JMAN



ブータン国

## 貿易産業省電力局

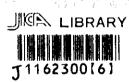
国際協力事業団

# ブータン国

# プナチャンチュ水力発電事業計画調査

# 最終報告書

Vol. 🎚 付 録



2001年2月

源 開 社 電 発 式 株 会



No. 5

## 国際協力事業団

ブータン国

## 貿易産業省電力局

# ブータン国

# プナチャンチュ水力発電事業計画調査

# 最終報告書

# Vol. Ⅲ 付 録

2001年2月

,

電源開発株式会社



.

Chapter 6: Meteorology and Hydrology
Calculation Result of DAMBRK
Simulation of 1994 GLOF
Simulation of GLOF from Luggye Lake
Simulation of GLOF from Raphstreng Lake
Calculation Result of Reservoir Sedimentation

Chapter 7: Geology Geologic Logs of Drill Holes Photographs of Cores Result of Permeability Test Geologic Logs of Pits Result of Seismic Prospecting Result of Water Level Measurement in Drill Holes Result of Laboratory Tests Photographs of Rock Core Samples Photographs of Soil Samples Results of Petrographic Examination

Chapter 11: Feasibility Design Calculation of Surging

Chapter 12: Construction Plan and Construction Cost Estimate Construction Plan and Construction Schedule

- 1. River Diversion Work
- 2. Dam
- 3. Underground Settling Basin
- 4. Headrace Tunnel
- 5. Surge Tank
- 6. Penstock Tunnel and Powehouse Complex
- 7. Detailed Construction Schedule

#### **Project Cost Estimate**

- 1. Permanent Facilities for Employer and Engineer
- 2. Road Improvement Cost
- 3. Construction Power Supply
- 4. Land Acquisition Compensation Cost

# CHAPTER 6

# METEOROLOGY AND HYDROLOGY

#### METEOROLOGY AND HYDROLOGY

Calculation Result of DAMBRK

- Simulation of 1994 GLOF
- Simulation of GLOF from Luggye Lake
- Simulation of GLOF from Raphstreng Lake

Calculation Result of Reservoir Sedimentation

.

# Calculation Result of DAMBRK (1/3)

## Simulation of 1994 GLOF

. .

#### ANALYSIS OF THE DOWNSTREAM FLOOD HYDROGRAPH

#### PRODUCED BY THE DAM BREAK OF

RUN1 T :

ON

1994 GLOF

BASED ON PROCEDURE DEVELOPED BY DANNY L. FREAD, PH. D., SR. RESEARCH HYDROLOGIST

QUALITY CONTROL TESTING AND OTHER SUPPORT BY JANICE M. LEWIS, RESEARCH HYDROLOGIST

HYDROLOGIC RESEARCH LABORATORY W23, OFFICE OF HYDROLOGY NOAA, NATIONAL WEATHER SERVICE SILVER SPRING, MARYLAND 20910

****	******	****	*****	*****	****
***					***
***	SUMMARY	0F	INPUT	DATA	***
***					***
****	*****	***	*****	*****	****

#### INPUT CONTROL PARAMETERS FOR RUN1 1 :

P <b>ARAME</b> TER ++++++++++++++++++++++++++++++++++++	VARIABLE	VALUE ******
NUMBER OF DYNAMIC ROUTING REACHES	KKN	1
TYPE OF RESERVOIR ROUTING	KUI	0
NULTIPLE DAM INDICATOR	MULDAN	0
PRINTING INSTRUCTIONS FOR INPUT SUMMARY	KDMP	5
NO. OF RESERVOIR INFLOW HYDROGRAPH POINTS	ITEH	2
INTERVAL OF CROSS-SECTION INFO PRINTED OUT WHEN J	NK=9 NPRT	0
FLOOD-PLAIN MODEL PARAMETER	KFLP	0
METRIC INPUT/OUTPUT OPTION	METRIC	1

IOPUT= 1 0 0 0 0 0 1 1 0 0 0 0

#### RUN1 1 : RESERVOIR

#### TABLE OF ELEVATION VS SURFACE AREA

SURFACE	AREA	(SQ	KM)	El	EVATION	(M)	•
	SA (K)				HS/	(K)	
******	*****	***	****	***	*****	****	****

1, 1	4560.00
0.9	4535.00
0. 0	0,00
0. 0	0. 00
0.0	0.00
0.0	0, 00
0.0	0.00
0.0	0, 00

.

RUN1 1 : RESERVOIR AND BREACH PARAMETERS

· •

PARAMETER ***********************************		VAR1ABLE *****		
LENGTH OF RESERVOIR	KM	RLM	2. 10	
ELEVATION OF WATER SURFACE	M	YO	4561.00	
SIDE SLOPE OF BREACH		Z	0.00	
ELEVATION OF BOTTOM OF BREACH	M	YBNIN	4535. 00	÷.,
WIDTH OF BASE OF BREACH	<b>M</b>	BB	35.00	
TIME TO NAXIMUM BREACH SIZE	HOUR	TFH	3. 50	
ELEVATION (MSL) OF BOTTOM OF DAM	M	DATUM	4535.00	
VOLUME-SURFACE AREA PARAMETER		VOL.	0,00	
ELEVATION OF WATER WHEN BREACHED	M	HF	4561.00	
ELEVATION OF TOP OF DAM	M	HD .	4561.00	
ELEVATION OF UNCONTROLLED SPILLWAY CREST	M	HSP	0.00	
ELEVATION OF CENTER OF GATE OPENINGS	M	HGT	0. 00	
DISCHARGE COEF. FOR UNCONTROLLED SPILLWAY		CS	0.00	
DISCHARGE COEF. FOR GATE FLOW		CG	0. 00	
DISCHARGE COEF. FOR UNCONTROLLED WEIR FLOW	I	CDO	0.00	
DISCHARGE THRU TURBINES	CMS	QT	50. 00	
CDO SHOULD NOT BE 0.0 IF OVERTOPPING MAY C	CCUR		-	

DHF (INTERVAL BETWEEN INPUT HYDROGRAPH ORDINATES) = 0.00 HRS. TEH (TIME AT WHICH COMPUTATIONS TERMINATE) = 24,0000 HRS. BREX (BREACH EXPONENT) = 0.000 MUD (MUD FLOW OPTION) = 0 IWF (TYPE OF WAVE FRONT TRACKING) = 0 KPRES (WETTED PERIMETER OPTION) = 0 .

KSL (LANDSLIDE PARAMETER) = 0

## INFLOW HYDROGRAPH TO RUN1 1 :

50.00 50.00

TIME OF INFLOW HYDROGRAPH ORDINATES

0.0000 100.0000

CROSS-SECTIONAL PARAMETERS FOR 1994 GLOF BELOW RUN1 1 :

PARAMETER ***********************************	VAR   ABLE *****	VALUE ******
NUMBER OF CROSS-SECTIONS	NS	6
MAXIMUM NUMBER OF TOP WIDTHS	NCS	2
NUMBER OF CROSS-SECTIONAL HYDROGRAPHS TO PLOT	NTT	ĉ
TYPE OF OUTPUT OTHER THAN HYDROGRAPH PLOTS	jnk	1
CROSS-SECTIONAL SMOOTHING PARAMETER	KSA	0
DOWNSTREAM SUPERCRITICAL OR NOT	KSUPC	1
NO. OF LATERAL INFLOW HYDROGRAPHS	LQ	5
NO. OF POINTS IN GATE CONTROL CURVE	KCG	0

NUMBER OF CROSS-SECTION WHERE HYDROGRAPH DESIRED (MAX NUMBER OF HYDROGRAPHS = 6)

\*\*\*\*\*\*

1 2 3 4 5 6 CROSS-SECTIONAL VARIABLES FOR 1994 GLOF BELOW RUN1 1 :

PARAMETER	UNITS	VARIABLE
*** <del>**</del> ******	******	*****
LOCATION OF CROSS-SECTION	KM	XS(()
ELEVATION (MSL) OF FLOODING AT CROSS-SECTION	i M	FSTG(I)
ELEV CORRESPONDING TO EACH TOP WIDTH	M	HS (K, I)
TOP WIDTH CORRESPONDING TO EACH ELEV (ACTIVE FLOW PORTION)	. M	BS (K, I)
TOP WIDTH CORRESPONDING TO EACH ELEV (OFF-CHANNEL PORTION)	M	BSS (K, 1)
NUMBER OF CROSS-SECTION		f
NUMBER OF ELEVATION LEVEL		К

```
CROSS-SECTION NUMBER 1
****
XS(1) = 0.000 FSTG(1) =
                          0.00
HS ...
        4535.0 4560.0
BS ...
         50.0 150.0
BSS ...
          0.0
               0, 0
CROSS-SECTION NUMBER 2
*****
XS(1) =
       36.500 FSTG(1) =
                         0.00
HS ...
        3160.0 3180.0
B$ ...
         50.0 100.0
BSS ...
          0.0
                0.0
CROSS-SECTION NUMBER 3
*****
       76.100 FSTG(1) =
XS(1) =
                         0, 00
HS ...
        1580.0 1600.0
BS ...
        70.0 200.0
BSS ...
          0,0
               0.0
CROSS-SECTION NUMBER 4
*****
XS(I) = 110.800 FSTG(I) =
                         0.00
HS ... 1170.0 1190.0
BS ...
        55.0 100.0
BSS ...
          0.0
              0.0
CROSS-SECTION NUMBER 5
*****
XS(I) = 171.500 FSTG(I) =
                          0.00
HS ...
         570.0 590.0
BS ...
         50.0 100.0
BSS ...
          0.0
                0.0
CROSS-SECTION NUMBER 6
*****
XS(1) = 219.200 FSTG(1) =
                         0.00
HS ...
         130.0
               150.0
BS ...
         100.0
               200.0
8SS ...
          0.0
                0.0
```

# 

PARAMETER UNITS VARIABLE

MINIMUM COMPUTATIONAL DISTANCE USED KM DXM (1) BETWEEN CROSS-SECTIONS

FKC(I)

#### CONTRACTION - EXPANSION COEFFICIENTS BETWEEN CROSS-SECTIONS

REACH NUMBER	DXM (I) *******	FKC(I) *******
1	2, 000	0, 000
2	2. 000	0. 000
3	2,000	0. 000
4	2.000	0, 000
5	2.000	0. 000

DOWNSTREAM FLOW PARAMETERS FOR BELOW RUN1 1 :	1994	GLOF	·
PARAMETER ***********************************	UNITS *******	VARIABLE *****	VALUE
MAX DISCHARGE AT DOWNSTREAM EXTREMITY	CNIS	QMAXD	0.0
MAX LATERAL OUTFLOW PRODUCING LOSSES	CMS /M	QLL	0.000
INITIAL SIZE OF TIME STEP	HOUR	DTHM	0.0000
INITIAL WATER SURFACE ELEVATION DOWNSTREAM	M	YDN	135.00
SLOPE OF CHANNEL DOWNSTREAM OF DAM	*	SOM	0.00
THETA WEIGHTING FACTOR		THETA	0, 00
CONVERGENCE CRITERION FOR STAGE	M	EPSY	0.000
TIME AT WHICH DAM STARTS TO FAIL	HOUR	TFI	0. 00
AT REACH= 2 DXM SHOULD BE CHANGED TO O		e to changi	E OF SLOPE CRITERIA
000 2 000 2 000 2 000 2 000			

2.000 2.000 2.000 2.000 2.000

LATERAL INFLOW REACH NUMBER

LQX (1)

1 2 3 4 5

(QL (L, 1), L=1, ITEH) 0. 0. (QL.(L, 2), L=1, ITEH) 70. 70. (QL (L, 3), L=1, ITEH) 100. 100. (QL(L, 4), L=1, ITEH) 0. 0. (QL (L, 5), L=1, ITEH) 0. 0.

TOTAL NUMBER OF CROSS SECTIONS (ORIGINAL+INTERPOLATED) (N) = 108 (MAXIMUM ALLOWABLE = 200

******					
*****					
***					***
***	SUMMARY	0F	OUTPUT	DATA	***
***					***
*****					
******					

			BOTTOM		REACH		
CR	OSS-SECTION		ELEVATION		LENGTH	SLOPE	
	NO.	KM	M	REACH NO.	KM	×	MESAGE
	1	0. 00	4535.00				
	2	36. 50	3160, 00	1	36.50	3. 77	
	3	76.10	1580.00	2	39, 60	3, 99	
	4	110. <b>80</b>	1170,00	3	34.70	1, 18	
	5	171. 50	570. 00	4	60. 70	0. 9 <del>9</del>	
	6	219. 20	130.00	5	47.70	0. 92	SLOPE LESS THAN 1% MAY CAUSE
0017104							

SUBCRITICAL FLOW

1

#### TOTAL VOLUME IN RESERVOIR BEHIND RUN1 1 : = 25.0 CU. M (MILLION)

DEFINITION OF VARIABLES IN RESERVOIR DEPLETION TABLE

PARAMETER		VARIABLE
*******	******	*****
TIME STEP FROM START OF ANALYSIS		I
ITERATIONS NECESSARY TO SOLVE FLOW EQUATIONS		ĸ
ELAPSED TIME FROM START OF ANALYSIS	HOUR	TTP(1)
TOTAL OUTFLOW FROM DAM	CMS	Q(I)
ELEVATION OF WATER SURFACE AT DAM	M	H2
ELEVATION OF BOTTOM OF BREACH	M	YB
EST DEPTH OF FLOW IMMEDIATELY DOWNSTREAM	M	D
SUBMERGENCE COEFFICIENT		SUB
VELOCITY CORRECTION		VCOR
TOTAL VOLUME DISCHARGED FROM TIME OF BREACH MILL	LION CU M	OUTVOL
BREACH WIDTH	M	88
RECTANGULAR BREACH DISCHARGE COEFFICIENT		COFR
INFLOW TO RESERVOIR	CNIS	Q1 (I)
BREACH OUTFLOW	CNS	OBRECH
SPILLWAY OUTFLOW	CNIS	QSPIL

#### RESERVOIR DEPLETION TABLE

									-						
	l	κτ	TP(1)	Q(I)	H2	YB	D	SUB	VCOR	OUTVOL	BB	COFR	QI (I)	OBRECH	QSPIL
ĸ			****	*****	*****	*****	*****	****	****	*****	****	****	****	*****	****
	,	0	0.000	50	4561.00	4561.00	4535. 44	1.00	1.00	0. 0	0.0	3. 10	50.	0.	50.
?			0.070	50	4560, 99	4560, 48	4535. 44	1.00	1.00	0. 0	0.7	3.10	50.	0.	50.
3		2	0. 140	52	4560, 99	4559, 96	4535. 45	1.00	1.00	0. 0	1.4	3, 10	50.	3.	50.
ł			0. 210	56	4560.99	4559, 44	4535. 47	1.00	1.00	0. O	2. 1	3, 10	50.	7.	50.
5			0. 280	64	4560.99	4558. 92	4535, 51	1.00	1.00	0. 1	2. 8	3. 10	50	14.	50.
3			0, 350	74	4560, 99	4558.40	4535, 56	1.00	1.00	0.1	3. 5	3.10	50.	25.	50.
i			0. 420	89	4560, 98	4557.88	4535. 62	1.00	1.00	0, 1	4.2	3.10	50.	39,	50.
3			0.490	107	4560, 97	4557. 36	4535.69	1.00	1.00	0, 1	4, 9	3. 10	50.	57.	50.
•			0. 560	129	4560.95	4556.84	4535.77	1.00	1.00	0. 1	5.6	3.10	50.	80.	50.
)			0.630	156	4560.93	4556. 32	4535.86	1.00	1.00	0. 2	6, 3	3.10	50.	107.	50.
í			0.700	188	4560.90	4555.80	4535.96	1.00	1.00	0. 2	7.0		50.	138.	50.
2			0.770	223	4560.87	4555. 28	4536.07	1.00	1.00	0.3	7.7	3, 10	50.	174.	50.
3			0.840	264	4560.82	4554.76	4536.18	1.00	1.00	0.3	8.4	3.10	50.	214.	50.
ţ			0.910	307	4560, 77	4554. 24	4536. 29	1.00	1.00	0, 4	9.1	3.10	50.	260.	48.
5			0. 980	353	4560.70	4553. 72	4536.40	1.00	1.00	0.5	9.8	3, 10	50.	309.	44.
3			1.050	403	4560. 62	4553, 20	4536. 52	1.00	1.00	0.6	10.5		50.	364.	40.
			1. 120	403	4560.54	4552.68	4536, 63	1.00	1.00	0.0	11.2		50.	422.	
7					4560, 43	4552. 16	4536.75	1.00	1.00	0.8	11.9		50.	485.	32.
3			1.190	516	4560, 43	4551.64	4536.88			1.0	12.6		50.	551.	28.
) J			1,260	579	-			1.00	1.00		13.3		50.	622.	28. 24.
)			1.330	645	4560.19	4551.12	4537.00	1.00	1.00	1.1			· 50.	695.	29. 20.
1			1,400	715	4560.04	4550.60	4537.12	1.00	1.00	1.3	14.0				
2			1.470	787	4559.88	4550, 08	4537.25	1.00	1.00	1.5	14.7		50.	772.	16.
3			1. 540	862	4559, 69	4549.56	4537.37	1.00	1.00	1.7	15.4		50. 50	851.	12.
4			1.610	940	4559.50	4549.04	4537.49	1.00	1.00	1.9	16.1	3.10	50. 60	932.	8.
5			1.680	1019	4559.28	4548. 52	4537.61	1.00	1.00	2.2	16.8		50. 50	1016.	4.
6			1.750	1100	4559.04	4548.00	4537.73	1.00	1.00	2.4	17.5		50.	1100.	0.
7			1.820	1185	4558.78	4547.48	4537.86	1.00	1,00	2. 7	18.2		· 50.	1186.	0.
8			1.890	1271	4558. 51	4546, 96	4537.97	1.00	1.00	3.0	18.9		50.	1271.	0.
9			1.960	1357	4558, 21	4546, 44	4538.09	1.00	1.00	3.4	19.6		50.	1357.	0.
0		2	2.030	1442	4557.89	4545, 92	4538.20	1.00	1.00	3.7	20.3		50.	1442.	0.
1			2.100	1526	4557.55	4545.40	4538.31	1,00	1.00	4.1	21.0		50.	1526.	0.
2			2.170	1609	4557.19	4544.88	4538.41	1.00	1.00	4.5	21.7		<b>50</b> .	1609.	0.
3		2	2. 240	1690	4556.81	4544, 36	4538. 51	1.00	1.00	4.9	22.4		<b>50</b> .	1690.	0.
4		2	2.310	1769	4556.41	4543, 84	4538.60	1.00	1.00	5.3	23. 1		50.	1769.	0.
5		2	2. 380	1845	4555.99	4543. 32	4538.69	1.00		5.8	23.8		50.	1848.	0.
6		2	2. 450	1919		4542.80						3.10	<b>5</b> 0.	1920.	0.
7			2. 520	1990		4542. 28			1,01			3.10	50.	1991.	0.
8			2. 590	2058		4541.78			1.01			3.10	50.	2059.	0.
9	)		2. 660	2123		4541, 24			1.01	7.8		3.10	50.	2123.	0.
0	)	2	2. 730	2184		4540. 72			1.01	8.3		3.10	<b>50</b> .	2184.	0.
1		2	2. 800	2241	4553.09	4540. 20	4539, 13	1.00	1.01	8.9	<b>28</b> . 0	) 3, 10	50.	2242.	0.
2	!	2	2.870	2295	4552.55	4539. 68	4539.19	1.00	1.01	9, 5	28. 7	3, 10	<b>50</b> .	2296.	0.
3	1	2	2. 940	2345	4552.00	4539. 16	4539. 24	1.00	1.02	10.0	29.4	3.10	<b>50</b> .	2346.	0.
4	ŀ	2	3.010										<b>50</b> .	2393.	0.
5	j	2	3, 080				4539, 33		1.02				<b>50</b> .	2436.	0.
e	5	2	3. 150	2476					1.02		31.5	5 3.10	<b>50</b> .	2476.	0.
-7	1	2	3. 220	2513	4549.64	4537. 08	4539. 41	1.00	1.03	12. 5			50.	2513.	0.
-8	3	2	3. 290	2547	4549. 02	4536, 56	4539, 45	1.00	1.03	13. 1	32. 9	3.10	<b>50</b> .	2548.	0.
.9	)	2	3. 360	2579	4548.40	4536.04	4539, 48	1.00	1.04	13.8	33.6	3 3, 10	<b>50</b> .	2580.	0.
iC	)	2	3, 430	2609	4547.76	4535. 52	4539. 51	1.00	1.05	14. 4	34. 3	3 3.10	50.	<b>2609</b> .	0.
														с. С. р.	

ì

#### RESERVOIR DEPLETION TABLE

ł	к	TTP(I)	Q(I)	H2	YΒ	D	SUB	VCOR	OUTVOL	BB	COFR	QI (I)	OBRECH	QSPIL
***	**	*****	******	******	*****	*****	****	****	****	****	****	*****	*****	****
51	2	3. 500	2638	4547.11	4535.00	4539, 54	1 00	1 05	15 1	<u> </u>	0 10	50	0800	•
52	2	3. 570	2058	4546.48	4535.00	4539.35	1.00	1.05 1.06	15, 1 15, 7	35, 0 35, 0	3, 10 3, 10	50. 50.	2638. 2454.	0. 0.
53	2	3, 640	2273	4545.89	4535.00	4539.17	1.00	1.06	16.3	35.0	3, 10	50.	2274.	0. 0.
54	2	3.710	2109	4545. 34	4535.00	4538.99	1.00	1.06	16, 9	35.0	3, 10	50. 50.	2109.	0. 0.
55	2	3. 780	1959	4544.83	4535.00	4538.82	1.00	1.06	17.4	35.0	3.10	50.	1959	0.
56	2	3.850	1823	4544. 36	4535.00	4538.67	1.00	1.08	17. 9	35.0	3, 10	50.	1823.	Ŭ,
57	2	3. 920	1699	4543, 92	4535.00	4538. 52	1.00	1.07	18. 3	35.0		50.	1699.	0.
58	2	3: 990	1585	4543. 51	4535.00	4538.38	1.00	1.07	18, 7	35.0		50.	1586.	0.
59	2	4.060	1482	4543, 13	4535.00	4538.25	1.00	1.07	19, 1	35.0	3, 10	50.	1482.	0
60	2	4.130	1387	4542.77	4535.00	4538.13	1.00	1.07	19.5	35. 0	3, 10	<b>50</b> .	1387.	0.
61	2	4. 200	1300	4542. 43	4535.00	4538.01	1.00	1.07	19.8	35. 0	3, 10	<b>5</b> 0.	1300.	0
62	2	4. 270	1220	4542.11	4535.00	4537.90	1.00	1.08	<u>2</u> 0. 1	35. 0	3, 10	50.	1220.	0
63	2	4. 340	1146	4541.82	4535.00	4537.80	1.00	1.08	20.4	35. 0	3. 10	50.	1147.	0
64	2	4, 410	1078	4541.54	4535.00	4537.70	1.00	1.08	20. 7	35. 0	3, 10	50.	1079.	0
65	2	4. 480	1016	4541.28	4535. 00	4537.61	1.00	1.08	21. 0	35. 0	3, 10	<b>50</b> .	1016.	0
66	2	4. 550	958	4541.03	4535.00	4537.52	1.00	1.08	21. <b>2</b>	35. 0	3, 10	<b>50</b> .	959.	0
67	2	4. 620	905	4540. 80	4535. 00	4537.44	1,00	1.08	21. 5	35. 0	3, 10	<b>50</b> .	<del>9</del> 05.	0
68	2	4. 690	855	4540. 58	4535.00	4537.36	1.00	1.08	21.7	35. 0		50.	855.	0
69		4.760	809	4540. 37	4535.00	4537.28	1.00	1.09	21. 9	35. 0		50.	809.	0
70	2	4.830	766	4540.18	4535.00	4537.21	1.00	1.09	22. 1	35. 0		50.	767.	0
71	2	4.900	727	4539.99	4535.00	4537.14	1.00	1.09	22. 3	35.0		50.	727.	0
72	2	4, 970	690	4539, 82	4535.00	4537.08	1,00	1,09	22. 5	35.0		50.	<b>6</b> 90.	0
73	2	5.040	655	4539.65	4535.00	4537.02	1.00	1.09	22.6	35.0	3.10	50.	656.	0
74	2	5.110	623 522	4539.50	4535.00	4536.96	1.00	1.09	22.8	35.0		50. 50	624.	0
75 76	2 2	5. 180	593	4539, 35 4539, 21	4535.00	4536.90	1.00	1.09	22.9	35.0	3, 10	50.	594.	0
70	2	5. 250 5. 320	565 539	4539.21	4535.00 4535.00	4536, 85 4536, 80	1.00 1.00	1.09 1.10	23. 1 23. 2	35.0	3.10	50.	566. 520	C
78	2	5. 320	514	4539.07	4535.00	4536. 20	1.00	1.10	23. 2 23. 4	35. 0 35. 0		50. 50.	539. 516	C C
79	2	5. 460	491	4538.83	4535.00	4536.70	1.00	1.10	23. 4	35.0		50.	515. <b>4</b> 92,	c c
80	2	5. 530	470	4538.71	4535.00	4536, 66	1.00	1.10	23.6	35.0		50.	470.	č
81	2	5. 600	449	4538.60	4535.00	4536.62	1.00	1.10	23.7	35.0		50.	450.	ċ
82	2	5.670	430	4538.50	4535.00	4536.58	1.00	1.10	23. 8	35.0		50.	431.	, (
83	2	5. 740	413	4538.40	4535.00	4536, 54	1.00	1.10	23, 9	35.0	3.10	50.	413.	ć
84	2	5.810	396	4538. 30	4535.00	4536, 50	1.00	1.10	24. 0	35. 0		50.	396.	(
85	2	5. 880	380	4538. 21	4535.00	4536, 46	1.00	1.10	24. 1	35. 0	3.10	50.	380.	(
86	2	5. <del>9</del> 50	365	4538, 13	4535. 00	4536, 43	1.00	1.10	24. 2	35. 0	3. 10	<b>50</b> .	365.	(
87	2	6. 020	351	4538.04	<b>4</b> 535. 00	4536, 40	1.00	1.10	24. 3	35. 0	3. 10	<b>5</b> 0.	351.	(
88	2	6. 090	337	4537, <del>96</del>		4536, 36	1.00	1.11	24. 4	35. 0	3.10	50.	338.	ť
89	2	6. 160	325	4537.89		4536, 33		1.11	24. 5	35. 0	3. 10	<b>50</b> .	325.	· (
90	2	6. 230	313			4536. 30		1.11	24. 6	35. 0		<b>50</b> .	313.	1
91	2		301			4536, 28	1.00	1.11	24. 7	35. 0		50.	302.	1
92	1	6. 370	291	4537.68	4535.00	4536.25	1.00	1.11	24.7	35.0		50.	291.	1
93	1	6, 440	281	4537.62	4535, 00	4536, 22		1.11	24. 8	35.0		<b>50</b> .	281.	I
94 05	1	6.510 6.590	271	4537.56	4535.00	4536.20		1.11	24.9	35.0		50. 50	272.	I
95 96	1 1	6.580 6.650	262 253	4537.50 4537.44	4535.00	4536, 17		1.11	24.9	35.0		50. 50	262.	
97	1	6. 720	200 245	4537.39	4535.00 4535.00	4536, 15 4536, 13		1.11 1.11	25. 0 25. 1	35.0		50. 50	254. 246	
98	1	6. 720 6. 790	240 237	4537.39	4535.00	4536, 13	1.00		25. 1 25. 1	35. 0 35. 0		50. 50.	246. 238.	
99	1	6.860	230			4536.09	1.00			35.0		50. 50.	238. 230.	
100	1	6, 930	223		4535.00		1.00				3.10	50.	230.	
	,	4, <b>40</b> 4	****	1941) NT	1000.00				£9. £	<b>UU. V</b>	V. IV	<i>.</i>	ELJ.	

#### RESERVOIR DEPLETION TABLE

ł	к	TTP(I)	Q(I)	H2	YB	D	SUB	VCOR	OUTVOL	BB	COFR	QI (I)	OBRECH	QSPIL
u <b>ķ</b>	**	*****	******	*****	*****	*****	****	****	******	****	****	****	*****	****
11	1	7.000	216	4537.19	4535.00	4536.05	1, 00	1, 11	25. 3	35. 0	3, 10	50.	217.	0.
)2	1	7.077	209	4537.15	4535, 00	4536.03	1.00	1. 11	25.4	35.0	3.10	50.	209.	0,
13	1	7. 162	202	4537.09	4535.00	4536.01	1.00	1.11	25.4	35. 0	3, 10	50.	202	0,
14	1	7. 255	194	4537.04	4535.00	4535. 98	1.00	1.11	25. 5	35. 0	3, 10	50.	195.	0.
+5	1	7.357	186	4536. 98	4535.00	4535, 96	1,00	1. 12	25. 6	35. 0	3. 10	50.	187.	0.
۱Ĝ	1	7. 470	178	4536. 93	4535.00	4535. <del>9</del> 4	1.00	1. 12	25. 6	35. 0	3.10	50.	179.	0.
17	1	7. 594	170	4536.87	4535.00	4535. 91	1.00	1. 12	25. 7	35. 0	3.10	50.	171.	0.
·8	1	7. 731	162	4536, 81	4535. 00	4535.88	1,00	1.12	25. 8	35. 0	3.10	50.	162.	0.
9	1	7. 881	. 154	4536. 74	4535.00	4535.86	1.00	1.12	25. 9	35. 0	3. 10	50.	154.	0,
0	1	8. 046	145	4536. 68	4535.00	4535. 83	1.00	1.12	26. 0	35. 0	3, 10	50.	146.	0.
1	1	8. 227	137	4536.62	4535.00	4535.80	1.00	1.12	26. 1	35. 0	3.10	50.	138.	0.
2	1	8. 427	129	4536, 55	4535.00	4535.77	1.00	1.12	26. 2	35. 0	3.10	50.	129.	0.
3	1	8.647	121	4536.49	4535, 00	4535.74	1,00	1.12	26. 3	35.0	3.10	50.	122.	0.
4	1	8.888	113	4536.42	4535.00	4535.71	1.00	1.12	26.4	35. 0	3.10	50.	114.	.0.
5	1	9.154	106	4536, 36	4535, 00	4535. 69	1.00	1. 12	26.5	35. 0	3, 10	50.	107	0.
6	1	9. 446	99	4536, 30	4535, 00	4535. 66	1.00	1. 12	26. 6	35.0	3.10	50.	100.	0.
7	1	9. 768	93	4536, 24	4535.00	4535. 63	1.00	1.12	26. 7	35. 0	3.10	50.	93.	· 0.
8	1	10. 122	87	4536, 19	4535.00	4535. 61	1.00	1.12	26.8	35. 0	3.10	50.	87.	0.
9	2	10.511	81	4536.14	4535.00	4535, 59	1.00	1.13	26. 9	35. 0	3.10	50.	82.	0.
0	2	10. <b>9</b> 39	76	4536. 09	4535. 00	4535. 56	1,00	1.13	27. 0	35. 0	3, 10	50.	76.	0.
1	2	11.410	71	4536.04	4535.00	4535.54	1.00	1.13	27. 2	35. 0	3.10	50.	72.	0.
2	2	11. 928	67	4536.00	4535, 00	4535. 52	1.00	1.13	27.3	35. 0	3.10	<b>5</b> 0.	68.	0.
3	2	12. 498	64	4535, 97	4535.00	4535. 51	1.00	1.13	27.4	35. 0	3.10	50.	64	0.
4	2	13.125	61	4535. 94	4535, 00	4535. 49	1.00	1.13	27.6	35. 0	3, 10	50.	61	0.
5	2	13.814	58	4535. 91	4535.00	4535.48	1.00	1.13	27.7	35. 0	3, 10	50.	59	0.
6	2	14. 573	56	4535.89	4535.00	4535. 47	1,00	1.13	27. 9	35.0	3, 10	50	57.	0.
7	2	15. 407	54	4535, 87	4535.00	4535.46	1.00	1.13	28. 0	35. 0	3. 10	50.	55.	0.
8	2	16. 325	53	4535.85	4535.00	4535.46	1.00	1.13	28. 2	35. 0	3.10	50.	53.	· 0.
9	2	17. 334	52	4535.84	4535.00	4535.45	1.00	1.13	28.4	35. 0	3, 10	50.	52.	0.
0	1	18. 445	51	4535.83	4535, 00	4535, 44	1,00	1. 13	28.6	35. 0	3.10	50.	52.	0.
1	1	19.666	51	4535, 83	4535, 00	4535. 44	1.00	1, 13	28. 8	35. 0	3.10	50.	51.	0.
2	1	21.010	50	4535. 82	4535. 00	4535.44	1.00	1.13	<b>29</b> . 1	35. 0	3.10	50.	51.	0.
3	1	22. 488	50	4535. 82	4535. 00	4535. 44	1,00	1, 13	29. 4	35. 0	3, 10	<b>50</b> .	50.	0.

...

3

,

PARAMETER ***********************************	UNITS ******* CMIS	VARIABLE ++++++ Q(1)	VALUE ************* 50.
MAX FLOW	CMS	QM	2638.
FINAL FLOW	CMS	Q (NU)	50.
TIME TO MAX FLOW	HRS	TP	3. 50
NUMBER OF TIME STEPS		NNU	133
TOTAL VOLUME DISCHARGED FROM RESERVOIR	MILLION CU M	DISVOL	29.

#### INITIAL CONDITIONS

(	QDI(1), 1=1,	N)					
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	120.	120.	120.	120.	120.
120.	120.	120.	120.	1 20.	120.	120.	120.
120.	120.	. 120.	120.	120.	120.	220.	220.
220.	220.	220.	220.	220.	220.	220.	220.
220.	220.	220.	220.	220.	220.	220.	220.
220.	<b>220</b> .	220.	220.	220.	220.	220.	220.
220.	220.	220.	220.	220.	220.	220.	220.
220.	220.	220.	220.	220.	220.	220.	<b>22</b> 0.
220.	220.	220.	220.	220.	220.	220.	220.
220.	<b>220</b> .	220.	220.	<b>220</b> .	<b>220</b> .	220.	220.
220.	220.	<b>220</b> .	220.	220.	220.	220.	220.
220.	<b>220</b> .	220.	220.				
(	YI(I),  =1,	N)					
4535.44	4459.05	4382.67	4306. 27	4229. 89	4153.50	4077.11	4000. 72
3924, 33	3847. 94	3771.56	3695.16	3618, 78	3542. 38	3466, 00	3389. 61
3313. 22	3236, 83	3160. 45	3077. 59	2994.38	2911.25	2828. 05	2744. 92
2661.72	2578. 59	2495. 39	2412. 25	2329.06	2245. 92	2162. 74	2079, 58

3313. 22	3236, 83	3160.45	3077. 59	2994.38	2911.25	2828. 05	2744. 92
2661.72	2578. 59	2495. 39	2412. 25	2329.06	2245. 92	2162. 74	2079. 58
1996, 41	1913. 26	1830. 09	1746. 93	1663.76	1580.60	1556.87	1532.77
1508.66	1484. 55	1460. 44	1436, 33	1412. 23	1388.12	1364.01	1339, 90
1315.80	1291. 69	1267.58	1243. 48	1219. 37	1195. 27	1171.17	1151.17
1131.17	1111.17	1091.17	1071.18	1051.18	1031, 18	1011. 18	991, 19
971. 19	951. 1 <del>9</del>	931, 19	911.20	891.20	871.20	851.20	831. 21
811.21	791. 21	771 <i>.</i> 21	751. 22	731. 22	711. 22	691.22	671. 23
651.23	631. 23	611.24	591.24	571. 24	552. 08	532. 91	513.75
494, 59	475. 44	456. 28	437. 13	417.97	398. 82	379.67	360. 52
341.37	322. 23	303. 08	283. 93	264. 79	245. 64	226. 50	207. 35
188. 21	1 <b>69</b> . 07	149. 93	130, 78				

TIME PARAMETERS OF OUTFLOW HYDROGRAPH INMEDIATELY DOWNSTREAM OF DAM

PARAMETER ***********************************		VAR1ABLE *****	VALUE *******
TIME TO FAILURE	HR	TFH	3. 500
TIME TO START OF RISING LIMB OF HYDROGRAPH	HR	TFO	0.000
TIME TO PEAK	HR	TP	3. 500
TIME STEP SIZE	HR	DTHI	0. 175
ROUTING COMPLETED.			
KTIME≂ 79 ALLOWABLE KTIME= 699	TT≂	24. 5	
PROFILE OF CRESTS AND TIMES FOR	1 <b>994</b> GLO	F	

BELOW RUN1 1 :

DISTANCE FROM DAM	MAX ELEV	MAX FLOW	TIME MAX	MAX VEL	FLOOD ELEV	TINE SLOOD
KN		CMS	ELEV-HRS	M/S	N	TIME FLOOD ELEV-HRS
******	*****	****	*****	******	m ******	****
0.000	4539, 52	2580	3. 522	9. 67	0.00	0. 00
2. 027	4463.15	2585	3. 522	9.67	0.00	0. 00
4. 055	4386.75	2583	3. 522	9. 71	0. 00	0.00
6. 082	4310. 37	2577	3. 522	9.69	0.00	0.00
8.110	4233. 97	2567	3. 522	9. 72	0, 00	0, 00
10. 137	4157.58	2554	3. 522	9, 70	0,00	0, 00
12. 165	4081.17	2539	3. 522	9. 72	0,00	0, 00
14, 192	4004.80	2542	3. 697	9, 72	0. 00	0. 00
16. 220	3928.40	2544	3. 697	9. 77	0. 00	0.00
18. 247	3852.02	2540	3.697	9. 76	0.00	0. 00
20. 274	3775. 63	2539	3. 784	9.80	0.00	0, 00
22. 302	3699, 25	2537	3. 784	9.81	0.00	0. 00
24. 329	3622.85	2533	3.872	9.84	0.00	0.00
26. 357	3546.48	2534	3.872	9.85	0.00	0.00
28. 384	3470.08	2531	3.872	9.88	0.00	0.00
30. 412	3393. 70	2523	3.872	9.89	0.00	0.00
32. 439	3317.30	2511		9. 91	0.00	0, 00
34.466	3240.92	2513	4.047	9.93	0.00	0. 00
36, 494	3164, 53	2515	4.047	9. 97	0.00	0.00
38. 578	3081.25	2582	4.047	10. 27	0.00	0.00
40. 662	2998.13	2576	4.047	9, 90	0.00	0.00
42. 745	2914.81	2566	4.047	10.00	0.00	0.00
44. 829 46. 913	2831.68	2567	4. 222	9, 70	0.00	0.00
48.997	2748.40	2569	4. 222	9.77	0.00	0.00
51.081	2665.25 2581.98	2566	4. 222	9.52	0.00	0.00
53, 165	2498.82	2559 2548		9.56	0.00	0.00
55. 249	2415.58	2554	4. 222 4. 397	9.34 0.28	0.00	0,00
57.333	2332. 41	2555	4. 397	9.3 <del>6</del> 9.19	0.00	0.00
59. 416	2249. 17	2552	4. 397	9. 19 9. 19	0.00	0.00
61. 500	2165. 99	2542	4. 397	9. 19 9. 03	0.00 0.00	0.00 0.00
63. 584	2082.77	2542	4. 572	9,03	0.00	0.00
65. 668	1999.60	2545	4. 572	8.90	0.00	0.00
67, 752	1916. 38	2540	4. 572	8. 88	0.00	0.00
69. 836	1833. 19	2528	4. 572	8.75	0.00	0.00
71. 920	1749. 98	2530	4. 747	8.73	0.00	0.00
74. 003	1666.80	2529	4. 747	8.63	0.00	0.00
76. 087	1583. 59	2524	4, 747	8.60	0.00	0.00
78. 128	1562.56	2615	4, 747	4. 35	0.00	0.00
80. 169	1535.43	2620	4. 922	10.04	0, 00	0.00
82. 210	1514.50	2615	4. 922	4.40	0.00	0.00
84. 251	1487. 24	2609	5. 097	13. 02	0.00	0.00
86. 291	1466, 41	2608	4. 922	4.46	0.00	0.00
88. 332	1439.06	2607	5. 272	12.51	0.00	0.00
90. 373	1418, 33	2598	5. 097	4. 53	0.00	0.00
92. 414	1390, 90	2609	5. 447	12.24	0.00	0.00
94, 455	1370. 22	2589	5, 272	4, 63	0.00	0.00
96, 496	1342.74	2598	5. 447	12. 59	0.00	0.00

. . . . . .

.

. . .. .

PROFILE OF CRESTS AND TIMES FOR 1994 GLOF BELOW RUNI 1 :

DISTANCE FROM DAM	MAX ELEV	MAX FLOW	TIME MAX	MAX VEL	FLOOD ELEV	TIME FLOOD
KM	Mar 🗸	CHIS	ELEV-HRS	M/S	M	ELEV-HRS
******	******	*****	*******	****	*****	*******
98, 536	1322. 14	2581	5.097	4.73	0.00	0. 00
100, 577	1294, 60	2580	5. 622	13.83	0,00	0.00
102, 618	1274.09	2568	5. 272	4.82	0.00	0.00
104, 659	1246. 44	2553	5. 797	13.14	0.00	0.00
106, 700	1226.03	2552	5. 447	4.94	0.00	0.00
108.741	1198.27	2551	5.972	13.03	0.00	0.00
110, 781	1177.99	2564	5. 622	5.06	0.00	0.00
112, 804	1154, 79	2567	5. 972	10.31	0.00	0.00
114, 827	1138.16	2568	5. 797	4.93	0.00	0.00
116.850	1114.60	2577	5. 972	11.51	0.00	0.00
118.873	1098.37	2563	5. 797	4.82	0.00	0.00
120, 896	1074.44	2579	5. 972	12.31	0.00	0.00
122, 919	1058.56	2579	5.972	4.72	0.00	0.00
124.942	1034.29	2574	6, 147	12.86	0.00	0.00
126, 965	1018.73	2584	6. 147	4.64	0.00	0.00
128, 988	994.13	2570	6. 322	13.36	0.00	0,00
131.011	978.87	2579	6. 322	4. 57	0.00	0.00
133, 034	954.00	2573	6. 322	13.83	0.00	
135. 057	938, 96	2566	6. 497	4.51	0.00	0.00
137, 080	913. 92		6. 497	4.01 14.18		0.00
139, 103		2581			0.00	0.00
	899.08 972.95	2567	6. 497	4.46	0.00	0.00
141.126	873, 85 850, 16	2569	6.672	14.36	0.00	0.00
143, 149	859, 16	2574	6.672	4.45	0.00	0.00
145.172	833, 80 810, 80	2552	6.847	14.38	0.00	0.00
147.195	819.20	2568	6.847	4.43	0,00	0.00
149, 218	793.77	2568	6.847 7.000	14.34	0,00	0.00
151.241	779. 21	2552	7.022	4, 41	0,00	0.00
153. 264	753, 77	2567	7.022	14, 47	0,00	0.00
155. 287	739.25	2545	7.022	4.40	0.00	0.00
157, 310	713.77	2553	7.197	14. 57	0,00	0.00
159.333	699, 29	2554	7.197	4, 41	0.00	0.00
161.356	673.75 650.00	2529	7.372	14, 58	0,00	0.00
163, 379	659.30	2547	7.372	4, 41	0.00	0.00
165, 402	633, 74	2538	7.372	14, 53	0,00	0.00
167, 425	619.29	2529	7.547	4.40	0.00	0.00
169.448	593, 77 570, 20		·· 7.547	14. 41	0,00	0.00
171, 471	579.30	2507	7.547	4, 38	0, 00	0.00
173, 545	554, 75	2526	7.722	13,05	0.00	0.00
175.618	540, 71	2515	7.722	4, 21	0,00	0.00
177.692	516.20	2506	7.897	13, 53	0.00	0, 00
179.766	502.14	2511	7.897	4.06	0.00	0.00 .
181.839	477.61	2477	7.897	13, 83	0,00	0, 00
183, 913	463.50	2457	8. 247	3,90	0.00	0, 00
185, 986	439. 25	2503	8. 247	14.01	0.00	0, 00
188,060	425.09	2513	8. 247	3, 81	0.00	0.00
190, 133	400, 71	2476	8. 247	14, 18	0.00	0.00
192. 207	386. 46	2445	8. 597	3, 68	0.00	0.00

194, 281	362, 39	2495	8. 597	14. 24	0.00	0.00
F	ROFILE OF CRESTS			1994 GLOF	•	
	BELO	W RUN1 1	:		·•	

DISTANCE FROM DAM KM *******	MAX ELEV M ********	MAX FLOW CMS *******	TIME MAX Elev-hrs *******	MAX VEL . M/S +++++++	FLOOD ELEV M *********	TIME FLOOD ELEV-HRS
196. 354	348.09	2494	8, 597	3.60	0.00	0. 00
198, 428	323, 91	2434	8. 947	13. 99	0.00	0.00
200. 501	309.50	2435	8. 947	3, 49	0,00	0, 00
202, 575	285, 58	2473	8. 947	14, 19	0.00	0. 00
204, 648	271.12	2447	8. <del>9</del> 47	3.40	0.00	0.00
206. 722	247, 17	2375	9, 297	14. 26	0.00	0.00
208. 795	232. 57	2403	9, 297	3.32	0, 00	0. 00
210, 869	208.82	2427	9. 297	13.86	0.00	0.00
212. 943	194, 18	2386	9. 297	3, 22	0.00	0.00
215.016	170. 44	2328	9, 647	14.17	0.00	0, 00
217.090	155.70	2368	9. 647	3.17	0.00	0.00
219, 163	132.08	2378	9. 647	13.72	0.00	0.00

.

. •

.

١

#### DISCHARGE HYDROGRAPH FOR 1994 GLOF ... STATION NUMBER 1 BELOW RUNI 1 : AT KM 0.00

GAGE ZERO = 4535.00 M MAX ELEVATION REACHED BY FLOOD WAVE = 4539.52 M FLOOD STAGE NOT AVAILABLE MAX STAGE = 4.52 M AT TIME = 3.522 HOURS MAX FLOW = 2580 CMS AT TIME = 3.522 HOURS

TIME	STAGE	FLOW								
HR .	M	CHIS	0	1000	2000	3000	4000	5000		
0. 0-	4535. 0 🚲	· 0	*							
0.2	0.5	57	. *	•	•	•	•		. •	
0.4	0, 6	87	. *	•	•	¢.	ĸ	•		
0.6	0.8	148	. *	•	•.	· •				
0.8	1.1	244	*	•	•		•	•		
1.0	1.4	371	. *	•		•	•			
1. <b>2</b>	1, 8	528	•	* .	•	•	•			
1.4	2. 1	717	•	* .			•	•		
1.6	2.5	929	•	≠.	•	•	•	•		
1.8	2.8	1161	•	. *	•	•	•	•		
2. 0	3. 2	1405	•	. +	k .	•	•			
2. 2	3.5	1643	•	•	* .	•	•	•		
2.4	3.7	1865	•	•	*.	•		•		
2.6	4.0	2066	·	•	. *	•	•	•		
2, 8	4.2	2240	•	•	. *	•	•	•		
3.0	4.3	2386	·			*	•	•		
3.2	4.4	2502	•		•	* .	-	•		
3.4	4.5	2576	•	•	•	* ,	•	•		
3.6	4.3	2384	•	•		<b>≭</b> .	,	•		(x, t)
3.8	3.8	1921	•	•	<b>.</b>	•	•	•		
4.0 4.2	3.4	1578 1304	·	•	<del>•</del> .	•	•	•		
4. Z 4. 4	3. 0 2. 7	1089	•		•	•	•	•		
4.6	2.5	922	•		•	•	•	•		
4. B	2.3	787	•		•	•	•	•		
5.0	2. 1	677	•	* · *		•	,	•		
5.2	1.9	587	•	* .	•	•	•	•		
5.4	1.8	513	·	* .	•	•	•	•		
5.6	1.6	451		*	•	•	•	•		
5, 8	1.5	399	. *				•			
6.0	1.4	355	. *							
6. 2	1.3	319	. *					•		
6.4	1.2	287	. *							
6. 6	1. <b>2</b>	260	. *							
6.8	1.1	237	. *							
7.0	1. 1	217	. 🔹			•				
7.2	1, 0	1 <del>9</del> 9	. *							
7.4	1.0	184	. *	•	•					
7.6	0, 9	170	. *	•	· · ·		•			
7.8	0.9	159	. *							
8, 0	0.8	148	. 🕈	•	•	•		. •		
8, 2	0.8	139	. *	•	•	•	•			
8.4	0, 8	131	. *	•	•	•		•		
8, 6	0.8	123	.*	•	•		•			
8.8	0.7	117	.*	•	•	•	•	•		
9,0	0.7	111	. *	,	•	•	٠	•		
9.2	0.7	106	, <b>*</b>	•	•	•	•	,		
9.4	0.7	101	.*	•	•	•	•	•		
9.6	0.7	97 02	.* .*	•	•	•	•	•		
9.8 10.0	0.6 0.6	93 89	. <del>*</del> . <b>*</b>	•	•	•				
IV. V	U. 0	09	. +	•	•	•	•	,		

0405	E 7EDA -								3.49 (FLOOD W	AVE	3164	53 M	
GAGE	- ZCKU -				NOT AVA			וסי	FLOOD W	AVC -	3104.	03 M	
		MAX ST.	AGE =	4, 53	M	AT	TIME	=	4.047	HOURS			
		MAX FL	ow =	2515	CMS	AT	TIME	Ξ	4, 047	HOURS			
ME	STAGE	FLOW											
IR	M	CMS	0	1000	200	5	- 300	00	4000	ŧ	5000		
	3160.0	0	*										
), 5	0.4	51	.*						•		,		
	0.4	51		•				•	•		•		
. 5		51		•				·	•		•		
2.0 2.5	0.5 2.3	55 789		• ·				•	•		•		
1.5 3.0	2.3 3.6	789 1659		Τ.	*	•		•					
. 5	4, 2	2225		•	·г .	*			•		•		
. 0	4.5	2506			•		*	•			•		
l. 5	4.0	2034				*							
i. O	3. 1	1350			*								
5.5	2.6	955		*									
. 0	2.1	700		* .		•		•					
. 5	1.8	530		¥.		•		•	•		•		
1.0 1.5	1.6 1.4	413 330	· *	•				•			•		
1.0 3.0	1.4	330 270	· *	•		•		•			•		
3.5	1.1	225	. *						•				
9.0	1.0	190	*					•					
9. 5	0. 9	163	. *			-					•		
), ()	0.8	142	. *			•		,					
), 5	0.8	126	. *			•					•		
1.0	0.7	113	. *	•		•		•			•		
1.5	0.7	102	.*	•		•		·	•	,	-		
2.0 2.5	0.6 0.6	93 86	.*			•		•	-		•		
3.0	0.6	80	. <del>*</del> . *	•		•		•	•		•		
3.5	0.6	75	.*			•		÷	•				
4.0		71	, <b>*</b>										
4.5	0.5	67	.*										
5.0	0.5	65	. *									-	
5.5	0.5	62	. *	•		•		٠					
8.0	0.5	60	. *	•		•					•		
6.5	0.5	59	.*	•		•		•			•		
7.0 7.5	0.5 0.5	57 56	.* .*	•		•		•		· .	•		
7.5 B.O	0.5	55	.* .*	•				•	,		•		
8.5	0.5	54	.*	:					•		•		
9.0	0.5	54	*										
9.5	0.5	53	.*										
D. O	0. 5	52	.*	··· •									
0.5	0.5	52	. *			•		•		•	•		
1.0	0.5	52	.*	,		•		·			•		
1.5	0.5	51 51	.*	•		•		•			•		
2.0 2.5	0. 4 0. 4	51 51	.* .*			·		·		•	•		
2.5 3.0	0.4	51	.* .*	•		•		•		•	-		
J. J	<b>V</b> . T	Ų1	• •	•		•		•		• • •	•		
												·.	

GAC	GE ZERO	= 1580, 00			ELEVATION NOT AVAIL	N REACHED BY	FLOOD WAVE	= 1583.59 N
			(AGE = .0W =			AT TIME = AT TIME =	4. 747 HOUR 4. 747 HOUR	
TIME	STAGE	FLOW						
HR	N	CMS	0	1000	2000	3000	4000	5000
	-1580.0	0						
0.5	0.6	125					•	
1.0	0.6	126	*			•	•	•
1.5	0.6	126	. <b>*</b>	-			•	
2.0	0.6	126			•	•	•	·
2.5	0.6	134	· · ·		•	•	•	•
2.5	0.6			•	•	•	•	•
3.0	0.8	188	· •	•	•	•	•	•
3. 5 4. 0	3.1	1962	. •	•		•	•	•
4.U 4.5			•	•	+			
	3.5	2439	•	•	•	* .	•	•
5.0	3.5	2441	•		•	* .	•	•
5.5	3.0	1885		•	*.	•	•	•
6.0	2.5	1372	•	• .	* .	٠	•	•
6.5	2. 2	1051	·	.*	·		•	
7.0	1.9	826	•	*.	•		•	•
7.5	1, 7	667	•	<b>*</b> ,			•	•
8.0	1.5	551		* .		•	٠	•
8.5	1.3	463	. '	¥ .	•		•	•
9.0	1.2	396	. *					
9.5	1. 1	345	. *					
10. 0	1.0	304	. +	•				
10. 5	1.0	272	. *					
11.0	0, <del>9</del>	246	<b>.</b> +					
11.5	0, 9	225	. *	•			•	
12.0	0.8	208	. 🔹			-		•
12.5	0, 8	194	. *				•	
13.0	0, 8	182	, 🔹				•	
13. 5	0.8	172	. *					•
14. 0	0, 7	164	. *		•	•	•	
14. 5	0, 7	157	, +					
15.0	0, 7	151	. *					•
15. 5	0.7	146	.*					
16. 0	0, 7	142	.*				•	
16.5	0, 7	139	. *				-	
17.0	0.7	136	.*					
17.5	0,6	133	*			•	•	
18.0	0,6	131	.*			<b>.</b>		
18.5	0, 8	129	.*					
19.0	0.6	128	*				•	
19, 5	0.6	127					•	
20.0	0.6	126		•	•	*	*	
20.5	0.6	125		•	•	•	•	•
20. 5	0.6	125		•	•	•	•	
21.0	0.6	123		·	•	•		•
				•		•	•	•
22. O	0.6	125		•	•	•	•	
22, 5	0.6	125	.*					

· · · ·

۰ .

GAG	F ZERO	= 1170 00	) M	MAY	FLEVATION	REACHED BY	FLOOD WAVE	≈ 1177 99 M	
Q/ 10					NOT AVAILA			- 1 <i>111</i> .30 M	
				7. 99		T TIME =			
		MAX FL	.O₩ =	2564	CMIS /	T TIME =	5.622 HOUR	NS .	
INE	STAGE	FLOW							
HR	M	CMS	0	1000	2000	3000	4000	5000	
0. 0-	1170. 0	0	*				•		
0.5	2. 3	293	. *					-	
	2.3	295	. *	*					
1.5	2.3	296	. *	•	•	•		•	
2.0	2.3	296	- *		•	•		•	
2.5	2.4	308	、 *	•	•			•	
3.0	2.4	320		•	•	•	•	•	
3.5	2.5	320		• •	•	•	•	•	
4.0 4.5	3.8 4 5	525		≠ . ⊥			•	•	
4.5 5.0	4.5 5.8	700 1150		τ <sup>τ</sup> .		•	•	•	
5.5	5.8 7.9	2511		, •	• •	• ·		•	
6.0	7.8	2515	•	•	•	• ·	•	•	
6.5	7.1	2110	•	•		÷ .	-	•	
7.0	6.3	1648		•	*	•		•	
7.5	5.6	1319		•	*	•	•	•	
8.0	5.0	1087		. *			•		
8. 5	4.5	911		*					
9.0	4, 1	776		*					
9.5	3.8	674		* .					
0.0	3.5	591		* .			•		
0.5	3. 3	528		* .					
1.0	3.1	476		* .					
1.5	3, 0	434	. *			,	•	•	
2.0	2.8	400	. *			•		• .	
2.5	2.7	371	. *	• •		•			
3.0	2.6	348	. *	•	•		•		
3.5	2.5	331	、 *	•		•		•	
4.0	2.5	320	. *	•	•			•	
4.5	2.4	312	. *	•	•	•		•	
5.0  5.5	2.4 2.4	307 302	. *	•	•	-			
15. 5 16. 0	2.4	298	. *	,	•	•		•	
6.5	2.3	296	*	•	•	•	•	•	
7.0	2.3	293	*		•	•	•	•	
17.5	2.3	291	*	•	•	•	•	•	
8.0	2.3	289	*			•	•	•	
8.5	2.3	287	*					•	
9.0	2.3	286	. *	•		•			
19.5	2. 2	285	. *						
20. 0	2. 2	284	. *					•	
20.5	2. 2	283	. *	•	•				
21.0	2. 2	282	. *		,				
21. 5	2. 2	282	, *						
22.0	2. 2	282	. *						
22. 5	2.2	281	. *	•	•	•		-	
23. 0	2. 2	281	. *						

.

DISC	HARGE HY	DROGRAPH FOF BELOW RUN	t 1994 ≰1 1 :	GLOF AT 1		TION NUMBER	85	
		F70 00 M	MAV CI	EVATION D		FLOOD WAVE	- 570 20 M	
GAGE	ZERO =	570.00 M	NOD STAGE N			FLUUD WAVE	- 379.30 M	
		MAX STAGE =			TTIME =	7,547 HOUR	s	
		MAX FLOW =	2508 C		T TIME =	7.547 HOUR		
			2000 0				-	
TIME	STAGE	FLOW						
HR	M ·	CMS 0	1000	2000	3000	4000	5000	
0.0 -		0 *				•		
0.5	3. 9	465 .	* .		•			
1.0	4. 1	<b>529</b> .	* .			•		
1.5	4. 2	535 .	*			•	•	
2.0	4.2	535 .	*	•	•	•	•	
2.5	4. 2	542 .	<b>*</b> ,	•	•	•	•	
3.0	4. 3	562 .	*,	•		•		
3.5	4. 3	570 .	* .		•	•		
4.0	4.6	624 .	* .	•	-	•	•	
4.5	4.8	660 .	* .	•	•	•	•	
5.0	4,9 E 0	685 . 709	* , •	•	•	•	•	
5.5	5.0	702	* .	•	•	•		
6.0 C.5	5.0	721 . 775 .	*. *	•		•		
6.5	5.3		···		•	-	•	
7.0 7.5	6.6 9.2	1131 . 2426 .	. •	·	* .		•	
8.0	9. 2 8. 9	2318		•	*		•	
8.5	8.2	1980	•	*				
9.0	7.5	1648	•	* .				
9.5	6.9	1386		*		-	-	
10.0	6, 4	1180	. *				•	
10.5	5.9	1024	*					
11.0	5. 5	895	*					
11.5	5. 2	790	*.				•	
12.0	4. 9	704 .	<b>*</b> ,					
12.5	4.6	636	* .			•		
13.0	4. 5	<b>6</b> 01 .	* .			•	•	
13. 5	4.4	580	* .	•	•	-		
14. 0	4.3	561 .	*.		•	•		
14. 5	4. 2	547	<b>*</b> .	•				
15.0	4.2	534	* .	•	•	•	•	
15.5	4.1	524	*	•	•	•	٠	
18.0	4, 1	516 .	* 、	•		•		
16.5	4, 1	510 .	* .	•	•	•		
17.0	4,0	504	∓ . ★	,	•	•	•	
17.5	4.0	499 . 495	÷		•	•		
18. 0 18. 5	4. 0 4. 0	495 . 491 .	* .	•	•		•	
18. 0 19. 0	4,0 3,9	488	*	•	•		•	
19.0	3.9	485 .	*	•	•		•	a.
20.0	3.9	483 .	*	•	•	•		
20.0	3.9	481 .	* .		•			
20. 5	3,9	479 .	*		· ·	•	•	
21.5	3,9	477 .	*					
22. 0	3,9	475	*					
22. 5	3, 9	474	*		•			
23. 0	3.9	473 .	* .					

DIS	CHARGE								STA		MBER	108		
		BE	LOW	RUNT	1:		A	I KN	<b>1</b> 219	. 16				
GAG	e zero	= 13	0. 00		MAX STAGE				EACHED BY	FLOOD	WAVE =	132.	08 M	
		MA	x st	AGE =	2.08				TIME ≓	9.647	HOURS			
				OW =					TIME =			:		
	STAGE		LOW											
HR	M 100 0		CMS		500		1000		1500	200	0	2500		
	~130.0		0		•		•		•		•	•		
0.5 1.0	0.8 0.8		480 619	• .	· *		•		•		•	•		
1.5	0.8		665			*	•		•		•	•		
2.0	0. B		671	•	•	*	:		•					
2.5	0.8		672			*								
3.0	0.8		676			*								
3. 5	0.8		681			*								
4.0	0.8	(	693			*								
4.5	0.8		<b>698</b>			*			•			•		
5.0	0.8		706	•		*					,	•		1 A
5.5	0.8			•	•	*	•					•		
6.0	0.8			•	•	*	•		•		,	•		
6.5	0.8			•	•	*	·		•		•	•		
7.0 7.5	0.8 0.8		732 752	•	•	*	•		•			•		
8.0	0.8		B05	•	•		•		•			•		
8.5	0.8		~~~		•	•	*.				,	•		
9.0	1.1		491		÷				*			•		
9.5	1. 9		230								*			
10.0	2.0	2	171								*			
10.5	1.7	1	794							*				
11.0	1.5	1	55 <del>9</del>						. *			•		
11.5	1.4		363		•		•		* .			•		
12.0	1.2		189		•		•	4	<b>۲</b> .			•		
12.5	1.1		053	•			. '	k.	•		•	•		1 - E
13, 0 13, 5	1.0		940 P44	•	•		*.		•		•	•		
14.0	1.0 0.9		844 764	•	·	*	Ŧ.		•		•	·		
14.5	0.8		701	•	•	*	•		•		•	•		
15.0	0.8		678			*								
15.5	0.8		674			*						•		
16.0	0, 8		668			*								. •
16.5	0.8		661			*								
17.0	0.8		657	•	•	*					•	•		
17.5	0.8		653	•	•	*	•				•	•		
18.0	0.8		649	•	•	*	•		•		•	•		
18.5 19.0	0.8 0.8		646 643	·	•	*	•		•		•	•		
19.5	0.8		640	•	•	*	•		•		•	•		
20.0	0.8		638	•	•	*	•		•		-	•		
20.5	0.8		635			*						:		
21.0	0, 8		633	•		*			•		•	•		
21. 5	0.8		632			*								
22. 0	0.8		630			*					•			
22. 5	0.8		628			*					•	•		
23. 0	0.8		627	•	•	*					•		•	

#### DISCHARGE HYDROGRAPH FOR 1994 GLOF STATION NUMBER 108

## Calculation Result of DAMBRK (2/3)

# Simulation of GLOF from Luggye Lake

#### ANALYSIS OF THE DOWNSTREAM FLOOD HYDROGRAPH

#### PRODUCED BY THE DAM BREAK OF

RUN2 :

ON

Luggye Lake

#### ANALYSIS BY

#### BASED ON PROCEDURE DEVELOPED BY DANNY L. FREAD, PH. D., SR. RESEARCH HYDROLOGIST

#### QUALITY CONTROL TESTING AND OTHER SUPPORT BY JANICE M. LEWIS, RESEARCH HYDROLOGIST

HYDROLOGIC RESEARCH LABORATORY W23, OFFICE OF HYDROLOGY NOAA, NATIONAL WEATHER SERVICE SILVER SPRING, MARYLAND 20910 INPUT CONTROL PARAMETERS FOR RUN2 :

PARAMETER *******	VARIABLE +++++++++	VALUE Homosofick
NUMBER OF DYNAMIC ROUTING REACHES	KKN	1
TYPE OF RESERVOIR ROUTING	KUI	0
MULTIPLE DAM INDICATOR	MULDAM	0
PRINTING INSTRUCTIONS FOR INPUT SUMMARY	KDMP	5
NO. OF RESERVOIR INFLOW HYDROGRAPH POINTS	ITEH	2
INTERVAL OF CROSS-SECTION INFO PRINTED OUT WHEN JN	K=9 NPRT	0
FLOOD-PLAIN MODEL PARAMETER	KFLP	0
METRIC INPUT/OUTPUT OPTION	METRIC	1

IOPUT= 1 0 0 0 0 0 1 1 0 0 0

ELEVATION OF BOTTOM OF BREACH

÷

RUN2 : RESERVOIR

YBMIN

M

4535.00

TABLE OF ELEVATION VS SURFACE AREA

	EX (SO KU)	ELEVATION ()	n	
		•	-	
	(K)	HSA (I		
	oleieleieleieleie	ieksk skoletekskoleteks	ojojojojek	
	1.0	4560. 00		
-				
	1.0	4535.00		
	0.0	0, 00		
	0.0	0, 00		
	0.0	0, 00		
	0.0	0, 00		
	0. 0	0.00		
	0.0	0.00		
RUN2 :	RESERV	OIR AND BREACH	I PARAMETEI	RS
PARAMETER		INITS	VARIABLE	VALUE
	a a la			
LENGTH OF RESERVOIR		NW.	RLM	2.10
ELEVATION OF WATER SURFAC	E	M	YO	4561.00
SIDE SLOPE OF BREACH			Z	0, 00

WIDTH OF BASE OF BREACH	M	BB	35.00	
TIME TO MAXIMUM BREACH SIZE	HOUR	TFH	3. 50	
ELEVATION (MSL) OF BOTTOM OF DAM	M	DATUM	4535.00	
VOLUME-SURFACE AREA PARAMETER		VOL	0. 00	
ELEVATION OF WATER WHEN BREACHED	° <b>M</b> − s	HF	4561.00	
ELEVATION OF TOP OF DAM	M	HD	4561.00	
ELEVATION OF UNCONTROLLED SPILLWAY CREST	M	HSP	0. 00	
ELEVATION OF CENTER OF GATE OPENINGS	M	HCT	0. 00	
DISCHARGE COEF. FOR UNCONTROLLED SPILLWAY		cs	0. 00	·
DISCHARGE COEF. FOR GATE FLOW		CG	0. 00	
DISCHARGE COEF. FOR UNCONTROLLED WEIR FLOW		CD0	0. 00	·
DISCHARGE THRU TURBINES	CMIS	QT	50.00	
CDO SHOULD NOT BE 0.0 IF OVERTOPPING MAY OCC	CUR			
DHF (INTERVAL BETWEEN INPUT HYDROGRAPH ORDIN	ATES) =	0. 00	HRS.	
TEH(TIME AT WHICH COMPUTATIONS TERMINATE) =	24.00	00 HRS.		
BREX (BREACH EXPONENT) = 0.000				
MUD (MUD FLOW OPTION) = 0				
MUD(MUD FLOW OPTION) = 0 IWF(TYPE OF WAVE FRONT TRACKING) = 0				
IWF (TYPE OF WAVE FRONT TRACKING) = 0				
IWF (TYPE OF WAVE FRONT TRACKING) = 0 KPRES (WETTED PERIMETER OPTION) = 0 KSL (LANDSLIDE PARAMETER) = 0 INFLOW HYDROGRAPH TO RUN2 :	·		· · · · · · · · · · · · · · · · · · ·	
IWF (TYPE OF WAVE FRONT TRACKING) = 0 KPRES (WETTED PERIMETER OPTION) = 0 KSL (LANDSLIDE PARAMETER) = 0 INFLOW HYDROGRAPH TO RUN2 :				
IWF (TYPE OF WAVE FRONT TRACKING) = 0 KPRES (WETTED PERIMETER OPTION) = 0 KSL (LANDSLIDE PARAMETER) = 0 INFLOW HYDROGRAPH TO RUN2 :				
IWF (TYPE OF WAVE FRONT TRACKING) = 0 KPRES (WETTED PERIMETER OPTION) = 0 KSL (LANDSLIDE PARAMETER) = 0 INFLOW HYDROGRAPH TO RUN2 :				
IWF (TYPE OF WAVE FRONT TRACKING) = 0 KPRES (WETTED PERIMETER OPTION) = 0 KSL (LANDSLIDE PARAMETER) = 0 INFLOW HYDROGRAPH TO RUN2 : 50.00 50.00				
IWF (TYPE OF WAVE FRONT TRACKING) = 0 KPRES (WETTED PERIMETER OPTION) = 0 KSL (LANDSLIDE PARAMETER) = 0 INFLOW HYDROGRAPH TO RUN2 : 50.00 50.00 TIME OF INFLOW HYDROGRAPH ORDINATES	Luggj	ve Lake	· · · · · · · · · · · · · · · · · · ·	
IWF (TYPE OF WAVE FRONT TRACKING) = 0 KPRES (WETTED PERIMETER OPTION) = 0 KSL (LANDSLIDE PARAMETER) = 0 INFLOW HYDROGRAPH TO RUN2 50.00 50.00 TIME OF INFLOW HYDROGRAPH ORDINATES 0.0000 100.0000 CROSS-SECTIONAL PARAMETERS FOR	Luggy	ve Lake VARIABLE	VALUE	
IWF (TYPE OF WAVE FRONT TRACKING) = 0 KPRES (WETTED PERIMETER OPTION) = 0 KSL (LANDSLIDE PARAMETER) = 0 INFLOW HYDROGRAPH TO RUN2 : 50.00 50.00 TIME OF INFLOW HYDROGRAPH ORDINATES 0.0000 100.0000 CROSS-SECTIONAL PARAMETERS FOR BELOW RUN2 : PARAMETER			¥ALUE ********	
IWF (TYPE OF WAVE FRONT TRACKING) = 0 KPRES (WETTED PERIMETER OPTION) = 0 KSL (LANDSLIDE PARAMETER) = 0 INFLOW HYDROGRAPH TO RUN2 : 50.00 50.00 TIME OF INFLOW HYDROGRAPH ORDINATES 0.0000 100.0000 CROSS-SECTIONAL PARAMETERS FOR BELOW RUN2 :		VARIABLE		

\*

NUMBER OF CROSS-SECTIONAL HYDROGRAPHS TO PLOT	NTT	5
TYPE OF OUTPUT OTHER THAN HYDROGRAPH PLOTS	JNK	1
CROSS-SECTIONAL SMOOTHING PARAMETER	KSA	0
DOWNSTREAM SUPERCRITICAL OR NOT	KSUPC	1
NO. OF LATERAL INFLOW HYDROGRAPHS	LQ	5
NO. OF POINTS IN GATE CONTROL CURVE	KCG	0

NUMBER OF CROSS-SECTION WHERE HYDROGRAPH DESIRED (MAX NUMBER OF HYDROGRAPHS = 6)

1 2 3 4 5

CROSS-SECTIONAL VARIABLES FOR Luggye Lake BELOW RUN2 :

PARAMETER ***********************************	UNITS *******	VARIABLE *****
LOCATION OF CROSS-SECTION	KM	XS(I)
ELEVATION (MSL) OF FLOODING AT CROSS-SECTION	M	FSTG(I)
ELEV CORRESPONDING TO EACH TOP WIDTH	M	HS (K, I)
TOP WIDTH CORRESPONDING TO EACH ELEV	M	BS(K, I)
(ACTIVE FLOW PORTION)		
TOP WIDTH CORRESPONDING TO EACH ELEV	M	BSS (K, I)
(OFF-CHANNEL PORTION)		
NUMBER OF CROSS-SECTION		I
NUMBER OF ELEVATION LEVEL		K

CROSS-SECTION NUMBER 1

0.000	FSTG(I)	Ξ	0.00
4535.0	4560.0		
50.0	150. 0		
0.0	0.0		
	0.000 4535.0 50.0	4535.0 4560.0 50.0 150.0	0.000 FSTG(I) = 4535.0 4560.0 50.0 150.0

#### CROSS-SECTION NUMBER 2

yajajajajajajajajajajajajajajajajajajaj								
XS(I) =	4.500	FSTG(I) =	0.00					
HS	4410.0	4430. 0						
BS	50.0	150. 0						
BSS	0.0	0.0						

#### CROSS-SECTION NUMBER 3

 $\begin{array}{rcl} XS\left(I\right) &=& 36.500 & FSTG\left(I\right) &=& 0.00 \\ HS & \ldots & 3160.0 & 3180.0 \\ BS & \ldots & 50.0 & 100.0 \\ BSS & \ldots & 0.0 & 0.0 \end{array}$ 

#### CROSS-SECTION NUMBER 4

#### 

XS(I) = 76.100 FSTG(I) = 0.00HS ... 1580.0 1600.0 BS ... 70.0 200.0 BSS ... 0.0 0.0

CROSS-SECTION NUMBER 5

yolojojojojojojojek			
XS(I) =	121.200	FSTG(I) =	0.00
HS	1095.0	1115.0	
BS	30.0	100. 0	
BSS	0, 0	0.0	

#### CROSS-SECTION NUMBER 6

	ajajajajajajaj	ojojojojeje	
XS(I) =	171.500	FSTG(I) =	0.00
HS	570.0	590.0	
BS	50.0	100. 0	
BSS	0.0	0.0	

#### MANNING N ROUGHNESS COEFFICIENTS FOR THE GIVEN REACHES (CM(K, I), K=1, NCS) WHERE I = REACH NUMBER

REACH	1	0. 050	0. 050
REACH	2	0. 050	0. 050
REACH	3	0. 050	0. 050
REACH	4	0. 050	0. 050
REACH	5	0. 050	0.050

CROSS-SECTIONAL	VARIABL	es for	1
BELO	W RUN	2 :	

Luggye Lake

.

PARAMETER Micholococococococococococococococococococ	UNITS ******	VARIABLE
MINIMUM COMPUTATIONAL DISTANCE USED BETWEEN CROSS-SECTIONS	КМ	DXM(I)
CONTRACTION - EXPANSION COEFFICIENTS		FKC(I)

CONTRACTION - EXPANSION COEFFICIENTS BETWEEN CROSS-SECTIONS

> REACH NUMBER DXM(I) FKC(I) njajajajajajaj yololololok 1 2.000 0.000 2 2.000 0.000 3 2.000 0, 000 4 2.000 0.000 5 2.000 0.000

DOWNSTREAM FLOW PARAMETERS FOR

Luggye Lake

PARAMETER ********	UNITS	VARIABLE ******	XALUE
MAX DISCHARGE AT DOWNSTREAM EXTREMITY	CMS	QMAXD	0.0
MAX LATERAL OUTFLOW PRODUCING LOSSES	cms /m	QLL	0.000
INITIAL SIZE OF TIME STEP	HOUR	DTHM	0. 0000
INITIAL WATER SURFACE ELEVATION DOWNSTREAM	M	YDN	575. 00
SLOPE OF CHANNEL DOWNSTREAM OF DAM	%	SOM	0. 00
THETA WEIGHTING FACTOR		THETA	0. 00
CONVERGENCE CRITERION FOR STAGE	N	EPSY	0.000
TIME AT WHICH DAM STARTS TO FAIL	HOUR	TFI	0. 00

AT REACH= 3 DXM SHOULD BE CHANGED TO 0.434 DUE TO CHANGE OF SLOPE CRITERIA

COMPUTATIONS WILL USE THE FOLLOWING DXM VALUES

2.000 2.000 2.000 2.000 2.000

LATERAL INFLOW REACH NUMBER

LOX (I)

1 2 3 4 5

(QL (L, 1), L=1, ITEH)0. 0. (QL (L, 2), L=1, ITEH)0. 0. (QL (L, 3), L=1, ITEH)70. 70. (QL (L, 3), L=1, ITEH)70. (QL (L, 3), L=1, ITE

(QL (L, 4), L=1, ITEH) 100. 100.

(QL(L, 5), L=1, ITEH) 0. 0.

TOTAL NUMBER OF CROSS SECTIONS (ORIGINAL+INTERPOLATED) (N) = 85 (MAXIMUM ALLOWABLE = 200

<u> keletetetetetetetetetetetetetetetetetete</u>					
zielejejejejejejejejejejejejejejejejejeje					
ala parte a					***
***	SUMMARY	0F	OUTPUT	DATA	xininik
aladia (k					***
<u> </u>					

		BOTTOM		REACH	
CROSS-SECTION		ELEVATION		LENGTH	SLOPE
NO.	KM	M	REACH NO.	KM	%
1	0.00	4535.00			
2	4.50	4410.00	1	4.50	2.78
3	36.50	3160.00	2	32.00	3.91
4	76.10	1580.00	3	39.60	3.99
5	121.20	1095.00	4	45.10	1.08
6	171.50	570.00	5	50. 30	1.04

MESAGE

TOTAL VOLUME IN RESERVOIR BEHIND RUN2 : = 25.0 CU. M (MILLION)

#### DEFINITION OF VARIABLES IN RESERVOIR DEPLETION TABLE

1

PARAMETER ***********************************	UNITS ******	VARIABLE
TIME STEP FROM START OF ANALYSIS		I
ITERATIONS NECESSARY TO SOLVE FLOW EQUATIONS		К
ELAPSED TIME FROM START OF ANALYSIS	HOUR	TTP(I)
TOTAL OUTFLOW FROM DAM	CMS	Q(I)
ELEVATION OF WATER SURFACE AT DAM	M	H2
ELEVATION OF BOTTOM OF BREACH	M	YB
EST DEPTH OF FLOW IMMEDIATELY DOWNSTREAM	M	D
SUBMERGENCE COEFFICIENT		SUB
VELOCITY CORRECTION		VCOR
TOTAL VOLUME DISCHARGED FROM TIME OF BREACH MIL	LION CU N	OUTVOL
BREACH WIDTH	M	BB
RECTANGULAR BREACH DISCHARGE COEFFICIENT		COFR
INFLOW TO RESERVOIR	CMS	QI (I)
BREACH OUTFLOW	CMS	QBRECH
SPILLWAY OUTFLOW	CMS	QSPIL

I ****		TTP(I)	Q(I) ********	H2 *******	¥B *******	D ******	SUB Notest	VCOR ****	OUTVOL.	BB ****	COFR	QI (I) *****	QBRECH	QSPIL
ተተተ	ጥጥ	*****	******	******	******	*****	****	****	<del>ŢŢŢŢŢŢŢŢŢŢ</del>	****	****	*****	****	*****
1	0	0, 000	50	4561.00	4561.00	4535.44	1.00	1.00	0.0	0.0	3.10	50.	0.	50.
2	2	0.070	50	4560. 99	4560.48	4535.44	1.00	1.00	0.0	0.7	3.10	50.	0.	50.
3	2	0.140	52	4560. 99	4559.96	4535.45	1.00	1.00	0.0	1.4	3.10	50.	3.	<b>50</b> .
4	1	0.210	56	4560. 99	4559. 44	4535.47	1,00	1.00	0.0	2.1	3.10	50.	7.	50.
5	1	0.280	64	4560, 99	4558.92	4535, 51	1,00	1.00	0. 1	2.8	3.10	50.	14.	50.
6	1	0.350	74	4560.98	4558.40	4535.56	1.00	1.00	0.1	3.5	3.10	50.	25.	50.
7	2	0,420	89	4560.98	4557.88	4535.62	1.00	1.00	0.1	4.2	3.10	50.	39.	50.
8	2	0.490	107	4560.96	4557.36	4535.69	1.00	1.00	0.1	4.9	3.10	50.	57.	50. 50
9	2	0.560	129	4560.95	4556.84	4535.77	1.00	1.00	0.1	5.6	3.10	50.	80.	50.
10 11	2 2	0.630 0.700	156 187	4560. 92 4560. 89	4556.32 4555.80	4535.87 4535.96	1.00 1.00	1.00 1.00	0.2 0.2	6.3 7.0	3. 10 3. 10	50.	107. 138.	50. 50
12	2	0.770	223	4560.85	4555.28	4536.07	1.00	1.00	0.2	7.7	3.10	50. 50.	138.	50. 50.
12	2	0.840	263	4560.81	4554.76	4536.18	1.00	1.00	0.3	8.4	3, 10	50.	214.	50. 50.
14	2	0.910	306	4560.75	4554.24	4536.29	1.00	1.00	0.3	9.1	3, 10	50.	258.	<b>48</b> .
15	2	0.980	351	4560.68	4553.72	4536.40	1.00	1.00	0, 5	9.8	3.10	50. 50.	308.	44.
16	2	1.050	401	4560.59	4553.20	4536. 51	1.00	1.00	0,6	10, 5	3.10	50.	361.	40.
17	2	1.120	455	4560.50	4552.68	4536.63	1.00	1.00	0.7	11.2	3.10	50.	419.	36.
18	2	1.190	512	4560.39	4552.16	4536.75	1.00	1.00	0.8	11.9	3.10	50.	481.	32.
19	2	1.260	574	4560.26	4551.64	4536.87	1.00	1. 00	1.0	12.6	3.10	50.	546.	28.
20	2	1.330	639	4560.12	4551.12	4536.99	1.00	1.00	1, 1	13.3	3.10	50.	615.	24.
21	2	1.400	707	4559. 97	4550.60	4537.12	1.00	1.00	1.3	14.0	3.10	50.	687.	20.
22	2	1.470	777	4559.79	4550. 08	4537.24	1.00	1.00	1.5	14.7	3.10	50.	762.	16.
23	2	1.540	851	4559.60	4549. 56	4537.36	1.00	1.00	1.7	15.4	3.10	50.	839.	12.
24	2	1.610	926	4559.39	4549. 04	4537, 48	1.00	1.00	1.'9	16.1	3.10	50.	918.	8.
25	-2	1. 680	1002	4559.16	4548. 52	4537.60	1:00	1.00	2.1	16, 8	3.10	50.	999.	4.
26	2	1,750	1080	4558, 91	4548.00		1.00	1,00	2.4	17.5	3.10	50.	1080.	0.
27	2	1.820	1162	4558.64	4547.48	4537.83	1.00	1.00	2.7	18.2	3.10	50.	1163.	0.
28	2	1.890	1245	4558.35	4546.96	4537.95		1.00	3.0	18.9	3.10	50.	1245.	0.
29	2	1.960	1327	4558.04	4546.44	4538.06	1.00	1.00	3, 3	19.6	3.10	50.	1327.	0.
30	2	2.030	1408	4557.70	4545.92	4538.17	1.00	1.00	3.7	20.3	3.10	50.	1409.	0.
31 32	2 2	2.100 2.170	1488 1567	4557.35 4556.98	4545.40 4544.88	4538.27 4538.37	1.00	1.00	4.0	21.0	3.10	50. 50.	1489.	0.
33	2	2. 240	1644	4556.59	4544.36	4538.46	1.00	1.00	4.4	22.4	3.10 3.10	50. 50.	1568. 1645.	0. 0.
34	2	2.310	1719	4556.17	4543.84	4538.55	1.00	1.00	4.8 5.2	23.1	3.10	50.	1720.	0. 0.
35	2	2.380	1792	4555.74	4543.32	4538.64	1.00	1:01	5.7	23.8	3.10	50. 50.	1792.	0.
36		2.450	1862		4542.80		1.00				3.10	50.	1862.	0.
37	2		1929		4542. 28			1. 01			3.10	50.	1930.	0.
38	2		1994		4541.76		1.00	1.01			3.10	50.	1994.	0.
39	2	2.660	2055	4553. <b>8</b> 5	4541.24	4538.94	1.00	1.01	7.6			50.	2055.	0.
40	2	2.7 <b>30</b>	2113	4553.34	4540, 72	4539.00	1.00	1. 01	8.1	27.3	3.10	50.	2114.	0.
41	2	2.800	2168	4552.81	4540, 20	4539, 06	1.00	1.01	8.7	28.0	3.10	50.	2169.	0.
42	2	2. <b>8</b> 70	2221	4552.27	4539, 68	4539. 12	1.00	1. 01	<b>9</b> . 2	28.7	3.10	<b>50</b> .	2221.	0.
43	2	2.940	2270	4551.72		4539.17	1.00	1.02	9.8	29.4	3.10	50.	2270.	0.
44	2		2316	4551.15		4539. 22	1.00	1.02	10.4	30.1		50.	2316.	0.
45	2	3.080	2359	4550.58	4538.12		1.00	1.02	11.0	30.8		50.	2360.	0.
46	2		2400	4549.99		4539.31	1.00	1.02	11.6		3.10	50.	2400.	0.
47	2		2438	4549, 39		4539.35	1.00	1.03	12.2	32.2		50.	2439.	0.
48	2		2474		4536.56			1.03			3.10	50. 50	2475.	0.
49	2		2509		4536.04		1.00				3.10	50. 50	2509.	0.
50	2	3.430	2542	404/.00	4535, 52	4039.40	1.00	1.05	14. 1	34.3	3.10	50.	2543.	0.

I	K TTP(I)	Q(I)	H2	YB	D	SUB	VCOR	OUTVOL	BB	COFR	QI (I)	QBRECH	QSPI
***	alaik alempikaikaik	*okolokajojek		****	***	aka ka	*	\$cicicicisisisis	*akakak	<b>kojojoj</b>	siajajaja		aka ka

2	3.500	2575	4546, 91	4535.00	4539.49	1.00	1.05	14.	7 35.	0 3.10	50.	2576.	0.
2	3.570	2398	4546.30	4535.00	4539, 31	1.00	1.06	15.	3 35.	0 3.10	50.	2399.	0.
2	3.640	2225	4545.73	4535.00	4539, 12	1.00	1.06	15.			50.	2225.	0.
2	3.710	2067	4545.20	4535.00	4538.95	1.00	1.06	16.			50.	2067.	0,
2	3.780	1923	4544.71	4535.00	4538.79	1.00	1.06	17.			50.	1924.	0.
2	3.850	1793	4544.25	4535, 00	4538, 64	1.00	1.07	17.			50.	1793.	0.
2	3.920	1674	4543.83	4535.00	4538.50	1.00	1.07	17.			50.	1674.	0.
2	3.990	1565	4543.43	4535.00	4538.37	1.00	1.07	18.			50.	1566.	0.
2	4.060	1466	4543.06	4535.00	4538.24	1.00	1.07	18.			50.	1466.	0.
2	4.130	1375	4542.72	4535.00	4538.12	1.00	1.07	19.			50.	1376.	0.
2	4.200	1292	4542.40	4535.00	4538.01	1.00	1.07	19.			50.	1292.	0.
2	4.270	1215	4542.09	4535.00	4537.90	1.00	1.08	19.			50.	1215.	0.
2	4.340	1144	4541.81	4535.00	4537.80	1.00	1.08	20.			50.	1145.	0. 0.
2	4.410	1079	4541.54	4535.00	4537.71	1.00	1.08	20.			50.	1079.	0. 0.
2	4.480	1019	4541.29	4535.00	4537.62	1.00	1.08	20.			50.	1019.	0. 0.
2	4.550	963	4541.05	4535.00	4537.54	1.00	1.08	20.			50.	963.	0. 0.
2	4.620	911	4540.83	4535.00	4537.46	1.00	1.08	20.			50.	903. 912.	0. 0.
2	4, 690	863	4540.62	4535.00	4537.38	1.00	1.08	21.			50. 50.	864.	
2	4.760	819	4540.42	4535.00	4537.31	1.00	1.00	21.			50. 50.	819.	0.
2	4.830	777	4540.23	4535.00	4537.24	1.00	1.09	21.			50. 50.	819. 778.	0.
2	4.900	739	4540.25	4535.00	4537.17	1.00	1.09	21.					0.
2	4.900	703	4539.88	4535.00	4537.11	1.00	1.09	21.			50. 50	739. 702	0.
2	5.040	669	4539.72	4535.00 4535.00	4537.05	1.00	1.09				50.	703.	0.
2	5.110	638	4539.57	4535.00	4536.99	1.00	1.09	22.1			50. 50	669.	0.
2	5.180	608		4535.00 4535.00				22.3			50.	638. 600	0.
2			4539.42		4536.94	1.00	1.09	22.			50.	609.	0.
2	5.250 5.320	581 555	4539.29	4535.00	4536.88	1.00	1.09	22.			50.	581. 555	0.
			4539.16	4535.00	4536.83	1.00	1.10	22.			50.	555.	0.
2 · 2	5,390	531	4539.03	4535.00	4536.79	1.00	1.10	22.			50.	531.	0.
	5.460	508	4538.91	4535.00	4536.74		1.10	23.			50.	508.	· 0.
2 2	5.530	486	4538.80	4535.00	4536.70	1.00	1.10	23.			50.	<b>48</b> 7.	0.
	5.600	466	4538.69	4535.00	4536.66	1.00	1.10	23.			50.	467.	0.
2	5.670	447	4538.59	4535.00	4536.62	1.00	1.10	23.			50. 50	448.	0.
2	5.740 5.810		4538.49	4535.00	4536.58	1.00	1.10	23.			50. 50	430.	0.
2		413	4538.40	4535.00	4536.54	1.00	1.10	23.			50.	413.	0.
	5.880	397	4538.31	4535.00	4536.50	1.00	1.10	23.			50.	397.	0.
2.		382	4538.22	4535.00	4536.47	1.00	1.10	23.			50.	382.	0.
2	6.020	·367	4538.14	4535.00	4536.44	1.00	1.10	23.		0 3.10	50.	368.	0.
2	6.090	354	4538.06	4535.00	4536.41	1.00	1.10	24.		0 3.10	50.	· 354.	0.
6	6.160	341	4537.99	4535.00	4536.38					0 3.10	50.	342.	· 0.
2	6.230	329	4537.92	4535.00	4536.35		1.11			0 3.10	50.	330.	0.
1	6.300	318	4537.85	4535.00		1.00		24.		0 3.10	50.	318.	0.
1	6.370	307	4537.78	4535.00	4536.29		1.11	24.		0 3.10	50.	307.	0.
1	6.440 6.510	297	4537.72	4535.00	4536.27	1.00				0 3.10	50.	297.	0.
1	6.510	287		4535.00	4536.24			24.		0 3.10	50.	287.	0.
1		277		4535.00				24.			50.	278.	0.
1	6.650	269		4535,00		1.00		24.			50.	269.	0.
1	6.720 6.700	260	4537.49		4536.17	1.00		24.		0 3.10	50.	261.	0.
1	6.790	252	4537.43		4536.15		1.11	24.		0 3.10	50.	253.	0.
1	6.860 6.020	244		4535.00	4536.13			24.		0 3.10	50.	245.	0.
1	6.930	237	4037.34	4535.00	4536.11	1.00	1.11	24.	9 35.	0 3.10	50.	238.	0.
											-		

I	к	TTP(I)	Q(I)	H2	YB	D	SUB	VCOR	OUTVOL		COFR	QI (I)	QBRECH	QSPIL
ala	**	skojejejejej	siajajajajajajaj		<del>Antojo joju</del> (	y o pologo je	akojojoje	nje je je je je	\$0 <b>01010101010</b> 101	xiciciek	*****	akakakak	aka ka	Activity in
101	1	7.000	230	4537.29	4535.00	4536. 09	1.00	1. 11	25. 0	35.0	3.10	50.	231.	0.
102	1		223	4537.24	4535.00	4536.07	1.00	1.11	25.0	35.0	3.10	50.	223.	0.
103	1		215	4537.19	4535.00	4536.05	1.00	1.11	25.1	35.0	3.10	50.	216.	0.
104	1		207	4537.13	4535.00	4536.03	1.00	1.11	25.2	35.0	3.10	50.	208.	0.
105	1		199	4537.08	4535.00	4536.00	1.00	1.11	25.2	35.0	3.10	50.	200.	0.
106	1		191	4537.02	4535.00	4535.98	1.00	1.12	25.3	35.0	3.10	50.	191.	0.
107	1		182	4536.96	4535.00	4535.95	1.00	1.12	25.4	35.0	3.10	50.	183.	0.
108	1		174	4536.89	4535.00	4535. 92	1.00	1.12	25.5	35.0	3.10	50.	174.	0.
109	1		165	4536.83	4535.00	4535.90	1.00	1.12	25.6	35.0	3.10	50.	165.	0.
110	1		156	4536.76	4535.00	4535.87	1.00	1.12	25.7	35.0	3.10	50.	157.	0.
111	1	8.227	147	4536.70	4535.00	4535.84	1.00	1.12	25. <b>8</b>	35.0	3.10	50.	148.	0.
112	1		139	4536.63	4535.00	4535.81	1.00	1.12	25.9	35.0	3.10	50.	139.	0.
113		8.647	130	4536, 56	4535.00	4535.78	1.00	1.12	26.0	35.0	3.10	50.	131.	0.
114		8, 888	122	4536.50	4535. 00	4535.75	1.00	1.12	26.1	35.0	3.10	50.	123.	0.
115	1	9. 154	114	4536.43	4535.00	4535.72	1.00	1.12	26. 2	35.0	3.10	50.	115.	0.
116	1	9. 446	107	4536.37	4535. 00	4535.69	1.00	1.12	26.3	35.0		50.	107.	0.
117	1	9.768	100	4536. 30	4535.00	4535.66	1.00	1.12	26.4	35.0	3.10	50.	100.	0.
118	1	10.122	93	4536.24	4535.00	4535.63	1.00	1.12	26.6	35.0		50.	93.	0.
119	2	10.511	87	<b>4</b> 536. 19	4535.00	<b>4</b> 535. 61	1.00	1.12	26.7	35.0		50.	87.	0.
120	2	10. 939	81	4536.13	4535.00	4535.59	1.00	1.13	26.8	35.0		50.	81.	0.
121	2	: 11.410	76	4536.09	4535.00	4535.56	1.00	1.13	27.0	35.0		50.	76.	. 0.
122	2	11. 928	71	4536.04	4535.00	4535. 54	1.00	1.13	27.1	35.0		50.	72.	0.
. 123	2	2 12.498	67	4536.00	4535.00		1.00		27.2	35.0		50.	68.	0.
124	2	2 13. 125	64	4535.97	4535. 00		1.00		27.4	35.0		50.	64.	· 0.
125	2	2 13.814	60	4535.93	4535.00				27.5	35.0		50.	61.	0.
126	. 2	2 14.573	58	4535.91	4535. 00		1.00		27.7	35.0		50:	58.	0.
127		2 15.407	56	4535. <b>8</b> 9	4535.00		1.00		27.9	35.0		50.	56.	0.
128	2	2 16. 325	- 54		4535.00		1.00		28.1	35.0		50.	55.	0.
129	) 2	2 17, 334	53	4535.85	4535.00		1.00		28.3	35.0		50.	53.	0.
130	) 2	2 1 <b>8. 44</b> 5	52		4535.00				28.5	35.0		50.	52.	0.
131	. 1	l 19.666	51		4535.00				•	35.0		50.	51.	· 0.
132		l 21.010			4535.00		1.00					50.	51.	0.
133	) ]	l <sup>-</sup> 22, 488	50	4535.82	4535.00	4535.44	1.00	1.13	29.2	35.0	3.10	50.	51.	0.

PARAMETER	UNITS	VARIABLE	VALUE
	*olotototok	<del>#chololok</del>	<del>yakakakakatokolok</del>
INITIAL FLOW	CMS	Q(1)	50.
MAX FLOW	CMS	QM	2576.
FINAL FLOW	CMS	Q (NU)	51.
TIME TO MAX FLOW	HRS	TP	3.50
NUMBER OF TIME STEPS		NNU	133
TOTAL VOLUME DISCHARGED FROM RESERVOIR MILL	ION CU M	DISVOL	29.

#### INITIAL CONDITIONS

((	DI(I), I=1,	, N)					
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	5 <b>0</b> .
50.	50.	50.	120.	120.	120.	120.	120.
120.	120.	120.	120.	120.	120.	120.	120.
120.	120.	120.	120.	120.	120.	220.	220.
220.	220.	220.	220.	220.	220.	220.	220.
220.	220.	220.	220.	220.	220.	220.	220.
220.	220.	220.	220.	220.	220.	220.	220.
220.	220.	220.	220.	220.	220.	220.	220.
220.	220.	220.	220.	220.	220.	220.	220.
220.	220.	220.	220.	220.			
(1	(I (I), I=1, I	N)					
4535.49	4472.96	4410.46	4332.28	4254.21	4176.03	4097.96	4019.78
3941.71	3863. 53	3785.46	3707.2 <b>8</b>	3629. 21	3551.03	3472.96	3394.78
3316.71	3238.53	3160.46	3077.57	2994.40	2911.23	2828.07	2744. 90
2661.73	2578.57	2495.41	2412.24	2329.08	2245, 90	2162.75	2079. 57
1996.42	1913, 25	1830.09	1746. 92	1663.76	1580. 60	1558.96	1536. 93
1514.90	1492.88	1470.85	1448. 83	1426.81	1404.78	1382.76	1360. 74
1338.73	1316.71	12 <b>94</b> . 70	1272. 69	1250. 68	1228.67	1206.66	1184.66
1162.66	1140.67	1118.69	1096.70	1075.68	1054.65	1033.63	1012.60
991.58	970. 55	949. 53	928. 51	907.49	886.47	865.45	844. 44
823.42	802.40	781.38	760. 37	739. 35	718.34	697.32	676, 31
655.29	634.28	613.26	592.25	571.24			

# TIME PARAMETERS OF OUTFLOW HYDROGRAPH IMMEDIATELY DOWNSTREAM OF DAM

PARAMETER ***********************************	UNITS *******	VARIABLE	VALUE
TIME TO FAILURE	HR	TFH	3. 500
TIME TO START OF RISING LIMB OF HYDROGRAPH	HR -	TFO	0.000
TIME TO PEAK	HR	TP	3. 500
TIME STEP SIZE	HR	DTHI	. 0. 175
ROUTING COMPLETED.			•
KTIME= 81 ALLOWABLE KTIME= 699	<b>TT</b> =	24. 1	

#### PROFILE OF CRESTS AND TIMES FOR Luggye Lake BELOW RUN2 :

DISTANCE FROM DAM KM	MAX ELEV M <del>Northert</del>	MAX FLOW CMS	TIME MAX ELEV-HRS *====================================	MAX VEL M/S	FLOOD ELEV M *******	TIME FLOOD ELEV-HRS
0.000	4539.92	2575	3,500	8.74	0.00	0.00
2, 250	4477.38	2553	3.500	8.59	0.00	0.00
4. 499	4414.81	2529	3, 500	8.47	0.00	0.00
6.499	4335.84	2510	3.500	10.64	0.00	0.00
8,499	4258.47	2491	3.500	8.67	0.00	0.00
10. 498	4179.67	2493	3.675	10.43	0.00	0. 00
12.498	4102.16	2 <b>494</b>	3.675	8.89	0.00	0.00
14. 498	4023.49	2489	3.762	10.32	0.00	0.00
16, 497	3945.86	2488	3.762	9.09	0.00	0.00
18.497	3867.31	2486	3,762	10.23	0.00	0.00
20. 497	3789.58	2480	3.762	9.27	0.00	0.00
22, 496	3711.11	2482	3.850	10, 17	0.00	0.00
24.496	3633.30	2478	3.850	9.42	0.00	0.00
26. 496	3554.89	2469	3,850	10.15	0.00	0.00
28.495	3477.01	2457	3.850	9.54	0.00	0.00
30, 495	3398.67	2456	4.025	10.14	0.00	0.00
32. 495	3320. 76	2459	4. 025	9.68	0.00	0.00
34.494	3242.46	2457	4. 025	10, 18	0.00	0.00
36. 494	3164.50	2450	4. 025	9,80	0.00	0.00
38.578	3081.15	2510		10.25	0.00	0.00
40.662	2998.08	2507	4.200	9.74	0.00	0.00
42.745	2914.74	2501	4.200	9.98	0.00	0.00
44.829	2831.64	2509	4.200	9,57	0.00	0.00
46. 913	2748.32	2503	4.200	9.73	0.00	0.00
48.997	2665.20		4. 200	9.38	0.00	0.00
51.081	2581.90	2494		9.52	0.00	0.00
53, 165	2498.78			9.22	0.00	0.00
55.249	2415.50	2492	4.375	9.33	0.00	0.00
57.333	2332.36	2486	4.375	9.00	0.00	0.00
59.416	2249.09	2478	4.650	9.14	0.00	0.00
61.500	2165.96	2484	4. 550	8, 92	0.00	0.00
63. 584	2082.71	2483	4. 550	8.99	0.00	0.00
65.668	1999.55	2405	4. 550	8.79	0.00	0,00
67.752	1916.30	2467	4. 725	8,83	0.00	0.00
69.836	1833.15	2407	4. 725	8.65	0.00	0.00
71.920	1749.92	2469	4. 725	8,69	0.00	0.00
74.003	1666.76	2462	4. 725	8, 53	0.00	0.00
76.087	1583.53	2455	4. 900	8.55	0.00	0.00
78. 137	1564.89	2557	4.900	4.09	0,00	0.00
80. 187	1539.48	2551	5, 075	9.30	0.00	0.00
82.236	1521.09	2544	4, 900	4.08	0,00	0.00
84. 286	1495.42	2544	5. 250	11.62	0,00	0.00
86, 336	1455.42	2545	5. 075	4.10	0.00	0.00
88.385	1451.38	2540	5.425	13.73	0,00	0.00
90, 435	1433. 48	2540	5. 250	4, 15	0,00	0.00
92. <b>484</b>	1407.38	2530	5. 425	4, 15 15, 70	0.00	0.00
94. 534	1389.64	2526	5. 425	4.21	0.00	0.00
<b>UU1</b>	1000.01	2020	U. 160	7.41	J. UV	0.00

# PROFILE OF CRESTS AND TIMES FOR Luggye Lake BELOW RUN2 :

LUW	RUNZ	

FROM DAM         MAX ELEV         MAX FLOW         TIME MAX ELEV-HRS         MAX VEL M/S         FLOOD ELEV         TIME FLOOD ELEV-HRS           98.633         1345.85         2512         5.425         4.27         0.00         0.00           100.683         1319.45         2508         5.775         15.21         0.00         0.00           102.733         1302.07         2496         5.600         4.35         0.00         0.00           104.782         1275.50         2499         5.950         15.39         0.00         0.00           106.832         1235.99         2482         5.960         15.35         0.00         0.00           110.931         1214.63         2479         5.775         4.52         0.00         0.00           117.096         2481         6.125         15.13         0.00         0.00           117.090         1143.91         2482         6.125         4.64         0.00         0.00           125.191         1084.48         2479         5.950         4.77         0.00         0.00           124.180         1100.16         2485         6.300         13.83         0.00         0.00           125.203	DISTANCE						
***98. 6331345. 6525125. 4254. 270. 000. 00100. 6831319. 4525085. 77515. 210. 000. 00104. 7821275. 5024995. 95015. 390. 000. 00106. 6321258. 3324665. 6004. 330. 000. 00106. 6321258. 3324665. 6004. 430. 000. 00108. 6821231. 6924825. 95015. 350. 000. 00110. 9311214. 6324795. 7754. 520. 000. 00117. 0801143. 9124826. 12515. 280. 000. 00117. 0801143. 9124826. 12515. 280. 000. 00121. 1801100. 1624856. 30015. 100. 000. 00122. 2151042. 2624836. 30013. 830. 000. 00123. 2261016. 0924736. 47513. 510. 000. 00132. 2261016. 0924736. 47513. 260. 000. 00133. 273931. 9124766. 65013. 030. 000. 00133. 273931. 9124766. 65013. 030. 000. 00133. 269974. 0024736. 4754. 860. 000. 00133. 269974. 0024716. 65013. 030. 000. 00 <tr< th=""><th></th><th>MAX ELEV</th><th>MAX FLOW</th><th>TIME MAX</th><th>MAX VEL</th><th>FLOOD ELEV</th><th>TIME FLOOD</th></tr<>		MAX ELEV	MAX FLOW	TIME MAX	MAX VEL	FLOOD ELEV	TIME FLOOD
98. $633$ 1345. $85$ 25125. $425$ 4. $27$ 0. 000. 00100. $683$ 1319. $45$ 25085. $775$ 15. $21$ 0. 000. 00102. $733$ 1302. 0724965. 6004. $35$ 0. 000. 00104. $782$ 1275. 5024996. 95015. $39$ 0. 000. 00106. $832$ 1258. $33$ 24865. 6004. $43$ 0. 000. 00108. $882$ 1231. $59$ 24825. 95015. $35$ 0. 000. 00110. $931$ 1214. $63$ 24795. $775$ 4. $52$ 0. 000. 00117. $080$ 1143. 9124826. 12515. 130. 000. 00119. 1301127. 3424795. 9504. 640. 000. 00121. 1801100. 1624856. 30015. 100. 000. 00123. 1911084. $48$ 24796. 1254. 840. 000. 00127. 2151042. 2624886. 30013. 830. 000. 00128. 2031058. 1524806. 30013. 830. 000. 00129. 2261016. 0924736. 4754. 870. 000. 00133. 250974. 0024796. 4754. 860. 000. 00133. 251974. 0024796. 4751. 860. 000. 00135. 261957. 8724676. 4751. 860. 000. 00135. 261957. 24716. 85513. 02<	KM	M	CMS	ELEV-HRS	M/S	M	ELEV-HRS
100.683 $1319.46$ $2508$ $5.775$ $15.21$ $0.00$ $0.00$ $102.733$ $1302.07$ $2496$ $5.600$ $4.35$ $0.00$ $0.00$ $104.782$ $1275.50$ $2499$ $5.950$ $15.39$ $0.00$ $0.00$ $106.832$ $1258.33$ $2486$ $5.600$ $4.43$ $0.00$ $0.00$ $108.882$ $1231.59$ $2482$ $5.950$ $15.35$ $0.00$ $0.00$ $110.931$ $1214.63$ $2479$ $5.775$ $4.52$ $0.00$ $0.00$ $112.981$ $1187.73$ $2481$ $6.125$ $15.13$ $0.00$ $0.00$ $117.080$ $1143.91$ $2482$ $6.125$ $15.28$ $0.00$ $0.00$ $117.180$ $1147.34$ $2479$ $5.950$ $4.77$ $0.00$ $0.00$ $121.180$ $1100.16$ $2485$ $6.300$ $15.10$ $0.00$ $0.00$ $122.203$ $1058.15$ $2480$ $6.300$ $13.83$ $0.00$ $0.00$ $127.215$ $1042.26$ $2483$ $6.300$ $13.83$ $0.00$ $0.00$ $123.250$ $974.00$ $2479$ $6.475$ $13.26$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $4.86$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $4.86$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $4.86$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $4.86$ $0.00$ <	yeyoloje <b>kojoje</b> k		****			s <del>iniojesje jeste jeste jest</del> eksk	, <b>prinicialojajajaja</b> je
100.683 $1319.46$ $2508$ $5.775$ $15.21$ $0.00$ $0.00$ $102.733$ $1302.07$ $2496$ $5.600$ $4.35$ $0.00$ $0.00$ $104.782$ $1275.50$ $2499$ $5.950$ $15.39$ $0.00$ $0.00$ $106.832$ $1258.33$ $2486$ $5.600$ $4.43$ $0.00$ $0.00$ $108.882$ $1231.59$ $2482$ $5.950$ $15.35$ $0.00$ $0.00$ $110.931$ $1214.63$ $2479$ $5.775$ $4.52$ $0.00$ $0.00$ $112.981$ $1187.73$ $2481$ $6.125$ $15.13$ $0.00$ $0.00$ $117.080$ $1143.91$ $2482$ $6.125$ $15.28$ $0.00$ $0.00$ $117.180$ $1147.34$ $2479$ $5.950$ $4.77$ $0.00$ $0.00$ $121.180$ $1100.16$ $2485$ $6.300$ $15.10$ $0.00$ $0.00$ $122.203$ $1058.15$ $2480$ $6.300$ $13.83$ $0.00$ $0.00$ $127.215$ $1042.26$ $2483$ $6.300$ $13.83$ $0.00$ $0.00$ $127.226$ $1016.09$ $2473$ $6.475$ $13.26$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $13.26$ $0.00$ $0.00$ $137.273$ $931.91$ $2476$ $6.650$ $13.03$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $4.86$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $4.86$ $0.0$							
100.683 $1319.46$ $2508$ $5.775$ $15.21$ $0.00$ $0.00$ $102.733$ $1302.07$ $2496$ $5.600$ $4.35$ $0.00$ $0.00$ $104.782$ $1275.50$ $2499$ $5.950$ $15.39$ $0.00$ $0.00$ $106.832$ $1258.33$ $2486$ $5.600$ $4.43$ $0.00$ $0.00$ $108.882$ $1231.59$ $2482$ $5.950$ $15.35$ $0.00$ $0.00$ $110.931$ $1214.63$ $2479$ $5.775$ $4.52$ $0.00$ $0.00$ $112.981$ $1187.73$ $2481$ $6.125$ $15.13$ $0.00$ $0.00$ $117.080$ $1143.91$ $2482$ $6.125$ $15.28$ $0.00$ $0.00$ $117.180$ $1147.34$ $2479$ $5.950$ $4.77$ $0.00$ $0.00$ $121.180$ $1100.16$ $2485$ $6.300$ $15.10$ $0.00$ $0.00$ $122.203$ $1058.15$ $2480$ $6.300$ $13.83$ $0.00$ $0.00$ $127.215$ $1042.26$ $2483$ $6.300$ $13.83$ $0.00$ $0.00$ $127.226$ $1016.09$ $2473$ $6.475$ $13.26$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $13.26$ $0.00$ $0.00$ $137.273$ $931.91$ $2476$ $6.650$ $13.03$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $4.86$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $4.86$ $0.0$	08 632	1945 05	9519	5 495	4 97	0.00	0.00
102.733 $1302.07$ $2496$ $5.600$ $4.35$ $0.00$ $0.00$ $104.782$ $1275.50$ $2499$ $6.950$ $15.39$ $0.00$ $0.00$ $106.832$ $1258.33$ $2466$ $5.600$ $4.43$ $0.00$ $0.00$ $108.882$ $1231.59$ $2482$ $5.950$ $15.35$ $0.00$ $0.00$ $110.931$ $1214.63$ $2479$ $5.775$ $4.52$ $0.00$ $0.00$ $112.981$ $1187.73$ $2481$ $6.125$ $15.13$ $0.00$ $0.00$ $115.031$ $1170.96$ $2481$ $5.950$ $4.64$ $0.00$ $0.00$ $117.080$ $1143.91$ $2482$ $6.125$ $15.28$ $0.00$ $0.00$ $123.191$ $1084.48$ $2479$ $5.950$ $4.77$ $0.00$ $0.00$ $121.180$ $1100.16$ $2485$ $6.300$ $15.10$ $0.00$ $0.00$ $123.191$ $1084.48$ $2479$ $6.125$ $4.84$ $0.00$ $0.00$ $127.215$ $1042.26$ $2483$ $6.300$ $4.86$ $0.00$ $0.00$ $133.226$ $974.00$ $2479$ $6.475$ $4.87$ $0.00$ $0.00$ $133.225$ $974.00$ $2479$ $6.475$ $4.86$ $0.00$ $0.00$ $133.226$ $947.00$ $2479$ $6.475$ $4.86$ $0.00$ $0.00$ $133.226$ $947.00$ $2479$ $6.475$ $4.86$ $0.00$ $0.00$ $133.226$ $947.69$ $2463$ $7.000$ $12.94$ $0.00$ <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
104.782 $1275.50$ $2499$ $5.950$ $15.39$ $0.00$ $0.00$ $106.832$ $1258.33$ $2486$ $5.600$ $4.43$ $0.00$ $0.00$ $108.882$ $1231.59$ $2482$ $5.950$ $15.35$ $0.00$ $0.00$ $110.931$ $1214.63$ $2479$ $5.775$ $4.52$ $0.00$ $0.00$ $112.981$ $1187.73$ $2481$ $6.125$ $15.13$ $0.00$ $0.00$ $115.031$ $1170.96$ $2481$ $5.950$ $4.64$ $0.00$ $0.00$ $117.080$ $1143.91$ $2482$ $6.125$ $15.28$ $0.00$ $0.00$ $121.180$ $1100.16$ $2485$ $6.300$ $15.10$ $0.00$ $0.00$ $121.180$ $1100.16$ $2485$ $6.300$ $15.10$ $0.00$ $0.00$ $125.203$ $1058.15$ $2480$ $6.300$ $13.83$ $0.00$ $0.00$ $129.226$ $1016.09$ $2473$ $6.475$ $13.51$ $0.00$ $0.00$ $131.238$ $1000.06$ $2478$ $6.475$ $4.86$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $4.86$ $0.00$ $0.00$ $137.273$ $931.91$ $2476$ $6.650$ $13.03$ $0.00$ $0.00$ $141.296$ $889.81$ $2465$ $6.825$ $13.02$ $0.00$ $0.00$ $137.273$ $931.91$ $2476$ $6.475$ $4.85$ $0.00$ $0.00$ $143.308$ $873.57$ $2471$ $6.825$ $4.83$ $0.00$							
106.832 $1258.33$ $2486$ $5.600$ $4.43$ $0.00$ $0.00$ $108.882$ $1231.59$ $2482$ $5.950$ $15.35$ $0.00$ $0.00$ $110.931$ $1214.63$ $2479$ $5.775$ $4.52$ $0.00$ $0.00$ $112.961$ $1167.73$ $2481$ $6.125$ $15.13$ $0.00$ $0.00$ $115.031$ $1170.96$ $2481$ $5.950$ $4.64$ $0.00$ $0.00$ $117.080$ $1143.91$ $2482$ $6.125$ $15.28$ $0.00$ $0.00$ $121.180$ $1100.16$ $2485$ $6.300$ $15.10$ $0.00$ $0.00$ $123.191$ $1084.48$ $2479$ $6.125$ $4.84$ $0.00$ $0.00$ $125.203$ $1058.15$ $2480$ $6.300$ $13.83$ $0.00$ $0.00$ $127.215$ $1042.26$ $2483$ $6.300$ $4.86$ $0.00$ $0.00$ $129.226$ $1016.09$ $2473$ $6.475$ $13.51$ $0.00$ $0.00$ $131.238$ $1000.06$ $2478$ $6.475$ $4.86$ $0.00$ $0.00$ $137.273$ $931.91$ $2476$ $6.650$ $13.03$ $0.00$ $0.00$ $137.273$ $931.91$ $2476$ $6.825$ $13.02$ $0.00$ $0.00$ $144.308$ $873.57$ $2471$ $6.865$ $13.02$ $0.00$ $0.00$ $143.308$ $873.57$ $2471$ $6.825$ $13.02$ $0.00$ $0.00$ $144.334$ $805.59$ $2465$ $7.000$ $12.80$ $0.00$							
108.862 $1231.59$ $2482$ $5.960$ $15.35$ $0.00$ $0.00$ $110.931$ $1214.63$ $2479$ $5.775$ $4.52$ $0.00$ $0.00$ $112.981$ $1187.73$ $2481$ $6.125$ $15.13$ $0.00$ $0.00$ $115.031$ $1170.96$ $2481$ $5.960$ $4.64$ $0.00$ $0.00$ $117.080$ $1143.91$ $2482$ $6.125$ $15.28$ $0.00$ $0.00$ $121.180$ $1100.16$ $2485$ $6.300$ $15.10$ $0.00$ $0.00$ $123.191$ $1084.48$ $2479$ $6.125$ $4.84$ $0.00$ $0.00$ $125.203$ $1058.15$ $2480$ $6.300$ $13.83$ $0.00$ $0.00$ $127.215$ $1042.26$ $2473$ $6.475$ $13.51$ $0.00$ $0.00$ $129.226$ $1016.09$ $2473$ $6.475$ $13.26$ $0.00$ $0.00$ $131.238$ $1000.06$ $2479$ $6.475$ $13.26$ $0.00$ $0.00$ $135.261$ $957.87$ $2467$ $6.475$ $4.86$ $0.00$ $0.00$ $137.273$ $931.91$ $2476$ $6.650$ $13.03$ $0.00$ $0.00$ $141.296$ $889.81$ $2465$ $6.825$ $13.02$ $0.00$ $0.00$ $143.308$ $873.57$ $2471$ $6.650$ $4.85$ $0.00$ $0.00$ $1445.320$ $847.69$ $2463$ $7.000$ $12.80$ $0.00$ $0.00$ $145.320$ $847.69$ $2465$ $7.298$ $12.84$ $0.0$							
110. 9311214. 6324795. 7754. 520. 000. 00112. 9811187. 7324816. 12515. 130. 000. 00115. 0311170. 9624815. 9504. 640. 000. 00117. 0801143. 9124826. 12515. 280. 000. 00119. 1301127. 3424795. 9504. 770. 000. 00121. 1801100. 1624856. 30015. 100. 000. 00123. 1911084. 4824796. 1254. 840. 000. 00125. 2031058. 1524806. 30013. 830. 000. 00127. 2151042. 2624836. 3004. 860. 000. 00129. 2261016. 0924736. 47513. 510. 000. 00131. 2381000. 0624786. 4754. 860. 000. 00133. 250974. 0024796. 47513. 260. 000. 00135. 261957. 8724676. 45513. 020. 000. 00139. 285915. 7224716. 6504. 850. 000. 00141. 296889. 8124656. 82513. 020. 000. 00143. 308873. 5724716. 8254. 830. 000. 001443. 308873. 5724716. 8254. 830. 000. 00147. 331831. 4124617. 0004. 810. 000. 00<							
112. 9811187. 732481 $6. 125$ 15. 13 $0. 00$ $0. 00$ 115. 0311170. 962481 $5. 950$ $4. 64$ $0. 00$ $0. 00$ 117. 0801143. 912482 $6. 125$ 15. 28 $0. 00$ $0. 00$ 119. 1301127. 342479 $5. 950$ $4. 77$ $0. 00$ $0. 00$ 121. 1801100. 162485 $6. 300$ 15. 10 $0. 00$ $0. 00$ 123. 1911084. 482479 $6. 125$ $4. 84$ $0. 00$ $0. 00$ 125. 2031058. 152480 $6. 300$ 13. 83 $0. 00$ $0. 00$ 127. 2151042. 262483 $6. 300$ 13. 83 $0. 00$ $0. 00$ 129. 2261016. 092473 $6. 475$ 13. 51 $0. 00$ $0. 00$ 131. 2381000. 062478 $6. 475$ $4. 87$ $0. 00$ $0. 00$ 133. 250974. 002479 $6. 475$ $4. 86$ $0. 00$ $0. 00$ 137. 273931. 912476 $6. 650$ 13. 03 $0. 00$ $0. 00$ 139. 285915. 722471 $6. 825$ 13. 02 $0. 00$ $0. 00$ 141. 296889. 812465 $6. 825$ 13. 02 $0. 00$ $0. 00$ 143. 308873. 572471 $6. 825$ $4. 83$ $0. 00$ $0. 00$ 145. 320847. 692465 $7. 000$ $4. 77$ $0. 00$ $0. 00$ 145. 320847. 612465 $7. 298$ $12. 84$ $0. 00$ $0. 00$							
115. 0311170. 96 $2481$ $5. 950$ $4. 64$ $0. 00$ $0. 00$ 117. 0801143. 91 $2482$ $6. 125$ $15. 28$ $0. 00$ $0. 00$ 119. 1301127. 34 $2479$ $5. 950$ $4. 77$ $0. 00$ $0. 00$ 121. 1801100. 16 $2485$ $6. 300$ $15. 10$ $0. 00$ $0. 00$ 123. 1911084. 48 $2479$ $6. 125$ $4. 84$ $0. 00$ $0. 00$ 125. 2031058. 15 $2480$ $6. 300$ $13. 83$ $0. 00$ $0. 00$ 127. 2151042. 26 $2483$ $6. 300$ $4. 86$ $0. 00$ $0. 00$ 129. 2261016. 09 $2473$ $6. 475$ $13. 51$ $0. 00$ $0. 00$ 131. 2381000. 06 $2478$ $6. 475$ $4. 87$ $0. 00$ $0. 00$ 135. 261957. 87 $2467$ $6. 475$ $4. 86$ $0. 00$ $0. 00$ 137. 273931. 91 $2476$ $6. 650$ $13. 03$ $0. 00$ $0. 00$ 141. 296889. 81 $2465$ $6. 825$ $13. 02$ $0. 00$ $0. 00$ 143. 308 $873. 57$ $2471$ $6. 825$ $4. 83$ $0. 00$ $0. 00$ 145. 320847. 69 $2463$ $7. 000$ $4. 81$ $0. 00$ $0. 00$ 145. 320847. 69 $2465$ $7. 000$ $4. 81$ $0. 00$ $0. 00$ 145. 320847. 69 $2465$ $7. 298$ $4. 76$ $0. 00$ $0. 00$ 153. 366763. 46 $2428$ $7. 298$ <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
117.080 $1143.91$ $2482$ $6.125$ $15.28$ $0.00$ $0.00$ $119.130$ $1127.34$ $2479$ $5.950$ $4.77$ $0.00$ $0.00$ $121.180$ $1100.16$ $2485$ $6.300$ $15.10$ $0.00$ $0.00$ $123.191$ $1084.48$ $2479$ $6.125$ $4.84$ $0.00$ $0.00$ $125.203$ $1058.15$ $2480$ $6.300$ $13.83$ $0.00$ $0.00$ $127.215$ $1042.26$ $2483$ $6.300$ $4.86$ $0.00$ $0.00$ $129.226$ $1016.09$ $2473$ $6.475$ $13.51$ $0.00$ $0.00$ $131.238$ $1000.06$ $2478$ $6.475$ $4.87$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $4.86$ $0.00$ $0.00$ $135.261$ $957.87$ $2467$ $6.475$ $4.86$ $0.00$ $0.00$ $137.273$ $931.91$ $2476$ $6.650$ $13.03$ $0.00$ $0.00$ $141.296$ $889.81$ $2465$ $6.825$ $13.02$ $0.00$ $0.00$ $143.308$ $873.57$ $2471$ $6.825$ $4.83$ $0.00$ $0.00$ $145.320$ $847.69$ $2463$ $7.000$ $12.80$ $0.00$ $0.00$ $147.331$ $831.41$ $2461$ $7.000$ $4.81$ $0.00$ $0.00$ $149.343$ $805.59$ $2465$ $7.298$ $12.84$ $0.00$ $0.00$ $157.390$ $72.140$ $2465$ $7.298$ $12.84$ $0.00$							
119. 1301127. 342479 $5.950$ 4.770.000.00121. 1801100. 162485 $6.300$ 15. 100.000.00123. 1911084. 482479 $6.125$ 4. 840.000.00125. 2031058. 152480 $6.300$ 13. 830.000.00127. 2151042. 262483 $6.300$ 4. 860.000.00129. 2261016. 092473 $6.475$ 13. 510.000.00131. 2381000. 062478 $6.475$ 4. 870.000.00133. 250974. 002479 $6.475$ 13. 260.000.00135. 261957. 872467 $6.475$ 4. 860.000.00137. 273931. 912476 $6.650$ 13. 030.000.00139. 285915. 722471 $6.855$ 4. 850.000.00141. 296889. 812465 $6.825$ 13. 020.000.00143. 308873. 572471 $6.825$ 4. 830.000.00145. 320847. 6924637. 00012. 940.000.00147. 331831. 4124617. 0004. 810.000.00153. 366763. 4624287. 29812. 860.000.00155. 378747. 1324517. 2984. 760.000.00155. 378747. 1324517. 2984. 760.000.00155. 378747.							
121.180 $1100.16$ $2485$ $6.300$ $15.10$ $0.00$ $0.00$ $123.191$ $1084.48$ $2479$ $6.125$ $4.84$ $0.00$ $0.00$ $125.203$ $1058.15$ $2480$ $6.300$ $13.83$ $0.00$ $0.00$ $127.215$ $1042.26$ $2483$ $6.300$ $4.86$ $0.00$ $0.00$ $129.226$ $1016.09$ $2473$ $6.475$ $13.51$ $0.00$ $0.00$ $131.238$ $1000.06$ $2478$ $6.475$ $4.87$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $13.26$ $0.00$ $0.00$ $135.261$ $957.87$ $2467$ $6.475$ $4.86$ $0.00$ $0.00$ $137.273$ $931.91$ $2476$ $6.650$ $13.03$ $0.00$ $0.00$ $139.285$ $915.72$ $2471$ $6.650$ $4.85$ $0.00$ $0.00$ $141.296$ $889.81$ $2465$ $6.825$ $13.02$ $0.00$ $0.00$ $143.308$ $873.57$ $2471$ $6.825$ $4.83$ $0.00$ $0.00$ $1443.308$ $873.57$ $2471$ $6.825$ $4.81$ $0.00$ $0.00$ $1443.308$ $873.57$ $2471$ $6.825$ $4.83$ $0.00$ $0.00$ $1443.308$ $873.57$ $2471$ $6.825$ $4.83$ $0.00$ $0.00$ $145.320$ $847.69$ $2463$ $7.000$ $4.81$ $0.00$ $0.00$ $155.789.27$ $2451$ $7.000$ $4.77$ $0.00$ $0.00$ <							
123. 1911084. 482479 $6. 125$ $4. 84$ $0. 00$ $0. 00$ 125. 2031058. 152480 $6. 300$ 13. 83 $0. 00$ $0. 00$ 127. 2151042. 262483 $6. 300$ 4. 86 $0. 00$ $0. 00$ 129. 2261016. 092473 $6. 475$ 13. 51 $0. 00$ $0. 00$ 131. 2381000. 062478 $6. 475$ $4. 87$ $0. 00$ $0. 00$ 133. 250974. 002479 $6. 475$ 13. 26 $0. 00$ $0. 00$ 135. 261957. 872467 $6. 475$ $4. 86$ $0. 00$ $0. 00$ 137. 273931. 912476 $6. 650$ 13. 03 $0. 00$ $0. 00$ 139. 285915. 722471 $6. 650$ $4. 85$ $0. 00$ $0. 00$ 141. 296889. 812465 $6. 825$ 13. 02 $0. 00$ $0. 00$ 143. 308873. 572471 $6. 825$ $4. 83$ $0. 00$ $0. 00$ 144. 31831. 412461 $7. 000$ $4. 81$ $0. 00$ $0. 00$ 147. 331831. 412461 $7. 000$ $4. 81$ $0. 00$ $0. 00$ 153. 366763. 462428 $7. 298$ $4. 76$ $0. 00$ $0. 00$ 155. 378747. 132451 $7. 298$ $4. 73$ $0. 00$ $0. 00$ 157. 390721. 402465 $7. 298$ $12. 85$ $0. 00$ $0. 00$ 161. 413 $679. 24$ 2436 $7. 595$ $12. 79$ $0. 00$ $0. 00$ <							
125.203 $1058.15$ $2480$ $6.300$ $13.83$ $0.00$ $0.00$ $127.215$ $1042.26$ $2483$ $6.300$ $4.86$ $0.00$ $0.00$ $129.226$ $1016.09$ $2473$ $6.475$ $13.51$ $0.00$ $0.00$ $131.238$ $1000.06$ $2478$ $6.475$ $4.87$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $13.26$ $0.00$ $0.00$ $135.261$ $957.87$ $2467$ $6.475$ $4.86$ $0.00$ $0.00$ $137.273$ $931.91$ $2476$ $6.650$ $13.03$ $0.00$ $0.00$ $139.285$ $915.72$ $2471$ $6.650$ $4.85$ $0.00$ $0.00$ $141.296$ $889.81$ $2465$ $6.825$ $13.02$ $0.00$ $0.00$ $143.308$ $873.57$ $2471$ $6.825$ $4.83$ $0.00$ $0.00$ $145.320$ $847.69$ $2463$ $7.000$ $12.94$ $0.00$ $0.00$ $147.331$ $831.41$ $2461$ $7.000$ $4.81$ $0.00$ $0.00$ $149.343$ $805.59$ $2465$ $7.000$ $12.80$ $0.00$ $0.00$ $153.366$ $763.46$ $2428$ $7.298$ $12.84$ $0.00$ $0.00$ $155.378$ $747.13$ $2451$ $7.298$ $12.85$ $0.00$ $0.00$ $157.390$ $721.40$ $2465$ $7.298$ $12.85$ $0.00$ $0.00$ $153.466$ $637.20$ $2458$ $7.595$ $12.79$ $0.00$ <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>							
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							
129.226 $1016.09$ $2473$ $6.475$ $13.51$ $0.00$ $0.00$ $131.238$ $1000.06$ $2478$ $6.475$ $4.87$ $0.00$ $0.00$ $133.250$ $974.00$ $2479$ $6.475$ $13.26$ $0.00$ $0.00$ $135.261$ $957.87$ $2467$ $6.475$ $4.86$ $0.00$ $0.00$ $137.273$ $931.91$ $2476$ $6.650$ $13.03$ $0.00$ $0.00$ $139.285$ $915.72$ $2471$ $6.650$ $4.85$ $0.00$ $0.00$ $141.296$ $889.81$ $2465$ $6.825$ $13.02$ $0.00$ $0.00$ $143.308$ $873.57$ $2471$ $6.825$ $4.83$ $0.00$ $0.00$ $145.320$ $847.69$ $2463$ $7.000$ $12.94$ $0.00$ $0.00$ $147.331$ $831.41$ $2461$ $7.000$ $4.81$ $0.00$ $0.00$ $149.343$ $805.59$ $2465$ $7.000$ $4.77$ $0.00$ $0.00$ $153.366$ $763.46$ $2428$ $7.298$ $12.84$ $0.00$ $0.00$ $155.378$ $747.13$ $2451$ $7.298$ $4.76$ $0.00$ $0.00$ $157.390$ $721.40$ $2465$ $7.298$ $12.85$ $0.00$ $0.00$ $163.425$ $662.86$ $2436$ $7.595$ $12.78$ $0.00$ $0.00$ $163.425$ $662.86$ $2436$ $7.595$ $12.84$ $0.00$ $0.00$ $165.436$ $637.20$ $2458$ $7.595$ $12.84$ $0.00$							
131. 2381000. 062478 $6.475$ $4.87$ $0.00$ $0.00$ 133. 250974. 002479 $6.475$ 13. 26 $0.00$ $0.00$ 135. 261957. 872467 $6.475$ $4.86$ $0.00$ $0.00$ 137. 273931. 912476 $6.650$ 13. 03 $0.00$ $0.00$ 139. 285915. 722471 $6.650$ $4.85$ $0.00$ $0.00$ 141. 296889. 812465 $6.825$ 13. 02 $0.00$ $0.00$ 143. 308873. 572471 $6.825$ $4.83$ $0.00$ $0.00$ 145. 320847. 692463 $7.000$ $12. 94$ $0.00$ $0.00$ 147. 331831. 412461 $7.000$ $4.81$ $0.00$ $0.00$ 149. 343805. 592465 $7.000$ $12. 80$ $0.00$ $0.00$ 151. 355789. 272451 $7.000$ $4.77$ $0.00$ $0.00$ 155. 378747. 132451 $7.298$ $12. 84$ $0.00$ $0.00$ 155. 378747. 132451 $7.298$ $4.76$ $0.00$ $0.00$ 157. 390721. 402465 $7.298$ $12. 85$ $0.00$ $0.00$ 161. 413679. 242431 $7.595$ $12. 78$ $0.00$ $0.00$ 163. 425662. 862436 $7.595$ $4.68$ $0.00$ $0.00$ 165. 436637. 202458 $7.595$ $12. 84$ $0.00$ $0.00$ 166. 436637. 202458 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>							
133. 250974. 00 $2479$ $6.475$ 13. 26 $0.00$ $0.00$ 135. 261957. 872467 $6.475$ $4.86$ $0.00$ $0.00$ 137. 273931. 912476 $6.650$ $13.03$ $0.00$ $0.00$ 139. 285915. 722471 $6.650$ $4.85$ $0.00$ $0.00$ 141. 296889. 812465 $6.825$ $13.02$ $0.00$ $0.00$ 143. 308873. 572471 $6.825$ $4.83$ $0.00$ $0.00$ 145. 320847. 692463 $7.000$ $12.94$ $0.00$ $0.00$ 147. 331831. 412461 $7.000$ $4.81$ $0.00$ $0.00$ 149. 343805. 592465 $7.000$ $12.80$ $0.00$ $0.00$ 151. 355789. 272451 $7.000$ $4.77$ $0.00$ $0.00$ 155. 378747. 132451 $7.298$ $12.84$ $0.00$ $0.00$ 157. 390721. 402465 $7.298$ $12.85$ $0.00$ $0.00$ 161. 413679. 242431 $7.595$ $12. 78$ $0.00$ $0.00$ 163. 425662. 862436 $7.595$ $12.79$ $0.00$ $0.00$ 165. 436637. 202458 $7.595$ $12.79$ $0.00$ $0.00$ 167. 448620. 812460 $7.595$ $4.68$ $0.00$ $0.00$							
135. $261$ 957. $87$ 24676. $475$ 4. $86$ 0. 000. 00137. $273$ 931. 9124766. 65013. 030. 000. 00139. $285$ 915. 7224716. 6504. $85$ 0. 000. 00141. $296$ 889. 8124656. $825$ 13. 020. 000. 00143. 308 $873. 57$ 24716. $825$ 4. $83$ 0. 000. 00145. 320847. 6924637. 00012. 940. 000. 00145. 320847. 6924657. 0004. 810. 000. 00147. 331831. 4124617. 0004. 810. 000. 00149. 343805. 5924657. 00012. 800. 000. 00151. 355789. 2724517. 0004. 770. 000. 00153. 366763. 4624287. 29812. 840. 000. 00155. 378747. 1324517. 2984. 760. 000. 00157. 390721. 4024657. 29812. 850. 000. 00161. 413679. 2424317. 59512. 780. 000. 00163. 425662. 8624367. 59512. 790. 000. 00165. 436637. 2024587. 59512. 790. 000. 00165. 436637. 2024587. 59512. 840. 000. 00167. 448620. 8124607. 5954. 680. 000.							
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			•				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							
143. $308$ 873. $57$ 24716. $825$ 4. $83$ 0. 000. 00145. $320$ 847. $69$ 24637. 00012. 940. 000. 00147. $331$ 831. 4124617. 0004. 810. 000. 00149. $343$ 805. $59$ 24657. 00012. 800. 000. 00151. $355$ 789. 2724517. 0004. 770. 000. 00153. $366$ 763. 4624287. 29812. 840. 000. 00155. $378$ 747. 1324517. 2984. 760. 000. 00157. $390$ 721. 4024657. 29812. 850. 000. 00159. $401$ 705. 0424597. 2984. 730. 000. 00161. $413$ 679. 2424317. 59512. 780. 000. 00165. $436$ 637. 2024587. 59512. 790. 000. 00167. $448$ 620. 8124607. 5954. 680. 000. 00169. $460$ 595. 0524397. 59512. 840. 000. 00					•		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		831.41					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	149, 343	805.59	2465	7.000	12. 80 <sup>-</sup>	0.00	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	151, 355	789.27	2451	7.000	4.77	0.00	0.00
157. 390721. 4024657. 29812. 850. 000. 00159. 401705. 0424597. 2984. 730. 000. 00161. 413679. 2424317. 59512. 780. 000. 00163. 425662. 8624367. 5954. 690. 000. 00165. 436637. 2024587. 59512. 790. 000. 00167. 448620. 8124607. 5954. 680. 000. 00169. 460595. 0524397. 59512. 840. 000. 00	153, 366	763.46	2428	7 298	12.84	0.00	0,00
159. 401705. 0424597. 2984. 730. 000. 00161. 413679. 2424317. 59512. 780. 000. 00163. 425662. 8624367. 5954. 690. 000. 00165. 436637. 2024587. 59512. 790. 000. 00167. 448620. 8124607. 5954. 680. 000. 00169. 460595. 0524397. 59512. 840. 000. 00	155. 378	747.13	2451	7.298	4.76	0.00	0.00
161. 413679. 2424317. 59512. 780. 000. 00163. 425662. 8624367. 5954. 690. 000. 00165. 436637. 2024587. 59512. 790. 000. 00167. 448620. 8124607. 5954. 680. 000. 00169. 460595. 0524397. 59512. 840. 000. 00	157.390	721.40	2465	7.298	12.85	0.00	0.00
163. 425662. 8624367. 5954. 690. 000. 00165. 436637. 2024587. 59512. 790. 000. 00167. 448620. 8124607. 5954. 680. 000. 00169. 460595. 0524397. 59512. 840. 000. 00	159.401	705.04	2459	7.298	4.73	0.00	0.00
165. 436637. 2024587. 59512. 790. 000. 00167. 448620. 8124607. 5954. 680. 000. 00169. 460595. 0524397. 59512. 840. 000. 00	161, 413	679.24	2431	7.595	12.78	0.00	0.00
167.448620.8124607.5954.680.000.00169.460595.0524397.59512.840.000.00	163. 425	662. 86	2436	7.595	4.69	0.00	0. 00
169.460 595.05 2439 7.595 12.84 0.00 0.00	165.436	637.20	2 <b>458</b>	7.595	12.79	0. 00	0.00
	167.448	620, 81	2460	7.595	4.68	0.00	0. 00
171. 471 578. 61 2416 7. 893 4. 62 0. 00 0. 00	169.460	595.05	2439	7.595	12.84	0.00	0.00
	171.471	578.61	2416	7.893	4.62	0. 00	0.00

OADE       TABLE       HAXE       SECURIC       NAT       THE       4.50       NAT       THE       3.500       DXRE       STANCE       NAT       STANCE       NAT       STANCE       NAT       STANCE       NAT       STANCE       NAT       STANCE       NAT       STANCE       STANCE       PLOP       3.500       DXRE       STANCE       NAT       STANCE       STANCE       NAT       STANCE       NAT       STANCE       NAT       STANCE       NAT       NAT       NAT       NAT       NAT       NAT       NAT		DISC	HARGE	HYDROGRAPI BELOW	i for RUN2	ւս	ggye			STATI( 0.0(	on number o	1			
MAX         STAGE         4.9         MAT         TIME         3.500         HORS           TIME         STAGE         CLUT         2576         GS         AT         1100         5000         5000           HR         M         GBS         0         1000         2000         3000         4000         5000           0.2         0.5         58         *         -         -         -         -           0.4         0.7         87         *         -         -         -         -           0.6         0.9         148         *         -         -         -         -         -           1.0         1.6         368         .         *         -         -         -         -         -           1.0         1.6         2.7         7         *         -		GAGE	ZER0		M			ATIO	REACHED			4539.	92 M		
HAX         FLOW         2.576         CAS         AT THE         3.500         HOURS           HB         M         CAS         0         1000         2000         3000         4000         5000           0.0         0.5         50         *         -         -         -         -           0.4         0.7         87         *         -         -         -         -           0.4         0.7         87         *         -         -         -         -           0.4         0.7         87         *         -         -         -         -           0.4         0.7         87         *         -         -         -         -           0.4         0.7         87         *         -         -         -         -           0.8         1.2         243         .         -         -         -         -         -           1.2         1.9         5263         -         -         -         -         -         -           2.4         4.0         1811         -         +         -         -         -         -				MAX ST							3 500 HOURS				
The:       STACE       PLON         HR       M       MS       0       1000       2000       3000       4000       5006         0.2       0.5       58       *       .       .       .       .       .         0.4       0.7       87       *       .       .       .       .       .         0.6       0.9       148       *       .       .       .       .       .         1.0       1.6       308       .       *       .       .       .       .         1.0       1.6       308       .       *       .       .       .       .         1.4       2.3       707       *       *       .       .       .       .         1.4       2.3       707       *       *       .       .       .       .       .       .         2.2       3.7       1509       .       *       .<															
$0.0$ $0.5$ $550$ $*$ $\cdot$ $\cdot$ $0.2$ $0.5$ $58$ $*$ $\cdot$ $\cdot$ $\cdot$ $0.6$ $0.7$ $87$ $*$ $\cdot$ $\cdot$ $\cdot$ $0.6$ $0.9$ $148$ $*$ $\cdot$ $\cdot$ $\cdot$ $1.6$ $2.43$ $*$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $1.2$ $1.9$ $523$ $*$ $\cdot$ $\cdot$ $\cdot$ $1.4$ $2.3$ $707$ $*$ $*$ $\cdot$ $\cdot$ $2.2$ $3.7$ $1737$ $*$ $*$ $\cdot$ $\cdot$ $2.4$ $4.0$ $8111$ $\cdot$ $*$ $\cdot$ $\cdot$ $2.4$ $4.0$ $8111$ $\cdot$ $*$ $\cdot$ $\cdot$ $2.4$ $4.0$ $8120$ $*$ $*$ $\cdot$ $\cdot$ $3.4$ $4.9$ $2528$ $\cdot$ $*$ $\cdot$ $\cdot$ $4.6$ $2.7$ $228$ $*$ $\cdot$ $\cdot$ $\cdot$ $4.6$ $2.7$ $228$ $*$	T	IME S	STAGE												
0.2       0.6       58       *       .       .         0.4       0.7       87       *       .       .         0.6       0.9       148       *       .       .         0.8       1.2       243       *       .       .         1.0       1.6       368       *       .       .         1.2       1.9       523       .       .       .         1.4       2.3       707       *       .       .       .         1.4       2.3       707       *       .       .       .         1.4       2.3       707       *       .       .       .         1.4       2.3       707       *       .       .       .         2.6       3.4       1973       .       *       .       .         2.4       4.0       1811       .       *       .       .       .         2.8       4.5       2169       .       .       .       .       .         3.0       4.6       2079       .       *       .       .       .         3.1       1079       .	ł	1R	M	CMS	0	1000		2000	300	0	4000	5000			
0.4 $0.7$ $87$ $*$ $  0.6$ $0.9$ $143$ $*$ $  1.0$ $1.6$ $243$ $*$ $  1.0$ $1.6$ $243$ $*$ $  1.4$ $2.3$ $707$ $*$ $  1.4$ $2.3$ $707$ $*$ $  1.6$ $2.7$ $916$ $*$ $  1.6$ $2.7$ $916$ $*$ $  2.0$ $3.4$ $1373$ $*$ $  2.6$ $4.3$ $2002$ $*$ $  2.6$ $4.3$ $2002$ $*$ $  2.8$ $4.5$ $2002$ $*$ $  3.6$ $4.6$ $2309$ $ *$ $ 3.8$ $4.1$ $828$ $   3.6$ $4.6$ $2798$	(	), ()	0.5	50	.*			•							
$0.6$ $0.9$ $1.48$ $*$ $\cdot$ <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>•</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>								•							
0.8 $1.2$ $243$ $*$ $  1.0$ $1.6$ $2.63$ $*$ $  1.4$ $2.3$ $707$ $*$ $  1.4$ $2.3$ $707$ $*$ $  1.6$ $2.7$ $916$ $*$ $  2.0$ $3.4$ $1373$ $ *$ $  2.1$ $3.7$ $1599$ $ *$ $  2.4$ $4.0$ $1811$ $ *$ $  2.6$ $3.7$ $1599$ $ *$ $  2.8$ $4.5$ $2169$ $ *$ $  3.0$ $4.6$ $2309$ $ *$ $  3.4$ $4.9$ $2528$ $ *$ $  3.6$ $4.6$ $2309$ $ *$ $  4.0$ $3.7$ $1566$ $ *$ $  4.0$ $3.7$ $1566$ $ *$ $  4.2$ $3.3$ $1292$ $ *$ $  4.4$ $3.0$ $1091$ $ *$ $  4.4$ $3.0$ $1091$ $    4.6$ $2.7$ $928$ $*$ $   4.4$ $3.0$ $1091$ $    4.4$ $3.0$ $1091$ $   -$ <t< th=""><th></th><th></th><th></th><th></th><th>. *</th><th>•</th><th></th><th>•</th><th></th><th>•</th><th>•</th><th>•</th><th></th><th></th><th></th></t<>					. *	•		•		•	•	•			
1. 01. 6368*1. 21. 9523*.1. 42.3707*.1. 62. 7916*.1. 83. 1139.*.2. 03. 41373.*.2. 23. 71599.*.2. 44. 01811.*.2. 64. 32002.*.3. 04. 62309*3. 44. 925283. 64. 623093. 64. 623093. 64. 623093. 715564. 82. 73. 84. 118884. 43. 010915. 22. 16025. 42. 05286. 41.32526. 61.32767. 81.01337. 41.11977. 51.01337. 61.01837. 71.11977. 7<					.*	•		٠							
1.2       1.9       623       *       .       .         1.6       2.7       916       *       .       .         1.8       3.1       1139       *       .       .         2.0       3.4       1373       *       .       .         2.4       4.0       1811       *       .       .         2.4       4.0       1811       *       .       .         2.6       4.3       2002       *       *       .       .         2.8       4.5       2169       .       *       .       .         3.0       4.6       2330       .       *       .       .         3.4       4.9       268       .       *       .       .         3.8       4.1       1888       *       *       .       .         4.0       3.7       1566       *       .       .       .         4.2       3.3       1292       .       *       .       .         4.2       3.3       1292       .       *       .       .         5.0       2.3       6900       .       .       <						٠		٠		•	•	•			
1.4       2.3       707       *       .       .         1.6       2.7       916       *       .       .         2.0       3.4       1373       .       *       .       .         2.0       3.4       1373       .       *       .       .         2.0       3.4       1373       .       *       .       .         2.2       3.7       1599       .       *       .       .         2.4       4.0       1811       .       *       .       .         2.6       4.3       2002       .       *       .       .         3.0       4.6       2309       .       *       .       .         3.2       4.8       2427       .       *       .       .         3.4       4.9       2528       .       .       .       .         3.4       1888       .       *       .       .       .         4.1       1888       .       *       .       .       .         4.2       3.0       1991       .       .       .       .         5.0       2.3 </th <th></th> <th></th> <th></th> <th></th> <th>• •</th> <th>•</th> <th></th> <th>•</th> <th></th> <th>•</th> <th>•</th> <th>•</th> <th></th> <th></th> <th></th>					• •	•		•		•	•	•			
I.6       2.7       916       *         1.8       3.1       1139       *       .         2.0       3.4       1373       *       .         2.2       3.7       1599       .       *       .         2.4       4.0       1811       *       .       .         2.6       4.3       2002       *       .       .         2.8       4.5       2169       .       *       .         3.0       4.6       2309       .       *       .         3.4       4.9       2528       .       *       .         3.6       4.6       2300       .       *       .         3.6       4.6       2300       .       *       .       .         3.6       3.7       1566       .       *       .       .         4.0       3.7       1566       .       *       .       .         4.8       2.6       798       .       .       .       .         5.0       2.3       600       .       .       .       .         5.4       1.6       .       .       .						ъ ,		•		•	•	٠			
1.8       3.1       1139        *          2.0       3.4       1373        *          2.2       3.7       1699        *          2.4       4.0       1811        *          2.6       4.3       2002        *          3.0       4.6       2309        *          3.2       4.8       2427        *          3.4       4.9       2528        *          3.4       4.9       2578        *          3.6       4.6       2300        *          3.8       4.1       1888        *          4.2       3.3       1922            4.4       3.0       1091        *           5.2       2.3       690       *            5.4       2.0       628       * </th <th></th> <th></th> <th></th> <th></th> <th></th> <th>*. L</th> <th></th> <th>•</th> <th></th> <th>•</th> <th>•</th> <th>•</th> <th></th> <th></th> <th></th>						*. L		•		•	•	•			
2.03.41373**2.23.71599**.2.44.01811**.2.64.32002**.2.84.52169*3.04.62309**.3.44.92528**.3.44.92528**.3.84.11888*.4.03.71556*.4.23.31292*.4.43.01292.*4.52.7928*.4.63.01292.*5.22.1600*.5.22.16286.41.43036.51.74166.61.32767.21.63356.41.43037.61.27.71.1137.81.01597.91.07.61.01837.71.1137.81.01707.91.07.11.17.6 <th></th> <th></th> <th></th> <th></th> <th>•</th> <th></th> <th></th> <th>•</th> <th></th> <th>•</th> <th>•</th> <th>•</th> <th></th> <th></th> <th></th>					•			•		•	•	•			
2.2       3.7       1599       *       .         2.4       4.0       1811       *       .       .         2.6       4.3       2002       *       .       .         3.0       4.6       2309       .       *       .       .         3.1       4.8       2427       .       *       .       .         3.4       4.9       2528       .       .       *       .       .         3.6       4.6       2330       .       *       .       .       .       .         3.8       4.1       1888       .       *       .       .       .       .         4.0       3.7       1566       .       *       .       .       .       .         4.1       3.0       1091       .       *       .       .       .       .         5.0       2.3       690       *       .       .       .       .       .         5.1       2.0       628       *       .       .       .       .       .         6.2       1.5       335       *       .       .       . <t< th=""><th></th><th></th><th></th><th></th><th>•</th><th>. •</th><th>*</th><th>•</th><th></th><th>•</th><th>•</th><th>•</th><th></th><th></th><th>•</th></t<>					•	. •	*	•		•	•	•			•
$2.4$ $4.0$ $1811$ $*$ $*$ $\cdot$ $\cdot$ $2.6$ $4.5$ $2002$ $*$ $*$ $\cdot$ $\cdot$ $3.0$ $4.6$ $2309$ $\cdot$ $*$ $\cdot$ $\cdot$ $3.2$ $4.8$ $2427$ $\cdot$ $*$ $\cdot$ $\cdot$ $3.4$ $4.9$ $5228$ $\cdot$ $*$ $\cdot$ $\cdot$ $3.4$ $4.9$ $5228$ $\cdot$ $*$ $\cdot$ $\cdot$ $3.6$ $4.6$ $2330$ $\cdot$ $*$ $\cdot$ $\cdot$ $3.8$ $4.6$ $2330$ $\cdot$ $*$ $\cdot$ $\cdot$ $4.0$ $3.7$ $1556$ $*$ $*$ $\cdot$ $\cdot$ $4.0$ $3.7$ $1556$ $*$ $*$ $\cdot$ $\cdot$ $4.6$ $2.7$ $928$ $*$ $*$ $\cdot$ $\cdot$ $4.6$ $2.7$ $928$ $*$ $*$ $\cdot$ $\cdot$ $4.6$ $2.7$ $928$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $2.3$ $690$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $2.3$ $690$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $1.8$ $467$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $1.8$ $467$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $\cdot$ $7.0$ $1.2$ $231$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ <					•	•	*	•		•	•	•		* A A A	
2.6       4.3       2002       .       *       .       .         2.8       4.5       2169       .       .       *       .       .         3.0       4.6       2309       .       .       *       .       .         3.2       4.8       2427       .       .       *       .       .         3.4       4.9       2528       .       .       *       .       .         3.6       4.6       2330       .       .       *       .       .         3.8       4.1       1888       .       *       .       .       .         4.0       3.7       1566       .       *       .       .       .         4.2       3.0       1091       .       *       .       .       .         4.6       2.7       928       *       .       .       .       .         5.0       2.3       690       *       .       .       .       .         5.4       2.0       528       .       *       .       .       .         5.4       1.7       116       .       . <td< th=""><th></th><th></th><th></th><th></th><th>•</th><th></th><th>•</th><th>*.</th><th></th><th>-</th><th>•</th><th>•</th><th></th><th></th><th></th></td<>					•		•	*.		-	•	•			
$2.8$ $4.5$ $2169$ $\cdot$ $*$ $\cdot$ $\cdot$ $3.2$ $4.6$ $2309$ $\cdot$ $*$ $\cdot$ $\cdot$ $3.4$ $4.9$ $2528$ $\cdot$ $*$ $\cdot$ $\cdot$ $3.6$ $4.6$ $2330$ $\cdot$ $*$ $\cdot$ $\cdot$ $3.8$ $4.1$ $1888$ $*$ $*$ $\cdot$ $\cdot$ $4.0$ $3.7$ $1556$ $*$ $*$ $\cdot$ $\cdot$ $4.2$ $3.3$ $1292$ $*$ $*$ $\cdot$ $\cdot$ $4.4$ $3.0$ $1091$ $*$ $*$ $\cdot$ $\cdot$ $4.6$ $2.7$ $928$ $*$ $\cdot$ $\cdot$ $\cdot$ $4.6$ $2.7$ $928$ $*$ $\cdot$ $\cdot$ $\cdot$ $4.6$ $2.7$ $928$ $*$ $\cdot$ $\cdot$ $\cdot$ $5.0$ $2.3$ $690$ $*$ $\cdot$ $\cdot$ $\cdot$ $5.6$ $1.7$ $416$ $*$ $\cdot$ $\cdot$ $\cdot$ $5.6$ $1.7$ $416$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.4$ $1.4$ $303$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $\cdot$ $7.2$ $1.1$ $213$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $\cdot$ $7.4$ $1.4$ $303$ $*$ $\cdot$ $\cdot$ $\cdot$ $7.6$ $1.0$ $183$ <td< th=""><th></th><th></th><th></th><th></th><th></th><th>ż</th><th></th><th>*</th><th></th><th></th><th>÷</th><th>÷</th><th></th><th></th><th></th></td<>						ż		*			÷	÷			
$3.2$ $4.8$ $2427$ $\cdot$ $\bullet$ $\cdot$ $3.6$ $4.6$ $230$ $\cdot$ $\bullet$ $\cdot$ $3.8$ $4.1$ $1888$ $\bullet$ $\bullet$ $\cdot$ $4.0$ $3.7$ $1566$ $\bullet$ $\bullet$ $\cdot$ $4.2$ $3.3$ $1292$ $\bullet$ $\bullet$ $\cdot$ $4.4$ $3.0$ $1091$ $\bullet$ $\bullet$ $\cdot$ $4.4$ $3.0$ $1091$ $\bullet$ $\bullet$ $\cdot$ $4.4$ $3.0$ $1091$ $\bullet$ $\bullet$ $\cdot$ $4.6$ $2.7$ $928$ $\bullet$ $\bullet$ $\cdot$ $5.0$ $2.3$ $690$ $\bullet$ $\cdot$ $\cdot$ $\cdot$ $5.0$ $2.3$ $690$ $\bullet$ $\cdot$ $\cdot$ $\cdot$ $5.6$ $1.8$ $467$ $\bullet$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $\bullet$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $\bullet$ $\cdot$ $\cdot$ $\cdot$ <						•			*	•	,	•			
3.4 $4.9$ $2528$ $*$ $*$ $ 3.8$ $4.1$ $1888$ $*$ $*$ $ 4.0$ $3.7$ $1556$ $*$ $  4.2$ $3.3$ $1292$ $*$ $  4.4$ $3.0$ $1091$ $*$ $  4.6$ $2.7$ $928$ $*$ $  4.8$ $2.5$ $798$ $*$ $  5.0$ $2.3$ $690$ $*$ $  5.2$ $2.1$ $602$ $*$ $  5.4$ $2.0$ $628$ $*$ $  6.4$ $1.6$ $372$ $*$ $  6.6$ $1.3$ $2252$ $*$ $  7.0$ $1.2$ $231$ $*$ $  7.4$ $1.1$ $197$ $*$ $  7.6$ $1.0$ $183$ <td< th=""><th>3</th><th>3. 0</th><th>4.6</th><th>2309</th><th></th><th>,</th><th></th><th></th><th>*</th><th></th><th></th><th></th><th></th><th></th><th></th></td<>	3	3. 0	4.6	2309		,			*						
$3.6$ $4.6$ $2330$ $*$ $*$ $\cdot$ $3.8$ $4.1$ $1888$ $*$ $\cdot$ $\cdot$ $4.0$ $3.7$ $1566$ $*$ $*$ $\cdot$ $4.2$ $3.3$ $1292$ $*$ $\cdot$ $\cdot$ $4.4$ $3.0$ $1091$ $*$ $\cdot$ $\cdot$ $4.6$ $2.7$ $928$ $*$ $\cdot$ $\cdot$ $4.6$ $2.6$ $798$ $*$ $\cdot$ $\cdot$ $5.0$ $2.3$ $690$ $*$ $\cdot$ $\cdot$ $\cdot$ $5.4$ $2.0$ $528$ $*$ $\cdot$ $\cdot$ $\cdot$ $5.4$ $2.0$ $528$ $*$ $\cdot$ $\cdot$ $\cdot$ $5.6$ $1.7$ $416$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.4$ $1.4$ $303$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.8$ $1.3$ $252$ $*$ $\cdot$ $\cdot$ $\cdot$ $7.2$ $1.1$ $133$ $*$ $\cdot$ <th>2</th> <th>3. 2</th> <th>4.8</th> <th>2427</th> <th></th> <th></th> <th></th> <th></th> <th>* .</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>	2	3. 2	4.8	2427					* .						
$3.8$ $4.1$ $1888$ $*$ $\cdot$ $4.0$ $3.7$ $1566$ $*$ $\cdot$ $\cdot$ $4.2$ $3.3$ $1292$ $*$ $\cdot$ $\cdot$ $4.4$ $3.0$ $1091$ $*$ $\cdot$ $\cdot$ $4.6$ $2.7$ $928$ $*$ $\cdot$ $\cdot$ $4.6$ $2.7$ $928$ $*$ $\cdot$ $\cdot$ $5.0$ $2.3$ $690$ $*$ $\cdot$ $\cdot$ $5.2$ $2.1$ $602$ $*$ $\cdot$ $\cdot$ $5.4$ $2.0$ $528$ $*$ $\cdot$ $\cdot$ $5.6$ $1.8$ $467$ $*$ $\cdot$ $\cdot$ $6.4$ $2.0$ $528$ $*$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $6.6$ $1.3$ $252$ $*$ $\cdot$ $\cdot$ $7.0$ $1.2$ $231$ $*$ $\cdot$ $\cdot$ $7.6$ $1.0$ $183$ $*$	3	3.4	4.9	252 <b>8</b>		•			*	•					
$4.0$ $3.7$ $1556$ $*$ $*$ $\cdot$ $4.2$ $3.3$ $1292$ $*$ $*$ $\cdot$ $4.4$ $3.0$ $1091$ $*$ $\cdot$ $\cdot$ $4.4$ $3.0$ $1091$ $*$ $\cdot$ $\cdot$ $4.4$ $3.0$ $1091$ $*$ $\cdot$ $\cdot$ $4.8$ $2.6$ $798$ $*$ $\cdot$ $\cdot$ $5.0$ $2.3$ $690$ $*$ $\cdot$ $\cdot$ $\cdot$ $5.4$ $2.0$ $528$ $*$ $\cdot$ $\cdot$ $\cdot$ $5.6$ $1.8$ $467$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.4$ $1.4$ $303$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.4$ $1.4$ $303$ $*$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $\cdot$ $7.0$ $1.2$ $231$ $*$ $\cdot$ $\cdot$ $\cdot$ $7.6$ $1.0$ $183$ $*$ <th></th> <th></th> <th></th> <th></th> <th></th> <th>•</th> <th></th> <th>•</th> <th>* .</th> <th></th> <th>•</th> <th></th> <th></th> <th></th> <th></th>						•		•	* .		•				
$4.2$ $3.3$ $1292$ $*$ $\cdot$ $\cdot$ $4.4$ $3.0$ $1091$ $*$ $\cdot$ $\cdot$ $4.6$ $2.7$ $928$ $*$ $\cdot$ $\cdot$ $4.8$ $2.5$ $798$ $*$ $\cdot$ $\cdot$ $5.0$ $2.3$ $690$ $*$ $\cdot$ $\cdot$ $5.2$ $2.1$ $602$ $*$ $\cdot$ $\cdot$ $5.4$ $2.0$ $628$ $*$ $\cdot$ $\cdot$ $5.6$ $1.8$ $467$ $*$ $\cdot$ $\cdot$ $5.6$ $1.7$ $416$ $*$ $\cdot$ $\cdot$ $6.0$ $1.6$ $372$ $*$ $\cdot$ $\cdot$ $6.4$ $1.4$ $303$ $*$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $7.0$ $1.2$ $231$ $*$ $\cdot$ $\cdot$ $7.4$ $1.1$ $197$ $*$ $\cdot$ $\cdot$ $7.8$ $1.0$ $170$ $*$					.• .	•		*.		•	•	•			
$4.4$ $3.0$ $1091$ $*$ $\cdot$ $\cdot$ $4.6$ $2.7$ $928$ $*$ $\cdot$ $\cdot$ $4.8$ $2.6$ $798$ $*$ $\cdot$ $\cdot$ $5.0$ $2.3$ $690$ $*$ $\cdot$ $\cdot$ $5.2$ $2.1$ $602$ $*$ $\cdot$ $\cdot$ $5.4$ $2.0$ $528$ $*$ $\cdot$ $\cdot$ $5.6$ $1.8$ $467$ $*$ $\cdot$ $\cdot$ $6.6$ $1.6$ $372$ $*$ $\cdot$ $\cdot$ $6.0$ $1.6$ $372$ $*$ $\cdot$ $\cdot$ $6.4$ $1.4$ $303$ $*$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $7.0$ $1.2$ $231$ $*$ $\cdot$ $\cdot$ $7.4$ $1.1$ $197$ $*$ $\cdot$ $\cdot$ $7.6$ $1.0$ $183$ $*$ $\cdot$ $\cdot$ $7.6$ $1.0$ $169$ $*$ <					•	•	*	•		•	•				
$4.6$ $2.7$ $928$ $*$ $\cdot$ $\cdot$ $4.8$ $2.5$ $798$ $*$ $\cdot$ $\cdot$ $5.0$ $2.3$ $690$ $*$ $\cdot$ $\cdot$ $5.2$ $2.1$ $602$ $*$ $\cdot$ $\cdot$ $5.4$ $2.0$ $528$ $*$ $\cdot$ $\cdot$ $5.4$ $2.0$ $528$ $*$ $\cdot$ $\cdot$ $5.6$ $1.8$ $467$ $*$ $\cdot$ $\cdot$ $5.6$ $1.7$ $416$ $*$ $\cdot$ $\cdot$ $6.0$ $1.6$ $372$ $*$ $\cdot$ $\cdot$ $6.4$ $1.4$ $303$ $*$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $7.0$ $1.2$ $231$ $*$ $\cdot$ $\cdot$ $7.0$ $1.2$ $231$ $*$ $\cdot$ $\cdot$ $7.6$ $1.0$ $183$ $*$ $\cdot$ $\cdot$ $7.8$ $1.0$ $170$ $*$ </th <th></th> <th></th> <th></th> <th></th> <th>••</th> <th>•</th> <th>*</th> <th>•</th> <th></th> <th></th> <th></th> <th></th> <th>•</th> <th></th> <th></th>					••	•	*	•					•		
4.8 $2.5$ $798$ $*$ .       .					•	.*		•		•	•	•			
5.0 $2.3$ $690$ $*$ .       .					•	*.		•	÷	•	•	•			
$5.2$ $2.1$ $602$ $*$ $\cdot$ $\cdot$ $5.4$ $2.0$ $628$ $*$ $\cdot$ $\cdot$ $5.6$ $1.8$ $467$ $*$ $\cdot$ $\cdot$ $5.6$ $1.7$ $416$ $*$ $\cdot$ $\cdot$ $6.8$ $1.7$ $416$ $*$ $\cdot$ $\cdot$ $6.6$ $1.7$ $335$ $*$ $\cdot$ $\cdot$ $6.2$ $1.5$ $335$ $*$ $\cdot$ $\cdot$ $6.4$ $1.4$ $303$ $*$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $7.0$ $1.2$ $231$ $*$ $\cdot$ $\cdot$ $7.2$ $1.1$ $213$ $*$ $\cdot$ $\cdot$ $7.4$ $1.1$ $197$ $*$ $\cdot$ $\cdot$ $7.8$ $1.0$ $170$ $*$ $\cdot$ $\cdot$ $8.0$ $1.0$ $149$ $*$ </th <th></th> <th></th> <th></th> <th></th> <th>-</th> <th>*. •</th> <th></th> <th>•</th> <th>· ·</th> <th>• '</th> <th>•</th> <th>•</th> <th></th> <th></th> <th></th>					-	*. •		•	· ·	• '	•	•			
$5.4$ $2.0$ $528$ $*$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $5.6$ $1.8$ $467$ $*$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $5.8$ $1.7$ $416$ $*$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $6.0$ $1.6$ $372$ $*$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $6.2$ $1.5$ $335$ $*$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $6.4$ $1.4$ $303$ $*$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $6.6$ $1.3$ $276$ $*$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $6.8$ $1.3$ $252$ $*$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $7.0$ $1.2$ $231$ $*$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $7.4$ $1.1$ $197$ $*$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $7.6$ $1.0$ $183$ $*$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $8.0$ $1.0$ $141$ $*$ <					•	* .		•		•	•	•			
5.6 $1.8$ $467$ $*$ $.$ $.$ $.$ $5.8$ $1.7$ $416$ $*$ $.$ $.$ $.$ $6.0$ $1.6$ $372$ $*$ $.$ $.$ $.$ $6.0$ $1.6$ $372$ $*$ $.$ $.$ $.$ $6.2$ $1.5$ $335$ $*$ $.$ $.$ $.$ $6.4$ $1.4$ $303$ $*$ $.$ $.$ $.$ $6.4$ $1.4$ $303$ $*$ $.$ $.$ $.$ $6.8$ $1.3$ $276$ $*$ $.$ $.$ $.$ $7.0$ $1.2$ $231$ $*$ $.$ $.$ $.$ $7.0$ $1.2$ $231$ $*$ $.$ $.$ $.$ $7.4$ $1.1$ $197$ $*$ $.$ $.$ $.$ $7.4$ $1.0$ $170$ $*$ $.$ $.$ $.$ $8.0$ $0.9$ $149$ $*$ $.$ $.$ <t< th=""><th></th><th></th><th></th><th></th><th></th><th>•</th><th>•</th><th>•</th><th></th><th>•</th><th>•</th><th>•</th><th></th><th></th><th></th></t<>						•	•	•		•	•	•			
5.8 $1.7$ $416$ $*$ .       .       .       . $6.0$ $1.6$ $372$ $*$ .       .       .       . $6.2$ $1.5$ $335$ $*$ .       .       .       . $6.2$ $1.5$ $335$ $*$ .       .       .       . $6.4$ $1.4$ $303$ $*$ .       .       .       . $6.6$ $1.3$ $276$ $*$ .       .       .       . $6.8$ $1.3$ $252$ $*$ .       .       .       . $7.0$ $1.2$ $231$ $*$ .       .       .       . $7.2$ $1.1$ $213$ $*$ .       .       .       . $7.4$ $1.1$ $197$ $*$ .       .       .       . $7.8$ $1.0$ $170$ $*$ .       .       .       . $8.2$ $0.9$ $149$ $*$ .       .       .       .      <					*										
6.0 $1.6$ $372$ *       .					· *										
6.2 $1.5$ $335$ $*$ .       .       .       . $6.4$ $1.4$ $303$ $*$ .       .       .       . $6.6$ $1.3$ $276$ $*$ .       .       .       . $6.8$ $1.3$ $252$ $*$ .       .       .       . $7.0$ $1.2$ $231$ $*$ .       .       .       . $7.0$ $1.2$ $231$ $*$ .       .       .       . $7.2$ $1.1$ $213$ $*$ .       .       .       . $7.4$ $1.1$ $197$ $*$ .       .       .       . $7.6$ $1.0$ $183$ $*$ .       .       .       . $8.0$ $1.0$ $159$ $*$ .       .       .       . $8.4$ $0.9$ $141$ $*$ .       .       .       . $9.0$ $0.8$ $120$ $*$ .       .       .       .      <					. *										
6.6 $1.3$ $276$ $*$ $.$ $.$ $.$ $.$ $6.8$ $1.3$ $252$ $*$ $.$ $.$ $.$ $.$ $7.0$ $1.2$ $231$ $*$ $.$ $.$ $.$ $.$ $7.0$ $1.2$ $231$ $*$ $.$ $.$ $.$ $.$ $7.2$ $1.1$ $213$ $*$ $.$ $.$ $.$ $.$ $7.4$ $1.1$ $197$ $*$ $.$ $.$ $.$ $.$ $7.6$ $1.0$ $183$ $*$ $.$ $.$ $.$ $.$ $7.8$ $1.0$ $170$ $*$ $.$ $.$ $.$ $.$ $8.0$ $1.0$ $159$ $*$ $.$ $.$ $.$ $.$ $8.4$ $0.9$ $141$ $.*$ $.$ $.$ $.$ $.$ $8.6$ $0.8$ $126$ $.*$ $.$ $.$ $.$ $.$ $9.2$ $0.8$ $109$ $.$					. *							•			
6.8 $1.3$ $252$ $*$ $.$ $.$ $.$ $.$ $7.0$ $1.2$ $231$ $*$ $.$ $.$ $.$ $.$ $7.2$ $1.1$ $213$ $*$ $.$ $.$ $.$ $.$ $7.4$ $1.1$ $197$ $*$ $.$ $.$ $.$ $.$ $7.6$ $1.0$ $183$ $*$ $.$ $.$ $.$ $.$ $7.6$ $1.0$ $183$ $*$ $.$ $.$ $.$ $.$ $8.0$ $1.0$ $159$ $*$ $.$ $.$ $.$ $.$ $8.2$ $0.9$ $149$ $*$ $.$ $.$ $.$ $.$ $8.4$ $0.9$ $141$ $*$ $.$ $.$ $.$ $.$ $8.6$ $0.9$ $133$ $*$ $.$ $.$ $.$ $.$ $9.0$ $0.8$ $120$ $*$ $.$ $.$ $.$ $.$ $9.4$ $0.8$ $109$ $*$ <	ť	5.4	1.4	303	. *	•									
7.0 $1.2$ $231$ $*$ .       .       .       .       . $7.2$ $1.1$ $213$ $*$ .       .       .       .       . $7.4$ $1.1$ $197$ $*$ .       .       .       .       . $7.6$ $1.0$ $183$ $*$ .       .       .       . $7.8$ $1.0$ $170$ $*$ .       .       .       . $8.0$ $1.0$ $159$ $*$ .       .       .       . $8.2$ $0.9$ $149$ $*$ .       .       .       . $8.4$ $0.9$ $141$ $*$ .       .       .       . $8.6$ $0.9$ $133$ $*$ .       .       .       . $9.0$ $0.8$ $120$ $*$ .       .       .       . $9.2$ $0.8$ $114$ $*$ .       .       .       .       . $9.4$ $0.8$ $109$ $*$ . <th></th> <th></th> <th></th> <th></th> <th>. *</th> <th>•</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>					. *	•									
7.2 $1.1$ $213$ $*$ .       .						•		·		•		•			
7.4 $1.1$ $197$ $*$ $7.6$ $1.0$ $183$ $*$ $7.8$ $1.0$ $170$ $*$ $8.0$ $1.0$ $159$ $*$ $8.2$ $0.9$ $149$ $*$ $8.4$ $0.9$ $141$ $*$ $8.6$ $0.9$ $133$ $*$ $8.6$ $0.9$ $133$ $*$ $9.0$ $0.8$ $126$ $*$ $9.2$ $0.8$ $114$ $*$ $9.4$ $0.8$ $109$ $*$ $9.6$ $0.7$ $104$ $*$						•		•		•	•	•			
7.6 $1.0$ $183$ $*$ $.$ $.$ $.$ $.$ $.$ $7.8$ $1.0$ $170$ $*$ $.$ $.$ $.$ $.$ $.$ $8.0$ $1.0$ $159$ $*$ $.$ $.$ $.$ $.$ $.$ $8.2$ $0.9$ $149$ $*$ $.$ $.$ $.$ $.$ $.$ $8.4$ $0.9$ $141$ $*$ $.$ $.$ $.$ $.$ $8.6$ $0.9$ $133$ $*$ $.$ $.$ $.$ $.$ $8.6$ $0.9$ $133$ $*$ $.$ $.$ $.$ $.$ $9.0$ $0.8$ $126$ $*$ $.$ $.$ $.$ $.$ $9.0$ $0.8$ $120$ $*$ $.$ $.$ $.$ $.$ $9.4$ $0.8$ $109$ $*$ $.$ $.$ $.$ $.$ $.$ $9.6$ $0.7$ $104$ $*$ $.$ $.$ $.$ $.$ $.$						•		•		,	•	•			
7.8 $1.0$ $170$ $*$ $8.0$ $1.0$ $159$ $*$ $8.2$ $0.9$ $149$ $*$ $8.4$ $0.9$ $141$ $*$ $8.6$ $0.9$ $133$ $*$ $8.6$ $0.9$ $133$ $*$ $9.0$ $0.8$ $126$ $*$ $9.2$ $0.8$ $114$ $*$ $9.4$ $0.8$ $109$ $*$ $9.6$ $0.7$ $104$ $*$ $9.8$ $0.7$ $100$ $*$						•		•		•	•	•			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						•		•		•	•	•			
8.2 $0.9$ $149$ $*$ .       .						,		•		•	•				
8.4       0.9       141       *       . </th <th></th> <th></th> <th></th> <th></th> <th></th> <th>•</th> <th></th> <th>•</th> <th></th> <th>•</th> <th>•</th> <th>•</th> <th></th> <th></th> <th></th>						•		•		•	•	•			
8.6       0.9       133       *       . </th <th></th> <th></th> <th></th> <th></th> <th></th> <th>•</th> <th></th> <th>•</th> <th></th> <th>•</th> <th>•</th> <th>·</th> <th></th> <th></th> <th></th>						•		•		•	•	·			
8.8       0.8       126       *       . </th <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>•</th> <th></th> <th>•</th> <th></th> <th>•</th> <th></th> <th></th> <th></th>								•		•		•			
9.0       0.8       120       *       . </th <th></th> <th>•</th> <th></th> <th></th> <th></th>												•			
9.2       0.8       114       *       . </th <th></th>															
9.4       0.8       109       *       . </th <th></th> <th>•</th> <th></th> <th></th> <th></th> <th></th>											•				
9.8 0.7 100 .*	9	9.4	0.8	109		•									
											•				
10.0 0.7 96 .*						•				•					
	10	0.0	0.7	96	. *	•		•			•	•			

	AMI/OD 1	HYDROGRAF			RRAG				TION NU	MEEK	3		
GACE	7.7FRO :	BELOW = 4410.00	RUN2	: MAY	តា ស	AT ATTON			. 50 FLOOD	WAVE -		01 M	
0701	S ZERU -	- 1710.00		STAGE					FLOOD	#ATE -	4414,	OI M	· .
		MAX ST		4.81			T TIM	ि व	3 500	HOURS			
		MAX FL		2530			T TIM			HOURS			
TIME	STAGE	FLOW											
HIR	М	CMS	0	1000		2000	3	000	400	0	5000		
0.0	0.5	50	. *										
0.5	0.5	57	*					•					
1.0	1.2	237	. *										
1.5	2.2	662		* .									
2.0	3.2	1230			k								
2.5	4.0	1801				*.							
3.0	4.5	2239				. *	L						
3.5	4.8	2530					*						
4.0	3.9	1732				* .		-					
4.5	3.0	1117		.*									
5.0	2.4	765		*.		•		•					
5.5	2.0	549	. *										
6.0	1.7	410	. *										
6.5	1.4	317	, *										
7.0	1.3	253	. *										
7.5	1.1	207	. *										
8.0	1.0	173	. *							•			
8.5	0.9	147	.*										
9.0	0.8	128	. *										
9.5	0.8	113	.*							•			
10, 0	0.7	101	. <b>*</b> ·	•				;		• •			
10, 5	0. 7	92	. *			•				•			
11.0	0.7	85	.*	٠		•				•			
11.5	0.6	79	.*	•		•				•			
12.0	0.6	74	. *			•				·.		•	
12.5	0.6	70	*	-		•	•	•		•	•		
13.0	0.6	67	.*	٠		•		•		•			
13.5	0.6	64	*	٠		•		·		•	•		
14.0	0.5	62	*	•		•		•		•	•		
14.5	0.5		.*	•		•	- '	•		•	•		
15.0	0.5	58	.* 	•		•••		•		•	•		
15.5 16.0	0.5	57 56	,* -	•		•		•		•	•		
16. 0 16. 5	0.5 0.5	56 55	. * 	•		·		•		•	•		
16.5 17.0	0.5 0.5	55 54	.* *	٠		•		•		٠	•		
17.0	0.5	54 54	.* .*	•		•		•		•	•		
11.5	0.5	53	.* .*	•		•		•		•	•		
18.5	0.5	53	.т . <b>*</b>	•		•		•		•	•		
19.0	0.5	52 52	. <del>*</del> . *	•		•		•	•	•	•		
19.5	0.5	52 52	*	•		•		•		•	•		
20.0	0.5	52	. *	•		•		•		•	•		
20.5	0.5	51	, *	•		•		•		•	•		
20.0	0.5	51	. <b>*</b>	•		•		:		•	•		
21.5	0.5	51	*	•		•		•		:	•		
22.0	0.5	51	*	•		•		:					
22.5	0, 5	51	*			•							
23.0	0.5	51	*			•							
						-				-	•		

	DIS	CHARGE	HYDROGI BEL(		for RUN2	Lu :	ggye	Lake AT	STA KM 36	TION NUM .49	BER	19		
	GAG	e zero	<b>= 3160</b> .	00 (				VATION AVAILA	Reached by	FLOOD W	AVE =	3164. 50	М	
			MAX	STA	GE =	4.50			TTIME ≈	<b>4. 025</b>	HOURS			
					<b>i</b> =				T TIME ≈	4. 025				
	TIME	STAGE	FL(	W										
	HR	M.	C	(S	0	500		1000	1500	2000		2500		
	0.0	0.5	Ę	55	*									
	0.5	0.5	£	53	*									
	1.0	0.6	e	50	. *									
	1.5	0.8	7	79	. *									
	2.0	0.9	ç	96 .	*			•	•					
	2.5	2.3	71	17			*							
	3.0	3.5	157	74	•				,*			•		
	3.5	4.2		34 .						•	*			
	4.0	4, 5		12								*,		
	4.5	4.1	203							.:	*			
	5.0	3.2	135	58 .		• •			* .					
	5.5	2.7	97			•		*.	•			.•		
	6.0	2.2		18 .		•	*	•						
	6.5	1.9	54	<b>18</b> .		.*								
	7.0	1.7	43	30		*,								
	7.5	1.5		17 .		* .		•				•		
	8.0	1.3		34		* .								
	8.5	1.2		37	. *	• .			•	•		•		
	9.0	(-1, 1)		)2										
	9, 5	1. 0		74 ,	*					:		•		
	10. 0	0.9		52	. *			•						
	10.5	0.9		34	*	•		•		•		•		
	11.0	0.8			*	•		•	•	•				
	11.5	0.8			*	•		•	•	•		•		
	12.0	0.7			* .	•		•	•	•		•		
		· · · 0: <i>1</i>			*	٠			`.			. •		
	13.0	0.6		35 · .		•		•		•		•		
		0.6			, *							•		
	14.0	0.6			*	•		•	•	•		•		
	14, 5	0.6			.* `	·		•	•	•		•		
	15.0	0.6			*	•		•		•		•	•	
	15.5	0.6			. *	•		•	•	•		•		
	16.0	0.5			. *	•		•		•		•		
	16.5	0.5			.*	•		•	•	•		•		
	17.0	0.5			.*	•		•	•	•		•		
	17.5	0.5			. *			•	•	•		•		
	18.0	0.5			.*	•		•	•	•		•		
	18.5	0.5			.*	•		•	•	•		•		
	19.0	0.5			. *	•		•	•	•		•		
	19.5	0.5			.*	•		•	•	•		•		
	20.0	0.5		54				•	•	•		•		
	20.5	0.5		54		•		•	•	•		•		
	21.0	0.5		54		•		•	•	•		•		
	21.5	0.5		54		•		•	•	•		•		
	22.0	0.5		54		•		•	•	•		•		
	22.5	0.5		54		•		•	•	•		•		
1	23. 0	0.5	£	53	*	,		•		•				

DIS	CHARGE	HYDROG BEL		FOR RUN2		ggye		 KM		TION NUMBER .09	38		
GAG	e zero	= 1580			MAX D STAGE				) BY	FLOOD WAVE =	= 15 <b>8</b> 3.53	М	
			STAG Flow		3. 52 2455	M CMS		AT TIME AT TIME					
TIME		FL			F 4 4		1000	15			0500		
HR	M		MS 0		500		1000	150	00	2000	2500		
0.0	0.6		25.	*	٠		•		•	•	•		
0.5 1.0	0.6 0.6		23. 30.	*	•		٠		•	•	•		
1.0	0.6		50. 51.	*	•		•		•	•	•		
2.0	0.6		64.	*	•				•	•			
2.5	0.6		67.	*	•		Ż			-			
3.0	0.7		71.	*						•			
3.5	0. 9		34.	;	* .								
4.0	3.0	18	64.		•					* .			
4.5	3.4	23	<b>46</b> .				•				*.		
5.0	3.5	24	05.								*.		
5.5	3.0	18			•				•	*.			
6. 0	2.5		80.		•		•	*	•	٠	•		
6.5	2.1		64.		•		. *	:	٠	•	•	•	
7.0	1.9		40.		•		*.		•		•		
7.5	1.6		83.		•	*	•		٠	۲	•		
8.0	1.5		66 . 77		.*		·		•		•		
8.5	1.3		77 . 10		*		•	÷	•	•	,		
9.0	1.2		10. 57.		*.				•	•	`		
9.5 10.0	1.1 1.0		ог. 16.		* .		•		•	• *	•		
10.5	1.0		83 .		* .		•		•	•	•		
11.0	0.9		56.		*		•			•			
11.5	0.9		33.		* .		÷						1
12.0	0.8		16.	*	ı,						• '		
12.5	0.8		01.	*	• .								
13.0	0.8	• 1	88 .	*	· ,					•			
13.5	0.7	· 1	78.	*	· .				•		•		
14.0	0.7		69 <i>.</i>	*			•		•	•			
14.5	0.7		62 :	*	•		•		•	•	•		
15.0	0.7		56 .	*	•		٠		•	٠	•		
15.5	0.7		50	, <b>*</b>	•		•		·	•	•		
16.0	0.7		46 .	. *	•		•		•	•	•		
16.5 17.0	0.6 0.6		.42 .39	· *	•		•		•	•	•		
17.5	0.6		.36	· •	•		•		•	•	•		
18.0	0.6		34	. <b>*</b>	•				÷	•	•		÷
18.5	0.6		32	*									
19.0	0.6		30	*									
19.5	0, 6		28	. *									
20. 0	0.6		27	. *						•			
20. 5	0.6		27	. *					•		•		
21.0	0.6		126	. *					•		•		
21.5	0.6		126	. *	•		•		•	•	•		
22.0	0.6		126	. *	•		•		•		•		
22.5	0.6		126	. *	•		•		•				
23.0	0.6		125	. *	•		•		•	•	•		

DIS	CHARGE I	HYDROGRAPH F BELOW F	?OR Li 2UN2 :			ATION NUMBER L.18	60
GAG	E ZERO =	= 1095.00 M	MA)	ELEVATION	REACHED BY	FLOOD WAVE	: = 1100.16 )
		F	LOOD STAGE	E NOT AVAIL	ABLE		
		MAX STAGE		BMI.	AT TIME =	6.300 HOU	RS
		MAX FLOW	= 2485	5 CMS	AT TIME =	6.125 HOU	RS
TIME	STAGE	FLOW					
HR	М	CMS 0	500	1000	1500	2000	2500
0.0	1.7	306 .	* .				
0.5	1.7	395 .	*.				
1.0	1.7	427 .	*.				
1.5	1.7	460 .	*.				
2.0	1.7	489	*				
2.5	1.7	497 .	*				
3.0	1.7	484	*				
3. 5	1.7	469	*.				
4.0	1.7	582		* .			
4.5	1.7	669 .		* .			
5.0	1.7	797.	•	* .	•	•	
5.5	2.8	1407 .			*.		
6. 0	5.0	2445 .					*.
6. 5	5. 1	2391 .	•			•	*.
7.0	4.5	1 <b>9</b> 95 .				*	
7.5	3.8	1589 .			. *	¥.	
8.0	3.2	1290 .			* .		
8.5	2.8	1073 .		. *			
9.0	2.5	911 .	•	*			
9.5	2.2	783.		* .			
10.0	<b>2.0</b> 1	683.		* .			
10. 5	1.8	605 .	•	* .	•		
11.0	. 1.7	541 .	. *	¥.			
11.5	1.7	506 .	*		•	•	•
12.0	1.7	483	*	.,			14
12.5	1.7	464	*.		•		
13.0	1.7	449 .	*,		5		•
13.5	1.7	437	*,	· .		•	•
14. 0	1. 7	428 .	*.	•			
14. 5	1.7	419 .	*.	•	•		
15.0	1.7	412 .	*.	•	•		
15.5	1.7	407 .	<b>*</b> .	•	•	•	•
16.0	1.7	402 .	*.	•	•	•	•
16.5	1.7		*.	•		•	•
17.0	1.7	393 .	*.		•	•	•
17.5	1.7	390 .	*.		•	•	•
18.0	1.7	387	*.	•	•	,	•
18.5	1.7	385 .	*,	•	•		•
19.0	1.7	383 .	*.	•	•	•	•
19.5	1.7	381 .	*.	•	•	•	
20.0	1.7	379 .	*.	•	•	•	
20.5	1.7	378 .	<b>*</b> .	•	•	•	•
21.0	1.7	377 .	*.	•	•	•	•
21.5	1.7	376 .	*.	•	•	•	•
22.0	1.7	375 .	* .	•	•	•	
22. 5	1,7	374 .	*				

Calculation Result of DAMBRK (3/3)

.

Simulation of GLOF from Raphstreng Lake

#### ANALYSIS OF THE DOWNSTREAM FLOOD HYDROGRAPH

#### PRODUCED BY THE DAM BREAK OF

RUN3 :

ON

#### Raphstreng

#### ANALYSIS BY

### BASED ON PROCEDURE DEVELOPED BY DANNY L. FREAD, PH.D., SR. RESEARCH HYDROLOGIST

QUALITY CONTROL TESTING AND OTHER SUPPORT BY JANICE M. LEWIS, RESEARCH HYDROLOGIST

> HYDROLOGIC RESEARCH LABORATORY W23, OFFICE OF HYDROLOGY NOAA, NATIONAL WEATHER SERVICE SILVER SPRING, MARYLAND 20910

INPUT CONTROL PARAMETERS FOR RUN3 :

PARAMETER ***********************************	VARIABLE * *******	YALLE ******	
NUMBER OF DYNAMIC ROUTING REACHES	KKN	1	
TYPE OF RESERVOIR ROUTING	KUI	0	
MULTIPLE DAM INDICATOR	MLLDAM	0	
PRINTING INSTRUCTIONS FOR INPUT SUMMARY	KDMP	5	
NO, OF RESERVOIR INFLOW HYDROGRAPH POINTS	ITEH	2	
INTERVAL OF CROSS-SECTION INFO PRINTED OUT WHEN J	<b>ik=9 npr</b> t	· 0	
FLOOD-FLAIN MODEL PARAMETER	KFLP	0	
METRIC INPUT/OUTPUT OPTION	METRIC	1	

÷

IOPUT= 1 0 0 0 0 0 1 1 0 0 0 0

RUN3 : RESERVOIR

TABLE OF ELEVATION VS SURFACE AREA

SURFACE AREA (SQ KM) SA(K)	ELEVATION (M) HSA(K)
<del>alajojojojojojojojojojojojojojojojojojoj</del>	noiok volateleteleteleteleteletek
1. 1	4440. 00
0. 9	4410.00
0. 0	0.00
0. 0	0.00
0. 0	0.00
0. 0	0.00
0. 0	0.00
0. 0	0.00

RUN3 :

₽₳₽₳₩₤₽₽₽₽ ٭٭٭٭٭٭٭٭٭			VALLE ******
LENGTH OF RESERVOIR	KM	RLM	1.90
ELEVATION OF WATER SURFACE	M	YO	4441.00
SIDE SLOPE OF BREACH		2	0.00
ELEVATION OF BOTTOM OF BREACH	м	YBMIN	4410.00
WIDTH OF BASE OF BREACH	M	BB	34.00
TIME TO MAXIMUM BREACH SIZE	HOUR	TFH	3. 50
ELEVATION (MSL.) OF BOTTOM OF DAM	M	DATUM	4410.00
VOLUME-SURFACE AREA PARAMETER		VOL	0.00
ELEVATION OF WATER WHEN BREACHED	М	HF	4441.00
ELEVATION OF TOP OF DAM	M	HD	4441.00
ELEVATION OF UNCONTROLLED SPILLWAY CREST	M	HSP	0.00
elevation of center of gate openings	М	HGT	0.00
DISCHARGE COEF. FOR UNCONTROLLED SPILLWAY		CS .	0. 00
DISCHARGE COEF. FOR GATE FLOW		CG	0. 00
DISCHARGE COEF. FOR UNCONTROLLED WEIR FLOW	i	CD0	0.00
DISCHARGE THRU TURBINES	OMS	QT	50, 00
CDO SHOULD NOT BE 0.0 IF OVERTOPPING MAY (	XXX R		
DHF (INTERVAL BETWEEN INPUT HYDROGRAPH ORD)	(NATES) =	= 0,00	) HRS.
TEH (TIME AT WHICH COMPUTATIONS TERMINATE)	= 24.0	0000 HRS.	
BREX (BREACH EXPONENT) = 0,000			·
MLD (MLD FLOW OPTION) = 0			
IWF (TYPE OF WAVE FRONT TRACKING) = 0			
KPRES (WETTED PERIMETER OPTION) = 0			

KSL (LANDSLIDE PARAMETER) = 0

#### INFLOW HYDROGRAPH TO RUN3 :

#### 

0.00 0.00

#### TIME OF INFLOW HYDROGRAPH ORDINATES

#### 0.0000 100.0000

# CROSS-SECTIONAL PARAMETERS FOR Raphstreng BELOW RUN3 :

PARAMETER	VARIABLE	VALUE ******
NUMBER OF CROSS-SECTIONS	NS	5
MAXIMUM NUMBER OF TOP WIDTHS	NCS	2
NUMBER OF CROSS-SECTIONAL HYDROGRAPHS TO PLOT	NTT	4
type of output other than hydrograph plots	JNK	1
CROSS-SECTIONAL SMOOTHING PARAMETER	KSA	0
DOWNSTREAM SUPERCRITICAL OR NOT	KSLPC	1
NO. OF LATERAL INFLOW HYDROGRAPHS	LQ	. 4
NO. OF POINTS IN GATE CONTROL CURVE	KCG	0

.

NUMBER OF CROSS-SECTION WHERE HYDROGRAPH DESIRED (MAX NUMBER OF HYDROGRAPHS = 6)

1 2 3 4

#### CROSS-SECTIONAL VARIABLES FOR Raphstreng BELOW RUN3 :

PARAMETER	UNITS	VARIABLE
	<b>Xojolojojoj</b>	xciololoix
LOCATION OF CROSS-SECTION	KM	XS(I)
ELEVATION (MSL.) OF FLOODING AT CROSS-SECTION	M	FSTG(I)
ELEV CORRESPONDING TO EACH TOP WIDTH	M	HS (K, I)
TOP WIDTH CORRESPONDING TO FACH FLEV	М	RS (K, I)
(ACTIVE FLOW PORTION)		
TOP WIDTH CORRESPONDING TO EACH FLEV	M	BSS (K, I)
(OFF-CHANNEL PORTION)		
NUMBER OF CROSS-SECTION		I
NUMBER OF ELEVATION LEVEL		К

CROSS-SECTION NUMBER 1

XS(I) =	0. 000	FSTG(I) =	0.00
HS	4410.0	4430. 0	
BS	50. 0	150. 0	
BSS	0.0	0. 0	

#### CROSS-SECTION NUMBER 2

XS(I) =	32. 000	FSTG(1) =	0.00	
НЗ	3160. 0	3180.0		
BS	50. 0	100. 0		
BSS	0. 0	0.0		

## CROSS-SECTION NUMBER 3

#### 

XS(I) =	71.600	FSTG(1)	= 0.00
HS	1580. 0	1600.0	
BS	70. 0	200. 0	
BSS	0. 0	0. 0	

#### CROSS-SECTION NUMBER 4

#### 

XS(I) =	116. 700	FSTG(I)	= 0.00
НЗ	1095. 0	1115.0	
BS	30. 0	100. 0	
BSS	0. 0	0. 0	

#### CROSS-SECTION NUMBER 5

#### 

•

XS(I) =	167. 000	FSTG(I) =	0.00
НЗ	570. 0	590. 0	
BS	50.0	100.0	
BSS	0. 0	0.0	

1

# MANNING N ROLCHNESS COEFFICIENTS FOR THE GIVEN REACHES (CM(K, I), K=1, NCS) WHERE I = REACH NUMBER REACH 1 ... 0.050 0.050 REACH 2 ... 0.050 0.050 REACH 3 ... 0.050 0.050 REACH 4 ... 0.050 0.050

#### CROSS-SECTIONAL VARIABLES FOR Raphstreng BELOW RUN3 :

PARAMETER	UNITS	VARIABLE
	<b>xiolojojojo</b> joj	<b>xoleisiole</b>

MINIMUM COMPUTATIONAL DISTANCE USED	KM	DXM(I)
BETWEEN CROSS-SECTIONS		

CONTRACTION - EXPANSION COEFFICIENTS FKC(I) BETWEEN CROSS-SECTIONS

REACH NUMBER	DXM (I) ******	FKC(1) *****
1	1.000	0.000
2	1.000	0.000
3	1. 000	0. 000
4	1.000	0. 000

#### DOWNSTREAM FLOW PARAMETERS FOR Raphstreng EELOW RUN3 :

PARAMETER	UNITS	VARIABLE	E VALLE
		<b>xiejojojej</b> k	<del>xiololololololololololo</del> k
MAX DISCHARGE AT DOWNSTREAM EXTREMITY	CMIS	QMAXD	0, 0
MAX LATERAL OUTFLOW PRODUCING LOSSES	oms /m	QL.	0. 000
INITIAL SIZE OF TIME STEP	HOUR	DTHM	0.0000
INITIAL WATER SURFACE ELEVATION DOWNSTREAM	M	YDN	575.00
SLOPE OF CHANNEL DOWNSTREAM OF DAM	%	SOM	0.00
THETA WEIGHTING FACTOR		THETA	0.00
CONVERGENCE CRITERION FOR STAGE	M	EPSY	0.000
TIME AT WHICH DAM STARTS TO FAIL	HOUR	TFI	0.00

•

#### CONPUTATIONS WILL USE THE FOLLOWING DXM VALUES

1.000 1.000 1.000 1.000

LATERAL INFLOW REACH NUMBER

LQX (I)

1 2 3 4

(QL (L, I), L=1, ITEH) 0. 0.

(QL(L, 2), L=1, ITEH) 0. 0.

(QL (L, 3), L=1, ITEH) 0. 0.

(QL (L, 4), L=1, ITER) 0. 0.

1

TOTAL NUMBER OF CROSS SECTIONS (ORIGINAL+INTERPOLATED) (N) = 167 . (MAXIMUM ALLOWABLE = 200

	****							
alaştaşı.	***							
*** SUMMARY OF OUTPUT DATA	*olot							
****	*ofox							
	-							

	BOTTOM		REACH	
	ELEVATION		LENGTH	SLOPE
KM	M	REACH NO.	KM	%

÷.,

1

2

3

4

32.00

39.60

45. 10

50.30

3. 91

3. 99

1.08

1.04

MESAGE

TOTAL	VOLUME	IN	RESERVOIR	BEHIND

**RUN3** 31.0 CU. M (MILLION) : **u** 

DEFINITION OF VARIABLES IN RESERVOIR DEPLETION TABLE

0.00 4410.00

32, 00 3160, 00

1580.00

1095.00

570.00

71.60

116.70

167.00

CROSS-SECTION

NO.

1

2

3

4

5

)

PARAMETER	UNITS	VARIABLE
TIME STEP FROM START OF ANALYSIS		I
ITERATIONS NECESSARY TO SOLVE FLOW EQUATIONS		К
ELAPSED TIME FROM START OF ANALYSIS	HOUR	TTP(I)
TOTAL OUTFLOW FROM DAM	CMS	Q(I)
ELEVATION OF WATER SURFACE AT DAM	M	H2
ELEVATION OF BOTTOM OF BREACH	M	YB
EST DEPTH OF FLOW IMMEDIATELY DOWNSTREAM	M	D
SLEMERGENCE COEFFICIENT		SUB
VELOCITY CORRECTION		WCOR
TOTAL VOLUME DISCHARGED FROM TIME OF BREACH MILLIC	NCUM	autval,
BREACH WIDTH	M	BB
RECTANGULAR BREACH DISCHARGE COEFFICIENT		cofr
INFLOW TO RESERVOIR	OMS	QI (I)
BREACH OUTFLOW	ONS	OBRECH
SPILLWAY CUTTFLOW	OMS	<b>QS</b> PIL

J		mm (7)			MISTION I							/- \		
I		TTP(I)	Q(I)	12	YB	D	SUB	VCOR	anva.	BB	COFR	QI (I)	GERECH	QSP1L
*okok		xololojojo	*	*olololok	*Ciolololok		xioloiok.	*okok:	*ototototototot	*crotor	*ototek	*cholock	<b>kolosloio</b> k	xojojojok
1	0	0, 000	50	4441.00	4441.00	4410. 44	1.00	1.00	0. 0	0.0	3. 10	0.	0.	50.
2	2	0. 070	50	4440. 99	4440. 38	4410. 44	1.00	1.00	0. 0	0.7	3.10	0.	1.	50.
3	1	0. 140	53	4440. 98	4439. 76	4410. 45	1.00	1.00	0. 0	1.4	3.10	0.	3.	50.
4	1	0. 210	58	4440. 97	4439. 14	4410. 48	1. 00	1.00	0. 0	2.0	3. 10	0.	9.	50.
5	1	0. 280	67	4440.95	4438.52	4410. 52	1.00	1.00	0. 1	2.7	3. 10	0.	18.	50.
6	1	0.350	80	4440. 94	4437.90	4410. 58	1.00	1.00	0. 1	3.4	3. 10	0.	31.	50.
7	2	0. 420	98	4440. 92	4437, 28	4410.65	1. 00	1.00	0. 1	4.1	3. 10	0.	48.	50.
8	2	0. 490	120	4440. 89	4436.66	4410. 74	1.00	1.00	0. 1	4.8	3. 10	0.	71.	50.
9	2	0. 560	148	4440.86	4436. 04	4410. 83	1.00	1.00	0. 2	5.4	3. 10	0.	99.	50.
10	2	0. 630	181	4440. 83	4435. 42	4410. 94	1.00	1.00	0.2	6. 1	3. 10	0.	132.	50.
11	2	0.700	220	4440. 78	4434. 80	4411.05	1. 00	1.00	0. 3	6.8	3. 10	0.	170.	50.
12	2	0.770	264	4440. 73	4434. 18	4411. 17	1.00	1.00	0.3	7.5	3. 10	0.	214.	50.
13	2	0.840	314	4440.66	4433.56	4411. 30	1. 00	1.00	0.4	8.2	3. 10	0.	264.	50.
14	2	0. 910	368	4440. 59	4432. 94	4411.42		1.00	0.5	8.8	3. 10	0.	320.	48.
15	2		425	4440.50	4432.32			1.00	0.6	9.5	3. 10	0.	381.	44.
16		1.050	488		4431.70		1.00		0. 7		3. 10	0.	448.	40.
17		1. 120	556	4440. 29	4431.08			1.00	0.8	10. 2	3. 10	0. 0.	-140. 520.	-10. 36.
18		1. 120	629	4440. 15	4430.46			1.00	0. 0 1. 0	11.6	3. 10	0. 0,	520. 597.	
19		1. 260	707	4440. 01	4429.84			1.00	1. 0	12.2		0.	679.	32. 28.
20		1. 330	789	4439.84	4429.22									
20		1. 330						1.00	1.3	12.9	3.10	0.	766.	24.
			876		4428.60	4412.37	1.00		1.5		3.10	0.	856.	20.
22	2	1. 470	966	4439.45		4412.51		1.00			3. 10	0.	950.	16.
` 23	2	1.540	1059	4439.23	4427.36	4412.64		1.00		15.0		• 0.	1047.	12.
24		1.610	1155		4426.74			1.00	2.3			0.	1147.	8.
25	2	1.680	1253		4426.12			1.00	2.6	16.3		0.	1249.	4.
26		1.750	1352	4438.42			1. 00	1.00	2. 9	17.0	-	0.	1353.	0.
2.		1.820	1457	-			1. 00				3. 10 <sup>.</sup>	0.	1457.	0.
- 28	2-		1562	4437.77			1.00			18.4		0.	1562.	0.
29		1.960	1666		<b>4423.64</b>					19.0		0.	1667.	0.
30		2.030	1770		4423. 02				4.5	19.7	3. 10	0.	1771.	0.
31		2. 100	1873	4436. 61	4422.40	4413.67	1.00	1.00	5. 0	20.4	3. 10	0.	<b>1874</b> .	0.
32	2	2. 170	1974		4421.7 <b>8</b>				5. 5	21. 1	3. 10	0.	1974.	0.
33	2	2. 240	2073	4435.72	4421. 16	4413.89	1.00	1.00	6. 0	21.8	3. 10	0.	2073.	0.
34	2	2.310	2169	4435. 24	4420. 54	4413. 99	1.00	1. 00	6. 5	22.4	3. 10	• 0.	21 <b>69</b> .	0.
35	2	2. 380	2261	4434. 73	4419. 92	4414.09	1.00	1.00	7.1	23.1	3. 10	0.	2262.	0.
36	2	2. 450	2351	4434. 20	4419. 30	4414. 18	1.00	1.00	7.6	23.8	3. 10	0.	2351.	0.
37	2	2. 520	2436	4433.65	4418.68	4414.27	1.00	1.00	8.2	24.5	3. 10	0.	2437.	0.
38	2	2. 590	2518	4433.08	4418.06	4414.35	1.00	1.01	8. 9	25.2	3. 10	0.	2518.	0.
39	2	2.660	2595	4432.49	4417.44	4414. 42	1.00	1.01	<b>9</b> . 5	25. <b>8</b>	3. 10	0.	2 <b>595</b> .	0.
40	2	2. 730	2667	4431.88	4416.82	4414. 49	1. 00	1.01	10. 2	2 <b>6</b> . 5	3. 10	0.	2668.	0.
41	2	2.800	2736	4431.25	4416.20	4414.56	1. 00	1. 01	10. 9	27.2	3. 10	0.	2736.	0.
42	2	2. 870	2799	4430.60	4415. 5 <b>8</b>	4414.62	1.00	1.01	11.5	27. <b>9</b>	3. 10	0.	27 <b>99</b> .	0.
43	2	2. <del>94</del> 0	2858	4429. 94	4414.96	4414.67	1.00	1.01	12.3	28.6	3. 10	0.	2858.	0.
44	2	3. 010	2912	4429. 25	4414. 34	4414.72	1.00	1.01	13. 0	29.2	3. 10	0.	2912.	0.
45	2	3. 080	2961	4428.56	4413.72	4414.77	1. 00	1.01	13.7	29. 9	3. 10	0.	2962.	0.
46	2	3. 150	3006		4413. 10		1.00			30.6		0.	3007.	0.
47	2	3. 220	3047		4412.48		1. 00	1.02		31.3		0.	3048.	0.
48	2	3.290	3084	4426. 38	4411.86	4414.88	1. 00	1.02		32.0		0.	3085.	0.
49	2	3. 360	3118		4411.24					32.6		0.	3118.	0.
50	2	3. 430	3148		4410.62					33.3		0.	3149.	0.
										-				••

			RLS.	ERVOIR DE	HETION T	AHE								
I	K	TTP(I)	Q(I)	112	YB	D	SLB	VCOR	απνα	BB	COFR	QI (I)	QERECH	QSPIL
*ototk		yololojojoj.	<del>de la </del>	Acticiciologick	yolololojoje;		*		xokxopiojojok	xoloiok	*uioiok	*****		<b>Hotoloi</b> ek
51		3. 500		4424.10	4410.00		1.00		18.4	34.0	3. 10	0.	3177.	0.
52		3. 570	2943	4423. 35	4410.00		1.00		<b>19</b> . 2	34.0	3, 10	0.	2943.	0.
53		3. 640	2720	4422.65	4410.00		1. 00	1.04	19. 9		3.10	0.	2721.	0.
54		3. 710	2518	4422.00	4410.00		1. 00	1.04	20.5	34. 0	3. 10	0.	2519.	0.
55	2	3. 780	2334	4421.39	4410.00	4414. 17	1. 00	1.05	21. 1	34.0	3. 10	0.	2335.	0.
56		3.850	2167	4420. 83	4410.00		1. 00		21.7		3. 10	0.	2168.	0.
57	2	3.920	2015	4420. 31	4410.00	4413. 83	1.00	1.05	22.2	34. 0	3. 10	0.	2016.	0.
58	2	3. 990	1876	4419.82	4410.00	4413.68	1.00	1.05	22.7		3. 10	0.	1877.	0.
59	2	4.060	1749	4419.36	4410. 00	4413. 53	1. 00	1.05	23. 2	34.0	3. 10	0.	1750.	0.
60	2	4. 130	1633	4418. 93	4410.00	4413. 40	1. 00	1.05	23.6	34.0	3. 10	0.	1634.	0.
61	2	4. 200	1527	4418.53	4410.00	4413. 27	1. 00	1.06	24.0	34.0	3. 10	0.	1527.	0.
62	2	4. 270	1429	4418. 15	4410.00	4413. 14	1. 00	1.06			3, 10	0.	1429.	0.
63	2	4. 340	1339	4417.80	4410.00	4413. 03	1. 00	1.06	24. 7	34. 0	3. 10	0.	133 <b>9</b> .	0.
64	2	4. 410	1256	4417.46	4410. 00	4412. 92	1. 00	1.06	25. 1	34. 0	3.10	0.	1256.	0.
65	2	4. 480	1180	4417.15	4410.00	4412. 82	1.00	1.06	25.4	34.0	3. 10	0.	1180.	0.
66	2	4. 550	1109	4416. <b>8</b> 6	4410. 00	4412. 72	1.00	1.06	25. 7	34. 0	3. 10	0.	1110.	0.
67	2	4. 620	1044	4416.58	4410. 00	4412.62	1.00	1.07	<b>25. 9</b>	34.0	3. 10	0.	1044.	0.
68	2	4. 690	983	4416. 32	4410.00	4412.53	1. 00	1.07	26.2	34. 0	3. 10	0.	<b>984</b> .	0.
69	2	4.760	927	4416. 07	4410. 00	4412.45	1.00	1.07	26.4	34.0	3. 10	0.	928.	0.
· 70	2	4. 830	<b>8</b> 76	4415. 83	4410. 00	4412. 37	1. 00	1.07	26.6	34.0	3. 10	0.	876.	0.
71	2	4.900	827	4415.61	4410. 00	4412. 29	1.00	1.07	26. 9	34.0	3, 10	0.	828.	0.
72	2	4. 970	782	4415. 40			1. 00	1.07	27.1	34.0	3. 10	0.	<b>78</b> 3.	0.
73		5.040	741	4415. 20	4410.00	4412. 15	1.00	1.07	27.3	34. 0	3. 10	0.	741.	0.
74	2	5.110	702	4415. 02	4410.00	4412. 08	1. 00	1.08	27.4	34.0	3. 10	0.	702.	0.
75	2	5. 180	665	4414. 84	4410. 00	4412. 02	1. 00	1.08	27.6	34.0	3. 10	0.	666.	0.
76	2	5.250	631	4414.67	4410.00	4411.96	1. 00	1.08	27.8	34.0	3.10	. 0.	632.	0.
77	2	5. 320	599	4414. 51	4410.00	4411.90	1.00	1.08	27. 9	34.0	3. 10	• <b>0.</b> •	600.	0.
78	2	5.390	570		4410. 00		•	1.08	28.1	<b>'34</b> . 0	3.10	0.	570.	0.
79		5.460		•		4411.79					3. 10	0.	542.	0.
80	2	5. 530	516	4414.07	4410.00	4411. 74	1. 00	1.08	28.3	34.0	3. 10	0.	516.	0.
81	2	5. 600	491			4411.69			2 <b>8</b> . 5	34.0	3. 10	0.	<b>49</b> 2.	0.
82	2		468	4413.81	4410.00	4411.64	1. 00	1.08	28.6	34.0	3.10	0.	<b>46</b> 9.	0.
83		5.740	446	4413. 69	4410.00	4411.60	1.00	1.09	28.7	34.0	3. 10	0.	447.	0.
84	2	5. 810	426			4411.55	1.00	1.09	28.8	34.0	3. 10	0.	427.	0.
<b>8</b> 5		5.880	<b>407</b>	4413.46	4410.00	4411.51	1. 00	1.09	28.9	34.0	3. 10	0.	407.	0.
86		5.950	389			4411. 47					3. 10	0.	<b>38</b> 9.	0.
87	2	6. 020	372			4411.43					3. 10	0.	372.	0.
88	2		356			4411.40			29. 2	34.0	3. 10	0.	356.	0.
89		6, 160				4411.36					3. 10	0.	341.	0.
90		6. 230				4411.33			29. 4	34. 0	3. 10	. 0.	327.	0.
91		6, 300				4411.29					3. 10	0.	313,	0.
92		6. 370				4411.26					3. 10	0.	300.	0.
93		6.440	287			4411.23					3. 10	0.	288,	0.
94		6.510	276			4411.20					3. 10	0.	276.	0.
95		6, 580	265			4411.17			(4) (4)		3. 10	0.	265.	0.
96		6,650	255			4411.15					3. 10	0.	255,	0.
97		6.720	245			4411.12					3. 10	0.	245,	0.
98		6, 790	235			4411.09					3.10	0.	236.	0.
99		6.860	226	4412.33		4411.07					3. 10	0.	227.	0.
100	1	6, 930	218	4412.27	4410.00	4411.04	1. 00	1. 10	30. 1	34. 0	3. 10	0.	218.	0.

					righton i									
I	ΚŤΊ		Q(I)	112	YB	D		VCOR	αλίγα.	BB	COFR	QI (I)	GERECH	QSPIL
*Pirite Aprilate	** **		******	*****	xolohohohok	xolotototot		xototok	*ofofofofofofok		*oforfort:	*olototek		xiojojojoj
101		. 000	210		4410.00			1.10	30. 1		3. 10	0.	210.	0.
102	27		201		4410.00		1.00		30. 2		3. 10	0.	202.	0.
103	2 7		193		4410.00		1.00				3. 10	0.	193.	0.
104	2 7				4410.00		1.00		30. 3		3. 10	0.	1 <b>84</b> .	0.
105	27				4410.00					34.0		0.	175.	0.
106		. 470			4410.00					34.0		0.	165.	0.
107	17				4410.00		1.00		30. 5	34.0	3. 10	0.	155.	0.
108	17				4410.00					34.0		0.	145.	· 0.
109	17				4410.00				30. 7	34.0	3. 10	0.	135.	0.
110	18				4410.00					34.0		0.	125.	0.
111		. 227			4410.00				30. 8	34, 0	3.10	0.	116.	0.
112	18				4410.00		1. 00	1.11	30. 9	34.0	3. 10	0.	106.	0.
113	18	647	96	4411, 31	4410.00	4410.64	1. 00	1. 11	31. 0	34.0	3. 10	0.	96.	0.
114	18		87	4411.22	4410.00	4410. 61	1.00	1.11	31. 0	34.0	3. 10	0.	87.	0.
115	19	. 154	78	4411.14	4410. 00	4410. 57	1.00	1.11	31. 1	34. 0	3, 10	0.	78.	0.
116	19	. 446	69	4411.05	4410. 00	4410. 53	1.00	1.11	31. 2	34.0	3. 10	0.	70.	0.
117	19	. 768	62	4410. 97	4410. 00	4410. 49	1. 00	1.12	31. 3	34.0	3. 10	0.	62.	0.
118	1 10	. 122	54	4410. <b>8</b> 9	4410. 00	4410.46	1.00	1.12	31. 4	34.0	3. 10	0.	55.	0.
119	1 10	511	47	4410.82	4410.00	4410.42	1. 00	1. 12	31.4	34.0	3. 10	0.	48.	0.
120	2 10	. 939	41	4410. 74	4410.00	4410. 39	1. 00	1.12	31. 5	34.0	3. 10	0.	42.	0.
121	01	1. 37	1766											
122	01	1.84	1766											
123	0 1	2. 36	1766											
124	01	2.93	1766											
125	0 1	3. 55	1766											
126	01	4. 24	1766											
127	0 1	5. 00	1766											
128	0 1	5. <b>84</b>	1766											
129	01	6. 75	1766											
130	01	7.76	1766										ż	
131	01	8. 87	1766											
132	02	0. 09	1766											
133	02	1. 44	1766											
134	02	2.92	1766											
135	02	4.54	1766									1		
	PARAME	TER						UNITS	VARIABLE	VA	LLE			
×	oloioloioloi	ojojojojo	icicicicicicicie				*	iojojojojojoj	: sjojojojojo :	i a la l	ojojojok			
	INITIA	L FLO	Ŵ					CMS	Q(1)		50.			
	MAX FL	OM						OMS	CM ·	31	77.			
	FINAL	FLOW						OMS	Q(NU)		50.			
	time 1	io max	FLOW					HRS	ΤP	3	8. 50			
										· .				
	NUMBER	r op t	THE STEPS						NNU		135			
	TOTAL	YOLUM	E DISCHARG	ed from f	<b>ESERVOIR</b>	ļ	MILLIO	N CU M	DISVOL.		31.			

	(QDI (1), I=1, N	D					
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
<b>50</b> .	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	<b>50</b> .	50.	50.	50.	50.
50.	50.	<b>50</b> .	50.	50.	50.	50.	50.
50.	50.	50.	<b>5</b> 0.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	50.
50.	50.	50.	<b>50</b> .	50.	50.	50.	50.
50.	50.	50.	50.	50.	50.	50.	

(YI (I), I≈1, N)

.

•		•					
4410. 44	4371.37	4332. 31	4293.25	4254. 19	4215. 12	4176.06	4137.00
4097.94	4058.87	4019. 81	3980.75	3941. <b>6</b> 9	3902.62	3863, 56	3824, 50
3785. 44	37 <b>4</b> 6. 37	3707. 31	3668.25	3629. 19	3590. 12`	3551, <b>06</b>	35 Ì 2. 00
3472. 94	3433. 87	3394. 81	3355.75	3316.69	3277.62	3238, 56	3199, 50
3160. 44	3119. 91	3079. 41	3038.88	2998. 38	2957.85	2917.35	2876.82
2836.32	2795. 79	2755. 29	2714.76	2674.26	2633.73	2593, 23	2552.70
2512. 19	2471.68	2431. 16	2390.64	2350. 14	2309. 61	2269.10	2228.58
2188.07	2147.56	2107.05	2066.53	2026. 02	1985. 50	1 <b>944</b> , 99	1904.47
1863.96	1823. 44	1782.93	1742. 41	1701.90	1661. 38	1620. 87	1580.35
1569. 59	1558.82	1548. 04	1537.27	1526.50	1515. 73	1504, 95	1494. 17
1483.40	1472.63	1461. 85	1451.08	1440. 31	1429. 53	1418.76	1407. 99
1397.21	1386.44	1375.67	1364.89	1354.12	1343.35	1332. 5 <b>8</b>	1321.80
1311.03	1300. 26	1289.49	127 <b>8</b> . 72	1267.94	1257. 1 <b>8</b>	1246.40	1235, 63
1224.86	1214. 09	1203.32	1192.55	1181.78	1171. 02	1160. 25	1149. 48
113 <b>8</b> . 71	1127.94	1117. 18	1106.41	1095.64	1085.14	1074.63	1064, 13
1053.63	1043.12	1032.62	1022.11	1011.61	1001.10	990, 60	980, 09
969.59	959. 08	948.58	938.08	927.57	917. 07	906, 56	896, 06
885.55	875.05	864.55	854.04	843. 54	833. 04	822.53	812. 03
801.53	791.02	780. 52	770. 02	759. 51	749. 01	738, 51	728.00
717.50	707.00	696.49	685.99	675, 49	664.99	654.48	643, 98
633. <b>48</b>	622. 97	612. 47	601.97	591.47	580, 96	570. 46	

1

#### TIME PARAMETERS OF OUTFLOW HYDROGRAPH IMMEDIATELY DOWNSTREAM OF DAM

PARAMETER	UNITS	VARIABLE	VALLE
	xiololololok	<del>xojojojojo</del> j	<del>xelejejejejejejejejeje</del> je
TIME TO FAILLRE	HR	TFH	3. 500
TIME TO START OF RISING LIMB OF HYDROGRAPH	HR	TFO	0.000
TIME TO PEAK	HR	TP	3.500
TIME STEP SIZE	HR	DIHI	0.175
ROUTING COMPLETED.			
KTIME= 249 ALLOWABLE KTIME= 699	TT=	24. 4	

.

-

1

# PROFILE OF CRESTS AND TIMES FOR Raphstreng

BELOW RUN3 :

DISTANCE	

DISTANCE							
FROM DAM	MAX ELEV	MAX FLOW	TIME MAX	MAX VEL	FLOOD FLEV		
KM	М	OMS	DEV-HRS	M/S	м	ELEV-HRS	
<del>Xololeloloix</del>	xioioioioioioie	<del>kolesko lesk</del>	<b>XOIOIOIOIO</b>	*Ciclololoiok			
0.000	4414.96	3164	3. 470	10. 22	0.00	0.00	
1.000	4375.91	3157	3. 470	10. 20	0.00	0.00	
2.000	4336.84	3149	3.470	10. 23	0.00	0.00	
2. <b>999</b>	4297.78		3.536	10. 23	0.00	0.00	
3. 999	4258.72	3145	3.543	10. 27	0. 00	0.00	
4. 999	4219.67	3146	3. 548	10. 28	0. 00	0. 00	
5, 999	4180.61	3145	3.568	10. 30	0. 00	0. 00	
6. 999	4141.55	3144	3.587	10. 32	0.00	0.00	
7. 999	4102. 49	3144	3. 597	10. 34	0. 00	0.00	
8. 998	4063.44	3144	3.607	10. 36	0.00	0. 00	
9, 998	4024.38	3143	3.627	10. 38	0. 00	0.00	
10.998	3985. 32	3143	3.656	10.40	0. 00	0.00	
11. 998	3946.26	3143	3.666	10. 43	0. 00	0.00	
12.998	3907.20	3143	3.686	10. 45	0.00	0.00	
13. 998	3868.14	3142	3.695	10. 47	0.00	0.00	
14. 997	3829.09	3141	3.705	10. <b>49</b>	0. 00	0.00	
15. 997	3790. 03	3141	3.725	10. 51	0. 00	0. 00	
16. 997	3750. 97	3140	3.745	10. 53	0. 00	0.00	
17.997	3711. 91	3140	3.764	10.56	0.00	0.00	
18.997	3672. 85	3139	3. 784	10. 58	0. 00	0.00	
19. 997	3633.80	3139	3.803	10.60	0.00	0. 00	
20. 996	3594.74	3138	3, 823	10. 63	0.00	0.00	
21.996	3555. 6 <b>8</b>	3137	3, 823,	10.65	0.00	0.00	
22. 996	3516.62	3137	3, 843	10.67	0.00	0. 00	
23, 996	3477.56	. 3137	3.862	10. 70	0, 00	0.00	
24.996	3438. 51 ·	3136	3, 882	10. 72	0, 00,	0.00	
25. 996	3399. 45	3136	3, 902	10. 75	0, 00	0.00	
26.995	3360. 39	3135	3, 921	10. 77	0.00	0. 00	
27.995	3321.33	3135	3, 921	10, 80	0, 00	0. 00	
28.995	32 <b>8</b> 2. 27	3134	3, 941	10. 82	0.00	0.00	
29.995	3243. 22	3134	3, 961	10. 85	0.00	0.00	
30. 995	3204.16	3133	3, 980	10.87	0. 00	0.00	
31, 995	3165.10	3133	4.000	10. 90	0.00	0.00	
33.010	3124. 49	3132	4.000	10. 99	0, 00	0.00	
34. 025	3083. 99	3132	4. 019	10. 81	0, 00	0.00	
35. 040	3043. 41	3132	4. 039	10. 83	0, 00	0.00	
36, 056	3002.89	3131	4. 059	10. 70	0. 00	0.00	
37.071	2962.32	3131	4.078	10. 70	0.00	0.00	
38.086	2921.79	3130	4. 098	10. 60	0.00	0. 00	
39, 101	2881.24	3130	4, 098	10. 57	0.00	0.00	
40, 116	2840. 70	3129	4.118	10. <b>49</b>	0.00	0. 00	
41, 132	2800. 15	3129	4. 137	10. 46	0.00	0. 00	
42, 147	2759. 62	3129	4. 157	10, 3 <del>9</del>	0. 00	0.00	
43, 162	2719.07	3128	4. 177	10. 35	0.00	0.00	
44. 177	2678. 53	3128	4. 196	10. 29	0, 00	0.00	
45, 192	2637.99	3127	4.216	10. 24	0.00	0. 00	
46, 208	2597.45	3127	4. 235	10. 1 <del>9</del>	0.00	0.00	
47. 223	2556. 91	3126	4. 235	10. 15	0.00	0. 00	

1

# PROFILE OF CRESTS AND TIMES FOR Raphstreng

RELOW RUN3 :

DISTANCE							
FROM DAM	MAX ELEV	MAX FLOW	TIME MAX	MAX VEL	FLOOD ELEV	TIME FLOOD	
KM	М	OMS	ELEV-HRS	M/S	M	ELEV-HRS	
<del>), iolojojojok</del>		******	<b>statestesteste</b>	<b>xalajajajaj</b> ajaj	<del>xolotolotolotok</del>		
48. 238	2516.37	3126	4. 255	10. 10	0. 00	0.00	
49. 253	2475. 83	3125	4.275	10. 05	0. 00	0, 00	
50. 269	2435.29	3125	4. 294	10.01	0.00	0.00	
51.284	2394.75	3125	4. 314	9.96	0.00	0.00	
52. 299	2354.22	3124	4. 334	9, 92	0.00	0.00	
53. 314	2313.68	3124	4. 353	9.88	0. 00	0. 00	
54. 329	2273.14	3123	4.373	9.84	0.00	0.00	
55. 345	2232. 60	3123	4. 393	9.80	0.00	0.00	
56.360	2192. 07	3123	4.412	9.75	0. 00	0.00	
57. 375	2151, 53	3122	4. 412	9.72	0. 00	0.00	
58.390	2111.00	3122	4. 432	9.68	0. 00	0.00	
59. 405	2070.46	3121	4. 471	9.64	0. 00	0.00	
60. 421	2029. 93	3121	4. 491	9.60	0. 00	0.00	
61. 436	1989. 39	3120	4.510	9.56	0. 00	0.00	
62. 451	1948.86	3120	4. 530	9. 53	0.00	0. 00	
63.466	1908.32	3119	4. 530	9.49	0.00	0. 00	
64. 482	1867.79	3119	4. 550	9.46	0. 00	0. 00	
65. 497	1827.26	3119	4. 569	9.42	0. 00	0. 00	
66. 512	17 <b>8</b> 6. 72	3118	4. 589	9. 39	0. 00	0.00	
67.527	1746. 19	3118	4.609	9.35	0.00	0.00	
68. 542	1705.66	3117	4.628	9.32	0.00	0. 00	
69.558	1665.13	3117	4. 648	9. 29	0.00	0.00	
70. 573	1624.59	3117	4.667	9. 26	0.00	0. 00	
71. 588	1584.06	3116	4.687	9. 22	0,00	0.00	
72.590	1576. 94	3115	4. 726	4. 30	0.00	0.00	
73. 592	1562.31	3113	4. 785	13. 02	0.00	0.00	
74. 5 <del>9</del> 4	1555. 64	3111	4.766	4. 22	0.00	0.00	
75. 596	1540, 65	3110	4.864	20. 45	0.00	0.00	
76.598	1534.27	3107	4.824	4. 20	0.00	0.00	
77.600	1519.06	3106	4.903	21. 20	0.00	0.00	
78.602	1512.86	3103	4. 883	4. 21	0, 00	0, 00	
79.604	1497.52	3102	4.962	21.08	0.00	0.00	-
80. 606	1491.42	3099	4.962	4. 24	0.00	0. 00	
81. 509	1476.02	3099	5. 021	20. 41	0.00	0.00	
82. 611	1469.98	3096	5. 021	4. 27	0.00	0.00	
83.613	1454.54	3095	5.060	19.36	0.00	0.00	
84. 615	1448.54	3092	5.080	4. 32	0, 00	0.00	
85.617	1433.06	3092	5. 119	20.35	0. 00	0.00	
86.619	1427.11	3089	5. 139	4.36	0.00	0.00	
87.621	1411.60	3088	5. 178	18.48	0.00	0.00	
88. 623 90. 695	1405.67	3086	5. 198	4.41	0.00	0.00	
89. 625 00. 627	1390. 14	3085	5.237	22.14	0.00	0. 00	
90. 627 01. 620	1384.24	3083	5.256	4.46	0.00	0. 00	
91. 629 92. 631	1368.68	3082	5, 296	21.51	0.00	0.00	
92. 631 93. 633	1362.82	3080	5.315	4. 51	0.00	0.00	
93. 633 94. 635	1347.24	3079 3077	5.355	20. 57	0.00	0.00	
95. 637	1341, 40 1325, 79	3077 3077	5.355	4.56	0.00	0.00	
00.001	1020.13	3017	5. 414	19.71	0. 00	0.00	•

1

#### PROFILE OF CRESTS AND TIMES FOR Raphstreng BELOW RUN3 :

DISTANCE FROM DAM MAX ELEV MAX FLOW TIME MAX MAX VEL FLOOD ELEV TIME FLOOD KM M CMS ELEV-HRS M/S ELEV-HRS M xololololok \*okoloslosloska \*otok \*oioie xho oloiok xie, \*\*\*\*\* 96.639 3075 1319.99 5.414 4.62 0.00 0.00 3074 97.641 1304.36 5.472 18.92 0.00 0.00 3072 98.643 1298.59 5.472 0.00 4.68 0.00 99.646 3071 20.73 1282.93 5.512 0.00 0.00 100.648 1277.19 3069 5.531 4.74 0.00 0.00 101.650 1261.52 3068 5.571 20.50 0.00 0.00 102.652 1255.80 3067 5.590 4.80 0.00 0.00 103.654 1240.11 3066 5.630 19.62 0.00 0.00 104.656 1234.43 3064 5.649 4.87 0.00 0.00 105.658 1218.71 3063 5.688 18.15 0.00 0.00 106.660 1213.06 3061 5.708 4.94 0.00 0.00 107.662 1197.32 3061 5.728 20. 21 0.00 0.00 108.664 1191.70 3059 5.767 5.01 0.00 0.00 109.666 1175.94 3058 5.787 18.86 0.00 0.00 110.668 1170.36 3057 5.806 5.09 0.00 0.00 111.670 1154.58 3056 5.845 20.32 0.00 0.00 112.672 1149.03 3054 5.865 5.17 0.00 0.00 113.674 1133.23 3053 5.885 18.65 0.00 0,00 114.676 1127.71 3052 5.924 5.26 0.00 0.00 115.678 1111.90 3051 5.944 19.47 0.00 0.00 116.680 1106.42 3050 5.983 5.35 0.00 0.00 117.686 1090.78 3049 6.003 19.33 0.00 0.00 118.692 1085.33 3047 6.022 5.34 0.00 0.00 119.698 1069.70 3046 6.042 19.18 0.00 0.00 120.704 1064.25 3045 6.081 5.33 0.00 0.00 121.710 1048.62 3044 6.101 17.75 0, 00 0.00 122.715 1043.16 3043 6.140 5.32 0.00 0.00 123.721 1027.54 3042 6.160 19.42 0.00 0.00 124.727 1022.08 3041 6.179 5.31 0.00 0.00 3040 125.733 1006.46 6.199 18.71 0.00 0.00 126.739 1001.01 3039 6.238 5.30 0.00 0.00 127.745 985.38 3038 6.258 20.000.00 0.00 3036 128.750 979.93 6.297 5.28 0.00 0.00 3036 129.756 964.31 6.317 21.77 0.00 0.00 130.762 958.85 3034 6.356 5.27 0.00 0.00 3034 131.768 943.23 6.356 19.35 0.00 0.00 132.774 937.78 3032 6.395 5.26 0.00 0.00 133.780 922.16 3032 6.415 21.22 0.00 0.00 134.785 916.70 3030 6.454 5.24 0.00 0.00 135.791 901.09 3030 6.474 19.02 0.00 0.00 136.797 895.63 3028 6.513 5.23 0.00 0.00 137.803 880.01 3028 6.533 21.74 0.00 0.00 874.56 3027 6.552 138.809 5.22 0.00 0.00 3026 6.572 17.27 139.815 858.94 0.00 0.00 3024 6.611 140.820 853.49 5.20 0.00 0.00 141.826 837.88 3024 6.631 18.64 0.00 0.00 142.832 832.42 3023 6.670 5.19 0.00 0.00 3022 143.838 816.81 6.690 20.85 0.00 0.00

# FROTTLE OF CREETS AND LIMES FOR Kaphstreng

BELOW RUN3 :

FROM DAM	MAX ELEV	MAX FLOW	TIME MAX	MAX VEL	FLOOD FLEY	TIME FLOOD
КМ	м	CMS	ELEV-HRS	M/S	м	ELEV-HRS
		**		xalojojojojoj		xololoioloioloiok
144. 844	811.35	3021	6.709	5.17	0.00	0.00
145. 850	795.74	3020	6.729	19. 11	0.00	0, 00
146. 855	790. 29	3019	6.768	5.16	0. 00	0.00
147.861	774.68	3018	6.788	18.09	0.00	0, 00
148.867	769. 22	3017	6.827	5.14	0. 00	0. 00
149, 873	753, 61	3016	6.847	17.72	0. 00	0.00
150. 879	748.16	3015	6.866	5. 13	0. 00	0.00
151. <b>884</b>	732.55	3014	6.886	20. 12	0.00	0.00
152. 890	727.09	3013	6. 925	5. 11	0.00	0.00
153. 896	711. <b>49</b>	3013	6, 945	16. 61	0. 00	0. 00
154.902	706. 03	3011	6, 984	5.10	0.00	0.00
155. 908	690.43	3011	7.004	18.86	0.00	0.00
156. 914	684.96	3009	7.004	5.08	0.00	0. 00
157. 919	669.36	3003	7.004	21.07	0. 00	0.00
158. 925	663.88	2994	7.004	5.06	0.00	0.00
159. 931	648.28	2982	7.004	17.58	0.00	0, 00
160. 937	642.78	2965	7.004	5.02	0. 00	0.00
161. 943	627.19	2959	7.293	19.98	0.00	0. 00
162. <del>94</del> 9	621.75	2972	7.293	5.00	0.00	0.00
163. 954	606.17	2983	7.293	22.71	0, 00	0.00
164.960	600.73	2996	7.293	6.00	0.00	0.00
165. 966	585.16	3012	7.293	16. 97	0.00	0.00
166. 972 -	579. 75	3038	7.293	· 5. 01	0.00	0.00

1

	GAC	e zero	BELOW = 4410.00	RUN3 M	: Max	FLEVAT	AT K TION R		.00 FLOOD WAVI	e = 4414.96 M		
	0/w	13 21340	- 1110. 00			NOT AV			112.22			
			MAX ST		4.96			TIME =	3,470 10	RS		
			MAX FL		3165		AT	' TIME =	3.470 HO	urs		
	TIME	STACE	FLOW									
	HR	M	OMS	0	1000	20	000	3000	4000	5000		
	0.0	4410.0	0	*						•		
	0.2	0.5		.*			•		٠	•		
	0.4	0.6	96	.*	•		,					
	0.6	0.9	168	. *	•		•	•	•			
	0.8	1, 2	287	. *			•	•	•	•		
	1.0	1.6	446	. *	•		·	•	•	•		
	1.2	2.0	644	•	* .		·		•	·		
	1.4	2.4	879	,	*		·	•	•	•		
	1.6	2.8	1143	•	.*		•		•	•		
	1.8	3.1	1429	•		*	·	,	•			
	2.0	3.5	1726	•	•	*	، بد	•	•	•		
	2.2	3.8	2016	•	٠		*	•	•	*		
	2.4	4.1	2285 2526	•	•			г. ж	•	•		
	2.6 2.8	4.4 4.6	2526 2732	•	•		•	≁ . ★	٠	•		
	2.8 3.0	4.0 4.7	2732 2901	•	•			*	•	•		
	3.0	4.8	3034	•	•		•	*	•			
	3.4	4.9	3135	•	•		•	.*	•			
	3.6	4.7	2848				÷	*.				
	3.8		2287		-		. ,	<b>*</b>				
	4.0		1859				*					
	4.2	3.3	1527			*						
	4.4	2.9	1268			*			•			
	4.6		1063		, ا	k						
	4.8	2.4	898		*.		•					
	5.0	2.2	765		*.	•			<i>,</i> .	. •		
	5.2	° 2. 0	656	· ·	* .		•	•	•		-	
	5.4		566	•	∗ .	•	• '	•		•		
	5.6		492	. '	<b>*</b> .		•.	. •	· .	•		
	5.8		430	. *	•		•	•	•	•		
	6.0		377		•		•	•	•	•		
	6. 2		333		•		•	•	•	•		
	6.4		295				•	•	•			
	6.6		262		•		•	•		•		
	6.8		235		•		•	٠	•	•		
	7.0				•			٠	•	•		
	7.2				•		•	•	•	•		
	7.4 •7.6				•		•	•	•	•		
	- 7.8				•		•	•	•	•	·	
	8. C				•		•	•	•	•		
	8.2				•		•	•	•			
	8.4				•		÷	•		•		
	8.6				•			•	•			
÷	8.8						•	•	•	,		
	9. (							•				
	9.2							•				
	. 9.4											
	9. (											
	9.1											
	10. (			.*								

	DIS	icharge	HYDROGRAP <del>I</del> BELOW	i for Run3	Raphs :	treng		КМ -		TION NUMBER . 99	33			
	GAG	e zero	= 3160.00 max st/	FLOOD	MAX STAGE 5. 10	NOT A	VATLA	REACHEI VELE VT TIME		FLOOD WAVE = 4.000 HOLRS		10 M		
			MAX FLC	₩ =	3133	OMS		AT TIME		4.000 HOURS				
	TIME	STACE	FLOW											
	HR	M	CMS	0	1000	2	000	300	00	4000	5000			
		3160. 0	0						•	,				
	0. 25	0.4	50		•									
	0.50	0.4	50		•		•		•					
	0.75	0.4	50		-		•		•	•				
	1.00	0.4	51		٠		•		•					
	1. 25 1. 50	0.4 0.4	51 51		•		·		•	•	·			
	1. 30	0.4	51 58		•		·		•	•	•			
	2.00	0.9	178		•		•		•		•			
	2. 25	2.3	831		*		•		•	•	•			
	2.50	3.2	1392			*	•			•	•			
	2. 75	3.7	1840			,	*.			•				
	3. 00	4.2	2245				. *	:						
	3. 25	4.6	257 <b>8</b>					*						
	3. 50	4.8	2834					*		•				
	3. 75	5.0	3023						*	•				
	4.00	5.1	3133	•	•				.*	٠				
	4.25	4.6	2663		•			*	•					
	4.50	4.1	2129		•		.*		•	••••	•			
	4.75 5.00	3.6	1726		•	*	•			-	•			
	5. 00 5. 05	3.2	1416		•	*	•		•		•			
	5. 25 5. 50 ·	2.9 2.6	1175 9 <b>85</b>		. * *		•		•	• •.	•	· .		
	5. 75	2.3	833		<u>т</u> .		•		•	•	•			
	6.00	2. 1	711		*		·		•	•				
	6. 25	1.9	611		<b>*</b>	-	•		•	•	•			
	6. 50	1.8	528	*							•		-	
	6. 75	1.6	460	· *							÷			
	7.00	1.5	403	. *										
	7.25	1.4	356	. *										
	7. 50	1.3		. *	•					•				
	7.75	1.2		. *					•	•				
	8,00	1.1		. *	•		•		•	•				
	8.25	1.1		. *	•		•		•	•	•			
	8. 50 8. 75	1.0		. *	•		•		•	•	·			
	a. 15 9, 00	1.0 0.9		. * . *	•		•		•	•	·			
	9. 25	0.8		, *	•		•		•	•	·			
	9, 50	0.8	138				•		•	•	·			
	9.75	0.8		*					•	•	•			
	10.00	0.7		.*			÷			•	•			
	10.25	0.7		. *					•					
	10. 50	0.7		.*										
	10.75	0.6		. *	•									
	11.00	0.6		*	•					•				
	11.25	0.6		.*						•				
	11.50	0.5		.*	•		4		•					
	11.75	0.5		.*	•		•							
	12.00	0.5		.*	•		•		•	•				
1	12. 25	0.5	59	. *	•		•		•	٠	٠			

1

÷

# DISCHARGE INDROGRAPH FOR Raphstreng ... STATION NUMBER 72 BELOW RUN3 : AT KM 71.59

#### GAGE ZERO = 1580.00 M MAX ELEVATION REACHED BY FLOOD WAVE = 1584.06 M FLOOD STAGE NOT AVAILABLE MAX STAGE = 4.06 M AT TIME = 4.687 HOURS

MAA	31/106 =	4.00 M	AT TIME	1.007 100105
MAX	FLOW =	3117 OMS	AT TIME =	4.687 HOURS

TIME S		FLOW	-			0000	1000	5000		
	M	ONS	0	1000	2000	3000	4000	5000		
0. 0-15		0	*	•	•	•	•	•		
0.5	0, 4	51	.*	•	•	•	•	•		
1.0	0.4	51	*	٠	•	•	•	•		
1.5	0.4	51	.*	•	•	•	•	•		
2.0	0.4	51	.*	•	•	•	•	•		
2.5	0.4	52	.*	•	•	•	•	•		
3.0	0.4	52	.*	•	•	•	. •	•		
3.5	1.7	690	•	* .	•	•	•	•		
4.0	3.6	2547	•		•	* .		•		
4.5	4.0	3032	•	•	•	*		•		
5.0	3.7	2688				*	•	•		
5.5	3.0	1878	•		*.	•	•	•		
6. 0	2.5	1360		•	* .	•	•	•		
6.5	2.1	1016		*	•	•		•		
7.0	1.8	778		*.		٠		•	,	
7.5	1.6	612		*.			•	•		
8.0	1.4	490		* .		•				
8.5	1.2	397	•	* .		, • <u>;</u>	•	•		
9.0	1. 1	327	, ×	¥.		•		•		
9.5	1.0	273		× .		•	•			
10. 0	0.9	229	. *		•		٠.			
10. 5	0.8	195	. *	•	. •			•		
11.0	. 0.7	167	. *		•	•				
11.5	0.7·	144	*		۰.	۰.	·			
12. 0	0.6	126	*		1.		· •	•		
12.5	0.6	110	.*						•	
<b>13</b> . 0	0.5	97	*		÷., .	•		•		
13. 5 <sup>.</sup>	0.5	86	.*				•	•		
14. 0	0.5	76	*							
14.5	0.4	68	*			•	,	• .		
15.0	0.4	62	*.			•				
15. 5	0.4	57	*			•				
16. 0	0.4	54	*				•	•		
16. 5	0.4	52	.*			•				
17.0	0.4	52						•		
17.5	0.4	53		,				•		
18. 0	0.4	53						•		
18.5	0.4	53		·· · ·	•					
19. 0	0.4	52			•			•		
<b>19</b> . 5	0. 4	52						•		
20. 0	0.4	52								
20.5	0.4	53		,				•		
21.0	0.4	52								
21.5	0.4	5								
22.0	0.4	5								
22.5	0.4	5								
23.0	0.4	5								

			RUN3	:	AT K						
GAG	e zero	= 1095.00		MAX FLI STAGE NO			' FLOOD WAVE =	= 1106.42 )	1		
		MAX ST MAX FI		11.42 M 3050 CM		`TIME = `TIME =					
	STAGE	FLOW									
HR	M	OMS		1000	2000	3000	4000	5000			
	1095.0		*	•	٠	•		•			
0.5	2. 3	112		•	•	•		•			
1.0	2.7	157			. •	٠		•			
1.5	2. <b>8</b>	169		•	•			•			
2.0	2.8	169		•	,	•		•			
2.5	2.8	169		•	•	•	•	•			
3.0	2.8	171		•	•		•	٠			
3.5	3.0	188	. *	•	•		•				
4.0	3.2	207		•	•	٠		•			
4.5 5.0	3.3 4.1	218	*	•	•	•	•	•			
5. U 5. 5	4. 1 10. 7	322 2664		•	*	سور		-			
5. 5 6. 0	10.7	3047		•	,	·····		•			
6. 5	10.5	2506		•	•	* .		٠			
7.0	9.3	1904			*.	··· ·		•			
7.5	8.3	1486			*	•	•				
8.0	7.4	1180		· . *		•	•	•			
8.5	6.7	951		*							
9.0	6. 1	780		*.							
9.5	5.6	647		* .				•			
10. 0	5. 1	542	. *								
10. 5	4.7	460	. *			;					
11. 0	4.4	393	. *					• •			
11.5	4. 1	340	*	•	•						
12. 0	3. <b>8</b>	295		•	÷	•	• •	· .			
12. 5	3.5	258		•	:.	٠.	•				
13. 0	3.3			•		•	•	•			
13.5	3.1	203		٠			•	•			
14.0	3.0	188		•	•	•	•	•			
14.5	3.0			•	•	•	•	•			
15.0	2.9			•	•			•			
15. 5 16. 0	2.8			·	•	•	•	•			
16. 0 16. 5	2. <b>8</b> 2. 7			•	•		,	•			
10. 5	2.7			·	•	•		•			
17.5	2.7			•	•	•	•	•			
18.0	2.6		<b>.</b> *	•	-	•	•	•			
18.5	2.6		.*	•				•			
19.0	2.6		.*			•	•	•			
19.5	2.6		.*			•					
20. 0	2.6		.*								
20. 5	2.6		.*							· .	
21. 0	2.6		.*					•			
21.5	2.6		.*								
22.0	2.6		.*	•							
22.5	2.6		.*			•					
23. 0	2.6	143	<b>, *</b>			•		•			

Calculation Result of Reservoir Sedimentation

•

#### **Calculation of Deposit Shape**

#### (1) Calculation Process (EPDC/KCC FLOW500 MODEL)

- i) Non-uniform flow calculation for the initial river sections
- ii) Calculation of friction velocities (u\*) at respective sections
- iii) Calculation of sediment load based on the Lane-Kalinske formula
- iv) Estimate of riverbed movement by equation of continuity and then surface elevation of deposit

(Numerical Analysis based on  $\frac{\partial z}{\partial t} = 1/(1-\lambda) \cdot 1/B \cdot \frac{\partial (q_B \cdot B)}{\partial x}$ )

- v) Related calculation of the above on daily basis
- (2) Prerequisite for Calculation
  - vi) Diameter of Particle

Uniform diameter was adopted in this calculation. d=0.65 mm was adopted to make annual sediment load approximately  $610 \times 10^3$ m<sup>3</sup>/year in the Lane-Kalinske formula, and then the porosity of 0.4 was used.

- vii) River Discharge The river discharge at Wangdi Rapids GS was used.
- viii) Reservoir Elevation

The reservoir surface used for the calculation is set at 1,154 m.

(3) Lane-Kalinske Formula

 $q_{B} = q \cdot C_{0} \cdot P$  $C_{0} = 5.55 \cdot \triangle F(w_{0}) \cdot \{1/2 \cdot (u \cdot / w_{0}) \cdot \exp(-(w_{0} / u \cdot)^{2})^{1.61}$ 

Where

q<sub>s</sub>: Suspended load (per unit width )

q: Inflow

C<sub>0</sub>:Density of Suspended

w<sub>0</sub>:Sedimentation Rate

u.: Friction Velocity

## Caluculation Result of Reservoir Sedimentation

No.	Distance	Accumulative Distance Elevation of Riverbed(m)				
	(m)	(m)	Initial Condition	1Year	2Year	3Year
1	0	0	1,095.00	1,095.00	1,095.00	1,095.00
2	176	176	1,100.00	1,100.00	1,100.00	1,100.00
3	143	319	1,105.00	1,105.00	1,105.00	1,105.00
4	271	590	1,110.00	1,110.00	1,110.00	1,110.00
5	308	898	1,115.00	1,115.00	1,115.00	1,115.00
6	244	1,142	1,120.00	1,120.00	1,120.00	1,120.00
7	308	1,450	1,122.50	1,122.50	1,122.50	1,122.50
8	. 308	1,758	1,125.00	1,125.00	1,125.00	1,125.27
9	298	2,056	1,130.00	1,130.00	1,134.36	1,150.40
10	96	2,152	1,135.00	1,135.21	1,152.78	1,150.03
11	199	2,351	1,140.00	1,152.22	1,153.57	1,153.83
12	192	2,543	1,145.00	1,153.55	1,154.45	1,154.9
13	148	2,691	1,150.00	1,154.32	1,155.30	1,155.9
14	216	2,907	1,152.50	1,155.80	1,156.64	1,157.1
15	216	3,122	1,155.00	1,157.51	1,158.07	1,158.4
16	140	3,262	1,160.00	1,158.69	1,159.04	1,159.4
17	223	3,485	1,162.50	1,160.59	1,160.62	1,160.9
18	223	3,709	1,165.00	1,162.47	1,162.22	1,162.4
19	269	3,978	1,167.50	1,164.66	1,164.17	1,164.2
20	269	4,246	1,170.00	1,166.72	1,166.11	1,166.1
21	352	4,598	1,171.00	1,169.19	1,168.63	1,168.6
22	352	4,950	1,172.00	1,171.44	1,171.11	1,171.1
23	352	5,302	1,173.00	1,173.53	1,173.57	1,173.6
24	352	5,654	1,174.00	1,175.58	1,176.04	1,176.1
25	352	6,006	1,175.00	1,177.75	1,178.53	1,178.7
26	5 332	6,338	1,177.50	1,180.01	1,180.93	1,181.1
27	/ 332	6,670	1,180.00	1,182.52	1,183.39	1,183.5
28	481	7,151	1,185.00	1,186.58	1,187.07	1,187.1
29	375	7,526	1,190.00	1,190.00	1,190.00	1,190.0

(1/4)

Caluculation Result of Reservoir Sedimentation

N	Distance	Accumulative Distance	Elevati	on of River	bed (m)	(2/4)
No.	(m)	(m)	Initial Condition	4Year	5Yeaqr	6Year
1	0	0	1,095.00	1,095.00	1,095.00	1,095.00
2	176	176	1,100.00	1,100.00	1,100.00	1,100.00
3	143	319	1,105.00	1,105.00	1,105.00	1,105.00
4	271	590	1,110.00	1,110.00	1,110.00	1,110.00
5	308	898	1,115.00	1,115.00	1,115.00	1,115.00
6	244	1,142	1,120.00	1,120.00	1,120.00	1,120.00
7	308	1,450	1,122.50	1,122.50	1,122.67	1,130.66
8	308	1,758	1,125.00	1,135.22	1,151.29	1,152.75
9	298	2,056	1,130.00	1,153.04	1,153.17	1,153.95
10	96	2,152	1,135.00	1,153.54	1,153.65	1,154.41
11	199	2,351	1,140.00	1,154.41	1,154.56	1,155.44
12	192	2,543	1,145.00	1,155.45	1,155.63	1,156.49
13	148	2,691	1,150.00	1,156.31	1,156.52	1,157.32
14	216	2,907	1,152.50	1,157.61	1,157.87	1,158.57
15	216	3,122	1,155.00	1,158.96	1,159.26	1,159.84
16	140	3,262	1,160.00	1,159.85	1,160.17	1,160.69
17	223	3,485	1,162.50	1,161.30	1,161.64	1,162.07
18	223	3,709	1,165.00	1,162.77	1,163.11	1,163.47
19	269	3,978	1,167.50	1,164.57	1,164.91	1,165.20
20	269	4,246	1,170.00	1,166.39	1,166.71	1,166.96
21	352	4,598	1,171.00	1,168.82	1,169.11	1,169.31
22	352	4,950	1,172.00	1,171.29	1,171.53	1,171.71
23	3 352	5,302	1,173.00	1,173.78	1,173.99	1,174.14
24	352	5,654	1,174.00	1,176.31	1,176.48	1,176.61
25	5 352	2. 6,006	1,175.00	1,178.85	1,178.99	1,179.10
26	5 332	6,338	1,177.50	1,181.26	1,181.37	1,181.46
27	7 332	. 6,670	1,180.00	1,183.69	1,183.77	1,183.83
28	3 481	7,151	1,185.00	1,187.23	1,187.27	1,187.30
29	375	5 7,526	5 1,190.00	1,190.00	1,190.00	1,190.00

(2/4)

### Caluculation Result of Reservoir Sedimentation

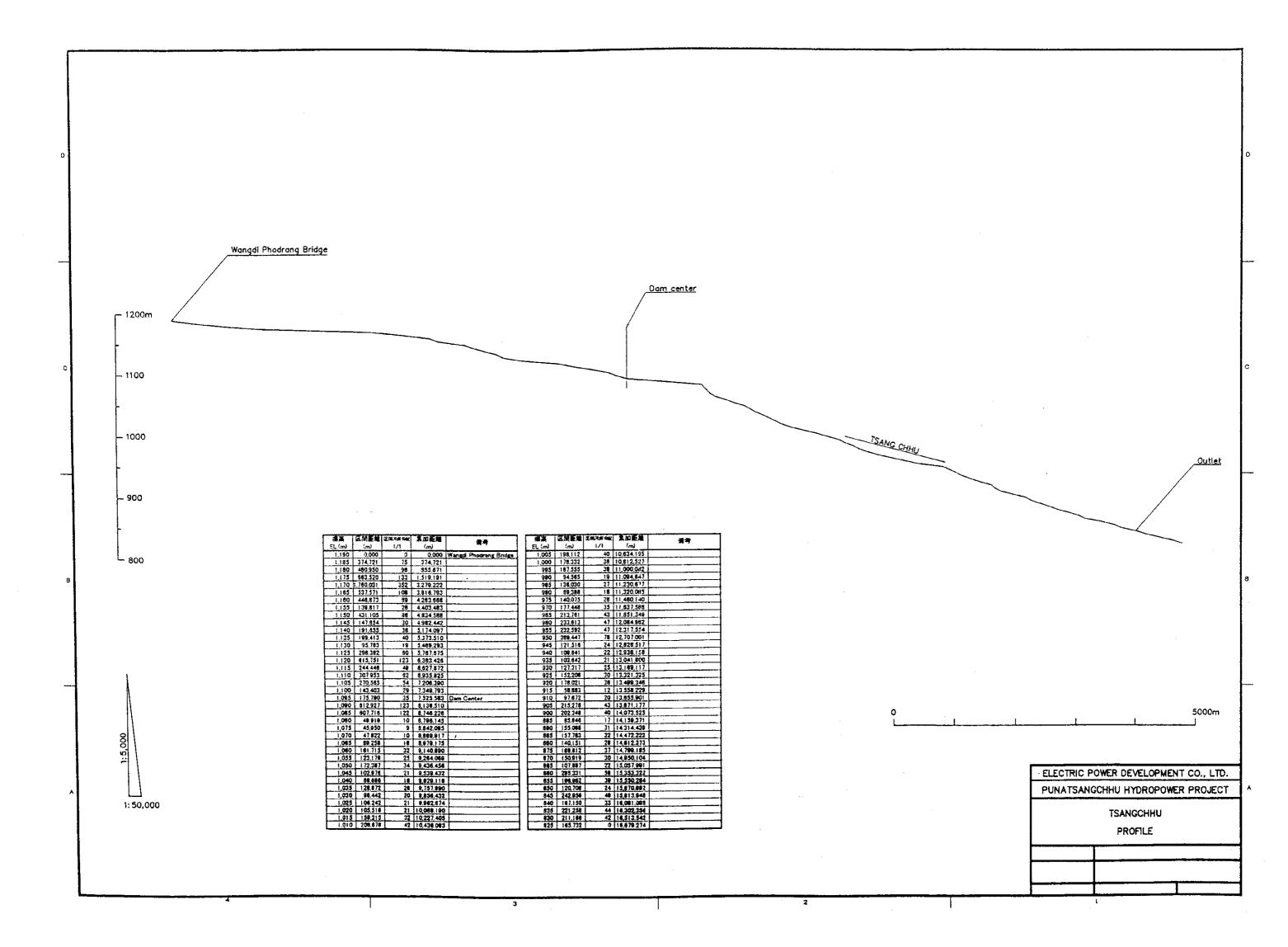
•

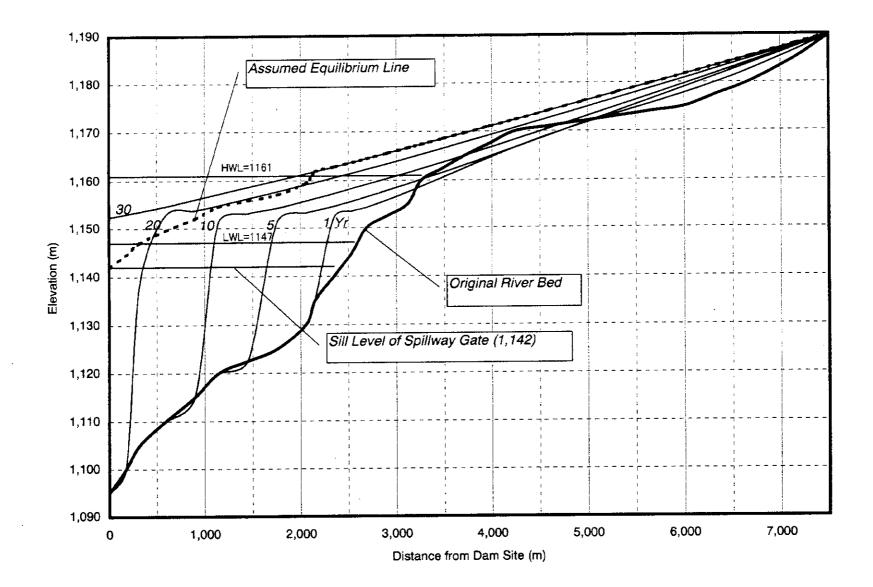
	Distance	Accumulative Distance	<b>1</b> 21 42	on of River	hed (m)	(3/4)
No.		(m)				9Year
	(m)		Initial Condition	7Year	8Year	
1	0	0	1,095.00	1,095.00	1,095.00	1,095.00
2	176	176	1,100.00	1,100.00	1,100.00	1,100.00
3	143	319	1,105.00	1,105.00	1,105.00	1,105.00
4	271	590	1,110.00	1,110.00	1,110.00	1,110.00
5	308	898	1,115.00	1,115.00	1,115.00	1,115.00
6	244	1,142	1,120.00	1,120.97	1,133.34	1,141.32
7	308	1,450	1,122.50	1,151.39	1,152.63	1,152.83
8	308	1,758	1,125.00	1,153.01	1,153.76	1,154.00
9	298	2,056	1,130.00	1,154.11	1,155.05	1,155.42
10	96	2,152	1,135.00	1,154.57	1,155.55	1,155.94
11	199	2,351	1,140.00	1,155.62	1,156.60	1,157.02
12	192	2,543	1,145.00	1,156.70	1,157.65	1,158.07
13	148	2,691	1,150.00	1,157.58	1,158.47	1,158.89
14	216	2,907	1,152.50	1,158.90	1,159.70	1,160.09
15	216	3,122	1,155.00	1,160.25	1,160.94	1,161.31
16	140	3,262	1,160.00	1,161.13	1,161.77	1,162.12
17	223	3,485	1,162.50	1,162.55	1,163.10	1,163.42
18	223	3,709	1,165.00	1,163.98	1,164.45	1,164.75
19	269	3,978	1,167.50	1,165.72	1,166.11	1,166.38
20	269	4,246	1,170.00	1,167.47	1,167.80	1,168.04
21	352	4,598	1,171.00	1,169.79	1,170.06	1,170.27
22			1,172.00	1,172.13	1,172.37	1,172.54
23					1,174.71	1,174.85
24				1,176.89	1,177.08	1,177.20
25						
20						
2						1,184.10
2	1					
2					1	

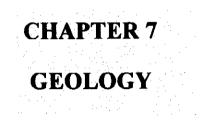
(3/4)

Caluculation Result of Reservoir Sedimental	lion
---	------

No.	Distance	Accumulative Distance	Elevati	on of Rive	bed (m)	
110,	(m)	(m)	Initial Condition	10Year	20Year	30Year
1	0	0	1,095.00	1,095.00	1,095.00	1,152.34
2	176	176	1,100.00	1,100.00	1,100.00	1,153.00
3	143	319	1,105.00	1,105.00	1,138.17	1,153.54
4	271	590	1,110.00	1,110.00	1,152.64	1,154.59
5	308	898	1,115.00	1,115.09	1,153.74	1,156.00
6	244	1,142	1,120.00	1,151.05	1,154.74	1,157.15
7	308	1,450	1,122.50	1,153.04	1,156.18	1,158.59
8	308	1,758	1,125.00	1,154.20	1,157.67	1,160.05
9	298	2,056	1,130.00	1,155.67	1,159.15	1,161.48
10	96	2,152	1,135.00	1,156.18	1,159.63	1,161.94
11	199	2,351	1,140.00	1,157.27	1,160.63	1,162.90
12	192	2,543	1,145.00	1,158.33	1,161.61	1,163.83
13	148	2,691	1,150.00	1,159.17	1,162.37	1,164.55
14	216	2,907	1,152.50	1,160.39	1,163.48	1,165.61
15	216	3,122	1,155.00	1,161.62	1,164.61	1,166.68
16	140	3,262	1,160.00	1,162.43	1,165.35	1,167.38
17	223	3,485	1,162.50	1,163.74	1,166.54	1,168.50
18	223	3,709	1,165.00	1,165.06	1,167.75	1,169.63
19	269	3,978	1,167.50	1,166.68	1,169.22	1,171.00
20	269	4,246	1,170.00	1,168.32	1,170.71	1,172.39
21	352	4,598	1,171.00	1,170.51	1,172.69	1,174.22
22	352	4,950	1,172.00	1,172.75	1,174.70	1,176.07
23	352	5,302	1,173.00	1,175.03	1,176.74	1,177.93
24	352	5,654	1,174.00	1,177.34	1,178.80	1,179.81
25	352	6,006	1,175.00	1,179.69	1,180.88	1,181.71
26	332	6,338	1,177.50	1,181.91	1,182.86	1,183.51
27	332	6,670	1,180.00	1,184.16	1,184.84	1,185.31
28	481	7,151	1,185.00	1,187.44	1,187.74	1,187.95
29	375	7,526	1,190.00	1,190.00	1,190.00	1,190.00





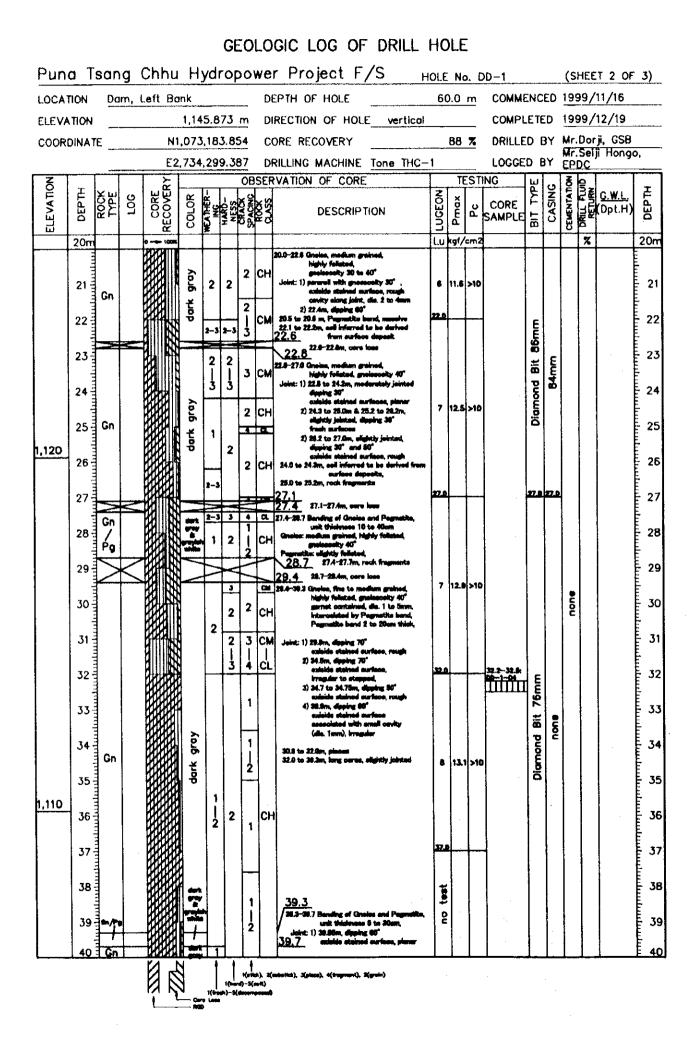


#### GEOLOGY

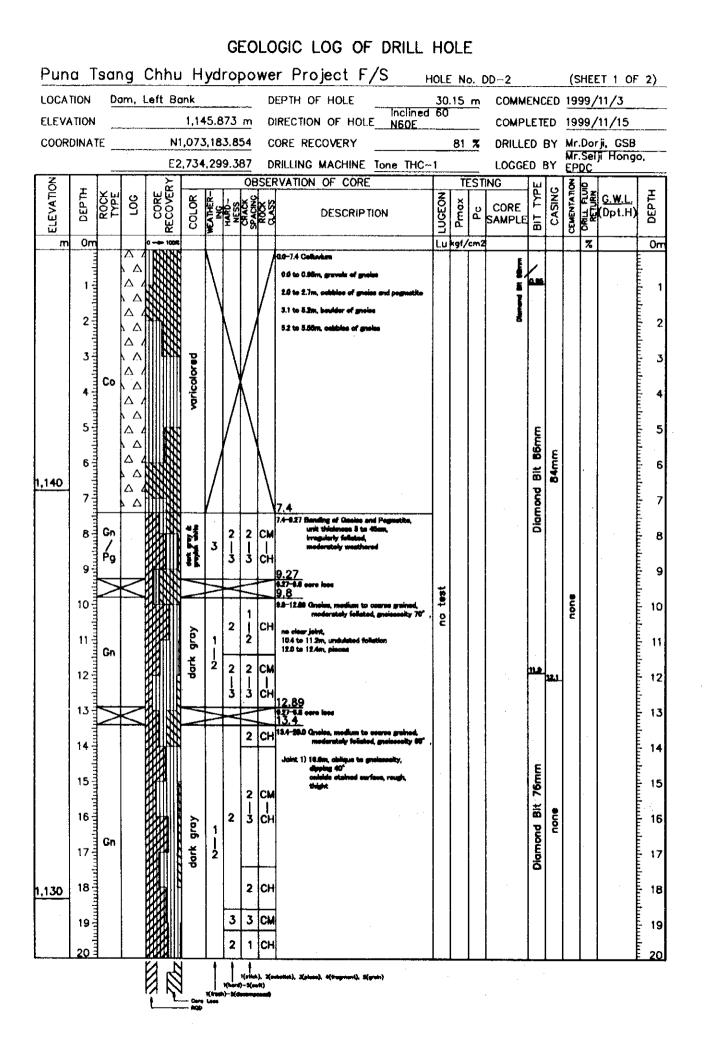
Geologic Logs of Drill Holes Photographs of Cores Result of Permeability Test Geologic Logs of Pits Result of Seismic Prospecting Result of Water Level Measurement in Drill Holes Result of Laboratory Tests Photographs of Rock Core Samples Photographs of Soil Samples Results of Petrographic Examination **Geologic Logs of Drill Holes** 

. .

Pun	a Ĩ	sar	ng l	Chhi	u H	l yc	Iro	po	we	r Project F/S H	01.1	E No	o. [	<u>DD-1</u>			(S	HEE	T 1 OF	3)
LOCAT	TION									EPTH OF HOLE					ENC	εD	19	99/1	1/16	
ELEVA										RECTION OF HOLE vertical							_			
COORI	DINA	TE _								ORE RECOVERY									ji, GSB i Honga	<u>,</u>
Z		<del></del>		<u>د</u> ح	2,73	4,2	99.5			RILLING MACHINE Tone THC	1 T			LOGGE			<u>89</u>			
ELEVATION	DEPTH	ROCK TYPE	LOG	CORE RECOVERY	COLOR	WEATHER-	HARD-	SPACING	NON NON	DESCRIPTION	LUGEON	* .	<u> </u>	CORE SAMPLE	BIT TYPE	CASING	CEMENTATION	DRILL FLUID RETURN	<u>G.W.L.</u> (Dpt.H)	DEPTH
m	Orr			0	-	-	+			0.0-7.0 Column	Lu	kgf/	′cm2					7.		0m
1,140	1 2 3 4 5 5 6 6 7 1	Co			<ul> <li>varicolored</li> </ul>					1.1 to 1.30m, outbles of groins 2.25 to 2.30m, grovels of groins and pagnetite 3.5 to 4.5m, grovels and outbles of groins 5.0 to 7.0m, boulder of groins 5.0 to 7.0m, boulder of groins 7.0 7.4–11.1 Banding of Gavies and Pagnetite,	no test				Diamond Bit 101mm	98mm				1 2 3 4 5 6 7
	8 9 10	Gn / Pg			dark gray & grayish whit	3	3   2	23		unit thicknesse 10 to 30cm Gradest moderatally wasthered, fine to seedlar grained, analyzeolty 30 to 40" Pagmatike: moderatally weathered, course grained, orkystal dis. 8 to 10 mm, massive John: 1) permul with preseebly 30", orields stabled extraor, planar 2) oblique to graisesety 30", oxielde stabled extraor, nough isrecols fillings at 8.2m (I on thick) 2,4-7.8m; highly jointed, asside stained extraore	<1	5.8	×5		7.5	7.6	none			<b>8</b> 9 10
						3	2			11.1–18.2 Grains, fine to modium grained, Highly follated, gnolesselty 30°	12.0									
	12					Ż	3-2	3		Joint: 1) pararoll with grossoulty 30° , coinide stained surface, planer					Ē					12
1,130	13 14 15	Gn			dark gray			2		2) oblique to grainseaty 60°, cristele statuet surface, reagh dissolved surface, reagh (2mm wide) 12.0–12.4m: fragments of reak, exide stained	•	10.9	>10		Diamond Bit 56mm	84mm				13 14 15
	16					2	2	-	СН					16.416.8: 80101						16
	17-										17.0			10.0-10.05x 00-1-02						- 17
	18 19 20	Pg Gn /Pg			H-11		2-3	1		18.2 18.3-18.8 Pagmethe, 18.8-course grained, dia. 10mm or more manades, no joint 18.8-20.0 kreader bending of Groise and Pagmetic, eligibily to medianticly jointed, exists statud earliese	8	11.8		18.5-18.8 19.5-18.8 19-1-53 111111						18 19 20
						e Loos	1(hard h)-0(a	)-3(m	#)	katlat), Xalaan), «(keepmani), S(grain)										



LOCA				Left B		z	····'			EPTH OF HOLE										-
ELEV	TION				1,14	15.8	373	m	0	RECTION OF HOLE vertical			_							
COOR	DINA									ORE RECOVERY		88	7.	ORILLE	50 I	ЗY	Mr.	Dor	ji, GSB	;
					2,734					RILLING MACHINE Tone THC-							L.	Cal	ji Hong	jū
N	<u> </u>			Ъ Х	<b>—</b>	·		OE	SE	RVATION OF CORE			EST		TT	· · · ·		·		T
ELEVATION	HL d 30	ROCK	POL	CORE RECOVERY	COLOR	MCATHER- ING	HARD- NESS	CRACK		DESCRIPTION	LUCEON		Cm2	CORE SAMPLE	BIT TYPE	CASING	CEMENTATION		<u>G.W.L.</u> (Dpt.H)	X
	40/11					+	┢		<u> </u>	30.7-44.2 Gnoice, medium grained,	LU	<b>r</b>								ŧ
	41 -									highly foliated, gnoisecoity 40° gernet contained, dia. isse then firm, Joint: 1) 43.6 to 43.7m, deping 70°,										1111
	*1			1111	<u>ک</u>					autoide stained surface, rough thight,	ļ									
	42	Gn			gray	Ĩ		1		41.4 to 41.5 m. Pegnatike hand, massive 44.3										
					ť	1	2	2	СН	44.2-46.1 Banding of Grootes and Pognatile, unit thisingses 2 to 10cm.										11111
	43									Jaint: 1) 44.8m, 45.1m, 45.8m, 46.7m, dipping 40 to 50°;	test									
										ovioide stained surface, rough to planar	2									
	44		<u> </u>							2) 46.0m, dipping 30° aminide stained surface, planar 2) 48.2m, dipping 70°										
	45	<b>3</b> /7.9				2	2-3	3	CM	45.1 exists stained externs, planar										
1,100					gray	Ι,		1		45.1-47.0 Grains, modern grained, highly failated, grainscolty 40" garnet contained, da. less than irren										TTTTT
	46	Gn			Г	li	2	ļį	Сн		'			 						1.111
					Ч Тор	2		2		gernet die. 2 to 5mm	47.0									
	47	) Gn	Ň			2	3	3-4	См	47,0 47,25 47.0-47,25m, care less 47,25 48.8 Banding of Oneios and Pagnatike,										Lu u
	48 -	1			T					unit thickness 1 to 6cm, 47.25 te 47.0m, pieces,					ļ					11 LA
	- The second secon	Pg								reck surfaces are stained by 48.6 iron caluide					E					
	49							1	ł	48.8–61.5 Queles, fire to medium greined, highly foliated, greinesty 20 to 50°					76mm					THEFT
	-				l ĉ	1	2	1	Сн	a general a weather the second and	5	13.1	>10	50.1~50.8	Bit	2				1111
	50-2	Gn			Ť			<b>~</b>	ĺ	counter stained surface, rough, 48.5 to 38.5 m, Garnet Gnoise,		[			Ð	anon	Buou		51.0	E
	51 -				τ					garnet da. 2 to Smar					Diamon				12/15 V	
						Ļ	Ļ	<b> </b>		51.5 31.3-322 Banding of Grouiss and Pagnetike,					ð				-	1121
	52	an/Pa				2	3	3-4	CM	52.2 unit thickness 2 to Gam, 52.2 \$1.8 to 52.1m, pieces 52.2 55.2 Grains, firm to medium grained,	62.0	-			ĺ			ĺ '		
						1				SC2 - So.2 Growin, we to monitor growing, highly foliated, growinscolty 20" gernet certained, die less than Jour										1111
	53-		x		gray	I				Juint 1) 52.4m, along grainsonity, dipping 40° cuintin statued exception, planar,										
	54 -	Gn			dark	1				2) 84.1m, story graincostly, dipping 90" evides statued surface, planar,		ł								LTTT:
					ĕ			1		3) 57.7m, skiligue to grainscolty, dipping 40° fresh surface, planar,	5	15.1	10.1							TTTT
	55		<u> </u>				2	12	Сн	55.2 53.3 to 53.5 m, Pagmatha, massive 55.2-55.8 Bending of Onoires and										1111
1,090		in/Py				1		1		Pagmethe,					1					11111
	56				gray		ĺ			56.6-57.9 Groins, firm to median grained,										1111
	57-	Gn			11	1				highly foliated, geolescolty 20° gerret, certained, dis. loss then 2mm	<b>57.</b> 0	ļ								11111
			1		1 ab		}			57.9								1		
	58		<b>—</b> —	HHH	-	╞╾		-	╞╼═	57.8-08.8 Banding of Gnoice and Pognetike,										
		Gn			#					unit thisimes 2 to 30am, Causias, high fallated, graiseweity 80° Pagmatica, slightly fallated		15.1	10.1							
	59-	Pg				<b>1</b>	2	2	CH	57.8 to SB.Am, pieces, rock surfaces are stained by									}	
	60	L	<u> </u>		1		L	Ļ		iron calaida	-						L.	<u> </u>		Ē



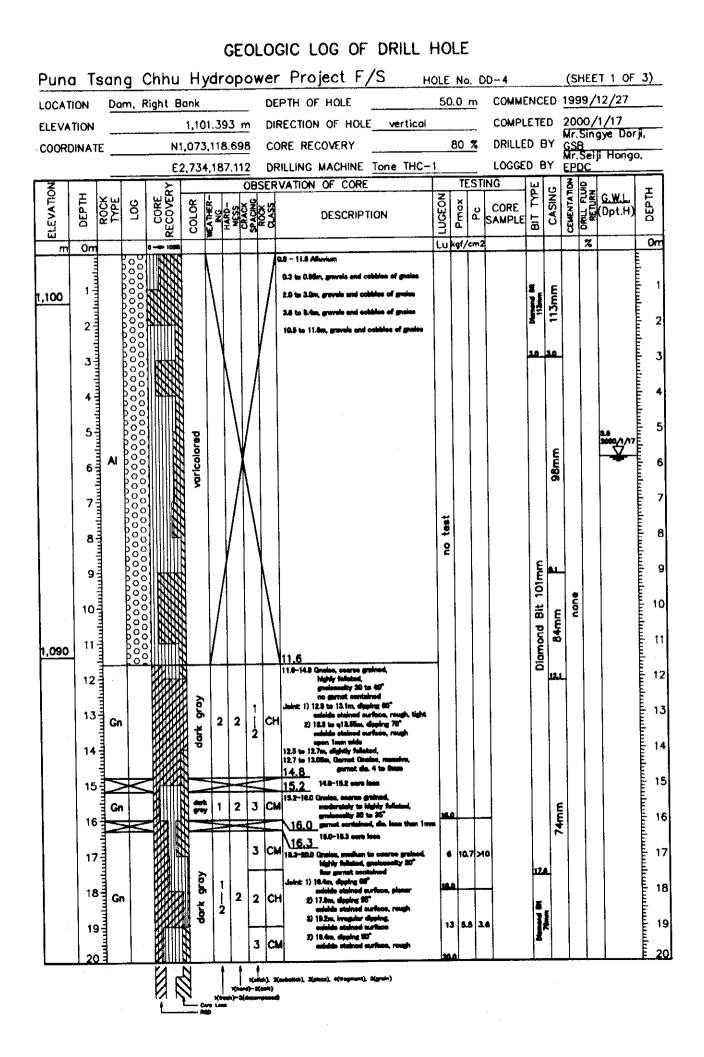
								GE	0	LO	GIC LOG OF DRILL	HC	LE	•							
Pun	a T	san	g	Chł	۱u	H	ydı	op	0	ve	r Project F/S +	IOLE	No	). D	D-2			(Sł	IEE	T 2 OF	2)
LOCAT	ION					nk					PTH OF HOLE	-60			COMME						
ELEVA											RECTION OF HOLE NODE										<b></b>
COOR	DINAT	E																		ji, USB i Hongo	<u>э,</u>
z			<u>.</u>			,734	,29	9.30			RILLING MACHINE Tone THC-				LOGGE NG					<u> </u>	
ELEVATION	DEPTH	S S S S S S S S S S S S S S S S S S S	90J	CORE	KECUVER	COLOR	WEATHER-	HARD- NESS	CRACK	ROCK Q.ASS	DESCRIP TION		Pmox	Рс	CORE SAMPLE	BIT TYP	CASING	CEMENTATION	DRILL FLU RETURN	<u>G.W.L.</u> (Dpt.H)	DEPTH
	20m			0-++- 11111						_	20.0-24.8 Gasies, mailium to course gained,	Lu	kgf/	cm2					7		20m
	21										moderately foliated, generately 80° Joint: 1) 23.85m, dyping 30°,										21
	22					gray	1				existe stained exclose, planer, tight 2) 24.80m, elong gnobecosty.										22
	23	Gn				dark g	2		1		depleg 67 colaida atalead surface, planar 24.9.										23
	24							2		сн	24.9-25.7 Pagnacha, massiva, coarse grained, crystal dis. 10 to 20mm Joint: 1) 24.95m, 2 esta, disping 40°					76mm					24
	25	Pg					1		1		exiside stained surfees, planar tight 2) 25.1m, kragalor exiside stained surfees, reagh					Diamond Bit	anon	9uoc			25
	26	1			H				12		28.7–27.0 Banding of Gnoles and Pogmetite, unit thisleness 1 to 10em, Gnoles, course grained,					Ŭ.					26
	27-	Ýg				and an	2		1		algithy to moderately foliated, 27.0 27.0-61.15 Onelia, median grahed, highly foliated, genimeraty 50°										27 1
	28				11	gray	-	-	Ŀ		Joint: 1) along groovenity 80°, eminide stained surface, planar, tight										28
	29	Gn				dark g	2	2   3	2   3	СМ	28.1 to 28.7 m, slighty worth-red										29
	30			R			ī	ī	2	СН			ļ								Ę 30
											30.15m, bottom of hole										متفقات فالمتعادين أعتقنا بمعادين أعيين انتقدا ويتبالون فاستداد يتبعا ويساعين والتتع إيرينا تعتدا ويتبع
					711-	2777 88	×.		-0-10	n), 2( 1041) waand	unistich), Kalana), 4(begmani), 5(grain)										

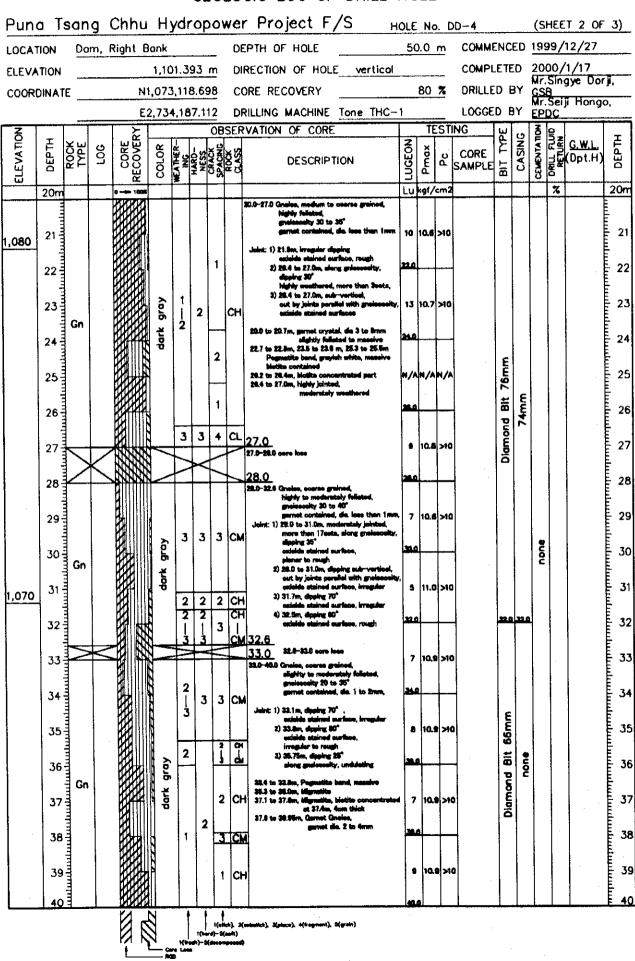
.

										GIC LOG OF DRILL										
Pun	a T	sar	ŋg	Chhu	I H	yd	roj	po	we	r Project F/S	HOL	EN	<u>o. [</u>	D-3			(S	HEE	T 1 OF	3>
										EPTH OF HOLE										···
ELEVA										IRECTION OF HOLE vertice										
COORI	JINAI	£	· · ·	N	11,07 2 7 3/	3,15 1 25	8.9 6 5	<u> </u>	С 0	ORE RECOVERY		33	<u>%</u>	DRILLE	D E	3Y 	Mr. Mr.	Dor Sel	ji, GSB ji Hong	o,
E				<u>با</u>	2,70	1,23	0.0	OB		RVATION OF CORE		Т	EST	NG	ы Ш					
ELEVATION	DEPTH	ROCK	ГОC	CORE RECOVERY	COLOR	HER-	កំន	X	×8		LUGEON	ŏ	U	NG CORE SAMPLE	٤	CASING	CEMENTATION	L FLUI	<u>G.W.L</u> . (Dpt.H)	DEPTH
	õ	<b>α</b> ⊢		REC C	ខ្លី	WEATHER- ING	Ϋ́́	28 8	83 8	DESCRIP TION	L C C	E	٩	SAMPLE	ΒI	Ş	CEME		τορι.π)	В
m	<u>0m</u>		2020							0.0-20.0 Abeára	Lu	kgf/	/cm2					7		Om
1,100	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Ai			varicolored					0.0 to 2.45m, gravels and oddblas of grains and pagnetits 2.45 to 3.8m, builder of grains 8.7 to 8.2m and 8.30 to 7.3m, builder of augun-yoks 7.3 to 7.8m, gravels of grains 7.4 to 8.8m, builder of grains 8.8 to 10.5m, gravels and oddblas of grains 10.8 to 10.5m, gravels and oddblas of grains 10.8 to 20.5m, gravels and oddblas of grains 10.8 to 20.5m, gravels and oddblas of grains					Diamond Bit 76mm 🐹 Diamond Bit 86mm 🗱 Diamond Bit 86mm	84mm E	enor	no woter return		$\begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ \end{array}$
	20																			20
					1			1	). X=	detict), 3(place), 4(trapment), 5(grain)										
					] 000	1(\$raah) Loos	(hard) )-3(di													

Pune	a T	san	.g (	Chhu	H	<b>/d</b> r	ор	ov	vei	r Project F/S на	DLE	Na	. DI	D-3			(Sh	IEE	T 2 OF	3)
LOCAT	ION	Da	m, L	eft Bo	nk			_	DE	EPTH OF HOLE	60	0.0	m	COMME	NCE	D	200	0/	1/14	
ELEVA		<b>.</b>			1,10	6.60	)2	m	DI	RECTION OF HOLE vertical				COMPL	ETE	D	200	0/:	2/12	<del>,</del>
COORI	DINAT	ε		N	1,07.	5,15	8.9	<u>71</u>	CC	ORE RECOVERY	·	33	7	DRILLE	DB	Y	Mr.( Mr.S	)or Selj	i, GSB Honga	<u> </u>
				E2	,734	,256	5.50	9	Df	RILLING MACHINE Tone THC-	1	тс	STI			Y T	EPD	C		
ELEVATION	DEPTH	ROCK TYPE	10C	CORE RECOVERY	COLOR	WEATHER-	NESS	SPACING OF	SER SSVD	DESCRIPTION	LUGEON	Pmax	Pc	NG CORE SAMPLE	BIT TYPE	CASING			<u>G.W.L.</u> (Dpt.H)	DEPTH
	20m		 2 _ 0	0							Lu	kgf/	cm2			_		7		20m
1,080	21 22 23 24 25 26 27 28 29 30 31 32 33 31 32 33 34 35 36				varicolored					20.0-438 Alkolan 20.0 to 22.0m, gravels and colletes of grains, pagentito and grains, pagentito and metasodimentary reduc	no test		cm2		Diamond Bit 76mm	74mm	evor	no water return		21 21 22 23 24 25 27 28 29 29 20 27 28 29 29 20 27 28 29 29 20 27 28 29 29 20 27 28 29 29 29 29 20 27 28 29 29 29 29 20 27 28 29 29 29 20 27 28 29 29 29 20 27 28 29 29 20 27 28 29 29 20 27 28 29 29 20 27 28 29 29 20 27 28 29 20 27 28 29 20 27 28 29 20 27 28 29 20 27 28 29 20 27 28 29 20 27 28 29 20 27 28 29 20 27 28 29 20 27 28 29 20 27 28 29 20 27 28 29 20 27 28 20 27 27 28 20 27 27 27 28 20 27 27 27 27 28 20 27 27 27 27 27 27 27 27 27 27 27 27 27
	39 40	utintain															None K			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
						×***		1(ell 1(ell (decent		(adabis), Ljohan), 4(tragmant), 3(grain) *										

								Gl	EO	LC	DGIC LOG OF DRILL	HC	LE	•							
oun	a T	sar	ig I	Chl	hu	H	yd	roj	00	we	er Project F/S H	OLE	No	<u>). (</u>	D-3			(Sł	HEE	T 3 OF	3)
.0CA1											DEPTH OF HOLE										
											DIRECTION OF HOLE vertical										
200 <b>R</b> [	DINAT	Έ			N1	,07.	3,15	58.9	71	(	CORE RECOVERY DRILLING MACHINE Tone THC- RVATION OF CORE		33	%	DRILLE	DE	3Y	Mr. Mr.	Dor Sei	ji, GSB ji Hongo	
					E2.	734	,25	6.5	09	0 700	DRILLING MACHINE Tone THC-	1	тс	<u>ет</u>		D E	9Y 	<u>EP</u> [	<u>)</u> 		
ELEVATION	DEPTH	ROCK TYPE	гос	CORE	ECOVERI	COLOR	KATHER-	HARD- NESS	CKACK BACK		DESCRIPTION	UCEON	Pmax	Ъс Ъс	ING CORE SAMPLE	BIT TYPE	CASING	CEMENTATION	DRILL FLUID RETURN	<u>G.W.L.</u> (Dpt.H)	DEPTH
- <u></u>	40m			ا ح <b>ب</b> ہ	108K	<u> </u>	*					Lu	kg1/1	cm2					7.		40m
	41		00000								40.0-40.0 Alkrium 40.0 to 44.25m, gravels of grains and pagnetics										41
	42										44.25 to 48.0m, bouider of groke 46.9 to 53.0m, gravala, adablas and bouiders of grains						ε				42
	43										53.5 to 60.8m, gravels and cobbles of groise and pogmetite						74mm	none			43
	44																				43 - 44
	45		00000													E	45.0	45.0			45
060	46		00000													Bit 76mm					46 47 48 49 50
	47				i i i i i i i i i i i i i i i i i i i				$\ $							Diamond B					47
	48															Dìa		Ð	E		- 48
	49 50-	AI				varicolored			Y			test						cemented	ir return		49 - 50
	51		00000			varice						ę							no water		
	52		0000												1						52
	53-				7777												BLOL				53
·	54 ·			N												517		53.7			54
	55															E					55
,050	56	111111	00000	Ň.												it 66mm					56
	57	لللتعالية	00000	Ž												Diamond Bit		Non			57
	58	Ittilli														Dian		ľ			51 52 53 54 55 55 56 57 58 59 60
	59 60	rhistore																			59 60
	60	·	ዋፊ		777- (B				ni)-3	(neil)	Harbatta), Xaiza), 4(tragment), 5(grain)	_			<u> </u>						60

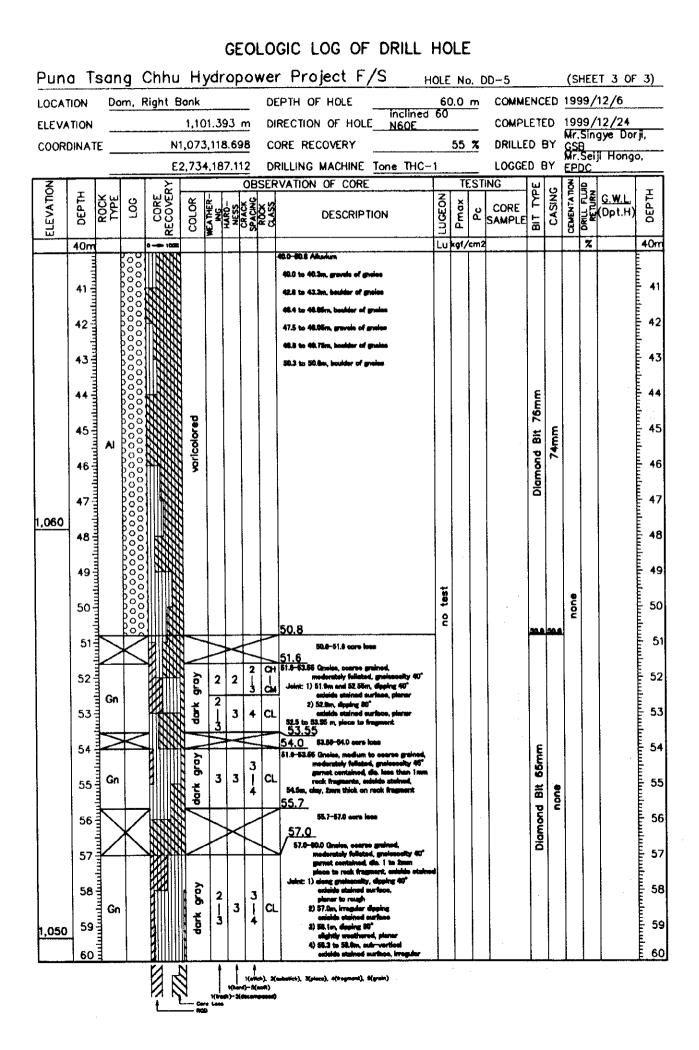




LOCA ELEV/ COOR			<u> </u>	•	1,1 11,07	01.3 3,11	93 8.6	m 98	D C	EPTH OF HOLE IRECTION OF HOLE vertical ORE RECOVERY	ļ 	80		COMPL	LE TE	ED 9Y	20 Mr. GS	00/ Sin	1/17	
					<b></b>	4,10	\$7.1	12	U	RILLING MACHINE Tone THC	-1			LOGGE		3Y	<u>EP</u>	DC		
ELEVATION	_	ROCK TYPE	LOG	CORE RECOVERY		WEATHER-	HARD-	CRACK	A00X	DESCRIPTION		Pmax	Рс	CORE SAMPLE	BIT TYPE	CASING	CEMENTATION		<u>G.W.L.</u> (Dpt.H)	+
	40m					-		+-	-	40.0-40.0 Groins, medium gruined,	Lu	kg1/	/cm2	<u> </u>				7		F
. <u>.060</u>	41					1.	2	1	сн сн	grainseaty 40 to 30° garret contained, die. 1 to Bren Juint: 1) 40.0m and 40.0m, deping 55° activite stained author, planar	7		>10							وإمتيها لتعمل متعامين المتعام معامير والمتعام مناهمة فمتعام ماليتهما متعما متعاميت المتعام متعام تعاليتهما
	42						3		СМ	2) 41.2m, dipping 60° slightly weathered, planar 2) 42.85m and 44.8m, dipping 80°	42.0	╞								1 1 1 1 1
	43		:		Γ Λ					esticide stained surface, planar 4) 44.7m, deng griessoulty, disping 45° esticide stained surface, planar to reagh	8		<b>30</b>		66mm					يدينا يتعايينها
	44	Gn			gray	1		1	ļ	<ul> <li>B) 44.7 to 44.3m, auto-vertical addide stained surface, rough</li> <li>6) 48.5 to 46.3m, slong grainwalty,</li> </ul>			.							Length
	45			88	dark	12	2	İ	сн	Seets, slipping 40° axialdo staland excluse, rough	8	10.9	>10		Diamond Bit	none	none			in the
						2		2		Crack 1) 41.5 to 41.8m, sub-vertical, oxisite stained, irregular	-	ļ			No.	•				<u>chu</u>
	46				8					42.5 to 42.6 m, pieces 42.6 to 43.1m, Pagenatita,					<u>o</u>					استط
	47								ļ	biotite concentrated part is observed	3	10.9	э٩							سلس
:							3	i		46.4 to 48.3m, Pagmatite band biotite concentrated part is observed, 5 to 10cm thick	-									L L L L
1	48					2	2	i	СН	47.4 to 48.0m, pieces 48.7 to 48.0m, pieces to short pores										line:
ł	49	1		<b>1</b> 4.			3	3	СМ	49.0 48.0-49.5 cere ices	5	10.9	>10							ոսի
		G				2	2-3	2-3		48.0-46.5 cere loss 49.5 48.5-50.0 Grates, course grained,	50.0									iii)
										50.0m, bottom of hole										ومقلعه فالمعمل ومعالمه والمعالم ومالموه المروم لمرموا ومقارر ومالمور المروا ومعالم والمعدا ومروا ومعارمه
								)—3(m	M)	botich), X(elaca), 4(tregment), Merrin)										under

Pun	a T	sar	ng (	Chhu	Н	ydı	ro	ро	we	er Project F/S н	IOLE	No	o. C	D-5			(S	HEE	T 1 OF	3)
LOCA				Right E						DEPTH OF HOLE	6	0.0		COMMI						
ELEVA	TION				1,1	01.3	93	m	D	DIRECTION OF HOLE NOOE				COMPL	ETE	D	19	99/	12/24 gye Dor	
COORI		Έ		N	1,07	3,11	8.6	98	¢	CORE RECOVERY		55	7	DRILLE	D F	ΞY	Mr. GS	Sing B	gye Dor	j.
		<u> </u>		3	2,73	4,18	37.1	12	D	RILLING MACHINE Tone THC-	1			LOOOL	DE	ΞY	Mr. EP	Sei DC	i Hongo	o, 
N	r	хш		ERΥ		<u>п</u>	1	ÓĒ	ISEF	RVATION OF CORE	Z	F	ST	NG	ΡE	<u>9</u>	Nor	o Žz	0.441	Ţ
ELEVATION	DEPTH	R S C K R C K	LOG	CORE RECOVERY	COLOR	MEA THER	- S	CRACK	¥%	DESCRIPTION	LUGEON	Pmax	Pc	CORE	BIT TYPE	CASING	CEMENTATION	E D	<u>G.W.L.</u> (Dpt.H)	DEPTH
				RE	8	8	I "	09	<sup>∞</sup> 0	×		a. kg1/			B		8			0m
	Om		600							0.0 - 50.8 Alierium	Lu	KGI/	Cm2					7		Um
	1									0.0 to 12.0m, gravele of grains and pegmetite gravel dia. 3 to 30cm										1
1,100	1									12.0 to 13.0m, bouider of grains										
	2									14.5 to 18.0m, boulder of grains										2
	1								$\ $	17.2 to 18.5m, boulder of groles						Ę				
	3															113mm				3
	4																			- 4
	5-																			5
	6						N								101mm	4.1				6
	7														Bit					7
															Diamond					
	8														<u>D</u>					8
	9			ЩВ												98mm				9
	1.1.1				Pero			Y			test					80				1     2     3     4     5     6     7     8     9     10
	10	AI			varicolored			I			no te						e uou			10
	11				Ìġ			A			2									11
	11 -				1															
	12		0000000				11				1					12.1				12
	12																			
1,090	13-		500	5																13
	13 14		600					1				l			13.6					14
			200				1		N											
	15-			11118																15
	15- 16-								l.						Ê	Ę				16
	16		5°ŏ												Bit 86mm	B4mm				16
	17		200												H BH					17
	17 18												1		Diamond					
	18		680								1				Dian					18
	19-		200																	19
1			500					1												
L	20	1	000		N N	1	1		1		<u> </u>	1	L	<u> </u>	L		L	L		20
				88			 1(he 1	H(uffs (4) 2() (decom	unit)	(aubatick), 3(piace), 4(fragment), 3(grain) . A										
					Cer RG	e Lini )				•										

#### Puna Tsang Chhu Hydropower Project F/S HOLE No. DD-5 (SHEET 2 OF 3) COMMENCED 1999/12/6 Dam, Right Bank DEPTH OF HOLE 60.0 m LOCATION inclined 60 COMPLETED 1999/12/24 1,101.393 m DIRECTION OF HOLE ELEVATION N60E Mr.Singye Dorji, DRILLED BY N1,073,118.698 CORE RECOVERY 55 % GSB Mr.Selji Hongo, COORDINATE LOGGED BY E2,734,187,112 DRILLING MACHINE Tone THC-1 EPDC OBSERVATION OF CORE TESTING 이지 <u>G.W.L</u>. 기대(Dpt.H) CEMENTATION CORE RECOVERY BIT TYPE CASING ELEVATION DEPTH DEPTH LUGEON Pmox ROCK g COLOR RATHER-HARD-NESS CRACK SPACING ROCX CORE 5 DESCRIPTION SAMPLE 20m 7 Lukgt/cm2 20m 20.0-40.0 Allunia 20.0 to 23.5m, bouid 21 21 🗄 22 22 23 23 24 24 1,080 25 25 26 26 -27 27 Bit B6mm 84mm 28 28 -29 29 Dlamond varicolored test Pone 1111111 30 30 AI 2 31 31 = 32 32 🗄 33 33 34 34 ومقتقيه والانتقالية والمستركم المسترك والمستركية 35 35 36 1,070 36 37 37 74mm 38 38 Mark H 39 39 Ì alich), Mainm), 4(Page a) 20 ni), S(grain) **3(**m



Puna Tsang Chhu Hydropower Project F/S HOLE NO. DD-6 (SHEET 1 OF 4)														· 4)											
LOCATION Dom, Right Bank																			NCED 2000/1/24						
ELEVATION 1,129.499 m							DIRECTION OF HOLE vertical					icol	COMP			LET	ED	2000/2/25							
COORDINATEN1,073,037.539									С	CORE RECOVERY					65 % DRILLED				BY	Mr.Singye Dorji, Y GSB					
<b>ب</b>	<u></u>				2,73	4,20	)4.4			DRILLING MACHINE Tone THC-1 SERVATION OF CORE										8Y	LFUC				
ELEVATION	Ŧ	¥ω	0	CORE RECOVERY	~	L	<u>r.                                    </u>		ISE	RVA1	TION	OFC	ORE		-+	z		EST		μ	ÿ	NOL	Ng	<u>G.W.L</u> . (Dpt.H)	Ξ
EVA	DEPTH	R S C K C K	ю Со	50	COLOR	EA THER-	NESS NESS	ACK ACK	ROCK		(	DESC	RIPTIC	ON		LUGEON	Ртох	Po	CORE	11-18	CASING	CEMENTATION	RETUR	(Dpt.H)	DEPTH
ᆸ	Orn		<b> </b>	4		2	II -	08		1				·		<u> </u>		cm2				8	50 76		
						$\mathbf{t}$	┢─	┼──		0.0-11	LS Cellu	vium					ngi/				┢──		*		0m
	1					1				1.0 1	e 1. <b>16</b> m,	grudes	and cobi	tion of grain	•	ĺ				11Jmm		1	1		
						1				1.85	to 3.360	n, gravak grada	t, cubbiy H	n and baside	ers of	ĺ				Bit 11		1	ļ		
	_			840		$\left( \right)$			$\left\{ \right\}$	5.0 1	o 8.0m, 1	benådar (	rf gnaine		.						ĺ	[			2
						$\left( \right)$		-		1				ties of grain	• (					Shoe	1	[			
	3									1.01	BITCOM,	gravida Umulan	and pag	provides						Cosing					- 3
1,120	2 3 4 5 6 7 8 8 8		⊾∆							1		• • • • • •	r of grai		.					40					4
										1	11.4 to 12.55m, gravels and cabbles -14.0 to 16.65m, gravels and cabbles														
										1		n, graval	and sol	ibles of											5
							Į.			1		ia and pa	and pegrantite							Ē					
	6 7								{									113mm				6			
				1111					ł	1												7			
								1	}								:								
	8						$\left  \right $			1										I	}				1 1 2 3 4 5 6 7 8 9 10 11 11
	9								ł										:		ł		ε		9
					3			V		1						-			:	F			return		
	10-	Co	Δ		varicolored		{	I								o test			1	101mm		none	water		10
					ğ		1	N	1							2			1						
	11							1	l											d Bit			2	ł	-
	12						11												:	Diamond	12.1				12
																				å					
	13-						11								1				ł	i					13
	14											1				ļ									
							I																14		
	15								ļ												98mm				15
							ļ	Į	Ņ												98				
	16																				ļ				16
	17																								17
																			:						· '
	18																ļ			161	18.1				18
			Δ					}												20 20 20	Ē				
1,110	19					V														Diamond Bill Diamond Bill	84mm				19
L	20				<u> </u>	Ļ	Ļ	Ļ												ă	Ŀ				20
				06		ł		+{e#e 1} 1}-11(se		nentict ),	Kpinzi),	-	mi), sign	<b>h)</b>											
					۷ 	9(944 1 Long	k)-8(4																		

