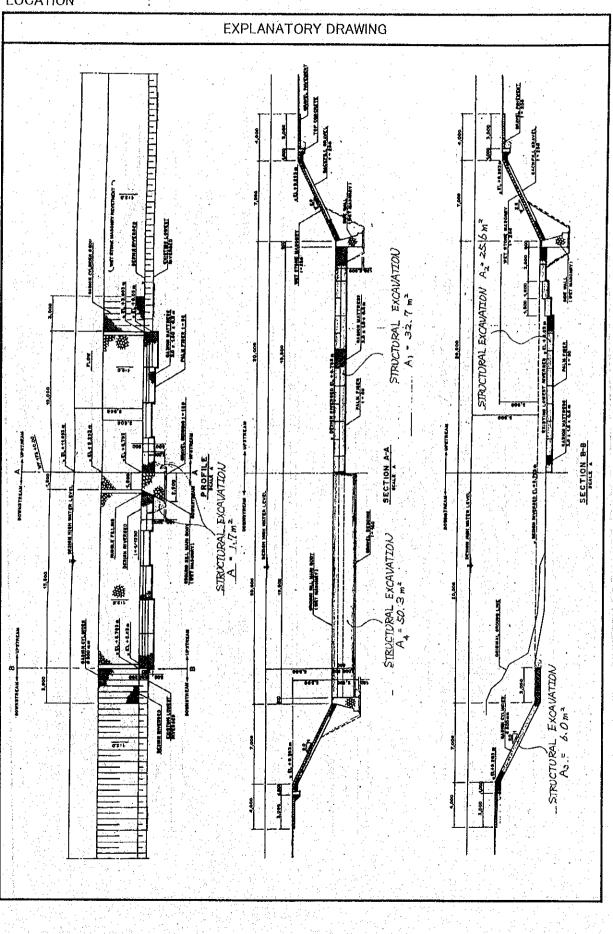
CALCULATION		RESULT
CODVICENTE LE NY CLYLERYON		
STRUCTURAL EXCAVATION		
$V_1 = 32.70 \times (1.50 + 1.50) \times 2$	= 196.20	
	170.20	
$V_2 = 25.6 \times (12.50 + 9.00) \times 2$	= 1100.80	
$V_3 = 6.00 \times (3.00 + 3.00) \times 2$		
<u>13 0.00 X (3.00 + 3.00) X Z</u>	= 72.00	<u> </u>
$V_4 = 50.30 \times 3.50 \times 2$	= 352.10	
TOTAL		
TOTAL	= 1721.10	1721.10 m ⁻
	<u>terre de la composición de la composici</u> Esta de la composición	
		nan san san san san san san san san san
BACKFIIL WITH SELECTED SOIL		
$V_1 = (6.0 + 0.3) \times (1.50 + 1.50) \times 2$	= 37.80	
$V_2 = (7.6 + 0.3) \times (12.50 + 9.00) \times 2$	= 339.70	
$V_3 = 0.7 \times (3.00 + 3.00) \times 2$	= 4.20	
	= 4.20	
$V_4 = (4.9 + 0.3) \times 3.50 \times 2$	= 36.40	
$V_5 = 1.70 \times 39.0$		
<u>()</u>	= 66.30	
TOTAL	= 484.40	484,40 m ³
	<u>,一般</u> 我就算了错过。 11.1.1.4.1.1.4.1	

4.2 Ground Sill without Head at WF. 173 LOCATION : GROUNDSILL WITHOUT HEAD AT WF. 173

GROUND SILL WITHOUT HEAD AT WF. 173 STRUCTURAL EXCAVATION

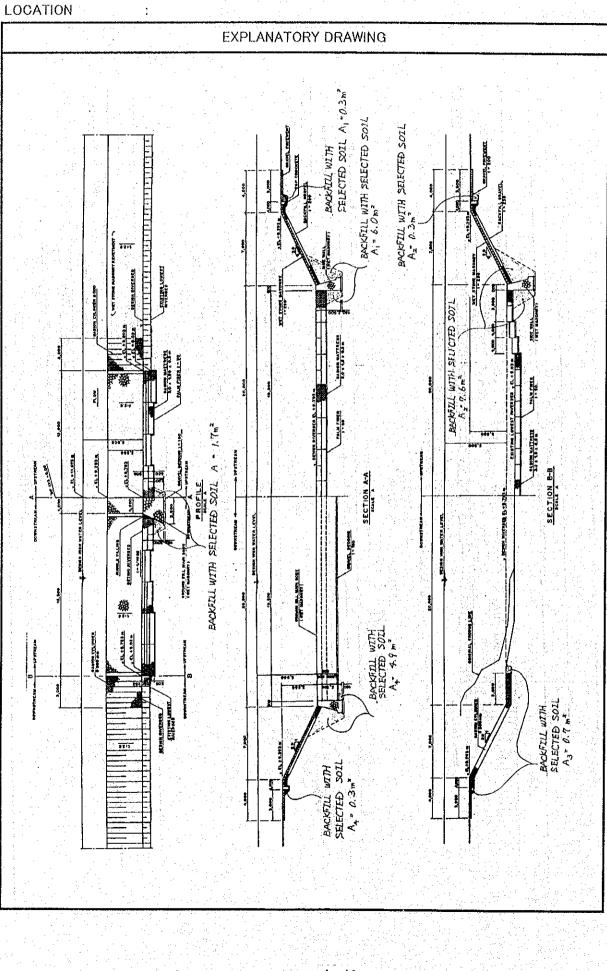
TYPE OF WORK LOCATION

0



GROUND SILL WITHOUT HEAD AT WF. 173 BACKFILL WITH SELECTED SOIL

TYPE OF WORK



TYPE OF WORKMAIN BODY AND SIDEWALLLOCATION:GROUNDSILL WITHOUT HEAD AT WF.173

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	CALCULATION		RESUL
S WE	T STONE MASONRY	a se l'espectator de la case de la La case de la	and the second second
A ₁ =	$= (1.50 + 2.50) \times \frac{1}{2} \times 2.00 =$	4.000 m ²	
V _L =	= 4.00 x 39.00 ==	156.000	
A	$= (0.50 + 1.00) \times \frac{1}{2} \times 2.00 + (0.50 \times 1.20) =$	2.10 m ²	
<u> </u>	$- (0.30 + 1.00) \times \frac{1}{2} \times \frac{2.00}{100} + (0.30 \times 1.20) =$	2.10 m	
V ₂ =	= 2.10 x 29.00 x 2 =	121.800	
<u> </u>			
	$TOTAL (V_1 + V_2) =$	277.800	277.800 r
		n an de la service de la s La service de la service de	
	i de presidente de la francés de la companya de la dependencia de la companya de la companya de la companya de		
	al de la contrata la companya de la construcción de la construcción de la construcción de la construcción de la Construcción de la construcción de	<u>in in service de la tractione de la composition de la comp</u>	
	<u>na serie de la constante de la</u> La constante de la constante de		
	이 가 집 집 것같 것 이 방 것 이 많이 많이 가지 않는 것 같아. 이 가 있는 것 같은 것 같은 것 같은 것 같이 많이	그렇게 사람이 많은 이야지 않는 것이 아파 가지?	 A March 1999 August 199
		i de la francia de la composición de la De la composición de l	
	AVEX DEDDING		
₽ GR 4	AVEL BEDDING		
5 GRA	AVEL BEDDING		
	AVEL BEDDING = 1.50 x (2.50 + 0.15 x 2) =	0.420 m ²	
A ₁ =	= 1.50 x (2.50 + 0.15 x 2) =		
	= 1.50 x (2.50 + 0.15 x 2) =	0.420 m ² = 16.380	
A ₁ =	= 1.50 x (2.50 + 0.15 x 2) = = 0.42 x 39.00	= 16.380	
A ₁ =	= 1.50 x (2.50 + 0.15 x 2) =	= 16.380	
A ₁ = V ₁ = A ₂ =	= 1.50 x (2.50 + 0.15 x 2) = = 0.42 x 39.00	= 16.380	
$A_1 = V_1 = A_2 = V_2 $	$= 1.50 \times (2.50 + 0.15 \times 2) =$ $= 0.42 \times 39.00$ $= 0.15 \times (1.20 + 0.15 \times 2) =$ $= 0.225 \times (29.00 + 0.15 \times 2) \times 2$	= 16.380 0.225 m ² = 13.185	
A ₁ = V ₁ = A ₂ =	$= 1.50 \times (2.50 + 0.15 \times 2) =$ $= 0.42 \times 39.00$ $= 0.15 \times (1.20 + 0.15 \times 2) =$ $= 0.225 \times (29.00 + 0.15 \times 2) \times 2$	= 16.380 0.225 m ² = 13.185	29.565 m
$A_1 = V_1 = A_2 = V_2 $	$= 1.50 \times (2.50 + 0.15 \times 2) =$ $= 0.42 \times 39.00$ $= 0.15 \times (1.20 + 0.15 \times 2) =$ $= 0.225 \times (29.00 + 0.15 \times 2) \times 2$ $= TOTAL (V_1 + V_2) =$	= 16.380 0.225 m ² = 13.185 29.565	
$A_1 = V_1 = A_2 = V_2 $	$= 1.50 \times (2.50 + 0.15 \times 2) =$ $= 0.42 \times 39.00$ $= 0.15 \times (1.20 + 0.15 \times 2) =$ $= 0.225 \times (29.00 + 0.15 \times 2) \times 2$ $TOTAL (V_1 + V_2) =$	= 16.380 0.225 m ² = 13.185	
$A_1 = V_1 = A_2 = V_2 $	$= 1.50 \times (2.50 + 0.15 \times 2) = $ $= 0.42 \times 39.00$ $= 0.15 \times (1.20 + 0.15 \times 2) = $ $= 0.225 \times (29.00 + 0.15 \times 2) \times 2$ $TOTAL (V_1 + V_2) = $	= 16.380 0.225 m ² = 13.185 29.565	29.565 m
$A_1 = V_1 = A_2 = V_2 $	$= 1.50 \times (2.50 + 0.15 \times 2) =$ $= 0.42 \times 39.00$ $= 0.15 \times (1.20 + 0.15 \times 2) =$ $= 0.225 \times (29.00 + 0.15 \times 2) \times 2$ $TOTAL (V_1 + V_2) =$	= 16.380 0.225 m ² = 13.185 29.565	29.565 m
A ₁ = V ₁ = V ₂ =	$= 1.50 \times (2.50 + 0.15 \times 2) =$ $= 0.42 \times 39.00$ $= 0.15 \times (1.20 + 0.15 \times 2) =$ $= 0.225 \times (29.00 + 0.15 \times 2) \times 2$ $TOTAL (V_1 + V_2) =$	= 16.380 0.225 m ² = 13.185 29.565	29.565 m
$A_1 = V_1 = A_2 = V_2 $	$= 1.50 \times (2.50 + 0.15 \times 2) =$ $= 0.42 \times 39.00$ $= 0.15 \times (1.20 + 0.15 \times 2) =$ $= 0.225 \times (29.00 + 0.15 \times 2) \times 2$ $TOTAL (V_1 + V_2) =$	= 16.380 0.225 m ² = 13.185 29.565	29.565 m
A ₁ = V ₁ = V ₂ =	$= 1.50 \times (2.50 + 0.15 \times 2) =$ $= 0.42 \times 39.00$ $= 0.15 \times (1.20 + 0.15 \times 2) =$ $= 0.225 \times (29.00 + 0.15 \times 2) \times 2$ $TOTAL (V_1 + V_2) =$	= 16.380 0.225 m ² = 13.185 29.565	29.565 m
$A_{1} = V_{1} = V_{2} = V_{2$	$= 1.50 \times (2.50 + 0.15 \times 2) =$ $= 0.42 \times 39.00$ $= 0.15 \times (1.20 + 0.15 \times 2) =$ $= 0.225 \times (29.00 + 0.15 \times 2) \times 2$ $TOTAL (V_1 + V_2) =$	= 16.380 0.225 m ² = 13.185 29.565	29.565 m

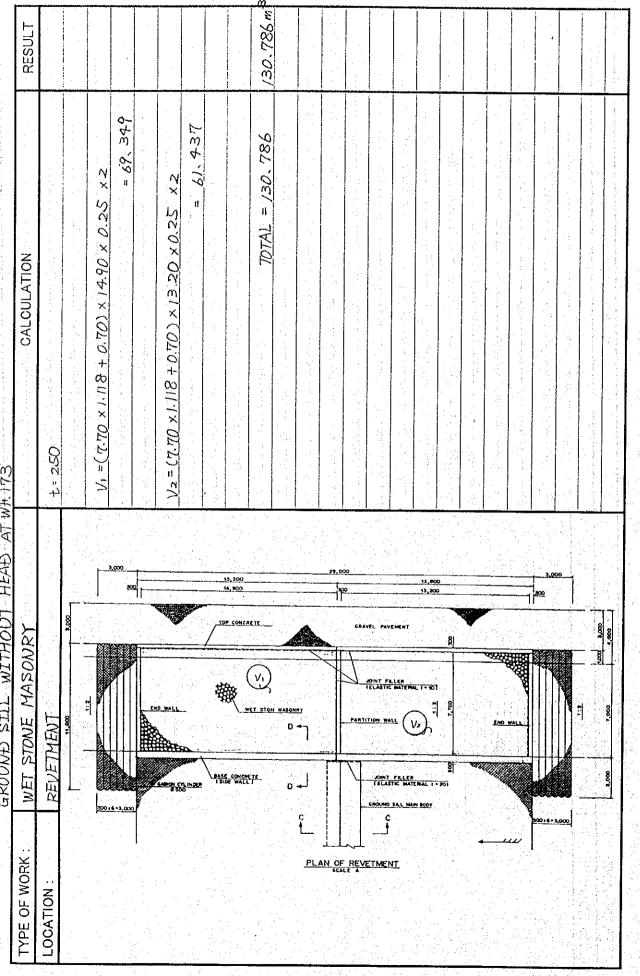
TYPE OF WORK : LOCATION :

MAIN BODY GROUNDSILL WITHOUT HEAD AT WF.173

CALCULATION		RESULT
5 RUBBLE STONE FILLING		e Aller an an
n an de la companya de la companya En esta de la companya		
$V = \frac{1}{2} \times 1.00 \times 0.50 \times 39.00 = 0$	9.750	9.750 m ³
	alenter e le terre i l'ester	a state for the second
	egi (h. 1997), de en de la Constante Recentration de la Constante	
<u>na na 1999 na manga kabupatén ng kabupatén ng kabupatén ng kabupatén ng kabupatén ng kabupatén ng kabupatén ng</u> Kabupatén di kabupatén kabupatén ng kabupatén kabupatén kabupatén ng Kabupatén ng kabupatén ng kabupatén ng kab		
JOINT FILTER		
t = 10, ELASTIC MATERIAL		
t = 10, ELASTIC MATERIAL		
$A_1 = (1.50 + 2.50) \times \frac{1}{2} \times 2.00 \times 3 =$	12.000	
$A_2 = \{(0.50 + 1.00) \times \frac{1}{2} \times 2.00 + (0.50 \times 1.20) \times 2 =$	4.200	
<u>en andre en en dia anna da chara anna anna anna anna anna anna anna </u>		
TOTAL =	16.200	16.200 m ²
	10.000	
	<u>et de la sette de la seco</u> ndada de la secondada da secondada da secondada da secondada da secondada da secondada En esta de la secondada da second	
日 GABION MATRESS		
t = 500		
$V_1 = 40.00 \times 6.00 \times 0.50 =$	120.000	
<u> </u>	120.000	
$V_2 = 40.00 \times 3.00 \times 0.50 \times 2$ =	120.000	
an a		
	120.000	
	240.000	
$V_4 = 40.00 \times 3.00 \times 1.00 \times 2$ =	240.000	a sharar ay a Tana ay ay ay ay ay ay
$V_5 = 40.00 \times 3.00 \times 0.50 =$	60.000	
TOTAL =	660.000	660.000 m ³
	and a second	

		<u> </u>				·					
r	T	 	 N	·····		: :	· · · · · · · · · · · · · · · · · · ·			· .	 q
RESULT			11 79, 760 m 2								
<i>wħ.\rS</i> calculation	AI = 40.00 × (15.50+0.247+0.25+0.26+0.25)	H2 = 70.00 × (12.00) + 0.24 (+ 0.25 + 0.25 + 0.25) = 5.19.480	707AL = 1179.760								
GROUND STIL WITHOUT HEAD AT GROUND STIL WITHOUT HEAD AT YPE OF WORK: DALM FIBER FILTER		UP374EAM		DC310N HIEH WARK C F L (HH HI RIVEASCO 1-1/1250			EL + 11,693 m EL + 1		· · · ·		
	LOCATION			4 - 4	4						

GROUND SILL WITHOUT HEAD AT WF 173



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TYPE OF WORK : LOCATION :

REVETMENT GROUNDSILL WITHOUT HEAD AT WF.173

	CALCULATION		RESUL
GRAV	/EL BEDDING	anton en transverse segué Antonio de la composición de la composición de la composición de la composición de la	
a si statu			
1. sat.	<u>an an a</u>		
.t ≕	250		ala da esta esta esta esta esta esta esta est
	$\frac{(7.70 \times 1.118 + 0.70) \times 14.90 \times 0.25 \times 2}{(7.70 \times 1.118 + 0.70) \times 13.20 \times 0.25 \times 2} =$	69.349	
V ₂ =	$(7.70 \times 1.118 + 0.70) \times 13.20 \times 0.25 \times 2 =$	61.437	
	TOTAL =	130.786	130.786
	IOIAL -	130.700	150.780
<u> </u>			
<u>at 11 is</u>	ter han te galage ter dit tela disa di ter angli area sa sa juli juli. Ng Angli Angli Angli ang ang ter pangan ang ang ang ang ter pangang ang	<u>, e ser en el la ser en el la ser el la s</u>	
<u>to se etido se</u> Tori ta stati	<u>에 가 있었다. 사람이 있는 것 같은 것은 것은 것은 것은 것은 것은 것이 있다. 것은 </u>	<u>in an an an teor</u> in. Talain an Antairte an teor	
	ani ang	·····	
na shekara			
in an			
es et gibblede			
		ta ay hata gara dalah s	
		이 관련을 보면 물건을 물건을	
			· · · · · · · · · · · · · · · · · · ·
СЕМЈ	ENT MORTAR POINTTING		
CEMI	ENT MORTAR POINTTING		
		262.015	
CEMI <u>A</u> ₁ =	ENT MORTAR POINTTING (7.826 + 1.00) x 14.90 x 2 =	263.015	
A ₁ =	(7.826 + 1.00) x 14.90 x 2 =		
	(7.826 + 1.00) x 14.90 x 2 =	263.015 233.006	
A ₁ =	(7.826 + 1.00) x 14.90 x 2 =		
A ₁ =	(7.826 + 1.00) x 14.90 x 2 =		496.021 r
A ₁ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 =	233.006	496.021 r
A ₁ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 =	233.006	496.021 r
A ₁ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 = TOTAL =	233.006 496.021	
A ₁ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 = TOTAL =	233.006 496.021	
A ₁ = A ₂ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 = TOTAL =	233.006 496.021	
A ₁ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 = TOTAL =	233.006 496.021	
A ₁ = A ₂ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 = TOTAL =	233.006 496.021	
A ₁ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 = TOTAL =	233.006 496.021	
A ₁ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 = TOTAL =	233.006 496.021	
A ₁ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 = TOTAL =	233.006 496.021	
A ₁ = A ₂ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 = TOTAL =	233.006 496.021	
A ₁ = A ₂ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 = TOTAL =	233.006 496.021	
A ₁ = A ₂ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 = TOTAL =	233.006 496.021	
A ₁ = A ₂ =	(7.826 + 1.00) x 14.90 x 2 = (7.826 + 1.00) x 13.20 x 2 = TOTAL =	233.006 496.021	

TYPE OF WORK:REVETMENTLOCATION:GROUNDSILL WITHOUT HEAD AT WF.173

CALCULATION		RESULT
5 TOP CONCRETE		
t = 29.00 m/side		
CONCRETE (TYPE – C1)	<u>e legiero sigoras</u> El la concerción	
$V = 29.00 \times 2 \times 1.80 / 10.00 m =$	10.440	10.440 m ³
GRAVEL BEDDING	<u>an an a</u>	
$V = 29.00 \times 2 \times 0.75 / 10.00 m =$	4.350	4.350 m ³
	4.330	4.330 m
• FORM (H < 4.0 m)		
V = 29.00 x 2 12.18 / 10.00 m =	70.644	70.644 m ²
REINFORCING BAR		
$W = 29.00 \times 2 \times 0.094 / 10.00 =$		
$W = 29.00 \times 2 \times 0.094 / 10.00 =$	0.545	0.545 tf
JOINT FILTER		
$A = 29.00 \times 2 \times 2.605 / 10.00 =$	15,109	15.109 m ²
an an an an an Anna an Anna an Anna an		i i sena de la composición de la compos
F GABION CYLINDER		
GABION CYLINDER (Ø 500)		
$L = 3.00 + 7.00 \times 1.118 + 1.00 =$	11.826	
$V = \pi / 4 \times 0.50^2 \times 11.826 \times 6 \times 2 \times 2 =$	55.729	55.729 m ²
SOIL FILLING		
$V = (11.826 \times 0.50 \times 3.00) \times 2 \times 2 - 55.729 =$	15.227	15.227 m ³

TYPE OF WORK :END WALL (REVETHENT)LOCATION :GROUNDSILL WITHOUT HEAD AT WF.173

	CALCULATION		RESULT
a an an Array			
GRA GRA	VEL BEDDING		
			a the second of the
<u> </u>		0.000	
A =	$(0.10 + 0.30) \times \frac{1}{2} \times 0.20 + (0.40 \times 0.10) =$	= 0.080 m ²	
V =	0.080 x (7.818 + 0.558) x 2 x 2 =	= 2.680	2.680 m ³
			2.000 m
E CON	CRETE (TYPE - C1)		
			and the second
(ТҮРІ	$\mathbf{E} = \mathbf{C} \mathbf{I}$		
<u></u>			
A =	$(7.826 + 7.818) \times \frac{1}{2} \times 0.60 + (0.70 + 0.558) \times \frac{1}{2}$	$= 5.071 \text{ m}^2$	
i de alterations de Transformations	n an the contract of the second s The second sec	- 3.0 /1 m	
<u>v</u> =	5.071 x 0.30 x 2 x 2	• 6.058	6.058 m ³
	<u>n ne filozofi za za zakone na zakone zako Elegen interezen elementea zakone z</u>		
		e el cato de la constance de la	
			tra e se se se se
5 FOR	M (H < 4.0 m)		
(H < 4			
(<u>n < 4</u>	. .	an <u>i ang sing ang kang ang sing ang sing</u> Ng sagang ang ang ang sing sing sing sing sing sing sing si	
A =	$\{(7.826+7.818) \times \frac{1}{2} \times 0.60 + (0.70+0.588) \times (0.70+0.588)$	¹ / ₂ x 0.60}	
	x 2 x 2 x 2	·····	
		40.565	
		40.303	40.565 m ²
		40.303	40.565 m ²
		40.303	40.565 m ²
			40.565 m ²

TYPE OF WORK	:	END WALL (REVETMENT)
LOCATION	:	GROUNDSILL WITHOUT HEAD AT WF.173

	RESULT
F REINFORCING BAR	
en en kontra de la constructiva de En entre de la constructiva de la c	
• D13 $(W = 1.04 \text{ kgf/m})$	
n = 6 Bars	
$L = (7.826 + 0.70) - 0.05 \times 2 = 8.426 \text{ m/Bar}$	and a second
$W_1 = 6 \text{ Bars x } 8.426 \text{ x } 1.04 \text{ x } 2 \text{ X } 2 = 210.313$	
<u>ne al l'al de la seconda en en el la seconda de la sec Recentra el la seconda de la</u>	
• D 10 (W = 0.617 kgf/m)	
$n = (8.426: 0.30) + 1 = 29.09 \cong 30 Bars$	
$L = (0.20 \times 2 + 0.50 \times 2 + 15 \times 0.01) = 1.550 \text{ m/Bar}$	
$W_2 = 30 \text{ Bars x } 1.55 \text{ x } 0.617 \text{ x } 2 \text{ x } 2 = 114.762$	
e en la forma la companya de la comp En la companya de la c	
TOTAL $(W_1 + W_2) = 325.075 \text{ kgf}$	0.325 tf
en e	n an Allin an Allin A Roman an Allin
영상 등 유명상 등 사람이다. 이는 전체가 있는 것은 가지 않는 것이다. 이는 것은 것은 것이다. 이는 것은 것은 것이다. 이는 것은 것이다. 이는 것은 것은 것이다. 이는 것이다. 유명상 등 사람이 있는 것이다. 것은 것이다. 이는 것이 같은 것이다. 이는 것이 같은 것이다. 이는 것이다. 것이 같은 것이다. 이는 것이 같은 것이 같은 것이다. 같은 것이 같은 것	
더 JOINT FILTER	
t = 10, ELASTIC MATERIAL	
$A = (7.826 + 0.70) \times 0.25 \times 2 \times 2 = 8.526$	8.526 m ²
가 있었다. 이 사람은 가슴에 가지 않는 것 같은 것은 것은 것은 것을 하는 것이 있는 것이 있다. 이 가지 않는 것은 것은 것은 것은 것은 것은 것을 하는 것을 하는 것을 가지 않는 것을 하는 것 같은 것은	
en e	

4 - 49

TYPE OF WORK:PARTITION WALL (REVETMENT)LOCATION:GROUNDSILL WITHOUT HEAD AT WF.173

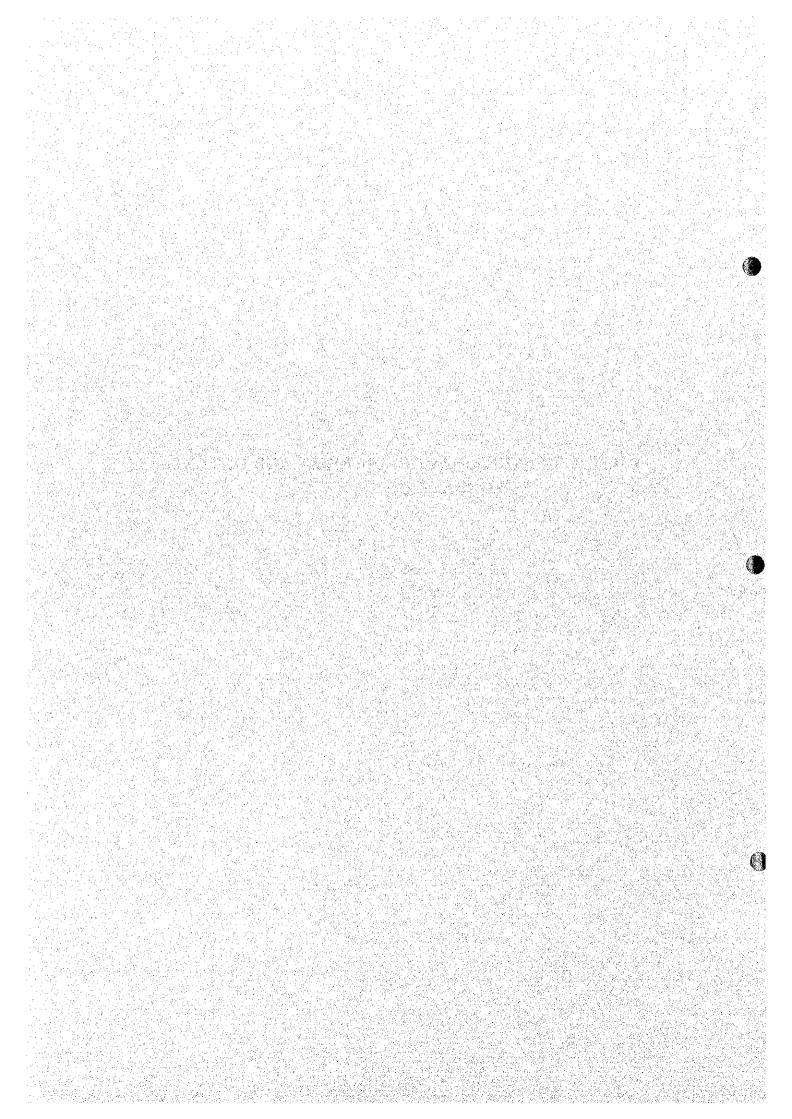
CALCULATION	RESULT
	and share a k
E CONCRETE (TYPE-C1)	
(TYPE – C1)	
$A = \{(7.826 + 7.819) \times \frac{1}{2} \times 0.50 + (0.70 + 0.582) \times \frac{1}{2} \times 0.50\} = 4.232 \text{ m}^2$	
$V = 4.232 \times 0.30 \times 2 = 2.539$	2.539 m ³
	2.339 III
n de la completa de la construcción de la construcción de la construcción de la construcción de la construcción La decisión de la construcción de la construcción de la construcción de la seguina de la construcción de la cons	
· 가슴 나는 가슴 수가 있었는 것 같은 것 같이 있는 것이 있는 것 같은 것 같은 것 같은 것 같은 것 같이 있는 것이 있는 것 같이 있는 것 같이 있는 것 같이 있는 것이 있는 것이 있는 것이 있 같이 같이 있는 것 같이 있는 것 같이 있는 것이 있는 것이 있는 것 같이 있는 것 같이 있는 것 같이 있는 것 같이 있는 것이 없는 것이 있는 것이 있는 것이 있는 것이 있는 것이 있는 것이 있는 것	en de la constante de la const Constante de la constante de la c
5 FORM (H < 4.0 m)	
(H < 4.0 m)	
$A = \{(7.826 + 7.819) \times \frac{1}{2} \times 0.50 + (0.70 + 0.582) \times \frac{1}{2} \times 0.50\} \times 2 \times 2$	
= 16.927	16.927 m ²
	16.927 m ²
= 16.927	16.927 m ²
= 16.927	16.927 m ²
= 16.927	16.927 m ²
= 16.927 F GRAVEL BEDDING	16.927 m ²
= 16.927	16.927 m ²
$= 16.927$ $= 16.927$ $= GRAVEL BEDDING$ $A = (0.50 + 0.70) \times \frac{1}{2} \times 0.10 = 0.060 \text{ m}^2$	
$= 16.927$ $= 16.927$ $= GRAVEL BEDDING$ $A = (0.50 + 0.70) \times \frac{1}{2} \times 0.10 = 0.060 \text{ m}^2$	16.927 m ²
$= 16.927$ $= 16.927$ $= GRAVEL BEDDING$ $A = (0.50 + 0.70) \times \frac{1}{2} \times 0.10 = 0.060 \text{ m}^2$	
$= 16.927$ $= 16.927$ $= GRAVEL BEDDING$ $A = (0.50 + 0.70) \times \frac{1}{2} \times 0.10 = 0.060 \text{ m}^2$	1.008 m ³
$= 16.927$ $= 16.927$ $= GRAVEL BEDDING$ $A = (0.50 + 0.70) \times \frac{1}{2} \times 0.10 = 0.060 \text{ m}^2$ $V = 0.06 \times (7.819 + 0.582) \times 2 = 1.008$	1.008 m ³
$= 16.927$ $= 16.927$ $= GRAVEL BEDDING$ $A = (0.50 + 0.70) \times \frac{1}{2} \times 0.10 = 0.060 \text{ m}^2$ $V = 0.06 \times (7.819 + 0.582) \times 2 = 1.008$	1.008 m ³
$= 16.927$ $= 16.927$ $= GRAVEL BEDDING$ $A = (0.50 + 0.70) \times \frac{1}{2} \times 0.10 = 0.060 \text{ m}^2$ $V = 0.06 \times (7.819 + 0.582) \times 2 = 1.008$	1.008 m ³
$= 16.927$ $= 16.927$ $= GRAVEL BEDDING$ $A = (0.50 + 0.70) \times \frac{1}{2} \times 0.10 = 0.060 \text{ m}^2$ $V = 0.06 \times (7.819 + 0.582) \times 2 = 1.008$	1.008 m ³
$= 16.927$ $= 16.927$ $= GRAVEL BEDDING$ $A = (0.50 + 0.70) \times \frac{1}{2} \times 0.10 = 0.060 \text{ m}^2$ $V = 0.06 \times (7.819 + 0.582) \times 2 = 1.008$	1.008 m ³

3

TYPE OF WORK:PARTITION WALL (REVETMENT)LOCATION:GROUNDSILL WITHOUT HEAD AT WF.173

CALCULATION		RESULT
REINFORCING	· · · · · · · · · · · · · · · · · · ·	
• D13 $(W = 1.04 \text{ kgf/m})$		
n = 6 Bars		
$L = (7.826 + 0.70) - 0.05 \times 2 =$	8.426 m / Bar	
W		
$W_1 = 6 Bars \times 8.426 \times 1.04 \times 2 =$	105.156	
• D 10 $(W = 0.617 \text{ kgf}/\text{m})$		
$n = (8.426 : 0.30) + 1 = 29.09 \simeq$	30 Bars	
$L = (0.20 \times 2 + 0.40 \times 2 + 15 \times 0.01) =$		
$W_2 = 30 \text{ Bars x } 1.35 \times 0.617 \text{ x } 2 =$	49.977	<u> </u>
	49.977	
$TOTAL (W_1 + W_2) =$	155.133 kgf	0.155 tf
		· · · · · · · · · · · · · · · · · · ·
JOINT FILTER		
t = 10, ELASTIC MATERIAL		n de statuer a be The statue
$A = (7.826 + 0.70) \times 0.25 \times 2 =$	4.263	4.263 m ²
		and and an and a second se
	n an	
		· · · ·

CHAPTER 5 DRAINAGE SLUICEWAY AND OUTLET WORKS



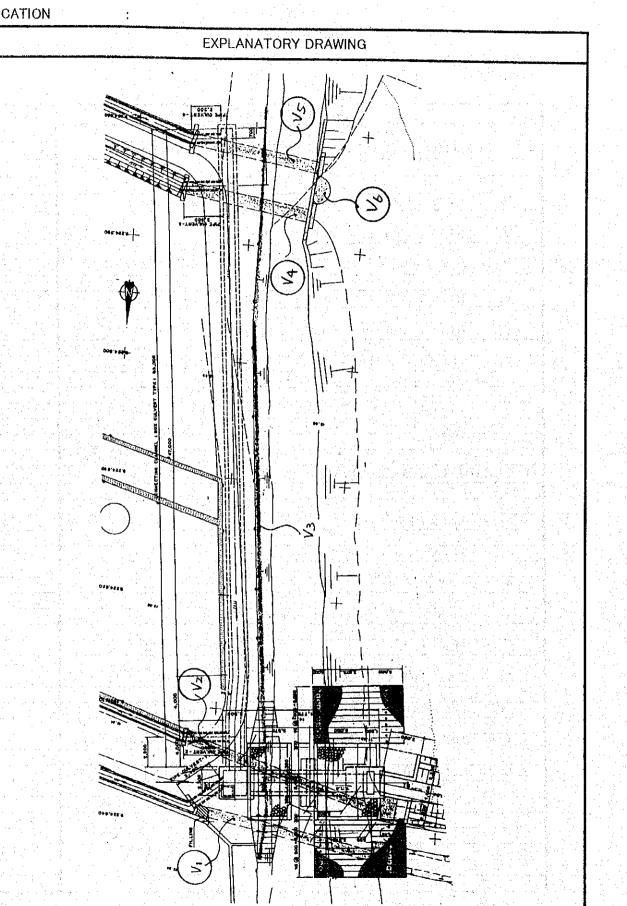
a stars	CALCULATION	RESULT
8 D)	EMOLITION AND REMOVAL OF EXISTING STRUCTURE	
<u>.</u>		
V ₁	$= \{(1.70 \times 1.80) - (1.10 \times 1.10)\} \times 17.50 = 32.375$	
V ₂	$= \{(1.50 \times 1.40) - (0.90 \times 0.70)\} \times 19.50 = 28.665$	
· V3	$= (1.00 \times 0.50) \times 65.00 = 32.500$	
<u>V</u> ₃	$= \{(1.50 \times 1.50) - (0.90 \times 0.80)\} \times 11.50 = 17.595$	
V4	$= \{(1.70 \times 1.50) - (0.90 \times 1.00)\} \times 12.00 = 19.800$	
× /		
۷5	$= 2.00 \times 1.00 \times 11.00 = 22.000$	
	TOTAL = 152.938	153.0 m ³
	이 같은 것은 것 같아요. 이 가지 않는 것 같아요. 가지 않는 것 같아요. 이 가지 않는 것 같아요. 가지 않는 것을 하는 것이 가지 않는 것 같아요. 가지 않는 것 같아요. 이 가지 않는 것 같 같이 하는 것 같아요. 이 같아요. 이 같아요. 아프로	
¹ C	LEARING AND GRUBBING	
A	$= 5.20 \times (18.70 + 3.00) = 112.840$	
A	= 3.00 x 16.70 $=$ 50.100	
<u>A</u> 2	$= 3.00 \times 16.70 = 50.100$	
A	= 4.778 x 16.70 = 79.793	
Δ.	$= (16.70 \times 1.00) + (16.70 + 14.20) \times \frac{1}{2} \times 3.70 = 73.865$	
- 114		
As	$= 14.20 \times 3.155 = 44.801$	
A	$= (5.00 + 3.00) \times \frac{1}{2} \times 5.00 = 20.000$	
6		
A ₇	$= 1.27 \times 4.00 = 5.080$	
A	= 2.00 x 55.00 = 110.00	
A	= 1.27 x 3.50 $=$ 4.445	
A	$a_0 = 1.27 \text{ x } 2.50$ = 3.175	
<u></u>	T O T A L = 504.099	504 0 m²
		504.0 m ²

5.) Drainage Sluiceway at WF. 172R + 15m TYPE OF WORK : DRAINAGE SLUICEWAY AT WF. 172R + 15m LOCATION :

PRAINAGE SLUICEWAY AT WF. 172R+15M : DEDOLITION AND REMOVAL OF EXISTING STRUCTURES

LOCATION

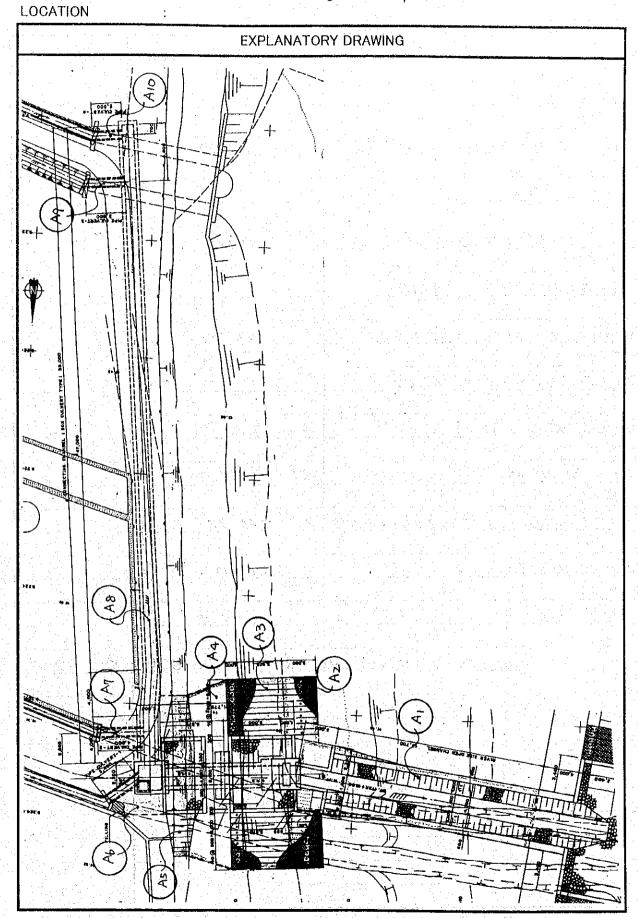
TYPE OF WORK



DRAINAGE SLUICEWAY AT WF. 172R + 15M : CLEARING AND GRUBBING

TYPE OF WORK

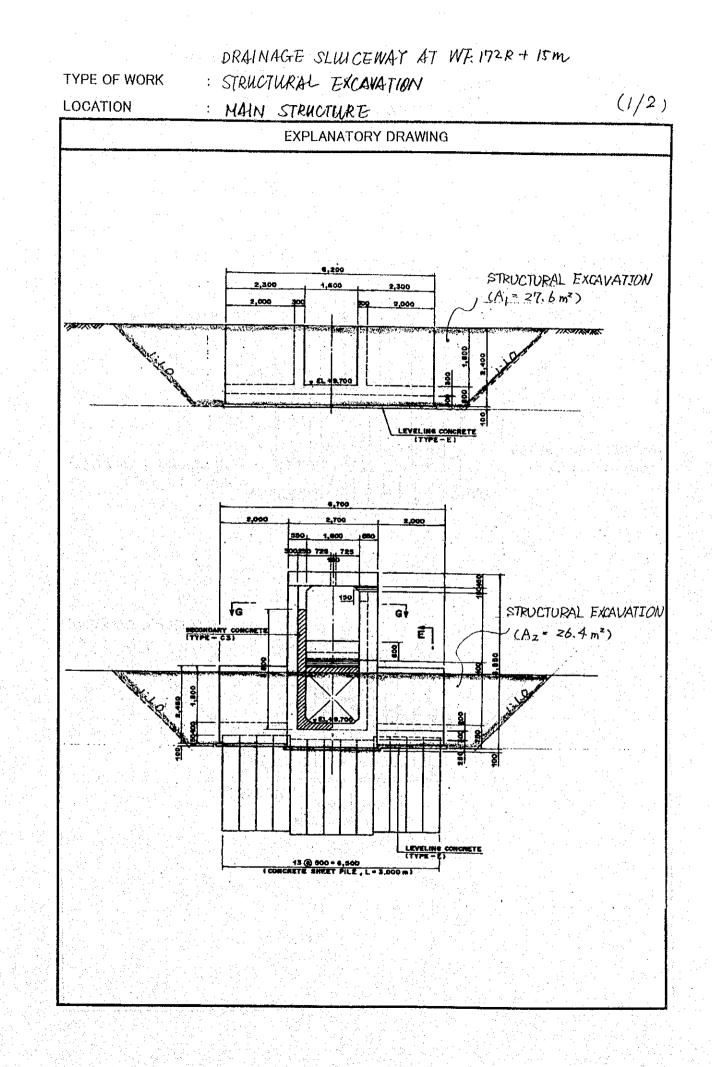
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DRAINAGE SLUICEWAY AT WH. 172R+15m STRUCTURAL EXCAVATION

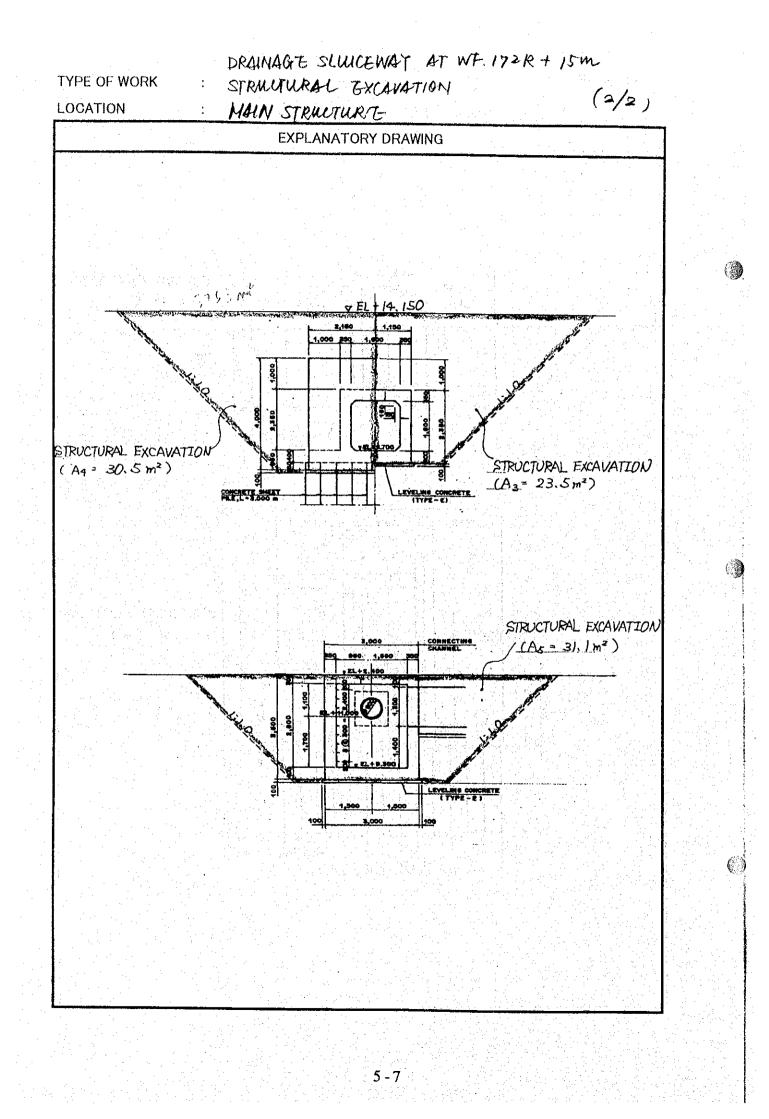
TYPE OF WORK

CALCULATION	RESULT
$A_1 = 27.60 \mathrm{m}^2$	
$V_1 = 27.60 \times (2.341 + 3.659) \times \frac{1}{2} = 82.80$	
$A_2 = 26.40 \text{ m}^2$	
$V_2 = 26.40 \times (0.50 + 1.00) = 39.60$	
$A_3 = 23.50 \text{ m}^2 \times 2 = 47.00$	
$V_3 = (47.00 + 61.00) \times / 2 \times 4.20 = 226.80$	
$A_4 = 30.50 \text{ m}^2 \times 2 = 61.00$	<u>n dia ana kaominina dia</u> Trans dia mandritra dia mampina dia mampi
$1_4 = 61.00 \times 1.30 = 79.30$	
$/4 = 6/.00 \times 1.30 = 79.30$	
$A_{\rm S} = 31.10 \ {\rm m}^2$	ne an ann an Anna an Anna an Anna Anna Anna
$\sqrt{5} = (23, 50 + 3).10) \times 2 \times \frac{1}{2} \times 4.775 = 260.72$	
16 = 31.10 × 3.00 × 2 = 9186.60	
<u>그는 것 같은 것은 것 같은 것은 것이 있는 것이 같은 것은 것이 있는 것이 있다. 것은 것은 것은 것은 것은 것이 없다. 것이 있는 것은 것은 것이 없다. 것이 있는 것은 것이 있다. 것이 있는 것이 있다. 것이 있는 것이 있는 것이 있다. 것이 있는 것이 있는 것이 있는 것이 있는 것이 있다. 것이 있는 것이 있는 것이 있는 것이 있는 것이 있는 것이 있다. 것이 있는 것이 없는 것이 있는 것이 없는 것이 있는 것이 없는 것이 있는 것이 없는 것이 없는 것이 없는 것이 없는 것이 없는 것이 있 같이 있는 것이 없는 것이 있 않는 것이 없는 것이 있 것이 있는 것이 없는 것이 있 것이 없는 것이 있 않는 것이 없는 것이 없 않이 않이 않은 것이 없는 것이 있 것이 않아, 것이 않아, 것이 않아, 것이 않아, 것이 않아, 것이 않아, 것이 없는 것이 없는 것이 없는 것이 없는 것이 없다. 것이 없는 것이 없는 것이 없는 것이 없이 않아, 않아, 것이 않이 않 않아, 않아, 것이 없는 것이 없이 않아, 않아, 않아, 않아, 않아, 않아, 않아, 않아, 않아, 않이 않이 않이 않아, 것이 없 않이 </u>	
$70TAL(V_1+V_2+V_3+V_4+V_5+V_6) = 875.83$	2 875.82 m
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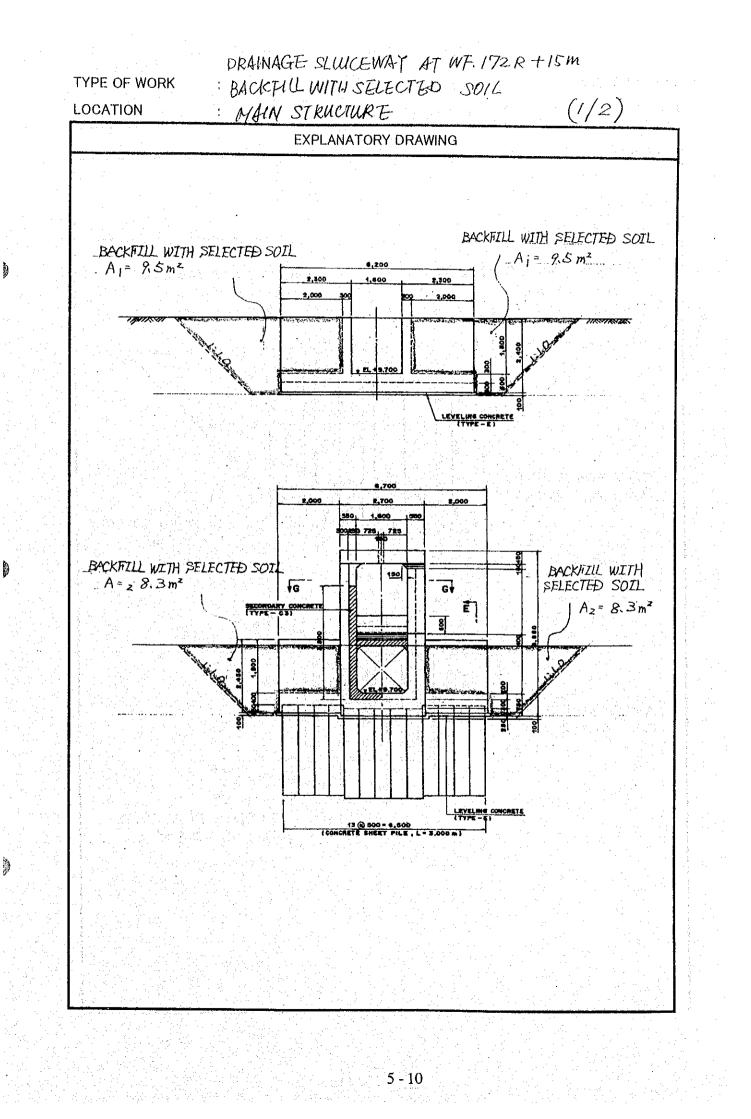
i) V

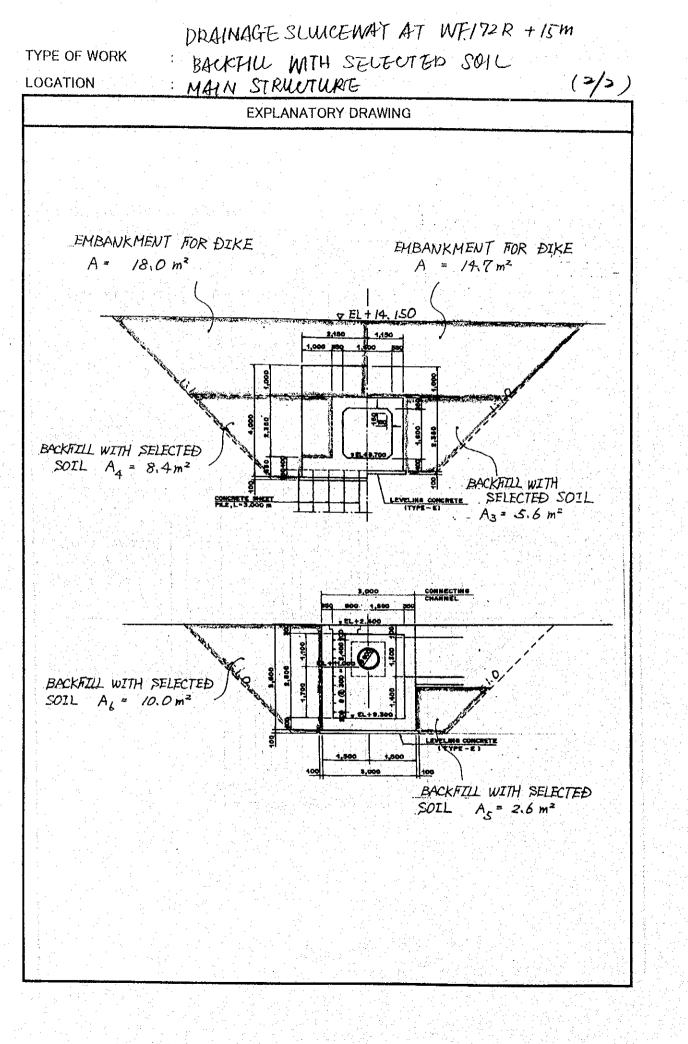
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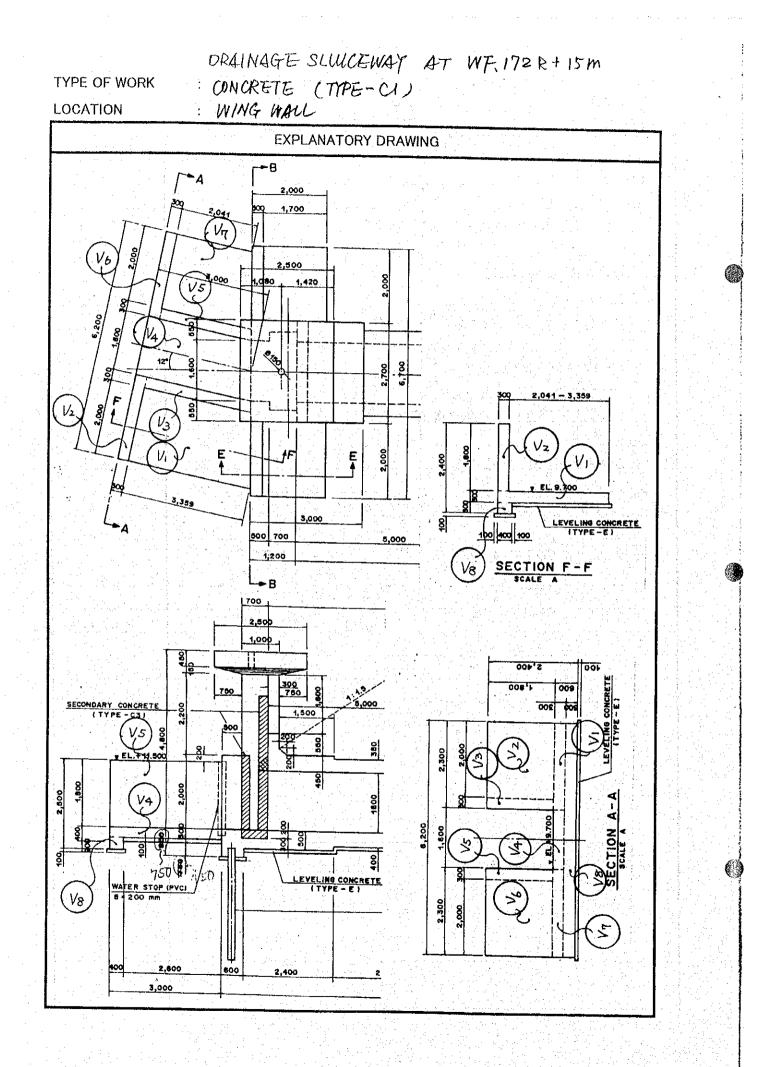
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- 	RESULT								 -			-				-		130.86 m				
<i>wh</i> : <i>1</i> 12 <i>R</i> + <i>1</i> 5 <i>m</i>	CALCULATION		VI = 1/3 × 14.70 × 2 × 3.75 = 36.75		1/2 = 14.70 × 2 × 1.30 = 38.22	13 - 18.00 × 2 × 1.30 = 46.80		14 = 14.70 × 2 × 1,40 = -41.16	Vs = 1/3 × 14.70 × 2 × 3.75 = 36.75		(Beduction for Revetment)		$U_6 = -(3, 4b6 + 2, 493) \times 6.70 = -39, 93$	(Peduction for Gabion Cylinder)	Vy = - (4,778 + 1,00) × 0.50 × 3.00×2 = -28.89			1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1				
DRAINAGE SLUICEWAY AT WHIT			Beck Sc	С. С. С. С. С. С. С. С. С. С. С. С. С. С	A_*.	18, (SE	2 m	(EĐ		100							14.7	m² XII SFLI		1TH Đ	SOI	
												5 - 8	,									

CALCULATION	RESULT
$A_1 = 9.50 \text{m}^2$	
<u>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</u>	
$V_1 = 9.50 \times 2 \times (2.34) + 3.659) \times \frac{1}{2}$	
<u> </u>	= 57.00
$A_2 = 8.30 \text{m}^2$	 <u>Andreas Constructions and Andreas Constructions</u> <u>Andreas Constructions</u> <u>Andreas Constructions</u> <u>Andreas Constructions</u> <u>Andreas Constructions</u> <u>Andreas Constructions</u> <u>Andreas Constructions</u>
Vz = 8.30×2 × (0.50+1.00)	= 74.00
$A_3 = 5.60 \text{ m}^2 \times 2 = 11.20$	
V3 = (11.20 + 16.80) × 1/2 × 4.20	= 58.80
$A_4 = 8.40 \text{ m}^2 \times 2 = 16.80$	
$J_4 = 16.80 \times 1.30$	= 21.84
$A_5 = 2.60 \text{ m}^2$	
$Vs = z.60 \times 3.00$	= 7.80
$A_6 = 10.0 \text{m}^2$	
<u>16 - 70.0 m</u>	
Vb = (11.20 + 20.00) × 1/2 × 4.775	= 74,49
	= 74.49
$l_{7} = 10.00 \times (3.00 + 3.00)$	= 40.00
$TOTAL(V_1+V_2+V_3+V_4+V_5+V_4)$	$b + V_7) = 304.83$ 304.83 m ³
	· · · · · · · · · · · · · · · · · · ·





DRAINAGE SLUI TYPE OF WORK : CONCRETE CTYP LOCATION : WING WALL	ICEWAY AT WF. 172R + 15m PE - CI)	
CALCULA	ATION RESU	 T
(TYPE-CI)		
VI = (3,659 + 3.170) × 1/2 × 2.30 ×	0.30 = z.356	
V2 = 1.80 × 0.30 × 2.30	= 1.242	
V3= (2.87 + 2.934) × 1/2 × 0.30 ×	1.80 = 1.567	• •
in a state of the second s		
$V_4 = (3.17 + 2.83) \times \frac{1}{2} \times 1.60 \times 0$	<u>0.30 = 1.440</u>	
V5 = (2.53 + 2.466) × 1/2 × 0.30		
<u>vs (2.33) 2.700) x /2 x ().30</u>	×1.80 = 1.349	
V6 = 1.80 × 0.30 × 2.30	= 1.242	
$V_7 = (2.87 + 2.341) \times \frac{1}{2} \times 2.341$	$30 \times 0.30 = 1.798$	
V8 = 0.30 × 0.40 × 6.20	= 0.749	· · · ·
		· · · ·
	TOTAL = 11.738 11.738	
	<u>TOTAL = 11,738 11,738</u>	m) .
	그리고 가지는 것으로 내 같은 것으로 가지 않는 것이라.	
	and a second	<u> </u>
	<u>n konstruktion and and and and and and and and and an</u>	
		;



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• • • • •	RESULT								2.048 m ³					-				
17.R+1.Cm	CALCULATION	(TYPE-E)		$v_1 = o.b0 \times (b.20 + 0.10 \times 2) \times 0.10 = 0.384$	a se a ser a s A ser a ser a serva se	$V_{2} = (3, 280 + 1, 920) \times \frac{1}{2} \times (6, 20 + 0, 10 \times 2)$	 - 1, 66 4		707AL = 2.048									
DRATNAGE SINTCE WAY AT WIE INTOR WAY	TYPE OF WORK: 2. EVELTNG CONCRETE	LOCATION: WING WALL	. ·			2041 - 3,309	00			100 100	SECTION F-F	4						

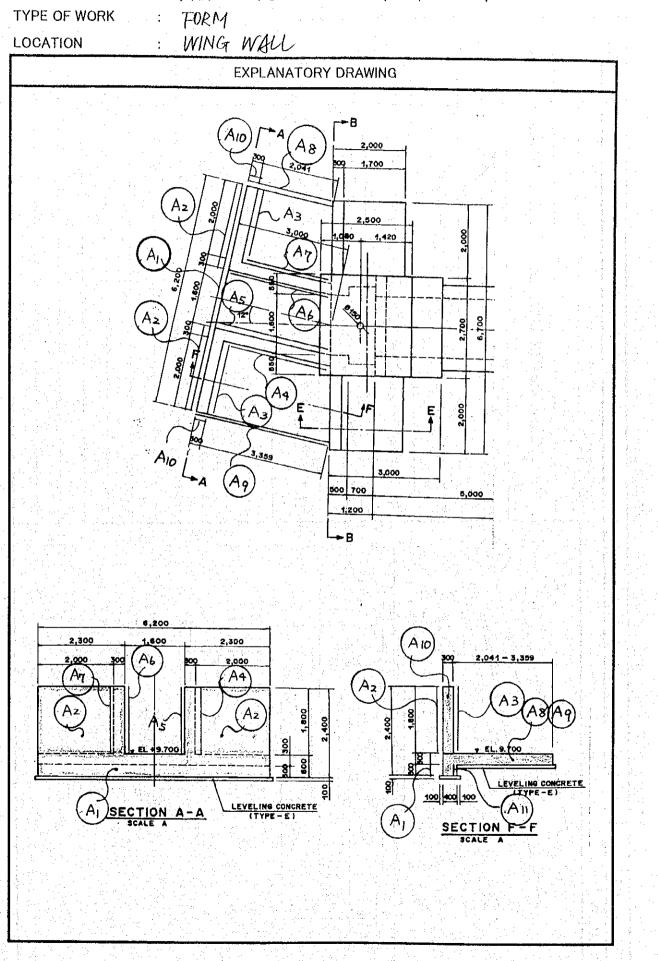
DRAINAGE SLUICEWAY AT WF. 172R + 15 m : FORM

TYPE OF WORK LOCATION

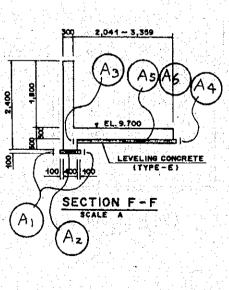
: WITHA	10.411		
E PUNTA	A second second	 	

LOCATION : WING WALL		
CALCULATIO	N	RESULT
(H < 7.0m)		
$A_1 = 0.60 \times 6.20$	= 3.720	
$A_2 = 2.30 \times 1.80 \times 2$	= 8,280	
$A_3 = 2.00 \times 1.80 \times 2$	= 7.200	
A4 = 2.934 × 1.80	= 5.281	
$As = 3.170 \times 1.80$	= 5.706	
$A_6 = 2.830 \times 1.80$	= 5.094	
Ay = 2.466 × 1.80	= 4,439	
A		
$A8 = (2.34) \times 0.30) + (0.30 \times 0.40)$) = 0,822	
$Aq = (3, 659 \times 0, 30) + (0.30 \times 0, 4)$	0) = 1.218	
A10 = 0.30 × 1.80 × 2		
<u> </u>	= 1.080	
A11 = 0.20 × 6.20	- 1 - 240	
	= 1, 240	
	TOTAL = 44,080	44.080 m ²
	1016- 77,000	<u>++,000 m</u>

DRAINAGE SLUICEWAY AT WF. 172R + 15m



	RESU		· ·			
2R+15m		CH < 4.0 m)	A) = (6, 20 + 0.10×2)×0.10×2 = 1, 280	Az = 0.60 × 0.10 × 2 = 0.120	$A3 = (6.20 \pm 0.10 \times 2) \times 0.10 = 0.640$	
DRAINAGE SLUICEWAY AT WF. 172R+15m	TYPE OF WORK FORM FOR LEVELING CONCRETE	LOCATION : WING WALL	(A) (A)		$A = \frac{1}{2} \left(\frac{1}{2} \right) \left($	



AT IOM	RESULT
20+0.10×2)×0.10×2 = 1.280	
$A_2 = 0.60 \times 0.10 \times 2$	
$= (6.20 \pm 0.10 \times 2) \times 0.10 = 0.640$	
-	
$(6.339 + 0.10 \times 2) \times 0.10 = 0.654$	
3.259 × 0.10 = 0.326	
941 × 0,10 × 194	
70TAL = 3.214	3.214 m2
	n de la composition de la comp

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-8

2,000 1,700

2,500 1,420

500 700 1,200

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3,000

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