## **CHAPTER 12 GROUNDWATER MODELLING**

#### 12.1 Groundwater Basin Management and Groundwater Modelling

Groundwater basin management aims at an effective utilization of groundwater that improves the living condition of the people, controls drying-up, contamination and other problems associated with the use of groundwater, and preserves safe environment (Shibasaki et al., 1995). To achieve this aim, it is important to determine the qualitative and quantitative goal of management. Numerical value of quantitative goal is determined based on the concept of permissible yield.

- 12.1.1 Permissible Yield
  - 1) Permissible Yield and Constraint Factors

The permissible yield can be defined as the "permissible amount of groundwater withdrawal for the residents of the area determined to compare the benefits resulting from the pumpage of groundwater and the risks that might arise from it" (Research Group for Water Balance, 1973).

Factors that determine the permissible yield generally include the following (Shibasaki et al., 1995):

- (1) Recharge factor (natural scientific factor): Water balance is maintained.
- (2) Economic factor: Cost of pumpage is below a certain level.
- (3) Legal factor: No violation of water rights of water laws.
- (4) Geo-environmental factor: Not causing dry-up of springs, land subsidence, seawater intrusion, or groundwater contamination.

Geo-environmental factor can be included under economic factor. All the factors above except recharge factor are considered as socio-scientific factors. Though each of these factors is not completely established in the present, it is pragmatic to combine these factors, and determine the permissible yield.

The relative importance of these factors differs depending on the changes in the natural conditions of groundwater or social conditions within communities (Fig. 12.1). The importance of determining factors for permissible yield depends on the circulating velocity, or renewability of the groundwater (Shibasaki et al., 1995). For humid areas with fast circulation and high renewability of the groundwater, the water balance is

important and the concept of sustainability is given a priority. On the contrary, for arid regions with a slow circulation and low renewability of the groundwater, the possibility of drying-up is increased, and the economic factor becomes more important.

2) Permissible Critical Groundwater Level

The permissible yield can refer to the groundwater level, which must be retained so that these factors are not violated. In other words, it can be called the permissible critical groundwater level. Groundwater level can be monitored easily by using observation wells and other existing wells. Therefore, if the permissible critical groundwater level is set up, and groundwater level is observed by using a monitoring system, the groundwater pumpage of a basin can be controlled to maintain the permissible yield.

The groundwater modelling is an effective tool to determine the permissible critical groundwater level or the permissible yield, showing an actual example in the following sections.

12.1.2 Work Elements of Groundwater Basin Management

In managing a groundwater basin, the following basic components should be taken into account: Monitoring system, Database, Prediction system, and Decision-making system (Shibasaki et al., 1995) (Fig. 12-2).

1) Monitoring System

Various parameters including groundwater levels, pumpage, groundwater quality should be monitored. Observation wells are used to measure groundwater levels, and their screens must be suitably equipped so that the water level can be measured separately for each aquifer.

2) Database System

A database system is necessary to effectively use and analyze large volume of data and information collected during monitoring. A database system is particularly needed for data on groundwater levels, groundwater withdrawals, and water quality. A database system is also used for geological logs in order to comprehend the structure of a groundwater basin.

3) Prediction System

Based on the findings of monitoring, the conditions of groundwater basin are predicted. The prediction results are used in determining appropriate measures for groundwater utilization. Groundwater modelling (groundwater simulation) is used for prediction. Modelling (Simulation) has been used effectively in predicting the permissible limits of groundwater withdrawal in areas of land subsidence or seawater intrusion in Japan.

It is not sufficient to plan a project by means of predicting once at the beginning of it. Prediction has to be reviewed and repeated every few years, and its accuracy must be enhanced every time.

4) Decision-Making System

Appropriate measures to be taken for groundwater management are determined on the basis of monitoring and prediction. The criterion on which these measures are decided depends upon the concept of permissible yield.

# 12.2 General Procedure of Groundwater Simulation

The groundwater simulation study is composed of the development of the aquifer model, calibration, prediction and evaluation as shown in Fig. 12-3. An aquifer model is developed with field data manipulated for computer input. After calibrating the model with observed data, prediction of the water level is executed by inputting future abstraction scenario. The predicted results are evaluated for optimum abstraction, taking the water balance, environmental impacts and economics into consideration.

## 12.2.1 Aquifer Modeling

Aquifer modeling is carried out by numerical groundwater model. The aquifer model simulates a three-dimensional groundwater flow in the phreatic or confined aquifer. The aquifer model is developed by using mainly topography, aquifer distribution, hydraulic characteristics, groundwater discharge and recharge, and groundwater quality.

## 12.2.2 Data Manipulation

Groundwater model study uses various kinds of input data such as aquifer characteristics, water levels, abstraction, recharge, etc. These data are processed for model inputs.

1) Hydrogeological Data

Hydrogeological data consists of geological and topographical maps, geophysical survey results, composite loggings of test boreholes and pumping tests. Based on these data, contour maps on the surface of aquifer, aquitard and hydrogeological basement are prepared. The contour maps including ground elevation are converted into computer codes. Also, distributions of aquifer characteristics are prepared and converted into computer codes.

2) Water Level

Water levels measured in field are modified to groundwater level elevation based on the ground height of observed points. Then contour maps are converted into computer codes.

3) Groundwater Use and Recharge

Based on the results of the well inventory (Hydrocensus), present groundwater use is estimated. Variation in groundwater use in the past is estimated from the statistical data. Groundwater recharge is estimated by using recharge equations and rainfall data.

# 12.2.3 Calibration of Model

The model is test-operated by inputting recharge and pumpage data and outputting the calculated groundwater level in each node. The output is compared with the observed water level records, and then the model will be modified/adjusted until final agreement between the calculated and the observed water level is achieved. Thus the model is calibrated and ready to predict water level fluctuations under various abstraction scenarios.

# 12.2.4 Model Prediction and Evaluation

On the basis of future groundwater abstraction plans, a tentative proposal for groundwater withdrawal plan is prepared. Then the plan is inputted into the calibrated model. The response of the model is evaluated by the following criteria, which should be decided upon the basis of the socio-economic and environmental conditions in the study area:

Evaluation Factor	Criteria
1. Water Balance	Abstraction should be less than the recharge
2. Environmental Impact	Influence to springs and dug wells should be allowable Salinity should be less than the water quality standard
3. Economics	Total pumping head should be less than the criterion

If the model response is not acceptable even for one criterion, then the withdrawal plan should be modified in terms of withdrawal, pumping pattern and borehole location. The model is operated until the final agreement with all the criteria is achieved. With the above steps of aquifer modelling, the optimum abstraction plan (the permissible yield) is fixed and groundwater management plan will be examined.

# 12.3 Description of Numerical Model

# 12.3.1 Introduction

It is considered that a model is a tool designed to represent a simplified version of reality, and properly constructed groundwater models, as they are also representations of reality, can be valuable predictive tools for groundwater resources management. Of groundwater models, a mathematical model is commonly used to study groundwater system.

A mathematical model consists of a set of differential equations that describe groundwater flow. Since the assumptions to solve analytically a mathematical model are fairly restrictive, numerical techniques are generally required to solve the mathematical model approximately under realistic situations.

There are many numerical techniques to solve differential equations. Among them, finite difference and finite element methods are representative (Fig. 12-4). The finite difference method is superior in less computer memory requirement and simplicity of data manipulation. The finite element method has excellence in flexibility of mesh formation. In practical aspect of groundwater flow simulation, there is little distinction between both methods. The finite difference method is applied for the proposed groundwater management plan of the study area, in consideration of data availability and accuracy of aquifer parameters.

#### 12.3.2 Groundwater Flow Model

1) Basic Equation of Groundwater Flow

The unsteady-state, three-dimensional movement of groundwater through heterogeneous and anisotropic porous media is described by the following partial-differential equation.

$$\frac{\partial}{\partial x}\left(K_{xx}\frac{\partial h}{\partial x}\right) + \frac{\partial}{\partial y}\left(K_{yy}\frac{\partial h}{\partial y}\right) + \frac{\partial}{\partial z}\left(K_{zz}\frac{\partial h}{\partial z}\right) - W = S_s\frac{\partial h}{\partial t} \quad (12-1)$$

Where, Kxx, Kyy and Kzz: values of hydraulic conductivity along the x, y and z coordinate axes, h: the potentiometric head, W: a volumetric flux per unit volume and represents source and/or sink of water, Ss: the specific storage of the porous media, t: time.

Equation (12-1), together with specified flow and/or head conditions at the boundaries of an aquifer system and specified initial-head conditions, constitutes a mathematical representation of a groundwater flow system. Numerical method, such as the finite difference method, is usually applied to solve equation (12-1).

2) Derivation of the Finite Difference Equation (McDonald and Harbaugh, 1988)

An aquifer system is discretized with a mesh of blocks called "cells" as illustrated in Fig. 12-5, the location of which are referenced with a row(*i*), column(*j*) and layer(*k*) coordinate system parallel to the *x*, *y* and *z* directions, respectively. The width of cells in the row direction, at a given column *j*, is defined  $r_j$ ; the width of cells in the column direction at a given row *i*, is defined  $c_i$ ; and the thickness of cells in a given layer *k*, is defined  $v_k$ . At center of each cell, there is a point called a "node" at which head is to be calculated.

From the application of the continuity condition, the sum of all flows into and out of the

cell is equal to the rate of change in storage within the cell, expressing as follows

$$\Sigma Q_i = \Delta S \quad (12-2)$$
.

Where,  $Q_i$ : flow rate into the cell, S: storage change within the cell over a time interval

*t*. For convenience flow entering cell is defined positive and outflow is defined negative.

A cell i,j,k and six adjacent cells are illustrated in Fig. 12-6. Applying finite difference method, groundwater flow is approximated by the node-to-node flow. Flow into cell i,j,k in the row direction from cell i,j-1,k is given by Darcy's law as

$$Q_{i,j-1/2,k} = KR_{i,j-1/2,k} \Delta c_i \Delta v_k \frac{h_{i,j-1,k} - h_{i,j,k}}{\Delta r_{j-1/2}} \quad (12-3)$$

Where,  $Q_{i,j-1/2,k}$ : volumetric fluid discharge through the face between cells *i*,*j*,*k* and *i*,*j*-1,*k*,  $h_{i,j,k}$ : head at node *i*,*j*,*k*,  $h_{i,j-1,k}$ : head at node *i*,*j*-1,*k*,  $KR_{i,j-1/2,k}$ : hydraulic conductivity along the row between nodes *i*,*j*,*k* and *i*,*j*-1,*k*,  $c_j v_k$ : area of the cell faces normal to the row direction,  $r_{j-1/2}$ : distance between nodes *i*,*j*,*k* and *i*,*j*-1,*k*. The hydraulic conductivity between the nodes is normally calculated as a harmonic mean.

$$KR_{i,j-1/2,k} = \frac{2KR_{i,j-1,k}KR_{i,j,k}}{KR_{i,j-1,k} + KR_{i,j,k}} \quad (12-4)$$

Similar expressions can be written approximating the flow into the cell through the remaining five faces. Flow in row direction through the face between cells i,j,k and i,j+1,k is expressed as

$$Q_{i,j+1/2,k} = KR_{i,j+1/2,k} \Delta c_i \Delta v_k \frac{h_{i,j+1,k} - h_{i,j,k}}{\Delta r_{j+1/2}} \quad (12-5)$$

While for the column direction, flow into the cell through the forward face is

$$Q_{i+1/2,j,k} = KC_{i+1/2,j,k} \Delta r_j \Delta v_k \frac{h_{i+1,j,k} - h_{i,j,k}}{\Delta c_{i+1/2}} \quad (12 - 6)$$

And flow into the cell through the rear face is

$$Q_{i-1/2,j,k} = KC_{i-1/2,j,k} \Delta r_j \Delta v_k \frac{h_{i-1,j,k} - h_{i,j,k}}{\Delta c_{i-1/2}} \quad (12-7)$$

For the vertical direction, inflow through the bottom face is

$$Q_{i,j,k+1/2} = KV_{i,j,k+1/2} \Delta r_j \Delta c_i \frac{h_{i,j,k+1} - h_{i,j,k}}{\Delta v_{k+1/2}} \quad (12 - 8)$$

While inflow through the upper face is given by

$$Q_{i,j,k-1/2} = KV_{i,j,k-1/2} \Delta r_j \Delta c_i \frac{h_{i,j,k-1} - h_{i,j,k}}{\Delta v_{k-1/2}} \quad (12-9)$$

The notation can be simplified by combining grid dimensions and hydraulic conductivity into a single constant ("hydraulic conductance"). Hydraulic conductance between nodes i,j-1,k and i,j,k can be written as

$$CR_{i,j-1/2,k} = KR_{i,j-1/2,k} \frac{\Delta c_i \Delta v_k}{\Delta r_{j-1/2}} \quad (12-10)$$

Storage change within the cell over a time interval *t* is expressed as follows.

$$\Delta S = Ss_{i,j,k} \frac{\Delta h_{i,j,k}}{\Delta t} \Delta r_j \Delta c_i \Delta v_k \quad (12 - 11)$$

Where,  $Ss_{i,j,k}$ : specific storage of cell i,j,k,  $h_{i,j,k}$ : head change over a time interval t,  $r_j$   $c_i$   $v_k$ : volume of cell i,j,k. Assuming  $t = t_m - t_{m-1}$ , an approximation to the time derivative of head at time  $t_m$  can be written as

$$\left(\frac{\Delta h_{i,j,k}}{\Delta t}\right)_{m} = \frac{h_{i,j,k}^{m} - h_{i,j,k}^{m-1}}{t_{m} - t_{m-1}} \quad (12 - 12)$$

Where,  $h_{i,j,k}^m$ : head of cell *i*,*j*,*k* at time  $t_m$ ,  $h_{i,j,k}^{m-1}$ : head of cell *i*,*j*,*k* at time  $t_{m-1}$  which precedes  $t_m$ .

Substituting equation (12-3), equations (12-5) through (12-9), and equations (12-11) and (12-12) into equation (12-2), and applying relationship in equation (12-10), finite difference approximation for cell i,j,k can be obtained as

$$CR_{i,j-1/2,k} \left( h_{i,j-1,k}^{m} - h_{i,j,k}^{m} \right) + CR_{i,j+1/2,k} \left( h_{i,j+1,k}^{m} - h_{i,j,k}^{m} \right) + \\CC_{i-1/2,j,k} \left( h_{i-1,j,k}^{m} - h_{i,j,k}^{m} \right) + CC_{i+1/2,j,k} \left( h_{i+1,j,k}^{m} - h_{i,j,k}^{m} \right) + \\CV_{i,j,k-1/2} \left( h_{i,j,k-1}^{m} - h_{i,j,k}^{m} \right) + CV_{i,j,k+1/2} \left( h_{i,j,k+1}^{m} - h_{i,j,k}^{m} \right) + OS_{i,j,k} \\= Ss_{i,j,k} \left( \Delta r_{j} \Delta c_{i} \Delta v_{k} \right) \frac{h_{i,j,k}^{m} - h_{i,j,k}^{m-1}}{t_{m} - t_{m-1}} \quad (12 - 13)$$

Where,  $QS_{i,j,k}$ : source or sink term of cell *i*,*j*,*k*.

An equation of this form is written for every cell in the calculation domain, and the system of equations is solved simultaneously for the heads at time  $t_m$ . Solving techniques of simultaneous equations are classified into direct and iterative methods. Finite difference approximation of three-dimensional groundwater flow produces a large system of simultaneous equations. Iterative method is superior to direct method in requirement of computer memory, and is usually used to solve such large system. Strongly Implicit Procedure method (SIP), Slice Successive Overrelaxation method (SSOR), and Preconditioned Conjugate Gradient method (PCG) are typical of iterative method. Precise explanation of solving techniques should be referred to McDonald and Harbaugh (1988), and Hill (1990).

#### 3) MODFLOW

MODFLOW (Modular Finite-Difference Ground-Water Flow Model) developed by U.S. Geological Survey (McDonald and Harbaugh, 1988; Harbaugh and McDonald, 1996), is widely used numerical model which can simulate groundwater flow in a three-dimensional heterogeneous and anisotropic medium. As mentioned in the following section, MODFLOW was applied to simulate groundwater flow systems in the Stampriet Artesian Basin.

In a three-dimensional finite difference model, vertical discretization can be seen as a sequence of horizontal layers. In complicated hydrogeological condition, this grid system causes a cell contain material from different stratigraphic units (Fig. 12-7(b)). In MODFLOW, vertical discretization can be viewed as an effort to represent individual aquifers or permeable zones by individual layers of the model (Fig. 12-7(c)). This distortion can be generated by giving the elevation of the top and bottom of the layer. It allows flexibility in discretizing, however, introduces small error into the finite difference approximation.

12.4 Conceptual Model

#### 12.4.1 Hydrogeologic Condition

From a geological point of view, there are major four formations. They are the Damara Sequence, the Nama Group, the Karoo Sequence and the Kalahari Beds. The relationships among four formations are unconformity. The Damara Sequence and the Nama Group consist of sandstone, shale and metamorphic rocks. They form the hydrogeological basement. The Karoo Sequence is divided into the Dwyka Group and the Ecca Group. The Dwyka Group is composed of tillite and mudstone, and is also a hydrogeological basement. The Ecca Group is divided into the Nossob, Mukorob, Auob

and the Rietmond Members. The Nossob Member is composed of sandstone and is a confined aquifer. The Lower Mukorob Member consists of shale and is an aquitard/ aquiclude. The Upper Mukorob Member consists of sandstone and is a confined aquifer. The Auob Member is composed of sandstone and shale. It contains three confined aquifers and two aquitards. However, it is difficult to clarify the distribution of these aquifers and aquitards over the whole study area. Therefore, the Auob Member is assumed to be one confined aquifer. The Lower Rietmond Member is composed of shale, and is an aquitard. The Upper Rietmond Member consists of sandstone, and is an unconfined or confined aquifer. The Kalkrand Basalt and the Karoo Dolerite intrude into the Auob and Rietmond Members and are considered to be an unconfined-confined aquifer or aquitard. The Kalahari Beds are composed of sand, gravel and calcrete. It is an unconfined aquifer. Between the Kalahari Beds and the Upper Rietmond Member, there is no distinct aquitard or low-permeability layer.

#### 12.4.2 Aquifer System

As a result of the above discussion, an aquifer system consisting of one unconfined aquifer and two confined aquifers with two confining layers (aquitards) was selected for the groundwater model in the Stampriet Artesian Basin. The unconfined aquifer represents the Kalahari and the Upper Rietmond aquifers. The first confined aquifer represents the Auob and the Upper Mokorob aquifers. The second confined aquifer represents the Nossob aquifer. The upper unconfined aquifer and the first confined aquifer are connected due to leakage through the first confining layer (the Lower Rietmond Member). The first confining layer is absent and the unconfined aquifer directly overlies the first confined aquifer with a large area of the Stampriet Basin. In that area, the lower part of the unconfined aquifer is assumed to be an aquitard. The second confined aquifer is considered to be isolated from upper aquifers (Table 12-1).

#### 12.5 Data Manipulation

#### 12.5.1 Grid Design

Considering the hydrogeological structure of the study area, modeled domains were defined as shown in Fig. 12-8. The model area covers all of the Stampriet Artesian Basin. The area of the domain is about  $125,000 \text{ km}^2 (303 \times 413 \text{ km})$ . The domain was divided by a grid at intervals of 6.3 km in the longitudinal and 6.9km in the latitudinal directions (see Fig. 12-9). Numbers of cells in row and column directions are 60 and 48 respectively. The application of a fixed grid system causes a slight error in the cell size, but it is negligible in practical application of the model (see Fig. 12-10).

# 12.5.2 Elevation of Top and Bottom of Layers

As mentioned previously, a deformed grid can be used in MODFLOW. Therefore, the study area was divided into 6 layers in vertical direction, and the elevations of the top and bottom of layers were given. The Model layers basically correspond to the Kalahari Beds, the Upper Rietmond Member, the Lower Rietmond Member, the Auob Aquifer, the Lower Mukorob Member, and the Nossob Aquifer. However, individual aquifers or aquitard cannot be represented by individual layers of the model, because of the complicated hydrogeological condition of the study area. The elevations of the top and bottom of layers were determined according to the following procedure.

## 1) Digitization of Isodepth and Isopach Maps

The isodepth and isopach maps shown in Section 8.3 were digitised for each cell;

- Surface Elevation
- Bottom of Kalahari Beds (Fig. 8.3-2)
- Isopach of Lower Rietmond Member (Fig. 8.3-3)
- Top of Auob Aquifer (Fig. 8.3-4)
- Isopach of Auob Aquifer (Fig. 8.3-5)
- Isopach of Lower Mukorob Member (Fig. 8.3-6)
- Isopach of Nossob Aquifer (Fig. 8.3-8)

Also, averaged value of "USGS Satellite 30 seconds Elevation Data" was used for the surface elevation of each cell.

The difference between the surface elevation and the bottom of the Kalahari Beds was assumed to be the thickness of the Kalahari Beds. If the value of bottom of the Kalahari Beds was higher than the surface elevation, it was revised to be lower than the surface (5 to 10 meters in thickness). In the area where the Kalahari Beds directly overlay the Auob Aquifer, the top of the Auob Aquifer was revised to be the same as the bottom of the Kalahari Beds.

The value obtained through subtracting the top of the Auob Aquifer from the bottom of the Kalahari Beds was assumed to be the thickness of the Rietmond Member. The thickness of the Upper Rietmond Member was calculated to subtract the thickness of the Lower Rietmond Member from that of the Rietmond Member.

The bottom of the Auob Aquifer was obtained to subtract the thickness of the Auob Aquifer from the top of it. The bottom of the Lower Mukorob Member was calculated to subtract the thickness of it from the bottom of the Auob Aquifer. Then, the bottom of the Nossob Aquifer was calculated to subtract the thickness of it from the bottom of the Lower Mokorob Member successively.

Digitized isodepth and isopach maps of aquifers and aquitards. These digitized isodepth maps were used for summing up groundwater use by aquifer.

2) Elevation of Model Layers

The abovementioned aquifers and aquitards do not sequentially lie on top of another, since the hydrogeological condition of the study area is complex. There are 22 combinations of overlaying of them as shown in Table 12-2. The combination of each cell is shown in Table 12-3.

Allotment of aquifers and aquitards to the model layers was executed according to the procedure given in Table 12-4. The bottom elevations of layers are shown in Table 12-5 to Table 12-10. Fig. 12-11 shows the N-S cross-sectional grid design at column 25. Fig. 12-12 shows the E-W cross-section at row 30 (Locations of sections are shown in Fig. 12-8).

#### 12.5.3 Boundary Condition

The model area is bounded by basement rocks on the north. However, the Kalahari Beds overlying basement rocks continue to the outside of the study area. Groundwater inflow can be expected across the border. Therefore, constant head condition was assumed at this boundary to approximate the groundwater inflow. On the western side, the distribution of the first and second confined aquifers is restricted at the border. This boundary was considered as a no flux condition. Near Kalkrand, groundwater level contours show outflow from the study area, therefore discharging condition was set on this border. On the southern border, the model area is bounded by basement rocks. No flux boundary condition was assumed. On the eastern side, the aquifers are continuous to the territory of Botswana and South Africa. Since groundwater level contours are almost perpendicular to the boundary, it was considered to be no flux condition. On the right bottom corner of the model, groundwater outflow can be expected across the border through the Kalahari Beds. Constant head condition was assumed to approximate the groundwater outflow.

The boundary conditions of the modelled area are shown in Fig. 12-8.

#### 12.5.4 Aquifer Constants

There are very few pumping test data, excluding the JICA test boreholes as mentioned in section 2.5. Distributions of the permeability of aquifers are shown in Figs. 12-13 to

12-15. The study area was divided into several zones based on these figures. The permeability of a zone is assumed to be homogeneous and isotropic. These values were modified in the process of model calibration.

All pumping tests, except one, were executed without observation boreholes, therefore accurate storativity values were not able to obtain. The storativity values of the aquifers set uniformly and then these values modified in the model calibration process.

#### 12.5.5 Groundwater Levels

The groundwater levels have been measured in the water level survey (section 2.8). The elevation survey of boreholes has been also done (section 2.7). Based on the results of these surveys, groundwater level contour maps were drawn. These maps were used in the model calibration.

There are 22 observation boreholes of the DWA. At these boreholes groundwater level changes have been measured monthly. Also, groundwater levels have been observed monthly in 30 NamWater boreholes. Observed groundwater level changes were used in the model calibration.

#### 12.5.6 Pumpage

1) Data Source and Estimation Method

Data source and estimation method of present groundwater use is shown in Table 12-11. Production rate of NamWater is monthly, and report of irrigation permit holders is also monthly. The results of the Hydrocensus are average values at the surveyed date.

If the number of people in a farm was unknown, it was estimated by using farm area and unit population. Also, number of stocks was estimated from farm area and carrying capacity, if it was unknown. Average value of the Hydrocensus is used in the ratio of small stocks and large stocks.

Information of farms, which have not been surveyed by the Hydrocensus, is only farm area in the DWA database. The number of people and stock was estimated in the same way as mentioned above.

2) Results of the Hydrocensus

Present groundwater use was estimated, mainly based on the results of the Hydrocensus. The results are summarized in Table 12-12. 3) Summary of NamWater Scheme

Production rates of NamWater scheme are summarized in Table 12-13, and variations of each scheme are shown in Fig. 12-16. Monthly production rates of each scheme are given in Appendix Table B-1 to B-28.

Total production increased from 482 thousand  $m^3$ /year in 1986 to 604 thousand  $m^3$ /year in 1999. The production of the Aranos scheme is largest and about 40% of total in 1999.

4) Summary of Irrigation Permits

The irrigation permits are valid for five years, and water allocation is prescribed in annual production per farm. Boreholes must be equipped with water gauges, but some are not equipped. Monthly productions should be reported, however the DWA records on each farm are incomplete.

Using values of same month in the previous year or in the following year, lacking records of the monthly production reports were estimated. The results are shown in Table 12-14.

Irrigation uses of the permit holders have a tendency to increase. However, it is 64% of the allocated amount in 1999. The relation to rainfall is not distinct. The production in 1997 with a lot of rain is smaller than those in 1996 and 1998 with little rainfalls. But, the production in 1995 is smaller than that in 1996, although the rainfall in 1995 is less than that in 1996 (Fig. 12-17). Also, the relationship between monthly production and monthly rain is not clear (Fig. 12-18).

The groundwater abstraction for irrigation use affects the groundwater level change. For example, the water level change of the Spes Bona observation borehole (WW32457) is almost consistent with the variation of irrigation use. The water level of this borehole is considered to represent the change of irrigation use (Fig. 12-19).

The unit consumption for irrigation was calculated based on the groundwater use of the permit holders and irrigated areas of the Hydrocensus. Using the allocated amounts, the unit consumption becomes 42.0 m<sup>3</sup>/day/ha. Using the reported products, the unit consumptions are 28.6 m<sup>3</sup>/day/ha in 1998 and 26.0 m<sup>3</sup>/day/ha in 1999 respectively. Excluding farms with very small consumption values, the unit consumptions become  $34.0 \text{ m}^3$ /day/ha in 1998 and  $31.0 \text{ m}^3$ /day/ha in 1999 (Table 12-14).

5) Present Groundwater Use by Usage Type

Basically using the unit consumptions of the Hydrocensus (Table 12-16), present groundwater use was estimated. Results are shown in Table 12-17 and Fig. 12-20. Total

groundwater use in the study area is estimated to be  $40,912 \text{ m}^3/\text{day}$  (14.9 million m<sup>3</sup>/year). Irrigation use amounts to 18,868 m<sup>3</sup>/day (6.9 million m<sup>3</sup>/year) and is 46% of total use. Stock watering use is 15,589 m<sup>3</sup>/day (5.7 million m<sup>3</sup>/year) and 38%. Domestic use is 6,455 m<sup>3</sup>/day (2.4 million m<sup>3</sup>/year) and 16%.

The distributions of present groundwater use by usage in each cell are shown in Figs. 12-21 to 12-24. The estimated groundwater use in a farm was divided among boreholes belonging to that farm. Then, the groundwater uses of boreholes were summed up for each cell. The location of boreholes was based on the results of the Hydrocensus and the DWA Database.

Domestic use is generally distributed over the study area. Pumping rate of almost cells is less than 10 m<sup>3</sup>/day. Near Aranos, there is only one cell with large pumping rate that is more than 500 m<sup>3</sup>/day (Fig. 12-22). Stock watering use is also generally distributed over the study area except the Aminuis region. Pumping rate of almost cells is less than 30 m<sup>3</sup>/day. There is no cell whose pumping rate is more than 500 m<sup>3</sup>/day (Fig. 12-23). Irrigation use centres on the Stampriet region, and expands along the Auob River and the road from Stampriet to Aranos. There is one cell whose pumping rate is more than 2000 m<sup>3</sup>/day. The ratio of cell with large pumping rate is high comparing with domestic or stock watering use (Fig. 12-24). Total groundwater use coincides with irrigation use in heavy pumping area. Generally groundwater use is dense in western half of the study area (Fig. 12-21).

6) Present Groundwater Use by Aquifer

#### (1) Present Groundwater Use by Aquifer

The estimated groundwater use in each borehole was divided into the aquifers based on the borehole construction information (i.e. screen depth, borehole depth, water strike depth) and the isodepth maps of aquifers. Unfortunately there are few boreholes with complete information. Therefore, dividing of the groundwater use into aquifers was done through the procedure shown in Table 12-18.

Results are shown in Table 12-19 and Figs. 12-25 to 12-31. Groundwater use from the Kalahari Aquifer amounts to 26,739 m<sup>3</sup>/day (9,8 million m<sup>3</sup>/year) and occupies 65% of total use. Groundwater use from the Auob Aquifer is estimated to be 13,622 m<sup>3</sup>/day (5.0 million m<sup>3</sup>/year) and 33%, and that from the Nossob Aquifer is merely 551 m<sup>3</sup>/day (0.2 million m<sup>3</sup>/year) and 1% (Fig. 12-25).

The domestic use from the Kalahari Aquifer amounts to 69% of total domestic use. These from the Auob Aquifer and the Nossob Aquifer are 24% and 7% respectively (Fig. 12-26). For the stock watering use, groundwater from the Kalahari Aquifer occupies 81%, and that from the Auob Aquifer is 19% (Fig. 12-27). The irrigation use is equally shared between the Kalahari Aquifer and the Auob Aquifer (Fig. 12-28).

In the Kalahari Aquifer, the stock watering use is 47%, and the irrigation and domestic use are 36% and 17% respectively (Fig. 12-29). In the Auob Aquifer, the irrigation use is prominent and is 67%. The stock watering and domestic use are 22% and 11% respectively (Fig. 12-30). In the Nossob Aquifer, the domestic use is 88%, and the irrigation and stock watering use are only 10% and 2% respectively (Fig. 12-31).

(2) Distribution of Present Groundwater Use by Aquifer

The distributions of present groundwater use by aquifer in each cell are shown in Figs. 12-32 to 12-34. The distributions of each usage by aquifer are shown in Figs. 12-35 to 12-43.

Groundwater use of the Kalahari Aquifer is distributed over almost all study area. Heavy pumping cells are concentrated in the Stampriet region, and there is a cell with pumping rate of 1,000-2,000 m<sup>3</sup>/day. Along the Auob River, cells with relatively large pumping rate expand (Fig. 12-32). Groundwater use of the Auob Aquifer is centred at the Stampriet region, and there is a cell whose pumping rate is more than 2,000 m<sup>3</sup>/day. Cells with small pumping rate spreads in the area to the southeast of Aranos (Fig. 12-33). Groundwater use of the Nossob Aquifer is dotted around the study area (Fig. 12-34).

The domestic use of the Kalahari Aquifer extends over the study area. The pumping rate of cells is generally less than 10 m<sup>3</sup>/day (Fig. 12-35). The distributed area of the domestic use of the Auob Aquifer is smaller than that of the Kalahari Aquifer. The pumping rate is almost less than 10 m<sup>3</sup>/day (Fig. 12-36). The domestic use of the Nossob Aquifer is very similar to total groundwater use of it (Fig. 12-37).

The stock watering use of the Kalahari Aquifer is widely distributed except Aminuis area. Pumping rate is generally less than  $30 \text{ m}^3/\text{day}$ . In the south-western part of the study area, there are several cells with pumping rate of 100-500 m<sup>3</sup>/day (Fig. 12-38). In the Auob Aquifer, the stock watering use is distributed around Stampriet, Aranos and Leonardville. Pumping rate is almost less than  $30 \text{ m}^3/\text{day}$  (Fig. 12-39). The stock watering use of the Nossob Aquifer is scarce (Fig. 12-40).

The irrigation use of the Kalahari Aquifer is concentrated to the Stampriet region, and expands along the Auob River and the road from Stampriet to Aranos (Fig. 12-41). That of the Auob Aquifer is only centred on Stampriet region. There is a cell whose

pumping rate is lager than 2000 m<sup>3</sup>/day (Fig. 12-42).

#### 7) Variation of Groundwater Use

The groundwater use variation from 1990 to 1999 was estimated by using the statistics and existing data (Table 12-20). In the domestic use, groundwater use variation in commercial farms and communal land was calculated from the population change. For commercial farms, annual population growth was estimated to be 0.68% based on the 1991 Population and Housing Census and the Hydrocensus. For communal land, annual population growth was estimated to be 2.14% in Aminuis and 2.48% in Nama land (see Chap.10). For village centre, the productions of NamWater (Table 12-13) were used directly.

The variation of the stock watering use was estimated by number of livestock. Based on the Hydrocensus 1986-1989 (DWA, 1986; 1987; 1989), the stock watering use in Area 1-3 amounted to 883,600m3/a, using unit consumptions 35 Litter/head for LS and 5 Litter/head for SS (Table 12-21). Based on the Hydrocensus, the stock watering use in the same area was estimated to be 735,000 m3/a, using the same unit consumptions. From these figures annual growth was calculated to be -1.82%.

From 1994 to 1999, production of the permit holders (Table 12-14) was used directly estimating the irrigation use variation. From 1990 to 1993, exponential approximation equation of productions from 1994 to 1999 was used (y=2.9754exp(0.1017x); y: annual production, x=year-1993).

The estimated results are shown in Table 12-22 and Figs 12-44 and 12-45. The groundwater use increased from 11.6 million  $m^3$ /year in 1990 to 14.9 million  $m^3$ /year in 1999. The stock water use decreased from 6.7 million  $m^3$ /year and 58% of total in 1990 to 5.7 million  $m^3$ /year and 38% in 1999. On the other hand, the irrigation use increased 2.7 million  $m^3$ /year and 23% of total in 1990 to 6.9 million  $m^3$ /year and 46% in 1999 (Fig. 12-44).

Groundwater from the Kalahari Aquifer increased from 8.4 million  $m^3$ /year in 1990 to 9.8 million  $m^3$ /year in 1999. That from the Auob Aquifer rapidly increased from 3.0 million  $m^3$ /year to 5.0 million  $m^3$ /year (Fig. 12-45).

#### 12.5.7 Recharge

It is difficult to estimate the groundwater recharge based on the runoff analysis (see section 2.2). Therefore, the groundwater balance analysis was applied to estimate it.

#### 1) Groundwater Balance in An Area

The groundwater balance in an area is expressed as follows.

$$R - D = S \frac{dh}{dt} \quad (12 - 14)$$

Where, *R*: recharge rate, *D*: discharge rate, *S*: storativity, dh/dt: groundwater level change in unit time. *R* means the groundwater inflow, *D* means the groundwater outflow and *Sdh/dt* is the storage change of groundwater in the area.

For the period without recharge, a regression curve of groundwater level is expressed by following exponential-type equation.

$$\frac{dh}{dt} = C(h - h_0) \quad (12 - 15)$$

Where, *h*: groundwater level,  $h_0$ : standard groundwater level (at this level, discharge rate becomes zero), *C*: constant. Substituting equation (12-15) into equation (12-14), the discharge rate (*D*) can be expressed as follows (where, R=0).

$$D = -SC(h - h_0)$$
 (12–16)

For the recharge period, a recharge rate (R) is expressed following equation, substituting equation (12-16) into equation (12-14).

$$R = -SC(h - h_0) + S \frac{dh}{dt}$$
$$= S \left\{ \frac{dh}{dt} - C(h - h_0) \right\} \quad (12 - 17)$$

From equation (12-17) the recharge rate can be estimated reading groundwater level on the observation borehole records.

#### 2) Recharge Estimation at Olifantswater

To estimate the recharge rate by the above method, it needs to select an observation borehole that represents natural recharge. Of course the recharge rate cannot be estimated from an observation borehole influenced heavily by pumping.

The Olifantswater WW21815 was selected for the recharge estimation. It has observed the groundwater level in the unconfined Kalahari aquifer. The groundwater level change of WW21815 differs from that of the Spes Bona WW32457, which is strongly effected by the irrigation groundwater use (see Fig. 12-19). It is considered to represent the natural

recharge-discharge process.

The water level of WW21815 shows a tendency to decrease annually. To calculate *C* and  $h_0$ , it is necessary to make a correction of the water level. As shown in Fig. 12-46, the correction value is 0.61m for 11 years (i.e. 5.5cm/year). The calculated *C* and  $h_0$  are 0.0167 and -15.245m respectively (Fig. 12-47).

Using equations (12-16) and (12-17), the monthly discharge and recharge rates were calculated. For the recharge calculation, it was assumed that the recharge occurs when water level is rising, and it equals zero when water level is declining. The results are shown in Fig. 12-46. Annual values are summarized in Table 12-24.

The discharge and recharge rates calculated from equations (12-16) and (12-17) are proportional to the storativity that equals the effective porosity in unconfined aquifer. The results of neutron logging of the JICA test boreholes show that the porosity of the Kalahari aquifer is about 25%. Using this value as an effective porosity, the calculated recharge rate exceeds rainfall. Therefore, the effective porosity is smaller than the porosity estimated by the neutron logging, and it seems that value from 2% to 5% is adequate.

These values were used for the initial setting of model calibration, and were revised in process of the calibration.

#### 12.6 Model Calibration

#### 12.6.1 Procedure of Model Calibration

Model calibration was carried out in the following steps:

- a. Calibrating groundwater level distribution by the steady-state calculation
- b. Calibrating groundwater level variation by the unsteady-state calculation
- c. Calibrating groundwater level change caused by 1/50 years rain (in 2000)

The first step of model calibration is to clarify the hydraulic conductivity and to make initial heads (1990) for unsteady-state calculation. Calculated heads were compared with groundwater level distribution based on the groundwater level survey. The second step of yearly unsteady-state calculation from 1990 to 1999 is to clarify the specific storage and recharge rate. Calculated head variations were compared with water level records of DWA and NamWater. Third step is to clarify the recharge rate with 1/50years rain (in 2000). Calculated head was compared with observed water level, then parameters (mainly hydraulic conductivity) and recharge rate were modified until final agreement between the calculated and the observed water level is achieved.

- 12.6.2 Calibrated Model
  - 1) Comparison between Observed and calculated results
    - (1) Groundwater Level Configurations

Calculated heads were compared with results of the groundwater level survey. The results of survey show distribution of groundwater level in 2000. Groundwater level changes between 1990 and 2000 are relatively small, therefore the configuration of groundwater level is considered to be almost unchanged. Calculated heads were also verified by observation well records of Jan. 1990.

Fig. 12-48 shows observed and calculated groundwater level configurations of the Kalahari Aquifer. From the 1300m to 1100m contours, calculated and observed heads are almost coincided. On the 1000m and 950m contours, differences between calculated and observed heads are slightly large. In that area, there were few measuring points therefore strict comparison is difficult. Comparison of the Auob Aquifer is shown in Fig. 12-49. From the 1300m to 1050m contours, calculated and observed heads well agree. The 1000m and 950m contours of the both are not in

agreement. Fig. 12-50 shows the configuration of the Nossob Aquifer. From 1250m to 1100m contours, the both are well coincided. In the eastern and southern part of the model, the both do not entirely agree. In these areas, configuration of observed head is not accurate since there are few measuring points.

Fig.12-51 shows comparison of observed and calculated heads at observation wells. If the both values coincide, corresponding point is plotted on a line of 45 ° angle. All points distributes along the line of 45 ° angle. The mean error that is the mean difference between measured and calculated head is 1.0m. The results indicate good agreement of the two.

(2) Variations of Groundwater Level

Observed and calculated groundwater level variations in 1990-1999 at observation wells are shown in Figs. 12-52 to 12-59. Observations are monthly, but calculated results are yearly. At Olifantswater, calculated heads of the Kalahari Aquifer well agree with the trend of observed groundwater level (WW21815). Calculated heads of the Auob Aquifer are approximately 1 meter higher than the observed one (WW21784). However, these well simulates the declining trend of the observed records (Fig. 12-52). At Gomchanas (WW8399) calculated heads are about 1.5 meters lower than observed groundwater level. Decline of calculated heads is slightly smaller than that of the observation (Fig. 12-53).

At Spes Bona calculated heads are approximately 2 meters lower than the observed heads (WW32457), however these well agree with the trend of observed variations (Fig. 12-54). Calculated heads at Boomplaas correspond to the observation (WW10120). These in 1998 and 1999 are slightly lower than the observation (Fig. 12-55).

At Tugela (WW22838) calculated heads of the Kalahari Aquifer are about 3 meters lower than the observed heads and these of the Auob Aquifer are about 4 meters lower than the observed ones. Both of calculated heads well coincide with the trend of declining observation records. Calculated heads of the Nossob Aquifer is approximately 5 meters higher than the observation. Decline of calculated heads is slightly smaller than that of the observation (Fig. 12-56).

At Gochas calculated heads of the Kalahari and Auob Aquifers are almost unchanged. Levels of the both correspond to the observation (WW7491, WW16343) approximately (Fig. 12-57). Calculated head of the Nossob Aquifer at Aranos well agree with the observed heads (WW7407) (Fig. 12-58). At Aminuis calculated heads are about 1 meter lower than the observed groundwater level (WW26164). Since observed variation is irregular, it is difficult to compare the trends of both (Fig. 12-59)

Gochas(WW7491, WW16343), Aranos(WW7407) and Aminuis(WW26164) are NamWater scheme wells. Therefore groundwater change caused by pumping is large, and it is difficult to clarify the trend of variation.

(3) Groundwater Level Change with 1/50 years rain

Groundwater level recovery in 2000 caused by heavy rain in 1999-2000 was calibrated, assuming pumping rates in 2000 and 2001 to be the same as that in 1999. Results are also shown in Figs. 12-52 to 12-59.

Calculated heads of the Kalahari Aquifer agree well with the observed recovery at Olifantswater. In the Auob Aquifer groundwater level recovery has not observed, however calculated heads indicate a little recovery (Fig. 12-52). At Gomchanas the observed records shows slight recovery and calculated head agree with it (Fig. 12-53).

Though observed heads at Spes Bona shows about 3 meters recovery, calculated heads continue to decline. This recovery is considered to arise from pumping rate change. In the calculation pumping rate in 2000 is the same as that in 1999, therefore the calculated heads do not agree with the observed recovery (Fig. 12-54). At Boomplaas, calculated and observed heads indicate the same situation as Spes Bona (Fig. 12-55).

At Tugela calculated heads of the Kalahari and Auob Aquifers coincide with about 2 meters recovery of the observed heads. Calculated heads of the Nossob Aquifer do not agree with slight recovery of observation (Fig. 12-56).

At Gochas, Aranos and Aminuis groundwater level recovery in the observed records are not distinct for the above-mentioned reason (Figs. 12-57 to 12-59).

#### 2) Water Budget in Calibration Period

Water Budget in 1999 and 2000 is given in Figs. 12-60 and 12-61. In 1999, well pumping rate (38,400 m<sup>3</sup>/day) considerably exceeded recharge rate (12,600 m<sup>3</sup>/day). To compensate this shortage, water released from the storage (24,000 m<sup>3</sup>/day) declining groundwater level. Pumping rate of the model doesn't agree with that of the study area, since the model area is smaller than the study area (Fig. 12-60).

In 2000, recharge rate (218,800 m<sup>3</sup>/day) increased by about 17 times that of 1999. With 1/50years rain, groundwater level recovered and the storage increased (181,900 m<sup>3</sup>/day) (Fig. 12-61).

# 3) Fixed Parameters

Hydraulic conductivity, Specific Storage (effective porosity) and recharge rate were modified to calibrate the model. The distributions of fixed hydraulic conductivity of model layer 1 to 6 are shown in Figs.12-62 to 12-67. The distribution of fixed specific storage and effective porosity of model layer 4 and 6 are shown in Figs. 12-68 and 1-69. Fixed hydraulic conductivity, specific storage and effective porosity are summarized in Table 12-25. Zone number in Figs. 12-62 to 12-69 corresponds to that in Table 12-25. Specific storage and effective porosity of model layer 1 to 3, and 5 sets uniformly to be zone 1.

Recharge rate is summarized in Table 12-26 and distribution of zones is shown in Fig. 12-70. Zone number in Fig. 12-70 corresponds to that in Table 12-26. In ordinary years (1990-1999), recharge rate is very small except zone 6. Results of Carbon-14 and Tritium analysis support this low recharge rate. At zone 6 relatively large recharge rate was needed to prevent cells form drying up, since the aquifers locate at high altitude. In 2000 with 1/50 years rain, recharge rate increased to about 1 to 3% of annual rainfall to calibrate the groundwater level change at observation wells.

- 12.7 Model Prediction
- 12.7.1 Prediction Cases
  - 1) Pumpage

To predict the groundwater level change caused by pumping rate change, 6 cases shown in Table 2-27 were studied. Cases 1 and 2 were assumed to keep present groundwater use. For case 3 irrigation use was increased to 120% of present. For cases 4 to 6 irrigation use was decreased to 70%, 50%, 0% respectively. Indicating the calibration results, groundwater level depletion in Stampriet area is major problem in the basin. Therefore change of irrigation use that causes the depletion was studied. Prediction period for each case is 100 years.

2) Recharge

Recharge rate will vary in prediction period, but there is no precise recharge analysis to obtain probability of recharge at present. Calibrated recharge rate was used as an average of long period. For Cases 2 to 6, recharge rate with1/50years rain was assumed in 30th and 80th year (Fig. 12-71).

#### 12.7.2 Constraints on Permissible Yield

As mentioned in section 12.1.1, constraints on permissible yield are social scientific matter except water balance. Therefore it is difficult to define the constraints. Here, following constraints are assumed. These are not complete and should be revised with exhaustive argue.

#### 1) Water Balance Constraint

Groundwater abstraction should be within the possible amount of recharge on arbitrary spatial and time scales. In this study time scale is determined to be one year, therefore annual amount of pumpage must not exceed that of the possible recharge. In other words, the groundwater level must recover to the initial level at the end of one hydrologic year. Following table shows the criteria for the annual residual drawdown.

Rank	Annual Residual	Description
	Drawdown (m)	
А	0.00 - 0.03	Allowable: Not surely safe, but allowable if there
		is no alternative plan
В	0.03 - 0.10	Undesirable: The aquifer storage will be possibly
		depleted in future
С	0.11 -	Not Allowable: The aquifer storage will be
		probably depleted in near future

#### Criteria for Water Balance Constraint

#### 2) Water Quality Constraint

In this simulation groundwater quality is not studied, since groundwater level change is considered to be small and it would not cause groundwater quality change. However, there are high salinity zones ("salt blocks"), and groundwater quality is one of the problems in this basin. Prediction of groundwater quality is the subject for a future study.

3) Environmental Constraint

Influences on existing springs and vegetations are possible environmental constraints to be considered. According to the environmental analysis (see Chap. 14), springs in this basin already dried up decades ago. Therefore, the impact on existing springs can be negligible. Decline or recovery of groundwater level will affects the vegetations in this basin. However, no quantitative analysis on the relationship between groundwater level and vegetations has been done. In this study, the influence on vegetations was neglected. It is the subject for a future study.

4) Economical Constraint

This constraint comes from the limits of pump lift. Average PID (Pump Installed Depth) is 46 meters and average groundwater level depth is 29 meters based on the Hydorocensus. As a result, the total drawdown should be within about 10 meters. Otherwise the pump must be altered to suit deeper water level, which will cost more. Criteria for the economic constraint are shown in the following table.

ernerna ror B	e on onne e on on anne	
Rank	Total Drawdown after	Description
	100 years (m)	
А	0 – 10	Good: No problems in practical use
В	10 - 20	Allowable: Well yield may decrease
C	20 >	Undesirable: Pump should be changed

Criteria for Economic Constraint

#### 12.7.3 Model Prediction

In Figs. 12-72 to 12-89, predicted results are shown as drawdown after 100 years for each aquifer and case. Calculation of bottom area of the model was unstable and there were incomprehensible head differences. These differences were ignored in figures. Also, groundwater level variations at observation wells are shown in Figs. 12-90 to 12-92.

1) Case 1

Groundwater pumpage is kept at the rate of 1999 (14.9 million  $m^3/$  year) in this case. Maximum drawdown of the Kalahari Aquifer will exceed 30 meters, and the Kalahari Aquifer will dry up within 35 years at Spes Bona (Figs. 12-72 and 12-91). It corresponds to the rank C (Not Allowable) of water balance constraint and the rank C (Undesirable) of economic constraint. In Stampriet area there is no observation well of the Kalahari Aquifer then the predicted results are not calibrated. However, the results can show the trend of the variation of groundwater level. Maximum drawdown in the Auob Aquifer is 14 meters at Stampriet (Figs. 12-78 and 12-91). It corresponds to the rank C (Not Allowable) of water balance constraint and the rank B (Allowable) of economic constraint. When a cell dries up, the MODFLOW automatically eliminates pumpage in that cell. Therefore, the groundwater level in the Auob Aquifer is slightly recovered, when the Kalahari Aquifer dries up and the pumpage of the aquifer is eliminated.

At Olifantswater drawdown in the Kalahari Aquifers is 3 meters and that of the Auob

Aquifer is 3 meters also (Fig. 12-90). These correspond to the rank A (Allowable) of water balance constraint and the rank A (Good) of economic constraint. At Tugela drawdown in the Kalahari Aquifer is 1 meter. It corresponds to the rank A of water balance and economic constraints. Drawdown in the Auob and Nossob Aquifers are 5 meters and 4 meters respectively (Fig. 12-92). These classified into the rank B (Undesirable) of water balance constraint and the rank A of economic constraint.

2) Case 2

Pumping rate is the same as that of Case 1 (14.9 million m<sup>3</sup>/ year). In 30th and 80th years it is assumed to get recharge with 1/50years rain. At Spes Bona drawdown in the Kalahari and Auob Aquifers are the same as these of Case 1 (Figs. 12-73 and 12-79). The Kalahari Aquifer will dry up within 35 years (Fig. 12-91). The classifications are the same as these of Case 1. In the Stampriet area no recharge condition is set (Fig. 12-70), therefore no groundwater level recovery is calculated in the year with 1/50years rain. The drawdown of the Kalahari Aquifer is accelerated with increase of groundwater level decline. The Kalahari Aquifer is unconfined aquifer. When a decline of groundwater level becomes larger, the transmissivity of unconfined aquifer becomes smaller. Pumping rate in the aquifer is constant. Therefore, acceleration of decline is observed.

At Olifantswater groundwater level of the Kalahari Aquifer shows the recovery of about 0.4 meters in the year with 1/50years rain. Drawdown for 100 years reaches about 2.6 meters. Groundwater level of the Auob Aquifer shows the recovery of about 0.2 meters in the year with 1/50years rain. Total drawdown is about 2.2 meters (Fig. 12-90). These correspond to the rank A of water balance and economic constraints.

At Tugela groundwater level of the Kalahari Aquifer indicates the recovery of 0.7 meters in the year with 1/50years rain. The recovery of the Auob Aquifer with that rain is 0.6 meters. Total drawdown of the Kalahari Aquifer is 0.8 meters. These of the Auob and Nossob Aquifers are 3.0 meters and 2.8 meters respectively (Fig. 12-92). The results are classified into the rank A of water balance and economic constraints.

3) Case 3

Pumping rate of irrigation use is increased to 120% in this case. Total pumping rate is 109% of Case 1 (16.3 million  $m^3$ / year). Maximum drawdown of the Kalahari Aquifer will exceed 30 meters, and the Kalahari Aquifer will dry up within 25 years at Spes Bona (Figs. 12-74 and 12-91). It corresponds to the rank C of water balance constraint and economic constraint. Maximum drawdown in the Auob Aquifer exceeds 20 meters at Stampriet (Figs. 12-78 and 12-91). It corresponds to the rank C of water balance and

#### economic constraints.

At Olifantswater groundwater levels of the Kalahari and Auob Aquifers are slightly lower than these of Case 2. The differences of total drawdown between the both are less than 0.1 meters (Fig. 12-90). These correspond to the rank A of water balance and economic constraints. At Tugela groundwater level of the Kalahari Aquifer is almost the same as that of Case 2. Drawdown of the Auob and Nossob Aquifers are 0.05 and 0.1 meters lower than these of Case 2 (Fig. 12-92). These are classified into the rank A of both constraints.

#### 4) Case 4

In this case the pumping rate of irrigation use is reduced to 70% of Case 1. Total pumping rate is 86% of Case 1 (12.9 million  $m^3$ / year). At Spes Bona the period to dry up in the Kalahari Aquifer extends for 80 years (Fig. 12-91). However, maximum drawdown in Stampriet area exceeds 30 meters (Fig. 12-75). It corresponds to the rank C of water balance and economic constraints. Total drawdown of the Auob Aquifer at Spes Bona is 3.4 meters. Maximum drawdown in Stampriet area is less than 10 meters (Fig. 12-81). It is classified into the rank B of water balance and the rank A of economic constraint.

At Olifantswater groundwater level of the Kalahari and Auob Aquifers are 0.06 to 0.15 meters higher than these of Case 2, and are classified into the rank A of water balance and economic constraints (Fig. 12-90). At Tugela groundwater level of the Kalahari Aquifer is almost the same as that of Case 2. Drawdown of the Auob and Nossob Aquifers are 0.07 and 0.21 meters higher than these of Case 2 (Fig. 12-92). These are classified into the rank A of both constraints.

5) Case 5

The pumping rate of irrigation use is reduced to 50% of Case 1 in this case. Total pumping rate is 77% of Case 1 (11.5 million  $m^3$ / year). At Spes Bona total drawdown of the Kalahari Aquifer is almost 0 meter, however total drawdown of 5 to 9 meters remains in Stampriet area (Figs. 12-76 and 12-91). The water balance constraint is the rank B and economic constraint is the rank A. Total drawdown of the Auob Aquifer is 3.0 meters, and it corresponds to the rank A of both constraints (Figs. 12-82 and 12-91).

At Olifantswater groundwater level of the Kalahari and Auob Aquifers are 0.1 and 0.25 meters higher than these of Case 2, and correspond to the rank A of both constraints (Fig. 12-90). At Tugela groundwater level of the Kalahari Aquifer is almost the same as that of Case 2. Drawdown of the Auob and Nossob Aquifers are 0.12 and 0.25 meters higher than these of Case 2 (Fig. 12-92). These are classified into the rank A of both constraints.

#### 6) Case 6

The pumping rate of irrigation use is reduced to 0% (abolishing irrigation) of Case 1 in this case. Total pumping rate is 54% of Case 1 (8.1 million  $m^3$ / year). At Spes Bona groundwater level of the Kalahari Aquifer shows the recovery of 21 meters (Fig. 12-77 and 12-91). It corresponds to the rank A of water balance and economic constraints. Groundwater level of the Auob Aquifer shows the recovery of 15.5 meters, and it corresponds to the rank A of both constraints (Figs. 12-83 and 12-91).

The model layer 1 and 2 correspond to the Kalahari Aquifer as mentioned before. The model layer 1 at Spes Bona is dry cell (inactive) in the calibration periods and the bottom altitude of it is 1155m. The model layer 2 is unconfined until groundwater level recovers to 1155m. When groundwater level reaches to 1155m, the model layer 2 becomes confined condition. Storativity of confined aquifer is smaller than that of unconfined aquifer in two orders. Then groundwater level recovers suddenly in 2014. This recovery causes the model layer 1 to be active (re-wetting). The model layer 1 is unconfined and the groundwater level recovers to be gradual.

At Olifantswater groundwater level of the Kalahari and Auob Aquifers are 0.25 and 0.5 meters higher than these of Case 2, and correspond to the rank A of both constraints (Fig. 12-90). At Tugela groundwater level of the Kalahari Aquifer is almost the same as that of Case 2. Drawdown of the Auob and Nossob Aquifers are 0.25 and 0.7 meters higher than these of Case 2 (Fig. 12-92). These are classified into the rank A of both constraints.

12.8 Evaluation of Permissible Yield

#### 12.8.1 Permissible Yield in the Basin

1) Water Balance

Results of water balance in prediction period are shown in Figs. 12-93 to 12-103 for ordinary year (after 10 years) and year with 1/50years rain (after 30 years). After 30 years pumping rate from wells reduced since pumping rate of dry cells is eliminated by the MODFLOW. In ordinary year total groundwater outflow (pumping + outflow at boundary) exceeds the groundwater inflow (recharge + inflow from boundary) and is compensated by the groundwater storage release, declining groundwater levels. In year with 1/50years rain, the groundwater inflow exceeds temporarily the groundwater outflow and increases the groundwater storage, recovering groundwater levels.

#### 2) Results of Prediction

As shown in previous section, predicted results in Stampriet area are different from these of other area. Therefore, the results were evaluated for Stampriet area and remaining other area respectively. Results of the model prediction in the Stampriet Basin were summarized as bellow:

Area		Stamprie	t area			Other	area	
Constraint	Water E	Balance	Econon	nic	Water E	Balance	Econom	nic
Aquifer Case	Kala	Auob	Kala	Auob	Kala	Auob	Kala	Auob
1	NA	NA	UD	А	А	A/UD	G	G
2	NA	NA	UD	А	А	А	G	G
3	NA	NA	UD	UD	А	А	G	G
4	NA	UD	UD	G	A	A	G	G
5	UD	А	G	G	А	А	G	G
6	A	A	G	G	A	A	G	G

**Relation to Expected Constraints** 

Remarks: G=Good, A=Allowable, UD=Undesirable, NA=Not Allowable Kala = Kalahari Aquifer, Auob = Auob Aquifer

3) Permissible Yield

Present groundwater abstraction (Case1, Case 2) is acceptable in the Stampriet Basin except Stampriet area. In this area groundwater is mainly used for stock watering and domestic purposes. It is considered that groundwater use will not increase remarkably. In Tugela area declines of groundwater level are slightly large with present groundwater pumpage. Careful monitoring is necessary.

In Stampriet area, the Kalahari Aquifer will dry up in near future, if present groundwater abstraction is kept. From the above results, pumping plan of Case 5 (reducing irrigation use to 50%) and Case 6 (reducing irrigation use to 0%) are acceptable in Stampriet area. Case 4 (reducing irrigation use to 70%) is not allowable since the Kalahari Aquifer will dry up within 80 years. To prevent the dry-up of aquifer, groundwater pumping for irrigation use is at least reduced to 50% of that in 1999, which is almost the same as the irrigation use in 1992.

#### 4) Steps to Permissible Yield

(1) Schedule of Protective Measures

As protective measures differ for each area, their specific schedule needs to be suitably set respectively for each area. Based on the experience in Japan, the following stages can be considered in general (Shibasaki et al., 1995).

i) Research Stage

A preliminary reconnaissance based on available information is carried out in order to learn the general conditions of the basin. For all the boreholes in the basin, registration, arrangement of well inventory, measurement of groundwater level and pumping rate, and submission of its report should be ensured.

Base on these data, a preliminary review is carried out, minimum level of facilities for monitoring is set up, and the permissible (yield) critical groundwater level is tentatively worked out. In this stage, construction of new boreholes is strictly regulated.

The period for the first stage is desirably within a few years, even for areas without substantial data.

ii) Observation and Arrangement Stage

Based on the permissible critical groundwater level determined initially in the first stage for each area, groundwater level and extraction are observed, and groundwater pumpage for each area is reduced. The deduction of groundwater pumpage is closely related to the socio-economic factors as well as with the general utilization of water resources including the possibility of development of alternative water sources such as dams.

In the second stage, the monitoring system is further improved, and the data are comprehensively analyzed. Then for each area, each municipal unit (cities and towns), of for smaller zones, permissible yield are determined. For this second stage, a period of five years would be practical.

iii) Stage for Intensive Enforcement Measures

As long as measures are strictly enforced in the second stage, the objectives to stop groundwater problems may be considered to be mostly achieved. If groundwater level still cannot be regained, a third stage may be considered in which intensified restriction on pumpage, intensive alteration of water sources, and measures for artificial recharge should be resorted to.

For the realization of effective groundwater basin management, besides technological improvements, legal and social issues such as the improvement of groundwater utilization system should be considered.

(2) Steps to Permissible Yield in the Study Area

For the study area, groundwater management may be in a transition period from the first stage to the second stage. For the present, observation of groundwater levels should be continued using the monitoring system that made by this study. Improving the groundwater model based on the observation results, tentative permissible yield in this study should be revised precisely.

Urgent measures to be taken are preventing the increase of groundwater abstraction. In order to achieve this, it is important to inform farmers of the present situation in the basin, and to make farmers understand the problems that will occur with present groundwater use. Therefore the farmers may be cooperative to reduce the pumpage.

Meanwhile measures reducing pumping rate to the permissible yield should be prepared. It is considered to apply permits strictly to irrigation use. Charging system for groundwater use is worth considering.

#### 12.8.2 Future Improvement in Modelling

The modelling of the Stampriet Artesian Basin is based on the knowledge at present. Therefore, modification of the model will be expected in future observations and investigations.

There is no observation well of the Kalahari Aquifer in Stampriet area, where serious problems are estimated to occur in near future. New Kalahari observation wells are necessary to monitor the variation of groundwater level and to improve the model accuracy.

The calculation model in this study was unstable at the bottom area of the model and there were incomprehensible head differences. Future improvement is necessary to enhance the model accuracy.

Groundwater pumping rate was estimated by using many assumptions. The reports from permit holders are incomplete. It is necessary to report monthly abstraction properly. For domestic and stock watering use, there are no data on the variation of pumping rate. It is recommended to select sample wells and to install the flow meter.

The recharge rate is unknown at present. A basic hydrologic and hydrochemical study is necessary to estimate accurate recharge rate.

The model calibration should be improved based on the future studies above mentioned and the observation results of the monitoring system. It is recommended to model the groundwater quality, investigating the influence of "salt block".

		Formation	Lithology	Hydrogeolo	gical Structure
		roimation	Linology	Aquifer Type	Conceptual Model
	К	alahari Beds	Sand, Gravel, Calcrete	Unconfined aquife	(aquitard)
		Karoo Dolerite	Dolerite	Aquitard-	Unconfined aquifer
ce		Kalkrand Basalt	Basalt	Unconfined aquife	
nen			Sandstona	Unconfined-	Leakage
Seq	Ę.	Rietmond member	Sanusione	confined aquifer	▲ (aquitard)
ğ	ijo		Shale	Aquitard	1st confining layer absent
aro	a G	Auch member	Sandstone	Confined aquifer	▼
	ည္သ		Shale	Aquitard	1st confined aquifer
	щ	Mukorob member	Sandstone	Confined aquifer	
			Shale	Aquitard	2nd confining layer
		Nossob member	Sandstone	Confined aquifer	2nd confined aquifer
		Dwyka Group	Tillite, Mudstone	Basement	
	N	lama Group	Sandstone, Shale	Basement	
	Dan	nara Sequence	Metamorphic rock	Basement	Hydrogeological Basement

Table 12-1 Hydrogeological Structure in the Stampriet Artesian Basin

Table 12-2 Combination of Aquifers and Aquitards

	В	С	Κ	Μ	Α	L	Ρ	Q	R	\$	Τ	۷	W	X	Y	D	Ε	]	J	G	Н	0
Kalahari Beds	-	Х	X	Х	Х	Х	Х	Х	Х	X	Х	Х	Х	Х	Х	-	-	-	—	-	-	-
Basalt	Х	Х	-	-	-	_	—	—	—		-	—	-	—	-	-	-	-	_	—	-	—
Upper Rietmond	—	—	-	–	-	-	Х	Х	Х	-	-	X	Х	Х	Х	X	Х	X	X	-	-	-
Lower Rietmond	-	-	-	-	-	Х	Х	Х	Х	X	X	Х	—	—	-	-	-	Х	Х	X	-	- 1
Auob Aquifer	—	—	-	-	Х	-	Х	-	Х	X	-	Х	Х	-	Х	Х	-	Х	-	X	-	-
Lower Mokorob	-	_	-	Х	Х	-	X	Х	-	Х	X	-	Х	Х	-	X	Х	Х	Х	Х	X	-

1) Basalt: Kalkrand Basalt

2) The Nossob Aquifer is assumed to be isolated form upper aqufers

# Table 12-3 Combination of Aquifers and Aquitard for Each Cell

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\*Symbols correspond to those in Table12-2

Symbol	0	В	с	A	Ρ	Q	R	w	x	Y	S
Layer 1	10m	20m	ТК	0.5*TK	٦K	ТК	ТК	ТК	ТК	ТК	0.75*TK
Layer 2	10m	50m	50m	0.25*TK	TUR	TUR	TUR	0.75*TUR	0.75+TUR	0.75+TUR	0.25*TK
Layer 3	10m	50m	50m	0.25*TK	TLR	TLR	TLR	0.25*TUR	0.25+TUR	0.25*TUR	TLR
Layer 4	10m	100m	100m	TA	TA	0.25*TLM	TA	TA	0.25*TLM	TA	ΤA
Layer 5	10m	10m	10m	TLM	TLM	[0.75 <b>+TLM</b>	10m	TLM	0.75*TLM	10m	TLM
Layer 6	10m	10m	10m	-	1	-	-	-	-	-	-
Symbol	т	v	L	м	к	I	J	D	E	G	н
Layer 1	0.75*TK	0.75*TK	0.75*TK	0.5*TK	ТК	0.25*TUR	0.25*TUR	0.25*TUR	0.25*TUR	0.25*TLR	0.125*TLM
Layer 2	0.25*TK	0.25*TK	0.25*TK	0.25*TK	10m	0.75*TUR	0.75*TUR	0.5*TUR	0.5*TUR	0.25*TLR	0.125*TLM
Layer 3	TLR	TLR	_TLR	0.25*TK	10m	TLR	TLR	0.25*TUR	0.25*TUR	0.5*TLR	0.125*TLM
Layer 4	0.25*TLM	TA	10m	0.25*TLM	10m	TA	0.25*TLM	TA	0.25*TLM	TA	0.125*TLM
Layer 5	0.75*TLM	10m	10m	0.75*TLM	10m	TLM	0.75*TLM	TLM	0.75*TLM	TLM	0.5*TLM
Layer 6	[ -	-	10m	-	10m	-	-	-	1	-	

Table 12-4 Procedure of Aquifer Allotment to Model Layer

\*) TK: Thickness of Kalahari Beds

TUR Thickness of Upper Rietmond Member

TLR Thickness of Lower Rietmond Member

TA: Thickness of Auob Aquifer

TLM: Thickness of Lower Mukorob Member

\*\*> Symbols correspond to those in Table12-2 and Table12-3.

# Table 12-5 Bottom Elevation of Model Layer 1

_	1	2 3	4	5	6	7	9	э	10	11	12	13	4 1	5 16	17	15	12	20	21	22	23	24	25	25	27	28	29	30	31	32	33 3	4 35	36	- 37	38	39	40	41	42	43	44 4	.5 45	5 47	48
1 95	4 181	5 1944	1740	675 'i	638 H	521 1	581 [155	54 150	34 15	15 15	06 15:	20 155	8 152	5 1495	1495	1461	1425	1413	1427	1446	1442	1439	1433	1467	1429	1422	:449	14€5	1507	1464 1	173 1472	451	1436	13ê2 -	1305	1285	1277 1	263 12	57 12	243 12	39 h236	8 1238	1238	1238
2 198	1 186	6 1996	1761 1	728 *	673 10	27 10	203 15	79 115:	6 15	03 14	96 14	6 152	3 155	3 1474	1433	1449	1432	1400	1404	1424	424	1425	1426	1441	1411	1418	:443	1482	148E	1463 14	143	:413	1379	1353	1950	1345	1310 1	273 12	59 12	49 12	47 1247	1 1247	1247	1247
4 . 67	G 199	1 7 G H	1 200 1	592	E 3E 1	EDE 1	08 15	13 15	14 14	02.12	95 14	12 161	3 1.40	1 697	1.402	1.405	1427	1400	1987	1305	1408	1475	1415	1414	139/1	1416	1433	1444	1.447	1642 1	124 1405	1992	1356	1949	1337	1.21.0	1208 1	285 12	25 12	65 10	45 174F	5 1256	1256	1756
1000	3 100	4 4 7 3 0	1720	7.4	C 4 C 14		2115 11 D.	17 115		40 14	70 1 0		0 1 45		1 400	1007	1100	1400	1202	40.00	+170	1000	10.54	LOOF.	1220	1404	+ 400	4.450	1 42 4	1405 1	200 4076	+ 170	1000	1040	1040	1000	1200	200 12	73 12	Sec 12	50 H200	0 4050	12.00	12.00
4 .03	3 101	1 1770	1729		646 I.	92 1	505 154	47 1104	49 10	43 14	70 19.	24   14.	9 146	1 1419	1403	1307	1402	1400	1392	1200	370	1292	1334	1595	1373	1464	· 450	1463	1424	1405 1.	100 1070	1.370	1354	1343	1312	12.39	1209 1	203 12	10 12	00 12	39 1233 A	1 12.3	12.3	12.9
2 <u>1:90</u>	8 176	4 1720	1712 1	650 I	529 1.	572 13	565 158	85 1156	92  14	92 14	79 14	58 144	2 145	2 1423	1385	1321	13/8	1385	1379	1360	างก	1380	1383	pa/a	1370	1406	:420	1430	1420	1401 1.	564 135t	1354	1342	1321	1:402	1288	1279 p	268 12	260 12	261 12	63 1263	1 1260	1260	1260
€ <u>1388</u>	0 179	6 1982	1689 1	606 1	641 1	545 16	568 155	55 150	08 14	59 14	69 14	54 144	B 144	9 1410	1384	1362	1357	1365	1357	1338	1354	1355	1950	1358	1374	1390	1390	1425	1443	1413 13	360 1359	*339	1327	131B -	1299	1288	1283 1	273 12	265 12	250 12	33 1230	1 1233	1230	1230
7 171.	5 183	8 1814	1584	521 <sup>1</sup>	e 75 🕅	548 13	42 14	74 143	59  14	47 14	48 14	41 145	C 143	4 1401	1387	1372	1358	1339	1339	1334	350	1334	1343	1354	1370	1375	-390	1420	1433 .	1400 13	860 1350	1 326	1315	1312	1293	1280	1265 [1	245 12	35 12	20 12	12 1212	2 1212	1212	1212
8 360	6 175	a 1720	1729 1	635 🗅	578 1-	495 1-	490 14-	45 143	34 14	36 14	28 14:	20 142	6 141	1389	1378	1367	1351	1335	1319	1322	1334	1326	1355	1363	1365	1365	1380	1395	1420	1390 1:	300  1340	1:290	1280	1280	1280	1270	1245 1	243 12	215 12	203 11	63 (1163	J [1163	1160	1160
3115E	1 1/20	8 1565	152B 1	504	453 1	448 11	45.5 14:	31 14	54 114	25 14	13 14	29 140	1 139	2 1377	1362	1352	1340	1333	1325	*aco	13:05	1301	1321	1329	1355	1350	:39D	141D	1417	1385 17	340 1332	1.310	128D	1260	1255	1245	1255 1	255 12	13 12	00 12	43 1243	3 1243	1243	1240
10 - 47	1 153	> 1477	1471 1	45.1 2.	431 2.	497 14	127 14	47 14	10 14	28 14	16 14	18 1 97	4 137	1369	1360	1340	1.241	1332	1318	1335	1286	1256	1306	1300	1340	1332	1340	1346	1393	1380 10	50 1320	1 2310	1290	1225	1200	1225	1255 1	247 12	00 12	200 12	30 1230	1 1237	1235	1235
11 1 1 1	0 1 1 1	0 1444	1.008	401 4	439	435 4.	174 144			42 14	00 10	-		1 2 2 4 8	1.244	1297	1200	1214	10.00	1990	1746	1040	1714	1000	1200	1426	1220	1.41.9	1310	1005 10		1 1 1 1 1 1	11176	1100	1162	1.111.0	1000 1	175 11	112 11	115 12	47 1041	7 1247	1047	1147
10 144	0 1.41	2 1441	4400 4	421	420 4	42.3 I*	100 444		- 114 - 40	74 40	03 113	12 100		1040	4004	1302	1220	1010	1000	1050	1240	1200	1213	1200	12.00	1030	10.50	1012	1010	130 7 14	00 400	4070	1273	1200	430	1220	1220 1	202 42	20 10	20 12	an 11241	1 1247	1247	1247
12 1413	2 41	C 11412	1432 1	424 1	4.52		4081 1144	10 1 1 22	90 10	110	CD II.a	42 11 24	u nac	5 11 22 1	1524	1315	1304	1304	1352	296	1250	1243	1265	1260	1363	13-2	1451	Taur	1270		20 1260	1 1270	1200	1220	1 1 7 4 1	1.60	1192 1	222 12	29 12	25 12	23 1220	1 1223	1223	1220
13 137	6 1 35	8 1370	1393 1	371	429 14	424	119 138	39 130	51 13	25 13	55 [13	47 134	2 133	5 1327	1317	1307	1301	1294	1298	1255	1245	1230	1270	12/8	1268	1297	1320	1320	1250	1275 13	260 126	1260	123D	11/6	1:43	1223	1219 1	220 12	<u>13 12</u>	217 112	13 1213	1 1219	1219	1219
14 135	1 :35	3 1391	1369 1	356 1:	339 ::	333 11:	345 13	54 13	57 13	54 13	49 13	i9  133	5 132	7 1322	1315	1305	13D0	1294	*250	1240	123D	1220	1243	1270	1275	*2 <b>9</b> 6	127D	1281	1263	1243 12	240 1240	1235	1220	1200	1184	1150	1160 1	225 12	204 12	03 12	20 1220	1 1223	1223	1220
15 132	9 :32	4 1318	1317 1	325 1	319 '3	309 🗄	313 134	41 13	50 13	47 13	42 13	27 131	8 131	1310	1305	1300	1295	1290	245	1240	1215	1210	1225	1265	1275	280	126D	1265	1260	1250 13	45 240	1230	1225	1220	1210	1205	1205 1	265 12	17 12	32 12	39 1233	1233	1239	1239
16 131	7 130	7 1302	130* 1	305 1	302 1:	298 😂	299  13:	23 [13:	39 [13	45 13	34 [13:	20 131	1 [131	1 1305	1290	1290	1291	1284	1250	1255	1220	1210	1225	1240	1260	270	1261	1245	1259	1250 12	245 235	1235	1230	1225	1220	1210	1210 1	210 12	200  11	95 12	10 1210	J 1210	1210	1210
17 131	8 130	2 1294	1292 1	295 10	294 13	294	295 130	06   13d	33 13	34 13	24 13	10 130	6 130	1291	1,261	1261	1262	1230	*250	1245	1225	1216	1200	1225	1250	*26D	1246	1245	1243	1245 13	40 233	1230	1225	1225	1225	1223	1223 1	223 12	15 12	210 [12	20 1220	1 1220	1223	1220
18132	0 22	6 12B3	128: 1	282 1	235 1:	273 1	276 125	77 132	22 13	14 13	11 12	75 127	5 122	1275	1275	1270	1255	1250	1255	1234	1230	1203	1194	1220	1225	*220	1241	1238	1235	1234 13	30 1230	1230	1225	1225	1220	1220	1220 1	215 12	10 12	00 12	05 1205	5 1205	1205	1205
19 239	2 1224	e 1278	1069 1	269 1	268 1	260	265 129	31 1.20	00 12	97 12	82 12	10 124	1 124	1 1241	1247	1255	1245	1250	t220	1206	1205	1220	1187	1190	1185	1200	123D	1235	1229	1226. 11	25 1220	1220	1220	1220	1210	1210	1210	210 12	05 11	BQ 11	70 11 7/	1 11 22	1177	11.72
20122	- 1100	9 1220	1245	245 0	248	148	156 112	21 125	27 12	89 12	10 10	10 100	H 125	1265	1251	1250	1220	1145	109	1125	1920	1990	1175	1160	1175	210	1226	1215	1202	1210 12	210 22*	1910	1210	1210	1200	1192	1160 1	160 11	75 11	60 11	00 1100	11100	1102	1100
20 33	0 1-22	5 1210 3 1368	1200	054 40	4+0  l. 007  44	125 14	142 112	4 15	57 112	07 12	17 12	20 1120	0 1120 E 1124	1233	1201	1005	1105	1150	+100	1320	12/00	1170	11.42	1152	1180	1226	1229	1140	1 / 8 / 1	11 8/1	200 1200	1275	1205	1202	1700	1000	1102	122 11	20 10	01 10	20 102	1 1/220	1020	1929
43	9 (13) a (1	3 1735 a 1735	1740	209 11	237 13	(33 K)	2.121	14 112	11 112	01 112	17 1121 27 122	20 123	o 124	1243	1230	1223	1195	1120	190	1220	1200	1178	1140	0011	1100	2.33	200	140	1100	1100 13	1203	1205	1200	1200	1100	1200	1190 1	1 40 11	20 10	10 10 10		10.0	1010	1010
22 :03	3 .3 .	0 1269	1280 1	226 13	225 13	223	225 12.	36 120	39 12	60 12	57 023	50 124	3 123	5 1230	1223	1200	1195	11.75	1195	1140	1200	1166	1135	1140	1170	:190	1165	1120	1523	1150 1	70 1160	1110	1180	1175	1165	1133	1163 1	140 10	150 10	33 10	20 1020	1 1050	1030	1628
23 30	7 130	6 1264	1246 1	222 1:	222 ::	222 112	219 12:	23 122	23 12	35 12	45 112	4* 123	5 123	1225	1230	1160	1160	1160	1220	:200	160	1140	1:45	1150	1100	150	114D	10/0	1123	<u>1150 p</u>	135 1120	1110	1120	1125	1140	1090	1080 1	343 3	בון סאי	110 110	20 11020	1 1 220	1020	1020
24 129	9 (2)	4 1263	1263 1	223 10	219	218 12	219 121	17 12	19 12	20 12	33 12	36 121	9 122	3 1210	1218	1210	1170	1140	1190	1205	1203	1202	1200	1170	1070	120	1040	1090	1:03	1113 1	20 1090	1075	1090	110D -	1670	1:20	1050 1	376 9	45 13	Ю <b>Д</b> Э	90 993	1 393	995	990
25 131	1 *26	8 1252	1253 1	237 1:	235 *:	205 12	204 120	25 121	10 12	17 12	24 12:	24 120	8 (1*S)	9 1192	1190	1195	1205	1160	1157	:170	120)	1203	1160	1150	1132	:159	1107	1110	1 '33	1045 10	1050	080	1110	1130	1110	1000	1071 1	C69 9	070 110	125 13	50 1050	1 1050	1050	1050
25 127	5 26	6 1229	1243 1	243 10	206 1	198 ]12	202 1119	48 120	54 12	30 12	09 (12)	på [121	0 1119	5 1206	1195	1190	1165	1185	•1A1	150	1135	1130	1180	1178	1123	1162	1172	1095	1115	1114 1	20 1122	1+0a0	1120	1070	1120	1*02	1067 1	323 13	10 15	170 10	63 1383	J 1080	1080	1080
27 125:	2 24	0 1213	1219 1	216 1:	219 🗄	193 11	194 119	94 119	35 12	21 12	02 12	10 120	0 119	1203	1200	1190	1160	1165	1155	151	1155	1125	1:01	1159	1132	:098	145	1097	1090	11:05 11	109 1115	1121	1070	1064	1064	1061	950	945 10	:00 10	11 0.69	00 11:00	11:00	1100	1100
28 27	7 25	4 1227	1205 1	198 10	200 11	204 1	194 116	39 III 9	91 11	96 12	at 12	33 120	2 1179	1 1186	1190	1175	1165	1155	1167	1173	1169	1111	1179	1173	1138	1096	1111	1102	10€8	1383 10	197 11C2	1099	1036	1055	1055	1053	943 1	050 10	10 10	10 10	ec 10ec	3 1080	1080	1090
29 130	7 + 27	6 1251	1223 1	203 1	193 *	186 1	177 1116	30 119	3 11	93 lit	95 12	1* 11:5	o hte	1 1172	1160	1155	1150	1159	1150	1158	L1€B	1155	1153	1178	1161	1129	1 DHD	1073	10€2	1000 10	1091	1.079	1053	1052	1650	1054	970 1	050 10	063 13	:65 1C	50 1050	3 1050	1050	1050
30 128	1.1126	5 1251	1215 1	203 1	234	146 11	158 111	70 111	72 11	82 117	87 117	11-8	5 11:8	1:75	1165	1155	1155	1153	1151	*148	1105	1086	1:46	1173	1174	1140	1021	1659	1050	1068 1	061 1072	1:067	1047	1048	950	1010	1050 1	053 10	45 10	150 10	40 1040	3 1040	1040	1D4D
31 1 28	3 4 9 7	9 1295	1217 1	212 1	215 +	103 1	173 116	81 111	74 11	72 11*	75 12	10 11 1	110	1 11 1 25	1165	1153	1154	1145	1134	130	1125	1043	1003	1155	1157	1150	112	1061	1642	1057 10	149 1051	1-041	1036	440	476	10.40	1050 1	C40 h0	10 0.0	30 10	90 1095	0.0000	1020	1020
22 192	0 1 2 2	a 1042	1245 1	223 1	214	231 12	204 111	51 112	48 11	10.11	\$7 11-1	20 11-2	5 118	11175	11.20	1171	1154	1140	1130	1115	1100	1095	1120	11192	11.45	1123	114	1054	1022	1038 1/	152 104	1020	1035	1020	090	1015	1035 1	025 10	10 40	00 110	00 1000	c 1000	1000	1000
20 1 20	6 1-20 5 1-20	0 1070	1240 1	1.50 1.	240 14	2.11 14					32 1 1	- <b>.</b>	E 1.0		1.10	1154	1160	11.46	1125	176	1106	1000	1120	1074	1.502	1000	106	1044	1020	1030	01 004	1022	1026	1046	000	1010	1010 1	010 10	16 10			0.000	030	0.00
33 : 29	5 (12)	0 1279	1256 1	198 1.	243 (0)	242 12	228 110	99   114 99   114	39 10	38 111	27 11 3	20 N : e	3 11 18	111/5	11.70	1100	1162	1135	1125	1110	100	1025	996	10.00	1063	1094	1,011	1044	1622	1005 1	vai 1.9au	1 11034	, uon	1041	9.40	0.00			<u>na na</u>	22 1 3	an aar	7 930	930	9.40
34 190	2 :25	/ 1243	1208 1	177.1	194 1	187 1	1/4 11	<u>ka ma</u>	<u>33  17</u>	<u>m 11</u>	<u>as n t</u>	<u>/* p*e</u>	118	: 1170	n*63	1165	1165	1145	1130	1120	110	1070	1028	1269	1069	1092	093	1026	1022	1039 10	137 1038	11:030	1040	1045	980	996	993	990 110	10 9	999 9	85 983	<u>, 985</u>	985	985
35 : 27:	5 24	5 1234	1204 1	183 1	194	175 11	159 114	42 11	17 [13	99 <u>1</u> 1	05 11:	95 178	0 117	1160	1-40	1145	1160	1155	1130	120	1115 i	1090	1030	1265	1076	1091	D74	1034	1013	1841 1	1023	1025	1038	970	93D	980	982	993 9	999 9	85 9	82 983	1 985	980	980
36 24	e 1121	<u>a 1219</u>	1228 1	207 1	176 17	143 1	119 110	28 110	03 110	95 I 1	61 11:	53 119	7 119	7 1175	1:60	1153	1150	1155	1120	1110	100	1105	1000	1053	1052	1059	031	1012	1004	1313 11	128 11014	1020	950	AED	96D	965	970	970 9	173   3	975 9	60 983	1 990	980	98D
37 ! 22:	2 119	9 1165	1185 1	173 !	156	099 10	359 I U	39 105	94 þ.C	87 11	ên 11:	¥2 119	7 121	1200	1.75	1160	1140	1140	1120	1070	1030	1000	970	1039	1044	1040	1030	1008	1002	1205 10	007 962	9+0	940	955	945	955	960	960 9	63 9	65 9	63 385	1 980	980	98D
38121	8 020	1 1190	1164 1	143 1	144 🕛	077 10	038 110	D2 191	77 110	86 1	84 11:	32 118	9. 121	1200	1160	1165	1150	1130	1110	1050	1020	975	1030	1029	1039	1032	021	1011	1001	1010 10	100	1010	950	950	940	950	950	945 j 🤅	65 9	460 j 9	65 965	j 965	965	965
39 27	1 129	1 1303	1244 1	127-1	117	054 10	045  10F	67 10	74 10	87 1	83  11	39 118	5 118	5 1180	1173	1163	1150	1120	1060	1035	1020	1056	1017	1039	1039	1030	101B	101D	958	1807 10	J19   930	935	955	950	94D	940	935	935 9	943 9	953 9	55 955	5 955	955	955
40 27	4 132	2 1323	1253 1	148 1	095 11	025 10	078 106	57 10	74 10	94 11	77 11	19 111	6 117	5 1170	h-\$0	1130	1120	1085	1065	1040	1097	1058	1016	960	960	940	93Q	1006	990	1001 14	14 95!	955	960	940	945	945	943	943 9	aa [ 9	50 9	60 960	1 960 L	960	960
41 1299	s 1:26	1 1332	1234 1	106 11	051	032 10	17A 104	43 105	57 1:	00 111	70 11	11 116	B 117	1178	1:35	1113	1112	1094	10E9	:050	1089	1055	957	1002	1000	970	978	963	938	1201 9	30 553	950	945	950	960	955	950	910 9	25 J	45 Э	55 955	5 955	955	955
42 : 35	e <b>1</b> 33	0 1245	1173 1	C95 11	022 1	058 N	351 103	34 136	51 17	17 113	65 113	:4 h1:6	1 116	1167	1720	1112	1103	1064	1064	1050	1016	985	959	970	100£	998	979	967	943	943 3	30 920	930	935	940	960	983	950	900 9	20 9	40 9	60 960	3 960	960	96D
41140	6 1 32	1 1269	1134 1	035	996 1	037 1/	137 106	12 10	55 10	97 11:	54 11	5 114	5 114	11150	1125	1112	1110	1000	1055	1026	1001	975	958	949	983 I	\$91	986	969	943	935		94B	920	93D	940	960	940	890 9	10 3	40 9	55 955	5 955	955	955
44 1 22	5 + 10	4 1202	1110 1	DAR	120	504 10	112 1/16	57 172	44 12	61 11	43 11 1	15 11 1	1 1 19	7 11-65	1141	1131	1120	1093	1053	1018	1004	0.91	667	545	960	1030	1027	1027	045	532 0	91 031	031	024	920	045	040	925	805 2	100 3	55 9	60 367	1 967	060	062
46 1.25	1 1 1 1 1 1 1	2 1104	1124 1	647	0.50	205 10	107 100	21 10	24 10	4+ 1+	05 110	17 107	4 1100	11454	1147	1112	1107	1/10.1	1079	1059	1020	1011	078	661	540	1075	1017	1015	212	324 0	51 95/	0.54	110	694	USD.	097	ana	957 0	27 3	57 9	6/1 261	1 261	Digit.	uer
40 100	- 40 - 400	2 1190 5 1004		00.1	074 0		27 10				10 10	10 100	a hai		11.40	1123	1.000	1087	1070	1050	1642	1010	500	501	0.51	000	1000	1010	1000	578 /	50 000	0.49	057	600	020	042	000	B00 5	40 5		46 548	5 000 5 045	0.46	0.00
40 130	3 32		1139 1	191	994 :	390 3	794 1103	03 10.	32 10	15 115	23 110	19 1100	3 1107	1.20	1.40		TURA	IUN /	.Un I	- U59	104.1	ILIN.	930	Anu .	901	340	roua.		LUN	370 3	nuu yee	940	967	1090	926	345	LOG	800 3	140 B	10 9	40 340	1 940	340	940
47 137	4 :27	1 1191	1132 p	C85 :	995 9	354 8	975 JIQ	44 1132	25 110	pa 12	<u>оя па</u>	13 187	7 135	3 11285	1135	1126	1101	1083	*057	1054	1044	1028	1203	974	569	999	996	997	999	961 1	33 932	950	966	979	930	915	850	900 9	40 9	35 9	30 930	1 990	930	930
48 136	8 123	8 1164	1145 1	091-11	009	370 1	975 99	39 103	25 3	95 9	92 10	07 102	3 104	9 1083	1121	1120	1105	1089	*072	10%6	1047	1637	1029	1,39€	950	996	1000	985	968	963 9	25 921	935	870	905	910	919	859	890 9	25 9	10 9	20 920	1 920	920	920
49 135	6 12'	9 1135	1137 1	125 H	015 :	978 9	970 95 97	11 100	30 B	93 9	75 9	85 101	3 137	2 1104	1100	107.9	1064	1083	*060	1055	1046	1044	102/3	1015	9E0	999	975	993	365	9E4 (	979 946	924	E6.9	905	927	893	850	891 9	10 9	21 9	00 900	1 900	900	300
50 133	3 222	2 1135	1108 (1	101 1	001	993 9	964 99	92 100	32 3	84 9	65 9	33 99	4 130	1 1295	1073	1067	1048	1036	:091	1050	1040	1043	1035	1015	950	:006	995	989	367	984 9	180 98F	948	930	852	866	857	શ્વસ	876 9	63 9	06 8	80 880	1 960	860	1 880 [
51 134	5 123	7 1153	1113 1	C83 11	003 :	991 9	568 96	57 98	82 3	79 9	55 9	57 97	3 99	7 1072	1079	1068	1041	1052	1085	1073	1064	105*	1025	1010	990	970	997	989	386	986 J (	93 976	959	942	915	908	305	843	859 8	850 8	60 9	03 903	3 903	903	903
52 1323	3 124	7 1161	1120 1	089 11	016 !	9.95 9	377 93	77 93	75 3	79 9	50 9	47 98	1 99	1058	1065	107E	1053	059	1086	1072	1062	1053	1039	1027	:005	998	971	992	363	983 9	84 981	970	945	926	.911	302	897	904 8	35 a	8 046	60 860	1 R60	860	860
53 132	2 12!	6 1161	1117 1	103 11	032 I	397 9	377 93	75 98	87 B	55 <del>3</del>	45 9	19 96	7 100	7 1004	1038	1064	1066	:071	1081	1055	1061	1057	1043	1024	1007	974	982	965	965	SBO 9	96 977	96B	949	930	915	904	895	790 8	15 8	30 8	40 840	J 840	840	843
54 132	1 124	9 1169	1145 1	• a2 11	029	997 -	122 119	97 100	24 3	62 3	47 9:	33 95	5 99	993	1007	1031	1050	:051	1052	105)	1060	1062	1048	1030 .	:0:7	997	985	978	963	981 9	976 976	967	948	932	919	905	760	765 8	acco a	a20 a	30 830	3 830	830	830
55 130	3 124	4 1194	1152 1	:15 11	031 11		150 10	11 98	52 3	35 9	30 9	11 45	5 38	1 979	369	1006	1034	1:037	1045	1048	1050	1055	1045	1028	1011	990	985	974	965	S61 9	73 971	964	950	932	922	810	790	775 7	90 8	10 A	20 820	J 820	820	820
45 121	4 124	0.196	1164 1	130 11	M7 1	anio	222 01	21 01	23 0	18 5	0 80	12 36	4 37	2 365	GR1	1002	1018	1042	101D	1010	1044	1040	1030	1021	0:00	996	990	976	977	962 0	54 94	960	04R	931	825	815	765	770 7	RE 9	0.5 9	12 812	5 815	815	a15
17 100	7 100	4 1100	1101	407.40			20 0			20 3	10 0	14 34	2 54	5 05F	970	1002	1040	2021	1015	1026	1015	1020	1/10/2	1027	1025	1010	ng.e	1004	Gen	955 0	157 0.90	040	393	842	820	817	785	758 1	182 1	197 A	D6 SING	t ar≠	ane	ane
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# Table 12-6 Bottom Elevation of Model Layer 2

1 2 3 4 5 6 7 8 9 10 11 12 13	14 15 18 17 18 19	20 21 22 23 24 25 26 27	28 29 30 31 32 33 34 35 36	37 38 39 40 41 42 43 44 45 46 47 48
1 1854 1805 1834 1730 1865 1828 1811 1581 1544 1524 1506 1498 1510	1548 1515 1478 1476 1451 1415 1	1403 1417 1438 1432 1429 1423 1457 1419 14	412 1439 1456 1497 1474 1463 1462 1451 1425 13	352 1295 1275 1267 1253 1241 1233 1228 1228 1228 1228 1228 1228
2 1971 1858 1886 1751 1718 1663 1817 1593 1569 1526 1493 1478 1486	1513 1548 1464 1423 1439 1422 1	1390 1394 1414 1414 1415 1418 1431 1401 14	408 1433 1472 1476 1453 1444 1427 1403 1369 11	343 1340 1335 1300 1283 1249 1239 1237 1237 1237 1237 1237
3 1899 1845 1788 1719 1677 1626 1596 1568 1543 1525 1493 1475 1463	1503 1480 1417 1392 1396 1417 1	1392 1372 1385 1388 1395 1405 1404 1380 14	406 1423 1434 1437 1429 1414 1392 1372 1348 13	33 1327 1308 1288 1275 1265 1255 1246 1248 1246 1246 1246 1246
4 1823 1801 1768 1749 1704 1636 1562 1545 1537 1539 1533 1468 1484	1449 1455 1409 1393 1377 1392 1	1396 1382 1358 1368 1379 1384 1385 1363 13	394 1420 1423 1414 1396 1378 1366 1360 1354 13	33 1302 1289 1279 1270 1263 1256 1249 1249 1249 1249 1249 1249
5 1798 1754 1710 1702 1650 1819 1562 1555 1575 1572 1482 1469 1458	1432 1440 1413 1375 1381 1368 1	1375 1369 1350 1361 1370 1373 1360 1380 13	398 1368 1370 1330 1400 1383 1356 1344 1332 13	11 1292 1278 1269 1258 1250 1251 1250 1250 1250 1250 1250 1250
6 1870 1788 1842 1579 1598 1831 1535 1658 1545 1498 1449 1459 1454	1438 1439 1400 1374 1352 1347 1	1355 1347 1328 1344 1345 1340 1348 1384 13	353 1353 1361 1340 1407 1370 1349 1329 1317 13	306 1289 1278 1270 1280 1255 1240 1220 1220 1220 1220 1220 1220
7 1705 1828 1804 1874 1811 1565 1838 1502 1464 1448 1437 1438 1431	1440 1424 1391 1377 1382 1348 1	1329 1329 1324 1340 1324 1333 1344 1346 13	349 1360 1355 1300 (250 1255 1275 (320 1310 13	310 1253 1235 1216 1196 1170 1190 1190 1190 1190 1190 1190 1190
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9 1571 1598 1578 1518 1494 1443 1438 1455 1421 1444 1415 1403 1419	1391 1382 1367 1352 1342 1330 1	1323 1315 1290 1295 1291 1311 1315 1330 113	310 1340 1320 1300 1315 1305 1285 1275 1280 13	75 1195 1196 1191 1184 1145 1185 1140 1140 1140 1140 1140 1140
10 1481 11522 1487 1481 1441 1421 1427 1417 1437 1409 1418 1408 1398	1364 1361 1359 1350 1339 1331 1	1322 1308 1295 1276 1240 (300 1280 1300 (3	320 1315 1310 1310 1315 1310 1260 1275 1245 12	200 1185 1180 1175 1120 1150 1180 1180 1180 1180 1180 1180 118
11 1438 1442 1431 1415 1411 1413 1413 1424 1414 1441 1437 1399 1352	1348 1347 1335 1334 1327 1310 1	1305 1298 1290 1235 1235 1240 1240 1280 1290 13	320 1290 1290 1290 1290 1295 1296 1295 1295 11	IAS (1A0 (180 1170 11A0 11A0 11A0 1224 1224 1224 1274 1274
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11 1348 1348 1340 (38) (38) (1414 1409 1370 135) (345 1345 1317	1372 1376 1317 1307 1207 1201 1	1284 1278 1205 1200 1200 1210 1225 1275 12	200 1200 1200 1245 1225 1215 1200 1180 1180 11	45 1156 1161 1179 1185 1120 1186 1154 1164 1164 1164
14 1741 1742 1281 1255 1148 1286 1287 1229 1244 1247 1244 1299 1376	1225 1217 1218 1205 1205 1200 1	1284 1240 1185 1185 1185 1280 1290 1290 1295 12	260 1260 1240 1215 1200 126 1150 1145 1145	06 1150 1105 1106 1001 1100 1100 1100 11
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17 1306 1282 1264 1282 1263 1284 1264 1265 1256 1265 1264 1274 1200	1250 1251 1241 1202 1198 1272 1	1210 1240 1203 1220 1200 1190 1165 1190 11		50 1100 1130 1140 1120 1080 1080 1075 1075 1075 1075
18 1310 1286 1273 1271 1272 1273 1223 1226 1247 1272 1264 1261 1223				
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22 1323 1300 1218 1160 1176 1175 1173 1175 1188 1189 1210 1207 1200	1190 1185 1174 1150 1150 1160 1	1155 1155 1145 1130 1120 1100 1090 1085 10	060 1070 1080 1085 1060 1080 1085 1075 1085 10	25 1040 1030 1048 1043 998 1023 1030 1030 1030 1030 1030
23 1297 1298 1274 1196 1172 1172 1172 1169 1173 1173 1185 1195 1191	1185 1178 1185 1145 1140 1140 1	1140 1140 1130 1125 1120 1105 1085 1070 10	060 1055 1050 1040 1020 1025 1065 1020 995 10	031 1039 1026 1020 988 976 1005 1005 1005 1005 1005 1005
24 1289 1264 1273 1253 1173 1169 1168 1189 1167 1169 1170 1183 1180	1169 1165 1158 1125 1130 1145 1	1125 1145 1140 1130 1120 1090 1085 1045 10	015 1010 995 1033 1020 1050 1055 1011 1023 10	229 1025 1030 990 1013 938 985 983 983 983 983 983
25 1301 1258 1242 1243 1227 1155 1155 1154 1155 1160 1167 1174 1174	1158 1143 1120 1120 1130 1155 11	1140 (135 1145 1140 1105 1064 1083 (091 11	134 1054 1055 1089 1015 1045 1030 1025 1030 10	X48 1039 963 1008 1004 955 980 983 863 983 983 983 983
26 1265 1256 1219 1233 1233 1156 1148 1152 1148 1154 1180 1169 1150	1160 1145 1085 1090 1155 1150 1	1150 1170 1130 1110 1110 1098 1164 1081 11	141 1181 1042 1068 1070 1080 1081 1020 1088 10	40 1085 1056 1004 853 875 955 975 875 975 975 975 975 975
27 1242 1236 1203 1208 1206 1209 1143 1144 1144 1145 1171 1152 1160	1150 1149 1085 1085 1155 1150 1	1160 1140 1145 1150 1100 1173 1154 1101 10	049 1123 1059 1045 1060 1070 1077 1085 1048 10	207 1007 1000 901 926 944 964 965 965 965 965 965 965
28 1267 1254 1217 1196 1168 (190 1194 1144 1139 1141 1146 1151 1150	1150 1148 1138 1145 1150 1140 1	1130 1150 1160 11155 1080 1170 1181 1109 10	048 1070 1061 1019 1049 1060 1063 1059 1058 5	1988 B97 994 925 938 833 935 945 845 945 945 945 945
29 1297 1266 1241 1213 1193 1183 1176 1167 1130 1143 1140 1145 1181	1140 1130 1122 1140 1150 1130 1	1155 1140 1155 1155 1133 1125 1109 1146 10	065 1030 1022 1006 950 1047 1053 1034 996 9	195 1002 925 930 940 934 923 923 923 923 923 923
30 1271 1255 1241 1205 1193 1194 1180 1148 11180 1122 1132 1137 1149	1135 1130 1125 1120 1130 1150 1	1140 1135 1130 1090 1050 1123 1164 1167 11	120 1051 1004 993 1018 1015 1036 1023 994 9	<b>194 931 939 945 938 929 938 913 913 913 913</b> 913
31 1273 1283 1225 1207 1202 1205 1183 1163 1151 1164 1162 1166 (150	1135 1130 1141 1130 1150 1155 1	1125 1120 1120 1105 1050 1000 1143 1161 11	140 1086 1011 981 1006 997 1000 993 986 9	25 825 940 941 935 918 900 693 893 890 690 893
32 1290 1248 1233 1235 1223 1238 1221 1194 1141 1138 1120 1147 (140	1135 1150 1141 1130 1160 1140 1	1115 1110 1090 1075 1025 980 1098 1133 11	116 1092 1002 956 979 1003 992 987 985 5	194 920 936 940 895 909 895 891 891 891 691 891
33 1285 1260 1268 1240 1188 1233 1233 1218 1159 1129 1088 1117 1140	1135 1158 1135 1125 1140 1150 1	1100 1070 1045 1030 990 960 1033 1042 10	057 1083 992 859 984 940 640 881 988 10	02 938 905 935 895 875 865 585 585 685 685 885
34 1292 1247 1233 1198 1107 1184 1177 1164 1160 1123 1092 1095 1168	1155 1165 1140 1110 1120 1100 1	1095 1065 1040 1010 980 950 1024 1024 10	256 1057 983 961 990 989 989 960 998 10	05 958 945 915 906 880 660 876 876 878 876 876
35 1265 1235 1224 1194 1173 1174 1165 1149 1132 1107 1069 1096 1183	1165 1170 1140 1115 1115 1100 1	1090 1060 1035 1000 975 945 1023 1038 10	045 1037 982 951 995 994 972 975 997 s	36 945 943 928 906 893 884 883 883 883 883 883 883
36 1236 1208 1209 1210 1197 1166 1133 1109 1098 1093 1085 1151 1185	1168 1169 1155 1115 1110 1095 1	1080 1055 1035 995 970 950 1014 1018 10	017 978 951 942 950 979 960 970 920 5	115 923 916 B99 891 891 689 B90 890 890 690 890
37 1212 1189 1176 1175 1183 1156 1089 1049 1078 1084 1077 1151 1188	1188 1203 1185 1120 1110 1090 1	1075 1050 1010 985 965 935 986 995 9	990 980 949 941 948 951 910 895 899 6	899 896 891 878 874 885 683 866 885 688 886 886 886
38 1208 1191 1160 1154 1133 1134 1067 1028 1092 1067 1076 1182 1184	1185 1203 1178 1125 1110 1090 1	1075 1040 1000 960 935 980 974 969 9	981 970 956 940 958 953 953 960 905 6	KK5 884 875 675 806 873 670 871 871 671 871 871 871
39 1251 1281 1293 1234 1117 1107 1044 1035 1077 1064 1077 1179 1185	1160 1161 1173 1105 1110 1090 11	1075 1040 985 945 1013 958 994 992 9	<u>983 969 960 941 956 974 906 915 921 6</u>	KO5 856 880 675 871 869 664 855 865 865 665 865
40 1264 1312 1313 1243 1138 1085 1015 1068 1057 1064 1084 1174 1174	1174 1171 1163 1113 1090 1090 11	1070 1035 990 1058 1019 958 935 920 9	900 900 958 935 950 972 875 920 921 5	KU3 889 678 873 869 866 868 866 866 866 866 866 866
41 1289 1271 1322 1224 1098 1041 1022 1089 1033 1047 1090 (168 1168	1164 1185 1166 1109 1090 1090 1	1070 1065 1055 1064 1017 900 960 960 9	965 935 915 885 950 885 850 900 920 E	196 855 869 868 858 858 859 881 881 861 861 861
42 1345 1320 1235 1160 1088 1012 1048 1041 1024 1051 1107 1163 1162	1158 1152 (154 1095 1090 (080 1)	1060 1035 1020 980 940 905 920 970 9	960 935 920 890 900 585 875 890 925 6	10 895 885 870 865 850 840 845 845 845 845 845
43 1395 1311 1259 1124 1075 986 1027 1027 1052 1045 1087 1152 1153	1143 1145 1145 1095 1090 1075 1	1070 1025 990 960 830 910 895 940 9	<u>955 945 925 890 685 905 895 900 665 8</u>	80 855 850 845 840 840 850 855 865 865 865 865
44 1385 1284 1193 1119 1038 980 984 1039 1057 1034 1051 1133 1103	1098 1135 1140 1095 1100 1090 1	1075 1025 980 965 940 925 995 910 9	993 993 991 895 680 865 880 880 952 8	160 868 865 856 850 863 850 940 940 940 940 940 940
45 1357 1282 1186 1124 1057 982 985 1017 1051 1024 1031 1095 1067	1071 1097 1125 1090 1120 1070 1	1075 1050 1050 1000 980 940 920 890 9	958 984 982 946 922 906 897 910 924 8	51 850 859 851 845 875 940 945 945 945 945 945 945
46 1355 1315 1181 1129 1071 984 980 984 1043 1022 1005 1043 1029	1050 1071 1120 1135 1110 1070 1	1045 1040 1040 1020 990 965 920 910 9	940 961 981 979 920 893 888 894 921 8	53 656 658 850 855 885 935 885 885 885 885 885 885
47 1364 1201 1181 1122 1075 985 974 965 1034 1015 990 998 1023	1069 1050 1083 1116 1120 1090 1	1070 1050 1035 1025 1005 975 940 935 9	960 939 958 964 913 871 671 900 923 9	44 859 535 843 870 870 870 890 690 890 890 890
48 1358 1218 1154 1138 1081 999 950 965 989 1018 985 982 997	1013 1048 1061 1109 1095 1100 ti	1060 1060 1040 1030 1020 1010 970 940 9	963 960 940 918 911 860 855 883 855 8	70 895 860 800 675 875 870 880 880 880 880 680
49 1346 1209 1125 1127 1115 1006 908 960 981 1020 983 965 976	1000 1069 1102 1085 1060 1046 1	1070 1050 1040 1030 1030 1015 965 940 9	70 962 954 948 947 939 891 859 810 8	60 690 650 785 650 905 890 670 670 870 870 870 870
50 1323 1212 1125 1098 1091 991 983 954 982 992 974 956 970	984 998 1079 1065 1065 1035 11	1016 1070 1045 1035 1030 1020 965 950 9	<b>284 965 957 953 350 945 927 899 875 7</b>	90 810 800 790 830 870 870 860 860 860 860 860
51 1335 1227 1143 1103 1073 993 971 958 957 972 989 945 947	963 987 1057 1050 1055 1031 10	1037 1080 1060 1055 1040 1020 990 960 9	350 968 959 955 953 949 944 919 896 B	57 549 548 785 520 525 800 570 570 870 870 870 870
52 1313 1237 1151 1110 1079 1006 975 967 967 965 969 940 937	971 987 1048 1040 1045 1050 10	1055 1065 1060 1050 1040 1025 1015 990 8	80 945 968 857 954 952 848 937 903 6	75 853 844 838 852 820 830 850 850 850 850 850
53 1312 1206 1151 1107 1093 1022 987 867 905 977 946 936 928	957 997 994 1033 1005 1020 10	1040 1045 1045 1050 1045 1030 1010 990 9	75 980 940 960 955 956 948 937 910 8	82 863 847 836 780 805 820 830 830 830 830 830
54 1311 1239 1179 1135 1092 1019 987 1012 1187 994 952 937 923	945 981 980 997 877 955 9	995 1015 1025 1045 1055 1040 1020 1005 9	980 985 980 940 958 952 945 938 909 6	86 859 853 770 775 790 810 820 820 820 820 820
55 1293 1234 1184 1142 1105 1021 991 970 1021 952 926 920 921	\$46 \$70 \$6\$ \$78 \$96 1024 1	930 970 995 1005 980 1000 1020 1000 9	860 970 965 950 940 952 946 935 912 B	85 874 800 780 785 750 800 810 810 810 810 810 810
56 1304 1239 1175 1174 1129 1037 970 932 911 913 906 916 928	954 962 956 971 992 1026 10	1032 900 915 910 910 810 1015 1000 9	985 975 970 965 945 935 939 933 911 8	88 815 805 775 760 775 795 805 805 805 805 805
57 1317 1224 1188 1181 1140 1053 959 910 909 907 910 902 914	932 936 945 968 1011 1030 10	1021 1005 1016 1005 680 890 1010 995 9	85 981 996 968 938 938 915 923 902 8	32 810 807 775 758 772 787 796 798 796 796 796 796
58 1292 1227 1206 1178 1142 1058 940 910 908 891 891 901 915	926 939 953 1004 1014 1014 10	1013 1007 1017 1002 1002 870 950 940 8	50 960 950 925 915 890 865 662 847 8	28 813 809 772 756 771 792 798 798 798 798 798 798
59 1256 1222 1210 1193 1145 1046 931 902 898 875 898 918 950	971 987 1008 993 1014 1047 10	1033 1055 1056 1024 1001 1005 920 910 B	10 920 915 900 895 870 855 897 847 8	11 810 803 771 752 769 789 798 798 798 798 798 798 798
60 1277 1212 1198 1165 1130 1062 914 887 882 683 930 944 984	1010 1039 1074 1035 1038 1059 10	1068 1066 1069 1043 1012 990 977 880 B	85 885 880 875 870 845 907 893 855 7	96 808 801 773 756 768 788 798 798 798 798 798 798 798

#### Table 12-7 Bottom Elevation of Model Layer 3



# Table 12-8 Bottom Elevation of Model Layer 4

	<u>1 2 3 4 5 6 7 9 9 10 11 12 13 14 15 16 17 18 79 20 21 22 23 24 25 26 27 28 29</u>	<u>30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48</u>
	11834 1765 1814 1710 1645 1608 1591 1561 1524 1504 1466 1478 1490 1528 1495 1456 1431 1395 1383 1397 1416 1412 1409 1403 1437 1399 1392 1497	1436 1477 1454 1443 1442 1431 1406 1332 1275 1255 1247 1233 1221 1213 1208 1208 1208 1208 1208 1208
	2 1951 1836 1866 1731 1698 1643 1577 1573 1249 1506 1473 1458 1465 1453 1528 1444 1403 1419 1402 1370 1374 1394 1394 1395 1396 1411 1381 1388 1413 1	1452 1455 1433 1424 1407 1383 '349 1323 1320 1315 1280 1243 1229 1219 1217 1217 1217 1217 1217 1217
	3 1879 1825 1768 1699 1857 1666 1576 1548 1523 1505 1473 1455 1443 1483 1460 1327 1372 1375 1397 1372 1352 1365 1366 1375 1365 1384 1375 1384 1370 1366 1403 1	1414 1417 1409 1394 1372 1352 1328 1313 1307 1288 1268 1255 1245 1235 1226 1226 1226 1226 1226 1226 1226 122
	4 1603 1761 1748 1729 1684 1616 1562 1525 1517 1519 1513 1446 1484 1429 1435 1389 1373 1357 1372 1375 1362 1388 1348 1359 1364 1365 1343 1374 1403	1403 1394 1375 1356 1366 1346 1340 1334 1313 1282 1263 1259 1250 1243 1236 1229 1229 1229 1229 1229 1229 1229
	5 1778 1734 1690 1682 1633 1599 1542 1535 1555 1555 1652 1462 1449 1438 1412 1420 1393 1255 1341 1448 1355 1349 1330 1344 1350 1356 1334 1340 1376 1330	1315 1265 1340 1366 1336 1324 1372 1291 1272 1258 1249 1238 1230 1231 1230 1230 1230 1230 1230 1230
	6 1860 1766 1822 1659 1575 *611 1615 1633 1525 1478 1429 1439 1434 1418 1419 1380 1354 1362 1327 1335 1327 1368 1322 1326 1322 1326 1324 1325 1320 1328 1324 1315 1315 1	1250 1275 1367 1350 1329 1309 1297 1266 1269 1258 1250 1240 1235 1220 1200 1200 1200 1200 1200 1200
	7 1885 1808 1784 1824 1591 1545 1618 1512 1444 1428 1417 1418 1411 1420 1404 1371 1357 1342 1326 1309 1309 1304 1320 1304 1313 1324 1330 1250 1255 1	1265 1260 1215 1220 1240 1303 1290 1795 1248 1230 1211 1191 1155 1150 1135 1135 1135 1135 1135 113
	8 1576 1728 1690 1639 1505 1548 1465 1465 1465 1465 1406 1398 1390 1396 1396 1395 1364 1397 1321 1305 1289 1292 1304 1296 1325 1345 1300 1240 1230 1	1210 1190 1200 1200 1210 1220 220 1210 1195 1170 1145 1130 1115 1120 1120 1120 1120 1120 1120 112
0 Feb         0 Feb        0 Feb         0 Feb	9 1551 1578 558 1436 1474 1423 1418 1435 1401 1424 1395 1383 1399 1371 1362 1347 1332 1322 1303 1303 1295 1270 1275 1271 1291 1295 1240 1200 1190 1	1185 1190 1185 1175 1188 1186 1186 1186 1180 1105 1090 1185 1070 1188 1090 1100 1100 1100 1100 1100 110
	*0 1441 1502 1447 1441 1421 1401 1407 1307 1417 1389 1398 1398 1396 1398 1344 1341 1339 1330 1319 1311 1302 1288 1275 1256 1220 1285 1735 1135 1170 1150 1	1160 1160 1173 1160 1130 1143 1120 1261 1265 1060 1055 1070 1050 1090 1075 1075 1075 1075 1075 1075 1075
	111416 1422 (411 1395 1391 1393 1393 1494 1394 1421 1412 1379 1332 1328 1322 1315 1314 1302 230 1265 1276 1270 1215 1160 1180 1180 1180 1165 1170 1145 1	1140 1135 1143 1140 1110 1100 1075 1343 1035 1030 1030 1055 1035 1075 <u>1130 1130 1130 1130 1130 1130</u>
	12 1382 1386 1382 1402 1394 1402 1394 1402 1471 1379 1405 1365 1341 1335 1312 1310 1306 1301 1294 1285 1279 1274 1272 1268 1145 1115 1130 1155 1160 1155 1125 11	1125 1165 1113 1090 1055 1643 1025 1000 1005 1015 10 <u>05 1080 1080 1090 1100 1100 1100 1100 1100</u>
	13 1348 1328 1340 1353 1341 1399 1394 1389 1355 1331 1325 1325 1317 1312 1366 1297 1287 1277 1271 1264 1258 1185 1130 1090 1120 1140 1140 1140 1130	1025 1075 1060 1000 1000 1000 995 1020 1075 1060 1075 1070 1000 1100 1100 1100 1100 110
	14 1321 1323 1361 1339 1328 1369 1363 1319 1324 1327 1324 1327 1324 1319 1309 1305 1297 1292 1285 1275 1270 1264 1220 1160 1155 1155 1150 1100 1055 1110 1105 1	1075 1050 1025 980 970 970 990 1075 1060 1035 1029 1035 1030 1035 1035 1035 1035 1035 1035
Image: Norm         Image: Norm        Norm        Norm       Norm	15 1259 1294 1288 1287 1295 289 1270 1283 1371 1320 1317 1312 1297 1288 1287 1296 1281 1360 135 1150 1085 1375 1055 1050 1353	1035 1020 980 970 SE0 1010 1040 1060 1060 1060 1060 1060 106
Prime         Prim<         Prim         Prim<         Prim<	16 1287 1277 1272 1271 1275 1272 1268 1269 1293 1139 1145 1134 1120 1111 1110 1105 1170 1165 1261 1254 1160 1135 1105 1055 1050 1345 1055 1050 1345	98C 985 983 96D 560 933 1015 1030 1040 1040 1040 00 933 980 970 970 970 970 970 970 970
N = 0.00	*71288 1272 1264 1262 1265 1264 1265 1264 1265 1106 1133 1134 1124 1110 1106 1101 1001 1150 1125 1252 1125 1130 1120 1100 1060 1020 1025 1045 1040 1000	93D 980 975 96D 940 953 960 990 1000 990 1000 980 975 860 980 980 980 980 980
1 000        000        000        000        000	18 1230 1265 1253 1251 1252 1255 1273 1076 1097 1122 1114 1111 1075 1075 1075 1075 1130 1115 1110 1110 1105 1095 1080 1040 1020 1025 1000 980 985	985 975 965 955 930 930 935 945 950 970 965 880 975 855 955 955 955 955 955 955 955
b) b) c) c         c) c	19 1302 1266 1246 1239 1239 1239 1239 1238 1060 1365 001 1100 1097 1092 1040 1040 1040 1040 1155 1120 1110 1105 1100 1056 1056 1056 1050 1056 1050 1055 1050 1055 1050 1055	975 975 965 96D 935 935 940 940 940 955 965 970 965 950 940 940 940 940 940 940
1 bit	20 1305 1283 1240 1228 1245 1048 1048 1048 1055 1077 1087 1088 1079 1050 1056 1061 1145 1115 1030 1060 1065 1050 1050 1020 930 970 995 1005 1000 990	980 970 965 960 940 935 925 950 940 950 945 955 960 945 925 925 925 925 925 925
20         20         000        000        000        000        000        000        000         000	21 1309 1273 1055 1036 1334 1037 1035 1042 1054 1051 1067 1077 1050 1055 1065 1045 1135 1165 1065 1055 1055 1055 1055 1055 105	975 960 955 960 945 948 935 933 925 940 926 990 926 925 960 960 960 960 960 960
1000         1000        10000        1000        1000        10	22 1303 1280 1058 1020 1025 1025 1025 1025 1025 1025 1025	9a0 980 955 950 945 935 930 910 930 935 930 910 945 945 945 945 945 945
1 - 2 - 1 - 2 - 1 - 2 - 2 - 2 - 2 - 2 -	23 1277 1276 1254 1246 1222 1222 1222 1222 1222 1222 1232 123	975 985 945 940 930 925 930 910 920 935 950 910 895 910 920 920 920 920 920 920 920
2         2        2         2         2         2	24 1269 1244 1253 1233 1233 1233 1019 1019 1019 1019 1017 1019 1020 1033 1036 1019 1115 1000 1045 1042 1045 1015 1000 1985 980 970 950 940 950 955	970 SE0 943 935 520 900 935 920 905 925 905 930 945 910 665 900 690 690 690 690 690 690
1 (2)         1 (2) <th< td=""><td>25 1281 1233 222 1223 1207 1005 1005 1005 1005 1005 1005 1007 1024 1024 1024 1006 993 1065 1045 1045 1045 1060 1035 935 1005 935 985 975 975 970 1070 985</td><td>930 1005 930 935 930 92C 920 920 935 890 915 970 650 670 665 665 665 665 665 665</td></th<>	25 1281 1233 222 1223 1207 1005 1005 1005 1005 1005 1005 1007 1024 1024 1024 1006 993 1065 1045 1045 1045 1060 1035 935 1005 935 985 975 975 970 1070 985	930 1005 930 935 930 92C 920 920 935 890 915 970 650 670 665 665 665 665 665 665
21         22         15         156         156         156         150        150        150        150        150        150      <	26 1245 1235 1195 1213 1213 1005 996 1002 998 1004 1010 1009 1000 1010 995 1055 1025 1080 1070 1085 1035 590 970 990 585 1065 960 1080 1190	965 960 945 955 950 92C 960 945 970 990 690 850 860 860 8645 845 845 845 845
2         2         1	27 1222 1213 1188 1198 1198 1189 933 934 934 935 1021 1002 1010 1000 993 1025 1025 1025 1025 1045 1075 1045 1010 1000 970 1080 1055 930 960 1080	995 930 945 950 960 960 960 960 900 930 875 855 830 640 845 640 840 840 840 840
2         2         1        1        1        1         1	28 1247 1234 1197 1176 1176 1176 1170 1174 994 989 991 595 1001 1000 1000 598 986 1100 1100 1000 1005 1030 1015 993 940 1025 1065 1000 960 1010	995 930 940 950 960 950 935 865 865 865 820 820 820 825 835 835 835 835 835 835
0 20 1 202 1 201         1 102	23 1277 1246 1221 1133 1173 1163 1156 1147 560 933 393 935 1011 930 960 977 1070 1050 1070 1055 1015 1010 955 1030 1020 1075 1050 1010 960	950 925 900 925 335 905 845 860 870 860 815 830 830 820 805 805 805 805 805 805
1 252         1 264         1 265         1 164 <th< td=""><td>30 1251 1235 1221 1185 1173 1174 1156 1122 1140 972 982 997 999 985 980 975 1065 1065 1065 1065 1060 990 985 980 980 1020 1020 1075 1085 1060 990</td><td>930 910 935 895 905 880 845 850 825 815 820 820 805 810 780 780 780 780 780 780</td></th<>	30 1251 1235 1221 1185 1173 1174 1156 1122 1140 972 982 997 999 985 980 975 1065 1065 1065 1065 1060 990 985 980 980 1020 1020 1075 1085 1060 990	930 910 935 895 905 880 845 850 825 815 820 820 805 810 780 780 780 780 780 780
c         c        c        c        c        c        c       <	31 1253 1243 1265 1167 1182 1185 1163 1163 1164 1131 1144 1142 1146 1303 985 980 1115 1085 1010 1015 1033 1020 990 965 945 915 1050 1090 1090 1040	940 895 930 930 910 875 855 820 820 815 805 800 785 760 770 770 770 770 770 770
a) rest         rigs         rigs        rigs        rigs <t< td=""><td>32 1270 1228 1213 1215 1203 1218 1201 1174 1121 1118 1100 1127 993 985 1125 1100 1000 1010 990 1010 996 960 985 960 935 900 995 1050 1065 1050</td><td>930 860 660 890 875 665 855 860 815 810 810 785 780 740 755 755 755 755 755 755 755</td></t<>	32 1270 1228 1213 1215 1203 1218 1201 1174 1121 1118 1100 1127 993 985 1125 1100 1000 1010 990 1010 996 960 985 960 935 900 995 1050 1065 1050	930 860 660 890 875 665 855 860 815 810 810 785 780 740 755 755 755 755 755 755 755
44         127         127         127         117         1144         1142         113         1147         1144         115<	33 1265 1240 1248 1220 1166 1213 1213 1213 1139 1139 1139 1109 1068 1097 900 965 1130 1095 1045 1005 1000 995 995 996 960 965 925 865 915 935 965 165 165	880 825 660 860 985 850 860 875 840 825 825 790 775 760 750 750 750 750 750 750 750 750
21         21         11/2         11/	34 1272 1227 1213 1178 1147 1164 1157 1*44 1140 1103 1072 1075 1162 1142 1135 1090 1025 1005 980 980 970 965 945 915 880 91C 915 985 1015	850 820 860 910 890 850 865 865 830 810 780 780 770 755 745 745 745 745 745
err         fib         fib <td>35 1245 1215 1204 1174 1153 1154 1145 1129 1112 1087 1269 1076 1174 1145 1130 1060 1020 1010 960 970 955 945 935 915 935 915 935 935 935 935 935 935</td> <td>870 820 925 925 960 850 870 815 820 830 810 790 770 755 755 755 755 755 755</td>	35 1245 1215 1204 1174 1153 1154 1145 1129 1112 1087 1269 1076 1174 1145 1130 1060 1020 1010 960 970 955 945 935 915 935 915 935 935 935 935 935 935	870 820 925 925 960 850 870 815 820 830 810 790 770 755 755 755 755 755 755
31          31         31	36 1216 1188 1182 1190 1177 1145 1113 1128 1073 1073 1075 1131 1173 1150 1133 1070 1020 1005 975 965 940 940 925 910 890 905 920 940 940 905	850 840 865 870 825 835 830 780 820 815 790 775 785 770 765 765 765 765 765 765 765
1 her         1 her <th< td=""><td>37 1192 1159 1155 1155 1155 1143 1135 1069 1029 1059 1054 1057 1131 1170 1155 1140 1095 1025 1005 975 955 940 905 900 890 880 8875 895 910 910</td><td>840 855 840 830 825 815 855 805 795 790 780 780 790 805 825 825 825 825 825 825</td></th<>	37 1192 1159 1155 1155 1155 1143 1135 1069 1029 1059 1054 1057 1131 1170 1155 1140 1095 1025 1005 975 955 940 905 900 890 880 8875 895 910 910	840 855 840 830 825 815 855 805 795 790 780 780 790 805 825 825 825 825 825 825
31         121         1221         1224         1027         1026        1026        1026	38 1188 1*71 1160 1134 1113 1114 1047 1006 1072 1047 1056 1173 1169 1165 1175 1085 1030 1005 975 955 975 890 855 860 880 870 905 910 855	855 860 825 850 840 830 815 810 730 780 770 770 780 810 810 810 810 810 810 810 810
0         1	39 1241 1227 1273 1224 1097 1087 1024 1015 1057 1044 1057 1166 1166 1166 1166 1169 1090 1020 1005 375 950 970 880 655 890 870 925 920 915 900	880 860 875 S05 875 860 800 780 770 770 765 770 780 780 795 795 795 795 795 795
1         1	40 1244 1292 1293 1223 1118 1265 595 1048 1037 1044 1264 1160 1155 1155 1122 1080 1015 980 970 950 915 870 930 895 835 885 875 875 875 870	870 835 835 855 785 810 810 793 780 770 785 770 785 750 735 735 735 735 735 735 735
2         3         1	41 1269 1281 1302 1204 1076 1021 1002 1046 1013 1027 1010 1151 1151 1151 1125 1075 1020 980 975 950 950 950 950 950 895 815 660 880 870 850	835 805 820 785 740 780 910 780 160 760 760 750 790 750 720 720 720 720 720 720 720 720
43         137         1124        112	42 1325 1300 1215 1140 1066 592 1028 1021 1004 1031 1387 1152 1145 1140 1133 1070 1310 980 960 940 920 515 675 840 805 725 870 860 805	785 765 795 780 750 740 780 775 795 790 775 796 797 775 760 795 755 730 730 730 730 730 730
44         164         102         102         101         103         113         113         103	43 1376 1291 1237 1104 1055 565 1007 1007 1007 102 1025 1067 1146 1147 1135 1134 1090 1000 975 955 950 905 870 840 820 790 770 835 870 840	835 745 730 740 735 755 755 795 835 780 750 755 790 800 755 755 755 755 755 755
c 5         135         126         1166         1104         1037         192         166         1104         1037         192         196         190        190        190         190<	44 1365 1264 1173 1099 1018 963 964 1019 1037 1014 1031 1113 1039 1093 1129 1115 1015 960 970 950 905 860 850 825 795 776 8:0 870 870	855 785 750 745 750 775 830 910 780 770 755 770 615 813 780 760 760 780 780 780
66         133         1135         1115         1105         1014         1105         1014         1105         1014        101	45 1337 1282 1166 1104 1027 562 565 997 1031 1004 1011 1075 1047 1066 1067 1110 1030 990 960 955 935 925 660 855 810 750 750 825 865	eso eoo 760 740 730 755 eos e10 175 755 770 790 e23 e23 795 795 795 795 795 795
17       144       144       141       1161       1122       1055       955       554       957 <th< td=""><td>4e 1335 1295 1171 1125 1051 364 550 964 1023 1002 965 1023 1009 1030 1066 1105 1095 970 935 910 900 500 880 855 825 755 810 810 850</td><td>eas and 7as 7as 7as 7ac 740 7as add 7as 7ad 600 7as 8ad 7as 8ad 8ad 8ad 8ad 8ad 8ad 8ad 8ad 8ad 8ad</td></th<>	4e 1335 1295 1171 1125 1051 364 550 964 1023 1002 965 1023 1009 1030 1066 1105 1095 970 935 910 900 500 880 855 825 755 810 810 850	eas and 7as 7as 7as 7ac 740 7as add 7as 7ad 600 7as 8ad 7as 8ad
46       13.4       11.6       10.1       17.2       9.40       9.45       9.62       9.72       9.93       10.41       10.66       10.9       9.03       9.01       10.5       9.75       8.75       8.75       7.55      7.55      7.55      7.55 <th< td=""><td>47 1344 1241 1161 1102 1055 965 954 945 1014 995 970 978 1003 1064 1045 1072 1095 1000 958 920 905 865 675 860 830 820 845 850 830</td><td>870 890 835 750 710 740 780 825 770 810 820 820 823 813 804 804 804 804 804</td></th<>	47 1344 1241 1161 1102 1055 965 954 945 1014 995 970 978 1003 1064 1045 1072 1095 1000 958 920 905 865 675 860 830 820 845 850 830	870 890 835 750 710 740 780 825 770 810 820 820 823 813 804 804 804 804 804
q         1105         11	49 113/8 113/8 113/8 113/8 111/2 1061 979 940 945 569 936 965 952 977 993 1041 1068 1090 1015 960 933 935 875 875 870 865 EC 865 870 865	eso eso eso eso 775 765 755 750 740 755 755 899 eso eso eso 785 775 775 775 775 775
50       103       107       971       563       934       962       972       934       936       930       93	49 1326 1*69 1105 1107 1025 986 948 940 961 1000 963 945 955 980 1064 1090 1060 968 920 900 895 885 885 885 880 875 900 850	875 875 860 875 815 775 775 770 740 710 689 755 820 800 770 768 765 765 765 765
51       1315       1207       1123       1023       <	50 1333 1 92 1105 1078 1071 971 563 934 562 972 954 936 955 954 978 1060 1035 1015 572 926 930 330 930 930 930 930 805 835 835 920 855	890 885 885 880 860 830 800 765 775 760 715 745 770 790 770 765 765 765 765 765 765
62       1233       1217       1131       1090       1059       926       955       947       947       947       947       947       947       947       102       110       102       105       105       920       920       920       920       920       925       955       940       850       930       850       830       830       830       830       830       830       830       830       830       930       955       940       955       950       900       905       855       840       875       843       805       700       770       768       768       800       810       <	51 1315 1207 1123 1083 1083 973 951 938 537 952 949 925 927 943 667 1041 1030 1015 981 967 955 925 925 920 910 910 905 900 900 905	895 890 885 880 855 880 855 880 765 775 775 758 794 792 780 850 850 850 850 850 850 850
53         1292         1166         1131         1007         1003         1007         1003         1007         1003         1007         1003         926         916         908         987         977         974         1020         963         985         990         900         905         895         900         900         905         895         900         900         905         895         900         900         905         895         900         900         905         895         900         900         905         895         900         900         905         895         900         900         905         900         900         905         895         900         900         905         895         900        900        900 <th< td=""><td>52 1293 1217 1131 1090 1059 385 555 947 947 945 349 920 317 851 967 1026 1024 1015 595 975 950 330 915 910 310 915 920 920 905</td><td>905 895 890 800 885 A75 A35 805 7AD 775 763 785 815 810 830 830 830 830 830 830</td></th<>	52 1293 1217 1131 1090 1059 385 555 947 947 945 349 920 317 851 967 1026 1024 1015 595 975 950 330 915 910 310 915 920 920 905	905 895 890 800 885 A75 A35 805 7AD 775 763 785 815 810 830 830 830 830 830 830
54 1291 1219 1154 1155 1072 39 667 92 1167 974 932 917 903 925 961 960 977 939 926 95 946 955 945 925 956 945 956 945 956 945 940 940 845 849 840 840 840 844 844 844 844 844 844 844	53 1292 1186 1131 1087 1073 1002 567 947 545 957 926 916 908 937 977 974 1020 963 585 950 945 930 920 908 855 690 900 905	895 900 900 695 885 875 645 815 800 773 768 700 785 800 810 810 810 810 810
51       1273       1214       1164       1122       1065       1301       920       900       900       920       900       900       900       900       910       910       910       910       910       910       910       910       910       910       910       910       910       910       910       910       910       910       920      <	54 1291 1219 1154 1115 1072 399 507 932 1167 974 332 917 303 925 361 960 577 939 936 955 945 925 936 935 310 850 885 865	905 905 905 900 898 890 660 816 603 790 750 755 770 790 800 800 800 800 800 800
b6       1284       1100       1017       950       912       891       893       886       804       942       913       914       913       944       914 <th< td=""><td>55 1273 1214 1164 1122 1085 1307 971 950 1001 932 906 900 90: 926 950 949 958 976 1004 915 925 910 855 855 875 800 870 890</td><td>915 920 925 920 903 886 655 823 820 780 760 745 760 780 750 790 790 790 790 790 790 790</td></th<>	55 1273 1214 1164 1122 1085 1307 971 950 1001 932 906 900 90: 926 950 949 958 976 1004 915 925 910 855 855 875 800 870 890	915 920 925 920 903 886 655 823 820 780 760 745 760 780 750 790 790 790 790 790 790 790
57 1201 1204 1168 1161 1120 1033 532 650 862 667 833 652 867 833 652 867 833 652 87 833 652 87 833 652 87 833 652 84 912 915 925 944 925 944 925 944 925 946 925 945 925 985 830 830 830 850 850 927 907 912 694 872 601 812 726 787 72 78 78 72 78 776 776 776 776 776 776 776 776 776	56 1294 1210 1156 1154 1109 1017 950 912 891 893 886 896 906 934 942 936 951 972 1008 1012 875 865 E4C 825 825 810 835 875 894	919 929 919 914 899 889 6cc 840 795 785 755 740 755 775 785 785 785 785 785 785 785 785
58 1272 1202 1186 1158 1122 1038 520 850 888 871 871 871 881 805 506 919 933 544 954 993 997 997 992 982 824 834 844 864 864 864 864 864 864 864 864 86	57 1293 1284 083 830 830 830 830 830 830 830 830 831 831 831 831 831 831 831 831 831 831	925 927 907 912 894 873 661 812 73C 787 755 738 752 787 775 776 776 776 776 776 776
59 1246 11202 1193 1173 1125 1226 911 882 873 655 818 896 930 851 967 986 933 94 1027 1013 1035 1035 1035 1035 1035 1035 827 824 834 844 844 845 855 887 873 827 791 750 783 757 732 749 769 781 778 778 778 778 778 778 778 778 778	58 1272 1207 1186 1158 1102 1238 320 830 888 871 871 881 835 536 313 384 934 594 933 937 997 992 982 824 834 844 864 864	884 864 864 864 864 844 857 827 808 793 789 752 736 751 772 778 778 778 778 778 778
60 1257 1192 1178 1146 1110 1042 894 667 842 663 910 924 964 990 1019 1054 1015 1018 1009 1048 1066 1049 1023 992 970 957 624 834 844 844 844 844 845 635 887 873 635 776 768 781 753 736 748 768 778 778 778 778 778	59 1246 1202 1190 1173 1125 1226 911 882 973 855 978 898 900 951 967 996 973 994 1027 1119 1035 1035 1005 1005 881 985 824 884 844 864	864 864 864 864 844 840 877 E27 791 790 783 751 732 749 769 778 778 778 778 778 778 778
	50 1257 1192 1178 114E 1110 1342 894 ECT 842 E53 910 924 964 990 1019 1054 1015 1018 1039 1048 1065 1049 1023 992 970 957 824 834 844	844 844 845 835 837 873 835 776 788 781 753 736 748 768 778 778 778 778 778 778 778 778

# Table 12-9 Bottom Elevation of Model Layer 5

1 2	3	4	5 6		7 в		, •o	<u>, 11</u>	12	13	14	15	•6	17	18	19	20	21	<b>2</b> 2	23	24	25	25	27	29	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	_47	<u></u>
1 1824 1775	1804	:700 163	5 1598	1561	1551	1514	1494	1476	1466	1480	1518 1	485 14	46 14	16 14	121 1	365 1	373	1387	1406	1432	1399	1393	1427	1389	1382	1409	1426	1467	1444	1433	1432	1421	1396	1322	1265	1245	1237	1223	1211	1203	1198	1193	:198 1	-9B	1198
2 1941 11826	1856	:721 168	6 1633	1587	1563	1539	1496	1463	1448	1456	1483 11	516 14	34 113	93 IT4	139 1	397 1	360	1364	1384	1384	1385	1385	1401	1371	1378	1403	1442	1445	1423	1414	1397	1373	1339	1313	13:0	1305	1270	1233	1219	1203	1207	1207	1287 1	207	1201
3 1659 1615	1758	1689 164	7 1595	1566	1536	1513	1495	1463	1445	1433	1473 1	450 13	87 130	12 pa	156 1	387 1	362	1342	1355	1358	1365	1375	1374	1350	1376	1393	1404	1407	1399	1364	1362	1342	1318	1303	1297	1278	1258	1245	1235	1225	1216	1216	1216 1	216	1210
4 1793 1771	1738	17-9 167	4 1505	1552	1515	1507	1509	1503	143E	1404	1419 1	425 13	79 13	13 112	147 1.	382 1	Je B	1352	1328	1338	1349	1324	1355	1333	1364	1390	1393	1384	1366	1348	1336	1330	1324	1303	1272	1239	1249	1243	1233	1226	1219	1219	1213 11	219	1235
5 1768 1724	16EU	1672 162	0 1089	1032	1525	1545	1092	1902	14.39	1428	1462 11	enti na 600 ko	70 1 2	40 µ 2 14   12	131 1	338 1	242	12.59	1323	1014	1340	1343	1330	1330	1305	13/05	1295	1275	1330	1358	1325	1314	1067	1281	*262	1245	1239	1225	1220	1221	11220	1223	1220 11	220	1220
5 1640 1730	1012	100	0 100-	10.60	10219	1010	1400	1419	1429	1424	1400 1			17 12	172 1	317 1	320	1017	1204	1010	1004	1202	1010	1334	1300	1005	1250	1205	1207	1340	1019	1239	1207	1270	200	1249	1176	1230	1123	1213	1190	1705	1000	LEGN	100
7 1073 1798	1774	1044 138	1 1000	1008	1.160	14.14	1418	1908	1404	1908	1410.1	334 13 272 42	40 112	0 12	152 1	211 1	239	1299	1294	1054	1006	1215	1075	1000	1210	1200	1100	1107	1100	1100	1233	1290	1100	1497	1200	11215	1110	1//05	1075	1060	1095	1095	1040 1	Data I	103
51000 THE	1660	AB9 133	a 1338 4 1417	1437	1450	1201	1414	1006	1272	1000	1361 1	282 42 282 42	43 15. 07 19	22 12	110 1	300 1	230	1279	1260	1254	12.66	1291	1295	1220	1170	1155	1150	115/1	1145	1125	1125	1115	1/10.5	100	1055	1242	1040	1125	1075	1/145	1010	1040	1010 1	040	1:0:0
10 1421 1202	1,748	400 14,	1 1905	1.400	1920	1407	1970	1000	1074	1940	1324 1	224 +2	00 112	20 12	200 1	201 1	230	+170	1265	1203	1210	1275	1005	1105	115/1	1105	1120	1115	1155	1110	1787	1060	1055	1000	1025	1202	0.00	1020	1005	1015	0.05	394	0.0	395	601
11 1458 11452	1407	1995 199 1995 199	1 1383	1.384	1904	1984	1411	1202	2369	1922	1339 1	212 43	06 13(	M 12	222 1	260 1	275	1270	1260	1205	1150	1127	1170	1155	1167	1115	1035	1085	1090	1000	1061	1030	1015	095	970	361	950	375	1025	395	1045	1045	1045 11	545	104
12 1372 1375	1372	1342 139	4 1392	7461	1368	1395	1355	1333	2326	1302	1300 1	296 112	91 12	24 19	275 1	265 1	264	t260	1258	1135	1105	1120	1145	1150	1145	1105	2075	1055	1050	1035	1000	98D	965	935	935	343	950	1000	1005	1020	1010	1010	1010 1	010	2010
13 1335 1318	1330	1354 133	1 1382	1384	1379	1.340	1321	1315	1315	1307	1392 1	206 12	17 12	17 12	267 1	261 1	254	124R	1175	1120	1080	1000	1110	1130	1130	1095	1045	1025	1005	975	350	94D	935	925	950	360	995	295	990	1015	1020	1020	1020 1	020	1:02
14 1311 1313	1551	1326 131	8 1250	1353	1309	1214	1917	1314	+ 9.70	1200	1795 1	287 17	92 12	25 112	¥5 1	260 1	254	210	1150	1 145	1125	1000	1090	1085	1/08/0	1055	1020	995	470	920	310	405	920	1005	990	965	980	1025	980	1000	965	265	965	965	392
15 1289 1284	1278	1277 128	5 1279	1269	1273	1501	1310	1307	1302	1287	1278 1	271 12	70 12	55 12	YED 1	255 1	250	1205	1150	1125	1120	1075	1055	1035	1010	995	590	965	920	910	315	945	970	990	990	1000	990	970	935	355	890	890	890	890	89
16 1277 1267	1262	1261 126	5 1262	1258	12.59	1283	1129	1135	:124	1:10	1 1 1 1	107 10	25 111		55 1	251 1	244	1150	1125	1045	:035	1020	995	1005	995	975	925	925	920	895	895	920	945	960	970	970	970	940	920	910	900	500	930	900	900
17 1278 1262	1254	1252 1125	5 1254	1254	1255	1096	1123	1124	1114	1103	1096 1	391 10	1111	20 11		242 11	105	0111	1090	1060	1010	970	970	1000	365	945	930	920	915	895	875	690	890	920	930	92:3	93D	910	905	910	910	910	910	910	31
18 1280 1256	1243	1241 124	2 1245	1053	1DEE	1087	1112	1104	1:101	1065	1055 1	065 10	55 10	55 10	45 1	070 11	¢75 i	1065	1050	1030	985	265	970	945	925	925	925	915	900	890	96C	860	865	875	650	900	895	910	905	865	895	865	895	885	85
19 1292 1256	1235	1229 122	9 1223	1050	1055	1071	1030	1087	1072	1030	1 030	030 11	45 10	55 10	50 II	060 1	C55 1	1045	1005	935	985	970	940	945	340	930	G15	910	900	895	865	865	870	870	870	885	895	900	835	863	870	870	870	870	87
20 1295 1259	1230	1216 103	5 1038	1:039	1D46	1061	1077	1078	:059	1040	1058 1	057 21	35 10	35 10	335 1	030 1	C15	1000	395	960	930	910	930	940	935	925	G15	905	900	890	970	665	855	890	870	983	875	885	890	875	855	855	855	BS5	85.
21 299 1263	1045	1026 102	4 1027	1025	1032	1044	1041	1577	:057	1050	1045 1	035 71	25 10	35 10	30 1	005	990	955	950	925	910	895	900	905	910	915	910	895	695	890	875	870	865	B60	855	870	850	820	850	855	890	990	890	esc	89
22 293 1270	1058	1020 101	6 1015	:013	1015	1025	1029	1050	:047	1040	1030	025 11	20 10	10 10	15	995	975	955	935	920	905	985	690	890	985	905	9:0	910	895	9E0	875	BC5	860	E40	850	865	650	940	815	860	875	975	875	875	67
23 1267 1266	1244	1036 101	2 1012	1012	1009	1013	1013	1025	1035	1033	1025 1	135 3.1	10	10 9	995 :	960	985	940	915	915	905	895	875	865	875	835	905	915	B75	870	960	850	825	835	845	860	875	835	625	840	850	850	850	650	85
24 1259 1234	1243	1223 101	3 1009	:008	1009	1007	1039	1010	1023	1026	1009 1	:05 0	80 10	15 9	ao	960	950	930	925	91D	910	903	680	870	863	B35	900 S	910	870	860	B45	82 <b>0</b>	825	825	640	620	855	930	785	820	610	U1C	610	810	81
25 1271 122B	1212	12*3 119	7 995	995	594	995	000	1007	1014	1014	998	983 10	55 99	95 9	980 :	995	970	920	925	920	915	905	900	900	1000	915	S10	935	B£0	860	855	B40	840	840	650	605	830	785	750	760	775	775	775	775	77
25 235 1226	1189	1203 120	3 995	568	992	368	994	1020	999	99 <b>C</b>	1000	985 (†0	25 9	15 10	120 1	005	995	960	910	830	915	910	995	8E5	1005	1055	890	630	875	885	680	845	885	865	662	900	600	760	770	765	750 (	750	750	750	75
27 22 1200	1173	1178 117	6 1279	583	994	984	985	1011	992	1000	990	989 110	12 9:	50 10	X4D 1	020 1	DO2	970	930	920	890	1503	975	910	983	1000	915	850	870	885	690	890	885	620	850	790	765	740	745	745	740	740	740	740	74
29 1237 1224	1167	:166 115	8 1160	1164	984	э7э	991	986	991	990	990	988 9	76 10	13 10	35 1	aca [	935	950	935	91D	850	995	985	920	BOD	930	915	650	850	875	685	680	865	790	820	785	735	730	720	720	730	730	730	730	73
29 1267 1236	1211	:163 115	3 1753	1145	1137	970	983	980	965	1601	960	97C 9	62 I C	10 10	025 1	303	985	940	930	915	950	935	990	965	925	875	865	643	620	845	855	830	770	780	790	770	720	730	725	715	700	700	700	700	70
33 1241 1225	1211	175 115	3 1:64	1155	1118	1135	962	972	977	989	975	970 9	65 10	); DC	000	985	970	945	910	935	865	935	990	1000	975	905	845	825	855	815	620	796	765	770	740	730	730	720	705	710	660	680	680	68D	-68
31 243 1233	1195	1177 117	2 1175	1153	1133	1:2:	1134	1132	113€	95D	975	970 10	6 <b>0 1</b> 10	15 9	40	945	955	940	910	650	960	Bab	955	995	1000	950	850	81C	655	8)0	620	790	775	735	735	725	715	700	685	665	£90	690	690	6.9D	69
32 250 1218	1203	1205 119	3 1208	1191	1164	1:13	1108	1090	1117	980	975 1	105 10	40 110	10 8	35	915	93D	930	200	875	850	E15	905	960	975	950	840	775	008	820	790	790	775	770	725	72¢	715 :	695	680	640	655 :	655	655	655	€5
33 255 1230	1239	1210 115	6 1203	12Q.s	1188	1729	1099	1058	1087	980	975 1	070 10	25 91	10 9	125	920	915	910	895	630	840	795	825	845	895	945	790	735	775	760	795	760	773	785	745	725	725	710	675	655	645	645	645	645	64
34 252 1217	1203	1168 113	7 1154	1147	1134	1:32	1093	1062	1065	1149	1117 1	055 10	15 9	<u>15 a</u>	925	203	B95	865	893	855	825	790	820	825	695	925	770	730	770	A20	79C	750	765	765	730	705	6BQ -	1 700	670	645	635	635	635	635	63
35 235 1205	1194	1164 114	3 1144	1135	1119	1102	1077	1059	1065	1155	1075 1	060 9	BO 9	4G S	30	903	685	870	BEC	645	825	795	625	845	685	R95	785	735	835	825	780	750	765	710	715	725	765	685	665	645	645	645	645	645	64
36 20€ 1176	1179	1160 116	7 1136	1103	1079	1DEB	1063	1055	1121	1150	1060 1	060 9	90 9	4G S	iZ5	690	690	855	855	840	825	605	820	835	855	825	770	760	790	775	730	745	733	675	715	710	680	665	675	660	650	650	650	65D	65
37 182 1159	1146	1145 113	3 1126	1059	1019	1046	1054	1D47	1121	1140	1095 1	070 10	15 9	45 8	25	893	870	855	820	8*5	805	795	790	810	830	835	770	785	770	760	785	730	755	730	690	680	670	670	680	698	7:0	710	710	71D	11
39 178 1161	1150	1124 110	3 1104	1037	538	1062	1037	1D46	1150	1130	1105 1	090 10	05 9.	50 S	25	890	870	840	805	790	775	795	785	825	Rac	875	795	798	755	780	750	735	715	705	6BC	670	660	660	663	665	695	695	695	595	69
39 1231 1251	1283	1204 108	7 1077	1014	1002	1047	1034	1047	1135	1130	1105 1	020 10	10 94	40 S	125	895	870	840	800	050	810	7.96	893	705	830	5/3	800	785	785	790	766	760	595	675	605	560	603	033	653	525	620	680	CEU I	500	50
40 234 1282	1283	1213 110	8 1025	385	1038	1027	1034	1054	1130	1115	1110 1	055 10	05 9.	5 S	100	990	870	835	790	850	815	705	805	795	790	7.40	790	72.5	740	740	640	620	710	630	6/5	600	603	035	676	535	620	525	620	5/16	50
41 1259 1241	1292	1194 TD5	E 1111	392	1038	1003	1017	1020	1127	1110	1100	010 020	00 94	+3 S	103	900	870	950	676	005	710	733	705	ano	730	775	705	725 805	733	700	620	690	723	695	TIVE	ECD.	670	530	680	542	616	515	615	515	100
42 .3.0 1290	1200	1004 104	C 962	507	0.1	1000	1021	1000	1122	1127	1035 1		20 0	+J 3	210	407	010	930	040	775	765	705	706	720	900	770	715	675	033	670	660	675	675	210	71.6	EGR	6.45	ESE	675	595	640	EAD	640	540	EA
43 - 306 1281	1769	1089 109	- 950 9 080	397	1020	1022	1004	1021	1102	1096	1/182	014 10	5/1 0	ra 2 10 6	120	910	BOD -	945	800	730	765	735	7.05	745	815	815	790	720	685	678	692	705	755	725	690	670	650	562	7.05	732	670	570	670	57D	67
44 3:05 1254	1.56	1004 100	a 350 7 080	365	GA7	1021	504	1001	1065	1037	1056 1	067 10	50 0		335	925	800	940 880	870	1125	800	750	730	730	765	815	795	735	625	675	665	695	735	730	665	655	665	685	740	743	695	685	665	685	ι ε <sub>B</sub>
45 2325 1995	1261	1099 102	1 954	351	954	1013	592	975	1013	990	1020 1	D*5 10	50 10	50 A	125	890	HE5	850	H5C	830	805	775	745	755	725	795	825	820	720	670	655	675	715	720	705	540	695	597	750	753	740	740	740	740	74
47 334 1231	1153	1092 104	F 955	044	935	1004	GRE	960	968	993	1054 1	105 10	22 10	15 9	150	910	RHD	865	845	BSD	815	785	775	800	805	780	815	835	780	700	650	675	710	745	6BO	710	715	710	740	783	725	725	725	725	72
48 2328 1198	1124	1106 105	1 969	931	935	950	98	955	952	967	963 1	031 10	30 110	15 9	150	980	BHD	865	835	835	830	825	620	825	830	620	805	780	780	720	705	690	680	66D	650	655	620	710	710	715	655	700	100	100	70
49 1316 1174	1095	1097 109	5 976	938	930	351	Gan	953	935	945	970 1	054 10	56 110		130	309	875	845	850	845	845	845	840	835	RED	650	835	830	835	825	763	710	700	685	640	505	610	£45	700	590	670	690	690	650	69
50 0298 1182	1095	1068 106	1 961	953	974	952	962	944	926	940	954	968 10	20 9	35 9	150	912	BEE	875	875	685	855	865	655	855	880	855	850	843	840	830	800	76D	715	565	670	660	640	670	695	700	10	/20	720	720	72
51 1305 1197	1113	1073 104	3 963	941	978	327	942	939	915	917	\$33	957 10	15 9	35 9	i50	921	902	895	970	870	860	865	865	038	860	865	855	845	835	835	520	775	735	585	675	585	690	730	745	750	640	843	640	640	84
52 1283 1207	1127	1060 104	9 976	945	937	937	935	939	910	907	941	957 10	18 9		155	935	910	895	870	660	855	B60	870	875	875	860	860	845	B25	830	820	785	735	700	660	585	110	740	600	800	620	820	820	820	82
3 282 11/5	1121	1077 106	3 992	957	937	935	947	916	9D6	ESE	927	967 9	54 9	io I s	125	930	925	895	880	870	860	850	840	840	850	855	840	845	B4D	830	815	785	745	715	765	723	130	750	775	790	<b>₩00</b>	800	800	600	ЯD
54 1261 1209	1149	1105 106	2 989	957	982	1157	964	922	907	E93	915	951 9	50 91	57 5	105	895	695	860	RED	865	875	850	630	830	830	840	845	845	B45	835	.925	600	750	745	750	760	740	745	760	760	790	790	790	790	79
5 263 1204	1154	1112 107	5 991	.761	940	991	922	ES6	890	E91	91E	940 9	19 9	18 8	156	394	655	865	845	830	800	815	810	800	810	830	850	855	860	855	950	630	795	110	805	770	750	735	750	770	780	760	780 (	780	76
55 1:274 1200	1:45	1144 109	9 1007	940	902	881	863	676	8E6	895	924	932 9	ZE 9.	<b>11</b> 9	<del>7</del> 52	999 1	002	815	805	775	760	760	745	770	810	845	870	663	87D	855	850	840	615	825	765	775	745	730	745	765	775	775	775	775	77
57 1287 1194	1758	1151 117	0 1023	929	880	879	877	ESED	872	684	902	905 9	15 9.	se i s	ien  1	200	941	975	986	975	765	765	765	765	835	846	876	878	858	863	845	630	846	602	790	777	745	729	742	757	766	766	766	766	76
58 262 1197	1775	1148 117	2 1026	910	880	878	861	E61	871	E95	896	909 9	23 9	14 9	194	984	983	377	987	972	972	775	795	795	E15	635	835	835	835	815	795	64Z	817	798	793	779	742	726	741	762	768	768	768	768	76
59 1236 1192	1180	1163 11*	5 1016	90:	872	868	845	EX.B	869	920	941	957 9	7E 9	:a 9	84 1	017 1	003	1025	1020	994	971	975	775	785	795	815	815	815	815	795	810	₿€7	817	78t	780	773	741	722	739	759	758	768	758	768	75
60 1247 1182	1169	1136 113	0 1032	884	857	632	853	900	914	954	960 1	009 10	44 1 D	35 10	XC0 1	529 1	D38	1056	1039	1013	962	960	947	775	785	7,95	795	795	800	820	877	B63	825	765	778	771	743	725	738	759	758	768	768	763	75
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# Table 12-10 Bottom Elevation of Model Layer 6

	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 7 19 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 <u>34 35 36</u>	37 38 39 40 41 42 43 44 45 48 47 48
	11114 1765 1794 1690 1625 1588 1571 1541 1504 1484 1466 1456 1470 1508 1475 1436 1496 1417 11375 1363 1377 1396 1392 1389 1383 1417 1379 1372 1399 1416 1457 1434 1423 1422 1411 1386	1312 1255 235 1227 1213 1201 1193 1169 7196 1769 1169 1166
	1111 1416 1646 (1711) 1270 1670 1677 1565 1670 1686 1467 1436 1436 1476 1470 1470 1470 1470 1470 1470 1470 1470	1908 1905 1295 1261 1229 1209 1100 1197 1197 1197 1197 1197
	3 1659 1605 1768 1679 1637 7586 1556 1528 1535 1435 1435 1423 1463 1440 1377 1352 1356 1377 1352 1345 1345 1345 1345 1364 1349 1366 1365 1394 1397 1369 1374 1352 1306	1293 1287 1268 1248 1233 1225 1215 1205 1205 1206 1206 1206
	4 1783 1761 1728 1709 1664 1596 1542 1505 1497 1499 1493 1426 1444 1409 1415 1369 1353 1337 1352 1355 1342 1316 1323 1339 1344 1345 1323 1354 1360 1383 1374 1356 1336 1326 1326 1320 1314	1293 1262 1249 1239 1230 1223 1216 1209 1209 1209 1209 1209
et beset bes	51758 1714 1670 1662 1610 1579 1572 1515 1535 1532 1442 1429 1418 1392 1400 1373 1335 1321 1326 1335 1321 1330 1333 1320 1333 1320 1336 1330 1285 1265 1320 1348 1376 1304 1292	1271  1252  1238  1229  1216  1210  1211  1210  1210  1210  1210  1210
bit         bit        bit        bit        bit        bit	e 1830 1746 1892 1839 1555 1591 1555 1591 1555 1591 1595 1458 1492 1419 1414 1398 1399 1360 1374 1312 1307 1315 1307 1325 1304 1305 1300 1306 1324 1295 1295 1295 1295 1347 1330 1309 1309 1309 1287	1266 1249 1238 1233 1220 1215 1220 1183 1180 1180 1180 1180
	2 100E 1200 1202 1202 1202 1202 1202 120	1078 1000 1005 11408 1166 1118 1105 1108 1005 1005 1005 1005
	/ Inch 1/88 1/64 1654 1511 525 1638 1922 1424 1406 1397 1395 129 1400 1254 1531 1607 1527 1209 1209 1209 1209 1209 1200 1224 120 1304 1600 1220 1223 1263 1200 1120 1200 1200 1200 1200 1200 120	
	8 1556 1708 1679 1585 1226 1245 1245 1445 1445 1395 1384 1385 1378 1370 1376 1363 1339 1326 1317 1301 1285 1229 1272 1284 1276 1305 1325 1270 1200 1193 1770 1170 1180 1180 1193 1190	1170 1180 1128 1108 1085 1065 1040 1828 1020 1020 1020 1020
100: C         00: C        00: C        00: C        00: C        00: C        00: C        00:	9 1531 1558 1558 1478 1454 403 1338 1415 1381 1404 1375 1363 1379 1351 1342 1327 1372 1302 1230 1283 1275 1251 1251 1271 1275 1210 1160 1145 1140 1140 1135 1135 1115 1105 1090	1075 1050 1030 1033 1010 1023 1030 1003 1000 1000
1 > 1 > 0         0         0         0         0         0         0         0         0         0         0         0         0	*01421 1482 1427 1421 1401 1381 1387 1377 1387 1387 1387 1387 138	1005 985 980 970 995 1010 1000 980 980 980 980 980
1 yr         0 yr        0 yr        0 yr        0	1 1020 1002 1001 1075 1021 1022 1020 1020 1020 1020 1020 102	960 950 940 945 950 935 975 1025 1025 1025 1025 1025
Dist         Dist        Dist        D		515 515 516 516 516 516 516 1016 1016 10
1 bit         1 bit        1 bit	12 1362 1366 1352 1342 1342 1342 1343 1365 1345 1321 1316 1292 1290 1266 1281 12/4 1265 1259 1294 1252 1246 1125 1045 1110 1135 1140 1133 1345 1040 1013 980 960 943	312 012 220 342 342 342 382 382 382 382 382 382
1 0 10         1 00        1 00        1 00        1 00        1 00        1 00        1 00        1 00        1 00       1 00        1 00       1 00	13 1326 1508 1320 1343 1321 1379 1374 1369 1333 1311 1365 1305 1297 1292 1286 1277 1257 1257 1251 1244 1236 155 1110 1676 1080 1100 1120 1120 1080 1065 985 955 \$30 900 915	905 930 960 970 970 950 955 995 995 995 995 995
1 5 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	14 1301 1303 1341 (1319 1308 1349 1343 1299 1344 1307 1304 1307 1304 1299 1289 1285 1277 1272 1265 1255 1255 1256 1244 1203 1140 1135 1115 1080 1380 1075 1065 1343 1000 975 950 900 890 985 900	965 970 940 950 955 945 975 945 945 945 945 945 945
1         1        1        1        1         1         1        1        1        1        1 </td <td>15 1279 1274 1288 1267 1275 250 1259 1259 1259 1259 1259 1259 1259 1259</td> <td>970 965 970 965 950 915 935 870 870 870 870 870</td>	15 1279 1274 1288 1267 1275 250 1259 1259 1259 1259 1259 1259 1259 1259	970 965 970 965 950 915 935 870 870 870 870 870
1 100         1 100        1 100        1 100        1 100        1 1		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
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	1/1/12/28 1/232 1/244 1/242 1/245 1/244 1/245 1/245 1/246 1/113 1/114 1/04 1/040 1/046 1/041 1/114 1/124 1/242 1/242 1/245 1/246 1/245 1/255 1/2	ACC ALC ACC ALC RAL 482 RAL RAL RAL RAC 830 830 840
	18 1270 1245 1233 1231 1232 1233 1253 1053 1056 1077 1102 1094 1091 1055 1055 1055 1055 1055 1055 1055	855 BED 880 875 BPD 885 BES 865 BES 865 BES
Dip         Dip        Dip        Dip        Dip        Dip	19 1282 1245 1226 1219 1219 1219 1219 1219 1219 1219	850 850 865 875 880 875 860 853 850 850 850 850
1 > b = 0.2         0.2         0.0         0.1         0.0        0.0        0.0        0.0        0.0        0.0        0.0        0.0 <td>20 1285 1243 1226 1226 1225 1228 1228 1228 1228 1228 1228 1228</td> <td>860 850 860 855 865 870 855 835 835 835 835 835 835</td>	20 1285 1243 1226 1226 1225 1228 1228 1228 1228 1228 1228 1228	860 850 860 855 865 870 855 835 835 835 835 835 835
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	22 1283 1269 1049 1010 1206 1005 1005 1005 1016 1019 1040 1037 1030 1015 1006 1005 1030 1995 1975 355 935 935 935 935 935 901 885 860 870 865 860 890 965 860 855 960 845 840	820 B40 848 B40 B20 795 840 855 855 855 855 855
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2         2	241249 1224 1233 1213 1203 999 996 999 996 999 900 1013 1001 969 1075 1070 995 960 950 930 910 965 830 850 860 860 850 860 80 850 860 80 850 860 80 850 860 80 850 80 850 80 850 80 80 850 80 80 850 80 80 850 80 80 850 80 80 80 80 80 80 80 80 80 80 80 80 80	805 820 830 845 810 765 800 790 790 790 790 790
vir	25 1251 1218 1279 1270 1187 445 446 446 446 456 457 1004 304 458 458 1045 575 565 975 975 975 975 975 905 805 805 805 805 805 805 805 805 805 8	820 830 765 810 765 740 760 755 755 755 755 755
1         1		
17 1222         11132         11145         11145         11145         11144         11144         11144	22 1225 1215 179 1193 1193 196 9/8 9/8 9/8 9/8 9/8 9/8 9/8 9/8 9/8 9/8	845 865 880 780 740 720 742 730 730 730 730 730
2         2         1       1        1        1	27 1202 1190 1163 1166 1166 1169 973 974 974 975 1001 982 990 975 369 995 930 1020 985 950 910 900 870 980 955 890 855 970 865 835 820 865 870 870 860	795 830 770 745 720 725 725 720 720 720 720 720 720
	28 1227 1214 1177 1156 1148 1150 1154 974 969 971 376 981 368 975 368 955 1020 1015 950 975 940 915 950 840 975 965 900 860 910 695 830 840 850 860 855 840	765 BOD 765 715 710 700 700 710 710 710 710 710 710
Dist         Dis         Dist         Dist	29 1257 1225 1201 1173 1153 1143 1136 1127 960 973 973 975 991 955 950 942 990 1005 580 955 920 915 955 930 915 970 945 905 855 845 820 795 620 833 805 745	755 770 750 700 710 705 695 580 680 680 582 680
vice         vice        vice        v	30 1231 1216 1201 1165 1153 1154 1126 1106 1100 050 562 067 073 055 567 045 361 045 361 045 361 045 361 045 365 95 805 805 805 805 805 805 805 805 700 795 770 751	745 715 710 715 700 885 690 560 650 550 560 660
11/22         11/16 <td< td=""><td></td><td>710 710 700 630 670 640 640 665 665 665 665</td></td<>		710 710 700 630 670 640 640 665 665 665 665
97/12/60         1136        1136        1136 <t< td=""><td></td><td>718 710 700 830 870 860 840 860 800 800 800 800</td></t<>		718 710 700 830 870 860 840 860 800 800 800 800
124         1720         1720         1720         1720         1720         172         170         170         170         70        70        70        70        70	32 1250 1208 1193 1395 1183 1198 1181 1154 1101 1098 1080 1107 960 055 1085 1020 990 915 895 910 910 910 860 855 830 795 885 940 955 940 820 755 780 830 773 760 745	745 730 695 680 660 650 615 630 630 530 530 530 530
41         41         1101         1101         1101         1101         1100         1100         1100         10000         1000        1000        1000	x3 1245 1220 1228 1200 1148 1193 1192 1178 1119 1089 1048 1077 355 350 1050 1055 950 905 905 905 890 875 660 820 775 605 825 825 825 925 770 715 755 760 775 740 750	763 720 700 590 670 540 630 520 620 520 620 620
21         21         112	34 1252 1207 1193 15158 1127 1144 1137 1124 1123 1083 1052 1055 1124 1092 1045 995 925 925 905 860 675 865 860 635 805 773 600 805 875 905 750 710 750 800 773 730 745	745 705 680 650 665 640 620 610 610 610 610 610 610
9         112         116         110         115         110	35 1255 1135 1184 1134 1134 1125 1109 1102 1092 1057 1049 1055 1105 1050 1042 350 420 910 660 655 850 840 825 825 775 805 825 775 805 825 775 715 815 825 763 730 745	593 595 700 590 550 540 520 520 520 520 520 620 620 620
m         m		545 534 501 545 540 540 535 535 535 535 635 635 635
11/11         11/12         11/13         11/13         11/13         11/13         11/14         11/13         11/13         11/14         11/13         11/14 <th< td=""><td></td><td></td></th<>		
as is is in	37 11.2 1149 1135 1123 1135 1123 1136 1049 1009 1038 044 11037 1111 1130 1076 1050 996 925 946 860 860 860 860 796 765 778 770 790 814 815 765 770 770 770 770 770 770 770 770 770 77	080 070 200 020 840 023 000 681 683 F.M. 683 CRS
ap = 12:3         11:23         11:24         11:25         11:5         10:5         10:40         10:23         17:0         10:5         17:0         10:5       10:5	38 1151 1142 1114 1033 1024 1027 996 1052 1027 1056 1140 112C 1065 106C 985 430 935 870 85C 820 785 765 775 765 805 810 805 770 765 705 705 705 705 705 705 705 705 705 70	685 665 650 640 640 640 640 670 670 670 670 670
40         1224         1	39 1221 1241 1253 1194 1077 1067 1004 995 1037 1024 1037 1125 1115 1065 1040 990 920 920 935 875 650 820 783 755 790 773 825 820 815 855 750 750 750 750 750 750 750 750 750 7	555 645 640 635 635 645 645 660 660 660 660 660 660
1       122       112       122       112       122       112       122       112       122       112       122       112       122       112       122       122       122       123	40 1224 1272 1273 1203 1098 1045 975 1028 1017 1024 1044 1120 1000 1035 985 915 680 870 650 815 770 830 795 735 785 775 770 770 770 770 735 725 735 735 735 735 735 735 735 735 735 73	570 655 545 635 635 650 615 600 600 600 600 600
1/12         1/12 <th< td=""><td>1 1000 1001 1000 1164 1005 1001 200 1000 000 1000 1000 1000 1</td><td>565 640 535 640 615 655 615 585 585 585 585 585 785</td></th<>	1 1000 1001 1000 1164 1005 1001 200 1000 000 1000 1000 1000 1	565 640 535 640 615 655 615 585 585 585 585 585 785
42       1124       <		COC C10 C00 C10 C10 100 010 011 011 011 01
43         132         121         1121         1122         112		
44       1145       <	43 (7456 [1271 1719 1064 [1035 ] 946 ] 987 [ 997 ] 1012 [1005 1047 ] 1121 [1122   1102   1004   0015 ] 925   870   870   875   870   785   755   735   705   685   750   775   745   710   655   645   655   645   655	090 C90 000 625 635 655 665 820 620 620 620 620
45       137       142       146       101       94       97       101       94       97       101       94       97       101       94       97       102       105       102       105       102       105       102       105       102       105       102       105       102	44 1345 1244 1163 1079 938 940 944 939 1017 694 1011 1093 1083 1078 1064 050 950 936 895 876 876 875 780 770 745 715 685 720 780 775 760 505 655 655 655 655 655 735	705 670 650 630 640 685 710 650 650 650 650 650
46       13-5       12/5       11:5       10/6       1031       344       540       944       1030       842       982       1030       1031       12/5       12/5       1330       710       700       730       710       700       635	45 13:7 1242 11:46 1084 1017 942 945 977 1311 984 991 1055 1027 1051 1057 1045 970 920 910 680 860 860 863 780 733 710 705 743 775 765 713 675 655 645 645 665 715	710 665 635 645 665 720 720 665 665 665 665 665
1         1	46 1415 1276 1155 1085 1031 944 940 944 1003 092 065 1002 999 1010 1041 1035 1015 910 970 945 830 800 800 765 755 725 730 730 730 730 705 200 650 650 655 655 655	700 665 620 675 670 730 730 720 720 720 720 720
41       1/2       1/		705 650 600 635 600 720 710 705 705 705 705 705
44       132       152       152       152       152       152       152       155       15	4/ 1/2/24 1/2/1 11/4* 10/47 10/52 9/49 9/49 9/29 9/49 9/29 9/59 9/58 9/58 10/49 10/2/ 10/27 10/5 9/71 19/91 16/20 16/64 8/29 15/0 1/52 1/50 1/50 1/50 1/50 1/50 1/50 1/50 1/50	
49       1326       1109       1365       1067       1075       966       920       941       980       943       925       946       960       144       990       943       925       940       940       920       941       940       943       925       941       940       943       925       941       940       952       943       950       943       950       943       950       943       950       943       940       943       925       943       944       940       950       943       950       943       950       943       950       943       950       943       950       943       950       943       950       943       950       943       950       943       950       943       950       943       950       943       950       943       950       943       950       943       950       943       950       943       940       <	48/2318 1178 1114 1098 11041 919 920 925 949 976 945 942 957 973 1016 100 1010 935 910 640 845 815 810 805 800 805 810 800 785 760 705 690 675 665	645 640 635 620 590 690 700 670 685 685 685 685
55         1728         1172         1283         1172         1283         1172         1285         1051         921         943         914         942         952         934         916         930         910         910         943         916         930         921         930         925         933         925         933         925         933         925         933         925         933         923         933         933         930         933         930         933         930         933	49 [1306   1169   1065   1067   1075   966   928   920   941   980   943   525   936   560   1044   1041   595   910   468   655   825   820   825   820   825   820   815   840   830   815   810   820   810   745   635   685	670 625 590 595 630 685 680 665 685 685 685 685
5 1225 1147 1103 103 923 53 91 918 917 932 929 502 907 924 947 101 975 920 947 101 975 920 941 162 885 863 855 842 850 860 845 850 840 840 800 800 800 800 800 800 800 80	50 17283 1172 1085 1058 1051 921 943 914 942 952 934 915 905 944 958 1010 970 945 897 651 800 802 805 805 805 805 805 805 805 805 805 805	655 660 650 630 660 685 690 700 710 710 710 710
111       102       101       1	51 1995 1142 1142 1142 1142 1142 314 314 317 32 323 374 GPE 017 92, 42 Phrn 975 975 311 822 885 861 855 865 865 865 865 865 865 865 865 865	675 670 675 680 720 735 740 830 830 830 830 830
52       127       117       111       1003       180       942       947       947       947       947       947       947       947       947       947       947       947       947       947       947       947       947       947       947       940       9		655 670 875 700 701 700 PID 810 PID 810 PID
53 1272 1166 1111 1057 1053 982 547 927 925 937 902 992 937 905 989 889 917 957 954 985 920 85 950 80 857 950 850 850 800 840 845 850 800 80 840 845 850 800 80 80 80 80 80 80 80 80 80 80 80 8	22 22/3 [137] [113] [113] [26] [335] [27] [327] [327] [327] [327] [327] [327] [347] [347] [347] [347] [340] [340] [340] [340] [340] [350]	
54 127 1199 1139 1095 1052 979 947 972 1147 154 912 997 893 965 944 970 957 90 947 972 1147 54 912 997 893 965 944 960 957 90 892 875 950 895 865 860 872 85 860 840 840 840 840 840 840 840 840 840 84	53 1272 1166 1111 1067 11053 982 947 927 925 037 906 896 888 917 957 954 985 920 325 920 890 875 855 850 843 830 830 843 845 830 815 830 810 780 740	10 695 713 720 743 755 780 790 790 790 790 790 790
55 253 1194 1144 1102 1055 381 551 930 9e1 912 8e8 8e0 8e1 902 913 928 928 91 912 8e8 8e0 8e1 902 939 955 984 850 860 840 825 785 780 785 785 860 845 850 845 850 845 850 845 850 845 850 845 850 845 850 845 850 845 850 845 850 845 850 785 780 740 725 740 750 770 770 770 770 770 770 770 770 77	54 1271 1139 1139 1139 1055 1052 979 947 972 1147 054 912 897 883 905 941 940 957 800 890 857 855 850 870 845 825 825 825 840 840 840 840 830 820 735 755	735 740 750 730 735 750 770 780 760 790 760 760 760
56 [264 1130 1138 1134 1049 927 530 82 877 673 665 86 892 871 673 665 876 896 914 922 876 931 952 988 932 810 800 770 755 75 740 765 905 840 865 875 665 860 845 826 815 775 765 733 723 723 725 755 765 765 765 765 765 765 765 765 76	55 1253 1194 1144 1102 1055 981 551 930 981 912 885 880 881 906 930 929 939 956 984 850 860 843 825 795 813 805 795 805 865 845 850 845 850 845 825 785	760 795 760 740 725 740 760 770 770 770 770 770
30 120 100 100 100 100 100 100 100 100 10	SE UREA 1130 1130 1130 1130 1130 1000 027 030 030 031 014 032 045 045 045 040 002 046 031 057 068 027 810 007 710 754 745 740 755 046 046 045 035 045 045 045 046 045 045 045 045 045 045 045 045 045 045	815 775 765 735 720 735 755 765 765 765 765 765
5/12/11/1144 [1146 [1141 [110]		702 770 767 728 719 327 747 756 766 766 766 766
58 1252 1147 11 - 6 1138 1122 1116 500 870 862 851 851 861 876 186 899 51 951 953 974 973 97 952 972 78 78 78 78 78 78 78 78 78 78 78 78 78	57 277 1184 1148 1141 1130 1113 919 870 857 857 870 852 674 892 835 302 928 971 993 981 905 979 953 700 760 760 760 841 871 873 853 858 835 220 630	
59 1226 1132 117C 1155 1105 1005 301 652 656 678 910 931 947 920 939 1004 935 958 978 758 758 758 758 758 758 758 758 758 7	59 252 1147 1166 1138 1102 1106 900 870 868 851 861 861 861 866 839 913 984 974 974 973 967 977 952 962 770 780 790 810 830 830 830 830 830 805 765 832 807	769 773 769 732 715 731 752 756 758 758 758 758
es 237 1172 1158 1126 1050 1122 874 847 822 843 860 304 944 970 959 1004 935 958 1019 1028 1046 1029 1003 972 953 937 770 780 750 790 785 756 876 183 815 756 766 761 733 716 728 748 758 758 758 758 758 758 758 758	59 1226 1182 117C 1153 1105 1106 801 652 1856 637 91C 937 91C 931 947 965 953 974 1007 993 1015 1016 964 961 965 770 760 790 610 8t0 810 805 785 900 857 807	771 770 763 731 712 729 749 758 758 758 758 758
	60 1227 1172 115E 1126 1126 1122 874 847 822 943 860 364 944 970 959 1034 935 598 1019 1028 1046 1129 1003 972 950 937 770 780 730 790 785 750 810 867 853 815	756 768 761 733 716 728 748 758 758 758 758 758 758

Use	Source	Number	Estimation Method
Domestic	Hydrocesus	1208	Number of People × Unit Consumption
		farms	Area $\times$ Unit Population $\times$ Unit Consumption
	DWA Database	43 farms	Area $\times$ Unit Population $\times$ Unit Consumption
	NamWater	8 schemes	Monthly Abstraction
Stock Watering	Hydrocensus	1208	Number of Stock ×Unit Consumption
; ;		farms	Area / Carrying Capacity × Unit Consumption
	DWA Database	43 farms	Area / Carrying Capacity × Unit Consumption
Irrigation	Hydrocesus	61 farms	Irrigated Area $\times$ Unit Consumption
	Permit Holders	41 farms	Monthly Abstraction

Table 12-11 Data Source and Estimation Method of Present Groundwater Use

Table 12-	12	Results	of the	Hydorcensus
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Number of farms	1,251	
In the study area		
Surveyed farms	1,208	
Number of boreholes	5,726	
Number of boreholes in use	4,467	
People on farms	9,403	on 1006 farms
Number of stock		on 1058 farms
Large stock	103,211	
Small stock	1,268,154	
Ratio of SS and LS	12.29SS/LS	
Irrigated area	566.5ha	on 102 farms
Present groundwater use		on 879 farms
Domestic	3,045m <sup>3</sup> /day	
Stock watering	9,919m <sup>3</sup> /day	
Irrigation	15,096m <sup>3</sup> /day	
Total	28,060m <sup>3</sup> /day	
Unit population	1.93capita/1000ha	Average of 831 farms
Unit consumption	_	
Domestic	408 Litter/day/capita	Average of 623 farms
Large stock	37 Litter/day/head	Average of 828 farms
Small stock	7 Litter/day/head	Average of 146 farms
Irrigation	27.3m <sup>3</sup> /day/ha	Average of 84 farms
Carrying capacity		
Large stock	16ha/head	Average of 668 farms
Small stock	3ha/head	Average of 899 farms

# Table 12-13 Productions of NamWater Scheme

Unit: m<sup>3</sup>/year

Ye	ear	Aranos	Leonardville	Stampriet	Gochas	Koes	Kries	Aminius	Onderombapa	Total
1	986	207595	80694	24827	61709	61406	12297	22652	11254	482434
1	987	225373	84926	51959	67458	44592	17887	18513	13202	523910
1	988	229445	87990	67216	64131	52437	18400	19248	14823	553690
1	989	214061	78646	64532	73652	60886	19219	18771	20666	550433
1	990	231499	69701	55087	73004	72619	18769	18706	24018	563403
<u> </u>	991	236790	64453	47509	76924	81159	15914	22593	25438	570780
1	992	260828	72529	41392	74089	78686	13210	19317	30185	590236
[ 1	993]	243750	63862	38674	63065	83641	9952	15755	28608	547307
1	994	254894	60571	48707	63944	80505	10729	17990	29316	566656
1	995	264970	64721	50059	62323	73234	10347	27178	28513	581345
1	996	227863	62789	56417	60807	70285	10601	25324	24056	538142
1	997	220427	61257	59878	58163	66449	10377	25355	15341	517247
1	998	242633	71640	68915	62978	75638	11403	37308	20992	591507
1	999	236212	70295	76305	60264	79451	11309	43866	26768	604470

# Table 12-14 Estimated Irrigation Uses of Permit Holders

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
1994	241315	222371	213846	174800	175911	163299	199301	238937	334090	362365	418580	421244	3166060
1995	340450	269628	223514	209903	184949	182637	214159	278014	329975	424403	500396	485130	3643159
1996	414956	454732	425074	347015	338009	324907	254633	368545	371801	405419	471203	447132	4623428
1997	333611	318775	325190	275168	224816	262489	228166	342431	349942	406533	408957	410482	3886560
1998	424061	398935	432321	430346	308883	318409	323477	430729	479120	522470	613145	643734	5320701
1999	492834	502211	391590	604674	370264	296724	309408	357167	379680	478150	554038	584171	5320909

\*) Allocated amount: 8,350,000 m3/year

						×	
Data		Farms	Irrigated Area (ha)	Imgation Use(m³/a)	Unit Consumption (m³/d/ha)	Ratio (%)	Remarks
Allocated amount				5979000	42.0	100	
Monthly Reports	1998	20	383 5	4003193	28.6	68	
wonting reports	1999	1999	000.0	3640425	26.0	62	
Hydrocensus				4139438	29.6	70	
Allocated amount				4352000	37.6	100	Excluding low unit
Monthly Reports	1998	25	217 5	3939017	34.0	90	consumption
	1999		517.5	3589689	31.0	82	iams
Hydrocensus				3630628	31.3	83	

Table 12-15 Estimation of Unit Consumption from Irrigation Permits

Table 12-16 Used Assumptions for Groundwater Use Estimation

Items	Unit	Data Source
Unit Population	1.93 capita/ha	Hydorcensus
Unit Consumption		
Domestic		
Commercial Farms	400 Litter/day/capita	Hydrocensus
Communal Land	30 Litter/day/capita	Chap.10
Stock Watering		
SS	8 Litter/day/head	Hydrocensus
LS	37 Litter/day/head	Hydorcensus
Irrigation	28m3/day/ha	Permit Holders
Carrying Capacity		
SS	3ha/head	Hydorocensus
LS	16ha/head	Hydorcensus
Ratio of SS / LS	12.29	Hydorcensus

Domestic Use	Population	Unit Consumption	Groundwater	Groundwater Use
		(Litter/day/capita)	Use (m <sup>3</sup> /day)	(thousand m <sup>3</sup> /a)
Commercial Farms	14,089	400	4,368	1,594
Communal Land	11,588")	30	348	127
Village Centres			1,739	635
(NamWater Scheme)				
Subtotal			6,455	2,356
Stock Watering Use	Head	Unit Consumption	Groundwater	Groundwater Use
		(Litter/day/head)	Use (m <sup>3</sup> /day)	(thousand m <sup>3</sup> /a)
SS	1,415,675	8	11,326	4,134
LS	115,221	37	4,263	1,556
Subtotal			15,589	5,690
Irrigation Use	Area	Unit Consumption	Groundwater	Groundwater Use
	(ha)	(m <sup>3</sup> /day/ha)	Use (m <sup>3</sup> /day)	(thousand m <sup>3</sup> /a)
Permit Holders			14,578	5,321
Others	153.2	28	4,290	1,566
Subtotal			18,868	6,887
Total			Groundwater	Groundwater Use
			Use (m <sup>3</sup> /day)	(thousand m <sup>3</sup> /a)
			40,912	14,933

Table 12-17 Present Groundwater Use

\*) See Table 12-20

Priority	Borehole	Decision of Aquifer	Number of
	Information		Wells
1	Screen depth	Aquifer in which screen exists	28
2	Borehole depth	Aquifer in which bottom of borehole exists	3,405
3	Water strike depth	Aquifer in which deepest water strike occurred	17
4	Water strike aquifer	Aquifer in which deepest water strike occurred	135
5	No information	Unconfined (Kalahari) Aquifer	1,648
		Total	5,233

Table 12-18 Procedure of Groundwater Use Dividing into Aquifers

Use	Unit	Kalahari	Auob	Nossob	Total	%
	m³/d	4,426	1,546	483	6,455	
Domestic	1000m <sup>3</sup> /a	1,615	564	176	2,356	15.8
	%	68.6	24.0	7.5	100.0	
	m³/d	12,580	2,954	55	15,589	
Stock Watering	1000m <sup>3</sup> /a	4,592	1,078	20	5,690	38.1
	%	80.7	18.9	0.4	100.0	
	m³/d	9,733	9,122	13	18,868	
Irrigation	1000m <sup>3</sup> /a	3,553	3,330	5	6,887	46.1
	%	51.6	48.3	0.1	100.0	
	m³/d	26,739	13,622	551	40,912	
Total	1000m <sup>3</sup> /a	9,760	4,972	<b>20</b> 1	14,933	100.0
	%	65,4	33.3	1.3	100.0	

Table 12-19 Present Groundwater Use by Aquifer

Table 12-20 Estimation Sources of Groundwater Use Variation 1990-1999

Year	Commercial	Commur	hal Land	Stock	Irrigation*11)
	Farms *1)	Aminuis* <sup>4)</sup>	Nama Land* <sup>6)</sup>	Watering* <sup>8)</sup>	(million m <sup>3</sup> /a)
				(m <sup>3</sup> /a)	
1989	-	-	-	883,600* <sup>9)</sup>	_
1990	13,260	7,670	1,800	867,479	2,193018
1991	13,350*2)	7,830* <sup>5)</sup>	1,850	851,652	2.427783
1992	13,440	8,000	1,910	836,113	2,68768
1993	13,530	8,170	1,960	820,859	2.9754
1994	13,620	8,340	2,010	805,882	3.29392
1 <b>995</b>	13,720	8,520	2,070	791,179	-
1996	13,800	8,700	2,130	776,744	-
1997	13,900	8,890	2,190	762,572	-
1998	14,000	9,080	2,250	748,659	-
1999	14,090* <sup>3)</sup>	9,280	2,310*7)	735,000* <sup>10)</sup>	-

1) Annual growth 0.68%

2) Population and Housing Census 1991

3) Estimated number based on the Hydrocensus (excluding R0132/A+R0134+R0249/Rem)

4) Annual growth 2.14%

5) From Chap.10

6) Annual growth 2.48%

7) Estimated number based on the Hydorocensus (population of M0120+R0237+M0238)

8) Annual growth -1.82%

9) Based on the Hydrocensus 1986-1989, Area1-3 (Table12-22)

10) Based on the Hydrocensus

11) Exponential function approximation y=2.9754Exp(0.1017x)

		Area 1	Area 2	Area3	Total		
Surveyed Area	5140	8095	7500	20735			
Number of Farms	62	117	99	278			
Number of Wells	563	439	836	1838			
Number of Stocks	Large	8000	-	12000	-		
	Small	122000	-	16000	-		
Irrigation Area (ha)		330.0	13.4	40.0	383.4		
	Domestic	200000	700000	530000	1430000	15%	
Groundwater Use	Stock Water	300000	370000	440000	1110000	12%	
(m <sup>3</sup> /year)	Irrigation	6100000	240000	570000	6910000	73%	
	Total	6600000	1310000	1540000	9450000	100%	
Aquifer (m <sup>3</sup> /year)	Kalahari	400000	710000	1490000	2600000	28%	
riquitor (in / jear)	Artesian	6200000	600000	50000	6850000	72%	

Table 12-21 Results of Hydrocensus 1986-1989

Source: Geohydrology Division, Department of Water Affairs, South West Africa/Namibia, 1986; 1987; 1989

Unit Consumption, Large Stock: 35Liter/d/head, Small Stock: 5Liter/d/head Irrigation: 50m<sup>3</sup>/d/ha (Drip Irrigation 16.7 m<sup>3</sup>/d/ha)

1986–1989 (A) Farms Wells Irrigation Area (ba)	Area1 55 505 320.8	Area2 68 323	Area3 72	Total
Farms Wells Irrigation Area (ha)	55 505 320.8	68 323	72	105
Wells Irrigation Area (ha)	505 320.8	323		190
Irrigation Area (ha)	320.8	010	636	1464
		21.3	16.5	358.6
Drip Irrigation Area (ha)				
Domestic Use (m³/a)	216200	396600	499000	1111800
Stock Water (m³/a)	271900	234800	376900	883600
Irrigation Use (m <sup>3</sup> /a)	5853700	389500	300200	6543400
Total (m³/a)	6341800	1020900	1176100	8538800
1999 (B)	Area1	Area2	Area3	Total
Farms	99	73	89	261
Wells	497	342	721	1560
People	1815	795	1077	3687
Large Stock	3750	4964	4950	13664
Small Stock	95928	91605	120306	307839
Irrigation Area (ha)	408.7	40.0	31.8	480.5
Production of Permit				
Holders (m³/a) <sup>1)</sup>	1090991	69136	0	1160127
Converted Irrigation				
Area (ha) <sup>2)</sup>	72.9	4.6	0.0	77.5
Total (ha)	481.6	44.6	31.8	558.0
Drip Irrigation Area (ha	i 10.0	2.0	18.0	130.0
Domestic Use (m <sup>3</sup> /a)	248800	205700	159500	614000
Stock Water (m <sup>3</sup> /a)	221600	230600	282800	735000
Irrigation Use $(m^3/a)^{3}$	8789200	813950	580350	10183500
Irrigation Use $(m^3/a)^{4}$	7450867	705700	360400	8516967
Total −1 (m³⁄a) <sup>5)</sup>	7921267	1142000	802700	9865967
Total −2 (m³/a) <sup>6)</sup>	9259600	1250250	1022650	11532500
Farms (B)/(A)	180%	107%	124%	134%
Wells (B)/(A)	98%	106%	113%	107%
Irrigated Area (B)/(A)	150%	209%	193%	156%
Domestic Use (B)/(A)	115%	52%	32%	55%
Stock Water (B)/(A)	82%	98%	75%	83%
Irrigation Use (B)3)/(A)	150%	209%	193%	156%
Irrigation Use (B)4)/(A)	127%	181%	120%	130%
Total-1/(A)	125%	112%	68%	116%
Total-2/(A)	146%	122%	87%	135%

# Table 12-22 Comparison of Results of Hydrocensus between 1986-1989

and 1999

1) Farms without Hydrocensus record, but with permit

2) Using unit consumption of  $41 \text{m}^3/\text{d}/\text{ha}$ 

3) Unit consumption: 50m<sup>3</sup>/d/ha

4) Unit consumption: 50m3/d/ha, Drip Irrigation: 16.7m3/d/ha

5) Using Irrigation use 4)

6) Using Irrigation use 3)

Table 12-23 Variation of Groundwater Use

Vear	[	Domestic Use (m <sup>3</sup> /day)			S	tock Water	ing (m³/da	y)	1	rrigation U	se (m³/day	)	Gr	oundwater	Use (m³/da	ay)
real	Kalahari	Auob	Nossob	Subtotal	Kalahari	Auob	Nossob	Subtotal	Kalahari	Auob	Nossob	Subtotal	Kalahari	Auob	Nossob	Total
1990	4228	1219	492	5939	14848	3486	65	18398	3856	3614	5	7475	22931	8319	561	31812
1991	4205	1180	474	5859	14577	3422	63	18063	4269	4001	6	8275	23051	8603	542	32196
1992	4201	1252	628	6081	14311	3360	62	17733	4726	4429	6	9161	23238	9041	696	32975
1993	4132	1237	629	5998	14050	3299	61	17410	<b>523</b> 1	4903	7	10141	23413	9439	697	33549
1994	4210	1208	667	6086	13793	3239	60	17092	6157	5149	8	11313	24161	9596	735	34491
1995	4340	1262	562	6164	13542	3179	59	16780	7216	5881	9	13106	25098	10323	630	36051
1996	4365	1160	553	6078	13295	3121	58	16474	9626	6758	11	16396	27285	11040	621	38947
1997	4305	1201	553	6059	13052	3065	57	16173	8215	5657	9	13881	25572	9923	619	36114
1998	4344	1598	406	6348	12814	3009	56	15878	10307	8543	13	18862	27464	13150	474	41088
1999	4426	1546	483	6455	12580	2954	55	15589	9733	9122	13	18868	26739	13622	551	40912
Year	Don	nestic Use	(1000m <sup>3</sup> /y	/ear)	Stoc	k Watering	(1000m <sup>3</sup> /)	/ear)	Irrig	gation Use	1000(m³/y	ear)	Grou	ndwater Us	e (1000m³/	'year)
Year	Dor Kalahari	nestic Use Auob	(1000m <sup>3</sup> /y Nossob	vear) Subtotal	Stoc Kalahari	k Watering Auob	(1000m³/) Nossob	/ear) Subtotal	Irrig Kalahari	ation Use Auob	1000(m³/y Nossob	ear) Subtotal	Grour Kalahari	ndwater Us Auob	e (1000m³/ Nossob	'year) Total
Year 1990	Don Kalahari 1543	nestic Use Auob 445	(1000m <sup>3</sup> /y Nossob 180	vear) Subtotal 2168	Stoc Kalahari 5419	k Watering Auob 1272	(1000m <sup>3</sup> /) Nossob 24	/ear) Subtotal 6715	Irrig Kalahari 1407	ation Use Auob 1319	1000(m³/y Nossob 2	ear) Subtotal 2728	Grour Kalahari 8370	ndwater Us Auob 3037	e (1000m³/ Nossob 205	'year) Total 11611
Year 1990 1991	Don Kalahari 1543 1535	nestic Use Auob 445 431	(1000m <sup>3</sup> /y Nossob 180 173	vear) Subtotal 2168 2138	Stoc Kalahari 5419 5321	k Watering Auob 1272 1249	(1000m <sup>3</sup> /) Nossob 24 23	/ear) Subtotal 6715 6593	Irrig Kalahari 1407 1558	ation Use Auob 1319 1460	1000(m <sup>3</sup> /y Nossob 2 2	ear) Subtotal 2728 3020	Grour Kalahari 8370 8413	Auob 3037 3140	e (1000m <sup>3</sup> / Nossob 205 198	/year) Total <u>11611</u> 11752
Year 1990 1991 1992	Don Kalahari 1543 1535 1533	nestic Use Auob 445 431 457	(1000m <sup>3</sup> /y Nossob 180 173 229	rear) Subtotal 2168 2138 2220	Stor Kalahari 5419 5321 5223	k Watering Auob 1272 1249 1226	(1000m <sup>3</sup> /) Nossob 24 23 23	/ear) Subtotal 6715 6593 6473	Irrig Kalahari 1407 1558 1725	ation Use Auob 1319 1460 1617	1000(m <sup>3</sup> /y Nossob 2 2 2	ear) Subtotal 2728 3020 3344	Grou Kalahari 8370 8413 8482	Auob 3037 3140 3300	e (1000m <sup>3</sup> / Nossob 205 198 254	<sup>/</sup> year) Total <u>11611</u> 11752 12036
Year 1990 1991 1992 1993	Don Kalahari 1543 1535 1533 1508	nestic Use Auob 445 431 457 452	(1000m <sup>3</sup> /y Nossob 180 173 229 230	rear) Subtotal 2168 2138 2220 2189	Stoc Kalahari 5419 5321 5223 5128	k Watering Auob 1272 1249 1226 1204	(1000m <sup>3</sup> /s Nossob 24 23 23 22	/ear) Subtotal 6715 6593 6473 6354	Irrig Kalahari 1407 1558 1725 1909	ation Use Auob 1319 1460 1617 1790	1000(m³/y Nossob 2 2 2 2	ear) Subtotal 2728 3020 3344 3702	Groui Kalahari 8370 8413 8482 8546	ndwater Us Auob 3037 3140 3300 3445	e (1000m <sup>3</sup> / Nossob 205 198 254 254	<sup>/</sup> year) <u>Total</u> 11611 11752 12036 12245
Year 1990 1991 1992 1993 1994	Don Kalahari 1543 1535 1533 1508 1537	nestic Use Auob 445 431 457 452 441	(1000m <sup>3</sup> /y Nossob 180 173 229 230 243	rear) Subtotal 2168 2138 2220 2189 2221	Stor Kalahari 5419 5321 5223 5128 5035	k Watering Auob 1272 1249 1226 1204 1182	(1000m <sup>3</sup> /s Nossob 24 23 23 22 22	/ear) Subtotal 6715 6593 6473 6354 6239	Irrig Kalahari 1407 1558 1725 1909 2247	ation Use Auob 1319 1460 1617 1790 1879	1000(m <sup>3</sup> /y Nossob 2 2 2 2 3	ear) Subtotal 2728 3020 3344 3702 4129	Groui Kalahari 8370 8413 8482 8546 8546 8819	Auob 3037 3140 3300 3445 3503	e (1000m <sup>3</sup> / Nossob 205 198 254 254 254 268	year) Total 11611 11752 12036 12245 12589
Year 1990 1991 1992 1993 1994 1995	Don Kalahari 1543 1535 1533 1508 1537 1584	nestic Use Auob 445 431 457 452 441 461	(1000m <sup>3</sup> /y Nossob 180 173 229 230 243 205	rear) Subtotal 2168 2138 2220 2189 2221 2250	Stoc Kalahari 5321 5223 5128 5035 4943	k Watering Auob 1272 1249 1226 1204 1182 1161	(1000m <sup>3</sup> /s) Nossob 24 23 23 22 22 21	vear) Subtotal 6715 6593 6473 6354 6239 6125	Irrig Kalahari 1407 1558 1725 1909 2247 2634	ation Use Auob 1319 1460 1617 1790 1879 2147	1000(m <sup>3</sup> /y Nossob 2 2 2 2 3 3 3	ear) Subtotal 2728 3020 3344 3702 4129 4784	Groun Kalahari 8370 8413 8482 8546 8819 9161	Aucb 3037 3140 3300 3445 3503 3768	e (1000m <sup>3</sup> / Nossob 205 198 254 254 254 268 230	ýyear) Total 11611 11752 12036 12245 12589 13158
Year 1990 1991 1992 1993 1994 1995 1996	Dor Kalahan 1543 1535 1533 1508 1537 1584 1593	nestic Use Auob 445 431 457 452 441 461 424	(1000m <sup>3</sup> /y Nossob 180 173 229 230 243 205 205 202	vear) Subtotal 2168 2138 2220 2189 2221 2250 2218	Stor Kalahari 5321 5223 5128 5035 4943 4853	k Watering Auob 1272 1249 1226 1204 1182 1161 1139	(1000m <sup>3</sup> /) Nossob 24 23 23 22 22 21 21 21	vear) Subtotal 6715 6593 6473 6354 6239 6125 6013	Irrig Kalahari 1407 1558 1725 1909 2247 2634 3514	zation Use Auob 1319 1460 1617 1790 1879 2147 2467	1000(m <sup>3</sup> /y Nossob 2 2 2 2 2 3 3 4	Bar) Subtotal 2728 3020 3344 3702 4129 4784 5984	Grout Kalahari 8370 8413 8482 8546 8819 9161 9959	ndwater Us Aucob 3037 3140 3300 3445 3503 3768 4030	e (1000m <sup>3</sup> ) Nossob 205 198 254 254 268 230 227	ýyear) Total 11611 11752 12036 12245 12589 13158 14216
Year 1990 1991 1992 1993 1994 1995 1996 1997	Dor Kalahan 1543 1535 1533 1508 1537 1584 1593 1571	nestic Use Auob 445 431 457 452 441 461 424 438	(1000m <sup>3</sup> /y Nossob 180 173 229 230 243 205 202 202 202	vear) Subtotal 2168 2138 2220 2189 2221 2250 2218 2218 2212	Stoc Kalahari 5419 5321 5223 5128 5035 4943 4853 4853 4764	k Watering Auob 1272 1249 1226 1204 1182 1161 1139 1119	(1000m <sup>3</sup> /) Nossob 24 23 23 22 22 21 21 21 21	/ear) Subtotal 6715 6593 6473 6354 6239 6125 6013 5903	Irrig Kalahari 1407 1558 1725 1909 2247 2634 3514 2998	ation Use Auob 1319 1460 1617 1790 1879 2147 2467 2065	1000(m <sup>3</sup> /y Nossob 2 2 2 2 3 3 3 4 3 4 3	Bar) Subtotal 2728 3020 3344 3702 4129 4784 5984 5067	Grout Kalahari 8370 8413 8482 8546 8819 9161 9959 9334	ndwater Us Auob 3037 3140 3300 3445 3503 3768 4030 3622	e (1000m³/ Nossob 205 198 254 254 268 230 227 226	ýyear) Total 11611 11752 12036 12245 12589 13158 14216 13181
Year 1990 1991 1992 1993 1994 1995 1996 1997 1998	Dor Kalahari 1543 1535 1533 1508 1537 1584 1593 1571 1586	nestic Use Auob 445 431 457 452 441 461 424 438 583	(1000m <sup>3</sup> /y Nossob 180 173 229 230 243 205 202 202 202 148	ear) Subtotal 2168 2138 2220 2189 2221 2250 2218 2218 2212 2212 2317	Stoc Kalahari 5419 5321 5223 5128 5035 4943 4853 4764 4677	k Watering Auob 1272 1249 1226 1204 1182 1161 1139 1119 098	(1000m <sup>3</sup> /) Nossob 24 23 23 22 22 21 21 21 21 20	vear) Subtotal 6715 6593 6473 6354 6239 6125 6013 5903 5796	Irria Kalahari 1407 1558 1725 1909 2247 2634 3514 2998 3762	Auob 1319 1460 1617 1790 1879 2147 2467 2065 3118	1000(m <sup>3</sup> /y) Nossob 2 2 2 2 3 3 3 4 3 5	Bar) Subtotal 2728 3020 3344 3702 4129 4784 5984 5984 5067 6885	Grout Kalahari 8370 8413 8482 8546 8819 9161 9959 9334 10025	ndwater Us Auob 3037 3140 3300 3445 3503 3768 4030 3622 4800	e (1000m <sup>3</sup> ) Nossob 205 198 254 254 268 230 227 226 173	Yyear) Total 11611 11752 12036 12245 12589 13158 14216 13181 14997