LEANING WALL (CONCRETE TYPE)

TYPE OF WORK

FORM

LOCATION : WF. 105R ~ WF. 110R+ ZZ.O

					103	CA	LCUL	ATIO		<<1 <i>U</i>						RESULT
		P-00-					т	Nr. Cakula	tion for Form(Fr	ont and Back)					1	
I		block	HI	1112	distance	front A1	113	destance	IA2	111	1113	back distance	IA3		6004 T1(m2)	
l		L1 12/	6,373	6.424	14,500	93.213	1.000	15.000	706.599 329,220	5,951 6.055	6.055	14,500	87.044	706.599	1593,456	
ı		13	6.484	6,411	. 10,000	લામ	1.000	10.000	329,220	6,055	6.055	10,000	60.552	329.220 329.220	783.836 783.836	
ı		1.5	6,373	6,373	10.000	63.726	1.000	10.000	326.425 323.630	6.055 5.951	5,951 5,951	10,000	60.030 59.508	326.425 323.630	111.165 110.191	
ł		1.7	6.373	6.261	10,000	63.726 63.167	1,000 0.956	10,000	323,630 320,545	5.951 5.951	5.95E 5.846	10,000	59,508 58,986	323.630 320.585	770,494 763,323	
ĺ		1.8	6.261 6.149	6.149	10,000	62.019 60.931	0.950	10,000	314.995 309,405	5,84G 5,742	5,742 5.63 8	10,000	57,912 56.292	314.995	719,981	
İ	1 27	L10 L11	6.037 5.935	5.925 5.814	10,000	59.813 58.695	0.900	15.000	455.34E 476.760	5,638 5,533	5.533 5.429	10.000	55,854 54,810	455.348	1026.362 1067,025	
ļ	13 15 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	L12	5.814	5,702 5.478	10,000	\$7.577 \$5.900	0.900	17.000	497.055 511,200	5.129	5,324	10.000	\$3,766	497.055	1105,452	
l		LIL	5.478 5.366	5.366 5.255	10.000	\$4.223 53.105	0.850	19,000	. \$23,194	5.324 5.116	5.116 5.011	10,000	52.200 50.631	511.200 523. 94	1130.500 1151.244	
ŀ		1.16	5.255	\$,031	10.000	31.428	0.850	20.000	539.550 548.919	5.011 1.207	4.907	10.000	49.590 48.024	539.550 548.919	1111.795	
Ì		1.17	5.031 4.807	4.807 4.584	10,000	49,192 46,956	0.800	22,000 23,000	549.912 549.194	1,698 1,489	4,489	10.000	45.936 43.848	549.912 549.194	1194,952 1189,192	
I		1.19 1.20	1.581	4.360 1.137	10.000	42,484	0.800	24.000 25.000	\$46,210 \$40,425	1.280	4.072 3.863	10.000	41.760 39.672	546.240 540.425	1178.960	
ŀ		1.21	4.137 4.248	4,248	10,000	43,925 43,602	0.750	26,000 27,000	554,775 599,427	3.863 3.967	3,967	10,000	39.150	354.775	1190.625	<u> </u>
ı		1.23	1.472	4.696	10.000	15,838	0.600	28.000	652,932	1.176	4.176	10,000	40,716 42.804	599.127 652.932	1283,172 1394,506	
l		125	4.919	4.919 5.031	10,000	48,074 49,751	0.800	29.000 30.000	708.673 758.265	4,385	4.594 4.698	10,000	44.892	758.265	1510.312	Constitution of the
ĺ	<u>ti kiti ili ili</u> i	1.26	5.031	5.087	1.500	22.765	0.850	31 000	366.037	1.698	1,750	4,500	21.258	366.037	776,097 28982.453	
ĺ				10.00	100		Table, C	akubion f	or Form(Sides)	W.						
ŀ		section I	0.150	1.650	5,700	A1 5.985				total 12(m2) 8.535						
I		2 3	0,450	1.650 1.650	5.800	6,020	2.550	1.000	2.550	\$.640			100			
ſ	\$1.75 to 11. \$4	4	0.450	1.650	5.800 5.800	6.090	2.550	1,000	2.550 2.550	8.640						
ŀ		6	0.150 0.150	1.650 1.650	5.700	5.985 5.985	2,550	1,000	2.550 2.550	#.535 #.535						
l		7 -	0.450	1.560	5,700 5,600	5.729 5.628	2,450 2,450	0.950	2.325 2.328	8.056 7.956						
ŀ	1 1 1 1 1 1	9 10	0.450	1.560	5.500 5.400	5.528 5.184	2.450	0.950	2.32¥ 2.070	7,855 7.254						
ļ,		11	0.450	1,470	5.300	5.088	2,300	0.900	2.070	7.158				7		
l		. 13	0.450	1,470	5,200 5,100	4,896	2.300 2.300	0.900	2.070 2.070	7.062 6.966						
ŀ		15	0.450 0.450	1,380	4.900	4,484	2.150	0.850	1,828	6.311						
ĺ.		16	0.450	1.380	4.700	4.30t 3.915	2.150	0.850	1.828	6.12% 5.515	20 20					
ľ		18	0,450 0.450	1.290	4,300	3.741 3.567	2.000	0.800	1.600 1.600	5.341 5.167						. The state
ŀ		20	0.450	1.200	3,900	3.218 3.053	1.850	0.750	1.388	4.605			7	4	The Land Committee	
ŀ		22	0.450	1.290	3.800	3.30%	1.450 2.000	0.750 0.800	1,358	1,110 1.906			1, 1	100		
ľ	· · · · · · · · · · · · · · · · · · ·	23 24	0.450	1.290	4,000 4,200	3.480 3.654	2,000	0.800	1,600	-5.080 5.254			3			
ŀ		25 26	0.450	1.290	4.400	3,828 4,110	2.000 2.150	0.800	1.600	5.428 5,915			7,11			
l		27	0.450	1.380	4.550	4.163	2.150	0.850	1.828	5.991 180.162						
ŀ		le. Calculation			7 . S.			-	7 - 5 - 5 - 5	180,102]			4 J. J. I			
L		block d	istarice [\(m2)		ſ	TOTAL					1.2		
		11 12	14,500	10.000	0.150	1.500		[5	ides	28082.453 180.162	7					
ŀ	<u>a 194</u> 4 Mar 5 A 1	1.3 1.4	10,000	10.000	0.150	1.500		ľ	op Concrete	38.854 28301.468			3 1			<u> </u>
		1.5	10,000	10,000	0.150	1.500		_								
		L.7 1.8	10,000	10,000	0.150	1.500							7			
_		1.9 Li0	10.000	10.000	0.150	1.500								· '.,	<u>-</u>	
		LII	10,000	10,000	0.150	1.500		3.14		* .		1.00				
		L12 L13	10,000	10.000	0.150	1.500										
-		1,14	10.000 10.000	10.000	0.150 0.150	1.500			1		100	1				<u> </u>
		I.16	10,000	10.002	0.150	1.500		17.								
_		L18	10.000	10.002	0.150 0.150	1,500			and the second			e e i e		1.7		
		1_20	10.000	10.002	0.150	1.500						3 ⁴ 1				
ľ		1.21 1.22	10.000	10.000	0.150	1.500				100				1.1	-	
_	3	L23 L24	10.000	10.002	0.150 0.150	1.500			1 - 2 - 2 - 2				1.00			
		L25 1.26	10.000	1,500	0,150 0,150	0.675		-11	er Borr						* .	
-	i i			259,021		38.854			11. 33.	- 17 t			in the second		_	
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				(4. 1.1.) 		11/21	garte.							100		
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			6			30 Aug.		100	1.1.1				100		・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・	01.468m

LEANING WALL (CONCRETE TYPE)

TYPE OF WORK

: JOZNT FILLER : WE 1058 ~ WE 1108+22

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	<u> </u>			<u> </u>						• •
					Calculation			1 2 1 1 4 4		
	section	0.450	_2 1 1.650	5,700	A1 L 5,985	2:550		.2	total T2(m2)	
0.0	2	0.450	1.650	5,800	6,090	2,550	1.000	2.550	8.640	
	3	0.450	1.650	5.800	6,090	2.550	1.000	2.550	8.640	٠.
	4	0.450	1.650	5.800	6.090	2.550	1.000	2,550	8.640	
1 1 1 1	5	0.450	1.650	5.700	5.985	2.550	1.000	2.550	8,535 —	
	6 7	0,450	1,650 1,560	5.700 5.700	5.985 5.729	2.550 2.450	1.000 0.950	2,550 2,328	8.535 8.056	
	8	0.450	1.560	5.600	5.628	2.450	0.950	2.328	7,956	
	9	0.450	1.560	5.500	5,528	2.450	0.950	2.328	7.855	
	10	0.450	1.470	5.400	5,184	2.300	0.900	2.070	7.254	<u>: :</u>
	11	0.450	1.470	5.300	5,088	2,300	0.900	2.070	7.158	
	12	0.450 0.450	1.470	5.200	4.992	2.300	0.900	2.070	7.062	
 .	14	0.450	1.470	5.100 4.900	4.896 4.484	2.300	0,900 0.850	2.070 1.828	6,966	
	15	0.450	1.380	4.800	4.392	2.150	0,850	1.828	6.220	
	16	0.450	1.380	4.700	4.301	2.150	0.850	1.828	6.128	Ü.,
	17	0.450	1.290	4.500	3.915	2.000	0,800	1,600	5.515	
	18	0.450	1.290	4.300	3.741	2.000	0.800	1.600	5.341	
	19 20	0.450 0.450	1.290	4,100 3,900	3.567 3.218	2.000 1.850	0.800	1,600 1,388	5,167	
	21	0.450	1.200	3.700	3.053	1.850	0.750	1.388	4.605 4.440	
	22	0.450	1.290	3.800	3,306	2.000	0.800	1.600	4.906	
	23	0.450	1.290	4.000	3.480	2.000	0.800	1.600	5.080	
	24	0.450	1.290	4.200	3.654	2.000	0.800	1.600	5.254	
	25	0.450 0.450	1.290	4.400 4.500	3.828 4.118	2.000	0.800	1,600 1.828	5.428 5.945	<u> </u>
	27	0.450	1.380	4.550	4.163	2.150	0.850	1.828	5.991	
						4.44			171.627	
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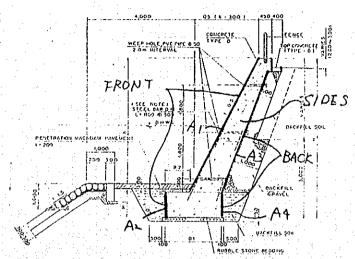
TYPE OF WORK

LEANING WALL (CONCRETE)

LOCATION

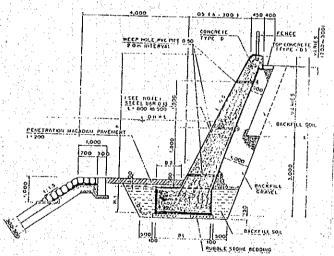
: WF. 105R ~ WF. 110R+22.0

EXPLANATORY DRAWING



STANDARD CROSS SECTION OF LEANINGWALL (RINGHT BANK)

FOR FORM



STANDARD CROSS SECTION OF LEANINGWALL (RINGHT BANK)

FOR JOINT FILLER

RESULT		828.800 m	18 S. 180m	
PCV	(2) L3 = 1.3m / place (3) L3 = 1.3m / place L = 21, 7 L2 + 23 = 3.2m N = (4.5+240.0+14.5) = 2.59	L = 259 x 3.2 m = 828.8 m - FILTER CLOTH A = 0840 m²/d, 359 = 115, 260		
TYPE OF WORK: WEEP HOLE LOCATION: (C)	00 000 000 000 000 000 000 000 000 000 000 000	SS SECTION OF LEANINGWALL (RII	100 000 000 000 000 000 000 000 000 000	OETAIC OF WEEP HOLE

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	RESULT		486.012 m																						
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	7				1460 1430 1400			\$ 00.0						8	BACKELL	δετ. 	105 PACKETE 5017		RINGHT						
	FENCE							05 1 h - 300 3	5:4			-		f			900	400 RUBBL E	SINGWALL						
									WEEP HOLE, PVC PIPE & SO			NOTE 00 MAR 043 00 00 00 500		09') ~	T 13F	ero.	5	000	SCALE C						
	STEEL							000,4	WEEP FOLE			STECK WAR 0-43 60 1- 600 44 500	1: -			1, 82		ĺ	SECTION						
::\L													PENETRATION MACHDAN PENEURIT	000 002	$-\frac{9}{8}$	-1]			STANDARD CROSS SECTION OF LEANINGWALL					. V H.	
		er er Villende Villende											KTRATION MA	3	\ \frac{1}{2}	3/			TANDARD						
	WORK	 ≥											<u>.</u>		- 6	001	,309.		ωl						
	TYPE OF WORK:	LOCATION																							
	_	2										2 -	146	5	. 4. 1						·			<u> </u>	

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2.6 LEANING WALL (WET STONE MASONRY)

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE) LOCATION : WF. $65L + 3.0 \text{ m} \sim \text{WF.} 65L + 28.0 \text{ m}$

: LEANING WALL-1

1 1.285 1.905 3.100 4.945 3.555 2.835 0.900 2 1.285 2.000 3.574 5.871 3.650 2.930 0.900 3 1.285 2.067 3.908 6.550 3.717 2.997 0.900				: ··			CUL	ATI	UN	<u>. 1</u>	4.75.34					R.	ESUI
1 1.285 1.905 3.100 4.945 3.555 2.835 0.900 2 1.285 2.000 3.574 5.871 3.650 2.930 0.900 3 1.285 2.067 3.908 6.550 3.717 2.997 0.900 section A2	TRUCT	'UR	ALE	XC	AVATION												
1 1.285 1.905 3.100 4.945 3.555 2.835 0.900 2 1.285 2.000 3.574 5.871 3.650 2.930 0.900 3 1.285 2.067 3.908 6.550 3.717 2.997 0.900 section A2	ureas, ja		14.14 <u> </u>					1					<u> </u>				
2 1.285 2.000 3.574 5.871 3.650 2.930 0.900 3 1.285 2.067 3.908 6.550 3.717 2.997 0.900 3 1.2876 1.650 1.950 0.300 0.540 8.361 2 2.961 1.650 1.950 0.300 0.540 9.372 3 3.021 1.650 1.950 0.300 0.540 10.111 2 8.866 10.158 90.063 3 9.741 7.158 69.728 17.316 159.791 159.791 159.791 V = 159.791 159.791 159.791 159.791 V = 1.285 2.000 3.574 5.871 3.650 2.930 0.900 3 1.285 2.067 3.908 6.550 3.717 2.997 0.900 3 1.285 2.067 3.908 6.550 3.717 2.997 0.900 3 1.285 2.067 3.908 6.550 3.717 2.997 0.900 4 1 0.653 1.650 1.750 0.100 0.170 0.418 2.000 3 0.653 1.650 1.750 0.100 0.170 0.418 2.000 3 0.653 1.650 1.750 0.100 0.170 0.418 2.000 3 0.835 2.288 2.288 7.158 16.377 1 0.835 2.288 2.288 7.158 16.377 3 1.585 2.288 2.288 7.158 16.377 3 3 3.85 2.288 2.288 7.158 16.377 3 3 3 3.85 2.288 2.288 7.158 16.377 3 3 3 3.85 2.288 2.288 7.158 16.377 3 3 3 3.85 2.288 2.288 7.158 16.377 3 3 3 3 3 3 3 3 3	section	1				L							<u>. </u>	?	14.		
3 1.285 2.067 3.908 6.550 3.717 2.997 0.900 3 1.2876 1.650 1.950 0.300 0.540 8.361 2 2.961 1.650 1.950 0.300 0.540 9.372 3 3.021 1.650 1.950 0.300 0.540 9.372 3 3.021 1.650 1.950 0.300 0.540 10.111 2 8.866 10.158 90.063 3 9.741 7.158 69.728 17.316 159.791 V = 159.791	· ·	1	* *	I.									L		السند		
Section A2		2										2.930		0.9	00		
1 2.876							3.90					2.997		0.9	00		4.
2 2.961 1.650 1.950 0.300 0.540 9.372 3 3.021 1.650 1.950 0.300 0.540 10.111	section	/							,		- 1	A2+A3					
3 3.021 1.650 1.950 0.300 0.540 10.111	1 1 1 1 1 1	1					1.95	0	0.300			8.361		- 14.		13	
Section ave distance(m) volume(m²)	<u> 1848 - 1848 - 1</u>	2							0.300	0.54	10	9.372		- 1			
1 2 8.866 10.158 90.063		- 1		- 1					0.300	0.54	Ю	10.111					
3 9.741 7.158 69.728	section	8	ave	(listance(m)	volum	1e(m³)	1.1									et i
3 9.741 7.158 69.728		1	1,100,100	2.77					1					192 19			
N = 159.791 159.791		2	<u> </u>							e sib j							
ACKFILL WITH SELECTED SOIL Cotion L1		3	9.7	41			69.72	8		10 T		Maria.	7	20 2 T			
ACKFILL WITH SELECTED SOIL Cotion L1 L2 H1 A1 L3 L4 H2					17.316	1	59.79	1		212 47							
ACKFILL WITH SELECTED SOIL Cotion L1 L2 H1 A1 L3 L4 H2								. 1.					•				
ACKFILL WITH SELECTED SOIL Cotion L1 L2 H1 A1 L3 L4 H2	V =	159	7.791	- ,-,			. 1,							1	4, 5, 44	159	.791
ction L1 L2 H1 A1 L3 L4 H2 1 1.285 1.905 3.100 4.945 3,555 2.835 0.900 2 1.285 2.000 3.574 5.871 3.650 2.930 0.900 3 1.285 2.067 3.908 6.550 3.717 2.997 0.900 ction A2 L5 L6 H3 A3 L7 H4 1 0.653 1.650 1.750 0.100 0.170 0.418 2.000 2 0.653 1.650 1.750 0.100 0.170 0.418 2.000 3 0.653 1.650 1.750 0.100 0.170 0.418 2.000 ction A4 A1+A2+A3+A4 ave distance(m) volume(m³) 0.000 1 0.835 2.288 2.288 10.158 23.240 0.000 3 0.835 2.288 2.288 7.158 </th <th>1 1 1 de 1 1 de</th> <th></th> <th>200</th> <th></th> <th>1.5</th> <th>1718 117</th> <th></th> <th></th> <th></th> <th></th> <th>411</th> <th>12.4</th> <th></th> <th>1.00</th> <th></th> <th></th> <th></th>	1 1 1 de 1 1 de		200		1.5	1718 117					411	12.4		1.00			
ction L1 L2 H1 A1 L3 L4 H2 1 1.285 1.905 3.100 4.945 3,555 2.835 0.900 2 1.285 2.000 3.574 5.871 3.650 2.930 0.900 3 1.285 2.067 3.908 6.550 3.717 2.997 0.900 ction A2 L5 L6 H3 A3 L7 H4 1 0.653 1.650 1.750 0.100 0.170 0.418 2.000 2 0.653 1.650 1.750 0.100 0.170 0.418 2.000 3 0.653 1.650 1.750 0.100 0.170 0.418 2.000 ction A4 A1+A2+A3+A4 ave distance(m) volume(m³) 0.000 1 0.835 2.288 2.288 10.158 23.240 0.000 3 0.835 2.288 2.288 7.158 </th <th></th> <th>:</th> <th></th> <th></th> <th></th> <th>9 4 A</th> <th><u> </u></th> <th></th> <th></th> <th></th> <th>13.5</th> <th></th> <th>-</th> <th></th> <th>100</th> <th></th> <th><u> </u></th>		:				9 4 A	<u> </u>				13.5		-		100		<u> </u>
ction L1 L2 H1 A1 L3 L4 H2 1 1.285 1.905 3.100 4.945 3,555 2.835 0.900 2 1.285 2.000 3.574 5.871 3.650 2.930 0.900 3 1.285 2.067 3.908 6.550 3.717 2.997 0.900 ction A2 L5 L6 H3 A3 L7 H4 1 0.653 1.650 1.750 0.100 0.170 0.418 2.000 2 0.653 1.650 1.750 0.100 0.170 0.418 2.000 3 0.653 1.650 1.750 0.100 0.170 0.418 2.000 ction A4 A1+A2+A3+A4 ave distance(m) volume(m³) 0.000 1 0.835 2.288 2.288 10.158 23.240 0.000 3 0.835 2.288 2.288 7.158 </th <th>100 100 100 100</th> <th>1 1</th> <th></th> <th></th> <th></th> <th>100 100</th> <th>1.55</th> <th></th> <th></th> <th>file and the file</th> <th></th> <th>the second of the</th> <th></th> <th></th> <th></th> <th></th> <th></th>	100 100 100 100	1 1				100 100	1.55			file and the file		the second of the					
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2 0.835 2.288 2.288 10.158 23.240 3 0.835 2.288 2.288 7.158 16.377 3 39.617	1 2 3 ction 1 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	L1 A2	1.285 1.285 1.285 0.653 0.653 0.653	L2 L5	1.905 2.000 2.067 1.650 1.650	H1 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	3.100 3.574 3.908 1.750 1.750	Н3	5.87 6.550 0.100 0.100 0.100	A3	3.650 3.717 0.170 0.170 0.170	2,83 2,93 2,99 L7 0,4	35 30 97 18	0.9 0.9 0.9 H4 2.0 2.0	00		
3 0.835 2.288 2.288 7.158 16.377 39.617	1 2 3 ction 1 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	L1 A2	1.285 1.285 1.285 0.653 0.653 0.653	L2 L5	1.905 2.006 2.067 1.650 1.650 1.650	H1 5 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3.100 3.574 3.908 1.750 1.750	Н3	5.87 6.550 0.100 0.100 0.100	A3	3.650 3.717 0.170 0.170 0.170	2,83 2,93 2,99 L7 0,4	35 30 97 18	0.9 0.9 0.9 H4 2.0 2.0	00		
39.617	1 2 3 ction 1 2 3 ction 1 2 1 ction 1	L1 A2	1.285 1.285 1.285 0.653 0.653 0.653	L2 L5	1.905 2.000 2.067 1.650 1.650 1.650 +A2+A3+A4 2.288	H1 5 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3.100 3.574 3.908 1.750 1.750	Н3	5.87 6.550 0.100 0.100 0.100 nce(m)	A3) volum	3.650 3.717 0.170 0.170 0.170 e(m³)	2.83 2.93 2.99 L.7 0.43 0.43	35 30 97 18	0.9 0.9 0.9 H4 2.0 2.0	00		
	1 2 3 ction 1 2 3 ction 1 2 2 3 ction 1 2	L1 A2	1.285 1.285 1.285 0.653 0.653 0.653 0.835	L2 L5	1,905 2,006 2,067 1,650 1,650 1,650 +A2+A3+A4 2,288 2,288	H1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	3.100 3.574 3.908 1.750 1.750 1.750	Н3	5.87 6.550 0.100 0.100 0.100 nce(m)	5	3.650 3.717 0.170 0.170 0.170 e(m³)	2.83 2.93 2.99 L.7 0.43 0.43	35 30 97 18	0.9 0.9 0.9 H4 2.0 2.0	00		
V = 39.617 m	2 3 section 1 2 3 3 section 1 2 3 3 section 1 2 2	L1 A2	1.285 1.285 1.285 0.653 0.653 0.653 0.835	L2 L5	1,905 2,006 2,067 1,650 1,650 1,650 +A2+A3+A4 2,288 2,288	H1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	3.100 3.574 3.908 1.750 1.750 1.750	Н3	5.87 6.550 0.100 0.100 0.100 nce(m)	5	3.650 3.717 0.170 0.170 0.170 e(m³) 23.240 16.377	2.83 2.93 2.99 L.7 0.43 0.43	35 30 97 18	0.9 0.9 0.9 H4 2.0 2.0	00		
V ~ 39.017	2 3 section 1 2 3 3 section 1 2 3 3 section 1 2 2	L1 A2	1.285 1.285 1.285 0.653 0.653 0.653 0.835	L2 L5	1,905 2,006 2,067 1,650 1,650 1,650 +A2+A3+A4 2,288 2,288	H1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	3.100 3.574 3.908 1.750 1.750 1.750	Н3	5.87 6.550 0.100 0.100 0.100 nce(m)	5	3.650 3.717 0.170 0.170 0.170 e(m³) 23.240 16.377	2.83 2.93 2.99 L.7 0.43 0.43	35 30 97 18	0.9 0.9 0.9 H4 2.0 2.0	00		
	1 2 3 section 1 2 3 section 1 2 3 3 section 1 2 3 3	A2	1.285 1.285 1.285 0.653 0.653 0.653 0.835 0.835	L2 L5	1,905 2,006 2,067 1,650 1,650 1,650 +A2+A3+A4 2,288 2,288	H1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	3.100 3.574 3.908 1.750 1.750 1.750	Н3	5.87 6.550 0.100 0.100 0.100 nce(m)	5	3.650 3.717 0.170 0.170 0.170 e(m³) 23.240 16.377	2.83 2.93 2.99 L.7 0.43 0.43	35 30 97 18	0.9 0.9 0.9 H4 2.0 2.0	00		
	1 2 3 section 1 2 3 section 1 2 3 3 section 1 2 3 3	A2	1.285 1.285 1.285 0.653 0.653 0.653 0.835 0.835	L2 L5	1,905 2,006 2,067 1,650 1,650 1,650 +A2+A3+A4 2,288 2,288	H1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	3.100 3.574 3.908 1.750 1.750 1.750	Н3	5.87 6.550 0.100 0.100 0.100 nce(m)	5	3.650 3.717 0.170 0.170 0.170 e(m³) 23.240 16.377	2.83 2.93 2.99 L.7 0.43 0.43	35 30 97 18	0.9 0.9 0.9 H4 2.0 2.0	00	39.6	17 m
	1 2 3 section 1 2 3 section 1 2 3 3 section 1 2 3 3	A2	1.285 1.285 1.285 0.653 0.653 0.653 0.835 0.835	L2 L5	1,905 2,006 2,067 1,650 1,650 1,650 +A2+A3+A4 2,288 2,288	H1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	3.100 3.574 3.908 1.750 1.750 1.750	Н3	5.87 6.550 0.100 0.100 0.100 nce(m)	5	3.650 3.717 0.170 0.170 0.170 e(m³) 23.240 16.377	2.83 2.93 2.99 L.7 0.43 0.43	35 30 97 18	0.9 0.9 0.9 H4 2.0 2.0	00	39.6	17 m

	<u> </u>		CALCULA	TION			e e e e e e e e e e e e e e e e e e e	RESU
BACKFIL	L WITH C	RAVEL						
	<u> </u>	<u>n in in N</u>						
section	LI	Hl	Al	L2	1.17.13.8	H2	A2	
1	0.418	1.850	0.773		0.83	5 1.10	0 0.919	
2	0.418	1.850	0.773		0.83	5 1.57	4 1.315	
3	0.418	1.850	0.773		0.83	5 1.90	8 1.594	
section	A1+A2	ave	distance(m)	volun	ne(m³)		1 12 1	
1	1.691							
2	2.087	1.889	10.158		19.19	1		The state of
3	2.366	2.227	7.158		15.93	8		4 4 5 5.
1 4 4 5 5					35.129	9		
	yay Arman			L		eri v A. t.		
V = 3	5.129	a et i ye.					yeta a	35.129
		14454.4						
1 100			, J. J. J. J. J. J. J. J. J. J. J. J. J.	Add to		The state of the s		
						9 P , 1		W-1
CONCRE	TE TYPE I)			Trans.			
section	elevation	distance	(m) L		t	w	V(m ³)	
1	4.475			. 411				
2	4.945		10.158 1	0.169	0.150	0.450	0.686	
			The state of the s	5 1 25 1	44.4			
3	5.27ϵ	i	7.158	7.166	0.150	0.450	0.484	
3	5.276	<u> </u>	7.158	7.166	0.150	0.450	0.484	
3	5.276		7.158	7.166	0.150	0.450	·	
			7.158	7.166	0.150	0.450	<u> </u>	1 170 m
	5.276 E: V		7.158	7.166	0.150	0.450	<u> </u>	1.170 m
CONCRET	E: V			7.166 			1.170	1:170 n
CONCRET	E: V	= 1.170	distance(m)				<u> </u>	1:170 m
CONCRET	E: V	= 1.170	distance(m)	L			1.170 A1(m²)	1.170 m
CONCRET	E: V section 6	= 1.170 elevation 4.475 4.945	distance(m)	L 10	0.169	0.150	1.170 A1(m²)	1.170 n
CONCRET	E: V section e	= 1.170 elevation 4.475 4.945	distance(m)	L 10	0.169 7.166		1.170 A1(m²) 1.525 1.075	1:170 m
CONCRET	E: V section e	= 1.170 elevation 4.475 4.945	distance(m)	L 10	0.169	0.150	1.170 A1(m²)	1:170 m
CONCRET	E: V section 6	= 1.170 elevation 4.475 4.945	distance(m) 10.158 7.158	10	0.169 7.166 7.335	0.150 0.150	1.170 A1(m²) 1.525 1.075 2.600	1.170 m
CONCRET	E: V section e	= 1.170 elevation 4.475 4.945 5.276	distance(m) 10.158	10	0.169 7.166 7.335	0.150 0.150	1.170 A1(m²) 1.525 1.075	1.170 m
CONCRET	E: V section 1 2 3	= 1.170 elevation 4.475 4.945 5.276	distance(m) 10.158 7.158	10	0.169 7.166 7.335	0.150 0.150	1.170 A1(m²) 1.525 1.075 2.600	1:170 m
CONCRET	E: V section 1 2 3	= 1.170 Elevation 4.475 4.945 5.276	distance(m) 10.158 7.158	10	0.169 7.166 7.335	0.150 0.150	1.170 A1(m²) 1.525 1.075 2.600	1:170 m
CONCRET A2= Total=A1	E: V section 6 1 2 3 0. +A2=	= 1.170 Elevation 4.475 4.945 5.276	distance(m) 10.158 7.158	10	0.169 7.166 7.335	0.150 0.150	1.170 A1(m²) 1.525 1.075 2.600	
CONCRET A2= Total=A1	E: V section 6 1	= 1.170 elevation 4.475 4.945 5.276	distance(m) 10.158 7.158	10	0.169 7.166 7.335	0.150 0.150	1.170 A1(m²) 1.525 1.075 2.600	2.735 m
CONCRET A2= Total=A1	E: V section 6 1	= 1.170 elevation 4.475 4.945 5.276	distance(m) 10.158 7.158	10	0.169 7.166 7.335	0.150 0.150 0.150	1.170 A1(m²) 1.525 1.075 2.600	
CONCRET A2=	E: V section 6 1	= 1.170 elevation 4.475 4.945 5.276	distance(m) 10.158 7.158 0.450 5 m ²		0.169 7.166 7.335	0.150 0.150 0.150	1.170 A1(m²) 1.525 1.075 2.600	2.735 m
CONCRET A2= Total=A1	E: V section 6 1	= 1.170 elevation 4.475 4.945 5.276	distance(m) 10.158 7.158 0.450 5 m ²		0.169 7.166 7.335	0.150 0.150 0.150	1.170 A1(m²) 1.525 1.075 2.600	
CONCRET A2= Total=A1	E: V section 6 1	= 1.170 elevation 4.475 4.945 5.276	distance(m) 10.158 7.158 0.450 5 m ²		0.169 7.166 7.335	0.150 0.150 0.150	1.170 A1(m²) 1.525 1.075 2.600	2.735 m
CONCRET A2= Total=A1	E: V section 6 1	= 1.170 elevation 4.475 4.945 5.276 150 * 2.73 = 2.735	distance(m) 10.158 7.158 0.450 5 m ²		0.169 7.166 7.335	0.150 0.150 0.150	1.170 A1(m²) 1.525 1.075 2.600	2.735 m

			CAL	CULA	ATION							RESU	JL
AVEL	BEDDING	3					18 11				9		
									3-12				
section	B1	t 5.55	A		Ave		dista	nce(m)	`	V(m³)			• •
1	1.770	1.1.		0.197	1 1 1								:
2	1.865		_1	0.206	0		1 1	10.158		0.91			٠.
3	1.932	0.100	(0.213	0	.210		7.158		0.64			ia,
	NAT.							17.316	5	1.55	8		
V - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		1 H 2 27 H 1 H 2 2									1. 1		
V = 1	.558				<u> </u>	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1					·	1.558	n
\$1.5 m													
ET STO	NE MAS	ONRY 🔠		9 - 3 - 3									
<u>) (</u>							115						7
section	L1		H1	12	A1		L3		H2			大疗法	
1	0.450			3.100	l	2.356		1.770		0.800]		
2	0.450		<u> </u>	3.574		2.886		1.865		0.800			
3	0.450			3.908		3.286		1.932	, j	0.800			
section	A2	A1+A2		Table (distanc	e(m)	V2	?(m³)	- 1-				
1	1.416			4,50		1 44 7							
2	1.492			4.075	1	0.158	I	41.391	1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2				
3	1.545	4.831	4	4.604		7.158		32.958	*		7,5		:
											1		. `
		20 10 10 10 10 10 10 10 10 10 10 10 10 10			total			74.349					
<u> </u>					total			74.349]		
V = 7	4.349				total			74.349			<u> </u>	74.349	9 ₁
V = 7	4.349				total			74.349				74.349	9 1
\$1 3.1.4		R POINTI	NG		total			74.349				74.349	9 1
\$1 3.1.4		R POINTI	NG		total			74.349				74.34	9
MENT	MORTAI	front				To	p.			Al+A	2	74.34	9
\$1 3.1.4	MORTAI						p.			A1+A	2	74.34	9
EMENT section	MORTAI	front distance(m)) A1		12	To distanc	op e(m)	A2				74.34	9 1
Section 1 2	MORTAL L1 3.466 3.996	front distance(m)	A1 8 37.8	397	0.450	To distanc	op e(m)	A2 8 4.5	71	42.46	8	74.34	<u>3</u>
EMENT section	MORTAI	front distance(m)	A1 8 37.8	397	12	To distanc	op e(m)	A2 8 4.5	71	42.46 33.15	8	74.34	9
Section 1 2	MORTAL L1 3.466 3.996	front distance(m)	A1 8 37.8	397	0.450	To distanc	op e(m)	A2 8 4.5	71	42.46	8	74.34	9
Section 1 2	MORTAL L1 3.466 3.996	front distance(m)	A1 8 37.8	397	0.450	To distanc	op e(m)	A2 8 4.5	71	42.46 33.15	8	74.34	9
Section 1 2	L1 3.466 3.996 4.369	front distance(m)	A1 8 37.8	397	0.450	To distanc	op e(m)	A2 8 4.5	71	42.46 33.15	8	74.34 <u>9</u>	
section 1 2 3	L1 3.466 3.996 4.369 5.627	front distance(m)	A1 8 37.8	397	0.450	To distanc	op e(m)	A2 8 4.5	71	42.46 33.15	8		
section 1 2 3	L1 3.466 3.996 4.369 5.627	front distance(m)	A1 8 37.8	397	0.450	To distanc	op e(m)	A2 8 4.5	71	42.46 33.15	8		
section 1 2 3	L1 3.466 3.996 4.369 5.627	front distance(m)	A1 8 37.8	397	0.450	To distanc	op e(m)	A2 8 4.5	71	42.46 33.15	8		
section 1 2 3	L1 3.466 3.996 4.369 5.627	front distance(m) 10.15 7.15	8 37.8 8 29.5	397	0.450 0.450	Todistanc	pp ee(m) 10.15 7.15	A2 8 4.5	71 21	42.46 33.15	8		
section	L1 3.466 3.996 4.369 5.627	front distance(m) 10.15 7.15	8 37.8 8 29.5	397	0.450 0.450	To distanc	pp e(m) 10.15 7.15	A2 58 4.5 58 3.2	71 21	42.46 33.15 75.62	8		
section 1 2 3 A = 7 INT FII section	L1 3.466 3.996 4.369 5.627	front distance(m) 10.15 7.15	A1 8 37.8 8 29.5	397 938	0.450 0.450 0.450 1.770	distanc	opp e(m) 10.15 7.15	A2 58 4.5 58 3.2	71 21 A1	42.46 33.15 75.62	8 9 7		
section 1 2 3 A = 7 INT FII section 1	L1 3.466 3.996 4.369 5.627 LLER	front distance(m) 10.15 7.15 L2 1.070 1.165	8 37.8 8 29.9 11 3.100	397 938 A1 2.356	0.450 0.450 0.450 L3 5 1.770 5 1.865	Toddistance	op e(m) 10.15 7.15	A2 58 4.5 58 3.2 A2 1.416	71 21 A1	42.46 33.15 75.62	8 9 7		
section 1 2 3 A = 7 INT FII section 1 2	MORTA) L1 3.466 3.996 4.369 5.627 LLER L1 0.450 0.450	front distance(m) 10.15 7.15 L.2 1.070 1.165	8 37.8 8 29.5 11 3.100 3.574	A1 2.356 2.886	0.450 0.450 0.450 L3 5 1.770 5 1.865	Toddistance	op e(m) 10.15 7.15	A2 8 4.5' 8 3.2' A2 1.416 1.492	71 21 A1	42.46 33.15 75.62 1+A2 - 4.37	8 9 7 7 1		
section 1 2 3 A = 7 INT FII section 1 2	L1 3.466 3.996 4.369 5.627 LLER L1 0.450 0.450 0.450	front distance(m) 10.15 7.15 L.2 1.070 1.165	8 37.8 8 29.5 11 3.100 3.574	A1 2.356 2.886	0.450 0.450 0.450 L3 5 1.770 5 1.865	Toddistance	op e(m) 10.15 7.15	A2 8 4.5' 8 3.2' A2 1.416 1.492	71 21 A1	42,46 33,15 75.62 1+A2 - 4,37 4.83	8 9 7 7 1		71

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE)

: WF. 65L + 3.0 m ~ WF. 65L + 28.0 m : LEANING WALL-1

g de la composición della comp		CALCULATION	RESULT
WEEP HO	OLE		
7710 777			
PVC PIPE	\$ Ø 50		
$n_1 = 17.3$	316/3.0	<u></u>	
2	107:510 117:41 117:11		
$n_1 = 17.3$	316/3.0	<u> </u>	2.550 m
$L_1 = 6x$	0.8	= 4.800	
$L_2 = 6x$	1 15	= 6.900	
32	1110		
$L = L_1 +$	- L ₂	11.700	11.700 m
FILTER C	LOTH	ovinska og til store fra statte skaller og til store til skalle skaller og til store til statte skaller og til Det og til skaller og til statte skaller og til skaller og til skaller og til skaller og til skaller og til sk	
A = 0.64	10 m² / plac	$e \times 6 \times 2$ = 7.680	7.680 m ²
	, p. 2.0.0		7.000 III
			Liber Barre
STEEL FI	ENCE		E TOME PLANTS
L = 17.3	135 m	는 기능하게 된 일이 하는 것을 가장하는 것들이 되었다. 그런 것으로 보고 있는 것으로 되었다. [1] 사용 : [1] [1] - 1 (1) : [2] - 2 (2) : [2] - 2 (2) : [2] - 2 (2) : [2] - 2 (2) : [2] - 2 (2) : [2] - 2 (2) :	17.335 m
15 - 17.3	133 III		11.335 m
4 (3,1)			
SCAFFOL	DING		
	section	front A1	
	1	3.466 A	
	2	3.996 10.158 37.897	The state of
	3	4.369 7.158 29.938	
		67.835	
A = 6	7 825		67.835 m²
A = 0	17.655		67.833 m
	4.4		
		는 사람들이 되었다. 이 사람들은 사람들이 되는 사람들이 가는 것이 되었다. 그는 것이 되었다. 사람들은 사람들이 가득하는 것이 되었다. 사람들이 가득하는 것이 되었다. 그런 것이 되었다.	
			

1.0		100	1.5	CAL	CULAT	ION	$\mathbb{E}_{\{ \{ j, k \} \in \mathcal{K}_{k} \in \mathcal{K}_{k} \in \mathcal{K}_{k} \}}$				RES	ULT
TRUCTU	JRAL E	XCAV	ATIO	V							et general	170
				7								
section	L1		L2	H1		A1	L3	L4				
3		1.285	1.793		2,540	3.910	3.268	2.60	58			J. 1
4	4.50	1.285	1.819	:	2.671	4.140	3.294	2.69	94	: 4		
5		1.285	1.819		2.671	4.140	5 3.294	2.69	94			
section	H2		A2	L5		L6	H3	A3				
3		0.750	2.226	1	1.475	1.775	5 0.300	0.48	38			
4		0.750	2.246		1.475	1.77:	0.300	0.4	88			
5		0.750	2.246		1.475	1.77:	5 0.300	0.48	88			
section	A1+A2	+A3	ave	dist	ance(m)	volume(m3)	The second					4
3		6.623		W 1, 100								
4	35 6	6.879	6.751		2.684	18.12	i i					
5		6.879	6.879		5.000	34.39	7	1 5 5				
						52.518	3			17		
		ا						-	. لـــ المرازية			
V = 5	2.518										52.51	$8 \mathrm{m}^3$
											55.5 x	
		1						<u> </u>				
ACKFIL	T WIT	U CET	ECTE!	0.00	11				<u> </u>		4 7 7 4	
											4 4 6	
AUILLIL	<i>(L)</i>	เรอเก		0.30	11)	<u>a detroj e ordaĝo poj eleta</u> La la la ĝoj de oj troj						1
		<i>V</i>	w to fi			13	Па	[₁	12			
section	L1	L2	Hi		A1	L3 0.875	L4		H2 0.750]		
section 3	L1 0.835	L2 0.610	H1 0	.750	A1 0.542	0.875	0.:	500	0.750			
section 3	L1 0.835 0.835	L2 0.610 0.610	H1 0	.750 .750	A1 0.542 0.542	0.875 0.875	0.: 0.:	500	0.750 0.750			
section 3 4 5	L1 0.835 0.835 0.835	L2 0.610 0.610 0.610	H1 0	.750 .750	A1 0.542 0.542 0.542	0.875 0.875 0.875	0.: 0.: 0.:	500	0.750			
section 3 4 5 section	L1 0.835 0.835 0.835 A2	L2 0.610 0.610 0.610 L5	H1 0 0 0 1.6	.750 .750 .750	A1 0.542 0.542 0.542 H3	0.875 0.875 0.875 A3	0.: 0.: 0.: L7	500 500	0.750 0.750 0.750	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1		
section 3 4 5 section 3	L1 0.835 0.835 0.835 A2 0.516	L2 0.610 0.610 0.610 L5 1.475	H1 0 0 0 1.6	.750 .750 .750	A1 0.542 0.542 0.542 H3 0.300	0.875 0.875 0.875 A3 0.488	0.: 0.: 0.: L7	500 500 500	0.750 0.750 0.750			
section 3 4 5 section 3 4	L1 0.835 0.835 0.835 A2 0.516	L2 0.610 0.610 0.610 L5 1.475	H1 0 0 0 16	.750 .750 .750 .750	A1 0.542 0.542 0.542 H3 0.300 0.300	0.875 0.875 0.875 A3 0.488 0.488	0.5 0.5 0.5 L7 0.6	500 500 500 418	0.750 0.750 0.750			
section 3 4 5 section 3 4 5 5	0.835 0.835 0.835 0.835 A2 0.516 0.516	L2 0.610 0.610 0.610 L5 1.475 1.475	H1 0 0 0 L6 1 1 1 1	.750 .750 .750 .775 .775 .775	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300	0.875 0.875 0.875 A3 0.488 0.488	0.: 0.: 0.: L7 0.:	500 500 500 418 418	0.750 0.750 0.750			
section 3 4 5 section 3 4	L1 0.835 0.835 0.835 A2 0.516	L2 0.610 0.610 0.610 L5 1.475	H1 0 0 0 0 1.6 1 1 1 1 1 A1+A	.750 .750 .750 .775 .775 .775	A1 0.542 0.542 0.542 H3 0.300 0.300	0.875 0.875 0.875 A3 0.488 0.488	0.: 0.: 0.: L7 0.:	500 500 500 418 418	0.750 0.750 0.750			
section 3 4 5	L1 0.835 0.835 0.835 A2 0.516 0.516 0.516	L2 0.610 0.610 L5 1.475 1.475 A4	H1 0 0 0 1.6 1 1 1 A1+A A3+A	.750 .750 .750 .775 .775 .775 .775	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300	0.875 0.875 0.875 A3 0.488 0.488	0.: 0.: 0.: L7 0.:	500 500 500 418 418	0.750 0.750 0.750			
section 3 4 5 section 3 4 5 section 3 section 3 3	L1 0.835 0.835 0.835 A2 0.516 0.516 0.516 H4	L2 0.610 0.610 L5 1.475 1.475 A4	H1 0 0 16 1 1 A1+A A3+A	.750 .750 .750 .775 .775 .775 .775 \\\\\\\\\\\\\\\\\\\	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300 ave	0.875 0.875 0.875 A3 0.488 0.488 0.488 distance(m)	0.: 0.: 0.: L7 0.: 0.: volume(m	500 500 500 418 418 418	0.750 0.750 0.750			
section 3 4 5	L1 0.835 0.835 0.835 A2 0.516 0.516 0.516 H4 2.000 2.000	L2 0.610 0.610 L5 1.475 1.475 1.475 A4 0.835 0.835	H1 0 0 0 0 1.6 1 1 1 A1+A3+A 2 2 2	.750 .750 .750 .775 .775 .775 .775 \\\\\\\\\\\\\\\\\\\	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300 ave	0.875 0.875 0.875 A3 0.488 0.488 0.488 distance(m)	0.: 0.: 0.: L7 0.: 0.: volume(m	500 500 500 418 418 418 418 3)	0.750 0.750 0.750			
section 3 4 5 section 3 4 5 section 3 section 3 3	L1 0.835 0.835 0.835 A2 0.516 0.516 0.516 H4	L2 0.610 0.610 L5 1.475 1.475 A4	H1 0 0 0 0 1.6 1 1 1 A1+A3+A 2 2 2	.750 .750 .750 .775 .775 .775 .775 \\\\\\\\\\\\\\\\\\\	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300 ave	0.875 0.875 0.875 A3 0.488 0.488 0.488 distance(m)	0.0 0.0 0.1 L7 0.4 0.4 volume(m	500 500 418 418 418 33) 389	0.750 0.750 0.750			
section 3 4 5	L1 0.835 0.835 0.835 A2 0.516 0.516 0.516 H4 2.000 2.000	L2 0.610 0.610 L5 1.475 1.475 1.475 A4 0.835 0.835	H1 0 0 0 0 1.6 1 1 1 A1+A3+A 2 2 2	.750 .750 .750 .775 .775 .775 .775 \\\\\\\\\\\\\\\\\\\	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300 ave	0.875 0.875 0.875 A3 0.488 0.488 0.488 distance(m)	0.: 0.: 0.: L7 0.: 0.: volume(m	500 500 418 418 418 33) 389	0.750 0.750 0.750			
section 3 4 5	D1 0.835 0.835 0.835 A2 0.516 0.516 0.516 H4 2.000 2.000 2.000	L2 0.610 0.610 L5 1.475 1.475 1.475 A4 0.835 0.835	H1 0 0 0 0 1.6 1 1 1 A1+A3+A 2 2 2	.750 .750 .750 .775 .775 .775 .775 \\\\\\\\\\\\\\\\\\\	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300 ave	0.875 0.875 0.875 A3 0.488 0.488 0.488 distance(m)	0.0 0.0 0.1 L7 0.4 0.4 volume(m	500 500 418 418 418 33) 389	0.750 0.750 0.750		1820	
section 3 4 5	L1 0.835 0.835 0.835 A2 0.516 0.516 0.516 H4 2.000 2.000	L2 0.610 0.610 L5 1.475 1.475 1.475 A4 0.835 0.835	H1 0 0 0 0 1.6 1 1 1 A1+A3+A 2 2 2	.750 .750 .750 .775 .775 .775 .775 \\\\\\\\\\\\\\\\\\\	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300 ave	0.875 0.875 0.875 A3 0.488 0.488 0.488 distance(m)	0.0 0.0 0.1 L7 0.4 0.4 volume(m	500 500 418 418 418 33) 389	0.750 0.750 0.750		18.29	1 m ³
section 3 4 5	L1 0.835 0.835 0.835 A2 0.516 0.516 0.516 44 2.000 2.000 2.000	L2 0.610 0.610 L5 1.475 1.475 A4 0.835 0.835	H1 0 0 0 0 1.6 1 1 1 A1+A3+A 2 2 2	.750 .750 .750 .775 .775 .775 .775 \\\\\\\\\\\\\\\\\\\	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300 ave	0.875 0.875 0.875 A3 0.488 0.488 0.488 distance(m)	0.0 0.0 0.1 L7 0.4 0.4 volume(m	500 500 500 418 418 418 33) 389 902	0.750 0.750 0.750		1. 1.1%	
section 3 4 5	L1 0.835 0.835 0.835 A2 0.516 0.516 0.516 44 2.000 2.000 2.000	L2 0.610 0.610 L5 1.475 1.475 1.475 A4 0.835 0.835	H1 0 0 0 0 1.6 1 1 1 A1+A3+A 2 2 2	.750 .750 .750 .775 .775 .775 .775 .42+ .44 .380 .380	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300 ave	0.875 0.875 0.875 A3 0.488 0.488 0.488 distance(m)	0.0 0.0 0.1 L7 0.4 0.4 volume(m	500 500 500 418 418 418 33) 389 902	0.750 0.750 0.750			
section 3 4 5	L1 0.835 0.835 0.835 A2 0.516 0.516 0.516 44 2.000 2.000 2.000	L2 0.610 0.610 0.610 L5 1.475 1.475 A4 0.835 0.835	H1 0 0 0 0 1.6 1 1 1 A1+A3+A 2 2 2	.750 .750 .750 .775 .775 .775 .775 .42+ .44 .380 .380	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300 ave	0.875 0.875 0.875 A3 0.488 0.488 0.488 distance(m)	0.0 0.0 0.1 L7 0.4 0.4 volume(m	500 500 500 418 418 418 33) 389 902	0.750 0.750 0.750		1. 1.1%	
section 3 4 5	L1 0.835 0.835 0.835 A2 0.516 0.516 0.516 44 2.000 2.000 2.000	L2 0.610 0.610 0.610 L5 1.475 1.475 A4 0.835 0.835	H1 0 0 0 0 1.6 1 1 1 A1+A3+A 2 2 2	.750 .750 .750 .775 .775 .775 .775 .42+ .44 .380 .380	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300 ave	0.875 0.875 0.875 A3 0.488 0.488 0.488 distance(m)	0.0 0.0 0.1 L7 0.4 0.4 volume(m	500 500 500 418 418 418 33) 33)	0.750 0.750 0.750			
section 3 4 5	L1 0.835 0.835 0.835 A2 0.516 0.516 0.516 44 2.000 2.000 2.000	L2 0.610 0.610 L5 1.475 1.475 A4 0.835 0.835	H1 0 0 0 1.6 1 1 A1+A A3+A 2 2 2 2	.750 .750 .750 .775 .775 .775 .775 .42+ .44 .380 .380	A1 0.542 0.542 0.542 H3 0.300 0.300 0.300 ave	0.875 0.875 0.875 A3 0.488 0.488 0.488 distance(m)	0.0 0.0 0.1 L7 0.4 0.4 volume(m	500 500 500 418 418 418 33) 33)	0.750 0.750 0.750			

4 /77//77		1 1 7 J	. 4.1		LCULA	ATION		٠. ٠.				RESUL'
ACKFIL	L WITH	GRA	VEL		1 1 1 1 1 1			<u> </u>				
		· · · · · · · · · · · · · · · · · · ·			·		u Circle				en (fr	
section	1		HI		A1		L2		H2	18 1		
3	I			1.850		0.773		0.835		0.540		
4	1			1.850		0.773	<u> </u>	0.835		0.671		
5				1.850				0.835				
section	A2		A1+A		ave	Co. 1 (3.41).	distance	(m)	voli	ıme(m³)	_	
3	 	.451		1.224		1.070		0.00	1	0.101	-	
5		.560		1.333		1.278		* *		3.431		
	U.	.500	- 4.	1.333		1.333		5.000		6.665		
	l		<u> </u>					- · · · · · · · · · · · · · · · · · · ·	L	10.096	ו ב	
V = 1	0.006	1 - 1 - 12 - 12 - 12 - 12 - 12 - 12 - 1		er en er er er er er er er er er er er er er				<u> </u>			- 10 .	10.006 3
ν 1	0.030	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1			North Color		<u> </u>	<u></u>		<u> </u>		10.096 m ³
ONCRE	TE TYPE	· D							<u> </u>	<u> </u>		
OITORES.	LULIE	, ,,,		<u> </u>		<u>entre villedi.</u> Distribution				<u>in 1 milion de la companya de la co</u>	and only	
block	h1	h2		distar	nce I	Ü ,	t	w	- T	V(m³)		
L1	The state of the s) 2		2		2.687	0.150	0.4		0.181	-	
L2	2.671		.671			5.000	0.150	0.4	44 4	0.338		
					100					0.519		
and the second second												
					11/0.50		1012 111		- 1		-	
ONCRET	E: '	V = (0.519								-J	0.519 m^3
ONCRET	TE:	V = (0.519									0.519 m ³
		V = (distar	nce I			A	1 (m²)]	0.519 m ³
se		elevatio			nce I			A	l (m²)			0.519 m ³
se	ection 6	elevatio 5	on	distar	nce I	2.719			1 (m²)			0.519 m ³
se	ection 6	elevatio 5. 5.	on .276	distar 2			0.1	50				0.519 m³
se	ection 6	elevatio 5. 5.	on .276 .400	distar 2	.684	2.719	0.1	50 50	0.40	53		0.519 m ³
se	5 6	elevation 5.5.5.5.	on .276 .400 .400	distar 2. 5.	.684	2.719 5.019 7.738	0.1	50 50	0.40 0.7: 1.10	53		0.519 m³
se	5 6	elevation 5.5.5.5.	on .276 .400 .400	distar 2. 5.	.684	2.719 5.019 7.738	0.1	50 50	0.40 0.7: 1.10	53		0.519 m³
se	ection 6 4 5 6	5 5 5 0.150	.276 .400 .400	distan 2. 5.	.684 .000	2.719 5.019 7.738	0.1	50 50	0.40 0.7: 1.10	53 51		0.519 m³
se	ection 6 4 5 6	elevation 5.5.5.5.	.276 .400 .400	distan 2. 5.	.684	2.719 5.019 7.738	0.1	50 50	0.40 0.7: 1.10	53 51		0.519 m ³
A2= Total=A1	ection 6 4 5 6	5 5 5 0.150	on .276 .400 .400 *	distan 2 5 0 63 m	.684 .000	2.719 5.019 7.738	0.1	50 50	0.40 0.7: 1.10	53 51		
A2= Total=A1	ection 6 4 5 6	5 5 5 0.150	on .276 .400 .400 *	distan 2 5 0 63 m	.684 .000	2.719 5.019 7.738	0.1	50 50	0.40 0.7: 1.10	53 51		0.519 m ³
A2= Total=A1 DRM:	ection 6 4 5 6	5. 5. 5. 0.150 A = 1	on .276 .400 .400 *	distan 2 5 0 63 m	.684 .000	2.719 5.019 7.738	0.1	50 50	0.40 0.7: 1.10	53 51		
A2= Total=A1 DRM:	ection 6 4 5 6	5. 5. 5. 0.150 A = 1	on .276 .400 .400 *	distan 2 5 0 63 m	.684 .000	2.719 5.019 7.738	0.1	50 50	0.40 0.7: 1.10	53 51		
A2= Total=A1 DRM:	ection 6 4 5 6 1+A2=	5. 5. 5. 0.150 A = 1	on .276 .400 .400 * 1.363	distan 2 5 0 63 m	.684	2.719 5.019 7.738	0.1 0.1 000 place	50 50 sees =	0.40 0.7: 1.10	53 51		
A2= Total=A1 DRM: RAVEL:	BEDDIN BEDDIN	elevation 5	on .276 .400 .400 * 1.363	distan 22 55 0. 53 m	.684 .000 .450	2.719 5.019 7.738 3.0	0.1 0.1 0.0 0.1 0.1 0.1	50 50	0.40 0.7: 1.10	0.203		
A2= Total=A1 DRM: Block 3	ection 6 4 5 6 1+A2= BEDDIN k B1	6levatio 5 5 5 0.150 A = 1 G	on .276 .400 .400 * 1.363	distar 2 5 0 0 0 100	.684 .000 .450 **	2.719 5.019 7.738 * 3.0	0.1 0.1 000 placence(m) 2.684	50 50 sees =	0.44 0.73 1.11	0.203		
A2= Total=A1 DRM: RAVEL block	ection 6 4 5 6 1+A2= BEDDIN k B1	elevation 5	on .276 .400 .400 * 1.363	distan 22 55 0. 53 m	.684 .000 .450	2.719 5.019 7.738 * 3.0	0.1 0.1 000 place nce(m) 2.684 5.000	50 50 sees =	0.44 0.7: 1.10	0.203		
A2= Total=A1 DRM: Block 3	ection 6 4 5 6 1+A2= BEDDIN k B1	6levatio 5 5 5 0.150 A = 1 G	on .276 .400 .400 * 1.363	distar 2 5 0 0 0 100	.684 .000 .450 **	2.719 5.019 7.738 * 3.0	0.1 0.1 000 placence(m) 2.684	50 50 sees =	0.44 0.73 1.11	0.203		
A2= Total=A1 DRM: RAVEL block 3 4	ection 6 4 5 6 1+A2= BEDDIN k B1	6levatio 5 5 5 0.150 A = 1 G	on .276 .400 .400 * 1.363	distar 2 5 0 0 0 100	.684 .000 .450 **	2.719 5.019 7.738 * 3.0	0.1 0.1 000 place nce(m) 2.684 5.000	50 50 sees =	0.44 0.7: 1.10	0.203		

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE) LOCATION : WF. 65L + 3.0 m \sim WF. 65L + 28.0 m : LEANING WALL-2

LOCATION

1	us Hyjsk				CAI	CUI	LATIC	N						RES	SULT
WI	ET STO	NE MA	SC	NRY		÷						Ser Ma			4.1.4
								٠	44.5						
1	section	L1		L2	H1		Al		L3		H2				
	3	0.4		0.958		.540		1.788		1.558		0.650			
7.	4	0.4		0.984		671	1	1.915		1.584		0.650	1		
4. V	5		50	0.984		671	4	1.915		1.584		0.650		11111	
	section	A2		A1+A2		3	distar	ice(m)	V2((m³)			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
24	3	1.0		2.80		- 1 - 1 - 1									
	4			2.945		.873	1.0	2.684		7.711		1 1.11			
: :	5	1.0	30	2.945	2	.945		5.000		4.726	3.4				
							total	<u> </u>	2	2.437		1.7			
			·							1914					
	V = 22	2.437				<u> </u>				<u> </u>			4 1 1/2	22.43	$7 \mathrm{m}^3$
		<u> </u>			1	<u> </u>			<u> </u>	1 1 1 1	<u> </u>	<u>. 17</u>	3 2 5 5 5 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		
CE	MENT	MORT	AR	POINT	NG		<u> </u>			45.000	<u> </u>	<u>. 1903 j</u>		1	
			<u> </u>			<u> </u>									
		T 1	1	front			7.0				2 4	A1+/	12		
		Ll	(11	stance(m)	Ai	- 12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	L2	dista	ınce(m) A	.2 : :	A. A.	<u>19</u> K		
	4	2.840 2.986		2 60	7	010	0.450			0.4	000	0.0			
-	5	2.986	10.00	2.68 ⁴ 5.000		.818 .931	0.450		2.6		.208	9.0			
-	<u> </u>	2.900		3.000	114.	931	0.450	'	5.0	00 2	.250	17.1			
L		Print with	L						<u> </u>		<u> </u>	26.2	37		
- 4	A = 20	5 207								1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				06.00	7 2
	71 20	J. Z. (7 /)							<u> </u>	North Control	1994 1 74 1	Notes to	1 1 1	26.20	/ m-
Ю	INT FIL	LER						<u> </u>				<u>in erseren</u> en ski			
														6 ,	
	section	Li1	9 h.,	L2	H1	A1	L	3 1	<u>12</u>	A2	A	1+A2			
		3 0.4	50		2.540	1.7			0.650	1.01		2.801			
		4 0.4	50	I	2.671	1.9	- A - A - A - A - A - A - A - A - A - A			1.03		2.945			
		5 0.4	50		2.671	1.9			0.650	1.03		2.945			
			F .								<u> </u>	8.691	e fig.		
			- : '.			114		· .	1 1				in and		
	A = 8.	691					ela j						757	8.691	m^2
						43.75.7		1,110		()	- :		7 3		
		Y . 33 .								ign i i	- 1. 1.		3.75	Person	Task'A
5.3			1				100			1.5		10 100			
1.5		4 1 4			1 6 6		14,75					. 3 4 1 7			
:							1.7	25. J.	6		11.7	14 h.			
			٠						wija ja				3 4 7 7 1		
- 1	<u> </u>							ea Più la	+ 1, 1		a i				
	<u> </u>	<u> </u>				1	1.18						17.		5 + + 1
		<u> </u>		1.6					<u> </u>		- 1			10%1	
1 : 1 :		1.44				1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		7	100	A Break	· · · · · · ·	V 4 - 44 - 1, 1, 1, 1 - 4	1711	· · · · · · · · ·	

		CALC	JLATION			RESULT
WEEP HOL	E				green Tital son	y a february
PVC PIPE ø	50		1, 3			
					gardina di Araba di Araba	
n = 7.684	/3.0			= 3		ng at the same
$L = 3 \times 0.$	85			= 2.550		2.550 m
FILTER CLO	OTH .					
A = 0.640	m ² /place x 3			= 1.920		1.920 m ²
STEEL FEN	ICE					justa i i i
L = 7.738	m					7.738 m
Service 12. 1 Th				ari irrijayuwa		74 JAN 1
SCAFFOLI	ING					Harata i
JOINT OLD				The state of the s		
			front			
	section	L1	distance(m)	A1		
	3	2.840				
	4	2.986	2.684	7.818		
	5	2.986	5.000	14.931		
				22.749		
				n Francisco segui.		
A = 22	.749	. E. Garage and A. Santana				HERALDER L
Teradolla a v						22.749 m ²
■ Company of the Com						22.749 m ²
						22.749 m ²
						22.749 m²
						22.749 m²
						22.749 m²
						22.749 m²
						22.749 m²
1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -						

CALCULATION	RESULT
STRUCTURAL EXCAVATION	
See Attached Table	
V = 237.682	237.682 m ³
BACKFILL WITH SELECTED SOIL	
See Attached Table	
V = 61.951	61.951 m ³
BACKFILL WITH GRAVEL	
See Attached Table	
V = 50.113	50.113 m ³
	a production of the state of th
CONCRETE TYPE D	
See Attached Table	
CONCRETE: V = 1.830	1.830 m ³
	and 100 100 100 100 100 100 100 100 100 10
FORM: $A = 4.201$	4.201 m ²
GRAVEL BEDDING	
See Attached Table	1.42.35
V=2.437 . The second respectively and the first second respectively.	2.437 m ³
WET STONE MASONRY	
See Attached Table	
V = 109.007	109.007 m ³
CEMENT MORTAR POINTING	
See Attached Table	
A = 111.810	111.810 m ²
JOINT FILLER	
See Attached Table	
A = 8.153	8.153 m ²
WEEP HOLE	
PVC PIPE Ø 50	
$n_1 = 27.110/3.00 \mathrm{m} = 9$	
$n_2 = 27.110/3.00 \mathrm{m} = 9$	

$L_1 = 9 \times 0.85$ = 7.650 $L_2 = 9 \times 1.15$ = 10.350 $L_3 = L_1 + L_2$ = 18.000 m	8.000 m
$a_2 = 9 \times 1.15 = 10.350$	3.000 m
	3.000 m
$L = L_1 + L_2 = 18.000 \mathrm{m}$	3.000 m
$L = L_1 + L_2 = 18.000 \mathrm{m}$	3.000 m
FILTER CLOTH	
	1.520 m ²
	des desse si
TEEL FENCE	
$L = 27.110 \mathrm{m}$	7.110 m
L = L + L + L + L + L + L + L + L + L +	7.110 III
CAFFOLDING	
See Attached Table	
and the control of th	9.625 m ²
	7.4
en gang kitabah kerajah di gang pang labah di dibang di bahar bahaja dan bahaja di bahasa keraja keramatan dib	
<u> 보는 도시한 설립 등은 도시 전환은 이 분호의 그림, 기본 장신 시스템 기본 시간 설립 등을</u>	Tajaringka di T
	<u> </u>
	

CALCULATION	RÉSULT
STRUCTURAL EXCAVATION	
See Attached Table	
V = 54.108	54.108 m ³
BACKFILL WITH SELECTED SOIL	
See Attached Table	
V = 18.857	18.857 m ³
BACKFILL WITH GRAVEL	· 14.4 年 17.4 本 1
See Attached Table	
V = 10.393	10.393 m ³
CONCRETE TYPE D	
See Attached Table	a Sabbara
CONCRETE: $V = 0.535$	0.535 m ³
	Value of the Company
FORM: $A = 1.398$	1.398 m ²
GRAVEL BEDDING	
See Attached Table	
V = 1.485	1.485 m ³
WET STONE MASONRY	
See Attached Table	
V = 23.111	23.111 m ³
CEMENT MORTAR POINTING	
See Attached Table	
A = 26.998	26.998 m ²
JOINT FILLER	
See Attached Table	
A = 8.685	8.685 m ²
WEDD HOVE	
WEEP HOLE	
DVC DIDL a 50	
PVC PIPE Ø 50	
n = 7.922 / 3.00 m = 3	
T	
L = 0.90 / 3.00 m = 2.700 m	

CALCULATION CALCULATION	RESULT
FILTER CLOTH	
$A = 0.640 \text{ m}^2 / \text{place x 3 places} = 1.920$	1.920 m ²
STEEL FENCE	
$L = 7.973 \mathrm{m}$	7.973 m
SCAFFOLDING	
See Attached Table	
A = 23.433	23,433 m ²
ur en vier de Verrei en Reimen et de virre de la rementación de la completa de la completa de la completa de v Transferancia de la completa de la c	
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE)
LOCATION : RAILWAY BRIDGE + 20.0 m ~ WF.70L + 13.00 m

CALCULATION		RESULT
STRUCTURAL EXCAVATION		
$L_1 = 1.50 + 0.60 \times 2$	= 2.700	
7 0 700 1 10 0 20 1 1 10 0 70	2.500	
$L_2 = 2.700 + 1.10 \times 0.30 + 1.10 \times 0.50$	= 3.580	
$L_3 = 0.45 + 0.80 / 1.044$	= 1.216	The second of the Case
$L_4 = L_2 - L_5 = 3.850 - 1.500$	= 2.300	
$L_5 = 0.60 + 0.60 + 0.30$	= 1.500	
1. $A_1 = (2.700 + 3.580) \times 1.10 / 2$	= 3.454	
2. $A_2 = (1.216 + 2.300) \times 2.65/2$	= 4.659	
2. A2 = (1.210 / 2.300) X 2.037 2		
$3. A_3 = 0.316 \times 0.20 / 2$	= 0.032	
TOTAL A	= 8.145	
$V = 8.145 \times (260.00 - 25.00)$	= 1914.075	1914.075 m ³
BACKFILL WITH SELECTED SOIL		
DACKTED WITH GELECTED BOIL		
1. $A_1 = (0.60 + 0.60 + 0.80 \times 0.30) \times 0.80/2$	= 0.576	
2. $A_2 = (0.60 + 0.60 + 0.80 \times 0.50) \times 0.80 / 2$	= 0.640	
3. $l_1 = 0.60 + 0.60 + 0.80 \times 0.50$ $l_2 = l_1 + 0.10 = 1.600 + 0.10$	= 1.600 = 1.700	
$A_3 = (1.600 + 1.700) \times 0.10 / 2$	= 0.165	
13 **(1.000 * 1.700) X 0.10 / 2		
4. $A_4 = 0.4 / 1.044 \times (1.75 + 0.15) + 0.40$		
/ 1.044 x 0.20	= 0.805	
TOTALA	= 2.186	
V = 2.196 - (260.00 - 25.00)	512 710	612.010 3
$V = 2.186 \times (260.00 - 25.00)$	= 513.710	513.710 m ³
BACKFILL GRAVEL		
PIROMANA CARTEM	<u>and and a first of the second and a second </u>	or the discount of the second
1. $A_1 = 0.40 / 1.044 \times 1.750$	= 0.670	
		<u> </u>

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE)
LOCATION : RAILWAY BRIDGE + 20.0 m ~ WF.70L + 13.00 m

CALCULATION		RESULT
$2. A_2 = 0.80 / 1.044 \times 1.20$	= 0.920	
TOTAL A	1.600	
TOTAL A	= 1.590	
$V = 1.590 \times (260.00 - 25.00)$	= 373.650	373.650 m ³
GRAVEL BEDDING		
$V = 0.15 \times 1.70 \times (260.00 - 25.00)$	= 59.925	59.925 m ³
V 0.13 x 1.70 x (200.00 22.00)	37,723	39.923 III
WET STONE MASONRY		
$A = (0.45 + 0.90) \times 3.10 / 2 + 0.65 \times 1.50$	= 3.068	
$V = 3.068 \times (260.00 - 25.00)$	= 720.980	720.980 m ³
	,20,,00	720.750 III
CEMENT MORTAR POINTING		
7.70	<u> </u>	
$L = 3.10 \times 1.118 + 0.45$	= 3.916	
$A = 3.916 \times (260.00 - 25.00)$	= 920.260	920.260 m ²
CONCRETE TYPE D		
CONCRETE		
$V = 0.45 \times 0.15 \times (260.00 - 25.00)$	= 15.863	15.863 m ³
FORM		
$A_1 = 0.15 \times (260.00 - 25.00)$	= 35.250	
$A_2 = 0.15 \times 0.45 \times 23 \text{ places}$	= 1.553	
	26.000	2<000
TOTAL A	= 36.803	36.803 m ²
JOINT FILLER		
$a = (0.45 \pm 0.90) \times 3.10 / 2 + 1.50 \times 0.65$	= 3.068	
A = 2.048 v.02 places	- 70.56A	70.574
A = 3.068 x 23 places	= 70.564	70.564 m ²

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE)
LOCATION : RAILWAY BRIDGE + 20.0 m ~ WF.70L + 13.00 m

CALCULATION RESULT WEEP HOLE PVC PIPE Ø 50 = (260.00 - 25.00) / 1.800131 = 98.250 $L_1 = 131 \times 0.75$ 104.800 $L_2 = 131 \times 0.80$ $L = L_1 + L_2$ 203.050 203.050 m FILTER CLOTH $A = 0.640 \text{ m}^2/\text{place x } 131 \text{ x } 2$ 167.680 167.680 m² STEEL FENCE L = 260.00 - 25.00235.000 235.000 m SCAFFOLDING $A = 3.10 \times 1.118 \times (260.00 - 25.00)$ 814.463 814.463 m² TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE)
LOCATION : RAILWAY BRIDGE + 35.0 m ~ WF.72R + 32.00 m

CALCULATION		RESULT
STRUCTURAL EXCAVATION		en en en en en en en en en en en en en e
1. $H = 2.365 \text{ m}$		
	1016	
$L_1 = 0.45 + 0.80 / 1.044$	= 1.216	
$L_2 = 3.580 - 0.60 \times 2 - 0.30 \times 0.50 \times 2$	= 2.080	
$L_2 = 3.380 - 0.60 \times 2 - 0.30 \times 0.30 \times 2$	- 2.000	
$L_3 = 2.700 + 1.10 \times 0.50 + 1.10 \times 0.30$	= 3.580	
		110
$L_4 = (0.50 + 0.10) \times 2 + 1.50$	= 2.700	
$A_1 = (1.216 + 2.080) \times 2.365 / 2$	= 3.898	
$A_2 = (3.580 + 2.700) \times 1.100 / 2$	= 3.454	
TOTAL A	= 7.352	
2. H = 2.557 m		16.8%
	4.014	
$A_1 = (1.216 + 2.080) \times 2.557/2$	= 4.214	
$A_2 = (3.580 + 2.700) \times 1.100 / 2$	= 3.454	
$A_2 = (3.380 \pm 2.700) \times 1.10072$	- 3.434	
TOTAL A	= 7.668	
$V = (7.352 + 7.668) / 2 \times (390.00 - 35.00)$	= 2666.050	2666.050 m ³
BACKFILL WITH SELECTED SOIL		
1. A = $(0.60 + 0.60 + 0.80 \times 0.30) \times 0.80 / 2$	= 0.576	
2. A = $(0.60 + 0.60 + 0.80 \times 0.50) \times 0.80 / 2$	= 0.640	
	1.000	
$3. l_1 = 0.60 + 0.80 \times 0.50$	= 1.000	
$I_2 = 1.000 + 0.10 \times 0.5 \times 2$	= 1.100 = 0.105	
$A = (1.000 + 1.100) \times 0.10 / 2$	= 0.105	
$4. A_1 = 0.40/1.044 \times (1.315 + 0.15)$	= 0.561	
$A_2 = 0.40 / 1.044 \times (1.513 + 0.13)$ $A_2 = 0.40 / 1.044 \times (1.507 + 0.15)$	= 0.635	
$A_2 = 0.407 \cdot 1.044 \times (1.307 + 0.13)$ $A = (A_1 + A_2)/2$	= 0.598	
$\frac{A - (A_1 + A_2)/2}{TOTAL A}$	= 1.919	
	<u>i sa dia dia dia dia dia dia dia dia dia di</u>	
$V = 2.186 \times (260.00 - 25.00)$	= 681.245	681.245 m ³
The state of the control of the cont	<u> 1999 - 1985 - T. F. Frank T. H., 1991 - 1994 - 198</u>	<u>and the state of </u>

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE)
LOCATION : RAILWAY BRIDGE + 35.0 m ~ WF.72R + 32.00 m

CALCULATION		RESULT
BACKFILL GRAVEL		
	0.504	
1. $A_1 = 0.40 / 1.044 \times 1.315$	= 0.504	
$A_2 = 0.40 / 1.044 \times 1.507$	= 0.577	
$A = (A_1 + A_2)/2$	= 0.541	
2. A = $0.80 / 1.044 \times (2.00 - 0.80)$	= 0.920	
TOTAL A	= 1.461	
V 1/41 (200 00 25 00)	710 CCC	610.255 3
$V = 1.461 \times (390.00 - 35.00)$	= 518.655	518.655 m ³
GRAVEL BEDDING		
CAN YEL DEDUNING A 11 - 12 - 13 - 13 - 13 - 13 - 13 - 13 -		
$V = 0.15 \times 1.70 \times (390.00 - 35.00)$	= 90.525	90.525 m ³
7. 0.13 x 1.70 x (320.00 = 33.00)		90.525 111
WET STONE MASONRY		
1. $A_1 = (0.45 + 0.90) \times (1.315 + 2.00 - 0.80) / 2$	= 1.698	
$A_2 = (0.45 + 0.90) \times (1.507 + 2.00 - 0.80) / 2$	= 1.827	
$A = (A_1 + A_2)/2$	= 1.763	
$2. A = 0.65 \times 1.50$	= 0.975	
TOTAL A	= 2.738	
$V = 2.738 \times (390.00 - 35.00)$	= 971.990	971.990 m ³
CEMENT MORTAR POINTING		
$L_1 = (2.365 + 0.30) \times 1.118$	= 2.979	
$L_2 = (2.557 + 0.30) \times 1.118$	= 3.194	
A = (2.070 2.10A) (200.00 2.5.00 4.0	1007.701	A SERVER BOOK
$A_1 = (2.979 + 3.194) \times (390.00 - 35.00) / 2$	= 1095.701	
A = (200.00 25.00) + 0.45	- 160.760	
$A_2 = (390.00 - 35.00) \times 0.45$	= 159.750	
TOTAL A	- 1255 AS1	1255 451 2
The second secon	= 1255.451	1255.451 m ²
	ration for the constant of the first parties.	

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE)
LOCATION : RAILWAY BRIDGE + 35.0 m ~ WF.72R + 32.00 m

CALCULATION		RESULT
CONCRETE TYPE D		
CONCRETE		
$V = 0.45 \times 0.15 \times (390.00 - 35.00)$	= 23.963	23.963 m ³
FORM		
$A_1 = 0.15 \times (390.00 - 35.00)$	= 53.250	
	0.000	
$A_2 = 0.15 \times 0.45 \times 34 \text{ places}$	= 2.295 = 55.545	55.545 m²
Telephone Control of the Control of	= 33.343	33.343 111
TOTAL DILLED 4 10 EL ACTIC MATERIAL		
JOINT FILLER t = 10, ELASTIC MATERIAL		
1. $A_1 = (0.45 + 0.90) \times (1.315 + 2.00 - 0.80) / 2$	= 1.698	
$A_1 = (0.45 + 0.90) \times (1.515 + 2.00 - 0.80) / 2$ $A_2 = (0.45 + 0.90) \times (1.507 + 2.00 - 0.80) / 2$	= 1.827	
$A_2 = (0.45 + 0.50) \times (1.50 + 2.00 + 0.60) \times 2$ $A_1 = (A_1 + A_2)/2$	= 1.763	
$2. A = 0.65 \times 1.50$	= 0.975	
TOTAL A	= 2.738	
$A = 2.738 \times 34 \text{ places}$	= 93.092	93.092 m ²
WEEP HOLE		
PVC PIPE Ø 50		
		and a state of the state of
$\mathbf{n} = (390.00 - 35.00) / 1.800$	= 197	
	4.67.560	
$L_1 = 197 \times 0.75$	= 147.750	
	- 177 200	
$L_2 = 197 \times 0.90$	= 177.300	
	= 325.050	325.050 m
$\mathbf{L} = \mathbf{L}_1 + \mathbf{L}_2$		323.030 111
FILTER CLOTH		
HERECOM		
$A = 0.640 \text{ m}^2 / \text{place x } 197 \text{ x } 2$	= 252.160	252.160 m ²
STEEL FENCE		
L = 390.00 - 35.00	= 355.000	355.000 m
SCAFFOLDING		
$A = (2.979 + 3.194) \times (390.00 - 35.00) / 2$	= 1095.701	1095.701 m ²

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE) LOCATION : WF.74R + 20.0 m \sim WF.78R + 40.0 m

CALCULATION DESCRIPTION OF THE PROPERTY OF THE	RESULT
STRUCTURAL EXCAVATION	MARIE RELEASE
See Attached Table	
V = 1828.115	1828.115 m ³
BACKFILL WITH SELECTED SOIL	
See Attached Table	
V = 514.512	514.512 m ³
	216 F 47.3
BACKFILL WITH GRAVEL	
See Attached Table	
V = 508.832	508.832 m ³
CONCRETE TYPE D	
See Attached Table	
CONCRETE: 14.608 makes the section of the contract of the cont	14.608 m ³
· · · · · · · · · · · · · · · · · · ·	
FORM: $A = 32.461$	32.461 m ²
GRAVEL BEDDING	
See Attached Table	有以其一人 (4)。2
V = 58.430	58.430 m ³
WET STONE MASONRY	
See Attached Table	
V = 770.957	770.957 m ³
CEMENT MORTAR POINTING	
See Attached Table	
A = 944.192	944.192 m ²
JOINT FILLER	连续各位等于包括
See Attached Table	
A = 71.250	71.250 m ²
WEEP HOLE	
PVC PIPE Ø 50	
$n_1 = 216.409 / 1.8 \text{ m} = 390$	
$n_2 = 216.409 / 1.8 \text{ m} = 390$	
$I_1 = 0.8 \mathrm{m/place}$	
$l_2 = 1.0 \mathrm{m/place}$	
	MESS WEAR

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE) LOCATION : WF.74R + 20.0 m \sim WF.78R + 40.0 m

CALCULATION	RESULT
$L_1 = 390 \times 0.8 = 312.0 \text{ m}$	
$L_2 = 390 \times 1.0 = 390.0 \text{ m}$	
$L = L_1 + L_2 = 702.000 \text{ m}$	702.000 m
FILTER CLOTH	
$N = n_1 + n_2 = 780$	
$\mathbf{N} = \mathbf{n}_1 + \mathbf{n}_2 = -780$	
$A = 0.640 \text{ m}^2/\text{place} \times 780 = 499.200$	499.200 m ²
STEEL FENCE (GALVANIZED)	
$L = 216.409 \mathrm{m}$	216.409 m
SCAFFOLDING	
See Attached Table	047,900 2
A = 846.808	846.808 m ²
에 가는 살이 가는 것으로 생각하는 것이 없는 것이 없었다. 사람들이 있는 것으로 가장 되는 것을 보는 것으로 가장 되었다. 그는 것으로 보다 것으로 보다 되었다. 기가는 것으로 가장 사용하는 것으로 가장 하는 것으로 가장 하는 것으로 보는 것을 보고 있다. 그런 것으로 보고 있다. 그런 것으로 보고 있다. 그런 것으로 보고 있다. 그런 것으로 보고 있다.	

LEANING WALL (WET STONE MASONRY TYPE) LOCATION: WF.74R+20m \sim WF.78R+40m

	1.	. Å		177	i.			į.					i 			Ź			• •						
	volume(m³)		108.373	84.475	84.475	84.475	84.475	84.475	84.475	84.475	84 475	84.475	84.475	84.475	84.475	84.475	84.475	84,475	84.475	84.475	84.475	84.475	114.717	1828.115	
V	volu		ľ																				Ŀ		
errogen eyeneselekteri	distance(m)		12.829	10.000	10.000	10.000	10:000	10.000	10.000	10.000	10:000	10.000	10.000	10:000	10.000	10:000	10.000	10,000	10.000	10.000	10.000	10.000	13,580		
10.00	avc		8,448	8.448	8,443	8.448	8.448	8.448	8.448	8.448	8,448	8.448	8.448	8.448	8.448	8.448	8,448	8,448	8.448	8,448	8.448	8.448	8.448		
CALCULATION FOR STRUCTURAL EXCAVATION	A1+A2+A3	8.448	8.448	8.448	8,448	8.448	8.448	8,448	8 448	8.448	8.448	8.448	8.448	8.448	8.448	8.448	8.448	8.448	8.448	8 448	8.448	8.448	8.448		
EXCA	A3)	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540	0.540		
URAL	H3	0.300	0.300	0.300	0.300	0300	0.300	0.306	0.300	0.300	0.300	0.300	0.300	0.300	0.300	0300	0.300	0.300	0300	0.300	0.300	0.300	0.300		
RUCT	9	1.950	1.950	1.950	1.950	1.950	1.950	1.950	1.950	1.950	1.950	1 950	1.950	1.950	1.950	1.950	1.950	1.950	1.950	1.950	1.950	1.950	1.950		
OR ST	1.5	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650	1.650		l N
TION F	A2	2.745	2.745	2.745	2.745	2,745	2.745	2.745	2.745	2,745	2.745	2.745	2.745	2.745	2.745	2.745	2.745	2,745	2.745	2.745	2.745	2.745	2.745	1.5	
CULAT	Н2	006'0	0060	0.900	0.900	0.900	0060	0.900	0060	0.000	0060	0.000	0060		0.900	0.900	0.900	006.0	0.900	0.900	0.900	0.000	0.000		
- 1	1.4	2.600	2.600	2.600	2.600	2.600	2.600	2.600	2,600	2,600	2.600	2.600	2.600	2.600	2,600	2.600	2.600	2,600	2,600	2.600	2.600	2.600	2.600		
TABLE.	1.3	3.500	3,500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3,500		
Ţ	A1	5.163	5.163	5,163	5:163	5.163	5.163	5.163	5.163	5.163	5.163	5.163	5.163	5.163	5.163	5.163	5.163	5.163	5.163	5.163	5.163	5.163	5.163		
	HI	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3,500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500	3.500		Č
	1.2	1.700	1.700	1.700	1.700	1,760	1.700	1.700	1.700	1.700	1.700	1.700	1.700	1.700	1.700	1.700	1.700	1,700	1.700	1.700	1.700	1,700	1.700		
	11	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1.250	1,250	1.250	1.250		
	section		2	3	4	2	9	7	6 0	6	10	Ξ	12	13	14	5	9	17	18	19	ଯ	21	22		

						TARIE	- 1		A TY	Z.	2 2	K E11 I	CALCITI ATTON FOR BACKETT WITH SELECTED SOIT	CEI E	THE CHILL	HQ5					
section	12	1.2	IHI	[V	[1]	[7 H2		A2		() ()		12		1 1 1	1/2		A1+A2+A3+A4		ave	distance(m)	Volumetra
	0.950	0.500	0.000	0.653	0 0 20	0.500	0000	0.653	1.650	1.750	0.100	0.170	0.475			0.903		2.378	1		
2	0.950	0.500	006'0	0.653	0.950	0.500	0.000	0.653	1.650	1.750	0.100	0.170	0.475	1.900		0.903	10 10 10	2.378	2.378	12.829	30.
e.	0.950	0.500	0.900	0.653	0.950	0.500	006.0	0.653	1.650	1.750	0.100	0.170	0.475	1,900		0.903	V	2.378	2.378	10.000	
4	0.950	0.500	0060	0.653	0:620	0.500	006 0	0.653	1.650	1.750	0.100	0.170	0.475	Г		0.903		2.378	2.378	10.000	23.
<u>`</u>	0.950	0.500	0.900	0.653	0.950	0.500	006.0	0.653	1.650	1.750	0.100	0.170	0.475	1.900		0.903		2.378	2378	10.000	L
9		0.500	0.000			0.500	006'0	0.653	1.650	1.750	0.100	0.170	0.475	1.900		0.903		2.378	2.378	10.000	
7	0.950	0.500	0.900		0.950	0.500	0.900	0.653	1.650	1.750	0.100	0.170	0.475	1.900		0.903		2.378	2.378	10.000	
8	0.950	0.500	0.600	0.653	0.950	0.500	0.900	0.653	1.650	1.750	0.100	0.170	0.475	2006:1		0.903		2.378	2.378	10.000	Ŀ
6	0.950	0.500	0.000	0.653	0.950	0.500	0.900	0.653	1.650	1.750	0.100	0.170	0.475	1.900		0.903	1	2.378	2.378	10.000	L
2	0.950	0.500	0.000	0.653	0.950	0.500	0.900	0.653	1 650	1.750	0.100	0.170	0.475	1.80		0.903		2.378	2.378	10.000	L
=	0.950	0.500	0.900	0.653	0.050	0.500	0.000	0.653	1.650	1.750	0.100	0.170	0.475	1.900		0.903		2.378	2.378	10.000	
2	0.950	0.200	0.900	0.653	0.950	0.500	006.0	0.653	1.650	1.750	0.100	0.170	0.475	1.900		0.903		2.378	2.378	10.000	
13	0.950	0.500	0060		0.950	0.500	0.000	0.653	1.650	1.750	0.100	0.170	0.475	1.900		0.903		2.378	2378	10.000	23.7
14	0.950	0.500	0.900		0.950	0.500	0.000	0.653	1.650	1.750	0.100	0.170	0.475	1.900		0.903		2.378	2.378	10.000	
15		0.500	0.900		-	0.500	0.000	0.653	1.650	1.750	0.100	0.170	0.475	1.900	1	0.903		2.378	2.378	10.000	1
9	0.950		0.900		0.950	0.500	0060	0.653	1.650	1.750	0.100	0.170	0.475	1.900	1.00	0.903	. 4, 2, .	2.378	2.378	10.000	23.7
17	0.950	-	0.900		0.950	0.500	006.0	0.653	1.650	1.750	0.100	0.170	0.475	1.900	1.00	0.903		2.378	2.378	10:000	23.7
≈	-	7.1	0000		0.950	0.500	0.90	0.653	1.650	1.750	0.100	0.170	0.475	1.900	NC-11	0.903	2000	2.378	2.378	10.000	23.7
<u></u>		$\overline{}$	8		0.950	0.500	0.00	0.653	1.650	1.750	0.100	0.170	0.475	1.900		0.903		2.378	2.378	10.000	23.7
ଛ	1111	0,500	0060		•	0.50 80	800	0.653	1.650	- 1	0 18	0.170	0.475	1.000	- 1 - 2 - 2	0:503		2.378	2.378	10.000	33.7
21	~ t	28	0000		. Į	0.500	80	0.653	1 650	1.750	0.100	0.170	0.475	1,900	1	0.903		2.378	2.378	10.000	23
22	0.950	0.00	0.000	0.653	0.050	0.500	0000	0.653	1.650	1.750	0.100	0.170	0.475	1.900	£.;	0.903		2.378	2.378	13.580	32.2
		-	1				· .	2	-		_							-			2 7 1 2

LEANING WALL (WET STONE MASONRY TYPE) LOCATION: WF.74R+20m \sim WF.78R+40m

TABLE. CALCULATION FOR BACLFILL WITH GRAVEL

section	LI	HI	Al	ΑI	L2	112	A2	A1+A2	ave	distance(m)	volunc(m³)
I	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	4.00		
2	0.475	1.750	0.831	0.831	0.950	1,600	1.520	2.351	2.351	12.829	30.164
3	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23,513
4	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
- 5	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10,000	23.513
6	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
7	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
8	0.475	1.750	0,831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
9	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
10	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
11	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
12	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2:351	2.351	10.000	23.513
13	0,475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
14	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
15	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
16	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
17	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
18	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
19	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
20	0.475	1.750	0.831	0.831	0.950	1.600	1,520	2,351	2.351	10.000	23.513
21	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	10.000	23.513
22	0.475	1.750	0.831	0.831	0.950	1.600	1.520	2.351	2.351	13.580	31.930
					14年2月	W	LL 6 1 1 1	\$10 E	: .		508.832

TABLE. CALCULATION FOR RUBBLE STONE BEDDING

	4 ()		
block	i " " .	distance	V(m³)
LI	0.15	12.829	3.464
1.2	0.15	10.000	2.700
L3	0.15	10.000	2.700
I.4	0.15	10.000	2.700
L5	0.15	10.000	2.700
L6	0.15	10.000	2.700
L7	0.15	10.000	2.700
L8	0.15	10.000	2.700
L.9	0.15	10.000	2.700
L10	0.15	: 10.000	2.700
LII	0.15	10.000	2.700
L12	0.15	10.000	2.700.
L13	0.15	10.000	2.700
L14	0.15	10.000	2.700
LI5	0.15	10.000	2.700
L16	0.15	10.000	2.700
L17	0.15	10.000	2.700
L18	0.15	10.000	2.700
L19	0.15	10.000	2.700
L20	0.15	10,000	2.700
L21	0.15	13.580	3.667
		216.409	58,430

TABLE. CALCULATION FOR WET STONE MASONRY

section	Li	L2	HI	A1	ave	distance(m)	V1(m³)	L3	H2	A2	distance(m)	V2(m³)	V1+V2(m³)
1	0.450	0.900	3.500	2.363	3, 7		14 J. F	1.600	0.750	1.200	N 705 65		57 THE 1 TO 1 TO 1
2 .	0.450	0.900	3.500	2.363	2.363	12.829	30.309	1.600	0.750	1.200	12.829	15.395	45.703
3	0,450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
4	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
5	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
6	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
7	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
8	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
9	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
10	0,450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
11	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
12	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
. 13	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
14	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
. 15	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
16	0.450	0.900	3.500	2.363	2.363	10,000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
17	0.450	0.900	3,500	2.363	2.363	10.000	23.625	1.600	0.750	1,200	10.000	12.000	35.625
18	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
. 19	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
20	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
21	0.450	0.900	3.500	2.363	2.363	10.000	23.625	1.600	0.750	1.200	10.000	12.000	35.625
22	0.450	0.900	3.500	2.363	2.363	13.580	32.083	1.600	0.750	1.200	13.580	16.296	48.379
						1 4	511.266			Quality 1	total	259.691	770.957

LEANING WALL (WET STONE MASONRY TYPE) LOCATION: WF.74R+20m ~ WF.78R+40m

Table. Calculation for Cement Mortal Pointing

18 18 18 18 18 18 18 18 18 18 18 18 18 1							
					Тор		A1+A2
block	H2	distance	A1	Ll	distance	A2	
L1	3.913	12.829	50.200	0.450	12.829	5.773	55,973
L2	3.913	10.000	39,130	0.450	10.000	4.500	43,630
L3	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L4	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L5	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L6	3.913	10.000	39.130	0.450	10.000	4.500	43,630
L7	3.913	10.000	39.130	0.450	10.000	4.500	43,630
L8	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L9	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L10	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L11	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L12	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L13	3.913	10.000	39.130	0.450	10,000	4.500	43.630
L14	3.913	10,000	39.130	0.450	10.000	4.500	43.630
L15	3.913	10.000	39.130	0.450	10.000	4.500	43,630
L16	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L17	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L18	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L19	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L20	3.913	10.000	39.130	0.450	10.000	4.500	43.630
L21	3.913	13.580	53.139	0.450	13.580	6.111	59.250
	% 1		14,247				944.192

Table. Calculation for Concrete(Top Concrete)

block	L	t	W	V(m3)
L1	12.829	0.150	0.450	0.866
L2	10.000	0.150	0.450	0.675
L3	10.000	0.150	0.450	0.675
I.A	10,000	0.150	0.450	0.675
L5	10.000	0.150	0.450	0.675
L6	10.000	0.150	0.450	0.675
L.7	10.000	0.150	0.450	0.675
L8	10.000	0.150	0.450	0.675
L9	10.000	0.150	0.450	0.675
L10	10.000	0.150	0.450	0.675
LII	10.000	0.150	0.450	0.675
L12	10.000	0.150	0.450	0.675
L13	10.000	0.150	0.450	0.675
L14	10.000	0.150	0.450	0.675
L15	10,000	0.150	0.450	0.675
L16	10.000	0.150	0.450	0.675
L17	10.000	0.150	0.450	0.675
L18	10.000	0.150	0.450	0.675
L19	10.000	0.150	0.450	0.675
L20	10.000	0.150	0.450	0.675
L21	13.580	0.150	0.450	0.917
				14.608

LEANING WALL (WET STONE MASONRY TYPE) LOCATION: WF.74R+20m ~ WF.78R+40m

 (Top	Concre	ete)

	(T	op Concre	ete)	
block	distance	L	w	A(m2)
LI	12.829	12.829	0.150	1.924
L2	10,000	10.000	0.150	1.500
L3	10.000	10.000	0.150	1.500
L4	10,000	10.000	0.150	1.500
L5	10.000	10.000	0.150	1.500
L6	10.000	10.000	0.150	1,500
L7	10.000	10.000	0.150	1.500
L8	.10.000	10.000	0.150	1.500
L9	10.000	10.000	0.150	1.500
L10	10.000	10.000	0.150	1.500
LII	10.000	10.000	0.150	1.500
L12	10.000	10.000	0.150	1.500
L13	10.000	10.000	0.150	1.500
L14	10.000	10.000	0.150	1.500
L15	10.000	10.000	0.150	1.500
L16	10.000	10.000	0.150	1.500
L17	10.000	10.000	0.150	1.500
L18	10.000	10.000	0.150	1.500
L19	10.000	10.000	0.150	1.500
L20	10.000	10.000	0.150	1.500
L21	13.580	13.580	0.150	2.037
		216.409		32.461

section L1 L2 H1 A1 L3 H2 A2 total T2(m2) 1 0.450 0.900 3.500 2.363 1.600 0.750 - 2 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 3 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 4 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 5 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 6 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 8 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 10 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 11 0.450 0.900			12	ibie, Ca	iculatio	n for Joi	nt riner	100	<u>politic desperanta de la compansa d</u>
2 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 3 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 4 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 5 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 6 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 7 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 8 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 9 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 10 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 11 0.45	section	Ll 💠	L2	HI	A1	L3	H2	A2	total T2(m2)
3 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 4 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 5 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 6 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 7 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 8 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 9 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 10 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 11 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 12 0.4		0.450	0.900	3.500	2.363	1.600	0.750		
4 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 5 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 6 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 7 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 8 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 9 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 10 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 11 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 12 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 12 0.		0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
5 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 6 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 7 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 8 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 9 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 10 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 11 0.450 0.990 3.500 2.363 1.600 0.750 1.200 3.563 12 0.450 0.990 3.500 2.363 1.600 0.750 1.200 3.563 12 0.450 0.990 3.500 2.363 1.600 0.750 1.200 3.563 14 0	3	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
6 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 7 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 8 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 9 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 10 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 11 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 12 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 13 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 14 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 15	4	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
7 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 8 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 9 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 10 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 11 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 12 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 13 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 14 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 15 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 16 <td< td=""><td>5</td><td>0.450</td><td>0.900</td><td>3.500</td><td>2.363</td><td>1.600</td><td>0.750</td><td>1.200</td><td>3.563</td></td<>	5	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
8 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 9 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 10 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 11 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 12 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 13 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 14 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 15 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 16 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 17 <t< td=""><td>6</td><td>0.450</td><td>0.900</td><td>3.500</td><td>2.363</td><td>1.600</td><td>0.750</td><td>1.200</td><td>3.563</td></t<>	6	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
9 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 10 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 11 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 12 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 13 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 14 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 15 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 16 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 17 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 18 <	7	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
10 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 11 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 12 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 13 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 14 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 15 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 16 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 17 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 18 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 19	8	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
11 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 12 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 13 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 14 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 15 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 16 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 17 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 18 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 19 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 20	9	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
12 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 13 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 14 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 15 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 16 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 17 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 18 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 19 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 20 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 21	10		0.900		2.363	1.600	0.750	1.200	3,563
13 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 14 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 15 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 16 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 17 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 18 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 19 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 20 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 21 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 21	11	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
14 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 15 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 16 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 17 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 18 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 19 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 20 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 21 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 21 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 22	12	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
15 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 16 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 17 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 18 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 19 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 20 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 21 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 21 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 22 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563	13	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
16 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 17 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 18 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 19 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 20 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 21 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 22 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 22 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563	14	0.450	0.900			1.600	0.750	1.200	3.563
17 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 18 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 19 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 20 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 21 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 22 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 22 0.450 0.900 3.500 2.363 1.600 0.750 - -	15	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3,563
18 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 19 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 20 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 21 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 22 0.450 0.900 3.500 2.363 1.600 0.750 - -	16	0.450	0.900			1.600	0.750	1.200	3.563
19 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 20 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 21 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 22 0.450 0.900 3.500 2.363 1.600 0.750 - -	17	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
20 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 21 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 22 0.450 0.900 3.500 2.363 1.600 0.750 - -	18	0.450		3.500	2.363	1.600	0.750	1.200	3.563
21 0.450 0.900 3.500 2.363 1.600 0.750 1.200 3.563 22 0.450 0.900 3.500 2.363 1.600 0.750 - -	19	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
22 0.450 0.900 3.500 2.363 1.600 0.750 -	20	0.450	0.900	3.500	2.363	1.600	0.750		3.563
	21	0.450	0.900	3.500	2.363	1.600	0.750	1.200	3.563
71.250	22	0.450	0.900	3.500	2.363	1.600	0.750	-	
							1.		71.250

Table. Calculation for Scaffolding

		fro	nt	
block	H1	H2	distance	Al
Li	3.913	3.913	12.829	50.200
L2	3.913	3.913	10,000	39.130
L3	3.913	3.913	10.000	39.130
L4	3.913	3.913	10.000	39.130
L5	3.913	3.913	10.000	39.130
L6	3.913	3.913	10.000	39.130
L7	3.913	3.913	10.000	39.130
L8	3.913	3.913	10.000	39.130
L9	3.913	3.913	10.000	39.130
L10	3.913	3.913	10.000	39.130
LII	3.913	3.913	10.000	39.130
L12	3.913	3.913	10.000	39.130
L13	3.913	3.913	10.000	39.130
L14	3.913	3.913	10.000	39.130
L15	3.913	3.913	10.000	39.130
L16	3.913	3.913	10.000	39.130
L17	3.913	3.913	10.000	39.130
L18	3.913	3.913	10.000	39.130
L19	3.913	3.913	10.000	39.130
L20	3.913	3.913	10.000	39.130
L21	3.913	3.913	13.580	53.139
	i in in in in in in in in in in in in in			846.808

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE)
LOCATION : WF.91R + 25.0 m ~ WF.94R + 22.0 m

CALCULATION		RESULT
STRUCTURAL EXCAVATION		
$A = (3.50 + 5.305) \times \frac{1}{2} \times 1.35 + (1.55 + 2.20)$		
	14.006	
$V = 14.01 \times (150.00 + 6.00 + 1.50) = $	2206.600	2206.600 m ³
BACKFILL WITH SELECTED SOIL		
$A = (0.70 + 1.85) \times \frac{1}{2} \times 1.15 + (0.70 + 1.054)$		
$x \frac{1}{2} \times 1.05 + (0.50 \times 2.795) =$	3.785	
$V = 3.785 \times (150.00 + 6.00 + 1.50)$	596.138	596.138 m ³
BACKFILL GRAVEL		
$A_1 = (0.50 \times 2.795) + (1.00 \times 2.236)$	3.634	
$V_1 = 3.634 \times 150.00$	545.100	
$A_2 = (0.50 \times 2.795)$	1.398	
$V_2 = (3.634 + 1.398) \times \frac{1}{2} \times 6.00 =$	15.096	
$V_3 = 1.398 \times 1.50$	2.097	
	562.293	562.293 m ³
GRAVEL BEDDING		1,344,34
$V = 0.15 \times 2.30 \times (150.00 + 6.00 + 1.50 + 0.10 \times 2) =$	54.407	54.407 m ³
WET STONE MASONRY		
$A_1 = (0.45 + 1.20) \times \frac{1}{2} \times 4.60 + 0.90 \times 2.10 =$	5.685	
$V_1 = 5.685 \times 150.00 =$	852.750	
$A_2 = (0.45 + 1.20) \times \frac{1}{2} \times 3.50 + 0.90 \times 2.10 =$	4.778	
$A_2 = (0.45 + 1.20) \times \% \times 3.50 + 0.90 \times 2.10 =$	* **.//0	
$V_2 = (5.685 + 4.778) \times \frac{1}{2} \times 6.00$	31.389	
$V_3 = 4.778 \times 1.50$ = TOTAL $(V_1 + V_2 + V_3)$ =	7.167 891.306	891.306 m ³
$TOTAL (V_1 + V_2 + V_3) =$. 071.300	ווו סטכ. ו כס

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE)
LOCATION : WF.91R + 25.0 m ~ WF.94R + 22.0 m

CALCULATION		RESULT
CEMENT MORTAR POINTING		
$A_1 = (0.45 + 5.143) \times 150.00$	= 838.950	
$A_2 = (5.143 + 3.913) \times \frac{1}{2} \times 6.00 + 0.45 \times 6.00$	= 29.868	
$A_2 = (3.143 + 3.913) \times /2 \times 0.00 + 0.43 \times 0.00$	2).000	
$A_3 = (3.913 + 0.45) \times 1.50$	= 6.545	
TOTAL A	= 875.363	875,363 m ²
CONCRETE TYPE D		
CONCRETE TYPE D	<u>tija ot alterational Satisfacial et et et al.</u> Let alteration in et et al.	
CONCRETE		
$V = 0.15 \times 0.60 \times (150.00 + 6.00 + 1.50)$	= 14.175	14.175 m ³
FORM (H < 4,0 m)		
$A_1 = 0.15 \times (150.00 + 6.00 + 1.50)$	= 23.625	
A) - 0.13 x (130.00 + 0.00 + 1.50)	25.025	
$A_2 = 0.15 \times 0.60 \times 18 \text{ places}$	= 1.620	
TOTAL A	= 25.245	25.245 m ²
JOINT FILLER t = 10, ELASTIC MATERIAL		
JOINT FILLER (= 10, ELASTIC MATERIAL		
$A = \{(0.45 + 1.20) \times \frac{1}{2} \times 4.60 + 0.90 \times 2.10\}$		
x 15 places	= 82.275	82.275 m ²
WEEP HOLE		
NVC 2002 - 60		
PVC PIPE Ø 50		
Upper side (L = 0.75 m/pipe)		
$L_1 = 6 \text{ pipes} / 10.00 \text{ m x } 150.00 \text{ x } 0.75 \text{ m/pipe}$	= 67.500	
Middle side (L = 1.00 m/pipe)		
$L_2 = 5 \text{ pipes} / 10.00 \text{ m} \times 150.00 \times 1.00 \text{ m/pipe}$	= 75.00	
T T T T T T T T T T T T T T T T T T T		<u>, salatan 1964.</u> Barangan 19
Lower side (L = 1.20 m/pipe) $L_3 = 6 \text{ pipes} / 10.00 \text{ m} \times 150.00 \times 1.20 \text{ m/pipe}$	= 108.00	
L3 — 0 hibes / 10.00 iii x 150.00 x 1.20 iii/pipe	- 100.00	
TOTAL L	= 250.500	250.500 m

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE)
LOCATION : WF.91R + 25.0 m ~ WF.94R + 22.0 m

CALCULATION	RESULT
FILTER CLOTH	
n = 255 places	
$A = 0.640 \text{ m}^2 / \text{place x } 255 = 163.200$	163.200 m ²
STEEL FENCE (GALVANIZED)	
Y = 100,00 ± 00,00 ± 100	157.500
L = 150.00 + 6.00 + 1.50 = 157.500	157.500 m
SCAFFOLDING	
$A_1 = 4.807 \times 150.00 = 721.050$	
	<u>, e des 16 es de de de 1900.</u> Tales de 1900 de 1900 de 1900 de 1900 de 1900 de 1900 de 1900 de 1900 de 1900 de 1900 de 1900 de 1900 de 1900
$A_2 = (4.807 + 3.913) \times \frac{1}{2} \times 6.00 = 26.160$	
$A_3 = 3.913 \times 1.50 = 5.870$	
TOTAL A = 753.080	753.080 m ²
- 10 - 15 - 15 - 15 - 15 - 15 - 15 - 15	
	Maria Parlati Englis
	in a kind
。	
	<u>. Pîrî Kînê peyênî.</u> Talênê bi ku

LEANING WALL (WET STONE MASONRY TYPE) WF.148L + 22.02 \sim WF.149L TYPE OF WORK:

LOCATION

### STRUCTURAL EXCAVATION A_1 = \{(2.85 + (0.625 + 2.85 + 0.444)\} \times \forall_2 \times 1.25 = 4.231 m^2		CALCULATION	RESULT
$A_{1} = \{(2.85 + (0.625 + 2.85 + 0.444)) \times 1/2 \times 1.25 = 4.231 \text{ m}^{2} \}$ $A_{2} = (2.444 + 1.30) \times 1/2 \times 3.50 = 6.552 \text{ m}^{2} \}$ $A = 10.783 \text{ m}^{2} \}$ $V = 10.783 \times (60.00 + 11.03 \times 2) = 884.853 = 884.9 \text{ m}^{2} \}$ $BACKFILL WITH SELECTED SOIL$ $A_{1} = (0.60 + 1.125) \times 1/2 \times 1.05 = 0.906 \text{ m}^{2} \}$ $A_{2} = (0.75 + 0.80) \times 1/2 \times 0.10 = 0.078 \text{ m}^{2} \}$ $A_{3} = (0.50 + 0.838) \times 1/2 \times 0.95 = 0.636 \text{ m}^{2} \}$ $V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868 = 201.868 \text{ m}^{2} \}$ $BACKFILL WITH GRAVEL$ $A_{1} = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^{2} \}$:
$A_2 = (2.444 + 1.30) \times \frac{1}{2} \times 3.50 = 6.552 \text{ m}^2$ $A = 10.783 \text{ m}^2$ $V = 10.783 \times (60.00 + 11.03 \times 2) = 884.853 = 884.9 \text{ m}^3$ $BACKFILL WITH SELECTED SOIL$ $A_1 = (0.60 + 1.125) \times \frac{1}{2} \times 1.05 = 0.906 \text{ m}^2$ $A_2 = (0.75 + 0.80) \times \frac{1}{2} \times 0.10 = 0.078 \text{ m}^2$ $A_3 = (0.50 + 0.838) \times \frac{1}{2} \times 0.95 = 0.636 \text{ m}^2$ $V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868 = 201.868 \text{ m}^2$ $F BACKFILL WITH GRAVEL$ $A_1 = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^2$		STRUCTURAL EXCAVATION	
$A_2 = (2.444 + 1.30) \times \frac{1}{2} \times 3.50 = 6.552 \text{ m}^2$ $A = 10.783 \text{ m}^2$ $V = 10.783 \times (60.00 + 11.03 \times 2) = 884.853 = 884.9 \text{ m}^3$ $BACKFILL WITH SELECTED SOIL$ $A_1 = (0.60 + 1.125) \times \frac{1}{2} \times 1.05 = 0.906 \text{ m}^2$ $A_2 = (0.75 + 0.80) \times \frac{1}{2} \times 0.10 = 0.078 \text{ m}^2$ $A_3 = (0.50 + 0.838) \times \frac{1}{2} \times 0.95 = 0.636 \text{ m}^2$ $A = 2.460 \text{ m}^2$ $V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868 = 201.868 \text{ m}^2$ $BACKFILL WITH GRAVEL$ $A_1 = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^2$			
$A_2 = (2.444 + 1.30) \times \frac{1}{2} \times 3.50 = 6.552 \text{ m}^2$ $A = 10.783 \text{ m}^2$ $V = 10.783 \times (60.00 + 11.03 \times 2) = 884.853 = 884.9 \text{ m}^3$ $BACKFILL WITH SELECTED SOIL$ $A_1 = (0.60 + 1.125) \times \frac{1}{2} \times 1.05 = 0.906 \text{ m}^2$ $A_2 = (0.75 + 0.80) \times \frac{1}{2} \times 0.10 = 0.078 \text{ m}^2$ $A_3 = (0.50 + 0.838) \times \frac{1}{2} \times 0.95 = 0.636 \text{ m}^2$ $A = 2.460 \text{ m}^2$ $V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868 = 201.868 \text{ m}^2$ $BACKFILL WITH GRAVEL$ $A_1 = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^2$		$A_1 = \{(2.85 + (0.625 + 2.85 + 0.444)) \times \frac{1}{2} \times 1.25 = 4.231 \text{ m}^2\}$	
A = 10.783 m^2 V = $10.783 \times (60.00 + 11.03 \times 2)$ = 884.853	一		
$V = 10.783 \times (60.00 + 11.03 \times 2) = 884.853 \qquad 884.9 \text{ m}^2$ $BACKFILL WITH SELECTED SOIL$ $A_1 = (0.60 + 1.125) \times \frac{1}{2} \times 1.05 = 0.906 \text{ m}^2$ $A_2 = (0.75 + 0.80) \times \frac{1}{2} \times 0.10 = 0.078 \text{ m}^2$ $A_3 = (0.50 + 0.838) \times \frac{1}{2} \times 0.95 = 0.636 \text{ m}^2$ $A = 2.460 \text{ m}^2$ $V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868 = 201.868 \text{ m}^2$ $BACKFILL WITH GRAVEL$ $A_1 = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^2$		$A_2 = (2.444 + 1.30) \times \frac{1}{2} \times 3.50 = 6.552 \text{ m}^2$	
$V = 10.783 \times (60.00 + 11.03 \times 2) = 884.853 \qquad 884.9 \text{ m}^2$ $BACKFILL WITH SELECTED SOIL$ $A_1 = (0.60 + 1.125) \times \frac{1}{2} \times 1.05 = 0.906 \text{ m}^2$ $A_2 = (0.75 + 0.80) \times \frac{1}{2} \times 0.10 = 0.078 \text{ m}^2$ $A_3 = (0.50 + 0.838) \times \frac{1}{2} \times 0.95 = 0.636 \text{ m}^2$ $A = 2.460 \text{ m}^2$ $V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868 = 201.868 \text{ m}^2$ $BACKFILL WITH GRAVEL$ $A_1 = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^2$	<u> </u>		
BACKFILL WITH SELECTED SOIL $A_1 = (0.60 + 1.125) \times \frac{1}{2} \times 1.05$ = 0.906 m² $A_2 = (0.75 + 0.80) \times \frac{1}{2} \times 0.10$ = 0.078 m² $A_3 = (0.50 + 0.838) \times \frac{1}{2} \times 0.95$ = 0.636 m² $A_3 = (0.50 + 0.838) \times \frac{1}{2} \times 0.95$ = 0.636 m² $A_1 = 0.460 \times (60.00 + 11.03 \times 2)$ = 201.868 201.868 m²		A 244 € 1 48 10.783 m ⁻	
BACKFILL WITH SELECTED SOIL $A_1 = (0.60 + 1.125) \times \frac{1}{2} \times 1.05$ = 0.906 m² $A_2 = (0.75 + 0.80) \times \frac{1}{2} \times 0.10$ = 0.078 m² $A_3 = (0.50 + 0.838) \times \frac{1}{2} \times 0.95$ = 0.636 m² $A_3 = (0.50 + 0.838) \times \frac{1}{2} \times 0.95$ = 0.636 m² $A_1 = 0.460 \times (60.00 + 11.03 \times 2)$ = 201.868 201.868 m²		$V = 10.783 \times (60.00 + 11.03 \times 2) = 884.853$	884.9 m³
$A_{1} = (0.60 + 1.125) \times \frac{1}{2} \times 1.05 = 0.906 \text{ m}^{2}$ $A_{2} = (0.75 + 0.80) \times \frac{1}{2} \times 0.10 = 0.078 \text{ m}^{2}$ $A_{3} = (0.50 + 0.838) \times \frac{1}{2} \times 0.95 = 0.636 \text{ m}^{2}$ $A = 2.460 \text{ m}^{2}$ $V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868 = 201.868 \text{ m}$ $A_{1} = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^{2}$			
$A_{1} = (0.60 + 1.125) \times \frac{1}{2} \times 1.05 = 0.906 \text{ m}^{2}$ $A_{2} = (0.75 + 0.80) \times \frac{1}{2} \times 0.10 = 0.078 \text{ m}^{2}$ $A_{3} = (0.50 + 0.838) \times \frac{1}{2} \times 0.95 = 0.636 \text{ m}^{2}$ $A = 2.460 \text{ m}^{2}$ $V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868 = 201.868 \text{ m}$ $A_{1} = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^{2}$			
$A_{1} = (0.60 + 1.125) \times \frac{1}{2} \times 1.05 = 0.906 \text{ m}^{2}$ $A_{2} = (0.75 + 0.80) \times \frac{1}{2} \times 0.10 = 0.078 \text{ m}^{2}$ $A_{3} = (0.50 + 0.838) \times \frac{1}{2} \times 0.95 = 0.636 \text{ m}^{2}$ $A = 2.460 \text{ m}^{2}$ $V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868 = 201.868 \text{ m}$ $A_{1} = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^{2}$	<u> </u>	DACKERY WITH SELECTED SOIL	
$A_{2} = (0.75 + 0.80) \times \frac{1}{2} \times 0.10 = 0.078 \text{ m}^{2}$ $A_{3} = (0.50 + 0.838) \times \frac{1}{2} \times 0.95 = 0.636 \text{ m}^{2}$ $A = 2.460 \text{ m}^{2}$ $V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868 = 201.868 \text{ m}$ $BACKFILL WITH GRAVEL$ $A_{1} = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^{2}$		DACKFILL WITH SELECTED SOIL	
$A_{2} = (0.75 + 0.80) \times \frac{1}{2} \times 0.10 = 0.078 \text{ m}^{2}$ $A_{3} = (0.50 + 0.838) \times \frac{1}{2} \times 0.95 = 0.636 \text{ m}^{2}$ $A = 2.460 \text{ m}^{2}$ $V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868 = 201.868 \text{ m}$ $BACKFILL WITH GRAVEL$ $A_{1} = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^{2}$			
$A_3 = (0.50 + 0.838) \times \frac{1}{2} \times 0.95$ = 0.636 m ² $A = 2.460 \text{ m}^2$ $V = 2.460 \times (60.00 + 11.03 \times 2)$ = 201.868 201.868 m $A_1 = 0.40 \times 2.10 + 0.80 \times 1.55$ = 2.080 m ²		$A_1 = (0.60 + 1.125) \times \frac{1}{2} \times 1.05 = 0.906 \text{ m}^2$	
$A_{3} = (0.50 + 0.838) \times \frac{1}{2} \times 0.95 = 0.636 \text{ m}^{2}$ $A = 2.460 \text{ m}^{2}$ $V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868 = 201.868 \text{ m}^{2}$ $A_{1} = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^{2}$			
$A = 2.460 \text{ m}^2$ $V = 2.460 \text{ x} (60.00 + 11.03 \text{ x} 2) = 201.868 201.868 \text{ m}^2$ $BACKFILL WITH GRAVEL$ $A_1 = 0.40 \text{ x} 2.10 + 0.80 \text{ x} 1.55 = 2.080 \text{ m}^2$		$A_2 = (0.75 + 0.80) \times \frac{1}{2} \times 0.10 = 0.078 \text{ m}^2$	
$A = 2.460 \text{ m}^2$ $V = 2.460 \text{ x} (60.00 + 11.03 \text{ x} 2) = 201.868 201.868 \text{ m}^2$ $BACKFILL WITH GRAVEL$ $A_1 = 0.40 \text{ x} 2.10 + 0.80 \text{ x} 1.55 = 2.080 \text{ m}^2$	P 3. 7	$\Delta_{-} = (0.50 + 0.838) \times \frac{16}{4} \times 0.95$	
$V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868$ 201.868 m BACKFILL WITH GRAVEL $A_1 = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^2$		A3 = (0.50 + 0.050) k // X 0.55	
E BACKFILL WITH GRAVEL $A_1 = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^2$		$A = 2.460 \text{ m}^2$	
$A_1 = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^2$		$V = 2.460 \times (60.00 + 11.03 \times 2) = 201.868$	201.868 m°
$A_1 = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^2$			
$A_1 = 0.40 \times 2.10 + 0.80 \times 1.55 = 2.080 \text{ m}^2$			
	5	BACKFILL WITH GRAVEL	
		A = 0.40 + 2.10 + 0.80 + 1.55	
V = 2.08 x (60.00 + 11.03 x 2) = 170.685 m		A ₁ = 0.40 X 2.10 ± 0.80 X 1.55 = 2.080 m	
		$V = 2.08 \times (60.00 + 11.03 \times 2) = 170.685$	170.685 m³
,"我就是这个大概就是这种是一种,我们都也是自己的。""自己的时候,我们就是这个大概,我们就是这个大概的。""我们就是这一样,我们就是这个人,我们就是这个人,			
☐ RUBBLE STONE BEDDING		DIDDI E CTONE DENDING	
- VODDE STOUD DEDUMA	<u> </u>	AUDDLE STUILD DEDUING	
$A = 0.15 \times (1.75 + 0.10 \times 2) = 0.293 \text{ m}^2$		$A = 0.15 \times (1.75 + 0.10 \times 2) = 0.293 \text{ m}^2$	
$V = 0.293 \times (60.00 + 11.03 \times 2) = 24.044$ 24.044 m		$V = 0.293 \times (60.00 + 11.03 \times 2) = 24.044$	24.044 m ³

TYPE OF WORK : LOCATION :

LEANING WALL (WET STONE MASONRY TYPE) WF.148L + 22.02 \sim WF.149L

1 1	CALCULATION	RESULT
7	WET STONE MASONRY	
		
	$A_1 = (0.45 \times 1.00) \times \frac{1}{2} + 3.80 + (0.80 \times 1.75) = 4.155 \text{ m}^2$	
- '	$V = 4.155 \times (60.00 + 11.03 \times 2) = 340.595$	340.959 m ³
	V — 4.155 X (00.00 T 11.05 X 2)	340.939 III
		Table
r 	SCAFFOLDING	
72 -1		
	$A = 1.118 \times 3.80 \times (60.000 + 11.03 \times 2) = 348.624$	348.624 m ²
7	CEMENT MORTAR POINTING	
	$A = (1.118 \times 3.50 + 0.45) \times (60.000 + 11.03 \times 2) = 358.028$	358.028 m²
5	CONCRETE	Anglia (Arthur Burne) Anglia (Arthur Barthar)
	• CONCRETE (TYPE – D)	
	$A = 0.45 \times 0.15 = 0.068 \text{ m}^2$	
5.2.		
	$V = 0.068 \times (60.00 + 11.03 \times 2) = 5.580$	5.580 m ³
	• FORM (H < 4.0 m)	
<u> </u>	$A_1 = 0.15 \times (60.00 + 11.03 \times 2) = 12.309$	
	$A_2 = 0.15 \times 0.45 \times 9 \text{ places} = 0.608$	
	$\overline{TOTAL} = 12.917$	12,917 m²
		12,717 III

LEANING WALL (WET STONE MASONRY TYPE) WF.148L + 22.02 ~ WF.149L TYPE OF WORK : LOCATION :

CALCULATION	RESULT
♂ JOINT FILTER	
t = 10, ELASTIC MATERIAL	
	B "" "
$A = \{(0.45 + 1.00) \times 1/2 \times 3.80 + (0.80 \times 1.75)\} \times 7 \text{ places}$	
= 29.085	29.085 m ³
29.065	29.063 11
	FAMILY IN
Ø WIPE HOLE	
PVC Pipe Ø 50	
Upper side (L ₁ = 0.75 m/pipe)	
$L_1 = 6 \text{ pipes } \times 0.75 \times 8 \text{ places} = 36.000$	
Les de la companya de	
Middle side $(L_2 = 0.90 \text{ m/pipe})$	
国民 人名英索萨斯特 医乳腺 医连续离子 经过分 医神经征氏法氏征后征 人名西拉里	
$L_2 = 5 \text{ pipes x } 0.90 \text{ x } 8 \text{ places} = 36.000$	
Lower side $(L_3 = 1.05 \text{ m/pipe})$	
$L_3 = 6 \text{ pipes x } 1.05 \text{ x } 8 \text{ places} = 50.400$	
TOTAL = 122.400	122.400 m
Filter Cloth	
$A = 0.64 \text{ m}^2/\text{place} \times 136 \text{ places} = 87.040$	87.040 m ²
5 STEEL FENCE	TALLY BULL
	92.060
$L = 60.00 + 11.03 \times 2 = 82.060$	82.060 m
	<u> </u>

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE) LOCATION : WF.175R + $16.94 \text{ m} \sim \text{WF.}178\text{R}$

CALCULATION		RESULT
STRUCTURAL EXCAVATION		
1. $A_1 = (1.50 + 2.20) \times 3.40 / 2$	= 6.290	
1. $A_1 = (1.30 \pm 2.20) \times 3.4072$	- 0.290	
$2. A_2 = (2.90 + 4.15) \times 1.20 / 2$	= 4.230	
TOTALA	10.520	
TOTAL A	$= 10.520 \mathrm{m}^2$	
$V = 10.520 \times 130.00$	= 1367.600	1367.600 m ³
BACKFILL WITH SELECTED SOIL		
$1. A_1 = 0.50 \times 2.00$	= 1.000	
2. $A_2 = (0.80 + 1.04) \times 0.90 / 2$	= 0.828	
3. $A_3 = (0.50 + 0.95) \times 0.90 / 2 + (0.95 + 1.75)$		
x 0.10/2	= 0.788	
TOTALA	$= 2.616 \mathrm{m}^2$	
IOTALA	- 2.010 III	
$V = 2.616 \times 130.00$	= 340.080	340.080 m ³
BACKFILL GRAVEL		
DACAFILL GRAVEL		
$1. A_1 = 0.510 \times 1.850$	= 0.944	April 1885 April 1885 April 1885 April 1885 April 1885 April 1885 April 1885 April 1885 April 1885 April 1885
A 1 200 1 200	1 026	
$2. \ A_2 = 1.020 \times 1.800$	= 1.836	
TOTALA	$= 2.780 \text{ m}^2$	Vising Vising V
$V = 2.780 \times 130.00$	= 361.400	361.400 m ³
GRAVEL BEDDING		
$A = 0.10 \times 2.10$	= 0.210	
$V = 0.210 \times 130.00$	= 27.300	27.300 m ³
WET STONE MASONRY		
1. $A_1 = (0.45 + 1.20) \times 3.80 / 2$	= 3.135	
A CONTRACTOR OF THE CONTRACTOR		

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE) LOCATION : WF.175R + 16.94 m \sim WF.178R

CALC	ULATION		RESULT
$2. A_2 = 1.90 \times 0.80$		= 1.520	
	TOTAL A	$= 4.655 \text{ m}^2$	
$V = 4.655 \times 130.00$		- 606 150	Z05 1503
V - 4.653 X 150.00		= 605.150	605.150 m ³
CEMENT MORTAR POINTING			
$A = (0.45 + 3.801) \times 130.00$		= 552.630	552.630 m ²
CONCRETE TYPE D			
CONCRETE TYPE D			
$A = 0.150 \times 0.60$		= 0.090	
$V = 0.09 \times 130.00$		= 11.700	11.700 m ³
FORM			
FORIV			
$A_1 = 0.15 \times 130.00$		= 19.500	
$A_2 = 0.15 \times 0.60 \times 15 \text{ places}$		= 1.350	
			2000
	IOIALA	= 20.850	20.850 m ²
JOINT FILLER t = 10, ELASTIC M	ATERIAL		
1. $A_1 = (0.45 + 1.20) \times 3.80 / 2$		= 3.135	
$2. A_2 = 1.90 \times 0.80$		= 1.520	
	A	$= 4.655 \text{ m}^2$	
	$A_1 + A_2$	= 4.033 m	
A = 4.655 x 12 places		= 55.860	55.860 m ²
STEEL FENCE			
L = 130.0			130.000 m
SCAFFOLDING			
JOAF CEDATO			
$A = 4.137 \times 130.0$		= 537.810	537.810 m ²

TYPE OF WORK : LEANING WALL (WET STONE MASONRY TYPE)
LOCATION : WF.175R + 16.94 m ~ WF.178R

CALCULATION	RESULT
WEEP HOLE	
1. UPPER SIDE (I = 0.8 m)	
$L_1 = 1 \text{ pipe} / 3.0 \text{ m} \times 130 \text{ m} \times 0.8 \text{ m} / \text{pipe}$ = 34.667	
2. LOWER SIDE $(l = 1.10 \text{ m})$	yikata (a. a. a. a. ya za ile Nafi
T. = 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	
$L_2 = 1 \text{ pipe} / 3.0 \text{ m} \times 130 \text{ m} \times 1.10 \text{ m} / \text{pipe}$ = 47.667	
TOTALL = 82.334	82.334 m
3. FILTER CLOTH	02.334 111
$n = 130/3 \times 2 = 87$	
$A = 0.64 \text{ m}^2/\text{ place x } 87 = 55.680$	55.680 m ²
· 《主义》:	
	estimation in the second
	<u>to de la companya di mangana di m</u> Tanggana di mangana di m