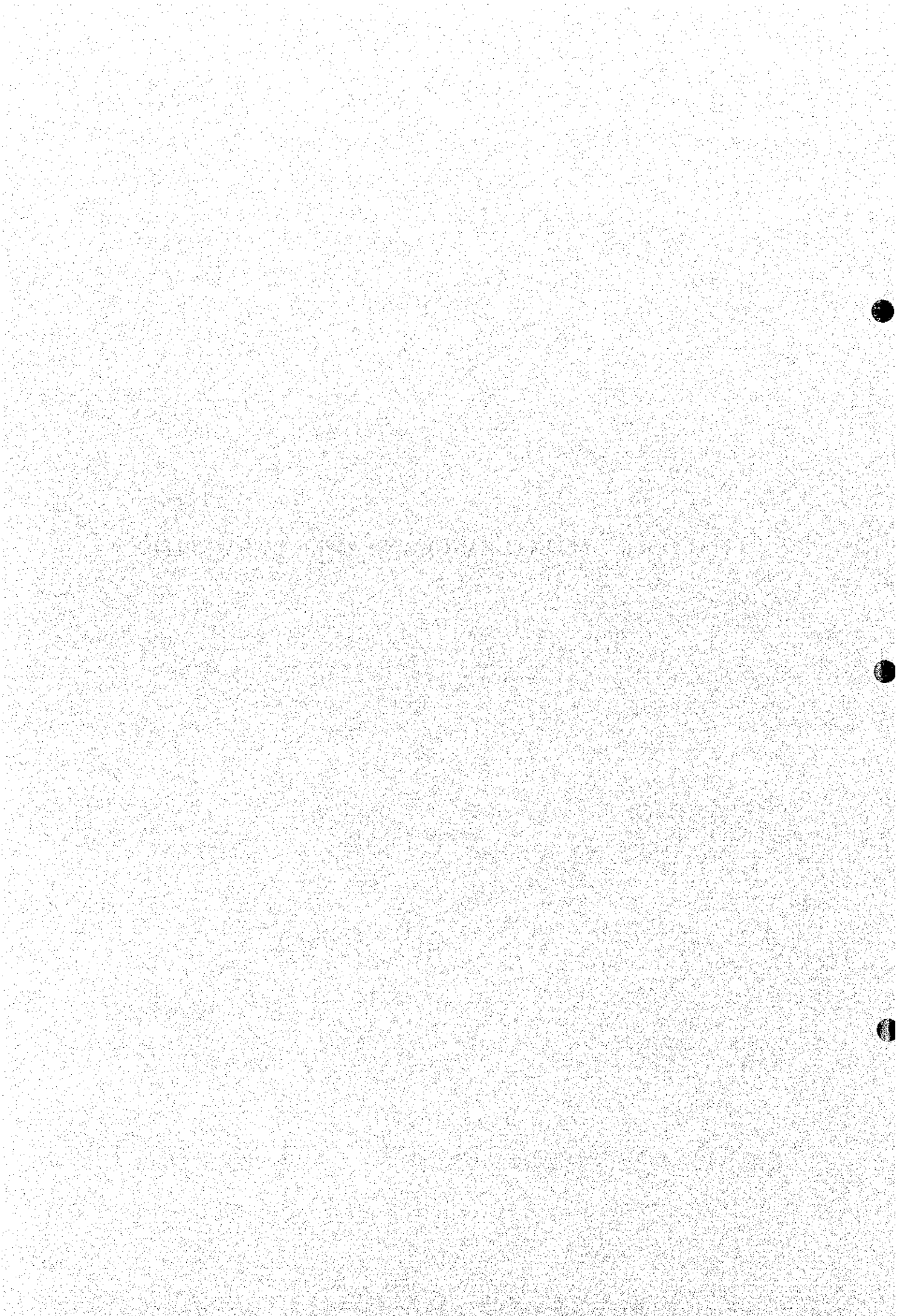


CHAPTER 6 MAINTENANCE AND AMENITY FACILITIES



6.1 Mooring Facility

TYPE OF WORK : MOORING FACILITIES

LOCATION :

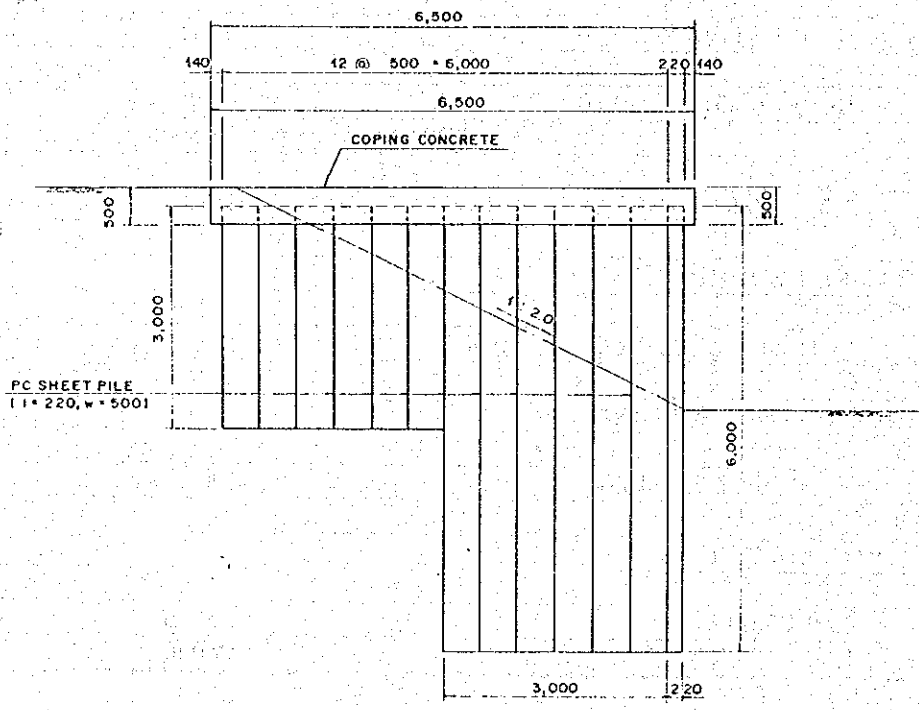
PER 1 PLACE

CALCULATION	RESULT
STRUCTURAL EXCAVATION	
$A = (6.28 + 7.78) \times \frac{1}{2} \times 3.00$	= 21.090 m ²
$V_1 = 21.09 \times 10.00$	= 210.900
$V_2 = \frac{1}{2} \times 6.00 \times 3.00 \times 6.00$	= 54.000
$V_3 = (1.50 + 0.90) \times \frac{1}{2} \times 0.60 \times (5.00 + 1.414 \times 6.00) \times 2$	= 19.416
$V_4 = 1.118 \times 6.00 \times 1.00 \times (5.00 + 1.414 \times 6.00) \times 2$	= 180.901
$V_5 = 0.60 \times 1.00 \times 5.00 \times 2$	= 6.000
$V_6 = (1.20 + 2.80) \times \frac{1}{2} \times 0.60 \times 10.00$	= 12.000
$V_7 = (4.80 + 6.10) \times \frac{1}{2} \times 0.50 \times 10.00$	= 27.250
$V_8 = 1.202 \times 4.50 \times 0.50 \times 10.00$	= 27.045
TOTAL V	= 537.510
	537.510 m ³
BACKFILL WITH SELECTED SOIL	
$A_1 = (0.50 + 1.10) \times \frac{1}{2} \times 0.60$	= 0.480
$A_2 = (0.50 + 1.00) \times \frac{1}{2} \times 0.50$	= 0.375
$A_3 = (0.50 + 0.80) \times \frac{1}{2} \times 0.30$	= 0.195
TOTAL A	= 1.050 m ²
$V = 1.05 \times 10.00$	= 10.500
	10.500 m ³
GRAVEL BEDDING	
$V = (6.31 \times 0.25 + 0.50 \times 0.25) \times 10.00$	= 17.025
	17.025 m ³
RUBBLE STONE FILLING	
$V = \frac{1}{2} \times 0.50 \times 0.75 \times 10.00$	= 1.875
	1.875 m ³
GABION MATTRESS	
$A = 0.50 \times 3.00$	= 1.50 m ²
$V = 1.50 \times 10.00$	= 15.000
	15.000 m ³

MOORING FACILITIES

PER 1 PLACE

TYPE OF WORK: LOCATION:	PC SHEET PILE	CALCULATION	RESULT
		- PC SHEET PILE	
		$L_1 = 6.00 \text{ m/pile}$ $L_2 = 4.00 \text{ m/pile}$	
		$L = (6.00 \text{ m/pile} \times 18 \text{ piles} + 4.00 \text{ m/pile} \times 6 \text{ piles}) \times 2$	
		$= 264.000$	264.000m
		• DRIVING	
		$L_1 = 4.50 \text{ m/pile} \times 12 \text{ piles} \times 2 = 108.000$	
		$L_2 = 3.00 \text{ m/pile} \times 3 \text{ piles} \times 2 = 18.000$	
		$L_3 = 3.50 \text{ m/pile} \times 3 \text{ piles} \times 2 = 21.000$	
		$L_4 = 3.00 \text{ m/pile} \times 6 \text{ piles} \times 2 = 36.000$	
		TOTAL = 183.000	183.000m



TYPE OF WORK : MOORING FACILITIES

LOCATION :

PER 1 PLACE

CALCULATION		RESULT
PC SHEET PILE		
PC SHEET PILE		
$L_1 = 6.00 \text{ m / pile} \quad L_2 = 4.00 \text{ m / pile}$		
$L = (6.00 \text{ m / pile} \times 18 \text{ piles} + 4.00 \text{ m / pile} \times 6 \text{ piles}) \times 2$		$= 264.000$
		264.000 m
DRIVING		
$L_1 = 4.50 \text{ m / pile} \times 12 \text{ piles} \times 2$		$= 108.000$
$L_2 = 3.00 \text{ m / pile} \times 3 \text{ piles} \times 2$		$= 18.000$
$L_3 = 3.50 \text{ m / pile} \times 3 \text{ piles} \times 2$		$= 21.000$
$L_4 = 3.00 \text{ m / pile} \times 6 \text{ piles} \times 2$		$= 36.000$
TOTAL L		$= 183.000$
		183.000 m
COPING CONCRETE		
CONCRETE TYPE C1		
$V = (0.50 + 0.50 - 0.22 \times 0.25) \times (6.50 + 6.00) \times 2$		$= 4.875$
		4.875 m ³
GRAVEL BEDDING		
$V = (6.50 + 6.00) \times 2 \times 0.10 \times 0.24$		$= 0.600$
		0.600 m ³
FORM (H < 4.0 m)		
$A_1 = (0.50 \times 2 + 0.14) \times (6.50 + 6.00) \times 2$		$= 28.500$
$A_2 = 0.50 \times 0.50 \times 2 \times 2$		$= 1.000$
TOTAL A		$= 29.500$
		29.500 m ²
REINFORCING BAR		
D13 (W = 1.04 kg.f / m)		
$n_1 = 7 \text{ bars}$		
$W_1 = (6.50 + 6.00 - 0.05 \times 2) \times 7 \text{ bars} \times 1.04$		$= 90.272$

TYPE OF WORK : MOORING FACILITIES
 LOCATION :

PER 1 PLACE

CALCULATION		RESULT
D10 (W = 0.617 kg.f / m)		
$n_2 = (6.50 + 6.00 - 0.05 \times 2) : 0.30 + 1$	$\div 42$ bars	
$L = 0.40 \times 3$	$= 1.200$ m / bar	
$W_2 = 42 \times 1.20 \times 0.617 \times 2$	$= 62.194$	
TOTAL W		$= 152.466$ kg.f
		0.152 tf
BASE CONCRETE		
CONCRETE TYPE C1		
$V = 3.15 \text{ m}^3 / 10.00 \text{ m} \times 10.00 \text{ m}$	$= 3.150$	3.150 m^3
GRAVEL BEDDING		
$V = 0.80 \text{ m}^3 / 10.00 \text{ m} \times 10.00 \text{ m}$	$= 0.800$	0.800 m^3
FORM (H < 4.0 m)		
$A = 13.45 \text{ m}^2 / 10.00 \text{ m} \times 10.00 \text{ m}$	$= 13.450$	13.450 m^2
REINFORCING BAR		
$W = 0.039 \text{ tf} / 10.00 \text{ m} \times 10.00 \text{ m}$	$= 0.039$	0.039 tf
LOG PILE (Dia 150, L = 2.0 m / pile)		
$L = 10.00 \text{ m} / 10.00 \text{ m} \times 10.00 \text{ m}$	$= 10.000$	10.000 m
CONCRETE STEPS		
CONCRETE TYPE D		
$V = \{(6.31 + 1.00) \times 0.50 - \frac{1}{2} \times 0.30 \times 0.45$ $\times 10\} \times 10.00$	$= 29.800$	29.800 m^3
FORM (H < 4.0 m)		
$A_1 = 0.30 \times 10.00 \times 10$	$= 30.000$	
$A_2 = 0.25 \times 10.00$	$= 2.500$	
TOTAL A		$= 32.500$ m^2
REINFORCING BAR		
D13 (W = 1.04 kg.f / m)		
$n_1 = (6.31 + 0.45 - 0.05 \times 2) : 0.30 + 1$	$= 24$ bars	
$L = (10.00 - 0.05 \times 2)$	$= 9.90$ m / bar	
$W_1 = 24 \times 9.90 \times 1.04$	$= 247.104$	

TYPE OF WORK : MOORING FACILITIES

LOCATION :

PER 1 PLACE

CALCULATION		RESULT
$n_2 = (10.00 - 0.05 \times 2) : 0.30 + 1$	= 34 bars	
$L = (6.31 + 0.45 - 0.05 \times 2)$	= 6.660 m / bar	
$W_2 = 6.66 \times 34 \times 1.04$	= 235.498	
TOTAL W	= 482.602 kg.f	0.483 tf
RUBBLE STONE BEDDING		
$A_1 = 1.118 \times 6.00 \times 0.40 + \frac{1}{2} \times 0.40 \times 0.80$	= 4.283 m ²	
$V_1 = 4.283 \times 5.00 \times 2$	= 42.830	
$A_2 = \frac{1}{2} \times (1.118 \times 6.00)^2$	= 22.499 m ²	
$V_2 = 22.499 \times 0.40 \times 2$	= 17.999	
TOTAL V	= 60.829	60.829 m ³
STONE FACING		
$A_1 = (1.50 + 0.90) \times \frac{1}{2} \times 0.60$	= 0.720 m ²	
$A_2 = 1.118 \times 6.00 \times 0.60$	= 4.025 m ²	
$A_3 = 1.00 \times 0.60$	= 0.600 m ²	
TOTAL A	= 5.345 m ²	
$V_1 = 5.345 \times 5.00 \times 2$	= 53.450	
$V_2 = \left\{ \frac{1}{2} \times (1.118 \times 6.00)^2 \times 0.60 + 0.720 \times 1.118 \times 6.00 \right\} \times 2$	= 36.658	
TOTAL V	= 90.108 m ³	90.108 m ³

6.2 Riverside Approach Steps

TYPE OF WORK :
LOCATION : APPROACH STEPS TYPE - WA (RIVER SIDE)

CALCULATION	RESULT
☐ STRUCTURAL EXCAVATION	
$A_1 = (1.4 + 2.0) \times 0.6 : 2$	$= 1.02$
$V_1 = 1.02 \times 3.40$	$= 3.468$
$A_2 = (1.4 + 2.0) \times 0.6 : 2$	$= 1.02$
$V_2 = 1.02 \times 0.8$	$= 0.816$
TOTAL	$= 4.284$
	4.284 m³
☐ BACKFILL WITH SELECTED SOIL	
$A_1 = (0.6 + 1.2) \times 0.6 : 2$	$= 0.54$
$V_1 = 0.54 \times 3.4$	$= 1.836$
$A_2 = (0.6 + 1.2) \times 0.6 : 2$	$= 0.54$
$V_2 = 0.54 \times 0.8 \times 2$	$= 0.864$
TOTAL	$= 2.700$
	2.700 m³

TYPE OF WORK :
 LOCATION : APPROACH STEPS TYPE - WA (RIVER SIDE)

CALCULATION		RESULT
☐ WET STONE MASONRY		
1. 0.8 x 0.2 x 1.0	=	0.16
2. 0.8 x 0.2 x 1.6	=	0.256
3. 0.8 x 0.2 x 2.2	=	0.352
4. 0.8 x 0.2 x 2.8	=	0.448
5. 0.8 x 0.7 x 3.4	=	0.544
	V =	1.76
		1.760 m ³
☐ GRAVEL BEDDING		
V = 0.1 x 0.9 x 3.6	=	0.324
		0.324 m ³
☐ CEMENT MORTAR POINTING		
• SIDE		
0.2 x 1.0	=	0.2
0.2 x 1.6	=	0.32
0.2 x 2.2	=	0.44
0.2 x 2.8	=	0.56
0.2 x 3.4	=	0.68
	TOTAL:	2.200
• FRONT		
0.8 x 1.0 x 2	=	1.600
• TOP		
3.4 x 0.8	=	2.720
	TOTAL	6.52
		6.520 m ²
☐ JOINT FILTER		
A = 0.2 x 1.0 + 0.2 x 1.6 + 0.2 x 2.2 + 0.2 x 2.8 + 0.7 x 3.4		
	=	2.2
		2.200 m ²

TYPE OF WORK :
 LOCATION : APPROACH STEPS TYPE - WA (LAND SIDE)

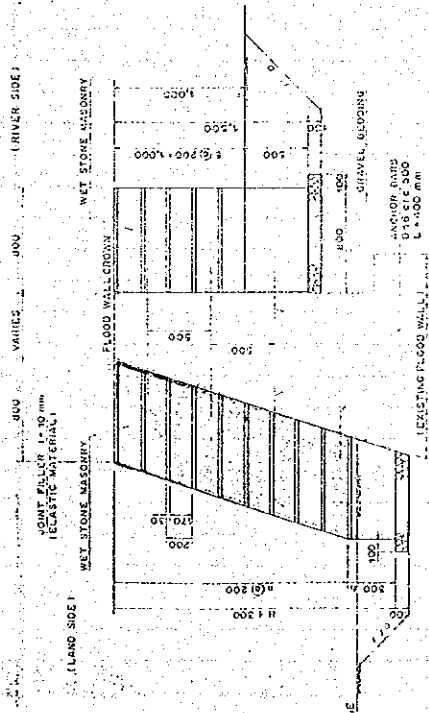
CALCULATION			RESULT
▣ STRUCTURAL EXCAVATION			
$A_1 = (1.750 + 1.250) \times 0.4 : 2$	=	0.6	
$V_1 = 0.6 \times 5.8$	=	3.48	
$A_2 = (0.6 + 1.0) \times 0.4 : 2$	=	0.32	
$V_2 = 0.32 \times 1.250 \times$	=	0.800	
TOTAL = $V_1 + V_2$			4.280 m³
▣ BACKFILL WITH SELECTED SOIL			
$A_1 = (1.0 + 0.6) \times 0.4 : 2$	=	0.32	
$V_1 = 0.32 \times 6.00$	=	1.92	
$A_2 = (0.6 + 1.0) \times 0.4 : 2$	=	0.32	
$V_2 = 0.32 \times 0.6 \times 2$	=	0.384	
TOTAL = $V_1 + V_2$			2.304 m³

TYPE OF WORK :
 LOCATION : APPROACH STEPS TYPE - WA (LAND SIDE)

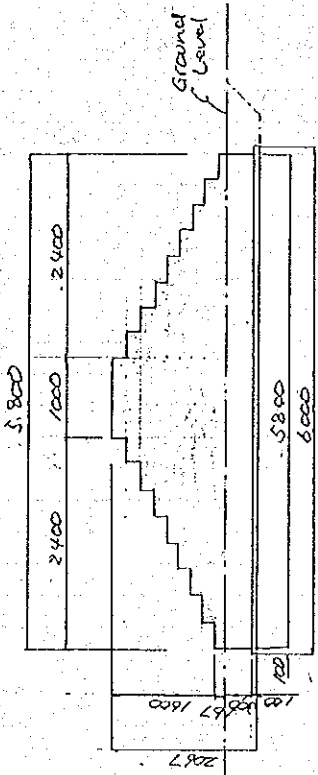
CALCULATION		RESULT
WET STONE MASONRY		
BLOCK		
1. $0.8 \times 0.2 \times 1.0$	=	0.16
2. $0.8 \times 0.2 \times 1.6$	=	0.256
3. $0.8 \times 0.2 \times 2.2$	=	0.352
4. $0.8 \times 0.2 \times 2.8$	=	0.448
5. $0.8 \times 0.2 \times 3.4$	=	0.544
6. $0.8 \times 0.2 \times 4.0$	=	0.640
7. $0.8 \times 0.2 \times 4.6$	=	0.736
8. $0.8 \times 0.2 \times 5.2$	=	0.832
9. $(0.8 \times 0.67) \times 0.367 : 2 \times 5.8$	=	1.565
TOTAL:		5.533
		5.533 m ³
GRAVEL BEDDING		
$V = (0.76 + 0.73) \times 0.1 : 2 \times 6.0$	=	0.447
		0.447 m ³

APPROACH STEPS TYPE - W.A. (LAND SIDE)

TYPE OF WORK:	CEMENT MORTAR PLASTERING	CALCULATION	RESULT
LOCATION:	(LAND SIDE)	SIDES	
		$0.2 \times 1.0 = 0.2$	
		$0.2 \times 1.6 = 0.32$	
		$0.2 \times 2.2 = 0.44$	
		$0.2 \times 2.8 = 0.56$	
		$0.2 \times 3.4 = 0.68$	
		$0.2 \times 4.0 = 0.80$	
		$0.2 \times 4.6 = 0.92$	
		$0.2 \times 5.2 = 1.04$	
		$0.067 \times 5.8 = 0.389$	
		TOTAL = 5.349	
		FRONT	
		$A = (1.6 + 0.067) \times 0.8 = 1.334$	
		TOP	
		$A = 5.8 \times 0.8 = 4.640$	
		TOTAL = 11.323	11.323 m ²



SECTION B-B
SCALE A



TYPE OF WORK :
 LOCATION : APPROACH STEPS TYPE - WA (LAND SIDE)

CALCULATION			RESULT
☞ JOINT FILTER			
0.2 x 1.0	=	0.2	
0.2 x 1.6	=	0.32	
0.2 x 2.2	=	0.44	
0.2 x 2.8	=	0.56	
0.2 x 3.4	=	0.68	
0.2 x 4.0	=	0.80	
0.2 x 4.6	=	0.92	
0.2 x 5.2	=	1.04	
0.367 x 5.8	=	2.129	
TOTAL:			7.089 m²
☞ ANCHOR BARS			
• D 16 (1.580 kgf/m)			
1. L ₁ = 0.4 x 2	=	0.8	
2. L ₂ = 0.4 x 5	=	2.0	
3. L ₃ = 0.4 x 9	=	3.6	
L = L ₁ + L ₂ + L ₃	=	6.4	
N = 6.4 x 1.580	=	10.112	10.112 kgf

TYPE OF WORK : CONCRETE STEPS
 LOCATION : APPROACH STEPS (TYPE-WA-2)

PER 1 PLACE

CALCULATION		RESULT
STRUCTURAL EXCAVATION		
$A_1 = (1.20 + 4.30) \times \frac{1}{2} \times 1.20$	= 3.300	
$A_2 = (1.118 \times 6.30 + 0.70) \times 0.60$	= 4.646	
$A_3 = (0.80 + 1.80) \times \frac{1}{2} \times 0.80$	= 1.040	
TOTAL A		= 8.986 m ²
$V = 8.986 \times 1.80$	= 16.175	16.175 m ³
BACKFILL WITH SELECTED SOIL		
$A_1 = (0.50 + 1.20) \times \frac{1}{2} \times 0.70$	= 0.595	
$A_2 = (1.50 + 1.90) \times \frac{1}{2} \times 0.30$	= 0.510	
$A_3 = (0.50 + 1.10) \times \frac{1}{2} \times 0.60$	= 0.480	
TOTAL A		= 1.585 m ²
$V = 1.585 \times 1.80$	= 2.853	2.853 m ³
GRAVEL BEDDING		
Average Height : h = 2.650 m		
$A = (1.118 \times 6.30 + 0.70) \times 0.25$	= 1.936	
$V = 1.936 \times 1.20$	= 2.323	2.323 m ³
CONCRETE TYPE D		
Average Height : h = 2.650 m		
CONCRETE TYPE D		
$V = \{(1.118 \times 6.30 + 0.70) \times 0.35 - \frac{1}{2} \times 0.40 \times 0.20 \times 14\}$	= 2.580	2.580 m ³
FORM (H < 4.0 m)		
$A = 0.20 \times 1.20 \times 14$	= 3.360	3.360 m ²

TYPE OF WORK : CONCRETE STEPS
 LOCATION : APPROACH STEPS (TYPE-WA-2)

PER 1 PLACE

CALCULATION		RESULT
REINFORCING BAR (D13, W = 1.04 kg.f / m)		
$n_1 = (1.118 \times 6.30 + 0.70 - 0.05 \times 2) : 0.30 + 1$	$\div 27$ bars	
$L_1 = (1.20 - 0.05 \times 2)$	$= 1.10$ m / bar	
$W_1 = 27 \times 1.10 \times 1.04$	$= 30.888$	
$n_2 = (1.20 - 0.05 \times 2) : 0.30 + 1$	$\div 6$ bars	
$L_2 = 1.118 \times 6.30 + 0.70 - 0.05 \times 2$	$= 7.643$ m / bar	
$W_2 = 7.643 \times 6 \times 1.04$	$= 47.692$	
TOTAL W = 78.580 kg.f		0.079 tf
SIDE WALL		
CONCRETE TYPE C1		
$V = 1.233 \text{ m}^3 / 2.936 \text{ m} \times 7.743$	$= 3.252$	3.252 m ³
GRAVEL BEDDING		
$V = 1.089 \text{ m}^3 / 2.936 \text{ m} \times 7.743$	$= 2.872$	2.872 m ³
FORM (H < 4.0 m)		
$A = 11.782 \text{ m}^2 / 2.936 \text{ m} \times 7.743$	$= 31.072$	31.072 m ²
REINFORCING BAR		
$W = 0.059 \text{ tf} / 2.936 \text{ m} \times 7.743$	$= 0.156$	0.156 tf
JOINT FILLER		
$A = 2.055 \text{ m}^2 / 2.936 \text{ m} \times 7.743$	$= 5.420$	5.420 m ²
BASE CONCRETE		
CONCRETE TYPE C1		
$V = 3.150 \text{ m}^3 / 10.00 \text{ m} \times 1.80$	$= 0.567$	0.567 m ³
GRAVEL BEDDING		
$V = 0.80 \text{ m}^3 / 10.00 \text{ m} \times 1.80$	$= 0.144$	0.144 m ³
FORM (H < 4.0 m)		
$A = 13.240 \text{ m}^2 / 10.00 \text{ m} \times 1.80$	$= 2.383$	2.383 m ²

TYPE OF WORK : CONCRETE STEPS
 LOCATION : APPROACH STEPS (TYPE-WA-2)

:
:
:

PER 1 PLACE

CALCULATION	RESULT
REINFORCING BAR	
$W = 0.101 \text{ tf} / 10.00 \text{ m} \times 1.80$	0.018 tf
TOP CONCRETE	
CONCRETE TYPE C1	
$V = 2.10 \text{ m}^3 / 10.00 \text{ m} \times 1.80$	0.378 m ³
GRAVEL BEDDING	
$V = 0.80 \text{ m}^3 / 10.00 \text{ m} \times 1.80$	0.144 m ³
FORM (H < 4.0 m)	
$A = 14.210 \text{ m}^2 / 10.00 \text{ m} \times 1.80$	2.558 m ²
REINFORCING BAR	
$W = 0.098 \text{ tf} / 10.00 \text{ m} \times 1.80$	0.018 tf
JOINT FILLER	
$A = 3.120 \text{ m}^2 / 10.00 \text{ m} \times 1.80$	0.562 m ²

TYPE OF WORK : CONCRETE STEPS
 LOCATION : APPROACH STEPS (TYPE-WB)

PER 1 PLACE

CALCULATION		RESULT
STRUCTURAL EXCAVATION		
$A_1 = \frac{1}{2} \times 1.80 \times 0.90$	= 0.810	
$A_2 = (1.118 \times 2.00 + 0.70) \times 0.60$	= 1.762	
$A_3 = (0.80 + 1.80) \times \frac{1}{2} \times 0.80$	= 1.040	
TOTAL A	= 3.612 m ²	
$V_1 = 3.612 \times 3.60$	= 13.003	
$V_2 = \left\{ \frac{1}{2} \times 0.60 \times 1.20 + (2.795 + 1.00) \times 0.50 \right\}$ $\times 2.00 \times 2$	= 9.030	
TOTAL V	= 22.033	22.033 m ³
BACKFILL WITH SELECTED SOIL		
$A_1 = (0.50 + 1.10) \times \frac{1}{2} \times 0.60$	= 0.480	
$A_2 = (0.50 + 0.80) \times \frac{1}{2} \times 0.30$	= 0.195	
$V_1 = 0.480 \times 3.60$	= 1.728	
$V_2 = 0.195 \times 2.00 \times 2$	= 0.780	
TOTAL V	= 2.508	2.508 m ³
GRAVEL BEDDING		
$A = (1.118 \times 2.00 + 0.70) \times 0.25$	= 0.734	
$V = 0.734 \times 3.00$	= 2.202	2.202 m ³
RUBBLE STONE FILLING		
$V = \frac{1}{2} \times 0.60 \times 1.20 \times 7.60$	= 2.736	2.736 m ³
GABION CYLINDER ϕ 500		
$V = \frac{\pi}{4} \times 0.50^2 \times (2.795 + 1.00) \times 4.00 \times 2$	= 5.961	5.961 m ³
SOIL FILLING		
$V = (2.795 + 1.00) \times 2.00 \times 2 - 5.961$	= 1.629	1.629 m ³

TYPE OF WORK : CONCRETE STEPS
 LOCATION : APPROACH STEPS (TYPE-WB)

PER 1 PLACE

CALCULATION		RESULT
CONCRETE TYPE D		
CONCRETE TYPE D		
$V = \{(1.118 \times 2.00 + 0.70) \times 0.35 - \frac{1}{2} \times 0.40 \times 0.20 \times 5\} \times 3.00$	= 2.483	2.483 m ³
FORM (H < 4.0 m)		
$A = 0.20 \times 3.00 \times 5$	= 3.000	3.000 m ²
REINFORCING BAR (D13, W = 1.04 kg.f / m)		
$n_1 = (1.118 \times 2.00 + 0.70 - 0.05 \times 2) : 0.30 + 1$	≅ 11 bars	
$L_1 = (3.00 - 0.05 \times 2)$	= 2.90 m / bar	
$W_1 = 11 \times 2.90 \times 1.04$	= 33.176	
$n_2 = (3.00 - 0.05 \times 2) : 0.30 + 1$	≅ 11 bars	
$L_2 = 1.118 \times 2.00 + 0.70 - 0.05 \times 2$	= 2.836 m / bar	
$W_2 = 2.836 \times 11 \times 1.04$	= 32.444	
TOTAL W = 65.620 kg.f		0.066 tf
SIDE WALL		
CONCRETE TYPE C1		
$V = (2.236 + 0.70) \times 0.70 \times 0.30 \times 2$	= 1.233	1.233 m ³
GRAVEL BEDDING		
$V = \{(0.10 \times 0.30) + (0.10 + 0.211) \times \frac{1}{2}\} \times (2.236 + 0.70) \times 2$	= 1.089	1.089 m ³
FORM (H < 4.0 m)		
$A = \{(2.236 + 2.420) \times \frac{1}{2} + (0.70 + 0.535) \times \frac{1}{2}\} \times 2 \times 2$	= 11.782	11.782 m ²
REINFORCING BAR		
D13 (W = 1.04 kg.f / m)		
$n_1 = 6$ bars		
$L_1 = (2.236 + 0.70 - 0.05 \times 2)$	= 2.836 m / bar	
$W_1 = 6 \times 2.836 \times 1.04 \times 2$	= 35.393	

TYPE OF WORK : CONCRETE STEPS
 LOCATION : APPROACH STEPS (TYPE-WB)

PER 1 PLACE

CALCULATION	RESULT
D10 (W = 0.617 kg.f / m)	
$n_2 = (2.236 + 0.70 \times 2) : 0.30 + 1$	$\cong 11$ bars
$L_2 = (0.20 \times 2 + 0.60 \times 2 + 15 \times 0.01)$	$= 1.750$ m / bar
$W_2 = 11 \times 1.75 \times 0.617 \times 2$	$= 23.755$
TOTAL W	$= 59.148$ kg.f
	0.059 tf
JOINT FILLER	
$A = (1.118 \times 2.00 + 0.70) \times 0.35 \times 2$	$= 2.055$
	2.055 m ²
BASE CONCRETE	
CONCRETE TYPE C1	
$V = (0.50 + 0.75) \times \frac{1}{2} \times 0.50 \times 3.00$	$= 0.938$
	0.938 m ³
GRAVEL BEDDING	
$V = (3.00 + 0.10 \times 2) \times 0.10 \times 0.70$	$= 0.224$
	0.224 m ³
FORM (H < 4.0 m)	
$A = (0.50 + 0.75) \times 3.00 + (0.50 + 0.75) \times \frac{1}{2} \times 0.50 \times 2$	$= 4.375$
	4.375 m ²
REINFORCING BAR	
D13 (W = 1.04 kg.f / m)	
$n_1 = 6$ bars	
$L_1 = (3.00 - 0.05 \times 2)$	$= 2.900$ m / bar
$W_1 = 6 \times 2.900 \times 1.04$	$= 18.096$
D10 (W = 0.617 kg.f / m)	
$n_2 = (3.00 - 0.05 \times 2) : 0.30 + 1$	$\cong 11$ bars
$L_2 = (0.40 + 0.43 + 0.63 + 0.447 + 15 \times 0.01)$	$= 2.057$ m / bar
$W_2 = 11 \times 2.057 \times 0.617$	$= 13.961$
TOTAL W	$= 32.057$ kg.f
	0.032 tf

TYPE OF WORK : CONCRETE STEPS
LOCATION : APPROACH STEPS (TYPE-WB)

PER 1 PLACE

CALCULATION		RESULT
LOG PILE		
$L = 2.00 \text{ m / pile} \times 3 \text{ piles}$	$= 6.000$	6.000 m
TOP CONCRETE		
CONCRETE TYPE C1		
$V = 2.10 \text{ m}^3 / 10.00 \text{ m} \times 3.60$	$= 0.756$	0.756 m^3
GRAVEL BEDDING		
$V = 0.80 \text{ m}^3 / 10.00 \text{ m} \times 3.60$	$= 0.288$	0.288 m^3
FORM (H < 4.0 m)		
$A = 14.210 \text{ m}^2 / 10.00 \text{ m} \times 3.60$	$= 5.116$	5.116 m^2
REINFORCING BAR		
$W = 0.098 \text{ tf} / 10.00 \text{ m} \times 3.60$	$= 0.035$	0.035 tf
JOINT FILLER		
$A = 3.120 \text{ m}^2 / 10.00 \text{ m} \times 3.60$	$= 1.123$	1.123 m^2

TYPE OF WORK : CONCRETE STEPS
 LOCATION : APPROACH STEPS (TYPE-WB)

PER 1 PLACE

CALCULATION		RESULT
STRUCTURAL EXCAVATION		
$A_1 = \frac{1}{2} \times 1.80 \times 0.90$	= 0.810	
$A_2 = (1.118 \times 2.00 + 0.70) \times 0.60$	= 1.762	
$A_3 = (0.80 + 1.80) \times \frac{1}{2} \times 0.80$	= 1.040	
TOTAL A	= 3.612 m ²	
$V_1 = 3.612 \times 3.60$	= 13.003	
$V_2 = \left\{ \frac{1}{2} \times 0.60 \times 1.20 + (2.795 + 1.00) \times 0.50 \right\}$ $\times 2.00 \times 2$	= 9.030	
TOTAL V	= 22.033	22.033 m ³
BACKFILL WITH SELECTED SOIL		
$A_1 = (0.50 + 1.10) \times \frac{1}{2} \times 0.60$	= 0.480	
$A_2 = (0.50 + 0.80) \times \frac{1}{2} \times 0.30$	= 0.195	
$V_1 = 0.480 \times 3.60$	= 1.728	
$V_2 = 0.195 \times 2.00 \times 2$	= 0.780	
TOTAL V	= 2.508	2.508 m ³
GRAVEL BEDDING		
$A = (1.118 \times 2.00 + 0.70) \times 0.25$	= 0.734	
$V = 0.734 \times 3.00$	= 2.202	2.202 m ³
RUBBLE STONE FILLING		
$V = \frac{1}{2} \times 0.60 \times 1.20 \times 7.60$	= 2.736	2.736 m ³
GABION CYLINDER Ø 500		
$V = \frac{\pi}{4} \times 0.50^2 \times (2.795 + 1.00) \times 4.00 \times 2$	= 5.961	5.961 m ³
SOIL FILLING		
$V = (2.795 + 1.00) \times 2.00 \times 2 - 5.961$	= 1.629	1.629 m ³

TYPE OF WORK : CONCRETE STEPS
 LOCATION : APPROACH STEPS (TYPE-GB-1)

PER 1 PLACE

CALCULATION		RESULT
STRUCTURAL EXCAVATION		
$A_1 = \frac{1}{2} \times 1.80 \times 0.90$	= 0.810	
$A_2 = (1.118 \times 4.800 + 0.70) \times 0.60$	= 3.640	
$A_3 = (0.80 + 1.80) \times \frac{1}{2} \times 0.80$	= 1.040	
TOTAL A	= 5.490 m ²	
$V_1 = 5.490 \times 3.60$	= 19.764	
$V_2 = \left\{ \frac{1}{2} \times 0.60 \times 1.20 + (5.925 + 1.00) \times 0.50 \right\}$ $\times 2.00 \times 2$	= 15.290	
TOTAL V	= 35.054	35.054 m ³
BACKFILL WITH SELECTED SOIL		
$A_1 = (0.50 + 1.10) \times \frac{1}{2} \times 0.60$	= 0.480	
$A_2 = (0.50 + 0.80) \times \frac{1}{2} \times 0.30$	= 0.195	
$V_1 = 0.480 \times 3.60$	= 1.728	
$V_2 = 0.195 \times 2.00 \times 2$	= 0.780	
TOTAL V	= 2.508	2.508 m ³
GRAVEL BEDDING		
$A = (1.118 \times 4.80 + 0.75) \times 0.25$	= 1.517	
$V = 1.517 \times 3.00$	= 4.551	4.551 m ³
BASE CONCRETE		
CONCRETE TYPE C1		
$V = 0.938$		0.938 m ³
GRAVEL BEDDING		
$V = 0.224$		0.224 m ³
FORM (H < 4.0 m)		
$A = 4.375$		4.375 m ²

TYPE OF WORK : CONCRETE STEPS
 LOCATION : APPROACH STEPS (TYPE-GB-1)

PER 1 PLACE

CALCULATION	RESULT
REINFORCING BAR	
W = 0.032	0.032 tf
LOG PILE	
L = 6.000	6.000 m
TOP CONCRETE	
CONCRETE TYPE C1	
V = 0.756	0.756 m ³
GRAVEL BEDDING	
V = 0.288	0.288 m ³
FORM (H < 4.0 m)	
A = 5.116	5.116 m ²
REINFORCING BAR	
W = 0.035	0.035 tf
JOINT FILLER	
A = 1.123	1.123 m ²
SIDE WALL	
CONCRETE TYPE C1	
V = 1.233 m ³ / 2.936 m x 6.066 = 2.547	2.547 m ³
GRAVEL BEDDING	
V = 1.089 m ³ / 2.936 m x 6.066 = 2.250	2.250 m ³
FORM (H < 4.0 m)	
A = 11.782 m ² / 2.936 m x 6.066 = 24.343	24.343 m ²
REINFORCING BAR	
W = 0.059 tf / 2.936 m x 6.066 = 0.122	0.122 tf
JOINT FILLER	
A = 2.055 m ² / 2.936 m x 6.066 = 4.246	4.246 m ²

TYPE OF WORK : CONCRETE STEPS
 LOCATION : APPROACH STEPS (TYPE-GB-1)

PER 1 PLACE

CALCULATION		RESULT
CONCRETE TYPE D		
$V = \{(1.118 \times 4.80 + 0.70) \times 0.35 - \frac{1}{2} \times 0.40\}$		
$\times 0.20 \times 12$	$= 4.930$	
FORM (H < 4.0 m)		
$A = 0.20 \times 3.00 \times 12$	$= 7.200$	7.200 m ²
REINFORCING BAR (D13, W = 1.04 kg.f / m)		
$n_1 = (1.118 \times 4.80 + 0.70 - 0.05 \times 2) / 0.30 + 1$	$= 21$ bars	
$L_1 = (3.00 - 0.05 \times 2)$	$= 2.90$ m / bar	
$W_1 = 21 \times 2.90 \times 1.04$	$= 63.336$	
$n_2 = (3.00 - 0.05 \times 2) / 0.30 + 1$	$= 11$ bars	
$L_2 = 1.118 \times 4.80 + 0.70 - 0.05 \times 2$	$= 5.966$ m / bar	
$W_2 = 11 \times 5.966 \times 1.04$	$= 68.251$	
TOTAL W	$= 131.587$ kg.f	0.132 tf
RUBBLE STONE FILLING		
$V = \frac{1}{2} \times 0.60 \times 1.20 \times 7.60$	$= 2.736$	2.736 m ³
GABION CYLINDER Ø 500		
$V = \frac{\pi}{4} \times 0.50^2 \times (5.925 + 1.00) \times 4.00 \times 2$	$= 10.878$	10.878 m ³
SOIL FILLING		
$V = (5.925 + 1.00) \times 0.50 \times 2 - 10.878$	$= 2.972$	2.972 m ³

TYPE OF WORK :

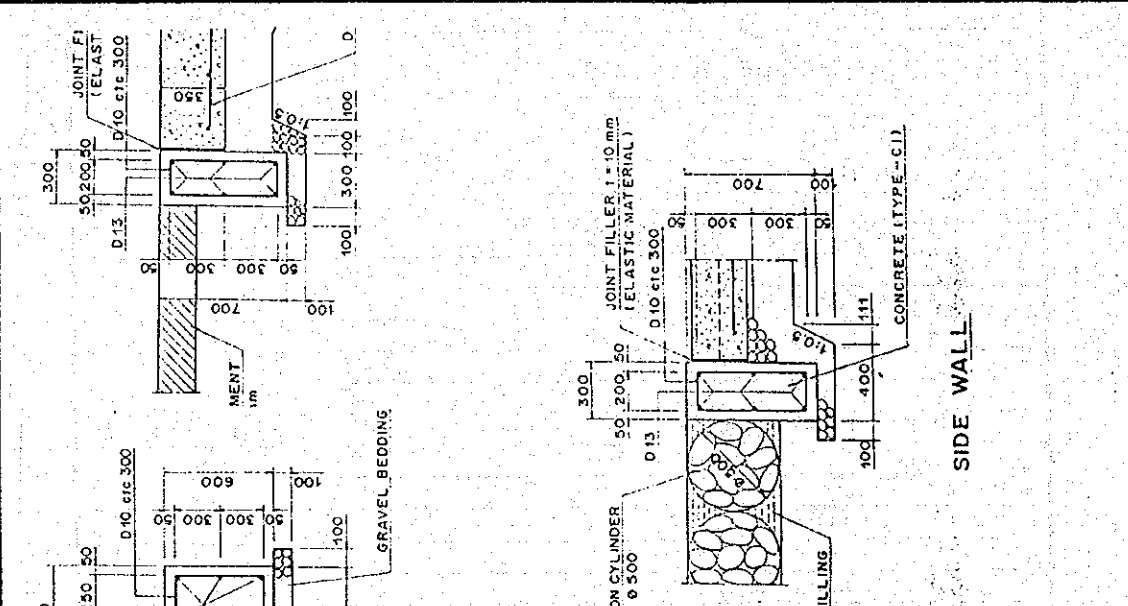
LOCATION : APPROACH STEP TYPE - G2

CALCULATION			RESULT
STRUCTURAL EXCAVATION			
$A = (2.3 + 2.7) \times 0.6 : 2$	=	1.500	
$A = 1.3 \times 2.9$	=	3.770	
$A = (6.3 + 3.25) \times 1.0 : 2$	=	4.775	
$A = (2.8 + 1.2) \times 0.7 : 2$	=	1.400	
TOTAL	=	11.445	
$V = 11.445 \times 3.6$	=	41.202	41.202 m³
BACKFILL WITH SELECTED SOIL			
$(0.5 + 1.3) \times 0.8 : 2$	=	0.720	
$(0.5 + 1.2) \times 0.7 : 2$	=	0.595	
$(0.4 + 1.4) \times 1.0 : 2 - 0.5 \times 1.0$	=	0.400	
TOTAL	=	1.715	
$V = 1.715 \times 3.6$	=	6.174	6.174 m³

TYPE OF WORK :
 LOCATION : APPROACH STEP TYPE - G2

CALCULATION		RESULT
☐ GRAVEL BEDDING		
1) REVETMENT		
$V = (0.7 + 9.890) \times 0.25 \times 3.0$	=	7.943
2) BASE CONCRETE		
$V = 0.800 \text{ m}^3 / 10.0 \text{ m} \times 3.6 \text{ m}$	=	0.288
3) TOP CONCRETE		
$V = 0.625 \text{ m}^3 / 10.0 \text{ m} \times 3.6 \text{ m}$	=	0.225
4) END WALL		
$V = 0.810 \text{ m}^3 / 10.0 \text{ m} \times (0.535 + 9.994) \times 2$	=	17.056
	V	= 25.512
		25.512 m³
☐ CONCRETE TYPE - D		
• CONCRETE		
$A_1 = (10.872 + 0.7) \times 0.329$	=	3.807
$A_2 = 0.4 \times 0.2 : 2 \times 19$	=	0.760
$A = A_1 - A_2$	=	3.047
$V = 3.047 \times 3.0 \text{ m}$	=	9.141
		9.141 m³
• FORM		
$A = 0.2 \times 3.0 \times 19$	=	11.4
		11.400 m²

APPROACH STEP TYPE G2

TYPE OF WORK:	CONCRETE TYPE C, FORM	CALCULATION	RESULT
LOCATION:		<p>① BASE CONCRETE</p> <ul style="list-style-type: none"> CONCRETE $V = 3.150 \text{ m}^3 / 10.0 \text{ m} \times 3.6 \text{ m} = 1.134$ FORM $V = 13.240 \text{ m}^3 / 10.0 \text{ m} \times 3.6 \text{ m} = 4.766$ <p>② TOP CONCRETE</p> <ul style="list-style-type: none"> CONCRETE $V = 2.100 \text{ m}^3 / 10.0 \text{ m} \times 3.6 \text{ m} = 0.756$ FORM $A = 14.400 \text{ m}^2 / 10.0 \text{ m} \times 3.6 \text{ m} = 5.184$ <p>③ END WALL</p> <ul style="list-style-type: none"> CONCRETE $A = (0.770.535) \times 0.7 + 2 + (10.062 + 9.994) \times 0.7 + 2 = 3.942$ $V = 3.942 \times 0.3 \times 2 = 2.365$ FORM $3.942 \times 2 = 7.884$ 	<p>1.134 m³</p> <p>4.766 m³</p> <p>0.756 m³</p> <p>5.184 m²</p> <p>2.365 m³</p> <p>7.884 m²</p>

APPROACH STEP TYPE G2

TYPE OF WORK: LOCATION:	DEFORMED REINFORCING BAR	RESULT
		<p>① BASE CONCRETE</p> $0.101 \text{ tf}/10.0\text{m} \times 3.60\text{m} = 0.036$ <p>② TOP CONCRETE</p> $0.095 \text{ tf}/10.0\text{m} \times 3.60\text{m} = 0.034$ <p>③ END WALL</p> $0.101 \text{ tf}/\text{place} \times 2 = 0.202 \text{ tf}$ <p>④ STEP</p> <p>D13 (1.04 kgf/m)</p> <p>HORIZONTAL</p> $l = 3.0 - 0.05 \times 2 = 2.900$ $n = (10.872 + 0.7 - 0.05 \times 2) \div 0.3 + 1 = 39$ $W = 2.9 \times 39 \times 1.04 = 117.624 \text{ kgf}$ <p>VERTICAL</p> $l = 10.872 + 0.7 - 0.05 \times 2 = 11.472$ $n = (3.0 - 0.05 \times 2) \div 0.3 + 1 = 11$ $W = 11.472 \times 11 \times 1.04 = 131.239$ <p>TOTAL</p> $= 248.863$

TYPE OF WORK :
 LOCATION : APPROACH STEP TYPE - G2

CALCULATION		RESULT
☒ JOINT FILTER		
1) TOP CONCRETE		
$A = 0.35 \times 3.0$	$= 1.05 \text{ m}^2$	1.050 m^2
2) SIDE WALL		
$L = 0.7 + 10.062$	$= 10.762$	
$A = 10.762 \times 0.35 \times 2$	$= 7.533$	7.533 m^2
☒ GABION CYLINDER		
$\varnothing = 500 \text{ mm}$		
$a = \pi / 4 \times 0.5^2$	$= 0.196$	
$V = 0.196 \times 8 \times (1.0 + 7.826 + 3.0)$	$= 18.543$	
☒ SOIL FILLING		
$V_1 = 0.5 \times (1.0 + 7.826 + 3.0) \times 4.0$	$= 23.652$	
$V_2 = 18.543$		
$V = V_1 - V_2$	$= 5.109$	5.109 m^3

TYPE OF WORK :

LOCATION : APPROACH STEP TYPE - G2

CALCULATION		RESULT
GABION MATTRESS		
$A = 3.0 \times 0.5 + 1.5 \times 0.5$	= 2.25	
$V = 2.25 \times 3.0 \text{ m}$	= 6.75	6.750 m ³
RUBBLE STONE FILLING		
$A = 1.0 \times 0.5 : 2 \times 2$	= 0.5	
$V = 0.5 \times 3.0 \text{ m}$	= 1.5	1.500 m ³

TYPE OF WORK :
 LOCATION : APPROACH STEP TYPE GA-3

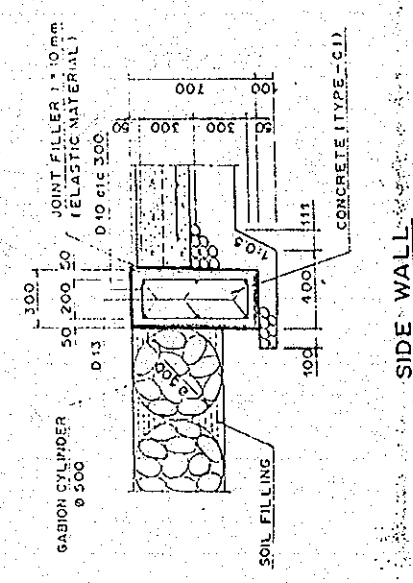
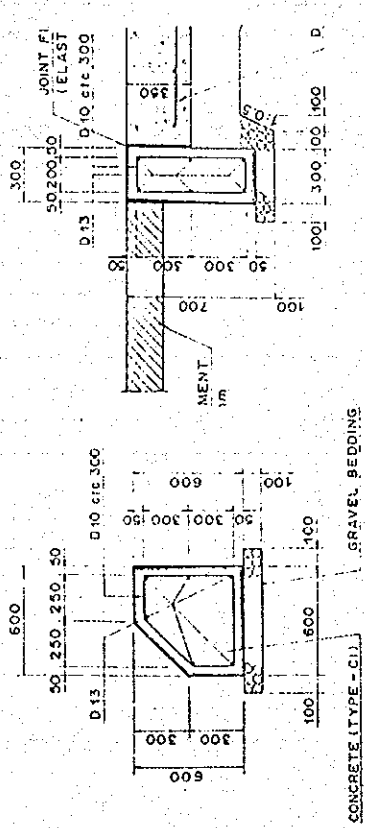
CALCULATION			RESULT
☐ STRUCTURAL EXCAVATION			
1)	$(2.9 + 2.2) \times 0.6 : 2$	=	1.53
2)	8.6×1.3	=	11.18
3)	$(2.7 + 4.3) \times 0.5 : 2$	=	1.75
4)	$(1.2 + 2.7) \times 0.7 : 2$	=	1.365
	A	=	15.825
	V = 15.825 x 1.800	=	28.485
			28.485 m ³
☐ BACKFILL WITH SELECTED SOIL			
1)	$(0.5 + 1.3) \times 0.8 : 2$	=	0.72
2)	$(0.5 + 1.2) \times 0.7 : 2$	=	0.595
3)	$(1.2 + 1.7) \times 0.5 : 2$	=	0.725
	A	=	2.040
	V = 2.040 x 1.800	=	3.672
			3.672 m ³

TYPE OF WORK :
 LOCATION : APPROACH STEP TYPE GA-3

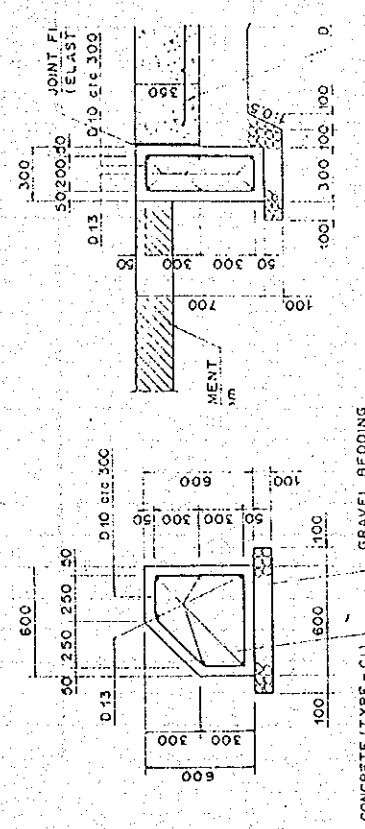
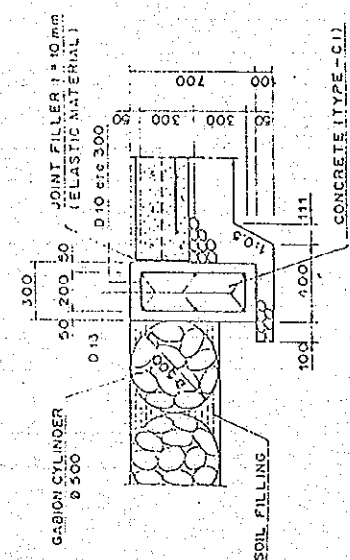
CALCULATION			RESULT
☐ GRAVEL BEDDING			
1) BASE CONCRETE			
$0.800 \text{ m}^2 / 10.0 \text{ m} \times 1.8 \text{ m}$	=	0.144	0.144 m ³
2) TOP CONCRETE			
$2.100 \text{ m}^2 / 10.0 \text{ m} \times 1.8 \text{ m}$	=	0.378	0.378 m ³
3) SIDE WALL			
$0.810 \text{ m}^3 / 10.0 \text{ m} \times (10.9 + 0.7) \times 2$	=	1.879	1.879 m ³
4) STEP			
$10.9 \times 0.25 \times 1.2$	=	3.27	3.27 m ³
☐ CONCRETE TYPE - D			
• CONCRETE			
$V_1 = (10.9 + 0.7) \times 0.329 \times 1.2$	=	4.580	
$V_2 = 0.4 \times 0.2 \times 23 \times 1.2$	=	2.208	
$V = V_1 - V_2$	=	2.372	2.372 m ³
• FORM			
$A = 0.2 \times 1.2 \times 23$	=	5.52	5.52 m ³

APPROACH STEPS TYPE GA-3
CONCRETE TYPE C1

TYPE OF WORK :	CALCULATION	RESULT
LOCATION :	① BASE CONCRETE	
	• CONCRETE	
	$V = 3.150 \text{ m}^3 / 10.0 \text{ m} \times 1.8 \text{ m} = 0.567$	0.567 m ³
	• FORM	
	$A = 13.240 \text{ m}^2 / 10.0 \text{ m} \times 1.8 \text{ m} = 2.083$	2.383 m ²
	② TOP CONCRETE	
	• CONCRETE	
	$V = 2.100 \text{ m}^3 / 10.0 \text{ m} \times 1.8 \text{ m} = 0.378$	0.378 m ³
	• FORM	
	$A = 14.000 \text{ m}^2 / 10.0 \text{ m} \times 1.8 \text{ m} = 2.520$	2.520 m ²
	③ SIDE WALL	
	• CONCRETE	
	$V = (10.9 + 0.7) \times 0.7 \times 0.3 = 2.436$	2.436 m ³
	• FORM	
	$A = (10.9 + 0.7) \times 0.7 \times 2 = 16.24$	16.240 m ²



APPROACH STEPS TYPE GA-3

TYPE OF WORK: LOCATION:	DEFORMED REINFORCING BAR	CALCULATION	RESULT	
	 <p>Technical drawing showing a cross-section of a concrete step. It includes dimensions for concrete width (600), height (300), and reinforcement details (D10 bars, 300 spacing). Labels include 'CONCRETE (TYPE-C1)', 'GRAVEL BEDDING', and 'JOINT FILLER (ELASTIC MATERIAL)'.</p>	① BASE CONCRETE		
		$0.101 \text{ tf} / 10.0 \text{ m} \times 1.8 \text{ m} = 0.018$	0.018 tf	
		② TOP CONCRETE		
		$0.095 \text{ tf} / 10.0 \text{ m} \times 1.8 \text{ m} = 0.017$	0.017 tf	
		③ SIDE WALL		
		$0.095 \text{ tf} / 10.0 \text{ m} \times (10.9 + 0.7) \times 2 = 0.110$	0.110 tf	
	 <p>Technical drawing showing a cross-section of a gabion cylinder. It includes dimensions for concrete width (300), height (300), and reinforcement details (D10 bars, 300 spacing). Labels include 'GABION CYLINDER', 'SOIL FILLING', 'CONCRETE (TYPE-C1)', and 'JOINT FILLER (ELASTIC MATERIAL)'.</p>	③ STEP		
		D13 (104 kgf/m)		
		HORIZONTAL		
		$P = 1.2 - 0.05 \times 2 = 1.100$		
		$W = 1.1 \times 3.9 \times 1.04 = 44.616$		
		VERTICAL		
		$P = 10.9 + 0.7 - 0.05 \times 2 = 11.5$		
		$W = (1.2 - 0.05 \times 2) \div 0.3 + 1 = 4$		
		$W = 11.5 \times 4 \times 1.04 = 47.84$		
		TOTAL		
		$= 92.456$	0.092 tf	

TYPE OF WORK :
 LOCATION : APPROACH STEP TYPE GA-3

CALCULATION		RESULT
☐ JOINT FILTER		
t = 10.0 mm ELASTIC MATERIAL		
1) TOP CONCRETE		
$0.710 \text{ m}^2 / 10.0 \text{ m} \times 1.200 \text{ m}$	=	0.445
		0.445 m ²
2) SIDE WALL		
L = 10.9 + 0.7	=	11.600
A = 11.60 x 0.35 x 2	=	8.120
		8.120 m ²
☐ GABION CYLINDER		
• Ø 500 mm		
A = $\pi / 4 \times 0.5^2$	=	0.196 m ²
V = 0.196 x 8 x (3.0 + 5.4)	=	13.171
		13.171 m ³
☐ SOIL FILLING		
V ₁ = 0.5 x (3.0 + 5.4) x 4.0	=	16.800 m ³
V ₂ = 13.171 m ³		
V = V ₁ - V ₂	=	3.629
		3.629 m ³

TYPE OF WORK :
 LOCATION : APPROACH STEP TYPE GA-4

CALCULATION			RESULT
☐ STRUCTURAL EXCAVATION			
1)	$(2.0 + 2.7) \times 0.7 : 2$	=	1.645
2)	$(1.2 + 0.9) \times 0.2 : 2$	=	0.210
3)	1.0×2.1	=	2.100
4)	$(3.9 + 1.9) \times 0.7 : 2$	=	2.030
5)	$(1.9 + 1.3) \times 0.4 : 2$	=	0.640
	TOTAL	=	6.625
V =	6.625×1.8	=	11.925
			11.925 m ³
☐ BACKFILL WITH SELECTED SOIL			
1)	$(0.5 + 1.0) \times 0.9 : 2$	=	0.675
2)	$(2.8 + 1.6) \times 0.5 : 2$	=	1.100
3)	$(1.3 + 0.6) \times 0.7 : 2$	=	0.665
	TOTAL A	=	2.440
V =	2.440×1.8	=	4.392
			4.392 m ³

TYPE OF WORK :
 LOCATION : APPROACH STEP TYPE GA-4

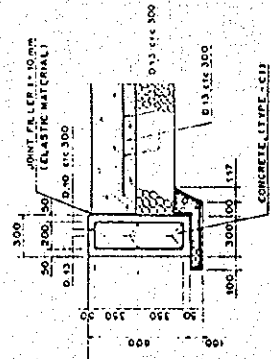
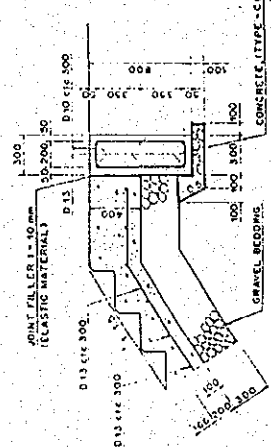
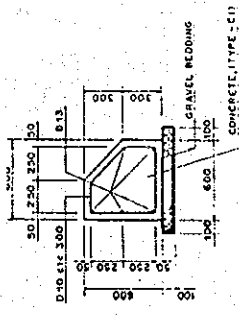
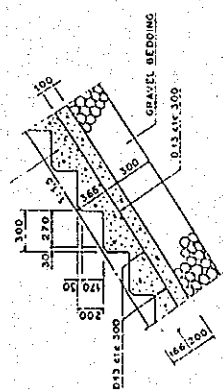
CALCULATION		RESULT
☐ GRAVEL BEDDING		
1) STEP		
$0.3 \times (5.65 + 0.7) \times 1.2 \text{ m}$	=	2.286
		2.286 m ³
2) BASE CONCRETE		
$0.800 \text{ m}^3/10.0 \text{ m} \times 1.8 \text{ m}$	=	0.144
		0.144 m ³
3) TOP CONCRETE		
$0.700 \text{ m}^3/10.0 \text{ m} \times 1.8 \text{ m}$	=	0.126
		0.126 m ³
4) SIDE WALL		
$0.700 \text{ m}^3/10.0 \text{ m} \times (5.65 + 0.7) \times 2$	=	0.889
		0.889 m ³
☐ CONCRETE TYPE - D		
• CONCRETE		
$V_1 = 0.366 \times (6.0 + 0.7) \times 1.2$	=	2.943
$V_2 = 0.2 \times 0.3 : 2 \times 1.2 \times 15$	=	0.54
$V = V_1 - V_2$	=	2.403
		2.403 m ³
• FORM		
$A = 0.2 \times 1.2 \times 15$	=	3.600
		3.600 m ²

APPROACH STEP TYPE GA-4

TYPE OF WORK:	CONCRETE TYPE C1	CALCULATION	RESULT	
LOCATION:				
<p>BASE CONCRETE SCALE 9</p> <p>SIDE WALL SCALE 9</p> <p>TOP CONCRETE SCALE 9</p>	① BASE CONCRETE			
	CONCRETE			
	$V = 3.150 \text{ m}^3 / 10.0 \text{ m} \times 1.80 \text{ m} = 0.567$		0.567 m ³	
	- FORM			
	$A = 13.240 \text{ m}^2 / 10.0 \text{ m} \times 1.80 \text{ m} = 2.383$		2.383 m ²	
	② TOP CONCRETE			
	CONCRETE			
	$V = 2.400 \text{ m}^3 / 10.0 \text{ m} \times 1.80 \text{ m} = 0.432$		0.432 m ³	
	- FORM			
$A = 16.000 \text{ m}^2 / 10.0 \text{ m} \times 1.80 \text{ m} = 2.88$		2.880 m ²		
③ SIDE WALL				
CONCRETE				
$V = (6.0 + 0.7) \times 0.3 \times 0.8 \times 2 = 3.216$		3.216 m ³		
- FORM				
$A = (6.0 + 0.7) \times 0.8 \times 4 = 21.44$		21.440 m ²		

APPROACH STEP TYPE GA-4

TYPE OF WORK :	CALCULATION		RESULT
LOCATION :			
	① BASE CONCRETE		0.018 tf
	$0.101 \text{ tf} / 10.0 \text{ m} \times 1.8 \text{ m} = 0.018$		
	② TOP CONCRETE		0.018 tf
	$0.100 \text{ tf} / 10.0 \text{ m} \times 1.8 \text{ m} = 0.018$		
	③ SIDE WALL		0.067 tf
	$0.100 \text{ tf} / 10.0 \text{ m} \times (6.0 + 0.7) \times 2 = 0.067$		
	④ STEP		
	D13 (1.04 kgf/m)		
	• HORIZONTAL		
	$l = 1.2 - 0.05 \times 2 = 1.10 \text{ m}$		
	$n = (6.0 + 0.7 - 0.05 \times 2) \div 0.371 = 23$		
	$w = 1.1 \times 23 \times 1.04 = 26.312 \text{ kgf}$		
	• VERTICAL		
	$l = 6.0 + 0.7 - 0.05 \times 2 = 6.60$		
	$n = (1.2 - 0.05 \times 2) \div 0.371 = 4$		
	$w = 6.6 \times 4 \times 1.04 = 29.040 \text{ kgf}$		
	TOTAL		0.055 tf



APPROACH STEP TYPE GA-4

TYPE OF WORK:	JOINT FILLER		RESULT
LOCATION:	CALCULATION		
10mm Elastic Material			
① TOP CONCRETE			
	$A = 4.240 \text{ m}^2 / 10.0\text{m} \times 1.2 \text{ m} = 0.509$		0.509 m ²
② SIDE WALL			
	$A = (6.0 + 0.7) \times 0.4 \times 2 = 5.36$		5.360 m ²

