社会開発調查部報告書 C.3

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JAPAN INTERNATIONAL COOPERATION AGENCY (JICA)

MINISTRY OF SETTLEMENT AND REGIONAL DEVELOPMENT THE REPUBLIC OF INDONESIA

## THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

## **FINAL REPORT**

COMIPONIENTI' C: URBANI DRAINIAGE SYSTIEM IMPROVEMENT

VOLUME

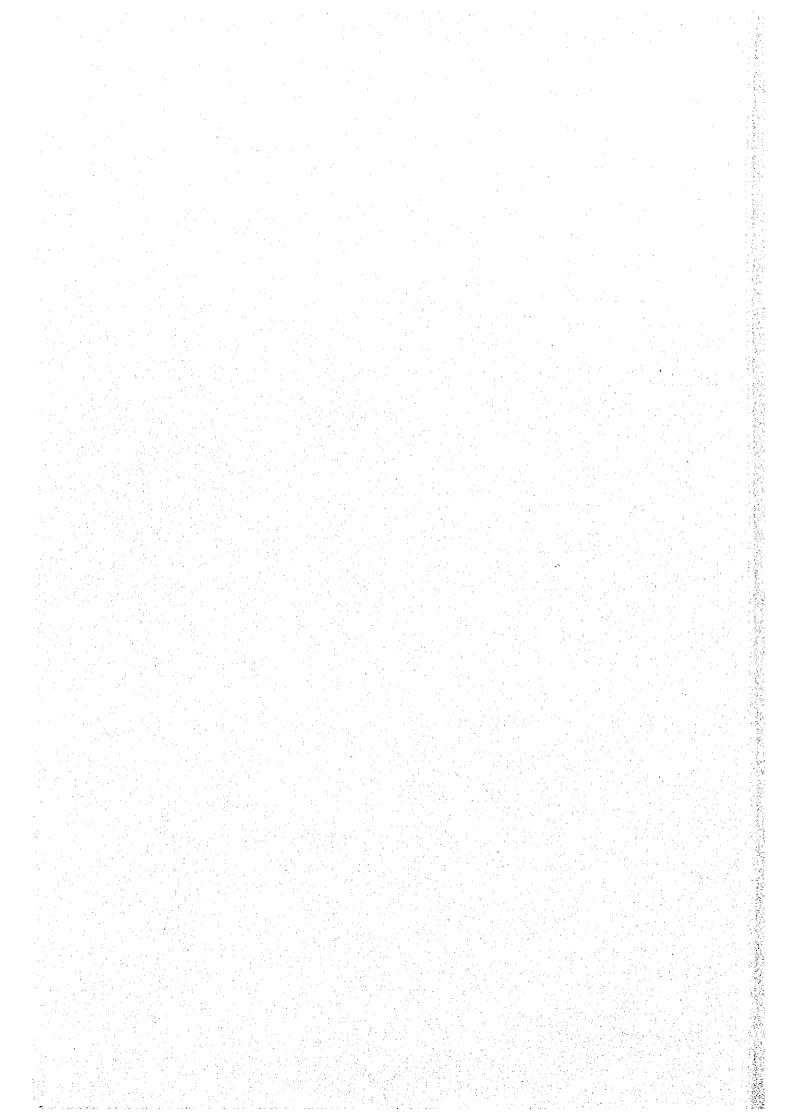
WORK QUANTITY CALCULATION



CTI ENGINEERING INTERNATIONAL CO., LTD. IN ASSOCIATION WITH PACIFIC CONSULTANTS INTERNATIONAL

> AND PASCO INTERNATIONAL INC.

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#### JAPAN INTERNATIONAL COOPERATION AGENCY (JICA)

### MINISTRY OF SETTLEMENT AND REGIONAL DEVELOPMENT THE REPUBLIC OF INDONESIA

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## THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

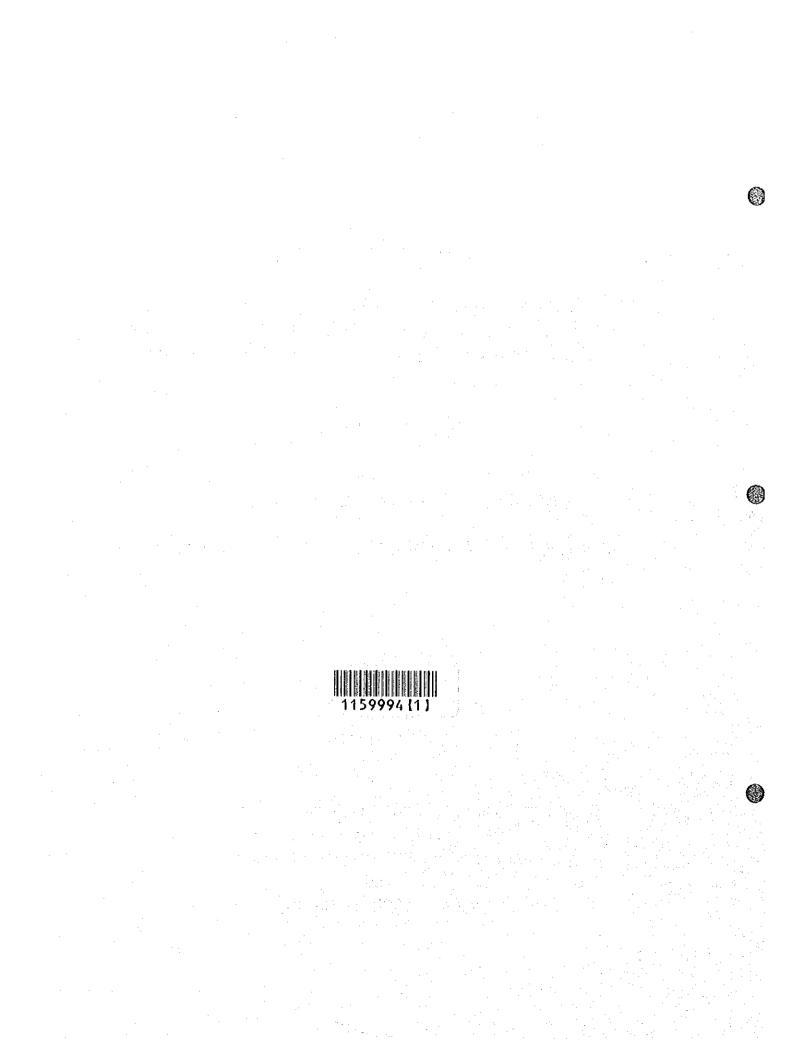
## **FINAL REPORT**

### COMPONENT C: URBAN DRAINAGE SYSTEM IMPROVEMENT

## VOLUME III WORK QUANTITY CALCULATION

AUGUST 2000

CTI ENGINEERING INTERNATIONAL CO., LTD. IN ASSOCIATION WITH PACIFIC CONSULTANTS INTERNATIONAL AND PASCO INTERNATIONAL INC.



#### **CONSTITUTION OF THE REPORT**

1. SUMMARY

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#### 2. COMPONENT A : WEST FLOODWAY/GARANG RIVER IMPROVEMENT

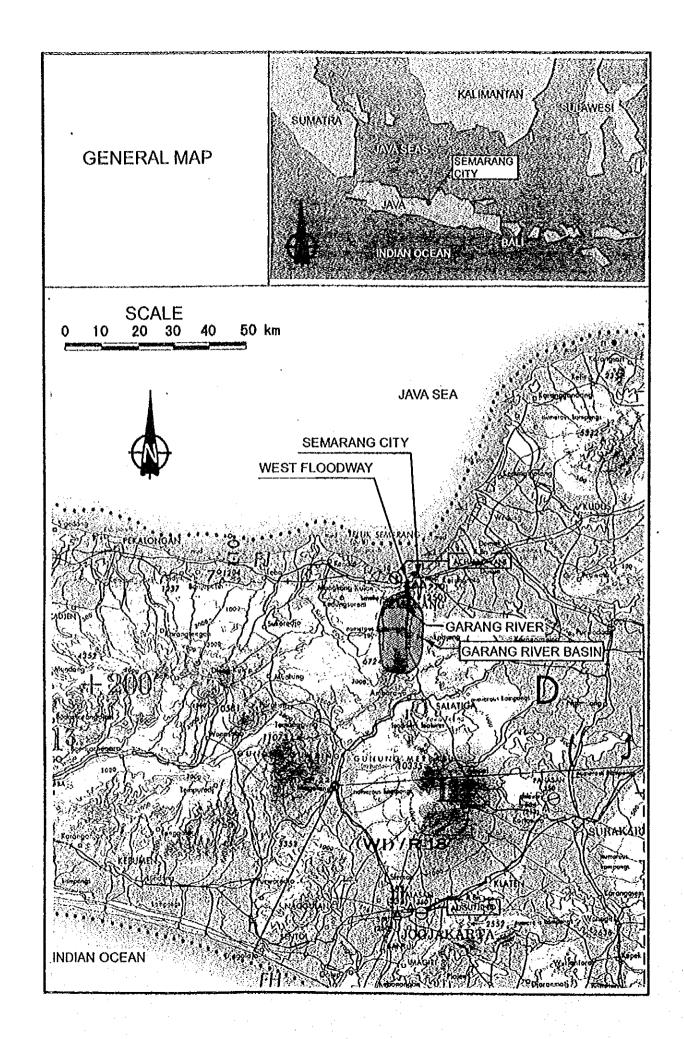
VOLUME IMAIN REPORTVOLUME IIDESIGN CRITERIAVOLUME IIIDESIGN NOTESVOLUME IVWORK QUANTITY CALCULATIONVOLUME VCONSTRUCTION PLANNINGVOLUME VICOST ESTIMATEVOLUME VIIDATA BOOK

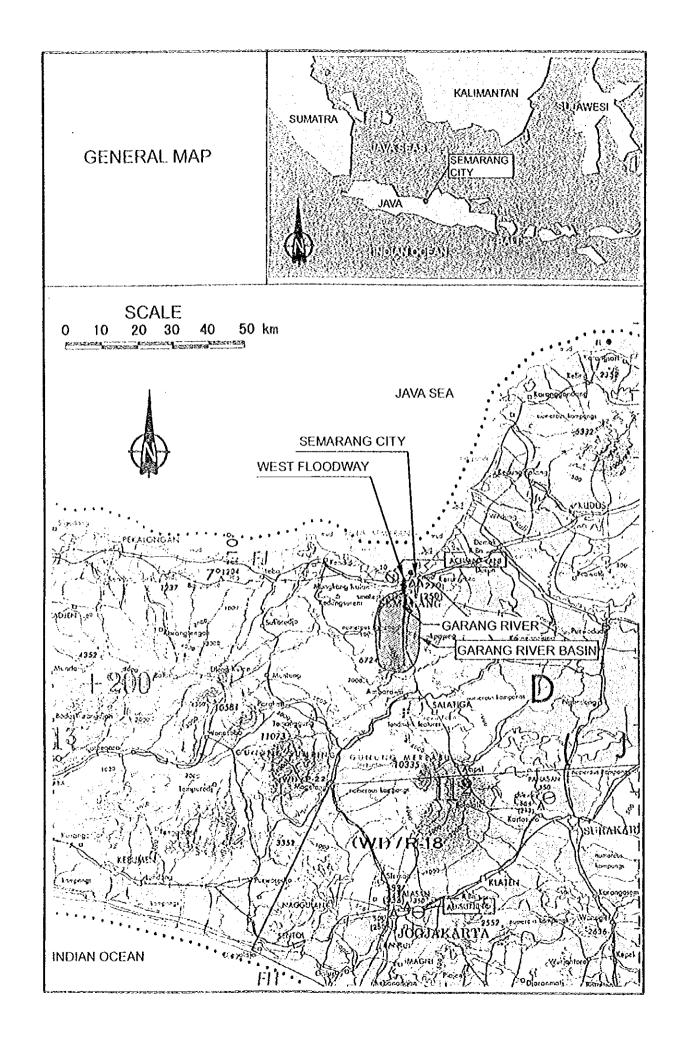
#### 3. COMPONENT B : JATIBARANG MULTIPURPOSE DAM CONSTRUCTION

<b>VOLUME I</b>	MAIN REPORT
<b>VOLUME II</b>	DESIGN CRITERIA
<b>VOLUME III</b>	DESIGN NOTES
<b>VOLUME IV</b>	WORK QUANTITY CALCULATION
VOLUME V	CONSTRUCTION PLANNING
VOLUME VI	COST ESTIMATE
VOLUME VII	DATA BOOK
VOLUME VIII	ANNEX

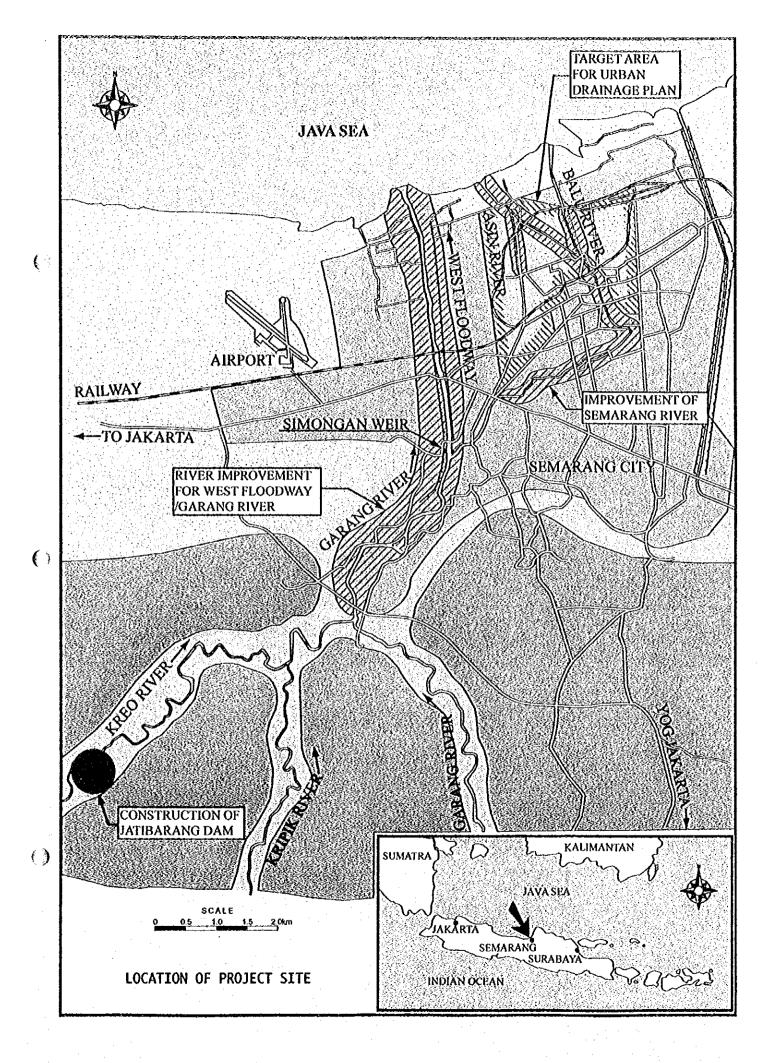
#### 4. COMPONENT C : URBAN DRAINAGE SYSTEM IMPROVEMENT

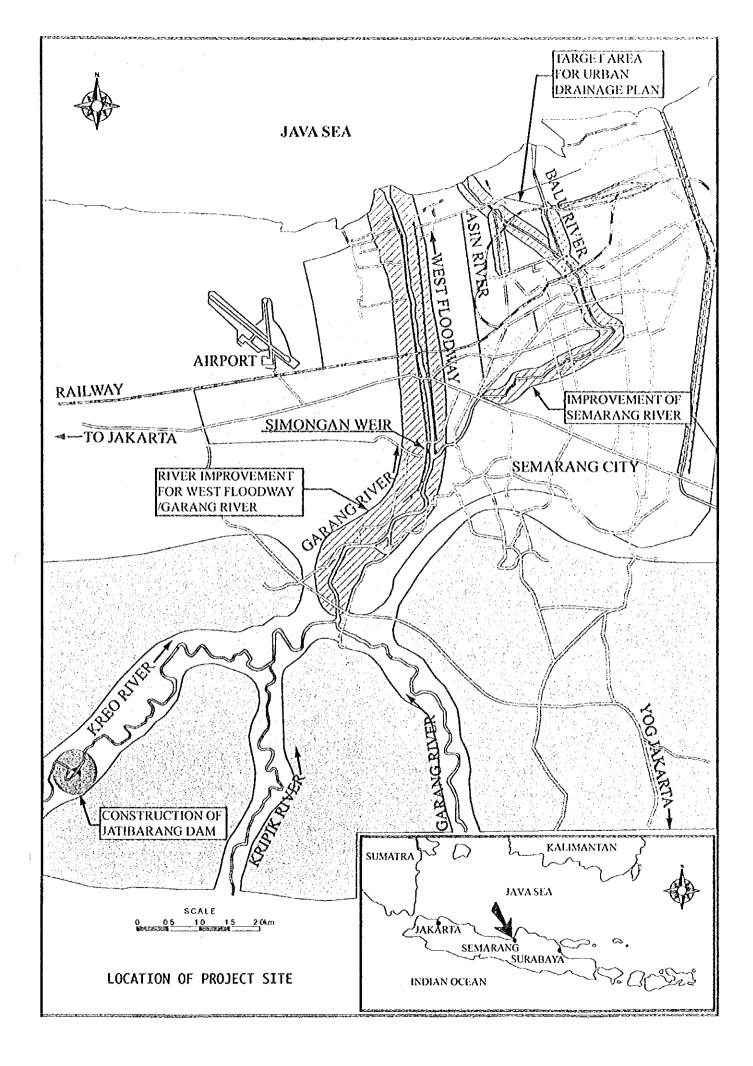
VOLUMEI	MAIN REPORT
VOLUME II	DESIGN NOTES
VOLUME III	WORK QUANTITY CALCULATION
<b>VOLUME IV</b>	CONSTRUCTION PLANNING
VOLUME V	COST ESTIMATE
VOLUME VI	<b>DATA BOOK</b>

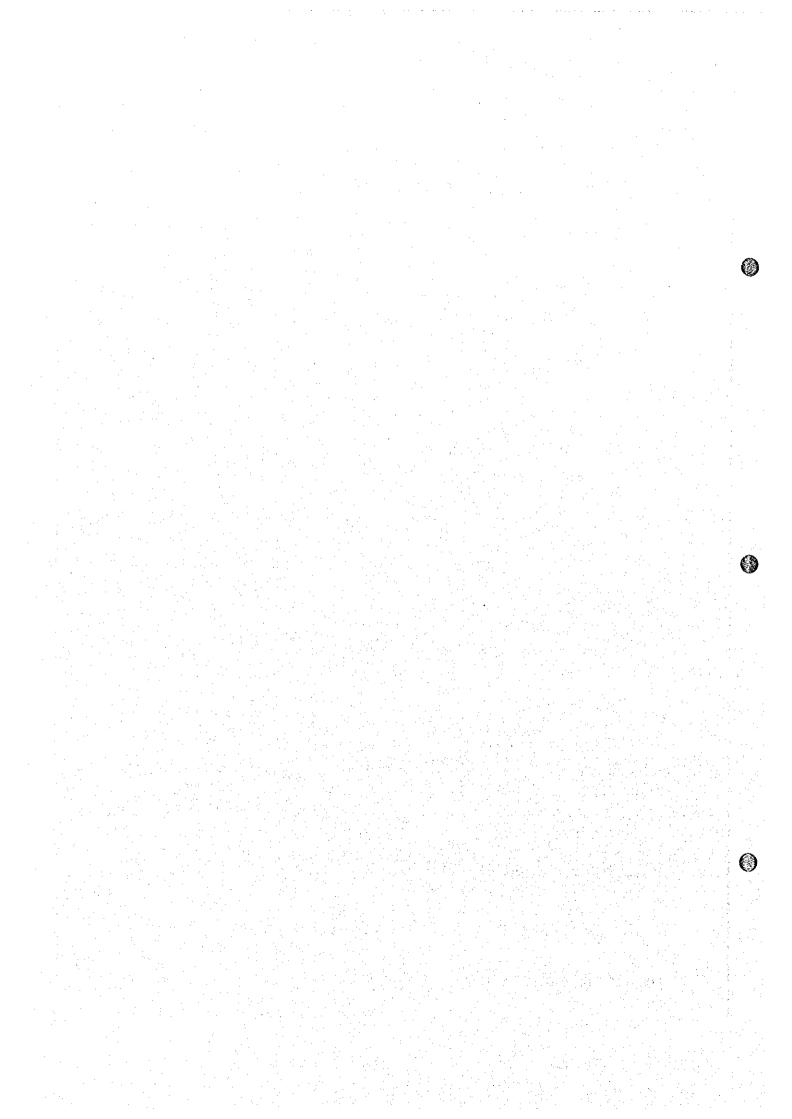




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## VOLUME III WORK QUANTITY CALCULATION

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PACKAGE 1 SEMARANG RIVER DRAINAGE SYSTEM IMPROVEMENT

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Package 1: A General

Compone	IN SEMARANG ent: Urban Drainage System Improvement	nt	1	——————————————————————————————————————	
Package 1:	Semarang River Drainage System Improvement	1		ł,	- <del>-  </del>
	BILL OF QUANTITIES				
ltem No.	Description	Unit	Quantity		
			Guantity		
A Ā.1	GENERAL	ļ			
	Mobilization and Demobilization	L.S.		. <u> </u>	
A.2	Establishment				
A.2.1	Temporary Construction Road	L.S.			1
A.2.2 A.2.3	Contractor's Site Office and Facilities	L.S.			
A.2.3 A.3	Engineer's Site Office and Facilities	L.S.	! 		
A.3 A.4	Drawings Surveying	L.S.	<u> </u>		
		L.S.	<u> </u>		
B	CHANNEL WORKS	-			
B.1	Preparatory Works		1		
8.1.1	Clearing of Garbage	L.S.	l l		
B.2	Channel Excavation		<u></u>		
B.2.1	······································	ļ	<u> </u>		
0.2.1	Excavation below Water Level including Hauling and Treatment of Contaminated	m <sup>3</sup>	58,409		
0	DIKE RAISING				
C.1	Dike Raising	1			
C.1.1	Structural Excavation	m <sup>3</sup>	1,643		
C.1.2	Backfill with Selected Soil	m <sup>3</sup>	762		
C.1.3	Chipping of Existing Dike Surface	 	4,988		
C.1.4	Sand Bedding	m <sup>3</sup>	190		
C1.5	Wet Stone Masonry	m <sup>3</sup>	╉━╍──╺┈╍╍┞──	ł	
C1.6	Joint Filler, 10 mm thick (Elastic Material)	m <sup>2</sup>	1,672		
C1.7	Pointing	m <sup>2</sup>	4,997		
)	INSPECTION ROAD		-1,007		
2 D.1	Pavement				
D.1.1	Sand Bedding	3	0.000		
D.1.2	Concrete Block Pavement	m <sup>3</sup>	3,520		<u> </u>
D.1.2 D.1.3	Concrete Block Pavement	m <sup>2</sup>	58,664		
D.1.3 D.1.4	Concrete Kerb	m <sup>3</sup>	141		<u> </u>
		m <sup>3</sup>	1,408		
	MISCELLANEOUS WORKS				
E.1.1	Preparatory Works				
E.1.1 E.1.2	Coffering and Dewatering Demolition of Existing Concrete	L.S.			
.2	Secondary Channel Outlet Closures	Ĺ.S.			-
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E.2.1 E.2.2		2	180		
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	form work	m <sup>2</sup>	217		
E.2.4	Backfill with Selected Soil	m <sup>3</sup>	153		

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1 - 1

## Package 1: B Channel Works

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	Name of Structure	SEMARANG RIVER	Category Calculation	WORK VOLUME	Page	1/1
	<u>SUMM</u>	ARY OF CHANNEL EX	CAVATION	······································	<u></u>	
:	1. E	xcavation including Haulin	ng and Treatmen	t = 58.409 m³		
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#### **EXCAVATION OF SEMARANG RIVER**

Cross Section	Distance	EYCAN	ATION		LL	ero in			· · · · · · · · · · · · · · · · · · ·
Closs section	(in)	AREA	VOLUME	AREA	VOLUME	STRIP LENGTH OF STRIPPING	VOLUME	AREA	UT VOLUMI
		(m <sup>2</sup> )	(m <sup>1</sup> )	(m²)	(m <sup>3</sup> )	(m)	(m <sup>2</sup> )	(m <sup>2</sup> )	(m')
SMR- 00	0.000	44.389	Ī					Ť	
SMR- 01	32.190	39.065	1343.200						
SMR- 02	27.090	37.283	1034.140	•					
SMR- 93	33.510	54.129	1531.610						
SMR- 04	37.620	35.622	1688.219						
SMR- 05	22.420	17.874	599 699	· · ·			· ·		
SMR- 06	25.960	83.353	1313.933						······
SMR- 07	27.050	25.658	1474.373	4.667	63.120	9.675			j .
SMR- 03	29.720	44.247	1058.784	1.832	96.571	8.055		0.0001	0.0
SMR- 09	33.370 27.390	60.777	1752.323	1.527	56.037	8.080			0.0
SMR- 10 SMR- 11	33.400	43.660	1430.262	1.092	35.860	6.026 7.925		6.1430	1.9
SMR- 12	31.490	53.727	1716.419	1.134	10.819	7.923			2.3
SMR- 13	29.450	52 175	1559 406	1.437	43.013	6.663		0.0966	 I.4
SMR- 14	29.500	56 787	1607.191	0.065	22.827	2.485		0.2480	5.0
SMR- 15	28.610	61.312	-1689.411			2.102		3.1694	48.8
SMR- 16	30.140	53.382	1728.446	0.131	1.974	1.981		1.3211	67.6
SMR- 17	32.300	56.094	1768.037	1.971	33.949	7.921			21.3
SMR- 18	32.360	51.875	1746.930	2.687	75.373	7.843			
SMR- 19	31.100	46.453	1528.989	1.318	62.289	3.976		1.6905	26.2
SMR- 20	29.100	35.076	1186.240	1.653	43.230	6.302		1.8248	51.1
SMR- 21	28.330	31.495	942.971	1.348	42.498	5.469	-		25.8
SMR- 21+23	19.960	53.220	815.450						
SMR- 23	31.840	11.710	1033.680				·····		÷ · ·
SMR- 24 SMR- 25	32.290 32.740	13.746 19.576	410.993 545,492						
SMR- 26	31.380	19.570	618.575					<u> </u>	
SMR- 20	29.820	14.281	508.873						
			404.208						<u>.</u>
SMR- 28	1 29.7201	17.9701							
SMR- 28 SMR- 29	29.720 30.260	12.920							
SMR- 29 SMR- 30 SUB SMR-[N1 SMR- N2	30.260 28.930 TOTAL1 27.650 14.970	14.017 8.873 1207.912 14.268 62.590	407.560 331.112 \$35438.934 <sup>*</sup> 319.925 575.280	22.365	655.057	90.294		8.494	ş 
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N4 SMR- N5 SMR- N5 SMR- N5 SMR- N5 SMR- N7 SMR- N7 SMR- N8 SMR- N9 SMR- N10 SMR- N12	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.059 61.961 67.934 67.842 42.642	407.560 331.112 \$35438.934 <sup>2</sup> 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2045.336 2084.905 1880.628 1911.401 1972.147 1599.812	22.365	655.057	90.294		8.494	252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N5 SMR- N5 SMR- N7 SMR- N7 SMR- N7 SMR- N10 SMR- N10 SMR- N11 SMR- N13	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.059 61.961 67.934 67.842 42.642 0.325	407.560 331.112 \$35438.934 <sup>2</sup> 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2045.336 2024.905 1880.628 1911.401 1972.147 1599.812 569.745	22.365	655.057	90.294	0.000		252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N5 SMR- N5 SMR- N7 SMR- N7 SMR- N7 SMR- N10 SMR- N10 SMR- N11 SMR- N13	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.059 61.961 67.934 67.842 42.642 0.325	407.560 331.112 \$35438.934 <sup>2</sup> 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2045.336 2084.905 1880.628 1911.401 1972.147 1599.812	22.365	655.057		0.000		252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N4 SMR- N5 SMR- N5 SMR- N5 SMR- N7 SMR- N7 SMR- N7 SMR- N10 SMR- N10 SMR- N11 SMR- N13	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.059 61.961 67.934 67.842 42.642 0.325	407.560 331.112 \$35438.934 <sup>2</sup> 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2045.336 2024.905 1880.628 1911.401 1972.147 1599.812 569.745		655.057		0.003		252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N5 SMR- N5 SMR- N5 SMR- N5 SMR- N5 SMR- N5 SMR- N5 SMR- N5 SMR- N13 SMR- N13 SUB SMR- 43 SMR- 44	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520 TOTAL2	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.059 61.961 67.934 67.842 42.642 0.325 	407.560 331.112 \$35438.934 \$575.280 1338.590 2086.169 2134.003 2669.154 2015.356 2084.905 1880.628 1911.401 1972.147 1599.812 569.745 \$21187.116		655.057		0.003		252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N5	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520 TOTAL2	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.050 61.961 67.934 67.842 42.642 0.325 	407.560 331.112 \$35438.934 <sup>2</sup> 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2045.356 2084.905 1889.628 1911.401 1972.147 1599.812 569.745 \$21187.116 108.099		655.057		0.008	0.000	252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N15 SMR- N13 SUB SMR- N13 SUB SMR- 43 SMR- 45 SMR- 45 SMR	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520 TOTAL2	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.059 61.961 67.934 67.842 42.642 0.325 7.551 14.304 32.248	407.560 331.112 \$35438.934 <sup>2</sup> 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2045.356 2084.905 1889.628 1911.401 1972.147 1599.812 569.745 \$21187.116 108.099 289.596		655.057		0.003	0.000	252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N5 SMR- N6 SMR- N5 SMR- N6 SMR- N7 SMR- N7 SMR- N8 SMR- N9 SMR- N10 SMR- N10 SMR- N11 SMR- N12 SMR- N12 SMR- N13 SUB SMR- 43 SMR- 43 SUB	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520 TOTAL2 27.450 26.510 27.440 27.440	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.050 61.961 67.934 67.842 42.642 0.325 718.575 7.551 14.304 32.248 54.104	407.560 331.112 (35438.934) <sup>2</sup> 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2015.356 2024.905 1880.628 1911.401 1972.147 1599.812 569.745 21187.116 108.099 289.596 638.698 (4.1036.493)	0.000	655.057		0.000	0.000	252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N5 SMR- N6 SMR- N5 SMR- N6 SMR- N7 SMR- N6 SMR- N7 SMR- N7 SMR- N7 SMR- N7 SMR- N7 SMR- N1 SMR- N10 SMR- N10 SMR- N11 SMR- N12 SMR- N12 SMR- N13 SUB SMR- 45 SUB SMR- 46	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520 TOTAL2 27.450 26.510 27.440 27.450 26.510 27.440 27.440	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.050 61.961 67.934 67.842 42.642 0.325 7.551 14.304 32.248 54.104	407.560 331.112 (35438.934) <sup>2</sup> 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2015.356 2024.905 1880.628 1911.401 1972.147 1599.812 569.745 259.745 21187.116 108.099 289.596 638.698 (1036.493) 746.257	0.000	655.057		0.009	0.000	252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N5 SMR- N6 SMR- N5 SMR- N7 SMR- N5 SMR- N5 SUB SMR- 45 SMR- 45 SMR- 45	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520 TOTAL2 27.450 26.510 27.450 26.510 27.440 29.400 29.580	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.050 61.961 67.934 67.842 42.642 0.325 718.575 7.551 14.304 32.248 54.104 18.518 17.932	407.560 331.112 \$35438.934? 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2015.356 2024.905 1880.628 1911.401 1972.147 1599.812 569.745 21187.116 108.099 289.596 638.698 \$29.596 638.698 \$29.596 638.698 \$29.596 638.698 \$29.596 638.698 \$29.596 638.698 \$20.575 539.089	0.000	655.057		0.000	0.000	252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N5 SUB SMR- 45 SUB SMR- 45 SMR- 45	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520 TOTAL2 27.450 26.510 27.450 26.510 27.440 29.580 31.250	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.050 61.961 67.934 67.842 42.642 0.325 718.575 7.551 14.304 32.248 54.104 18.518 17.932 17.388	407.560 331.112 \$35438.934? 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2045.356 2084.905 1880.628 1911.401 1972.147 1599.812 569.745 21187.116 108.099 289.596 638.698 \$44.257 539.089 551.869	0.000	655.057		0.009	0.000	252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N5 SUB SMR- 45 SMR- 45 SM	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520 TOTAL2 27.450 26.510 27.450 26.510 27.440 29.400 29.580	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.059 61.961 67.934 67.842 42.642 0.325 718.575 7.551 14.304 32.348 54.104 18.518 17.932 17.388 16.934	407.560 331.112 \$35438.934? 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2015.356 2084.905 1880.628 1911.401 1972.147 1599.812 569.745 21187.116 108.099 289.596 638.698 \$29.596 638.698 \$44.257 539.089 551.869 527.177	0.000	655.057		0.000	0.000	252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N5 SUB SMR- 45 SUB SMR- 45 SMR- 45	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520 TOTAL2 27.450 26.510 27.450 26.510 27.440 29.580 31.250 30.720	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.050 61.961 67.934 67.842 42.642 0.325 718.575 7.551 14.304 32.248 54.104 18.518 17.932 17.388	407.560 331.112 \$35438.934? 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2045.356 2084.905 1880.628 1911.401 1972.147 1599.812 569.745 21187.116 108.099 289.596 638.698 \$44.257 539.089 551.869	0.000	655.057		0.000	0.000	252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N14 SMR- N15 SMR- N5 SMR- N5 SM	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520 26.520 26.520 27.450 26.510 27.450 26.510 27.440 29.580 31.250 30.720 30.580	14.017 8.873 1207.912 14.268 62.590 68.580 68.488 71.493 65.247 65.155 62.059 61.961 67.934 67.842 42.642 0.325 7.551 14.304 32.348 54.104 18.518 17.932 17.388 16.934 3.508	407.560 331.112 \$35438.934? 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2045.356 2084.905 1880.628 1911.401 1972.147 1599.812 569.745 21187.116 108.099 289.596 638.698 \$44.257 539.089 551.869 527.177 312.553	0.000	655.057 0.000		0.000	0.000	0.00
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N14 SMR- N15 SMR- N5 SMR- N5 SMR	30.260 28.930 7OTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520 7.07AL2 27.450 26.510 27.440 27.450 26.510 27.440 29.580 31.250 30.720 30.580 31.550 29.700 30.480	14.017         8.873         1207.912         14.268         62.590         68.580         68.488         71.493         65.247         65.155         62.050         61.961         67.934         67.842         42.642         0.325         7.551         14.304         32.248         54.104         18.518         17.388         16.934         3.508         18.975         11.254         11.294	407.560 331.112 \$35438.934 <sup>2</sup> 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2045.356 2084.905 1889.628 1911.401 1972.147 1599.812 569.745 21187.116 108.099 289.596 638.698 \$45.1036.493 746.257 539.089 551.869 527.177 312.553 251.666 418.889 343.625	0.000	655.057 0.000		0.000	0.000	252.03
SMR- 29 SMR- 30 SUB SMR- N1 SMR- N2 SMR- N3 SMR- N3 SMR- N3 SMR- N5 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N13 SMR- N14 SMR- N15 SMR- N5 SMR- N5 SM	30.260 28.930 TOTAL1 27.650 14.970 20.410 30.440 30.490 39.040 31.370 32.780 30.330 29.430 29.050 28.960 26.520 26.520 27.450 26.510 27.450 26.510 27.440 29.580 31.250 30.720 30.580 31.550 29.700	14.017         8.873         1207.912         14.268         62.590         68.580         68.488         71.493         65.247         65.155         62.059         61.961         67.934         67.842         42.642         0.325         7.551         14.304         32.248         54.104         18.518         17.388         16.934         3.508         18.975         11.254	407.560 331.112 \$35438.934? 319.925 575.280 1338.590 2086.169 2134.003 2669.154 2045.356 2094.905 1880.628 1911.401 1972.147 1599.812 569.745 21187.116 108.099 289.596 638.698 \$446.257 539.089 551.869 527.177 312.553 551.666 448.889	0.000	655.057 0.000		0.000	0.000	0.00

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•	Cross Section	Distance (m)	EXCAV AREA	ATION VOLUME	AREA	ILL VOLUME	STRII LENGTH OF	PPING VOLUME	AREA	UT VÕLUME
·			(m <sup>2</sup> )	(m <sup>3</sup> )	(m²)	(m <sup>3</sup> )	STRIPPING (m)	(m <sup>-</sup> )	(m <sup>*</sup> )	(m <sup>3</sup> )
=	SMR- 55	31.370	16.366	457,177	( 11 /			(111)		
-	SMR- 56	30.760	3.616	307.325						
	SMR- 57	35,140	9.160	224.464					·	
	SMR- 58	37.220	20.634	554.450						
T	SMR- 59	29.590	26.065	690.869						
	SMR- 60	27.660	19.764	633.775						
	SMR- 61	26 170	14.859 15.149	453.034 372.696						
Ļ	SMR- 62 SMR- 63	24.840 28.930	20.161	510.758						
	SMR- 64	28.930	12.321	438.997		······································				<u> </u>
	SMR- 65	25,410	15.535	353.912						<u> </u>
	SMR- 66	26.150	19.063	452.371						
F	SMR- 67	31.430	12.826	501.144						
	SMR- 68	32 870	10.708	386.788		1. A			L	<u> </u>
	SMR- 69	34.380	9.897	351.213						]
	SMR- 69+14	12.890	17.486	176.486 206.092						
_  -	SMR- 70 SMR- 71	16.180 31.130	14.785	354.471			· · · · · · · · · · · · · · · · · · ·			
-	SMR- 72	28.440	18.274	170.091						· · · · · · · · ·
	SMR- 72	31.430	16.191	541.609			······			
· .	SMR- 74	31.850	10.239	420 895		1				
T	SMR- 75	32.100	12.282	361.464						
E	SMR- 76	32.820	18.080	498.247		·		· · · ·		<u> </u>
	SMR- 77	30.760	18.525	562.985					1997 - B	
.	SMR- 78	28.940 28.030	17.062	515,344						
	SMR- 79 SMR- 80	30.210	20.349	605.070						
ŀ	SMR- 81	29,790	21.518	623 614			1			
ŀ	SMR- 82	27.590	20.392	578,155				· · · · ·		
ł	SMR- 83	28.870	21.132	599,400					·	
· †	SMR- 84	29,510	20.886	619.972	1					
Ē	SMR- 85	29.720	9.357	449.409				· · · ·		
	SMR- 86	29.590	17.167	392.413		· · · · ·				
ł	SMR- 87 SMR- 88	30.730 33.630	11.062 5.649	433.729 281.000					<u> </u>	
-	<u>SMR- 89</u>	35.230	1.624	128.117					·	· · · ·
. F	SMR- 90	31.720	1.013	41.816	1		1		and second second	an an an an a
ł	SMR- 90+11	11.180	22.191	129 728		3		and the second fit		
. [	SMR- 91	14.820	16.756	288.623					<b></b>	
[	SMR 92	22.640	15.055	360.100	<u> </u>			· · · · · · · · · · · · · · · · · · ·	·	
- I	SMR- 93	20.830	5.436	213.409						
	SMR- 94 SMR- 95	26,750 28,930	10.472	212.768						
ŀ	SMR- 75	25.270	9.337	323.209						
	SMR- 97	27.470	7.384	229.662						
ł	SMR- 98	27.280	9.945	236 375				and the second		
. 1	SMR- 99	30.560	11.261	324.026	F					1
· - [	SMR- 100	28,886	8.621	287.092						
	SMR- 101	30,800	9,974	286.369		· · ·				
ļ	SMR-102 SMR-103	30.820 33.100	18.143	433 283					<b> </b>	
	SMR- 105 SMR- 104	33.100	17.287	531.272				<u> </u>		
	SMR- 104	39.510	7.157	133.463			-			
	SMR- 106	33.710	8.789	268 768	<b>_</b>					
	SMR- 106+13	5.280	20.376	76.995					ļ	
	SMR- 107	27,780	6.139	368.291					ļ	
	SMR- 108	32,100	7.157	215.385			+	1		
	SMR- 109	27.130 28.510	7.191	194.632				<b> </b>		+
	SMR 110 SMR 111	28.510	9.540			-	+		<u> </u>	1 N. 1
1	SMR- 112	29,760		255,900						
	SMR- H3	30.230								
	SMR-114	26.020		336.11-	i -					
	SMR- 115+15	13.340		209.980					ļ	
	SMR- 116	16.510								<b> </b>
	SMR- 116+8	9.646	19.217	179.16						
	SMR- 117	20.680	9.541	297.359						<b> </b>
	SMR- 118	29.190 28.280							<b> </b>	
. 1	SMR 119									

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Cross Section	Distance (m)	EXCAVA AREA	VOLUME	AREA	ILL VOLUME	STRI LENGTH OF STRIPPING	PPING VOLUME	AREA	VOLUME
	-	(m <sup>2</sup> )	(m <sup>3</sup> )	(m <sup>2</sup> )	(m <sup>3</sup> )	(m)	(m²)	(m²)	(m <sup>1</sup> )
SMR- 120	26.970	22.432	424.524			1			
SMR- 121	27.900	17.954	563.397						
SMR- 121+3	4.190	19.217	77.873						
SMR- 122	27.150	9.541	390 391 325.344			·			
SMR- 123 SMR- 124	29.900 29.940	9.934	331.658						·
SMR- 125	30.050	10.417	305.777				· · · · ·		
SMR- 126	29.950	13.962	365.075						
SMR- 126+17	17.570	11.807	252.735				· · ·		
SMR- 127	15.520	3.815	144.509		····				······
SMR- 128	31.650	6.612	165.007						
SMR- 129	35.800	8.759	275.143						
SMR- 130 SMR- 131	31.860 29.090	5.650 12.049	22.9.537 257.424						
SMR- 131	27.430	12.884	341.948						
SMR- 133	28.070	4 175	239.419			[			
SMR- 134	29.290	8.022	178.622		· · · · · · · · · · · · · · · · · · ·				
SMR- 135	26.360	7.196	200.566						
SMR- 156	29.830	12.269	290.316						
SMR- 137	30.300	13.614	392.118				. • •		
SMR- 137+14 SMR- 138	14.290 19.300	14.746	202.631			[			
SMR- 135 SMR- 139	31.960	10.656	360.606						
SMR- 140	32.540	10.558	345.154		11			·- ·	in the second
SMR- 141	33.270	10.047	342.769						
SMR- 142	32.920	10 365	335 979		dia et				
SMR- 142+23	24,480	12 828	283.878	: · ·		1.1			
SMR- 143	6.690	13.391	87.701						· · · · · · · · · · · · · · · · · · ·
SMR- 144 SMR- 145	28.320 	6.010 6.663	274.719 171.273	0.039	1.076	0.411	12.290	· · · · · · · · · · · · · · · · · · ·	
SMR- 145 SMR- 146		- 10.006	258.033	0.015	0.444	2.061	61.898		
SMR- 147		. 6.982	247.170	0.009	0.251	0.393	10.813		
SMR- 148		J 8.601	202.492		-			·····	
SMR- 149	28.170	9.247	251.381		1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -		1	
SMR- 150	22.690	6.844	182.551		a ta ang sa sa		aut e		
SMR- 151	27.270	8.484	209.000			2000 - 12 A.	1 A. 1		
SMR- 152 SMR- 153	27.550	9.312	245.141 265.856						· · · · · ·
SMR- 154	29.000	11.752	276.307						
SMR- 155	28.050	8.914	289.839						
SMR- 156	31.550	6.463	242.571			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			1999 - <b>2</b> 99 - 20
SMR- 156+17	17.820	8.785	135.863			•		1.1.1	
SMR- 157	FI.910	8.282	101.633	:	· · · · · · · · · · · · · · · · · · ·				e e con
SMR- 158 SMR- 159	30.760	8.491	257.963						· · ·
SMR- 160	29.920	8.175	249.327	0.059	1.865	0.163	14.755		
SMR- 161	33.360		284.053	0.0.7	1.303	0.405	14.735		
SMR- 162	30.190	7 191	221.421			an an an an an an			
SMR- 153	29.250	9.373	242.262						
SMR- 164	29.700	7.384	248.841			1 A.A.			
SMR- 165	29.490	6.922	210.936		: :.				
SMR- 166 SMR- 167	28.000 30.580	7.497	201.873 250.920		n an		1772) 1972 - 1972 1973 - 1972		a desta a La constante
SMR- 167	30.580	9.080	272.515				n an		
SMR+ 168+7	7.010	8.994	63.349						n de la company. La company
SMR- 169	23.540	8.176	202.087						and the second second
SMR- 170	29.980	11.190	290 302						44.201.2
SMR- 171	29.390	11.149	328.278			÷	1 - E - E - S		
SMR-172	27.720	9.706	289.046					41	
SMR- 173 SMR- 174	30.840 33.000	9.563 8.599	297.120 299.676		<b>\</b>				
SMR- 175	31.710	8.125	299.676			<b> </b>			<u>i v tek</u>
SMR- 176	30.660	9.520	270.498	n gord					in the sector of the
SMR- 177	27.740	7.757	239.642						I 4. 1
SMR- 178	~ 27.400	6.465	194.849	1			a na sa		
SMR- 179	28.310	7.630	199.513					· · ·	an Angela
SMR- 180	24.320	8.307	193.789			<b>I</b>			
SMR- 181	28.810	6.502	213.322 219.344					<u>, , , , , , , , , , , , , , , , , , , </u>	
SMR- 182								10 A 10 A 10 A	

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Cross Section	Distance	EXCAVA			ĹĹ	<u>eroi</u>	PPING	······	CUT
Cross Section	(m)	AREA	VOLUME	AREA	VOLUME	LENGTH OF STRIPPING	VOLUME	AREA	VOLUM
·		(m <sup>2</sup> )	(m <sup>3</sup> )	(m <sup>2</sup> )	(m <sup>3</sup> )	(m)	(m²)	(m²)	(m³)
SMR- 183	31.360	9.588	271.721						
SMR- 184	30.450	8.129	269.743						
SMR- 185	30.000	8.324	246.805						
SMR- 186	30.850	\$.007	251.916						
SMR+ 187	33.000	7.350	253.394						L
SMR- 188	31.030	6.113	208.883						
SMR- 189	29.880	6.407	187.055						
SMR- 190	29.660	5.104	170.706						[
SMR- 191	26.320	7.638	167.676						
SMR- 192	29.440	6.463	207.554						[
SMR- 193	28.440	7.206	- 194.371						
SMR- 194	31.120	6.937	220.072						
SMR- 195	29.740	2.777	144.449				· · · · · · · · · · · · · · · · · · ·		
SMR- 195+17 SMR- 196	17.180	5.103	67.686					··· · · · · · · · · · · · · · · · · ·	
SMR- 190	13.110	5 393	68.799					·····-•	
SMR- 197 SMR- 198	30.170	5.288	171.717 164.883				· · · · · · · · · · · · · · · · · · ·		
SMR- 198 SMR- 199	30.110	5.915	164.885						<b>-</b>
SMR- 199 SMR- 200	30.020	5.725	174,717			·			
SMR- 200	30.020	5.457	168.739	0.026	0.789	0.425	12.814	<b>.</b>	
SMR- 202	30.080	4.310	146.890	0.050	1.530	0.163	14.066		<u> </u>
SMR- 203	30.720	5.667	153.244	0.023	0.686	0.425	12.785	· · · · · · · · · · · ·	
SMR- 204	29.390	6.048	172.159						
SMR- 205	29.770	6.393	185.195						]
SMR- 206	25.650	5,972	158.580					·	
SMR- 207	32.070	6.799	204.780						
SMR- 208	30.130	6.061	193.742		····				
SMR- 209	30.120	5.683	176.868					<u>.</u>	
SMR- 210	30.150	5.762	172.540						· ·
SMR- 211	22.740	0.574	72.049						
SMR- 212	30.400	5.338	89.874						
SMR- 213	30.050	6.040	170.960		:				
SMR- 214	29.790	6.654	189.080	- 10 - 10 - 10 			<u></u>		
SMR- 215	31.090	7.038	212.841						
SMR- 215+22	22,730	6.446	153.242			·			
SMR- 216	7.110	7.517	51.942						
SMR- 217	30.640	6.563	215.710	0.026	0.790		13.040		
SMR- 218	29.940	6.455	194.878	0.033	0.988	0.437	13.220		•
SMR- 219	30.550	6.016	190.485	0.006	0.192	0.404	12.352		
SMR- 220	30.540	5.522	176.180		0.913	0.837	25.541		
SMR- 221 SMR- 222	30.520	6.792	187.909	0.054	1.631	0.861	25.976 26.673		
SMR- 223	31.050	6.228	197.266	0.0.14	1.052	0.670			
SMR- 225	29.230	6.635	197.200					. <u>.</u>	
SMR- 225	29.380	6.215	188.763						
SMR- 225+10	10.180	6.628	65.371	·		I			
SMR- 226	19,780	5.825	123.139	0.043	1.080	0.769	19.235		
SMR- 227	30.240	5.891	177.138	0.067	2.021	0.865	25.976		
SMR- 228	29.800	6.014	177 375	0.017	0.185	0.133	12.641		
SMR- 229	28.560	5.850	169.408	0.021	0.598	0.115	11.657		
SMR- 230	27.660	4.108	137.714	0.007	0.211	0.407	11.612		
SMR- 231	29.430	6.108	150.329	0.006	0.168	0.030	0.876		
SMR- 232	29.560	6.735	189.822						
SMR- 233	29.270	6.418	192.492	0.035	1.040	2.541	74.798		
SMR- 234	29.610	6.214	187.013	0.016	0.483	2.463	73.210	· .	
SMR- 235	29.840	5.703	177.800	0.076	2.072	0.818	22.164		
SMR- 235+24	24.350	6.084	143.502		a se				
SMR-236	6.750	5.848	40.270	0.022	0.411	0.882	16.290		
SMR- 237	30.210	5.685	174.207	0.006	0.193	0.102	12.159		. <u>.</u>
SMR- 238	30.360	5.603	171.349						
SMR- 239	29.810	5.388	163.816						
SMR- 240	29.510	5.417	159 432		an the second second				
SMR- 241	29.920	4.269	144.915						
SMR-241+13	13.850	0.731	34.628		1		1. A.	· · · ·	

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SUB TOTAL4 2136.101 58408.814 0.742 221569 18.543 236.844 0.000

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# Package 1: C Dike Raising

Name of Structure	DIKE RAISING FOR SEMARANG RIVER	Category of calculation	WORK VOI	UME	Page	
	SUMMAR	Y OF WORK V	OLUME			
		<u></u>	<u>× 2 YIII</u>			
1. STRU	JCTURE EXCAVATION		=	1,642.7	4 m <sup>3</sup>	
2. COM	PACTED SAND		=	189.2	20 m <sup>3</sup>	
3. WET	COBBLE MASONRY		=	1,671.6	6 m <sup>3</sup>	
4. BACI	K FILL	· .	=	762.3	0 m <sup>3</sup>	
5. CHIP	PING		==	4,988.2	3 m <sup>2</sup>	· .
6. POIN	TING		· · · · · · · · · · · · · · · · · · ·	4,996.9	7 m <sup>2</sup>	
7. JOIN	TFILLER	n de la companya de La companya de la comp		71.1	5 m′	

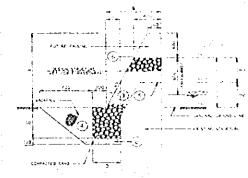
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NOTES: SEE PAGE I-8 and PAGE I-5 A. H/W Colble maroney = 1650.093 + 21.569 = 1,671.66 m<sup>3</sup> B. Chipping = 4451.234 + 536.844 = 4,988.23 m<sup>3</sup>

1 - 7

## WORK VOLUME OF DYKE RAISING FOR RIGHT SIDE OF SEMARANG RIVER



(1) = STRUCTURE EXCAVATION (m<sup>3</sup>)

0

0

860.953 101.210 939.821 380.537 2172.733 2583.035

- (2) = COMPACTED SAND (m<sup>3</sup>)
- (3) = WET COBBLE MASONRY (m<sup>3</sup>)
- (4) = BACK FILL (m<sup>3</sup>)
- $(5) = CHIPPING(m^2)$
- (6) = PLASTERING (m<sup>2</sup>)

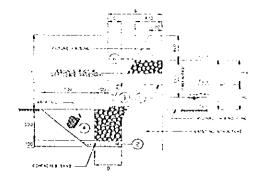
					· .															÷.,			
STA	DIST	ELI	EL.2	EL.3	н.	H.2	11.3	н	В	с	D			A R	E A				1	YOL	UME	• • • •	
(SMR)	(m)	(m)	(15)	(m)	(11)	(m)	(m)	(m)	(m)	(m)	(m)	ι Π	(2)	(3)	(4)	(5)	(6)	(1)	(1)	(3)	(4)	(5)	(6)
45	29.410	+0.28	+1,060	+0.35	0.780	0.070	0.710	1.180				0.573			0.225		1.472	16.909	2.083	21.257	6.617	29,100	43.836
46	29.602	+0.25 +0.25		+0.34 +0.30	0.813	0.090	0.723	1.213 1.216				0.577 0.590					1.509 1.512	17.268	2.138	22.156	6.660	28.959	44.718
48	31.099 30.686	+0.27	+1.069	+0.29	0.799	0.020	0.779	1.199	0.800	0.390	0.590	0.594	0.074	0.766	0.225	0.922	1 <u>.493</u>	<u>18.403</u> 17,910	2.290	23,784 22 548	6.997 6.904	29.206 28.647	46.736 45.017
<u>49</u> 50	30.579	+0.32	<u> </u>	+0.35 +0.36	I	0.040		1.152 1.205	0.803			<u>0.574</u> 0.575					1.441	17.554 18.357	<u>2.161</u> 2 278	<u>21.841</u> 23.820	<u>6.880</u> 7.035	<u>29.743</u> 30.587	44.963 47.670
51	<u>31.267</u> 29.710	+0.23	+1.079	+0.28	0.849	0.050		1.249				0.600 0.586					1.549 1.553	17.608	2.192	23.273	6.685	29.230	46.077
<u>52</u> 53	<u>30.465</u> 20.447	+0.23 +0.27		+0.33 +0.28	0.852	0.010			0 803			0.602	0.075	<u>0.789</u>	0 225	0.911	1.511	18.083 12.305	2.252	23.718	<u>6.855</u> 4.601	<u>29.292</u> 20.460	46.669
<u>53+17</u> 54	13.524	+0.11 +0.20		+0.28		0.170			0.889			0 602 0.623				<u>1.090</u> 0.911	1.692 1.593	8 287	1.043	11.656	3.043	13,532	22.214
55	<u>31.430</u> 30.735	+0,17	+1.091	+0.21	0.921	0.040	0.881	1.321	0.851	0.441	0.641	0.624	0.079	0.881	0.225	0.945	1.630	19.608 19.059	2.482	27.535 26.246	7.072 6.915	<u>29,165</u> 28,864	50.642 48.405
<u>56</u> 57	35 330	+0.27 +0.31	+1.093	+0.24	r	-0.030 0.070						0.616 0.575				0.934 0.978	1.520 1.478	21.028	2.621	27.224	7.949 8 327	<u>33,772</u> 35,997	<u>52.956</u> 55.161
58	37.008 29.189	+0.29	+1.098	+0.23	0.808	-0.060	0.868	1,208	0.804	0.434	0 6 3 4	0.620	0,078	0.827	0.225	<u>0.967</u> 0.911	1.503	22.110	<u>2.760</u> 2.304	28 572 24.920	6 568	27.412	15 383
<u>59</u> 60	26.460	+0.20 +0.35		+0.21	0,900	0.010						0.627 0.562					1.441	<u>15,725</u> 14,704	1.959 1.812	<u>20.606</u> 17.693	<u>5.954</u> 5.750	<u>25,145</u> 25,427	40 312 35,703
61	25.554 24.943	+0.43	+1.104	+0.34		-0.090 0.030						0.559 0.578				1. <u>001</u> 0.934	<u>1.354</u> 1.445	14.554	1.802	17.743	5.612	24,122	34,905
$\frac{62}{63}$	28.923 26.951	+0.48		+0.42	0.628	-0,060	0 688	1,028	0.714	0.344	0.511	0.565	0.669	0.645	0.225	0.967	1.302	<u>16.547</u> 14.461	2.035	<u>19.660</u> 15.061	6.508	<u>27.486</u> 25,461	<u>39.731</u> 32.693
64 65	25.371	+0.64	+1.109 +1.111	+0.62		-0.020 0.030			0.635 0.691		0.445	0.507				0.922	1.124	12.901	1.516	12.447	5.708	24.252	30.115
66	<u>26.534</u> 31.344	+0.27	+1.113	+0.72	0.843	0.450	0.393	1.243	0.822	0.197	0,397	0.478	0.055	0.432	0.225	1.403	1.543	13.110 14.895	1.522	<u>13.147</u> 14.528	5,970 7.052	<u>31.742</u> 42.227	<u>37.043</u> <u>46.</u> 281
67	32.692	+0.39		+0.74	0.725	0.350			0.763 0.739			0.473			0.225		1.411 1.357	15.212	1.718	13.748	7.356	42,216	45.2.7 50.040
69	<u>34.032</u> 12.863	+0.24	+1.120	+0.77	0.880	0 530	0.350	1.280	0.840	0.175	0.375	0.465	0.053	0.451		1.493 1.493	1.584	15.707 5.925	0.666	5.598	2.894	19,199	20 165
<u>69+14</u> 70	16.137	+0.27 +0.19		+0.80	0.851	0.530				0.161	0.381	0.469	0.053	0.471	0.225	1.537	1.612	7.463	0.840	<u>7.187</u> 14.286	<u>3.631</u> 6.995	<u>24.446</u> 47.446	25.766 50.390
71 72	31.090 28.466	+0.23 +0.26		+0.78	0.894	0.550	0 3 4 4 0 2 5 6	<u>1 294</u>			0.372	0.463	0.052	0.448	0.225	1.515		12,938	1.445	11.914	6,405	43,601	45.086
.13	31.301 31.611	+0.30		+0.87	0.828	0.570	0.258	1.228	0.814	0,129	0.329	0.437	0.043	<u>0.358</u>	0.225	1.532	1.526	<u>13.823</u> 14.121	<u>1.521</u> 1.563	11.693	<u>7.043</u> 7.112	<u>48,293</u> 49,655	4 <u>8.422</u> 50,386
74	31.923	+0.18 +0.21		+0.81	*	0.630	1					0.455				1.604		14,954	1.694	15.031	7.183	49.253	52 <u>578</u>
76	<u>32 574</u> 30.692	+0.26	+1.137	+0.74	0.877	0.480	0.397	1.277	0.839	0.199	0.399	0.479	0.055	0,493	0.225	1.437	1.581	15.636	<u>1.792</u> 1.678	<u>16.288</u> 15.276	7.329 6.906	<u>47.526</u> 45.638	<u>52.321</u> 49.933
77	28.105	+0.18		+0.75		0.570						0.477 0.445					1.673	12.955	<u>1.457</u> 1.410	12.429 11.340	<u>6.324</u> 6.348	42 891 43,217	45.033 44.200
79	28.215	+0.25	+1.146		0.895	0.580										1.548		12.693 13,779	1.545	12.689	6.765	44.039	46 029
80 81	29,804	+0.38	+1.149		0.769	0.430			0.776	0.151	0.351	0.451	0.050	0.387	0.225			<u>13.595</u> 12.495	1.521	12.056	<u>6.706</u> 6.254	41.435 40.243	43,224 41,180
- <u>82</u> 83	27,795 29.008	+0.33	+1.155 +1.157			0.530						0,449				1.493		12.888	1.423	10.972	6.527	43,620	44.031
81	28.537 29.696	+0.42	+1 160	+0.92	0.740	0.500	0.240	1.140	0.770	0.120	0.320	0.432	0.047	0.330	0.225	1.459	1.427	12.444	<u>1.361</u> 1.478	<u>9,919</u> 11,591	6.421 6.682	<u>42,434</u> 43.659	41,961 44 561
85	29.642	+0.25	9 <u>+1.16</u> 1 7 +1.162			0.520						0.465				1.481	<u>1.574</u> 1.597	13.575	1.521	12.722	<u>6.669</u> 6.909	45.071 45.657	<u>46.999</u> 47.174
87	30,705 33,344	+0.38	1.163	+0.8	0.783	0.460	0.323	1.183	<u>0,79</u> 2	0.167	0.362	0.457	0.051	0.410	0.225	1.414	1.475	<u>11.932</u> 15.140	<u> </u>	13.125	7.502	45,481	47.165
83 \$9	34.985	+0.49	+ <u>1.16</u> +1.16			0.370			0.733	0.138		0.443	0.045	0.351	0.22	1.314	1.343	<u>15.633</u> 13.785	<u>1.731</u> 1.527	12.738	7 <u>.872</u> 6.934	46.350 40.140	<u>47,178</u> 40,921
90	30.818	+0.5	-			0.330										5 <u>1.269</u> 5 1.112		5.090	0.570	4.198	2 503	13.274	13.943
90+11 91	14,457		1 +1.167 1 +1.161	+0.5	0.527	-0.120	0.617	0.927	0.664	0.32	0.52	0,551	0.061	0.586	0.22	1.034	1.189	7.338 12.182	<u>0.862</u> 1.431	<u>6.932</u> 11,679	<u>3.253</u> 5.398	15.517 26.283	<u>17.192</u> 29.054
_ <u>92</u> 	23.991		) +1.168 1 +1.169	3 +0.8	0 568	0 230	0 338	0.968	0.684	0.169	0.369	0.461	0.05	0.387	0.22	5 <u>1.157</u> 5 1.481	1.639	10.778	1.226	10.288	5,137	30.123	32.808 45.535
94	27.405	+0.20	+1.170	+0.71	<u>0.970</u>	0.580	0.390	1.376	0.885	0.19	5 0.39	5 0.477	0.055	0.505	0.22	1.548	1.634	11 100		13.958 14.006	<u>6.166</u> 6.354	41.516 43.888	47.461
95 96	25.900	+0.13	1 +1.173 3 +1.176		0.963	0.590	0.426	1.440	5 0.923	0.213	0.41	0.488	0.056	0.554	0.22	s <u>  1.59</u> 3	1.677	12.428	<u>1,424</u> 1.573	<u>13.489</u> 15.447	<u>5.828</u> 6.330	40.829 45.450	44.627 50.158
97	28.133	+0.1	+1.180	+0.7	1.070	0.660	0.410	0 1.470	0.935	0.20	5 0.40	5 0.483	0.050	5 0.544	0.22	5 1.638	1.796 1.990	13.640	1.581	16.471	6.232	47.070	52,432
98 99	<u>30.491</u> 28.841	+0.1	5 +1.18. 3 +1.18	1 +0.7	1.057	0.610	0.447	1,45	0.925	0.22	10.42	0.191	0.05	0.57	0.22	5 1.582	1.782	12 071	1.768 1,391	18.635 15.237	<u>6.860</u> 6.489	<u>50.964</u> 45.949	57,498 50,308
100 101	30.639	1 +0 2	) +1.19   +1.19		3 0.990	0.630	0.360	1.39	0.89	0.18	0.38	0.468	0.05	0.480	0.22	5 1.604	1.707	14.399	1.634	14.872	6.891	48.813	52.176 49.848
102	30.830		5 +1 19	5 +0.7	0.836	0 350	0.18	1 230	0.818	0 24	0 44	0 500	0.05	0.56	0.22	1.29	1.535	15.071	1.741	16.201	6.937	44.292	+7.0+0

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#### WORK VOLUME OF DYKE RAISING FOR LEFT SIDE OF SEMARANG RIVER



Ć :

- (1) = STRUCTURE EXCAVATION (m)
- (1) = COMPACTED SAND (m<sup>1</sup>)
- (3) = WET COBBLE MASONRY (m<sup>3</sup>)
- (+) = BACK FILL (m<sup>3</sup>)
- $(5) = CHIPPING(m^2)$
- (6) = PLASTERING (m<sup>2</sup>)

STA	DIST	EL.1	EL.2	EL.3	11.1	H.2	нз	I	8	с	D			AR	E A					VOL	UME		
(SMR)	(m)	(m)	(m)	(m)	(m)	_(m)_	(m)	(a)	(m)	(m)	(m)	(U)	(2)	(3)	(4)	(5)	(6)	())	(1)	())	(1)	(5)	(6)
- 45	29.410		+1.060		0.930									0.533				14.086	1.612	14.360	6.617	41.430	45,644
46	29.692		+1.063	+0.70	0.773		0.363 0.366							0.413 0.456				13.894	1.576	13.304	6.660	41.039	44.221
48	31.099	+0.32	+1.069	+0.69	0.749	0,370	0.379	1.149	0.775	0.190	0.390	0.474	0.054	0.452	0.225	1.314	1.437	<u>14.671</u> 14.550	<u>1.658</u> 1.658	<u>14,118</u> 14,075	<u>6.997</u> 6.904	42,419 41,169	46.041 45.017
<u>49</u> 50	30.579	+0.27 +0.21	+1.072 +1.075		0.802	0.420	0.382							0.465 0.524			1.497 1.567	14,756	1.695	13.115	6.880	42.051	46.843
51	31.267	+0.22	+1.079	+0.71	0.859	0.490	0.369	1 259	0.830	0.185	0.385	0.471	0.053	0.46-1	0.225	1.448	1.560	<u>15.027</u> 13.998	<u> </u>	15.444	7.035	<u>44.221</u> 42.019	<u>48.894</u> 45.413
<u>52</u> 53	30.465		+1.032		0.802	0.430								0.456			1.497	14.107	1.590	13.123	6.855	42.916	45,477
53+17	20.447		+1.087	+0.76	0.507	0.180	0.327	0.907	0.654	0.164	0.364	0.458	0.051	0.369	0 225	1.101	1.167	9.330 6.197	<u>1.014</u> 0.695	7,912 5,225	<u>4.601</u> 3.043	25.946	27.150
54	<u>13.524</u> 31.430		+1.088											0.404 0.433				14.516	1.634	13.149	7.072	42.519	45.020
<u>55</u> 56	30.735	+0.21	+1.091 +1.093	+0.74 +0.76		0.420								0.436				14.218	<u>1.601</u>	13.345	6.915	44 327	46.85
57	35.330		+1.095	+0.69	0.855	0,450	0.405							0.495				<u>16.630</u> 17.836	1.888	<u>16.448</u> 18.166	7.949 8 327	<u>51.547</u> 50.685	<u> </u>
<u>58</u> 59	29.189		+1.093 +1.100			0.390								0.486 0.423			<u>1.492</u> 1.461	13.783	1.567	13.272	6.568	39,650	43.09
60	26,460	10.34	+1,102	+0.75	0.762	0,410	0.352	1.162	0.781	0.176	0.376	0.466	0.053	0.432	0 225	1.358	1.452	12,272	<u>1.384</u> 1.313	<u>11.311</u> 10.549	<u>5.954</u> 5,750	<u>36.239</u> 35.712	<u>38.53</u> 37.41
61	24.943		+1.104											0.394 0.359			1.477	11.187	1.241	9.390	5.612	34 301	35.04
63	28,923	+0.69	+1.108	+0.89	0.418	0.200	0.218	0.818	0.609	0.109	0.309	0.425	0.016	0.275	0.225	1.124	1.067	12.599 11.429	<u>1.377</u> 1.231	<u>9.178</u> 7.515	6.508	<u>35.247</u> 32 392	34.719
61 65	25.371	+0.56 +0.42	+1.109		0.549		0.209							0.282				11.036	1.205	8.256	5.708	33.329	32 809
66	26.534		+1.113		0.823	0.580	0.243	1.223	0.812	0.122	0.322	0.433	0.017	0.343	0.225	1.548	1.520	11.678 13.390	1.283	9.442 10.259	5.970 7.052	<u>38.417</u> 49.937	38.37 48.38
67	32.692		+1.115											0.311				13.789	1.481	9.911	7.356	50.257	47.97
63	34.032		+1.117											0 229				14.023	1.486	8.912 4.066	<u>7.657</u> 2.894	<u>48.702</u> 18.043	45.09 17.50
69+1-	12.863	+0.37	+1.121	+0.80	0.751	0.430	0.321	1.151	0.776	0.161	0.361	0.456	0.051	0.403	0.225	1.381	1.440	5.520 7.414	0.598	6.685	3.631	22 281	23.42
<u>70</u> 71	31.090	+0 30	+1.122		0.772 0.824									0.425 0.418			<u>1.46</u> 3 1.522	[4.300	1.606	13.110	6.995	44,144	46 39
72	28,466	+0.48	+1,126	+0.83	0.646	0.350	0.296	1.046	0.723	0,148	0 348	0.449	0.050	0.366	0.225	1.291	1.322	12.897	1.438	<u>11.164</u> 11.141	<u>6.405</u> 7.043	<u>39.145</u> 41.294	40.478
<u>- 73</u> 74	31.611		+1.128											0.346 0.414			<u>1.347</u> 1.729	14.026	1.547	12.007	7.112	48.242	48,619
75	<u>31.923</u> 32.574		+1,133											0.380				14.380 15.196	1.599	12.666	7.183	47,468 42.063	48.65 45.220
76	30,692		+1.137											0.471 0.339				14.212	1.601	12.421	6.906	37,402	39.98
- <u>77</u> - <u>78</u>	28.105	+0.56	+1.140											0.330				12.449 12.439	1,372	<u>9.399</u> 9.435	6,324 6,348	33.464 35.015	<u>33.72</u> 35.05
79	28,215		+1.146		0.565									0.338				13.283	1.462	9.938	6.765	35.635	35.77
<u>80</u> 81	29.804		+1.149		0.489		0.212	0.872	0.636	0.106	0.306	0,424	0.046	0 <u>.323</u> 0.277	0.225	1.191	1.128	12.880	1.402	<u>8.928</u>	6.706 6.254	<u>34.821</u> 34.494	<u>33.89</u> 30.77
82	27.795		+1.155				0.085	0.835	0.618	0.043	0.243	0.386	0.039	0.172	0.225	1.291	1.086	11.244	<u>1,179</u> 1,205	<u>6 233</u> 6 330	6.527	39.404	34.95
<u>- 83</u> 84	29.537		+1,157											0.264 0.333				12.481	1.342	<u>8.821</u>	6.646	42,930	40.95
85	<u>29.696</u> 29.642	+0.34	+1.161	+0,84	0.821	0.500	0.321	1.221	0.811	0.161	0.361	0.156	0.051	0.415	0.225	1.459	1.518	<u>13,189</u> 13,486	<u>1.456</u> 1.507	11.098 12.035	<u>6.682</u> 6.669	<u>43.659</u> 42.420	44.06 44.01
86	30.705	+0.43	+1.162				0.312	1.16 <u>2</u> 1.133	0.781	0.156	0.356	0.454	0.051 0.050	0.397 0.376	0 225 0 225	1.403 1.392	1.452	13.840	1.539	11.878	6.909	42.911	41.08
88	33.344	+0.52	+1.164	+0.87	0.611	0.350	0.291	1.044	0.722	0.147	0.347	0.448	0.050	0.364	<u>0.225</u>	1.291	1.320	<u>14.940</u> 15.476	<u>1.656</u> 1.705	12.346 12.039	7.502	<u>44.735</u> 44.785	45.67 45_C
<u>89</u> 90	- 30.818	+0.58	+1.165											0.324 0.361				13.785	1.527	10.549	6.934	35.661	36.41
90+1	11.148	+0.85	+1.167	+0.90	0.317	0.050	0.267	0.717	0.559	0.134	0.334	0.440	0.048	0.298	0,225	0.956	0.954	<u>5.007</u> 6.970	<u>0.556</u> 0.800	<u>3.671</u> 6.107	2.508	13.900	<u>11.51</u> 16.14
91	23.993	140.56	+1.167 +1.168	+0.62	0.607	0.060	0.547	1.007	0.704	0.274	0.474	0.524	0.062	0.547	0.225	0.967	1.279	12.722	1.521	14.404	5.398	26 288	34,31
<u>92</u> 93	22.833	1+0.10	+1.169	+0.78	0.869	0.480	0.389	1.269	10.835	0.195	10.395	0.477	0.054	0.484	0.225	1.437	1.572	11.566	1,357	<u>12.991</u> 14.773	<u>5.137</u> 6.166	30.378 36.001	<u>35.99</u> 42.01
91	27.405	+0.37	+1.170	+0.63	0.800	0.260	1 0.540	1,200	0.800	0.270	0.470	0.522	0.062	0 594 0.605	0,225	1.191	1.494	14.712	1.746	16.938	6.354	34,731	43.19
<u>95</u> 96	25.900	1.0.19	+1.173			0.410	0.586	1.396	10.898	0.293	0.493	0.536	0.064	0.687	0.225	1.358	1.714	13.671 14.880	<u>1.631</u> 1.777	<u>16.735</u> 18.171	5.828 6.330	<u>34.024</u> 36.486	42 450
97	28.133	+0.34	+1.180	+0.64	0.840	0.300	0.540	1.240	0.820	0.270	0,470	0.522	0.062	0.605	0.225	1.235	1.539	14,138	1.664	15.634	6.232	34.218	41.43
<u>98</u> 99	- 30.491	1+0.42	+1.183 +1.187			0.390	0.577	1.367	0.884	0.289	0.489	0.533	0.064	0.524 0.671	0.225	1.336	1.681	15.733	1.860	18.215	6.860 6.489	<u>39.203</u> 40.145	47.78
100	28.841	+0.16	+1.190	+0.65	1.030	i o 490	0 540	11.430	0915	10.270	0.470	0.522	10.062	0.656	0.225	1.448	1.752	<u>15.215</u> 15.226	<u>1.815</u> 1.772	19.136 17.203	6.894	44.189	50.63
<u>101</u> 102	30.830	<u>1+0.11</u>	+1.193				0.373	1.253 1.296	0.827	0.187	0.387	0.472	0.054	0.467 0.487	0.225 0.225	1.437	1.554	14.609	1.664	14.696	6.937	44,809	48.64
Σ	1692.274															SIDE		781,784	87.991	7(0.272	380.762	2278.501	2413.93
<b>د</b>	<b></b>							·	• : •			<del></del>		R	IGHT	SIDE	• •	860.95264	101.210	939.821	380.537	2172.733	1583.03
the states of the second se		11.	· · ·				:	÷			·					SIDE				1650.093		4451.234	4996.96

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Package 1: D Inspection Road

Name of Structure	INSPECTION ROAD FOR SEMARANG RIVER IMPROVEMENT	Category Calculation	WORK VOLUME	Page	9/2
	SUMMARY OF IN	SPECTION ROA	D WORK VOLU	<u>ME</u>	
1. 8	SAND BEDDING		= 3,519	.82 m <sup>3</sup>	•
2. (	CONCRETE BLOCK		= 58,663	.70 m²	
3. 0	CEMENT MORTAR		= 140	.79 m³	

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INSPECTION ROAD FOR SEMARANG RIVER IMPROVEMEN		Category Alculation			Page	10/2
	241+13, [	<i>,</i> = 5,866.37	m,			
nd Bedding = 0.06 × 5	× 11,732.1	74 = 3,519.8	2 m <sup>3</sup>		• .	
oncrete Block Pavement	$t = 2 \times 0.0$	3 × 0.2 × 11	,732.74 =	58,663.7	m²	
ement Mortar = $2 \times 0.03$	8 × 0.2 × 1	1,732.74 =	140.79 m³	2.1		
oncrete Curb = 2 × 0.2 >	< 0.3 × 11,	732.74 = 1,4	407.93 m³			
-						
• •						
	RIVER IMPROVEMEN ength of Road a. SM No.45 to SM No. r both side = 2 × 5,866. and Bedding = 0.06 × 5 oncrete Block Pavement ement Mortar = 2 × 0.02	ength of Road a. SM No.45 to SM No.241+13, L r both side = $2 \times 5,866.37 = 11,732$ and Bedding = $0.06 \times 5 \times 11,732$ . poncrete Block Pavement = $2 \times 0.00$ cement Mortar = $2 \times 0.03 \times 0.2 \times 10^{-1}$	POR SEMARATO       Catculation         RIVER IMPROVEMENT       Catculation         ength of Road       a. SM No.45 to SM No.241+13, L = 5,866.37         r both side = $2 \times 5,866.37 = 11,732.74$ m       and Bedding = $0.06 \times 5 \times 11,732.74 = 3,519.8$ oncrete Block Pavement = $2 \times 0.03 \times 0.2 \times 11$ cement Mortar = $2 \times 0.03 \times 0.2 \times 11,732.74 = 3,519.8$	FORSEMARANG RIVER IMPROVEMENTCatculationVOLUength of Road a. SM No.45 to SM No.241+13, L = $5,866.37$ m, r both side = $2 \times 5,866.37 = 11,732.74$ mand Bedding = $0.06 \times 5 \times 11,732.74 = 3,519.82$ m <sup>3</sup>	FORSEMARANG RIVER IMPROVEMENTCalculationVOLUMEength of Road a. SM No.45 to SM No.241+13, L = 5,866.37 m, r both side = $2 \times 5,866.37 = 11,732.74$ mwith side = $2 \times 5,866.37 = 11,732.74$ mand Bedding = $0.06 \times 5 \times 11,732.74 = 3,519.82$ m³oncrete Block Pavement = $2 \times 0.03 \times 0.2 \times 11,732.74 = 58,663.7$ ement Mortar = $2 \times 0.03 \times 0.2 \times 11,732.74 = 140.79$ m³	FORSEMARANG RIVER IMPROVEMENTCalculationVOLUMEPageength of Road a. SM No.45 to SM No.241+13, L = 5,866.37 m, r both side = $2 \times 5,866.37 = 11,732.74$ mand Bedding = $0.06 \times 5 \times 11,732.74 = 3,519.82$ m³ oncrete Block Pavement = $2 \times 0.03 \times 0.2 \times 11,732.74 = 58,663.7$ m² ement Mortar = $2 \times 0.03 \times 0.2 \times 11,732.74 = 140.79$ m³

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Package 1: E Miscellaneous Works

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Name of Structure	SECONDARY CHANNEL OUTLET CLOSING ON SEMARANG RIVER	Category of calculation	WORK VOLUME	Page 1/1
	ARY OF SECONDARY CH RANG RIVER, WORK VOI		ET CLOSING ON	
I. STI	RUCTURAL EXCAVATION		= 179	9.71 m <sup>3</sup>
2. CH	IPPING OF EXISTING OUT	LET SURFACE	= 108	8.13 m <sup>2</sup>
	NCRETE TYPE CI INCLUE	an Maria di Santa		2.97 m <sup>3</sup>
	FORM			
		and a second		
4. BA	CKFILL WITH SELECTED	SOIL	= 152	2.93 m <sup>3</sup>
e a				
			• •••	• • • • •
			· · · · · · · · · · · · · · · · · · ·	

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NQ.	POSITION	4 ·	r ·								
INQ.			1	OIMEN	ISION				WORK V	OL LINE	
- F		TYPE	W	h	н	T	CHIPIN	G FORM	MASS	STRUCTURE	FARTH
L	STRUCTURE	1	(mm)	(mm)	(mm)	( , , , , , , , , , , , , , , , , , , ,	(m <sup>2</sup> )	(m <sup>2</sup> )	CONCRETE	EXCAVATION	! FILL
1	SML. 24+5	1	1 500	050	4 200		1	-	1 (m3)	(m <sup>3</sup> )	[ [m3]
			1,500	950	1,300	500	1.70	4.15	1.04	1.11	2.47
2	SML.31+5	1 11	-	270	1,490	500	0.64	7.38	1.85	4.74	3.36
3	SML 54 ±17	1	1,810	1,230	2,550	900	1 00	+	+		· · ·
4	SMR. 22+20	11		f			3.84	12.72	5.72	10.07	7.79
			4,000	1,060	1,060	500	6.12	8.48	2.12	ł	5.51
5	SMR. 42+6	- 11		250	840	500	0.59	2.08	0.52	0.99	0.61
6	SMR.49+11	1	1,000	1,000	1,730	650	1.95		<u> </u>	j	-
7	SMR . 52+29			}			····	4.53	1.47	2.55	2.63
8	····	⊢-···		<u> </u>							
<b>_</b>	SMR. 54+10			460	1,180	500	1.08	3.73	0.93	1.77	1.12
9	SML.56+30	- 11		100	330	500	0.24	0.32	0.08	0 13	!
10	SML.57+31	1	480	240	730			1			0.07
11	SML .60+12					500	0.48	1.18	0.30	0.89	0.66
<u> </u>			510	60	550	500	0.32	1.04	0.26	0.91	0.60
12	SML .61+5	1	750	500 ·	1,310	500	0.88	3.28	0.82	2.67	2.18
13	\$ML.62+0	H.		120	140	500	0.28	0.58	0.14		·
14	SML 62+26	1	630	590	}	·				0.01	0.01
15	SML .64+15				1,490	500	0.91	3.50	0.88	3.05	2.49
h			680	500	1,430	500	0.84	3.67	0.92	3.34	2.65
16	SMR.65+11	H	-	170	630	500	0.40	1.20	0.30	0.55	0.33
17	SMR.55+11.	Ш	_	370	1,150	500	U. 87	3.80	0.95	1.93	
18	SMR.55+5	1	850	390				•			1, 24
-19	SMR. 57+0				1,120	500	0.82	2.97	0.74	2.35	1.87
20	SMR.61+22	11	-	120	870	500	0.28	2.63	0.66	1.43	0.97
21	SMR .63+13	11	-	160	510	500	0.38	0.75	0.40		• • • • • • • • • •
22	SML.66+26		800					}-· -· -	0.19	0.32	0.18
i	·		890	530	1,380	500	0.98	3.90	0.98	3.15	2.62
23	SML .70+11	1	2,000	1,100	2,280	800	3.36	11.90	4.76	8.66	7. 22
24	SML .72+49	1	970	850	1,860	650	1.74		···	• • • •	
25	SML .73+29	11						5.65	1.04	4.52	3.24
		'		170	830	500	0.40	2.24	0.56	1.15 📑	0.73
26	SML .72+28		600	1,720	2,840	1,050	4.24	5.92	3.11	4.67	3.22
27	SML .74+33	I I	480	1,340	2,270	850	2.69	3.94	1 66	1	·
28	SML.81+47							3.91	1.66	- <u>2.99</u>	2.32
F			720	1,720	2,650	1,000	4.16	5.55	2.78	3.42	3.01
29	SMR.81+19	-1	510	1,760	2,810	1,050	4.23	5.07	2.66	3.90	2.86
30	SMR. 83+8	1	540	1,710	2,770	1,050	4.16	5.24	2.75	4.04	2.94
34	SML. 83+13	1	2,780	1,230	2,460	850				i	
32	SML.89+27					}	4.45	16.70	7.10	11.36	9.82
			1,600	1,220	2,210	800	3.23	9.03	3.61	5.60	5.20
33	SMR.91+3		2,720	2,000	4,160	1,550	10.42	31.96	24.77	32.23	25.86
34	SML.98+6		730	870	1,370	500	1.24	2.50	0.63	1.14	1.49
35	SML .106+6	1	2,450	1,440	2,840	1,000	5.33	17.84			•••
36	SHI (071.00					.,			8.92	13.23	19.36
}	SML .107+22	<u> </u>	1,990	820	1,800	600	2.13	9.08	2.72	6.26	6.43
37	SML .115+22	н		600	1,360	500	1.41	4.70	1.17	2.19	1.39
38	SML .115+24	1	2,320	1,700	2,660					<u>-</u>	
39			-,			1,000	5.72	7.00	3.50	6.68	7.13
	SML.116+32		·	1,000	1,910	700	2.36	8.51	2.98 -	3.77	2.36
40	SML. 116 +32	1	910	620	950	500	1.08	1.95	0.49	0.70	1.04
41	SML.116+33	11	-	280	610	500	0.66	0.93			
42	SMR.119+14	1	600					i-	0.23	0.35	0.20
			600		640	500	0.80	0.81	0.20	0.16	0.41
43	SMR.120+22	_!	1,172	500	610	500	1.09	1.45	0.36	G. 22	0.74
44	SMR .123+2	a	- 1	600	1,170	500	0.66	3.23	0.81	· · ·	
45	SML .123+11		600			——— i				1,26	2.81
+			500	650	910	500	0.90	1.05	0.26	0.33	0.56
46	SML 124+29		610	1,100	1,110	500	1.41	1.35 ;	0.34	0.11	V.91
47	SML.126+1	1	610	730	1,130	500	1.04	1.70	0.43	0.72	0.95
48	SML .126+2	1	_	600						··· - ···	• • • •
	····	}			810	500	0.66	1.24	0.31	0. 28	0.21
	SML.128+1	_!!		1,000	1,870	700	2.36	8.07	2.82	3.48	2.18
50	\$ML,426 +29	"	-	130	890	500	0.31	2.73	0.68	1.49	1.00
51	SMR.130+18	11		800	1,530	550	1.88	5.47			
52	SML.120+33	}	_ <b>_</b>						1.50	2.28	1.48
				1,000	2,060	700	2.36	10.29	3.60	5.03	3.16
	SML .431 +2			1,000	1,830	650	2.36	7.64	2.48	3.19	2.08
54	SMR.133+20	B		800	1,290	500	1.85	3.53	0.86	1.16	0.82
100	SML ,139+11	11	-	800	1,090	500	1.88		•••• i-	•	····
55							1.00	2.26	0.57	0.53	0.46
}	SMI AAO 170	I		I	!						
}	SML .140+32	н		800	1,130	500	1.88	2.49	0.62	0.64	0.51

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TABLE OF SECONDARY CHANNEL OUTLET CLOSING ON SEMARANG RIVER