TYPE OF WORK : REVETMENT FOR SLOPE OF 1:2.0 LOCATION : WF.178R ~ WF.179R (UPPER CHANNEL) LOCATION

CALCULATION		RESULT
STRUCTURAL EXCAVATION		RESOLT
$V = 71.745 \mathrm{m}^3 / 15.0 \mathrm{m} \times 80.00$	= 382.640	382.640 m ³
BACKFILL WITH SELECTED SOIL		
$V = 22.695 \mathrm{m}^3 / 15.0 \mathrm{m} \times 80.00$	= 121.040	121.040 m ³ ;
WET STONE MASONRY		
WEI STUIL MASUIRY		
$V = 22.851 \text{m}^3 / 15.0 \text{m} \times 80.00$	= 121.872	121.872 m ³
ZZ.031 III / 13.0 III & 0.00	121.072	121.0/2 Hr
CEMENT MORTAR POINTING		
$A = 73.500 \text{ m}^3 / 15.0 \text{ m} \times 80.00$	= 392.000	392.000 m ²
WEEP HOLE		
PVC PIPE Ø 50		
n = 53 $L = 8.0 \text{ m} / 15.0 \text{ m} \times 80.0 \text{ m}$	40.669	40.660
L, = 8.0 m / 15.0 m x 80.0 m = 35.0 m at 1.0 m x 80.0 m	= 42.667	42.667 m
FILTER CLOTH		
	= 34.133	34.133 m ²
	34,133	J4.133 III
GABION CYLINDER Ø 500 (GALVANIZED AND CO	OATED WITH PVC)	
n = 20		A STATE
	$= 0.196 \mathrm{m}^2$	
$V = 20 \times 0.196 \times (3.00 + 5.366)$	$= 32.795 \mathrm{m}^3$	32.795 m ³
SOIL FILLING		
$V_1 = 10.0 \times 0.50 \times (3.00 + 5.366)$	- 41 92A	
37 37 37	= 41.830 = 32.795	
	= 9.035	9.035 m ³
		7.033 III
		in a rest

(A			- p-w swap	~~~	7			•											-						
	RESULT			2000			121.915m3			5.600 m3			2.400 m ³			1.867mg			0.23/m3						
	OALCUEATION					() REVETIMENT	22,859 m3/15.0 x 80.0 m = 12/9/5		8 BASE CONCRETE	1.05 m 1 15.0m x 80.0m = 5.6		3 TOP COUCKETE	0.450 m3/15.0m x 80.0m = 2.4		& PARTITION WIALL	0.350 m3/150m x 80.0m = 1.867		@ END WALL	0.33/ m3 x / w/oce	200 100 100 100 100 100 100 100 100 100	200 000 000 000 000 000 000 000 000 000	062 0	3		END WALL STALE C
	TYPE OF WORK: GRAPEL BEDDING	LOCATION:	009	300 200 CONCRETE, TYPE - C4	00000000	000	5000	Sio 400 So GRAVEL BE	500	1	TRION 1	Tools	2000 20 - 10 - 10 - 10 - 10 - 10 - 10 -	052 0 052	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		TOP CONCRETE (2) SCALE 6 SCALE 6					The second secon		STANDA DEPOS SECTION OF PERTINENT (UPPER CHANNEL)	

RESULT	17.600 m3	16.240m²	28,635 nd	0.833 3	86.053m2	109.083m²	\$.954m	
CALCULATION	00NCRE7E	M3 /15,0m x 80,0m = 16.240	m3/1/5.0m x 80.0m = 38.635	m3 / place x / place = 0.893	8ASE CONCRETE 16,135 m=115.0m x 80.0m = 86.053 700 CONCRETE	mx 80,0m= 108,083 x80,0m= 227,099	1 / 1 place X 1/ place = 1	
· CONCORE	3300	3.045 m³ (3)		0.893 70PM	0 845E CC 16,135		1	
, FORM	200 200 200 200 200 200 200 200 200 200	CONGRETE_TYPE_EL . 300_ 100	A CANE	200, 20 200 200 CALINDO	SEALE C SEALE C SEALE C SEALE C SEALE C			
TYPE OF WORK: CONCRETE	\$00 200 CONCRETE, TYPE-	S	2 - 74	2005 05 000 00 000 000 000 000 000 000 0	84			

· ·	4	· ·	****			•	25.	·Z															
RESULT			0.741 +f				0.757 of				0,277 +f				0.055+f								
CALCULATION		O BASE CONCRETE.	N= 0:139 + 1/15.0m x 80.0m = 0.741		5 TOP CONCRETE		W= 0.142 + /13.0m x 80.0m = 0.757		(3) PARTITION WALL	1	111 = 0,052 ++ 15,0m x 80,0m = 0,277		& END WALL		w= 0.055 +f / place x/ place = 0.055								「
	TYPE OF WORK: REIN FORCING SOFT	COCATION		0 43	000 S 000 000 S		50 400 30 GRAVEL BEDDING	<u> </u>		000 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	00 00 00 00 00 00 00 00 00 00 00 00 00	10 100 20 20 20 20 20 20 20 20 20 20 20 20 2	001 002 003	000	NATURE DOMESTICATION OF THE TOTAL TO	TOP CONCRETE (2)		8:	050 (Control of Contr		00 000 001	ō	

	 ·	Y												:			. :			
RESULT			24.763m2		8 588m²			0,853 m2				1.490 m2								
CALCUEATION	(C) TOP CONCRETE(2)		A= 4.643 m3/15.0 mx 80.0m = 24,763	S PARTITION WALL	A = 1.798 m2 /15,0m x 80,0m = 9.589	BASE CONCRETE.		A= 0.160 m / 15,0m x 80,0m = 0.853		(4) END WALL		A= 1,490 m2/ Dace x 1 place = 1,490								
TANDER TANKE			-1-	1 1	SO 400 SO GRAVEL BEDDING SO 100 SO 100 SO 100 SO 100 SO SO SO SO SO SO SO		ON TOOL OF THE PRINCIPLE AND T	ET STONE MASCORY.	200 CELASTIC MATERIAL	- 600 c	od:	GRAVEL BEOOK	TOP CONCRETE (2)		12.1.43710 MATERIAL 0.00000.00.00.00.00.00.00.00.00.00.00.0		S S S S S S S S S S S S S S S S S S S	END WALL	A CAMPAGE AND A	

2.2 Reverment for Channel Side Slope of 1:1.5: REVETMENT FOR SIDE Slope 1:2 AND 1:1.5

TYPE OF WORK

LOCATION

: WF (3L) - WF (-9L)

CALCULATION	RESULT
D.2 : Reverment for side slope 1:1.5	
D.2.1: Structural Excavation	5,289.407 m
D. 2.2 Backfill with Selected soil.	658.140 m
D. 2.3 gravel Bedding.	1,097.189 m
D. 2. 9. Wet stone Masonry.	1,597.004 M
D. 2.5 Cement Mortar Pointing on Riverside Surface of Wet Stone M	us 4,005.003 m
D. 2.6 : Concrete, Type CI Including Formwork	262 954 M
D. 2.7. Deformed Reinforcing Bars	9,836.825 Ks
D. 2.8. Log pile, Dia 150 mm L = 3.00m	1,299 m
D. 2.9 joint Filler, 10mm thick [Elastic Material].	368-802 m
D. 2.10 Weep Hole, Dia somm Including Filter cloth	1,140 Nos
D. 2.11 Gabion Cylinder Dia 500 mm/ Galvanized and Coaled	
with Puc/.	
D. 2-12: Soil Filling	473.317 M
D. 2.13 : Gabion Mattress t = 500 mm/ Galvanized/	제 📗 😅 😘 기상을 보고 🧗
D.2.13: Gabion Mattress t=500 mm/Galvanized/. D.2.14: Rubble stone Filling/Dia 50 to 150 mm/.	
D.2.13: Gabion Mattress t=500 mm/Galvanized/. D.2.19: Rubble stone Filling (Dia 50 to 150 mm/.	
D.2.19: Rubble stone Filling (Dia 50 to 150 mm).	0/
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Revetment for side slope of 1=2 (stone facing type	e/ 2,207.850 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation	2,207.850 M
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation	2,207.850 M
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m
D.2.19: Rubble stone Filling (Dia 50 to 150 mm). D.3: Reverment for Side slope of 1=2 (Stone Facing type D.3.1: Structural Excavation D.3.2: Rubble stone Bedding (Dia 50 to 150 mm).	1,374.638 m

RESULT												:			5,289.9071						658. 190m2			
CALCULATION	D.2.1. Structural Excavation	VI= 1/3.0 x0.75/x693.099} = 1.496.961	1(2.9×0.6) x 693.0989 =1,118.983	16.0x0.80/x1/2 fx698.914 = 1,556.194	1(1.3+3.1/x/2x0.8 fx698.919=1,141.209	5,263.397			V2 = 1605+0.7/x/2x0.10 x5.0029x62= 18.626	105+07/x/2×0,10×5,20gx 2 = 0,629	19.250 = 19.250	13=4/0.5+0.9/x/2x0.20 x 5.007/x2 = 1.402	10.6+1.2/x1/2 x 0.60 x 5.007 fx 2 = 5.408	Y3.	5,289.407		D. 2.2 . Back Fill With Selected Soil	V=1/05+0.6/x/2x0.19x698-919 = 35.663	10.7+1.3/x1/2x0.6/x698 919 =389.098	11.6 + 2.0/x 1/2 x 0.23 x 698.919. = 233.929	7070			
REVETMENT FOR SIDE CLOPE 1: 2 XND 121-5	WF (32) - WF (-92)	2.27		1 moluded D.3.1.		100 mg	// / / / / / / / / / 	10,000	_ {		1.00	0.10	10.5	090	750		78.							《《文···································
TYPE OF WORK:	LOCATION:	O Kevetment ON	3.0 64		/\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		8.0		Part tion will	(A)	4,100,5		30			0.2.2	200	9,/		0.80	7	Ţij.	20	

							,																	
RESULT						1							C	1.097.1891				1.597.009 14	1				4,005.003 th	
CALCULATION	D. 2.3 GRAVEL BEDDING.	VI=/(0.1x1.1/x 623.094) = 68.590	10.5+1.15/x/2 x 0.4 fx 623.099 = 205.621	4/3.7×0.3/×628.619\$ = 697.752	1/0,15+0.335/x/2x0,35/x628.619 = 53.359	\$10.8+0.85/x1/2×0.10 3x 628.619 = 51.861	887 £ 201 = 10 000 000 000 000 000 000 000 000	12=110.5+07/x/20.10x5002/x62 = 18.626	= 0.624	V2	V3=9/0.5+0.6/x/2x010x5.0074x2=0.551	1102+03/x/2x0.10x5.00x/x 2= 0.250	V3	681.8601 1,097.189	D24 Wet stone masonry	V=1/0.5+1.0/x1/2x1.33×693.099 = 627.017	164.507 +0.5/x0.3 fix 695.759 = 969.987	. 400-1651		D. 2 5 . Cement Mortar Pointing on Riverside Susface	A=410.5+0.7/x643 0996	160,5+4.507/x695.759, ==3,233.290	800-500'F 74404	
TYPE OF WORK: REVETMENT FOR SIDE SIOPE 1:2 AND 1:1.5	LOCATION: W= (34) - W= (-94)		O.S. O. Geverner (2) Parities	0.335	1.0 + 1.0 +	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10.35 (a)			020.5	3 2 1 113 180 1 2 145,75% 3 End well		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			0.2.5							《《新···································	

RESULT										9 262.959 m3				10 mg	. 224						02	25. 9,836.825 Kg		1.299. m	
CALCULATION	D. Z. 6 Concrete, Type CI Including Formwork.	10.3×0.6/×5.007 9×62 == 55.878	10.3×0.6/×5.20 /× 2 = 1.872		(0,3x0.2/x5.007/x2 = 2.103	V3=1/10.3×0.6/×648.4194-	13.19 x 0.075 x 0.15/x 439 = 115.565	03+06/x1/2x0.34×648919=87.536		TOTAL 262.959		Deformed Reinforcing Bars.	WI=4(1159×1.5)×0.62} = 1,073.220	16x320.839/x1.09} =2,002.009	2.520/2 = 3.075.	W2=1/(36×1-7/×0.62) = 37.999	16×10.019/x1.09/ = 62.987	= 100.931	2163×1.95/×0.62/ =2,815.067	116×698.919/x1.09/ =4,046.103	021.199,0=	9,836-825	D. 2.8 Log pile Dia 150 mm , L = 3.0 m	933 x 3.00/3 = 1,299	
REVETIMENT FOR SIDE STOPE 1:24ND 1=1.5		1 - 1 JAN V= 1	10.3 10 10 10 10 10 10 10 10 10 10 10 10 10	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 10 1 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	@ End woll 1=935 40.75 V3=1/1	Bace Concrete.	1	D.10 00 T		1159 6 1.5 120 830	10.2, 0.13	(a) = 1, 11, (b) 6.10 Concerned 6	7		120 C	Z X X X	1	1		3.0 M		0.2.8		

													**.	-		-		 · .		1 1		
RESULT												368.802 m			50N 0511							
CALCULATION	D. 2.9 JOINT FILLER, 10 mm thick	A)=4/0.5+1.0/x/2×1.3 3x69 = 62.400	1/0.3 x 623.299/f = 186.988	476	AZ=1/0.3×5.007/×62/ = 93.130	1/2	42 (= 96.250	43=1/0.3×5.007/×29	11	1/2	43	100 5 808 368 302 10 70 7 A Lo 368 .802 10	D. 2. 10 Weep Hole Dia 50 mm		PVC = 04		D 2-11 Gabion cylinder Dia 500 mm	STAN GENERAL STANDERS		· · · · · · · · · · · · · · · · · · ·	から、 かれからない とう するける とれいちのはでいいませんのいにいているのか。	
TYPE OF WORK . REVETMENT FOR SIDE SLOPE 1:2 AND 1:15	WF/34/- WF/-96).	mbot will	, 2°00	623		"" / Sartition will	1.0 564 × 3.0	0303	7 202		0.2.10	12 12 12 12		2.5 + 2.5			× × × × × × × × × × × × × × × × × × ×		The second of th	《《《集书》的《《诗》的诗《文》、《《古》、《《文》、《《文》、《《文》、《文》、《文》、《文》、《文》、《文》、《文》		

TYPE OF WORK:	REVETMENT FOR SIDE STOPE 1:2 AND 1:1.5	CALCULATION	RESULT
LOCATION:	WF/341-WF(-9L)	D. 2.12 5076 Filling	
n 9, 9		V= 1/0.5+1.2/x/2x0.7/x692.094= 382.641	
		1/0.1+0.37/x/2×0.6/x693.099= 90.676	
7.7	0,37	TOTAL 973,317	973.317 m
1		D. 2.13 Gabion Mattress £=500 mm.	
10/50			
		NOTHING TO	
0.2.13.			-
100	130 7 140 106	の とう (1) の事刊 (1) とうできからできない。 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	1
		D. 2-14 RUBBLE STONE FILLING (DIA 50 to 150 MM	
		NOTHING.	
D. 2-19.			
3	NOTHING		
	(1) 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
And the second s			

		,								 	···				_			 		
RESULT		-			2,207.8501				1,379.638m					2,901.653 14						
CALCULATION	D.3 Revetment for side slope of 122.	D.3.1 structured excoudion	V=1/1.2x0.9/x698.919 = 311.239	1×698.919 =1,896.611	2.207.850	D.3.2 Rubble stone Bedding (Dia 50 to 150 mm).	V= 1/3.9+4.1/x1/2x0.9 \$x648.914= 972.621		11	D. 3.3 Stone Facing lova 250 to 900 mm		1/2:0+2.25/x/2.6/x698.919 = 826.728	11.0 × 0.5 /× 698.919 6 = 329.207	70746 2,901.653						
TYPE OF WORK: REVEYAENT FOR SIDE SIDE 1:2 AND 1:1.5	WF (3L) - WF (-9L).		0.3.		K1//	0.3.2		4.1	Color of the second of the sec		2.00	2.3.3	9:0			化对应分离 化二甲二乙酰胺 化二甲酰胺 化二甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基	在这个时间,不是一个一个,不是一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个			

ON. ONOTE OF 12,5 V = 943.200 m,3 ONE OF 12,5 V = 867.592 m3	RESULT
7.5 200 m 7.2,0 7.5,0	
200 m 200 m 7:2,0 592 m	
1.2.0 m	
1:3.0	
1.2.0	
592	
OF 1.1.5 ~ 1:2.0	
357,240 B	
70146	2188,032m

									-		Ŋ	-			·····		·	,		,,,,	<u></u>	pi-1-ai- a-a	 ·	
RESULT											1817.872 n													
CALCULATION		O SLOPE OF 1:1.5	V = 93.040 m3		(2) SLOPE OF 1:20	8 = 1		3 SLOPE OF 11,5~112,0	V = 357240 m3		77202					一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个								
LACKTILL WITH SELECTTO SOIL			(1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	000000000000000000000000000000000000000	X 200	1	1.0	300 Mg	1,500			1 stone	MASORIES	The state of the s	A. F. 600	ero co					S,000 CADAM P (FMCNT 70) COUCHE COUCHE	EMETRAI		
TYPE OF WORK	OCATION				3		7 4)	STA	NDAR	D CR	oss	SECTI	ои с	F RE	VETA	AENT	<u>(su</u>	OPE	4:1.5	<u>51</u>				

RESULT											٠									
		TOTAL	022.17	10,073		1879		207.0		614.299			 							
NOI		1:13~	2,400	7.200		902.0		0.706		101.285 614.299										
CALCULATION		1.2.0	4.850	5.673		3.530				249,499										
		1115	6,400	3,200		2.251				263.515										
			BASE	700		PART.		2ND		REVT.							25			
BEDDING	をある。 のはまのは (を) からぬまる										100.1 FILLE 1.40mm 3000 6.2376 WAIERIAL 3070030	212 1 00011200		000 000 000 000 000 000 000 000 000 00		SCALE B				
GRAVEL					200 200		1 001	16 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 -	300		الم	SOZOO SO CARVEL PANENTINI			CTFE CIT	SCALC.				
TYPE OF WORK:	LOCATION				866 92		033	65	<u>च</u> .81			LLASTIC MATERIAL	X		> 100 mm				· · · · · · · · · · · · · · · · · · ·	

	T	7	T	Ť	T	7	T	T	.	7	Т		,	3	1	Ţ	 	~			·	-	
RESULT														421.760 M								12 m	
CALCULATION		a score or 127.5		V = 270,874 m3		3 SLOPE OF 112,0		V= 248,441 m3		(3) SLOPE OF 111,5~11.3.D		V = 102, 445		772				· · · · · · · · · · · · · · · · · · ·		「			
STONE MASONRY						NWL CA	1800		6500			ET 310MI		15000	1000 COO	1100 1		\$.900 1000 200		S.OX VEMENT 17 20 CONCRETE SECTION	PENETRAI		the control of the co
TYPE OF WORK: WET S	LOCATION:			र्क्षास्त्र स्त्री वेष	O BAC	METTE	BIALE S	3000 30		CONCR	/				AYEL GI	N. N	《中国·西班牙·西班牙·西班牙·西班牙·西班牙·西班牙·西班牙·西班牙·西班牙·西班牙						the terms of war was sent to be the sent of the sent o

RESULT			1918.929		
TYPE OF WORK: CEMENT HORTAR POINTING	Sold Sold Sold Sold Sold Sold Sold Sold	3,000 750 300 300 800 10 10 10 10 10 10 10 10 10 10 10 10 1	TOTAL STORE MARCH RESIDENCE CHANGE RESIDENCE C	Toric (TVI	
			2 - 88		

r		Т				·	~	; 	·		·	·	~~~~		-100		 ₹						
DEOLE H	1,1201.1			-					: : :	1				E. A									
																-							
		72746		38.802	248,255	EX8 84	786.500	27.118	158.403	5.082	16.94												
ATION	-	1.15 ~		6.387	43.005	9.450	75.037 40.050	2,117	70.580 14.116	2.541	8.470												
CALCULATION		1:20		13.615	92,130	15.243				2,541	8.470												
		111.5		16.800	114.120	23.200	107.600	14.416	73.707				Cenci	70RM									
				700		BASE		PAT.		2N2													
TYPE OF WORK: CONCRETE, FORM			000 000 UNIVERSITY OF THE PROPERTY OF THE PROP		00:1 00:1 00:1 00:1 00:1 00:1 00:1 00:1		300 JOO JOO JOO JOO JOO JOO JOO JOO JOO J		BASE CONCRETE			8 1000000000000000000000000000000000000		Toursetty.	TO CONCRETE (1)		300 20 30 30 30 30 30 30 30 30 30 30 30 30 30	CANATIONAL PROPERTY AND A CONTROL OF THE CONTROL OF		COSTO CONTRACTOR CONTR	PARTITION WALL	The second secon	

RESULT																			
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	_	707AL	4964	1.800		1287		0.258	:		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\								
TION		1375~	0.280	208.0		0,123		62110											
CALCULATION		1:2,0	5,763	0.805		945.0													
		11.15	111.0	0.693		0.615		0.129										a construction of the second	
			70P	BASE		PART,		END										the second of the second of	and the second second second
ORK: DEFORMED REINFORCING BARS			0000	1 0012		20 20 00 00 00 00 00 00 00 00 00 00 00 0	,	BASE CONVICTE		CP 1 - 10 30 200 50	THE STATE OF THE S	Construction of the constr	Constant of the second of the	PARTITION WALL	 A second of the control of the control				
TYPE OF WORK:	LOCATION		4d	601	***	,													

30/VT FILLER 70 P 24/64D /9704 9/368 44/344 70 P 20/VT FILLER 30/VT FIL	RESULT	4C	カカ		10		83	3.4										
FILLER TOP CONCRETE SCALE B SCALE B		1:1.5 1:2.0 1:5.0	878.6 407.91 app.42		9558 348K1 754.81		3.529 3.529	7.524			· · · · · · · · · · · · · · · · · · ·	(の)の (の)の (の)の (の)の (の)の (の)の (の)の (の)の	(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きなない)(大きな					
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RESULT																		
CALCULATION		1:7.5 1:2.0 1:2.0 TOTAL	PV C 36,000 36,000 14.400 86.40	 FILTER 30.720 28.800 11.520 71.040	111 81 5 # 8 W					· · · · · · · · · · · · · · · · · · ·								
TYPE OF WORK: NEEP HOLE	LOCATION					The second of th	PVC PIPE 8 50	T STONE MASONRY	A PLYS		CRAVEL BEDDING	HIGH ALLAW BO HVLEG	SCACENCE TO THE STATE OF THE ST				《《《《·································	是一个人,我们就是一个人,就是一个人,我们就是一个人,我们就是一个人,我们也不是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人

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RESULT						-			1				-	78.006m3											
CALCULATION		O SLOPE OF 11,5	1.	V= 30,000 m3		(2) SLOPE OF 112,0		V = 34.88/m3		3 SLOPE OF 1150 120		V = 125 M3		7+102											
STONE FILLING									300				7.29		EEP NO.	\$500		700		MAČADI PAYEMI	INTERIOR	,			
AURRLE	9.75			0000'6	- N.W.	RUYEL	3.000	. 4	,,, 		wet	STONE W	A SOUTHY	СНАУ	EL BIOG	NUS									
TYPE OF WORK:				000	BACKE	ALL SOIL	1,300	1000		concact E-Cil	S														

TYPE OF WORK: SOIL FILLING	CALCULATION	RESULT
	V = 19.773	アンノスかん
300		
50 500 50		
JOINT FILLER 1=10 CONCRETE, TYPE - C1		
1 7 2 1 1 2 2 2 1 1 2 2 2 1 1 2 2 2 1 2		
<u>D 10 @ 3000 E 10 00 00 00 00 00 00 00 00 00 00 00 00 </u>		
0 0 0		
300		:
		3 : 3 : 3 : 3 : 3 : 3 : 3 : 3 : 3 : 3 :

RESULT		35.7672																
CALCULATION		1 = 35.767 mg															· · · · · · · · · · · · · · · · · · ·	
TYPE OF WORK	LOCATION: Section of the section of		COS	50 200 50	JOINT FILLER 1=10		1013	D 10 @ 300 N	. 200 c	GABION CYLINGEN I	200 300		77.400 1.114.4000 1.114.41000	7H Q 2 Q 2 P 1 W 1 C 2 P 1 W 1 W 1 W 1 W 1 W 1 W 1 W 1 W 1 W 1	CALLUDER CHUNDER	《《古诗篇》《古诗诗》《《古诗······························		

= 2.400 2.400 % = 1.200 m3 = 0.706 m3 = 0.706 m3 = 101.285 101	· .
= 2.400 = 0.706 0.706	
O BASE CONCRETE V = 1.20m²/15.0m × 30.0m V = 0.60 m³/15.0m × 30.0m V = 0.60 m³/15.0m × 30.0m V = 0.50 m³/16.0m × 30.0m V = 0.706 m²/16.0m × 30.0m V = 0.706 m²/16.0m × 30.0m V = 0.706 m²/16.0m × 30.0m V = 0.706 m³/16.0m × 30.0m Tolor = 0.706 m²/16.0m × 30.0m	
TYPE OF WORK: 648 LVEL BENDING LOCATION: Soo	

		•			•	-						•					-		
RESULT														1					
CALCULATION			V= (50,789 + 51.656) +2/15.0m	x 30,0m = 102,445															
WET STONE MASONRY						7	400		4,0	000.			200		(C) (X,000 3,700	î.	D.H.S.		
TYPE OF WORK:	1 OCATION	1							2	- 10	0								

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RESULT		317,432,2																		
CALCULATION	A=>(9,014+0.7)+(11,18+0.7)>+2	x (30,0 -0,3x2) = 3/2,432														1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1				
TYPE OF WORK: CEMENT MORTAR POINTING				400	** ## *\			-10		10,0	000		2,000		0.H					

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	RESULT	J 998	0.2901f	4.530-16	0,123 Tf		0,1297	9.13.1.75 D.844		
•		2 - 4 - 4 - 4	= 0.290	= 4.536	60 = 01/23 0		= 0,129	70746		
	CALCULATION	15.207 x	19/ Y	15,0 7 2	place x 1 pl		e x / place			
	CAL	TOP CONCRETE	8ASE CONCRETE	(0.093+0.058)x	123 71	WALL	127 tt/dace	TYPE - C! FILLING	009	GABION CYLINDER
	8	0 70P W=(0,		w = (0.0	W	QMZ	W/W	300 200 50 200 50 201 FILLING	10000000000000000000000000000000000000	200 300 (00 100 100 100 100 100 100 100 100 1
	ORCING BAR.	CONCRETE, TYPE - C1	009 000 000 000 000 000 000 000 000 000	SO GRAVEL PROUND 1	CONCRETE TYPE-C1	GRAVEL SEDDING		JOHT FILLER 1810 (ELASTIC MATERIAL)	055 055 00	2
	DETORMED REINFORCING BARS	300 200	6.43	SO	9 00 (0) O (0)	005 051	50 CONCRETE, T'PE-	000 000 000 000 000 000	GRAVEL BED	対し、対し、対し、対し、対し、対し、対し、対し、対し、対し、対し、対し、対し、対
		oc	005 005	៉ុក្	860 860	001	SO .200. JOINT FILLER : #10	085 085 00	000000000000000000000000000000000000000	
	TYPE OF WORK	LOCATION			2 - 10)2	JOINT : ELAS			

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RESULT				6.387 m3	,	43,005 m2				2 450 mg		40,350m			2.117 m3	14.116 m3				2.541 mg		8.470 m2	ツモレウ// くか
CALCUCATION		O TOP CONCRETE	SOUCEETE.	V= 3,150 m3/15.0m × 15,207 x 2 = 6,387	2) LORH	A= 2x210 m2/15,0m x 15.207 x2 = 43,005		@ BASK CONCRETE	1) CONCRETE	V= 4.725 m / 15.0m x 15.0m x 2 = 8.450 m3		A = 20,175 m3/13,0m x 15,0mx2 = 40,350 m3	@ PARTITION WALL	1) COUCRETE	V= 2,117 m3/place x 1 place = 2,117 m3	A=14.116 m2/ place = 14116m2		@ ZND NALL	1) CONCRETE	1 place x 1 place = 2.541	2) FORH	A = 8 470 milplac x / place = 8,470 8	・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・
TYPE OF WORK: CONCRETE, FORM	LOCATION			300 200 CONCRETE. TYPE - C.		0002	\$00000		300		٦	SI ELASTIC MATERIALS		S S S S S S S S S S S S S S S S S S S	0	JOHNT FILLERA # 10	I ELASTIC MATERIAL!	000000000000000000000000000000000000000		OS CONTRACTOR OF THE PROPING	300		

707.41 CONCRETE 20.495 m3
707.4L FORM 108.941 m3

7x2 = 9,368 9,368m² Kace = 3,529 3.529m² Cae = 3,529 3.529m²
PARTITION WALL = 3.529 m² / place x / place = 3.529 END WALL = 3.529 m² / place x / place = 3.529
1 = 3.529 m3/ place x / place = 3,529
CONCRETE, TYPE - C1 SOIL FILLING SOIL FILLING SOIL FILLING SOIL
SOIL FILLING SOIL FILLING SOID SOO

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RESULT				,	14.400 m					11.520m2										T	
CALCULĂTION	· PUC PIPE & SD		n= 9 /15,0m x 15,0mx 2 = 18		2 × 8 × 5.8	· FILTER CLOTH		n=18 places		A: 18x0.64 milplace = 11.520						· · · · · · · · · · · · · · · · · · ·					
TYPE OF WORK: NEEP HOLE							000 CONTRACTOR OF THE CONTRACT		E D 50	STONE MASONRY	1000	0/23	CRAVEL DECOUNG	DETAIL OF WEEP HOLE				,是是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们	我说话,我们也没有一个人们是不是一个人,我们也没有一个人们,我们就是一个人,我们也是不是一个人们的人,我们就是一个人们的人,我们就是一个人们的人们的人们的人们的人们的人们的人们的人们的人们的人们们的人		

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	RESULT			67.500m3	:																					
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	ATTON			SIX																		-				
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	TYPE OF WORK:	LOCATION:																								
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	RESULT			13.72596	1																	
	CALCULATION		V= (5.625 + 7.5) + 2/15.0m x 15.0m x 2	52/5/ =																		
	TYPE OF WORK: RUBBLE STONE FILLING	LOCATION:	i.			7,4	•	₹0/	eren i e	700		10,	چ چ چ		1.17	3,000		H.W				