No. 51

JAPAN INTERNATIONAL COOPERATION AGENCY (JICA)

C.2

MINISTRY OF SETTLEMENT AND REGIONAL DEVELOPMENT THE REPUBLIC OF INDONESIA

THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

FINAL REPORT

COMPONENT C: URBAN DRAINAGE SYSTEM IMPROVEMENT

> VOLUME III DESIGN NOTES

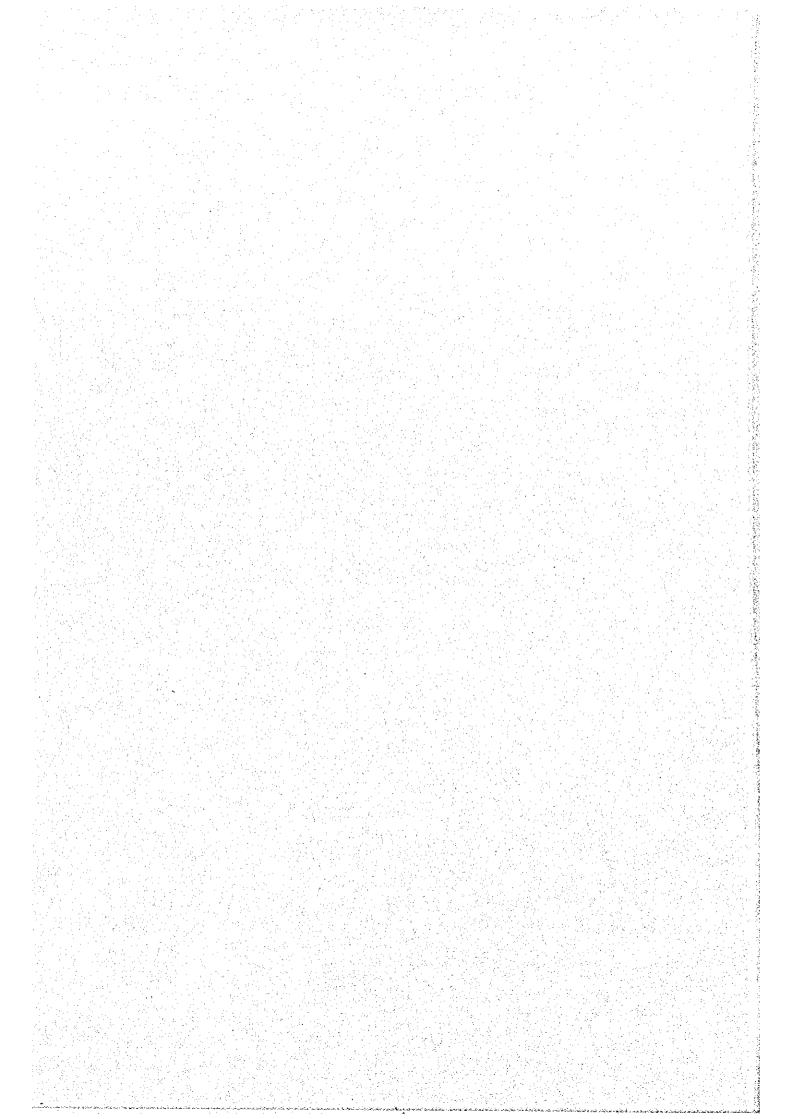


AUGUST 2000

CTI ENGINEERING INTERNATIONAL CO., LTD. IN ASSOCIATION WITH PACIFIC CONSULTANTS INTERNATIONAL

> AND **PASCO INTERNATIONAL INC.**





JAPAN INTERNATIONAL COOPERATION AGENCY (JICA)

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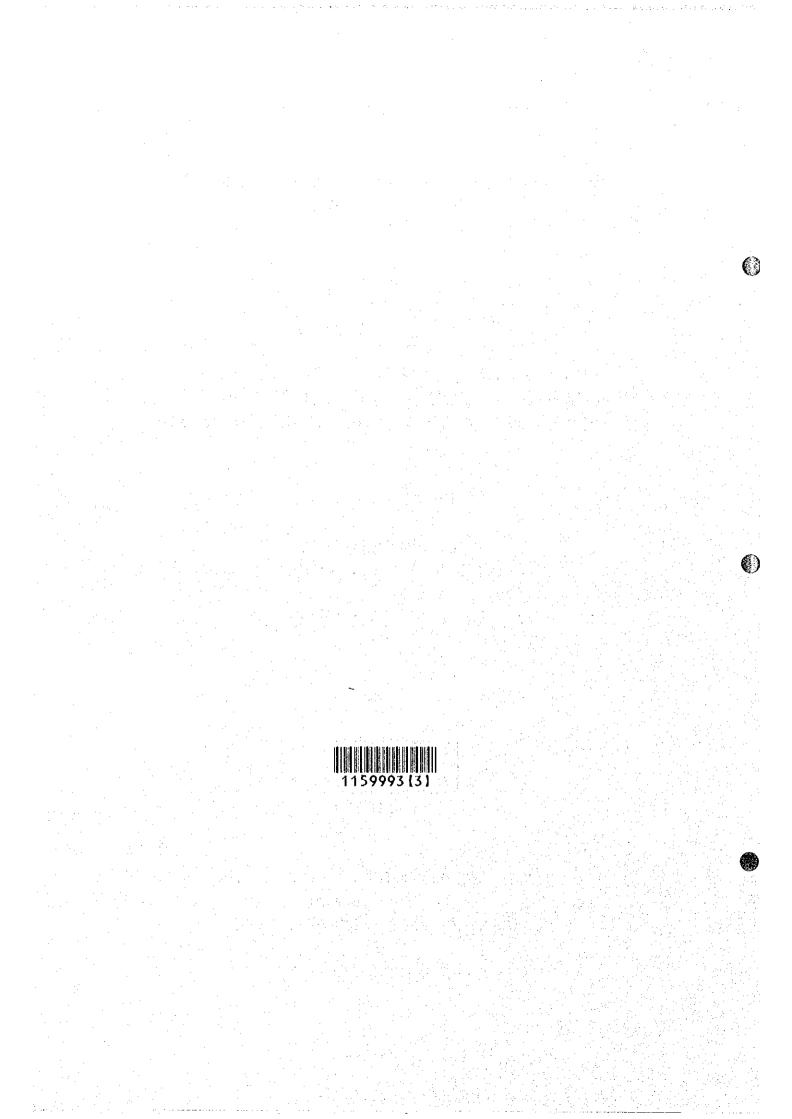
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VOLUME II DESIGN NOTES

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PASCO INTERNATIONAL INC.



CONSTITUTION OF THE REPORT

1. SUMMARY

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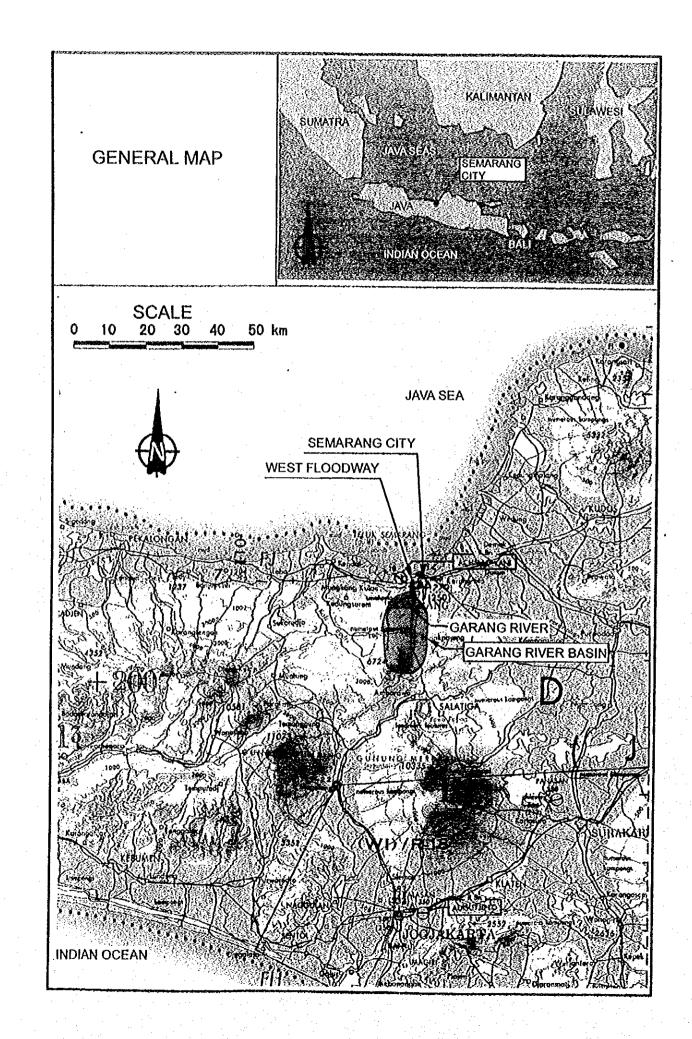
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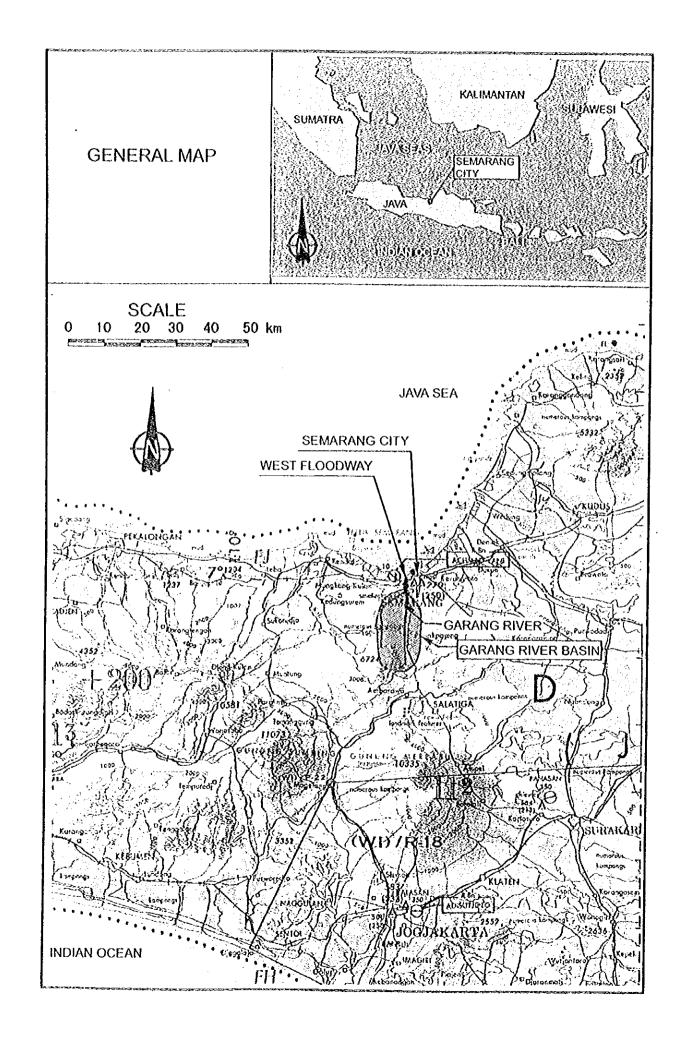
3. COMPONENT B : JATIBARANG MULTIPURPOSE DAM CONSTRUCTION

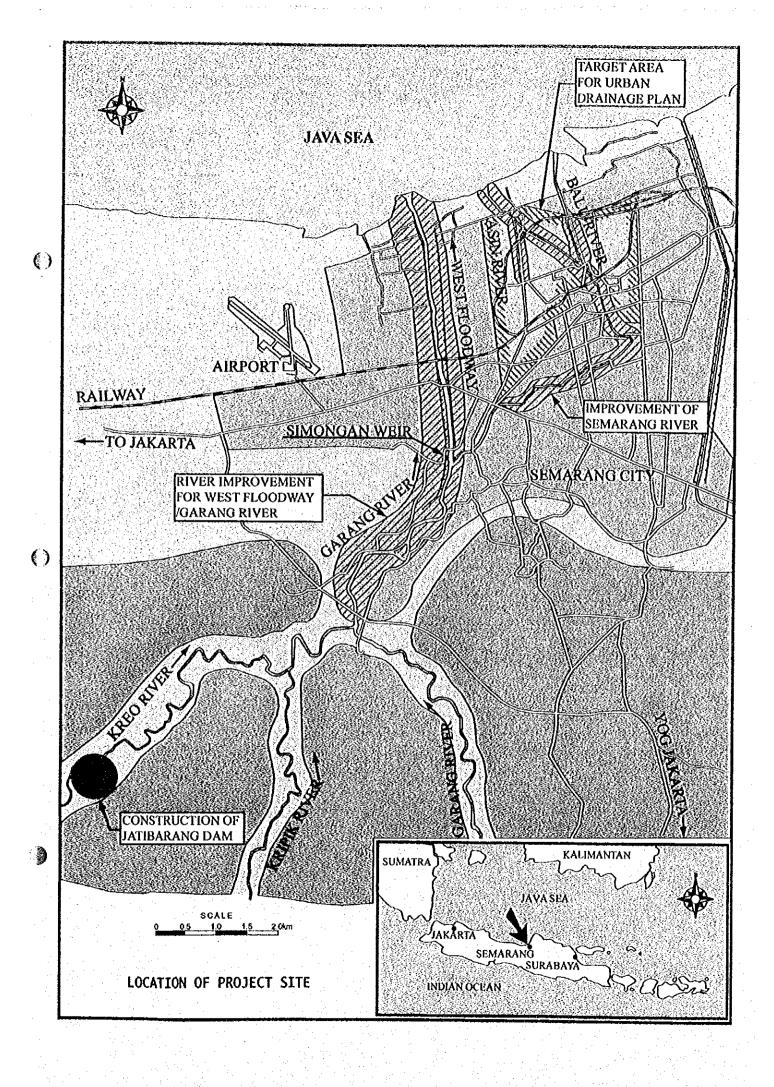
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VOLUME II	DESIGN CRITERIA
VOLUME III	DESIGN NOTES
VOLUME IV	WORK QUANTITY CALCULATION
VOLUME V	CONSTRUCTION PLANNING
VOLUME VI	COST ESTIMATE
VOLUME VII	ΔΑΤΑ ΒΟΟΚ
VOLUME VIII	ANNEX

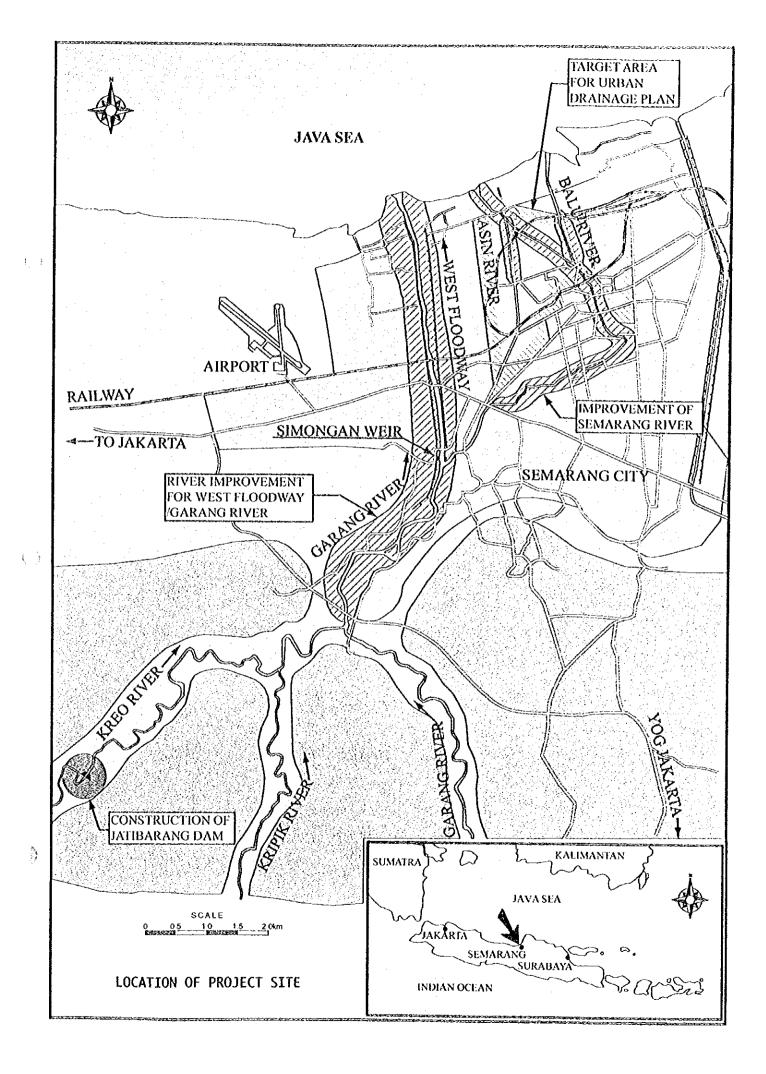
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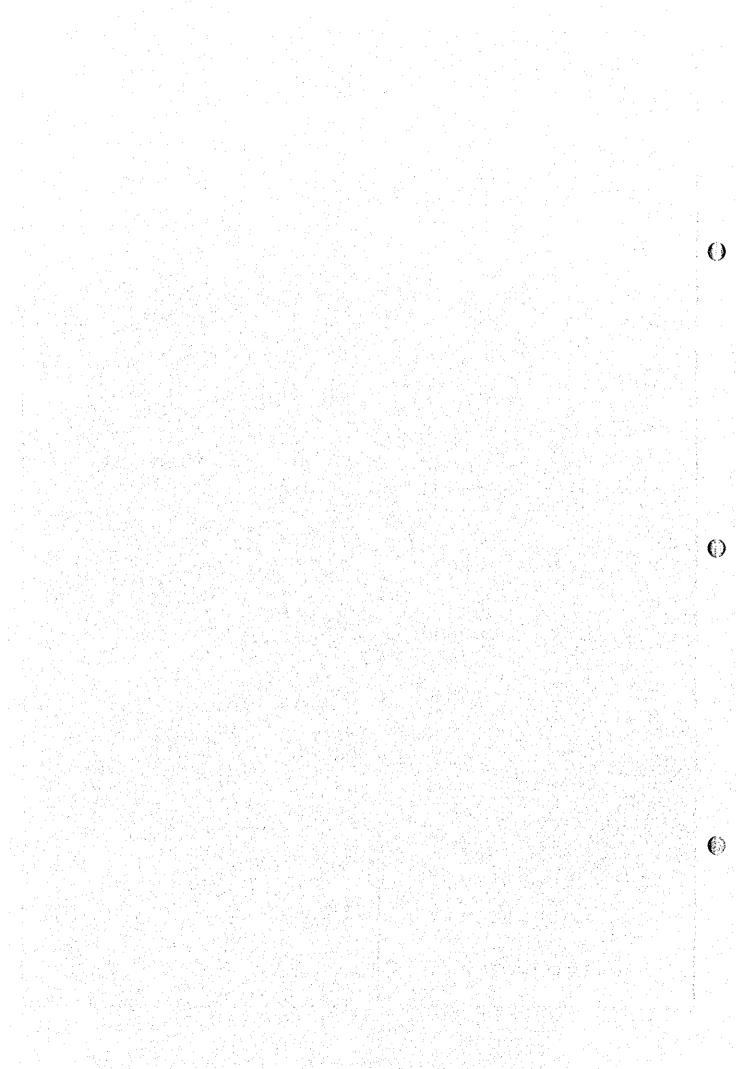
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TERMS AND ABBREVIATIONS

INDONESIAN GOVERNMENT AGENCIES AND ORGANIZATIONS

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GOI :	Government of Indonesia
BAPPENAS :	Badan Perencanaan Pembangunan National (National Development Planning Board)
BAPPEDA :	Badan Perencanaan Pembangunan Daerah (Provincial Develop- ment Planning Board)
BINAMARGA :	Directorate General of Road and Bridge, Ministry of Public Works
BAPEDAL :	Badan Pengendalian Dampak Lingkungan (Environmental Impact Assessement Board)
BPN :	Badan Pertanahan Nasional (National Land Agency)
BPP :	Balai Penyuluhan Pertanian (Agricultural Extension Center)
DPU :	Departemen Pekerjaan Umum (Ministry of Public Works)
DGWRD :	Directorate General of Water Resources Development, Ministry of Public Works
DGCK :	Directorate General of Cipta Karya (Housing, Building and Urban Development, Ministry of Public Works)
DGRD :	Directorate General of Research and Development, Ministry of Public Works)
DOR :	Directorate of Rivers
DPUP :	Dinas Pekerjaan Umum Propinsi (Provincial Public Works Services)
IHE	Institute of Hydraulic Engineering (Bandung)
РЈКА :	Perusahaan Jawatan Kereta Api (Railway Company, Old Name)
PERUMKA :	Perusahaan Umum Kereta Api (Indonesian Railway Public Corporation, New Name)
PDAM :	Perusahaan Daerah Air Minum (Water Works Company)
PMG :	Pusat Meteorologi dan Geofisika (Center of Meteorology and Geographysics)
PLN :	Perusahaan Listrik Negara (State Electricity Corporation)
P3SA :	Proyek Pengembangan dan Penyelidikan Sumber-Sumber Air (Water Resources Development and Investigation Project)
JAPANESE GOV	ERNMENT / INTERNATIONAL ORGANIZATIONS
GOJ :	Government of Japan
JICA :	Japan International Cooperation Agency

- MOC : Ministry of Construction, Japan
 - iii

JEM :	Japan Electric Machine Industry	
ADB :	Asian Development Bank	
	International Bank for Reconstruction and Development (World Bank)	
UNDP :	United Nations Development Program	Ì
• WMO = = = = = = = = = = = = = = = = = = =	World Meteorological Organization	
ASTM :	American Society for Testing and Materials	
ASME :	American Society of Mechanical Engineer	
USASI : IEC :	United States of America Standards International Electrotechnical Committee	
NEMA :	National Electrical Manufacturers Association	

3. MEASUREMENT UNITS

(Length)

(Weight)

mm :	millimeter(s) g, gr	gram(s)
cm :	centimeter(s) kg	kilogram(s)
• m • • • • • • • • • • • • • •	meter(s) t, ton :	tonnage (s)
km :	kilometer(s)	

george Astronom

(Area) (Time) mm² square millimeter(s) second(s) sec., s square centimeter(s) min cm² minute(s) m² square meter(s) h (hrs) hour(s) km² square kilometer(s) d (dys) day(s) ha(has) hectare(s) y, yr(yrs) year(s) (Volume) (Discharge) 1.14 cubic centimeter(s) cm³ l, Itr liter(s) m³ cubic meter(s) EL., El. Elevation

(Combined Units)

cm/sec, cm/s : centimeter per second m/sec, m/s : meter per second
km/hr, km/h : kilometer per hour
Stress
kgf/cm ² : kilogram per square centimeter
tf/m ² : ton per square meter
N/mm ² : newton per square millimeter

iν

Мра	:	mega pascal in the second department of the second s
Discharge		and the second and a special second
ltr/sec, I/s	:	liter per second set of set set of the set
m³/sec, m³/s	:	cubic meter per second
m³/yr, m³/y	:	cubic meter per year
(Note : Other	coi	mbined units may be constructed similarly as above)

Electricity

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MW at the set of	: megawatt	GW		gegawatt
MWh	: megawatt hour	GWh	t en je	gegawatt hour
kV	: kilovolt			

MONETARY TERMS

¥	 Japanese Yen
US\$	United States Dollar
Rp.	Indonesian Rupiah

5. INDONESIAN TERMS

	· 建碱酸化 网络维护学校 计图片 化合同合金 的
JKT	: Jakarta
Jawa	: Java
Propinsi	: Province
Kabupaten, Kab.	: District (Regency)
Kotamadya, Kodya	: Municipality
Kecamatan, Kec.	: Sub-District
Desa	: Village (Rural Area)
Kampung, Kp.	: Village (Rural Area)
Kelurahan	: Village (Urban Area)
Kali, Sungai	: River
Gunung	: Mountain
Rawa	: Swamp
Danau	: Lake
Laut	: Sea
PT .	: Incorporated or Limited
РРТ	: Panitia Pembebasan Tanah (Land Acquisition Committee)
KOMPUS	: Komisi Pusat (Central Committee for Environmental Impact Assessment)
KA-ANDAL	: Terms of Reference of Environmental Impact Statement
ANDAL	: Environmental Impact Statement

RKL		• :	Environmental Management Plan	
RPL		:	Environmental Monitoring Plan	
AMDAL		:	Environmental Impact Assessment	
BPPM2		:	Semarang Port Bench Mark	en Serte de
SPB		:	Semarang Peil Baru (New Semarang Level)	
TTG	t Sec	:	Tanda Tinggi Geodesi (National Bench Mark)	

6. OTHERS

JRATUNSELUNA PROJECT : Water Resources Development Projects for Jragung, Tuntang. Serang. Lusi and Juwana Rivers

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$f_{i}(x_{i}) \in C^{1}(G) \times C^{1}(G)$	Funtang, Serang, Lusi and Juwana Rivers
SSUDP	: Semarang and Surakarta Urban Development Program
IUIDP	: Integrated Urban Infrastructures Development Program
SWL	Surcharge Water Level
DFWL	: Design Flood Water Level
PMP	: Probable Maximum Precipitation
PMF	: Probable Maximum Flood
EIRR	: Economic Internal Rate of Return
JIS	: Japanese Industrial Standard
USASI	: United States of America Standards
SWR	: Shadow Wage Rate
CIF	: Cost, Insurance and Freight
VAT	: Value Added Tax.

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CHAPTER 1 SEMARANG RIVER DRAINAGE SYSTEM IMPROVEMENT

1.1 Non-uniform Flow Calculation

lame of tructure	SEMARANG RIVER	Category Calculation	Non-uniform Flow Calculation	Page	1/18

Non-uniform Flow Calculation

Non-uniform calculation was made to design the high water level of Semarang River when design discharge flows.

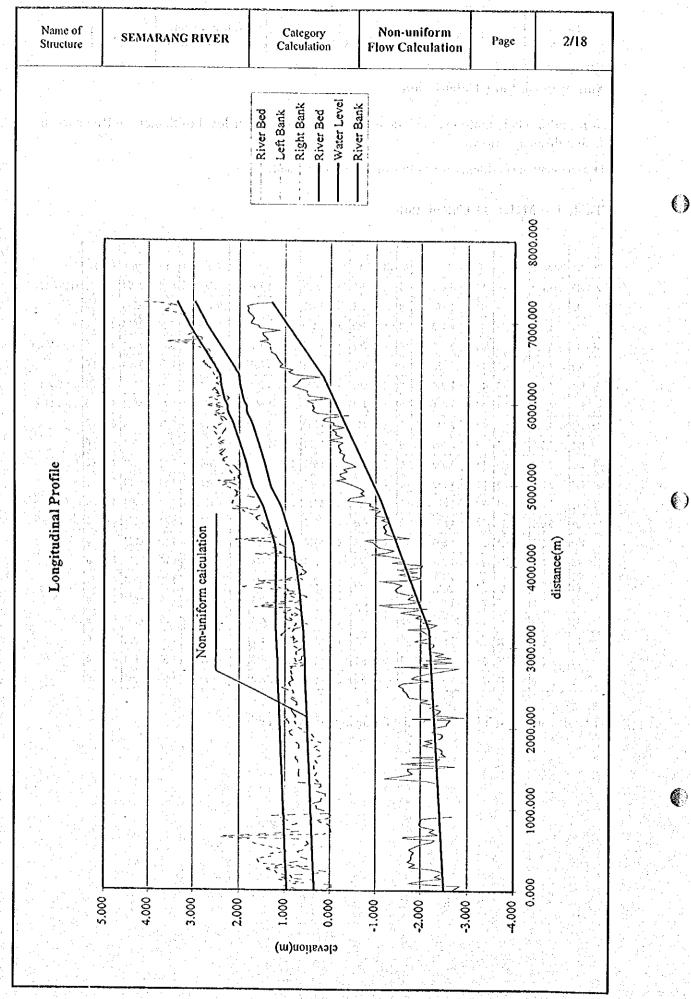
The calculation conditions are as shown the following table.

Table 1 MIKE 11 Calculation

	1. A.		Botom	Bank																
Sec.No	Distance	Change	દા	EL	80	m	X١	Yi	X2	Y2	X3	Y3	X4	Y4	X5	Y5	n	Q	dQ	
241+13	7,223	0.000	1.280	5.280	6	0	0	5.280	0	1.280	3	1.280	6	1.280	6	5.280	0.024	16	16	Tugu Muda
212	6,341	0.882	0.178	4.178	6	0	0	4.178	0	0.178	3	0.178	6	0.178	6	4.178	0.024	16	0	
211	6,311	0.912	0.140	4.140	8	0	0	4.140	0	0.140	4	0.140	8	0.140	8	4.140	0.024	16	0	
195+17	5,858	1.365	-0.238	3.762	8	0	Ó	3.762	0	-0.238	4	-0.238	8	-0.238	8	3.762	0.024	21	5	Gajah Mada
162	4,861	2.352	-1.068	2.932	8	0	0	2.932	0	-1.068	4	-1.068	8	-1.068	8	2.932	0.024	21	0	
161	4,830	2.393	-1.094	2.906	14	0	0	2.906	0	-1.094	7	-1.094	14	-1.094	14	2.906	0.024	46	25	Kimangun
138	4,152	3.071	-1.546	2.454	14	0	0	2.454	0	-1.546	7	-1.546	14	-1.546	14	2.454	0.024	46	0	Sarkoro
137+14	4,133	3.090	-1.559	2.441	18	0	0	2.441	0	-1.559	9	-1.559	18	-1.559	18	2.441	0.024	46	0	
121	3,635	3.588	-1.891	2.109	18	0	0	2.109	0	-1.891	9	-1.891	18	-1.891	18	2.109	0.024	46	0	
120	3,607	3.616	-1.910	2.090	19	0	0	2.090	Ó	-1.910	9.5	-1.910	19	-1.910	19	2.090	0.024	46	0	
107	3,230	3.993	-2.161	1.839	19	0	0	1.839	0	-2.161	9.5	-2.161	19	-2.161	19	1.839	0.024	46	0	
106+13	3,202	4.021	-2.180	1.820	19	0	0	1.820	0	-2.180	9.5	-2.180	19	-2.180	19	1.820	0.024	46	0	Railway
101	3,026	4.197	-2.197	1.803	19	0	0	1.803	0	-2.197	9.5	-2.197	19	-2.197	19	1.803	0.024	46	0	
100	2,996	4.227	-2.200	1.800	20	0	0	1.800	0	-2.200	10	-2.200	20	-2.200	20	1.800	0.024	46	0	
95	2,856	4.367	-2.214	1.786	20	0	0	1.786	0	-2.214	10	-2.214	20	-2.214	20	1.786	0.024	46	0	
- 94	2,827	4.396	-2.217	1.783	20	2	0	1.783	8	-2.217	18	·2.217	28	-2.217	36	1.783	0.031	46	0	
32	975	6.248	-2.403	1.598	20	2	0	1.598	8	-2.403	18	-2.403	28	-2.403	36	1.598	0.031	46	0	
31	939	6.284	-2.406	1.594	24	2	0	1.594	8	2.406	20	-2.406	32	-2.406	40	1.594	0.031	65	19	Asin
21	632	6.591	·2.437	1.563	24	2	0	1.563	8	-2.437	20	-2.437	32	-2.437	40	1.563	0.031	65	0	· ·
20	604	6.619	-2.440	1.560	38	2	0	1.560	8	-2.440	27	-2.440	46	-2.440	54	1.560	0.031	65	0	
. 0	0	7.223	-2.500	1.500	38	2	0	1.500	8	-2.500	27	-2.500	46	-2.500	54	1.500	0.031	65	0	

The calculation result is shown in the following graph and tables.

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	5	Name o Structur		SEMA	RANG	RIVER	er Lit	Categ Calcul			on-unifor v Calcula	1 1 1 1 1 1 1 1 1 1 1 1
		•bacatat	<u>-</u>	·····			,_ 	·		.		······································
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	÷	Tabla	2 Sor	narana	Rivar N	locian '	Wator	Level Ca	lculati	on		
		Table						Proposed			Proposed	I
				ACCM.	Bed	Bank	Bank	River Bed		River Bank		
		LINE 0.00	DIS 0.000	DIS 0.000		0.110	0.580		0.350		-	
		1.00	31.846		-2.750	0.030	0.870		0.353			
		2.00	27.987		-2.840	-0.140	1.060		-0.355		-1/10,000	
)		-3.00-	31.043	90.876	-1.740	-0.370			0.358		_	
		4.00	36,860	127.736	-2.090	0.390	1.120					
		5.00	22.456	150.192	-2.450	1.060	0.830		0.363		1/10,000	
		-6.00-	25.568	175.760	-2.310	0.960	0.860	2.482	0.365	0.965	-1/10,000-	
· ·		7.00	26.373	-202.133	-2.430	0.390	1.150	-2.480	0.367	0.967	1/10,000	
		8.00	28.665	230.798	-2.480	0.070	1.200	-2.477	0.370	0.970	1/10,000	to the second second
ta te d		9.00	33.341	264.139	-2.250	0.570	-1.450	-2.474	0.373	i · .		
	14	10.00	27.443	291.582	-1.750	1.200	0.490		0.376	0.976	1/10,000	
		11.00	31.949	-323.531	-1.890	0.990	1.550	-2.468	0.379		1/10,000	
		12.00	31.554	355.085	-1.720	0.690	1.580		0.381	0.981	1/10,000	
		13.00	29.428	384.513	-1.800	0.500	1.620		0.384	0.984	1/10,000	
	- Area	14.00	29.015	413.528	-1.800	0.710			0.386		1/10,000	
		15.00	28.856		-1.810	0.660	1.350		0.388		1/10,000	<u>i e de pertensi e en e</u>
		16.00	30.170	472.554	-1.860	0.720	0.940		0.391		1/10,000	
		17.00	31.600	504.154	-1.750	0.520	1.080	1	0.394		1/10,000	
	14 14 B	18.00	31.975	1	-1.870	0.580	1.390	2	0.397		1/10,000 1/10,000	
		19.00	31.203		-1.990	0.470	1.650		0.400		1/10,000	
		20.00 21.00	29.103		-2.250	0.520	1.770	1 N N	0.402		1/10,000	
): * I		21+23	20.230	645.161	-1.620	2.200	2.400		0.406		-1/10,000	Bridge(JL.Serskko Usman Janatin)
/	ан 19	22.00	11.419	656.580	-1.620	2 400	2.400	54 C 15 C	0.407	1.007	1/10,000	
	12	23.00	31.891	688.471	-2.380	1.360	0.150	1 5 5 1	0.409		-1/10,000-	
		24.00	32.525	720.996	-2.190	0.690	-0.030	4. April 10 (1997)	0.410		-1/10,000-	
		25.00	32.689		-2.300	- 1.030	-0.010		0.412	1.012	1/10,000	
		-26.00-				0.980	-0.030	-2.422	0.416	1.016	1/10,000	
		27.00	29.832			0.710	0.060	2.419	0.420	1.020	1/10,000	
		28.00	39.708	854.443	-2.000	0.930	0.320	2.415	0.424	1.024	1/10,000	
		29.00	30.227	884.670	-2.030	1.050	0.040		0.411			
		30.00	28.811		-2.670	1.290	-0.040		0.430			
		NT	30.000		e ar le j	0.040	0.040		0.432		1/10,000	
		N2	30.000			0.100	0.100		0.434			Asin River
	1 N	N3		1003.481		0.300	0.300		0.436		1/10,000	a ta gang kanta pang kanta.
	0	-N4-		1033.481		0.300	0.300		0.438			in an gran de grane de grande ^e rr
		N5		1063.481	1972 - 14 	0.400	- 0.400		0.440		1/10,000	and a second
		N6	1	1093.481	5	0.200	0.200		0.442		1/10,000	
		N7		1123.481		0.200 0.100	0.200		0.444	1.044	1/10,000	
		N8 N9		1153.481 1183.481		0.100	0,100	1	0.446 0.448		1/10,000	
		-N10-		1213.481		0.300	-0.300		0.440		1/10,000	
7		N10		1213.401		0.300	0.300		0.450	1.1.2.2.4.4.4.1	1710,000	
		N12		1273.481		0.200	0.300		0.454		1/10,000	n de la facto de la composición de la c
		-N13-		1303.481		0.200		and the second	-0.456	1 - N - N - N	1/10,000	
		43.00	1.4.4.4	1320.808	-2.330	0.710	0.240	1 1 1 1 1 1	0.457			
	4	44.00	2 A A A	1347.489	-2.140	0.690	0.290	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.458			<u>n an a Berling en Ellan el Terren</u> Transforment
		45.00		1374.719	-1.200	0.630		125 S S S S S S S S S S S S S S S S S S S	0.460			
		46.00		1404.120		0.700			-0.463			
		47.00		1433.722	-1.830			2 - A S. L.	0.466	1.1.1		

	Name o Structur		SEMA	RANG	RIVER		Categ Calcul			on-unifor w Calcula		Page	4/18
	1 (6.64)		1464.821	1 7 (4)		L	0.454				······································	L *	L
	48.00 49.00		1404.821	-1.740 -1.720	0.690	0.290				1 -		· · · · · · · · · · · · · · · · · · ·	
	45.00 50.00		1526.086	2.730	0.690	0.360	-2.350	0.472 0.475	1.07			sign and the state	- 54, a 43
	51.00		1557.353	-1.580	0.040	0.360	N	Contract of the second	1.07			<u> </u>	· · · · · · · · · · · · · · · · · · ·
	52.00		1587.063	-1.560	0.710	0.280	-2.344 -2.341	0.479	1.079				
	53.00		1617.528	-2.340	- 0.770	0.550	-2.341	0.482	, 1.082 1.08				
	53+17	L I	1637.975	-1.820	0.760	0.280	-2.336		•	£ .	022	(C)	
	54.00		1651.499	-1.020	0.760	0.200	-2.330	0.487	1.08	F	Bhoge	(Steel)	
·	55.00		1682.929	-2.540	0.760	0.210	-2.335	0.488	1.088	•	· · · · ·	<u></u>	
	56.00		1713.664	-2.450	0.740	0.210	-2.337	0.491	1.09	-	· .	82 - <u>1</u> - <u>1</u>	
•	57.00		1748.994	-2.410	0.690	0.240	-2.329	1.2	1.093				
, ,	58.00		1746.994	-2.910	0.690	0.380	1 N N N N N N N N N N N N N N N N N N N	0.495	1.09	1	-		a di se se
	59.00		1815.191	-2.040			-2.321	0.498	1.098		1 1 ² 11	<u>la sette en secon</u>	
	<u>59.00</u> 60.00		1841.651		0.760	0.210	-2.318	0.500	1.100	1 · ·		<u>1 (1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1</u>	
	61.00		1891.651	2.090	0.750	0.430	2.316	0.502	1.10	1	1		1. I. I. I.
				2.420	0.800	0.340	-2.313	0.504	1.104		1.5	<u>ar ar far i</u>	t de até
	62.00 63.00	24.943 28.923		2.470	0.820	0.380	-2.311	0.506	1.10	1			
•	64.00		1921.071	-2.470	0.890	0.420	-2.308	0.508	1.108				
ŗ	65.00	25.371		-2.250	0.900	0.620	-2.305	0.509	1.10	F			
	65.00 66.00			-2.300	0.820	0.610	-2.303	0.511	1.111		<u></u>		
	1 1		1999.927	-2.270	0.870	0.720	-2.300	0.513	1.11.				
	67.00	31.344		-2.550	0.910	0.740	-2.297	0.515	1.119				
•	68.00		2063.963	2.570	0.910	0.790	2.294	0.517	1.117				
:	69.00	- I	2097.995	-2.640	0.980	0.770	-2.290	0.520	1.120				
	69+14	• • •	2110.858	-1.810	0.800	0.800	-2.289	0.521	1.121	1 1 1 1 1 1 1 1	Bridgr	(Conkrete)	
	70.00		2126.995	-2.930	0.780	0.760	-2.287	0.522	1.12				
	71.00	1	2158.085	-2.280	0.800	0.780	-2.284	0.524	1.124	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.1		
	72.00		2186.551	-2.390	0.830	0.840	-2.281	0.526	1.120		1.14		
	73.00		2217.852	2.430	0.850	0.870	-2 278	0.528	1.12			denti <u>se de la c</u>	
			2249.463	-2.200	0.840	0.810	-2.275	0.530	1.130			Har Mar	
	75.00		2281.386	-2.380	0.820	0.730			1.13	1.1.1			
	76.00		2313.960	-1.990	0.740	0.740	-2.269		1.137		<u></u>		的复数
	77.00		2344.652	-2.160	0.850	0.750	-2.266	0.540	1.140	• · · · ·			
	78.00		2372.757	-1.750	0.880	0.860	-2.263	0.543	1.14		<u> </u>		
	79.00		2400.972	-1.720	0.870	0.830	-2.260	0.546	1.140	1	1.2	$p_{i}(1,2) = 1/12$	
	80.00		2431.041	-1.690	0.880	0.810	· .	0.549	1.149				
	81.00		2460.845	1.620	0.940	0.850	-2.254	0.552	1.15	1 4 4			
	82.00		2488.640	-1.620	1.070	0.860	-2.251	0.555	1.15	1. 1		24 J. A. A. A.	
	83.00		2517.648	-1.510	0.980	0.890	-2.248	0.557	1.15		100		1.74
	84.00		2547.185	-1.620	0.920	0.920	-2.245	0.560	1.160				
ž.	85.00		2576.881	2.190	0.840	0.810	-2.242	0.561	1.16	1			
	86.00		2606.523	-1.800	0.850	0.860	-2.239	0.562	1.162				
	87.00		2637.228	1.910	0.870	0.840	-2.236	0.563	1.16	 A second sec second second sec			
	88.00		2670.572	-2.170	0.870	0.860	-2.233	0.564	1.164				
	89.00		2705.557	-2.520	0.910	0.890	-2.229	0.565	1.165				
ċ	90.00		2736.375	2.830	0.840	0.850	-2.226	0.567	1.167				
	90+11		2747.521	-1.420	0.900	0.830	-2.225	0.567	1.16		Bridgr	(Conkrete), Baru I	River
Ż	91.00		2761.978	-2.160	0.620	0.520	5 - C - C - C - C - C - C - C - C - C -	1 A A A A A A A A A A A A A A A A A A A	1.167	1.5.1	1.25		
	92.00		2785.971	-2.050	0.580	0.830		0.568	1.16		2.4		
	93.00		2808.804	-2.670	0.780	0.760	-2.219	0.569	1,169				• • • • • • • • •
	94.00		2836.209	-2.120	0.630	0.780	4 10 10 10	0.570	1.17(1.1		
	95.00		2864.450	-2.650	0.640	0.800	-2.214		1.17				34/9/2
	96.00		2890.350	-2.310	0.590	0.750	-2.211	0.576	1.176				
2	97.00		2918.483	2.500	0.640	0.770	-2.208	0.580	1.180	1/10,000			
	98.00	27.698	2946.181	2.180	0.720	0.710	-2.205	0.583	1.18	1/10,000	1		ente à 17

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	Name o Structur		SEM.	RANG	RIVEI	2	Cates Calcul			lon-unifo w Calcul		5/1
	99.00	30.491	2976.672	-2.170	0.610	0.740	-2.202	0.587	1.18	1/10,000		
•	100.00	28.841	3005.513	-2.280	0.650	0.830			1.19			
	101.00	<u>30.63</u> 9	3036.152	-2.280	0.820	0.820	2.196	0.593	1.19	3 1/10,000	-	
	102.00		3066.982	-1.870		0.710	-2.193	0.596	1.19		-	· · · ·
	103.00		3099.884	2.140		0.810			1.19			
	104.00		3132.458	-2.230	1.100	0.840		0.602	1.20			
	105.00	r 1	3172.290	-2.100		0.850			1.20	-		
	106.00 106+13	33.821 4.804	3206.111 3210.915	-2.010 -1.720		0.800	1		1.21		0.711	<u> </u>
	100+13	9.009	3238.692	-1.720		0.940		0.610	1.21		Rail Way	· · ·
	108.00		3271.038	-2.350		0.020		0.613	1.21	1		<u> </u>
;	109.00		3298.513	-2.040	1. S.			0.626	1.21			
	110.00		3326.921	2.220	1.000	0.850		0.831	1.21			
	111.00	30.471	3357.392	-1.890	0.850	0.930	-2.081	0.637	1.21	1		
	112.00		3387.169	-2.000	0.720	0.830	-2.061	0.643	1.21	0 1/1,500		
	113.00		3417.346	-1.550	0.850	1.050	1	0.648	1.21	1		
	114.00		3443.412	-1.840	5.5	0.890		0.652	1.21			
	115.00		3471.266	-2.140	0.770	0.840		0.656	1.21			· · · · · ·
	115+14 116.00		3484.574	-1.420 -1.190	1.620	1.680		0.658	1.21		JL Mpulantular	
	116+8		3510.546	1.080	1.490	1.250	<u> </u>	0.661	1.21		JL.Suprapto	
	117.00		3531.243	-1.700	0.870	1.450	· · · · · · · · · · · · · · · · · · ·	0.665	1.21	1		
;	118.00		3560.108	-1.990	0.540	0.690		0.668	1.21	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		<u> </u>
	119.00	27,772	3587.880	1.720	0.570	0.760	1.928	0.672	1.21			
	120.00	25.930	3613.810	-1.800	0.530	0.860	•1.910	0.676	1.21	1/1,500		
	121.00		3640.795	-1.910	0.740	0.990	1	0.681	1.21			
	121+3	- 1	3643.179	1.710	0.920	1.030		0.682	1.21	1.1	Bridge(Foot Path)	n na sa
	122.00 123.00		3670.372	-1.480	0.710	0.980	1 i	0.687	1.21			
.	123.00		3700.233 3730.109	-1.440	1.180	0.930		0.694	1.21			
	125.00		3760.154	-1.590	1.630	1.190		0.708	1.21			
	126.00		3790.065	-1.380	1.380	1.450		0.715	1.21			
	126+17		3806.996		1.600	1.600		0.719	1.21	1.1	JL. Agus Salim	
•	127.00	15.377	3822.373	-1.780	0.980	0.610		0.723	1.21(1/1,500		
			3854.293	2.010	0.820	0.740	1 A A A A A A A A A A A A A A A A A A A	0.730	1.21	1		
	129.00		3890.927	1.510	0.590	0.670	1 A A A	0.739	1.21	1		
	130.00		3922.903	-1.920	0.540	0.560	14.5	0.746	1.21(1		
	131.00		3951.947	-1.470	0.670	0.630	14 A A	0.754	1.210	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
	132.00 133.00		3979.384 4007.567	-2.000 -2.040	0.620	0.690		0.762	1.210		and second damage	
	134.00		4036.716	1.370	0.750	0.070		0.780	1.21			
	135.00		4062.961	-1.650	0.890	0.810	-1.611	0.786	1.210			
			4092.783	1.540	0.880	0.970	1.591	0.793	1.210	A 199 Aug. 2018		
	137.00		4123.105	-1.230	1.210	1.260	-1.571	0.800	1.210	1 1 1		
	137+14	14.224	4137.329	-0.900	1.220	1.680	-1.561	0.803	1.210	1/1,500	JL Gong Gong	
	138.00	1	4156.691	1.210	0.990	1.090	1.548	0.806	1.210	1/1,500		
			4188.816	-1.420	0.990	1.190	-1.527	0.815	1.215			
			4221.458	-1.080	0.970	1.280	-1.505	0.822	1.222			
			4254.848	-1.000	1.110	1.190	-1.483	0.830	1.230			· · · · ·
			4287.986 4312.489	-0.940 -0.750	1.310	1.300	-1.461	0.847	1.247	[3] S. S. San, A. S.	H Delaise	<u> </u>
	142+25		4312.489	-0.750 -0.880	2.080	1.900 1.890	-1.445 -1.440	0.860	1.260		JL Pekajan	
	143.00		5 A	-0.000	, c.uqu	1.020	-1.440	V.004	1.404	1. 11,000		

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	Name o Structur		SEM/	ARANG	RIVEI		Cate Calcu	gory lation		Non-unifo ow Calcul		Page	6/18
	1 146.00	30 93	4400.688	-1.190	1.270	13	20 1.386	0.911	1.3	11 00000			
	147.00	29.268	1		4	1.3				-		e Allin a Mire Allin - Allin -	<u>er (k. ep</u>
	148.00		4457.240			14		1	1				
	149.00	28.782	4486.022			1.4		1 A 1 A 1	1.1.1				
	150.00	24.71	4510.741	-1.230	N 11	1.5	4		A. C. S.		1	1 - 1997 - 1997 - 1997	19 - 19 - 19 - 19 - 19 - 19 - 19 - 19 -
	151.00	27.75	4538.492	-1.300	1.510	- 1.5		1.11	1.1.1			<u> </u>	
	152.00	28.040	4566.532	-1.120	1.640	1.62		1				· · · · · · · · · · · · · · · · · · ·	
	153.00		4595.570		1.660	1.65	50 1258	1.019	1.4				
	154.00		4622.561		1.540	1.68	50 -1.238	1.034	1.4	34 1/1,500	-	<u> </u>	
	155.00		4650.975			1.88	-1.219	1.050	1,4	50 1/1,500			
	156.00	31.659	1	-1.110		1.94		l	1.40	\$ 1/1,500	-		
	156+17		4700.471	0.850		1.82		(a) (b) (c) (c)	1.4		Bridge	(Foot Path)	
	157.00 158.00		4712.377	-1.060		1.97			1.48			te the equ	
	158.00		4743.145	0.860	1.570	2.13		1.109	1.50			and a trad	· · · ·
	160.00		4773.224 4803.586	-0.880	1.560	2.16		1.133	1.5.				at the second
4	161.00		4837.009	-0.380	1.650	2.13	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.162	1.58			sta Bag Cha.	
	162.00		4867.297	-0.440	2.070	2.13	1.1	1.194 1.223	1.59		JL.Kim	angun Sarkoro	1993
	163.00	29.407		-0.660	2.050	1.99		1.223	1.62 1.64		-		
	164.00		4926.451	0.740	2.100	2.10	and the second second	1.231	1.68				
	165.00		4956.060	-0.660	2.130	2.19		1.309	1.70	1	-	n her her	· · · · · ·
1	166.00		4984.616	-0.540	2.030	2.36		1.326	1.72		·		
	167.00		5015.162	0.400	2.170	2.22		1.344	1.74	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
	168.00	30.255	5045.417	-0.250	2.370	2.46		1.359	1.75				et lei set i s
	168+7	6.961	5052.378	-0.110	1.980	2.11		1.362	1.76		II Seh	andaran	
1	169.00	23.477	5075.855	0.340	2.030	2.10	•		1.77		-		<u>a anta a</u> . Ta anta a
	170.00	29.969	5105.824	0.220	2.030	2.15	0 -0.865	1.387	1.78				
	171.00		5135.289	-0.210	1.910	2.16	0.841	1.401	1.80	1 1/1,200			
	172.00		5163.061	0.370	2.010	2.20	0 -0.818	1.413	1.81	3 1/1,200			
	173.00	31.041		-0.290	2.060	2.19		1.427	1.82	7 1/1,200	-		
	174.00		5227.622	-0.560	2.100	2 23			1.84	2 1/1,200	-	a la sector de la sector	
4			5259.637	0.460		2.33	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.456	1.85			1997 a 218	
			5290.306	-0.300	2.340	2.36			1.87	1		na lung tin na	
	177.00 178.00		5318.599 5346.798	-0.270	2.340	2.33	1 1	1.487	1.88			and while the set	A of Sec. 5
	179.00		5375.486	-0.290 -0.310	2.230 2.410	2.30	1 A A A A A A A A A A A A A A A A A A A	1.502	1.90		-		
	180.00		5400.757	-0.310	2.410	2.44 2.46		1.518	1.91				
	181.00		5429.513	-0.230	2.310	2.40		1.532 1.548	1.93			an a	
			5460.428	-0.180	2.270	2.38		1.540		8 1/1,200 5 1/1,200			· · · · · · · · · · · · · · · · · · ·
-			5492 272	0.180	2 270	2.38			1.98		a wat	<u></u>	
			5522.700	-0.280	2,410	2.49		1.600	2.00			Gandul	
Ċ,			5552.702	0.040	2.280	2.45		1.617	2.01				
	185.00	30.742	5583.444	-0.270	2.350	2.40		1.634	2.03		24 - 1	energine brite The state	
2.57	187.00	35.685	5619.129	-0.110	2.370	2.49		1.653	2.05				
•			5650.164	-0.130	2.340	2.54	0 0.412	1.671	2.07				
			5680.052	-0.040	2.290	2.48	1 1 1 1 1 M 1 1 1	1.688	2.08		1 1 1 4		
	f 1		5709.773	-0.310	2.290	2.55	0 -0.362	1.704		4 1/1,200			
/			5737.331	0.070	2.280	2.42	0 0.339	1.719	2.11	1 T T T T T T T			
			5766.910	-0.070	2.250	2.32		1.740	2.14				
			5795.337	0.170	2.280	2.37		1.760	2.16	1/1,200			
2			5826.448	0.110	2.320	2.41		1.788	2.18		1, 1, 7	Čer v	<u> </u>
:			5856.172	-0.410	2.530	2.53		1.815		5 1/1,200			
	195+17	17.251	5873.423	0.110	2.320	2.41	-0.226	1.830	2.23	1/1,200	JL Gaja	h Mada	<u></u>

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1			<u> </u>				<u> </u>				ar ana dait a r ai provins			
		Name o		SEMA	RANG	RIVER		Categ			n-unifor		Page	7/1
		Structur	e			14		Calcula	tion	Flow	Calcula	tion	- ·	
•			L-		·····		l			L				- L
		106.00	12 980	5886.403	0.310	2.370	2.550	-0.215	1.836	2.236	1/1,200	ı——		
н. 1911 - Ал		197.00		5916.570		2.320	2.440		1.851	2.251	1/1,200			
		198.00		5945.778		2.310		-0.165	1.851	2.251	1/1,200			
		199.00	30.113	5975.891	0.400	2.500	2.720	-0.140	1.851	2.251	1/1,200			·
	-	200.00	30.118	6006.009	0.390	2.440	2.400	-0.115	1.881	2.281	1/1,200			
		201.00		6036.266	0.530	2.260	2.430	-0.090	1.911	2.311	1/1,200		<u></u>	,
	•	202.00		6066.337	0.020	2.220	2.650	-0.065	1.923	2.323	1/1,200			
		203.00		6097.084	0.490	2.280	2.370	-0.039	1.936	2.336	1/1,200			
$\lambda_{ij} = \lambda_{ij} \lambda_{ij}$	ς.	204.00		6126.471	0.520	2.460	2.500	-0.015 0.010	1.947 1.959	2.347 2.359	1/1,200	<u> </u>	<u></u>	
		205.00		6156.275 6181.908	0.520	2.480	2.500	0.010	1.959	2.355	1/1,200		<u>a 1. 1. 1.</u>	
n de la composition de la comp	-	200.00		6213.821	0.840	2.370	2.480	0.058	1.982	2.382	1/1,200			
		208.00		6243.998	0.730	2.500	2.450	0.083	1.989	2.389	1/1,200			
		209.00		6274.126	0.700	2.420	2.390	0.108	1.996	2.396	1/1,200		् सन्दर्भ स्ट्राई	
		210.00	30.166	6304.292	0.650	2.410	2.490	0.133	2.001	2.401	1/1,200		in the second	
		211.00	22.778	6327.070	0.240	2.410	2.440	0.152	2,005	2.405	1/1,200	JL.Thar	nno	
		212.00		6357.467	0.790	2.410	2.550		2.011	2.411	1/800			
	11	213.00		6387.530	0.930	2.470	2.560	0.228	2.044	2.444	1/800	<u> </u>)
		214.00		6417.285	0.830	2.530	2.590	0.265	2.076	2.476	1/800			
		215.00	1 N 1 M 1	6448.434 6471.223	1.120	2.550	2.650	0.304	2.106 2.128	2.506 2.528	1/800 1/800	Bridgel	Fool Path)	
		215+22		6478.643	1.050	2.710		0.333	2.120	2.525	1/800			
		217.00	F · · · ·	6509.535	1.110	2.780	2.510	0.381	2.173	2.573	1/800			
		218.00		6539.482	1.150	2.700	2.530	0.418	2.209	2.609	1/800			
	1	219.00	30.668	6570.150	1.180	2.720	2.630	0.456	2.242	2.642	1/800			· <u>-</u>
	4	220.00	30.555	6600.705	1.210	2.650	2.630	0.494	2.275	2.675	1/200	1	Ansatz in	• ;
		221.00	30.614	6631.319	1.310	2.620	2.670	0.533	2.309	2.709	1/800	i		
		222.00	1.1	6661.168					2.342	2.742	1/800	- 44 - ₁₄		
		223.00		6692.376	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.860	2.880	0.609	2.378	2.778	1/800 1/800			
		224.00 225.00		6721.600 6750.735	1.330	2.840	2.890 3.430	0.646	2.411	2.811	1/800			
		225.00		6760.961	1.590	3.510	3.610	0.695	2.445	2.857	1/800	JL Peke		
	- 197	226.00	1.1.1.1.1.1.1	6780.781		2.800	2.860	0.720	2.480	2.880	1/800			
	1	227.00	· ·	6811.039	1.430	2.810	2.860	0.757	2.515	2.915	1/800			
		228.00	29.804	6840.843	1.490	3.120	2.910	0.795	2.549	2.949	1/800			
		229.00	4.5	6869.719	1.510	2.940	3.020	0.831	2.582	2.982	1/800			· · · · ·
	12	230.00		6898.320	1.110	3.000	3.100	0.867	2.614	3 0 1 4	1/800	4 °		
		231.00		6927.857	1.570	3.040	3.090	0.903	2.648	3.048	1/800		<u>11 - 14 - 14 - 14 - 14 - 14 - 14 - 14 -</u>	
		232.00	1 A A A A A A	6957.506	and the second second	3.090	3.110		2.680	3.080 3.108	1/800		<u> </u>	
		233.00		6986.861 7016.476	1.760	3.080 3.120	3.060 3.120	0.977	2.708	3.108	1/800	• 1	1	<u> </u>
	14	234.00	8 - N - F	7046.311	1.690	3.050	3.110	(1) A. M.	2.765	3.165	1/800			
		1	S	7070.684	and a set of the	3.140	3.210	1	2.788	3.188	1/800	Bridge(Water)	<u> </u>
		236.00	1 A	7077.412		3.140	3.210		2.794	3.194	1/800			
		237.00	1 / · · · ·	7107.625	- N. C	3.190	3.340	1.128	2.823	3.223	1/800	-		
		238.00	1.1	7137.982	1.820	3.310	3.680	1.166	2.852	3.252	1/800	1 1		• • • • •
		239.00	1.1.1.1.1	7167.798		3.290	3.490	1.203	2.880	3.280	1/800			1.1.1.1
		240.00	1 3 2 3 4 1	7197.315		3.360	3.500	1.240	2.908	3.308	1/800			
		241.00	1 1 1 1	7227.217	1.630	3.570	3.610	1.278	2.937	3.337	1/800			
			1 1 5 5 5 5	7241.076		4.010	5	1.295	2.950	3.350	1/800	Tugu M	- またい ようたいたいた	
		242+20	1.200	7241.076	ココージャー・1	4.570	4.980		1.38.54	0.400		Tugu M	uda	
		243.00	1 N N	7241.076		4.970 4.830	1			0.400		Bridge		
	1.5	244.00	14.1	7241.076	1.790	4.050	4.030		1.11	0.400	18 J. C. S.	Sinde		<u> </u>

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Name of Structure	SEMA	ARANG RIVER	Cat	egory ulation	Non-un Flow Caic		Page	8/18
					L		l_	
:								
		Table	3 Mike 1	1 Calculat	ion Outpu	t i sta		
	DATA PARA)UNDARY FIL \LCULATED		EM(12).8SF FEB-1998,	15:15	
					EMARANG S	SEMARANG	SEMARANG	
	н 1998 1		0.000	0.098	0.196	0.294	0.392	
	1998 1	1 0 10	2.81	2.88	2.76 2.77	2.65	2.55	
	1998 1 1998 1	1 0 20 1 0 30	3.12	2.84	2.74	2.64	2.54	
,	1998 1	1 0 30	2.83	2.88 2.83	2.78	2.67	2.57	
	1998 1 1998 1	1 0 50	2.84	2.89	2.78	2.67;	2.57	
	1998 1	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3.09 2.85	2.83	2,72	2.62	2.53 2.57	
	1998 1	1 1 20	3.08	2.82	2.71	2.62	2.53	
	1998 1 1998 1	1 1 30 1 1 40	2.86	2.9	2.79 2.71	2.68	2.56 2.54	
	1998 1	1 1 50	2.87	2.9	2.8	2.68	2.56	
	1998 1 1998 1	1 2 0 1 2 10	3.05 2.88	2.8	2.7	2.61	2.54	
	1998 1	1 2 20	3.03	2.79	2.69	2.61	2.55	
	1998 1 1998 1	1 2 30 1 2 40	2.89	2.93	2.81 2.67	2.67	2.53	
	1998 1	1 2 50	2.91	2.94	2.81	2.61	2.56 2.51	rah tahu Nasi tahu
	1998 1 1998 1	1 3 0 1 3 10	2.98	2.75	2.66 2.81	2.62	2.58	
	1998 1	1 3 20	2.94	2.72	2.65	2.63	2.48 2.61	
	1998 1 1998 1	1 3 30 1 3 40	2.95	2.96	2.79 2.64	2.6	2.44	
	1998 1	1 3 50	2.97	2.96	2.76	2.65 2.55	2.63	
	1998 1	1 4 0	2.84	2.65	2.63	2.67	2.66	
		FIL : SEM(12).R	and the second second	UNDARY FIL		em(12).BSF		
	Para	ME : SEM(12).R	· · · · · · · · · · · · · · · · · · ·	LCULATED :		FEB 1998,		
	ана стана стана При стана с При стана				EMARANG S			
		OUR : MIN	0.489	0.587	0.685	0.783	0.881	
	1998 1	1 0 0	2.46	2.37	2.28	2.2	2.13	
	1998 1 1998 1	1 0 10 1 0 20	2.47	2.38	2.29	2.2	2.13	
	1998 1	1 0 20	2.44	2.36 2.37	2.27 2.28	2.19 2.19	2.12	
	1998 1	1 0 40	2.44	2.35	2.20	2.19	2.11	[ALT] 같은 비사
	1998 1	1 0 50	2.46	2.36	2.27	2.19	2.11	
	1998 1	1 1 0	2.44	2.36	2.28	2.2	2,12	
	1998 1	1 1 10	2.46	2.36	2.27	2.18	2.1	
	1998 1 1998 1	1 1 20 1 1 30	2.45	2.37	2.29	2.21	2.13	
	1998 1	1 1 30	2.45	2.35	2.25 2.3	2.17	2.1 2.14	
	1998 1	1 1 50	2.40	2.38	2.24	2.22	2.14	
	1998 1	1 2 0	2.47	2.39	2.31	2.23	2.14	
	1998 1	1 2 10	2.42	2.32	2.23	2.15	2.09	

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lame of tructure	SEM	ARA	NG RIVER		egory ulation		niform lculation	Page	9/18
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			ана се		·.				
						·	. <u></u>		
	998 1		2 20	2.48	2.41	2.32			
	998 1 998 1		2 30	2.4	2.3	2.22			
	998 1	: I : 1	2 40 2 50	2.5	2.43	2.34 2.21			
	998 1	1	3 0	2.53	2.44	2.34			
	998 1	i 1	3 10	2.35	2.27	2.2			
	998 1	$\overline{1}$	3 20	2.55	2.46	2.34	2.23		
	998 1	1	3 30	2.33	2.25	2.2	2.15		
	998 1	1		2.57	2.46	2.33	2.2		
	998 1	1	3 50	2.3	2.24	2.2	2.17		
1	998, 1		4 0	2.58	2.45	2.29	2.16	2.07	T
	DAT	ÀFIL	E : SEM	(12).RDF B0	DUNDARY F	ILE :	SEM(12).8	SF	1
			TER : SEM				9-FEB-199		
			• . •		· · · · ·	and the second second		SEMARANO	5
	L. L		: MIN	0.912	1.007	1.101	1.196		
			and the second		· · ·	· . · · · · · ·		· · · ·	
	998 1 998 1	1	0 0	2.11	2.01	1.94			
	998 1	1	• •	2.14	2.01	1.95 1.94	1.89 1.88		
	998 1	1		2.13	2	1.94	1.00		
	998 1	-1	0 40	2.1	2	1.93	1.88		
	98 1	1	0 50	2.12	1.99	1.93	1.86		
	998 1	1	1 0	2.11	2.01	1.94	1.88		
	98 1	1	1 10	2.12	1.99	1.92	1.86		
	998 1	1	1 20	2.11	2.01	1.95	1.88	1.82	
	998 1		1 30	2.11	1.98	1.92	1.86		
	998 1	1	1 40	2.12	2.01	1.95	1.88		
	98 1	1	1 50	2.11	1.98	1.92	1.87		
	98 1	1	2 0	2.12	2.01	1.94	1.87		
	98 1		2 10	2.11	1.99	1.93	1.87		
	98 1 98 1	1	2 20	2.12	2.01	1.93	1.86		
	98 1	1	2 30 2 40	2.11	1.99	1.94 1.92	1.88 1.85		
	98 1	-1	2 50	2.12	2	1.92	1.05		A CONTRACTOR
	98 1	-1	3 0	2.12	1.99	1.95	1.84	1.84	
	98 1	-īl	3 10	2.12	2.02	1.97	1.04	1.85	
	98 1	$\overline{1}$	3 20	2.1	1.97	1.89	1.82	1.03	
19	98 1	1	3 30	2.13	2.04	1.98	1.92	1.86	
19	98 1	1	3 40	2.08	1.94	1.87	1.81	1.76	
	98 1	1	3 50	2.15	2.06	2	1.94		
19	98 1	1	4 0	2.06	1.92	⇒ 1.86	1.81	1.77	
	DAT/ Par/		e : Sem([er : Sem()	12).RDF BO 12).RRF CA	A		SEM(12).89 9-FEB-1998		
	 		SEI	ARANG SEI	MARANG SP	MARANG	SEMARANG	SEMARANC	
	H.	OLIR	: MIN	1.386		1.575	1.670	1.765	
							<u>.</u>		
	98 1	1	0 0	1.76	1.71	1.65	1.6	1.55	
110	98 1	- 1	0 10	1.77	1.71	1.65	1.6	1.55	and the
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Name of Structure	S	EMAR	ANG	RIVER		tegory culation	Non-un Flow Calc	iform ulation	Page	10/18
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n Linter				·						
Г	1998	-	11-1	20		·····				·
	1998	-1	$\frac{1}{1}$	30	$\frac{1.76}{1.75}$	1.7	1.64	1.58		
	1998	1-	il-i	40	1.75	1.69	1.64	1.59		
	1998	$-\overline{\mathbf{i}}$	iti	50	1.76	1,69	1.63	1.58		
	1998	-îl	1 2		1.74	1.68	1.65	1.59		
	1998	1		10	1.74	1.00	1.63	1.57		
	1998	1		20	1.74	1.68	1.65	1.6		
	1998	1		30	1.77	1.71	1.62	1.57		
	1998		2		1.73	1.67	1.66	1.6		
	1998	11	2		1.78	1.72	1.62	1.57		
	1998		3		1.72	1.67	1.66	1.6		
	998				1.78	1.07	1.62	1.58		
	998	ī		20	1.72	1.72	1.65	1.59		
	998	11		30	1.72	1.07	1.63	1.59	1.55	
	998	1 1		40	1.72	1.68	1.64	1.58	1.52	
	998	1 1	+	50	1.72	1.00	1.64	1.6	1.56	
	998		1-4	0	1.73	1.7	1.63	1.57	1.51	
				<u> </u>	1.75	1./	1.66	1.62	1.57	
		ATA (**	íe 🔅	001					where we wanted to see the	
		ATA FI		: SEM	(12).RDF BC	UNDARY FI	LE : SE	M(12).BS	where we wanted to see the	
		ata fi Arami		: Sem : Sem	(12).RDF BC (12).RRF CA	UNDARY FI		M(12).BS	F	
		ARAM	TER	: SEM	(12).RRF CA	LCULATED	: 9.	.M(12).BS FEB-1998	F 3, 15:15	
		ARAM		: SEM	(12).RRF CA	LCULATED	: 9-1 MARANG SE	M(12),BS FEB-1998 MARANG	F 3, 15:15 SEMARANG	
	P.	ARAM	ter R : Min	: SEM Se	(12).RRF CA MARANG SE 1.859 19	LCULATED MARANG SE 954.000	: 9.1 MARANG SE 2.049	M(12),BS FEB-1998 MARANG 2.144	F 3, 15:15 SEMARANG 2.238	
	P, 998j	ARAM(HOUF 1 1	TER R : Min	: SEM SE N 0	(12).RRF CA MARANG SE 1.859 19 1.5	LCULATED MARANG SE 954.000 1.46	: 9-1 MARANG SE 2.049 1.42	M(12).BS FEB-1998 MARANG 2.144 1.37	F 3, 15:15 SEMARANG 2.238 1.33	
1	P/ 998 998	ARAM(HOUF 1 1 1 1	TER R : Min 0 0	: SEM SE N 0 10	(12).RRF CA MARANG SE 1.859 19 1.5 1.5	LCULATED MARANG SE 954.000 1.46 1.45	: 9. MARANG SE 2.049 1.42 1.4	M(12),BS FEB-1998 MARANG 2.144 1.37 1.36	F 3, 15:15 SEMARANG 2.238 1.33 1.32	
	998 998 998 998	ARAM(HOUF 1 1 1 1 1 1	TER R : Mir 0 0	: SEM SE 1 10 20	(12).RRF CA MARANG SE 1.859 19 1.5 1.5 1.49	LCULATED MARANG SE 954.000 1.46 1.45 1.45 1.44	: 9-1 MARANG SE 2.049 1.42 1.4 1.4	M(12).BS FEB-1998 MARANG 2.144 1.37 1.36 1.36	F 3, 15:15 SEMARANG 2.238 1.33 1.32 1.32	
	998 998 998 998 998	ARAM(HOU) 1 1 1 1 1 1 1 1	TER R : MIN 0 0 0	: SEM SE 0 10 20 30	(12).RRF CA MARANG SE 1.859 19 1.5 1.5 1.49 1.48	LCULATED MARANG SE 954.000 1.46 1.45 1.44 1.44	: 9- MARANG SE 2.049 1.42 1.4 1.4 1.39	M(12).BS FEB-1998 MARANG 2.144 1.37 1.36 1.36 1.36 1.35	F 3, 15:15 SEMARANG 2.238 1.33 1.32 1.32 1.31	
	998 998 998 998 998 998	ARAM(HOUI 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TER : Min 0 0 0 0 0	: SEM SE 10 20 30 40	(12).RRF CA MARANG SE 1.859 19 1.5 1.5 1.49 1.48 1.49	LCULATED MARANG SE 054.000 1.46 1.45 1.44 1.44 1.44	: 9- MARANG SE 2.049 1.42 1.4 1.4 1.39 1.39	M(12).BS FEB-1998 MARANG 2.144 1.37 1.36 1.36 1.36 1.35 1.35	F 3, 15:15 SEMARANG 2.238 1.33 1.32 1.32 1.31 1.31	
	998 998 998 998 998 998 998	ARAM(HOUF 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TER : Min 0 0 0 0 0	: SEM SE 0 10 20 30 40 50	(12).RRF CA MARANG SE 1.859 19 1.5 1.5 1.49 1.48 1.49 1.48 1.49 1.48	LCULATED MARANG SE 954.000 1.46 1.45 1.44 1.44 1.44 1.44 1.43	: 9- MARANG SE 2.049 1.42 1.4 1.4 1.39 1.39 1.39	M(12).BS FEB-1998 MARANG 2.144 1.37 1.36 1.36 1.35 1.35 1.35	F 3, 15:15 SEMARANG 2.238 1.33 1.32 1.32 1.31 1.31 1.31 1.31	
	998 998 998 998 998 998 998 998 998	ARAM(HOUI 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TER : Min 0 0 0 0 0	: SEM SE 0 10 20 30 40 50 0	(12).RRF CA MARANG SE 1.859 19 1.5 1.5 1.49 1.48 1.49 1.48 1.48 1.48	LCULATED MARANG SE 954.000 1.46 1.45 1.44 1.44 1.44 1.44 1.43 1.44	: 94 MARANG SE 2.049 1.42 1.4 1.4 1.39 1.39 1.39 1.39 1.39	M(12).BS FEB-1998 2.144 1.37 1.36 1.36 1.35 1.35 1.35 1.35 1.35	F 3, 15:15 SEMARANG 2.238 1.33 1.32 1.32 1.31 1.31 1.31 1.31 1.31	
	P, 998 998 998 998 998 998 998 998 998	ARAM(HOUF 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TER : Min 0 0 0 0 0	: SEM SE 10 20 30 40 50 0 10	(12).RRF CA MARANG SE 1.859 19 1.5 1.5 1.49 1.48 1.49 1.48 1.48 1.48 1.48 1.48	LCULATED MARANG SE 954.000 1.46 1.45 1.44 1.44 1.44 1.44 1.43 1.44 1.44 1.44	: 9-1 MARANG SE 2.049 1.42 1.4 1.4 1.39 1.39 1.39 1.39 1.39 1.39 1.39	M(12).BS FEB-1998 2.144 1.37 1.36 1.36 1.35 1.35 1.35 1.35 1.35 1.35	F 3, 15:15 SEMARANG 2.238 1.33 1.32 1.32 1.31 1.31 1.31 1.31 1.31 1.31	
	998 998 998 998 998 998 998 998 998 998	ARAM(HOUF 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TER 0 0 0 0 0 0 0 0 0 1 1 1	: SEM SE 10 20 30 40 50 0 10 20	(12).RRF CA MARANG SE 1.859 19 1.5 1.5 1.49 1.49 1.48 1.49 1.48 1.48 1.49 1.48 1.49 1.48	LCULATED MARANG SE 954.000 1.46 1.45 1.44 1.44 1.44 1.43 1.44 1.44 1.44 1.44	: 9- MARANG SE 2.049 1.42 1.4 1.4 1.39 1.39 1.39 1.39 1.39 1.4 1.39	M(12).BS FEB-1998 2.144 1.37 1.36 1.36 1.35 1.35 1.35 1.35 1.35 1.35 1.35 1.35	F 3, 15:15 SEMARANG 2.238 1.33 1.32 1.32 1.31 1.31 1.31 1.31 1.31 1.31 1.31 1.31 1.31	
	998 998 998 998 998 998 998 998 998 998	ARAM(HOUF 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TER 0 0 0 0 0 0 0 0 0 1 1 1 1	: SEM SE 10 10 20 30 40 50 0 10 20 30	(12).RRF CA MARANG SE 1.859 19 1.5 1.5 1.49 1.48 1.49 1.48 1.48 1.48 1.48 1.49 1.48 1.49 1.48 1.49 1.48	LCULATED MARANG SE 054.000 1.46 1.45 1.44 1.44 1.44 1.44 1.43 1.44 1.44 1.43 1.44	: 9- MARANG SE 2.049 1.42 1.4 1.4 1.39 1.39 1.39 1.39 1.39 1.4 1.39 1.4	M(12).BS FEB-1998 2.144 1.37 1.36 1.36 1.35 1.35 1.35 1.35 1.35 1.35 1.35 1.35	F 3, 15:15 SEMARANG 2.238 1.33 1.32 1.32 1.31 1.31 1.31 1.31 1.31 1.31 1.31 1.31 1.31	
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	1998	1	1		40	0.76	0.74	0.72	0.7	0.68	
	1998	1	1		50	0.77	0.74	0.72	0.7	0.68	
	1998	1	1	2	0	0.76	0.74	0.72	0.7	0.68	
	1998	1	1	2	10	0.77	0.74	0.72	0.7	0.68	
· · · · · ·	1998	<u> </u>	1	2	20	0.77	0.75	0.72	0.7	0.68	
	1998	<u></u>	1	2	30	0.77	0.74	0.72	0.7	0.68	
	1998	· 1	1		40	0.76	0.74	0.72	0.7	0.68	
	1998 1998			2	50	0.77	0.74	0.72	0.7	0.68	
	1998	- <u>1</u> +			0 10	0.76	0.74	0.72	0.7	0.68	
	1998	-++	- <u>+</u> -		20	0.77	0.75	0.72	0.7	0.68	
	1998	1	1		30	0.78	0.74	0.72	0.7	0.68	
	1998	5 1	$-\frac{1}{1}$		40	0.76	0.75	0.72	0.71	0.69	
1 1 L L L	1998	$\frac{1}{1}$	Ť		50	0.70	0.74	0.72	0.7	0.68	
	1998	1	-i+	4	0	0.77	0.74	0.72	0.7	0.68 0.68	
.		1	. 1		<u>_</u>	I			U.7	0.00	

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Name of Structure		SEMAR	ANG	RIVE	R		Category alculation	•		uniform alculatio	n .	Page	13/18
·									· · · ·				
					2				а. 1	· ·			
	[DATA				0.000	DOLINDA			001//10			1
							BOUNDA			SEM(12			
				1:5	-						-	, 15:15	
			4. V. F									EMARANO	
		HO	JR:N	IIN :		3.616	3.70	3.3	3789.000) 3.8	366	3.944	
	1998	• •		0 0	• • •	0.7			0.67		.66	0.64	
1997 - 1997 -	1998		- ł) 10		0.69		8			.65	0.63	
	1998	1 1	*) 20		0.68			0.65		64	0.63	
	1998) 30		0.68			0.65		.63	0.62	
	1998) 40		0.67			0.64		.63	0.61	and the second
	1998) 50	L	0.68			0.65		.64	0.62	
	1998		1	0	<u></u>	0.68			0.65		63	0.62	
	1998			10		0.67			0.65		63	0.62	
	1998			20		0.68	0.6		0.65		64	0.62	
	1998		$\frac{1}{1}$	30		0.67	0.6		0.65		63	0.62	
	1998		11 1	40	1	0.68	0.6		0.65		63	0.62	
	1998 1998		$\frac{1}{1}$	50		0.68	0.6		0.65		64	0.63	
	1998			2 0 2 10		0.68 0.67	0.6 0.6		0.65		63	0.62	
	1998			2 20		0.67	0.6	1	0.65		64 63	0.63	
	1998		$\frac{1}{1}$			0.67			0.65		64	0.62	
	1998			2 40		0.68	0.6		0.65		64	0.62	and the state
	1998			2 50		0.67	0.0		0.65		63	0.62	
	1998		$\frac{1}{1}$			0.68	0.6		0.65		64	0.63	
	1998			10		0.68	0.6	Ť	0.65		63	0.62	t By
	1998	-1^{-1}		20		0.67	0.6		0.65	1	64	0.63	
	1998	$ \overline{1} $		1 30		0.68	0.6		0.65	1 .	63	0.62	
	1998	1	-	40		0.67	0.6		0.65		64	0.62	
	1998		1 3	50		0.68			0.65	·	64	0.62	
	1998		1 4			0.67			0.65		64	0.62	
		DATA	H F		M(12		BOUNDA			SEM(12			
							CALCULA			9.FEB-1			
	<u>* : : : :</u>						431 - 14 <u></u>	2012	· · · · · ·	·			
			े 10 में फ		1. E .						-	EMARANG	
	$< c \Omega$	1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 -	JR : M		· · · · · ·	4.021	4.10		4.197		· · ·	4.297	
	1998		-i ~			0.63			0.6).6	0.59	
	1998			10	1	0.62	0.		0.58		59	0.58	
	1998			20		0.62	0.		0.59		59	0.58	
	1998			30		0.6			0.56		57	0.55	
	1998			40		0.6	0.5		0.58		58	0.57	
	1998		1 0	50	، ژور خرف چ	0.61	0.5		0.58		58	0.57	
	1998		1 1	0	- <u></u>	0.61	0.5		0.58		58	0.57	
	1998		1]	10	· ; · -	0.61	0.5		0.57		58	0.56	
	1998		$\frac{1}{1}$	20		0.61	0.5		0.58		58	0.57	
	1998 1998		$\frac{1 \cdot 1}{1 \cdot 1}$	30		0.61	0.5		0.57		58 58	0.56 0.57	
	1 I U U X											11 5 /1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

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Structure	f s	EMAR/	ANG R	IVER		ategory lculation	Non-uni Flow Calc		Page	14/18
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	÷.,	1.11								
en tot			n en			aliana ana ang	n an training and training and training			
		a star	anda Tabla				italia en 1240. Nationalem		u te Maria	
			e estas Alta da	an An Anna an			det sinderfahr. Antone en johan			
	1998	1 1	2	0	0.6	0.59	0.57	0.57	0.57	·
	1998			10	0.62	0.6	0.59	0.59	0.58	
•	1998			20	0.6	0.59	0.57	0.57	0.56	al an an
	1998			30	0.61	0.6	0.58	0.59	0.57	
	1998 1998			40	0.61	0.59	0.57	0.57	0.57	1. A.
	+	$\frac{1}{1}$		50	0.61	0.59	0.58	0.58	0.57	· .
5 (14) (14)	1998 1998		3	0	0.61	0.6	0.58	0.58	0.57	
	1998	1 1		10	0.6	0.59	0.57	0.58	0.56	
	1998	$\frac{1}{1}$		20	0.61	0.6	0.58	0.58	0.57	
	1998	$-\frac{1}{1}$		30	0.61	0.59	0.58	0.58	0.57	
	1998	$\frac{1}{1}$ 1		40 50	0.61	0.59	0.58	0.58	0.57	
	1998	$\frac{1}{1}$ $\frac{1}{1}$	4		0.61	0.59	0.58	0.58	0.57	
		1 <u>1</u>	· · · · · ·	0	0.61	0.59	0.57	0.57	0.56	
		ATA FIL		SEM(12	2).RDF B	oundary fi	LE: SE	EM(12).BSF		
	l P	ARAME	TER ;	SEM(12	2).RRF C	ALCULATED	: 9	FEB-1998,	15:15	an an an an
				SEM/	RANG SI	EMARANG SE				
		HOUR	A MAIN							
1.1.1			• • 1401 A		4.367	4.392				1. A.
	1998	1 1		1. 1. 1. 1. 1.	4.367	4.392	4.488	4.584	4.680	
	1998 1998	1 1	0	0	0.58	0.58	4.488	4.584	4.680 0.56	
	1998	$\begin{array}{c c}1 & 1\\\hline 1 & 1\\\hline 1 & 1\end{array}$	0	0	0.58	0.58	4.488 0.57 0.58	4.584 0.56 0.58	4.680 0.56 0.57	
		1 1	0 0 0	0 10 20	0.58 0.56 0.57	0.58 0.59 0.57	4.488 0.57 0.58 0.57	4.584 0.56 0.58 0.56	4.680 0.56 0.57 0.55	
	1998 1998	1 1	0 0 0 0 0	0 10 20 30	0.58 0.56 0.57 0.54	0.58 0.59 0.57 0.57	4.488 0.57 0.58 0.57 0.56	4.584 0.56 0.58 0.56 0.55	4.680 0.56 0.57 0.55 0.54	
	1998 1998 1998 1998 1998 1998	1 1	0 0 0 0	0 10 20	0.58 0.56 0.57 0.54 0.56	0.58 0.59 0.57 0.57 0.56	4.488 0.57 0.58 0.57 0.56 0.56	4.584 0.56 0.58 0.56 0.55 0.55	4.680 0.56 0.57 0.55 0.54 0.55	
	1998 1998 1998 1998 1998 1998 1998	1 1	0 0 0 0	0 10 20 30 40	0.58 0.56 0.57 0.54 0.56 0.55	0.58 0.59 0.57 0.57 0.56 0.58	4.488 0.57 0.58 0.57 0.56 0.56 0.56 0.56	4.584 0.56 0.58 0.55 0.55 0.55 0.55	4.680 0.56 0.57 0.55 0.54 0.55 0.55	
	1998 1998 1998 1998 1998 1998 1998 1998	1 1	0 0 0 0 0 0 1	0 10 20 30 40 50	0.58 0.56 0.57 0.54 0.56 0.55	0.58 0.59 0.57 0.57 0.56 0.58 0.58	4.488 0.57 0.58 0.57 0.56 0.56 0.56 0.57 0.56	4.584 0.56 0.58 0.55 0.55 0.55 0.55 0.56 0.55	4.680 0.56 0.57 0.55 0.54 0.55 0.55 0.55	
	1998 1998 1998 1998 1998 1998 1998 1998	1 1	0 0 0 0 0 1 1 1 1 2	0 10 20 30 40 50 0 10 20	0.58 0.56 0.57 0.54 0.56 0.55 0.56	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.56 0.57	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.55 0.55 0.55	4.680 0.56 0.57 0.55 0.54 0.55 0.55 0.55 0.55	
	1998 1998 1998 1998 1998 1998 1998 1998	1 1	0 0 0 0 1 1 1 1 1 1 2	0 10 20 30 40 50 0 70 20 30	0.58 0.56 0.57 0.54 0.56 0.55 0.56 0.55	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.58 0.58 0.57	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.56 0.57 0.56	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.55 0.56 0.56 0.56	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
	1998 1998 1998 1998 1998 1998 1998 1998	1 1	0 0 0 0 1 1 1 2 1 2 1 2 1 2	0 10 20 30 40 50 0 70 20 30 40 50 50 70 70 70 70 70 70 70 70 70 7	0.58 0.56 0.57 0.54 0.56 0.55 0.56 0.55 0.57	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.58 0.57 0.57	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.56 0.57 0.56 0.56	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.55 0.56 0.56 0.55	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
	1998 1998 1998 1998 1998 1998 1998 1998	1 1	0 0 0 0 1 1 1 2 1 2 1 2 1 2 1 2	0 10 20 30 40 50 0 7 10 20 30 40 50 50 50 50 7 50 50 50 50 50 50 50 50 50 50	0.58 0.56 0.57 0.54 0.56 0.55 0.55 0.55 0.57 0.55	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.57 0.57 0.57	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.56 0.57 0.56 0.56 0.56 0.57	4.584 0.56 0.58 0.55 0.55 0.55 0.55 0.56 0.56 0.55 0.56 0.55 0.56	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
	1998 1998 1998 1998 1998 1998 1998 1998	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0 0 0 0 1 1 1 2 1 2 1 2	0 10 20 30 40 50 50 20 30 40 50 50 50 50 50 50 50 50 50 5	0.58 0.56 0.57 0.54 0.56 0.55 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.55	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.57 0.58 0.56	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.56 0.57 0.56 0.56	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.56 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
	1998 1998	1 1	0 0 0 0 1 1 1 1 2 1 2 1 2 2	0 10 20 30 50 50 7 10 20 30 40 50 50 50 50 50 50 50 50 50 5	0.58 0.56 0.57 0.54 0.56 0.55 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.56 0.56	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.57 0.58 0.56 0.58	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.56 0.56 0.56 0.56 0.57 0.56 0.57 0.56	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
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	1998 1998	1 1 1 1	0 0 0 0 1 1 1 1 2 1 2 2 2 2 2 2 2 2 2 2	0 10 20 30 40 50 0 20 30 40 50 0 40 50 0 40 50 0 40 50 50 50 50 50 50 50 50 50 5	0.58 0.56 0.57 0.54 0.55 0.55 0.55 0.57 0.55 0.57 0.55 0.55	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.58 0.56 0.58 0.56 0.58 0.56 0.58	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.57 0.57 0.57 0.56 0.57 0.57 0.57 0.57 0.57 0.56 0.57	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
	1998 1998	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0 0 0 0 1 1 1 1 1 2 2 2 1 2 2 2 2 2 2 2	0 10 20 30 40 50 0 40 50 0 40 50 30 40 50 50 50 50 50 50 50 50 50 5	0.58 0.56 0.57 0.54 0.55 0.55 0.55 0.57 0.55 0.57 0.55 0.56 0.56 0.56 0.56 0.56 0.57	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.58 0.56 0.58 0.56 0.58 0.56 0.58 0.56 0.58 0.56	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.56 0.55 0.56 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
	1998 1998	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0 0 0 1 0 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2	0 10 20 30 40 50 50 70 70 70 70 70 70 70 70 70 7	0.58 0.56 0.57 0.54 0.55 0.55 0.55 0.57 0.55 0.57 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.57 0.55	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.58 0.56 0.58 0.56 0.58 0.56 0.58 0.56 0.58 0.57 0.57	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.56 0.56 0.56 0.57 0.56 0.57 0.56 0.56 0.57 0.56 0.57 0.56 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.56 0.57 0.56 0.57 0.5	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.56 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
	1998 1998	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0 0 0 1 1 1 1 1 2 1 2 2 2 2 2 2 2 2 3	0 10 20 30 40 50 50 7 40 50 7 40 50 7 40 50 7 5 5 5 50 50 5 50 50 5 50 5	0.58 0.56 0.57 0.54 0.55 0.55 0.55 0.57 0.55 0.57 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55 0.56 0.56 0.55 0.55 0.55 0.55 0.56 0.56 0.55 0.57 0.55 0.55 0.55 0.55 0.55 0.57 0.55 0.55 0.57 0.57 0.57 0.55 0.57 0.57 0.55 0.57 0	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.58 0.56 0.58 0.56 0.58 0.56 0.58 0.56 0.58 0.57 0.57 0.57	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.57 0.56 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.56 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55 0.56 0.55 0.55 0.56 0.55 0.56 0.55 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.56 0.55 0.56 0.56 0.55 0.56 0.56 0.55 0.56 0.56 0.55 0.56 0.56 0.56 0.56 0.56 0.55 0.56	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
	1998 1998	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0 0 0 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2	0 10 20 30 40 50 0 7 10 20 30 40 50 0 10 50 0 10 50 0 10 50 10 50 10 50 10 10 10 10 10 10 10 10 10 1	0.58 0.56 0.57 0.54 0.55 0.55 0.55 0.57 0.55 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55 0	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.58 0.56 0.58 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.56 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55 0.56 0.55 0.56 0.55 0.55 0.56 0.55 0.56 0.55 0.55 0.56 0.56 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
	1998 1998	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0 0 0 0 1 1 1 1 2 1 2 1 2 2 2 3 2 4 2 5 3 3 1 3 2 2 4 2 5 3 3 1 3 2	0 10 20 30 50 50 50 7 10 50 7 10 50 7 10 50 7 10 10 10 10 10 10 10 10 10 10	0.58 0.56 0.57 0.54 0.55 0.55 0.55 0.57 0.55 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.55 0.57 0.55 0.55 0.57 0.57 0	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.58 0.56 0.58 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.57 0.57 0.57	4.488 0.57 0.58 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57 0.56 0.57	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.56 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.57	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
	1998 1998	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0 0 0 0 1 1 1 1 2 1 2 1 2 2 1 2 2 2 2 2	0 10 20 30 50 50 50 50 70 70 70 70 70 70 70 70 70 7	0.58 0.56 0.57 0.54 0.55 0.55 0.55 0.57 0.55 0.57 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.58 0.56 0.58 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.57 0.57 0.57 0.57	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.57 0.57 0.57 0.57 0.57 0.57 0.57 0.57 0.57	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.56 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55 0.56 0.55 0.56 0.55 0.55 0.56 0.55 0.56 0.55 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.56 0.55 0.56 0.55 0.56 0.56 0.56 0.55 0.55 0.56 0.56 0.55 0.56 0.55	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
	1998 1998	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0 0 0 0 0 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 3 3 3 3 3 3 3 3 3 3	0 10 20 30 50 50 50 50 70 70 70 70 70 70 70 70 70 7	0.58 0.56 0.57 0.54 0.55 0.55 0.55 0.57 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.55 0.57 0.55 0.55 0.57 0.55 0.55 0.57 0.55 0.57 0.55 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.57 0.55 0.57 0.57 0.55 0.57 0	0.58 0.59 0.57 0.57 0.57 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.58 0.56 0.58 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.57 0.57 0.57 0.57	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.57 0.56 0.57	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.55 0.56 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55 0.56 0.55 0.56 0.55 0.55 0.56 0.55 0.56 0.55 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.57 0.57 0.55 0.57	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	
	1998 1998	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0 0 0 0 1 1 1 1 1 1 2 1 2 2 1 2 2 1 2 2 2 2	0 10 20 30 40 50 50 7 0 7 10 20 30 40 50 7 10 50 7 10 10 7 10 10 7 10 10 10 10 10 10 10 10 10 10	0.58 0.56 0.57 0.54 0.55 0.55 0.55 0.57 0.55 0.57 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0.56 0.55 0.57 0.55 0	0.58 0.59 0.57 0.57 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.58 0.56 0.58 0.56 0.58 0.56 0.58 0.57 0.57 0.57 0.57 0.57 0.57 0.57 0.57	4.488 0.57 0.58 0.57 0.56 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.56 0.57 0.57 0.57 0.57 0.57 0.57 0.57 0.57 0.57 0.57 0.57	4.584 0.56 0.58 0.55 0.55 0.55 0.56 0.56 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.55 0.56 0.55 0.56 0.55 0.55 0.56 0.55 0.56 0.55 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.55 0.56 0.56 0.55 0.56 0.55 0.56 0.56 0.56 0.55 0.55 0.56 0.56 0.55 0.56 0.55	4.680 0.56 0.57 0.55 0.55 0.55 0.55 0.55 0.55 0.55	

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Name of Structure	s S	EMARANG RIVER	Ca Cal	tegory culation	Non-ui Flow Cal	niform Iculation	Page	15
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		1						. 1
	1 C	· ·			and and a second se			
				n in the state of				
I					вс.	001/10) D	er] .
а. 		DATA FILE : SEN PARAMETER: SEN	1(12).RDF B			SEM(12).B 9-FEB-199		
			• •					
1 A.		the second se					SEMARANG	
		HOUR : MIN	4.776	4.873	4.969	5.065		
1. A.	1998	1 1 0 0	0.55	0.54	0.54	0.53	1	
	1998	1 1 0 10	0.56	0.55	0.55	0.54		
. :	1998	1 1 0 20	0.55	0.54	0.53	0.53		1.4
	1998 1998	1 1 0 30 1 1 0 40	0.53	0.53	0.52	0.51 0.52		1. A.
	1998	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.54	0.54	0.53	0.52		
	1998	1 1 0 30 1 1 1 0	0.54	0.54	0.53	0.52		1 · ·
	1998		0.54	0.54	0.53	0.52		a de la
1	1998	1 1 1 20	0.55	0.54	0.53	0.52		
	1998	1 1 1 30	0.54	0.53	0.53	0.52	0.52	
	1998	1 1 1 40	0.55	0.54	0.54	0.53		
	1998	1 1 1 50	0.54	0.53	0.52	0.52		1.1
- 1 - 1 - E	1998	1 1 2 0	0.55	0.54	0.53	0.53		
	1998	1 1 2 10	0.54	0.54	0.53	0.52		
	1998	1 1 2 20	0.54	0.54	0.53	0.52		
	1998	1 1 2 30	0.55	0.54	0.53	0.53		
	1998	1 1 2 40	0.54	0.53	0.52	0.52		
	1998 1998	1 1 2 50 1 1 3 0	0.55	0.54	0.54	0.53		11. L
	1998	1 1 3 0 1 1 3 10	0.54	0.53	0.04	0.52		
	1998	1 1 3 10	0.55	0.54	0.54	0.53	0.52	
	1998	1 1 3 30	0.54	0.54	0.53	0.53	0.51	
	1998	1 1 3 40	0.55	0.54	0.53	0.52	0.51	
	1998	1 1 2 50	0.54	0.53		0.52		
	1998	1 1 4 0	0.55	0.54	0.53	0.53		· · ·
ſ	1	ATA FILE : SEM	(12).RDF B	OUNDARY F	F : .	SEM(12).BS	۶F	
		ARAMETER : SEM				FEB-199		
		1	MARANG SI	an state a state	N 85.5	 Applied as the 		
		HOUR : MIN	5.257	5.353	5,449	5,545	5.641	
	1000		ほうしょう たち					· · · ·
	1998 1998	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.51	0.5	0.49		
	1998	1 1 0 10 1 1 0 20	0.52	0.52	0.51	0.5	0.49 0.48	
	1998		0.51	0.5	0.5	0.49		
	1998	1 1 0 30	0.51	0.49	0.48	0.48	0.47	
	1998	أخطعهم ومطعجه منسبة تؤدده بالموده	0.51	0.5	0.49	0.49		
			0.5	0.5	0.49	0.48	0.48	
	1998	1 1 1 10	0.51	0.51	0.5	0.49	0.49	
	1998	1 1 1 20	0.5	0.49	0.49	0.48	0.47	
	1998	1 1 30	0.51	0.51	0.5	0.49	0.49	
	1998	1 1 1 40	0.51	0.5	0.49	0.48	0.47	
-	1998	1 1 1 50	0.5	0.5	0.49	0.49	0.48	
	1998	1 1 2 0	0.51	0.51	0.5	0.49	0.48	251 - 11
	1998	1 1 2 10	0.5	0.49	0.49	0.48	0.47	

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Name of Structure	SEMARANG RIVER	Category Calculation	Non-uniform Flow Calculation	Page	16/18
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1998				10					0.47
1998	1								
1998	1	1 -				,	·	0.48	0.47
1998	1					1	0,5	0.5	0.49
1998	1		2					0.48	0.47
1998	1	1	3				0.49	0.49	0.49
1998	1	1	3		,	0.51	0.5	0.49	0.48
1998	1	1	3			0.49	0.49	0.48	0.48
1998	1	1	3	30			0.5	0.5	0.49
1998	1	1	3	40		0.49	0.49	0.48	0.47
1998	1	1	3	50	1	0.51	0.5	0.5	0.49
1998	1	1	4	0	0.51	0.5	0.49	0.48	0.47
	DAT	A FIL	E	: S	EM(12).RDF	BOUNDARY	FILE	SEM(12).BS	
	PAR	AME	TER	: Š	EM(12).RRF	CALCULATE	D	9-FEB-1998	
		<u>.</u>			Contract of the second s	and the second	and the second		
	្រំ		: MI	NI :	SEMARANG	SEMARANG	SEMARANG	SEMARANG	
					5.737	5.834	5.930	6.026	6.122
1998	1	1	0	0		0.47	0.47	0.461	0.45
1998	1	1	0	10		0.48	0.47	0.46	0.45
1998	1	1	0	20	0.47	0.46	0.46	0.45	0.44
1998	1	1	0	30		0.46	0.45	0.44	0.44
1998	1	1	0	40		0.47	0.46	0.46	0.45
1998	1	1	0	50	0.47	0.46	0.45	0.44	0.43
1998	1	1	1	0	0.47	0.47	0.46	0.46	0.45
1998	1	- 1	1	10		0.47	0.46	0.45	0.44
1998	1	1	1	20	0.46	0.46	0.45	0.45	0.44
1998	1	1	1	30	0.48	0.48	0.47	0.46	0.45
1998	1	1	1	40	0.46	0.46	0.45	0.44	0.43
1998	1	-1	_1	50	0.48	0.47	0.47	0.46	0.46
1998	1	-1	2	0	0.47	0.46	0.45	0.44	0.43
1998	1	1	2	10	0.47	0.46	0.46	0.46	0.46
1998	1	1	2	20	0.48	0.47	0.46	0.45	0.44
1998	1	_1	2	30	0.46	0.46	0.45	0.45	0.45
1998	1	_1	2	40	0.49	0.48	0.47	0.46	0.44
1998	1	1	2	50	0.46	0.45	0.45	0.44	0.44
1998	1	1	3	0	0.48	0.48	0.47	0.46	0.45
1998	1	1	3	10	0.47	0.46	0.45	0.44	0.43
1998	ľ	-1	3	20	0.48	0.47	0.47	0.47	0.46
1998	1	1	3	30	0.47	0.46	0.45	0.44	0.43
1998	1	1	3	40	0.47	0.47	0.47	0.46	0.46
1998	1	1	3	50	0.48	0.47	0.46	0.44	0.43
1998	1	1	4	0	0.46	0.46	0.46	0.46	0.46
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Name of Structure	SEMARANG RIVER	Category Calculation	Non-uniform Flow Calculation	Page	17/18

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	DATA FILE : S	SEM(12).RDF	BOUNDARY	FILE :	SEM(12).BSF	
	PARAMETER : \$				9-FEB-1998,	
	HOUR : MIN	SEMARANG 6.218		SEMARANG 6.365	SEMARANG S 6.461	6.527
	1998 1 1 0 0		and the second			0.41
	1998 1 1 0 10					0.42
	1998 1 1 0 2	0.43	0.42		0.39	0.39
	1998 1 1 0 3			0.4		0.41
	1998 1 1 0 4			0.42		0.4
5	1998 1 1 0 50			0.39		0.4
- 11		0.45				0.41
	1998 1 1 1 1				0.37	0.39
	1998 1 1 1 20		0.43	0.42	0.42	0.42
	1998 1 1 1 30	0.44				0.39
	1998 1 1 1 4	0.43	0.42			0.41
÷ 1	1998 1 1 1 50				0.39	0.4
		0 0.42			0.4	
	1998 1 1 2 1				0.4	0.41
·	1998 1 1 2 20			0.39		0.39
	1998 1 1 2 30			0.42		0.42
	1998 1 1 2 40					0.39
1	1998 1 1 2 50			0.42	0.41	0.43
		0 0.44		0.4	0.39	0.38
	1998 1 1 3 1			0.42	0.41	0.43
	1998 1 1 3 2			0.4		0.39
	1998 1 1 3 3			0.41	0.41	0.42
	1998 1 1 3 4		0.44	0.41		0.39
	1998 1 1 3 5			0.4		0.42
		0.46	·			0.4
	DATA FILE : S	SEM(12).RDF	BOUNDARY	FILE :	SEM(12).BSF	
	PARAMETER : 3	SEM(12).RRF	CALCULATE	D :	9 FEB 1998,	15:15
		SEMARANG	SEMARANG	SEMARANG	SEMARANG SI	EMARANG
	HOUR : MIN	6.626		6.825		7.024
	1998 1 1 0	0 0.4		0.38		
ė,	1998 1 1 0 10			0.4		0.38
1	1998 1 1 0 20	0 0.38	0.37	0.36	0.35	0.34
÷	1998 1 1 0 3		0.4	0.4		0.4
	1998 1 1 0 4			0.36		0.32
1	1998 1 1 0 5	0.39				0.41
		0 0.41				0.32
	1998 1 1 1 1	0 0.38	0.38	0.38	0.38	0.4

Name of Structure	SEMARANG RI	VER	Category Calculation	Non-uniform Flow Calculation	Page	18/18
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	a di panala di seria Seria di seria di seria Seria di seria di seria di seria Seria di seria		an de Santa Alexandre de Carlos Alexandre de Carlos Alexandre de Carlos	n de la substance de la substan La substance de la substance de La substance de la substance de		
	DATA FILE :	SEM(12).(RDF BOUNDARY F	1LE : SEM(12).F	SF 11	
	DATA FILE : PARAMETER :	SEM(12).	RDF BOUNDARY F RRF CALCULATED	D: 9-FEB-199	98, 15:15	
	DATA FILE : PARAMETER : HOUR : MIN	SEM(12).I	RRF CALCULATED		98, 15:15	
	PARAMETER : HOUR : MIN 98 1 1 0	SEM(12).I SEMAR/ 7.1 0 0	RRF CALCULATEC ANG SEMARANG S 124 7.223 1.36 0.35	D: 9-FEB-199	98, 15:15	
19	PARAMETER : HOUR : MIN 98 1 1 0 98 1 1 0	SEM(12).I SEMAR 7.1 0 0 10 0	RRF CALCULATED ANG SEMARANG S 124 7.223 1.36 0.35 1.37 0.35	D: 9-FEB-199	98, 15:15 3 SEMARANG	
19 19 19	PARAMETER : HOUR : MIN 98 1 1 0 98 1 1 0 98 1 1 0 98 1 1 0 98 1 1 0	SEM(12).I SEMAR 7.1 0 0 10 0 20 0 30	RRF CALCULATEC ANG SEMARANG S 124 7.223 1.36 0.35	D: 9-FEB-199	98, 15:15 3 SEMARANG	

1 1 1 1 1 1 1					0.01	0.00			1 1
1998	1	1	0	20	0.32	0.35	,	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
1998	1	1	0	30	0.4	0.35	20 g - 4		
1998	1	1	0	40	0.3	0.35			
1998	1	1	0	50	0.43	0.35	· · · · ·		
1998	1	1	1	0	0.28	0.35			
1998	1	1	1	10	0.44	0.35		21	
1998	1	1	1	20	0.27	0.35	n ye î porte de la composition		
1998	1	1	1	30	0.45	0.35			
1998	1	1	1	40	0.26	0.35			
1998	1	1	1	50	0.45	0.35	- <u> </u>		
1998	1	1	2	-0	0.26	0.35			
1998	1	1	2	10	0.45	0.35			
1998	1	1	2	20	0.26	0.35			
1998	1	1	2	30	0.45	0.35			
1998	1	1	2	40	0.27	0.35		· · · · · · · · · · · · · · · · · · ·	
1998	1	1	2	50	0.44	0.35			
1998	1	1	3	Ő	0.28	0.35			
1998	1	1	3	10	0.43	0.35			
1998	1	1	3	20	0.29	0.35		<u> </u>	
1998 -	1	1	3	30	0.42	0.35			
1998	1	1	3	40	0.3	0.35			
1998	- I -	1	3	50	0.41	0.35			
1998	1	1	4	0	0.31	0.35			
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