Name of Structure	2000年 東邦港 3	Asin Gate	Category of calculation	Stress Analysis	Page	75/416
		er Estate				
	artyr i			in the second of the first of the second of		
				and the second section of the sectio		
				ing the state of t		
1			2			3
				arandak a najaharatan Tanggaran		
			المادية المادي المادية المادية المادي		Symmetric Symmetric	
						8
						3,960
	ing die der die der die der der die der der der der der der der der der de	a di kacamatan di k Kacamatan di kacamatan di kacama		g Popisi je sapaja nji	ing Ny Amerika	
			galanda da d			
. · L	<u>5</u>	· · · · · · · · · · · · · · · · · · ·	<u>π </u>	<u> </u>	Δ	9 10
·	<b></b>		10.600		ing the life	<b>→</b> 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		entino di Terresia. Ngjara		Δ Pil	e Locati	on
				Figure	- 31	
					4	
						•
		t programme in the second of t				
mara met S						

Name of	Asin Gate	Category of	Stress Analysis	Page	76 / 116
Structure		calculation		1	

Case-5: Seismic condition, No water

Case-7: Seismic condition, Water at right

Case-6: Seismic condition, Water at left Case-8: Seismic condition, Water at both

Loads to be considered are as follows:

- self-weight
- water weight and water pressure
- · earth pressure
- · weight of O/M bridge and O/M equipment
- earthquake force

Load conditions are shown in Figure-32 to Figure-39.

#### 4) Results of stress analysis

Summary of results are as follows:

(details see attached Figure-40 to 47)

		Nor	mal		
	1	2	3	4	
Bending Moment	25.828	29.204	29.204	30.186	
Shear Stress	41.625	41.625	43.410	41.625	
Axial Stress	62.100	62.100	62.100	62.100	
Displacement	0.1819	0.2049	0.2101	0.2365	
	Seismic				
	5	6	7	8	
Bending Moment	33.674	38.961	35.991	41.508	
Shear Stress	41.625	41.625	41.625	41.625	
Axial Stress	62.100	62.100	62.100	62.100	
Displacement	0.2477	0.2324	0.2625	0.2870	

#### 3. O/M Bridge

Refer to the results of Baru Gate.

 $\gamma_{i} = \frac{1}{4} (\gamma_{i} + \gamma_{i}) \frac{1}{4} (\gamma_{i} + \gamma_{i})$ 

Case 1 : normal-dry

	Load
1	1.285 (tf)
(3)	0.500 (tf)
3	7. 282 (tf)
4	2.885 (tf)
5	7. 500 (tf)
6	22.500 (tf)
7	15.000 (tf)
Self-v	veight included

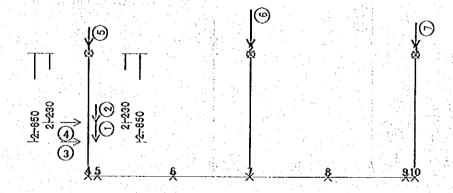
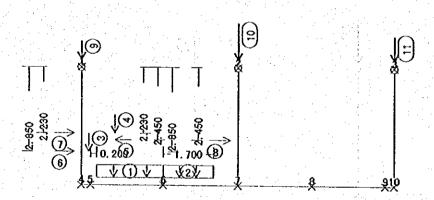


Figure - 32

Case 2 : normal-left water

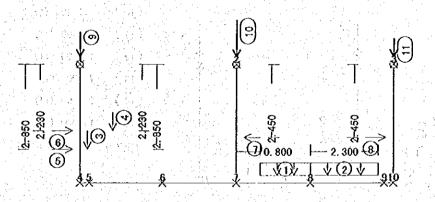
	Load
1	7.550 (tf/m)
	7.550 (tf/m)
(2)	7.550 (tf/m)
	7.550 (tf/m)
3	1.285 (tf)
4	0.500 (tf)
(5)	-11.400 (tf)
6	7. 282 (tf)
0	2.885 (tf)
8	11.400 (tf)
9	7.500 (tf)
(10)	22,500 (tf)
(II)	15.000 (tf)
Self-w	eight included



Case 3 : normal-right water

Load 7.550 (tf/m) 7.550 (tf/m) 2 7.550 (tf/m) 7.550 (tf/m) (3) 1.285 (tf) 0.500 (tf) (5) 7.282 (tf) 6 2.885 (tf) -11.400 (tf) (i)(8) 11.400 (tf) (9) 15,000 (tf) (10) 22.500 (tf) (11) 7.500 (tf)

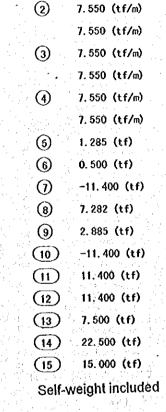
Self-weight included



(

### Asin Pier+Footing (Normal)

Case 4 : normal-wet

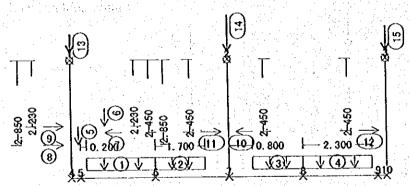


Load

7.550 (tf/m)

7.550 (tf/m)

(i)



# Asin Pier+Footing (Seismic) Case 1 : seismic-dry

Load

- 11.625 (tf)
- (2) 0.825 (tf)
- (3) 7.500 (tf)
- (4) 2.475 (tf)
- (5) 22.500 (tf)
- (6) 1.650 (tf)
- (7) 15.000 (tf)

#### Self-weight included

Seismic Force KH = 0.11

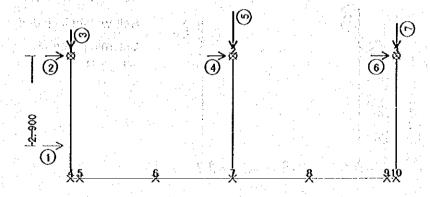


Figure - 36

Asin Pier+Footing (Seismic)

Case 2 : seismic-left water

<b>\</b>		( <del>-</del> )	
	1.9		
900	86 - <u>6</u>		
(a) 1 (b) 200 (c) 1 (c)	₩ - 6 - 1. 700 b		
X <del>X</del>	<del>-                                    </del>	<del>-</del>	<del>\$10</del>

Load (1) 7.375 (tf/m) 7.375 (tf/m) 2 7.375 (tf/m) 7.375 (tf/m) (3) -10.900 (tf) 4 11.625 (tf) (5) 10.900 (tf) **(6)** 0.555 (tf) (7) 0.825 (tf) (8) 7.500 (tf) (9) 2.475 (tf) (10) 22.500 (tf) (11) 1.650 (tf) (12) 15.000 (tf)

Self-weight included

Seismic Force KH = 0.11

Case 3 : seismic-right water

Load

7.375 (tf/m)

7.375 (tf/m)

7.375 (tf/m) 7.375 (tf/m)

11.625 (tf)

-10,900 (tf)

0.555 (tf)

1.650 (tf)

15.000 (tf)

2.475 (tf)

22.500 (tf)

0.825 (tf)

7.500 (tf)

Self-weight included

Seismic Force KH = 0.11

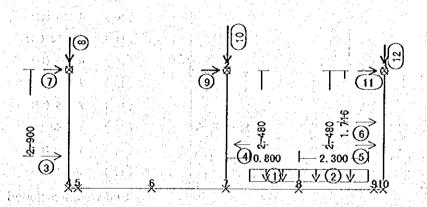
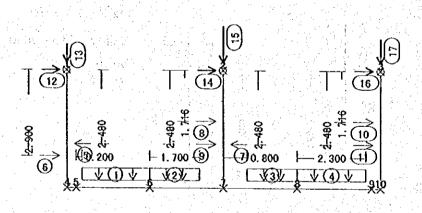


Figure - 38

## Asin Pier+Footing (Seismic) Case 4 : seismic-wet



	Load
1	7.375 (tf/m)
	7.375 (tf/m)
2	7.375 (tf/m)
	7.375 (tf/m)
3	7.375 (tf/m)
	7.375 (tf/m)
4	7.375 (tf/m)
	7.375 (tf/m)
(5)	-10.900 (tf)
6	11.625 (tf)
0	-10.900 (tf)
8	0.555 (tf)
9	10.900 (tf)
(10)	0,555 (tf)
	10.900 (tf)
(12)	0.825 (tf)
13	7.500 (tf)
14	2. 475 (tf)
(15)	22.500 (tf)
(16)	1.650 (tf)
(17)	15.000 (tf)
Self-w	eight included
Seismi кн = 0	ic Force . 11

Asin Pier+Footing (Normal) Case 1: normal-dry Deformation

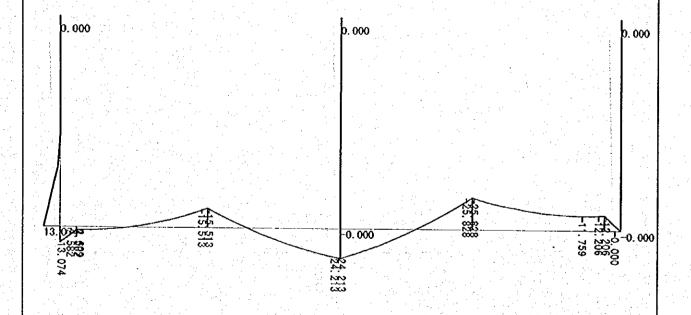
Figure - 40 (1)

()

Asin Pier+Footing (Normal)

Case 1: normal-dry

Bending Moment Scale | : 30.19tf·m max. : -25.83 tf·m



Asin Pier+Footing (Normal) Case 1: normal-dry **Shear Stress** Scale |----|: 43.41tf | max.: 41.63 tf 0.000 0.000 0.000 0.000 Figure - 40 (3)

()

Asin Pier+Footing (Normal) Case 1: normal-dry **Axial Stress** Scale |----- : 62.10tf max. : 62.10 tf **1**, 500 15.000 22 500 8.975 Figure - 40 (4)

90/116

 $k = 1 + \frac{1}{2} + \frac{1}{2} + \frac{1}{2} + \frac{1}{2}$ 

Asin Pier+Footing (Normal)

Case 2: normal-left water

Bending Moment Scale | : 30. 19tf·m max. : 29. 20 tf·m

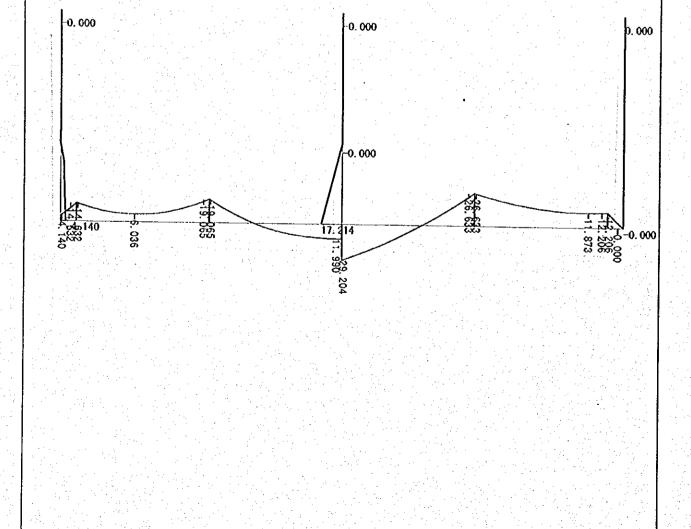


Figure - 41 (2)

Case 2: normal-left water

**Shear Stress** 

Scale |----|: 43.41tf

max.: 41.63 tf

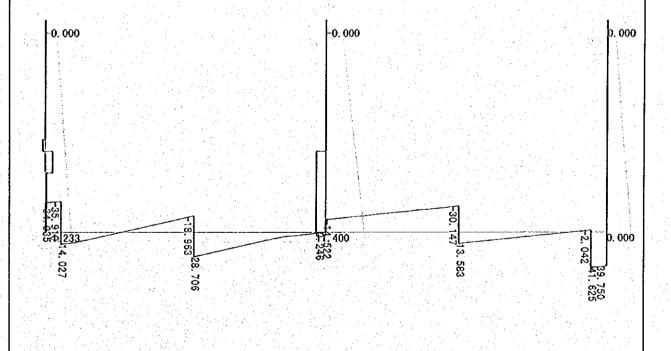


Figure-41 (3)

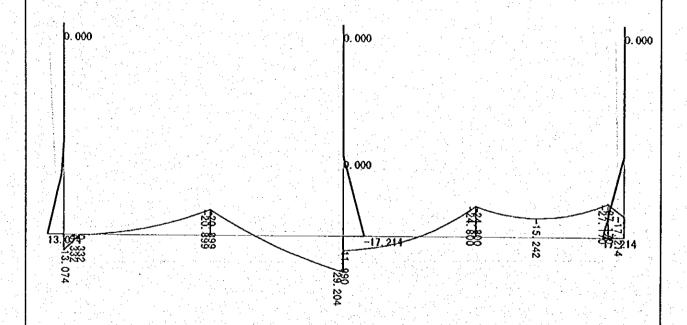
Asin Pier+Footing (Normal) Case 2: normal-left water **Axial Stress** Scale |---|: 62.10tf max.: 62.10 tf []. 500 15.000 22 500 62. 109. #. 63 63

Asin Pier+Footin	g (Normal)				
Case 3: normal	-right water				
			•		
Deformation	Scale   :	0. 237cm n	1ax. : 0.210 cm	1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		•	•		
					•
			* *		
			•		
			•		
er de la companya de					

【 (注: X ) . 注 ( ) \$ ( ) ; ( )

Case 3: normal-right water

Bending Moment Scale |----|: 30.19tf·m max.: 29.20 tf·m



Case 3: normal-right water

**Shear Stress** 

Scale | : 43.41tf | max. : -43.41 tf

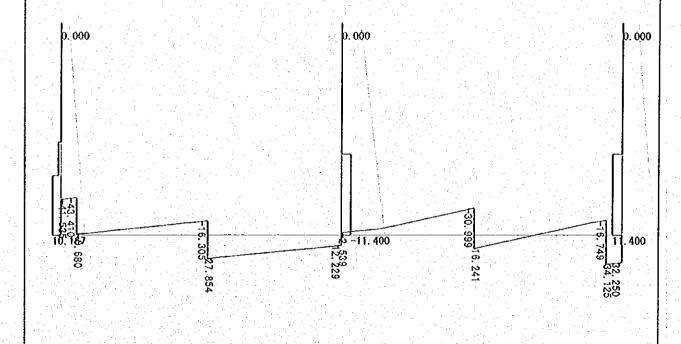
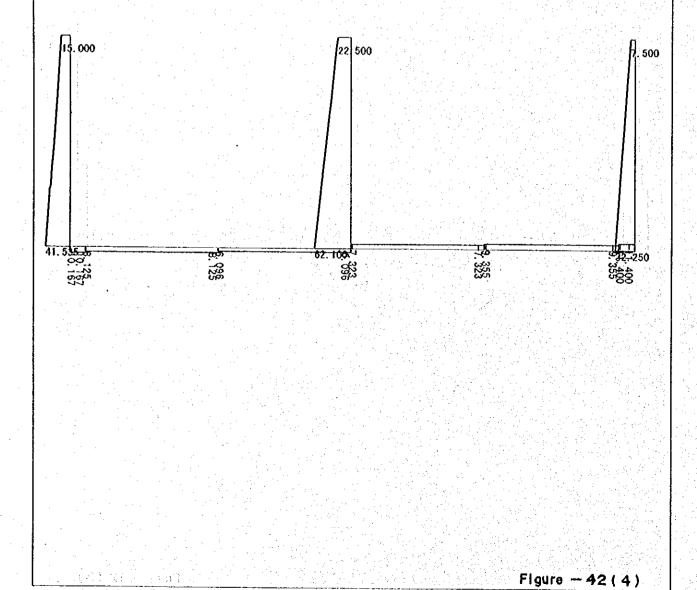


Figure - 42 (3)

Case 3: normal-right water

**Axial Stress** 

Scale |----|: 62.10tf max.: 62.10 tf



Asin Pier+Footing (Normal)  Case 4: normal-wet					
Ogot 4. homer not		•	\$ · ·	-	
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2					
Deformation Scale   : 0.237cm max.: 0.237	1 cm		1 + 1 ·	Mark the second	
		•			
				*	
			-		
	•				
	:				
					*
	:				
en e					
					,
				111	
		. •	*		
				٠	
				**	
				1 -	
				in the second	
			* **	1	
				: • 1	ļ
				100	
					ļ
				- <u> </u>	
					1
			100	<u> </u>	11
	<u> </u>		1 1	1000	1
		:			)
					٠.
					٠.
连续的 医阿里斯氏氏征医氏征 医二十二氏征		e e e e e e e e e e e e e e e e e e e			
					1
			I surface		
秦朝的自己的原始,只是此的对方,不管的也是	e e e				
	and the second second	And the second second			

Case 4: normal-wet

Bending Moment Scale |----|: 30.19tf·m max. : -30.19 tf·m

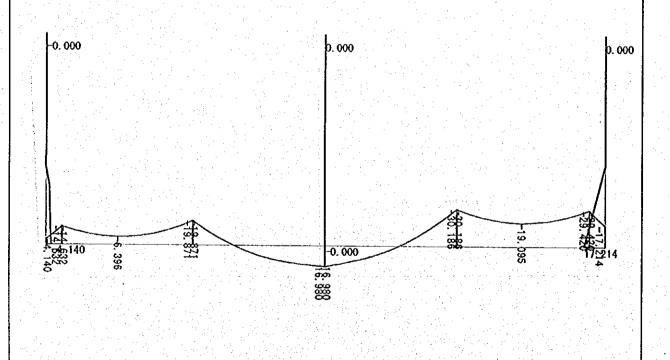


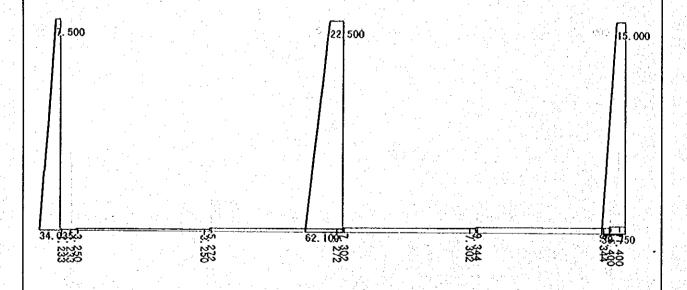
Figure - 43 (2)

Asin Pier+Footing (Normal) Case 4: normal-wet Shear Stress Scale |----|: 43.41tf | max. : 41.63 tf 0.000 0.000 000 Figure - 43 (3)

Case 4: normal-wet

Axial Stress

Scale |----|: 62.10tf max.: 62.10 tf



Asin Pier+Footing (Seismic)	the state of the s
Case 1: seismic-dry	
Deformation Scale ├────────────────────────────────────	<b>0.248 cm</b>
	•
	·
[존문] 볼 바다 그들는 그리고 안 먹다 보고 있다.	
그래면 한 얼마나는 어때는 건데 그렇게	
트림했다. 중요 중이 하다 하고 생기 있는 아이들이다.	
<u> </u>	
불지하는 사람들은 사람들이 되었다.	
그 후반 등으로 돌못하다 하나 있는데 그리다 하고 있다.	Figure - 44 (1)

Case 1: seismic-dry

Bending Moment Scale |--- : 41.51tf·m max.: 33.67 tf·m

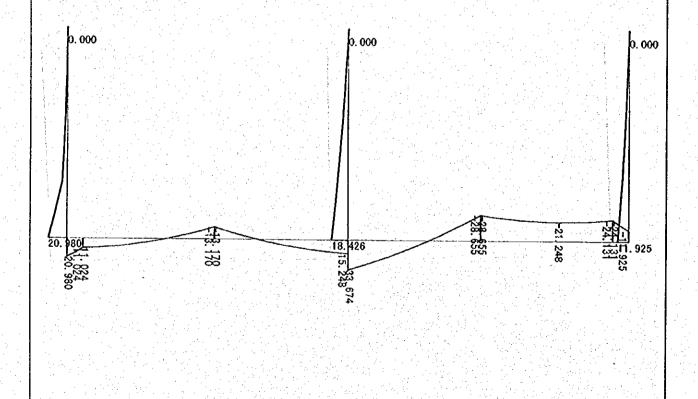


Figure - 44 (2)

Asin Pier+Footing (Seismic) Case 1: seismic-dry Shear Stress Scale |---|: 41.63tf max. : 41.63 tf 2. 475 D. 825 1.650 622 Figure - 44 (3)

Case 1: seismic-dry

Axial Stress

Scale |---|: 62.10tf max. : 62.10 tf

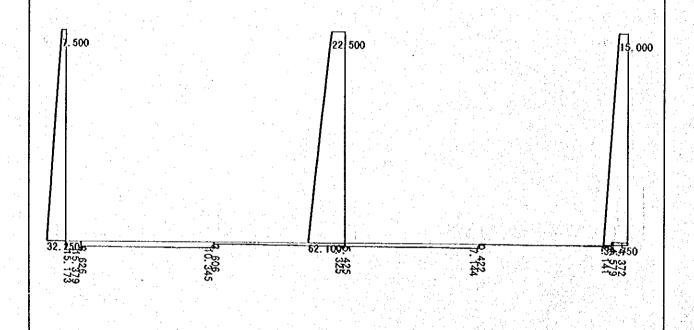
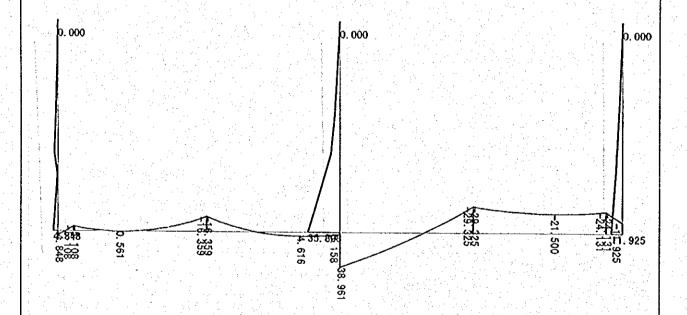


Figure - 44 (4)

Case 2: seismic-left water  Deformation Scale   : 0.287cm Max. ; 0.232 cm	Asin Pier+Footing					A LANGE OF A
	Odse 2: seismic	rert water	•		•	
	Deformation	Scale	: 0. 287cm	max. : 0.232 cm		iste date to
		•				
						•
						1 1 1
				1		1
						- 31
		** *				
						21. 1. 2. 1.
						4
그는 문화 그릇을 가는 사람들이 얼마나는 살이 보는 사람이 나는 말을 하는 것이다.						
我看过了一直再说,说话,我看到一块的话,还是说,一个一点一点,还是这一点,不是一个一直看了一点,就是一个一块,一点一点一点,不						
#####################################						

Printer Spilling

Case 2: seismic-left water



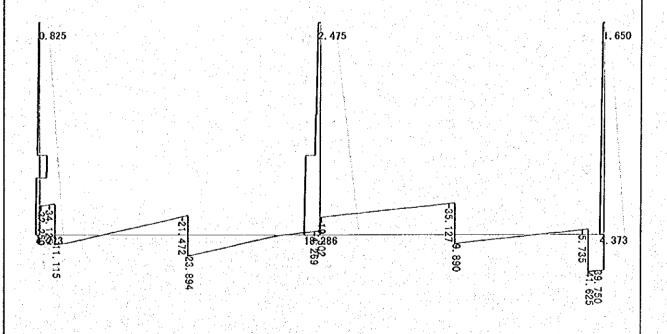
Case 2: seismic-left water

Shear Stress

美国美国民产品的国际

(

Scale |----| : 41.63tf max. : 41.63 tf

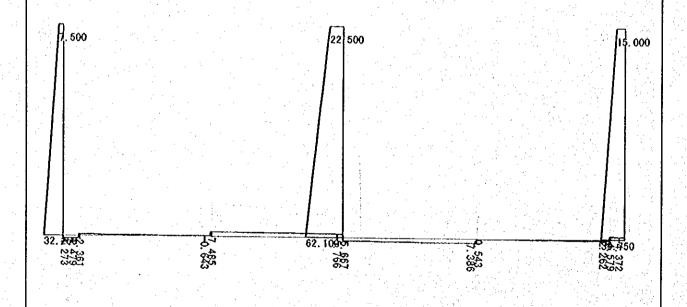


Case 2: seismic-left water

**Axial Stress** 

Literative designation

Scale |----|: 62.10tf max.: 62.10 tf



Asin Pier+Footing (Seismic)	
Case 3: seismic-right water	and the control of the control of the second
Deformation Scale   : 0.287cm	max. : 0.263 cm
원인도 불편되지 않아 등 사람이 보냈다. 물이	
	[ 종류회교 ( 우리 그 다니 - 트립트 )
그는 아이는 가는 경기들으로 먹는 남이 동생을 하는	
"我们是不是不得到的,我们们是我们的一种,我们不是一定的,我们就是一个人的。" 化二氯化二氯化二氯化二氯	
	2 값 돌려.하셨습니까 용상하는 그리다면

121366 8 800

Case 3: seismic-right water

Bending Moment Scale : 41.51tf·m max. : -35.99 tf·m

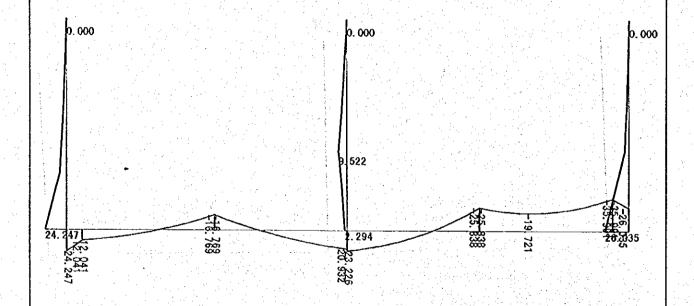


Figure - 46 (2)

141.程序的系统。

Case 3: seismic-right water

**Shear Stress** 

Scale |----|: 41.63tf | max. : -41.62 tf

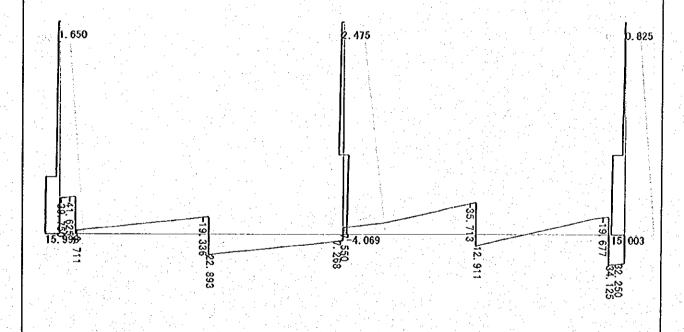
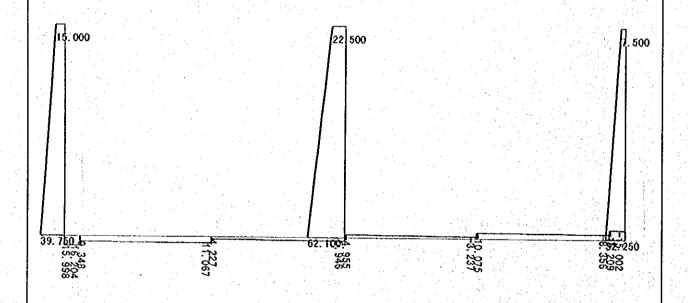


Figure -46 (3)

Case 3: seismic-right water

**Axial Stress** 

Scale |----|: 62.10tf | max. : 62.10 tf



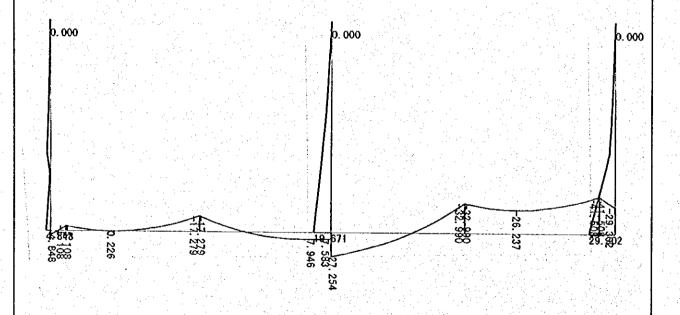
Asin Pier+Footing (Seismic)
Case 4: seismic-wet
Deformation Scale
Tangging Hand State
│ 요리를 만들었다. 중화하는데 경화를 열고하는데 요마요 ㅎㅎ 한다는데 되는데 되는데 하는데 하다.
[파르돌팔프] [11] 프린스 레이트 프린스 레이트 프로그 네트 네트 네트 네트 네트
[ ] 그렇게 할아 먹는데 하는 마음의 그들도 있는데 먹는 말했다면 하다고 있는 다른데 다음
] : [ [ [ [ [ [ [ [ [ [ [ [ [ [ [ [ [ [
1975   1975

Case 4: seismic-wet

( to be about )

**Bending Moment** 

Scale | : 41.51tf·m max. : -41.51 tf·m

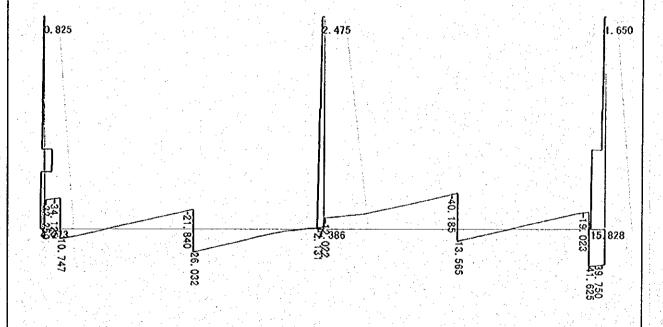


Case 4: seismic-wet

Shear Stress

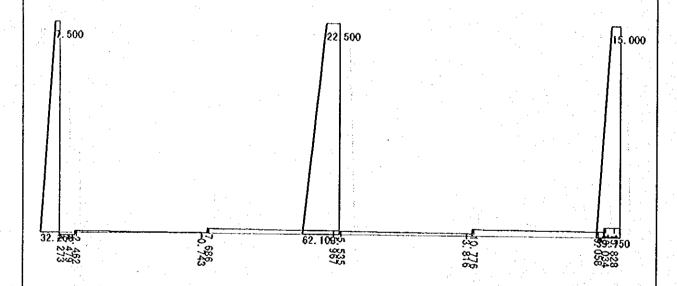
(E)

Scale |---|: 41.63tf max. : 41.63 tf



Case 4: seismic-wet

Axial Stress Scale |----|: 62.10tf max.: 62.10 tf



- 2.1 Asin Pumping Station
- 2.1.4 Reinforcing Bar Arrangement Calculation of Gate

N. C.					
Name of Structure	Asin Gate	Category of calculation	Reinforc arrange	T PHOD	1/10
General cond Allowab Allowab Allowab Minimu	ate frame 2) Pier and tition of calculation le compressive stress of concrete tensile stress of rein coverage of concrete m ratio of reinforcing by	of concrete: rete: nforcing bar: : 15 cm at footi	3) O/M bridge  Normal 75 kg/cm <sup>2</sup> 7.5 kg/cm <sup>2</sup> 1400 kg/cm <sup>2</sup>	Seismic 112,5 kg/cm <sup>2</sup> 11,25 kg/cm <sup>2</sup> 2100 kg/cm <sup>2</sup>	
end column of (II) as shown	rts of main reinforcing f gate (I, III), center col in following Fig1. St are also shown in Fig-	lumn of gate (IV) tress checkpoints	, footing of gat	e (V) and slab of c	ontrol room
2	4 II 5 6 7 II 8	<b>9</b>			
I	IV	III Me	mber I, III: mber IV: mber V: mber II:	end column of ga center column of footing of gate slab of control ro	gate frame
1	17 V V V V V V V V V V V V V V V V V V V	10 1 to	18:	checkpoint of me	mber stress

Stresses at each checkpoint are shown in Table-1.

Load for calculation and cross section of each member are shown in Table-2 and Fig-2.

Main reinforcing bar arrangement (calculation results are shown in Table-3)

Member I, III: end column of gate frame

① (outside) : D19@125 mm ② (inside) : D16@125 mm ③ : D13@125 mm

Member IV: center column of gate frame

① : D16@125 mm ② : D13@125 mm

Member IV: footing of gate

① and ② : D22@125 mm

Member II: slab of control room

① : D22@125 mm ② : D19@125 mm

24,103 0.819 31.689 29.707 52.179 23.976 2.000 14.686 49.089 26.661 2.209 42.658 58.095 -0.028 6.745 . O ß 0 50.000 24.103 2.000 51.120 -2.209 2.209 26.661 -0.576 -2.435 61.437 92.535 S S 1.054 -4.057 ⋖ -13.769 -29.957 15.008 -3.697 13.769 14.245 -29.251 -19.766 -15.431 -33.659 4.270 28.288 -28.016 -15.43137.218 -18.8540.706 8.931 Z 26.545 31.845 29.507 24.343 53.458 5.508 1.674 2.536 43.986 43.274 17.317 22.831 53.541 8.627 6.091 0.862 Ö Ŋ 0 26.505 52.402 34.343 2.536 5.598 48.812 -8.627 -15.903-12.024 -2.087 <u>.</u> 1.674 92,450 61.352S ď <del>---</del> 15.397 28.168 -30.778 -15,397 14.667 14.630 -13.959-30.750 -13.95911.054 -25.855 -12.641 32.104 -30.936 3.237 37.079 4.975 2.581 × Normal -1.996 29.708 29.519 0.815 24.142 24.331 58.569 49.707 16.978 51.089 0 15,536 50.457 1.710 8.663 0.286 ζŊ 0 24.142 50.039 -8.663 -7.006 -4.032 48.800 0.815 1.996 -5.318 1.710 24.331 90.324 59.226 F C ∢ -28.255 13.812 -29.085 -3.616 -13.81214.296 -13.954 14.606 11.379 -13.954-26.176 29.187 -31.15130.882 -29.241 -18.785-0.860 1.695 ⋈ 26.432 31.918 -2.499 31.729 5.635 26.621 52,140 41.290 23.126 21.684 53.379 2.213 42.041 0.286 ഗ 0 52.329 26.432 -0.591 2.365 2,499 51.090 -2.213 1.029 2.213 26.621 94,745 63.647 3.994 5.635 Q E ∢ 14.645 -15.245 -30.983 15.245 .30.124 -15.388 -2.843 14.956 -15.388 -32.43436.319 1.695 49.835 34.624 -30.524-0.860 4.351 3.412 Ζ 7 က 10 2 ដ ¢3 せ 2 Ó rO <u>-</u>  $\infty$ တ Ħ 9 17 8

Stress at checkpoints (Gate frame-Normal condition)

[able-1 (1)

1	
ondition	
Ü	
ismic	
s (Gate frame-Seismic	
(Gate	
計	
Stress at checkpo	•
atc	
58	
Stre	
_	•
<u>ت</u>	
Table-1 (2) Stress	
۲	

Γ		r	Γ	<b>—</b>	T		· · · · ·	<u> </u>	Γ	Γ	T	Г— <del>-</del> -		·	<u> </u>	l	T	Ι	<b>T</b>	1
		Ø	4.622	2.110	18.030	0	35.820	25.655	0	32.695	6.219	6.384	63.973	46.573	34.923	5.568	41.283	43.549	16.367	8.084
	RO	Ą	42.499	18.030	0.264	ţ	4.494	0.879	<b>←</b> -	4.373	32.695	57.164	-7.705	-1.238	4.802	-6.057	-6.268	5.943	92.573	61.475
	· ·	M	16.968	2.360	<b>.</b>	17.760	-45.306	-13.347	15.068	-31.416	-31.416	24.791	-42.098	-38.410	59.836	7.529	-23.090	16.968	52.306	31.347
		S	10.991	4.526	20.424	0	37.926	23.493	0	30.357	5.688	12.786	67.824	48.992	29.029	11.342	38.336	45.943	2.598	9.221
	LO	A	44.893	20.424	0.321	1	5.573	0.936	<b>←</b>	3.821	30.357	54.826	-14.107	-7.908	-2.081	-0.192	5.840	12.312	92.516	61.418
nic		M	23.513	0.683	÷	17.999	-46.895	-12.205	14.646	-29.871	-29.871	31.494	-48.100	-36.279	53.444	14.508	-24.785	23.513	38.936	34.690
Seismic		<b>S</b>	4.424	1.912	18.299	0	35.551	23.616	- 0	30.234	5.607	12.725	71.001	53.940	27.742	4.716	45.929	43.818	8.729	8.339
	FC	<b>. . . .</b>	42.768	18.299	0.066	€	4.691	0.997		3.761	30.234	54.703	-14.046	-7.838	-2.000	-6.232	-6,443	5.745	9.266	59.168
	and the second	M	12.901	1.662	1.662	17.489	-44.582	-12.531	14.583	-29.542	-29.542	31.286	-47.854	-36.504	52.439	8.108	-23.271	15.901	44.330	32.051
		S	11.116	1.651	20.226	0	38.124	25.465	0	32.885	6.352	6.517	64.633	45.779	34.538	10.216	37.257	45.745	9.235	8.995
	FO	A	44.695	20.226	0.195	1.32	5.447	-0.746	<b>—</b>	4.506	32.885	57.354	-7.838	-1.381	4.649	-0.088	5.955	12.437	94.687	63.589
		M	24.132	-1.186	1.186	18.187	-47.444	-13.467	15.157	-39,932	-31.932	25.460	-41.824	-38.114	59.168	12.252	-24.225	24.132	-46.916	33.977
			1	. 2	3	4	5	9	7	8	6	10	11	12	13	14	15	16	17	18

## Table-2 and Figure-2

Table-2 (1)
Member I and III (End column)

		Normal			Seismic	
	0	2	3	(1)	2	3
Moment	16	12	51	32	32	61
Axial Stress	27	49	54	33	55	54
Shear Stress	3	9	16	7	13	19

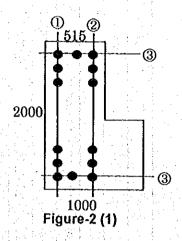


Table-2 (2)
Member IV (Center column)

	Nor	mal	Seis	smic
	0	0	①	2
Moment	9	51	53	61
Axial Stress	93	54	93	54
Shear Stress	7	16	17	19

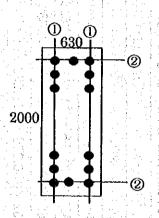
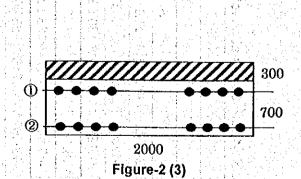


Figure-2 (2)

Table-2 (3)

Member IV (Footing of gate)

	Nor	mal	Seis	smic
	0	2	0	2
Moment	34	38	49	60
Axial Stress	-1	-3	-15	4
Shear Stress	43	23	68	35



# Table-2 and Figure-2 (continued)

Table-2 (4)
Member II (Slab of control room)

ger gereker au	Nor	mal	Seis	mic
	0	2	(1)	0
Moment	31	16	48	19
Axial Stress	3	2	6	0
Shear Stress	32	0	39	0

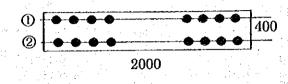
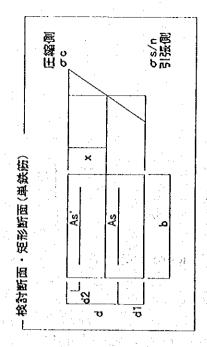


Figure-2 (4)

()



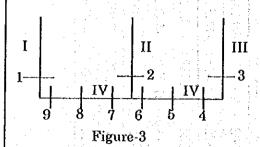
	(t)	Ç.	0 2	0	0	0	0 X	А Д	0 X	о Я	0 X	0 X	0 X	0.000 0 K	О Ж	0 X	У О	0 X	0 X	о Х	
	コンケートかん	7 C C C C C C C C C C C C C C C C C C C	0, 399	0.977	0.943	1, 700	1.207	1.724	4.017	2.354	6.347	3.582	4.044	0.000	4, 929	0.000	0.073	1; 697	0.986	1, 409	
	過	~~~	ο Υ	4 0 ス	レ 0 ス		4 О Х	о Х	4 0 ス	2 م	ი გ	о Х	0 X	4 О Ж	50 K	ა გ	7 7	о Х	0 7	0 7	
sult	鉄筋引張 民士師	(kef/cm2)	651.6	296.	1524.7	1794.1	1001.4	1831.	1033.	1282.1	1596.5	1948.1	1241.0	1306. 4	1916.5	1580.5	37.7	2021.	818	1497.	
Result	沿属		0 3	0 저	0 지	О Қ	0 7	0 자	0 7	42.1 O K	о Я	0 저	о Я	о Я	о Х	O 자	о Х	О Қ	О 7	о х	
計算結果	いが上田額を大田	(kef/cm)	32. 2	25. 1	64. 1	71.9	35. 1	46.8	32. 7	42. 1	46.2	66.8	48.2	53.9	74.7	63.9	14.3	79.8	28.70	38.3	
	せん野力	o t	3.000	9.000	7. 000	13.000	16.000	19,000	43.000	23, 000	68.000	35,000	32, 000	000 0	39, 000	000.0	7.000	17.000	16.000	19.000	Shear Stress
	中華	Z (‡	27, 000	49,000	33,000	55,000	54,000	54,000	-1.000	-3.000	-15,000	4.000	3.000	2.000	6.000	0.000	93.000	93.000	54,000	54, 000	Axial Stress
	田げたが	(Tf.m)	16,000	12,000	32, 000	32.000	51.000	61.000	34,000	38.000	49.000	60.000	31,000	16.000	48, 000	19. 000	9.000	53.000	51.000	61.000	Moment
	鉄筋沢		0.0055	0,000 0,0038	0.000 0.0055	0.000 0.0038	0.000 0.0005	0. 000 0. 0005	0. 000 0. 0052	0.000 0.0056	0.000 0.0052	0.0056	6900 0 000 0	0. 000 0. 0076	0. 000 0. 0069	0. 000 0. 0076	0. 000 0. 0030	0. 000 0. 0030	0. 000 0. 0005	0.0005	
	开格铁 铁纸电影	δ. (Cm <sup>2</sup> )	0.00	0,000	0.00	0.000	0.000	0.000	000 0	0.000	000.0	000 '0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
	3]張鉄筋 鉄筋量	S (2)	45.843	31, 769	45.843	31, 769	5.219	5, 219	61.932	61.932	61.932	61.932	61.932	45.843	61.932	45.843	31. 769	31. 769	6.385	6,385	Area of Reinfor
	計算幅	ာ (ရှိ (ရှိ	200.0	200.0	200.0	200.0	51.5	51.5	200.0	200.0	200, 0	200.0	200 0	200.0	200.0	200.0	200.0	200.0	၀ မ	63.0	
n of Cale	圧縮鉄筋かぶり	ก(€ 20 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0	0.0	0	0	0.0	0.0	0.0	0.0	
Condition of Cale	篵	- °E	10.0	10.0	10.0	10.0	10.0	10.0	10.0	15.0	10.0	15.0	0.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	
斯面形状	<b>一分配が下</b>	σ <sup>(m)</sup>	41.5	41.5	41.5	41.5	190.0	190.0	60.0	55.0	0.09	55.0	45.0	30.0	45.0	30.0	53.0	53.0	190.0	190.0	
1	那所 海州	台灣	1	7	က	4	2	9	7	80	6	0	=	12	13	14	15	16	17	138	

Table - 3

Name of Structure	Asin Gate	Category of calculation	Reinforcing bar arrangement	Page	7/10
				(	L

### 2) Pier and Footing

Calculated parts of main reinforcing bar arrangement are classified into three members, such as end pier (I, III), center pier (II) and footing (VI) as shown in Fig.-3. Stress checkpoints of members for calculation of reinforcing bar arrangement are also shown in Fig-3.



Member I. III: Member II:

end pier center pier Member IV: footing 1 to 5:

checkpoint of member stress

Stresses at each checkpoint are shown in Table-4.

Load for calculation and cross section of each member are shown in Table-5 and Fig-4.

Main reinforcing bar arrangement (calculation results are shown in Table-6)

Member I, III: end pier

> (1) (outside): D19@125 ② (inside) D16@125

Member II: center pier

> ① and ② : D16@125

Member IV: footing

> (1) and (2) D19@125

#### 3) O/M bridge

Conditions for analysis assumed as same as for Baru Pumping Station Gate O/M Bridge. Required reinforcing bar arrangement is D19@125 mm.

		Table-4 S	tress at c	Stress at checkpoints (Pier and Footing)	ts (Pier an	d Footing				i.			Aat :	
			No Water		Wat	Water at Left side	side	Wat	Water at Right side	side	Wat	Water at Both side	side	_
		×	A	တ	M	Ą	മ	M	Ą	S	×	A	V	,
	-	13.074	34,035	10.167	-14.140	34.035	0.233	13.074	41.535	10.167	4.140	34.035	1.233	
	67	0	62.100	0	-17.214	62.100	11.400	-17.214	62.100	11.400	0	62.100	0	
	ო	<b>+</b>	39.750	<b>t</b> -	0	39.750	0	17.214	32.250	11.400	17.214	39.750	11.400	
Ž		-12.206	2.021	43.989	-12.206	0.231	43.667	-27.170	-11.400	50.874	-29.420	-11.400	57.119	
mal		-25.828	4.045	41.090	-26.633	4.066	43.730	-24.800	-9.355	47.240	-30.186	-9.344	52.646	
	9	24.213	€-	12.204	29.204	1	14.522	11.980	-7.323	2.539	16.980	-7.302	6.690	
	2	<b>L</b>	6.075	8.078	11.990	-5.293	0.246	29.204	6.096	12.229	<b>←</b>	-5.272	2.564	
	∞	-15.513	8.115	38.754	-19.065	<b>←</b>	47.039	-20.899	8.125	44.159	19.871	. ←	50.309	
	6	13.074	10.167	35.910	-14.632	-3.261	49.937	13.074	10.167	43.410	-14.632	3.250	49.615	
	П	20.980	32.250	15.173	4.848	32.250	4.273	24.247	39.750	15.999	4.848	32.250	4.273	
	77	18.426	62.100	6.831	35.898	62.100	18.286	9.522	62.100	4.069	19.671	62.100	7.386	
	က	11.925	39.750	4.373	11.925	39.750	4.373	26.035	32.250	15.003	29.302	39.750	15.828	
S.o.s.	4	-24.131	-4.732	47.628	-24.131	-4.732	47.360	-35.991	-15.002	53.802	-41.508	-15.828	60.648	
Bic S	က	-28.655	7.144	42.366	-29.325	7.386	45.017	-25.838	-10.075	48.624	-32.990	-10.760	53.750	
	ဖ	33.674	5.425	17.119	38.961	5.667	19.502	23.226	-4.955	7.550	27.254	-5.535	2.022	
	7	15.248	5.325	5.555	4.616	-5.766	4.269	20.932	5.946	7.268	7.946	-5.967	9.131	
	ω	-13.170	10.345	36.670	-16.359	-7.485	45.366	-16.769	11.067	42.229	-17.279	-7.686	47.879	
	6	-20.980	15.379	34.125	4.848	4.273	45.240	-24.247	16.204	41.625	-6.108	1-	44 879	
													1.	

2 - 182

## Table-5 and Figure-4

Table-5 (1)
Member I and III (End Pier)

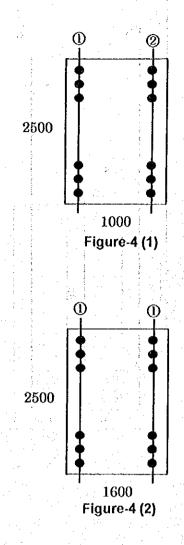
:	No	rmal	Seis	mic
	①	2	0	2
Moment	14	18	25	30
Axial Stress	42	40	40	40
Shear Stress	11	12	16	16

Table-5 (2)
Member I and III (Center Pier)

	Normal ①	Seismic (1)
Moment	- 18	36
Axial Stress	63	63
Shear Stress	12	19

Table-5 (3)
Member IV (Footing of gate)

	Nor	mal	Seis	mic
	0	2	0	2
Moment	31	30	42	39
Axial Stress	-10	4	-16	5
Shear Stress	53	15	61	20



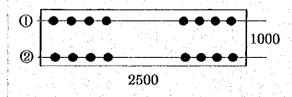
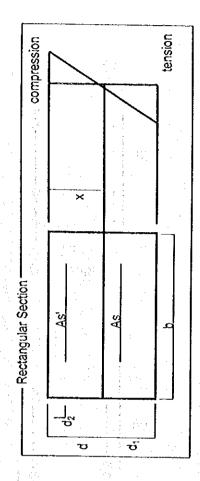


Figure-4 (3)

()



					Condition o	Condition of Calculation						Result	
section number	effective height	cover	cover	calculation width	bar area tensile	bar area compression	bar ratio	bending moment	axial force	shearing force	concrete compression stress	bar tensile stress	concrete shearing stress
	d (cm)	<del>3</del>	d2 (cm)	b (cm)	As (cm²)	As' (cm²)		M (ff.m)	N(#)	(#) O	αc (kaf/cm²)	as (kaf/cm²)	c c (kaf/cm²)
•	0.06	-			57.304	00000	0.0025	14.000	42.000	11.000	5.8	40.2	0.276
7	0.06		0.0	-	39.711	0.000	0.0018		40.000	12.000	8.2	128	0.421
က	0.06				57.304		0.0025	25.000	40.000	16.000		227.6	000
4	90.0				39,711	0.000	0.0018	į	40.000	16.000	. 25	443.5	0 710
ည	150.0	10.0	0.0	250.0			0.0015	•	63.000	12.000		14	0.037
9	150.0				57.304	0000	0.0015		63.000	19.000	0.9		0.278
<b>~</b>	0.06				57.304		0.0025	31.000	-10.000	53.000	13.4	738.3	2.557
œ	85.0				57.304	0000	0.0027		4.000	15.000	14.7	635.5	0 769
တ	0.06	10.0	0.0		57.304	0.000	0.0025	42.000	-16.000	61.000	18.0	1021.3	2.941
5	85.0	15.0	0.0		57.304	0.000	0.0027	39.000	5.000	20.000	19.2	828	1.025

Table - 6