TYPE OF WORK: LOCATION:

WING WALL DRAINAGE SLUICEWAY AT WF.172R + 15 m

CALCULATION	RESULT
	KLOODI
□ WATER STOP	
77.2.2.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4	
B = 200  mm	
$L = (1.80 + 0.15) \times 2 + (1.60 + 0.15 \times 2) = 5.800$	5.800 m
6,200	
2,300 1,600 2,300	
2,000 300 2,000	<u>, a 1941 a j</u>
WATER STOP	gradie Teragher
₹ EL +9.700	
SECTION A A LEVELING CONCRETE	70. F 24. 1 7
SECTION A-A LEVELING CONCRETE SCALE A (TYPE-E)	
	the second of the
5 JOINT FILTER	
5 JOINT FILTER	
□ JOINT FILTER  t = 10, ELASTIC MATERIAL	
t = 10, ELASTIC MATERIAL	3.007 m <sup>2</sup>
t = 10, ELASTIC MATERIAL	3.007 m <sup>2</sup>
$t = 10$ , ELASTIC MATERIAL $A = (0.30 \times 6.339) + (0.307 \times 1.80) \times 2 = 3.007$	3.007 m <sup>2</sup>
$t = 10$ , ELASTIC MATERIAL $A = (0.30 \times 6.339) + (0.307 \times 1.80) \times 2 = 3.007$	3.007 m <sup>2</sup>
$t = 10$ , ELASTIC MATERIAL $A = (0.30 \times 6.339) + (0.307 \times 1.80) \times 2 = 3.007$ 6,200  2,300  1,600  2,300	3.007 m <sup>2</sup>
$t = 10$ , ELASTIC MATERIAL $A = (0.30 \times 6.339) + (0.307 \times 1.80) \times 2 = 3.007$	3.007 m <sup>2</sup>
t = 10, ELASTIC MATERIAL  A = (0.30 x 6.339) + (0.307 x 1.80) x 2 = 3.007  6,200  2,300 1,600 2,300  2,000 300 2,000	3.007 m <sup>z</sup>
t = 10, ELASTIC MATERIAL  A = (0.30 x 6.339) + (0.307 x 1.80) x 2 = 3.007  6,200  2,300 1,600 2,300  2,000 300 500 2,000	3.007 m <sup>2</sup>
t = 10, ELASTIC MATERIAL  A = (0.30 x 6.339) + (0.307 x 1.80) x 2 = 3.007  6,200  2,300 1,600 2,300  2,000 300 500 2,000	3.007 m <sup>2</sup>
t = 10, ELASTIC MATERIAL  A = (0.30 x 6.339) + (0.307 x 1.80) x 2 = 3.007	
t = 10, ELASTIC MATERIAL  A = (0.30 x 6.339) + (0.307 x 1.80) x 2 = 3.007	
t = 10, ELASTIC MATERIAL  A = (0.30 x 6.339) + (0.307 x 1.80) x 2 = 3.007  6,200  2,300 1,600 2,300  2,000 900 900 2,000	
t = 10, ELASTIC MATERIAL  A = (0.30 x 6.339) + (0.307 x 1.80) x 2 = 3.007  6,200  2,300 1,600 2,300  2,000 300 2,000	
t = 10, ELASTIC MATERIAL  A = (0.30 x 6.339) + (0.307 x 1.80) x 2 = 3.007	
t = 10, ELASTIC MATERIAL  A = (0.30 x 6.339) + (0.307 x 1.80) x 2 = 3,007  6,200  2,300 1,600 2,000  2,000  2,000  2,000  2,000  2,000  3,000  2,000  3,000	
t = 10, ELASTIC MATERIAL  A = (0.30 x 6.339) + (0.307 x 1.80) x 2 = 3.007  2,300	

DRAINAGE SLUICEWAY AT WF. 172R+15 m

TYPE OF WORK

: CONCRETE (TYPE-CI) : BOX CULVERT

LOCATION

CALCULATION	RESULT
(TYPE-CI)	
$V_1 = \{(2.30 \times 2.35) - (1.60 \times 1.60) + \frac{1}{2} \times 0.15^2 \times 4\} \times 8.775$	5 / 41 / 4 / 4 / 4
<b>≈</b> 25,36	$\rho$
Vz = (1.00 × 0.40 × 1.30 ) × 2 = 1.040	
V3 = 0.25 x 1.30 x 4.30 = 1.398	
V4 = 1.00 x 4.30 x 0.30 + 1/2 x 0.152 x 2.30 x 2	
= 1,342	
Vs = 1.00 x 2.35 x 0.30 x 2 = 1.410	
할 수 있는 눈도 이 집은 모양을 보고 함께를 보는 수 있다면 살아 들어가는 모든 것 같아요요 된다.	
	<del></del>
(Deduction for PC Sheet Pile)	
(Deduction for PC Sheet Pile)  V6 = - (0.25 × 0.22 × 4.50) = -0.248	
V6 = - (0.25 x 0.22 x 4.50) = -0.248	
	30.302 m <sup>3</sup>
V6 = - (0.25 × 0.22 × 4.50) = -0.248	
V6 = - (0.25 x 0.22 x 4.50) = -0.248	
V6 = - (0.25 x 0.22 x 4.50) = -0.248	
V6 = - (0.25 × 0.22 × 4.50) = -0.248	
$V6 = -(0.25 \times 0.22 \times 4.50)$ = $-0.248$	
$V6 = -(0.25 \times 0.22 \times 4.50)$ = $-0.248$	
$V6 = -(0.25 \times 0.22 \times 4.50)$ = $-0.248$	
$V6 = -(0.25 \times 0.22 \times 4.50)$ = $-0.248$	
$V6 = -(0.25 \times 0.22 \times 4.50)$ = $-0.248$	
$V6 = -(0.25 \times 0.22 \times 4.50)$ = $-0.248$	
$V6 = -(0.25 \times 0.22 \times 4.50)$ = $-0.248$	
$V6 = -(0.25 \times 0.22 \times 4.50)$ = $-0.248$	

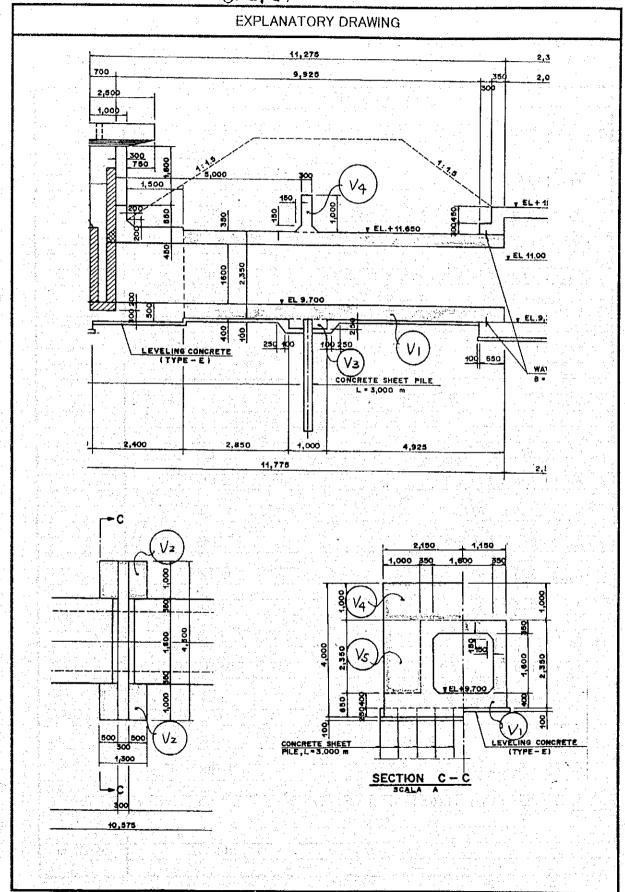
DRAINAGE SLUICEWAY AT WF. 172R + 15M

TYPE OF WORK

CONCRETE (TYPE-CI)

LOCATION

BOX CULVET



BOX CULVERT DRAINAGE SLUICEWAY AT WF.172R + 15 m TYPE OF WORK TYPE OF WORK : LOCATION :

	CALCULATION	RESULT
5	LEVELLING CONCRETE	
<u> </u>	(TYPE – E)	
<del></del> -	(IIFE-E)	
· ·	$V_1 = 0.10 \times 2.50 \times 6.825 = 1.706$	And the second
		1 24
	$V_2 = 0.10 \times 4.50 \times 1.30 = 0.585$	
٠.		
	$V_3 = (0.10 + 0.35) \times \frac{1}{2} \times 0.25 \times 4.50 \times 2 = 0.506$	
		Section 1
·	TOTAL = 2,797	2.797 m <sup>3</sup>
7 - 7 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		
	ing the first through the experience of the experience of the first of	
5	FORM	
	(H < 4.0 m)	200
		alaj kaj
-	$A_1 = 2.35 \times 3.20 \times 2 = 15.040$	
•:		
	$A_2 = 2.35 \times 4.625 \times 2 = 21.738$	
<u> </u>	$A_3 = 0.65 \times 1.00 \times 2 \times 2 = 2.600$	Market Mark
	$A_3 = 0.65 \times 1.00 \times 2 \times 2 = 2.600$	
	$A_4 = 3.35 \times 1.00 \times 2 \times 2 = 13.400$	1.000
	14 3.53 & 1.60 & 2.4 & 2.5	
	$A_5 = 0.65 \times 1.30 \times 2 = 1.690$	
	$A_6 = 0.30 \times 3.35 \times 2 = 2.010$	
4	$A_7 = 1.30 \times 8.775 \times 2 = 22.815$	the second se
	A = 100 + 3 20 + 3	
	$A_8 = 1.00 \times 2.30 \times 2 = 4.600$	
<u> </u>		er valgeringen van de skriver van de
	$A_9 = \sqrt{2 \times 0.15 \times 8.775 \times 4} = 7.446$	
	A = 120 - 9.775	
	$A_{10} = 1.30 \times 8.775 = 11.408$	
	$A_{11} = (2.30 \times 2.35) - (1.60 \times 1.60) + \frac{1}{2} \times 0.15 \times 4 = 2.890$	
	$A_{11} = (2.30 \times 2.33) - (1.00 \times 1.00) + 72 \times 0.13 \times 4 = 2.890$	
	TOTAL = 105.637	105.637 m <sup>2</sup>

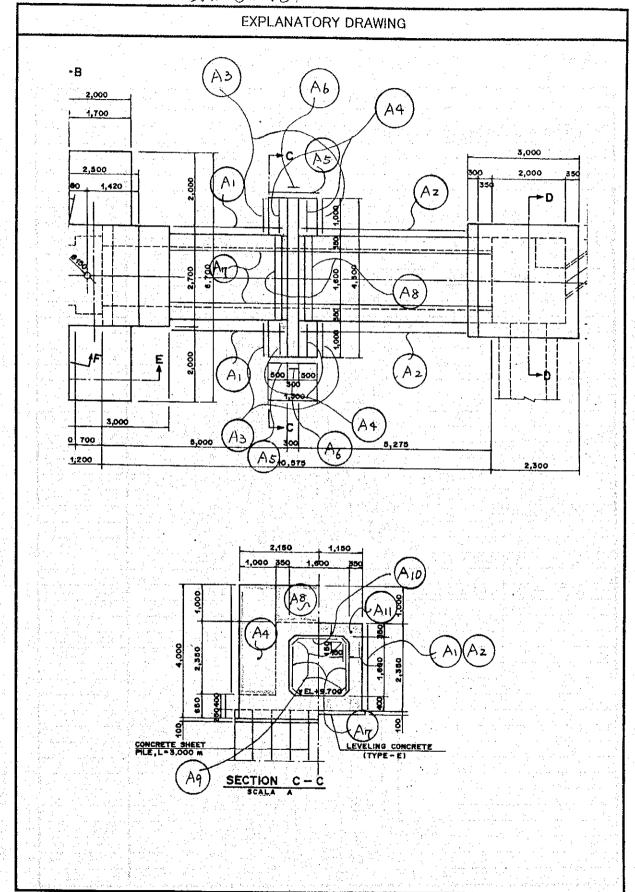
DRAINAGE SLUICEWAY AT WF. 1728 + 15 m

TYPE OF WORK

FORM

LOCATION

BOX CULVET



BOX CULVERT DRAINAGE SLUICEWAY AT WF.172R + 15 m TYPE OF WORK : LOCATION :

CALCULATION	RESULT
☐ FORM FOR LEVELLING CONCRETE	
FORM FOR LEVELLING CONCRETE	
(H < 4.0 m)	
$A_1 = 0.10 \times 6.825 \times 2 = 1.365$	
$A_2 = 0.10 \times 1.30 \times 2 = 0.260$	
$A_3 = (0.10 + 0.35) \times \frac{1}{2} \times 0.25 \times 4 = 0.225$	
TOTAL = 1.850	1.850 m <sup>3</sup>
101AL - 1.039	1,050 iii
1,000 350 1,000 350	
8	
- TE 19700	
5 SCAFFOLDING CONCAIR SHEET LEVELING CONCAI	m.
$(A_2)$ SECTION C-C $(A_1)$	
$A_1 = 3.35 \times 0.30 \times 2 = 2.010$	
$A_2 = 3.35 \times 1.00 \times 2 \times 2$ = 13.400	
가 하는 것이 되는 것이 되는 것이 되는 것이 되는 것이 되어 되었다. 그는 것이 되는 것이 되는 것이 되는 것이 되었다. 	
TOTAL # 15.410	15.410 m <sup>2</sup>
AI 1,000 \$50, 1,000 ped	
7 7 900	
CONCRETE SHEET LEVELING CONCRETE PLE,L-3,000 m (TYPE-E)	
SECTION C-C	

TYPE OF WORK SUPPORTING	CALCULATION	RESULT
LOCATION: BOX CULUERT		
	V={(1,60×1,60) - 1/2×0.152 \ x 8,775	
	22,365	22,365 m3
1,150		
1,000 asq 1,900 beg		
Q (TEL+\$700)		
00 00 00 00 00 00 00 00 00 00 00 00 00		
PLE,L=3.000 m		
SECTION C-C		

DRAINAGE SLUICEWAY AT WF. 172R + 15 m

TYPE OF WORK

: CONCRETE (TYPE-CI) : GATE PIER

LOCATION : GATE PIER

CALCULATION	RESULT
	aured per per e
V <sub>1</sub> = 0.30 × 1.80 × 2.00 × 2 = 2.160	
$V_2 = 0.40 \times 2.00 \times 2.00 \times 2$ = 3.200	
$V_3 = 0.25 \times 0.60 \times 2.00 \times 2$ = 0.600	
$V4 = (3.00 \times 0.50 + 0.25 \times 0.60) \times 2.70 - (0.20 \times 0.70)$	
x <i>z./o</i>	
= 4.16	
Vs = 1.60 x 1.50 x 0.55 x 2 = 2.640	
$V_6 = 2.70 \times 0.45 \times 1.50 + \frac{1}{2} \times 0.20^2 \times 2.70 = 1.877$	
$V_{\Pi} = 1.00 \times 0.30 \times 1.60$ = 0.480	
$V8 = (0.55 \times 0.30 + 0.70 \times 0.30) \times 4.40 \times 2 = 3.300$	
Vq = 0.50 x 0.55 x 2.20 x 2 = 1.210	
$V_{10} = \{(2.50 + 1.00) \times \frac{1}{2} \times 0.15 \times (0.55 + 0.70) \times \frac{1}{2}\} \times 2$	
= 0.328	
$V_{11} = 2.50 \times 2.70 \times 0.45 - \frac{15}{4} \times 0.15^{2} \times 0.45 = 3.030$	
(Deduction for PC Sheet Pile)	
$V_{12} = -(6.50 \times 0.22 \times 0.25)$ = -0.358	
70TA) = 22.628	22.628 m <sup>3</sup>

DRAINAGE SLUICEWAY AT WF. 172R + 15 M

TYPE OF WORK

CONCRETE (TYPE-CI) (1/2) LOCATION GATE PIER **EXPLANATORY DRAWING** 2,000 1,700 V8 12\* 500 700 5,000 1;200 2,700 **-** B 1,600 550 700 SECONDARY CONCRETE V8 SECTION G-G SECONDARY CONCRETE 750 LEVELING CONCRETE WATER STOP (PVC)

2,600

3,000

2,850

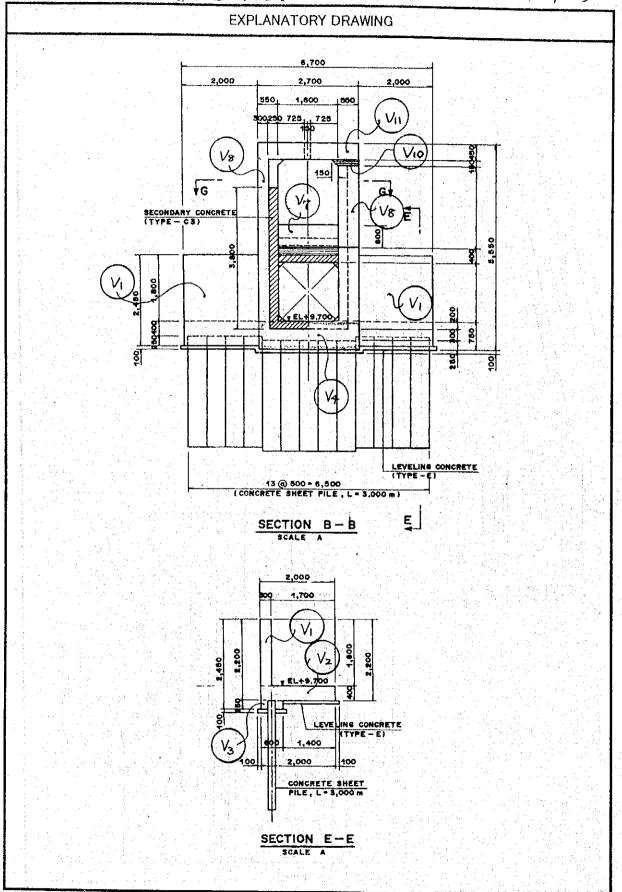
DRAINAGE SLUICEWAY AT WF. 172R + 15m

TYPE OF WORK

CONCRETE (TYPE-CI)

LOCATION : GATE PIER

(2/2)



									•						-								
	RESULT											-			1,751 m3								
72R + 15m	CALCULATION	(TYPE-E)		$V_1 = 0.80 \times 0.10 \times (2.00 + 0.10) \times 2 = 0.336$	and the second of the second o	$V_2 = 1.50 \times 0.10 \times (2.00 + 0.10) \times 2 = 0.630$		$V_3 = 0.80 \times 0.10 \times (2.70 + 0.10 \times 2) = 0.232$		V4 = 2.40 × 0.10 ×(2.70+0.10×2) = 0.696	(Deduction for PC Sheet Pile)		Vs = - (6.50 × 0.10 × 0.22) = -0.143	The second of th	707AL = 1.75		· · · · · · · · · · · · · · · · · · ·						
DRAINAGE SLUICEWAY AT WIF.)		LOCATION: GATE PLER	(c) (GO)			SONCRIE - C3 )	1.500 3.500 7.500	0000 7 000 000 000 000 000 000 000 000	81 / / / / / / / / / / / / / / / / / / /	789		900 780 1,50 20 1,50 1,400	009 00 00 00 00 00 00 00 00 00 00 00 00	Section 1	100 2,350	100)	008*8	y EL	1,400 DOO DNCRE LE, L	VE M	)O m	ICRET	

TYPE OF WORK : GATE PIER

LOCATION : DRAINAGE SLUICEWAY AT WF.172R + 15 m

CALCULATION		RESULT
1 2000		
FORM		
	<u> </u>	
(H < 4.0 m)		
$A_1 = 2.00 \times 2.45 \times 2 =$	7,000	
$A_2 = 2.00 \times 1.80 \times 2 = $	7.200	
$A_3 = 2.00 \times 0.40 \times 2$	1.000	
$A_4 = \{(0.40 \times 2.00) + (0.25 \times 0.60)\} \times 2 =$		
$A_5 = 0.30 \times 1.80 \times 2$	1.080	
$A_6 = 0.15 \times 2.00 \times 2$	0.600	
$A_7 = \{(0.25 \times 0.60) + (0.50 + 3.00) + (2.20 \times 1.00) + (0.50 + 3.00) + (0.50$	1.00 x 2.50)	
x ½ x 0.15 + (0.45 x 2.50)} x 2		
and Replicate \$5 Milking 1970 and revisit 1970 are \$5.	23.675	184.832435
$A_8 = (2.95 \times 0.55) \times 2 + (0.75 \times 1.60) =$	4.445	
$A_9 = 0.10 \times 2.75$	0.270	
$A_{10} = (2.35 \times 0.20) \times 2$	- 0.940	
$A_{11} = (2.20 \times 0.30) \times 2$	1.320	
$A_{12} = (2.40 \times 0.25) \times 2$	1.200	
$A_{12}^{1} = (0.20 \times 1.60) \times 2$		41 1 1 1 1 1 1 1
$A_{13} = (2.20 \times 0.50) \times 2$		
$A_{14} = (4.40 \times 0.25) \times 2$	T1777	end of the second
$A_{15} = (4.40 \times 0.70) \times 2$	V., V.	
$A_{16} = (1.60 \times 0.30) \times 2$		
$A_{17} = (1.95 \times 0.55) \times 2$		
$A_{18} = (0.35 \times 1.60)$	- 0.560	
$A_{19} = 1.00 \times 1.60$	= 1,600	
$A_{20} = \sqrt{2} \times 0.20 \times 2.70$	- 0.764	
$A_{21} = \left\{ (0.55 + 0.70x1/2x)0.15 + 0.75 \right\} x4 =$	= 1.912	
$A_{22} = 0.45 \times 2.50 \times 2$	= 2.250	
$A_{23} = (1.60 \times 1.00) + (0.25 \times 0.70) \times 2$	= 1.950	
TOTAL	= <i>77.37</i> 1	77.371 m²
		4. 医斯罗斯氏

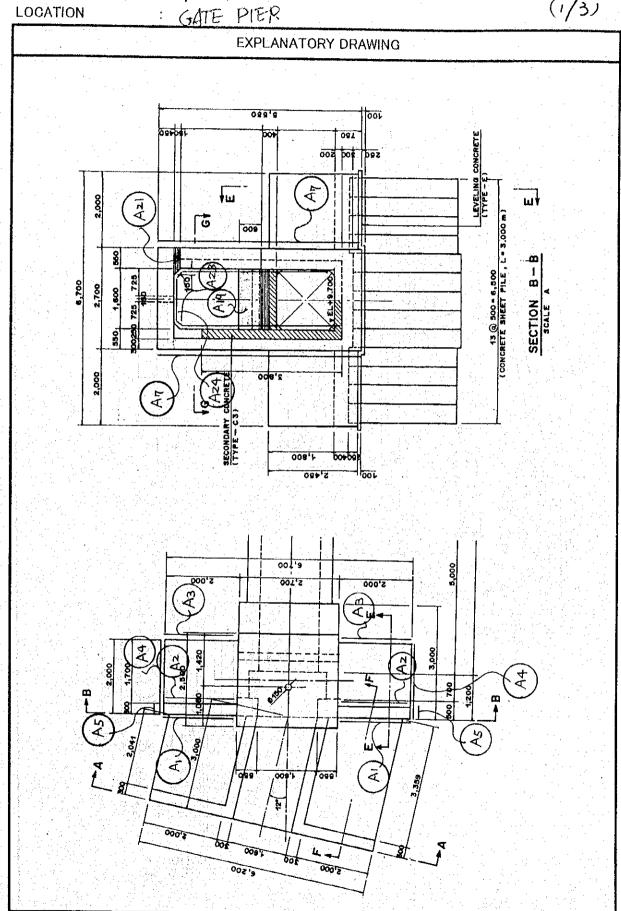
DRAINAGE SLUCEWAY AT WF 172 R + 15 M

TYPE OF WORK

FORM

LOCATION

(1/3)



DRAINAGE SLUICEWAY AT WF172R + 15W

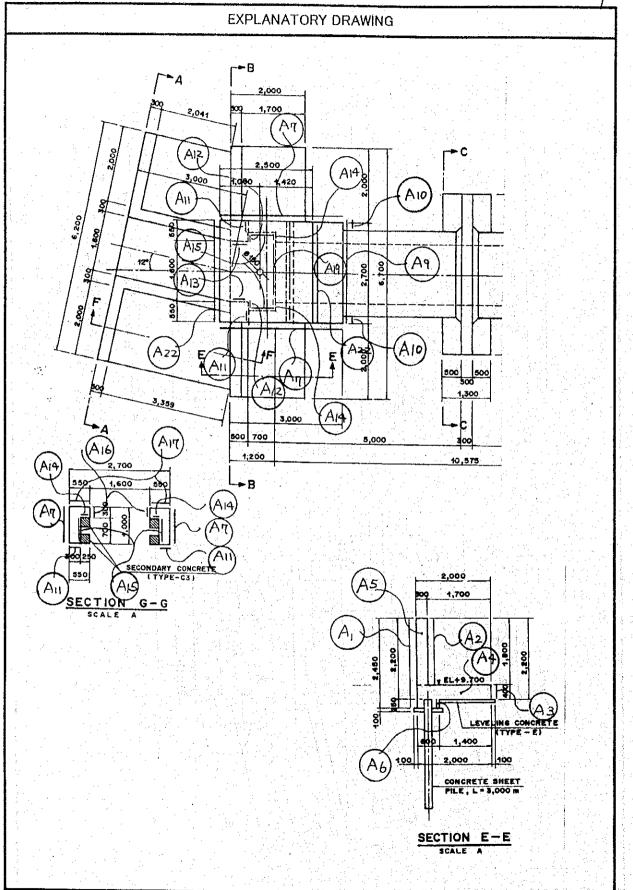
TYPE OF WORK

FORM

LOCATION

: GATE PLER

(2/3)

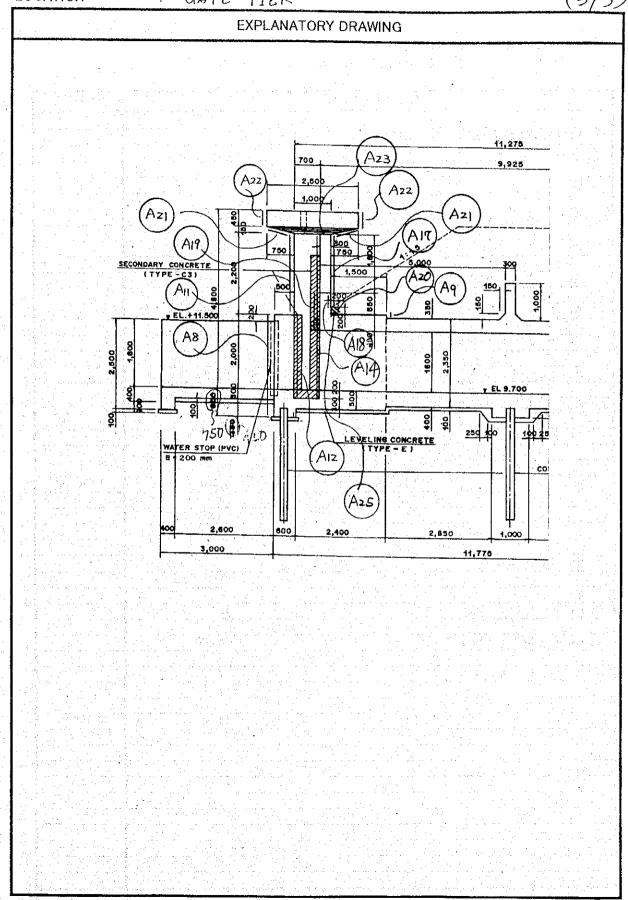


DRAINAGE SLICEWAY AT WF172R+15M

TYPE OF WORK

FORM

LOCATION : GATE PIER (3/3)



TYPE OF WORK: LOCATION:

GATE PIER DRAINAGE SLUICEWAY AT WF.172R + 15 m

CALCULATION		RESULT
FORM FOR LEVELLING CONCRETE		
(1) = 10 = 1		
(H < 4.0 m)		
$A_1 = 0.10 \times (2.00 + 0.10) \times 2 \times 2$	= 0.840	
$A_2 = 0.10 \times (2.00 + 0.10) \times 2 \times 2$	= 0.840	
112 0.10 X (2.00 + 0.10) X Z X Z	- 0.840	
$A_3 = 0.10 \times 0.80 \times 2$	= 0.160	
$A_4 = 0.10 \times 1.50 \times 2$	= 0.300	
	0.500	
$A_5 = 0.10 \times 2.90 \times 2$	= 0.580	
$A_6 = 0.10 \times 2.90$	= 0.290	
$A_7 = 0.10 \times 0.80 \times 2$	= 0.160	
$A_8 = 0.10 \times 2.50 \times 2$	= 0.500	
TOTAL	= 3.670	3.670 m²
		3.070 M
F SCAFFOLDING		
$A_1 = 4.80 \times 2.70$	- 12.000	
	12.900	and the second of the second o
	= 12.960	
$A_2 = 4.80 \times 2.50 \times 2$	= 24.000	
	fare alignetic state	
$A_2 = 4.80 \times 2.50 \times 2$	= 24.000	
$A_2 = 4.80 \times 2.50 \times 2$ $A_3 = 2.75 \times 2.70$	= 24.000 = 7.425	
$A_2 = 4.80 \times 2.50 \times 2$ $A_3 = 2.75 \times 2.70$ TOTAL	= 24.000 = 7.425	
$A_2 = 4.80 \times 2.50 \times 2$ $A_3 = 2.75 \times 2.70$ TOTAL	= 24.000 = 7.425 = 44.385	44.385 m <sup>2</sup>
$A_2 = 4.80 \times 2.50 \times 2$ $A_3 = 2.75 \times 2.70$ TOTAL	= 24.000 = 7.425 = 44.385	44.385 m <sup>2</sup>
$A_2 = 4.80 \times 2.50 \times 2$ $A_3 = 2.75 \times 2.70$ TOTAL	= 24.000 = 7.425 = 44.385	44.385 m <sup>2</sup>
$A_2 = 4.80 \times 2.50 \times 2$ $A_3 = 2.75 \times 2.70$ TOTAL	= 24.000 = 7.425 = 44.385	44.385 m <sup>2</sup>
$A_2 = 4.80 \times 2.50 \times 2$ $A_3 = 2.75 \times 2.70$ TOTAL	= 24.000 = 7.425 = 44.385	44.385 m²

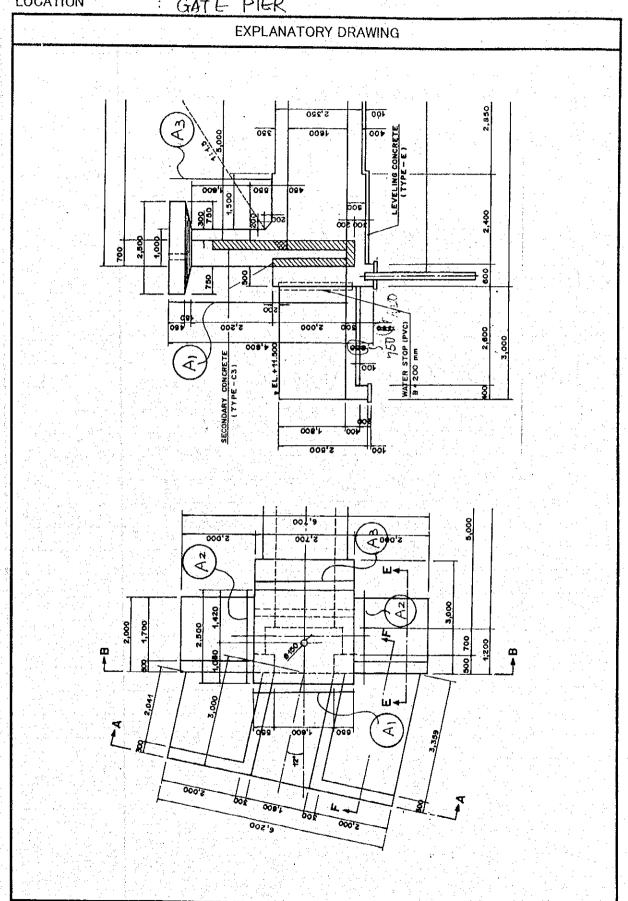
DRAINAGE SLUICEWAY AT WF. 172R + 15 m

TYPE OF WORK

: SCAFFOLDING

LOCATION

: GATE PIER



DRAINAGE SLUICEWAY AT WF. 172R +15 m

TYPE OF WORK

LOCATION

SUPPORTING GATE PIER

CALCULATION RESULT  $V_1 = \{(1.60 \times 1.60) - \frac{1}{2} \times 0.15^2 \times 4\} \times 1.80 = 4.527$ V2= {(2.30+2.15)x/2 x0.75 - 1/2 x0.202} x 2.70 = *4.45*2  $V_3 = (4.35 + 4.20) \times \frac{1}{2} \times 0.75 \times 2.70 = 8.657$ V4 = \((4.20 × 1.60) - (/2 × 0.152 × 2) \ x 0.70 4.688 V4' = \((1.60 \times 1.60) - (1/2 \times 0.152 \times 2) \forall \times 0.30 0.761 23.085 m³ TOTAL = 23.085

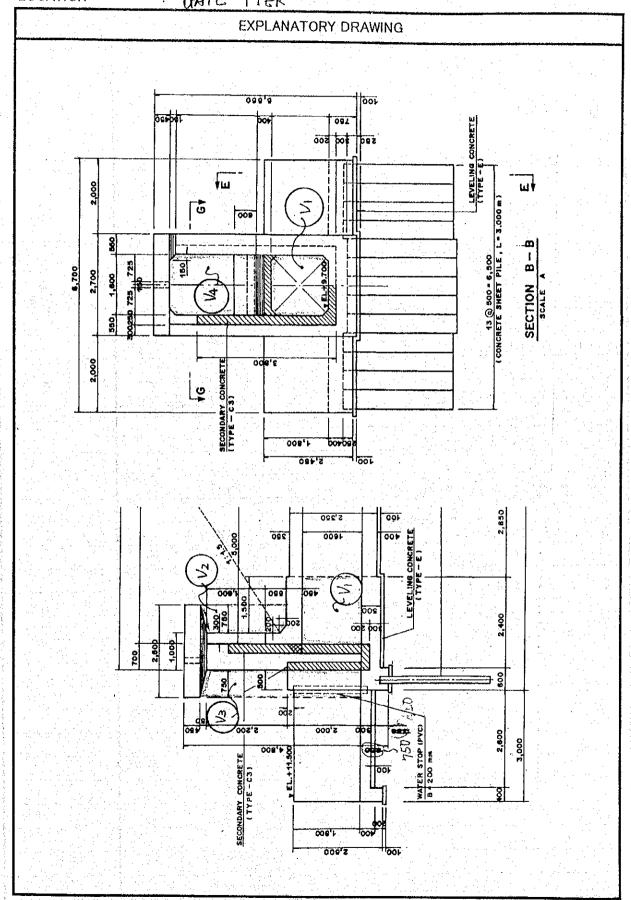
DRAINAGE SLUICEWAY AT WF. 172 R + 15 m

TYPE OF WORK

SUPPORTING

LOCATION

GATE PIER



DRAINAGE SLUICEWAY AT WF. 172R + 15m

TYPE OF WORK

: SECONDARY CONCRETE

GATION : GATE PIER CALCULAT	ION	RESULT
SECONDARY CONCRETE (TYPE-C	23)	
-LUNINI CONCERNA		
V1 = 0.20 × 0.70 × 2.10	= 0.294	
V2 = 0.20 × 0.25 × 2.00 × 2	= 0.200	
$V_3 = 0.25 \times 0.25 \times 3.70 \times 2$	= 0.463	
V4 = 0.25 x 0.50 x 1.60	= 0.200	
	70TAL = 1.157	1.157 m3
DRM (H < 4.0m)		
A1 = 0.25 x 2.00 x 2	- 1.000	
A2 = 0,25 x 3,70 x 2	= 1.850	
A3 = 0.20 x 2.00 x 2	= 0.800	
A4 = 0.25 x 3.70 x 2	F 1 1, 8.50	
As = 0.25 x 1.60	= 0.400	
A6 = 0.50 × 1.60	= 0.800	
		1 700 3
	TOTAL = 6.700	b.700 m <sup>2</sup>

DRAINAGE SLUICEWAY AT WF. 172R + 15 m

TYPE OF WORK

SECONDARY CONCRETE

<u> </u>	CALCULATION	$(\frac{2}{2})$ RESULT
ANCHOR BAR (DIG	1 = 200 mg /Pat \	
Z-10-11011 - 1010	1 - Comm / par )	
(side)		
CP10E)		
W - 0 D-0		
$N_1 = 9 Bars \times Z \times -$	$\leq = 36  \text{Bars}$	
$N_2 = 5 Bars \times 2 \times 3$	2 = 40 Bars	
(Bottom)		
n3 = 5 Bars x 3	= 15 Bars	
TOP		
114 = 3 Bars x 3	e 9 Bars	
	TOTAL = 100 Bars	
W = 100 Bars x 0.20	$\times 1.58 \frac{19\%}{m} = 31.600 \frac{1}{8}$	0.032 tf
<u> 18 - 18 18 18 18 18 18 18 18 18 18 18 18 18 </u>		
	<u> 강경 교육 기계를 참</u> 하는데, 하는 그는 이 바라 가는 이 이 이 이 기계를 받는다.	

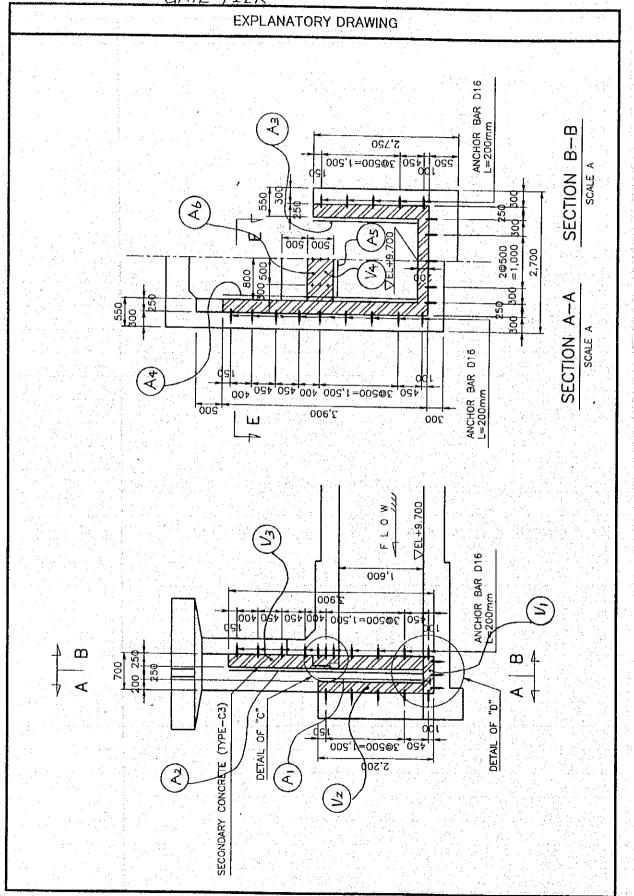
TYPE OF WORK

DRAINAGE SLUICEWAY AT WF. 172R + 15 m

SECONDARY CONCRETE

LOCATION

: GATE PIER



TYPE OF WORK : GATE PIER LOCATION : DRAINAGE SI DRAINAGE SLUICEWAY AT WF.172R + 15 m

CALCULATION		RESULT
5 SEEPAGE BLOCKING		
PC SHEET PILE		
$n_1 = 6.70 : 0.50 = 13.40 \cong$		
$n_2 = 4.30 : 0.50 = 8.60 \cong$	9 piles	
$L = (13+9) \times 3.00 =$	66.000	66.000 m
• PILING		
N Value : N = 27 (AVERAGE)  L = 21 piles x 3.00 =	66,000	66.000
L - 21 piles x 3.00	66.000	66.000 m
➡ HAND RAIL AND LADDER		
L HAND KAIL AND LADDEK		
(GALVANIZED STEEL)		
• STEEL PIPE Ø75 (W = 5.77 kgf/m)		
$n_1 = 6 \text{ pipes}$ $(W - 3.77 \text{ kgr/m})$		
$L_1 = 1.40 \text{ m/pipe}$		
$W_1 = 6 \text{ pipes } \times 1.40 \times 5.77 =$	48.468	
A Company of the A Street Company of the Company of	40,100	
• STEEL PIPE Ø 50 (W = 2.63 kgf/m)		
$n_2 = 4 \text{ pipes}$		
$L_2 = 0.80 \mathrm{m}\mathrm{/pipe}$		
$W_2 = 4 \text{ pipes } \times 0.80 \times 2.63 = $	8.416	
$n_3 = 4$ pipes		
$L_3 = 2.20 \text{m/pipe}$	ang di Basar di Kabupatèn K	The state of the state of
$W_3 = 4 \text{ pipes x } 2.20 \text{ x } 2.63 = $	23.144	
$n_4 = 2$ pipes		
$L_4 = 2.40 \text{ m/pipe}$		
$W_4 = 2 \text{ pipes } x 2.40 x 2.63 =$	12.624	
	The second of th	w .
$n_s = 2 \text{ pipes}$	A RESTRICTED TO	
$L_5 = 4.76 \text{ m/pipe}$ $W_5 = 2 \text{ pipes } \times 4.76 \times 2.63 =$	26.020	
$W_5 = 2 \text{ pipes } \times 4.76 \times 2.63 =$	25.038	<u> </u>
• ROUND BAR Ø 16 (W = 1.58 kgf/m)		
$n_6 = 31 \text{ pipes}$		
$L_6 = 1.10 \text{ m/pipe}$	<u>n in de la companya di manaka di</u> Tanggarangan dan menganggan di manakan di menganggan beranggan di menganggan beranggan beranggan beranggan ber	
$W_6 = 31 \text{ pipes } \times 1.10 \times 1.58 =$	53.878	
	23.070	
$n_7 = 5 \text{ pipes}$		
$L_7 = 1.58 \text{m/pipe}$		
$W_1 = 5 \text{ pipes } \times 0.60 \times 1.58 =$	4.740	
TOTAL $(W_1 + W_2 + W_3 + W_4 + W_5 + W_6 + W_7) =$	176.308	0.176 tf

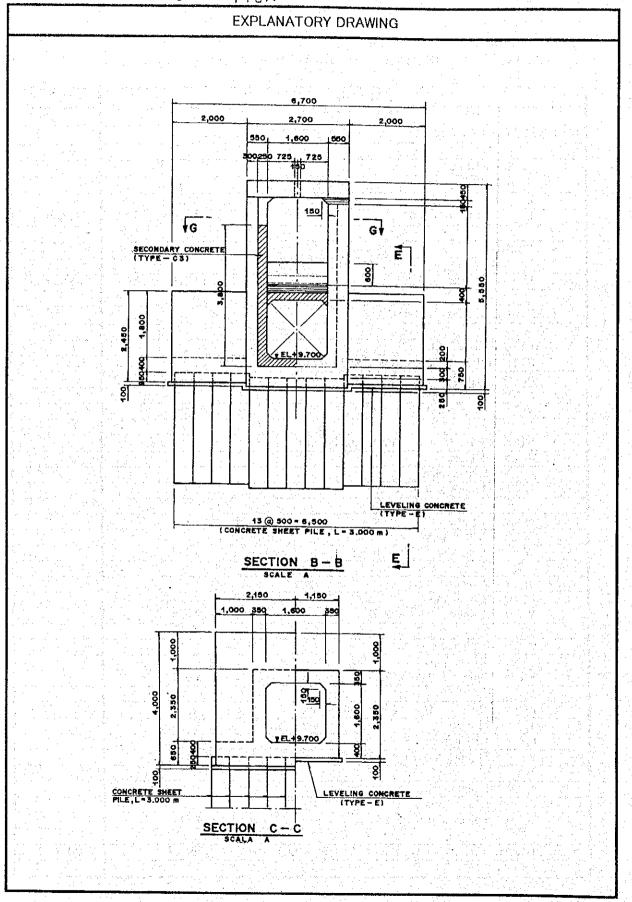
DRAINAGE SLUICEWAY AT WF. 172R+ 15 M

TYPE OF WORK

: SEE PAGE BLOCKING

LOCATION

: GATE PIER



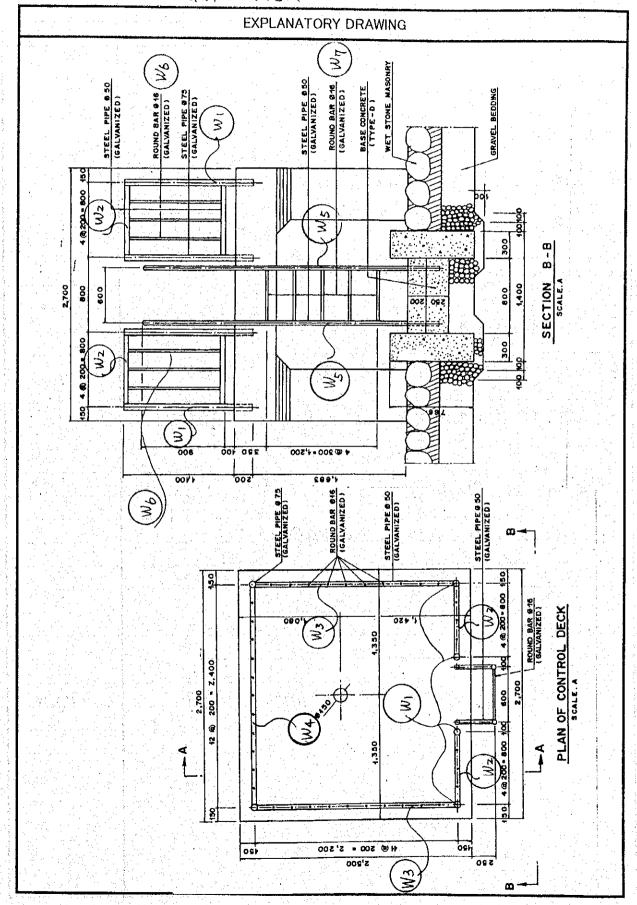
DRAINAGE SLUICEWAY AT WF172R + 15 M

TYPE OF WORK

HAND RAIL AND LADDER

LOCATION

GATE PIER



DRAINAGE SLUICEWAY AT WF. 172R+15m

TYPE OF WORK

CONCRETE (TYPE-CI)

LOCATION : CONNECTING BOX

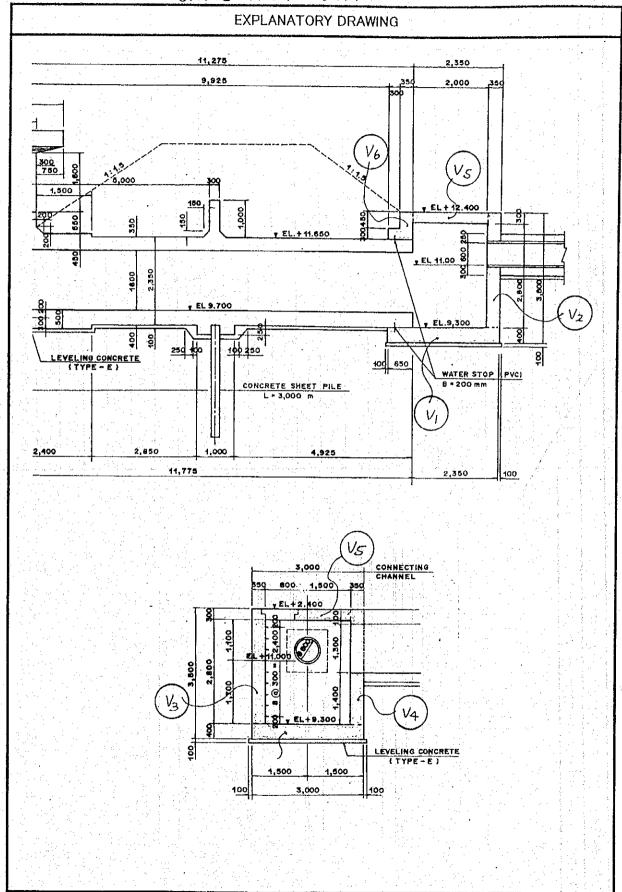
CALCULA	HON	RESULT
(TYPE-CI)		
$V_1 = 3.00 \times 3.00 \times 0.40$	= 3,600	
12 = 3.00 x 3.10 x 0.35 - (7/4 x 0.74	4° × 0.35 ) = 3,104	
13 = 2.00 x 3.10 x 0.35	= 2.170	
4 = 2.00 × 3.10 × 0.35 - (1.30)	×1.00×0.35) = 1.715	
15 = 2.00 x 2.30 x 0.30	= /.38 <i>0</i>	
( - ( o o o o o o o o o o o o o o o o o		
6 = (0.30 × 0.65 + 0.45 × 0.35) ×	3.00 = 1.058	
7 = 2.35 × 0.35 × 0.65 × 2		
( - 2.33 × 0.33 × 0, 63 × 2	= 1.069	
Deduction for Opening?		
occurrent to opening		
$\frac{1}{8} = -\{(1.00 \times 1.00 \times 0.15) + (0.15)\}$	80 10 80 10 15 1	
	SU ~V.SU XV. IS / ]	
	= -0.246	
9 = 0.49 × 0.98 × 0.15 × 2	= 0.144	
	TOTAL = 13.994	13,994 m³

DRAINAGE SLUICEWAY AT WF. 172R + 15 M

TYPE OF WORK

CONCRETE (TYPE-CI)

LOCATION : CONNECTING BOX



DRAINAGE SLUICEWAY AT WF. 172R+15m

TYPE OF WORK LOCATION

: FORM

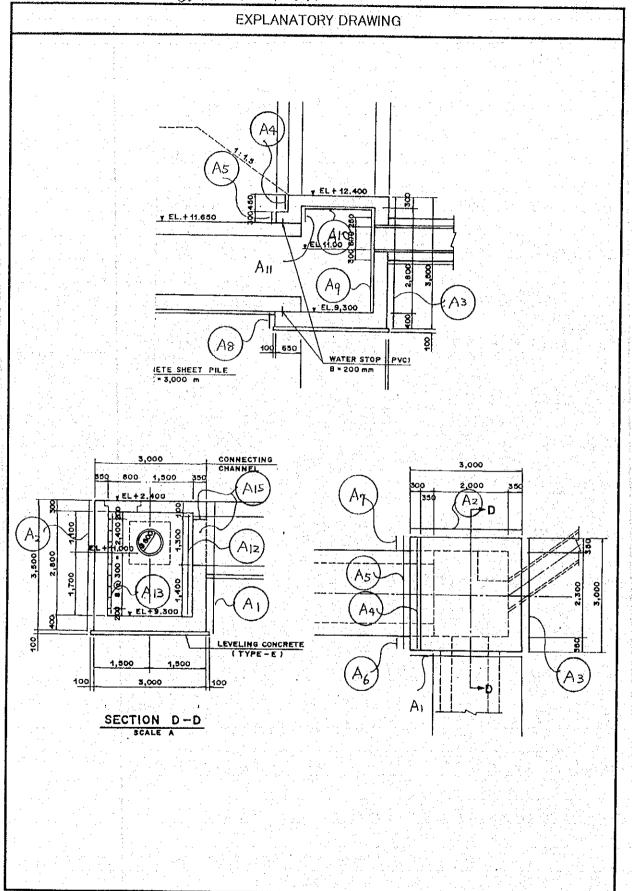
: CONNECTING BOX CALCULATION RESULT (H < 4.0m) $A_1 = \{(3.00 \times 3.05) + (0.45 \times 2.70)\} - (1.30 \times 1.00)$ = 9.065  $A_2 = (3.00 \times 3.05) + (0.45 \times 2.70)$ = 10.365  $A_{3} = (3.50 \times 3.00) - \frac{70}{4} \times 0.75^{2}$ = 10.058 A4 = 0.45 x 3.00 = 1.350  $A_5 = 0.30 \times 3.00$ = 0.900 Ab = 2.40 x 0.35 = 0.840 $A_{7} = 2.40 \times 0.35$ = 0.840 A8 = 0.30 × 3.00 = 0.900  $A9 = 2.80 \times 2.30 - \sqrt[10]{4} \times 0.74^2$ = 6.010 A10 = 2.00 × 2.30 - (0.80 × 0.80) = 3.960  $A_{\rm II} = 2.30 \times 0.45$ = 1.035  $A_{12} = 2.80 \times 2.00 - (1.30 \times 1.00)$ = 4.300 A13 = 2.80 x 2.00 = 5.600 A14 = (1.00 × 0.15)× 4 = 0.600  $A_{15} = (1.30 \times 0.35) \times 2 + (1.00 \times 0.35) = 1.260$ TOTAL = 57.083 57,083 m2 DRAINAGE SLUICEWAY AT WF. 1728 + 15 M

TYPE OF WORK

FORM

LOCATION

: CONNECTING BOX



TYPE OF WORK: CONNECTING BOX

LOCATION : DRAINAGE SLUICEWAY AT WF.172R + 15 m

	CALCULATION		RESULT
FORM FOR LEVELLING C	ONCDETE		
FURIN FUR LEVELLING C	ONCREIE		
(H < 4.0 m)			
A = 0.10 - 2.20 - 2		- 0.640	
$A_1 = 0.10 \times 3.20 \times 2$		= 0.640	
$A_2 = 0.10 \times 3.20 \times 2$		= 0.640	
	<u> </u>		
	TOTAL	= 1.280	1.280 m²
		EL + 12,400	
	T EL. + 11.650		
	y EL.+11.650 8		
		, EL 11.00 \$	
		, EL.9,300	
		3	
	_ <u>(to</u> c	WATER STOP PVC) 8	
	- ETE SHEET PILE	B = 200 mm	
WATER STOP	$(\stackrel{\leftarrow}{A})$		
		$A_2$ $A_1$	
B = 200 m	4,925		
		2,350 100	
$L = 2.30 \times 2 + 2.35 \times 2$		= 9.300	9.300 m
		<u>nto estilization de l'état, o per</u> Etation de la company	

TYPE OF WORK: LOCATION:

CONNECTING BOX

DRAINAGE SLUICEWAY AT WF.172R + 15 m

	CALCULATION		RESULT
SCAFFOLDING			
$A_1 = 3.50 \times 3.00$		10.50	
$A_1 = 3.50 \times 3.00$		= 10.50	The Artistan
$A_2 = 3.50 \times 3.00$		= 10.50	
		10.30	
$A_3 = 3.50 \times 3.00$		= 10.50	
$A_4 = 3.50 \times 0.35 \times 2$	<u> </u>	= 2.45	4
	TOTAL	= 33.950	33.950 m <sup>2</sup>
	TOTAL	_ 33.930	33.930 m
		,000 200,	
		7-0	
			3 7 38 7 3
<u>an alaman ny faritr'i Arabina. Ilay ao ao amin'ny faritr'i Arabina.</u>			
<u>andres de la parteral de la casa de la casa</u>		~	
SUPPORTING			
$V = 2.80 \times 2.00 \times 2.30$		= 12.880	12.880 m <sup>3</sup>
$v = 2.80 \times 2.00 \times 2.30$		= 12.880	12.880 m <sup>3</sup>
$v = 2.80 \times 2.00 \times 2.30$			12.880 m <sup>3</sup>
$v = 2.80 \times 2.00 \times 2.30$	5.126		12.880 m <sup>3</sup>
$v = 2.80 \times 2.00 \times 2.30$			12.880 m³
$v = 2.80 \times 2.00 \times 2.30$	5.126		12.880 m <sup>3</sup>
$v = 2.80 \times 2.00 \times 2.30$	1.120 10 5,000		12.880 m <sup>3</sup>
	19 3,000 10 11,11,000		12.880 m <sup>3</sup>
	19 3,000 10 11,11,000		
	192 3,000 114,11,000		
	10 10 10 10 10 10 10 10 10 10 10 10 10 1		
	132 3/000 322 3/000 341 1100 8 411 1100 8 (1)		
	112 1,000 112 1,000 11,110 \$ 11,120 \$ 11,130 \$ 11,130 \$		
	192 3,000 192 3,000 193 1100 5 194 1100 5 194 1100 5 194 1100 5		
	11 100 S		
	112 5,000 112 5,000 113 5,000 114 5,000		
	112 5,000 S		
	1115 112 1,000 11 1,000 1 11 1,000 1		

DOINT FILLER	.	RESULT
WG BOX	T=10, ELASIIC MAIERIAL	
2,350	A= (2.30+2.35)x2 × 0.65 = 6.045	6.045 m²
2,000 350 250 250 250 350 350 350 350 350 350 350 350 350 3		
000	The region of the control of the con	
v EL+12.400		
0920		
009,8 008,8		
- 1 . EL.9.300		
00+		
B=200 #B		
2,350   100	The state of the s	

TYPE OF WORK:

RIVERSIDE OPEN CHANNEL DRAINAGE SLUICEWAY AT WF.172R + 15 m LOCATION

CALCULATION	RESULT
CONCRETE	
• (TYPE – D)	
$A = (0.60 + 0.70) \times \frac{1}{2} \times 0.10$	$= 0.065 \text{ m}^2$
$V = 0.065 \times (18.70 + 3.00) \times 2$	= 2.821   2.821   m3
5,200	
	0 600
TOPCONCACTE	10 (600)
WET STONE MASONRY	
ann /	<u>-11</u>
CONTACT DECOMES	
SECTION C - C	
SECTION C - C	
FORM	
(H < 4.0 m)	
$A = 0.10 \times (18.70 + 3.00) \times 2$	$=$ 4.340 $m^2$
<del>하는 사람이 살아야</del> 하는데 하는데 하를 갖고 하시네요?	
3,200	00 (800
10P SONCALTE 1200 (1800 1.2)	
WET STONE MASONRY	
	17.19
(A) (\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	
	41 (A)
GRAYEL BEDRING	
SECTION C-C	
大大电影 不知 医二氯甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基	

TYPE OF WORK : LOCATION : RIVERSIDE OPEN CANNEL DRAINAGE SLUICEWAY AT WF.172R + 15 m

CALCULATION	RESULT
→ WET STONE MASONRY	
$A_1 = 1.555 \times 0.25 \times 2 + (2.141 + 2.307) \times \frac{1}{2} \times 0.25$	
$= 1.334 \text{ m}^2$	
$V_1 = 1.334 \times (18.70 + 4.00) = 30.280$	
$V_1 = 1.334 \times (18.70 + 4.00) = 30.280$	
$A_2 = 1.60 \times 0.25 = 0.400 \text{ m}^2$	
$V_2 = (0.40 + 1.334) \times 1/2 \times 2.40 = 2.081$	
$V_3 = 1.60 \times 0.35 \times 0.60 = 0.336$	
TOTALOULY	22 (00 1
$T \hat{O} T \hat{A} L (V_1 + V_2 + V_3) = 32.699$	32,699 m <sup>3</sup>
GRAVEL BEDDING	
$A_1 = 1.621 \times 0.20 \times 2 + (2.307 + 2.523) \times \frac{1}{2} \times 0.10$	
= 0.890 m <sup>2</sup>	
$V_1 = 1.890 \times (18.70 + 4.00) = 20.203$	
$A_2 = 1.60 \times 0.10 = 0.160 \text{ m}^2$	
$V_2 = (0.16 + 0.89) \times \frac{1}{2} \times 2.40 = 1.260$	
TOTALOUTY	21.462 3
$TOTAL(V_1 + V_2) = 21.463$	21.463 m <sup>3</sup>
	3.47

TYPE OF WORK:

LOCATION

RIVERSIDE OPEN CHANNEL DRAINAGE SLUICEWAY AT WF.172R + 15 m

CALCULATION	RESUL
STRUCTURAL EXCAVATION	
$A = (2.358 + 5.20) \times \frac{1}{2} \times 120$	= 40.535 m <sup>2</sup>
$V = 4.535 \times (22.70 + 25.10) \times \frac{1}{2}$	= 108.387 108.4 m
9,200 400 1,200 1,600 1,2	00 ,600
JOP CONCRETE , 1200 120	
MET STONE MASONEY	
	/ /
9027	
Trypres -	<u></u>
GRAVEL BEDDING	8
SECTION C - C	
	ing belong the single of the s
CEMENT MORTAR POINTING	
CEMENT MORTAR POINTING	
CEMENT MORTAR POINTING $A_1 = 1.555 \times (18.70 + 4.00) \times 2$	= 70.597
$A_1 = 1.555 \times (18.70 + 4.00) \times 2$	
	= 70,597 = 3.732
$A_1 = 1.555 \times (18.70 + 4.00) \times 2$	
$A_1 = 1.555 \times (18.70 + 4.00) \times 2$ $A_2 = \frac{1}{2} \times (1.555 \times 2.40) \times 2$	= 3.732
$A_1 = 1.555 \times (18.70 + 4.00) \times 2$	
$A_1 = 1.555 \times (18.70 + 4.00) \times 2$ $A_2 = \frac{1}{2} \times (1.555 \times 2.40) \times 2$	= 3.732
$A_1 = 1.555 \times (18.70 + 4.00) \times 2$ $A_2 = \frac{1}{2} \times (1.555 \times 2.40) \times 2$ TOTAL	= 3.732 = 74.329 74.329 m
$A_1 = 1.555 \times (18.70 + 4.00) \times 2$ $A_2 = \frac{1}{2} \times (1.555 \times 2.40) \times 2$ TOTAL	= 3.732 = 74.329 74.329 m
$A_{1} = 1.555 \times (18.70 + 4.00) \times 2$ $A_{2} = \frac{1}{2} \times (1.555 \times 2.40) \times 2$ $TOTAL$	= 3.732 = 74.329 74.329 m
$A_{1} = 1.555 \times (18.70 + 4.00) \times 2$ $A_{2} = \frac{1}{2} \times (1.555 \times 2.40) \times 2$ $TOTAL$ $\frac{10P CONCSELU}{4000} = \frac{5,200}{1.500} = \frac{1,500}{1.500}$	= 3.732 = 74.329 74.329 m
$A_1 = 1.555 \times (18.70 + 4.00) \times 2$ $A_2 = \frac{1}{2} \times (1.555 \times 2.40) \times 2$ TOTAL  TOTAL  TOTAL  TOTAL  SOUL SOUL SOUL SOUL SOUL SOUL SOUL SOUL	= 3.732 = 74.329 74.329 m
$A_1 = 1.555 \times (18.70 + 4.00) \times 2$ $A_2 = \frac{1}{2} \times (1.555 \times 2.40) \times 2$ TOTAL  TOTAL  JOP CONCRETE  SOUL 1510NE MASONBY  WEI STONE MASONBY	= 3.732 = 74.329 74.329 m
$A_1 = 1.555 \times (18.70 + 4.00) \times 2$ $A_2 = \frac{1}{2} \times (1.555 \times 2.40) \times 2$ TOTAL  TOTAL  TOTAL  SOO 1500 1500 1500 1500 1500 1500 1500 15	= 3.732 = 74.329 74.329 m
$A_1 = 1.555 \times (18.70 + 4.00) \times 2$ $A_2 = \frac{1}{2} \times (1.555 \times 2.40) \times 2$ TOTAL  TOTAL  TOTAL  SOO LEGAL  WEI STONE MASONNY  SOLUTION  SOLUTION	= 3.732 = 74.329 74.329 m
A <sub>2</sub> = ½ x (1.555 x 2.40) x 2  TOTAL  TOP CONCRETE.  WET STONE MASONNY  GRAVEL PEOPLY	= 3.732 = 74.329 74.329 m
A <sub>1</sub> = 1.555 x (18.70 + 4.00) x 2  A <sub>2</sub> = ½ x (1.555 x 2.40) x 2  TOTAL  TOTAL  JOP CONCRETE.  WET. STONE MASONBY  SECTION C - C	= 3.732 = 74.329 74.329 m
A <sub>1</sub> = 1.555 x (18.70 + 4.00) x 2  A <sub>2</sub> = ½ x (1.555 x 2.40) x 2  TOTAL  TOTAL  SOO 1500 1500 1500 1500 1500 1500 1500 15	= 3.732 = 74.329 74.329 m
A <sub>1</sub> = 1.555 x (18.70 + 4.00) x 2  A <sub>2</sub> = ½ x (1.555 x 2.40) x 2  TOTAL  TOTAL  TOTAL  SECTION C - C SCALE 8	= 3.732 = 74.329 74.329 m
A <sub>1</sub> = 1.555 x (18.70 + 4.00) x 2  A <sub>2</sub> = ½ x (1.555 x 2.40) x 2  TOTAL  TOTAL  TOTAL  SOO 1500 1500  SECTION C - C  SCALE 8	= 3.732 = 74.329 74.329 m

TYPE OF WORK: REINFORCEMENT OF EXISTING DIKE

LOCATION

CALCULATION		RESULT
☐ STRUCTURAL EXCAVATION		
$A_1 = (2.00 + 2.80) \times \frac{1}{2} \times 0.80$	$= 1.920 \text{ m}^2$	
(2.00) 1 7 7 7 0.00	1.720 III	
$A_2 = 1.90 \times 2.00$	= 3.800 m <sup>2</sup>	
A	= 5.720 m <sup>2</sup>	
$V = 5.720 \times 20.00$	= 114.40	114.40 m <sup>3</sup>
	114.40	114.40 III
☐ BACKFILL WITH SELECTED SOIL		
$A_1 = (0.50 + 0.9) \times 1/2 \times 0.90$	- 0.620 <sup>2</sup>	
$A_1 = (0.30 \pm 0.9) \times 2 \times 0.90$	= 0.630 m <sup>2</sup>	
$A_2 = (0.50 + 2.2) \times \frac{1}{2} \times 2.10$	= 2.835 m <sup>2</sup>	
A	= 3.465 m <sup>2</sup>	
		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
V = 3.465 x 20.00	= 69,300	69.300 m <sup>3</sup>
		02.500 III

TYPE OF WORK : REINFORCEMENT OF EXISTING DIKE LOCATION :

CALCULATION		RESULT
F EMBANKMENT		
FEWBAINENT		
• EMBANKMENT		
		100000000000000000000000000000000000000
$A = (2.50 + 1.00) \times \frac{1}{2} \times 3.00$	= 5.250 m <sup>2</sup>	
V = 5.25 x 20.00	= 105.00	105.00 m <sup>3</sup>
		105.00 III
SOIL SODDING		
$L = 1.202 \times 4.5$	= 1.803 m	
	1.000 III	
$A = 1.803 \times 20.00$	= 36.06	36.06 m <sup>2</sup>
		e di susuale di S
WET STONE MASONRY		
WET STONE MASONRY		
$A = (0.40 + 1.00) \times \frac{1}{2} \times 1.80$	$= 1.260 \text{ m}^3$	STAR FRANK
V = 1.26 x 20.00	= 25,200	25.200 m <sup>3</sup>
1.20 X 20,00	<del>-</del> 23.200	25.200 m
GRAVEL BEDDING		
A = 1.20 x 0.10	0.100	
A = 1.20 X 0.10	= 0.120 m <sup>2</sup>	
$V = 0.12 \times 20.00$	= 2.400	2.400 m <sup>3</sup>
OPMENTS MODELLE POSTEROLO		
CEMENT MORTAR POINTTING		
$A = (1.10 + 0.40) \times 20.00$	= 30.000	30.000 m <sup>2</sup>
		30,000 111

TYPE OF WORK: LOCATION: REVETMENT DRAINAGE SLUICEWAY AT WF.172R + 15 m

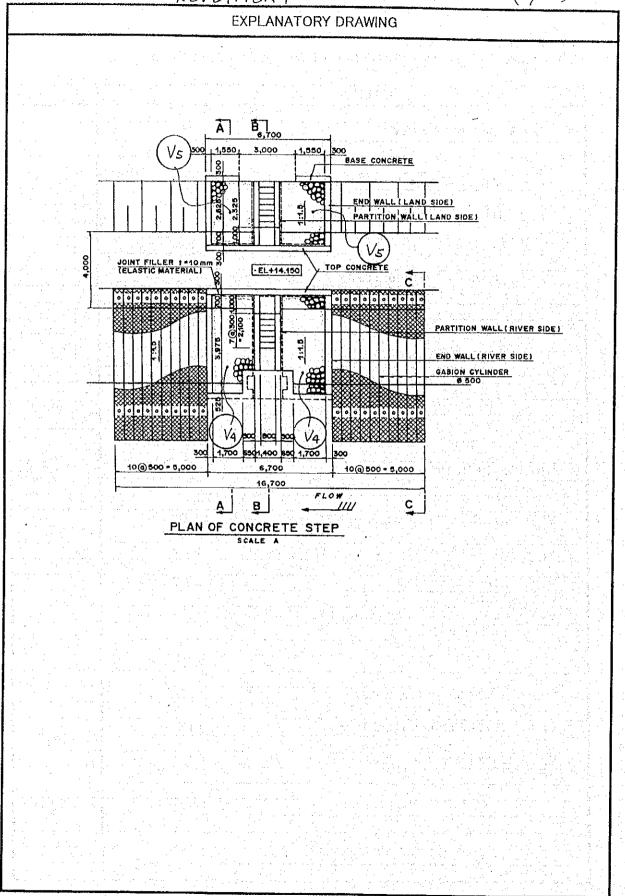
CALCULATION	RESULT
- WITE CEONE M. COMMY	
WET STONE MASONRY	
$V_1 = \{(11.18 + 0.70) \times 0.25 \times 3.70\} \times 2 = 21.978$	
$V_2 = \{(11.18 + 7.379) \times \frac{1}{2} \times 0.25 \times 1.20\} \times 2 = 5.568$	
$V_3 = 7.379 \times 0.25 \times 1.60 = 2.952$	
V. COS A 4 (772.) O (70.) A 20. A 170. A 20. COS A 170.	
$V_4 = \{(0.525 + 4.778 + 0.70) \times 0.30 \times 1.70 + (3.967 + 0.70) \times 0.30 \times 0.65\} \times 2$	
X 0.30 X 0.03 X 2 (Specific Property of the Control	
7.943	
$V_5 = \{(3.155 + 0.70) \times 0.30 \times 2.35\} \times 2 = 5.436$	
	42.077
TOTAL = 43.877	43.877 m <sup>3</sup>
andra de la companya de la companya De la companya de la	
F GRAVEL BEDDING	
$V_1 = \{(11.18 + 0.70) \times 0.25 \times 3.70\} \times 2 = 21.978$	and the second
7/ (411.0.1.7.270) -1/ - 0.05 - 1.00) - 2	
$V_2 = \{(11.18 + 7.379) \times \frac{1}{2} \times 0.25 \times 1.20\} \times 2 = 5.568$	
$V_3 = 7.379 \times 0.25 \times 1.60 = 2.952$	
$V_4 = \{(0.525 + 4.778 + 0.70) \times 0.30 \times 1.70 + (3.967 + 0.70)\}$	
x 0.30 x 0.65} x 2	
1919   1949   19	
$V_5 = (3.967 + 0.70) \times 0.30 \times 0.80 = 1.120$	
V <sub>3</sub> - (3.907 + 0.70) x 0.30 x 0.80 - 1.120	
$V_6 = \{(3.155 + 0.70) \times 0.30 \times 2.35\} \times 2 = 5.436$	
$V_7 = (3.155 + 0.70) \times 0.30 \times 0.80 = 0.925$	
	45.55
TOTAL = 45.922	45.922 m³

DRAINAGE SLUCEWAY AT WF. 172R+ 15M

TYPE OF WORK

WET STONE MASONRY

LOCATION : REVETIMENT (1/2



DRAINAGE SLUICEWAY AT WF. 172R + 15 m

TYPE OF WORK

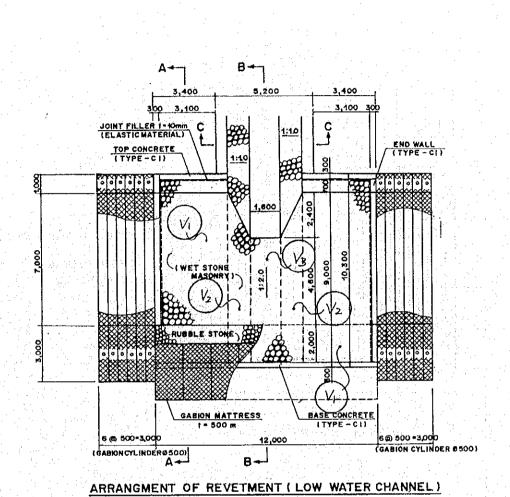
: WET STONE MASONRY

**EXPLANATORY DRAWING** 

LOCATION

REVETMENT

(2/2)



DRAINAGE SLUICEWAY AT WF. 172R + 15 M

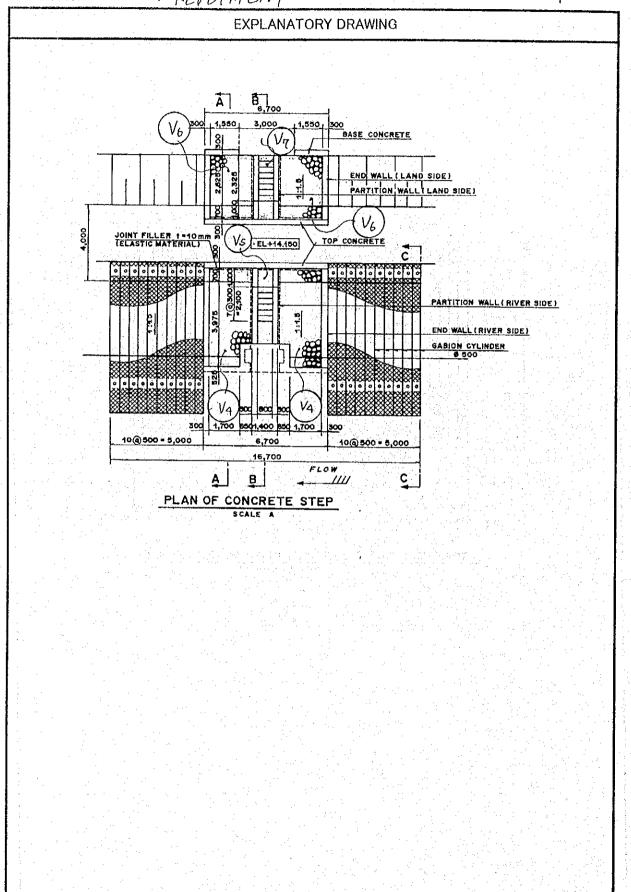
TYPE OF WORK

: GRAVEL BEDDING

LOCATION

: REVETMENT

(1/2)



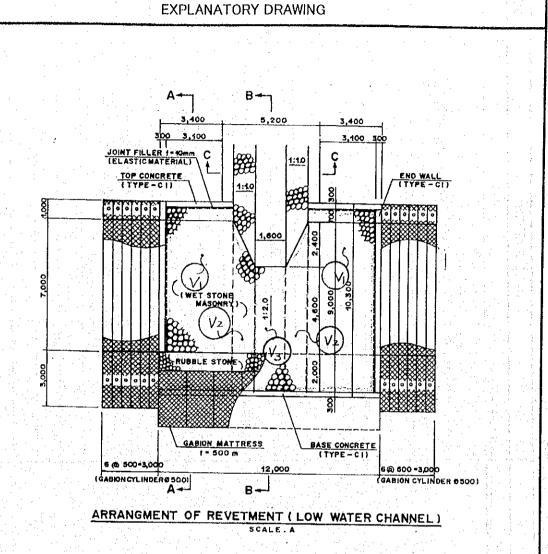
DRAINAGE SLUICEWAY AT WF. 172R + 15M

TYPE OF WORK

GRAVEL BEDDING

LOCATION : REVETMENT

(2/2)



DPAINAGE SUDICEMAY AT UNF 17224-15m   CALCULATION   RESULT	7	RESULT						:									30 g				1	
		RE	,	-													14					
(RIVER SIDE) 9,325 (LAND SIDE)  3,500 4,000 2,625  1,200 7@300-2,000 1,000 2,000 1,000 228 8@300-2,400  STEEL LADDER 700 800 700  CONCRETE TYPE-D) TOP CONCRETE TYPE-C11  VEL+14,150  SECTION B-B		CALCULATION	(TYPE-D)		ü	18 × 18 × 18 × 18 × 18 × 18 × 18 × 18 ×	= 1.61 × 0.80			) =		427		= 1.427 × 0.80			ıı V					
101.11	DRAINAGE SLUICEWAY	CONCRETE (TYPE -	REVETMENT				1,200	3,3	OSON OSON TEEL ONCRE	)-2/10 LADOE	70	DEDO:	TOP OSL	4,000 ,000 concr	150 130	70		2,625 300 =	2,400 OF "C	00,200 - 1,000 00 00 00 00 00 00 00 00 00 00 00 00		

	RESULT											3.063 m2	1.				1				
z + i z m	CALCULATION	(H<4,0m)		A1=020×080 × 7	Az=1/2 x0.03 x 0.80 x 7 = 0.238	A3 = 0.20 × 0.80 × 8 = 1.280		A4 = 0.15 x 0.80 = 0.120		AS = N2 × 0.03 × 0.80 × 9 = 0.305		70741 = 3,063									
DRAINAGE SLUICEWAY AT WF. 192R+115m	TORRESPONDENCE	REVETMENT	02.3	000/1-002(9)/		1,200	3,	RIVER 300 (@ 300 STEEL	LADDI	x0 1	700 V	4,000 2,000 CONC FE-10 EL+11	1.160 1.160		8@	DETAI	2,400 L OF	<u>c"</u>	8 <u>0</u> 800-1,600th0	 **************************************	
	TYPE OF WORK:	LOCATION									5 - 6										

TYPE OF WORK:

LOCATION

REVETMENT DRAINAGE SLUICEWAY AT WF.172R + 15 m

CALCULATION		RESULT
□ TOP CONCRETE		
10r CONCRETE		
CONCRETE (TYPE-C1)		
$V_1 = (4.00 \times 2) \times 1.80 / 10.00 \text{ m}$	= 1.440	
$V_2 = (6.70 \times 2) \times 2.10 / 10.00 \mathrm{m}$	- 2.014	
	= 2.814	e v Telegrapiska i Statiska i Sta Tarista i Statiska i S
TOTAL	= 4.254	4.254 m <sup>3</sup>
GRAVEL BEDDING		
$V_1 = (4.00 \times 2) \times 0.75 / 10.00 \text{ m}$	= 0.600	
$V_2 = (6.70 \times 2) \times 0.800 / 10.00 \text{ m}$	= 1.072	
TOTAL	= 1.672	1.672 m <sup>3</sup>
• FORM (H < 4.0 m)		
$A_1 = (4.00 \times 2) \times 12.18 / 10.00 \text{ m}$	= 9.744	
$A_2 = (6.70 \times 2) \times 14.2 / 10.00 \text{ m}$	= 19.041	
TOTAL	= 28.785	28.785 m²
REINFORCING BAR		
$W_1 = (4.00 \times 2) \times 0.094 / 10.00 \text{ m}$	= 0.075	
$W_2 = (6.70 \times 2) \times 0.098 / 10.00 \text{ m}$	= 0.131	
TOTAL	= 0.206	0.206 tf
JOINT FILTER		
$A_1 = (4.00 \times 2) \times 2.605 / 10.00 \text{ m}$	= 2.084	
$A_2 = (6.70 \times 2) \times 3.120 / 10.00 \text{ m}$	= 4.181	
TOTAL	= 6.265	6.265 m <sup>2</sup>
10174	<del>-</del>	0.203 In
		an