICE THEN 1390
1020 '
1030 '
1040    FOR IC=ICS TO ICE
1050        CON=CST+CIN*IC
1060        FOR K=1 TO 4
1070            FC(K)=FP(K)-CON
1080            IF FC(K)=0 THEN FC(K)=FC(K)+DELTA F
1090        NEXT
1100 '
1110        KC=0
1120        IF FC(1)*FC(2)>0 THEN 1160 ELSE KC=KC+1
1130        XR(KC)=XP(1)-FC(1)*DX/(FC(2)-FC(1))
1140        YR(KC)=YP(1)
1150 '
1160        IF FC(2)*FC(3)>0 THEN 1200 ELSE KC=KC+1
1170        XR(KC)=XP(2)
1180        YR(KC)=YP(2)-FC(2)*DY/(FC(3)-FC(2))
1190 '
1200        IF FC(3)*FC(4)>0 THEN 1240 ELSE KC=KC+1
1210        XR(KC)=XP(3)+FC(3)*DX/(FC(4)-FC(3))
1220        YR(KC)=YP(3)
1230 '
1240        IF FC(4)*FC(1)>0 THEN 1280 ELSE KC=KC+1
1250        XR(KC)=XP(4)
1260        YR(KC)=YP(4)+FC(4)*DY/(FC(1)-FC(4))
1270 '
1280        IF KC<2 THEN 1380
1290        IF KC=2 THEN 1370
1300        D1=(XR(1)-XR(2))^2+(YR(1)-YR(2))^2
1310        D2=(XR(1)-XR(4))^2+(YR(1)-YR(4))^2
1320        IF D1<D2 THEN 1360
1330            LINE (XR(1),-YR(1))-(XR(4),-YR(4)),COL,,LN
1340            LINE (XR(2),-YR(2))-(XR(3),-YR(3)),COL,,LN
1350        GOTO 1380
1360            LINE (XR(3),-YR(3))-(XR(4),-YR(4)),COL,,LN
1370            LINE (XR(1),-YR(1))-(XR(2),-YR(2)),COL,,LN
1380    NEXT
1390 NEXT
1400 NEXT
1410 RETURN
1420 '
1430 '-----SUBROUTINE *STATG.F-----
1440 '          MAX. AND MIN. VALUES OF F(I,J)
1450 '-----
1460 '*STATG.F
1470 FMX=-VNULL : FMN=VNULL
1480 FOR I=1 TO NX
1490     FOR J=1 TO NY
1500         IF F(I,J)>VNULL THEN 1530

```

```

1505     IF F(I,J)<-9999 THEN 1530
1510     IF FMX<F(I,J) THEN FMX=F(I,J)
1520     IF FMN>F(I,J) THEN FMN=F(I,J)
1530     NEXT
1540     NEXT
1550     RETURN
1560 '
1570 '-----SUBROUTINE *SCREEN.FULL-----
1580 '           SET UP DISPLAY AND AXES
1590 '-----
1600 '*SCREEN.FULL
1610     SCREEN 3 : CLS 1
1620     XMAX=XMIN+(NX-1)*DX
1630     YMAX=YMIN+(NY-1)*DY
1640 '
1650     PRINT
1660     PRINT "-----SET UP DISPLAY-----"
1670     INPUT " FULL(1) OR WITH MARGIN (2) ";LD
1680     IF LD=1 THEN SCALE=0 ELSE SCALE=.5
1690     GOSUB 1760
1700 '
1710     GOSUB 1960
1720     GOSUB 2290
1730     INPUT " RESET ? (Y/N) ";A$
1740     IF A$="Y"OR A$="y" THEN 1610
1750     RETURN
1760 '
1770 '-----SUBROUTINE *WINDOW.FULL-----
1780 '           DEFINE WINDOW
1790     DIM KANJI(141)
1800 '           IF VIEW IS (0,0)-(639,399) THEN
1810 '           DOMAIN : XMIN=<X=<XMAX, YMIN=<Y=<YMAX
1820 '           MARGIN : REMAIN SCALEx100% AT FOUR SIDES
1830 '-----
1840 '*WINDOW.FULL
1850     WX=(XMAX-XMIN)/1.6
1860     WY=YMAX-YMIN
1870     IF WX<WY THEN WW=WY ELSE WW=WX
1880     XW1=XMAX-1.6*(1+SCALE)*WW
1890     XW2=XMAX+1.6*SCALE*WW
1900     YW1=-YMAX-SCALE*WW
1910     YW2=-YMAX+(1+SCALE)*WW
1920     WINDOW SCREEN (XW1,YW1)-(XW2,YW2)
1930     VIEW (0,0)-(639,399)
1940     WINDOW (XW1,YW1)-(XW2,YW2)
1950     RETURN
1960 '
1970 '-----SUBROUTINE *LABEL.PARAMETER-----
1980 '           AXES AND INPUT FILE INFORMATION
1990 '           LD = 1 [ONLY SCALE], LD=2 [WITH COMMENT]
2000 '-----
2010 '*LABEL.PARAMETER
2020     XWD=XMAX-XMIN
2030     YWD=YMAX-YMIN
2040     PRINT "-----AXES-----"
2050     INPUT " Auto(A) OR Manual(M) ";LA$
2060     IF LA$="M" OR LA$="m" THEN 2170
2070 '
2080     IF XWD>YWD THEN WD=XWD ELSE WD=YWD
2090     NP=INT(LOG(WD)/LOG(10))
2100     WP=10^(NP-1)
2110     WSTEP=10^NP
2120     IF WD/WSTEP<2 THEN WSTEP=WSTEP/5
2130     XSTART=INT(XMIN/WSTEP+.0001)*WSTEP
2140     YSTART=INT(YMIN/WSTEP+.0001)*WSTEP
2150     RETURN
2160 '
2170     PRINT "Xmin=";XMIN;" Xmax=";XMAX;" DIF. =" ;XWD
2180     PRINT "Ymin=";YMIN;" Ymax=";YMAX;" DIF. =" ;YWD
2190     INPUT " INTERVAL =" ;WSTEP
2200 ' IF WSTEP<XWD/20 OR WSTEP<YWD/20 THEN 2170
2210     INPUT " START POINT OF x-AXIS =" ;XSTART
2220     INPUT " START POINT OF y-AXIS =" ;YSTART
2230     IF LD=1 THEN RETURN
2240     NP=INT(LOG(WSTEP)/LOG(10))
2250     WP=10^NP
2260     PRINT " [ SCALE = ABOUT";WP;" ]"
2270     INPUT " SCALE =" ;WP

```



```

2280 RETURN
2290 '
2300 '-----SUBROUTINE *LABEL.DRAW-----
2310 '     DRAW AXES AND INPUT FILE INFORMATION
2320 '     LD(1) = 1 [ONLY SCALE],   LD(2) = 2 [WITH COMMENT]
2330 '-----
2340 '*LABEL.DRAW
2350 JC=0 : KMIN=10 : CLH=1
2360 LINE (XMIN,-YMIN)-(XMAX,-YMAX),COLF,B
2370 '                                     [x-AXIS]
2380   FOR WXP=XSTART TO XMAX STEP WSTEP
2390     IF WXP<XMIN THEN 2470
2400     LINE (WXP,-YMIN-WW/60)-(WXP,-YMIN),COLF
2410     LINE (WXP,-YMAX+WW/60)-(WXP,-YMAX),COLF
2420     IF LD=1 THEN 2470
2430     WYP=YMIN-WW/200 : WXPP=WXP/WP
2440     IF WXPP>32767 THEN 2470
2450     IV=INT(WXP/WP+.01) : KN$=STR$(IV)
2460     GOSUB 2700                                     'GOSUB *VDRAW.GRP
2470   NEXT
2480   IF WP=1 OR LD=1 THEN 2530
2490     WXP=XMAX-WW/20 : WYP=YMIN-WW/30
2500     KN$="x"+STR$(WP)
2510     GOSUB 2700                                     'GOSUB *VDRAW.GRP
2520 '                                     [y-AXIS]
2530 JC=1
2540   FOR WYP=YSTART TO YMAX STEP WSTEP
2550     IF WYP<YMIN THEN 2630
2560     LINE (XMIN,-WYP)-(XMIN+WW/60,-WYP),COLF
2570     LINE (XMAX-WW/60,-WYP)-(XMAX,-WYP),COLF
2580     IF LD=1 THEN 2630
2590     WXP=XMAX : WYPP=WYP/WP
2600     IF ABS(WYPP)>32767 THEN 2630
2610     IV=INT(WYPP+.01) : KN$=STR$(IV)
2620     GOSUB 2700                                     'GOSUB *VDRAW.GRP
2630   NEXT
2640   IF LD=1 THEN RETURN
2650     KMIN=80
2660     WXP=XMIN : WYP=YMAX+WW/30
2670     KN$=COMMENT$
2680     GOSUB 2700                                     'GOSUB *VDRAW.GRP
2690 RETURN
2700 '
2710 '-----SUBROUTINE *VDRAW.GRP-----
2720 '     TYPE CHARACTERS(KN$) ON DISPLAY
2730 '     ORIGIN      : (WXP,WYP)  <--- WORLD
2740 '     JC=0 -----> DRAW UNDER ORIGIN
2750 '     JC=1 -----> DRAW RIGHT OF ORIGIN
2760 '     KMIN      : NUMBERS OG CHAECTERS
2770 '     CLH       : COLOUR
2780 '-----
2790 '*VDRAW.GRP
2800 'DIM AX(250)
2810 KL=LEN(KN$)
2820   IF LEFT$(KN$,1)<>" " THEN 2840
2830   KL=KL-1 : KN$=RIGHT$(KN$,KL)
2840   IF KL>KMIN THEN KL=KMIN
2850   KSX=PMAP(WXP,0)+7
2860   IF JC=0 THEN KSX=KSX-4*KL-6
2870   KSY=PMAP(-WYP,1)+6-9*JC
2880   IF (KSY-2)*(KSY-391)=>0 THEN RETURN
2890   FOR IK=1 TO KL
2900     MKL=ASC(MID$(KN$,IK,1))
2910     KSX=KSX+7*(IK-1)
2920     KSY=PMAP(-WYP,1)+4-7*JC
2930     IF (KSX-2)*(KSX-631)=>0 THEN 2970
2940   LOCATE 1,1:PRINT CHR$(MKL)
2950   'GET(0,0)-(20,20),AX
2960   '   PUT (KSX,KSY),AX,XOR
2970 NEXT
2980 RETURN
2990 '
3000 '
3010 '
3020 '
3030 '
3040 '-----SUBROUTINE *GRID.IN-----
3050 '     READ X-Y CORDINATES DATA FROM FILE

```

```

3060 ' (IF FILE NAME="NO", GOTO RETURN)
3070 '-----
3080 '*GRID.IN
3090 IFLG=1
3100 PRINT
3110 PRINT "-----INPUT GRID DATA-----"
3120 PRINT "FILE NAME : NO: NO READING"
3130 PRINT "RETURN KEY: FILES 2"
3140 INPUT "GRID DATA FILE NAME ->",NFGI$
3150 IF NFGI$="" THEN FILES 2:GOTO 3100
3160 IF NFGI$="NO" OR NFGI$="no" THEN RETURN
3170 IFLG=-1
3180 OPEN NFGI$ FOR INPUT AS #1
3190 IF EOF(1) THEN 3320
3200 INPUT #1,NX,NY,XMIN,YMIN,DX,DY
3210 PRINT "GRID : Nx=";NX;" Ny=";NY
3220 FOR I=1 TO NX
3230 FOR J=1 TO NY
3240 IF EOF(1) THEN 3320
3250 INPUT #1,F(I,J)
3260 NEXT
3270 NEXT
3280 IF EOF(1) THEN CMNTG$=" ":GOTO 3310
3290 INPUT #1,CMNTG$
3300 PRINT " [";CMNTG$;"]"
3310 IFLG=0
3320 CLOSE #1
3330 RETURN
3340 '-----SUBROUTINE *OBSDAT.IN-----
3350 ' READ (X,Y,Z) DATA FROM FILE
3360 ' (WHEN INPUT FILE NAME=NO, RETURN WITHOUT READING)
3370 '-----
3380 '
3390 '*OBSDAT.IN
3400 IFLG=1
3410 PRINT
3420 PRINT "-----READ DATA FROM FILE-----"
3430 PRINT " FILE NAME =NO ---->NO READING"
3440 PRINT " RETURN KEY ----> FILES 2"
3450 INPUT " FILE NAME ? ---->",NFDI$
3460 IF NFDI$="NO" OR NFDI$="no" THEN RETURN
3470 IF NFDI$="" THEN FILES 2 : GOTO 3410
3480 IF NFDI$="NO" OR NFDI$="no" THEN RETURN
3490 '
3500 OPEN NFDI$ FOR INPUT AS #1
3510 FOR K=1 TO MXDT
3520 IF EOF(1) THEN 3560
3530 INPUT #1,XD(K),YD(K),ZD(K)
3540 IF XD(K)>VNULL THEN 3560
3550 NEXT
3560 ND=K-1
3570 IFLG=0
3580 IF EOF(1) THEN CMNTD$=" " : GOTO 3600
3590 INPUT #1,CMNTD$
3600 CLOSE #1
3610 RETURN
3620 '-----SUBROUTINE *XYZ.PARAMETER-----
3630 ' PARAMETER TO DISPLAY OBSERVED DATA
3640 '-----
3650 '*XYZ.PARAMETER
3660 PRINT "---DISPLAY OBSERVED DATA---"
3670 JCC=0 : CLH=COLZ
3680 INPUT "-----DISPLAY VALUES? (Y/N) ";ZP$
3690 IF ZP$="n" OR ZP$="N" THEN RETURN
3700 INPUT " Auto(A) OR Manual(M)? ";SD$
3710 ' Zmax :MAX. OF ZD(K)
3720 ZMAX=ABS(ZD(1))
3730 FOR K=2 TO ND
3740 IF ABS(ZD(K))>ZMAX THEN ZMAX=ABS(ZD(K))
3750 NEXT
3760 ' SCALING OF VALUES
3770 NPZ=INT(LOG(ZMAX)/LOG(10)+.0001)
3780 WPZ=10^(NPZ-2)
3790 IF SD$="m" OR SD$="M" THEN 3800 ELSE RETURN
3800 PRINT " MAX. (Z) =";ZMAX
3810 PRINT " {SCALE = ABOUT";WPZ;"}"
3820 INPUT " SCALE =",WPZ
3830 INPUT " LOCATION : (0)UNDER OR (1)RIGHT ? =",JCC

```

```

3840 RETURN
3850 '-----SUBROUTINE *XYZ.DRAW-----
3860 '      DISPLAY OBSERVED DATA ON GRAPHICS
3870 '-----
3880 '*XYZ.DRAW
3890 '
3900 IF ZP$="n" OR ZP$="N" THEN 3970
3910 IF WPZ=1 THEN 3970
3920 KN$="x"+STR$(WPZ)
3930 KMIN=20 : JC=0
3940 WXP=XMIN+(XMAX-XMIN)/20 : WYP=YMAX
3950 GOSUB 2700
3960 '
3970 KMIN=4
3980 JC=JCC
3990 DP=(XMAX-XMIN)/100
4000 FOR K=1 TO ND
4010     IF XD(K)<XMIN OR XD(K)>XMAX THEN 4100
4020     IF YD(K)<YMIN OR YD(K)>YMAX THEN 4100
4030     LINE (XD(K)+DP,-YD(K))- (XD(K)-DP,-YD(K)),1
4040     LINE (XD(K),-YD(K)-DP)- (XD(K),-YD(K)+DP),1
4050     IF ZP$="n" OR ZP$="N" THEN 4100
4060     WXP=XD(K):WYP=YD(K)
4070     IF ABS(ZD(K)/WPZ)>9999 THEN PRINT "SCALE OVER!!!": GOTO 4100
4080     KN$=STR$(CINT(ZD(K)/WPZ))
4090     GOSUB 2700
4100     NEXT
4110 RETURN
4120 '
4130 DIM BALL(62)
4140 KEY OFF:CLS
4150 CIRCLE(20,20),20
4160 PAINT(20,20)
4170 GET(0,0)-(40,40),BALL
4180 FOR I=1 TO 7
4190 LINE(60*I,40*I)-STEP(200,100),IMOD2,BF
4200 NEXT
4210 FOR I=1 TO 170
4220 PUT(3*I+20,2*I),BALL,XOR
4230 PUT(3*I+20,2*I),BALL,XOR
4240 NEXT
4250 END

```

APPENDIX B

COMPUTER PROGRAMS AND RELATED  
DATA FOR MOC MODEL

```

$LARGE
SUBROUTINE CHMOT
DOUBLE PRECISION TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT,TITLE
DOUBLE PRECISION XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,
HMIN,PYR,ANFCTR
COMMON /PRMJ/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,
NUMOBS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,
NPNTMV,NPNTVL,NPNTD,NPNCHV,NPDEL,C,ICLK
COMMON /PRMC/ NODEID(040,040),NPCELL(020,020),NPOLD(020,020),
LIMBO(0500),IXOBS(05),IYOBS(05)
COMMON /HEDA/ THCK(040,040),TMWL(05,50),TMOBS(50)
COMMON /HEDB/ TMRX(040,040,2),VPRM(040,040),HI(040,040),
HR(040,040),HC(040,040),HK(040,040),WT(040,040),
REC(040,040),RECH(040,040),TIM(100),AOPT(20),TITLE(10),XDEL,YDEL,
S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR,ANFCTR
COMMON /HEDC/ MX,MY,MMX,MMY,NMX,NMY,MCHK
COMMON /CHMA/ PART(3,06400),CONC(020,020),TMCN(05,50),VX(040,040),
VY(040,040),CONINT(020,020),CNRECH(020,020),POROS,
SUMTCH,BETA,TIMV,STORM,STORMI,CMSIN,CMSOUT,FLMIN,
FLMOT,SUMIO,CELDIS,DLTRAT,CSTORM
COMMON /CHMR/ RF,DK,RHOB,THALF,DECAY,ADSORB,SORBI,DMASS1,CSTM2,
EKF,XNF,XNFM1,FCTRF,EKL,CEC,EKLCEC,FCTRL,CINMAX,
RF2MIN,RF2MAX,CZERO,IREACT,EK,EKCEC,FCTRE,CTOT,C3,C4,C5,C6
DIMENSION IC(020)
*****
C TMFY=86400.0*365.25
C TMYR=SUMT/TMFY
C TCHD=SUMTCH/86400.0
C TCHYR=SUMTCH/TMFY
C ERR1=0.0
C ERR3=0.0
C IF (MOD(IMOV,NPNTMV).NE.0.AND.(IMOV.NE.NMOV.OR.
1 (MOD(N,NPNT).NE.0.AND.N.NE.NTIM.AND.IPRNT.EQ.0)))
2 GO TO 100
C *****
C ---PRINT CONCENTRATIONS---
WRITE (6,160)
WRITE (6,170) N
IF (N.GT.0) WRITE (6,180) TIM(N)
WRITE (6,190) SUMT
WRITE (6,450) SUMTCH
WRITE (6,200) TCHD
WRITE (6,210) TMYR
WRITE (6,460) TCHYR
WRITE (6,380) IMOV
WRITE (6,220)
DO 20 IY=1,NMY
DO 10 IX=1,NMX
10 IC(IX)=NINT(CONC(IX,IY))
20 WRITE (6,240) (IC(IX),IX=1,NMX)
C *****
C IF (N.EQ.0) GO TO 150
C IF (NPDEL.C.EQ.0) GO TO 50
C ---PRINT CHANGES IN CONCENTRATION---
WRITE (6,230)
WRITE (6,170) N
WRITE (6,180) TIM(N)
WRITE (6,190) SUMT
WRITE (6,450) SUMTCH
WRITE (6,200) TCHD
WRITE (6,210) TMYR
WRITE (6,460) TCHYR
WRITE (6,380) IMOV
WRITE (6,220)
DO 40 IY=1,NMY
DO 30 IX=1,NMX
30 IC(IX)=NINT(CONC(IX,IY)-CONINT(IX,IY))
40 WRITE (6,240) (IC(IX),IX=1,NMX)
C *****
C ---PRINT MASS BALANCE DATA FOR SOLUTE---
50 RESID=SUMIO-CSTM2+DMASS1
SUMIN=FLMIN-CMSIN
IF (SUMIN.EQ.0.0) GO TO 60
ERR1=RESID*100.0/SUMIN
IF (SUMIO.GT.(STORMI+SORBI)) GO TO 70
60 IF (STORMI.EQ.0.0) GO TO 70

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ERR3=-100.0*(RESID)/(STORMI+SORBI-SUMIO)
70 WRITE (6,220)
WRITE (6,250)
WRITE (6,220)
WRITE (6,260) FLMIN
WRITE (6,270) FLMOT
RECIN=-CMSIN
RECOUT=-CMSOUT
WRITE (6,290) RECIN
WRITE (6,280) RECOUT
WRITE (6,295) DMASS1
WRITE (6,296) ADSORB
WRITE (6,298) SORBI
WRITE (6,300) SUMIO
WRITE (6,310) STORMI
WRITE (6,320) STORM
WRITE (6,330) CSTORM
WRITE (6,332) CSTM2
WRITE (6,340)
WRITE (6,350) RESID
WRITE (6,360) ERR1
80 IF (STORMI.EQ.0.0) GO TO 100
IF (SUMIN.NE.0.0.AND.SUMIO.GT.(STORMI+SORBI)) GO TO 100
WRITE (6,370)
WRITE (6,360) ERR3
C *****
C ---PRINT HYDROGRAPHS AFTER 50 STEPS OR END OF SIMULATION---
100 IF (NUMOBS.LE.0) GO TO 150
IF (S.GT.0.0) THEN
IF (IMOV.NE.NMOV.OR.
1 (MOD(N,50).NE.0.AND.N.NE.NTIM.AND.IPRNT.EQ.0)) GO TO 150
ELSE
IF (MOD(IMOV,50).NE.0.AND.IMOV.NE.NMOV) GO TO 150
END IF
WRITE (6,390) TITLE
WRITE (6,400) INT
IF (S.GT.0.0) WRITE (6,410)
IF (S.EQ.0.0) WRITE (6,420)
C ---TABULATE HYDROGRAPH DATA---
MOZ=0
IF (S.GT.0.0) GO TO 110
NTO=NMOV
IF (NMOV.GT.50) NTO=MOD(IMOV,50)
GO TO 120
110 NTO=N
IF (N.GT.50) NTO=MOD(N,50)
120 IF (NTO.EQ.0) NTO=50
DO 140 J=1,NUMOBS
TMYR=0.0
JX=IXOBS(J)
JY=IYOBS(J)
WRITE (6,430) J,IXOBS(J),IYOBS(J)
C1INT=0.0
IX=JX-MX+1
IY=JY-MY+1
IF (JX.LT.MX.OR.JY.LT.MY.OR.JX.GT.MMX.OR.JY.GT.MMY) GO TO 125
C1INT=CONINT(IX,IY)
GO TO 127
125 WRITE (6,435)
127 WRITE (6,440) MOZ,WT(JX,JY),C1INT,
1TMYR
DO 130 M=1,NTO
TMYR=TMOBS(M)/TMFY
130 WRITE (6,440) M,TMWL(J,M),TMCN(J,M),TMYR
140 CONTINUE
C *****
C 150 RETURN
C *****
C
C
C
160 FORMAT (1H1,13HCONCENTRATION/)
170 FORMAT (1X,23HNUMBER OF TIME STRPS = ,1I5)
180 FORMAT (8X,16HDELTA T = ,1G12.5)
190 FORMAT (8X,16HTIME(SECONDS) = ,1G12.5)
200 FORMAT (3X,21HCHEM. TIME(DAYS) = ,1E12.5)
210 FORMAT (8X,16HTIME(YEARS) = ,1E12.5)
220 FORMAT (1H )

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I 661R
I 670
I 680
I 690
I 700
I 710
I 720
I 730
I 740
I 750
I 751R
I 752R
I 753R
I 760
I 770
I 780
I 790
I 795R
I 810
I 820
I 830
I 841
I 846R
I 850
I 860
I 870
I 880
I 921
I 923
I 924
I 925
I 926
I 927
I 928
I 931
I 940
I 950
I 960
I 970
I 980
I 990
I1000
I1010
I1020
I1031
I1041
I1050
I1060
I1070
SI1074
SI1076
I1080
SI1082
SI1083
SI1084
SI1085
SI1086
SI1087
SI1088
SI1091
I1100
I1110
I1120
I1130
I1140
I1150
I1166
I1170
I1180
I1190
I1200
I1210
I1220
I1230
I1240
I1250
I1260
I1270

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230 FORMAT (1H1,23HCHANGE IN CONCENTRATION/) I1280
240 FORMAT (1H0,20I5) I1290
250 FORMAT (1H ,21HCHEMICAL MASS BALANCE) I1300
260 FORMAT (8X,25HMASS IN BOUNDARIES = ,1E12.5) I1310
270 FORMAT (8X,25HMASS OUT BOUNDARIES = ,1E12.5) I1320
280 FORMAT (8X,25HMASS PUMPED OUT = ,1E12.5) I1330
290 FORMAT (8X,25HMASS PUMPED IN = ,1E12.5) I1340
295 FORMAT (8X,25HMASS LOST BY DECAY = ,1E12.5) I1341R
296 FORMAT (8X,25HMASS ADSORBED ON SOLIDS= ,1E12.5) I1342R
298 FORMAT (8X,25HINITIAL MASS ADSORBED = ,1E12.5) I1343R
300 FORMAT (8X,25HINFLOW MINUS OUTFLOW = ,1E12.5) I1350
310 FORMAT (8X,25HINITIAL MASS DISSOLVED = ,1E12.5) I1361R
320 FORMAT (8X,25HPRESENT MASS DISSOLVED = ,1E12.5) I1371R
330 FORMAT (8X,25HCHANGE MASS DISSOLVED = ,1E12.5) I1381R
332 FORMAT (8X,25HCHANGE TOTL.MASS STORED= ,1E12.5) I1382R
340 FORMAT (1H ,5X,53HCOMPARE RESIDUAL WITH NET FLUX AND MASS ACCUMULA I1390
TION: ) I1400
350 FORMAT (8X,25HMASS BALANCE RESIDUAL = ,1E12.5) I1410
360 FORMAT (8X,25HERROR (AS PERCENT) = ,1E12.5) I1420
370 FORMAT (1H ,5X,55HCOMPARE INITIAL MASS STORED WITH CHANGE IN MASS I1430
STORED: ) I1440
380 FORMAT (1X,23H NO. MOVES COMPLETED = ,1I5) I1450
390 FORMAT (1H1,10A8//) I1460
400 FORMAT (1H0,5X,65HTIME VERSUS HEAD AND CONCENTRATION AT SELECTED O I1470
BSERVATION POINTS//15X,19HPUMPING PERIOD NO. ,I4////) I1480
410 FORMAT (1H0,16X,19HTRANSIENT SOLUTION////) I1490
420 FORMAT (1H0,15X,21HSTEADY-STATE SOLUTION////) I1500
430 FORMAT (1H0,20X,22HOBS.WELL NO. X Y,17X,1HN,6X,40HHEAD (FT) I1510
1 CONC.(MG/L) TIME (YEARS)//24X,I3,9X,I2,3X,I2//) I1520
435 FORMAT (1H ,3X,45H** NOTE ** THIS OBS. WELL IS LOCATED OUTSIDE/16 SI1525
1X,24HOF THE TRANSPORT SUBGRID) SI1526
440 FORMAT (1H ,58X,I2,6X,F7.1,8X,F7.3) I1531
450 FORMAT (1H ,2X,21HCHEM.TIME(SECONDS) = ,E12.5) I1540
460 FORMAT (1H ,2X,21HCHEM.TIME(YEARS) = ,E12.5) I1550
END I1560-
C *** RETRD2 ***** K 10
C K 20

$LARGE
SUBROUTINE CNCON G 10
DOUBLE PRECISION TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT,TITLE G 20
DOUBLE PRECISION XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT, G 30
1 HMIN,PYR,ANFCTR G 32
DOUBLE PRECISION DXINV,DYINV,ARINV,PORINV G 35
DOUBLE PRECISION FLW G 40
DOUBLE PRECISION DCYFCT,DCYT,DCYT2 G 42
COMMON /PRMJ/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY, G 51
1 NUMOBS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND, G 61
2 NPNTMV,NPNTVL,NPNTD,NPNCHV,NPDELC,ICLK G 72
COMMON /PRMC/ NODEID(040,040),NPCELL(020,020),NPOLD(020,020), SG 77
1 LIMBO(0500),IXOBS(05),IYOBS(05) G 78
COMMON /HEDA/ THCK(040,040),TMWL(05,50),TMOBS(50) SG 101
COMMON /HEDB/ TMRX(040,040,2),VPRM(040,040),HI(040,040), SG 111
1 HR(040,040),HC(040,040),HK(040,040),WT(040,040), SG 121
2 REC(040,040),RECH(040,040),TIM(100),AOPT(20),TITLE(10),XDEL,YDEL, SG 125
3 S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR,ANFCTR G 131
COMMON /HEDC/ MX,MY,MMX,MMY,NMX,NMY,MCHK SG 135
COMMON /XINV/ DXINV,DYINV,ARINV,PORINV G 140
COMMON /CHMA/ PART(3,06400),CONC(020,020),TMCN(05,50),VX(040,040), SG 152
1 VY(040,040),CONINT(020,020),CNRECH(020,020),POROS, SG 161
2 SUMTCH,BETA,TIMV,STORM,STORMI,CMSIN,CMSOUT,FLMIN, G 165
3 FLMOT,SUMIO,CELDIS,DLTRAT,CSTORM G 171
COMMON /DIFUS/ DISP(020,020,4) G 181
COMMON /CHMC/ SUMC(020,020),VXBDY(040,040),VYBDY(040,040) SG 192
COMMON /CHMR/ RF,DK,RHOB,THALF,DECAY,ADSORB,SORBI,DMASS1,CSTM2, G 196R
1 EKF,XNF,XNFM1,FCTRF,EKL,CEC,EKLCEC,FCTRL,CINMAX, G 197R
2 RF2MIN,RF2MAX,CZERO,IREACT,EK,EKCEC,FCTRE,CTOT,C3,C4,C5,C6 G 198R
COMMON /CHMR2/ CRETRD(020,020),CRDCOF(020,020),CELDY(020,020) G 199R
DIMENSION CNCNC(020,020),CNOLD(020,020),CAVG(020,020) G 202R
C ***** G 210
DO 10 IX=1,NMX SG 232
DO 10 IY=1,NMY SG 242
CNOLD(IX,IY)=CONC(IX,IY) G 250
CAVG(IX,IY)=CONC(IX,IY) G 255R
10 CNCNC(IX,IY)=0.0 G 260
APC=0.0 G 270
NZERO=0 G 280
TVA=AREA*TIMV G 290

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	TVA2=TVA*0.5	G 295R
	TMCHK=TIMV*10.0	G 296R
	SRDCY=0.0	G 297R
	RFAREA=RF*AREA	G 307R
C	*****	G 310
C	---CONC. CHANGE DUE TO:	G 321R
C	MIXING AT SOURCE CELLS...	G 322R
C	...WITH DECAY OF RECHARGE DURING TIME INCREMENT	G 323R
	CONST=TIMV	G 341R
	DCYFCT=TIMV*DECAY	G 342R
	RFFCT=CONST/RF	G 344R
	DCYT=1.DO	G 346A
	DCYT2=1.DO	G 346B
	IF(DECAY.NE.0.0) THEN	G 346C
	DCYT=DEXP(-DCYFCT)	G 346D
	DCYT2=DEXP(-DCYFCT*0.5DO)	G 346E
	END IF	G 346F
	GO TO 70	G 347R
20	DO 60 IX=1,NMX	SG 352
	DO 60 IY=1,NMY	SG 362
	JX=IX+MX-1	SG 366
	JY=IY+MY-1	SG 367
	IF (THCK(JX,JY).EQ.0.0) GO TO 60	SG 371
	CALL RETRD2(CAVG(IX,IY),RF2,RDCOEF)	G 384R
	EQFCT=RFFCT/(THCK(JX,JY)*RF2)	SG 385R
	C1=CAVG(IX,IY)	G 401R
	IF (ABS(C1).LT.1.0E-20) C1=0.0	MULTICS
	C2=C1	G 403R
	CLKCN=C1	G 411R
	SLEAK=(HK(JX,JY)-WT(JX,JY))*VPRM(JX,JY)	SG 421
	IF (SLEAK.GE.0.0) GO TO 25	G 425R
	CLKCN=CNRECH(IX,IY)*DCYT2	G 431A
	SRDCY=SRDCY+(CNRECH(IX,IY)-CLKCN)*SLEAK*TVA	G 432R
25	CONTINUE	G 435R
	CNREC=C1	G 450
	CNREC2=C1	G 455
	RATE=REC(JX,JY)*ARINV	SG 461
	IF (RATE.GE.0.0) GO TO 27	G 471R
	CNREC=CNRECH(IX,IY)*DCYT2	G 472A
	SRDCY=SRDCY+(CNRECH(IX,IY)-CNREC)*RATE*TVA	G 473R
27	IF (RECH(JX,JY).GE.0.0) GO TO 29	SG 474R
	CNREC2=CNRECH(IX,IY)*DCYT2	G 476A
	SRDCY=SRDCY+(CNRECH(IX,IY)-CNREC2)*RECH(JX,JY)*TVA	SG 477R
29	CONTINUE	G 478R
	DIV=RATE+SLEAK+RECH(JX,JY)	SG 481
	IF (THALF.GT.TMCHK.OR.THALF.EQ.0.0) GO TO 37	G 482R
	IF (DIV.GE.0.0) GO TO 37	G 484R
	IF (CNOLD(IX,IY).LE.0.0.OR.CONC(IX,IY).LE.0.0) GO TO 37	G 486R
C	NEXT CALC IS EQUIVALENT TO C1=EXP((ALOG(CNOLD)+ALOG(CONC))*0.5)	G 488A
	C1=SQRT(CNOLD(IX,IY)*CONC(IX,IY))	G 488B
C	IF (NPCELL(IX,IY).LE.0) C1=CNOLD(IX,IY)*DCYT2	G 489A
37	CONTINUE	G 592R
	DELC=EQFCT*(C1*DIV-RATE*CNREC-SLEAK*CLKCN-RECH(JX,JY)*CNREC2)	SG 597
40	CNCNC(IX,IY)=CNCNC(IX,IY)+DELC	G 610
C	---CONC. CHANGE DUE TO DISPERSION FOR TIMV---	G 621R
C	---DISPERSION WITH TENSOR COEFFICIENTS---	G 630
	IF (BETA.EQ.0.0) GO TO 60	G 635
	IF (MCHK.EQ.1) GO TO 39	SG 638
	X1=DISP(IX,IY,1)*(CAVG(IX+1,IY)-C2)	G 651R
	X2=DISP(IX-1,IY,1)*(CAVG(IX-1,IY)-C2)	G 661R
	Y1=DISP(IX,IY,2)*(CAVG(IX,IY+1)-C2)	G 671R
	Y2=DISP(IX,IY-1,2)*(CAVG(IX,IY-1)-C2)	G 681R
	XX1=DISP(IX,IY,3)*(CAVG(IX,IY+1)+CAVG(IX+1,IY+1)-CAVG(IX,IY-1)-CAV	G 691R
	1G(IX+1,IY-1))	G 701R
	XX2=DISP(IX-1,IY,3)*(CAVG(IX,IY+1)+CAVG(IX-1,IY+1)-CAVG(IX,IY-1)-C	G 711R
	1AVG(IX-1,IY-1))	G 721R
	YY1=DISP(IX,IY,4)*(CAVG(IX+1,IY)+CAVG(IX+1,IY+1)-CAVG(IX-1,IY)-CAV	G 731R
	1G(IX-1,IY+1))	G 741R
	YY2=DISP(IX,IY-1,4)*(CAVG(IX+1,IY)+CAVG(IX+1,IY-1)-CAVG(IX-1,IY)-C	G 751R
	1AVG(IX-1,IY-1))	G 761R
	GO TO 48	SG 762
39	X1=0.0	SG 763A
	X2=0.0	SG 763B
	Y1=0.0	SG 763C
	Y2=0.0	SG 763D
	XX1=0.0	SG 763E
	XX2=0.0	SG 763F
	YY1=0.0	SG 763G



	YY2=0.0	SG 763H
	IF (IX.GE.NMX) GO TO 41	SG 763I
	X1=DISP(IX,IY,1)*(CAVG(IX+1,IY)-C2)	SG 763J
41	IF (IX.LE.1) GO TO 42	SG 763K
	X2=DISP(IX-1,IY,1)*(CAVG(IX-1,IY)-C2)	SG 763L
42	IF (IY.GE.NMY) GO TO 43	SG 763M
	Y1=DISP(IX,IY,2)*(CAVG(IX,IY+1)-C2)	SG 763N
43	IF (IY.LE.1) GO TO 46	SG 763O
	Y2=DISP(IX,IY-1,2)*(CAVG(IX,IY-1)-C2)	SG 763P
44	IF (IY.GE.NMY) GO TO 47	SG 764
	IF (IX.GE.NMX) GO TO 45	SG 765
	XX1=DISP(IX,IY,3)*(CAVG(IX,IY+1)+CAVG(IX+1,IY+1)-CAVG(IX,IY-1)-CAV	SG 766A
	1G(IX+1,IY-1))	SG 766B
45	IF (IX.LE.1) GO TO 48	SG 766C
	XX2=DISP(IX-1,IY,3)*(CAVG(IX,IY+1)+CAVG(IX-1,IY+1)-CAVG(IX,IY-1)-C	SG 766D
	1AVG(IX-1,IY-1))	SG 766E
46	IF (IX.LE.1) GO TO 48	SG 766F
	IF (IY.GE.NMY) GO TO 47	SG 766G
	IF (IX.GE.NMX) GO TO 48	SG 766H
	YY1=DISP(IX,IY,4)*(CAVG(IX+1,IY)+CAVG(IX+1,IY+1)-CAVG(IX-1,IY)-CAV	SG 766I
	1G(IX-1,IY+1))	SG 766J
47	IF (IY.LE.1) GO TO 48	SG 766K
	IF (IX.LE.1.OR.IX.GE.NMX) GO TO 48	SG 766L
	YY2=DISP(IX,IY-1,4)*(CAVG(IX+1,IY)+CAVG(IX+1,IY-1)-CAVG(IX-1,IY)-C	SG 766M
	1AVG(IX-1,IY-1))	SG 766O
48	CONTINUE	SG 768
	CNCNC(IX,IY)=CNCNC(IX,IY)+EQFCT*(X1+X2+Y1+Y2+XX1-XX2+YY1-YY2)	G 772
60	CONTINUE	G 780
C	*****	G 790
	GO TO 110	G 820
C	*****	G 830
C	---CONC. CHANGE AT NODES DUE TO CONVECTION---	G 840
C	... AND DECAY---	G 841R
	70 DO 90 IX=1,NMX	SG 852
	DO 90 IY=1,NMY	SG 862
	JX=IX+MX-1	SG 866
	JY=IY+MY-1	SG 867
	IF (THCK(JX,JY).EQ.0.0) GO TO 90	SG 871
	APC=NPCELL(IX,IY)	G 880
	IF (APC.GT.0.0) GO TO 80	G 890
	IF (REC(JX,JY).NE.0.0.OR.VPRM(JX,JY).GT.0.09) GO TO 90	SG 901
	NZERO=NZERO+1	G 910
	GO TO 90	G 920
	80 CONC(IX,IY)=SUMC(IX,IY)/APC	G 930
	CAVG(IX,IY)=(CONC(IX,IY)+CNOLD(IX,IY))*0.5	G 935R
	90 CONTINUE	G 940
C	---CHECK NUMBER OF CELLS VOID OF PTS.---	G 950
	IF (NZERO.GT.0) WRITE (6,290) NZERO,IMOV	G 980
	IF (NZERO.LE.NZCRIT) GO TO 20	G 970
	TEST=99.0	G 980
	WRITE (6,300)	G 990
	WRITE (6,320)	G1000
	DO 100 IY=1,NMY	SG1011
100	WRITE (6,330) (NPCELL(IX,IY),IX=1,NMX)	SG1021
	GO TO 20	G1030
C	*****	G1040
C	---CHANGE CONCENTRATIONS AT NODES---	G1050
	110 DO 130 IX=1,NMX	SG1062
	DO 130 IY=1,NMY	SG1072
	JX=IX+MX-1	SG1076
	JY=IY+MY-1	SG1077
	IF (THCK(JX,JY).EQ.0.0) GO TO 120	SG1081
	CNCPCT=0.0	G1084G
	IF (CONC(IX,IY).GT.0.0) CNCPCT=CNCNC(IX,IY)/CONC(IX,IY)	G1085G
	CONC(IX,IY)=CONC(IX,IY)+CNCNC(IX,IY)	G1090
	SUMC(IX,IY)=0.0	G1110
	IF (CNCPCT.LT.0.0) SUMC(IX,IY)=CNCPCT	G1125G
	GO TO 130	G1150
120	IF (CONC(IX,IY).GT.0.0) WRITE (6,310) JX,JY,CONC(IX,IY)	SG1161
	CONC(IX,IY)=0.0	G1170
130	CONTINUE	G1180
C	*****	G1190
C	---CHANGE CONCENTRATION OF PARTICLES---	G1200
	DO 180 IN=1,NP	G1210
	IF (PART(1,IN).EQ.0.0) GO TO 180	G1220
	INX=ABS(PART(1,IN))+0.5	G1230
	INY=ABS(PART(2,IN))+0.5	G1240
	JNX=INX-MX+1	SG1244

	JNY=INY-MY+1	SG1245
C	---UPDATE CONC. OF PTS. IN SINK/SOURCE CELLS---	G1250
	IF (REC(INX,INY).NE.0.0) GO TO 140	G1260
	IF (VPRM(INX,INY).LE.0.09) GO TO 150	G1270
140	PART(3,IN)=CONC(JNX,JNY)	SG1281
	GO TO 180	G1290
150	IF (CNCNC(JNX,JNY).LT.0.0) GO TO 170	SG1301
160	PART(3,IN)=PART(3,IN)+CNCNC(JNX,JNY)	SG1311
	GO TO 180	G1320
170	IF (CONC(JNX,JNY).LE.0.0) GO TO 160	SG1331
	IF (SUMC(JNX,JNY).LT.-1.0) GO TO 160	SG1341
	PART(3,IN)=PART(3,IN)+PART(3,IN)*SUMC(JNX,JNY)	SG1351
180	CONTINUE	G1360
	WRITE (6,280) TIM(N),TIMV,SUMTCH	G1370
C	*****	G1380
C	---COMPUTE MASS BALANCE FOR SOLUTE---	G1390
	CSTORM=0.0	G1400
	STORM=0.0	G1410
	ADSORB=0.0	G1411R
	ADSRB2=0.0	G1412R
	DO 270 IX=1,NMX	SG1422
	DO 270 IY=1,NMY	SG1432
	JX=IX+MX-1	SG1435
	JY=IY+MY-1	SG1436
	IF (THCK(JX,JY).EQ.0.0) GO TO 270	SG1441
	C1=CONC(IX,IY)	G1442R
	C1B=C1*THCK(JX,JY)	SG1443R
	IF (DECAY.NE.0.0) THEN	G1445A
	DELDCY=CNOLD(IX,IY)*(1.0-DCYT)	G1445B
	IF (IREACT.GE.2) DELDCY=DELDCY+SORB2(CNOLD(IX,IY))*(1.0-DCYT)*C3	G1445C
	DMASS1=DMASS1-DELDCY*THCK(JX,JY)*RFAREA	SG1447R
	END IF	G1447R
	SUMC(IX,IY)=0.0	G1450
	WTFCT=0.0	G1455
C	---COMPUTE MASS OF SOLUTE IN STORAGE---	G1460
	STORM=STORM+C1B	G1471A
C	---COMPUTE MASS ADSORBED---	G1472R
	ADSORB=C1B+ADSORB	G1474R
	IF (IREACT.GE.2) ADSRB2=ADSRB2+THCK(JX,JY)*SORB2(C1)	SG1475R
C	---ACCOUNT FOR MASS PUMPED IN, OUT, RECHARGED, & DISCHARGED---	G1480
	IF (REC(JX,JY)) 200,210,190	SG1491
190	FCT1=NPOLD(IX,IY)	G1492
	FCT2=NPCELL(IX,IY)	G1494
	IF (FCT2.GT.0.0) WTFCT=FCT1/FCT2	G1496
	CMSOUT=CMSOUT+REC(JX,JY)*TIMV*((1.0-WTFCT)*CNOLD(IX,IY)+WTFCT*C1)	SG1498R
	GO TO 210	G1510
200	CMSIN=CMSIN+REC(JX,JY)*CNRECH(IX,IY)*TIMV	SG1521
210	IF (RECH(JX,JY)) 230,240,220	SG1531
220	CMSOUT=CMSOUT+RECH(JX,JY)*TVA2*(CNOLD(IX,IY)+C1)	SG1538R
	GO TO 240	G1550
230	CMSIN=CMSIN+RECH(JX,JY)*CNRECH(IX,IY)*TVA	SG1561
C	*****	G1570
C	---ACCOUNT FOR BOUNDARY FLOW---	G1580
240	IF (VPRM(JX,JY).EQ.0.0) GO TO 265	SG1586
	FLW=VPRM(JX,JY)*(WT(JX,JY)-HK(JX,JY))	SG1601
	IF (FLW.GT.0.0) GO TO 250	G1610
	IF (FLW.LT.0.0) GO TO 260	G1620
	GO TO 265	G1625
C	---MASS IN BOUNDARY DURING TIME STEP---	G1640
250	FLMIN=FLMIN+FLW*CNRECH(IX,IY)*TVA	G1650
	GO TO 265	G1655
C	---MASS OUT DURING TIME STEP---	G1670
260	FCT1=NPOLD(IX,IY)	G1672
	FCT2=NPCELL(IX,IY)	G1674
	IF (FCT2.GT.0.0) WTFCT=FCT1/FCT2	G1676
	FLMOT=FLMOT+FLW*TVA*((1.0-WTFCT)*CNOLD(IX,IY)+WTFCT*C1)	G1679R
265	NPOLD(IX,IY)=NPCELL(IX,IY)	G1682
	NPCELL(IX,IY)=0	G1684
	IF (IREACT.GE.2) THEN	G1686R
	CALL RETRD2(C1,CRETDR(IX,IY),CRDCOF(IX,IY))	G1687A
	IF (DECAY.NE.0.0)	G1687B
1	CELDY(IX,IY)=EXP(-DCYFCT*CRDCOF(IX,IY)/CRETDR(IX,IY))	G1687C
	END IF	G1688R
270	CONTINUE	G1690
C	---SUBGRID BOUNDARIES---	SG1692A
	IF (MCHK.EQ.0) GO TO 275	SG1692B
	YT=YDEL*TIMV	SG1692C
	XT=XDEL*TIMV	SG1692D

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DO 272 IY=MY,MMY
IX=MX
JY=IY-MY+1
FLW=TMRX(IX-1,IY,1)*(HK(IX-1,IY)-HK(IX,IY))
IF (FLW.GT.0.0) FLMIN=FLMIN+FLW*YT*CNOLD(1,JY)*DCYT
IF (FLW.LT.0.0) FLMOT=FLMOT+FLW*YT*CNOLD(1,JY)*DCYT
IX=MMX
FLW=TMRX(IX,IY,1)*(HK(IX+1,IY)-HK(IX,IY))
IF (FLW.GT.0.0) FLMIN=FLMIN+FLW*YT*CNOLD(NMX,JY)*DCYT
272 IF (FLW.LT.0.0) FLMOT=FLMOT+FLW*YT*CNOLD(NMX,JY)*DCYT
DO 274 IX=MX,MMX
IY=MY
JX=IX-MX+1
FLW=TMRX(IX,IY-1,2)*(HK(IX,IY-1)-HK(IX,IY))
IF (FLW.GT.0.0) FLMIN=FLMIN+FLW*XT*CNOLD(JX,1)*DCYT
IF (FLW.LT.0.0) FLMOT=FLMOT+FLW*XT*CNOLD(JX,1)*DCYT
IY=MMY
FLW=TMRX(IX,IY,2)*(HK(IX,IY+1)-HK(IX,IY))
IF (FLW.GT.0.0) FLMIN=FLMIN+FLW*XT*CNOLD(JX,NMY)*DCYT
274 IF (FLW.LT.0.0) FLMOT=FLMOT+FLW*XT*CNOLD(JX,NMY)*DCYT
275 CONTINUE
C *****
C ---COMPUTE CHANGE IN MASS OF SOLUTE STORED---
C ---COMPUTE MASS LOST BY DECAY---
STORM=STORM*AREA
ADSORB=(ADSORB*DK+ADSRB2)*RHOB/POROS*AREA
CSTORM=STORM-STORMI
CSTM2=CSTORM+ADSORB-SORBI
DMASS1=DMASS1+SRCDCY
SUMIO=FLMIN+FLMOT-CMSIN-CMSOUT
C *****
C ---REGENERATE PARTICLES IF 'NZCRIT' EXCEEDED---
IF (TEST.GT.98.0) CALL GENPT
TEST=0.0
C *****
C RETURN
C *****
C
C
C
C
280 FORMAT (3H ,11HTIM(N) = ,1G12.5,10X,11HTIMV = ,1G12.5,10X,
19HSUMTCH = ,G12.5)
290 FORMAT (1H0,5X,40HNUMBER OF CELLS WITH ZERO PARTICLES = ,I4,5X,9
1HIMOV = ,I4/)
300 FORMAT (1H0,5X,44H*** NZCRIT EXCEEDED --- CALL GENPT ***/)
310 FORMAT (1H ,5X,37H***CONC.GT.0.AND.THCK.EQ.0 AT NODE = ,2I4,4X,7HC
1ONC = ,G10.4,4H ***)
320 FORMAT (1H0,2X,6HNPCELL/)
330 FORMAT (1H ,4X,20I3)
END

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$LARGE
SUBROUTINE GENPT
DOUBLE PRECISION TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT,TITLE
DOUBLE PRECISION XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,
1 HMIN,PYR,ANFCTR
INTEGER PTID
COMMON /PRMJ/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,
1 NUMOBS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,
2 NPNTMV,NPNTVL,NPNTD,NPNCHV,NPDEL,ICLK
COMMON /PRMC/ NODEID(040,040),NPCELL(020,020),NPOLD(020,020),
1 LIMBO(0500),IXOBS(05),IYOBS(05)
COMMON /HEDA/ THCK(040,040),TMWL(05,50),TMOBS(50)
COMMON /HEDB/ TMRX(040,040,2),VPRM(040,040),HI(040,040),
1 HR(040,040),HC(040,040),HK(040,040),WT(040,040),
2 REC(040,040),RECH(040,040),TIM(100),AOPT(20),TITLE(10),XDEL,YDEL,
3 S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR,ANFCTR
COMMON /HEDC/ MX,MY,MMX,MMY,NMX,NMY,MCHK
COMMON /CHMA/ PART(3,06400),CONC(020,020),TMCN(05,50),VX(040,040),
1 VY(040,040),CONINT(020,020),CNRECH(020,020),POROS,
2 SUMTCH,BETA,TIMV,STORM,STORMI,CMSIN,CMSOUT,FLMIN,
3 FLMOT,SUMIO,CELDIS,DLTRAT,CSTORM
COMMON /CHMP/ PTID(06400)
DIMENSION RPT(16),RNT(16),RP(16),RN(16),IPT(16)
C *****
IONED=0
IF (NX.EQ.3.OR.NY.EQ.3) IONED=1

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F1=0.30 D 180
F2=1.0/3.0 D 190
IF (NPTPND.EQ.4) F1=0.25 D 200
IF (NPTPND.EQ.5.AND.IONED.EQ.1) F1=0.25 D 202
IF (NPTPND.EQ.9) F1=1.0/3.0 D 210
IF (NPTPND.EQ.8.AND.IONED.NE.1) F2=0.25 D 221
IF (NPTPND.EQ.8.AND.IONED.EQ.1) F1=1.0/3.0 D 222
IF (NPTPND.EQ.16) F1=0.25 D 223
IF (NPTPND.EQ.16) F2=0.125 D 224
NCHK=NPTPND D 230
IF (NPTPND.EQ.5.OR.NPTPND.EQ.9) NCHK=NPTPND-1 D 240
IF (TEST.GT.98.) GO TO 10 D 250
C ***** D 260
C ---INITIALIZE VALUES--- D 270
  STORM=0.0 D 280
  CMSIN=0.0 D 290
  CMSOUT=0.0 D 300
  FLMIN=0.0 D 310
  FLMOT=0.0 D 320
  SUMIO=0.0 D 330
C ***** D 340
10 DO 20 IN=1,NPMAX D 345
  PTID(IN)=0 D 355
  DO 20 ID=1,3 D 365
20 PART(ID,IN)=0.0 D 370
  DO 30 IA=1,16 D 381
  RP(IA)=0.0 D 390
  RN(IA)=0.0 D 400
  RPT(IA)=0.0 D 401
  RNT(IA)=0.0 D 402
30 IPT(IA)=0 D 410
C ---SET UP LIMBO ARRAY--- D 420
  DO 40 IN=1,500 D 430
40 LIMBO(IN)=0 D 441
  IND=1 D 450
C ***** D 490
C ---INSERT PARTICLES--- D 500
C ---TRACK PARTICLE LOCATIONS IN COORDINATES OF PRIMARY GRID--- SD 505
  DO 410 IX=1,NMX SD 512
  JX=IX+MX-1 SD 515
  DO 410 IY=1,NMY SD 522
  JY=IY+MY-1 SD 525
  IF (THCK(JX,JY).EQ.0.0) GO TO 410 SD 531
  KR=0 D 540
  KR2=0 D 541
  TEST2=0.0 D 550
  METH=1 D 560
  NPCELL(IX,IY)=0 D 570
  NPOLD(IX,IY)=NPTPND D 575
  C1=CONC(IX,IY) D 580
  IF (NPTPND.EQ.1) GO TO 150 D 585
  IF (C1.LE.1.0E-05) TEST2=1.0 D 590
  IF (IX.EQ.1.OR.IX.EQ.NMX.OR.IY.EQ.1.OR.IY.EQ.NMY) TEST2=1.0 SD 595
  IF (VPRM(JX,JY).GT.0.09) TEST2=1.0 SD 601
  IF (REC(JX,JY).NE.0.0) TEST2=1.0 SD 611
  IF (THCK(JX+1,JY+1).EQ.0.0.OR.THCK(JX+1,JY-1).EQ.0.0.OR.THCK(JX-1, SD 621
1JY+1).EQ.0.0.OR.THCK(JX-1,JY-1).EQ.0.0) TEST2=1.0 SD 631
  IF ((THCK(JX,JY+1).EQ.0.0.OR.THCK(JX,JY-1).EQ.0.0.OR.THCK(JX+1,JY) SD 641
1.EQ.0.0.OR.THCK(JX-1,JY).EQ.0.0).AND.NPTPND.GT.5) TEST2=1.0 SD 651
  CNODE=C1*(1.0-F1) D 660
  IF (TEST.LT.98.0.OR.TEST2.GT.0.0) GO TO 70 D 670
  SUMC=CONC(IX+1,IY)+CONC(IX-1,IY)+CONC(IX,IY+1)+CONC(IX,IY-1) D 680
  IF (NCHK.EQ.4) GO TO 60 D 690
  SUMC=SUMC+CONC(IX+1,IY+1)+CONC(IX+1,IY-1)+CONC(IX-1,IY+1)+CONC(IX- D 700
11,IY-1) D 710
60 AVC=SUMC/NCHK D 720
  IF (AVC.GT.C1) METH=2 D 730
C ---PUT 4 PARTICLES ON CELL DIAGONALS--- D 740
C D 750
70 DO 140 IT=1,2 D 760
  EVET=(-1.0)**IT D 770
  DO 140 IS=1,2 D 780
  IF (IONED.EQ.1.AND.IT.EQ.1.AND.IS.EQ.2) GO TO 140 D 782
  IF (IONED.EQ.1.AND.IT.EQ.2.AND.IS.EQ.1) GO TO 140 D 783
  EVES=(-1.0)**IS D 790
  KR=KR+1 D 793
  IF (NPTPND.EQ.16) GO TO 72 D 795
  PART(1,IND)=JX+F1*EVET SD 801

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	PART(2,IND)=JY+F1*EVES	SD 811
	PART(2,IND)=-PART(2,IND)	D 820
	PART(3,IND)=C1	D 830
	IPT(KR)=IND	D 833
	PTID(IND)=KR	D 834
	IF (IONED.EQ.1.AND.IS.EQ.2) PTID(IND)=4	D 834A
	GO TO 76	D 835
72	IF (TEST.LT.98.0.OR.TEST2.GT.0.0) GO TO 135	D 841
76	IF (TEST.LT.98.0.OR.TEST2.GT.0.0) GO TO 139	D 845
	IXD=IX+EVET	D 850
	IYD=IY+EVES	D 860
	IF (METH.EQ.2) GO TO 80	D 890
	PARTC=CNODE+CONC(IXD,IYD)*F1	D 901
	GO TO 90	D 910
80	PARTC=2.0*C1*CONC(IXD,IYD)/(C1+CONC(IXD,IYD))	D 921
90	IF (C1-CONC(IXD,IYD)) 100,110,120	D 930
100	RPT(KR)=CONC(IXD,IYD)-PARTC	D 941
	RNT(KR)=C1-PARTC	D 951
	GO TO 130	D 960
110	RPT(KR)=0.0	D 971
	RNT(KR)=0.0	D 981
	GO TO 130	D 990
120	RPT(KR)=C1-PARTC	D1001
	RNT(KR)=CONC(IXD,IYD)-PARTC	D1011
130	IF (NPTPND.EQ.16) GO TO 135	D1012
	PART(3,IND)=PARTC	D1013
	RP(KR)=RPT(KR)	D1014
	RN(KR)=RNT(KR)	D1015
	GO TO 139	D1016
135	DO 138 ITT = 1,2	D1017
	EVET2=(-1.0)**ITT	D1018
	DO 138 ISS = 1,2	D1019
	IF(IONED.EQ.1.AND.ITT.EQ.1.AND.ISS.EQ.2) GO TO 138	D1019A
	IF(IONED.EQ.1.AND.ITT.EQ.2.AND.ISS.EQ.1) GO TO 138	D1019B
	EVES2=(-1.0)**ISS	D1021
	PART(1,IND)=(JX+F1*EVET)+F2*EVET2	SD1022A
	PART(2,IND)=(JY+F1*EVES)+F2*EVES2	SD1023A
	PART(2,IND)=-PART(2,IND)	D1024
	KR2=KR2+1	D1025
	IF (TEST.LT.98.0.OR.TEST2.GT.0.0) GO TO 136	D1026
	PART(3,IND) = PARTC	D1027
	RP(KR2) = RPT(KR)	D1028
	RN(KR2) = RNT(KR)	D1029
	IPT(KR2) = IND	D1031
	GO TO 137	D1032
136	PART(3,IND) = C1	D1033
137	PTID(IND)=KR2	D1034
	IF(IONED.EQ.1) THEN	D1034A
	IF(IT.EQ.1.AND.ISS.EQ.2) PTID(IND)=4	D1034B
	IF(IT.EQ.2) THEN	D1034C
	IF(ISS.EQ.1) PTID(IND)=13	D1034D
	IF(ISS.EQ.2) PTID(IND)=16	D1034E
	END IF	D1034F
	END IF	D1034G
	IND=IND+1	D1035
138	CONTINUE	D1036
	GO TO 140	D1037
139	IND=IND+1	D1038
140	CONTINUE	D1039
	IF (NPTPND.EQ.16) GO TO 290	D1045
	IF ((NPTPND.EQ.5.AND.IONED.NE.1).OR.NPTPND.EQ.9) GO TO 150	D1051
	IF (NPTPND.EQ.8.AND.IONED.EQ.1) GO TO 150	D1052
	GO TO 160	D1060
C	---PUT ONE PARTICLE AT CENTER OF CELL---	D1070
150	PART(1,IND)=JX	SD1076
	PART(2,IND)=-JY	SD1091
	PART(3,IND)=C1	D1100
	PTID(IND)=5	D1105
	IND=IND+1	D1110
	IF (NPTPND.EQ.1) GO TO 410	D1115
C	---PLACE NORTH, SOUTH, EAST, AND WEST PARTICLES---	D1120
160	IF (NPTPND.LT.8) GO TO 290	D1130
	IF(IONED.EQ.1) GO TO 290	D1132
	CNODE=C1*(1.0-F2)	D1140
	DO 280 IT=1,2	D1150
	EVET=(-1.0)**IT	D1160
	PART(1,IND)=JX+F2*EVET	SD1171
	PART(2,IND)=-JY	SD1181

PART(3,IND)=C1	D1190
IF (EVET.LT.0) PTID(IND)=6	D1192
IF (EVET.GT.0) PTID(IND)=8	D1194
IF (TEST.LT.98.0.OR.TEST2.GT.0.0) GO TO 220	D1200
IXD=IX+EVET	D1210
KR=KR+1	D1220
IPT(KR)=IND	D1230
IF (METH.EQ.2) GO TO 170	D1240
PART(3,IND)=CNODE+CONC(IXD,IY)*F2	D1250
GO TO 180	D1260
170 PART(3,IND)=2.0*C1*CONC(IXD,IY)/(C1+CONC(IXD,IY))	D1270
180 IF (C1-CONC(IXD,IY)) 190,200,210	D1280
190 RP(KR)=CONC(IXD,IY)-PART(3,IND)	D1290
RN(KR)=C1-PART(3,IND)	D1300
GO TO 220	D1310
200 RP(KR)=0.0	D1320
RN(KR)=0.0	D1330
GO TO 220	D1340
210 RP(KR)=C1-PART(3,IND)	D1350
RN(KR)=CONC(IXD,IY)-PART(3,IND)	D1360
220 IND=IND+1	D1370
PART(1,IND)=JX	SD1381
PART(2,IND)=JY+F2*EVET	SD1391
PART(2,IND)=-PART(2,IND)	D1400
PART(3,IND)=C1	D1410
IF (EVET.LT.0) PTID(IND)=7	D1412
IF (EVET.GT.0) PTID(IND)=9	D1414
IF (TEST.LT.98.0.OR.TEST2.GT.0.0) GO TO 280	D1420
IYD=IY+EVET	D1430
KR=KR+1	D1440
IPT(KR)=IND	D1450
IF (METH.EQ.2) GO TO 230	D1460
PART(3,IND)=CNODE+CONC(IX,IYD)*F2	D1470
GO TO 240	D1480
230 PART(3,IND)=2.0*C1*CONC(IX,IYD)/(C1+CONC(IX,IYD))	D1490
240 IF (C1-CONC(IX,IYD)) 250,260,270	D1500
250 RP(KR)=CONC(IX,IYD)-PART(3,IND)	D1510
RN(KR)=C1-PART(3,IND)	D1520
GO TO 280	D1530
260 RP(KR)=0.0	D1540
RN(KR)=0.0	D1550
GO TO 280	D1560
270 RP(KR)=C1-PART(3,IND)	D1570
RN(KR)=CONC(IX,IYD)-PART(3,IND)	D1580
280 IND=IND+1	D1590
C	D1600
290 IF (TEST.LT.98.0.OR.TEST2.GT.0.0) GO TO 410	D1610
SUMPT=0.0	D1620
C	D1630
---COMPUTE CONC. GRADIENT WITHIN CELL---	D1640
DO 300 KPT=1,NCHK	D1650
IK=IPT(KPT)	D1660
300 SUMPT=PART(3,IK)+SUMPT	D1670
CBAR=SUMPT/NCHK	D1680
C	D1690
---CHECK MASS BALANCE WITHIN CELL AND ADJUST PT. CONCS.---	D1700
SUMPT=0.0	D1710
IF (CBAR-C1) 310,410,330	D1720
310 CRCT=1.0-(CBAR/C1)	D1730
IF (METH.EQ.1) CRCT=CBAR/C1	D1740
DO 320 KPT=1,NCHK	D1750
IK=IPT(KPT)	D1760
PART(3,IK)=PART(3,IK)+RP(KPT)*CRCT	D1770
320 SUMPT=SUMPT+PART(3,IK)	D1780
CBARN=SUMPT/NCHK	D1790
GO TO 350	D1800
330 CRCT=1.0-(C1/CBAR)	D1810
IF (METH.EQ.1) CRCT=C1/CBAR	D1820
DO 340 KPT=1,NCHK	D1830
IK=IPT(KPT)	D1840
PART(3,IK)=PART(3,IK)+RN(KPT)*CRCT	D1850
340 SUMPT=SUMPT+PART(3,IK)	D1860
CBARN=SUMPT/NCHK	D1870
350 IF (CBARN.EQ.C1) GO TO 410	D1880
C	D1890
---CORRECT FOR OVERCOMPENSATION---	D1900
CRCT=C1/CBARN	D1910
DO 360 KPT=1,NCHK	D1920
IK=IPT(KPT)	
PART(3,IK)=PART(3,IK)*CRCT	
C	
---CHECK CONSTRAINTS---	

```

IF (PART(3,IK)-C1) 360,380,370
360 CLIM=C1-RP(KPT)+RN(KPT)
IF (PART(3,IK).LT.CLIM) GO TO 390
GO TO 380
370 CLIM=C1+RP(KPT)-RN(KPT)
IF (PART(3,IK).GT.CLIM) GO TO 390
380 CONTINUE
GO TO 410
390 TEST2=1.0
DO 400 KPT=1,NCHK
IK=IPT(KPT)
400 PART(3,IK)=C1
410 CONTINUE
NP=IND-1
IF (INT.EQ.0) CALL CHMOT
C *****
RETURN
C *****
END
D1930
D1940
D1950
D1960
D1970
D1980
D1990
D2000
D2010
D2020
D2030
D2040
D2050
D2061
D2070
D2080
D2090
D2100
D2110-

$LARGE
SUBROUTINE ITERAT
DOUBLE PRECISION DMIN1,DEXP,DLOG,DABS
DOUBLE PRECISION TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT,TITLE
DOUBLE PRECISION XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,
1 HMIN,PYR,ANFCTR
DOUBLE PRECISION DXINV,DYINV,ARINV,PORINV
DOUBLE PRECISION B,G,W,A,C,E,F,DR,DC,TBAR,TKM,COEF,BLH,BRK,CHK,QL,
1 BRH
DOUBLE PRECISION TOTLQ,TOTLQI,TPIN,TPOUT,PQIN,PQOUT,DELQ
COMMON /PRMJ/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,
1 NUMOBS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,
2 NPNTMV,NPNTVL,NPNTD,NPNCHV,NPDELC,ICLK
COMMON /HEDA/ THCK(040,040),TMWL(05,50),TMOBS(50)
COMMON /HEDB/ TMRX(040,040,2),VPRM(040,040),HI(040,040),
1 HR(040,040),HC(040,040),HK(040,040),WT(040,040),
2 REC(040,040),RECH(040,040),TIM(100),AOPT(20),TITLE(10),XDEL,YDEL,
3 S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR,ANFCTR
COMMON /BALM/ TOTLQ,TOTLQI,TPIN,TPOUT
COMMON /XINV/ DXINV,DYINV,ARINV,PORINV
DIMENSION W(040), B(040), G(040)
C *****
KOUNT=0
PQIN=0.DO
PQOUT=0.DO
C DO NOT REPEAT SOLUTION FOR STEADY-STATE
IREPET=0
IF (S.EQ.0.0.AND.(N.GT.1.OR.(INT.GT.1.AND.ICLK.EQ.0))) THEN
IREPET=1
GO TO 120
END IF
C ---COMPUTE ROW AND COLUMN---
C ---CALL NEW ITERATION PARAMETER---
10 REMN=MOD(KOUNT,NITP)
IF (REMN.EQ.0) NTH=0
NTH=NTH+1
PARAM=AOPT(NTH)
C *****
C ---ROW COMPUTATIONS---
TEST=0.DO
RHO=S/TIM(N)
BRK=-RHO
DO 50 IY=1,NY
DO 20 M=1,NX
W(M)=0.DO
B(M)=0.DO
G(M)=0.DO
20 CONTINUE
DO 30 IX=1,NX
IF (THCK(IX,IY).EQ.0.0) GO TO 30
COEF=VPRM(IX,IY)
QL=-COEF*WT(IX,IY)
A=TMRX(IX-1,IY,1)*DXINV
C=TMRX(IX,IY,1)*DXINV
E=TMRX(IX,IY-1,2)*DYINV
F=TMRX(IX,IY,2)*DYINV
TBAR=A+C+E+F
C 10
C 20
C 30
C 40
C 50
C 60
C 70
C 80
C 82
SC 111
SC 121
SC 131
SC 135
C 141
C 146
C 160
SC 172
C 180
C 190
C 192
C 193
C 195
C 196
C 197A
C 197B
C 197C
C 197D
C 200
C 210
C 220
C 230
C 240
C 250
C 260
C 270
C 280
C 290
C 300
C 310
C 320
C 330
C 340
C 350
C 360
C 370
C 380
C 390
C 400
C 410
C 420
C 430
C 440
C 450

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      TMK=TBAR*PARAM
      BLH=-A-C-RHO-COEF-TMK
      BRH=E+F-TMK
      DR=BRH*HC(IX,IY)+BRK*HK(IX,IY)-E*HC(IX,IY-1)-F*HC(IX,IY+1)+QL+RECH
1(IX,IY)+REC(IX,IY)*ARINV
      W(IX)=BLH-A*B(IX-1)
      B(IX)=C/W(IX)
      G(IX)=(DR-A*G(IX-1))/W(IX)
30 CONTINUE
C
C      ---BACK SUBSTITUTION---
      DO 40 J=2,NX
      IJ=J-1
      IS=NX-IJ
40 HR(IS,IY)=G(IS)-B(IS)*HR(IS+1,IY)
50 CONTINUE
C
C      *****
C      ---COLUMN COMPUTATIONS---
      DO 90 IX=1,NX
      DO 60 M=1,NY
      W(M)=0.DO
      B(M)=0.DO
60 G(M)=0.DO
      DO 70 IY=1,NY
      IF (THCK(IX,IY).EQ.0.0) GO TO 70
      COEF=VPRM(IX,IY)
      QL=-COEF*WT(IX,IY)
      A=TMRX(IX,IY-1,2)*DYINV
      C=TMRX(IX,IY,2)*DYINV
      E=TMRX(IX-1,IY,1)*DXINV
      F=TMRX(IX,IY,1)*DXINV
      TBAR=A+C+E+F
      TMK=TBAR*PARAM
      BLH=-A-C-RHO-COEF-TMK
      BRH=E+F-TMK
      DC=BRH*HR(IX,IY)+BRK*HK(IX,IY)-E*HR(IX-1,IY)-F*HR(IX+1,IY)+QL+RECH
1(IX,IY)+REC(IX,IY)*ARINV
      W(IY)=BLH-A*B(IY-1)
      B(IY)=C/W(IY)
      G(IY)=(DC-A*G(IY-1))/W(IY)
70 CONTINUE
C
C      ---BACK SUBSTITUTION---
      DO 80 J=2,NY
      IJ=J-1
      IB=NY-IJ
      HC(IX,IB)=G(IB)-B(IB)*HC(IX,IB+1)
      IF (THCK(IX,IB).EQ.0.0) GO TO 80
      CHK=DABS(HC(IX,IB)-HR(IX,IB))
      IF (CHK.GT.TOL) TEST=1.DO
80 CONTINUE
90 CONTINUE
C
C      *****
      KOUNT=KOUNT+1
      IF (TEST.EQ.0.0) GO TO 120
      IF (KOUNT.GE.ITMAX) GO TO 100
      GO TO 10
C
C      *****
C      ---TERMINATE PROGRAM -- ITMAX EXCEEDED---
100 WRITE (6,160)
      DO 110 IX=1,NX
      DO 110 IY=1,NY
110 HK(IX,IY)=HC(IX,IY)
      CALL OUTPT
      STOP
C
C      *****
C      ---SET NEW HEAD (HK)---
120 DO 130 IY=1,NY
      DO 130 IX=1,NX
      IF (THCK(IX,IY).EQ.0.0) GO TO 130
      UPDATE THICKNESS*POROSITY FOR TRANSIENT FLOW
      IF (IREPET.EQ.0) THEN
      THCK(IX,IY)=THCK(IX,IY)+S*(HC(IX,IY)-HK(IX,IY))
      IF (THCK(IX,IY).LE.0.0) THEN
      WRITE (6,170) IX,IY
      THCK(IX,IY)=0.0
      END IF
      HR(IX,IY)=HK(IX,IY)

```

```

C 460
C 470
C 480
C 490
C 500
C 510
C 520
C 530
C 540
C 550
C 560
C 570
C 580
C 590
C 600
C 610
C 620
C 630
C 640
C 650
C 660
C 670
C 680
C 690
C 700
C 710
C 720
C 730
C 740
C 750
C 760
C 770
C 780
C 790
C 800
C 810
C 820
C 830
C 840
C 850
C 860
C 870
C 880
C 890
C 900
C 910
C 920
C 930
C 940
C 950
C 960
C 970
C 980
C 990
C1000
C1010
C1020
C1030
C1040
C1050
C1060
C1070
C1080
C1090
C1100
C1110
C1120
C1130
C1140
C1150
C1154
C1155
C1156
C1157A
C1157B
C1157C
C1157D
C1160

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DOUBLE PRECISION XDEL, YDEL, S, AREA, SUMT, RHO, PARAM, TEST, TOL, PINT,      A 100
1      HMIN, PYR, ANFCTR                                                    A 102
DOUBLE PRECISION TINIT, TIMX                                              A 104
DOUBLE PRECISION TINT                                                      A 111
DOUBLE PRECISION TMSUM, TDEL                                              A 114
DOUBLE PRECISION TOTLQ, TOTLQI, TPIN, TPOUT                              A 117
DOUBLE PRECISION DXINV, DYINV, ARINV, PORINV                              A 118
INTEGER PTID                                                                A 119
COMMON /PRMJ/ NTIM, NPMP, NPNT, NITP, N, NX, NY, NP, NREC, INT, NNX, NNY,   A 121
1      NUMOBS, NMOV, IMOV, NPMAX, ITMAX, NZCRIT, IPRNT, NPTPND,           A 131
2      NPNTMV, NPNTVL, NPNTD, NPNCHV, NPDEL, ICHK                        A 142
COMMON /PRMC/ NODEID(040,040), NPCELL(020,020), NPOLD(020,020),          SA 147
1      LIMBO(0500), IXOBS(05), IYOBS(05)                                A 148
COMMON /HEDA/ THCK(040,040), TMWL(05,50), TMOBS(50)                      SA 171
COMMON /HEDB/ TMRX(040,040,2), VPRM(040,040), HI(040,040),             SA 181
1      HR(040,040), HC(040,040), HK(040,040), WT(040,040),           SA 185
2 REC(040,040), RECH(040,040), TIM(100), AOPT(20), TITLE(10), XDEL, YDEL, SA 191
3      S, AREA, SUMT, RHO, PARAM, TEST, TOL, PINT, HMIN, PYR, ANFCTR    A 201
COMMON /HEDC/ MX, MY, MMX, MMY, NMX, NMY, MCHK                            SA 205
COMMON /HEDD/ TINIT, TIMX                                              A 207
COMMON /XINV/ DXINV, DYINV, ARINV, PORINV                                A 208
COMMON /BALM/ TOTLQ, TOTLQI, TPIN, TPOUT                                A 209
COMMON /CHMA/ PART(3,06400), CONC(020,020), TMCN(05,50), VX(040,040),   SA 212
1      VY(040,040), CONINT(020,020), CNRECH(020,020), POROS,         SA 215
2      SUMTCH, BETA, TIMV, STORM, STORMI, CMSIN, CMSOUT, FLMIN,       A 221
3      FLMOT, SUMIO, CELDIS, DLTRAT, CSTORM                            A 231
COMMON /CHMC/ SUMC(020,020), VXBDY(040,040), VYBDY(040,040)           SA 233
COMMON /CHMP/ PTID(06400)                                               A 237
COMMON /CHMR/ RF, DK, RHOB, THALF, DECAY, ADSORB, SORBI, DMASS1, CSTM2,   A 238A
1      EKF, XNF, XNFM1, FCTRF, EKL, CEC, EKLCEC, FCTRL, CINMAX,      A 238B
2      RF2MIN, RF2MAX, CZERO, IREACT, EK, EKCEC, FCTRE, CTOT, C3, C4, C5, C6 A 238C
COMMON /CHMR2/ CRETRD(020,020), CRDCOF(020,020), CELDCY(020,020)      A 238D
COMMON /DIFUS/ DISP(020,020,4)                                         A 239
C      COMMON /SAVEBF/ ANSC, ANSH, ANSV
C      CHARACTER*1 ANSC, ANSH, ANSV
C      DIMENSION HKS(40)
C
C      *****
C      ---LOAD DATA---
C      INT=0
C      TMSUM=0.00
C      CALL PARLOD
C      CALL GENPT
C      *****
C      ---START COMPUTATIONS---
C      ---COMPUTE ONE PUMPING PERIOD---
C      DO 150 INT=1, NPMP
C      IF (INT.GT.1) TMSUM=TMSUM+PYR
C      IF (INT.GT.1) CALL PARLOD
C      REMN=1.0
C      ---COMPUTE ONE TIME STEP---
C      DO 130 N=1, NTIM
C      IPRNT=0
C      ---LOAD NEW DELTA T---
C      TINT=SUMT-TMSUM
C      TDEL=DMIN1(TIM(N), PYR-TINT)
C      SUMT=SUMT+TDEL
C      TIM(N)=TDEL
C      IF (NPNT.GT.0) REMN=MOD(N, NPNT)
C      IF (SUMT.GE.(PYR+TMSUM)) IPRNT=1
C      *****
C      CALL ITERAT
C      IF (REMN.EQ.0.OR.N.EQ.NTIM.OR.IPRNT.EQ.1) CALL OUTPT
C      CALL VELO
101 CALL MOVE
C
C      SAVE CONCENTRATION FOR THIS TIME STEP?
C
C      IF(NPNCHV.NE.0.AND.N.EQ.NTIM) THEN
C
C      WRITE DATA FLAGS
C
C      IF(ANSC.EQ.'Y'.OR.ANSH.EQ.'Y'.OR.ANSV.EQ.'Y') THEN
C      XDELS=XDEL
C      YDELS=YDEL
C      WRITE(7) NX, NY, XDELS, YDELS
C      WRITE(7) ANSC, ANSH, ANSV
C      ENDIF

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```

C
C WRITE TIME INFORMATION
C
C IF(ANSC.EQ.'Y'.OR.ANSH.EQ.'Y'.OR.ANSV.EQ.'Y') THEN
C WRITE(7) N,INT,SUMT
C ENDIF
C
C WRITE CONCENTRATIONS IF DESIRED
C
C IF(ANSC.EQ.'Y') THEN
C DO 127 IY=1,NY
C 127 WRITE(7) (CONC(IX,IY),IX=1,NX)
C ENDIF
C
C WRITE HEADS IF REQUESTED
C
C IF(ANSH.EQ.'Y') THEN
C DO 103 IY=1,NY
C
C STORE HEADS IN SINGLE PRECISION
C
C DO 102 IIII=1,NX
C 102 HKS(IIII)=HK(IIII,IY)
C 103 WRITE(7) (HKS(IIII),IIII=1,NX)
C ENDIF
C
C WRITE VELOCITIES IF REQUESTED
C
C IF(ANSV.EQ.'Y') THEN
C DO 100 IY=1,NY
C 100 WRITE(7) (VX(IX,IY),IX=1,NX)
C DO 108 IY=1,NY
C 108 WRITE(7) (VY(IX,IY),IX=1,NX)
C ENDIF
C ENDIF
C ***** A 480
C IF (SUMT.GE.(PYR+TMSUM)) GO TO 140 A 621
C 130 CONTINUE A 630
C ***** A 640
C 140 CONTINUE A 660
C 150 CONTINUE A 690
C ***** A 700
C ENDFILE(6) A 702
C IF (NPNCHV.EQ.0) GO TO 155 A 703
C IF(ANSC.NE.'Y'.AND.ANSH.NE.'Y'.AND.ANSV.NE.'Y') GO TO 155
C ENDFILE(7) A 704
C 155 CONTINUE A 705
C CALL CLRPG(0,7,0)
C STOP A 710
C ***** A 720
C END A 730-

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$LARGE
C ***** A 10
C * A 20
C * SOLUTE TRANSPORT AND DISPERSION IN A POROUS MEDIUM * A 30
C * NUMERICAL SOLUTION --- METHOD OF CHARACTERISTICS * A 40
C * PROGRAMMED BY J. D. BREDEHOEFT AND L. F. KONIKOW * A 50
C * REVISED APRIL 1979, MARCH 1980 * A 55
C * REVISED DECEMBER 1980 * A 56
C * REVISED AUGUST 1981, JUNE 1982 * A 57
C * REVISED OCTOBER 1983 * A 58
C * REV. JUNE-AUG. 1984 BY W. SANFORD TO ALLOW 16 PTS. PER NODE * A 59
C * REV. MAY-AUG. 1985 BY L. KONIKOW AND M. PERSON TO INCLUDE: * A 59R
C * DECAY AND EQUILIBRIUM SORPTION-DESORPTION REACTIONS * A 60R
C * * SA 61
C * REV. JULY-DEC.1985 TO ALLOW SECONDARY SUBGRID FOR TRANSPORT * SA 62
C * REVISED JULY 1986 * A 63
C * REVISED MARCH 1987 BY D.J. GOODE * A 64
C * REVISED MAY 1987 BY D.J. GOODE * A 67
C * REVISED JANUARY 1988 * A 68A
C * REVISED NOVEMBER 1988 * A 68B
C * REV. MARCH 1989 BY D.J. GOODE FOR NONLINEAR EQUILIBRIUM * A 68C
C * SORPTION AND ION-EXCHANGE FOR MONO AND DIVALENT IONS * A 68D
C * * A 69R
C ***** A 70
C *****

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C WRITE DATA FLAGS
C
C IF(ANSC.EQ.'Y'.OR.ANSH.EQ.'Y'.OR.ANSV.EQ.'Y') THEN
C XDELS=XDEL
C YDELS=YDEL
C WRITE(7) NX,NY,XDELS,YDELS
C WRITE(7) ANSC,ANSH,ANSV
C ENDIF
C
C WRITE TIME INFORMATION
C
C IF(ANSC.EQ.'Y'.OR.ANSH.EQ.'Y'.OR.ANSV.EQ.'Y') THEN
C WRITE(7) N,INT,SUMT
C ENDIF
C
C WRITE CONCENTRATIONS IF DESIRED
C
C IF(ANSC.EQ.'Y') THEN
C DO 127 IY=1,NY
C 127 WRITE(7) (CONC(IX,IY),IX=1,NX)
C ENDIF
C
C WRITE HEADS IF REQUESTED
C
C IF(ANSH.EQ.'Y') THEN
C DO 103 IY=1,NY
C
C STORE HEADS IN SINGLE PRECISION
C
C DO 102 IIII=1,NX
C 102 HKS(IIII)=HK(IIII,IY)
C 103 WRITE(7) (HKS(IIII),IIII=1,NX)
C ENDIF
C
C WRITE VELOCITIES IF REQUESTED
C
C IF(ANSV.EQ.'Y') THEN
C DO 100 IY=1,NY
C 100 WRITE(7) (VX(IX,IY),IX=1,NX)
C DO 108 IY=1,NY
C 108 WRITE(7) (VY(IX,IY),IX=1,NX)
C ENDIF
C ENDIF
C *****
C IF (SUMT.GE.(PYR+TMSUM)) GO TO 140 A 480
C 130 CONTINUE A 621
C ***** A 630
C 140 CONTINUE A 640
C ***** A 660
C 150 CONTINUE A 690
C ***** A 700
C ENDFILE(6) A 702
C IF (NPNCHV.EQ.0) GO TO 155 A 703
C IF (ANSC.NE.'Y'.AND.ANSH.NE.'Y'.AND.ANSV.NE.'Y') GO TO 155
C ENDFILE(7)
C 155 CONTINUE A 704
C STOP A 705
C ***** A 710
C END A 720
C ***** A 730-

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\$LARGE

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SUBROUTINE MOVE F 10
DOUBLE PRECISION TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT,TITLE F 20
DOUBLE PRECISION XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT, F 30
1 HMIN,PYR,ANFCTR F 31A
DOUBLE PRECISION DXINV,DYINV,ARINV,PORINV F 32
DOUBLE PRECISION DCYFCT,DCYT,DCYT2 F 33
INTEGER PTID F 36
COMMON /PRMJ/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY, F 41
1 NUMOBS,NMOV,IMOV,NPMAK,ITMAX,WZCRIT,IPRNT,NPTPND, F 51
2 NPNTMV,NPNTVL,NPNTD,NPNCHV,NPDELC,ICLK F 62
COMMON /PRMC/ NODEID(040,040),NPCELL(020,020),NPOLD(020,020), SF 67
1 LIMBO(0500),IXOBS(05),IYOBS(05) F 68
COMMON /HEDA/ THCK(040,040),TMWL(05,50),TMOBS(50) SF 91
COMMON /HEDB/ TMRX(040,040,2),VPRM(040,040),HI(040,040), SF 101
1 HR(040,040),HC(040,040),HK(040,040),WT(040,040), SF 111
2 REC(040,040),RECH(040,040),TIM(100),AOPT(20),TITLE(10),XDEL,YDEL, SF 115

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3          S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR,ANFCTR      F 121
COMMON /HEDC/ MX,MY,MMX,MMY,NMX,NMY,MCHK                          SF 125
COMMON /XINV/ DXINV,DYINV,ARINV,PORINV                            F 130
COMMON /CHMA/ PART(3,06400),CONC(020,020),TMCN(05,50),VX(040,040), SF 142
1          VY(040,040),CONINT(020,020),CNRECH(020,020),POROS,     SF 151
2          SUMTCH,BETA,TIMV,STORM,STORMI,CMSIN,CMSOUT,FLMIN,       F 155
3          FLMOT,SUMIO,CELDIS,DLTRAT,CSTORM                       F 161
COMMON /CHMC/ SUMC(020,020),VXBDY(040,040),VYBDY(040,040)       SF 169
COMMON /CHMR/ RF,DK,RHOB,THALF,DECAY,ADSORB,SORBI,DMASS1,CSTM2,   F 173R
1          EKF,XNF,XNFM1,FCTRF,EKL,CEC,EKLCEC,FCTRL,CINMAX,       F 174A
2          RF2MIN,RF2MAX,CZERO,IREACT,EK,EKCEC,FCTRE,CTOT,C3,C4,C5,C6 F 174B
COMMON /CHMR2/ CRETRD(020,020),CRDCOF(020,020),CELDCY(020,020) F 175R
COMMON /CHMP/ PTID(06400)                                         F 177
C *****
WRITE (6,680) NMOV                                               F 190
IF (THALF.GT.0.0.AND.THALF.LT.TIMV) WRITE (6,685)                F 200
SUMTCH=SUMT-TIM(N)                                               F 205R
IONED=0                                                            F 210
IF(NX.EQ.3.OR.NY.EQ.3) IONED=1                                    F 211A
F1=0.30                                                            F 211B
F2=1.0/3.0                                                         F 212
IF (NPTPND.EQ.4) F1=0.25                                          F 214
IF (NPTPND.EQ.5.AND.IONED.EQ.1) F1=0.25                          F 216
IF (NPTPND.EQ.9) F1=F2                                           F 217
IF (NPTPND.EQ.8.AND.IONED.NE.1) F2=0.25                           F 218
IF (NPTPND.EQ.8.AND.IONED.EQ.1) F1=F2                             F 222A
IF (NPTPND.EQ.16) F1=0.25                                         F 222B
IF (NPTPND.EQ.16) F2=0.125                                        F 223
CONST1=TIMV*DXINV/RF                                              F 224
CONST2=TIMV*DYINV/RF                                              F 251R
DCYFCT=TIMV*DECAY                                                 F 261R
DCYT=1.DO                                                          F 265R
DCYT2=1.DO                                                         F 268A
IF(DECAY.NE.0.0) THEN                                             F 268B
  DCYT=DEXP(-DCYFCT)                                              F 268C
  DCYT2=DEXP(-DCYFCT*0.5DO)                                       F 268D
END IF                                                             F 268E
DO 8 IY=1,NMY                                                      F 268F
JY=IY+MY-1                                                         F 269A
DO 8 IX=1,NMX                                                      SF 269B
JX=IX+MX-1                                                         F 269C
CRETRD(IX,IY)=1.0                                                 SF 269D
CRDCOF(IX,IY)=1.0                                                 F 269E
CELDCY(IX,IY)=1.0                                                 F 269F
IF (IREACT.LE.1.OR.THCK(JX,JY).EQ.0.0) GO TO 8                   F 269G
CALL RETRD2(CONC(IX,IY),CRETRD(IX,IY),CRDCOF(IX,IY))             SF 269H
IF (DECAY.NE.0.0)                                                 F 269I
1  CELDCY(IX,IY)=EXP(-DCYFCT*CRDCOF(IX,IY)/CRETRD(IX,IY))       F 269J
8 CONTINUE                                                         F 269K
C ---MOVE PARTICLES 'NMOV' TIMES---                                F 270
DO 650 IMOV=1,NMOV                                                F 280
10 NPTM=NP                                                         F 290
C ---MOVE EACH PARTICLE---                                        F 300
DO 590 IN=1,NP                                                     F 310
IF (PART(1,IN).EQ.0.0) GO TO 590                                  F 320
KFLAG=0                                                            F 330
NLOC=0                                                             SF 335
C *****                                                        F 340
C ---COMPUTE OLD LOCATION---                                       F 350
20 XOLD=PART(1,IN)                                                F 400
IX=XOLD+0.5                                                        F 410
JX=IX-MX+1                                                         SF 415
IFLAG=1                                                            F 420
IF (PART(2,IN).GE.0.0) GO TO 30                                   F 430
IFLAG=-1                                                            F 440
PART(2,IN)=-PART(2,IN)                                           F 450
30 YOLD=PART(2,IN)                                                F 460
IY=YOLD+0.5                                                        F 470
JY=IY-MY+1                                                         SF 475
IF (THCK(IX,IY).EQ.0.0) GO TO 590                                 F 482
C *****                                                        F 490
C ---COMPUTE NEW LOCATION AND LOCATE CLOSEST NODE---             F 500
C ---LOCATE NORTHWEST CORNER---                                    F 510
IVX=XOLD                                                            F 520
IVY=YOLD                                                            F 530
IXE=IVX+1                                                          F 540
IYS=IVY+1                                                          F 550
C *****                                                        F 560

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C	---	LOCATE QUADRANT, VEL. AT 4 CORNERS, CHECK FOR BOUNDARIES---	F 570
		CELDX=XOLD-IX	F 580
		CELDY=YOLD-IY	F 590
		ICD=9	F 595
		IF (CELDX.EQ.0.0.AND.CELDY.EQ.0.0) GO TO 280	F 600
		IF (CELDX.GE.0.0.OR.CELDY.GE.0.0) GO TO 70	F 610
C		---PT. IN NW QUADRANT---	F 620
		VXNW=VXBDY(IVX, IVY)	F 630
		VXNE=VX(IXE, IVY)	F 640
		VXSW=VXBDY(IVX, IYS)	F 650
		VXSE=VX(IXE, IYS)	F 660
		VYNW=VYBDY(IVX, IVY)	F 670
		VYNE=VYBDY(IXE, IVY)	F 680
		VYSW=VY(IVX, IYS)	F 690
		VYSE=VY(IXE, IYS)	F 700
		ICD=1	F 705
		IF (THCK(IVX, IVY).EQ.0.0) GO TO 50	F 710
		IF (REC(IXE, IVY).EQ.0.0.AND.VPRM(IXE, IVY).LT.0.09) GO TO 40	F 720
		IF (THCK(IXE+1, IVY).NE.0.0) VXNE=VXNW	F 731
40		IF (REC(IVX, IYS).EQ.0.0.AND.VPRM(IVX, IYS).LT.0.09) GO TO 50	F 740
		IF (THCK(IVX, IYS+1).NE.0.0) VYSW=VYNW	F 751
50		IF (REC(IXE, IYS).EQ.0.0.AND.VPRM(IXE, IYS).LT.0.09) GO TO 270	F 760
		IF (THCK(IVX, IYS).EQ.0.0) GO TO 60	F 770
		IF (THCK(IXE+1, IYS).GT.0.0) VXSE=VXSW	F 782
60		IF (THCK(IXE, IVY).EQ.0.0) GO TO 270	F 790
		IF (THCK(IXE, IYS+1).GT.0.0) VYSE=VYNE	F 802
		GO TO 270	F 810
C			F 820
		70 IF (CELDX.LE.0.0.OR.CELDY.GE.0.0) GO TO 130	F 830
C		---PT. IN NE QUADRANT---	F 840
80		VXNW=VX(IVX, IVY)	F 850
		VXNE=VXBDY(IVX, IVY)	F 860
		VXSW=VX(IVX, IYS)	F 870
		VXSE=VXBDY(IVX, IYS)	F 880
		VYNW=VYBDY(IVX, IVY)	F 890
		VYNE=VYBDY(IXE, IVY)	F 900
		VYSW=VY(IVX, IYS)	F 910
		VYSE=VY(IXE, IYS)	F 920
		ICD=2	F 925
		IF (CELDX.EQ.0.0) GO TO 120	F 930
		IF (THCK(IXE, IVY).EQ.0.0) GO TO 100	F 940
		IF (REC(IVX, IVY).EQ.0.0.AND.VPRM(IVX, IVY).LT.0.09) GO TO 90	F 950
		IF (THCK(IVX-1, IVY).NE.0.0) VXNW=VXNE	F 961
90		IF (REC(IXE, IYS).EQ.0.0.AND.VPRM(IXE, IYS).LT.0.09) GO TO 100	F 970
		IF (THCK(IXE, IYS+1).NE.0.0) VYSE=VYNE	F 981
100		IF (REC(IVX, IYS).EQ.0.0.AND.VPRM(IVX, IYS).LT.0.09) GO TO 270	F 990
		IF (THCK(IXE, IYS).EQ.0.0) GO TO 110	F1000
		IF (THCK(IVX-1, IYS).GT.0.0) VXSW=VXSE	F1012
110		IF (THCK(IVX, IVY).EQ.0.0) GO TO 270	F1020
		IF (THCK(IVX, IYS+1).GT.0.0) VYSW=VYNW	F1032
		GO TO 270	F1040
120		IF (REC(IVX, IYS).EQ.0.0.AND.VPRM(IVX, IYS).LE.0.09) GO TO 270	F1050
		IF (THCK(IVX, IVY).EQ.0.0) GO TO 270	F1080
		IF (THCK(IVX, IYS+1).GT.0.0) VYSW=VYNW	F1072
		GO TO 270	F1080
C			F1090
		130 IF (CELDY.LE.0.0.OR.CELDX.GE.0.0) GO TO 190	F1100
C		---PT. IN SW QUADRANT---	F1110
140		VXNW=VXBDY(IVX, IVY)	F1120
		VXNE=VX(IXE, IVY)	F1130
		VXSW=VXBDY(IVX, IYS)	F1140
		VXSE=VX(IXE, IYS)	F1150
		VYNW=VY(IVX, IVY)	F1160
		VYNE=VY(IXE, IVY)	F1170
		VYSW=VYBDY(IVX, IVY)	F1180
		VYSE=VYBDY(IXE, IVY)	F1190
		ICD=3	F1195
		IF (CELDY.EQ.0.0) GO TO 180	F1200
		IF (THCK(IVX, IYS).EQ.0.0) GO TO 160	F1210
		IF (REC(IVX, IVY).EQ.0.0.AND.VPRM(IVX, IVY).LT.0.09) GO TO 150	F1220
		IF (THCK(IVX, IVY-1).NE.0.0) VYNW=VYSW	F1231
150		IF (REC(IXE, IYS).EQ.0.0.AND.VPRM(IXE, IYS).LT.0.09) GO TO 160	F1240
		IF (THCK(IXE+1, IYS).NE.0.0) VXSE=VXSW	F1251
160		IF (REC(IXE, IVY).EQ.0.0.AND.VPRM(IXE, IVY).LT.0.09) GO TO 270	F1260
		IF (THCK(IVX, IVY).EQ.0.0) GO TO 170	F1270
		IF (THCK(IXE+1, IVY).GT.0.0) VXNE=VXNW	F1282
170		IF (THCK(IXE, IYS).EQ.0.0) GO TO 270	F1290
		IF (THCK(IXE, IVY-1).GT.0.0) VYNE=VYSE	F1302

GO TO 270	F1310
180 IF (REC(IXE,IVY).EQ.0.0.AND.VPRM(IXE,IVY).LE.0.09) GO TO 270	F1320
IF (THCK(IVX,IVY).EQ.0.0) GO TO 270	F1330
IF (THCK(IXE+1,IVY).GT.0.0) VXNE=VXNW	F1342
GO TO 270	F1350
C	F1360
190 IF (CELDY.LE.0.0.OR.CELDX.LE.0.0) GO TO 260	F1370
---PT. IN SE QUADRANT---	F1380
C	F1390
200 VXNW=VX(IVX,IVY)	F1400
VXNE=VXBDY(IVX,IVY)	F1410
VXSW=VX(IVX,IYS)	F1420
VXSE=VXBDY(IVX,IYS)	F1430
VYNW=VY(IVX,IVY)	F1440
VYNE=VY(IXE,IVY)	F1450
VYSW=VYBDY(IVX,IVY)	F1460
VYSE=VYBDY(IXE,IVY)	F1465
ICD=4	F1470
IF (CELDY.EQ.0.0) GO TO 240	F1480
IF (CELDX.EQ.0.0) GO TO 250	F1490
IF (THCK(IXE,IYS).EQ.0.0) GO TO 220	F1500
IF (REC(IXE,IVY).EQ.0.0.AND.VPRM(IXE,IVY).LT.0.09) GO TO 210	F1511
IF (THCK(IXE,IVY-1).NE.0.0) VYNE=VYSE	F1520
210 IF (REC(IVX,IYS).EQ.0.0.AND.VPRM(IVX,IYS).LT.0.09) GO TO 220	F1531
IF (THCK(IVX-1,IYS).NE.0.0) VXSW=VXSE	F1540
220 IF (REC(IVX,IVY).EQ.0.0.AND.VPRM(IVX,IVY).LT.0.09) GO TO 270	F1550
IF (THCK(IXE,IVY).EQ.0.0) GO TO 230	F1562
IF (THCK(IVX-1,IVY).GT.0.0) VXNW=VXNE	F1570
230 IF (THCK(IVX,IYS).EQ.0.0) GO TO 270	F1582
IF (THCK(IVX,IVY-1).GT.0.0) VYNW=VYSW	F1590
GO TO 270	F1600
240 IF (REC(IVX,IVY).EQ.0.0.AND.VPRM(IVX,IVY).LE.0.09) GO TO 270	F1610
IF (THCK(IXE,IVY).EQ.0.0) GO TO 270	F1622
IF (THCK(IVX-1,IVY).GT.0.0) VXNW=VXNE	F1630
GO TO 270	F1640
250 IF (REC(IVX,IVY).EQ.0.0.AND.VPRM(IVX,IVY).LE.0.09) GO TO 270	F1650
IF (THCK(IVX,IYS).EQ.0.0) GO TO 270	F1662
IF (THCK(IVX,IVY-1).GT.0.0) VYNW=VYSW	F1670
GO TO 270	F1680
C	F1690
260 IF (CELDX.EQ.0.0.AND.CELDY.LT.0.0) GO TO 80	F1700
IF (CELDX.LT.0.0.AND.CELDY.EQ.0.0) GO TO 140	F1710
IF (CELDX.GT.0.0.AND.CELDY.EQ.0.0) GO TO 200	F1720
IF (CELDX.EQ.0.0.AND.CELDY.GT.0.0) GO TO 200	F1730
WRITE (6,690) IN,IX,IY	F1740
270 CONTINUE	F1741A
C	F1741B
--- CHECK FOR ADJACENT NO-FLOW BOUNDARIES---	F1741C
GO TO (1270,1275,1280,1285,1290) ICD	F1742A
GO TO 1290	F1742B
1270 IF (THCK(IXE,IVY).EQ.0.0) GO TO 1272	F1742C
IF (THCK(IVX,IYS).EQ.0.0) GO TO 1273	F1742D
IF (THCK(IVX,IVY).EQ.0.0) GO TO 1274	F1742E
GO TO 1290	F1742F
1272 VXNE=VXSE	F1742G
IF (THCK(IVX,IYS).GT.0.0) GO TO 1274	F1742H
1273 VYSW=VYSE	F1742I
1274 VXNW=VXSW	F1742J
VYNW=VYNE	F1744A
GO TO 1290	F1744B
1275 IF (THCK(IVX,IVY).EQ.0.0) GO TO 1277	F1744C
IF (THCK(IXE,IYS).EQ.0.0) GO TO 1278	F1744D
IF (THCK(IXE,IVY).EQ.0.0) GO TO 1279	F1744E
GO TO 1290	F1744F
1277 VXNW=VXSW	F1744G
IF (THCK(IXE,IYS).GT.0.0) GO TO 1279	F1744H
1278 VYSE=VYSW	F1744I
1279 VXNE=VXSE	F1744J
VYNE=VYNW	F1746A
GO TO 1290	F1746B
1280 IF (THCK(IXE,IYS).EQ.0.0) GO TO 1282	F1746C
IF (THCK(IVX,IVY).EQ.0.0) GO TO 1283	F1746D
IF (THCK(IVX,IYS).EQ.0.0) GO TO 1284	F1746E
GO TO 1290	F1746F
1282 VXSE=VXNE	F1746G
IF (THCK(IVX,IVY).GT.0.0) GO TO 1284	F1746H
1283 VYNW=VYNE	F1746I
1284 VXSW=VXNW	F1746J
VYSW=VYSE	
GO TO 1290	



1285	IF (THCK(IVX,IYS).EQ.0.0) GO TO 1287	F1748A
	IF (THCK(IXE,IVY).EQ.0.0) GO TO 1288	F1748B
	IF (THCK(IXE,IYS).EQ.0.0) GO TO 1289	F1748C
	GO TO 1290	F1748D
1287	VXSW=VXNW	F1748E
	IF (THCK(IXE,IVY).GT.0.0) GO TO 1289	F1748F
1288	VYNE=VYNW	F1748G
1289	VYSE=VYSW	F1748H
	VXSE=VXNE	F1748I
1290	CONTINUE	F1749A
C	*****	F1750
C	---BILINEAR INTERPOLATION---	F1760
	CELXD=XOLD-IVX	F1770
	CELDXH=AMOD(CELXD,0.5)	F1780
	CELDX=CELDXH*2.0	F1790
	CELDY=YOLD-IVY	F1800
C	*****	F1810
C	---X VELOCITY---	F1820
	VXN=VXNW*(1.0-CELDX)+VXNE*CELDX	F1830
	VXS=VXSW*(1.0-CELDX)+VXSE*CELDX	F1850
	XVEL=(VXN*(1.0-CELDY)+VXS*CELDY)/THCK(IX,IY)	F1871
C	---Y VELOCITY---	F1900
	CELDYH=AMOD(CELDY,0.5)	F1910
	CELYD=CELDYH*2.0	F1921
	VYW=VYNW*(1.0-CELYD)+VYSW*CELYD	F1931
	VYE=VYNE*(1.0-CELYD)+VYSE*CELYD	F1951
	YVEL=(VYW*(1.0-CELDX)+VYE*CELDX)/THCK(IX,IY)	F1971
C	GO TO 290	F2000
280	XVEL=VX(IX,IY)/THCK(IX,IY)	F2010
	YVEL=VY(IX,IY)/THCK(IX,IY)	F2021
290	DISTX=XVEL*CONST1	F2031
	DISTY=YVEL*CONST2	F2040
	IF (IREACT.GE.2) THEN	F2050
	RF2INV=1.0/CRETRD(JX,JY)	F2052R
	DISTX=DISTX*RF2INV	SF2053R
	DISTY=DISTY*RF2INV	F2054R
	ENDIF	F2055R
C	*****	F2056R
C	---BOUNDARY CONDITIONS---	F2060
	TEMPX=XOLD+DISTX	F2070
	TEMPY=YOLD+DISTY	F2080
	INX=TEMPX+0.5	F2090
	INY=TEMPY+0.5	F2100
	IF (THCK(INX,INY).GT.0.0) GO TO 330	F2110
C	*****	F2120
C	---X BOUNDARY---	F2130
	IF (THCK(INX,IY).EQ.0.0) GO TO 300	F2140
	PART(1,IN)=TEMPX	F2150
	GO TO 310	F2160
300	BEYON=TEMPX-IX	F2170
	IF (BEYON.LT.0.0) BEYON=BEYON+0.5	F2180
	IF (BEYON.GT.0.0) BEYON=BEYON-0.5	F2190
	PART(1,IN)=TEMPX-2.0*BEYON	F2200
	INX=PART(1,IN)+0.5	F2210
	TEMPX=PART(1,IN)	F2220
C	*****	F2230
C	---Y BOUNDARY---	F2240
310	IF (THCK(INX,INY).EQ.0.0) GO TO 320	F2250
	PART(2,IN)=TEMPY	F2260
	GO TO 340	F2270
C	*****	F2280
C	320 BEYON=TEMPY-IY	F2290
	IF (BEYON.LT.0.0) BEYON=BEYON+0.5	F2300
	IF (BEYON.GT.0.0) BEYON=BEYON-0.5	F2310
	PART(2,IN)=TEMPY-2.0*BEYON	F2320
	INY=PART(2,IN)+0.5	F2330
	TEMPY=PART(2,IN)	F2340
	GO TO 340	F2350
330	PART(1,IN)=TEMPX	F2360
	PART(2,IN)=TEMPY	F2370
340	CONTINUE	F2380
	JNX=INX-MX+1	F2390
	JNY=INY-MY+1	SF2395
	IF (MCHK.EQ.0) GO TO 342	SF2396
	IF (JNX.LT.1.OR.JNX.GT.NMX.OR.JNY.LT.1.OR.JNY.GT.NMY) NLOC=1	SF2397
C	*****	SF2398
	IF (NLOC.GT.0) GO TO 345	F2400
		SF2405

342	CONTINUE	SF2407
C	---SUM CONCENTRATIONS AND COUNT PARTICLES---	F2410
C	---DECAY PARTICLES---	F2414R
	IF (DECAY.NE.0.0) THEN	F2415A
	IF (IREACT.LE.1) THEN	F2415B
	PART(3,IN)=PART(3,IN)*DCYT	F2416R
	ELSE	F2417R
	PART(3,IN)=PART(3,IN)*CELDY(JX,JY)	SF2418A
	END IF	F2418B
	END IF	F2419R
	SUMC(JNX,JNY)=SUMC(JNX,JNY)+PART(3,IN)	SF2421
	NPCELL(JNX,JNY)=NPCELL(JNX,JNY)+1	SF2431
C	*****	F2440
345	CONTINUE	SF2445
C	---CHECK FOR CHANGE IN CELL LOCATION---	F2450
	IF (IX.EQ.INX.AND.IY.EQ.INY) GO TO 580	F2460
C	---CHECK FOR CONST.-HEAD BDY. OR SOURCE AT OLD LOCATION---	F2470
	IBD=0	SF2478
C	IF (REC(IX,IY).LT.-0.1) GO TO 350	FXXX
C	IF (REC(IX,IY).GT.0.1) GO TO 360	FXXX
	IF (REC(IX,IY).LT.0.0) GO TO 350	F2480
	IF (REC(IX,IY).GT.0.0) GO TO 360	F2490
	IF (VPRM(IX,IY).LT.0.09) GO TO 348	SF2501
	IF (WT(IX,IY).GT.HK(IX,IY)) GO TO 350	F2510
	IF (WT(IX,IY).LT.HK(IX,IY)) GO TO 360	F2520
348	IF (MCHK.EQ.0) GO TO 540	SF2522
	IF (JX.EQ.1.AND.VXBDY(IX-1,IY).GT.0.0.AND.JNX.GT.JX) IBD=1	SF2523
	IF (JX.EQ.NMX.AND.VXBDY(IX,IY).LT.0.0.AND.JNX.LT.JX) IBD=1	SF2524
	IF (JY.EQ.1.AND.VYBDY(IX,IY-1).GT.0.0.AND.JNY.GT.JY) IBD=1	SF2525
	IF (JY.EQ.NMY.AND.VYBDY(IX,IY).LT.0.0.AND.JNY.LT.JY) IBD=1	SF2526
	IF (IBD.EQ.1) GO TO 350	SF2527
	GO TO 540	F2530
C	*****	F2540
C	---CREATE NEW PARTICLES AT BOUNDARIES---	F2550
350	IF (IFLAG.GT.0) GO TO 550	F2560
	KFLAG=1	F2570
360	CONTINUE	F2581
C	*****	F2630
C	---GENERATE NEW TEMPORARY PARTICLE---	F2641
	IF (NPTM.EQ.NPMAX) GO TO 600	F2650
	NPTM=NPTM+1	F2660
	IP=NPTM	F2670
C		F2700
390	IF (KFLAG.EQ.0) GO TO 398	F2705
	IF (IBD.EQ.1) GO TO 525	SF2708
	ITEM=PTID(IN)	F2845
	GO TO 399	F2855
398	IF (IREACT.LE.1) THEN	F2864R
	SUMC(JX,JY)=SUMC(JX,JY)+CONC(JX,JY)*DCYT2	SF2865R
	ELSE	F2866R
	SUMC(JX,JY)=SUMC(JX,JY)+CONC(JX,JY)*SQRT(CELDY(JX,JY))	SF2867R
	END IF	F2869R
	NPCELL(JX,JY)=NPCELL(JX,JY)+1	SF2876
	IF (NPOLD(JX,JY).GT.0) NPOLD(JX,JY)=NPOLD(JX,JY)-1	SF2886
	IF (IFLAG.GT.0) GO TO 441	F2895
	IF (KFLAG.EQ.0) GO TO 441	F2899
399	IF (NPTPD.EQ.16) GO TO 400	F2901
	GO TO (401,411,421,431,441,451,461,471,481),ITEM	F2906
	GO TO 441	F2915
400	GO TO (482,483,484,485,486,487,488,489,490,491,492,493,494,495,	F2921
	1 496,497),ITEM	F2922
	GO TO 441	F2924
401	PART(1,IP)=IX-F1	F2925
	PART(2,IP)=IY-F1	F2935
	PTID(IP)=1	F2945
	GO TO 530	F2955
411	PART(1,IP)=IX-F1	F2965
	PART(2,IP)=IY+F1	F2975
	PTID(IP)=2	F2985
	GO TO 530	F2995
421	PART(1,IP)=IX+F1	F3005
	PART(2,IP)=IY-F1	F3015
	PTID(IP)=3	F3025
	GO TO 530	F3035
431	PART(1,IP)=IX+F1	F3045
	PART(2,IP)=IY+F1	F3055
	PTID(IP)=4	F3065
	GO TO 530	F3075

441	PART(1,IP)=IX	F3085
	PART(2,IP)=IY	F3095
	PTID(IP)=5	F3105
	GO TO 530	F3115
451	PART(1,IP)=IX-F2	F3125
	PART(2,IP)=IY	F3135
	PTID(IP)=6	F3145
	GO TO 530	F3155
461	PART(1,IP)=IX	F3165
	PART(2,IP)=IY-F2	F3175
	PTID(IP)=7	F3185
	GO TO 530	F3195
471	PART(1,IP)=IX+F2	F3205
	PART(2,IP)=IY	F3215
	PTID(IP)=8	F3225
	GO TO 530	F3235
481	PART(1,IP)=IX	F3245
	PART(2,IP)=IY+F2	F3255
	PTID(IP)=9	F3265
	GO TO 530	F3266
482	PART(1,IP)=IX-F1-F2	F3267
	PART(2,IP)=IY-F1-F2	F3268
	PTID(IP)=1	F3269
	GO TO 530	F3271
483	PART(1,IP)=IX-F1-F2	F3272
	PART(2,IP)=IY-F1+F2	F3273
	PTID(IP)=2	F3274
	GO TO 530	F3275
484	PART(1,IP)=IX-F1+F2	F3276
	PART(2,IP)=IY-F1-F2	F3277
	PTID(IP)=3	F3278
	GO TO 530	F3279
485	PART(1,IP)=IX-F1+F2	F3281
	PART(2,IP)=IY-F1+F2	F3282
	PTID(IP)=4	F3283
	GO TO 530	F3284
486	PART(1,IP)=IX-F1-F2	F3285
	PART(2,IP)=IY+F1-F2	F3286
	PTID(IP)=5	F3287
	GO TO 530	F3288
487	PART(1,IP)=IX-F1-F2	F3289
	PART(2,IP)=IY+F1+F2	F3291
	PTID(IP)=6	F3292
	GO TO 530	F3293
488	PART(1,IP)=IX-F1+F2	F3294
	PART(2,IP)=IY+F1-F2	F3295
	PTID(IP)=7	F3296
	GO TO 530	F3297
489	PART(1,IP)=IX-F1+F2	F3298
	PART(2,IP)=IY+F1+F2	F3299
	PTID(IP)=8	F3301
	GO TO 530	F3302
490	PART(1,IP)=IX+F1-F2	F3303
	PART(2,IP)=IY-F1-F2	F3304
	PTID(IP)=9	F3305
	GO TO 530	F3306
491	PART(1,IP)=IX+F1-F2	F3307
	PART(2,IP)=IY-F1+F2	F3308
	PTID(IP)=10	F3309
	GO TO 530	F3311
492	PART(1,IP)=IX+F1+F2	F3312
	PART(2,IP)=IY-F1-F2	F3313
	PTID(IP)=11	F3314
	GO TO 530	F3315
493	PART(1,IP)=IX+F1+F2	F3316
	PART(2,IP)=IY-F1+F2	F3317
	PTID(IP)=12	F3318
	GO TO 530	F3319
494	PART(1,IP)=IX+F1-F2	F3321
	PART(2,IP)=IY+F1-F2	F3322
	PTID(IP)=13	F3323
	GO TO 530	F3324
495	PART(1,IP)=IX+F1-F2	F3325
	PART(2,IP)=IY+F1+F2	F3326
	PTID(IP)=14	F3327
	GO TO 530	F3328
496	PART(1,IP)=IX+F1+F2	F3329
	PART(2,IP)=IY+F1-F2	F3331

	PTID(IP)=15	F3332
	GO TO 530	F3333
497	PART(1,IP)=IX+F1+F2	F3334
	PART(2,IP)=IY+F1+F2	F3335
	PTID(IP)=16	F3336
	GO TO 530	F3337
525	DLX=INX-IX	SF3425
	PART(1,IP)=TEMPX-DLX	SF3435
	DLY=INY-IY	SF3455
	PART(2,IP)=TEMPY-DLY	SF3465
	PART(2,IP)=-PART(2,IP)	SF3475
	IF (IREACT.LE.1) THEN	F3478A
	PART(3,IP)=CONC(JX,JY)*DCYT	SF3478B
	ELSE	F3478C
	PART(3,IP)=CONC(JX,JY)*CELDCY(JX,JY)	SF3478D
	END IF	F3478E
	SUMC(JX,JY)=SUMC(JX,JY)+PART(3,IP)	SF3479
	NPCELL(JX,JY)=NPCELL(JX,JY)+1	SF3481
	GO TO 540	SF3483
C		F3510
530	PART(2,IP)=-PART(2,IP)	F3520
	PART(3,IP)=CONC(JX,JY)	SF3531
C	*****	F3550
C	---CHECK FOR DISCHARGE BOUNDARY AT NEW LOCATION---	F3560
540	IFLAG=1	F3571
550	IF (NLOC.GT.0) GO TO 565	SF3575
	IF (VPRM(INX,INY).GT.0.09.AND.WT(INX,INY).LT.HK(INX,INY)) GO TO 56	SF3581
	10	F3590
C	IF (REC(INX,INY).GT.0.1) GO TO 560	FXXX
	IF (REC(INX,INY).GT.0.0) GO TO 560	F3600
	GO TO 590	F3610
C	*****	F3620
C	---PUT PT. IN LIMBO IF PT. DENSITY NOT INCREASED---	F3625
560	IF (NPOLD(JNX,JNY).LE.0) GO TO 590	SF3636
565	CONTINUE	SF3638
	PART(1,IN)=0.0	F3645
	PART(2,IN)=0.0	F3650
	PART(3,IN)=0.0	F3660
	IF (NLOC.GT.0) GO TO 567	SF3661
	SUMC(JNX,JNY)=SUMC(JNX,JNY)-CONC(JNX,JNY)	SF3663
	NPCELL(JNX,JNY)=NPCELL(JNX,JNY)-1	SF3665
	NPOLD(JNX,JNY)=NPOLD(JNX,JNY)-1	SF3667
567	CONTINUE	SF3668
	DO 570 ID=1,500	F3670
	IF (LIMBO(ID).GT.0) GO TO 570	F3680
	LIMBO(ID)=IN	F3690
	GO TO 590	F3700
570	CONTINUE	F3710
C		F3720
580	IF (IFLAG.LT.0) PART(2,IN)=-TEMPY	F3730
590	CONTINUE	F3750
C	---END OF LOOP---	F3760
C	*****	F3762
C		F3763
C	---INSERT TEMPORARY PARTICLES INTO LIMBO LOCATIONS---	F3764
	IF(NPTM.EQ.NP) GO TO 620	F3765
	IN=NPTM	F3766
	DO 595 IL=1,500	F3767
	IP=LIMBO(IL)	F3768
	IF(IP.EQ.0) GO TO 595	F3769
	PART(1,IP)=PART(1,IN)	F3771
	PART(1,IN)=0.0	F3772
	PART(2,IP)=PART(2,IN)	F3773
	PART(2,IN)=0.0	F3774
	PART(3,IP)=PART(3,IN)	F3775
	PART(3,IN)=0.0	F3776
	PTID(IP)=PTID(IN)	F3777
	PTID(IN)=0	F3778
	LIMBO(IL)=0	F3779
	IN=IN-1	F3781
	IF(IN.LE.NP) GO TO 596	F3782
595	CONTINUE	F3783
596	NPTM=IN	F3784
	GO TO 620	F3785
C	---RESTART MOVE IF PT. LIMIT EXCEEDED---	F3790
600	WRITE (6,700) IMOV,IN	F3800
	TEST=100.DO	F3810
	CALL GENPT	F3820

```

DO 610 IX=1,NMX
DO 610 IY=1,NMY
SUMC(IX,IY)=0.0
610 NPCELL(IX,IY)=0
TEST=0.DO
GO TO 10
C *****
620 SUMTCH=SUMTCH+TIMV
C ---ADJUST NUMBER OF PARTICLES---
NP=NPTM
WRITE (6,670) NP,IMOV
C *****
C CALL CNCON
C *****
C ---STORE OBS. WELL DATA---
IF (NUMOBS.LE.0) GO TO 650
IF (S.GT.0.0) THEN
  IF (IMOV.NE.NMOV) GO TO 650
  J=MOD(N,50)
ELSE
  J=MOD(IMOV,50)
END IF
IF (J.EQ.0) J=50
TMOBS(J)=SUMTCH
DO 630 I=1,NUMOBS
  TMWL(I,J)=HK(IXOBS(I),IYOBS(I))
  IX=IXOBS(I)-MX+1
  IF (IXOBS(I).LT.MX.OR.IXOBS(I).GT.MMX) GO TO 630
  IY=IYOBS(I)-MY+1
  IF (IYOBS(I).LT.MY.OR.IYOBS(I).GT.MMY) GO TO 630
  TMCN(I,J)=CONC(IX,IY)
630 CONTINUE
C ---PRINT CHEMICAL OUTPUT---
650 CALL CHMOT
C *****
660 RETURN
C *****
C
C
C
670 FORMAT (1H0,2X,2HNP,7X,2H= ,8X,I4,10X,11HIMOV = ,8X,I4)
680 FORMAT (1H0,10X,61HNO. OF PARTICLE MOVES REQUIRED TO COMPLETE THIS
1 TIME STEP = ,I4//)
685 FORMAT (1H0,5X,51H*** CAUTION *** DECAY HALF-LIFE IS LESS THAN TI
1MV;/23X,24HACCURACY MAY BE AFFECTED/23X,34H(REDUCE TIMV BY DECREAS
2ING CELDIS))
690 FORMAT (1H0,5X,53H*** WARNING *** QUADRANT NOT LOCATED FOR PT.
1 NO. ,I5,11H , IN CELL ,2I4)
700 FORMAT (1H0,5X,17H *** NOTE *** ,10X,23HNPTM.EQ.NPMAx --- IMOV=
1,I4,5X,8HPT. NO.= ,I4,5X,10HCALL GENPT/)
END
SF3831
SF3841
F3850
F3860
F3870
F3880
F3890
F3900
F3910
F3920
F3930
F3940
F3950
F3960
F3971
F3983
F3985
F3987
F3993
F3997
F4000
F4005
F4010
F4020
F4030
F4040
SF4042
SF4043
SF4044
SF4045
SF4051
SF4053
F4060
F4084
F4090
F4100
F4110
F4120
F4130
F4140
F4150
F4160
F4170
F4174R
F4175R
F4176R
F4180
F4190
F4200
F4210
F4220-

$LARGE
SUBROUTINE OUTPT
DOUBLE PRECISION TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT,TITLE
DOUBLE PRECISION XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,
1 HMIN,PYR,ANFCTR
DOUBLE PRECISION TOTLQ,TOTLQI,TPIN,TPOUT,PQIN,PQOUT,DELQ,QOUT,QIN,
1 QNET,DDRW
DOUBLE PRECISION QSTR,TPUM,PUMP,TOTLQN,SRCS,SINKS,ERRMB,DENOM,
1 PCTERR
COMMON /PRMJ/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,NUMO
1BS,NMOV,IMOV,NPMAx,ITMAX,NZCRIT,IPRNT,NPTPND,NPNTMV,NPNTVL,NPNTD,N
2PNCHV,NPDELC,ICLK
COMMON /HEDA/ THCK(040,040),TMWL(05,50),TMOBS(50)
COMMON /HEDB/ TMRX(040,040,2),VPRM(040,040),HI(040,040),
1 HR(040,040),HC(040,040),HK(040,040),WT(040,040),
2 REC(040,040),RECH(040,040),TIM(100),AOPT(20),TITLE(10),XDEL,YDEL,
3 S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR,ANFCTR
COMMON /BALM/ TOTLQ,TOTLQI,TPIN,TPOUT
DIMENSION IH(040)
C *****
TIMD=SUMT/86400.
TIMY=SUMT/(86400.0*365.25)
C ---PRINT HEAD VALUES---
WRITE (6,120)
WRITE (6,130) N
H 10
H 20
H 30
H 31A
H 32
H 32A
H 33
H 34
H 40
H 50
H 81
SH 91
SH 101
SH 111
SH 115
H 121-
H 126
SH 142
H 150
H 160
H 170
H 180
H 190
H 200

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	WRITE (6,140) SUMT	H 210
	WRITE (6,150) TIMD	H 220
	WRITE (6,160) TIMY	H 230
	WRITE (6,170)	H 240
	DO 10 IY=1,NY	H 250
10	WRITE (6,180) (HK(IX,IY),IX=1,NX)	H 260
	IF (N.EQ.0) GO TO 110	H 270
C	*****	H 280
C	---PRINT HEAD MAP---	H 290
	WRITE (6,120)	H 300
	WRITE (6,130) N	H 310
	WRITE (6,140) SUMT	H 320
	WRITE (6,150) TIMD	H 330
	WRITE (6,160) TIMY	H 340
	WRITE (6,170)	H 350
	DO 30 IY=1,NY	H 360
	DO 20 IX=1,NX	H 370
20	IH(IX)=NINT(HK(IX,IY))	H 381
30	WRITE (6,190) (IH(ID),ID=1,NX)	H 390
C	*****	H 400
C	---COMPUTE WATER BALANCE AND DRAWDOWN---	H 410
	QSTR=0.DO	H 420
	PUMP=0.DO	H 430
	PQIN=0.DO	H 432
	PQOUT=0.DO	H 434
	TPUM=0.DO	H 440
	QIN=0.DO	H 450
	QOUT=0.DO	H 460
	QNET=0.DO	H 470
	DELQ=0.DO	H 480
	PCTERR=0.DO	H 500
	WRITE (6,290)	H 510
C		H 520
	DO 80 IY=1,NY	H 530
	DO 70 IX=1,NX	H 540
	IH(IX)=0	H 551
	IF (THCK(IX,IY).EQ.0.0) GO TO 70	H 560
	IF (REC(IX,IY).GT.0.0) GO TO 32	H 562
	PQIN=PQIN+REC(IX,IY)	H 564
	GO TO 34	H 566
32	PQOUT=PQOUT+REC(IX,IY)	H 568
34	IF (RECH(IX,IY).GT.0.0) GO TO 36	H 572
	PQIN=PQIN+RECH(IX,IY)*AREA	H 574
	GO TO 38	H 576
36	PQOUT=PQOUT+RECH(IX,IY)*AREA	H 578
38	IF (VPRM(IX,IY).EQ.0.0) GO TO 60	H 582
	DELQ=VPRM(IX,IY)*AREA*(WT(IX,IY)-HK(IX,IY))	H 590
	IF (DELQ.GT.0.0) GO TO 40	H 600
	QOUT=QOUT+DELQ	H 610
	GO TO 50	H 620
40	QIN=QIN+DELQ	H 630
50	QNET=QNET+DELQ	H 640
60	DDRW=HI(IX,IY)-HK(IX,IY)	H 650
	IH(IX)=NINT(DDRW)	H 661
	QSTR=QSTR+DDRW*AREA*S	H 670
70	CONTINUE	H 680
C	---PRINT DRAWDOWN MAP---	H 690
	WRITE (6,300) (IH(IX),IX=1,NX)	H 700
80	CONTINUE	H 710
	TPUM=PQIN+PQOUT	H 716
	PUMP=TPIN+TPOUT	H 721
	TOTLQN=TOTLQ+TOTLQI	H 745
	SRC=QSTR-TPIN+TOTLQI	H 755
	SINKS=TPOUT-TOTLQ	H 765
	ERRMB=SRC-SINKS	H 775
	DENOM=(SRC+SINKS)*0.5DO	H 785
	IF (DENOM.EQ.0.0) GO TO 100	H 795
	PCTERR=ERRMB*100.DO/DENOM	H 805
C	---PRINT MASS BALANCE DATA FOR FLOW MODEL---	H 830
100	WRITE (6,240)	H 840
	WRITE (6,211) TPIN	H 842
	WRITE (6,212) TPOUT	H 844
	WRITE (6,250) PUMP	H 850
	WRITE (6,230) QSTR	H 860
	WRITE (6,202) TOTLQI	H 862
	WRITE (6,203) TOTLQ	H 864
	WRITE (6,260) TOTLQN	H 866
	WRITE (6,270) ERRMB	H 880

	WRITE (6,280) PCTERR	H 883
	WRITE (6,201)	H 886
	WRITE (6,202) QIN	H 889
	WRITE (6,203) QOUT	H 892
	WRITE (6,204) QNET	H 895
	WRITE (6,211) PQIN	H 898
	WRITE (6,212) PQOUT	H 901
	WRITE (6,210) TPUM	H 910
C	*****	H 940
110	RETURN	H 950
C	*****	H 960
C		H 970
C		H 980
C		H 990
	120 FORMAT (1H1,23HHEAD DISTRIBUTION - ROW)	H1000
	130 FORMAT (1X,23HNUMBER OF TIME STEPS = ,1I5)	H1010
	140 FORMAT (8X,16HTIME(SECONDS) = ,1G12.5)	H1020
	150 FORMAT (8X,16HTIME(DAYS) = ,1E12.5)	H1030
	160 FORMAT (8X,16HTIME(YEARS) = ,1E12.5)	H1040
	170 FORMAT (1H )	H1050
	180 FORMAT (1H0,10F12.7)	H1055
	190 FORMAT (1H0,30I4)	SH1071
	201 FORMAT (1H0,2X,33HRATE MASS BALANCE -- (IN C.F.S.) //)	H1073
	202 FORMAT (4X,29HLEAKAGE INTO AQUIFER = ,E12.5)	H1076
	203 FORMAT (4X,29HLEAKAGE OUT OF AQUIFER = ,E12.5)	H1083
	204 FORMAT (4X,29HNET LEAKAGE (QNET) = ,E12.5)	H1086
	210 FORMAT (4X,29HNET WITHDRAWAL (TPUM) = ,E12.5)	H1093
	211 FORMAT (4X,29HRECHARGE AND INJECTION = ,E12.5)	H1096
	212 FORMAT (4X,29HPUMPAGE AND E-T WITHDRAWAL = ,E12.5)	H1103
	230 FORMAT (4X,29HWATER RELEASE FROM STORAGE = ,1E12.5)	H1120
	240 FORMAT (1H0,2X,38HCUMULATIVE MASS BALANCE -- (IN FT**3) //)	H1125
	250 FORMAT (4X,29HCUMULATIVE NET PUMPAGE = ,1E12.5)	H1140
	260 FORMAT (4X,29HCUMULATIVE NET LEAKAGE = ,1E12.5)	H1150
	270 FORMAT (1H0,7X,25HMASS BALANCE RESIDUAL = ,G12.5)	H1160
	280 FORMAT (1H ,7X,25HERROR (AS PERCENT) = ,G12.5//)	H1170
	290 FORMAT (1H1,8HDRAWDOWN)	H1180
	300 FORMAT (3H ,25I5)	SH1191
	END	H1200-

\$LARGE

	SUBROUTINE PARLOD	B 10
	DOUBLE PRECISION DMIN1,DEXP,DLOG,DABS	B 20
	DOUBLE PRECISION TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT,TITLE	B 30
	DOUBLE PRECISION XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,	B 40
1	HMIN,PYR,ANFCTR	B 42
	DOUBLE PRECISION FCTR,TIMX,TINIT,PIES,YNS,XNS,RAT,HMX,HMY	B 50
	DOUBLE PRECISION ANTIM	B 54
	DOUBLE PRECISION DXINV,DYINV,ARINV,PORINV	B 57
	DOUBLE PRECISION ALPHA1,ANITP	B 61
	DOUBLE PRECISION TOTLQ,TOTLQI,TPIN,TPOUT	B 62
	INTEGER OVERRD	B 65
	CHARACTER*26 REACTN(9)	B 67R
	COMMON /PRMJ/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,	B 71
1	NUMOBS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,	B 81
2	NPNTMV,NPNTVL,NPNTD,NPNCHV,NPDEL,ICLK	B 92
	COMMON /PRMC/ NODEID(040,040),NPCELL(020,020),NPOLD(020,020),	SB 97
1	LIMBO(0500),IXOBS(05),IYOBS(05)	B 98
	COMMON /HEDA/ THCK(040,040),TMWL(05,50),TMOBS(50)	SB 121
	COMMON /HEDB/ TMRX(040,040,2),VPRM(040,040),HI(040,040),	SB 131
1	HR(040,040),HC(040,040),HK(040,040),WT(040,040),	SB 141
2	REC(040,040),RECH(040,040),TIM(100),AOPT(20),TITLE(10),XDEL,YDEL,	SB 145
3	S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR,ANFCTR	B 151
	COMMON /HEDC/ MX,MY,MMX,MMY,NMX,NMY,MCHK	SB 155
	COMMON /HEDD/ TINIT,TIMX	B 157
	COMMON /CHMA/ PART(3,06400),CONC(020,020),TMCN(05,50),VX(040,040),	SB 162
1	VY(040,040),CONINT(020,020),CNRECH(020,020),POROS,	SB 171
2	SUMTCH,BETA,TIMV,STORM,STORMI,CMSIN,CMSOUT,FLMIN,	B 175
3	FLMOT,SUMIO,CELDIS,DLTRAT,CSTORM	B 181
	COMMON /CHMR/ RF,DK,RHOB,THALF,DECAY,ADSORB,SORBI,DMASS1,CSTM2,	B 181R
1	EKF,XNF,XNFM1,FCTRF,EKL,CEC,EKLCEC,FCTRL,CINMAX,	B 183R
2	RFZMIN,RFZMAX,CZERO,IReact,EK,EKCEC,FCTRE,CTOT,C3,C4,C5,C6	B 184R
	COMMON /BALM/ TOTLQ,TOTLQI,TPIN,TPOUT	B 186
	COMMON /XINV/ DXINV,DYINV,ARINV,PORINV	B 200
	COMMON /CHMC/ SUMC(020,020),VXBDY(040,040),VYBDY(040,040)	SB 212
	DATA REACTN/	'NONE
1	'LINEAR SORPTION	','FREUNDLICH SORPTION
2	'LANGMUIR SORPTION	','MONOVALENT ION EXCHANGE

	3 'Divalent ION EXCHANGE', 'MONO-Divalent ION EXCHANGE',	B 216R
	4 'DI-MONOvalent ION EXCHANGE', 'DECAY ONLY' /	B 217R
C	*****	B 220
	IF (INT.GT.1) GO TO 10	B 230
	WRITE (6,750)	B 240
	READ (5,720) TITLE	B 250
	WRITE (6,730) TITLE	B 260
C	*****	B 270
C	---INITIALIZE TEST AND CONTROL VARIABLES---	B 280
	STORMI=0.0	B 290
	SORBI=0	B 295R
	RHOB=0.0	B 296R
	DK=0.0	B 297R
	CINMAX=0.0	B 298R
	TEST=0.00	B 300
	EKF=0.0	B 301R
	EKL=0.0	B 302R
	EK=0.0	B 303R
	XNF=1.0	B 304R
	CEC=0.0	B 305R
	CTOT=0.0	B 306R
	RF2MIN=1.0	B 307R
	RF2MAX=1.0	B 308R
	TOTLQ=0.00	B 310
	TOTLQI=0.00	B 315
	TPIN=0.00	B 317
	TPOUT=0.00	B 318
	SUMT=0.00	B 320
	SUMTCH=0.0	B 330
	INT=0	B 340
	IPRNT=0	B 350
	MX=1	SB 353
	MY=1	SB 354
	MCHK=0	SB 355
	NCA2=0	SB 356
	NCA=0	B 360
	N=0	B 370
	IMOV=0	B 380
	NMOV=0	B 390
	ICLK=0	B 395
	DMASS1=0.0	B 396R
	RF=1.0	B 397R
	DECAY=0.0	B 398R
	THALF=0.0	B 399R
C	*****	B 400
C	---LOAD CONTROL PARAMETERS---	B 410
	READ (5,740) NTIM,NPMP,NX,NY,NPMAX,NPNT,NITP,NUMOBS,ITMAX,NREC,NPT	B 420
	1PND,NCODES,NPNTMV,NPNTVL,NPNTD,NPDEL,PNPCHV,IReact	B 431A
	NMX=NX	SB 432
	NMY=NY	SB 433
	MMX=NX-1	SB 434
	MMY=NY-1	SB 435
C	---READ UPPER LEFT AND LOWER RIGHT NODAL COORDS. OF	SB 436
C	TRANSPORT SUBGRID, IN FREE FORMAT, IF NX.LT.0---	SB 437
	IF (NX.GT.0) GO TO 5	SB 438A
	NX=-NX	SB 438B
	MCHK=1	SB 438C
	READ (5,*) MX,MY,MMX,MMY	SB 438D
	NMX=MMX-MX+1	SB 439A
	NMY=MMY-MY+1	SB 439B
5	CONTINUE	SB 439H
	READ (5,800) PINT,TOL,POROS,BETA,S,TIMX,TINIT,XDEL,YDEL,DLTRAT,CEL	B 440
	1DIS,ANFCTR	B 450
C	---READ REACTION TERMS IN FREE FORMAT---	B 454R
	IF (IReact.EQ.1) READ (5,*) DK,RHOB,THALF	B 456R
	IF (IReact.LT.-1.OR.IReact.GT.7) IReact=0	B 457R
	IF (IReact.EQ.-1) READ (5,*) THALF	B 458R
	IF (IReact.EQ.2) READ (5,*) RHOB,EKF,XNF,THALF	B 459R
	IF (IReact.EQ.3) READ (5,*) RHOB,EKL,CEC,THALF	B 461R
	IF (IReact.GE.4) READ (5,*) RHOB,EK,CEC,CTOT,THALF	B 462R
	XNFM1=XNF-1.	B 463R
	FCTRF=RHOB*EKF*XNF/POROS	B 464R
	EKLCEC=EKL*CEC	B 465R
	FCTRL=RHOB*EKLCEC/POROS	B 466R
	EKCEC=EK*CEC	B 467R
	IF (CTOT.GT.0.0) FCTRE=RHOB*EKCEC/(POROS*CTOT)	B 468A
	C3=RHOB/POROS	B 468B
	C4=EKCEC	B 468C



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C5=C4*CEC
C6=CTOT*CTOT
C CZERO IS THE MINIMUM CONC. LEVEL FOR NONLINEAR RETARDATION
CZERO=0.9E-15
CALL RETRD2(1.E-15,RF2MAX,RDCOEF)
CZERO=1.E-15
NNX=NX-1
NNY=NY-1
NP=NPMAX
DXINV=1.DO/XDEL
DYINV=1.DO/YDEL
ARINV=DXINV*DYINV
PORINV=1.DO/POROS
RF=1.0+(DK*RHOB/POROS)
IF (THALF.GT.0.0) DECAY=ALOG(2.0)/THALF
C ---PRINT CONTROL PARAMETERS---
WRITE (6,755)
WRITE (6,760)
WRITE (6,770) NX,NY,XDEL,YDEL
IF (MCHK.GT.0) WRITE (6,775) NMX,NMY,MX,MY,MMX,MMY
WRITE (6,780) NTIM,NPMP,PINT,TIMX,TINIT
WRITE (6,790) S,POROS,BETA,DLTRAT,ANFCTR
WRITE (6,870) NITP,TOL,ITMAX,CELDIS,NPMAX,NPTPND
IF (NPTPND.NE.4.AND.NPTPND.NE.5.AND.NPTPND.NE.8.AND.NPTPND.NE.9.
1.AND.NPTPND.NE.16.AND.NPTPND.NE.1) WRITE(6,880)
IF (NPTPND.EQ.1) WRITE (6,882)
IF((NX.EQ.3.OR.NY.EQ.3).AND.NPTPND.NE.1) WRITE(6,883)
IF (NITP.LE.0) WRITE (6,885)
WRITE (6,888)
WRITE (6,890) NPNT,NPNTMV,NPNTVL,NPNTD,NUMOBS,NREC,NCODES,NPNCHV,N
1PDELC,IReact
IF (IReact.EQ.-1) THEN
  WRITE (6,891) REACTN(9)
  IReact=0
ELSE
  WRITE (6,891) REACTN(IReact+1)
END IF
IF (IReact.GE.1) THEN
  WRITE (6,892) RHOB
  IF (IReact.EQ.1) THEN
    WRITE (6,893) DK,RF
  ELSE
    IF (IReact.EQ.2) WRITE (6,894) EKf,XNF
    IF (IReact.EQ.3) WRITE (6,895) EKl,CEC
    IF (IReact.GE.4) WRITE (6,896) EK,CEC,CTOT
    IF (BETA.EQ.0.0) WRITE (6,897)
  END IF
END IF
IF (DECAY.NE.0.0) WRITE (6,898) THALF,DECAY
GO TO 20
C *****
C ---READ DATA TO REVISE TIME STEPS AND STRESSES FOR SUBSEQUENT
C PUMPING PERIODS---
10 READ (5,1080) ICHK
IF (ICHK.LE.0) WRITE (6,1110) INT
IF (ICHK.LE.0) GO TO 20
C ---REINITIALIZE REC AND CNRECH IN REC CELLS---
C AND RESET MINIMUM RETARDATION
IF (NREC.GT.0.OR.(IReact.GE.2.AND.IReact.LE.7)) THEN
  CINMAX=0.0
  DO 12 IY=2,NNY
  DO 12 IX=2,NNX
  JX=IX-MX+1
  JY=IY-MY+1
  IF (REC(IX,IY).NE.0.0) THEN
    REC(IX,IY)=0.DO
    IF (JX.GT.0.AND.JX.LE.NMX.AND.JY.GT.0.AND.JY.LE.NMY)
1 CNRECH(JX,JY)=0.0
  END IF
  IF (JX.GT.0.AND.JX.LE.NMX.AND.JY.GT.0.AND.JY.LE.NMY) THEN
    IF (CONC(JX,JY).GT.CINMAX) CINMAX=CONC(JX,JY)
    IF ((VPRM(IX,IY).NE.0.0.OR.RECH(JX,JY).LT.0.0)
1 .AND.CNRECH(JX,JY).GT.CINMAX) CINMAX=CNRECH(JX,JY)
  END IF
12 CONTINUE
CALL RETRD2(CINMAX,RF2MIN,RDCOEF)
IF (IReact.EQ.2.AND.XNFM1.GT.0.0) RF2MIN=RF2MAX
END IF

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B 468D
B 468E
B 468F
B 468G
B 468H
B 469R
B 470
B 480
B 490
B 500
B 510
B 520
B 530
B 532R
B 534R
B 540
SB 545
B 550
B 560
SB 565
B 570
B 580
B 590
B 601
B 612
B 614
B 614A
B 615
SB 617
B 620
B 631R
B 632A
B 632B
B 632C
B 632D
B 632E
B 632F
B 633R
B 634R
B 636R
B 637R
B 638R
B 639R
B 641R
B 642R
B 643R
B 644R
B 645R
B 648R
B 650
B 660
B 670
B 680
B 690
B 695
B 701
B 702
B 703A
B 703B
B 703C
B 704A
B 704B
SB 704C
SB 704D
B 704E
B 705B
SB 707A
SB 707B
B 707C
SB 707D
SB 707E
SB 707F
SB 707G
B 707H
B 708
B 708A
B 708B
B 709

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READ (5,1070) NTIM, NPNT, NITP, ITMAX, NREC, NPNTMV, NPNTVL, NPNTD, NPDEL  B 710
1, NPNCHV, PINT, TIMX, TINIT  B 720
WRITE (6,1080) INT  B 730
WRITE (6,1090) NTIM, NPNT, NITP, ITMAX, NREC, NPNTMV, NPNTVL, NPNTD, NPDEL  B 740
1C, NPNCHV, PINT, TIMX, TINIT  B 750
*****  B 760
C ---LIST TIME INCREMENTS---  B 770
C 20 DO 30 J=1,100  B 780
TIM(J)=0.DO  B 790
30 CONTINUE  B 800
PYR=PINT*86400.DO*365.25DO  B 805
TIM(1)=TINIT  B 810
IF (NPNTMV.EQ.0) NPNTMV=999  B 815
IF (S.GT.0.0) THEN  B 821
DO 40 K=2,NTIM  B 830
40 TIM(K)=TIMX*TIM(K-1)  B 840
WRITE (6,470)  B 850
WRITE (6,490) (TIM(K),K=1,NTIM)  B 861
IF (TINIT.GT.PYR) WRITE (6,475)  B 865
ELSE  B 871
50 ANTIM=NTIM  B 882
DO 55 K=1,NTIM  B 884
55 TIM(K)=PYR/ANTIM  B 886
WRITE (6,480)  B 891
WRITE (6,490) (TIM(K),K=1,NTIM)  B 892
END IF  B 893
*****  B 900
C ---INITIALIZE MATRICES---  B 910
C 60 IF (INT.GT.1) GO TO 100  B 920
DO 70 IY=1,NY  B 930
DO 70 IX=1,NX  B 940
VPRM(IX,IY)=0.DO  B 950
THCK(IX,IY)=0.0  B 970
RECH(IX,IY)=0.DO  B 980
REC(IX,IY)=0.DO  B1000
NODEID(IX,IY)=0  B1010
TMRX(IX,IY,1)=0.DO  B1020
TMRX(IX,IY,2)=0.DO  B1030
HI(IX,IY)=0.DO  B1040
HR(IX,IY)=0.DO  B1050
HC(IX,IY)=0.DO  B1060
HK(IX,IY)=0.DO  B1070
WT(IX,IY)=0.DO  B1080
VX(IX,IY)=0.0  B1090
VY(IX,IY)=0.0  B1100
VXBDY(IX,IY)=0.0  B1110
VYBDY(IX,IY)=0.0  B1120
70 CONTINUE  B1160
DO 75 IY=1,NMY  SB1161
DO 75 IX=1,NMX  SB1162
CNRECH(IX,IY)=0.0  SB1163
CONC(IX,IY)=0.0  SB1164
CONINT(IX,IY)=0.0  SB1165
SUMC(IX,IY)=0.0  SB1166
NPCELL(IX,IY)=0  SB1167
75 CONTINUE  SB1168
*****  B1170
C ---READ OBSERVATION WELL LOCATIONS---  B1180
C IF (NUMOBS.LE.0) GO TO 100  B1190
WRITE (6,755)  B1195
WRITE (6,900)  B1200
DO 80 J=1,NUMOBS  B1210
READ (5,700) IX,IY  B1220
WRITE (6,810) J,IX,IY  B1230
IXOBS(J)=IX  B1240
80 IYOBS(J)=IY  B1250
DO 90 I=1,NUMOBS  B1260
DO 90 J=1,50  B1270
TMWL(I,J)=0.0  B1280
90 TMCN(I,J)=0.0  B1290
*****  B1300
C ---READ PUMPAGE DATA -- (X-Y COORDINATES AND RATE IN CFS)---  B1310
C ---SIGNS : WITHDRAWAL = POS.; INJECTION = NEG.---  B1320
C ---IF INJ. WELL, ALSO READ CONCENTRATION OF INJECTED WATER---  B1330
C 100 IF (NREC.LE.0) GO TO 120  B1340
IF (INT.GT.1.AND.ICHK.LE.0) THEN  B1346A
IF (IREACT.GE.2.AND.IREACT.LE.7) WRITE (6,899) RF2MIN  B1346B
RETURN  B1346C

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END IF	B1346D
WRITE (6,755)	B1347
WRITE (6,910)	B1350
DO 110 I=1,NREC	B1360
READ (5,710) IX,IY,FCTR,CNREC	B1370
JX=IX-MX+1	SB1372
JY=IY-MY+1	SB1373
IF (JX.LT.1.OR.JY.LT.1.OR.JX.GT.NMX.OR.JY.GT.NMY) GO TO 105	SB1374
IF (FCTR.LT.0.0) CNRECH(JX,JY)=CNREC	SB1382
IF (FCTR.LT.0.0.AND.CNREC.GT.CINMAX) CINMAX=CNREC	B1384R
105 REC(IX,IY)=FCTR	SB1392
110 WRITE (6,820) IX,IY,REC(IX,IY),CNREC	SB1402
CALL RETRD2(CINMAX,RF2MIN,RDCOEF)	B1404R
IF (IREACT.EQ.2.AND.XNFM1.GT.0.0) RF2MIN=RF2MAX	B1405R
C *****	B1410
120 IF (INT.GT.1) THEN	B1421R
IF (IREACT.GE.2.AND.IREACT.LE.7) WRITE (6,899) RF2MIN	B1422R
RETURN	B1423R
END IF	B1424R
AREA=XDEL*YDEL	B1430
WRITE (6,755)	B1435
WRITE (6,690) AREA	B1440
WRITE (6,600)	B1450
WRITE (6,610) XDEL	B1460
WRITE (6,610) YDEL	B1470
C *****	B1480
C ---READ TRANSMISSIVITY IN FT**2/SEC INTO VPRM ARRAY---	B1490
C ---FCTR = TRANSMISSIVITY MULTIPLIER ---> FT**2/SEC---	B1500
WRITE (6,530)	B1510
WRITE (6,755)	B1515
READ (5,550) INPUT,FCTR	B1520
DO 160 IY=1,NY	B1530
IF (INPUT.EQ.1) READ (5,560) (VPRM(IX,IY),IX=1,NX)	B1540
DO 150 IX=1,NX	B1550
IF (INPUT.NE.1) GO TO 130	B1560
VPRM(IX,IY)=VPRM(IX,IY)*FCTR	B1570
GO TO 140	B1580
130 VPRM(IX,IY)=FCTR	B1590
140 IF (IX.EQ.1.OR.IX.EQ.NX) VPRM(IX,IY)=0.DO	B1600
IF (IY.EQ.1.OR.IY.EQ.NY) VPRM(IX,IY)=0.DO	B1610
150 CONTINUE	B1620
160 WRITE (6,840) (VPRM(IX,IY),IX=1,NX)	B1631
C *****	B1640
C ---SET UP COEFFICIENT MATRIX --- BLOCK-CENTERED GRID---	B1650
C ---AVERAGE TRANSMISSIVITY --- HARMONIC MEAN---	B1660
IF (ANFCTR.NE.0.0) GO TO 170	B1670
WRITE (6,1050)	B1680
ANFCTR=1.DO	B1690
170 PIES=3.1415927D0*3.1415927D0/2.DO	B1700
YNS=NY*NY	B1710
XNS=NX*NX	B1720
HMIN=2.DO	B1730
DO 180 IY=2,NNY	B1740
DO 180 IX=2,NNX	B1750
IF (VPRM(IX,IY).EQ.0.0) GO TO 180	B1760
TMRX(IX,IY,1)=2.DO*VPRM(IX,IY)*VPRM(IX+1,IY)/	B1771
1 ((VPRM(IX,IY)+VPRM(IX+1,IY))*XDEL)	B1781
TMRX(IX,IY,2)=2.DO*VPRM(IX,IY)*VPRM(IX,IY+1)/	B1791
1 ((VPRM(IX,IY)+VPRM(IX,IY+1))*YDEL)	B1801
C ---ADJUST COEFFICIENT FOR ANISOTROPY---	B1810
TMRX(IX,IY,2)=TMRX(IX,IY,2)*ANFCTR	B1820
C ---COMPUTE MINIMUM ITERATION PARAMETER (HMIN)---	B1830
IF (TMRX(IX,IY,1).EQ.0.0) GO TO 180	B1840
IF (TMRX(IX,IY,2).EQ.0.0) GO TO 180	B1850
RAT=TMRX(IX,IY,1)*YDEL/(TMRX(IX,IY,2)*XDEL)	B1860
HMX=PIES/(XNS*(1.DO+RAT))	B1870
HMY=PIES/(YNS*(1.DO+(1.DO/RAT)))	B1880
IF (HMX.LT.HMIN) HMIN=HMX	B1890
IF (HMY.LT.HMIN) HMIN=HMY	B1900
180 CONTINUE	B1910
IF (NX.GT.3.AND.NY.GT.3) GO TO 185	B1912
HMX=PIES/XNS	B1913
HMY=PIES/YNS	B1914
HMIN=DMIN1(HMIN,HMX,HMY)	B1915
185 CONTINUE	B1916
C *****	B1920
C ---READ AQUIFER THICKNESS---	B1930
WRITE (6,510)	B1940

WRITE (6,755)	B1945
READ (5,550) INPUT,FCTR	B1950
DO 210 IY=1,NY	B1960
IF (INPUT.EQ.1) READ (5,540) (THCK(IX,IY),IX=1,NX)	B1970
DO 200 IX=1,NX	B1980
IF (INPUT.NE.1) GO TO 190	B1990
THCK(IX,IY)=THCK(IX,IY)*FCTR	B2000
GO TO 200	B2010
190 IF (VPRM(IX,IY).NE.0.0) THCK(IX,IY)=FCTR	B2020
200 CONTINUE	B2030
WRITE (6,500) (THCK(IX,IY),IX=1,NX)	B2041
C ---STORE THICKNESS*POROSITY IN THCK ARRAY---	B2043
DO 205 IX=1,NX	B2044
205 THCK(IX,IY)=THCK(IX,IY)*POROS	B2045
210 CONTINUE	B2046
C *****	B2050
C ---READ DIFFUSE RECHARGE AND DISCHARGE---	B2060
WRITE (6,830)	B2070
WRITE (6,755)	B2075
READ (5,550) INPUT,FCTR	B2080
DO 240 IY=1,NY	B2090
IF (INPUT.EQ.1) READ (5,560) (RECH(IX,IY),IX=1,NX)	B2100
DO 230 IX=1,NX	B2110
IF (INPUT.NE.1) GO TO 220	B2120
RECH(IX,IY)=RECH(IX,IY)*FCTR	B2130
GO TO 230	B2140
220 IF (THCK(IX,IY).NE.0.0) RECH(IX,IY)=FCTR	B2150
230 CONTINUE	B2160
240 WRITE (6,840) (RECH(IX,IY),IX=1,NX)	B2170
C *****	B2180
C ---COMPUTE PERMEABILITY FROM TRANSMISSIVITY---	B2190
C ---COUNT NO. OF CELLS IN AQUIFER---	B2200
C ---SET NZCRIT = 2% OF THE NO. OF CELLS IN THE AQUIFER---	B2210
DO 250 IX=1,NX	B2220
DO 250 IY=1,NY	B2230
IF (THCK(IX,IY).EQ.0.0) GO TO 250	B2240
VPRM(IX,IY)=(VPRM(IX,IY)*POROS)/THCK(IX,IY)	B2251
NCA=NCA+1	B2260
IF (MCHK.EQ.0) GO TO 250	SB2262
IF (IX.LT.MX.OR.IX.GT.MMX) GO TO 250	SB2263
IF (IY.LT.MY.OR.IY.GT.MMY) GO TO 250	SB2264
NCA2=NCA2+1	SB2265
250 CONTINUE	B2271
C	B2280
AAQ=NCA*AREA	B2290
NZCRIT=(NCA+25)/50	B2300
IF (MCHK.GT.0) NZCRIT=(NCA2+25)/50	SB2301
IF (NZCRIT.EQ.0) NZCRIT=1	SB2305
WRITE (6,620)	B2310
WRITE (6,755)	B2315
DO 260 IY=1,NY	B2320
WRITE (6,840) (VPRM(IX,IY),IX=1,NX)	B2322
DO 260 IX=1,NX	B2324
260 VPRM(IX,IY)=0.DO	B2326
IF (MCHK.EQ.0) GO TO 265	SB2332
AAQ2=NCA2*AREA	SB2333
WRITE (6,633)	SB2334
WRITE (6,635) NCA,AAQ	SB2335
WRITE (6,634)	SB2336
WRITE (6,630) NCA2,AAQ2,NZCRIT	SB2337
GO TO 267	SB2338
265 CONTINUE	SB2339
WRITE (6,630) NCA,AAQ,NZCRIT	B2340
267 CONTINUE	SB2345
C *****	B2350
C ---READ NODE IDENTIFICATION CARDS---	B2360
C ---SET VERT. PERM., SOURCE CONC., AND DIFFUSE RECHARGE---	B2370
C ---SPECIFY CODES TO FIT YOUR NEEDS---	B2380
WRITE (6,570)	B2390
READ (5,550) INPUT,FCTR	B2400
DO 280 IY=1,NY	B2410
IF (INPUT.EQ.1) READ (5,640) (NODEID(IX,IY),IX=1,NX)	B2420
DO 270 IX=1,NX	B2430
270 IF (INPUT.NE.1.AND.THCK(IX,IY).NE.0.0) NODEID(IX,IY)=FCTR	B2440
280 WRITE (6,580) (NODEID(IX,IY),IX=1,NX)	B2450
WRITE (6,920) NCODES	B2460
IF (NCODES.LE.0) GO TO 310	B2470
WRITE (6,930)	B2480

DO 300 IJ=1,NCODES	B2490
READ (5,850) ICODE,FCTR1,FCTR2,FCTR3,OVERRD	B2500
DO 290 IX=1,NX	B2510
DO 290 IY=1,NY	B2520
IF (NODEID(IX,IY).NE.ICODE) GO TO 290	B2530
VPRM(IX,IY)=FCTR1	B2540
JX=IX-MX+1	SB2544
JY=IY-MY+1	SB2545
IF (JX.LT.1.OR.JY.LT.1.OR.JX.GT.NMX.OR.JY.GT.NMY) GO TO 285	SB2546
CNRECH(JX,JY)=FCTR2	SB2551
IF (FCTR2.GT.CINMAX) CINMAX=FCTR2	B2553R
285 CONTINUE	SB2555
IF (OVERRD.NE.0) RECH(IX,IY)=FCTR3	B2560
290 CONTINUE	B2570
WRITE (6,860) ICODE,FCTR1,FCTR2	B2580
300 IF (OVERRD.NE.0) WRITE (6,1100) FCTR3	B2590
310 WRITE (6,590)	B2600
WRITE (6,755)	B2615
DO 320 IY=1,NY	B2610
320 WRITE (6,840) (VPRM(IX,IY),IX=1,NX)	B2621
C *****	B2630
C ---READ WATER-TABLE ELEVATION---	B2640
WRITE (6,670)	B2650
WRITE (6,755)	B2655
READ (5,550) INPUT,FCTR	B2660
DO 350 IY=1,NY	B2670
IF (INPUT.EQ.1) READ (5,660) (WT(IX,IY),IX=1,NX)	B2680
DO 340 IX=1,NX	B2690
IF (INPUT.NE.1) GO TO 330	B2700
WT(IX,IY)=WT(IX,IY)*FCTR	B2710
GO TO 340	B2720
330 IF (THCK(IX,IY).NE.0.0) WT(IX,IY)=FCTR	B2730
340 CONTINUE	B2740
350 WRITE (6,680) (WT(IX,IY),IX=1,NX)	B2750
C *****	B2760
C ---SET INITIAL HEADS---	B2770
DO 360 IX=1,NX	B2780
DO 360 IY=1,NY	B2790
HI(IX,IY)=WT(IX,IY)	B2800
HC(IX,IY)=HI(IX,IY)	B2810
HR(IX,IY)=HI(IX,IY)	B2820
360 HK(IX,IY)=HI(IX,IY)	B2830
C	B2840
CALL OUTPT	B2850
C *****	B2860
C ---COMPUTE ITERATION PARAMETERS---	B2870
DO 370 ID=1,20	B2880
AOPT(ID)=0.DO	B2890
370 CONTINUE	B2900
ANITP=NITP-1.DO	B2910
ALPHA1=DEXP(DLOG(1.DO/HMIN)/ANITP)	B2920
AOPT(1)=HMIN	B2930
DO 380 IP=2,NITP	B2940
380 AOPT(IP)=AOPT(IP-1)*ALPHA1	B2950
C	B2960
WRITE (6,450)	B2970
WRITE (6,460) (AOPT(IP),IP=1,NITP)	B2981
C *****	B2990
C ---READ INITIAL CONCENTRATIONS AND COMPUTE INITIAL MASS STORED---	B3000
C ---IF USING SMALLER SUBGRID FOR TRANSPORT, READ INITIAL	SB3005
C CONCENTRATION ARRAY FOR SUBGRID NODES ONLY---	SB3006
READ (5,550) INPUT,FCTR	B3010
CFCTR2=DK*RHOB/POROS	B3016R
DO 420 IY=1,NMY	SB3021
JY=IY+MY-1	SB3025
IF (INPUT.EQ.1) READ (5,660) (CONC(IX,IY),IX=1,NMX)	SB3031
DO 410 IX=1,NMX	SB3041
JX=IX+MX-1	SB3045
IF (INPUT.NE.1) GO TO 390	B3050
CONC(IX,IY)=CONC(IX,IY)*FCTR	B3060
GO TO 400	B3070
390 IF (THCK(JX,JY).NE.0.0) CONC(IX,IY)=FCTR	SB3081
400 CONINT(IX,IY)=CONC(IX,IY)	B3090
CFCTR=CONINT(IX,IY)*THCK(JX,JY)*AREA	SB3093R
SORBI=SORBI+CFCTR*CFCTR2	B3094R
IF (IREACT.GE.2)	B3095A
1 SORBI=SORBI+RHOB/POROS*AREA*THCK(JX,JY)*SORB2(CONINT(IX,IY))	SB3095B
IF (CONINT(IX,IY).GT.CINMAX) CINMAX=CONINT(IX,IY)	B3095C

410	STORMI=STORMI+CFCTR	B3097R
420	CONTINUE	B3110
	CALL RETRD2(CINMAX,RF2MIN,RDCOEF)	B3112R
	IF (IREACT.EQ.2.AND.XNFM1.GT.0.0) RF2MIN=RF2MAX	B3113R
	IF (IREACT.GE.2.AND.IREACT.LE.7) WRITE (6,899) RF2MIN	B3114R
C	*****	B3120
C	---CHECK DATA SETS FOR INTERNAL CONSISTENCY---	B3130
	DO 440 IX=1,NX	B3140
	DO 440 IY=1,NY	B3150
	IF (THCK(IX,IY).GT.0.0) THEN	B3161
	IF (IX.EQ.1.OR.IY.EQ.1.OR.IX.EQ.NX.OR.IY.EQ.NY)	B3162
	1 WRITE (6,935) IX,IY	B3163
	GO TO 430	B3164
	END IF	B3165
	IF (TMRX(IX,IY,1).GT.0.0) WRITE (6,940) IX,IY	B3170
	IF (TMRX(IX,IY,2).GT.0.0) WRITE (6,950) IX,IY	B3180
	IF (IX.NE.1) THEN	B3182
	IF (TMRX(IX-1,IY,1).GT.0.0) WRITE (6,940) IX,IY	B3183
	END IF	B3184
	IF (IY.NE.1) THEN	B3185
	IF (TMRX(IX,IY-1,2).GT.0.0) WRITE (6,950) IX,IY	B3186
	END IF	B3187
	IF (NODEID(IX,IY).GT.0) WRITE (6,960) IX,IY	B3190
	IF (WT(IX,IY).NE.0.0) WRITE (6,970) IX,IY	B3200
	IF (RECH(IX,IY).NE.0.0) WRITE (6,980) IX,IY	B3210
	IF (REC(IX,IY).NE.0.0) WRITE (6,990) IX,IY	B3220
430	IF (TMRX(IX,IY,1).GT.0.0.OR.TMRX(IX,IY,2).GT.0.0) GO TO 440	B3231
	IF (IX.NE.1) THEN	B3232
	IF (TMRX(IX-1,IY,1).GT.0.0) GO TO 440	B3233
	END IF	B3234
	IF (IY.NE.1) THEN	B3235
	IF (TMRX(IX,IY-1,2).GT.0.0) GO TO 440	B3236
	END IF	B3237
	IF (NODEID(IX,IY).GT.0.0) WRITE (6,1000) IX,IY	B3240
	IF (WT(IX,IY).NE.0.0) WRITE (6,1010) IX,IY	B3250
	IF (RECH(IX,IY).NE.0.0) WRITE (6,1020) IX,IY	B3260
	IF (REC(IX,IY).NE.0.0) WRITE (6,1030) IX,IY	B3270
	IF (THCK(IX,IY).GT.0.0) WRITE (6,1040) IX,IY	B3280
440	CONTINUE	B3290
C	*****	B3300
	RETURN	B3310
C	*****	B3320
C		B3330
C		B3340
C		B3350
450	FORMAT (1H1,20HITERATION PARAMETERS)	B3360
460	FORMAT (3H ,1G20.6)	B3370
470	FORMAT (1H1,27HTIME INTERVALS (IN SECONDS))	B3380
475	FORMAT (1H0,5X,65H*** WARNING *** INITIAL TIME STEP IS LONGER TH	B3384
	1AN PUMPING PERIOD/25X,34H***ADJUST EITHER TINIT OR PINT.***/)	B3385
480	FORMAT (1H1,15X,17HSTEADY-STATE FLOW//5X,55HTIME INTERVALS (IN SEC	B3391
	1) FOR SOLUTE-TRANSPORT SIMULATION)	B3401
490	FORMAT (3H ,10G12.5)	B3410
500	FORMAT (3H ,25F5.1)	SB3421
510	FORMAT (1H1,22HAQUIFER THICKNESS (FT))	B3430
530	FORMAT (1H1,30HTRANSMISSIVITY MAP (FT*FT/SEC))	B3450
540	FORMAT (20G3.0)	B3460
550	FORMAT (11,G10.0)	B3470
560	FORMAT (20G4.1)	B3480
570	FORMAT (1H1,23HNODE IDENTIFICATION MAP//)	B3490
580	FORMAT (1H ,40I3)	SB3501
590	FORMAT (1H1,45HVERTICAL PERMEABILITY/THICKNESS (FT/(FT*SEC)))	B3510
600	FORMAT (1H0,10X,12HX-Y SPACING:)	B3520
610	FORMAT (1H ,12X,10G12.5)	B3530
620	FORMAT (1H1,24HPERMEABILTY MAP (FT/SEC))	B3540
630	FORMAT (1H0,05X,05X,44HNO. OF FINITE-DIFFERENCE CELLS IN AQUIFER =	SB3551
	1 ,I4//10X,28HAREA OF AQUIFER IN MODEL = ,G12.5,10H SQ. FT.////1	B3560
	20X,47HNZCRIT (MAX. NO. OF CELLS THAT CAN BE VOID OF/20X,56HPARTI	B3570
	3CLES; IF EXCEEDED, PARTICLES ARE REGENERATED) = ,I4//)	B3580
633	FORMAT (1H0,///2X,26HFLOW MODEL (PRIMARY GRID):/)	SB3582
634	FORMAT (1H0,///2X,18HTRANSPORT SUBGRID:/)	SB3583
635	FORMAT (1H0,05X,05X,44HNO. OF FINITE-DIFFERENCE CELLS IN AQUIFER =	SB3584
	1 ,I4//10X,28HAREA OF AQUIFER IN MODEL = ,G12.5,10H SQ. FT./)	SB3585
640	FORMAT (20I1)	B3590
660	FORMAT (20G4.0)	B3610
670	FORMAT (1H1,11HWATER TABLE)	B3620
680	FORMAT (1H ,20F5.0)	B3630
690	FORMAT (1H0,10X,19HAREA OF ONE CELL = ,G12.4)	B3640

700	FORMAT (2I2)	B3650
710	FORMAT (2I2,2G8.2)	B3660
720	FORMAT (10A8)	B3670
730	FORMAT (1H0,10A8)	B3680
740	FORMAT (18I4)	B3691R
750	FORMAT (1H1,77HU.S.G.S. METHOD-OF-CHARACTERISTICS MODEL FOR SOLUTE 1 TRANSPORT IN GROUND WATER)	B3700 B3710
755	FORMAT (1H )	SB3715
760	FORMAT (1H0,21X,21HI N P U T D A T A)	B3720
770	FORMAT (1H0,23X,16HGRID DESCRIPTORS//13X,30HNX (NUMBER OF COLUM 1NS) = ,I4/13X,28HNY (NUMBER OF ROWS) = ,I6/13X,29HXDEL (X 2-DISTANCE IN FEET) = ,F7.1/13X,29HYDEL (Y-DISTANCE IN FEET) = ,F7 3.1)	B3730 B3740 B3750 B3760
775	FORMAT (1H0,18X,31HSECONDARY SUBGRID FOR TRANSPORT//16X,30HNMX ( SB3763 1NUMBER OF COLUMNS) = ,I4/16X,30HNMY (NUMBER OF ROWS) = ,I SB3764 24//16X,38HCROSS-REF. TO PRIMARY GRID IX IY/46X,8H --- --/18 SB3765 3X,28HFIRST NODE (UPPER LEFT) AT: ,2I4/18X,28HLAST NODE (LOWER RIGH SB3766 4T) AT: ,2I4)	SB3767
780	FORMAT (1H0,23X,16HTIME PARAMETERS//13X,40HNTIM (MAX. NO. OF TI 1ME STEPS) = ,I6/13X,40HNMP (NO. OF PUMPING PERIODS) 2 = ,I6/13X,39HPINT (PUMPING PERIOD IN YEARS) = ,F11.3/13X,39 3HTIMX (TIME INCREMENT MULTIPLIER) = ,F10.2/13X,39HTINIT (INIT 4IAL TIME STEP IN SEC.) = ,F8.0)	B3770 B3780 B3791 B3800 B3810
790	FORMAT (1H0,14X,34HHYDROLOGIC AND CHEMICAL PARAMETERS//13X,1HS,7X, 129H(STORAGE COEFFICIENT) = ,5X,F9.6/13X,28HPOROS (EFFECTIVE 2 POROSITY),8X,3H= ,F9.3/13X,39HBETA (LONGITUDINAL DISPERSIVITY SB3841 3) = ,F7.1/13X,31HDLTRAT (RATIO OF TRANSVERSE TO/21X,30HLONGITUDI SB3851 4NAL DISPERSIVITY) = ,F9.2/13X,39HANFCTR (RATIO OF T-YY TO T-XX) 5 = ,F12.6)	B3820 B3830 B3841 B3851 B3860 B3870
800	FORMAT (12G5.0)	B3880
810	FORMAT (1H ,16X,I2,5X,I2,4X,I2)	B3890
820	FORMAT (1H ,7X,2I4,3X,F9.4,3X,F8.2)	B3895
830	FORMAT (1H1,39HDIFFUSE RECHARGE AND DISCHARGE (FT/SEC))	B3910
840	FORMAT (1H ,1P10E10.2)	B3920
850	FORMAT (I2,3G10.2,I2)	B3930
860	FORMAT (1H0,7X,I2,7X,E10.3,5X,F9.2)	B3940
870	FORMAT (1H0,21X,20HEXECUTION PARAMETERS//13X,39HNITP (NO. OF ITE 1RATION PARAMETERS) = ,I4/13X,39HTOL (CONVERGENCE CRITERIA - ADI 2P) = ,E9.2/13X,39HITMAX (MAX.NO.OF ITERATIONS - ADIP) = ,I4/13X,3 34HCELDIS (MAX.CELL DISTANCE PER MOVE/24X,28HOF PARTICLES - M.O.C.) 4 = ,F8.3/13X,30HNPMAX (MAX. NO. OF PARTICLES),7X,2H= ,I4/12X,3 52H NPTPND (NO. PARTICLES PER NODE),6X,3H= ,I4)	B3950 B3960 B3971 B3980 B3990 B4000
880	FORMAT (1H0,5X,47H*** WARNING *** NPTPND MUST = 1,4,5,8,9, OR 16)	B4011A
882	FORMAT (1H0,5X,58H*** CAUTION *** USE OF NPTPND=1 MAY CAUSE LOSS O 1F ACCURACY)	B4012A B4012B
883	FORMAT (1H0,5X,56H*** ONE-DIMENSIONAL *** WILL USE ONLY 1 ROW OF P 1ARTICLES/13X,35HUSE 2 PARTICLES FOR NPTPND = 4 OR 5/13X,35HUSE 3 P 2ARTICLES FOR NPTPND = 8 OR 9/13X,31HUSE 4 PARTICLES FOR NPTPND = 1 36)	B4013A B4013B B4013C B4013D
885	FORMAT (1H0,5X,38H*** WARNING *** NITP MUST BE POSITIVE)	B4015
888	FORMAT (1H1)	SB4017
890	FORMAT (1H0,23X,15HPROGRAM OPTIONS//13X,30HNPNP (TIME STEP INTER 1VAL FOR/21X,18HCOMPLETE PRINTOUT),7X,3H= ,I4/13X,31HNPNTMV (MOVE 2INTERVAL FOR CHEM./21X,28HCONCENTRATION PRINTOUT) = ,I4/13X,30HN 3PNTVL (TIME STEP INTERVAL FOR/21X,'VELOCITY PRINTOUT; 0=NEVER;'/ 4 21X,'-1=FIRST TIME STEP;'/21X,'-2=LAST TIME STEP)',7X,3H= ,I4/ 5 13X,'NPNTD (PRINT OPTION-DISP.COEF.'/21X, 6 '0=NO; 1=FIRST TIME STEP;'/21X,'2=ALL TIME STEPS)',8X,3H= ,I4/ 7 13X,'NUMOBS (NO. OF OBSERVATION WELLS'/ 8 21X,'FOR HYDROGRAPH PRINTOUT) = ',I4/ 9 13X,'NREC (NO. OF PUMPING WELLS) = ',I5/ \$ 13X,'NCODES (FOR NODE IDENT.)',9X,2H= ,I5/ 1 13X,'NPNCHV (TIME STEP INTERVAL FOR'/21X,'VELOCITY PRINTOUT ON'/ 2 21X,'FILE UNIT 7; 0=NEVER;'/21X,'-1=FIRST TIME STEP;'/ 3 21X,'-2=LAST TIME STEP)',7X,2H= ,I5/ 4 13X,'NPDEL (PRINT OPT.-CONC. CHANGE) = ',I4/ 5 13X,'IREACT (REACTION SPECIFIER) = ',I5)	B4020 B4030 B4041 B4045 B4051 B4055 B4061 B4065 B4071 B4075 B4081 B4091 B4101 B4111 B4118R B4126R B4127R
891	FORMAT (//13X,'REACTION - ',A26/)	B4128A
892	FORMAT (13X,'RHOB (BULK DENSITY) = ',1PE12.5)	B4128B
893	FORMAT (13X,'DK (DISTRIBUTION COEFFICIENT) = ',1PE12.5/ 1 13X,'RF (RETARDATION FACTOR) = ',1PE12.5)	B4128C B4128D
894	FORMAT (13X,'EKF (FREUNDLICH SORPTION CONSTANT)= ',1PE12.5/ 1 13X,'XNF (FREUNDLICH SORPTION SLOPE) = ',1PE12.5)	B4128E B4128F
895	FORMAT (13X,'EKL (LANGMUIR SORPTION CONSTANT) = ',1PE12.5/ 1 13X,'CEC (CATION EXCHANGE CAPACITY) = ',1PE12.5)	B4128G B4128H
896	FORMAT (13X,'EK (ION EXCHANGE CONSTANT) = ',1PE12.5/ 1 13X,'CEC (CATION EXCHANGE CAPACITY) = ',1PE12.5/ 2 13X,'CTOT (TOTAL SOLUTE CONCENTRATION) = ',1PE12.5)	B4128I B4128J

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897 FORMAT (/ ' *** WARNING *** BETA.EQ.0.0 AND SORPTION-EXCHANGE IS', B4129A
1 ' NONLINEAR') B4129B
898 FORMAT (/13X,'THALF (HALF LIFE OF DECAY,IN SEC) = ',1PE12.5/ B4129C
1 13X,'DECAY (DECAY CONSTANT=LN 2/THALF) = ',1PE12.5) B4129D
899 FORMAT (1H0,' MINIMUM NONLINEAR RETARDATION FACTOR FOR THIS', B4129E
1 ' PUMPING PERIOD'//10X,' RF2MIN = ',1PE12.4) B4129F
900 FORMAT (1H0,10X,29HLOCATION OF OBSERVATION WELLS//17X,3HNO.,5X,1HX B4130
1,5X,1HY/) B4140
910 FORMAT (1H0,10X,28HLOCATION OF PUMPING WELLS//11X,28HX Y RA B4150
1TE(IN CFS) CONC./) B4160
920 FORMAT (1H0,5X,37HNO. OF NODE IDENT. CODES SPECIFIED = ,I2) B4170
930 FORMAT (1H0,10X,41HTHE FOLLOWING ASSIGNMENTS HAVE BEEN MADE:/5X,51 B4180
1HCODE NO. LEAKANCE SOURCE CONC. RECHARGE) B4190
935 FORMAT (1H ,5X,54H*** WARNING *** THCK.NE.0.0 ON BOUNDARY AT NOD B4195
1E IX =,I4,6H, IY =,I4) B4196
940 FORMAT (1H ,5X,61H*** WARNING *** THCK.EQ.0.0 AND TMRX(X).GT.0.0 B4200
1 AT NODE IX =,I4,6H, IY =,I4) B4210
950 FORMAT (1H ,5X,61H*** WARNING *** THCK.EQ.0.0 AND TMRX(Y).GT.0.0 B4220
1 AT NODE IX =,I4,6H, IY =,I4) B4230
960 FORMAT (1H ,5X,61H*** WARNING *** THCK.EQ.0.0 AND NODEID.GT.0.0 B4240
1 AT NODE IX =,I4,6H, IY =,I4) B4250
970 FORMAT (1H ,5X,56H*** WARNING *** THCK.EQ.0.0 AND WT.NE.0.0 AT N B4260
1ODE IX =,I4,6H, IY =,I4) B4270
980 FORMAT (1H ,5X,58H*** WARNING *** THCK.EQ.0.0 AND RECH.NE.0.0 AT B4280
1 NODE IX =,I4,6H, IY =,I4) B4290
990 FORMAT (1H ,5X,58H*** WARNING *** THCK.EQ.0.0 AND REC.NE.0.0 AT B4300
1 NODE IX =,I4,6H, IY =,I4) B4310
1000 FORMAT (1H ,5X,61H*** WARNING *** TMRX.EQ.0.0 AND NODEID.GT.0.0 B4321
1 AT NODE IX =,I4,6H, IY =,I4) B4330
1010 FORMAT (1H ,5X,56H*** WARNING *** TMRX.EQ.0.0 AND WT.NE.0.0 AT N B4341
1ODE IX =,I4,6H, IY =,I4) B4350
1020 FORMAT (1H ,5X,58H*** WARNING *** TMRX.EQ.0.0 AND RECH.NE.0.0 AT B4361
1 NODE IX =,I4,6H, IY =,I4) B4370
1030 FORMAT (1H ,5X,58H*** WARNING *** TMRX.EQ.0.0 AND REC.NE.0.0 AT B4381
1 NODE IX =,I4,6H, IY =,I4) B4390
1040 FORMAT (1H ,5X,58H*** WARNING *** TMRX.EQ.0.0 AND THCK.GT.0.0 AT B4401
1 NODE IX =,I4,6H, IY =,I4) B4410
1050 FORMAT (1H0,5X,45H*** WARNING *** ANFCTR WAS SPECIFIED AS 0.0/23 B4420
1X,34HDEFAULT ACTION: RESET ANFCTR = 1.0) B4430
1060 FORMAT (I1) B4440
1070 FORMAT (10I4,3G5.0) B4450
1080 FORMAT (1H1,5X,25HSTART PUMPING PERIOD NO. ,I2//2X,75HTHE FOLLOWIN B4460
1G TIME STEP, PUMPAGE, AND PRINT PARAMETERS HAVE BEEN REDEFINED:/) B4470
1090 FORMAT (1H0,14X,9HNTIM = ,I4/15X,9HNPNT = ,I4/15X,9HNITP = , B4480
1I4/15X,9HITMAX = ,I4/15X,9HNREC = ,I4/15X,9HNPNTMV = ,I4/15X,9H B4490
2NPNTVL = ,I4/15X,9HNPNTD = ,I4/15X,9HNPELDC = ,I4/15X,9HNPNCNV = B4500
3,I4/15X,9HPINT = ,F10.3/15X,9HTIMX = ,F10.3/15X,9HTINIT = ,F1 B4510
40.3/) B4520
1100 FORMAT (1H ,46X,E10.3) B4530
1110 FORMAT (1H1,5X,25HSTART PUMPING PERIOD NO. ,I2//2X,23HNO PARAMETER B4532
1S REDEFINED/) B4533
END B4540-

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$LARGE
SUBROUTINE RETRD2(CONC,RF2,RDCOEF) K 30
C K 40
C ***** K 50
DOUBLE PRECISION AA,BB,CC,QUADX K 60
COMMON /CHMR/ RF,DK,RHOB,THALF,DECAY,ADSORB,SORBI,DMASS1,CSTM2, K 70
1 EKF,XNF,XNFM1,FCTRF,EKL,CEC,EKLCEC,FCTRL,CINMAX, K 80
2 RF2MIN,RF2MAX,CZERO,IREACT,EK,EKCEC,FCTRE,CTOT,C3,C4,C5,C6 K 90
C ***** K 100
C ---COMPUTE NONLINEAR RETARDATION FACTOR (RF2) AND CORRECTION TERM K 110
C FOR DECAY OF SORBED SOLUTE (RDCOEF)--- K 120
C K 130
RF2=1.0 K 140
RDCOEF=1.0 K 150
IF (IREACT.LE.1) RETURN K 160
C=CONC K 170
IF (C.LE.CZERO) THEN K 180
RF2=RF2MAX K 190
RDCOEF=RF2MAX K 200
RETURN K 210
END IF K 220
C K 230
C ---FREUNDLICH ISOTHERM--- K 240

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IF (IREACT.EQ.2) THEN
  TERM=FCTRF*C**XNFM1
  RF2=1.+TERM
  RDCOEF=1.+TERM/XNF
C
C
C ---LANGMUIR ISOTHERM---
ELSE IF (IREACT.EQ.3) THEN
  DINV=1./(1.+EKL*C)
  TERM=FCTRL*DINV
  RF2=1.+TERM*DINV
  RDCOEF=1.+TERM
C
C ---MONOVALENT ION EXCHANGE---
ELSE IF (IREACT.EQ.4) THEN
  RF2=1.+FCTRE/((C/CTOT*(EK-1.))+1.))**2)
  RDCOEF=1.+FCTRE*CTOT/((CTOT-C)+EK*C)
C
C ---DVALENT ION EXCHANGE---
ELSE IF (IREACT.EQ.5) THEN
  CTOT2=CTOT*0.5
  RF2=1.+FCTRE/((C/CTOT2*(EK-1.))+1.))**2)
  RDCOEF=1.+FCTRE*CTOT2/((CTOT2-C)+EK*C)
C
C ---MONOVALENT-DIVALENT ION EXCHANGE---
ELSE IF (IREACT.EQ.6) THEN
  C2=C*C
  AA=CTOT-C
  BB=C2*EK
  CC=-EKCEC*C2
  CBAR=QUADX(AA,BB,CC,1.DO)
  RDCOEF=1.+C3*CBAR/C
  DCBAR=(CBAR*CBAR-CBAR*2.*C*EK+2.*C*EKCEC)/
  ((CTOT-C)*2.*CBAR+C2*EK)
  RF2=1.+C3*DCBAR
C
C ---DVALENT-MONOVALENT ION EXCHANGE---
ELSE
  C2=C*C
  AA=4.DO*EK*C
  BB=-4.DO*C4*C-C6+4.DO*C*CTOT-C2*4.DO
  CC=C5*C
  CBAR=QUADX(AA,BB,CC,-1.DO)
  RDCOEF=1.+C3*CBAR/C
  A=(-4.*CBAR*CBAR*EK-CBAR*(-4.*C4+4.*CTOT-8.*C)-C5)
  B=(4.*EK*C*(2.*CBAR-CEC)-C6+4.*C*CTOT-4.*C2)
  IF (B.EQ.0.0) THEN
    RF2=1.+C3*1.E-10
  ELSE
    RF2=1.+C3*A/B
  END IF
END IF
RETURN
END
C
C *** SORB2 *****
C
C FUNCTION SORB2(CONC)
C
C *****
C DOUBLE PRECISION AA,BB,CC,QUADX
C COMMON /CHMR/ RF,DK,RHOB,THALF,DECAY,ADSORB,SORBI,DMASS1,CSTM2,
C 1 EK,F,XNF,XNFM1,FCTRF,EKL,CEC,EKLCEC,FCTRL,CINMAX,
C 2 RF2MIN,RF2MAX,CZERO,IREACT,EK,EKCEC,FCTRE,CTOT,C3,C4,C5,C6
C *****
C ---SORB2 IS SORBED CONCENTRATION CORRESPONDING TO CONC IN SOLUTION
C
C SORB2=0.0
C IF (IREACT.LE.1) RETURN
C C=CONC
C IF (C.LE.CZERO) RETURN
C
C ---FREUNDLICH ISOTHERM---
C IF (IREACT.EQ.2) THEN
C SORB2=EKF*C**XNF
C
C ---LANGMUIR ISOTHERM---
C ELSE IF (IREACT.EQ.3) THEN
C SORB2=EKLCEC*C/(1.+EKL*C)
C

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K 250
K 260
K 270
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K 350
K 360
K 370
K 380
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K 410
K 420
K 430
K 440
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K 750
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K 770
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K 800
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K 820
K 830
K 840
K 850
K 860
K 870
K 880
K 890
K 900
K 910
K 920
K 930
K 940
K 950
K 960
K 970
K 980
K 990
K1000
K1010
K1020

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C      ---MONOVALENT ION EXCHANGE---
      ELSE IF (IREACT.EQ.4) THEN
      SORB2=EKCEC*C/(C*(EK-1.)+CTOT)
C
C      ---DIBALENT ION EXCHANGE---
      ELSE IF (IREACT.EQ.5) THEN
      SORB2=EKCEC*C/(2.*C*(EK-1.)+CTOT)
C
C      ---MONOVALENT-DIBALENT ION EXCHANGE---
      ELSE IF (IREACT.EQ.6) THEN
      AA=CTOT-C
      C2=C*C
      BB=C2*EK
      CC=-EKCEC*C2
      SORB2=QUADX(AA,BB,CC,1.DO)
C
C      ---DIBALENT-MONOVALENT ION EXCHANGE---
      ELSE
      AA=4.DO*EK*C
      C2=C*C
      BB=-4.DO*C4*C-C6+4.DO*C*CTOT-C2*4.DO
      CC=C5*C
      SORB2=QUADX(AA,BB,CC,-1.DO)
      END IF
      RETURN
      END
C      *** QUADX *****
C
C      DOUBLE PRECISION FUNCTION QUADX(A,B,C,D)
C
C      *****
C      DOUBLE PRECISION A,B,C,D,T
C      ---SOLVE QUADRATIC EQUATION---
      T=B*B-4.DO*A*C
      IF (T.LT.0.0) THEN
      QUADX=-B/(2.DO*A)
      ELSE
      QUADX=(-B+D*DSQRT(T))/(2.DO*A)
      END IF
      RETURN
      END

```

```

$LARGE
SUBROUTINE VELO
DOUBLE PRECISION DMIN1,DEXP,DLOG,DABS
DOUBLE PRECISION TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT,TITLE
DOUBLE PRECISION XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,
1 HMIN,PYR,ANFCTR
DOUBLE PRECISION RATE,SLEAK,DIV
COMMON /PRMJ/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,
1 NUMOBS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,
2 NPNTMV,NPNTVL,NPNTD,NPNCHV,NPDEL,C,ICLK
COMMON /HEDA/ THCK(040,040),TMWL(05,50),TMOBS(50)
COMMON /HEDB/ TMRX(040,040,2),VPRM(040,040),HI(040,040),
1 HR(040,040),HC(040,040),HK(040,040),WT(040,040),
2 REC(040,040),RECH(040,040),TIM(100),AOPT(20),TITLE(10),XDEL,YDEL,
3 S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR,ANFCTR
COMMON /HEDC/ MX,MY,MMX,MMY,NMX,NMY,MCHK
COMMON /CHMA/ PART(3,06400),CONC(020,020),TMCN(05,50),VX(040,040),
1 VY(040,040),CONINT(020,020),CNRECH(020,020),POROS,
2 SUMTCH,BETA,TIMV,STORM,STORMI,CMSIN,CMSOUT,FLMIN,
3 FLMOT,SUMIO,CELDIS,DLTRAT,CSTORM
COMMON /CHMC/ SUMC(020,020),VXBDY(040,040),VYBDY(040,040)
COMMON /DIFUS/ DISP(020,020,4)
COMMON /CHMR/ RF,DK,RHOB,THALF,DECAY,ADSORB,SORBI,DMASS1,CSTM2,
1 EKF,XNF,XNFM1,FCTRF,EKL,CEC,EKLCEC,FCTRL,CINMAX,
2 RF2MIN,RF2MAX,CZERO,IREACT,EK,EKCEC,FCTRE,CTOT,C3,C4,C5,C6
*****
C      DO NOT RECOMPUTE VELOCITY OR DISP.COEFPS FOR STEADY-STATE FLOW
C      ISOLV=1
      IF (S.EQ.0.0.AND.ICLK.EQ.0.AND.(N.GT.1.OR.INT.GT.1)) THEN
      ISOLV=0
      GO TO 28
      END IF
C      ---COMPUTE VELOCITIES AND STORE---
      VMAX=1.0E-10
      VMAY=1.0E-10

```

	VMXBD=1.0E-10	E 250
	VMYBD=1.0E-10	E 260
	TMV=TIM(N)*1.0E5	E 275
	LIM=0	E 280
	MAXX=0	E 284
	MAXY=0	E 285
	MAXVXI=0	E 286
	MAXVXJ=0	E 287
	MAXVYI=0	E 288
	MAXVYJ=0	E 289
C		E 290
	DO 20 IX=1,NX	E 300
	DO 20 IY=1,NY	E 310
	IF (IX.GT.NMX.OR.IY.GT.NMY) GO TO 12	SE 315
	DO 10 IZ=1,4	E 320
10	DISP(IX,IY,IZ)=0.0	E 330
C		E 340
12	JCK=0	SE 343
	IF (IX.LT.(MX-1).OR.IY.LT.(MY-1).OR.IX.GT.(MMX+1).OR.IY.GT.(MMY+1)	SE 344
1)	JCK=1	SE 345
	IF (THCK(IX,IY).EQ.0.0) GO TO 20	E 350
	RATE=REC(IX,IY)/AREA	E 360
	SLEAK=(HK(IX,IY)-WT(IX,IY))*VPRM(IX,IY)	E 370
	DIV=0.DO	E 381
	IF (RATE.LT.0.0) DIV=RATE	E 382
	IF (SLEAK.LT.0.0) DIV=DIV+SLEAK	E 383
	IF (RECH(IX,IY).LT.0.0) DIV=DIV+RECH(IX,IY)	E 384
C		E 390
C	---VELOCITIES AT CELL BOUNDARIES---	E 580
C	TERM SAVED IS VELOCITY*THICKNESS*POROSITY	E 582
	VXBDY(IX,IY)=TMRX(IX,IY,1)*(HK(IX,IY)-HK(IX+1,IY))	E 585
	VYBDY(IX,IY)=TMRX(IX,IY,2)*(HK(IX,IY)-HK(IX,IY+1))	E 595
C	---VELOCITIES AT NODES---	E 605
C	TEMPORARILY SAVE SEEPAGE VELOCITY FOR PRINTING	E 607
	VX(IX,IY)=(0.5*(VXBDY(IX,IY)+VXBDY(IX-1,IY)))/THCK(IX,IY)	E 615
	VY(IX,IY)=(0.5*(VYBDY(IX,IY)+VYBDY(IX,IY-1)))/THCK(IX,IY)	E 625
	IF (JCK.EQ.0) THEN	SE 645
	IF (THCK(IX+1,IY).NE.0.0.AND.THCK(IX+1,IY).LT.THCK(IX,IY)) THEN	E 646
	ABVX=ABS(VXBDY(IX,IY))/THCK(IX+1,IY)	E 647
	ELSE	E 648
	ABVX=ABS(VXBDY(IX,IY))/THCK(IX,IY)	E 649
	END IF	E 651
	IF (THCK(IX,IY+1).NE.0.0.AND.THCK(IX,IY+1).LT.THCK(IX,IY)) THEN	E 652
	ABVY=ABS(VYBDY(IX,IY))/THCK(IX,IY+1)	E 653
	ELSE	E 654
	ABVY=ABS(VYBDY(IX,IY))/THCK(IX,IY)	E 655
	END IF	E 656
	IF (ABVX.GT.VMXBD) THEN	E 672
	VMXBD=ABVX	E 673
	MAXVXI=IX	E 674
	MAXVXJ=IY	E 675
	END IF	E 676
	IF (ABVY.GT.VMYBD) THEN	E 682
	VMYBD=ABVY	E 683
	MAXVYI=IX	E 684
	MAXVYJ=IY	E 685
	END IF	E 686
END IF		SE 687
C		E 690
	IF (DIV.GE.0.0) GO TO 20	E 700
	IF (JCK.GT.0) GO TO 20	SE 705
	TDIV=THCK(IX,IY)/DABS(DIV)	E 712
	IF (TDIV.GE.TMV) GO TO 20	E 722
	TMV=TDIV	E 724
	MAXX=IX	E 725
	MAXY=IY	E 726
20	CONTINUE	E 728
	TMV=TMV*RF*RF2MIN	E 729R
C	IF OUTPUT OF VELOCITIES ON CELL BOUNDARIES IS DESIRED,	E 731A
C	SEE LINES E 732, E 795A, E 839, E 909, E 986A, E1027A, AND E2399	E 731B
C	ACTIVATE NEXT 6 LINES TO COMPUTE BOUNDARY VELOCITIES FOR PRINTING	E 732
C	DO 25 IY=2,NNY	E 733
C	DO 25 IX=2,NNX	E 734
C	IF (THCK(IX,IY).EQ.0.0) GO TO 25	E 735
C	VXBDY(IX,IY)=VXBDY(IX,IY)/(THCK(IX,IY)+THCK(IX+1,IY))*2.	E 736
C	VYBDY(IX,IY)=VYBDY(IX,IY)/(THCK(IX,IY)+THCK(IX,IY+1))*2.	E 737
C	25 CONTINUE	E 738
C	*****	E 740

```

C      ---PRINT VELOCITIES---
28 IF (NPNTVL.EQ.0) GO TO 80
IF (NPNTVL.EQ.-2.AND.(N.EQ.NTIM.OR.IPRNT.EQ.1)) GO TO 30
IF (NPNTVL.EQ.-1.AND.N.EQ.1) GO TO 30
IF (MOD(N,NPNTVL).EQ.0) GO TO 30
GO TO 80
30 IF (ISOLV.EQ.0) THEN
DO 32 IY=2,NNY
DO 32 IX=2,NNX
IF (THCK(IX,IY).EQ.0.0) GO TO 32
VX(IX,IY)=VX(IX,IY)/THCK(IX,IY)
VY(IX,IY)=VY(IX,IY)/THCK(IX,IY)
C      ACTIVATE NEXT 2 LINES IF BOUNDARY VELOCITIES PRINTED
C      VXBDY(IX,IY)=2.0*VXBDY(IX,IY)/(THCK(IX,IY)+THCK(IX+1,IY))
C      VYBDY(IX,IY)=2.0*VYBDY(IX,IY)/(THCK(IX,IY)+THCK(IX,IY+1))
32 CONTINUE
ISOLV=-1
END IF
WRITE (6,320)
WRITE (6,330)
DO 40 IY=1,NY
40 WRITE (6,350) (VX(IX,IY),IX=1,NX)
C      ACTIVATE NEXT 3 LINES TO PRINT BOUNDARY VELOCITIES
C      WRITE (6,340)
C      DO 50 IY=1,NY
C      50 WRITE (6,350) (VXBDY(IX,IY),IX=1,NX)
WRITE (6,360)
WRITE (6,330)
DO 60 IY=1,NY
60 WRITE (6,350) (VY(IX,IY),IX=1,NX)
C      ACTIVATE NEXT 3 LINES TO PRINT BOUNDARY VELOCITIES
C      WRITE (6,340)
C      DO 70 IY=1,NY
C      70 WRITE (6,350) (VYBDY(IX,IY),IX=1,NX)
C      ---WRITE VELOCITIES TO FILE UNIT 7---
80 IF (NPNCHV.EQ.0) GO TO 110
CTS IF (NPNCHV.EQ.-2.AND.(N.EQ.NTIM.OR.IPRNT.EQ.1)) GO TO 90
CTS IF (NPNCHV.EQ.-1.AND.N.EQ.1) GO TO 90
CTS IF (MOD(N,NPNCHV).EQ.0) GO TO 90
IF(NPNCHV.EQ.-1.AND.(N.EQ.NTIM)) GO TO 90
GO TO 110
90 IF (ISOLV.EQ.0) THEN
DO 92 IY=2,NNY
DO 92 IX=2,NNX
IF (THCK(IX,IY).EQ.0.0) GO TO 92
VX(IX,IY)=VX(IX,IY)/THCK(IX,IY)
VY(IX,IY)=VY(IX,IY)/THCK(IX,IY)
C      ACTIVATE NEXT 2 LINES IF BOUNDARY VELOCITIES PRINTED
C      VXBDY(IX,IY)=2.0*VXBDY(IX,IY)/(THCK(IX,IY)+THCK(IX+1,IY))
C      VYBDY(IX,IY)=2.0*VYBDY(IX,IY)/(THCK(IX,IY)+THCK(IX,IY+1))
92 CONTINUE
ISOLV=-1
END IF
CTS WRITE (7,510) NX,NY,XDEL,YDEL,VMAX,VMAX
CTS DO 100 IY=1,NY
CTS WRITE (7,520) (VX(IX,IY),IX=1,NX)
CTS 100 WRITE (7,520) (VY(IX,IY),IX=1,NX)
C      SAVE VELOCITY*THICKNESS*POROSITY
110 IF (ISOLV.EQ.0) GO TO 240
DO 112 IY=2,NNY
DO 112 IX=2,NNX
IF (THCK(IX,IY).EQ.0.0) GO TO 112
VX(IX,IY)=VX(IX,IY)*THCK(IX,IY)
VY(IX,IY)=VY(IX,IY)*THCK(IX,IY)
C      ACTIVATE NEXT 2 LINES IF BOUNDARY VELOCITIES PRINTED
C      VXBDY(IX,IY)=VXBDY(IX,IY)*0.5*(THCK(IX,IY)+THCK(IX+1,IY))
C      VYBDY(IX,IY)=VYBDY(IX,IY)*0.5*(THCK(IX,IY)+THCK(IX,IY+1))
112 CONTINUE
IF (ISOLV.NE.1) GO TO 240
C      *****
C      ---COMPUTE NEXT TIME STEP---
WRITE (6,390)
WRITE (6,410) VMXBD,VMYBD
IF (IREACT.LE.0) GO TO 115
VMXBD=VMXBD/(RF*RF2MIN)
VMYBD=VMYBD/(RF*RF2MIN)
WRITE (6,394) VMXBD,VMYBD
115 TDELXB=CELDIS*XDEL/VMXBD

```

```

E 750
E 761
E 771
E 781
E 785
E 790
E 792
E 793A
E 793B
E 793C
E 794A
E 794B
E 795A
E 795B
E 795C
E 796
E 797
E 798
E 801
E 810
E 820
E 830
E 839
E 840
E 850
E 860
E 870
E 880
E 890
E 900
E 909
E 910
E 920
E 930
E 941
E 950
E 961
E 971
E 975
E 980
E 982
E 983A
E 983B
E 984
E 985A
E 985B
E 986A
E 986B
E 986C
E 987
E 988
E 989
E 991
E1000
E1010
E1020
E1021
E1022A
E1022B
E1023
E1024
E1025
E1026
E1027A
E1027B
E1027C
E1028
E1029
E1030
E1040
E1051
E1070
E1072R
E1077R
E1078R
E1079R
E1082R

```

```

TDELYB=CELDIS*YDEL/VMYBD
ITCD=0
IF (TDELYB.LT.TDELXB) ITCD=1
TIMV=AMIN1(TDELXB,TDELYB)
IF (AMAX1(VMXBD,VMYBD).LE.1.0E-10) WRITE(6,570)
WRITE (6,310) TMV,TIMV
IF (TMV.LT.TIMV) GO TO 120
LIM=-1
GO TO 130
120 TIMV=TMV
LIM=1
130 NTIMV=TIM(N)/TIMV
NMOV=NTIMV+1
WRITE (6,420) TIMV,NTIMV,NMOV
TIMV=TIM(N)/NMOV
WRITE (6,370) TIM(N)
WRITE (6,380) TIMV
C
IF (BETA.EQ.0.0) GO TO 200
C
*****
C
---COMPUTE DISPERSION COEFFICIENTS---
ALPHA=BETA
ALNG=ALPHA
TRAN=DLTRAT*ALPHA
XX2=XDEL*XDEL
YY2=YDEL*YDEL
XY2=4.0*XDEL*YDEL
DO 150 IX=2,MMX
DO 150 IY=2,MMY
IF (THCK(IX,IY).EQ.0.0) GO TO 150
JX=IX-MX+1
JY=IY-MY+1
IF (JX.LT.1.OR.JY.LT.1) GO TO 150
VXE=VXBDY(IX,IY)
VYS=VYBDY(IX,IY)
IF (THCK(IX+1,IY).EQ.0.0) GO TO 140
IF ((IX+1).GT.MMX) GO TO 140
C
---FORWARD COEFFICIENTS: X-DIRECTION---
VYE=(VYBDY(IX,IY-1)+VYBDY(IX+1,IY-1)+VYS+VYBDY(IX+1,IY))/4.0
VXE2=VXE*VXE
VYE2=VYE*VYE
VMGE=SQRT(VXE2+VYE2)
IF (VMGE.LT.1.0E-20) GO TO 140
DALN=ALNG*VMGE
DTRN=TRAN*VMGE
VMGE2=VMGE*VMGE
C
---XX COEFFICIENT---
DISP(JX,JY,1)=(DALN*VXE2+DTRN*VYE2)/(VMGE2*XX2)
C
---XY COEFFICIENT---
IF ((IY-1).LT.MY.OR.(IY+1).GT.MMY) GO TO 140
DISP(JX,JY,3)=(DALN-DTRN)*VXE*VYE/(VMGE2*XY2)
C
---FORWARD COEFFICIENTS: Y-DIRECTION---
140 IF (THCK(IX,IY+1).EQ.0.0) GO TO 150
IF ((IY+1).GT.MMY) GO TO 150
VXS=(VXBDY(IX-1,IY)+VXE+VXBDY(IX-1,IY+1)+VXBDY(IX,IY+1))/4.0
VYS2=VYS*VYS
VXS2=VXS*VXS
VMGS=SQRT(VXS2+VYS2)
IF (VMGS.LT.1.0E-20) GO TO 150
DALN=ALNG*VMGS
DTRN=TRAN*VMGS
VMGS2=VMGS*VMGS
C
---YY COEFFICIENT---
DISP(JX,JY,2)=(DALN*VYS2+DTRN*VXS2)/(VMGS2*YY2)
C
---YX COEFFICIENT---
IF ((IX-1).LT.MX.OR.(IX+1).GT.MMX) GO TO 150
DISP(JX,JY,4)=(DALN-DTRN)*VXS*VYS/(VMGS2*XY2)
150 CONTINUE
C
*****
C
---ADJUST CROSS-PRODUCT TERMS FOR ZERO THICKNESS---
DO 160 IX=2,MMX
DO 160 IY=2,MMY
JX=IX-MX+1
JY=IY-MY+1
IF (JX.LT.1.OR.JY.LT.1) GO TO 160
IF (THCK(IX,IY+1).EQ.0.0.OR.THCK(IX+1,IY+1).EQ.0.0.OR.THCK(IX,IY-1)
1) .EQ.0.0.OR.THCK(IX+1,IY-1).EQ.0.0) DISP(JX,JY,3)=0.0
IF (THCK(IX+1,IY).EQ.0.0.OR.THCK(IX+1,IY+1).EQ.0.0.OR.THCK(IX-1,IY

```

```

E1110
E1111
E1112
E1121
E1126
E1130
E1140
E1150
E1160
E1170
E1180
E1190
E1200
E1210
E1220
E1230
E1240
E1250
E1260
E1270
E1280
E1290
E1300
E1310
E1320
E1330
E1340
SE1351
SE1361
E1370
SE1375
SE1376
SE1377
E1380
E1390
E1400
SE1405
E1410
E1420
E1430
E1440
E1450
E1460
E1470
E1480
E1490
E1500
SE1511
E1520
SE1525
SE1531
E1540
E1550
SE1555
E1560
E1570
E1580
E1590
E1600
E1610
E1620
E1630
E1640
SE1651
E1660
SE1665
SE1671
E1680
E1690
E1700
SE1711
SE1721
SE1725
SE1726
SE1727
E1730
SE1741
E1750

```

	1).EQ.0.0.OR.THCK(IX-1,IY+1).EQ.0.0) DISP(JX,JY,4)=0.0	SE1761
160	CONTINUE	E1770
C	*****	E1780
C	---CHECK FOR STABILITY OF EXPLICIT METHOD---	E1790
	TIMDIS=0.0	E1800
	DO 170 IX=1,NMX	SE1811
	DO 170 IY=1,NMY	SE1821
	JX=IX+MX-1	SE1822
	JY=IY+MY-1	SE1823
	IF (THCK(JX,JY).LE.0.0) GO TO 170	SE1824
	IF (IX.EQ.1) THEN	E1825
	DISPX=DISP(IX,IY,1)	E1826
	ELSE	E1827
	DISPX=AMAX1(DISP(IX,IY,1),DISP(IX-1,IY,1))	E1828
	END IF	E1832
	IF (IY.EQ.1) THEN	E1833
	DISPY=DISP(IX,IY,2)	E1834
	ELSE	E1835
	DISPY=AMAX1(DISP(IX,IY,2),DISP(IX,IY-1,2))	E1836
	END IF	E1837
	TDCO=(DISPX+DISPY)/THCK(JX,JY)	SE1838
	IF (TDCO.GT.TIMDIS) TIMDIS=TDCO	E1839
170	CONTINUE	E1841
	TIMDC=0.5*RF*RF2MIN/TIMDIS	E1852R
	WRITE (6,440) TIMDC	E1860
	NTIMD=TIM(N)/TIMDC	E1870
	NDISP=NTIMD+1	E1880
	IF (NDISP.LE.NMOV) GO TO 180	E1890
	NMOV=NDISP	E1900
	TIMV=TIM(N)/NMOV	E1910
	LIM=0	E1920
180	WRITE (6,430) TIMV,NTIMD,NMOV	E1930
C	*****	E2040
200	IF (NMOV.EQ.1) GO TO 235	E2052
	IF (LIM) 210,220,230	E2054
210	WRITE (6,530)	E2060
	IF (ITCD.GT.0) THEN	E2062
	MJ=MAXVYJ+1	E2063
	WRITE (6,534) MAXVYI,MAXVYJ,MAXVYI,MJ	E2064
	ELSE	E2065
	MI=MAXVXI+1	E2066
	WRITE (6,535) MAXVXI,MAXVXJ,MI,MAXVXJ	E2067
	END IF	E2068
	GO TO 240	E2070
220	WRITE (6,540)	E2080
	GO TO 240	E2090
230	WRITE (6,550)	E2100
	WRITE (6,560) MAXX,MAXY	E2102
	GO TO 240	E2104
235	WRITE (6,580)	E2106
C	*****	E2110
C	---PRINT DISPERSION EQUATION COEFFICIENTS---	E2120
240	IF (NPNTD.EQ.0) GO TO 300	E2130
	IF (NPNTD.EQ.2) GO TO 250	E2140
	IF (NPNTD.EQ.1.AND.N.EQ.1) GO TO 250	E2150
	GO TO 300	E2160
250	WRITE (6,450)	E2170
	WRITE (6,460)	E2180
	DO 260 IY=1,NMY	SE2191
260	WRITE (6,500) (DISP(IX,IY,1),IX=1,NMX)	SE2201
	WRITE (6,470)	E2210
	DO 270 IY=1,NMY	SE2221
270	WRITE (6,500) (DISP(IX,IY,2),IX=1,NMX)	SE2231
	WRITE (6,480)	E2240
	DO 280 IY=1,NMY	SE2251
280	WRITE (6,500) (DISP(IX,IY,3),IX=1,NMX)	SE2261
	WRITE (6,490)	E2270
	DO 290 IY=1,NMY	SE2281
290	WRITE (6,500) (DISP(IX,IY,4),IX=1,NMX)	SE2291
C	*****	E2300
300	RETURN	E2310
C	*****	E2320
C		E2330
C		E2340
C		E2350
310	FORMAT (1H0,19H TMV (MAX. INJ.) = ,G12.5/20H TIMV (CELDIS) = ,G	E2361R
	112.5)	E2370
320	FORMAT (1H1,12HX VELOCITIES)	E2380

330	FORMAT (1H ,25X,8HAT NODES/)	E2390
C	ACTIVATE NEXT LINE IF BOUNDARY VELOCITIES PRINTED	E2399
C 340	FORMAT (1H0,25X,41HON BOUNDARIES (USING INTERFACE THICKNESS)/)	E2401
350	FORMAT (1H ,1P10E12.3)	E2411
360	FORMAT (1H1,12HY VELOCITIES)	E2420
370	FORMAT (3H ,11HTIM (N) = ,1G12.5)	E2430
380	FORMAT (3H ,11HTIMEVELO = ,1G12.5)	E2440
390	FORMAT (1H1,10X,29HSTABILITY CRITERIA --- M.O.C./)	E2450
394	FORMAT (1H0,5X,46HMAXIMUM EFFECTIVE SOLUTE VELOCITIES: X-VEL = ,	E2453R
1	1PE9.2,5X,8HY-VEL = ,1PE9.2)	E2454R
410	FORMAT (1H0,5X,35HMAXIMUM FLUID VELOCITIES: X-VEL = ,1PE9.2,5X,	E2471
1	8HY-VEL = ,1PE9.2)	E2472
420	FORMAT (1H0,8H TIMV = ,1PE9.2,5X,8HNTIMV = ,I5,5X,7HNMOV = ,I5/)	E2480
430	FORMAT (1H0,8H TIMV = ,1PE9.2,5X,8HNTIMD = ,I5,5X,7HNMOV = ,I5)	E2490
440	FORMAT (3H ,11HTIMEDISP = ,1E12.5)	E2500
450	FORMAT (1H1,32HDISPERSION EQUATION COEFFICIENTS,10X,33H=(D-IJ)*(B)	E2511
1*(POROS)/(GRID FACTOR))	E2521	
460	FORMAT (1H0,35X,14HXX COEFFICIENT/)	E2531
470	FORMAT (1H0,35X,14HYY COEFFICIENT/)	E2541
480	FORMAT (1H0,35X,14HXY COEFFICIENT/)	E2551
490	FORMAT (1H0,35X,14HYX COEFFICIENT/)	E2561
500	FORMAT (1H ,1P10E11.2)	E2571
510	FORMAT (2I4,2F10.1,2F10.7)	E2580
520	FORMAT (8F10.7)	E2590
530	FORMAT (1H0,10X,42HTHE LIMITING STABILITY CRITERION IS CELDIS)	E2600
534	FORMAT (1H ,4X,52HMAX. Y-VEL. IS CONSTRAINT AND OCCURS BETWEEN NOD	E2602
1ES (,I2,1H,,I2,7H) AND (,I2,1H,,I2,1H))	E2603	
535	FORMAT (1H ,4X,52HMAX. X-VEL. IS CONSTRAINT AND OCCURS BETWEEN NOD	E2604
1ES (,I2,1H,,I2,7H) AND (,I2,1H,,I2,1H))	E2605	
540	FORMAT (1H0,10X,40HTHE LIMITING STABILITY CRITERION IS BETA)	E2610
550	FORMAT (1H0,10X,58HTHE LIMITING STABILITY CRITERION IS MAXIMUM INJ	E2620
1ECTION RATE)	E2630	
560	FORMAT (1H ,15X,35HMAX. INJECTION OCCURS AT CELL IX = ,I3,7H IY =	E2635
1 ,I3)	E2636	
570	FORMAT (1H0,5X,47H*** WARNING *** DECREASE CRITERIA IN E 230-260)	E2637
580	FORMAT (1H0,10X,63H*TIME INCREMENT FOR SOLUTE TRANSPORT EQUALS TIM	E2638
1E STEP FOR FLOW*)	E2639	
END	E2640-	











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