

DESIGN CALCULATION COVER SHEET								
Project	Detailed Design on Port Reactivation Project in La Union Province.			Project Code	JC1N004			
Section	BUILDING WORKS			Calc. File No.				
Sub-Section	CONTAINER GATE			Calc. Index No.				
Subject:								
STRUCTURAL DESIGN								
Calculation Objective:								
<p>The objective of the calculation is to provide a safe structure for the occupation of the building, by the use of the Republic of El Salvador and American design standards.</p>								
References, Calculation Notes and Comments								
<p>The Structural Analysis has been made using the program: "STAAD-III rev 21.1W, RESEARCH ENGINEERS, Inc.". The analysis of the structure considers only the concrete frames to resist the lateral forces, not considering the walls in the model.</p> <p>One model for the structure has been constructed:</p> <p style="padding-left: 40px;">1- For the calculation of the Seismic and Dead & Live load.</p> <p>The Key for the STAAD-III rev 21.1W program is attached for future convinience.</p> <p>All the design has been made by calculations sheet created for the project in Microsoft Excel, and based in the following bibliography:</p> <ol style="list-style-type: none"> 1. Building Code Requirements for Structural Concrete (318M-99), American Concrete Institute (ACI). 2. Technical Specification for Seismic Design, Ministry of Public Works, El Salvador, 2001. 3. AISC, American Institute of Steel Construction, ninth Edition, 1989. 4. Technical Specification for Wind Design, Ministry of Public Works, El Salvador, 1997. 5. UBC, Uniform Building Code, Volume 2: Structural Engineering Design Provisions, 1997. 								
Rev	Prepared		No. of Pages	Checked		Reviewed		Superseded by Calc No.
	by	Date		by	Date	by	Date	
O	H. WATANABE	Jul-02	78	A. MORIOKA	Jul-02	<i>WJ</i>	11 July 02	
A				<i>[Signature]</i>				
B								
C								

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gate (cargo,container)					
	room	material	thickness	density	(kg/m2) weight
RF	Roof (metal)	metal roof			15
		purlin			15
		sub-beam			15
		beam			30
					75
2F	office	finish	30		60
		slab syste ceiling	200		345 precast prestress slab, 20 include top concrete t=50
					425
2F	Roof	finish			20
		concrete sl	150		360
		ceiling			20
					400
2F	Bridge wal	c pl			30
		porin			20
					50
1F	sidewalk	finish	30		60
		slab	120	2.4	288
					348
1F	office	finish	30		60
		slab	120	2.4	288
					348
1F	Pit	slab	250	2.4	600
					600
C.B	t=200mm				293 kg/m2
	t=150mm				226 kg/m2

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gate					
Floor	Room	Dead Load	Live Load	Total Load	Notes
			20	95	*
RF	roof	75	0	75	
2F	office	425	250	675	*
2F	roof	400	100	500	
2F	bridge wal	50	180	230	
1F	office	348	60	110	
1F	sidewalk	348	250	598	
1F	pit	600	180	528	
			350	698	
			150	498	
			2000	2600	
			1800	2400	

* The selfweight for the Columns & Beams calculated by the MultiFrame structural Analysis Program.

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Dead Load

X direction model position		unit weight	area,length	load
roof	roof	30 kg/m2 (exclude beam and sub beam self-weight)	3 m	0.09 t/m
roof top	roof	45 kg/m2 (exclude beam self-weight)	11.64 m2	0.524 t
roof bottom 1	roof	45 kg/m2	11.64 m2	0.524 t
roof bottom 2	RC beam	0.47 t/m	3 m	1.41 t
2nd floor 1 (7/8 axis)	CB (200)	0.293 t/m2	1.75 m	0.513 t/m
	bridge walk	0.05 t/m2	0.5 m	0.025 t/m
				0.538 t/m
2nd floor 2 (B-7 axis)	CB (200)	0.293 t/m2	5.25 m	1.538 t
	slab	0.425 t/m2	5.325 m2	2.263 t
	B-10	0.47 t/m	3 m	1.41 t
	CB-10	0.22 t/m	1.3 m	0.286 t
	stairs	0.05 t/m2	2 m2	0.1 t
	bridge walk	0.05 t/m2	4.4875 m2	0.224 t
				5.822 t
2nd floor 3 (B-8 axis)	CB (200)	0.293 t/m2	5.25 m	1.538 t
	slab	0.425 t/m2	5.325 m2	2.263 t
	B-10	0.47 t/m	3 m	1.41 t
	RC beam	0.3 t/m	3 m	0.9 t
	bridge walk	0.05 t/m2	3 m2	0.15 t
	bridge walk	0.05 t/m2	4.4875 m2	0.224 t
				6.486 t
2nd floor 4 (B-9 axis)	CB-10	0.22 t/m	1.3 m	0.286 t
	bridge walk	0.05 t/m2	2.6125 m2	0.131 t
				0.416625 t
2nd floor 5 (B-2 axis)	RC beam	0.3 t/m	6 m	1.8 t
	bridge walk	0.05 t/m2	7.775 m2	0.38875 t
				2.18875 t
2nd floor 6 (B-3,4,5,6)	CB-10	0.22 t/m	1.3 m	0.286 t
	bridge walk	0.05 t/m2	9.4 m2	0.47 t
	stairs	0.05 t/m2	2 m2	0.1 t
				0.856 t

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Dead Load				
X direction model position		unit weight	area,length	load
1st floor 1 (B-1/2,8/9)	FB-1 pit	0.77 t/m 0.6 t/m2	6 m 12 m2	4.62 t <u>7.2 t</u> 11.820 t
1st floor 2 (B-3/4,4/5,5/6,6/7)	FB-2 side walk 2nd roof CB (200)	0.47 t/m 0.348 t/m2 0.4 t/m2 0.293 t/m2	6 m 3.6 m2 2.43 m2 17.57625 m2	2.82 t 1.2528 t 0.972 t 5.149841 t <u>10.19464 t</u>
1st floor 3 (B-1,9 axis)	FB-1 side walk	0.77 t/m 0.348 t/m2	6 m 6 m2	4.62 t <u>2.088 t</u> 6.708 t
1st floor 4 (B-2,3,7,8 axis)	FB-1 side walk	0.77 t/m 0.348 t/m2	6 m 7.56 m2	4.62 t <u>2.631 t</u> 7.251 t
1st floor 5 (B-4,5,6 axis)	FB-1 side walk	0.77 t/m 0.348 t/m2	6 m 7.2 m2	4.62 t <u>2.5056 t</u> 7.126 t

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Live Load				
X direction model position		unit weight	area,length	load
roof	roof	20 kg/m ²	3 m	0.06 t/m
roof top	roof	20 kg/m ²	11.64 m ²	0.233 t
roof bottom 1	roof	20 kg/m ²	11.64 m ²	0.233 t
2nd floor 1 (7/8 axis)	bridge walk	0.18 t/m ²	0.5 m	0.090 t/m
				0.090 t/m
2nd floor 2 (B-7 axis)	office	0.25 t/m ²	5.325 m ²	1.331 t
	stairs	0.18 t/m ²	2 m ²	0.36 t
	bridge walk	0.18 t/m ²	4.4875 m ²	0.808 t
				2.499 t
2nd floor 3 (B-8 axis)	slab	0.25 t/m ²	5.325 m ²	1.331 t
	bridge walk	0.18 t/m ²	3 m ²	0.54 t
	bridge walk	0.18 t/m ²	4.4875 m ²	0.808 t
				2.679 t
2nd floor 4 (B-9 axis)	bridge walk	0.18 t/m ²	2.6125 m ²	0.470 t
				0.47025 t
2nd floor 5 (B-2 axis)	bridge walk	0.18 t/m ²	7.775 m ²	1.3995 t
				1.3995 t
2nd floor 6 (B-3,4,5,6)	bridge walk	0.18 t/m ²	9.4 m ²	1.692 t
	stairs	0.18 t/m ²	2 m ²	0.36 t
				2.052 t

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Live Load				
X direction model position		unit weight	area,length	load
1st floor 1 (B-1/2,8/9)	pit	2 t/m2	12 m2	<div style="display: flex; justify-content: space-between;"> 24 t </div> 24.000 t
1st floor 2 (B-3/4,4/5,5/6,6/7)	side walk 2nd roof	0.35 t/m2 0.1 t/m2	3.6 m2 2.43 m2	<div style="display: flex; justify-content: space-between;"> 1.26 t </div> <div style="display: flex; justify-content: space-between;"> 0.243 t </div> 1.503 t
1st floor 3 (B-1,9 axis)	side walk	0.35 t/m2	6 m2	<div style="display: flex; justify-content: space-between;"> 2.100 t </div> 2.1 t
1st floor 4 (B-2,3,7,8 axis)	side walk	0.35 t/m2	7.56 m2	<div style="display: flex; justify-content: space-between;"> 2.646 t </div> 2.646 t
1st floor 5 (B-4,5,6 axis)	side walk	0.35 t/m2	7.2 m2	<div style="display: flex; justify-content: space-between;"> 2.52 t </div> 2.520 t

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SEISMIC FORCES

$$V = C_s W$$

$$C_s = (A I C_o / R) (T_o / T)^{2/3}$$

Coefficient of Acceleration, $A =$

Importance Factor, $I =$

Response Modification Factor, $R =$

Soil Conditions Factors

$C_o =$

$T_o =$

Period of the Structure, $T = C_t h_n^{3/4}$

Type of structure coefficient, $C_t =$

Structure height, $h_n =$

$T =$ 0.342 seg

$C_s =$ 0.145

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Dead Load							
	1	2	3	4	5	6	
RF	1.24	2	2	2.2	2.3	2.2	
2F	1.46	3.6	2.3	2.3	2.3	2.3	
	7	8	9				
RF	4.3	4.6	1.20				
2F	8.9	10.5	1.9				
Live Load							
	1	2	3	4	5	6	
RF	0.0						
2F	0.0	0.5	0.7	0.7	0.7	0.7	
	7	8	9				
RF							
2F	1.7	2.2	0.2				
Each floor weight for seismic							
hight	1	2	3	4	5	6	
7.85 RF	1.2	2.0	2.0	2.2	2.3	2.2	
5.45 2F	1.5	4.1	3.0	3.0	3.0	3.0	
wh=	17.7	37.9	31.9	33.6	34.4	33.6	
	7	8	9				
RF	4.3	4.6	1.2				
2F	10.6	12.7	2.1				
wh=	91.7	105.1	20.7				

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Total weight for seismic

	1	2	3	4	5	6
RF	1.2	2.0	2.0	2.2	2.3	2.2
2F	2.7	6.1	5.0	5.2	5.3	5.2
	7	8	9			
RF	4.3	4.6	1.2			
2F	14.9	17.3	3.3			

Total seismic load

	1	2	3	4	5	6
	0.4	0.9	0.7	0.8	0.8	0.8
	7	8	9			
	2.2	2.5	0.5			

Each seismic load

	1	2	3	4	5	6
RF	0.2	0.4	0.4	0.4	0.4	0.4
2F	0.2	0.5	0.4	0.4	0.4	0.4
	7	8	9			
RF	0.8	0.9	0.2			
2F	1.4	1.6	0.3			

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Dead Load				
Y direction model (6 Frame)				
position		unit weight	area,length	load
roof 1 (tip of B-2)	roof	45 kg/m2 (exclude beam self-weight)	11.64 m	0.5238 t
roof 2	roof	45 kg/m2 (exclude beam self-weight)	23.28 m2	1.048 t
2nd floor 1 (B axis)	bridge walk	0.05 t/m2	2.95625 m2	0.148 t
				0.148 t
2nd floor 2 (tip of CB-10)	bridge walk	0.05 t/m2	2.95625 m2	0.148 t
	stairs	0.05 t/m2	2 m2	0.100 t
	bridge walk	0.05 t/m2	2.5 m2	0.125 t
				0.373 t
2nd floor 3 (C axis)	CB-10	0.216 t/m	1.2 m	0.259 t
	bridge walk	0.05 t/m2	2.5 m2	0.125 t
				0.384 t
1st floor 1 (tip of CB)	wall	0.5 t/m2	3.3912 m2	1.696 t
	side walk	0.35 t/m2	4.2 m2	1.470 t
				3.166 t
1st floor 2 (A,D axis)	side walk	0.35 t/m2	4.20 m2	1.47 t
	office	0.35 t/m2	3.60 m2	1.26 t
	2nd roof	0.40 t/m2	4.25 m2	1.70 t
	CB	0.29 t/m2	33.52 m2	9.82 t
	FB-1	0.77 t/m	11.71 m2	9.00 t
				23.25 t

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Dead Load

Y direction model (6 Frame)

position		unit weight	area,length	load
1st floor 3 (A/B,C/D)	office	0.35 t/m ²	1.2 m	0.42 t/m
1st floor 4 (B/C)	side walk	0.35 t/m ²	1.2 m	0.42 t/m
1st floor 5 (B,C axis)	side walk	0.35 t/m ²	7.2 m ²	2.52 t
	2nd roof	0.4 t/m ²	4.25 m ²	1.70 t
	CB	0.29 t/m ²	33.52 m ²	9.82 t
	FB-1	0.77 t/m	17.9125 m	13.76 t
				27.798 t

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Live Load

Y direction model (6 Frame)

position		unit weight	area,length	load
roof 1 (tip of B-2)	roof (exclude beam self-weight)	20 kg/m ²	11.64 m	0.2328 t
roof 2	roof (exclude beam self-weight)	20 kg/m ²	23.28 m ²	0.466 t
2nd floor 1 (B axis)	bridge walk	0.18 t/m ²	2.95625 m ²	0.532 t
				0.532 t
2nd floor 2 (tip of CB-10)	bridge walk	0.18 t/m ²	2.95625 m ²	0.532 t
	stairs	0.18 t/m ²	2 m ²	0.360 t
	bridge walk	0.18 t/m ²	2.5 m ²	0.45 t
				1.342 t
2nd floor 3 (C axis)	bridge walk	0.18 t/m ²	2.5 m ²	0.450 t
				0.450 t
1st floor 1 (tip of CB)	side walk	0.35 t/m ²	4.2 m ²	1.470 t
				1.470 t
1st floor 2 (A,D axis)	side walk	0.35 t/m ²	4.20 m ²	1.47 t
	office	0.25 t/m ²	3.60 m ²	0.90 t
	2nd roof	0.10 t/m ²	4.25 m ²	0.43 t
				2.80 t

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Live Load

Y direction model (6 Frame)

position	unit weight	area,length	load
1st floor 3 (A/B,C/D)	office 0.25 t/m ²	1.2 m	0.3 t/m
1st floor 4 (B/C)	side walk 0.35 t/m ²	1.2 m	0.42 t/m
1st floor 5 (B,C axis)	side walk 0.35 t/m ²	7.2 m ²	2.52 t
	2nd roof 0.1 t/m ²	4.25 m ²	0.43 t
			2.945 t

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Dead Load				
	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
RF	2.63	1.45	1.45	2.63
2F	1.47	2.25	1.85	1.47
Live Load				
	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
RF	0.84	0.33	0.34	0.84
2F	0	3.58	0.45	0
Each floor weight for seismic				
height	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
7.85 RF	3.5	1.8	1.8	3.5
5.45 2F	1.5	5.8	2.3	1.5
wh	35.25	45.75	26.59	35.25
Total weight for seismic				
	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
RF	3.5	1.8	1.8	3.5
2F	4.9	7.6	4.1	4.9
Total seismic load				
	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
	0.7	1.1	0.6	0.7
Each seismic load				
	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
RF	0.6	0.3	0.3	0.6
2F	0.2	0.8	0.3	0.2

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Dead Load

Y direction model (7 Frame)

position		unit weight	area,length	load
roof 1 (tip of B-2)	roof (exclude beam self-weight)	45 kg/m2	11.64 m	0.52 t
roof 2	roof (exclude beam self-weight)	45 kg/m2	23.28 m2	1.05 t
roof bottom (A,B axis)	B-5	0.468 t/m	1.775 m	0.83 t
2nd floor 1 (A/B)	CB (200)	0.293 t/m2	1.75 m	0.513 t/m
	office	0.425 t/m2	1.775 m	0.754 t/m
				1.267 t/m
2nd floor 2 (B axis)	bridge walk	0.05 t/m2	2.24375 m2	0.112 t
	CB (200)	0.293 t/m2	3.150625 m2	0.923133 t
	B-10	0.468 t/m	1.775 m	0.8307 t
				1.866 t
2nd floor 3 (tip of CB-10)	stairs	0.05 t/m	2 m	0.100 t
	bridge walk	0.05 t/m2	2.24375 m2	0.112 t
				0.212 t
1st floor 1 (tip of CB)	wall	0.5 t/m2	0.9 m	0.450 t/m
	side walk	0.35 t/m2	1.775 m	0.621 t/m
				1.071 t/m
1st floor 2 (A/B)	office	0.35 t/m2		0.35 t/m2
	CB	0.29 t/m2	5.40 m	1.58 t/m
				1.58 t/m
1st floor 3 (A axis)	office	0.35 t/m2	1.58 m2	0.55 t
	FB-1	0.77 t/m	4.49 m	3.45 t
	CB (200)	0.29 t/m2	8.52 m2	2.50 t
				6.49 t

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Dead Load					
Y direction model (7 Frame)					
position		unit weight	area,length	load	
1st floor 4 (B axis)	office	0.35 t/m ²	1.58 m ²	0.55 t	
	side walk	0.35 t/m ²	1.58 m ²	0.55 t	
	FB-1	0.77 t/m	4.49 m	3.45 t	
	CB (200)	0.29 t/m ²	8.52 m ²	2.50 t	
			-----	7.05 t	
1st floor 5 (B/C, C/D)	side walk	0.35 t/m ²		-----	0.35 t/m ²
1st floor 6 (C axis)	side walk	0.35 t/m ²	3.15 m ²	1.10 t	
	FB-1	0.77 t/m	4.49 m	3.45 t	
				-----	4.55 t
1st floor 7 (D axis)	side walk	0.35 t/m ²	1.58 m ²	0.55 t	
	FB-1	0.77 t/m	4.49 m	3.45 t	
				-----	4.00 t
2nd floor 4 (A axis)	CB (200)	0.29 t/m ²	3.15 m ²	0.92 t	
	B-10	0.47 t/m	1.78 m	0.83 t	
				-----	1.75 t

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Live Load

Y direction model (7 Frame)

position	unit weight	area,length	load
roof 1 (tip of B-2)	roof (exclude beam self-weight)	20 kg/m2 11.64 m	0.2328 t
roof 2	roof (exclude beam self-weight)	20 kg/m2 23.28 m2	0.466 t
2nd floor 1 (A/B)	office	0.25 t/m2 1.775 m	0.444 t/m
			0.444 t/m
2nd floor 2 (B axis)	bridge walk	0.18 t/m2 2.24375 m2	0.404 t
			0.404 t
2nd floor 3 (tip of CB-10)	stairs bridge walk	0.18 t/m 0.18 t/m2 2 m 2.24375 m2	0.360 t 0.404 t
			0.764 t
1st floor 1 (tip of CB)	side walk	0.18 t/m2 1.775 m	0.320 t/m
			0.320 t/m
1st floor 2 (A/B)	office	0.25 t/m2	0.25 t/m2
1st floor 3 (A axis)	office	0.25 t/m2 1.58 m2	0.39 t
			0.39 t

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
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Live Load					
Y direction model (7 Frame)					
position		unit weight	area,length	load	
1st floor 4 (B axis)	office	0.25 t/m2	1.58 m2	0.39 t	
	side walk	0.35 t/m2	1.58 m2	0.55 t	
				0.95 t	
1st floor 5 (B/C, C/D)	side walk	0.35 t/m2		0.35 t/m2	
	side walk	0.35 t/m2	3.15 m2	1.10 t	
				1.10 t	
1st floor 7 (D axis)	side walk	0.35 t/m2	1.58 m2	0.55 t	
					0.55 t

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.	Prepared by	H.WATANABE
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Dead Load

	A	B	C	D
RF	5.38	5.11	2.67	2.96
2F	8.65	9.41	1.42	1.42

Live Load

	A	B	C	D
RF	0.98	0.89	0.87	1
2F	1.2	2.6	0	0

Each floor weight for seismic

height	A	B	C	D
7.85 RF	6.4	6.0	3.5	4.0
5.45 2F	9.9	12.0	1.4	1.4
wh	103.61	112.55	35.53	38.83

Total weight for seismic

	A	B	C	D
RF	6.4	6.0	3.5	4.0
2F	16.2	18.0	5.0	5.4

Total seismic load

	A	B	C	D
	2.4	2.6	0.7	0.8

Each seismic load

	A	B	C	D
RF	1.1	1.1	0.6	0.6
2F	1.2	1.5	0.2	0.2

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
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Dead Load				
Y direction model (8 Frame)				
position		unit weight	area, length	load
roof 1 (tip of B-2)	roof	45 kg/m ² (exclude beam self-weight)	11.64 m	0.52 t
roof 2	roof	45 kg/m ² (exclude beam self-weight)	23.28 m ²	1.05 t
roof bottom (A,B axis)	B-5	0.468 t/m	1.775 m	0.83 t
2nd floor 1 (A/B)	CB (200) office	0.293 t/m ² 0.425 t/m ²	1.75 m 1.775 m	0.513 t/m 0.754 t/m
				1.267 t/m
2nd floor 2 (B axis)	bridge walk CB (200) B-10	0.05 t/m ² 0.293 t/m ² 0.468 t/m	2.24375 m ² 3.150625 m ² 1.775 m	0.112 t 0.923133 t 0.8307 t
				1.866 t
2nd floor 3 (B/C)	bridge walk bridge walk	0.05 t/m ² 0.05 t/m ²	3.69375 m ² 0.5 m	0.185 t 0.025 t/m
2nd floor 4 (C axis)	bridge walk CB-10	0.05 t/m ² 0.216 t/m	3 m ² 1.3 m	0.150 t 0.281 t
				0.431 t
2nd floor 5 (D axis)	bridge walk CB-10	0.05 t/m ² 0.216 t/m	1.5 m ² 1.3 m	0.075 t 0.281 t
				0.36 t

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Dead Load				
Y direction model (8 Frame)				
position		unit weight	area,length	load
1st floor 1 (tip of CB)	wall	0.5 t/m2	0.9 m	0.450 t/m
	side walk	0.35 t/m2	1.775 m	0.621 t/m
				1.071 t/m
1st floor 2 (A/B)	office	0.35 t/m2		0.35 t/m2
	CB	0.29 t/m2	5.40 m	1.58 t/m
				1.58 t/m
1st floor 3 (A axis)	office	0.35 t/m2	1.58 m2	0.55 t
	FB-1	0.77 t/m	4.49 m	3.45 t
	CB (200)	0.29 t/m2	8.52 m2	2.50 t
				6.49 t
1st floor 4 (B axis)	office	0.35 t/m2	1.58 m2	0.55 t
	side walk	0.35 t/m2	1.58 m2	0.55 t
	FB-1	0.77 t/m	4.49 m	3.45 t
	CB (200)	0.29 t/m2	8.52 m2	2.50 t
				7.05 t
1st floor 5 (B/C, C/D)	side walk	0.35 t/m2		0.35 t/m2
1st floor 6 (C axis)	side walk	0.35 t/m2	3.15 m2	1.10 t
	FB-1	0.77 t/m	4.49 m	3.45 t
				4.55 t
1st floor 7 (D axis)	side walk	0.35 t/m2	1.58 m2	0.55 t
	FB-1	0.77 t/m	4.49 m	3.45 t
				4.00 t
2nd floor 4 (A axis)	CB (200)	0.29 t/m2	3.15 m2	0.92
	B-10	0.47 t/m	1.78 m	0.83
				1.75

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Live Load				
Y direction model (8 Frame)				
position		unit weight	area,length	load
roof 1 (tip of B-2)	roof	20 kg/m ²	11.64 m	0.23 t
roof 2	roof	20 kg/m ²	23.28 m ²	0.47 t
2nd floor 1 (A/B)	office	0.25 t/m ²	1.775 m	0.444 t/m
				<u>0.444 t/m</u>
2nd floor 2 (B axis)	bridge walk	0.18 t/m ²	2.24375 m ²	0.404 t
				<u>0.404 t</u>
2nd floor 3 (B/C)	bridge walk	0.18 t/m ²	3.69375 m ²	0.665 t
	bridge walk	0.05 t/m ²	0.5 m	0.025 t/m
2nd floor 4 (C axis)	bridge walk	0.18 t/m ²	3 m ²	0.540 t
				<u>0.540 t</u>
2nd floor 5 (D axis)	bridge walk	0.18 t/m ²	1.5 m ²	0.270 t
				<u>0.27 t</u>
2nd floor 6 (C/D)	bridge walk	0.05 t/m ²	0.5 m	0.025 t/m
				<u>0.025 t/m</u>

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Live Load

Y direction model (8 Frame)

position	unit weight	area,length	load
1st floor 1 (along of CB)	side walk 0.35 t/m2	1.775 m	0.621 t/m <hr/> 0.621 t/m
1st floor 2 (A/B)	office 25.00 t/m2		<hr/> 25.00 t/m2
1st floor 3 (A axis)	office 0.25 t/m2	1.58 m2	0.39 t <hr/> 0.39 t
1st floor 4 (B axis)	office side walk 0.25 t/m2 0.35 t/m2	1.58 m2 1.58 m2	0.39 t 0.55 t <hr/> 0.95 t
1st floor 5 (B/C, C/D)	side walk 0.35 t/m2		<hr/> 0.35 t/m2
1st floor 6 (C axis)	side walk 0.35 t/m2	3.15 m2	1.10 t <hr/> 1.10 t
1st floor 7 (D axis)	side walk 0.35 t/m2	1.58 m2	0.55 t <hr/> 0.55 t

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Dead Load				
	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
RF	5.4	5.09	2.67	2.96
2F	8.57	10.15	3.6	2.57
Live Load				
	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
RF	1	0.88	0.87	1
2F	1.25	2.5	0.75	0.36
Each floor weight for seismic				
hight	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
7.85 RF	6.4	6.0	3.5	4.0
5.45 2F	9.8	12.7	4.4	2.9
wh	103.76	115.81	51.50	47.05
Total weight for seismic				
	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
RF	6.4	6.0	3.5	4.0
2F	16.2	18.6	7.9	6.9
Total seismic load				
	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
	2.4	2.7	1.1	1.0
Each seismic load				
	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
RF	1.1	1.1	0.6	0.7
2F	1.2	1.6	0.5	0.3

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Reaction of each point

	1	2	3	4	5	6	7	8	9
A	24.1	23.0	35.8	39.0	39.0	39.0	35.8	38.4	24.1
	26.2	11.3	3.8	6.4	6.4	6.4	3.8	11.8	26.2
	50.3	34.3	39.6	45.4	45.4	45.4	39.6	50.2	50.3
B	24.0	30.6	16.5	36.6	38.4	37.7	25.6	40.6	24.1
	26.0	30.8	3.9	8.6	8.4	8.6	4.2	32.7	26.2
	50.0	61.4	20.4	45.2	46.8	46.3	29.8	73.3	50.3
C	24.1	40.6	25.6	37.7	38.4	36.6	16.5	30.6	24.0
	26.2	32.7	4.2	8.6	8.4	8.6	3.9	30.8	26.0
	50.3	73.3	29.8	46.3	46.8	45.2	20.4	61.4	50.0
D	24.1	38.4	35.8	39.1	39.1	39.1	19.3	23.0	24.1
	26.2	11.8	3.8	7.0	7.0	7.0	3.1	11.3	26.2
	50.3	50.2	39.6	46.1	46.1	46.1	22.4	34.3	50.3

upper line DL
 middle line LL
 lower line TL=DL+LL

Total dead load = 1128.4 ton

Seismic load = 164.03 ton

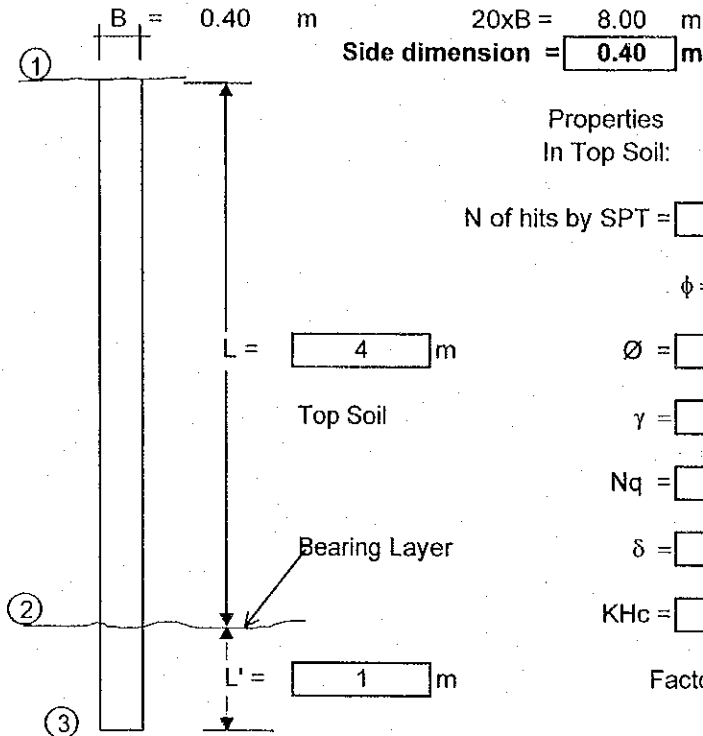
PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.	Prepared by	H.WATANABE
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Number of pile									
	1	2	3	4	5	6	7	8	9
A	1-40	1-40	1-40	1-40	1-40	1-40	1-40	1-40	1-40
B	1-40	1-45	1-40	1-40	1-40	1-40	1-40	2-40	1-40
C	1-40	2-40	1-40	1-40	1-40	1-40	1-40	1-45	1-40
D	1-40	1-40	1-40	1-40	1-40	1-40	1-40	1-40	1-40

Pile bearing strength	
diameter (cm)	strength (t)
40	58.4
45	74.0

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BEARING CAPACITY OF SQUARE DRIVEN CONCRETE PILES



Properties In Top Soil:	Properties In Bearing Stratum:
N of hits by SPT = <input type="text" value="8"/> N	<input type="text" value="50"/> N
$\phi = \sqrt{12N + 20}$	
$\phi = 29.80^\circ$	<input type="text" value="42.39"/> °
$\gamma = 1.430 \text{ ton/m}^3$	<input type="text" value="1.840"/> ton/m ³
$N_q = 21$	<input type="text" value="145"/>
$\delta = 22.35^\circ$	<input type="text" value="31.79"/> °
$KHc = 1$	<input type="text" value="1"/>
Factor of safety (F.S.) = <input type="text" value="3"/>	

Pressure due to soil:

Qult = Qt + Qf

- Tip Resistance (Qt)

$Q_p = P_t \times N_q \times A_t$ $P_t = P_3 = 7.56 \text{ ton/m}^2$

$P_1 = 0.00 \text{ ton/m}^2$
 $P_2 = 5.72 \text{ ton/m}^2$
 $P_3 = 7.56 \text{ ton/m}^2$

Pile Area = 0.160 m^2 **Qp = 175.39 ton**

- Friction Capacity (Qf) Consider Friction ? Y/N

$Q_f = \sum(KHc) \times P_o \times \text{TAN}(\delta) \times S$

$S_1 = 2BLD$	$S_1 = 3.20 \text{ m}^2$	$P_{o1} = (P_1 + P_2)/2$
$S_2 = 2BL'D$	$S_2 = 0.80 \text{ m}^2$	$P_{o2} = (P_2 + P_3)/2$

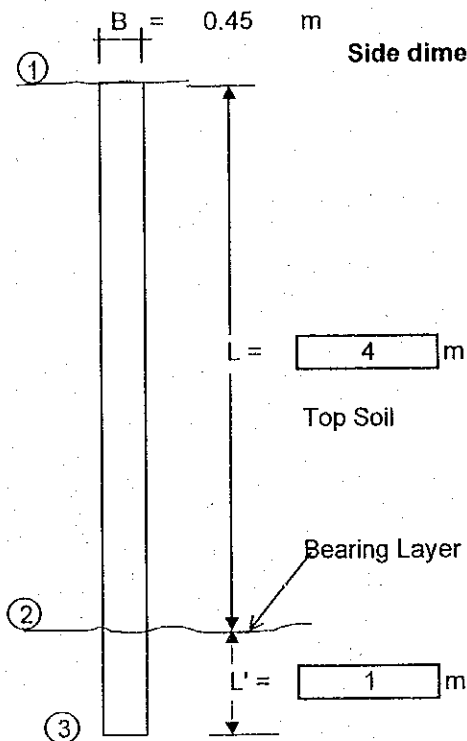
$P_{o1} = 2.860 \text{ ton/m}^2$ $P_{o2} = 6.640 \text{ ton/m}^2$ **Qf = 0.00 ton**

Qult = Qt + Qf Qult = 175.39 ton

$Q_{adm} = Q_{ult} / F.S.$ **Qadm = 58.46 ton**

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BEARING CAPACITY OF SQUARE DRIVEN CONCRETE PILES



Properties In Top Soil:	Properties In Bearing Stratum:
N of hits by SPT = <input type="text" value="8"/> N	<input type="text" value="50"/> N
$\phi = \sqrt{12N} + 20$	
$\phi =$ <input type="text" value="29.80"/> °	<input type="text" value="44.49"/> °
$\gamma =$ <input type="text" value="1.430"/> ton/m ³	<input type="text" value="1.840"/> ton/m ³
Nq = <input type="text" value="21"/>	<input type="text" value="145"/>
$\delta =$ <input type="text" value="22.35"/> °	<input type="text" value="33.37"/> °
KHc = <input type="text" value="1"/>	<input type="text" value="1"/>
Factor of safety (F.S.) = <input type="text" value="3"/>	

Pressure due to soil:

Qult = Qt + Qf

- Tip Resistance (Qt)

$Qp = Pt \times Nq \times At$

$Pt = P3 = 7.56 \text{ ton/m}^2$

P1 = <input type="text" value="0.00"/> ton/m ³
P2 = 5.72 ton/m ³
P3 = 7.56 ton/m ³

Pile Area = 0.203 m²

Qp = 222.04 ton

- Friction Capacity (Qf)

Consider Friction ? Y/N

$Qf = \Sigma(KHc) \times Pox \times TAN(\delta) \times S$

S1 = 2BLD S1 = 3.60 m²

Po1 = (P1 + P2)/2

S2 = 2BL'D S2 = 0.90 m²

Po2 = (P2 + P3)/2

Po1 = 2.862 ton/m²

Po2 = 6.642 ton/m²

Qf = 0.00 ton

Qult = Qt + Qf

Qult = 222.04 ton

Qadm = Qult / F.S.

Qadm = 74.01 ton

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PILE SEISMIC STRESS

Based on chung equation

mark	size (cm)	length (m)	I (cm ⁴)	kh (kg/cm ³)	(cm-l) (cm-l)	L	I 3
P1	40	5	2.13E+05	3.169	0.00472	2.4	0.022
P2	45	5	3.42E+05	2.901	0.00422	2.1	0.026

N of piles	nI 3	Q (t)	Q (t/n)	y0 (cm)	M0 (t m)	Mmax (t m)	Im (m)
36	0.806	154.2	4.3	0.2	4.5	0.9	3.3
2	0.052	9.9	4.9	0.2	5.8	1.2	3.7

Σ= 38 0.858 164.0

Young's Modulus, E = 3.00E+05 kg/cm²
 Seismic force, Q = 164.03 t

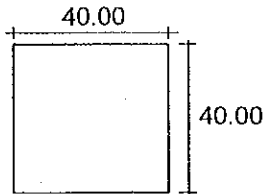
N = 9
 E0 = 63

40 x 40		
L (cm)	M (t m)	Q (t)
0	4.5	4.3
-50	2.6	3.3
-100	1.2	2.4
-150	0.2	1.6
-200	-0.4	1.0
-250	-0.8	0.5
-300	-0.9	0.2
-350	-0.9	-0.1
-400	-0.9	-0.2
-450	-0.7	-0.3
-500	-0.6	-0.3
-550	-0.5	-0.3
-600	-0.3	-0.2
-650	-0.2	-0.2
-700	-0.1	-0.2
-750	-0.1	-0.1

45 x 45		
L (cm)	M (t m)	Q (t)
0	5.8	4.9
-50	3.6	3.9
-100	1.9	2.9
-150	0.7	2.1
-200	-0.2	1.4
-250	-0.8	0.8
-300	-1.1	0.4
-350	-1.2	0.1
-400	-1.2	-0.1
-450	-1.1	-0.2
-500	-1.0	-0.3
-550	-0.8	-0.3
-600	-0.6	-0.3
-650	-0.5	-0.3
-700	-0.4	-0.3
-750	-0.2	-0.2

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PILE DESIGN



$f_c = 350.00 \text{ kg/cm}^2$

At release, $f_c = 280.00 \text{ kg/cm}^2$

Section Area = 1600 cm^2

Section Inertia = 213333.33 cm^4

- Prestressing Force

Cables.

Uncoated seven wire stress relieved strands.

Ultimate Strenght, $F_{pu} = 17,500 \text{ kg/cm}^2$

$\phi = 12.7 \text{ mm}$. Area = 92.90 mm.

of strands to use = 6

Prestressing force, $P_o = 0.70 F_{pu} A = 68.28 \text{ ton}$

Allowable stress

At service

$0.4 f_c = 140 \text{ kg/cm}^2$

At release

$0.4 f_c = 112 \text{ kg/cm}^2$

a) Stress at release

Axial Load, $P_a = 0.00 \text{ ton}$

Excentricity, $e = 0.00 \text{ cm}$

Moment, $M_a = 0.00 \text{ ton-m}$

$c = 20.00 \text{ cm}$

$(P_a + P_o) / A \pm (P_o e c / I + M_a c / I)$

42.68 ± 0.00

Stress 1 = $42.68 \text{ kg/cm}^2 < 0.4f_c \text{ o.k!!!}$

Stress 2 = $42.68 \text{ kg/cm}^2 < 0.4f_c \text{ o.k!!!}$

b) Stress at Service

Axial Load, $P_a = 58.40 \text{ ton}$

Excentricity, $e = 0.00 \text{ cm}$

Moment, $M_a = 4.54 \text{ ton-m}$

Prestress force, $P_e = 58.04 \text{ cm (15% losses)}$

$(P_a + P_e) / A \pm (P_e e c / I + M_a c / I)$

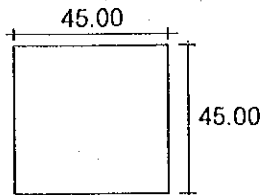
72.77 ± 42.56

Stress 1 = $115.33 \text{ kg/cm}^2 < 0.4f_c \text{ o.k!!!}$

Stress 2 = $30.22 \text{ kg/cm}^2 < 0.4f_c \text{ o.k!!!}$

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PILE DESIGN



$f_c =$ kg/cm^2

At release, $f_c =$ kg/cm^2

Section Area = cm^2

Section Inertia = cm^4

- Prestressing Force

Cables.

Uncoated seven wire stress relieved strands.

Ultimate Strength, $F_{pu} =$ kg/cm^2

$\phi = 12.7 \text{ mm}$. Area = 92.90 mm.

of strands to use = Prestressing force, $P_o = 0.70 F_{pu} A =$ ton

Allowable stress

At service

$0.4 f_c =$ kg/cm^2

At release

$0.4 f_c =$ kg/cm^2

a) Stress at release

Axial Load, $P_a =$ ton

Excentricity, $e =$ cm

Moment, $M_a =$ ton-m

$c =$ cm

$(P_a + P_o) / A \pm (P_o e c / I + M_a c / I)$

33.72 ± 0.00

Stress 1 = $33.72 \text{ kg/cm}^2 < 0.4f_c \text{ o.k!!!}$

Stress 2 = $33.72 \text{ kg/cm}^2 < 0.4f_c \text{ o.k!!!}$

b) Stress at Service

Axial Load, $P_a =$ ton

Excentricity, $e =$ cm

Moment, $M_a =$ ton-m

Prestress force, $P_e =$ cm (15% losses)

$(P_a + P_e) / A \pm (P_e e c / I + M_a c / I)$

65.20 ± 38.39

Stress 1 = $103.60 \text{ kg/cm}^2 < 0.4f_c \text{ o.k!!!}$

Stress 2 = $26.81 \text{ kg/cm}^2 < 0.4f_c \text{ o.k!!!}$

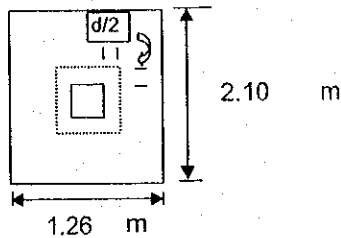
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FOOTING DESIGN

Design for foundation F-3

a) Punching

For Column



$\phi = 0.85$

Dead load P_D	=	30.60	ton
Live load P_L	=	30.80	ton
Seismic P_s	=	9.18	ton
$1.4D + 1.7L$	=	95.20	ton
$0.75(1.4D + 1.7L + 1.87S)$	=	84.27	ton
P_u	=	95.20	ton
d	=	66.00	cm
Column width	=	45.00	cm
Column base	=	45.00	cm
$b_o = 4(c+d)$	=	444	cm

$T_h = 80$ cm

$f_c = 210$ kg/cm²
20.59 Mpa

Concrete shear strength, V_c ACI 11.12

$\beta_c = 1.000$

$V_{c1} = \phi(1+2/\beta_c)\sqrt{f_c} b_o d/6 = 576.49$ ton

$\alpha_s = 40$

$V_{c2} = \phi(2+\alpha_s d/b_o)\sqrt{f_c} b_o d/12 = 249.29$ ton

$V_{c3} = \phi(1/3)\sqrt{f_c} b_o d = 384.33$

$V_c = 249.29 > 95.20$ o.k!!!

For Pile

$\phi = 0.85$

Distance from edge = 43.00 cm

Dead load P_D	=	17.84	ton/pile
Live load P_L	=	15.40	ton/pile
Carga sismica P_s	=	4.59	ton/pile
$1.4D + 1.7L$	=	51.16	ton
$0.75(1.4D + 1.7L + 1.87S)$	=	44.80	ton
P_u	=	51.16	ton
d	=	33.73	cm
Pile width	=	40.00	cm
Pile base	=	40.00	cm
$b_o = 4(c+d)$	=	294.92	cm

$\beta_c = 1$

$\alpha_s = 20$

$V_{c1} = \phi(1+2/\beta_c)\sqrt{f_c} b_o d/6 = 195.70$ ton

$V_{c2} = \phi(2+\alpha_s d/b_o)\sqrt{f_c} b_o d/12 = 232.13$ ton

$V_{c3} = \phi(1/3)\sqrt{f_c} b_o d = 130.47$

$V_c = 130.47 > 51.16$ o.k!!!

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b) Shear Reinforcement

Base = cm $f_y =$ kg/cm²

d = cm

$V_c = (1/6) \sqrt{f_c} b o d =$ 68.04 ton

$V_n = V_c + V_s$ $V_s = V_u / \phi - V_c$ $\phi = 0.85$

$V_u =$ 51.16 ton

$V_s =$ (7,861.1) kg

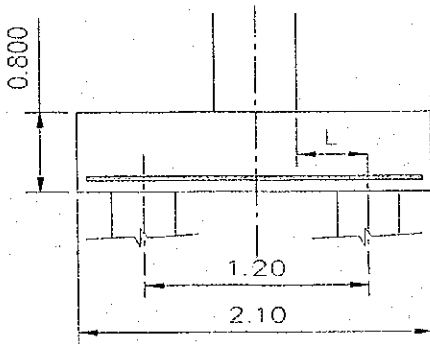
Bar denomination = Bar area = 1.27 cm²

of legs = Spacing, $S_{req} =$ -94.75 cm

Use 2 legs of N 4 @ 30 cm

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c) Reinforcing Steel



$$f_y = 4200 \text{ kg/cm}^2$$

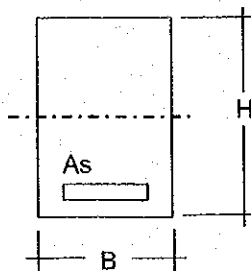
Moment generated by pile reaction

$$M = P_p \times L$$

$$L = 0.60 \text{ m}$$

$$M_1 = 1.4D + 1.7L = 30.69 \text{ ton-m}$$

$$M_2 = 0.75(1.4D + 1.7L + 1.87S) = 26.88 \text{ ton-m}$$



$$H = 80.00 \text{ cm}$$

$$b = 126.00 \text{ cm}$$

$$f_c = 280 \text{ kg/cm}^2$$

$$f_y = 4200 \text{ kg/cm}^2$$

Force for design: $M_u \text{ z-z} = 30.69 \text{ ton-m}$

$$d = 62.78 \text{ cm}$$

$$\text{Clear cover} = 5.00 \text{ cm}$$

$$f_y^2 / 1.7b f_c A_s^2 - f_y d A_s + M_u / \phi = \phi = 0.90$$

$$294.12 A_s^2 - 263666 A_s + 3410414.9 = 0 \quad A_s = 13.13 \text{ cm}^2$$

$$\left. \begin{aligned} A_{smin} &= (4/3)A_{sreq} \\ (4/3)A_{sreq} &= 17.50 \text{ cm}^2 \\ (14/f_y) b d &= 26.37 \text{ cm}^2 \end{aligned} \right\} A_{smin} = 17.50 \text{ cm}^2$$

$$A_{smax} : \quad \rho b = 0.0459 \quad A_{smax} (0.75\rho b) = 272.59 \text{ cm}^2$$

$$A_s = 17.50 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$$

$$\text{Bar denomination, } N = 6$$

$$\text{Bar Area } (A_v) = 2.85 \text{ cm}^2$$

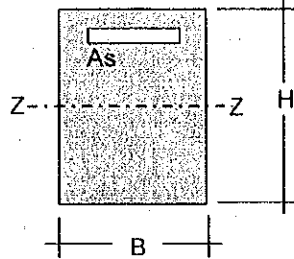
$$\text{Number of bars} = 6.14 \quad \text{Use } 7 - N6$$

$$\text{Pitch} = 18.59 \text{ cm} \quad 6 @ 18.5 \text{ cm}$$

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FOUNDATION BEAM FB-1 X-dir

BEAM DESIGN



H = 80.00 cm

b = 40.00 cm

f_c = 210 kg/cm²

f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z	COMBINATION	Mu z-z
Dead Loa	11.67	C1=1.4 DL+1.7 LL	19.30
Live Load	1.74	.75(1.4DL+1.7LL+1.8	17.70
Seismic x	2.30	.75(1.4DL+1.7LL+1.8	14.47
Seismic y	0.00		

Force for design: Mu z-z = 19.30 ton-m

d = 72.46 cm Clear cover = 5.00 cm

f_y²/1.7b²f_c As² - f_yd As + Mu/f f = 0.90

1235.29 As²304332 2144444 = 0 As = 7.26 cm²

As_{min} = (4/3)As_{req} :

(4/3)As _{req} =	9.68	cm ²	} As _{min} =	9.66	cm ²
(14/f _y) b d =	9.66	cm ²			

As_{max} : r_b = 0.0345 As_{max} (0.75r_b) = 74.91 cm²

As = 9.66 cm² o.k!! As < A_{max}

Bar denomination, N = 8 Bar Area (A_v) = 5.07 cm²

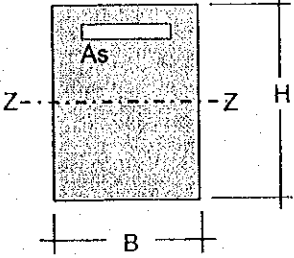
Number of bars = 1.91 Use 2 - N 8 4-D25

Minimum Base Required:

Max. bars per layer = 4 Minimum Base = 32.86 cm

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FOUNDATION BEAM FB-1 BEAM DESIGN Y-dir



H = 80.00 cm

b = 40.00 cm

f_c = 210 kg/cm²

f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z	COMBINATION	Mu z-z
Dead Loa	11.20	C1=1.4 DL+1.7 LL	38.66
Live Load	13.52	.75(1.4DL+1.7LL+1.8	32.35
Seismic x	2.39	.75(1.4DL+1.7LL+1.8	29.00
Seismic y	0.00		

Force for design: Mu z-z = 38.66 ton-m

d = 72.46 cm Clear cover = 5.00 cm

f_y²/1.7b²f_c As² - f_{yd} As + Mu/f = 0.90

1235.29 As² - 304332 As + 4295556 = 0 As = 15.03 cm²

As_{min} = (4/3)As_{req} :

(4/3)As _{req} = 20.04 cm ²	}	As _{min} = 9.66 cm ²
(14/f _y) b d = 9.66 cm ²		

As_{max} : rb = 0.0345 As_{max} (0.75rb) = 74.91 cm²

As = 15.03 cm² o.k!! As < A_{max}

Bar denomination, N = 8 Bar Area (A_v) = 5.07 cm²

Number of bars = 2.97 **Use 3 - N 8** 4-D25

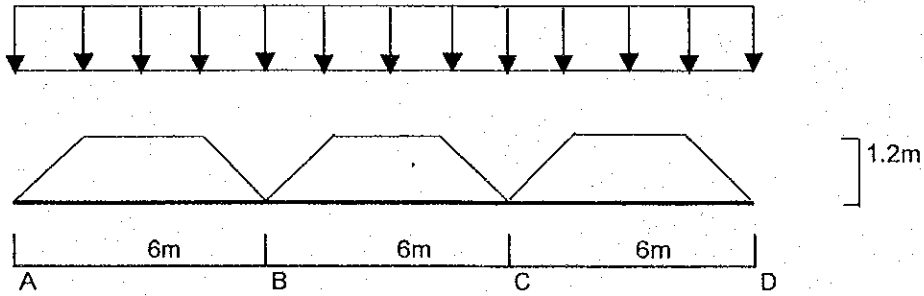
Minimum Base Required:

Max. bars per layer = 4 Minimum Base = 32.86 cm

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FB-2

Load Condition



for trapezoid weight

distribution weight

DL	0.35t/m ²	A/B, C/D	{ self weight CB (200) roof slab	0.50 t/m
		B/C		1.60 t/m
				0.48 t/m
				<hr/> 2.58 t/m
			self weight	0.50 t/m
LL	0.35t/m ²	A/B, C/D	roof slab	0.12 t/m

Stress Result

DL

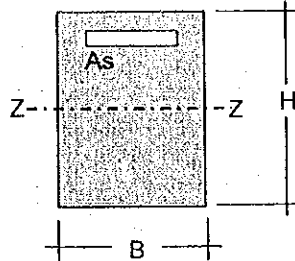
4.6	6.0	6.0	6.0	6.0	4.6
△	8.0	△	0.0	△	8.0

LL

0.7	1.4	1.4	1.4	1.4	0.7
△	1.2	△	0.3	△	1.2

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**FOUNDATION BEAM FB-2
BEAM DESIGN**



H = 65.00 cm
 b = 30.00 cm
 f_c = 210 kg/cm²
 f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Loa	8.00
Live Load	1.20
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	13.24
.75(1.4DL+1.7LL+1.8	9.93
.75(1.4DL+1.7LL+1.8	9.93

Force for design: Mu z-z = 13.24 ton-m

d = 57.46 cm

Clear cover = 5.00 cm

$$f_y^2 / 1.7b^2 f_c A_s^2 - f_y d A_s + M_u / f = 0.90$$

$$1647.06 A_s^2 - 241332 A_s + 1471111 = 0 \quad A_s = 6.37 \text{ cm}^2$$

A_{smin} = (4/3)A_{sreq} :

$$\left. \begin{array}{l} (4/3)A_{sreq} = 8.50 \text{ cm}^2 \\ (14/f_y) b d = 5.75 \text{ cm}^2 \end{array} \right\} A_{smin} = 5.75 \text{ cm}^2$$

$$A_{smax} : r_b = 0.0345 \quad A_{smax} (0.75r_b) = 44.55 \text{ cm}^2$$

$$A_s = 6.37 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$$

Bar denomination, N = 8

Bar Area (A_v) = 5.07 cm²

Number of bars = 1.26

Use 2 - N 8

3-D25

Minimum Base Required:

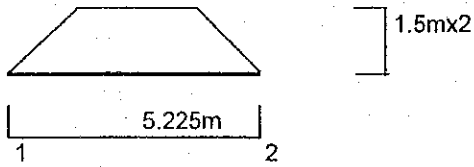
Max. bars per layer = 3

Minimum Base = 27.78 cm

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FB-3

Load Condition



for trapezoid weight

distribution weight

DL 0.60t/m²

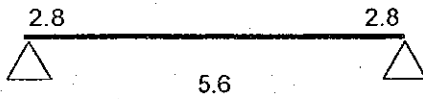
self weight

0.58 t/m

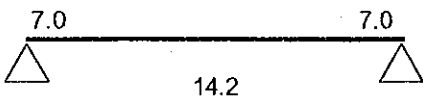
LL 2.00t/m²

Stress Result

DL

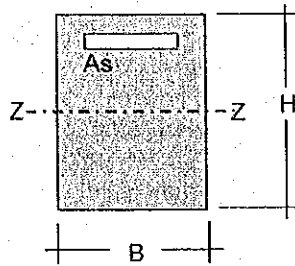


LL



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**FOUNDATION BEAM FB-1
BEAM DESIGN**



H = 80.00 cm
 b = 40.00 cm
 f_c = 210 kg/cm²
 f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Loa	5.60
Live Load	14.20
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	31.98
.75(1.4DL+1.7LL+1.8	23.99
.75(1.4DL+1.7LL+1.8	23.99

Force for design: Mu z-z = 31.98 ton-m

d = 72.46 cm

Clear cover = 5.00 cm

$$f_y^2 / 1.7 b f_c A_s^2 - f_y d A_s + M_u / f_c f = 0.90$$

$$1235.29 A_s^2 - 304332 A_s + 3553333 = 0 \quad A_s = 12.29 \text{ cm}^2$$

A_{smin} = (4/3)A_{sreq} :

$$\left. \begin{array}{l} (4/3)A_{sreq} = 16.39 \text{ cm}^2 \\ (14/f_y) b d = 9.66 \text{ cm}^2 \end{array} \right\} A_{smin} = 9.66 \text{ cm}^2$$

$$A_{smax} : r_b = 0.0345 \quad A_{smax} (0.75 r_b) = 74.91 \text{ cm}^2$$

$$A_s = 12.29 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$$

Bar denomination, N = 8

Bar Area (A_v) = 5.07 cm²

Number of bars = 2.43

Use 3 - N 8

4-D25

Minimum Base Required:

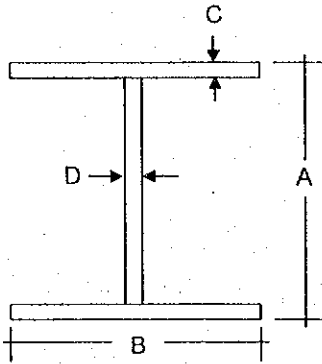
Max. bars per layer = 4

Minimum Base = 32.86 cm

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Roof Beam

B1



Beam type = **W10X22**

A = **10.17** in

B = **5.75** in

C = **0.36** in

D = **0.240** in

Area = **6.490** in²

I = **118.00** in⁴

Yc = **5.085** in

S = **23.21** in³

Pd = **0.90** ton

Md = **0.70** ton-m

PL = **0.40** ton

ML = **0.30** ton-m

PS = **0.40** ton

MS = **1.10** ton-m

P/A(d+L)	31.05	} <div style="display: inline-block; vertical-align: middle; margin-left: 10px;"> <p>Fy = 36 ksi</p> <p>444.63 kg/cm²</p> <p>0.6 Fy = 1512.00 kg/cm² o.k.!!</p> </div>
P/A(d+L+s)	30.45	
Md+ L/S =	262.97	
Ms+d+L/S=	414.18	

- Shear

Max. Shear = **700.0** kg

Fv = V / (h tw) = **44.45** kg/cm²

0.4 Fy = **1008.00** kg/cm² **o.k.!!**

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Roof Beam B2

Beam type = **W12X40**

A = **11.94** in
 B = **8.01** in
 C = **0.52** in
 D = **0.300** in

Area = 11.800 in² I = 310.00 in⁴
 Yc = 5.970 in S = 51.93 in³

Pd = **1.00** ton Md = **1.80** ton-m from analysis
 PL = **0.30** ton ML = **0.20** ton-m
 PS = **0.10** ton MS = **0.00** ton-m

$$\left. \begin{array}{l} P/A(d+L) \quad 17.08 \\ P/A(d+L+s) \quad 13.79 \\ Md+L/S = \quad 235.04 \\ Ms+d+L/S = \quad 176.28 \end{array} \right\} \begin{array}{l} F_y = \mathbf{36} \text{ ksi} \\ 252.12 \text{ kg/cm}^2 \\ 0.6 F_y = 1512.00 \text{ kg/cm}^2 \quad \mathbf{o.k.!!} \end{array}$$

- Shear

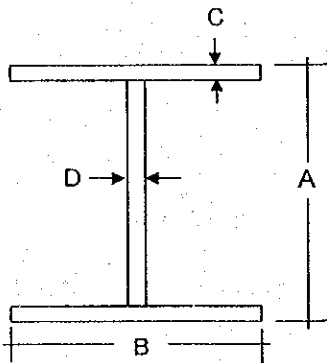
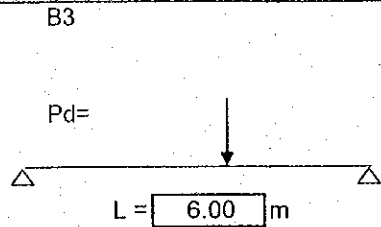
Max. Shear = 900.0 kg

$F_v = V / (h t_w) = 38.94 \text{ kg/cm}^2$

0.4 F_y = 1008.00 kg/cm² **o.k.!!**

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Roof Beam



DL = 45 kg/m²
 LL = 20 kg/m²
 LLd = 0 kg/m²
 Tributary Width = 3.88 m

$Pd = 523.8$ kg
 $Wd = \text{selfw.} = 27.00$ kg/m

$PL = 232.8$ kg
 $PLd = 0$ kg

Beam type = **W8x18**

$A = 8.14$ in

$B = 5.25$ in

$C = 0.33$ in

$D = 0.230$ in

Area = 5.260 in²

$Yc = 4.070$ in

$Fy = 36$ ksi

$I = 61.90$ in⁴

$S = 15.21$ in³

$Md = 0.91$ ton-m

$ML = 0.35$ ton-m

$Md / S = 364.00$ } 504.12 kg/cm²
 $ML / S = 140.11$ } $0.6 Fy = 1512.0$ kg/cm² **o.k.!!**

- Shear

Max. Shear = 459.3 kg

$Fv = V / (h tw) = 38.03$ kg/cm²

$0.4 Fy = 1008.00$ kg/cm² **o.k.!!**

- Deflection

$d_{admi.} = L/360 = 1.67$ cm

$E = 2.0E+10$ kg/m²

$d_{dead} = 0.54$ cm

$d_{Total} = 0.54$ cm **o.k.!!**

$d_{live} = 0.00$ cm

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Roof Beam B4

DL = 30 kg/m²
 LL = 20 kg/m²
 LLd = 0 kg/m²

Tributary Width = 3.00 m

Wd1 = 90.0 kg/m
 Wd2 = selfw. = 8.00 kg/m
 Wd = 98.00 kg/m

WL = 60.0 kg/m

Beam type = C4x5.4

A = 4 in
 B = 1.584 in
 C = 0.296 in
 D = 0.184 in

Area = 1.590 in²
 Yc = 2.000 in
 Fy = 36 ksi

I = 3.85 in⁴
 S = 1.93 in³
 Md = 0.18 ton-m
 ML = 0.11 ton-m

Md / S = 584.61
 ML / S = 357.93 } 942.54 kg/cm²
 0.6 Fy = 1512.00 kg/cm² o.k.!!

- Shear

Max. Shear = 306.5 kg
 Fv = V / (h tw) = 64.55 kg/cm²
 0.4 Fy = 1008.00 kg/cm² o.k.!!

- Deflection

d adm. = L/360 = 1.08 cm
 E = 2.0E+10 kg/m²
 d dead = 0.88 cm
 d Total = 0.88 cm o.k.!!
 d live = 0.00 cm

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Polin

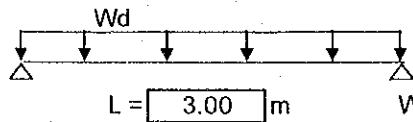
Dead Load = 20 kg/m²

Live load = 20 kg/m²

Tributary Width = 1.00 m

Wd = 20.0 kg/m

WL = 20.0 kg/m

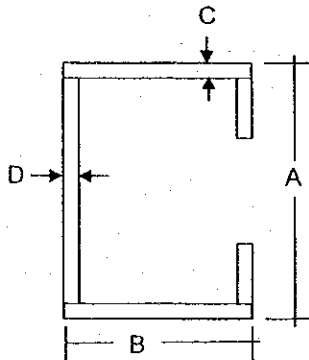


Wd1 = 20.0 kg/m

Wd2 = selfweight = 2.70 kg/m

Wd = 22.70 kg/m

WL = 20.0 kg/m



Beam type = C4x3/64

A = 4 in

B = 2 in

C = 0.0469 in

D = 0.0469 in

Area = 0.406 in²

I = 1.06 in⁴

Yc = 2.000 in

S = 0.53 in³

Fy = 36 ksi

Md = 0.03 ton-m

ML = 0.02 ton-m

$Md / S = 294.04$
 $ML / S = 259.06$

$\left. \begin{array}{l} 294.04 \\ 259.06 \end{array} \right\} 553.10 \text{ kg/cm}^2$
 $0.6 Fy = 1512.00 \text{ kg/cm}^2 \quad \text{o.k.!!}$

- Deflection

d adm. = L/360 = 0.83 cm

E = 2.0E+10 kg/m²

d dead = 0.27 cm

d Total = 0.50 cm o.k.!!

d live = 0.23

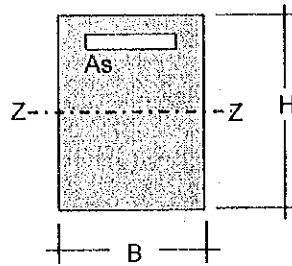
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<p>2nd Beam B11</p> <p style="text-align: center;">L = 6.40 m</p>	<p>DL = 30 kg/m² LL = 180 kg/m² LLd = 60 kg/m² Tributary Width = 0.50 m</p> <p>Wd1 = 15.0 kg/m Wd2 = selfw. = 38.00 kg/m Wd = 53.00 kg/m</p> <p>WL = 90.0 kg/m</p> <p>Beam type = C10x25</p> <p>A = 10 in B = 2.886 in C = 0.436 in D = 0.526 in</p>
<p>Area = 7.350 in² Yc = 5.000 in Fy = 36 ksi</p>	<p>I = 144.00 in⁴ S = 24.10 in³ Md = 0.27 ton-m ML = 0.46 ton-m</p>
<p>Md / S = 68.71 ML / S = 116.68</p>	<p>185.39 kg/cm² 0.6 Fy = 1512.00 kg/cm² o.k.!!</p>
<p>- Shear</p> <p>Max. Shear = 457.6 kg Fv = V / (h tw) = 13.48 kg/cm² 0.4 Fy = 1008.00 kg/cm² o.k.!!</p>	<p>- Deflection</p> <p>d adm. = L/360 = 1.78 cm E = 2.0E+10 kg/m² d dead = 0.09 cm d Total = 0.15 cm o.k.!! d live = 0.05 cm</p>

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RF BEAM

**B-5
BEAM DESIGN**



$H = 65.00$ cm
 $b = 30.00$ cm
 $f_c = 280$ kg/cm²
 $f_y = 4200$ kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE OF LOAD	MOMENT Mz-z
--------------	-------------

Dead Loa	1.30
Live Loa	0.10
Seismic	3.00
Seismic	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	1.99
.75(1.4DL+1.7LL+1.	5.70
.75(1.4DL+1.7LL+1.	1.49

Force for design: $Mu\ z-z = 5.70$ ton-m

$d = 57.46$ cm

Clear cover = 5.00 cm

$$f_y^2 / 1.7 b f_c A_s^2 - f_y d A_s + M_u f = 0.90$$

$$1235.29 A_s^2 - 41332.63333 A_s + 0 = 0 \quad A_s = 2.66 \text{ cm}^2$$

$A_{smin} = (4/3)A_{sreq}$:

$$\left. \begin{aligned} (4/3)A_{sreq} &= 3.55 \text{ cm}^2 \\ (14/f_y) b d &= 5.75 \text{ cm}^2 \end{aligned} \right\} A_{smin} = 3.55 \text{ cm}^2$$

$$A_{smax} : r_b = 0.0459 \quad A_{smax} (0.75r_b) = 59.40 \text{ cm}^2$$

$$A_s = 3.55 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$$

Bar denomination, N = 8

Bar Area (A_v) = 5.07 cm²

Number of bars = 0.70 Use 1 - N 8 3-D25

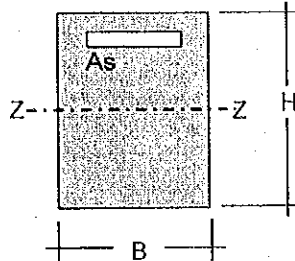
Minimum Base Required:

Max. bars per layer = 3 Minimum Base = 27.78 cm

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2nd Beam

**B-10
BEAM DESIGN**



H = 65.00 cm
 b = 30.00 cm
 f_c = 280 kg/cm²
 f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Loa	4.30
Live Loa	1.50
Seismic	8.10
Seismic	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	8.57
.75(1.4DL+1.7LL+1.	17.79
.75(1.4DL+1.7LL+1.	6.43

Force for design: Mu z-z = 17.80 ton-m

d = 57.46 cm

Clear cover = 5.00 cm

$$f_y^2 / 1.7 b f_c A_s^2 - f_y d A_s + M_u f = 0.90$$

$$1235.29 A_s^2 - 41332 A_s + 1977778 = 0$$

$$A_s = 8.57 \text{ cm}^2$$

Asmin = (4/3)Asreq :

$$\left. \begin{aligned} (4/3)A_{sreq} &= 11.43 \text{ cm}^2 \\ (14/f_y) b d &= 5.75 \text{ cm}^2 \end{aligned} \right\} A_{smin} = 5.75 \text{ cm}^2$$

$$A_{smax} : r_b = 0.0459 \quad A_{smax} (0.75 r_b) = 59.40 \text{ cm}^2$$

$$A_s = 8.57 \text{ cm}^2 \quad \text{o.k! } A_s < A_{max}$$

Bar denomination, N = 8

Bar Area (A_v) = 5.07 cm²

Number of bars = 1.69

Use 2 - N 8

4-D25

Minimum Base Required:

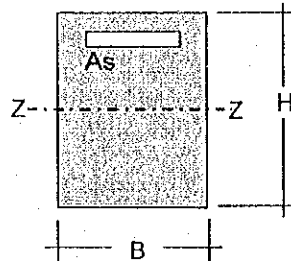
Max. bars per layer = 3

Minimum Base = 27.78 cm

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Canti Beam

**CB-10
BEAM DESIGN**



H = 30.00 cm
 b = 30.00 cm
 f'c = 280 kg/cm²
 fy = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Loa	0.39
Live Loa	0.75
Seismic	0.00
Seismic	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	1.82
.75(1.4DL+1.7LL+1.	1.37
.75(1.4DL+1.7LL+1.	1.37

Force for design: Mu z-z = 1.82 ton-m

d = 22.46 cm

Clear cover = 5.00 cm

$$f_y^2 / 1.7b f'_c A_s^2 - f_y d A_s + M_u f = 0.90$$

$$1235.29 A_s^2 - 4332 \cdot 202222 = 0 \quad A_s = 2.21 \text{ cm}^2$$

Asmin = (4/3)Asreq :

$$\left. \begin{aligned} (4/3)A_{sreq} &= 2.94 \text{ cm}^2 \\ (14/f_y) b d &= 2.25 \text{ cm}^2 \end{aligned} \right\} A_{smin} = 2.25 \text{ cm}^2$$

Asmax : rb = 0.0459 Asmax (0.75rb) = 23.22 cm²

As = 2.25 cm² o.k!! As < Amax

Bar denomination, N = 8

Bar Area (Av) = 5.07 cm²

Number of bars = 0.44 Use 1 - N8 2-D25

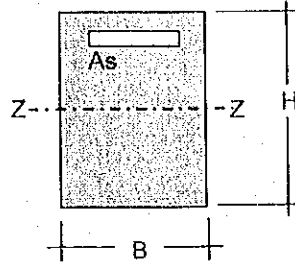
Minimum Base Required:

Max. bars per layer = 3 Minimum Base = 27.78 cm

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2nd Beam

B-12
BEAM DESIGN



H = 40.00 cm

b = 30.00 cm

f_c = 280 kg/cm²

f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE OF LOAD	MOMENT
	Mz-z

Dead Loa	1.30
Live Loa	0.60
Seismic	1.60
Seismic	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	2.84
.75(1.4DL+1.7LL+1)	4.37
.75(1.4DL+1.7LL+1)	2.13

Force for design: Mu z-z = 4.37 ton-m

d = 32.46 cm

Clear cover = 5.00 cm

$f_y^2/1.7b f_c A_s^2 - f_y d A_s + M_u f = 0.90$

$1235.29 A_s^2 - 36332 A_s + 485556 = 0$

As = 3.68 cm²

Asmin = (4/3)Asreq :

$(4/3)A_{sreq} = 4.91 \text{ cm}^2$
 $(14/f_y) b d = 3.25 \text{ cm}^2$

Asmin = 3.25 cm²

Asmax : rb = 0.0459 Asmax (0.75rb) = 33.56 cm²

As = 3.68 cm² o.k!! As < Amax

Bar denomination, N = 8

Bar Area (Av) = 5.07 cm²

Number of bars = 0.73

Use 1 - N 8

3-D25

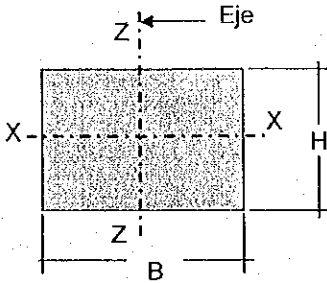
Minimum Base Required:

Max. bars per layer = 3

Minimum Base = 27.78 cm

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Column C1



H = m

B = m

f'c = kg/cm²

fy = kg/cm²

Area = 1,600 cm²

Inertia Z = 2.1E+05 cm⁴

Inertia Y = 2.1E+05 cm⁴

Forces and Moments

From Structural Analysis (ton , m) :

TYPE OF LOAD	AXIAL		MOMENT		SHEAR	
	P	Mz-z	Mx-x	Vx	Vz	
Dead Loa	5.10	2.10	1.00	0.20	0.10	
Live Loa	0.40	1.10	1.60	0.10	0.20	
Seismic Loa	0.00	3.90	0.00	0.60	0.00	
Seismic loa	0.00	0.00	5.30	0.00	0.70	

COMBINATI	Pu	Mu z-z	Mu x-x	Vu x	Vu z
C1	7.82	4.81	4.12	0.45	0.48
C2	5.87	10.28	---	1.34	---
C3	5.87	---	11.41	---	1.48

Forces for design.

Pu z = ton Pu x = ton

Mu x-x = ton-m Mu z-z = ton-m

Vu z = ton Vu x = ton

C1 = 1.4 DL + 1.7 LL

C2 = 0.75(1.4DL + 1.7LL + 1.87SLy)

C3 = 0.75(1.4DL + 1.7LL + 1.87SLz)

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Ortogonal Combination

$$MX = 100\%EQX + 30\%EQZ$$

$$MZ = 100\%EQZ + 30\%EQX$$

$$M_x = M_x + M_z(H/B)\left(\frac{1-b}{\beta}\right) \quad b = 0.65 \quad M_z = M_z + M_x(B/H)\left(\frac{1-b}{\beta}\right) \quad b = 0.65$$

Slenderness.

if $klu/r > 22$ Consider Slenderness .

$$k = 2.0 \quad lu = 15.7 \text{ m} \quad r = (\text{Inetia/Area})^{1/2}$$

Y Direction

$$r = 0.115 \text{ m} \quad klu/r = 271.932 > 22 \text{ Consider slenderness}$$

Z Direction

$$r = 0.115 \text{ m} \quad klu/r = 271.932 > 22 \text{ Consider slenderness}$$

Slenderness

$$Mc = dbMb + dsMs$$

$$db = cm / (1 - Pu/FP) \quad cm = 1.0$$

$$Pc = p^2EI / (klu)^2 \quad E = 2526713 \text{ ton/m}^2$$

$$Pu = 1.3 \times \text{Fuerza A} \quad 7.82 \text{ ton}$$

X Dir. :

Z Dir. :

$$\text{Inercia} = 0.0021 \text{ m}^2 \quad \text{Inercia} = 0.0021 \text{ m}^2$$

$$Pc = 53.96 \text{ ton} \quad Pc = 53.96 \text{ ton}$$

$$db = 1.184 \quad db = 1.184$$

$$\text{Mu x-x} = 12.17 \text{ ton-m}$$

$$\text{Mu z-z} = 13.50 \text{ ton-m}$$

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- Design by flexure and Axial load

Z Direction : $f = 0.70$

Gross Area (A_g) = 0.16 m² = 248.02 in²

$h = 0.40$ m = 15.75 in

$P = 5.87$ ton = 12.93 kips

$M = 12.17$ ton-m = 1056.12 kips-in

$P_u/A_g = 0.05$ $u/A_g h = 0.27$

From the Load-Moment strength interaction diagram R4-60.90,
the ρ value is:

$\rho = \boxed{1.5}$ % $A_s = A_g \times \rho = 24.00$ cm²

Bar denomination = $\boxed{8}$ Bar area = 5.07 cm²

Quantity of bars = 4.74

Coloca 6 N 8

X Direction : $f = 0.7$

Gross Area (A_g) = 0.16 m² = 248.02 in²

$h = 0.40$ m = 15.75 in

$P = 5.87$ ton = 12.93 kips

$M = 13.50$ ton = 1172.12 kips-in

$P_u/A_g = 0.05$ $u/A_g h = 0.30$

From the Load-Moment strength interaction diagram R4-60.90,
the ρ value is:

$\rho = \boxed{1}$ % $A_s = A_g \times \rho = 16.00$ cm²

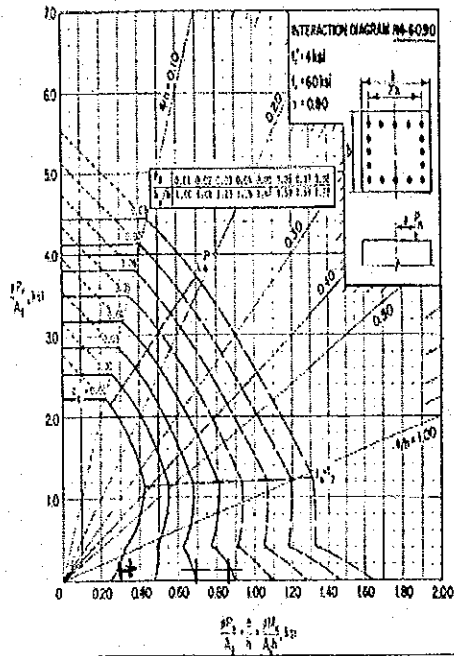
Bar Denomination = $\boxed{8}$ Bar area = 5.07 cm²

Quantity of bars = 3.16

Use 4 N8

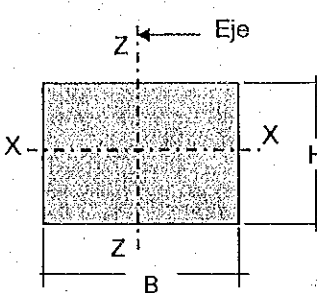
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COLUMNS 7.4.4—Load-moment strength interaction diagram for R4-60.90 columns



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Column C2



H = m

B = m

f'c = kg/cm²

fy = kg/cm²

Area = 2,025 cm²

Inertia Z = 3.4E+05 cm⁴

Inertia Y = 3.4E+05 cm⁴

Forces and Moments

From Structural Analysis (ton , m) :

TYPE OF LOAD	AXIAL		MOMENT		SHEAR	
	P	Mz-z	Mx-x	Vx	Vz	
Dead Loa	14.50	0.80	1.10	0.20	0.40	
Live Loa	3.10	0.60	0.00	0.20	0.00	
Seismic Loa	5.40	7.60	0.00	2.70	0.00	
Seismic Loa	2.60	0.00	6.90	0.00	2.40	

COMBINATI	Pu	Mu z-z	Mu x-x	Vu x	Vu z
C1	25.57	2.14	1.54	0.62	0.56
C2	26.75	13.83	---	4.80	---
C3	22.82	---	12.55	---	4.40

Forces for design.

Pu z = ton Pu x = ton

Mu x-x = ton-m Mu z-z = ton-m

Vu z = ton Vu x = ton

C1 = 1.4 DL + 1.7 LL

C2 = 0.75(1.4DL + 1.7LL + 1.87SLy)

C3 = 0.75(1.4DL + 1.7LL + 1.87SLz)

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Orthogonal Combination

$$MX = 100\%EQX + 30\%EQZ \qquad MZ = 100\%EQZ + 30\%EQX$$

$$M_x = M_x + M_z(H/B) \left(\frac{1-b}{\beta} \right) \quad b = 0.65 \qquad M_z = M_z + M_x(B/H) \left(\frac{1-b}{\beta} \right) \quad b = 0.65$$

Slenderness.

iF $klu/r > 22$ Consider Slenderness .

$$k = 1.0 \qquad lu = \boxed{5.45} \text{ m} \qquad r = (Inercia/Area)^{1/2}$$

Y Direction

$$r = 0.130 \text{ m} \qquad klu/r = 83.908 > 22 \text{ Consider slenderness}$$

Z Direction

$$r = 0.130 \text{ m} \qquad klu/r = 83.908 > 22 \text{ Consider slenderness}$$

Slenderness

$$Mc = dbMb + dsMs$$

$$db = cm / (1 - Pu/fP \text{ cm} = 1.0$$

$$Pc = \pi^2 EI / (klu)^2 \qquad E = 2526713 \text{ ton/m}^2$$

$$Pu = \text{Axial Force} = 26.75 \text{ ton}$$

X Dir. :

Z Dir. :

$$\text{Inercia} = 0.0034 \text{ m}^2 \qquad \text{Inercia} = 0.0034 \text{ m}^2$$

$$Pc = 717.25 \text{ ton} \qquad Pc = 717.25 \text{ ton}$$

$$db = 1.056 \qquad db = 1.048$$

$$Mu \text{ x-x} = 14.61 \text{ ton-m}$$

$$Mu \text{ z-z} = 13.15 \text{ ton-m}$$

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- Design by flexure and Axial load
 Z Direction : $f = 0.70$

Area Gruesa $0.20 \text{ m}^2 = 313.91 \text{ in}^2$
 $h = 0.45 \text{ m} = 17.72 \text{ in}$
 $P = 26.75 \text{ ton} = 58.98 \text{ kips}$
 $M = 14.61 \text{ ton-m} = 1267.75 \text{ kips-in}$

 $Pu/Ag = 0.19 \quad u/Agh = 0.23$

From the Load-Moment strength interaction diagram R4-60.90,
 the p value is:

$r = \boxed{1} \% \quad As = Ag \times r = 20.25 \text{ cm}^2$

Bar denomination = $\boxed{8}$ Bar area = 5.07 cm^2

Quantity of bars = 4.00

Use 4 N 8

X Direction : $f = 0.7$

Gross Area (A_g) = $0.20 \text{ m}^2 = 313.91 \text{ in}^2$
 $h = 0.45 \text{ m} = 17.72 \text{ in}$
 $P = 22.82 \text{ ton} = 50.32 \text{ kips}$
 $M = 13.15 \text{ ton} = 1141.59 \text{ kips-in}$

 $Pu/Ag = 0.16 \quad u/Agh = 0.21$

From the Load-Moment strength interaction diagram R4-60.90,
 the p value is:

$r ? \boxed{1} \% \quad As = Ag \times r = 20.25 \text{ cm}^2$

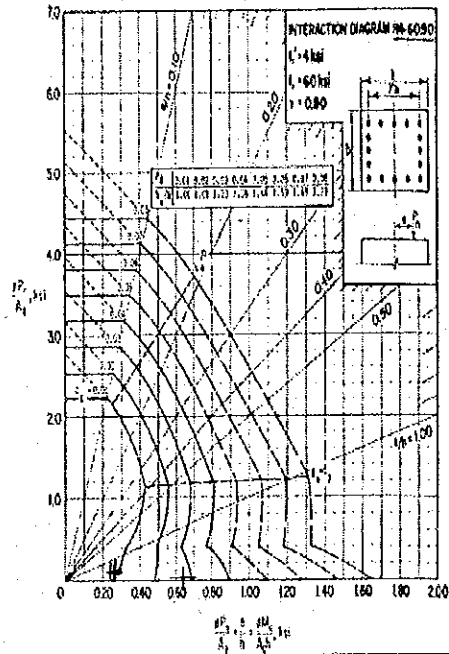
Bar Denomination = $\boxed{8}$ Bar area = 5.07 cm^2

Cantidad de varillas = 4.00 1371
11996.25

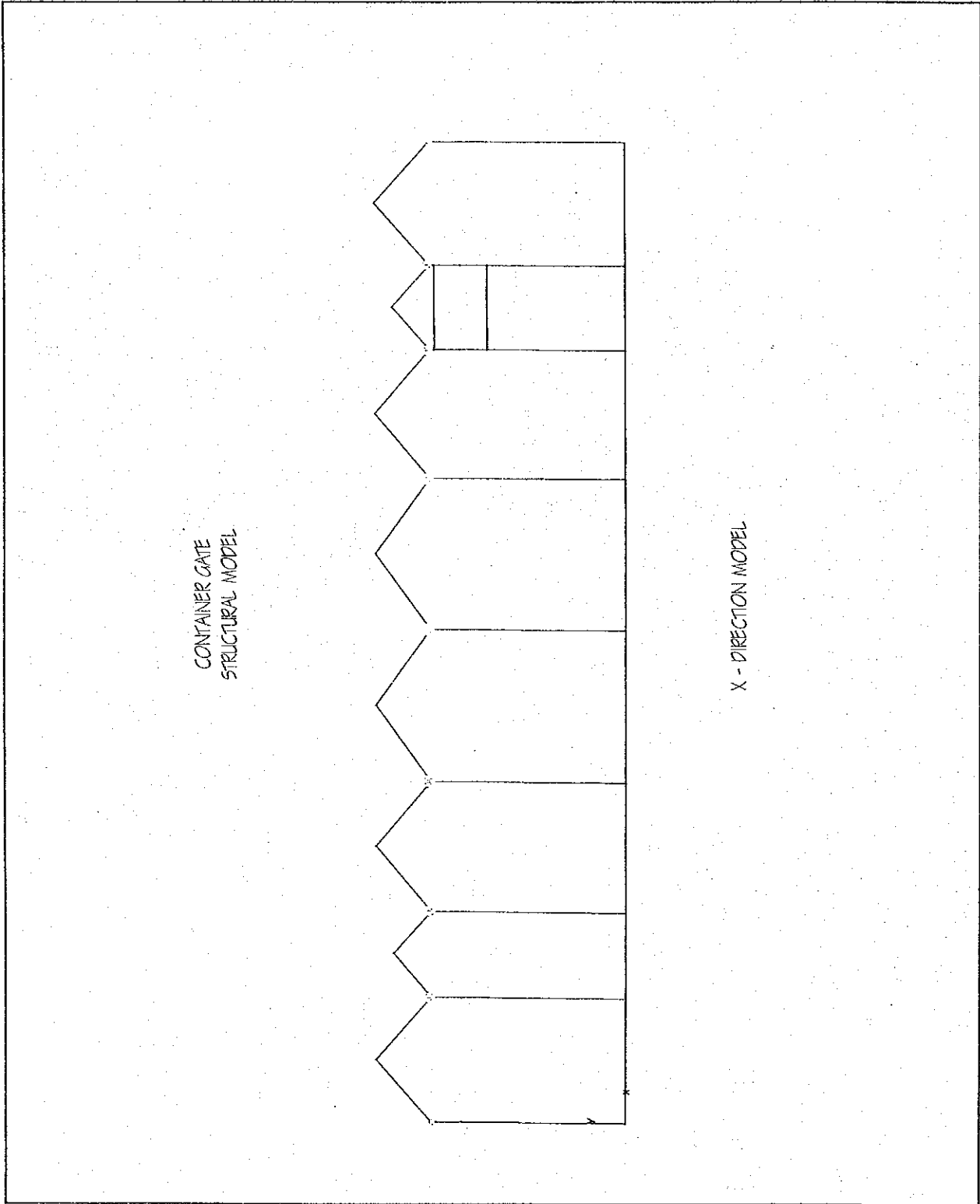
Use 4 N8

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COLUMNS 7.4.4—Load-moment strength interaction diagram for R4-60.90 columns



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Container Gate

Model X- direction

Node Coordinate

Node No.	x (m)	y (m)	z (m)
1	0	0	6
2	5.2	0	6
3	8.8	0	6
4	14.2	0	6
5	20.6	0	6
6	27	0	6
7	32.4	0	6
8	36	0	6
9	41.2	0	6
10	0	6.6	6
11	5.2	6.6	6
12	8.8	6.6	6
13	14.2	6.6	6
14	20.6	6.6	6
15	27	6.6	6
16	32.4	6.6	6
17	36	6.6	6
18	41.2	6.6	6
19	0	7.8	6
20	5.2	7.8	6
21	8.8	7.8	6
22	14.2	7.8	6
23	20.6	7.8	6
24	27	7.8	6
25	32.4	7.8	6
26	36	7.8	6
27	41.2	7.8	6
28	0	5.4	6
29	5.2	5.4	6
30	8.8	5.4	6
31	14.2	5.4	6
32	20.6	5.4	6
33	27	5.4	6
34	32.4	5.4	6
35	36	5.4	6
36	41.2	5.4	6
37	32.4	7.7	6
38	36	7.7	6
39	2.6	10.1	6
40	7	9.4	6
41	11.5	10.1	6
42	17.4	10.1	6
43	23.8	10.1	6
44	29.7	10.1	6
45	34.2	9.4	6
46	38.6	10.1	6

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Element data								
Member No.	node 1	node 2	length (m)	Member No.	node 1	node 2	length (m)	
1	1	2	5.2	46	22	42	3.9	
2	2	3	3.5	47	42	23	3.9	
3	3	4	5.4	48	23	43	3.9	
4	4	5	6.4	49	43	24	3.9	
5	5	6	6.4	50	24	44	3.5	
6	6	7	5.4	51	44	25	3.5	
7	7	8	3.5	52	25	45	2.3	
8	8	9	5.2	53	45	26	2.3	
9	1	28	5.4	54	26	46	3.4	
10	2	29	5.4	55	46	27	3.4	
11	3	30	5.4					
12	4	31	5.4					
13	5	32	5.4					
14	6	33	5.4					
15	7	34	5.4					
16	8	35	5.4					
17	9	36	5.4					
18	10	19	1.3					
19	11	20	1.3					
20	12	21	1.3					
21	13	22	1.3					
22	14	23	1.3					
23	15	24	1.3					
24	16	37	1.1					
25	17	38	1.1					
26	18	27	1.3					
27	28	10	1.1					
28	29	11	1.1					
29	30	12	1.1					
30	31	13	1.1					
31	32	14	1.1					
32	33	15	1.1					
33	34	16	1.1					
34	35	17	1.1					
35	36	18	1.1					
36	34	35	3.5					
37	37	25	0.2					
38	38	26	0.2					
39	37	38	3.5					
40	19	39	3.4					
41	39	20	3.4					
42	20	40	2.3					
43	40	21	2.3					
44	21	41	3.5					
45	41	22	3.5					

PROJECT: Detailed Design on Port Reactlvation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
SECTION: Contalner Gate	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page	62 / 178

Section						
Membe group	section	direction	Member group	section	direction	
1	Custom1	bd-40x80	51	W	W10x22	0
2	Custom1	bd-40x80	52	W	W10x22	0
3	Custom1	bd-40x80	53	W	W10x22	0
4	Custom1	bd-40x80	54	W	W10x22	0
5	Custom1	bd-40x80	55	W	W10x22	0
6	Custom1	bd-40x80				
7	Custom1	bd-40x80				
8	Custom1	bd-40x80				
9	Custom1	bd-40x40				
10	Custom1	bd-40x40				
11	Custom1	bd-40x40				
12	Custom1	bd-40x40				
13	Custom1	bd-40x40				
14	Custom1	bd-40x40				
15	Custom1	bd-45x45				
16	Custom1	bd-45x45				
17	Custom1	bd-40x40				
18	Custom1	bd-35x35				
19	Custom1	bd-35x35				
20	Custom1	bd-35x35				
21	Custom1	bd-35x35				
22	Custom1	bd-35x35				
23	Custom1	bd-35x35				
24	Custom1	bd-45x45				
25	Custom1	bd-45x45				
26	Custom1	bd-35x35				
27	Custom1	bd-40x40				
28	Custom1	bd-40x40				
29	Custom1	bd-40x40				
30	Custom1	bd-40x40				
31	Custom1	bd-40x40				
32	Custom1	bd-40x40				
33	Custom1	bd-45x45				
34	Custom1	bd-45x45				
35	Custom1	bd-40x40				
36	Custom1	bd-30x65				
37	Custom1	bd-45x45				
38	Custom1	bd-45x45				
39	Custom1	bd-30x65				
40	W	W10x22				
41	W	W10x22				
42	W	W10x22				
43	W	W10x22				
44	W	W10x22				
45	W	W10x22				
46	W	W10x22				
47	W	W10x22				
48	W	W10x22				
49	W	W10x22				
50	W	W10x22				

PROJECT: Detailed Design on Port Reactivation Project In La Union Province	Calc. File No.		Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page	63 / 78

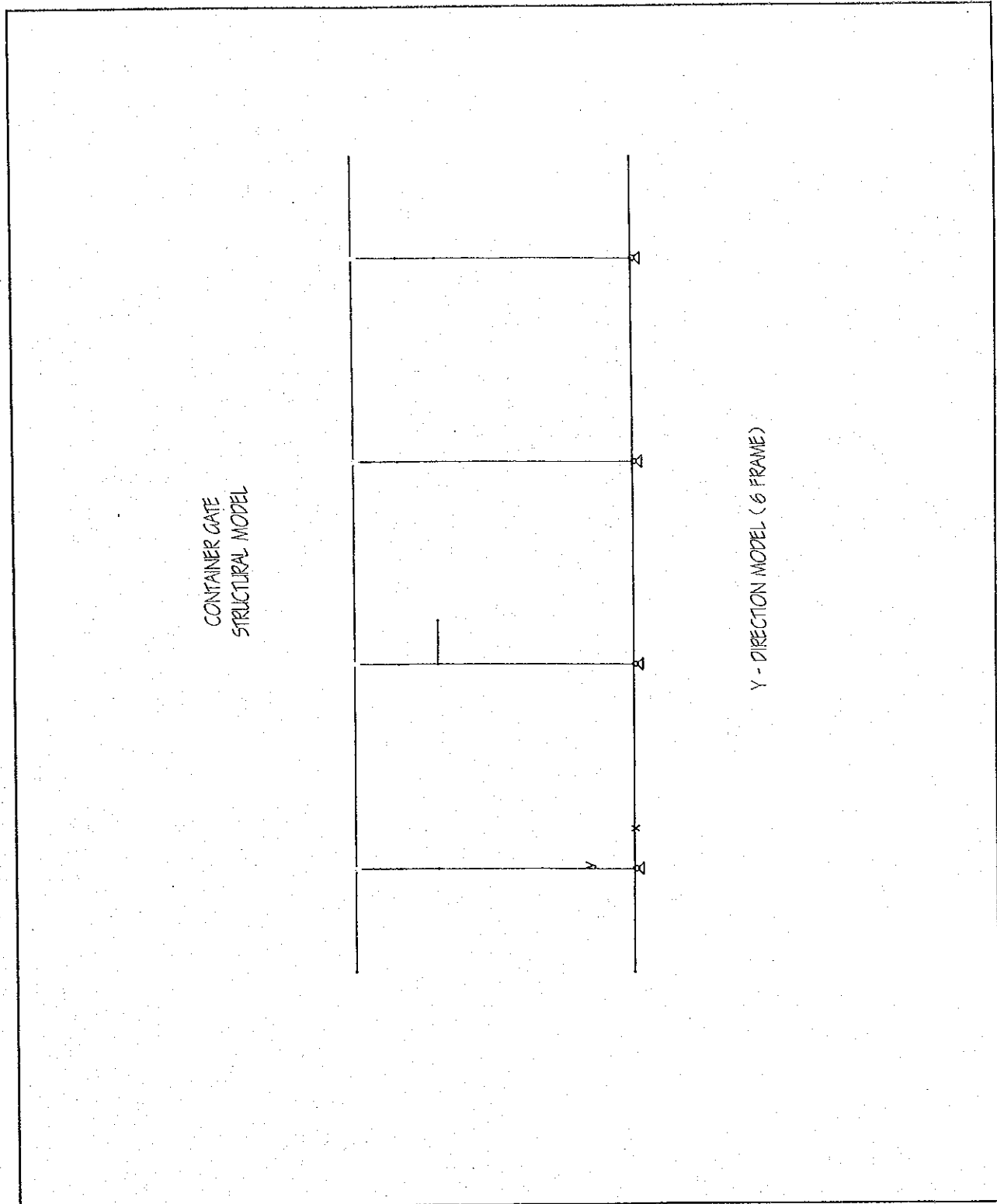
REACTION

DL Node	Rx	Ry	Rz	Mx	My	Mz	
1	0.268	14.357	0	0	0	0	0
2	0.112	21.011	0	0	0	0	0
3	0.131	16.549	0	0	0	0	0
4	0.097	36.618	0	0	0	0	0
5	0.028	38.386	0	0	0	0	0
6	-0.032	36.659	0	0	0	0	0
7	-0.238	25.633	0	0	0	0	0
8	-0.178	30.922	0	0	0	0	0
9	-0.188	14.561	0	0	0	0	0

LL Node	Rx	Ry	Rz	Mx	My	Mz	
1	0.161	8.822	0	0	0	0	0
2	0.013	16.329	0	0	0	0	0
3	0.062	3.544	0	0	0	0	0
4	0.037	8.573	0	0	0	0	0
5	0.011	8.346	0	0	0	0	0
6	-0.012	8.537	0	0	0	0	0
7	-0.212	3.894	0	0	0	0	0
8	0.071	18.106	0	0	0	0	0
9	-0.13	9.216	0	0	0	0	0

SL Node	Rx	Ry	Rz	Mx	My	Mz	
1	-0.56	-1.249	0	0	0	0	0
2	-0.774	-0.125	0	0	0	0	0
3	-0.73	0.538	0	0	0	0	0
4	-0.713	0.125	0	0	0	0	0
5	-0.659	0.182	0	0	0	0	0
6	-0.556	-0.308	0	0	0	0	0
7	-2.668	-7.345	0	0	0	0	0
8	-2.673	7.251	0	0	0	0	0
9	-0.366	0.933	0	0	0	0	0

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
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PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page	65 / 178

Container Gate

Model Y- direction 6 FRAME

Node Coordinate

Node No.	x (m)	y (m)	z (m)	z (m)
1	0	0	0	0
2	6	0	0	0
3	12	0	0	0
4	18	0	0	0
5	-3	0	0	0
6	21	0	0	0
7	0	5.45	0	0
8	6	5.45	0	0
9	12	5.45	0	0
10	18	5.45	0	0
11	0	6.55	0	0
12	6	6.55	0	0
13	12	6.55	0	0
14	18	6.55	0	0
15	0	7.85	0	0
16	6	7.85	0	0
17	12	7.85	0	0
18	18	7.85	0	0
19	-3	7.85	0	0
20	21	7.85	0	0
21	7.3	5.45	0	0

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page	66 / 178

Element data				
Member No.	node 1	node 2	length (m)	
1	1	2	6	
2	2	3	6	
3	3	4	6	
4	5	1	3	
5	4	6	3	
6	1	7	5.45	
7	2	8	5.45	
8	3	9	5.45	
9	4	10	5.45	
10	7	11	1.1	
11	8	12	1.1	
12	9	13	1.1	
13	10	14	1.1	
14	11	15	1.3	
15	12	16	1.3	
16	13	17	1.3	
17	14	18	1.3	
18	19	15	3	
19	18	20	3	
20	15	16	6	
21	16	17	6	
22	17	18	6	
23	8	21	1.3	

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page	67 / 178

Section			
Membe group	section	direction	
1	Custom1	bd-40x80	0
2	Custom1	bd-40x80	0
3	Custom1	bd-40x80	0
4	Custom1	bd-40x80	0
5	Custom1	bd-40x80	0
6	Custom1	bd-40x40	0
7	Custom1	bd-40x40	0
8	Custom1	bd-40x40	0
9	Custom1	bd-40x40	0
10	Custom1	bd-40x40	0
11	Custom1	bd-40x40	0
12	Custom1	bd-40x40	0
13	Custom1	bd-40x40	0
14	Custom1	bd-35x35	0
15	Custom1	bd-35x35	0
16	Custom1	bd-35x35	0
17	Custom1	bd-35x35	0
18	W	W12x40	0
19	W	W12x40	0
20	W	W12x40	0
21	W	W12x40	0
22	W	W12x40	0
23	Custom1	bd-30x30	0

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.	Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.	Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page 68 / 178

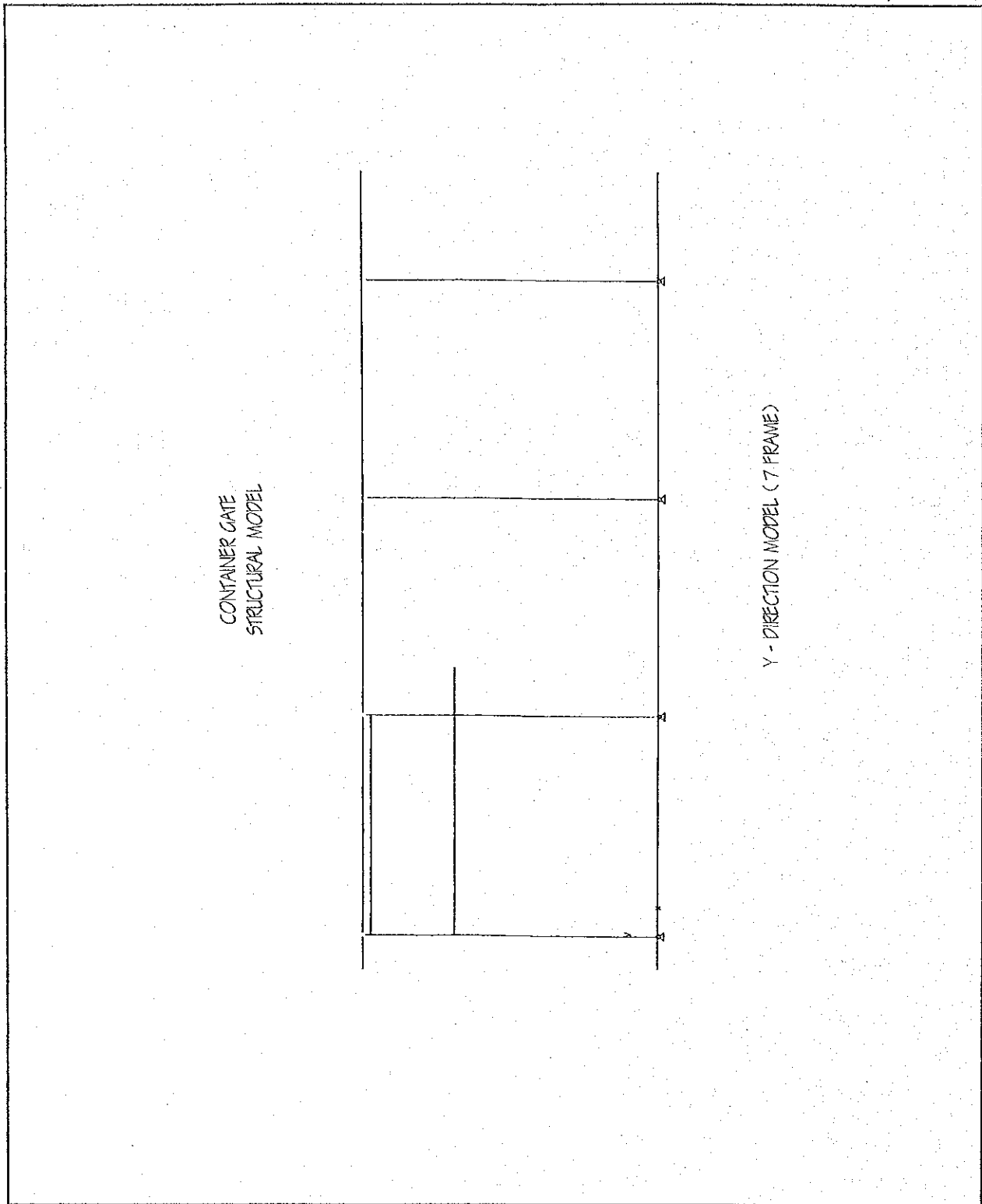
REACTION

DL Node	Rx	Ry	Rz	Mx	My	Mz
1	-0.121	39.002	0	0	0	0
2	0.113	37.724	0	0	0	0
3	-0.059	37.208	0	0	0	0
4	0.066	39.11	0	0	0	0

LL Node	Rx	Ry	Rz	Mx	My	Mz
1	-0.207	6.361	0	0	0	0
2	0.541	8.608	0	0	0	0
3	-0.194	4.819	0	0	0	0
4	-0.139	7.042	0	0	0	0

SL Node	Rx	Ry	Rz	Mx	My	Mz
1	-0.734	-1.526	0	0	0	0
2	-1.027	0.805	0	0	0	0
3	-0.807	-0.75	0	0	0	0
4	-0.732	1.471	0	0	0	0

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page	68 / 178



PROJECT: Detailed Design on Port Reactivation Project In La Union Province	Calc. File No.	Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.	Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	Page	70 / 178

Container Gate

Model Y- direction 7 FRAME

Node Coordinate

Node No.	x (m)	y (m)	z (m)
1	0	0	0
2	6	0	0
3	12	0	0
4	18	0	0
5	0	5.45	0
6	6	5.45	0
7	12	5.45	0
8	18	5.45	0
9	0	6.55	0
10	6	6.55	0
11	12	6.55	0
12	18	6.55	0
13	0	7.65	0
14	6	7.65	0
15	0	7.85	0
16	6	7.85	0
17	12	7.85	0
18	18	7.85	0
19	7.3	5.45	0
20	-3	7.85	0
21	21	7.85	0
22	-3	0	0
23	21	0	0
24	3	7.85	0
25	9	7.85	0
26	15	7.85	0

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page	2 / 178

Element data

Member No.	node 1	node 2	length (m)
1	1	2	6
2	2	3	6
3	3	4	6
4	1	5	5.45
5	2	6	5.45
6	3	7	5.45
7	4	8	5.45
8	5	9	1.1
9	6	10	1.1
10	7	11	1.1
11	8	12	1.1
12	9	13	1.1
13	10	14	1.1
14	13	15	0.2
15	14	16	0.2
16	11	17	1.3
17	12	18	1.3
18	5	6	6
19	13	14	6
20	6	19	1.3
21	15	24	3
22	20	15	3
23	16	25	3
24	17	26	3
25	18	21	3
26	22	1	3
27	4	23	3
28	24	16	3
29	25	17	3
30	26	18	3

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.	Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.	Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page 22 / 178

Section			
Membe group	section	direction	
1 Custom1	bd-40x80		0
2 Custom1	bd-40x80		0
3 Custom1	bd-40x80		0
4 Custom1	bd-45x45		0
5 Custom1	bd-45x45		0
6 Custom1	bd-40x40		0
7 Custom1	bd-40x40		0
8 Custom1	bd-45x45		0
9 Custom1	bd-45x45		0
10 Custom1	bd-40x40		0
11 Custom1	bd-40x40		0
12 Custom1	bd-45x45		0
13 Custom1	bd-45x45		0
14 Custom1	bd-45x45		0
15 Custom1	bd-45x45		0
16 Custom1	bd-35x35		0
17 Custom1	bd-35x35		0
18 Custom1	bd-30x65		0
19 Custom1	bd-30x65		0
20 Custom1	bd-30x30		0
21 W	W12x40		0
22 W	W12x40		0
23 W	W12x40		0
24 W	W12x40		0
25 W	W12x40		0
26 Custom1	bd-40x80		0
27 Custom1	bd-40x80		0
28 W	W12x40		0
29 W	W12x40		0
30 W	W12x40		0

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.	Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.	Checked by	A.MORIOKA
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REACTION

DL

Node	Rx	Ry	Rz	Mx	My	Mz
1	0.374	35.841	0	0	0	0
2	-0.408	34.967	0	0	0	0
3	-0.006	15.178	0	0	0	0
4	0.039	19.307	0	0	0	0

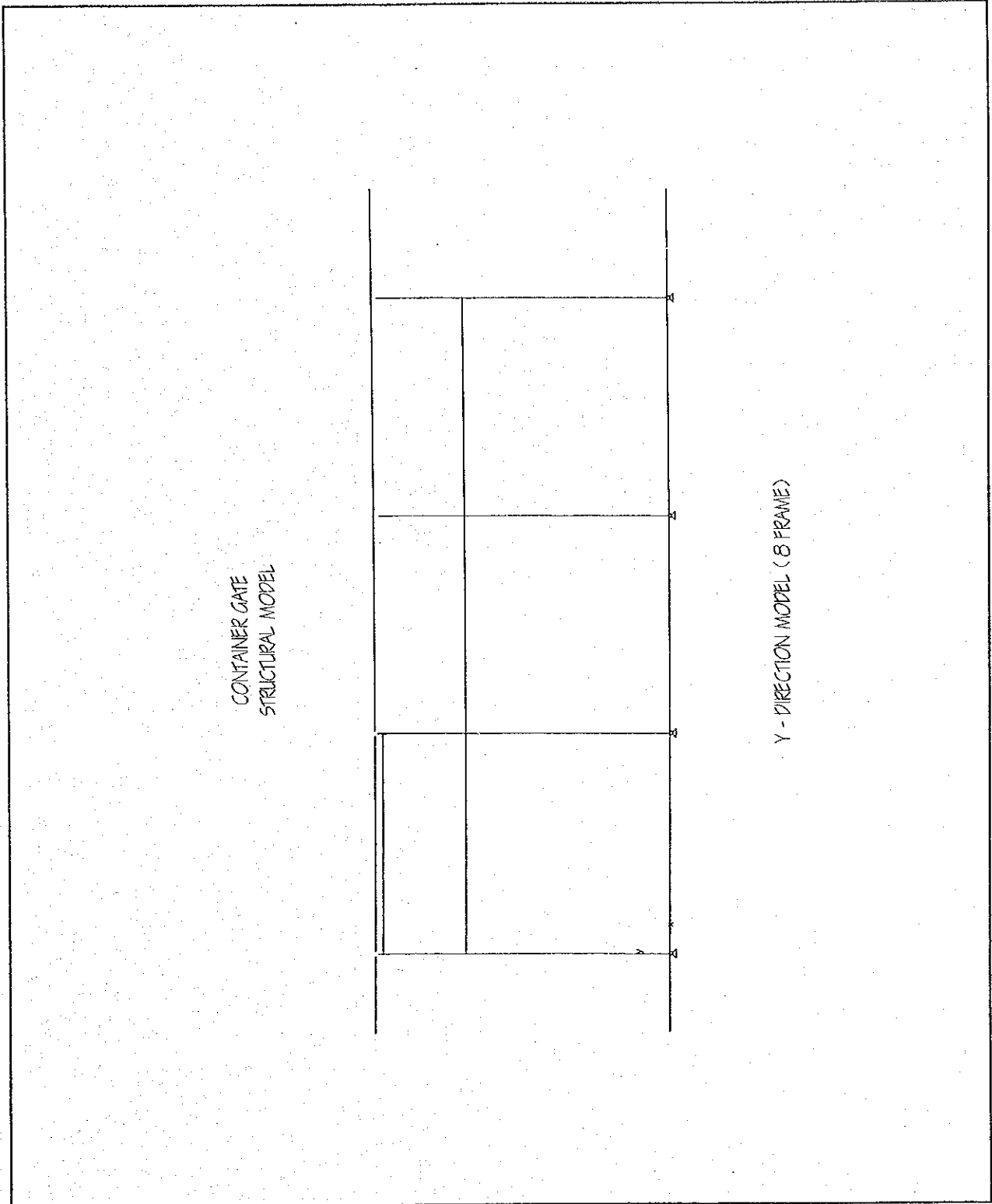
LL

Node	Rx	Ry	Rz	Mx	My	Mz
1	0.057	3.76	0	0	0	0
2	-0.046	6.653	0	0	0	0
3	-0.002	4.81	0	0	0	0
4	-0.009	3.055	0	0	0	0

SL

Node	Rx	Ry	Rz	Mx	My	Mz
1	-2.823	-6.046	0	0	0	0
2	-3.029	5.377	0	0	0	0
3	-0.334	0.192	0	0	0	0
4	-0.314	0.477	0	0	0	0

PROJECT: Detailed Design on Port Reactivation Project In La Union Province	Calc. File No.		Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page	28 / 78



PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page	25 / 178

Container Gate

Model Y- direction 8 FRAME

Node Coordinate

Node No.	x (m)	y (m)	z (m)
1	0	0	0
2	6	0	0
3	12	0	0
4	18	0	0
5	0	5.45	0
6	6	5.45	0
7	12	5.45	0
8	18	5.45	0
9	0	6.55	0
10	6	6.55	0
11	12	6.55	0
12	18	6.55	0
13	0	7.65	0
14	6	7.65	0
15	0	7.85	0
16	6	7.85	0
17	12	7.85	0
18	18	7.85	0
19	-3	7.85	0
20	21	7.85	0
21	-3	0	0
22	21	0	0
23	3	7.85	0
24	9	7.85	0
25	15	7.85	0

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page	26 / 78

Element data

Member No.	node 1	node 2	length (m)	
1	1	2	6	
2	2	3	6	
3	3	4	6	
4	1	5	5.45	
5	2	6	5.45	
6	3	7	5.45	
7	4	8	5.45	
8	5	9	1.1	
9	6	10	1.1	
10	7	11	1.1	
11	8	12	1.1	
12	9	13	1.1	
13	10	14	1.1	
14	13	15	0.2	
15	14	16	0.2	
16	11	17	1.3	
17	12	18	1.3	
18	5	6	6	
19	13	14	6	
20	15	23	3	
21	19	15	3	
22	16	24	3	
23	17	25	3	
24	18	20	3	
25	21	1	3	
26	4	22	3	
27	23	16	3	
28	24	17	3	
29	25	18	3	
30	6	7	6	
31	7	8	6	

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page	22 / 78

Section			
Membe group	section	direction	
1	Custom1	bd-40x80	0
2	Custom1	bd-40x80	0
3	Custom1	bd-40x80	0
4	Custom1	bd-45x45	0
5	Custom1	bd-45x45	0
6	Custom1	bd-40x40	0
7	Custom1	bd-40x40	0
8	Custom1	bd-45x45	0
9	Custom1	bd-45x45	0
10	Custom1	bd-40x40	0
11	Custom1	bd-40x40	0
12	Custom1	bd-45x45	0
13	Custom1	bd-45x45	0
14	Custom1	bd-45x45	0
15	Custom1	bd-45x45	0
16	Custom1	bd-35x35	0
17	Custom1	bd-35x35	0
18	Custom1	bd-30x65	0
19	Custom1	bd-30x65	0
20	W	W12x40	0
21	W	W12x40	0
22	W	W12x40	0
23	W	W12x40	0
24	W	W12x40	0
25	Custom1	bd-40x80	0
26	Custom1	bd-40x80	0
27	W	W12x40	0
28	W	W12x40	0
29	W	W12x40	0
30	Custom1	bd-30x40	0
31	Custom1	bd-30x40	0

PROJECT: Detailed Design on Port Reactivation Project In La Union Province	Calc. File No.	Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.	Checked by	A.MORIOKA
SUBJECT: Structural Input	Date	July-02	Page <i>28</i> / 178

REACTION

DL Node	Rx	Ry	Rz	Mx	My	Mz	
1	0.564	38.367	0	0	0	0	0
2	-0.462	43.118	0	0	0	0	0
3	0.01	24.896	0	0	0	0	0
4	-0.112	22.998	0	0	0	0	0

LL Node	Rx	Ry	Rz	Mx	My	Mz	
1	0.469	11.783	0	0	0	0	0
2	-0.208	23.461	0	0	0	0	0
3	0.055	22.675	0	0	0	0	0
4	-0.316	11.289	0	0	0	0	0

SL Node	Rx	Ry	Rz	Mx	My	Mz	
1	-2.107	-4.876	0	0	0	0	0
2	-2.372	3.647	0	0	0	0	0
3	-1.437	-0.442	0	0	0	0	0
4	-1.185	1.671	0	0	0	0	0

DESIGN CALCULATION COVER SHEET

Project	Detailed Design on Port Reactivation Project in La Union Province.	Project Code	JC1N004
Section	BUILDING WORKS	Calc. File No.	
Sub-Section	CONTAINER GATE	Calc. Index No.	

Subject:

STRUCTURAL DESIGN FOR SPREAD FOUNDATIONS

Calculation Objective:

The objective of the calculation is to provide a safe structure for the occupation of the building, by the use of the Republic of El Salvador and American design standards.

References, Calculation Notes and Comments

The Structural Analysis has been made using the program: "STAAD-III rev 21.1W, RESEARCH ENGINEERS, Inc.". The analysis of the structure considers only the concrete frames to resist the lateral forces, not considering the walls in the model.

One model for the structure has been constructed:

1- For the calculation of the Seismic and Dead & Live load.

The Key for the STAAD-III rev 21.1W program is attached for future convenience.

All the design has been made by calculations sheet created for the project in Microsoft Excel, and based in the following bibliography:

1. Building Code Requirements for Structural Concrete (318M-99), American Concrete Institute (ACI).
2. Technical Specification for Seismic Design, Ministry of Public Works, El Salvador, 2001.
3. AISC, American Institute of Steel Construction, ninth Edition, 1989.
4. Technical Specification for Wind Design, Ministry of Public Works, El Salvador, 1997.
5. UBC, Uniform Building Code, Volume 2: Structural Engineering Design Provisions, 1997.

Rev	Prepared		No. of Pages	Checked		Reviewed		Superseded by Calc No.
	by	Date		by	Date	by	Date	
O	R.MARTINEZ	Aug-02	7	A. MORIOKA	Aug-02	田村	14 Aug 02	
A	<i>[Signature]</i>			<i>[Signature]</i>				
B								
C								

PROJECT: Detailed Design on Port Reactivation Project In La Union Province	Calc. File No.	Prepared by	H.WATANABE
SECTION: Container Gate	Calc. Index No.	Checked by	A.MORIOKA
SUBJECT: Vertical reactions	Date	July-02	Page 1/3

Reaction of each point

	1	2	3	4	5	6	7	8	9
A	24.1	23.0	35.8	39.0	39.0	39.0	35.8	38.4	24.1
	26.2	11.3	3.8	6.4	6.4	6.4	3.8	11.8	26.2
	50.3	34.3	39.6	45.4	45.4	45.4	39.6	50.2	50.3
B	24.0	30.6	16.5	36.6	38.4	37.7	25.6	40.6	24.1
	26.0	30.8	3.9	8.6	8.4	8.6	4.2	32.7	26.2
	50.0	61.4	20.4	45.2	46.8	46.3	29.8	73.3	50.3
C	24.1	40.6	25.6	37.7	38.4	36.6	16.5	30.6	24.0
	26.2	32.7	4.2	8.6	8.4	8.6	3.9	30.8	26.0
	50.3	73.3	29.8	46.3	46.8	45.2	20.4	61.4	50.0
D	24.1	38.4	35.8	39.1	39.1	39.1	19.3	23.0	24.1
	26.2	11.8	3.8	7.0	7.0	7.0	3.1	11.3	26.2
	50.3	50.2	39.6	46.1	46.1	46.1	22.4	34.3	50.3

upper line DL
 middle line LL
 lower line TL=DL+LL

Total dead load = 1128.4 ton

Seismic load = 164.03 ton

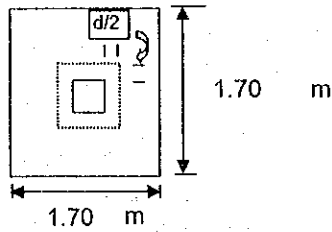
PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.	Prepared by	R.Martinez
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FOOTING DESIGN

Design for foundation F-1

a) Punching

For Column



$\phi = 0.85$

Dead load Pd =	35.80	ton
Live load PL =	3.80	ton
Seismic Ps =	17.90	ton
1.4D + 1.7L =	56.58	ton
0.75(1.4D + 1.7L + 1.87S) =	67.54	ton
Pu =	67.54	ton
d =	46.23	cm
Column width =	40.00	cm
Column base =	40.00	cm
bo = 4(c+d) =	344.92	cm

Th = 55 cm
 fc = 210 kg/cm²
 20.59 Mpa

Concrete shear strength, Vc ACI 11.12

$Vc1 = \phi(1+2/\beta_c)\sqrt{f_c} \text{ bod}/6 = 313.70 \text{ ton}$
 $\beta_c = 1.000$
 $Vc2 = \phi(2+\alpha_s d/b_o)\sqrt{f_c} \text{ bod}/12 = 132.60 \text{ ton}$
 $\alpha_s = 40$
 $Vc3 = \phi(1/3)\sqrt{f_c} \text{ bod} = 209.13$
 $Vc = 132.60 > 67.54 \text{ o.k!!!}$

b) Foundation Size

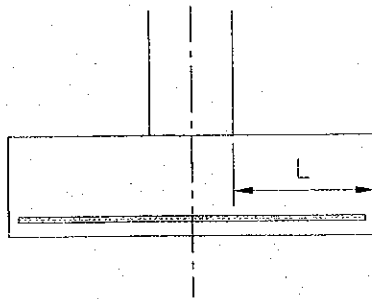
Soil Capacity = 20 ton/m² P = 54.27 ton

Square Foundation, Size = 1.65 m, ok!

Soil reaction = 18.78 ton/m²

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c) Reinforcing Steel



$$f_y = 4200 \text{ kg/cm}^2$$

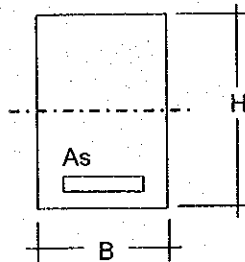
Moment generated by pile reaction

$$M = [(B - B_{\text{column}})/2]^2 \times \text{Soil reaction} / 2$$

$$L = 0.65 \text{ m}$$

$$M_1 = 1.4D + 1.7L = 5.17 \text{ ton-m}$$

$$M_2 = 0.75(1.4D + 1.7L + 1.87S) = 8.06 \text{ ton-m}$$



$$H = 55.00 \text{ cm}$$

$$b = 40.00 \text{ cm}$$

$$f_c = 280 \text{ kg/cm}^2$$

$$f_y = 4200 \text{ kg/cm}^2$$

Force for design: $M_u z-z = 8.06 \text{ ton-m}$

$$d = 46.23 \text{ cm}$$

$$\text{Clear cover} = 5.00 \text{ cm}$$

$$f_y^2 / 1.7b f_c A_s^2 - f_y d A_s + M_u / \phi = 0 \quad \phi = 0.90$$

$$926.47 A_s^2 - 194166 A_s + 895339.39 = 0 \quad A_s = 4.72 \text{ cm}^2$$

$$A_{s\text{min}} = (4/3)A_{s\text{req}}$$

$$(4/3)A_{s\text{req}} = 6.29 \text{ cm}^2$$

$$(14/f_y) b d = 6.16 \text{ cm}^2$$

$$A_{s\text{min}} = 6.16 \text{ cm}^2$$

$$A_{s\text{max}} : \rho b = 0.0459 \quad A_{s\text{max}} (0.75\rho b) = 63.73 \text{ cm}^2$$

$$A_s = 6.16 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{\text{max}}$$

$$\text{Bar denomination, } N = 7$$

$$\text{Bar Area } (A_v) = 3.88 \text{ cm}^2$$

$$\text{Number of bars} = 1.59 \quad \text{Use } 2 - N7$$

$$\text{Pitch} = 25.24 \text{ cm}$$

$$7 @ 25 \text{ cm}$$

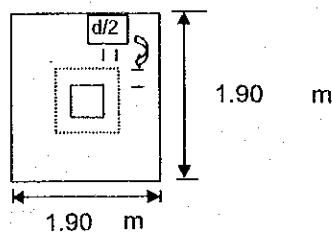
PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	R.Martinez
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FOOTING DESIGN

Design for foundation F-2

a) Punching

For Column



$$\phi = 0.85$$

Dead load Pd =	38.40	ton
Live load PL =	11.80	ton
Seismic Ps =	19.20	ton
1.4D + 1.7L =	73.82	ton
0.75(1.4D + 1.7L + 1.87S) =	82.29	ton
Pu =	82.29	ton
d =	46.23	cm
Column width =	40.00	cm
Column base =	40.00	cm
bo = 4(c+d) =	344.92	cm

$$Th = 55 \text{ cm}$$

$$f_c = 210 \text{ kg/cm}^2$$

$$20.59 \text{ Mpa}$$

Concrete shear strength, Vc ACI 11.12

$$Vc1 = \phi(1+2/\beta_c)\sqrt{f_c} \text{ bod}/6 = 313.70 \text{ ton}$$

$$\beta_c = 1.000$$

$$Vc2 = \phi(2+\alpha_s d/bo)\sqrt{f_c} \text{ bod}/12 = 132.60 \text{ ton}$$

$$\alpha_s = 40$$

$$Vc3 = \phi(1/3)\sqrt{f_c} \text{ bod} = 209.13$$

$$Vc = 132.60 > 82.29 \text{ o.k!!!}$$

b) Foundation Size

$$\text{Soil Capacity} = 20 \text{ ton/m}^2$$

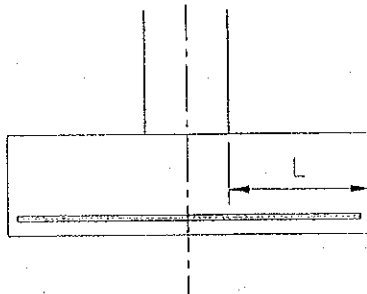
$$P = 68.71 \text{ ton}$$

$$\text{Square Foundation, Size} = 1.85 \text{ m, ok!}$$

$$\text{Soil reaction} = 19.03 \text{ ton/m}^2$$

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c) Reinforcing Steel



$f_y = 4200 \text{ kg/cm}^2$

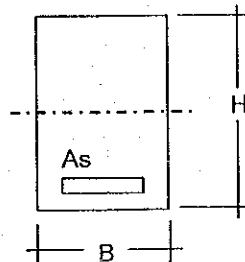
Moment generated by pile reaction

$M = [(B - B_{\text{column}})/2]^2 \times \text{Soil reaction} / 2$

$L = 0.75 \text{ m}$

$M_1 = 1.4D + 1.7L = 7.19 \text{ ton-m}$

$M_2 = 0.75(1.4D + 1.7L + 1.87S) = 10.41 \text{ ton-m}$



$H = 55.00 \text{ cm}$

$b = 40.00 \text{ cm}$

$f_c = 280 \text{ kg/cm}^2$

$f_y = 4200 \text{ kg/cm}^2$

Force for design: $M_u \text{ z-z} = 10.41 \text{ ton-m}$

$d = 46.23 \text{ cm}$

Clear cover = 5.00 cm

$f_y^2 / 1.7b f_c A_s^2 - f_y d A_s + M_u / \phi = \phi = 0.90$

$926.47 A_s^2 - 194166 A_s + 1156785.1 = 0 \quad A_s = 6.14 \text{ cm}^2$

$A_{smin} = (4/3)A_{sreq} :$
 $(4/3)A_{sreq} = 8.18 \text{ cm}^2$
 $(14/f_y) b d = 6.16 \text{ cm}^2$

$A_{smin} = 6.16 \text{ cm}^2$

$A_{smax} :$
 $\rho_b = 0.0459 \quad A_{smax} (0.75\rho_b) = 63.73 \text{ cm}^2$

$A_s = 6.16 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$

Bar denomination, $N = 7$

Bar Area (A_v) = 3.88 cm^2

Number of bars = $1.59 \quad \text{Use } 2 - N7$

Pitch = 25.24 cm

$7 @ 25 \text{ cm}$

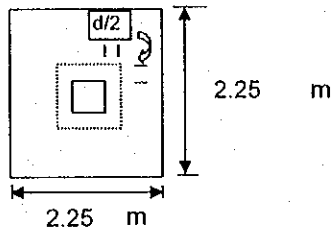
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FOOTING DESIGN

Design for foundation F-3

a) Punching

For Column



$$\phi = 0.85$$

Dead load PD =	40.60	ton
Live load PL =	32.70	ton
Seismic Ps =	20.30	ton
1.4D + 1.7L =	112.43	ton
0.75(1.4D + 1.7L + 1.87S) =	112.79	ton
Pu =	112.79	ton
d =	46.23	cm
Column width =	45.00	cm
Column base =	45.00	cm
bo = 4(c+d) =	364.92	cm

Th = 55 cm

f_c = 210 kg/cm²
20.59 Mpa

Concrete shear strength, V_c ACI 11.12

β_c = 1.000

$$V_{c1} = \phi(1+2/\beta_c)\sqrt{f_c} \text{ bod}/6 = 331.89 \text{ ton}$$

α_s = 40

$$V_{c2} = \phi(2+\alpha_s d/b_o)\sqrt{f_c} \text{ bod}/12 = 138.66 \text{ ton}$$

$$V_{c3} = \phi(1/3)\sqrt{f_c} \text{ bod} = 221.26$$

V_c = 138.66 > 112.79 o.k!!!

b) Foundation Size

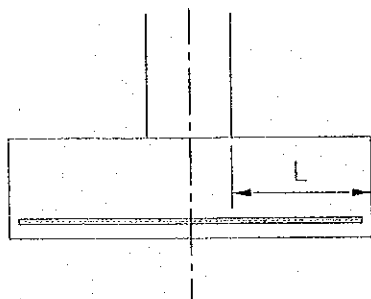
Soil Capacity = 20 ton/m² P = 99.98 ton

Square Foundation, Size = 2.24 m, ok!

Soil reaction = 19.75 ton/m²

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c) Reinforcing Steel



$$f_y = 4200 \text{ kg/cm}^2$$

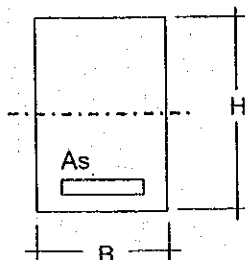
Moment generated by pile reaction

$$M = [(B-B_{\text{column}})/2]^2 \times \text{Soil reaction} / 2$$

$$L = 0.90 \text{ m}$$

$$M_1 = 1.4D + 1.7L = 11.24 \text{ ton-m}$$

$$M_2 = 0.75(1.4D + 1.7L + 1.87S) = 14.53 \text{ ton-m}$$



$$H = 55.00 \text{ cm}$$

$$b = 45.00 \text{ cm}$$

$$f_c = 280 \text{ kg/cm}^2$$

$$f_y = 4200 \text{ kg/cm}^2$$

Force for design: $M_u \text{ z-z} = 14.53 \text{ ton-m}$

$$d = 46.23 \text{ cm}$$

$$\text{Clear cover} = 5.00 \text{ cm}$$

$$f_y^2 / 1.7b f_c A_s^2 - f_y d A_s + M_u / \phi = 0 \quad \phi = 0.90$$

$$823.53 A_s^2 - 194166 A_s + 1614024.2 = 0 \quad A_s = 8.63 \text{ cm}^2$$

$$\begin{aligned} A_{s\text{min}} &= (4/3)A_{s\text{req}} \\ (4/3)A_{s\text{req}} &= 11.50 \text{ cm}^2 \\ (14/f_y) b d &= 6.93 \text{ cm}^2 \end{aligned} \quad A_{s\text{min}} = 6.93 \text{ cm}^2$$

$$A_{s\text{max}} : \quad \rho b = 0.0459 \quad A_{s\text{max}} (0.75\rho b) = 71.69 \text{ cm}^2$$

$$A_s = 8.63 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{\text{max}}$$

$$\text{Bar denomination, } N = 8$$

$$\text{Bar Area } (A_v) = 5.07 \text{ cm}^2$$

$$\text{Number of bars} = 1.70 \quad \text{Use } 2 - N8$$

$$\text{Pitch} = 29.92 \text{ cm} \quad 8 @ 29.5 \text{ cm}$$