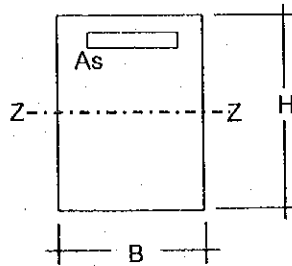


PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.	Prepared by	R.Martinez
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BEAM DESIGN (B-5)

Outer End



$H = 40.00$ cm
 $b = 25.00$ cm
 $f_c = 280$ kg/cm²
 $f_y = 4200$ kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE OF LOAD	MOMENT
	Mz-z
Dead Load	2.70
Live Load	1.20
Seismic Load x	5.01
Seismic Load z	0.81

COMBINATION	Mu z-z
C1	5.82
C2	11.39
C3	5.50

15.66
 3.72 C1 = 1.4 DL + 1.7 LL
 C2 = 0.75(1.4DL + 1.7LL + 1.87SLy)
 56.55 C3 = 0.75(1.4DL + 1.7LL + 1.87SLz)

Force for design: $Mu\ z-z = 11.39$ ton-m

$d = 32.46$ cm Clear cover = 5.00 cm

$f_y^2/1.7bf_c As^2 - f_y d As + Mu/\phi = 0$ $\phi = 0.90$

$1482.4As^2 - 136332 As + 1265725 = 0$ $As = 10.48$ cm²

$As_{min} = (4/3)As_{req}$:

$(4/3)As_{req} = 13.97$ cm²
 $(14/f_y) b d = 2.71$ cm² } $As_{min} = 2.71$ cm²

$As_{max} : \rho b = 0.0459$ $As_{max} (0.75\rho b) = 27.97$ cm²

$As = 10.48$ cm² o.k!! $As < A_{max}$

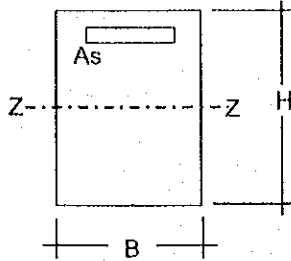
Bar denomination, N = 8 Bar Area (A_v) = 5.07 cm²

Number of bars = 2.07 Use 3 - N 8

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BEAM DESIGN (B-5)

Inner end



H = cm

b = cm

f_c = kg/cm²

f_y = kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE OF LOAD	MOMENT
	Mz-z

Dead Load	6.27
Live Load	1.80
Seismic Load x	2.95
Seismic Load z	5.96

COMBINATION	Mu z-z
C1	11.84
C2	13.02
C3	17.24

C1 = 1.4 DL + 1.7 LL

C2 = 0.75(1.4DL + 1.7LL + 1.87SL_y)

C3 = 0.75(1.4DL + 1.7LL + 1.87SL_z)

Force for design: Mu z-z = ton-m

d = cm

Clear cover = cm

$f_y^2/1.7bf_c As^2 - f_yd As + Mu/\phi = 0$ $\phi = 0.90$

$1482.4As^2 - 140532 As + 1915266.7 = 0$ $As = 16.50 \text{ cm}^2$

As_{min} = (4/3)As_{req} :

$(4/3)As_{req} = 22.00 \text{ cm}^2$
 $(14/f_y) b d = 2.79 \text{ cm}^2$

} As_{min} = 2.79 cm²

As_{max} : $\rho b = 0.0459$ As_{max} (0.75ρb) = 28.83 cm²

As = 16.50 cm² o.k!! As < A_{max}

Bar denomination, N =

Bar Area (A_v) = 5.07 cm²

Number of bars = 3.26 Use 4 - N 8

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b) Shear Reinforcement

Base = cm $f_y = \frac{4200}{411.89}$ kg/cm²

d = cm $f_c = \frac{280}{27.46}$ Mpa

$V_c = (1/6) \sqrt{f_c} b o d = 11.92$ ton

$V_n = V_c + V_s$ $V_s = V_u / \phi - V_c$ $\phi = 0.85$

TYPE OF LOAD	SHEAR
	Vy

Dead Load	3.79
Live Load	1.53
Seismic Load x	1.70
Seismic Load z	1.55

COMBINATION	Vy
C1	7.91
C2	8.31
C3	8.10

C1 = 1.4 DL + 1.7 LL
 C2 = 0.75(1.4DL + 1.7LL + 1.87SLy)
 C3 = 0.75(1.4DL + 1.7LL + 1.87SLz)

Force for design: $V_u = \frac{8.31}{}$ ton

$V_s = (2,141.1)$ kg

Bar denomination = Bar area = 0.71 cm²

of legs = Spacing, $S_{req} = -93.54$ cm

Max. spacing of shear reinforcement.

$d/2 = 16.73$ cm }
 30 mm = 30 cm } $S_2 = 16.73$ cm

$(1/3) (\sqrt{f_c} / 6) b w d = 746523.9$ Newton
 76,122 kg > V_s , o.k.

$S_2 = 16.73$ cm

Minimun Shear Reinforcement

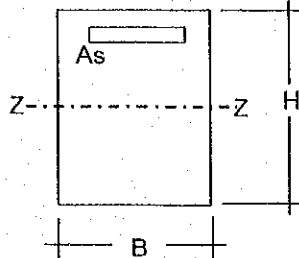
$A_v = (1/3) b w S / f_y$ $S_3 = 3 A_v f_y / b w$ $S_3 = 4402.5$ cm

Use 2 legs of N 3 @ 16 cm

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BEAM DESIGN (B-7)

Column end



$H = 60.00$ cm
 $b = 35.00$ cm
 $f_c = 280$ kg/cm²
 $f_y = 4200$ kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE OF LOAD	MOMENT Mz-z
Dead Load	24.99
Live Load	4.47
Seismic Load x	28.94
Seismic Load z	28.00

COMBINATION	Mu z-z
C1	42.59
C2	72.53
C3	71.21

$C1 = 1.4 DL + 1.7 LL$
 $C2 = 0.75(1.4DL + 1.7LL + 1.87SLy)$
 $C3 = 0.75(1.4DL + 1.7LL + 1.87SLz)$

Force for design: $Mu z-z = 72.53$ ton-m

$d = 52.14$ cm Clear cover = 5.00 cm

$f_y^2/1.7bf_c As^2 - f_yd As + Mu/\phi = 0$ $\phi = 0.90$

$1058.8As^2 - 218999 As + 8058566.7 = 0$ $As = 47.88$ cm²

$As_{min} = (4/3)As_{req}$:

$(4/3)As_{req} = 63.84$ cm²
 $(14/f_y) b d = 6.08$ cm² } $As_{min} = 6.08$ cm²

$As_{max} : \rho b = 0.0459$ $As_{max} (0.75\rho b) = 62.89$ cm²

$As = 47.88$ cm² o.k!! $As < A_{max}$

Bar denomination, $N = 10$ Bar Area (A_v) = 8.17 cm²

Number of bars = 5.86 Use 6 - N10

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b) Shear Reinforcement

Base = cm

$f_y = \frac{4200}{411.89}$ kg/cm²

d = cm

$f_c = \frac{280}{27.46}$ kg/cm²
Mpa

$V_c = (1/6) \sqrt{f_c} b o d = 16.26$ ton

$V_n = V_c + V_s$ $V_s = V_u/\phi - V_c$ $\phi = 0.85$

TYPE OF LOAD	SHEAR
	V _y

COMBINATION	V _y
C1	21.41
C2	25.57
C3	22.26

Dead Load	12.55
Live Load	2.26
Seismic Load x	6.78
Seismic Load z	4.42

C1 = 1.4 DL + 1.7 LL
C2 = 0.75(1.4DL + 1.7LL + 1.87SL_y)
C3 = 0.75(1.4DL + 1.7LL + 1.87SL_z)

Force for design: $V_u = \text{input } 25.57$ ton

$V_s = 13,822.4$ kg

Bar denomination =

Bar area = 1.27 cm²

of legs =

Spacing, S_{req} = 40.14 cm

Max. spacing of shear reinforcement.

$d/2 = 26.07$ cm
 $30 \text{ mm} = 30$ cm
 $S_2 = 26.07$ cm

$(1/3) (\sqrt{f_c} / 6) b w d = 1017929$ Newton
103,796 kg > V_s, o.k.

$S_2 = 26.07$ cm

Minimun Shear Reinforcement

$A_v = (1/3) b w S / f_y$

$S_3 = 3 A_v f_y / b w$

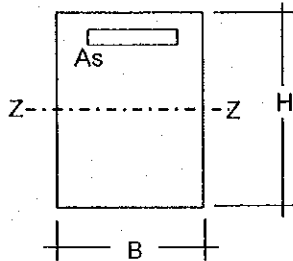
$S_3 = 8944.7$ cm

Use 2 legs of N 4 @ 26 cm

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BEAM DESIGN (B-7A)

Column End



H = 60.00 cm
 b = 35.00 cm
 $f_c = 280 \text{ kg/cm}^2$
 $f_y = 4200 \text{ kg/cm}^2$

Forces and Moments, from Structural Analysis (ton , m) :

TYPE OF LOAD	MOMENT
	Mz-z
Dead Load	32.51
Live Load	2.90
Seismic Load x	15.80
Seismic Load z	10.90

COMBINATION	Mu z-z
C1	50.44
C2	59.99
C3	53.12

C1 = 1.4 DL + 1.7 LL
 C2 = 0.75(1.4DL + 1.7LL + 1.87SLy)
 C3 = 0.75(1.4DL + 1.7LL + 1.87SLz)

Force for design: $Mu \text{ z-z} = 59.99 \text{ ton-m}$

d = 53.14 cm

Clear cover = 4.00 cm

$f_y^2/1.7b^2f_c As^2 - f_y d As + Mu/\phi = 0 \quad \phi = 0.90$

$1058.8As^2 - 223199 As + 6665833.3 = 0 \quad As = 36.02 \text{ cm}^2$

$As_{min} = (4/3)As_{req}$:

$(4/3)As_{req} = 48.03 \text{ cm}^2$
 $(14/f_y) b d = 6.20 \text{ cm}^2$ } $As_{min} = 6.20 \text{ cm}^2$

$As_{max} : \rho_b = 0.0459 \quad As_{max} (0.75\rho_b) = 64.10 \text{ cm}^2$

$As = 36.02 \text{ cm}^2 \quad \text{o.k!! } As < A_{max}$

Bar denomination, N = 10

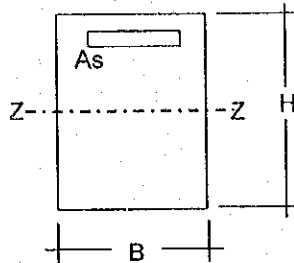
Bar Area (A_v) = 8.17 cm²

Number of bars = 4.41 Use 5 - N10

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BEAM DESIGN (B-2a)

Outer End



H = 65.00 cm

b = 35.00 cm

f_c = 280 kg/cm²

f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE OF LOAD	MOMENT
	Mz-z

Dead Load	16.17
Live Load	2.72
Seismic Load x	1.25
Seismic Load z	30.00

COMBINATION	Mu z-z
C1	27.26
C2	22.20
C3	62.52

15.66

3.72 C1 = 1.4 DL + 1.7 LL

C2 = 0.75(1.4DL + 1.7LL + 1.87SL_y)

56.55 C3 = 0.75(1.4DL + 1.7LL + 1.87SL_z)

Force for design: Mu z-z = 62.52 ton-m

d = 57.14 cm

Clear cover = 5.00 cm

$f_y^2/1.7b^2f_c As^2 - f_y d As + Mu/\phi = 0$ $\phi = 0.90$

$1058.8As^2 - 239999 As + 6946833.3 = 0$ $As = 34.06 \text{ cm}^2$

Asmin = (4/3)Asreq :

$$\left. \begin{array}{l} (4/3)Asreq = 45.42 \text{ cm}^2 \\ (14/f_y) b d = 6.67 \text{ cm}^2 \end{array} \right\} Asmin = 6.67 \text{ cm}^2$$

Asmax : $\rho b = 0.0459$ Asmax (0.75ρb) = 68.92 cm²

As = 34.06 cm² o.k!! As < Amax

Bar denomination, N = 10

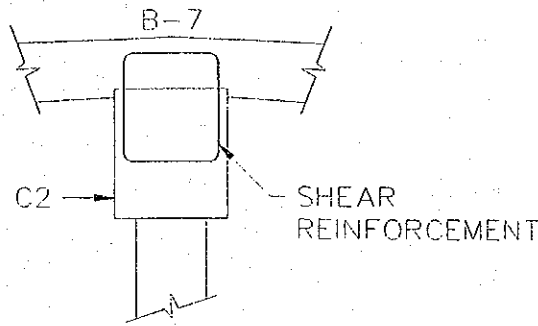
Bar Area (A_v) = 8.17 cm²

Number of bars = 4.17

Use 5 - N10

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BEAM-COLUMN CONNECTION
5-C Axis Intersection



$f_c = 280 \text{ kg/cm}^2$

$f_y = 4200 \text{ kg/cm}^2$

Forces from Structural Analysis (ton , m) :

TYPE OF LOAD	SHEAR
	V_y
Dead Load	12.87
Live Load	3.85
Seismic Load x	4.70
Seismic Load z	3.71

COMBINATION	V_y
C1	24.56
C2	25.01
C3	23.63

$C1 = 1.4 \text{ DL} + 1.7 \text{ LL}$
 $C2 = 0.75(1.4\text{DL} + 1.7\text{LL} + 1.87\text{SL}_y)$
 $C3 = 0.75(1.4\text{DL} + 1.7\text{LL} + 1.87\text{SL}_z)$

Use $V_y = 25.01 \text{ ton}$

Shear

$A_{vf} = V_n / f_y \mu$

$V_n = V_u / \phi$ $\phi = 0.85$ $V_u = 29.43 \text{ ton}$

$\mu = 1.0\lambda$

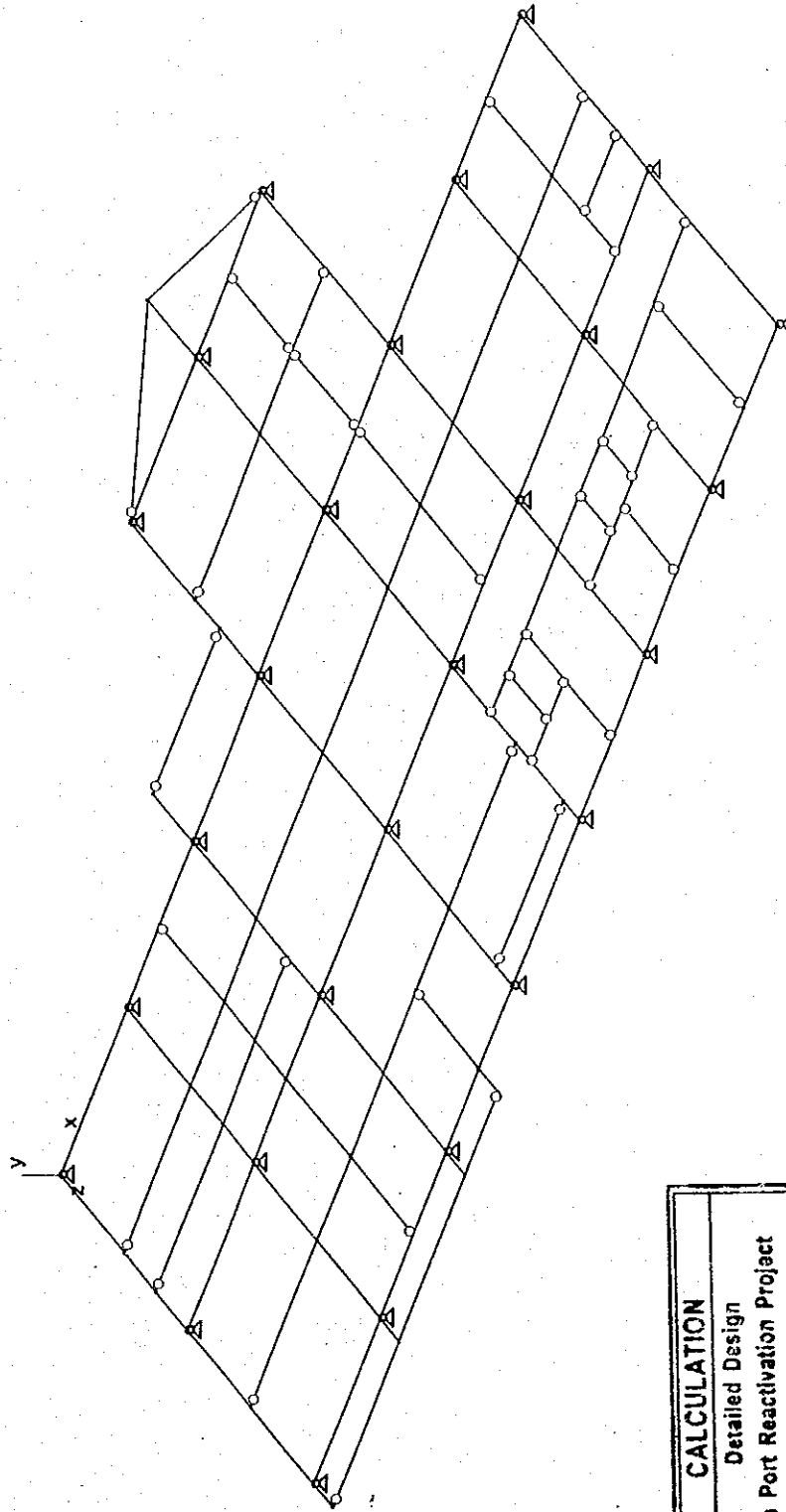
$\lambda = 1.0$ (Normal weight concrete) Increase = 1.2

$A_{vf} = 8.41 \text{ cm}^2$

Bar denomination = 4 Bar area = 1.27 cm^2

of legs = 2 # of hoops = 3.32

Use 4 Hoops N 4



FOUNDATION BEAM MODEL

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Administration Building Foundation Beam

Node Coordinate

Node No.	x (m)	y (m)	z (m)
1	0	0	0
2	6	0	0
3	12	0	0
4	18	0	0
5	24	0	0
6	30	0	0
7	36	0	0
8	42	0	0
9	0	0	8
10	6	0	8
11	12	0	8
12	18	0	8
13	24	0	8
14	30	0	8
15	36	0	8
16	42	0	8
17	0	0	16
18	6	0	16
19	12	0	16
20	18	0	16
21	24	0	16
22	30	0	16
23	36	0	16
24	42	0	16
25	18	0	-8
26	24	0	-8
27	30	0	-8
28	0	0	17.2
29	6	0	17.2
30	12	0	17.2
31	24	0	-11
32	12	0	-2.5
33	18	0	-2.5
34	18	0	-4
35	24	0	-4
36	30	0	-4
37	27	0	0
38	27	0	-8
39	27	0	-4
40	0	0	6
41	6	0	6
42	12	0	6
43	12	0	4
44	18	0	4
45	24	0	4
46	30	0	4
47	36	0	4

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Node Coordinate

Node No.	x (m)	y (m)	z (m)
48	42	0	4
49	27	0	8
50	27	0	4
51	39	0	0
52	39	0	8
53	39	0	4
54	0	0	12
55	6	0	12
56	12	0	12
57	18	0	12
58	24	0	12
59	9	0	0
60	9	0	8
61	9	0	16
62	9	0	6
63	9	0	12
64	15	0	16
65	15	0	12
66	15	0	17.2
67	18	0	15
68	24	0	15
69	24	0	10.5
70	30	0	10.5
71	36	0	10.5
72	42	0	10.5
73	27	0	16
74	27	0	10.5
75	24	0	13
76	27	0	13
77	25.5	0	10.5
78	25.5	0	13
79	42	0	6
80	39	0	6
81	39	0	16
82	39	0	10.5
83	30	0	12.5
84	36	0	12.5
85	32	0	10.5
86	34	0	10.5
87	32	0	12.5
88	34	0	12.5
89	33	0	12.5
90	33	0	16
91	0	0	4
92	6	0	4
93	9	0	4

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CHECKED BY	A.M.	JULY/02

Element data

Member No.	node 1	node 2	length (m)	Member No.	node 1	node 2	length (m)
1	1	2	6	50	34	25	4
2	2	59	3	51	35	26	4
3	3	4	6	52	36	27	4
4	4	5	6	53	25	31	6.708
5	5	37	3	54	31	27	6.708
6	6	7	6	55	34	35	6
7	7	51	3	56	35	39	3
8	9	10	6	57	37	6	3
9	10	60	3	58	38	27	3
10	11	12	6	59	39	36	3
11	12	13	6	60	39	38	4
12	13	49	3	61	37	39	4
13	14	15	6	62	40	91	2
14	15	52	3	63	41	92	2
15	17	18	6	64	42	43	2
16	18	61	3	65	40	41	6
17	19	64	3	66	41	62	3
18	20	21	6	67	43	3	4
19	21	73	3	68	44	4	4
20	22	90	3	69	45	5	4
21	23	81	3	70	46	6	4
22	9	40	2	71	47	7	4
23	17	54	4	72	48	8	4
24	10	41	2	73	43	44	6
25	18	55	4	74	44	45	6
26	11	42	2	75	45	50	3
27	19	56	4	76	46	47	6
28	12	44	4	77	47	53	3
29	20	67	1	78	49	14	3
30	13	45	4	79	50	46	3
31	21	68	1	80	50	37	4
32	14	46	4	81	49	50	4
33	22	83	3.5	82	51	8	3
34	15	47	4	83	52	16	3
35	23	84	3.5	84	53	48	3
36	16	79	2	85	53	51	4
37	24	72	5.5	86	52	80	2
38	4	33	2.5	87	54	9	4
39	5	35	4	88	55	10	4
40	6	36	4	89	56	11	4
41	25	26	6	90	57	12	4
42	26	38	3	91	58	69	1.5
43	28	17	1.2	92	54	55	6
44	29	18	1.2	93	55	63	3
45	30	19	1.2	94	56	65	3
46	26	31	3	95	57	58	3
47	3	32	2.5	96	59	59	3
48	33	34	1.5	97	60	60	3
49	32	33	6	98	61	61	3

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CHECKED BY	A. M.	JULY 02

Member No.	node 1	node 2	length (m)	Member No.	node 1	node 2	length (m)
99	62	42	3	150	92	2	4
100	63	56	3	151	93	59	4
101	62	93	2	152	91	92	6
102	60	62	2	153	92	93	3
103	63	60	4	154	93	43	3
104	61	63	4				
105	64	20	3				
106	65	57	3				
107	64	65	4				
108	66	64	1.2				
109	28	29	6				
110	29	30	6				
111	30	66	3				
112	67	57	3				
113	68	75	2				
114	67	68	6				
115	69	13	2.5				
116	70	14	2.5				
117	71	15	2.5				
118	72	16	2.5				
119	69	77	1.5				
120	70	85	2				
121	71	82	3				
122	73	22	3				
123	74	70	3				
124	73	76	3				
125	75	58	1				
126	76	74	2.5				
127	75	78	1.5				
128	77	74	1.5				
129	78	76	1.5				
130	78	77	2.5				
131	79	48	2				
132	80	53	2				
133	80	79	3				
134	81	24	3				
135	82	72	3				
136	81	82	5.5				
137	83	70	2				
138	84	71	2				
139	83	87	2				
140	85	86	2				
141	86	71	2				
142	87	89	1				
143	88	84	2				
144	87	85	2				
145	88	86	2				
146	89	88	1				
147	90	23	3				
148	90	89	3.5				
149	91	1	4				

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CHECKED BY	A. M.	JULY/02

Section					
Member group	section	direction	Member group	section	direction
1	Custom	bd-35x8	0	51	Custom bd-35x8
2	Custom	bd-40x8	0	52	Custom bd-35x8
3	Custom	bd-40x8	0	53	Custom bd-30x6
4	Custom	bd-40x8	0	54	Custom bd-30x6
5	Custom	bd-40x8	0	55	Custom bd-30x6
6	Custom	bd-40x8	0	56	Custom bd-30x6
7	Custom	bd-40x8	0	57	Custom bd-40x8
8	Custom	bd-35x8	0	58	Custom bd-35x8
9	Custom	bd-40x8	0	59	Custom bd-30x6
10	Custom	bd-40x8	0	60	Custom bd-25x4
11	Custom	bd-40x8	0	61	Custom bd-25x4
12	Custom	bd-40x8	0	62	Custom bd-35x8
13	Custom	bd-40x8	0	63	Custom bd-40x8
14	Custom	bd-40x8	0	64	Custom bd-40x8
15	Custom	bd-35x8	0	65	Custom bd-30x6
16	Custom	bd-40x8	0	66	Custom bd-30x6
17	Custom	bd-40x8	0	67	Custom bd-40x8
18	Custom	bd-40x8	0	68	Custom bd-40x8
19	Custom	bd-40x8	0	69	Custom bd-40x8
20	Custom	bd-40x8	0	70	Custom bd-40x8
21	Custom	bd-40x8	0	71	Custom bd-40x8
22	Custom	bd-35x8	0	72	Custom bd-40x8
23	Custom	bd-35x8	0	73	Custom bd-30x6
24	Custom	bd-40x8	0	74	Custom bd-30x6
25	Custom	bd-40x8	0	75	Custom bd-30x6
26	Custom	bd-40x8	0	76	Custom bd-30x6
27	Custom	bd-40x8	0	77	Custom bd-30x6
28	Custom	bd-40x8	0	78	Custom bd-40x8
29	Custom	bd-40x8	0	79	Custom bd-30x6
30	Custom	bd-40x8	0	80	Custom bd-25x4
31	Custom	bd-40x8	0	81	Custom bd-25x4
32	Custom	bd-40x8	0	82	Custom bd-40x8
33	Custom	bd-40x8	0	83	Custom bd-40x8
34	Custom	bd-40x8	0	84	Custom bd-30x6
35	Custom	bd-40x8	0	85	Custom bd-25x4
36	Custom	bd-40x8	0	86	Custom bd-25x4
37	Custom	bd-40x8	0	87	Custom bd-35x8
38	Custom	bd-35x8	0	88	Custom bd-40x8
39	Custom	bd-35x8	0	89	Custom bd-40x8
40	Custom	bd-35x8	0	90	Custom bd-40x8
41	Custom	bd-35x8	0	91	Custom bd-40x8
42	Custom	bd-35x8	0	92	Custom bd-30x6
43	Custom	bd-30x6	0	93	Custom bd-30x6
44	Custom	bd-30x6	0	94	Custom bd-30x6
45	Custom	bd-30x6	0	95	Custom bd-30x6
46	Custom	bd-35x8	0	96	Custom bd-40x8
47	Custom	bd-40x8	0	97	Custom bd-40x8
48	Custom	bd-35x8	0	98	Custom bd-40x8
49	Custom	bd-30x6	0	99	Custom bd-30x6
50	Custom	bd-35x8	0	100	Custom bd-30x6

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Section			Section			
Member group	section	direction	Member group	section	direction	
101	Custom	bd-25x4	0	151	Custom bd-25x4	0
102	Custom	bd-25x4	0	152	Custom bd-30x6	0
103	Custom	bd-25x4	0	153	Custom bd-30x6	0
104	Custom	bd-25x4	0	154	Custom bd-30x6	0
105	Custom	bd-40x8	0			
106	Custom	bd-30x6	0			
107	Custom	bd-25x4	0			
108	Custom	bd-25x4	0			
109	Custom	bd-30x6	0			
110	Custom	bd-30x6	0			
111	Custom	bd-25x4	0			
112	Custom	bd-40x8	0			
113	Custom	bd-40x8	0			
114	Custom	bd-30x6	0			
115	Custom	bd-40x8	0			
116	Custom	bd-40x8	0			
117	Custom	bd-40x8	0			
118	Custom	bd-40x8	0			
119	Custom	bd-30x6	0			
120	Custom	bd-30x6	0			
121	Custom	bd-30x6	0			
122	Custom	bd-40x8	0			
123	Custom	bd-30x6	0			
124	Custom	bd-25x4	0			
125	Custom	bd-40x8	0			
126	Custom	bd-25x4	0			
127	Custom	bd-25x4	0			
128	Custom	bd-30x6	0			
129	Custom	bd-25x4	0			
130	Custom	bd-25x4	0			
131	Custom	bd-40x8	0			
132	Custom	bd-25x4	0			
133	Custom	bd-25x4	0			
134	Custom	bd-40x8	0			
135	Custom	bd-30x6	0			
136	Custom	bd-30x6	0			
137	Custom	bd-40x8	0			
138	Custom	bd-40x8	0			
139	Custom	bd-30x6	0			
140	Custom	bd-30x6	0			
141	Custom	bd-30x6	0			
142	Custom	bd-30x6	0			
143	Custom	bd-30x6	0			
144	Custom	bd-25x4	0			
145	Custom	bd-25x4	0			
146	Custom	bd-30x6	0			
147	Custom	bd-40x8	0			
148	Custom	bd-25x4	0			
149	Custom	bd-35x8	0			
150	Custom	bd-40x8	0			

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Nodal Load

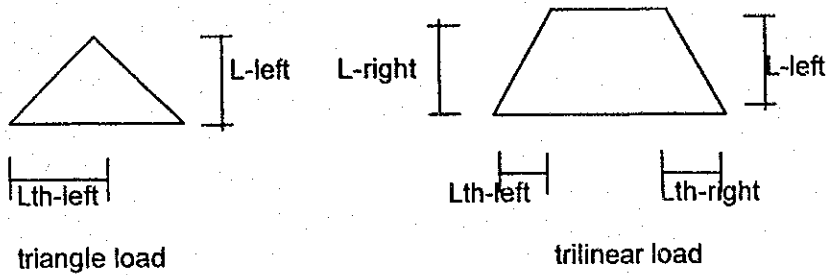
DL

Node No.	directio	(t)
84	Py	-0.89

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CHECKED BY	A. M.	JULY/02

Member Load

u : uniformly distributed load
 con : concentrated load
 Lth-left : length from left end
 Lth-right: length from right end
 L-left: load at left side
 L-right: load at right side



DL

member	load	type	Lth-left	Lth-right	L-left	L-right
53	Wy	u	-	-	-0.48	-
54	Wy	u	-	-	-0.48	-
65	Wy	u	-	-	-1.43	-
66	Wy	u	-	-	-1.43	-
101	Wy	trilinear	0	0	-1.43	-1.43
102	Wy	u	-	-	-1.43	-
1	Wy	u	-	-	-1.43	-
62	Wy	trilinear	0	0	-0.71	-0.71
23	Wy	u	-	-	-0.71	-
87	Wy	u	-	-	-0.71	-
109	Wy	u	-	-	-1.43	-
110	Wy	u	-	-	-1.43	-
104	Wy	u	-	-	-1.43	-
103	Wy	u	-	-	-0.71	-
2	Wy	u	-	-	-0.71	-
96	Wy	u	-	-	-0.71	-
100	Wy	u	-	-	-1.43	-
111	Wy	u	-	-	-1.43	-
107	Wy	u	-	-	-1.43	-
108	Wy	u	-	-	-1.43	-
105	Wy	trilinear	0	0	-0.71	-0.71
94	Wy	u	-	-	-0.71	-
106	Wy	u	-	-	-0.71	-
3	Wy	u	-	-	-1.43	-
47	Wy	u	-	-	-1.43	-
49	Wy	u	-	-	-0.35	-
114	Wy	u	-	-	-0.49	-
95	Wy	u	-	-	-0.49	-
4	Wy	u	-	-	-0.71	-
19	Wy	u	-	-	-1.43	-

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CHECKED BY		
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	A. M.	July/02

member	load	type	Lth-left	Lth-right	L-left	L-right
122	Wy	u	-	-	-1.43	-
127	Wy	u	-	-	-2.11	-
129	Wy	u	-	-	-2.11	-
130	Wy	u	-	-	-2.11	-
91	Wy	u	-	-	-2.11	-
125	Wy	u	-	-	-2.11	-
31	Wy	u	-	-	-1.43	-
113	Wy	u	-	-	-1.43	-
124	Wy	u	-	-	-2.11	-
126	Wy	u	-	-	-2.11	-
123	Wy	u	-	-	-1.06	-
12	Wy	u	-	-	-0.3	-
80	Wy	u	-	-	-1.43	-
81	Wy	u	-	-	-1.43	-
5	Wy	u	-	-	-1.43	-
57	Wy	u	-	-	-1.43	-
61	Wy	u	-	-	-1.43	-
59	Wy	trilinear	2	0	-1.43	-1.43
60	Wy	u	-	-	-1.43	-
58	Wy	u	-	-	-1.43	-
40	Wy	u	-	-	-0.71	-
52	Wy	u	-	-	-0.71	-
20	Wy	trilinear	1.5	0	-1.47	-1.47
147	Wy	trilinear	0	1.5	-1.47	-1.47
148	Wy	u	-	-	-1.43	-
146	Wy	u	-	-	-1.43	-
144	Wy	u	-	-	-1.43	-
145	Wy	u	-	-	-1.43	-
120	Wy	u	-	-	-1.43	-
141	Wy	u	-	-	-1.43	-
13	Wy	u	-	-	-1.43	-
6	Wy	u	-	-	-0.71	-
7	Wy	u	-	-	-0.71	-
85	Wy	trilinear	2	0	-1.43	-1.43
77	Wy	u	-	-	-1.43	-
84	Wy	trilinear	1.5	0	-1.43	-1.43
86	Wy	u	-	-	-1.43	-
132	Wy	u	-	-	-1.43	-
133	Wy	u	-	-	-1.43	-
14	Wy	trilinear	1.5	0	-1.43	-1.43
83	Wy	u	-	-	-1.43	-
136	Wy	u	-	-	-1.43	-
21	Wy	u	-	-	-1.43	-
134	Wy	u	-	-	-1.43	-
37	Wy	u	-	-	-1.43	-
72	Wy	u	-	-	-1.43	-
131	Wy	u	-	-	-1.43	-
149	Wy	trilinear	0	0	-0.71	-0.71
151	Wy	trilinear	0	0	-1.43	-1.43
1	Wy	u	-	-	-0.65	-
2	Wy	u	-	-	-0.743	-
3	Wy	u	-	-	-0.743	-

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CHECKED BY	A.M.	JULY/02

member	load	type	Lth-left	Lth-right	L-left	L-right
4	Wy	u	-	-	-0.743	-
5	Wy	u	-	-	-0.743	-
6	Wy	u	-	-	-0.743	-
7	Wy	u	-	-	-0.743	-
8	Wy	u	-	-	-0.65	-
9	Wy	u	-	-	-0.743	-
10	Wy	u	-	-	-0.743	-
11	Wy	u	-	-	-0.743	-
12	Wy	u	-	-	-0.743	-
13	Wy	u	-	-	-0.743	-
14	Wy	u	-	-	-0.743	-
15	Wy	u	-	-	-0.65	-
16	Wy	u	-	-	-0.743	-
17	Wy	u	-	-	-0.743	-
18	Wy	u	-	-	-0.743	-
19	Wy	u	-	-	-0.743	-
20	Wy	u	-	-	-0.743	-
21	Wy	u	-	-	-0.743	-
22	Wy	u	-	-	-0.65	-
23	Wy	u	-	-	-0.65	-
24	Wy	u	-	-	-0.743	-
25	Wy	u	-	-	-0.743	-
26	Wy	u	-	-	-0.743	-
27	Wy	u	-	-	-0.743	-
28	Wy	u	-	-	-0.743	-
29	Wy	u	-	-	-0.743	-
30	Wy	u	-	-	-0.743	-
31	Wy	u	-	-	-0.743	-
32	Wy	u	-	-	-0.743	-
33	Wy	u	-	-	-0.743	-
34	Wy	u	-	-	-0.743	-
35	Wy	u	-	-	-0.743	-
36	Wy	u	-	-	-0.743	-
37	Wy	u	-	-	-0.743	-
38	Wy	u	-	-	-0.65	-
39	Wy	u	-	-	-0.65	-
40	Wy	u	-	-	-0.65	-
41	Wy	u	-	-	-0.65	-
42	Wy	u	-	-	-0.65	-
43	Wy	u	-	-	-0.453	-
44	Wy	u	-	-	-0.453	-
45	Wy	u	-	-	-0.453	-
46	Wy	u	-	-	-0.65	-
47	Wy	u	-	-	-0.743	-
48	Wy	u	-	-	-0.65	-
49	Wy	u	-	-	-0.418	-
50	Wy	u	-	-	-0.65	-
51	Wy	u	-	-	-0.65	-
52	Wy	u	-	-	-0.65	-
53	Wy	u	-	-	-0.418	-
54	Wy	u	-	-	-0.418	-
55	Wy	u	-	-	-0.418	-

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CHECKED BY	A.M.	July 02

member	load	type	Lth-left	Lth-right	L-left	L-right
56	Wy	u	-	-	-0.418	-
57	Wy	u	-	-	-0.743	-
58	Wy	u	-	-	-0.65	-
59	Wy	u	-	-	-0.418	-
60	Wy	u	-	-	-0.232	-
61	Wy	u	-	-	-0.232	-
62	Wy	u	-	-	-0.65	-
63	Wy	u	-	-	-0.743	-
64	Wy	u	-	-	-0.743	-
65	Wy	u	-	-	-0.418	-
66	Wy	u	-	-	-0.418	-
67	Wy	u	-	-	-0.743	-
68	Wy	u	-	-	-0.743	-
69	Wy	u	-	-	-0.743	-
70	Wy	u	-	-	-0.743	-
71	Wy	u	-	-	-0.743	-
72	Wy	u	-	-	-0.743	-
73	Wy	u	-	-	-0.418	-
74	Wy	u	-	-	-0.418	-
75	Wy	u	-	-	-0.418	-
76	Wy	u	-	-	-0.418	-
77	Wy	u	-	-	-0.418	-
78	Wy	u	-	-	-0.743	-
79	Wy	u	-	-	-0.418	-
80	Wy	u	-	-	-0.232	-
81	Wy	u	-	-	-0.232	-
82	Wy	u	-	-	-0.743	-
83	Wy	u	-	-	-0.743	-
84	Wy	u	-	-	-0.418	-
85	Wy	u	-	-	-0.232	-
86	Wy	u	-	-	-0.232	-
87	Wy	u	-	-	-0.65	-
88	Wy	u	-	-	-0.743	-
89	Wy	u	-	-	-0.743	-
90	Wy	u	-	-	-0.743	-
91	Wy	u	-	-	-0.743	-
92	Wy	u	-	-	-0.418	-
93	Wy	u	-	-	-0.418	-
94	Wy	u	-	-	-0.418	-
95	Wy	u	-	-	-0.418	-
96	Wy	u	-	-	-0.743	-
97	Wy	u	-	-	-0.743	-
98	Wy	u	-	-	-0.743	-
99	Wy	u	-	-	-0.418	-
100	Wy	u	-	-	-0.418	-
101	Wy	u	-	-	-0.232	-
102	Wy	u	-	-	-0.232	-
103	Wy	u	-	-	-0.232	-
104	Wy	u	-	-	-0.232	-
105	Wy	u	-	-	-0.743	-
106	Wy	u	-	-	-0.418	-
107	Wy	u	-	-	-0.232	-

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CHECKED BY	A. M.	JULY/02

member	load	type	Lth-left	Lth-right	L-left	L-right
108	Wy	u	-	-	-0.232	-
109	Wy	u	-	-	-0.418	-
110	Wy	u	-	-	-0.418	-
111	Wy	u	-	-	-0.232	-
112	Wy	u	-	-	-0.743	-
113	Wy	u	-	-	-0.743	-
114	Wy	u	-	-	-0.418	-
115	Wy	u	-	-	-0.743	-
116	Wy	u	-	-	-0.743	-
117	Wy	u	-	-	-0.743	-
118	Wy	u	-	-	-0.743	-
119	Wy	u	-	-	-0.418	-
120	Wy	u	-	-	-0.418	-
121	Wy	u	-	-	-0.418	-
122	Wy	u	-	-	-0.743	-
123	Wy	u	-	-	-0.418	-
124	Wy	u	-	-	-0.232	-
125	Wy	u	-	-	-0.743	-
126	Wy	u	-	-	-0.232	-
127	Wy	u	-	-	-0.232	-
128	Wy	u	-	-	-0.418	-
129	Wy	u	-	-	-0.232	-
130	Wy	u	-	-	-0.232	-
131	Wy	u	-	-	-0.743	-
132	Wy	u	-	-	-0.232	-
133	Wy	u	-	-	-0.232	-
134	Wy	u	-	-	-0.743	-
135	Wy	u	-	-	-0.418	-
136	Wy	u	-	-	-0.418	-
137	Wy	u	-	-	-0.743	-
138	Wy	u	-	-	-0.743	-
139	Wy	u	-	-	-0.418	-
140	Wy	u	-	-	-0.418	-
141	Wy	u	-	-	-0.418	-
142	Wy	u	-	-	-0.418	-
143	Wy	u	-	-	-0.418	-
144	Wy	u	-	-	-0.232	-
145	Wy	u	-	-	-0.232	-
146	Wy	u	-	-	-0.418	-
147	Wy	u	-	-	-0.743	-
148	Wy	u	-	-	-0.232	-
149	Wy	u	-	-	-0.65	-
150	Wy	u	-	-	-0.743	-
151	Wy	u	-	-	-0.232	-
152	Wy	u	-	-	-0.418	-
153	Wy	u	-	-	-0.418	-
154	Wy	u	-	-	-0.418	-
1	Wy	u	-	-	-0.175	-
2	Wy	u	-	-	-0.175	-
3	Wy	u	-	-	-0.175	-
4	Wy	u	-	-	-0.175	-
8	Wy	u	-	-	-0.175	-

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CHECKED BY	A.M.	July/02

member	load	type	Lth-left	Lth-right	L-left	L-right
9	Wy	u	-	-	-0.175	-
10	Wy	u	-	-	-0.175	-
11	Wy	u	-	-	-0.175	-
15	Wy	u	-	-	-0.175	-
16	Wy	u	-	-	-0.175	-
17	Wy	u	-	-	-0.175	-
18	Wy	u	-	-	-0.175	-
22	Wy	u	-	-	-0.175	-
23	Wy	u	-	-	-0.175	-
24	Wy	u	-	-	-0.175	-
25	Wy	u	-	-	-0.175	-
26	Wy	u	-	-	-0.175	-
27	Wy	u	-	-	-0.175	-
28	Wy	u	-	-	-0.175	-
29	Wy	u	-	-	-0.175	-
38	Wy	u	-	-	-0.175	-
41	Wy	u	-	-	-0.175	-
43	Wy	u	-	-	-0.175	-
44	Wy	u	-	-	-0.175	-
45	Wy	u	-	-	-0.175	-
47	Wy	u	-	-	-0.175	-
48	Wy	u	-	-	-0.175	-
49	Wy	u	-	-	-0.175	-
50	Wy	u	-	-	-0.175	-
53	Wy	u	-	-	-0.175	-
55	Wy	u	-	-	-0.175	-
62	Wy	trilinear	0	0	-0.175	-0.175
63	Wy	trilinear	0	0	-0.175	-0.175
64	Wy	u	-	-	-0.175	-
65	Wy	u	-	-	-0.175	-
66	Wy	u	-	-	-0.175	-
67	Wy	u	-	-	-0.175	-
68	Wy	u	-	-	-0.175	-
73	Wy	u	-	-	-0.175	-
74	Wy	u	-	-	-0.175	-
87	Wy	u	-	-	-0.175	-
88	Wy	u	-	-	-0.175	-
89	Wy	u	-	-	-0.175	-
90	Wy	u	-	-	-0.175	-
92	Wy	u	-	-	-0.175	-
93	Wy	u	-	-	-0.175	-
94	Wy	u	-	-	-0.175	-
95	Wy	u	-	-	-0.175	-
96	Wy	u	-	-	-0.175	-
97	Wy	u	-	-	-0.175	-
98	Wy	u	-	-	-0.175	-
99	Wy	u	-	-	-0.175	-
100	Wy	u	-	-	-0.175	-
101	Wy	trilinear	0	0	-0.175	-0.175
102	Wy	u	-	-	-0.175	-
103	Wy	u	-	-	-0.175	-
104	Wy	u	-	-	-0.175	-

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CHECKED BY	A.M.	JULY/02

member	load	type	Lth-left	Lth-right	L-left	L-right
105	Wy	u	-	-	-0.175	-
106	Wy	u	-	-	-0.175	-
107	Wy	u	-	-	-0.175	-
108	Wy	u	-	-	-0.175	-
109	Wy	u	-	-	-0.175	-
110	Wy	u	-	-	-0.175	-
111	Wy	u	-	-	-0.175	-
112	Wy	u	-	-	-0.175	-
114	Wy	u	-	-	-0.175	-
5	Wy	u	-	-	-0.175	-
6	Wy	u	-	-	-0.175	-
7	Wy	u	-	-	-0.175	-
12	Wy	u	-	-	-0.175	-
13	Wy	u	-	-	-0.175	-
14	Wy	u	-	-	-0.175	-
19	Wy	u	-	-	-0.175	-
21	Wy	u	-	-	-0.175	-
30	Wy	u	-	-	-0.175	-
31	Wy	u	-	-	-0.175	-
32	Wy	u	-	-	-0.175	-
34	Wy	u	-	-	-0.175	-
36	Wy	u	-	-	-0.175	-
37	Wy	u	-	-	-0.175	-
39	Wy	u	-	-	-0.175	-
40	Wy	u	-	-	-0.175	-
42	Wy	u	-	-	-0.175	-
46	Wy	u	-	-	-0.175	-
51	Wy	u	-	-	-0.175	-
52	Wy	u	-	-	-0.175	-
54	Wy	u	-	-	-0.175	-
56	Wy	u	-	-	-0.175	-
57	Wy	u	-	-	-0.175	-
58	Wy	u	-	-	-0.175	-
59	Wy	u	-	-	-0.175	-
60	Wy	u	-	-	-0.175	-
61	Wy	u	-	-	-0.175	-
69	Wy	u	-	-	-0.175	-
70	Wy	u	-	-	-0.175	-
71	Wy	u	-	-	-0.175	-
72	Wy	u	-	-	-0.175	-
75	Wy	u	-	-	-0.175	-
76	Wy	u	-	-	-0.175	-
77	Wy	u	-	-	-0.175	-
78	Wy	u	-	-	-0.175	-
79	Wy	u	-	-	-0.175	-
80	Wy	u	-	-	-0.175	-
81	Wy	u	-	-	-0.175	-
82	Wy	u	-	-	-0.175	-
84	Wy	u	-	-	-0.175	-
85	Wy	u	-	-	-0.175	-
86	Wy	u	-	-	-0.175	-
113	Wy	u	-	-	-0.175	-

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CHECKED BY	A.M.	JULY/02

member	load	type	Lth-left	Lth-right	L-left	L-right
115	Wy	u	-	-	-0.175	-
116	Wy	u	-	-	-0.175	-
117	Wy	u	-	-	-0.175	-
118	Wy	u	-	-	-0.175	-
121	Wy	u	-	-	-0.175	-
122	Wy	u	-	-	-0.175	-
123	Wy	u	-	-	-0.175	-
124	Wy	u	-	-	-0.175	-
131	Wy	u	-	-	-0.175	-
132	Wy	u	-	-	-0.175	-
134	Wy	u	-	-	-0.175	-
135	Wy	u	-	-	-0.175	-
136	Wy	u	-	-	-0.175	-
91	Wy	u	-	-	-0.77	-
125	Wy	u	-	-	-0.77	-
126	Wy	u	-	-	-0.77	-
130	Wy	u	-	-	-1.53	-
120	Wy	u	-	-	-0.58	-
140	Wy	u	-	-	-0.58	-
141	Wy	u	-	-	-0.58	-
119	Wy	u	-	-	-0.17	-
127	Wy	u	-	-	-0.17	-
128	Wy	u	-	-	-0.17	-
129	Wy	u	-	-	-0.17	-
137	Wy	u	-	-	-0.17	-
138	Wy	u	-	-	-0.17	-
144	Wy	u	-	-	-0.17	-
145	Wy	u	-	-	-0.17	-
33	Wy	trilinear	1.5	1.5	-1.16	-1.16
139	Wy	triangle	1.5	-	-1.16	-
143	Wy	triangle	1.5	-	-1.16	-
148	Wy	trilinear	1.5	1.5	-3.32	-3.32
20	Wy	triangle	1.5	-	-1.16	-
147	Wy	triangle	1.5	-	-1.16	-
35	Wy	trilinear	1.5	1.5	-1.16	-1.16
136	Wy	trilinear	3	0	-0.77	-0.77
121	Py	con	1.5	1.5	-0.89	-0.89
83	Wy	u	-	-	-0.77	-
133	Wy	u	-	-	-0.77	-
149	Wy	trilinear	0	0	-0.175	-0.175
150	Wy	trilinear	0	0	-0.175	-0.175
151	Wy	trilinear	0	0	-0.175	-0.175
152	Wy	u	-	-	-0.175	-
153	Wy	u	-	-	-0.175	-
154	Wy	u	-	-	-0.175	-

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CHECKED BY	A. M.	JULY/02

Member Load

LL

member	load	type	Lth-left	Lth-right	L-left	L-right
1	Wy	u	-	-	-0.18	-
2	Wy	u	-	-	-0.18	-
3	Wy	u	-	-	-0.18	-
4	Wy	u	-	-	-0.18	-
5	Wy	u	-	-	-0.18	-
6	Wy	u	-	-	-0.18	-
7	Wy	u	-	-	-0.18	-
8	Wy	u	-	-	-0.18	-
9	Wy	u	-	-	-0.18	-
10	Wy	u	-	-	-0.18	-
11	Wy	u	-	-	-0.18	-
12	Wy	u	-	-	-0.18	-
13	Wy	u	-	-	-0.18	-
14	Wy	u	-	-	-0.18	-
15	Wy	u	-	-	-0.18	-
16	Wy	u	-	-	-0.18	-
17	Wy	u	-	-	-0.18	-
18	Wy	u	-	-	-0.18	-
19	Wy	u	-	-	-0.18	-
20	Wy	u	-	-	-0.18	-
21	Wy	u	-	-	-0.18	-
22	Wy	u	-	-	-0.18	-
23	Wy	u	-	-	-0.18	-
24	Wy	u	-	-	-0.18	-
25	Wy	u	-	-	-0.18	-
26	Wy	u	-	-	-0.18	-
27	Wy	u	-	-	-0.18	-
28	Wy	u	-	-	-0.18	-
29	Wy	u	-	-	-0.18	-
30	Wy	u	-	-	-0.18	-
31	Wy	u	-	-	-0.18	-
32	Wy	u	-	-	-0.18	-
34	Wy	u	-	-	-0.18	-
36	Wy	u	-	-	-0.18	-
38	Wy	u	-	-	-0.18	-
39	Wy	u	-	-	-0.18	-
40	Wy	u	-	-	-0.18	-
41	Wy	u	-	-	-0.18	-
42	Wy	u	-	-	-0.18	-
43	Wy	u	-	-	-0.18	-
44	Wy	u	-	-	-0.18	-
45	Wy	u	-	-	-0.18	-
46	Wy	u	-	-	-0.18	-
47	Wy	u	-	-	-0.18	-
48	Wy	u	-	-	-0.18	-
49	Wy	u	-	-	-0.18	-
50	Wy	u	-	-	-0.18	-
51	Wy	u	-	-	-0.18	-

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CHECKED BY	A.M.	JULY/02

member	load	type	Lth-left	Lth-right	L-left	L-right
52	Wy	u	-	-	-0.18	-
53	Wy	u	-	-	-0.18	-
54	Wy	u	-	-	-0.18	-
55	Wy	u	-	-	-0.18	-
56	Wy	u	-	-	-0.18	-
57	Wy	u	-	-	-0.18	-
58	Wy	u	-	-	-0.18	-
59	Wy	u	-	-	-0.18	-
60	Wy	u	-	-	-0.18	-
61	Wy	u	-	-	-0.18	-
62	Wy	trilinear	0	0	-0.18	-0.18
63	Wy	trilinear	0	0	-0.18	-0.18
64	Wy	u	-	-	-0.18	-
65	Wy	u	-	-	-0.18	-
66	Wy	u	-	-	-0.18	-
67	Wy	u	-	-	-0.18	-
68	Wy	u	-	-	-0.18	-
69	Wy	u	-	-	-0.18	-
70	Wy	u	-	-	-0.18	-
71	Wy	u	-	-	-0.18	-
72	Wy	u	-	-	-0.18	-
73	Wy	u	-	-	-0.18	-
74	Wy	u	-	-	-0.18	-
75	Wy	u	-	-	-0.18	-
76	Wy	u	-	-	-0.18	-
77	Wy	u	-	-	-0.18	-
78	Wy	u	-	-	-0.18	-
79	Wy	u	-	-	-0.18	-
80	Wy	u	-	-	-0.18	-
81	Wy	u	-	-	-0.18	-
82	Wy	u	-	-	-0.18	-
83	Wy	u	-	-	-0.18	-
84	Wy	u	-	-	-0.18	-
85	Wy	u	-	-	-0.18	-
86	Wy	u	-	-	-0.18	-
87	Wy	u	-	-	-0.18	-
88	Wy	u	-	-	-0.18	-
89	Wy	u	-	-	-0.18	-
90	Wy	u	-	-	-0.18	-
91	Wy	u	-	-	-0.18	-
92	Wy	u	-	-	-0.18	-
93	Wy	u	-	-	-0.18	-
94	Wy	u	-	-	-0.18	-
95	Wy	u	-	-	-0.18	-
96	Wy	u	-	-	-0.18	-
97	Wy	u	-	-	-0.18	-
98	Wy	u	-	-	-0.18	-
99	Wy	u	-	-	-0.18	-
100	Wy	u	-	-	-0.18	-
101	Wy	trilinear	0	0	-0.18	-0.18
102	Wy	u	-	-	-0.18	-
103	Wy	u	-	-	-0.18	-

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CHECKED BY	A. M.	JULY/02

member	load	type	Lth-left	Lth-right	L-left	L-right
104	Wy	u	-	-	-0.18	-
105	Wy	u	-	-	-0.18	-
106	Wy	u	-	-	-0.18	-
107	Wy	u	-	-	-0.18	-
108	Wy	u	-	-	-0.18	-
109	Wy	u	-	-	-0.18	-
110	Wy	u	-	-	-0.18	-
111	Wy	u	-	-	-0.18	-
112	Wy	u	-	-	-0.18	-
113	Wy	u	-	-	-0.18	-
114	Wy	u	-	-	-0.18	-
115	Wy	u	-	-	-0.18	-
116	Wy	u	-	-	-0.18	-
117	Wy	u	-	-	-0.18	-
118	Wy	u	-	-	-0.18	-
119	Wy	u	-	-	-0.18	-
121	Wy	u	-	-	-0.18	-
122	Wy	u	-	-	-0.18	-
123	Wy	u	-	-	-0.18	-
124	Wy	u	-	-	-0.18	-
125	Wy	u	-	-	-0.18	-
126	Wy	u	-	-	-0.18	-
127	Wy	u	-	-	-0.18	-
128	Wy	u	-	-	-0.18	-
129	Wy	u	-	-	-0.18	-
130	Wy	u	-	-	-0.18	-
131	Wy	u	-	-	-0.18	-
132	Wy	u	-	-	-0.18	-
133	Wy	u	-	-	-0.18	-
134	Wy	u	-	-	-0.18	-
135	Wy	u	-	-	-0.18	-
137	Wy	u	-	-	-0.18	-
138	Wy	u	-	-	-0.18	-
147	Wy	u	-	-	-0.18	-
37	Wy	u	-	-	-0.3	-
136	Wy	u	-	-	-0.3	-
120	Wy	u	-	-	-0.35	-
140	Wy	u	-	-	-0.35	-
141	Wy	u	-	-	-0.35	-
139	Wy	u	-	-	-0.35	-
142	Wy	u	-	-	-0.35	-
143	Wy	u	-	-	-0.35	-
146	Wy	u	-	-	-0.35	-
33	Wy	u	-	-	-0.525	-
35	Wy	u	-	-	-0.525	-
148	Wy	u	-	-	-1.05	-
149	Wy	trilinear	0	0	-0.18	-0.18
150	Wy	trilinear	0	0	-0.18	-0.18
151	Wy	trilinear	0	0	-0.18	-0.18
152	Wy	u	-	-	-0.18	-
153	Wy	u	-	-	-0.18	-
154	Wy	u	-	-	-0.18	-

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	H. W.	JUNE/02
	A. M.	JULY/02

Member	From Node	To Node	Section name	Length m	Max compr t	Max tens tens	Strong Shear t	Weak Shear t	Strong Mnt t-m	Weak Mnt t-m
DL										
60	39	38	bd-25x4	4	0	0	3.7	0	-3.7	0
61	37	39	bd-25x4	4	0	0	3.7	0	-3.7	0
80	50	37	bd-25x4	4	0	0	4.5	0	3.3	0
81	49	50	bd-25x4	4	0	0	-4.5	0	3.5	0
85	53	51	bd-25x4	4	0	0	-2.7	0	-2	0
86	52	80	bd-25x4	2	0	0	4.8	0	-5.9	0
102	60	62	bd-25x4	2	0	0	4.9	0	4.9	0
103	63	60	bd-25x4	4	0	0	-3	0	3.5	0
104	61	63	bd-25x4	4	0	0	-4	0	-3	0
107	64	65	bd-25x4	4	0	0	4.5	0	3.2	0
108	66	64	bd-25x4	1.2	0	0	-3.8	0	3.4	0
111	30	66	bd-25x4	3	0	0	3.9	0	3.4	0
124	73	76	bd-25x4	3	0	0	9.7	0	-17.9	0
126	76	74	bd-25x4	2.5	0	0	-11.1	0	-18.1	0
127	75	78	bd-25x4	1.5	0	0	6.8	0	-7.4	0
129	78	76	bd-25x4	1.5	0	0	-5.6	0	-5.5	0
130	78	77	bd-25x4	2.5	0	0	4.8	0	-3	0
132	80	53	bd-25x4	2	0	0	-6.2	0	-5.9	0
133	80	79	bd-25x4	3	0	0	-3.6	0	-2.7	0
144	87	85	bd-25x4	2	0	0	-1.8	0	-0.9	0
145	88	86	bd-25x4	2	0	0	-1.8	0	-0.9	0
148	90	89	bd-25x4	3.5	0	0	-6.2	0	-6.4	0
49	32	33	bd-30x6	6	0	0	2.8	0	-4.2	0
53	25	31	bd-30x6	6.71	0	0	-4.6	0	6.5	0
54	31	27	bd-30x6	6.71	0	0	4.5	0	6.1	0
55	34	35	bd-30x6	6	0	0	-2.9	0	6.9	0
56	35	39	bd-30x6	3	0	0	7	0	-9.9	0
59	39	36	bd-30x6	3	0	0	-5.3	0	-9.7	0
65	40	41	bd-30x6	6	0	0	-7.6	0	9.4	0
66	41	62	bd-30x6	3	0	0	9	0	9.4	0
73	43	44	bd-30x6	6	0	0	-2.1	0	-1.8	0
74	44	45	bd-30x6	6	0	0	-2.4	0	4.8	0
75	45	50	bd-30x6	3	0	0	6.1	0	-9.6	0
76	46	47	bd-30x6	6	0	0	1.8	0	5.3	0
77	47	53	bd-30x6	3	0	0	11	0	-13.6	0
79	50	46	bd-30x6	3	0	0	-6.5	0	-9.6	0
84	53	48	bd-30x6	3	0	0	-7	0	-13.4	0
92	54	55	bd-30x6	6	0	0	-2.7	0	5.6	0
93	55	63	bd-30x6	3	0	0	5.8	0	7.6	0
94	56	65	bd-30x6	3	0	0	5.6	0	7	0
95	57	58	bd-30x6	6	0	0	4.3	0	6.6	0
99	62	42	bd-30x6	3	0	0	-3.8	0	-8.7	0
100	63	56	bd-30x6	3	0	0	-7.6	0	-6.9	0
101	62	59	bd-30x6	6	0	0	6.1	0	-8.9	0
106	65	57	bd-30x6	3	0	0	-5.1	0	5.4	0
109	28	29	bd-30x6	6	0	0	-7.3	0		0
110	29	30	bd-30x6	6	0	0	6.4	0		0
114	67	68	bd-30x6	6	0	0	-3.2	0		0
119	69	77	bd-30x6	1.5	0	0	8.7	0		0

0	CALCULATION	
0	6.8	0
0	4.9	0
0	12.4	0
0		0
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CHECKED BY	A. M.	JULY/02

Member	From Node	To Node	Section name	Length m	Max compr t	Max tens tens	Strong Shear t	Weak Shear t	Strong Mnt t-m	Weak Mnt t-m
DL										
120	70		85 bd-30x6	2	0	0	8.2	0	11.6	0
121	71		82 bd-30x6	3	0	0	7.3	0	-9.7	0
123	74		70 bd-30x6	3	0	0	-14	0	-18.2	0
128	77		74 bd-30x6	1.5	0	0	3	0	-18.2	0
135	82		72 bd-30x6	3	0	0	-4.2	0	-9.9	0
136	81		82 bd-30x6	5.5	0	0	-7.1	0	-8.9	0
139	83		87 bd-30x6	2	0	0	7.9	0	-13.9	0
140	85		86 bd-30x6	2	0	0	1.5	0	-1.8	0
141	86		71 bd-30x6	2	0	0	-7.2	0	8.6	0
142	87		89 bd-30x6	1	0	0	4	0	-17.1	0
143	88		84 bd-30x6	2	0	0	-8.3	0	-14.4	0
146	89		88 bd-30x6	1	0	0	-4.5	0	-17.2	0
43	28		17 bd-30x6	1.2	0	0	-5.6	0	6.6	0
44	29		18 bd-30x6	1.2	0	0	-14.5	0	16.1	0
45	30		19 bd-30x6	1.2	0	0	-10.4	0	12.4	0
1	1		2 bd-35x8	6	0	0	-8.4	0	10	0
8	9		10 bd-35x8	6	0	0	-3.6	0	6.7	0
15	17		18 bd-35x8	6	0	0	-3.1	0	4	0
22	9		40 bd-35x8	2	0	0	10	0	13.5	0
23	17		54 bd-35x8	4	0	0	5.7	0	6.9	0
38	4		33 bd-35x8	2.5	0	0	6.3	0	7.7	0
39	5		35 bd-35x8	4	0	0	6.6	0	-11.8	0
40	6		36 bd-35x8	4	0	0	10.1	0	-15.2	0
41	25		26 bd-35x8	6	0	0	-3.6	0	7.1	0
42	26		38 bd-35x8	3	0	0	6.4	0	-8.7	0
46	26		31 bd-35x8	3	0	0	11.6	0	23.8	0
48	33		34 bd-35x8	1.5	0	0	1.4	0	-7	0
50	34		25 bd-35x8	4	0	0	-3.8	0	-6.9	0
51	35		26 bd-35x8	4	0	0	-10	0	21.3	0
52	36		27 bd-35x8	4	0	0	-7.5	0	-15.1	0
58	38		27 bd-35x8	3	0	0	-6.5	0	-8.8	0
62	40		1 bd-35x8	6	0	0	-5.4	0	-9.5	0
87	54		9 bd-35x8	4	0	0	-7.4	0	13.7	0
2	2		59 bd-40x8	3	0	0	8.1	0	9.7	0
3	3		4 bd-40x8	6	0	0	7.8	0	8.9	0
4	4		5 bd-40x8	6	0	0	-5.9	0	10.2	0
5	5		37 bd-40x8	3	0	0	10.4	0	-11.8	0
6	6		7 bd-40x8	6	0	0	5.2	0	9	0
7	7		51 bd-40x8	3	0	0	6.5	0	-7.6	0
9	10		60 bd-40x8	3	0	0	6.5	0	-9.3	0
10	11		12 bd-40x8	6	0	0	3.7	0	6.5	0
11	12		13 bd-40x8	6	0	0	-3.5	0	5.7	0
12	13		49 bd-40x8	3	0	0	5.1	0	-5.4	0
13	14		15 bd-40x8	6	0	0	-7.9	0	12.4	0
14	15		52 bd-40x8	3	0	0	9.6	0	-12.0	0
16	18		61 bd-40x8	3	0	0	3.6	0	0	0
17	19		64 bd-40x8	3	0	0	8.2	0	0	0
18	20		21 bd-40x8	6	0	0	-3.3	0	0	0
19	21		73 bd-40x8	3	0	0	11.1	0	0	0

0 CALCULATION		
0 Detailed Design		
0 on Port Reactivation Project		
0 in La Union Province		
CALC FILE No.:		
CALC INDEX No.:		PAGE/82
PREPARED BY		INITIAL DATE
H. W.		June/02
CHECKED BY		INITIAL DATE
A. M.		July/02

Member	From Node	To Node	Section name	Length m	Max compr t	Max tens tens	Strong Shear t	Weak Shear t	Strong Mnt t-m	Weak Mnt t-m
DL										
20	22	90	bd-40x8	3	0	0	9.4	0	14.7	0
21	23	81	bd-40x8	3	0	0	12.4	0	13.8	0
24	10	41	bd-40x8	2	0	0	18.5	0	21.2	0
25	18	55	bd-40x8	4	0	0	7.3	0	14.3	0
26	11	42	bd-40x8	2	0	0	7.3	0	14	0
27	19	56	bd-40x8	4	0	0	10	0	-19.9	0
28	12	44	bd-40x8	4	0	0	6.3	0	16.1	0
29	20	67	bd-40x8	1	0	0	9.2	0	-9	0
30	13	45	bd-40x8	4	0	0	10.7	0	30.5	0
31	21	68	bd-40x8	1	0	0	17.7	0	-14.7	0
32	14	46	bd-40x8	4	0	0	10.5	0	32.2	0
33	22	83	bd-40x8	3.5	0	0	12.2	0	-33.4	0
34	15	47	bd-40x8	4	0	0	14.3	0	34.1	0
35	23	84	bd-40x8	3.5	0	0	10.4	0	-27.3	0
36	16	79	bd-40x8	2	0	0	16.6	0	27.7	0
37	24	72	bd-40x8	5.5	0	0	6.7	0	-11.1	0
47	3	32	bd-40x8	2.5	0	0	8.7	0	14.2	0
57	37	6	bd-40x8	3	0	0	-10.2	0	-11.9	0
63	41	2	bd-40x8	6	0	0	-5.5	0	-14.4	0
64	42	43	bd-40x8	2	0	0	1.7	0	-1.7	0
67	43	3	bd-40x8	4	0	0	-5.3	0	11.9	0
68	44	4	bd-40x8	4	0	0	-4.3	0	7.9	0
69	45	5	bd-40x8	4	0	0	-5.1	0	8.3	0
70	46	6	bd-40x8	4	0	0	-5.1	0	10.6	0
71	47	7	bd-40x8	4	0	0	-5.8	0	-14.8	0
72	48	8	bd-40x8	4	0	0	-10	0	-20.1	0
78	49	14	bd-40x8	3	0	0	-4.1	0	-5.3	0
82	51	8	bd-40x8	3	0	0	-3.8	0	-7.7	0
83	52	16	bd-40x8	3	0	0	-8.9	0	-13	0
88	55	10	bd-40x8	4	0	0	-8.6	0	20	0
89	56	11	bd-40x8	4	0	0	-10.6	0	-19.3	0
90	57	12	bd-40x8	4	0	0	-10.8	0	-20.4	0
91	58	69	bd-40x8	1.5	0	0	-10.7	0	-32.3	0
96	59	3	bd-40x8	3	0	0	-7.7	0	8.8	0
97	60	11	bd-40x8	3	0	0	-6.8	0	-9.3	0
98	61	19	bd-40x8	3	0	0	-5.2	0	8.3	0
105	64	20	bd-40x8	3	0	0	-7.8	0	-10.4	0
112	67	57	bd-40x8	3	0	0	5	0	-20.4	0
113	68	75	bd-40x8	2	0	0	12.1	0	-33.7	0
115	69	13	bd-40x8	2.5	0	0	-21.7	0	30.9	0
116	70	14	bd-40x8	2.5	0	0	-26.9	0	33.9	0
117	71	15	bd-40x8	2.5	0	0	-22.3	0	34.4	0
118	72	16	bd-40x8	2.5	0	0	-12.7	0	26.2	0
122	73	22	bd-40x8	3	0	0	-12.7	0	-14.3	0
125	75	58	bd-40x8	1	0	0	-3.1	0	-33.5	0
131	79	48	bd-40x8	2	0	0	11.1	0	21	0
134	81	24	bd-40x8	3	0	0	-7.7	0	0	0
137	83	70	bd-40x8	2	0	0	-2.4	0	0	0
138	84	71	bd-40x8	2	0	0	-5.5	0	0	0
147	90	23	bd-40x8	3	0	0	-9.1	0	0	0

CALCULATION		
Detailed Design		
on Port Reactivation Project		
in Liaison Province		
CALC FILE No.:		
CALC INDEX No.:		PAGE 183
	INITIAL	DATE
PREPARED BY	H. W.	JUNE/02
CHECKED BY	A. M.	JULY/02

Member	From Node	To Node	Section name	Length m	Max compr t	Max tens tens	Strong Shear t	Weak Shear t	Strong Mnt t-m	Weak Mnt t-m
LL										
60	39	38	bd-25x4	4	0	0	-0.4	0	-0.4	0
61	37	39	bd-25x4	4	0	0	-0.4	0	-0.4	0
80	50	37	bd-25x4	4	0	0	0.4	0	0.3	0
81	49	50	bd-25x4	4	0	0	-0.4	0	0.3	0
85	53	51	bd-25x4	4	0	0	0.4	0	-0.3	0
86	52	80	bd-25x4	2	0	0	0.4	0	-0.5	0
102	60	62	bd-25x4	2	0	0	0.6	0	0.6	0
103	63	60	bd-25x4	4	0	0	-0.5	0	0.5	0
104	61	63	bd-25x4	4	0	0	-0.4	0	-0.3	0
107	64	65	bd-25x4	4	0	0	0.4	0	0.3	0
108	66	64	bd-25x4	1.2	0	0	-0.4	0	0.3	0
111	30	66	bd-25x4	3	0	0	0.4	0	0.3	0
124	73	76	bd-25x4	3	0	0	0.7	0	-1.2	0
126	76	74	bd-25x4	2.5	0	0	-0.7	0	-1.2	0
127	75	78	bd-25x4	1.5	0	0	0.4	0	-0.4	0
129	78	76	bd-25x4	1.5	0	0	-0.4	0	-0.3	0
130	78	77	bd-25x4	2.5	0	0	-0.2	0	-0.1	0
132	80	53	bd-25x4	2	0	0	-0.6	0	-0.5	0
133	80	79	bd-25x4	3	0	0	0.3	0	-0.2	0
144	87	85	bd-25x4	2	0	0	0	0	0	0
145	88	86	bd-25x4	2	0	0	0	0	0	0
148	90	89	bd-25x4	3.5	0	0	-1.8	0	-1.6	0
49	32	33	bd-30x6	6	0	0	0.5	0	-0.8	0
53	25	31	bd-30x6	6.71	0	0	-0.8	0	1.1	0
54	31	27	bd-30x6	6.71	0	0	0.8	0	1.1	0
55	34	35	bd-30x6	6	0	0	-0.7	0	1.2	0
56	35	39	bd-30x6	3	0	0	1.1	0	1.4	0
59	39	36	bd-30x6	3	0	0	-0.7	0	-1.2	0
65	40	41	bd-30x6	6	0	0	-0.7	0	0.9	0
66	41	62	bd-30x6	3	0	0	0.9	0	0.9	0
73	43	44	bd-30x6	6	0	0	-0.7	0	0.7	0
74	44	45	bd-30x6	6	0	0	-0.6	0	0.7	0
75	45	50	bd-30x6	3	0	0	0.9	0	-1.1	0
76	46	47	bd-30x6	6	0	0	0.5	0	0.9	0
77	47	53	bd-30x6	3	0	0	1.2	0	-1.6	0
79	50	46	bd-30x6	3	0	0	-1	0	-1.1	0
84	53	48	bd-30x6	3	0	0	-0.8	0	-1.6	0
92	54	55	bd-30x6	6	0	0	-0.7	0	0.9	0
93	55	63	bd-30x6	3	0	0	0.9	0	1	0
94	56	65	bd-30x6	3	0	0	0.7	0	0.9	0
95	57	58	bd-30x6	6	0	0	0.7	0	0.8	0
99	62	42	bd-30x6	3	0	0	-0.5	0	-0.8	0
100	63	56	bd-30x6	3	0	0	-0.8	0	0.9	0
101	62	59	bd-30x6	6	0	0	-0.5	0	-0.8	0
106	65	57	bd-30x6	3	0	0	-0.6	0	0.7	0
109	28	29	bd-30x6	6	0	0	-0.7	0	0	0
110	29	30	bd-30x6	6	0	0	0.6	0	0	0
114	67	68	bd-30x6	6	0	0	0.5	0	0	0
119	69	77	bd-30x6	1.5	0	0	0.8	0	0	0

0 CALCULATION		
0 Detailed Design		
0 Port Reactivation Project		
0 in La Union Province		
CALC FILE No.:		
CALC INDEX No.:		PAGE 184
PREPARED BY	INITIAL	DATE
	H. W.	JUNE/02
APPROVED BY	A. M.	JULY/02

Member	From Node	To Node	Section name	Length m	Max compr t	Max tens tens	Strong Shear t	Weak Shear t	Strong Mnt t-m	Weak Mnt t-m
LL										
120	70	85	bd-30x6	2	0	0	1	0	1.1	0
121	71	82	bd-30x6	3	0	0	1.2	0	-1.4	0
123	74	70	bd-30x6	3	0	0	-1.2	0	-1.4	0
128	77	74	bd-30x6	1.5	0	0	0.3	0	-1.4	0
135	82	72	bd-30x6	3	0	0	-0.8	0	-1.4	0
136	81	82	bd-30x6	5.5	0	0	-0.8	0	-1.1	0
139	83	87	bd-30x6	2	0	0	2	0	-3.2	0
140	85	86	bd-30x6	2	0	0	-0.4	0	-0.5	0
141	86	71	bd-30x6	2	0	0	-1.1	0	1.2	0
142	87	89	bd-30x6	1	0	0	1.3	0	-4.2	0
143	88	84	bd-30x6	2	0	0	-2	0	-3.2	0
146	89	88	bd-30x6	1	0	0	-1.3	0	-4.2	0
43	28	17	bd-30x6	1.2	0	0	-0.6	0	0.7	0
44	29	18	bd-30x6	1.2	0	0	-1.5	0	1.6	0
45	30	19	bd-30x6	1.2	0	0	-1.1	0	1.2	0
1	1	2	bd-35x8	6	0	0	-0.7	0	0.9	0
8	9	10	bd-35x8	6	0	0	-0.7	0	1.1	0
15	17	18	bd-35x8	6	0	0	-0.7	0	0.8	0
22	9	40	bd-35x8	2	0	0	1.2	0	1.8	0
23	17	54	bd-35x8	4	0	0	0.8	0	-1	0
38	4	33	bd-35x8	2.5	0	0	1.5	0	2.2	0
39	5	35	bd-35x8	4	0	0	1.4	0	-2.2	0
40	6	36	bd-35x8	4	0	0	1.2	0	1.8	0
41	25	26	bd-35x8	6	0	0	-0.7	0	1	0
42	26	38	bd-35x8	3	0	0	0.9	0	0.9	0
46	26	31	bd-35x8	3	0	0	2.1	0	4.2	0
48	33	34	bd-35x8	1.5	0	0	0.5	0	-1.5	0
50	34	25	bd-35x8	4	0	0	-0.8	0	-1.5	0
51	35	26	bd-35x8	4	0	0	-1.9	0	3.8	0
52	36	27	bd-35x8	4	0	0	-0.9	0	-1.7	0
58	38	27	bd-35x8	3	0	0	-0.6	0	-0.8	0
62	40	1	bd-35x8	6	0	0	-0.6	0	-1	0
87	54	9	bd-35x8	4	0	0	-1.1	0	1.8	0
2	2	59	bd-40x8	3	0	0	0.8	0	0.9	0
3	3	4	bd-40x8	6	0	0	0.6	0	0.8	0
4	4	5	bd-40x8	6	0	0	-0.6	0	1	0
5	5	37	bd-40x8	3	0	0	0.9	0	-1	0
6	6	7	bd-40x8	6	0	0	-0.6	0	0.9	0
7	7	51	bd-40x8	3	0	0	0.8	0	-0.9	0
9	10	60	bd-40x8	3	0	0	1.1	0	-1.3	0
10	11	12	bd-40x8	6	0	0	0.7	0	1	0
11	12	13	bd-40x8	6	0	0	-0.6	0	0.8	0
12	13	49	bd-40x8	3	0	0	0.7	0	0.7	0
13	14	15	bd-40x8	6	0	0	-0.6	0	1	0
14	15	52	bd-40x8	3	0	0	0.9	0	-1	0
16	18	61	bd-40x8	3	0	0	0.7	0	0	0
17	19	64	bd-40x8	3	0	0	1	0	0	0
18	20	21	bd-40x8	6	0	0	0.6	0	0	0
19	21	73	bd-40x8	3	0	0	0.7	0	0	0

0	CALCULATION	
0	Detailed Design	
0	on Port Reactivation Project	
0	in La Union Province	
CALC FILE No.:		
CALC INDEX No.:		PAGE 185
	INITIAL	DATE
PREPARED BY	A. W.	June/02
APPROVED BY	A. M.	July/02

Member	From Node	To Node	Section name	Length m	Max compr t	Max tens tens	Strong Shear t	Weak Shear t	Strong Mnt t-m	Weak Mnt t-m
LL	20	22	90 bd-40x8	3	0	0	1.4	0	-1.8	0
	21	23	81 bd-40x8	3	0	0	1.3	0	1.9	0
	24	10	41 bd-40x8	2	0	0	2.3	0	3.2	0
	25	18	55 bd-40x8	4	0	0	1.3	0	-2.2	0
	26	11	42 bd-40x8	2	0	0	1.4	0	2.5	0
	27	19	56 bd-40x8	4	0	0	1.3	0	-2.7	0
	28	12	44 bd-40x8	4	0	0	1.4	0	2.9	0
	29	20	67 bd-40x8	1	0	0	1.5	0	-1.3	0
	30	13	45 bd-40x8	4	0	0	1.6	0	3.5	0
	31	21	68 bd-40x8	1	0	0	1.5	0	-1.6	0
	32	14	46 bd-40x8	4	0	0	2	0	5.5	0
	33	22	83 bd-40x8	3.5	0	0	2.8	0	-6.2	0
	34	15	47 bd-40x8	4	0	0	2.4	0	6.1	0
	35	23	84 bd-40x8	3.5	0	0	2.7	0	-6	0
	36	16	79 bd-40x8	2	0	0	1.7	0	3.3	0
	37	24	72 bd-40x8	5.5	0	0	1	0	-1.9	0
	47	3	32 bd-40x8	2.5	0	0	1	0	1.9	0
	57	37	6 bd-40x8	3	0	0	-0.8	0	-1	0
	63	41	2 bd-40x8	6	0	0	-0.7	0	-1.3	0
	64	42	43 bd-40x8	2	0	0	0.5	0	-0.8	0
	67	43	3 bd-40x8	4	0	0	-1	0	1.7	0
	68	44	4 bd-40x8	4	0	0	-1.2	0	2.2	0
	69	45	5 bd-40x8	4	0	0	-1.3	0	2.2	0
	70	46	6 bd-40x8	4	0	0	-1	0	1.6	0
	71	47	7 bd-40x8	4	0	0	-0.9	0	-1.9	0
	72	48	8 bd-40x8	4	0	0	-0.8	0	-1.6	0
	78	49	14 bd-40x8	3	0	0	-0.6	0	-0.6	0
	82	51	8 bd-40x8	3	0	0	-0.6	0	-1	0
	83	52	16 bd-40x8	3	0	0	-0.6	0	-1.1	0
	88	55	10 bd-40x8	4	0	0	-1.7	0	3.2	0
	89	56	11 bd-40x8	4	0	0	-1.7	0	2.6	0
	90	57	12 bd-40x8	4	0	0	-1.8	0	2.9	0
	91	58	69 bd-40x8	1.5	0	0	-0.9	0	-2.7	0
	96	59	3 bd-40x8	3	0	0	-0.8	0	0.8	0
	97	60	11 bd-40x8	3	0	0	-1.1	0	-1.3	0
	98	61	19 bd-40x8	3	0	0	-0.8	0	1	0
	105	64	20 bd-40x8	3	0	0	-0.9	0	-1	0
	112	67	57 bd-40x8	3	0	0	0.8	0	-2.9	0
	113	68	75 bd-40x8	2	0	0	0.8	0	-2.8	0
	115	69	13 bd-40x8	2.5	0	0	-2.1	0	3.3	0
	116	70	14 bd-40x8	2.5	0	0	-4	0	5.7	0
	117	71	15 bd-40x8	2.5	0	0	-4.1	0	6.2	0
	118	72	16 bd-40x8	2.5	0	0	-1.9	0	3.1	0
	122	73	22 bd-40x8	3	0	0	-1	0	1.5	0
	125	75	58 bd-40x8	1	0	0	-0.2	0	-2.8	0
	131	79	48 bd-40x8	2	0	0	1.1	0	0	0
	134	81	24 bd-40x8	3	0	0	-0.6	0	0	0
	137	83	70 bd-40x8	2	0	0	-1.4	0	0	0
	138	84	71 bd-40x8	2	0	0	-1.4	0	0	0
	147	90	23 bd-40x8	3	0	0	-1.5	0	0	0

CALCULATION		
Detailed Design		
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CALC FILE No.:		
CALC INDEX No.:		PAGE 86
PREPARED BY		INITIAL DATE
H. W.		June/02
A. M.		July/02

REACTION

DL Node	Rx	Ry	Rz	Mx	My	Mz
1	0	11.276	0	0	0	0
2	0	22.801	0	0	0	0
3	0	30.255	0	0	0	0
4	0	20.429	0	0	0	0
5	0	28.024	0	0	0	0
6	0	30.585	0	0	0	0
7	0	16.9	0	0	0	0
8	0	13.812	0	0	0	0
9	0	19.967	0	0	0	0
10	0	38.868	0	0	0	0
11	0	30.838	0	0	0	0
12	0	20.402	0	0	0	0
13	0	41.098	0	0	0	0
14	0	47.645	0	0	0	0
15	0	54.146	0	0	0	0
16	0	38.116	0	0	0	0
17	0	12.972	0	0	0	0
18	0	28.09	0	0	0	0
19	0	33.339	0	0	0	0
20	0	19.173	0	0	0	0
21	0	32.141	0	0	0	0
22	0	34.372	0	0	0	0
23	0	31.956	0	0	0	0
24	0	14.416	0	0	0	0
25	0	7.725	0	0	0	0
26	0	31.535	0	0	0	0
27	0	16.67	0	0	0	0

CALCULATION		
Detailed Design		
on Port Reactivation Project		
in La Union Province		
CALC FILE No.:		
CALC INDEX No.:	PAGE 187	
	INITIAL	DATE
PREPARED BY	H. W.	June/02
CHECKED BY	A. M.	July/02

REACTION

LL Node	Rx	Ry	Rz	Mx	My	Mz	
1	0	1.162	0	0	0	0	0
2	0	2.712	0	0	0	0	0
3	0	3.661	0	0	0	0	0
4	0	3.563	0	0	0	0	0
5	0	4.282	0	0	0	0	0
6	0	3.619	0	0	0	0	0
7	0	2.232	0	0	0	0	0
8	0	1.36	0	0	0	0	0
9	0	2.984	0	0	0	0	0
10	0	6.514	0	0	0	0	0
11	0	5.345	0	0	0	0	0
12	0	3.98	0	0	0	0	0
13	0	5.131	0	0	0	0	0
14	0	7.143	0	0	0	0	0
15	0	7.954	0	0	0	0	0
16	0	4.247	0	0	0	0	0
17	0	1.777	0	0	0	0	0
18	0	3.965	0	0	0	0	0
19	0	4.072	0	0	0	0	0
20	0	2.99	0	0	0	0	0
21	0	2.696	0	0	0	0	0
22	0	5.212	0	0	0	0	0
23	0	5.502	0	0	0	0	0
24	0	1.597	0	0	0	0	0
25	0	1.643	0	0	0	0	0
26	0	5.495	0	0	0	0	0
27	0	1.889	0	0	0	0	0

CALCULATION		
Detailed Design on Port Reactivation Project in La Union Province		
CALC FILE No.:		
CALC INDEX No.:	PAGE 88	
	INITIAL	DATE
PREPARED BY	H.W	JUNE/02
	A.M.	JULY/02

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	R.Martinez
SECTION: Port Administration Building	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Dead & Live Load for 1st Floor	Date	July-02	Page	189 / 232

administration

Dead Load

	room	material	thickness	density	(kg/m ²) weight
		finish	30		60
1F	all room	slab	150		360
					420

Live Load

Floor	Room	Dead Load	Live Load	otal Loa	Notes
1F	cafeteria	420		770	
	kitchen		350		
1F	waiting	420		570	
	quarantine				
	toilet				
	vestibule				
1F	corridor	420	150	570	
	staircase				
1F	office	420	240	660	
	banks				
	first aid				
1F	police	420	180	600	
	inf.				
1F	guard rm	420	170	590	
	janitor				
1F	strage	420	600	1020	
	machine		540		
Canopy	roof	50	20	70	
			0		

C.B	t=200mm				293 kg/m ²
	t=150mm				226 kg/m ²

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	R.Martinez
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SUBJECT: Dead & Live Load for 1st Floor	Date	July-02	Page	190 / 232

Case	CB+WALL (DL)				
member	t	unit w	h, L		
53,54	RC	200	480	1	0.48 t/m
65,66	CB		295	4.85	1.43 t/m
101,102	CB		295	4.85	1.43 t/m
1	CB		295	4.85	1.43 t/m
62	CB		295	2.4	0.71 t/m
23,87	CB		295	2.4	0.71 t/m
109	CB		295	4.85	1.43 t/m
110	CB		295	4.85	1.43 t/m
103	CB		295	2.4	0.71 t/m
104	CB		295	4.85	1.43 t/m
2	CB		295	4.85	1.43 t/m
96	CB		295	2.4	0.71 t/m
100	CB		295	4.85	1.43 t/m
111	CB		295	4.85	1.43 t/m
107,108	CB		295	4.85	1.43 t/m
105	CB		295	2.4	0.71 t/m
94,106	CB		295	2.4	0.71 t/m
3	CB		295	4.85	1.43 t/m
47	CB		295	4.85	1.43 t/m
49	CB		295	1.2	0.35 t/m
114	CW		100	4.85	0.49 t/m
95	CW		100	4.85	0.49 t/m
4	CB		295	2.4	0.71 t/m
19,122	CB		295	4.85	1.43 t/m
127,129	RC	200	480	4.4	2.11 t/m
130	RC	200	480	4.4	2.11 t/m
91,125	RC	200	480	4.4	2.11 t/m
31,113	CB		295	4.85	1.43 t/m
124,126	RC	200	480	4.4	2.11 t/m
123	RC	200	480	2.2	1.06 t/m
12	CB		295	1	0.30 t/m
80,81	CB		295	4.85	1.43 t/m
5,57	CB		295	4.85	1.43 t/m
61	CB		295	4.85	1.43 t/m
57	CB		295	4.85	1.43 t/m
60	CB		295	4.85	1.43 t/m
58	CB		295	4.85	1.43 t/m
40	CB		295	2.4	0.71 t/m
52	CB		295	2.4	0.71 t/m
20	CB		295	4.85	1.43 t/m
147	CB		295	4.85	1.43 t/m
148	CB		295	4.85	1.43 t/m
146	CB		295	4.85	1.43 t/m

2/L

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	R.Martinez
SECTION: Port Administration Building	Calc. Index No.		Checked by	A.MORIOKA
SUBJECT: Dead & Live Load for 1st Floor	Date	July-02	Page	191 / 1232

Additional Load for model					
Case CB+WALL (DL)					
member					
144,145 CB	295	4.85		1.43 t/m	
120,141 CB	295	4.85		1.43 t/m	
13 CB	295	4.85		1.43 t/m	
6 CB	295	2.4		0.71 t/m	
7 CB	295	2.4		0.71 t/m	
85 CB	295	4.85		1.43 t/m	upper side
77 CB	295	4.85		1.43 t/m	
84 CB	295	4.85		1.43 t/m	right side
86,132 CB	295	4.85		1.43 t/m	
133 CB	295	4.85		1.43 t/m	
14 CB	295	4.85		1.43 t/m	right side
83 CB	295	4.85		1.43 t/m	
136 CB	295	4.85		1.43 t/m	
21,134 CB	295	4.85		1.43 t/m	
37 CB	295	4.85		1.43 t/m	
72,131 CB	295	4.85		1.43 t/m	
CASE	SLAB	(DL)			
member	t	unit w	h, L		
except structural slab		350	0.5	0.18 t/m	
91,125,126		1020	0.75	0.77 t/m	
130		1020	1.5	1.53 t/m	
120,140,141		770	0.75	0.58 t/m	
33		770	1.5	1.16 t/m	trapezoid
139,143		770	1.5	1.16 t/m	triangle
148		770	1.5	1.16 t/m	trapezoidx2
20,147		770	1.5	1.16 t/m	triangle
35		770	1.5	1.16 t/m	trapezoid
136		770	1	0.77 t/m	upper side
121		770	1.155	0.89 t/m	
83,133		770	1	0.77 t/m	

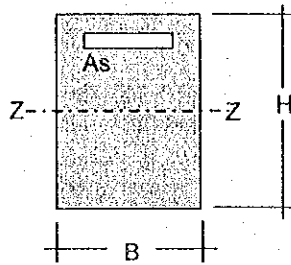
PROJECT: Detailed Design on Port Reactivation Project In La Union Province	Calc. File No.	Prepared by	R.Martinez
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CASE	LL	t	unit w	h, L	
			350	0.5	0.18 t/m
37,136			600	0.5	0.30 t/m
120,140,141			350	1	0.35 t/m
139,142,143,146			350	1	0.35 t/m
33,35			350	1.5	0.53 t/m
148			350	3	1.05 t/m

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
SECTION: Port Administration Building	Calc. Index No.		Checked by	A.MORIOKA
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2/3 axi FB-3 center

BEAM DESIGN



H = cm

b = cm

f_c = kg/cm²

f_y = kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O	MOMENT
LOAD	Mz-z

Dead Load	5.60
Live Load	0.30
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	8.35
0.75(1.4DL+1.7LL+1.87)	6.26
0.75(1.4DL+1.7LL+1.87)	6.26

Force for design: Mu z-z = ton-m

d = cm

Clear cover = cm

$f_y^2/1.7b^2f_c As^2 - f_y d As + Mu/f = f = 0.90$

1647.06 As² - 220332 927777.78 = 0 As = cm²

Asmin = (4/3)Asreq :

$(4/3)Asreq = 5.80 \text{ cm}^2$
 $(14/f_y) b d = 5.25 \text{ cm}^2$

} Asmin = cm²

Asmax : rb = 0.0345 Asmax (0.75rb) = cm²

As = cm² o.k!! As < Amax

Bar denomination, N =

Bar Area (Av) = cm²

Number of bars =

Use 2 - N 8

3-D25

Minimum Base Required:

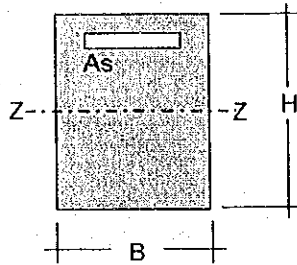
Max. bars per layer =

Minimum Base = cm

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.		Prepared by	H.WATANABE
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2/3 axi FB-4 end

BEAM DESIGN



H = 40.00 cm
 b = 25.00 cm
 f_c = 210 kg/cm²
 f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Load	3.30
Live Load	0.20
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	4.96
0.75(1.4DL+1.7LL+1.87	3.72
0.75(1.4DL+1.7LL+1.87	3.72

Force for design: Mu z-z = 4.96 ton-m

d = 32.46 cm

Clear cover = 5.00 cm

$$f_y^2 / 1.7 b f_c A_s^2 - f_y d A_s + M_u / f = f = 0.90$$

$$1976.47 A_s^2 - 136332 A_s + 551111.11 = 0 \quad A_s = 4.31 \text{ cm}^2$$

As_{min} = (4/3)As_{req} :

$$\left. \begin{array}{l} (4/3)A_{sreq} = 5.75 \text{ cm}^2 \\ (14/f_y) b d = 2.71 \text{ cm}^2 \end{array} \right\} A_{smin} = 2.71 \text{ cm}^2$$

As_{max} : rb = 0.0345 As_{max} (0.75rb) = 20.97 cm²

As = 4.31 cm² o.k!! As < A_{max}

Bar denomination, N = 8

Bar Area (A_v) = 5.07 cm²

Number of bars = 0.85

Use 1 - N 8

2-D25

Minimum Base Required:

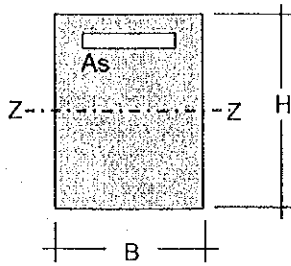
Max. bars per layer = 2

Minimum Base = 22.70 cm

PROJECT: Detailed Design on Port Reactivation Project In La Union Province	Calc. File No.		Prepared by	H.WATANABE
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2 span FB-4 end

BEAM DESIGN



H = cm

b = cm

f_c = kg/cm²

f_y = kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Load	3.10
Live Load	0.20
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	4.68
0.75(1.4DL+1.7LL+1.87)	3.51
0.75(1.4DL+1.7LL+1.87)	3.51

Force for design: Mu z-z = ton-m

d = cm

Clear cover = cm

$f_y^2/1.7b^2f_c As^2 - f_y d As + Mu/f = 0$ f = 0.90

1976.47 As²-136332 520000 = 0 As = 4.05 cm²

Asmin = (4/3)Asreq :

$(4/3)Asreq = 5.40 \text{ cm}^2$ }
 $(14/f_y) b d = 2.71 \text{ cm}^2$ } Asmin = 2.71 cm²

Asmax : rb = 0.0345 Asmax (0.75rb) = 20.97 cm²

As = 4.05 cm² o.k!! As < Amax

Bar denomination, N =

Bar Area (A_v) = 5.07 cm²

Number of bars = 0.80

Use 1 - N 8

2-D25

Minimum Base Required:

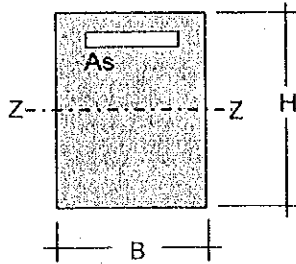
Max. bars per layer =

Minimum Base = 22.70 cm

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1 span FB-4 center

BEAM DESIGN



H = 40.00 cm
 b = 25.00 cm
 f'c = 210 kg/cm² *
 fy = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Load	3.40
Live Load	0.30
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	5.27
0.75(1.4DL+1.7LL+1.87	3.95
0.75(1.4DL+1.7LL+1.87	3.95

Force for design: Mu z-z = 5.30 ton-m

d = 32.46 cm

Clear cover = 5.00 cm

$$fy^2/1.7bf'c As^2 - fy d As + Mu/f = f = 0.90$$

$$1976.47 As^2 - 136332 \cdot 588888.89 = 0$$

$$As = 4.63 \text{ cm}^2$$

Asmin = (4/3)Asreq :

$$\left. \begin{array}{l} (4/3)Asreq = 6.17 \text{ cm}^2 \\ (14/fy) b d = 2.71 \text{ cm}^2 \end{array} \right\} Asmin = 2.71 \text{ cm}^2$$

$$Asmax : rb = 0.0345 \quad Asmax (0.75rb) = 20.97 \text{ cm}^2$$

$$As = 4.63 \text{ cm}^2 \quad \text{o.k!! } As < Asmax$$

Bar denomination, N = 8

Bar Area (Av) = 5.07 cm²

Number of bars = 0.91

Use 1 - N 8

2-D25

Minimum Base Required:

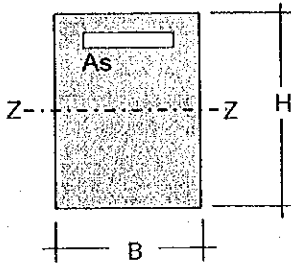
Max. bars per layer = 2

Minimum Base = 22.70 cm

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.	Prepared by	H.WATANABE
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1 span FB-4a center

BEAM DESIGN



H = 40.00 cm
 b = 25.00 cm
 f_c = 210 kg/cm²
 f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
-------------	-------------

Dead Load	7.30
Live Load	0.60
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	11.24
0.75(1.4DL+1.7LL+1.87)	8.43
0.75(1.4DL+1.7LL+1.87)	8.43

Force for design: Mu z-z = 11.24 ton-m

d = 32.46 cm

Clear cover = 5.00 cm

$$f_y^2/1.7b^2f_c A_s^2 - f_y d A_s + M_u/f = f = 0.90$$

$$1976.47 A_s^2 - 136332 A_s + 1248888.9 = 0 \quad A_s = 10.88 \text{ cm}^2$$

A_{smin} = (4/3)A_{sreq} :

$$\left. \begin{array}{l} (4/3)A_{sreq} = 14.50 \text{ cm}^2 \\ (14/f_y) b d = 2.71 \text{ cm}^2 \end{array} \right\} A_{smin} = 2.71 \text{ cm}^2$$

A_{smax} : rb = 0.0345 A_{smax} (0.75rb) = 20.97 cm²

A_s = 10.88 cm² o.k!! A_s < A_{max}

Bar denomination, N = 8

Bar Area (A_v) = 5.07 cm²

Number of bars = 2.15

Use 3 - N 8

2/2-D25

Minimum Base Required:

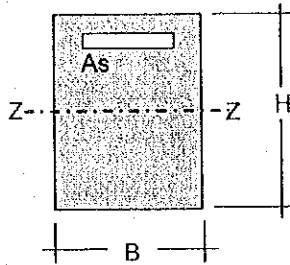
Max. bars per layer = 2

Minimum Base = 22.70 cm

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.	Prepared by	H.WATANABE
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1 span FB-4a center
toilet

BEAM DESIGN



H = 40.00 cm
 b = 25.00 cm
 f_c = 210 kg/cm²
 f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Load	6.70
Live Load	1.70
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	12.27
0.75(1.4DL+1.7LL+1.87)	9.20
0.75(1.4DL+1.7LL+1.87)	9.20

Force for design: Mu z-z = 12.27 ton-m

d = 32.46 cm

Clear cover = 5.00 cm

$$f_y^2/1.7b^2f_c A_s^2 - f_y d A_s + Mu/f = f = 0.90$$

$$1976.47 A_s^2 - 136333.3 = 0 \quad A_s = 12.13 \text{ cm}^2$$

A_{smin} = (4/3)A_{sreq} :

$$\left. \begin{array}{l} (4/3)A_{sreq} = 16.18 \text{ cm}^2 \\ (14/f_y) b d = 2.71 \text{ cm}^2 \end{array} \right\} A_{smin} = 2.71 \text{ cm}^2$$

A_{smax} : rb = 0.0345 A_{smax} (0.75rb) = 20.97 cm²

A_s = 12.13 cm² o.k!! A_s < A_{max}

Bar denomination, N = 8

Bar Area (A_v) = 5.07 cm²

Number of bars = 2.39 Use 3 - N 8 2/2-D25

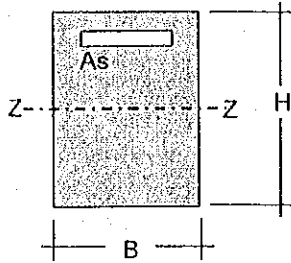
Minimum Base Required:

Max. bars per layer = 2 Minimum Base = 22.70 cm

PROJECT: Detailed Design on Port Reactivation Project in La Union Province	Calc. File No.	Prepared by	H.WATANABE
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B/C axi FB-3 END

BEAM DESIGN



$H = 60.00$ cm
 $b = 30.00$ cm
 $f_c = 210$ kg/cm²
 $f_y = 4200$ kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT
	Mz-z

Dead Load	8.00
Live Load	0.70
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	12.39
0.75(1.4DL+1.7LL+1.87	9.29
0.75(1.4DL+1.7LL+1.87	9.29

Force for design: $Mu_{z-z} = 12.39$ ton-m

$d = 52.46$ cm

Clear cover = 5.00 cm

$f_y^2 / 1.7 b f_c A_s^2 - f_y d A_s + M u / f = f = 0.90$

$1647.06 A_s^2 - 220332 A_s + 1376666.7 = 0 \quad A_s = 6.57 \text{ cm}^2$

$A_{smin} = (4/3)A_{sreq}$:

$(4/3)A_{sreq} = 8.76 \text{ cm}^2$
 $(14/f_y) b d = 5.25 \text{ cm}^2$

$A_{smin} = 5.25 \text{ cm}^2$

$A_{smax} : r_b = 0.0345 \quad A_{smax} (0.75r_b) = 40.68 \text{ cm}^2$

$A_s = 6.57 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$

Bar denomination, N = 8

Bar Area (A_v) = 5.07 cm^2

Number of bars = 1.30 Use **2 - N 8** 3-D25

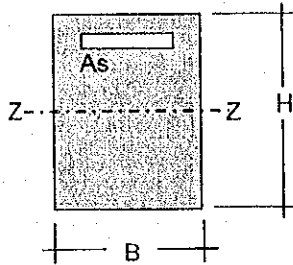
Minimum Base Required:

Max. bars per layer = 3 Minimum Base = 27.78 cm

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B/C axi FB-3 CENTER

BEAM DESIGN



H = 60.00 cm

b = 30.00 cm

f_c = 210 kg/cm²

f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE OF LOAD	MOMENT Mz-z
--------------	----------------

Dead Load	10.00
Live Load	0.80
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	15.36
0.75(1.4DL+1.7LL+1.87)	11.52
0.75(1.4DL+1.7LL+1.87)	11.52

Force for design: Mu z-z = 15.40 ton-m

d = 52.46 cm

Clear cover = 5.00 cm

$f_y^2/1.7bfc As^2 - f_yd As + Mu/f = f = 0.90$

1647.06 As² - 220332 As - 1711111.1 = 0

As = 8.28 cm²

Asmin = (4/3)Asreq :

(4/3)Asreq = 11.04 cm²
 (14/fy) b d = 5.25 cm²

Asmin = 5.25 cm²

Asmax : rb = 0.0345

Asmax (0.75rb) = 40.68 cm²

As = 8.28 cm²

o.k!! As < Amax

Bar denomination, N = 8

Bar Area (Av) = 5.07 cm²

Number of bars = 1.63

Use 2 - N 8

3-D25

Minimum Base Required:

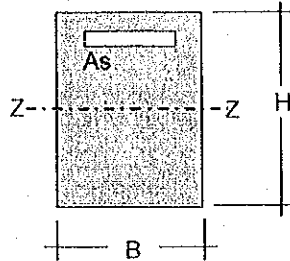
Max. bars per layer = 3

Minimum Base = 27.78 cm

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B/C axi FB-3 END
1/2 axis

BEAM DESIGN



$H = 60.00$ cm
 $b = 30.00$ cm
 $f_c = 210$ kg/cm²
 $f_y = 4200$ kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
Dead Load	11.50
Live Load	0.50
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	16.95
0.75(1.4DL+1.7LL+1.87)	12.71
0.75(1.4DL+1.7LL+1.87)	12.71

Force for design: $Mu_{z-z} = 16.95$ ton-m

$d = 52.46$ cm Clear cover = 5.00 cm

$f_y^2 / 1.7 b f_c A_s^2 - f_y d A_s + Mu / f = 0$ $f = 0.90$

$1647.06 A_s^2 - 220332 A_s + 1883333.3 = 0$ $A_s = 9.18$ cm²

$A_{smin} = (4/3)A_{sreq}$:

$(4/3)A_{sreq} = 12.24$ cm² }
 $(14/f_y) b d = 5.25$ cm² } $A_{smin} = 5.25$ cm²

$A_{smax} : r_b = 0.0345$ $A_{smax} (0.75r_b) = 40.68$ cm²

$A_s = 9.18$ cm² o.k!! $A_s < A_{max}$

Bar denomination, N = 8 Bar Area (A_v) = 5.07 cm²

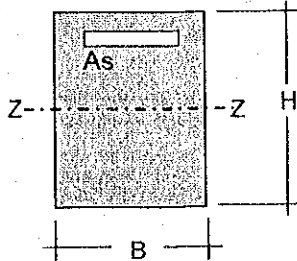
Number of bars = 1.81 Use 2 - N 8 3-D25

Minimum Base Required:

Max. bars per layer = 3 Minimum Base = 27.78 cm

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**B/C axi FB-3 CENTER
1/2 axis BEAM DESIGN**



H = 60.00 cm
 b = 30.00 cm
 $f_c = 210 \text{ kg/cm}^2$
 $f_y = 4200 \text{ kg/cm}^2$

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Load	12.40
Live Load	0.80
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	18.72
0.75(1.4DL+1.7LL+1.87	14.04
0.75(1.4DL+1.7LL+1.87	14.04

Force for design: $\mu_{z-z} = 18.72 \text{ ton-m}$

$d = 52.46 \text{ cm}$

Clear cover = 5.00 cm

$$f_y^2 / 1.7b^2 f_c A_s^2 - f_y d A_s + \mu / f = f = 0.90$$

$$1647.06 A_s^2 - 220332 A_s + 2080000 = 0 \quad A_s = 10.22 \text{ cm}^2$$

$A_{smin} = (4/3)A_{sreq}$

$$\left. \begin{aligned} (4/3)A_{sreq} &= 13.63 \text{ cm}^2 \\ (14/f_y) b d &= 5.25 \text{ cm}^2 \end{aligned} \right\} A_{smin} = 5.25 \text{ cm}^2$$

$$A_{smax} : r_b = 0.0345 \quad A_{smax} (0.75r_b) = 40.68 \text{ cm}^2$$

$$A_s = 10.22 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$$

Bar denomination, N = 8

Bar Area (A_v) = 5.07 cm²

Number of bars = 2.02 Use 3 - N 8 3-D25

Minimum Base Required:

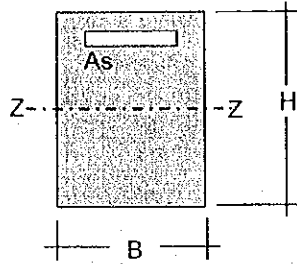
Max. bars per layer = 3 Minimum Base = 27.78 cm

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A/B axi FB-3 END

1/5 axis

BEAM DESIGN



H = 60.00 cm
 b = 30.00 cm
 $f_c = 210 \text{ kg/cm}^2$
 $f_y = 4200 \text{ kg/cm}^2$

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Load	9.80
Live Load	0.60
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	14.74
0.75(1.4DL+1.7LL+1.87)	11.06
0.75(1.4DL+1.7LL+1.87)	11.06

Force for design: $M_u \text{ z-z} = 14.74 \text{ ton-m}$

$d = 52.46 \text{ cm}$

Clear cover = 5.00 cm

$$f_y^2 / 1.7 b f_c A_s^2 - f_y d A_s + M_u / f = f = 0.90$$

$$1647.06 A_s^2 - 220332 A_s + 1637777.8 = 0 \quad A_s = 7.90 \text{ cm}^2$$

$A_{smin} = (4/3) A_{sreq}$:

$$\left. \begin{array}{l} (4/3) A_{sreq} = 10.53 \text{ cm}^2 \\ (14/f_y) b d = 5.25 \text{ cm}^2 \end{array} \right\} A_{smin} = 5.25 \text{ cm}^2$$

$$A_{smax} : r_b = 0.0345 \quad A_{smax} (0.75 r_b) = 40.68 \text{ cm}^2$$

$$A_s = 7.90 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$$

Bar denomination, N = 8

Bar Area (A_v) = 5.07 cm²

Number of bars = 1.56

Use 2 - N 8

3-D25

Minimum Base Required:

Max. bars per layer = 3

Minimum Base = 27.78 cm

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A/B axi FB-3 CENTER
1/5 axis **BEAM DESIGN**

H = 60.00 cm

b = 30.00 cm

f_c = 210 kg/cm²

f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
Dead Load	9.60
Live Load	0.40
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	14.12
0.75(1.4DL+1.7LL+1.87	10.59
0.75(1.4DL+1.7LL+1.87	10.59

Force for design: Mu z-z = 14.12 ton-m

d = 52.46 cm Clear cover = 5.00 cm

$f_y^2/1.7b^2f_c As^2 - f_yd As + Mu/f = f = 0.90$

1647.06 As²220332 1568888.9 = 0 As = 7.55 cm²

Asmin = (4/3)Asreq :

(4/3)Asreq = 10.06 cm² }
 (14/f_y) b d = 5.25 cm² }

Asmin = 5.25 cm²

Asmax : rb = 0.0345 Asmax (0.75rb) = 40.68 cm²

As = 7.55 cm² o.k!! As < Amax

Bar denomination, N = 8 Bar Area (A_v) = 5.07 cm²

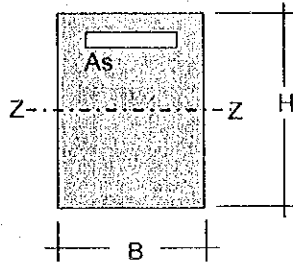
Number of bars = 1.49 Use 2 - N 8 3-D25

Minimum Base Required:

Max. bars per layer = 3 Minimum Base = 27.78 cm

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A/B axi FB-3a CENTER
6/7 axis **BEAM DESIGN**



H = 60.00 cm
 b = 30.00 cm
 $f_c = 210 \text{ kg/cm}^2$
 $f_y = 4200 \text{ kg/cm}^2$

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O	MOMENT
LOAD	Mz-z

Dead Load	19.70
Live Load	2.90
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	32.51
0.75(1.4DL+1.7LL+1.87)	24.38
0.75(1.4DL+1.7LL+1.87)	24.38

Force for design: $M_u \text{ z-z} = 32.51 \text{ ton-m}$

$d = 52.46 \text{ cm}$

Clear cover = 5.00 cm

$f_y^2/1.7b f_c A_s^2 - f_y d A_s + M_u/f = f = 0.90$

$1647.06 A_s^2 - 220332 A_s + 3612222.2 = 0 \quad A_s = 19.13 \text{ cm}^2$

$A_{smin} = (4/3)A_{sreq}$:

$(4/3)A_{sreq} = 25.51 \text{ cm}^2$
 $(14/f_y) b d = 5.25 \text{ cm}^2$

} $A_{smin} = 5.25 \text{ cm}^2$

$A_{smax} : r_b = 0.0345 \quad A_{smax} (0.75r_b) = 40.68 \text{ cm}^2$

$A_s = 19.13 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$

Bar denomination, N = 8

Bar Area (A_v) = 5.07 cm²

Number of bars = 3.78

Use 4 - N 8

3/2-D25

Minimum Base Required:

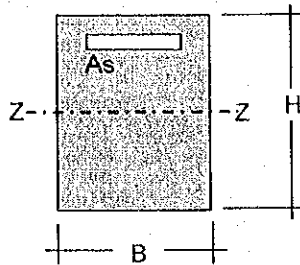
Max. bars per layer = 3

Minimum Base = 27.78 cm

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A/B axi FB-3a END

6/8 axis BEAM DESIGN



H = cm

b = cm

$f_c = 210$ kg/cm²

$f_y = 4200$ kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Load	13.50
Live Load	1.50
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	21.45
0.75(1.4DL+1.7LL+1.87	16.09
0.75(1.4DL+1.7LL+1.87	16.09

Force for design: $M_u z-z = 21.45$ ton-m

d = cm

Clear cover = cm

$f_y^2/1.7bf_c A_s^2 - f_y d A_s + M_u/f = f = 0.90$

$1647.06 A_s^2 - 220332 A_s + 2383333.3 = 0 \quad A_s = 11.87 \text{ cm}^2$

$A_{smin} = (4/3)A_{sreq}$:

$(4/3)A_{sreq} = 15.83 \text{ cm}^2$
 $(14/f_y) b d = 5.25 \text{ cm}^2$

} $A_{smin} = 5.25 \text{ cm}^2$

$A_{smax} : r_b = 0.0345 \quad A_{smax} (0.75r_b) = 40.68 \text{ cm}^2$

$A_s = 11.87 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$

Bar denomination, N =

Bar Area (A_v) = cm²

Number of bars =

Use 3 - N 8

3/2-D25

Minimum Base Required:

Max. bars per layer =

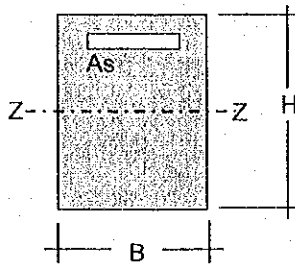
Minimum Base = cm

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A/B axi FB-3a CENTER

6/8 axis

BEAM DESIGN



H = 60.00 cm

b = 30.00 cm

f_c = 210 kg/cm²

f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O	MOMENT
LOAD	Mz-z

Dead Load	10.80
Live Load	0.90
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	16.65
0.75(1.4DL+1.7LL+1.87	12.49
0.75(1.4DL+1.7LL+1.87	12.49

Force for design: Mu z-z = 16.65 ton-m

d = 52.46 cm

Clear cover = 5.00 cm

$f_y^2/1.7b^2f_c As^2 - f_y d As + Mu/f = f = 0.90$

1647.06 As² - 220332 As + 1850000 = 0 As = 9.00 cm²

Asmin = (4/3)Asreq :

$(4/3)Asreq = 12.00 \text{ cm}^2$
 $(14/f_y) b d = 5.25 \text{ cm}^2$

} Asmin = 5.25 cm²

Asmax : rb = 0.0345 Asmax (0.75rb) = 40.68 cm²

As = 9.00 cm² o.k!! As < Amax

Bar denomination, N = 8

Bar Area (Av) = 5.07 cm²

Number of bars = 1.78

Use 2 - N 8

3/2-D25

Minimum Base Required:

Max. bars per layer = 3

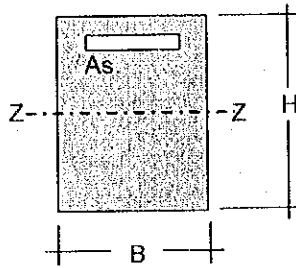
Minimum Base = 27.78 cm

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D axis FB-2 END

4 axis

BEAM DESIGN



H = 80.00 cm
 b = 35.00 cm
 $f_c = 210 \text{ kg/cm}^2$
 $f_y = 4200 \text{ kg/cm}^2$

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O	MOMENT
LOAD	Mz-z

Dead Load	0.40
Live Load	0.10
Seismic x	23.60
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	0.73
0.75(1.4DL+1.7LL+1.87	33.65
0.75(1.4DL+1.7LL+1.87	0.55

Force for design: $Mu_{z-z} = 33.70 \text{ ton-m}$

$d = 72.46 \text{ cm}$ Clear cover = 5.00 cm

$f_y^2 / 1.7 b f_c A_s^2 - f_y d A_s + M_u / f = f = 0.90$

$1411.76 A_s^2 - 304332 A_s + 3744444.4 = 0$ $A_s = 13.10 \text{ cm}^2$

$A_{smin} = (4/3) A_{sreq}$:

$(4/3) A_{sreq} = 17.47 \text{ cm}^2$
 $(14/f_y) b d = 8.45 \text{ cm}^2$ } $A_{smin} = 8.45 \text{ cm}^2$

$A_{smax} : r_b = 0.0345$ $A_{smax} (0.75 r_b) = 65.55 \text{ cm}^2$

$A_s = 13.10 \text{ cm}^2$ o.k!! $A_s < A_{max}$

Bar denomination, N = 8 Bar Area (A_v) = 5.07 cm²

Number of bars = 2.59 Use 3 - N 8 3-D25

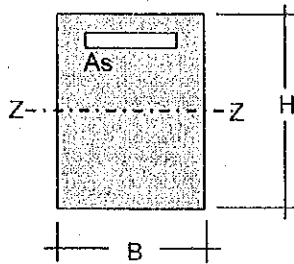
Minimum Base Required:

Max. bars per layer = 3 Minimum Base = 27.78 cm

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6 axis FB-2 CENTER

C/D axis BEAM DESIGN



H = 80.00 cm

b = 35.00 cm

f_c = 210 kg/cm²

f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Load	15.10
Live Load	1.70
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	24.03
0.75(1.4DL+1.7LL+1.87)	18.02
0.75(1.4DL+1.7LL+1.87)	18.02

Force for design: Mu z-z = 24.03 ton-m

d = 72.46 cm

Clear cover = 5.00 cm

$f_y^2/1.7b^2f_c As^2 - f_y d As + Mu/f = f = 0.90$

$1411.76 As^2 - 304332 As + 2670000 = 0$ As = 9.16 cm²

As_{min} = (4/3)As_{req} :

$(4/3)As_{req} = 12.22 \text{ cm}^2$
 $(14/f_y) b d = 8.45 \text{ cm}^2$

} As_{min} = 8.45 cm²

As_{max} : rb = 0.0345 As_{max} (0.75rb) = 65.55 cm²

As = 9.16 cm² o.k!! As < A_{max}

Bar denomination, N = 8

Bar Area (A_v) = 5.07 cm²

Number of bars = 1.81

Use 2 - N 8

3-D25

Minimum Base Required:

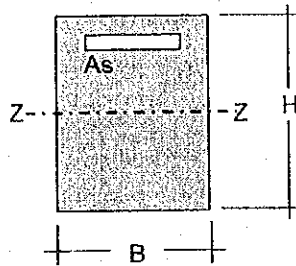
Max. bars per layer = 3

Minimum Base = 27.78 cm

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3 axis FB-1 OUTEREND

C axis BEAM DESIGN



H = cm
 b = cm
 f_c = kg/cm²
 f_y = kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Load	12.80
Live Load	1.80
Seismic x	67.10
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	20.98
0.75(1.4DL+1.7LL+1.87)	109.84
0.75(1.4DL+1.7LL+1.87)	15.74

Force for design: Mu z-z = ton-m

d = cm

Clear cover = cm

$$f_y^2/1.7bfc As^2 - f_yd As + Mu/f = f = 0.90$$

$$1235.29 As^2 - 302999 As + 1220444 = 0 \quad As = 50.80 \text{ cm}^2$$

As_{min} = (4/3)As_{req} :

$$\left. \begin{array}{l} (4/3)As_{req} = 67.73 \text{ cm}^2 \\ (14/f_y) b d = 9.62 \text{ cm}^2 \end{array} \right\} As_{min} = 9.62 \text{ cm}^2$$

As_{max} : rb = 0.0345 As_{max} (0.75rb) = 74.58 cm²

As = 50.80 cm² o.k!! As < A_{max}

Bar denomination, N =

Bar Area (A_v) = 8.17 cm²

Number of bars = 6.22

Use 7 - N 10

4/3-D32

Minimum Base Required:

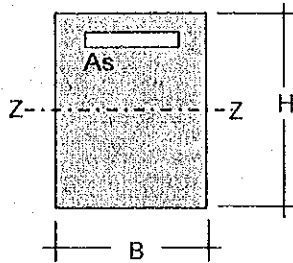
Max. bars per layer =

Minimum Base = 37.94 cm

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7 axis FB-1 INNEREND

B axis BEAM DESIGN



H = 80.00 cm

b = 40.00 cm

f_c = 210 kg/cm²

f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Load	34.40
Live Load	6.20
Seismic x	34.60
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	58.70
0.75(1.4DL+1.7LL+1.87	92.55
0.75(1.4DL+1.7LL+1.87	44.03

Force for design: Mu z-z = 92.55 ton-m

d = 72.14 cm

Clear cover = 5.00 cm

$f_y^2/1.7b f_c A_s^2 - f_y d A_s + M_u/f = f = 0.90$

$1235.29 A_s^2 - 302999 A_s + 10283333 = 0$ A_s = 40.69 cm²

A_{smin} = (4/3)A_{sreq} :

$(4/3)A_{sreq} = 54.25 \text{ cm}^2$
 $(14/f_y) b d = 9.62 \text{ cm}^2$ } A_{smin} = 9.62 cm²

A_{smax} : r_b = 0.0345 A_{smax} (0.75r_b) = 74.58 cm²

A_s = 40.69 cm² o.k!! A_s < A_{max}

Bar denomination, N = 10

Bar Area (A_v) = 8.17 cm²

Number of bars = 4.98

Use 5 - N 10

4/1-D32

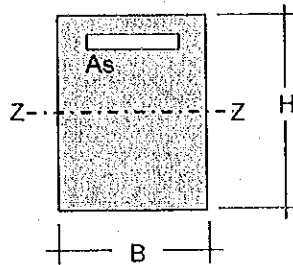
Minimum Base Required:

Max. bars per layer = 4

Minimum Base = 37.94 cm

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6 axis FB-1 CENTER
C/D axis **BEAM DESIGN**



$H = 80.00$ cm
 $b = 40.00$ cm
 $f_c = 210$ kg/cm²
 $f_y = 4200$ kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE OF LOAD	MOMENT Mz-z
--------------	-------------

Dead Load	36.40
Live Load	6.20
Seismic x	0.00
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	61.50
0.75(1.4DL+1.7LL+1.87)	46.13
0.75(1.4DL+1.7LL+1.87)	46.13

Force for design: $M_u z-z = 61.50$ ton-m

$d = 72.14$ cm

Clear cover = 5.00 cm

$$f_y^2 / 1.7 b f_c A_s^2 - f_y d A_s + M_u / f = f = 0.90$$

$$1235.29 A_s^2 - 302999 A_s + 6833333.3 = 0 \quad A_s = 25.13 \text{ cm}^2$$

$A_{smin} = (4/3)A_{sreq}$:

$$\left. \begin{aligned} (4/3)A_{sreq} &= 33.50 \text{ cm}^2 \\ (14/f_y) b d &= 9.62 \text{ cm}^2 \end{aligned} \right\} A_{smin} = 9.62 \text{ cm}^2$$

$$A_{smax} : r_b = 0.0345 \quad A_{smax} (0.75r_b) = 74.58 \text{ cm}^2$$

$$A_s = 25.13 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$$

Bar denomination, $N = 10$

Bar Area (A_v) = 8.17 cm²

Number of bars = 3.08

Use **4 - N 10**

4-D32

Minimum Base Required:

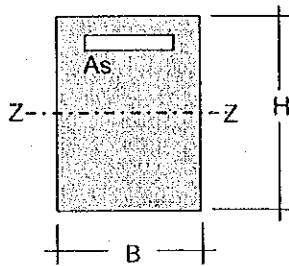
Max. bars per layer = 4

Minimum Base = 37.94 cm

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5 axis FB-1A OUTEREND

D axis BEAM DESIGN



H = cm
 b = cm
 f_c = kg/cm²
 f_y = kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Load	21.30
Live Load	3.80
Seismic x	91.50
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	36.28
0.75(1.4DL+1.7LL+1.87	155.54
0.75(1.4DL+1.7LL+1.87	27.21

Force for design: μ_{z-z} = ton-m

d = cm

Clear cover = cm

$f_y^2/1.7b f_c A_s^2 - f_y d A_s + \mu_{z-z} / f = f = 0.90$

$898.40 A_s^2 - 302999 A_s + 17282222 = 0 \quad A_s = 72.71 \text{ cm}^2$

$A_{smin} = (4/3)A_{sreq}$:

$(4/3)A_{sreq} = 96.95 \text{ cm}^2$
 $(14/f_y) b d = 13.23 \text{ cm}^2$

} $A_{smin} = 13.23 \text{ cm}^2$

$A_{smax} : r_b = 0.0345 \quad A_{smax} (0.75r_b) = 102.55 \text{ cm}^2$

$A_s = 72.71 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$

Bar denomination, N =

Bar Area (A_v) = cm²

Number of bars =

Use 9 - N 10

6/3-D32

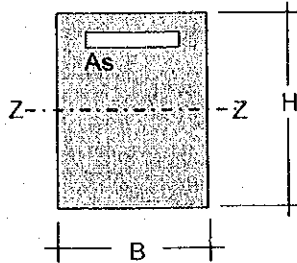
Minimum Base Required:

Max. bars per layer =

Minimum Base = cm

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**6 axis FB-1A INNEREND
B axis BEAM DESIGN**



H = 80.00 cm
 b = 55.00 cm
 $f_c = 210 \text{ kg/cm}^2$
 $f_y = 4200 \text{ kg/cm}^2$

Forces and Moments, from Structural Analysis (ton , m) :

TYPE O LOAD	MOMENT Mz-z
----------------	----------------

Dead Load	33.90
Live Load	5.70
Seismic x	53.30
Seismic y	0.00

COMBINATION	Mu z-z
C1=1.4 DL+1.7 LL	57.15
0.75(1.4DL+1.7LL+1.87)	117.62
0.75(1.4DL+1.7LL+1.87)	42.86

Force for design: $\mu_{z-z} = 117.62 \text{ ton-m}$

$d = 72.14 \text{ cm}$

Clear cover = 5.00 cm

$$f_y^2 / 1.7b f_c A_s^2 - f_y d A_s + \mu / f = f = 0.90$$

$$898.40 A_s^2 - 302999 A_s + 13068889 = 0 \quad A_s = 50.78 \text{ cm}^2$$

$A_{smin} = (4/3)A_{sreq}$:

$$\left. \begin{array}{l} (4/3)A_{sreq} = 67.70 \text{ cm}^2 \\ (14/f_y) b d = 13.23 \text{ cm}^2 \end{array} \right\} A_{smin} = 13.23 \text{ cm}^2$$

$$A_{smax} : r_b = 0.0345 \quad A_{smax} (0.75r_b) = 102.55 \text{ cm}^2$$

$$A_s = 50.78 \text{ cm}^2 \quad \text{o.k!! } A_s < A_{max}$$

Bar denomination, N = 10

Bar Area (A_v) = 8.17 cm²

Number of bars = 6.21

Use 7 - N 10

5/2-D32

Minimum Base Required:

Max. bars per layer = 5

Minimum Base = 44.29 cm

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2nd Floor CB-1

q = 0.30 t/m (self weight)
 PDL = 4.57875 t PLL = 1.1025 t
 MDL = 4.97 tm MLL = 1.16 tm

H = 50.00 cm
 b = 30.00 cm
 f_c = 280 kg/cm²
 f_y = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

Dead Loa	4.97	COMBINATION	Mu z-z
Live Load	1.16	C1=1.4 DL+1.7 LL	8.93

Force for design: Mu z-z = 8.93 ton-m

d = 42.46 cm Clear cover = 5.00 cm

$f_y^2/1.7bf_c As^2 - f_yd As + Mu/f = 0$ f = 0.90

1235.29 As²+78332 992222.2 = 0 As = 5.80 cm²

Asmin = (4/3)Asreq :

(4/3)Asreq =	7.73	cm ²	}	Asmin =	4.25	cm ²
(14/f _y) b d =	4.25	cm ²				

Asmax : rb = 0.0459 Asmax (0.75rb) = 43.90 cm²

As = 5.80 cm² o.k!! As < Amax

Bar denomination, N = 8 Bar Area (A_v) = 5.07 cm²

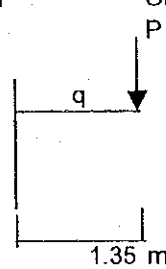
Number of bars = 1.14 Use 2 - N 8 3-D25

Minimum Base Required:

Max. bars per layer = 3 Minimum Base = 27.78 cm

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4th Floor CB-1

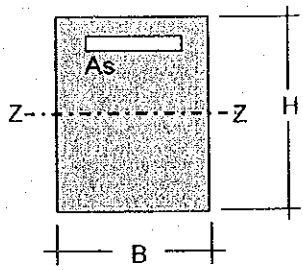


1.35 m

q = 0.30 t/m (self weight)

PDL = 5.681 t PLL = 0.081 t

MDL = 7.94 tm MLL = 0.11 tm



H = 50.00 cm

b = 30.00 cm

f'c = 280 kg/cm²

fy = 4200 kg/cm²

Forces and Moments, from Structural Analysis (ton , m) :

Dead Loa	7.94	COMBINATION	Mu z-z
Live Load	0.11	C1=1.4 DL+1.7 LL	11.31

Force for design: Mu z-z = 14.37 ton-m

d = 42.46 cm Clear cover = 5.00 cm

$f_y^2/1.7bf'c As^2 - f_y d As + Mu/f = 0.90$

1235.29 As² - 178332 1596667 = 0 As = 9.59 cm²

Asmin = (4/3)Asreq :

(4/3)Asreq = 12.79 cm²

(14/fy) b d = 4.25 cm²

}

Asmin = 4.25 cm²

Asmax : rb = 0.0459 Asmax (0.75rb) = 43.90 cm²

As = 9.59 cm² o.k!! As < Amax

Bar denomination, N = 8 Bar Area (Av) = 5.07 cm²

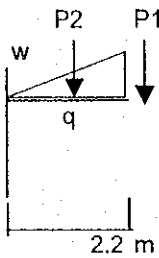
Number of bars = 1.89 **Use 2 - N 8** 3-D25

Minimum Base Required:

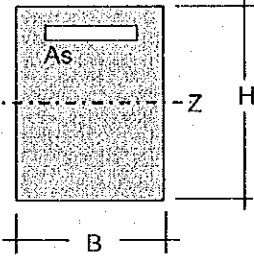
Max. bars per layer = 3 Minimum Base = 27.78 cm

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2nd Floor CB-2



$q = 0.25 \text{ t/m}$ (self weight)
 $wDL = 0.43 \text{ t/m}^2$ $wLL = 0.35 \text{ t/m}^2$
 $P1DL = 0.06 \text{ t}$ $P1LL = 0.44 \text{ t}$ stairs
 $P2DL = 0.125 \text{ t}$ $P2LL = 0.875 \text{ t}$
 $MDL = 2.46 \text{ tm}$ $MLL = 3.22 \text{ tm}$



$H = 40.00 \text{ cm}$
 $b = 40.00 \text{ cm}$
 $f_c = 280 \text{ kg/cm}^2$
 $f_y = 4200 \text{ kg/cm}^2$

Forces and Moments, from Structural Analysis (ton , m) :

Dead Loa	2.46	COMBINATION	Mu z-z
Live Load	3.22	C1=1.4 DL+1.7 LL	8.92

Force for design: $Mu \text{ z-z} = 8.92 \text{ ton-m}$

$d = 32.46 \text{ cm}$ Clear cover = 5.00 cm

$f_y^2 / 1.7 b f_c A_s^2 - f_y d A_s + Mu / f = 0.90$
 $926.47 A_s^2 + 136332 - 991111.1 = 0$ $A_s = 7.67 \text{ cm}^2$

$A_{smin} = (4/3) A_{sreq}$:

$(4/3) A_{sreq} = 10.23 \text{ cm}^2$	} $A_{smin} = 4.33 \text{ cm}^2$
$(14/f_y) b d = 4.33 \text{ cm}^2$	

$A_{smax} :$ $rb = 0.0459$ $A_{smax} (0.75rb) = 44.74 \text{ cm}^2$
 $A_s = 7.67 \text{ cm}^2$ **o.k!! $A_s < A_{max}$**

Bar denomination, $N = 8$ Bar Area (A_v) = 5.07 cm^2

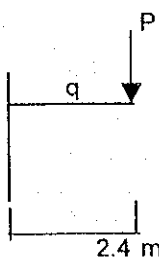
Number of bars = 1.51 **Use 2 - N 8** 3-D25

Minimun Base Required:

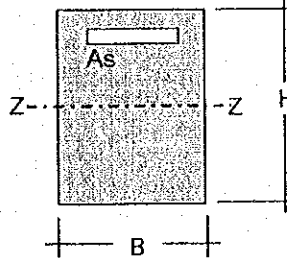
Max. bars per layer = 3 Minimum Base = 27.78 cm

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4th Floor CB-3



$q = 0.35 \text{ t/m}$ (self weight)
 $PDL = 7.020 \text{ t}$
 $PLL = 0.144 \text{ t}$
 $MDL = 17.86 \text{ tm}$
 $MLL = 0.35 \text{ tm}$



$H = 60.00 \text{ cm}$
 $b = 40.00 \text{ cm}$
 $f_c = 280 \text{ kg/cm}^2$
 $f_y = 4200 \text{ kg/cm}^2$

Forces and Moments, from Structural Analysis (ton , m) :

Dead Loa	17.86	COMBINATION	Mu z-z
Live Load	0.35	C1=1.4 DL+1.7 LL	25.59

Force for design: $Mu \text{ z-z} = 25.59 \text{ ton-m}$

$d = 52.46 \text{ cm}$ Clear cover = 5.00 cm

$f_y^2/1.7bf_c As^2 - f_yd As + Mu/f = 0$ $f = 0.90$
 $926.47 As^2 - 220332 As + 2843333 = 0$ $As = 13.69 \text{ cm}^2$

$As_{min} = (4/3)As_{req}$:
 $(4/3)As_{req} = 18.26 \text{ cm}^2$
 $(14/f_y) b d = 6.99 \text{ cm}^2$ } $As_{min} = 6.99 \text{ cm}^2$

As_{max} : $rb = 0.0459$ $As_{max} (0.75rb) = 72.31 \text{ cm}^2$

$As = 13.69 \text{ cm}^2$ o.k!! $As < A_{max}$

Bar denomination, N = 8 Bar Area (A_v) = 5.07 cm^2

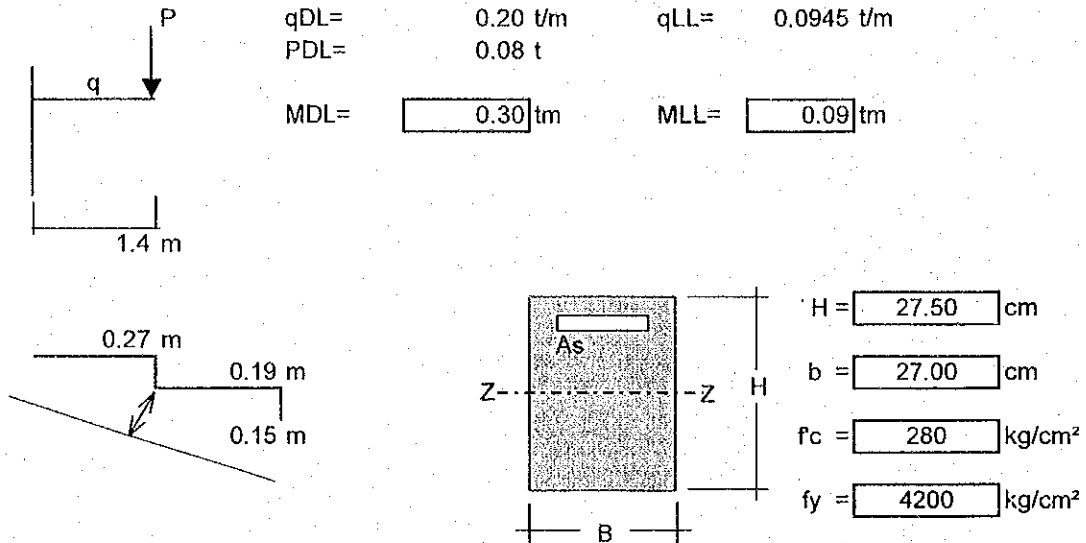
Number of bars = 2.70 Use **3 - N 8** 4-D25

Minimum Base Required:

Max. bars per layer = 4 Minimum Base = 32.86 cm

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RC STAIRS



Forces and Moments, from Structural Analysis (ton , m) :

Dead Loa	0.30	COMBINATION	Mu z-z
Live Load	0.09	C1=1.4 DL+1.7 LL	0.58

Force for design: $Mu \text{ z-z} = 0.58 \text{ ton-m}$

$d = 21.60 \text{ cm}$ Clear cover = 4.00 cm

$f_y^2/1.7bf_c As^2 - f_y d As + Mu/f \quad f = 0.90$

$1372.55 As^2 - 90699 \quad 64444.44 = 0 \quad As = 0.72 \text{ cm}^2$

$As_{min} = (4/3)As_{req}$:

$(4/3)As_{req} = 0.96 \text{ cm}^2$
 $(14/f_y) b d = 1.94 \text{ cm}^2$ } $As_{min} = 0.96 \text{ cm}^2$

$As_{max} : \quad r_b = 0.0459 \quad As_{max} (0.75r_b) = 20.09 \text{ cm}^2$

$As = 0.96 \text{ cm}^2 \quad \text{o.k!! } As < A_{max}$

Bar denomination, $N = 4$ Bar Area (A_v) = 1.27 cm^2

Number of bars = 0.76 Use 1 - N 4 2-D13

Minimum Base Required:

Max. bars per layer = 2 Minimum Base = 18.08 cm

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Slab S1 for 2nd roof

lx = 3.0 m

ly = 4.0 m

1.3

t = 15 cm

coefficient of bend (thioretical result fix end)

d = 10.35 cm	Mx1/(w lx ²) = 0.068
fc = 280 kg/cm ²	Mx2/(w lx ²) = 0.030
fy = 4200 kg/cm ²	My1/(w lx ²) = 0.056
	My2/(w lx ²) = 0.015

wDL = 0.515 t/m ²	wLL = 0.350 t/m ²
------------------------------	------------------------------

DL	LL
Mx1 = 0.32 tm/m	Mx1 = 0.21 tm/m
Mx2 = 0.14 tm/m	Mx2 = 0.09 tm/m
My1 = 0.26 tm/m	My1 = 0.18 tm/m
My2 = 0.07 tm/m	My2 = 0.05 tm/m

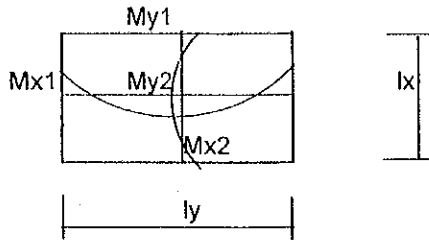
1.4DL+1.7LL	fy/1.7bfc'	fyd	Mu/f	
Mx1 = 0.81 tm/m	370.6	43470	89488 As =	2.10 cm ² /m
Mx2 = 0.36 tm/m	370.6	43470	39480 As =	0.92 cm ² /m
My1 = 0.66 tm/m	370.6	43470	73696 As =	1.72 cm ² /m
My2 = 0.18 tm/m	370.6	43470	19740 As =	0.46 cm ² /m

	Short Span			Long Span		
	Use Bar	Area cm ²	Pitch cm	Use Bar	Area cm ²	Pitch cm
End	3	0.71	34.0	3	0.71	41.4
Center	3	0.71	77.8	3	0.71	156.3

Thickness (mm)	Location	Shorter Side (Direction)				Longer Side (Direction)			
		Edge Strip		Middle Strip		Edge Strip		Middle Strip	
		End	Center	End	Center	End	Center	End	Center
S1 150	Top	D10-@200		-		D10-@250		-	
	Bottom	D10-@200		-		D10-@250		-	

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Slab S1 for 4th meeting room



$l_x = 3.5$ m
 $l_y = 6.0$ m
 $t = 15$ cm

coefficient of bend (thioretical result fix end)

$d = 10.35$ cm	$M_{x1}/(w l_x^2) = 0.080$
$f_c = 280$ kg/cm ²	$M_{x2}/(w l_x^2) = 0.038$
$f_y = 4200$ kg/cm ²	$My_1/(w l_x^2) = 0.057$
	$My_2/(w l_x^2) = 0.020$

$w_{DL} = 0.435$ t/m²
 $w_{LL} = 0.350$ t/m²

DL	LL
$M_{x1} = 0.43$ tm/m	$M_{x1} = 0.34$ tm/m
$M_{x2} = 0.20$ tm/m	$M_{x2} = 0.16$ tm/m
$My_1 = 0.30$ tm/m	$My_1 = 0.24$ tm/m
$My_2 = 0.11$ tm/m	$My_2 = 0.09$ tm/m

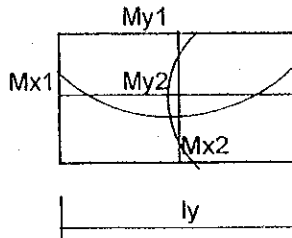
1.4DL+1.7LL		$f_y/1.7bfc'$	f_{yd}	M_u/f	
$M_{x1} = 1.18$ tm/m	370.6	43470	131102 As=	3.10 cm ² /m	
$M_{x2} = 0.56$ tm/m	370.6	43470	62273.6 As=	1.45 cm ² /m	
$My_1 = 0.84$ tm/m	370.6	43470	93410.3 As=	2.19 cm ² /m	
$My_2 = 0.29$ tm/m	370.6	43470	32775.6 As=	0.76 cm ² /m	

	Short Span			Long Span		
	Use Bar	Area cm ²	Pitch cm	Use Bar	Area cm ²	Pitch cm
End	3	0.71	23.0	3	0.71	32.5
Center	3	0.71	49.1	3	0.71	93.9

Thicknes (mm)	Location	Shorter Side (Direction)				Longer Side (Direction)			
		Edge Strip		Middle Strip		Edge Strip		Middle Strip	
		End	Center	End	Center	End	Center	End	Center
S1 150	Top	D10-@200		-		D10-@250		-	
	Bottom	D10-@200		-		D10-@250		-	

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Slab S2 for 2nd roof



lx = 3.0 m

ly = 4.0 m

1.3

t = 12 cm

coefficient of bend (thioretical result fix end)

d = 7.35 cm
 fc = 280 kg/cm²
 fy = 4200 kg/cm²

Mx1/(w lx ²) =	0.068
Mx2/(w lx ²) =	0.030
My1/(w ly ²) =	0.056
My2/(w ly ²) =	0.015

wDL = 0.443 t/m²

wLL = 0.020 t/m²

DL

Mx1 = 0.27 tm/m
 Mx2 = 0.12 tm/m
 My1 = 0.22 tm/m
 My2 = 0.06 tm/m

LL

Mx1 = 0.01 tm/m
 Mx2 = 0.01 tm/m
 My1 = 0.01 tm/m
 My2 = 0.00 tm/m

1.4DL+1.7LL

Mx1 =	0.40	tm/m
Mx2 =	0.18	tm/m
My1 =	0.33	tm/m
My2 =	0.09	tm/m

fy/1.7bfc'

fyd

Mu/f

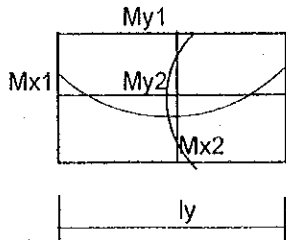
Mx1 =	370.6	30870	44485.6	As =		1.47	cm ² /m
Mx2 =	370.6	30870	19626	As =		0.64	cm ² /m
My1 =	370.6	30870	36635.2	As =		1.20	cm ² /m
My2 =	370.6	30870	9813	As =		0.32	cm ² /m

	Short Span			Long Span		
	Use Bar	Area cm ²	Pitch cm	Use Bar	Area cm ²	Pitch cm
End	3	0.71	48.6	3	0.71	59.2
Center	3	0.71	111.2	3	0.71	223.3

Thickness (mm)	Location	Shorter Side (Direction)				Longer Side (Direction)			
		Edge Strip		Middle Strip		Edge Strip		Middle Strip	
		End	Center	End	Center	End	Center	End	Center
S2 120	Top	D10-@200		-		D10-@250		-	
	Bottom	D10-@200		-		D10-@250		-	

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Slab S2 for top roof



lx = 3.0 m

ly = 3.5 m

1.2

t = 12 cm

coefficient of bend (thioretical result fix end)

d = 7.35 cm	Mx1/(w lx ²) = 0.065
fc = 280 kg/cm ²	Mx2/(w lx ²) = 0.030
fy = 4200 kg/cm ²	My1/(w lx ²) = 0.055
	My2/(w lx ²) = 0.028

wDL = 0.443 t/m²

wLL = 0.020 t/m²

DL

Mx1 = 0.26 tm/m
Mx2 = 0.12 tm/m
My1 = 0.22 tm/m
My2 = 0.11 tm/m

LL

Mx1 = 0.01 tm/m
Mx2 = 0.01 tm/m
My1 = 0.01 tm/m
My2 = 0.01 tm/m

1.4DL+1.7LL

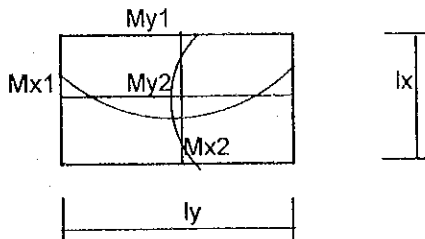
		fy/1.7bfc'	fyd	Mu/f	
Mx1 = 0.38 tm/m	370.6	30870	42523 As =	1.40 cm ² /m	
Mx2 = 0.18 tm/m	370.6	30870	19626 As =	0.64 cm ² /m	
My1 = 0.32 tm/m	370.6	30870	35981 As =	1.18 cm ² /m	
My2 = 0.16 tm/m	370.6	30870	18317.6 As =	0.60 cm ² /m	

	Short Span			Long Span		
	Use Bar	Area cm ²	Pitch cm	Use Bar	Area cm ²	Pitch cm
End	3	0.71	50.9	3	0.71	60.3
Center	3	0.71	111.2	3	0.71	119.2

Thicknes (mm)	Location	Shorter Side (Direction)				Longer Side (Direction)			
		Edge Strip		Middle Strip		Edge Strip		Middle Strip	
		End	Center	End	Center	End	Center	End	Center
S2 120	Top	D10-@200		-		D10-@250		-	
	Bottom	D10-@200				D10-@250			

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Slab S4 for 2nd landing



lx= 2.2 m
 ly= 2.3 m
 1.0
 t= 15 cm

coefficient of bend (thioretical result 2side fix end)

d= 10.35 cm	$Mx1/(w lx^2) =$	0.290
fc= 280 kg/cm ²	$Mx2/(w lx^2) =$	0.040
fy= 4200 kg/cm ²	$My1/(w ly^2) =$	0.290
	$My2/(w ly^2) =$	0.040

wDL= 0.425 t/m²
 wLL= 0.350 t/m²

DL	LL
Mx1= 0.60 tm/m	Mx1= 0.49 tm/m
Mx2= 0.08 tm/m	Mx2= 0.07 tm/m
My1= 0.60 tm/m	My1= 0.49 tm/m
My2= 0.08 tm/m	My2= 0.07 tm/m

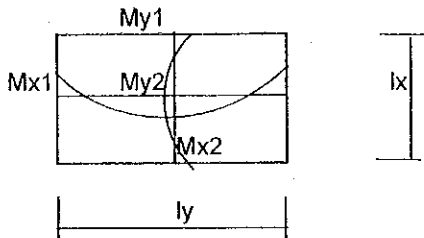
1.4DL+1.7LL	fy/1.7bfc'	fyd	Mulf	
Mx1= 1.67 tm/m	370.6	43470	185587 As=	4.44 cm ² /m
Mx2= 0.23 tm/m	370.6	43470	25598.2 As=	0.59 cm ² /m
My1= 1.67 tm/m	370.6	43470	185587 As=	4.44 cm ² /m
My2= 0.23 tm/m	370.6	43470	25598.2 As=	0.59 cm ² /m

	Short Span			Long Span		
	Use Bar	Area cm ²	Pitch cm	Use Bar	Area cm ²	Pitch cm
End	4	1.27	28.5	4	1.27	28.5
Center	3	0.71	120.4	3	0.71	120.4

Thicknes (mm)	Location	Shorter Side (Direction)				Longer Side (Direction)			
		Edge Strip		Middle Strip		Edge Strip		Middle Strip	
		End	Center	End	Center	End	Center	End	Center
S4 150	Top	D13-@200				D13-@200			
	Bottom	D10-@200				D10-@200			

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Slab S5 for 2nd landing



$l_x =$ 1.5 m
 $l_y =$ 2.8 m
 1.9
 $t =$ 15 cm

coefficient of bend (thioretical result 2side fix end)

$d =$ 10.35 cm	$Mx1/(w l_x^2) =$ 0.200
$fc =$ 280 kg/cm ²	$Mx2/(w l_x^2) =$ 0.030
$fy =$ 4200 kg/cm ²	$My1/(w l_x^2) =$ 0.270
	$My2/(w l_x^2) =$ 0.100

$wDL =$ 0.425 t/m²
 $wLL =$ 0.350 t/m²

DL	LL
$Mx1 =$ 0.19 tm/m	$Mx1 =$ 0.16 tm/m
$Mx2 =$ 0.03 tm/m	$Mx2 =$ 0.02 tm/m
$My1 =$ 0.26 tm/m	$My1 =$ 0.21 tm/m
$My2 =$ 0.10 tm/m	$My2 =$ 0.08 tm/m

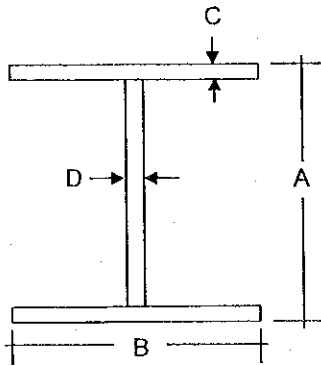
1.4DL+1.7LL	$fy/1.7bc'$	fyd	Mu/f	
$Mx1 =$ 0.54 tm/m	370.6	43470	59500 As=	1.39 cm ² /m
$Mx2 =$ 0.08 tm/m	370.6	43470	8925 As=	0.21 cm ² /m
$My1 =$ 0.72 tm/m	370.6	43470	80325 As=	1.88 cm ² /m
$My2 =$ 0.27 tm/m	370.6	43470	29750 As=	0.69 cm ² /m

	Short Span			Long Span		
	Use Bar	Area cm ²	Pitch cm	Use Bar	Area cm ²	Pitch cm
End	3	0.71	51.4	3	0.71	37.9
Center	3	0.71	346.4	3	0.71	103.5

Thickness (mm)	Location	Shorter Side (Direction)				Longer Side (Direction)			
		Edge Strip		Middle Strip		Edge Strip		Middle Strip	
		End	Center	End	Center	End	Center	End	Center
S5 150	Top	D10-@300				D10-@200			
	Bottom	D10-@300				D10-@200			

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B-1



Beam type = **W14x34**

A = **13.98** in

B = **6.745** in

C = **0.455** in

D = **0.285** in

Area = 10.000 in²

I = 340.00 in⁴

Yc = 6.990 in

S = 48.64 in³

Pd = **0.20** ton

Md = **1.70** ton-m

PL = **0.00** ton

ML = **1.70** ton-m

P/A(d+L)	3.10	}
P/A(d+L+s)	2.33	
Md+ L/S =	426.56	
Ms+d+L/S =	319.92	

Fy = **36** ksi

429.66 kg/cm²

0.6 Fy = 1512.00 kg/cm² **o.k.!!**

- Shear

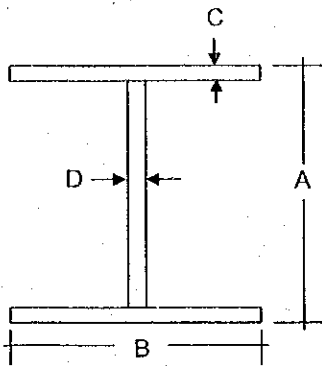
Max. Shear = 4200.0 kg

Fv = V / (h tw) = 163.39 kg/cm²

0.4 Fy = 1008.00 kg/cm² **o.k.!!**

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B-2



Beam type = **W8x10**

A = **7.89** in

B = **3.94** in

C = **0.205** in

D = **0.170** in

Area = 2.960 in²

I = 30.80 in⁴

Yc = 3.945 in

S = 7.81 in³

Pd = **0.50** ton

Md = **0.60** ton-m from analysis

PL = **0.50** ton

ML = **0.90** ton-m

$$\left. \begin{array}{l} P/A(d+L) \quad 52.36 \\ P/A(d+L+s) \quad 39.27 \\ Md+L/S = \quad 1172.43 \\ Ms+d+L/S = \quad 879.32 \end{array} \right\}$$

Fy = **36** ksi

1224.79 kg/cm²

0.6 Fy = 1512.00 kg/cm² o.k.!!

- Shear

Max. Shear = 200.0 kg

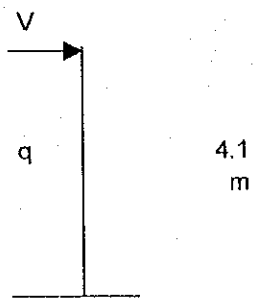
Fv = V / (h tw) = 23.11 kg/cm²

0.4 Fy = 1008.00 kg/cm² o.k.!!

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Column C1

Seismic Stress



P= 4.55 t

Cs= 0.185

V=Cs P 0.84 t

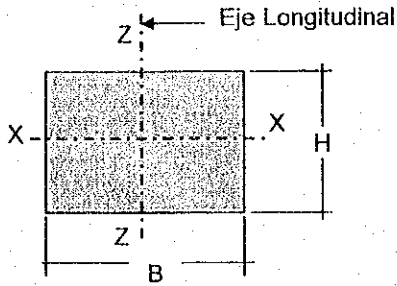
q= 0.04 t/m

Ms= 3.79 tm

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Column

C1



$H = 0.31 \text{ m}$

$B = 0.31 \text{ m}$

$f'c = 280 \text{ kg/cm}^2$

$f_y = 4200 \text{ kg/cm}^2$

Area = 961 cm²

Inertia Z = 7.7E+04 cm⁴

Inertia Y = 7.7E+04 cm⁴

Forces and Moments

From Structural Analysis (ton , m) :

TYPE O LOAD	AXIAL	MOMENT		SHEAR	
	P	Mz-z	Mx-x	Vx	Vz
Dead Loa	4.50	0.00	0.00	0.00	0.00
Live Load	2.40	0.00	0.00	0.00	0.00
Seismic Loa	0.00	3.79	0.00	1.00	0.00
Seismic Loa	0.00	0.00	3.79	0.00	1.00

COMBINATI	Pu	Mu z-z	Mu x-x	Vu x	Vu z
C1	10.38	0.00	0.00	0.00	0.00
C2	7.79	6.17	---	1.63	---
C3	7.79	---	6.17	---	1.63

Forces for design.

$Pu_z = 7.79 \text{ ton}$

$Pu_x = 7.79 \text{ ton}$

$Mu_{x-x} = 6.17 \text{ ton-m}$

$Mu_{z-z} = 6.17 \text{ ton-m}$

$Vu_z = 1.63 \text{ ton}$

$Vu_x = 1.63 \text{ ton}$

$C1 = 1.4 DL + 1.7 LL$

$C2 = 0.75(1.4DL + 1.7LL + 1.87SLy)$

$C3 = 0.75(1.4DL + 1.7LL + 1.87SLz)$

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Orthogonal Combination

$$MX = 100\%EQX + 30\%EQZ$$

$$MZ = 100\%EQZ + 30\%EQX$$

$$Mx = Mx + Mz(H/B) \left(\frac{1-b}{\beta} \right) \quad b = 0.65 \quad MZ = Mz + Mx(B/H) \left(\frac{1-b}{\beta} \right) \quad b = 0.65$$

Slenderness.

iF $klu/r > 22$ Consider Slenderness .

$$k = 2.0 \quad lu = \boxed{8.2} \text{ m} \quad r = (\text{Inetia/Area})^{1/2}$$

Y Direction

$$r = 0.089 \text{ m} \quad klu/r = 183.262 > 22 \text{ Consider slenderness}$$

Z Direction

$$r = 0.089 \text{ m} \quad klu/r = 183.262 > 22 \text{ Consider slenderness}$$

Slenderness

$$Mc = dbMb + dsMs$$

$$db = cm / (1 - Pu/fPc) \quad cm = 1.0$$

$$Pc = p^2EI / (klu)^2 \quad E = 2526713.3 \text{ ton/m}^2$$

$$Pu = 1.3 \times \text{Fuerza Ax} \quad 10.38 \text{ ton}$$

X Dir. :

Z Dir. :

$$\text{Inercia} = 0.0008 \text{ m}^2 \quad \text{Inercia} = 0.0008 \text{ m}^2$$

$$Pc = 71.36 \text{ ton} \quad Pc = 71.36 \text{ ton}$$

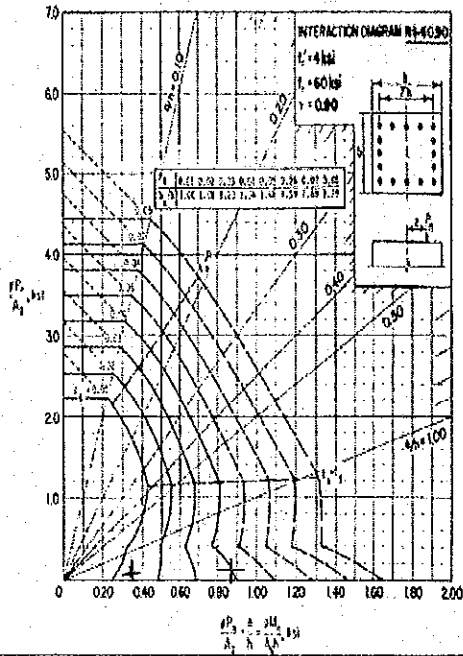
$$db = 1.185 \quad db = 1.185$$

$$\text{Mu x-x} = 7.31 \text{ ton-m}$$

$$\text{Mu z-z} = 7.31 \text{ ton-m}$$

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COLUMNS 7.4.4—Load-moment strength interaction diagram for R4-60.90 columns



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- Design by flexure and Axial load

Z Direction : $f = 0.70$

Gross Area (A_g) = 0.10 m² = 148.97 in²

$h = 0.31$ m = 12.21 in

$P = 7.79$ ton = 17.16 kips

$M = 7.31$ ton-m = 634.42 kips-in

$P_u/A_g = 0.12$ $M_u/A_g h = 0.35$

From the Load-Moment strength interaction diagram R4-60.90,
the ρ value is:

$\rho = 1.5\%$ $A_s = A_g \times \rho = 14.42$ cm²

Bar denomination = 8 Bar area = 5.07 cm²

Quantity of bars = 2.84

Colocar 4 N 8 5-D25

X Direction : $f = 0.7$

Gross Area (A_g) = 0.10 m² = 148.97 in²

$h = 0.31$ m = 12.21 in

$P = 7.79$ ton = 17.16 kips

$M = 7.31$ ton = 634.42 kips-in

$P_u/A_g = 0.12$ $M_u/A_g h = 0.35$

From the Load-Moment strength interaction diagram R4-60.90,
the ρ value is:

$\rho = 1.5\%$ $A_s = A_g \times \rho = 14.42$ cm²

Bar Denomination = 8 Bar area = 5.07 cm²

Quantity of bars = 2.84

Use 4 N 8