TYPE OF WORK : REVETMENT FOR SLOPE OF 1:1.5 \sim 1:2.0

(WET STONE MASONRY TYPE)

: WF.110R + 10.0 ~ WF.110R + 25.0 m : WF.104R + 17.0 ~ WF.104R + 32.0 m LOCATION

CALCULATION		RESULT
STRUCTURAL EXCAVATION		
$V = (176.850 + 180.39) / 2 / 15.0 \text{ m} \times 30.00$	= 357.240	357.240 m ³
BACKFILL WITH SELECTED SOIL		
BACKFILL WITH SELECTED SOIL		
$V = (17.445 + 20.640) / 2 / 15.0 \text{ m} \times 30.00$	= 38.085	38.085 m ³
		30.003 111
WET STONE MASONRY		
$V = (50.789 + 51.656) / 2 / 15.0 \text{ m} \times 30.00$	= 102.445	102.445 m ³
	<u>il desertions to the southern</u>	
CEMENT MORTAR POINTING		
$A = \{(9.014 + 0.70) + (11.18 + 0.70)\}/2$	<u>ann an air an Calaite (1967) an aithe ann Cath</u> Calainn an ann an Calainn an Calainn Air an	
$x (30.00 - 0.30 \times 2)$	= 317.432	317.432 m²
WEEP HOLE		
PVC PIPE Ø 50		
$n = 9/15.0 \times 15.0 \times 2$	= 18	
$L = 18 \times 0.80$	= 14.400	14.400 m
FILTER CLOTH		
$A = 0.640 \text{ m}^2/\text{place x } 18$	= 11.520	11.520 m ²
The second in Applace K 16.	11.520	11.520 III
GABION MATTRESS		
		Section 1. 1
$V = 33.750 \mathrm{m}^3 / 15.0 \mathrm{x} 15.0 \mathrm{x} 2$	= 67.500	67.500 m ³
RUBBLE STONE FILLING		
$V = (5.625 + 7.50)/2/15.0 \text{ m} \times 15.0 \text{ m} \times 2$	- 12 125	13.125 m ³
V = (3.025 + 7.50) / 27 13.0 m x 13.0 m x 2	7 13.123	13.123 111
GABION CYLINDER Ø 500 (GALVANIZED ANI	D COATED WITH PVC)	
$V = \frac{\pi}{4} \times 0.50^2 \times (3.00 + 11.18 + 1.00) \times 6.00$	= 17.884	17.884 m³
SOIL FILLING		
$V_1 = \frac{\pi}{4} \times 0.50^2 \times (3.00 + 11.18 + 1.00) \times 6.00$	= 17.884	
$V_2 = (3.00 + 11.18 + 1.00) \times 3.00 \times 0.50$	= 22.770	
$V_1 = V_2 - V_1$	= 4.886	4.886 m ³

								-	-	-			••			•			*****		and and an and an	ina tabundu.	44 24 20 <u>1</u>	Vidio ver	Paris de la	era era
RESULT				2.400 ms	,			1.200 m3				0.706 m3				6.706m²					101.2853		106.297 m3			
				= 2.400				1.200				0.706				0.708					101.285		TOTAL			
CALCULATION		Z		30.0m				x 30.0%				2 x 1 place =				m3/ dace x / place =		No/2		76) + 2/150m			7			
	A STATE OF THE STA	O BASE CONCRETE		V = 1.20m3/15.0m X		70% CONCRETE	A STATE OF THE STA	0.60 m3/15.0m		3 PARTITION WALL		0.706 mª / place		END WALL		201.0		3 STANDARD SECTION		V = (49.409+51.876) +2/15.0m	X 30,0 m					
		0		7		<u> </u>		*		<u>@</u>		<u>V</u> =		(B)		<u>\(\) \(\) \(\) \(\)</u>		<u> </u>		*				9		
4						빔					C III				0						007.2	0	00 Å			
GRAVEL BEDDING			300 200 CONCRETE, TYPE - C	0000000	00 (COS ISO GRAVEL OCEON	000 00s	300				00 200	-,	CONCORTE TANG-CO			300 600	90 90	00000		1					
6 RAV			"[<u>*</u>]			展 <u>京</u>	-8		SILVER I	000	- 21 [CLASTIC MATERIAL		000000000000000000000000000000000000000	8		7,400	-6						
TYPE OF WORK:	OCATION:																									
LE													2 - 3	37_												

entanti in terreta de la compania de

	-t											
RESULT		4,3497,5		4.5301f		0,123 7f		D1129+f	8.131H			
CALCULATION	O TOP CONCRETE.	W= (0.093+0.050)×15.207 x2=4.349	O BASE CONCRETE	w=(0,093+0,058)x15,0 x 2 = 4.530	3 PARTITION WALL	W = 0.123 +f/plag x / place = 0,123	@ END WALL	W = 0,129 ++ 1 place x 1 place = 0,129	02 000	STANT FILER 14-10 (ELASTIC MATERIALT) (STANEL) (STANEL) (STANEL) (STANEL) (STANEL)	S	
TYPE OF WORK: DEFORMED REINFORCING BARS	0095	300 200 CONCRETE	000 000	5 to 400 50 GRAVEL RE	00 00 00 00 00 00 00 00 00 00 00 00 00	CONCRETE, TYPE CONCRE	2 055 001	GRAVEL BED	SONT FILLER 1-10 SO SOLL FILLING CONCRETE, TYPE -C1	009 052 052 013 01003000 01003000 01003000	200 300 GRAVEL BEDDING (100 100 100 100 100 100 100 100 100 10	

	_	7	T	 		J	· J- ···-			·	•	¥													
g • • • •	RESULT				6.387 m3		43,005 m2				2450mg		40,350m				2.117 m3	14.116 m2				2.541 m3		8.470 m2	20.495m3
	CALCULATION		O TOP CONCRETE.	1) CONCRETE.	1= 3,150 m3/15,0m x 15,207 x 2 = 6.387	2) FORM	A= 21,210 m2/15,0m x 15,207 X2 = 43,005		3 BASE CONCRETE	1) CONCEETE	V= 4.725 m 15.0m x 15.0m x 2 = 9.450 m3	2) FORM	A = 20.175 m2/15,0m x 15,0mx2 = 40,350 m2		3 PARTITION NALL	1) CONCRETE	V = 2,117 m3/place x 1 place = 2,117 m3	A = 14.116 m2/ place x 1 place = 14.116m2		@ END NALL	1) concrett	3/place x 1 place = 2.54)	2) LORH	A = 8,470 m² / plac x 1 place = 8,470 8	TOTAL CONCRETE:
	TYPE OF WORK: CANDER TE FORM		005 001	0	Soul There is a second	St St St St St St St St	2000 00 00 00 00 00 00 00 00 00 00 00 00	O O O O O O O O O O O O O O O O O O O	000 000	о зо о зо о ялу	200 300	OOS OO	SO ZOOJ SO CONCRETE TYPE - U	2 -	0000	oz oz	SNIOCI TEACHER TO THE TEACHER THE THE TEACHER TO THE TEACHER THE TEACHER TO THE TEACHER THE THE	8	50 <u>50 50 50 50 50 50 50 5</u>	JOHN FILLER 18-10	,	2		200 300 I	

TOTAL CONCRETE 20.495m'
TOTAL FORM

																 and the same of		و في الجوائد المالية	and displayable	- 	. وفي إدراد	er see fave	hing in a
ilia .				4							•											•	
	RESULT			9.368m2		2000				3.529m2						0.630m2							
		O TOP CONCRETE		A = 4.620 m / 15,0m x 15:207x 2 = 9.368	(2) PARTITION WALL	A = 3.529 m = 12/20 0 1 20 = 8 529		3 FND WALL		A= 3.529 m3/ place x 1 place = 3.529		4 BASE CONCRETE.		a=(0.3+0.6) x0.3-2+0.3+0.6	= 0315 m2/place	A = 0.315 x 2 places = 0.630	· .						
	TYPE OF WORK: JOINT FILLER	LOCATION:	JOINT FILLER 110 - 20 200 500 50		200 200 500 500 500 500 500 500 500 500	00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	OMER OF THE PROPERTY OF THE PR	200	300 300 300 300	JOHNT FILLER 1-10 (ELASTIC MATERIAL)		000000000000000000000000000000000000000	OG GOOD GOOD GOOD GOOD GOOD GOOD GOOD G	900			SCASIIC MAILENALLI		0.13		200 300 CONSTRUCTION OF THE PROPERTY OF THE PR	00) (O) (O) (O) (O) (O) (O) (O) (O) (O) (O	

TYPE OF WORK : REVETMENT FOR SLOPE OF 1:2.0 (WET STONE MASONRY TYPE) LOCATION : WF.111L + 15.0 m \sim WF.111L + 90.0 m

CALCULATION		RESULT
STRUCTURAL EXCAVATION		1.1
$V = 180.390 \text{ m}^3 / 15.0 \text{ m} \times 72.143$	= 867.592	867.592 m ³
(R = 151.5) BACKFILL WITH SELECTED SOIL		
BACKFILL WITH SELECTED SOIL		
$V = 20.640 \mathrm{m}^3 / 15.0 \mathrm{m} \times 72.143$	= 99.269	99.269 m³
$\sqrt{R} = 20.040 \text{ m} / 13.0 \text{ m} \times 72.143$ (R = 151.5)	99,209	99.209 III
GRAVEL BEDDING		
1. FOR BASE CONCRETE		
$V = 0.70 \text{ m}^3 / 10.0 \text{ m} \times 69.286$	= 4.850	4.850 m ³
(R = 145.5)		
2. FOR TOP CONCRETE		
$V = 0.75 \text{ m}^3 / 10.0 \text{ m} \times 75.640$	= 5.673	5.673 m ³
(R = 158.35) 3. FOR PARTITION WALL		
5. FOR FARITION WALL		
$a = (0.40 + 0.60) \times 0.10 / 2$	= 0.050	
$V' = 0.05 \times (0.7 + 11.180 + 2.236)$	$= 0.706 \text{ m}^3/\text{ place}$	
$V = 0.706 \mathrm{m}^3 /\mathrm{place} \mathrm{x} 5\mathrm{places}$	= 3.530	3.530 m ³
4. FOR STANDARD SECTION		
$V = 51.876 \mathrm{m}^3 / 15.0 \mathrm{m} \times 72.143$	= 249.499	249.499 m ³
(R = 151.5)		
TOTAL	= 263.552	263.552 m ³
WET STONE MASONRY		
$V = 51.656 \mathrm{m}^3 / 15.0 \mathrm{m} \times 72.143$	= 248.441	248.441 m ³
(R = 151.5)		240.44111
CEMENT MORTAR POINTING		
$A = 174.636 \mathrm{m}^2/15.0 \mathrm{m} \times 72.143$	= 839.918	839.918 m ²
(R = 151.5)		

TYPE OF WORK: REVETMENT FOR SLOPE OF 1:2.0 (WET STONE MASONRY TYPE)

LOCATION : WF.111L + 15.0 m ~ WF.111L + 90.0 m

CALC	ULATION	RESULT
DEFORMED REINFORCING BAR		W I F
1. BASE CONCRETE		
$W = 0.1 \text{ tf} / 10.0 \text{ m} \times 69.286$	= 0.693	0.693 tf
(R = 145.5)		
2. TOP CONCRETE		3 1 1 3
$W = 0.094 \text{ tf} / 10.0 \text{ m} \times 75.640$	= 0.711	0.711 tf
3. PARTITION WALL		
W = 0.123 tf/place x 5 places	= 0.615	0.615 tf
The state of the s		
4. END WALL		
W = 0.120 of /mlass v 1 mlasss	= 0.129	0.129 tf
W = 0.129 tf/place x 1 places	$\frac{-0.129}{\text{TOTAL}} = 2.148$	2.148 tf
CONCRETE, FORM		
1. BASE CONCRETE		
A SECONOMIE DE LA COMPANIONE DEL COMPANIONE DE LA COMPANIONE DE LA COMPANIONE DELA COMPANIO		
CONCRETE		
$V = 2.20 \text{ m}^3 / 10.0 \text{ m} \times 69.286$	= 15,243	15,243 m ³
$V = 2.20 \text{ m} / 10.0 \text{ m} \times 69.280$ (R = 145.5)	- 13,243	15,245 11
FORM		
		75 027 -2
$A = 10.830 \text{ m}^2 / 10.0 \text{ m x } 69.286$	= 75.037	75.037 m ²
2. TOP CONCRETE		
		tra en St.
CONCRETE		
$V = 1.80 \mathrm{m}^3 / 10.0 \mathrm{m} \times 75.64$	= 13.615	13.615 m ³
(R = 158.35)		
FORM		
$A = 12.180 \mathrm{m^2}/10.0 \mathrm{m} \times 75.64$	= 92.130	92.130 m ²
$A = 12.180 \text{ m}^{2} / 10.0 \text{ m} \times 75.64$	- 92:13 U	72.130 III

TYPE OF WORK : REVETMENT FOR SLOPE OF 1:2.0 (WET STONE MASONRY TYPE) LOCATION : WF.111L + 15.0 m \sim WF.111L + 90.0 m

CALCULATION		RESULT
3. PARTITION WALL		jána, vidaljej
CONCRETE		9 3 1 1 7 7 7 1 1
XI 0.110 3 1 1	10.505	10 505
$V = 2.117 \text{m}^3 / \text{place} \times 5 \text{places} =$	= 10.585	10.585 m ³
FORM		
		AND PROPERTY OF A
$A = 14.116 \text{m}^2/\text{place x 5 places} =$	70.580	70.580 m ²
4. END WALL		Maria Andria
CONCRETE		
$V = 2.541 \text{ m}^3/\text{place x 1 places} =$	2.541	2.541 m ³
FORM		
$A = 8.470 \text{ m}^2/\text{place x 1 places} =$	8,470	8.470 m ²
TOTAL CONCRETE =	41.984	41.984 m ³
TOTAL FORM =	= 246.217	246.217 m ²
JOINT FILLER		
1. BASE CONCRETE		
I. BASE CONCRETE		
$A = 0.22 \mathrm{m^2} / 10.0 \mathrm{m} \mathrm{x} 69.286 \qquad =$	= 1.524	1.524 m ²
(R =145.5)		
2. TOP CONCRETE	or present the second of the	200 July 200 July 200
$A = 2.605 \text{ m}^2 / 10.0 \text{ m x } 75.640 =$	19.704	19.704 m ²
(R = 158.35)		
3. PARTITION WALL		
$A = 3.529 \text{ m}^3 / \text{place x 5 places} =$	= 17.645	17.645 m²
3.325 III 7 place X 5 places	TO IT IN THE STATE OF THE STATE	17.043 III
4. END WALL		
$A = 3.529 \text{ m}^3 / \text{place x 1 places} =$	= 3.529	3.529 m²
TOTAL A =	= 42.402	42.402 m ²

TYPE OF WORK: REVETMENT FOR SLOPE OF 1:2.0 (WET STONE MASONRY TYPE)

LOCATION : c

CALCULATION		RESULT
GABION MATTRESS t = 500 mm		
$L_1 = 69.048 \text{ m } (R = 145 \text{ m})$		
$L_2 = 68.929 \text{ m } (R = 144.75 \text{ m})$		n with the later of the later o
V = 60.049 + 0.5 + 2.0	102.672	
$V_1 = 69.048 \times 0.5 \times 3.0$ $V_2 = 68.929 \times 0.5 \times 1.5$	= 103.572 = 51.697	
V ₂ - 08.929 X U.3 X 1.3	= 155.269	155.269 m³
The first section of the first	133,209	133.209 III
RUBBLE STONE FILLING		
$A = 1/2 \times 1.0 \times 0.5 \times 2$	$= 0.500 \mathrm{m}^2$	
	and the first of the second second	
$V = 0.500 \times 69.762$	$= 34.881 \text{ m}^3$	34.881 m ³
(R = 146.5)		
GABION CYLINDER		
a coo (CALLANDED AND COARED WERLDYO)		
ø 500 (GALVANIZED AND COATED WITH PVC)		
$V = \frac{\pi}{4} \times 0.50^2 \times (3.00 + 11.18 + 1.00) \times 6 \times 2$	5.C. (1) C. (1)	35,767 m ³
$V = \frac{1}{4} \times 0.50 \times (3.00 + 11.18 + 1.00) \times 6 \times 2$	= 35./6/	33.707 III
SOIL FILLING		
SOIL FILLING		
$V_1 = \frac{\pi}{4} \times 0.50^2 \times (3.00 + 11.18 + 1.00) \times 6 \times 2$	= 35.767	
$V_1 = \frac{74}{4} \times 0.30 \times (3.00 + 11.18 + 1.00) \times 3.00 \times 0.50 \times 2$ $V_2 = (3.00 + 11.18 + 1.00) \times 3.00 \times 0.50 \times 2$	= 45.540	
$V_2 = (3.00 \pm 11.18 \pm 1.00) \times 3.00 \times 0.30 \times 2$	= 43.340	
$V = V_2 - V_1$	= 9.773	9.773 m ³
The control of the co		9.775 III
WEEP HOLE		
PVC PIPE Ø 50		
n = 9 / place x 5	= 45	
$1 = 45 \times 0.80$	= 36.000	36.000 m
FILTER CLOTH		
n = 45	<u>ang Pangalan Bahatan Jawa Jawa P</u> Ang pangganggan Bahatan	
$A = 0.640 \text{m}^2 / \text{place x } 45$	= 28.800	28.800 m ²
A y v.v. in / place A 73	- 20.000	20.000 III

TYPE OF WORK: REVETMENT FOR SIDE SLOP OF 1:2.0 (WET STONE MASONRY) WF.115R + 15.0 \sim WF.117R + 32.0

LOCATION :

		CALCULATION		RESULT
		CALCULATION		KLOULI
5	SRTRI	JCTURAL EXCAVATION		
	DACE 24.		A Committee of the Comm	
	A ₁ =	$4.25 \times 0.50 + 1.118 \times 6.70 \times 0.50 =$	5.870 m ²	
	Note that			
	$A_2 =$	$(0.30 + 0.725) \times \frac{1}{2} \times 0.85 =$	0.436 m ²	
	<u> </u>			e wijewajiji
	<u> </u>	A se	6.306 m²	
	V	$6.306 \times (119.50 + 92.30) \times \frac{1}{4} =$	667.81	667.8 m³
	<u></u> ¥	0.300 X (119.30 t) 92.30) X /2	007.61	007.6 111
8	BACK	FILL WITH SELECTED SOIL	<u>and the second of the second </u>	
- 10 mg/s	arty La			
	A =	$(0.30 + 0.725) \times \frac{1}{2} \times 0.85 =$	0.436 m ²	
	tak arkiki i	0.426		
*	V =	0.436 x 92.30 =	40.24	40.24 m ³
	<u>en de la como</u>		<u> </u>	
5	CEME	NT MORTAR POINTTING		
-:-			<u>an an a</u>	
1 1 1 1	$A_1 =$	1.118 x 6.40 x 14.70	105.181 m ² /15.00 m	
1			ar and a second of the second	
	A' =	$105.181 \text{ m}^2/15.00 \text{ m} \times 92.30 =$	647.214	
		2.05 14.70	50.075 70.500	
	A ₂ =	3.95 x 14.70 =	58.065 m ² /15.00 m	
	A ¹ =	58.065 m ² /15.00 m x 119.50 =	462.585	
	N. 194, 19			eprincipal de la company
		$TOTAL (A_1 + A_2) =$	1109.799	1109.799 m ²
	<u> </u>		and the first course the second the	No a star 1 such
<u> </u>	337000	TONE MACONINA		
<u> 8</u>	WETS	TONE MASONRY		
٠.	V ₁ ==	7.155 x 0.25 x 14.70 =	26.295 m ² /15.00 m	<u>an Araban da Arra</u> Jan Barra da Barra (1914)
			~V.#7J III / 1J.UV III	
	V1 =	26.295 m ² /15.00 m x 92.30 =	161.802	
:	V ₂ =	$3.95 \times 0.25 \times 14.70 =$	14.516 m ² /15.00 m	444 N. S.
. 5	121	4.5.4		e Tak af i ja taka i
: '	V' =	14.516 m ² /15.00 m x 119.50 =	115.644	
Later of		$TOTAL (V_1 + V_2) =$	277.446	277.446 m ²
_		101AD (11 P 12)	411.770	211,740 111

TYPE OF WORK : REVETMENT FOR SIDE SLOP OF 1:2.0 (WET STONE MASONRY) LOCATION : WF.115R + 15.0 \sim WF.117R + 32.0

	m²
$V_1 = 1.118 \times 6.40 \times 0.25 \times 14.70 = 26.295 \text{ m}^2/15.00 \text{ m}$ $V^1 = 26.295 \text{ m}^2/15.00 \text{ m} \times 92.30 = 161.802$ $V_2 = 3.95 \times 0.25 \times 14.70 = 14.516 \text{ m}^2/15.00 \text{ m}$ $V^1 = 14.516 \text{ m}^2/15.00 \text{ m} \times 119.50 = 115.644$ $TOTAL (V_1 + V_2) = 277.446 = 277.446$ $PWEEP HOLE$ $n = 12 \text{ places } / 15.00 \text{ m}$ $PVC \text{ pipe } \varnothing 50 \text{ (L = 0.80 m / pipe)}$	m ²
$V^{1} = 26.295 \text{ m}^{2}/15.00 \text{ m} \times 92.30 = 161.802$ $V_{2} = 3.95 \times 0.25 \times 14.70 = 14.516 \text{ m}^{2}/15.00 \text{ m}$ $V^{1} = 14.516 \text{ m}^{2}/15.00 \text{ m} \times 119.50 = 115.644$ $TOTAL (V_{1} + V_{2}) = 277.446 = 277.446$ $P \text{ WEEP HOLE}$ $n = 12 \text{ places } / 15.00 \text{ m}$ • PVC pipe $\varnothing 50$ (L = 0.80 m / pipe)	m [*]
$V^{1} = 26.295 \text{ m}^{2}/15.00 \text{ m} \times 92.30 = 161.802$ $V_{2} = 3.95 \times 0.25 \times 14.70 = 14.516 \text{ m}^{2}/15.00 \text{ m}$ $V^{1} = 14.516 \text{ m}^{2}/15.00 \text{ m} \times 119.50 = 115.644$ $TOTAL (V_{1} + V_{2}) = 277.446 = 277.446$ $P \text{ WEEP HOLE}$ $n = 12 \text{ places } / 15.00 \text{ m}$ $PVC \text{ pipe } \varnothing 50 \text{ (}L = 0.80 \text{ m} / \text{ pipe} \text{)}$	m²
$V_2 = 3.95 \times 0.25 \times 14.70$ = 14.516 m ² /15.00 m $V^1 = 14.516 \text{ m}^2/15.00 \text{ m} \times 119.50$ = 115.644 TOTAL $(V_1 + V_2)$ = 277.446 277.446 P WEEP HOLE P = 12 places / 15.00 m PVC pipe \emptyset 50 (L = 0.80 m / pipe)	m²
$V^{1} = 14.516 \text{ m}^{2}/15.00 \text{ m} \times 119.50 = 115.644$ TOTAL ($V_{1} + V_{2}$) = 277.446 277.446 \Box WEEP HOLE $D = 12 \text{ places } / 15.00 \text{ m}$ PVC pipe $\varnothing 50$ (L = 0.80 m / pipe)	m²
TOTAL $(V_1 + V_2) = 277.446$ 277.446 F WEEP HOLE $n = 12 \text{ places } / 15.00 \text{ m}$ PVC pipe Ø 50 (L = 0.80 m / pipe)	m²
TOTAL $(V_1 + V_2) = 277.446$ 277.446 F WEEP HOLE $n = 12 \text{ places } / 15.00 \text{ m}$ PVC pipe Ø 50 (L = 0.80 m / pipe)	m²
n = 12 places / 15.00 m • PVC pipe Ø 50 (L = 0.80 m / pipe)	m²
n = 12 places / 15.00 m • PVC pipe Ø 50 (L = 0.80 m / pipe)	
n = 12 places / 15.00 m • PVC pipe Ø 50 (L = 0.80 m / pipe)	
PVC pipe Ø 50 (L = 0.80 m / pipe)	
$n_1 = 12 \text{ places} / 15.00 \text{ m} \times 92.30 = 74 \text{ places}$	
$n_1 = 12 \text{ places } / 15.00 \text{ m} \times 92.30 = 74 \text{ places}$	
L = 74 places x 0.80 = 59.200	
• FILTER CLOTH	
$A = 0.856 \text{ m}^2/\text{place} \times 74 \text{ places} = 63.344$ 63.344	m²
□ BASE CONCRETE	<u> </u>
CONCRETE(TYPE - C1)	
$V = 2.20 \mathrm{m}^3/10.00 \mathrm{m} \times 92.30 = 20.306$	n ³
GRAVEL BEDDING	
$V = 0.70 \text{ m}^3/10.00 \text{ m} \times 92.30 = 6.461$ 6.461 1	n ³
• FORM (H < 4.0 m)	
$A = 10.83 \text{ m}^2/10.00 \text{ m} \times 92.30 = 99.961$ 99.961	m²
• REINFORCING BAR	
$W = 0.10 \text{ tf} / 10.00 \text{ m} \times 92.30 = 0.923$	f
	N.
• JOINT FILTER	2 4
$A = 0.22 \text{ m}^2/10.00 \text{ x } 92.30 = 2.031$ 2.031	

TYPE OF WORK : REVETMENT FOR SIDE SLOP OF 1:2.0 (WET STONE MASONRY)
LOCATION : WF.115R + 15.0 ~ WF.117R + 32.0

	CALCULATION		RESULT
7	TOP CONCRETE		
			ali ne leti i
,	CONCRETE (TYPE - C1)		
	$V = (0.60 + 0.75) \times \frac{1}{2} \times 0.30 \times 15.00 =$	3.038 m ³ /15.00 m	
	0000 3/15 00 00 00	18.694	18.694 m³
	$V^1 = 3.038 \text{m}^3/15.00 \text{m} \times 92.30 =$	16.034	10.05 7 111
<u> </u>	GRAVEL BEDDING	्रेड सम्बद्धाः संस्थितः संस्थितः संस्थितः । इ.स. सम्बद्धाः संस्थितः	
	$V = \{(0.40 \times 0.10) + \frac{1}{2} \times 0.30 \times 0.15\} \times 15.00 =$	0.938 m ³ /15.00 m	
			5.770
	$V^1 = 0.938 \text{m}^3/15.00 \text{m} \times 92.30$	5.772	5.772 m ³
- (FORM (H < 4.0 m)		
	$A = (0.60 + 0.75) \times 15.00 + (0.60 + 0.75) \times \frac{1}{2} \times 0.30 =$	20.453 m ² /15.00m	
<u></u> : :			
	$A^{T} = 20.453 \text{ m}^{2}/15.00 \text{ m} \times 92.30 =$	125.854	125.854 m²
•	REINFORCING BAR D 13 (W = 1.04 kgf/m)		
7:1	D 13 (W = 1.04 kg(7 iii)		
<u></u>	$n_1 = 6 \text{ Bars}$		
		02.076	
	$W_1 = (15.00 - 0.05 \times 2) \times 6 \text{ Bars } \times 1.04 =$	92.976	
<u>) (</u>	D 10 $(W = 0.617 \text{ kgf/m})$		
1			
	$n_2 = (15.00 - 0.05 \times 2) : 0.30 + 1 =$	51 Bars	
113	$L_2 = 0.20 + 0.50 + 0.619 + 0.224 + 15 \times 0.01 =$	1.693 m / Bar	
	$L_2 = 0.20 + 0.50 + 0.619 + 0.224 + 15 \times 0.01 =$		
1 1	$W_2 = 1.693 \times 51 \times 0.617$	53.274	
:	W = 146.250 kgf =	0.146 tf / 15.00 m	7 - A - A - A - A - A - A - A - A - A -
	$W^r = 0.146 \text{ tf} / 15.00 \text{ m} \times 92.30 =$	0.898	0.898 tf
7			
٠	JOINT FILTER		
-	n = 92.30 : 15.00 ≅	6 places	
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	$A_1 = (0.60 + 0.75) \times \frac{1}{2} \times 0.30 \times 6 \text{ places} =$	1.215	
1. 1	$A_1 = (0.60 + 0.75) \times \frac{1}{2} \times 0.30 \times 6 \text{ places} =$		
i	$A_2 = (0.25 \times 14.70) / 15.00 \text{ m} \times 92.30 =$	22.614	
		20 000	02.800
	TOTAL TOTAL	23.829	23.829 m

REVETMENT FOR SIDE SLOP OF 1:2.0 (WET STONE MASONRY) WF.115R + 15.0 ~ WF.117R + 32.0 TYPE OF WORK : LOCATION :

CALCULATION		RESULT
₽ PARTITION WALL		
• CONCRETE (TYPE – C1)		
$V = (0.30 + 0.50 \times 3.95) + (7.115 \times 0.50 \times 0.30) =$	1.000 31-1	
$V^{*} = (0.30 \pm 0.30 \times 3.93) \pm (7.115 \times 0.30 \times 0.30) = 0.660 \text{ m}^{3}/\text{place} \times 7 \text{ place} = 0.660 \text{ m}^{3}/\text{place}$	1.660 m³/place 11.620	11 6203
$V^{t} = 1.660 \text{ m}^{3}/\text{place} \times 7 \text{ place} =$	11.020	11.620 m ³
GRAVEL BEDDING		
	The second secon	
$V = (0.50 + 0.70) \times \frac{1}{2} \times 0.10 \times (3.95 + 7.115) =$	0.664 m ³ /place	
$V^{I} = 0.664 \text{ m}^{3}/\text{place} \times 7 \text{ place} =$	4.648	4.648 m ³
	Turing data shirt is	1 1 14 1 1 1 1
• FORM (H < 4.0 m)		
		, et la grande de la companya de la
$A = (3.95 + 7.115) \times 0.50 \times 2$		
A ¹ = 11,065 m ² /place x 7 places =	77.455	77.455 m ²
- PENICOPONO DAD		3.
REINFORCING BAR		
D 13 (W = 1.04 kgf/m)		
D 13 (W - 1.04 kgt / III)		
$n_1 = 6 \text{ Bars}$		
$W_1 = (3.95 + 7.115 - 0.05 \times 4) \times 6 \text{ Bars } \times 1.04 =$	67.798	
D 10 $(W = 0.617 \text{ kgf/m})$		
fill the five to take the experience before the contempt and the property of the		y 1.11 3114
	37 Bars	
$L_2 = 0.20 \times 2 + 0.50 \times 2 + 15 \times 0.01 =$	1.550 m / Bar	. 11.9
$W_2 = 37 \text{ Bars } \times 1.55 \times 0.617 = $	35.385	The Level Days
W=103.183 kgf =	0.10 tf/place	0.00
$W^1 = 0.103 \text{ tf/place } \times 7 \text{ place} =$	0.721	0.721 tf
• JOINT FILTER		
▼ JUNITELER TO SEE THE SECOND SECTION OF SECOND SE		
$A = (3.95 + 7.115) \times 0.25 =$	2.766 m ² /place	
$A^{1} = 2.766 \text{ m}^{2}/\text{place} \times 7 \text{ place} = $	19.362	
The second of th	17:502	
TOTAL	19.362	19.362 m²
		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,

RESULT												16.2 m									
RES						, 1		:				141									
OF 1: 2.0 (WET STONE MASONRY TYPE) CALCULATION		A, = (1,10 + 2,10) × 1/2 × 0,50 = 0.80 m²	A2= (300 + 200) × 1/2 × 1.00 = 3.50 m²		A3 = 1, 118 × 9.00 × 0.50 + 0.70 × 0.50 = 5,38 m²		Ag = (0.80 + 1.50) × 1/2 × 0.70 = 0.81 m²		A= 10.49 m²			V = 10.49 x 135.00		こうちょう かいこう かいないない アンドラ 大きな かんかん かいかい しょうしゅう しゅうかい かいかい しょうしゅう かいかい かいかい しょうしゅう しゅうしゅう しゅうしゅう しゅうしゅう		是一个人,我们就是一个人,我们就是一个人的人,我们就是一个人的人,我们就是一个人的人,也是一个人的人,也是一个人的人,也是一个人的人,也是一个人的人,也是一个人的人,也是一个人的人,也是一个人的人,					
OF WORK: STRUCTURAL EXCAUATION	LOCATION: WF. 137R + 60. 175 ~ WF. 139R + 61. 545			000	RUBI(L. 50A.			3,500	1,00 5, com	OLIC .	0001		WEEP H	Te	AASONEY A		2// 1//	• 200	PAVEMEN ZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZ		Mark 1977 1984年 Mark 1987 Mark 1988 Mark

TYPE OF WORK: REVETMENT FOR SIDE SLOPE OF 1:2.0

(WET STONE MASONRY TYPE)

LOCATION : WF.137R + 60.775 ~ WF.139R + 61.545

CALCULATION		RESULT
BACKFILL WITH SELECTED SOIL		
$A_1 = (0.50 + 1.00) \times \frac{1}{2} \times 0.50$	= 0.380	
$A_2 = (0.50 + 1.50) \times \frac{1}{2} \times 1.00 - (0.50)^2$	= 0.750	
$A_3 = (0.50 + 1.00) \times \frac{1}{2} \times 0.50$	= 0.380	
TOTAL A	$= 1.510 \mathrm{m}^2$	
$V = 1.51 \times 135.00$	= 203.850	203.900 m ³
	The North Annual Control of	
GRAVEL BEDDING		
$A_1 = 1.118 \times 9.00 \times 14.70 / 15.0 \text{ m}$	$= 147.911 \text{ m}^2 / 15.0 \text{ m}$	
$A_2 = 0.70 \times 14.70 / 15.0 \text{ m}$	$= 10.290 \text{ m}^2 / 15.0 \text{ m}$	1
$V = (147.911 + 10.290) / 15.0 \text{ m} \times 135.00 \times 0.25$	= 355.952	355.952 m ³
WET STONE MASONRY		
$A_1 = 1.118 \times 9.00 \times 14.70 / 15.0 \text{ m}$	$= 147.911 \text{ m}^2 / 15.0 \text{ m}$	
$A_2 = 0.70 \times 14.70 / 15.0 \text{ m}$	$= 10.290 \text{ m}^2 / 15.0 \text{ m}$	
	and the second s	
$V = (147.911 + 10.290) / 15.0 \text{ m} \times 135.00 \times 0.25$	= 355.952	355.952 m ³
CEMENT MORTAR POINTING		
$A_1 = 1.118 \times 7.00 \times 14.70 / 15.0 \text{ m}$	$= 115.042 \text{ m}^2 / 15.0 \text{ m}$	
$A_2 = 0.70 \times 14.70 / 15.0 \text{ m}$	$= 10.290 \mathrm{m^2/15.0 m}$	
$A = (115.042 + 10.290) / 15.0 \text{ m} \times 135.00$	= 1127.988	1127.988 m ²
71 (115.042 1 10.250)) 15.0 H. A. 155.00		
WEEP HOLE		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
WEBTHODE		
PVC PIPE Ø 50		
TYCTIE V JV		
n = 12 places / 15.0 m		
n = 12 places / 15.0 m		
T = 12 -1 / 15 0 125 0 + 0.90	= 86.400	86.400 m
L = 12 places / 15.0 m x 135.0 x 0.80	- 00.400	30.400 III
TIX DOWN OF COMM.		
FILTER CLOTH		
	00.440	00.440 2
$A = 0.856 \times 12 \text{ places/ } 15.0 \text{ m} \times 135.0$	= 92.448	92.448 m ²

							•						·				,	. .
H = 0	YESOL I	28.588 m³			9,096 m3		140 1729 112			1.299 tf				2.8.59 m2				
REVETMENT FOR SIDE SLOP OF 1: 2.0 CWET STONE HASONRY TYPE) BASE CONCRETE	~ WF. 139 R+61.545 .CONCRETE (TYPE-	- 28,588	(R=147,75)	GRAVEL BEDDING	V=0.70 m3/0.00m × 129.944 = 9.096	CONCRETE, TYPE - C1	A=10.83 m2/0.00m × 129.944 = 140.729	OOG	O SEINFORCTING BAR	GRAVEL BEDDING W = 0.10 tf/0.00 m x 129.944 = 1.299		· JOINT FILLER	《《《··································	A = 0.22 m/0.00 m × 129.944 = 2.859		· · · · · · · · · · · · · · · · · · ·		
REVETMENT FOR SI	WF.13TR+60.775				009	[st	D 13			50 400 50	00, 005 00,							
TYPE OF WORK:	LOCATION:						- 2000	2 00 00 \$	00'1									

()

(

ESSE T		24.989 m³	•	10. 4/2 m ³	169.090 m²	1.305tf		36.164m²	
SLOP OF 1:2.0 (WET STON)E MASONIRY TYPE) CALCULATION	· CONCRETE (TYPE-CI)	V=1.80 m3/0.00m x 138.826 = 24.989	AVE BEDDING	V=0.75"/0.00m × 138.826 = 10.412 1. FORM(H<4.0m)	A=12.18 ^{m²} /10.00m × 138.826 = 169.090 1. -REINHORCING BAR	Nm x 138.826 = 1.305	JOINT FILLER	A=2.605 m/10.00m x 138.826 = 36.164 3	
REVETMENT FOR STATE SLOP OF 1:2.0 TYPE OF WORK:	WF. 13			300 JOINT FILLER 1= 10 SO SO GRAVEL PAVEMENT O (ELASTIC MATERIAL)	D 40@3500	150 300 GRAVEL BEDDING			

	REVETMENT FOR SIDE SLOP OF 1:2	P OF 1:20 CWET STONE MASONRY TYPE)	
TYPE OF WORK:		CALCULATION	RESULT
LOCATION:	W.F. 137R+60.775 ~ W.F. 139R+61, 545		
		CONCRETE CTYPE-CI)	
		100	
		$V = 1.605 \text{ m}^{3}/\text{lace} \times 8 \text{ places} = 12.840$	12.840 m3
		·GRAVEL BEDDING	
		V = 0.639 m3/place x & places = 5.112	S. 112 mg
	50 200	- FORM (H<4.0m)	
(ELASTIC MATERIAL)	CONCRETE, TYPE-		
		A=10.703 m2/place x 8places = 85.624	85.624m2
Sec	2000		
osi	D 10@300 013 000 00	· REINFORCING BAR	
_			
	D) GRAVEL BEDDING	W = 0.097 + Place x 8 places = 0.776	0.776 tf
	00-000		
	100 100	JOINT FILLER	
		A = 2.691 m2/place x 8places = 21.528	21,528 m2
	《《《··································		

RESULT			C 740	£ + 20.0		1,704 m³			25.694 m²				0.204tf			S, 382 m2			
O CWET STONE MASONRY TYPE) CALCULATION		CONCRETE (TYPE-CI)	1)=10017 m3/Land 50 Land		-GRAVEL BEDDING	V = 1.852 " / place × 2 places = 1.704		· FORM (H<4.0m)	A = 12,847 " / place x 2places = 25,694		· REINFORCING BAR		W=0.102 + place x 2 places = 0.204		JOINT FILLER	A=2.691 "/place x 2 places = 5,382			
REVETMENT FOR SIDE SLOP OF 1:2.(TYPE OF WORK: END UMAL	LOCATION: WE 137R+60.775 ~ WE.139R+61、545					50 50 50 50 50 50 50 50 50 50 50 50 50 5	CONCRET		- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	25 D 10 0 3000 E C E C E C E C E C E C E C E C E C		GABION CYLINDER	200 300	18					March Ma

TYPE OF WORK : REVETMENT FOR SIDE SLOPE OF 1:2.0

(WET STONE MASONRY TYPE)

LOCATION : WF.137R + 60.775 ~ WF.139R + 61.545

CALCULATION	RESULT
GABION MATTRESS	
t = 500 mm	
$L_1 = 129.724 \text{m}$ $L_2 = 129.504 \text{m}$	
(R = 147.5) $(R = 147.25)$	
$V_1 = 0.50 \times 3.0 \times 129.724 = 194.586$	
$V_2 = 0.50 \times 1.5 \times 129.504 = 97.128$	
TOTAL V = 291.714	291.714 m ³
RUBBLE STONE FILLING	
$A = \frac{1}{2} \times 1.00 \times 0.50 \times 2$ = 0.500 m ²	
	22.500 3
$V = 0.50 \times 131,043 = 65.522$	65.522 m ³
$\overline{(R} = 149)$	
CLEVAN ON A PROPER A SOLO COLY WASHINGTON AND COLUMN WIFE	PH DVC
GABION CYLINDER Ø 500 (GALVANIZED AND COATED WI	IH FVC)
	27.864 m ³
$V = \frac{\pi}{4} \times 0.50^2 \times (3.00 + 7.826 + 1.00) \times 6.00 \times 2 = 27.864$	27.004 111
SOIL FILLING	
V	
$V_1 = (3.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2$ = 35.478	
$V_2 = -\pi/4 \times 0.50^2 \times (3.00 + 7.826 + 1.00) \times 6.00 \times 2 = -27.864$	
TOTAL V = 7.614	7.614 m ³
<u>。他们是一个大块,可能是一个特殊的特殊的,就是是一个人的现在,我们就是这种特殊的,让他们就</u> 一种的是一个人的,我们就是一个人的,我们就是一个人的,我们就是一个人的,我们就是一个人的。	

REVETMENT FOR SIDE SLOP OF 1:2 (WET STONE MASONRY) WF.153R – $5.0 \sim$ WF.155R – 5.0

LOCATION

	CALCULATION	RESULT
₽ STR	UCTURAL EXCAVATION	
A ₁ =	$= (1.10 + 2.60) \times \frac{1}{2} \times 0.60 = 1.110 \text{ m}$	7
Λ1	- (1.10 1 2.00) X /2 X 0.00	
A ₂ =	= $(3.10 + 6.10) \times \frac{1}{2} \times 1.00$ = 4.600 m	²
A	= 1.118 x 10.00 x 0.50 = 5.590 m	1921) 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
A ₃ =	= 1.118 X 10.00 X 0.30 - 5.390 m	
A ₄ :	$= (1.50 + 2.70) \times \frac{1}{2} \times 1.70 = 3.570 \text{ m}$	² A
	11.000	
	A = 14.870 n	
V	$= 14.870 \times 90.00 = 1338.30$	1338.3 m ³
FF DAC	CKFILL WITH SELECTED SOIL	na dia <mark>Papakan Kabupitan.</mark> Managaran
DAC	ANILI WIII DEDECTED COIL	
A ₁ :	$= (0.60 + 1.10) \times \frac{1}{2} \times 0.50 = 0.425 \text{ m}$	'
	= $(0.50 + 1.50) \times \frac{1}{2} \times 1.00 - 0.50^2$ = 0.750 m	2
A ₂	= (0.50 + 1.50) x ½ x 1.00 - 0.50 = 0.750 III	
A ₃ :	$= (0.50 + 2.20) \times \frac{1}{2} \times 1.60 = 2.160 \text{ m}$	3
	A = 3.335 m	2
V	$= 3.335 \times 90.00 = 300.150$	300.2 m ³
e CDA	VEL BEDDING	
D GRA		
V_{l}	= $(1.118 \times 12.00 \times 14.70 \times 0.25)/15.00 \text{ m} \times 60.00 = 197.215$	
V.	$= 1.118 \times (12.00 + 9.00) \times \frac{1}{2} \times 14.70 \times 0.25 \times 2 = 86.282$	
V ₂	- 1.110 X (12.00 ± 7.00) X 72 X 14.70 X 0.23 X 2 - 80.282	
	TOTAL = 283.497	283.497 m ³
5 WE	T STONE MASONRY	
V_1	= $(1.118 \times 12.00 \times 14.70 \times 0.25)/15.00 \text{ m} \times 60.00 = 197.215$	
	$= 1.118 \times (12.00 + 9.00) \times \frac{1}{2} \times 14.70 \times 0.25 \times 2 = 86.282$	
¥2	- 1.110 A (12.00 + 7.00) A /1 A 14.70 A 0.23 A 2 - 00.202	
i i se kalitan	TOTAL = 283.497	283.497 m ³
3. 24.4.2 2.14.2		<u>and the State of Annual Annual Community of the State of Annual Community of An</u>

TYPE OF WORK:

REVETMENT FOR SIDE SLOP OF 1:2.0 (WET STONE MASONRY)

LOCATION :

WF.153R - 5.0 ~ WF.155R - 5.0

	CALCULATION		RESULT
CEMENT MORTAR PO	INTTING		
$V_1 = \{(1.118 \times (10.00) - 0\}$	0.2} x 14.70 / 15.00 m x 6	0.00	
		= 645.036	
The second secon	00) 1/ 00) - 1/ 70 -	2	
$V_2 = \{1.118 \times (10.00 + 7.118)\}$.00) x ½ - 0.2)} x 14.70 x	= 273.214	
		2.0	
	TOTAL	= 918.250	918.250 m³
Bergarija (1905.) Bergarija (1906.)			
	er en	打仗·多数的 医阴道性 60 mm	
			
	in the first of the section of the s		
RUBBLE STONE FILL	ING		
		- 0.500 m²	
RUBBLE STONE FILL A = ½ x 0.50 x 1.00		= 0.500 m ²	
A = ½ x 0.50 x 1.00	x 2		45.000 m ³
	x 2		45,000 m ³
A = ½ x 0.50 x 1.00	x 2		45,000 m ³
A = ½ x 0.50 x 1.00	x 2		45,000 m ³
A = ½ x 0.50 x 1.00	x 2	= 45,000	
$A = \frac{1}{2} \times 0.50 \times 1.00$ $V = 0.50 \times 90.00$	x 2	= 45,000	
$A = \frac{1}{2} \times 0.50 \times 1.00$ $V = 0.50 \times 90.00$	x 2	= 45,000	
A = ½ x 0.50 x 1.00 V = 0.50 x 90.00	x 2	= 45.000	
$A = \frac{1}{2} \times 0.50 \times 1.00$ $V = 0.50 \times 90.00$	x 2	= 45.000	
$A = \frac{1}{2} \times 0.50 \times 1.00$ $V = 0.50 \times 90.00$	x 2	= 45.000	
$A = \frac{1}{2} \times 0.50 \times 1.00$ $V = 0.50 \times 90.00$	x 2	= 45.000	
$A = \frac{1}{2} \times 0.50 \times 1.00$ $V = 0.50 \times 90.00$	x 2	= 45.000	
$A = \frac{1}{2} \times 0.50 \times 1.00$ $V = 0.50 \times 90.00$	x 2	= 45.000	
$A = \frac{1}{2} \times 0.50 \times 1.00$ $V = 0.50 \times 90.00$	x 2	= 45.000	
$A = \frac{1}{2} \times 0.50 \times 1.00$ $V = 0.50 \times 90.00$	x 2	= 45.000	

REVETMENT FOR SIDE SLOP OF 1: 2.0 (WET STONE MASONRY) WF.153R $-5.0 \sim$ WF.155R -5.0TYPE OF WORK: LOCATION:

	CALCULATION	RESULT
3 G.	ABION MATTRESS	
		1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1
Α	$= 3.00 \times 0.50 + 1.50 \times 0.50 \qquad = 2.250 \text{ m}^2$	
* * * * *	$= 2.25 \times 90.00 = 202.500$	202 600 }
V	$= 2.25 \times 90.00 = 202.500$	202.500 m ³
1		
		
· · · · · · · · · · · · · · · · · · ·		
100		
	A STATE BOOK OF BEING FOR THE STATE OF THE STATE OF THE	
2 Ta Aust		
G	ABION CYLINDER	
200		
Ø		
V	$= \pi \times 0.50^2 \times (3.00 + 7.826 + 1.00) = 2.322 \text{ m}^3/\text{place}$	en a linux de la cele
<u>V</u>	$= 2.322 \text{ m}^3/\text{place x 6 place x 2} = 27.864$	27.864 m³
<u> </u>		
4		
•	SOIL FILLING	
W	$= (3.00 + 7.826 + 1.00) \times 0.50 \times 3.00 \times 2 = 7.614$	7.614 m³
Υ.	(3.00 + 7.820 + 1.00) x 0.30 x 3.00 x 2 = 7.014	7,014 III
J W	EEPHOLE	
- 202 4 8		
n	= 26 places / 15.00 m	
7, 7, 1,		
•	PVC pipe \varnothing 50 (L = 0.80 m / pipe)	
	$L = 0.80 \times 26 \text{ places} / 15.00 \text{ m} \times 90.00 = 124.800$	124,800 m
• <u>.</u>	FILTER CLOTH	
- 7.1	$A = 0.856 \text{m}^2/\text{places} \times 104 \text{places} = 89.024$	89.024 m ²
<u> </u>		
44.4		

TYPE OF WORK : REVETMENT FOR SIDE SLOP OF 1: 2.0 (WET STONE MASONRY) LOCATION : WF.153R - 5.0 \sim WF.155R - 5.0

	CALCULATION	117		RESULT
	A OF CONCIDENT			
r 134	ASE CONCRETE	<u> </u>		
•	CONCRETE (TYPE – C1)		10.000	
	$V = 2.20 \text{ m}^3/10.00 \text{ m} \times 90.00$	=	19.800	19.800 m ³
		<u> </u>		
•	GRAVEL BEDDING			
	$V = 0.70 \text{ m}^3/10.00 \text{ m} \times 90.00$	==	6.300	6.300 m ³
	PODY (MY 24 A)			
•	FORM $(H < 4.0 \text{ m})$ A = 10.83 m ² /10.00 m x 90.00	<u> </u>	07.470	05.450
	$A = 10.83 \text{ m}/10.00 \text{ m} \times 90.00$		97.470	97.470 m ²
	DEDIFORCING DAD			
•	REINFORCING BAR $W = 0.10 \text{ tf} / 10.00 \text{ m} \times 90.00$	<u>. 1 jir</u>	0.000	0.000 (6
	W - 0.10 tt / 10.00 m X 90.00		0.900	0.900 tf
	JOINT FILTER			
A	$A = 0.22 \text{ m}^2/10.00 \text{ m} \times 90.00$		1.980	1.980 m ²
	A - 0.22 III / 10,00 III X 70.00		1.700	1.78U m
5 p	ARTITION WALL (V)			
- 47	AKTITION WALL (Y)			
	CONCRETE (TYPE-C1)			
· · · ·	$V = (13.416 \times 0.50 \times 0.30)$		2.012 m³/place	
- 1.1 - 1.3 m	$V^{1} = 2.012 \text{ m}^{3}/\text{place x 5 places}$		10.060	10.060 m ³
	Ziotz in ipiaco x 3 piaces		10.000	10.000 111
•	GRAVEL BEDDING	<u> </u>		
	$V = (0.50 + 0.70) \times \frac{1}{2} \times 0.10 \times 13.416$	=	0.805 m³/place	jalienik istolik (j. 1811) 1499 alie mandi (j
	$V^{1} = 0.805 \text{ m}^{3}/\text{place x 5 places}$	=	4.025	4.025 m ³
			a Salata ta asaa aa aa	7.025 III
•	FORM (H < 4.0 m)			
12.1	$A = (13.416 \times 0.50 \times 2)$	=	13.416 m³/place	
	$A^{T} = 13.416 \text{m}^{3}/\text{place} \times 5 \text{places}$	==	67.080	67.080 m ²
1				
•	REINFORCING BAR			*5
	D 13 $(W = 1.04 \text{ kgf/m})$	9 - 1		
1. 1.	$n_1 = 6$ Bars		April Christian Christia	
	$W_1 = (13.416 - 0.05 \times 2) \times 6 \text{ Bars } \times 1.04$	=	83.092	
<u> </u>		(4.) 15 °		
	D 10 $(W = 0.617 \text{ kgf/m})$	a. yarra		
	$n_2 = (13.416 - 0.05 \times 2 + 15 \times 0.01)$		46 Bars	
	$L = 0.20 \times 2 + 0.40 \times 2 + 15 \times 0.01$	=	1.350 m/Bar	
	$W_1 = 1.35 \times 46 \times 0.617$	=	38.316	fore Art series
	W = 121.408 kgf	=	0.121 tf/place	
11.10	$W^1 = 0.121$ tf/place x 5 places	=	0.605	0.605 tf
	JOINT FILTER			
	$A = (13.416 \times 0.25) \times 5 \text{ places}$.	16.770	16.770 m ²
1919				

REVETMENT FOR SIDE SLOP OF 1: 20 (WET STONE MASONRY) WF.153R $-5.0 \sim$ WF.155R -5.0

TYPE OF WORK: LOCATION:

1 / 1 · 1 · 1	CALCULATION		RESUL
DA DOTOT	ON WALL (II)		
rakiiii	ON WALL (H)		
CONC	RETE(TYPE – C1)		
CONC	REFECTIVE CITY		
V =	${(0.470+0.60)x1/2x0.30+1/2x0.2)x0}$	25}r14.70	
1. 1. ¥ 1. 3. 1. 1. 3	(0.470 + 0.00)x17 2x0.30 + 17 2x0.2)x0	2.745 m ³ /15.00 m	4
		2.745 III /15.00 III	
V =	2.745 m ³ /15.00 m x 90.00 =	16.470	14.670 г
GRAV	EL BEDDING		
<u> </u>	e dige di producti di Managarita de la casa de la grif di castilità di Africa.		
V =	$\{1/2x0.275x0.138+0.30x0.10+(0.10+$	0.325) $x1/2x0.50$ }	
	x 14.70 =	2.282	ing the Asia
V ¹ =	2.282 m ³ /15.00 m x 90.00 =	13.692	13.692 r
FORM	(H < 4.0 m)		
1 Oldy	CAS S COMP.		
A =	${0.65+0.47+0.25}x17.70 =$	19.404 m ³ /15.00 m	
	(3.05) (3.17) (3.25) (3.17) (3.25) (3.25)	17,404 III 713,00 III	
A¹ =	19.404 m ² /15.00 m x 90.00 =	116.424	116.424
REINF	ORCING BAR		
70.10	AND		
ע (3	(W = 1.04 kgf/m)		
n ₁ =	7 Bars	<u>kon kontra kan kontra kan periwasan.</u> Bajan di kentra kan kan berasaran kentra	
$W_1 =$		106.228	
D 10	(W = 0.617 kgf/m)		
<u>- 131 (3.1.1</u>	(14.70 0.05 - 20 0.20 1.1	50 50	
n ₂ =	$(14.70 - 0.05 \times 2) : 0.30 + 1 = 0.20 + 0.50 + 0.42 + 0.11 + 15 \times 0.01 =$	50 Bars	10 10 10 10 10 10 10 10 10 10 10 10 10 1
W ₂ =		48.743	en de la estada
	W = 155.031 kgf =	0.155 tf/15.00m	
		and the second s	
W' =	0.155 tf / 15.00 m x 90.00 =	0.930	0.930 t
TONT	PHITOD		10 (27 10 24
JOINT			
A. =	$\{(0.47 + 0.60) \times \frac{1}{2} \times 0.30 + \frac{1}{2} \times 0.21 \times 0.25\}$	3 x 7 places	
4 * I	((Carris VioV) A. 2. 30 + 72 A 0.21 A 0.25	1.307	
$A_2 =$	1.118 x 0.25 x 14.70 x 7 places =	28.761	
. 2015.0	TOTAL	30.068	30.068 r

TYPE OF WORK :

REVETMENT FOR SIDE SLOP OF 1: 20 (WET STONE MASONRY) WF.153R - 5.0 ~ WF.155R - 5.0

LOCATION

CALCULATION 11 19 V		RESULT
END WALL	ing Kalibaga Batta ang	.
• CONCRETE (TYPE-C1)		
• CONCRETE (TIPE-CI)		
$V = (13.416 \times 0.60 \times 0.30) =$	2.415 m ² /place	
and the state of t		
$V^1 = 2.415 \text{ m}^3/\text{place x 2 place} =$	4.830	4.830 m ³
GRAVEL BEDDING		
V - (0.40 + 0.10) (0.10 0.20) (1.40 0.20)		
$V = \{(0.40 \times 0.10) + (0.10 + 0.30) \times \frac{1}{2} \times 0.20\}$ $\times 13.416 =$	1.073 m ³ /place	
	1.075 III /piace	
$V' = 1.037 \text{ m}^3/\text{place x 2 place} =$	2.146	2.146 m ³
		* * * * * * * * * * * * * * * * * * * *
• FORM (H < 4.0 m)		
A = 13.416 x 0.60 x 2 =	16.099 m ² /place	
$A^1 = 16.099 \text{ m}^2/10.00 \text{ m } \times 2 =$	32.198	32.198 m ²
	52.170	52.196 III
REINFORCING BAR		
D 13 $(W = 1.04 \text{ kgf/m})$		
$n_1 = 6 \text{ Bars}$		
$n_1 = 6 \text{ Bars}$		
$W_1 = (13.416 - 0.05 \times 2) \times 6 \text{ Bars } \times 1.04 =$	83.092	
D 10 $(W = 0.617 \text{ kgf/m})$	Tradition to the Control	Company Comment
$n_2 = (13.416 - 0.05 \times 2) : 0.30 + 1 =$	46 Bars	
$L = 0.20 + 0.50 + 0.42 + 15 \times 0.01 =$	1.550 / Day	
L = 0.2011 0.30 1 0.42 + 13 X 0.01	1.550 m/Bar	
$W_2 = 1.55 \times 46 \times 0.617 = $	43.992	
W = 127.084 kgf =	0.127 tf / place	
WI = 0.155 CF I		
W ¹ = 0.155 tf/place x 2 place =	0.254	0.254 tf
rakan di kamanan di termengan pengan pengan di pengan di pengan pengan pengan pengan berangan di Pengan Pengan Pengan di pengan di pengangan pengan di pengan		
JOINT FILTER	<u>An an taon taona 6 an Talaga.</u> Taona ao amin'ny faritr'i Anton-de-de-dam-	Tariye sayaya sa
	<u>and the Artist and States and Artist</u> And the of Takener Land Control of the	and the second s
$A = (13.416 \times 0.25) \times 2 \text{ places} =$	6.708	6.708 m ²
<u>and a summer community of the state of the </u>	<u>and and the second control of the second co</u>	The state of the s

TYPE OF WORK : LOCATION : EARTH RETAINING WALL (WET STONE MASONRY) WF.153R $-\,5.00\sim$ WF.155R $-\,5.00$

	CALCULATION	RESULT
8	WET STONE MASONRY	14 m
-	$A_1 = (0.80 + 0.50) \times \frac{1}{2} \times 1.00 = 0.650 \text{ m}^2$	
-	A) = (0.00 + 0.00) X /2 X 1.00	
	$A_2 = (1.00 + 0.50) \times \frac{1}{2} \times 1.600 = 1.200 \text{ m}^2$	
L	$V_1 = (0.65 + 1.20) \times \frac{1}{2} \times 15.00 = 13.875$	
	$V_2 = 1.20 \times 60.00 = 72.000$	
:	$V_3 = (1.20 + 0.65) \times \frac{1}{2} \times 15.00 = 13.875$	
	TOTALL(V) + V + V + V + V + V + V + V + V + V +	00.750 -3
	$T O T A L (V_1 + V_2 + V_3) = 99.750$	99.750 m ³
	<u>는 보고 있는 것이 되는 것이 되고 있었다. 그 보고 된 그 분구에는 이 생각에 되었다. 한 그 보고는 것이 되는 것이 되었다.</u> 그들은 사람들은 사용을 있는 것들은 사람들이 되는 그리는 수있는 것이 되는 것을 하고 있는 사람들이 되었다. 나를 다음	
8	GRAVEL BEDDING	
		新 <u>们。这一点。</u>
	$A_1 = 0.10 \times 1.00$ = 0.100 m ²	
70 11	$A_2 = 0.10 \times 1.20$ = 0.12 m ²	
	$V_1 = (0.10 + 0.12) \times \frac{1}{2} \times 15.00 \times 2 = 3.300$	
	$V_2 = 0.12 \times 60.00 = 7.200$	
	- 42 - 1 0.12 X 00.00	
	$TOTAL (V_1 + V_2) = 10.500$	10.500 m ³
-6-	CEMENT MORTAR POINTING	
	$A_1 = 0.50 \times 90.00 = 45.000$	
	$A_2 = 0.90 \times 60.00 = 54.000$	
		00.000 7
	TOTAL = 99.000	99.000 m ²
召		
	$A = (0.50 + 1.00) \times \frac{1}{2} \times 1.60 \times 5 \text{ places} = 6.000$	6.000 m ²

·	<u> </u>		1		Τ		·		·	·	···	Ţ*******		r			·				·			
H :: 1000	מבסטרו							•								1578.889	W. W.							
HASONRY TYPE) CALCII ATION) x 0, 5 + 2		x 0,3 + 2 = 0.3/5 m2		= 3,000 m²) x 10 + 2 = 4.900 m ³		x 0.3 + 2 =0.645m3		1 x 0, 3 + 2 = 0,428 m3		+ 3 + @ + 6 + 6 = 10.826m2		x 145.87 m = 1578.889	(R=142.15)							
12 O (NET STONE)		() (2,2 + 2,75		(S (1.2 + 0.9)		(3) 1, 0 × 3.0		(4.8+43.4)		(2,6 + 1,7)		(1.7 + 1.15)		TOTAL = 0 +3		1 = 10.826								
7 70K	TRUCTURAL EXCANATION	WF-103L+ 1.3m ~ WF.160L +34.				J. OC CO.		1.6		- /	X	TELESON	IOLE		3	1,000	1.0 MASE CO.	NCRETE CCI	0		CABIGI GOZI OR	<i>/</i> ``		
NOOW TO TAKE	TYPE OF WORN:	LOCATION				<u>s</u>	TAND	ARD	CROS	S SEC	NOIT	OF R	EVET.	MENT	(WF	.163 -	WF.1	66+2	7m)					

RESULT				:		,			200.717	MG														
		= 0.400 m	= 0,463 m2		=0.513 m2		= 1.376m2		717.005=	M 3					- 1 - 1									
		7 7	2 -		2 7		@		7 m	2,15m)													a haray ika sa	
MASOURY 79		6) X D.5	0,73 X 0,5		2.8) x 0.5		† (3) †		x 143.87	(R = 142.				- Committee of the comm										
ET STOWE		(1.0+0.	+5117		(125+0.		() = 7 V		1,376															
OF 112 D (WET STOWE MASOURY TYPE) O'SOIL	+ 32.0m	0	<u>©</u>		<u>@</u>		TOTA		ξ λ															
	+			GRAVI	3,000	ENT	1,000 200 70x				W	000				1	2,060	_300 						
7 FOX	-1.5m ~				OP CONCE	haa J	1			· · ·	MASOKR			1 600		1,000	3,800	2,00 RUSEI	O E STON	1	4.5			
REVETHEN											VEL OE				m	The coulding	1,500			S DESIGNATION IN STREET	00 X	(3)		
E OF WORK:	OCATION		· · · · · · · · · · · · · · · · · · ·		• <u>st</u>	ANDA	RD CF	ROSS	SECT	CION (OF RE	VETM E C	ENT	(WF.1	6 3 - V	/F.166	5+27	<u>m)</u>						
Type	007									2-	64													_

TYPE OF WORK : REVETMENT FOR SIDE SLOPE OF 1:2.0 (WET STONE MASONRY) LOCATION : WF.163L + 1.50 m \sim WF.166L + 32.0

CALCULATION		RESULT
GRAVEL BEDDING		
$A_1 = 1.118 \times 9.0 \text{ m} \times 14.70 / 15.0 \text{ m}$	$= 147.911 \text{ m}^2 / 15.0 \text{ m}$	Section 1
$A_2 = 0.70 \times 14.70 / 15.0 \text{ m}$	$= 10.290 \text{ m}^2 / 15.0 \text{ m}$	
V (147 01) 10 00 14 0 0 14 0 0 0 0 0 0 0 0 0 0 0 0		
$V = (147.911 + 10.29) / 15.0 \times 145.87 \times 0.25$	= 384.613	384.613 m ³
WET STONE MASONRY		
WEI STONE WASONKI - A STONE ST		
$A_1 = 1.118 \times 9.0 \text{ m} \times 14.70 / 15.0 \text{ m}$	$= 147.911 \text{ m}^2 / 15.0 \text{ m}$	
$A_2 = 0.70 \times 14.70 / 15.0 \text{ m}$	$= 10.290 \mathrm{m}^2 / 15.0 \mathrm{m}$	
$V = (147.911 + 10.29) / 15.0 \times 145.87 \times 0.25$	= 384.613	384.613 m ³
CEMENT MORTAR POINTING		
$A_1 = 1.118 \times 7.0 \text{ m} \times 14.70 / 15.0 \text{ m}$	$= 115.042 \mathrm{m}^2/15.0 \mathrm{m}$	
$A_2 = 0.70 \times 14.70 / 15.0 \text{ m}$	$= 10.290 \mathrm{m^2/15.0 m}$	
$V = (115.042 + 10.29) / 15.0 \times 145.87$	1010.010	
V (113.042 + 10.29)/ 13.0 x 143.8/	= 1218.812	1218.812 m ³
WEEP HOLE		
PVC PIPE Ø 50 (L = 0.80 m/pipe)		
n = 12 places / 15.0 m		
$L = 12 \text{ places} / 15.0 \text{ m} \times 145.87 \times 0.80$	= 93.357	93.357 m
FILTER CLOTH		
A = 0.056 × 12 × 1 × × × 15 0 × 145 007		
$A = 0.856 \times 12 \text{ places} / 15.0 \text{ m} \times 145.87$	= 99.892	99.892 m ²
GABION MATTRESS		
$t = 500 \mathrm{mm}$		
$L_1 = 141.820 \mathrm{m}$ $L_2 = 141.600 \mathrm{m}$		
(R = 137.5) $(R = 137.25)$		
$V_1 = 0.50 \times 3.0 \times 141.820$	= 212.730	
$V_2 = 0.50 \times 3.0 \times 137.250$	= 205.875	
TOTAL V	= 418.605	418.605 m ³

TYPE OF WORK : REVETMENT FOR SIDE SLOPE OF 1:2.0 (WET STONE MASONRY)

LOCATION : WF.163L + 1.50 m ~ WF.166L + 32.0

RUBBLE STONE FILLING $A = \frac{1}{2} \times 1.00 \times 0.50 \times 2$ $= 0.500 \text{ m}^2$ $V = 0.50 \times 143.120$ $= 71.560$ $(R = 139)$ GABION CYLINDER \emptyset 500 (GALVANIZED AND COATED WITH PVC) $V = \frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $= 30.221$ 30.221 m ³ SOIL FILLING $V_1 = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2$ $V_2 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_3 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_4 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_5 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_7 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_8 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2$ $V_9 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.$	CALCULATION	RESULT
$V = 0.50 \times 143,120 = 71.560 $ $(R = 139)$ GABION CYLINDER Ø 500 (GALVANIZED AND COATED WITH PVC) $V = \frac{\pi}{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = 30.221 $ 30.221 m^{3} SOIL FILLING $V_{1} = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2 = 38.478$ $V_{2} = -\frac{\pi}{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ $TOTAL V = 8.267 $ 8.267 m^{3}	UBBLE STONE FILLING	
$V = 0.50 \times 143,120 = 71.560 $ $(R = 139)$ GABION CYLINDER Ø 500 (GALVANIZED AND COATED WITH PVC) $V = \frac{\pi}{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = 30.221 $ 30.221 m^{3} SOIL FILLING $V_{1} = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2 = 38.478$ $V_{2} = -\frac{\pi}{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ $TOTAL V = 8.267 $ 8.267 m^{3}		
GABION CYLINDER Ø 500 (GALVANIZED AND COATED WITH PVC) $V = \sqrt[8]{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = 30.221$ 30.221 m ³ SOIL FILLING $V_{1} = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2 = 38.478$ $V_{2} = -\sqrt[8]{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ TOTAL V = 8.267 8.267 m ³	$x = \frac{1}{2} \times 1.00 \times 0.50 \times 2$ = 0.500 m ²	
GABION CYLINDER Ø 500 (GALVANIZED AND COATED WITH PVC) $V = \sqrt[8]{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = 30.221$ 30.221 m ³ SOIL FILLING $V_{1} = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2 = 38.478$ $V_{2} = -\sqrt[8]{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ TOTAL V = 8.267 8.267 m ³		
GABION CYLINDER # 500 (GALVANIZED AND COATED WITH PVC) $V = \frac{\pi}{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = 30.221$ 30.221 m ³ SOIL FILLING $V_{1} = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2 = 38.478$ $V_{2} = -\frac{\pi}{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ TOTAL V = 8.267 8.267 m ³		71.560 m ³
$V = \frac{\pi}{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = 30.221$ 30.221 m ³ SOIL FILLING $V_{1} = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2 = 38.478$ $V_{2} = -\frac{\pi}{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ TOTAL V = 8.267 8.267 m ³	(R = 139)	
$V = \frac{\pi}{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = 30.221$ 30.221 m ³ SOIL FILLING $V_{1} = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2 = 38.478$ $V_{2} = -\frac{\pi}{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ TOTAL V = 8.267 8.267 m ³		
SOLL FILLING $V_1 = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2 = 38.478$ $V_2 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ $TOTAL V = 8.267 \qquad 8.267 \text{m}^3$	ABION CYLINDER Ø 500 (GALVANIZED AND COATED WITH PVC)	
SOLL FILLING $V_1 = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2 = 38.478$ $V_2 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ $TOTAL V = 8.267 \qquad 8.267 \text{m}^3$		
SOIL FILLING $V_1 = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2 = 38.478$ $V_2 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ $TOTAL V = 8.267 8.267 m^3$	$v = \frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = 30.221$	30.221 m ³
$V_{1} = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2 = 38.478$ $V_{2} = -\frac{\pi}{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ $TOTAL V = 8.267 \qquad 8.267 \text{m}^{3}$		
$V_{1} = (4.00 + 7.826 + 1.00) \times 3.00 \times 0.50 \times 2 = 38.478$ $V_{2} = -\frac{\pi}{4} \times 0.50^{2} \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ $TOTAL V = 8.267 \qquad 8.267 \text{m}^{3}$	OIL FILLING	
$V_2 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ TOTAL V = 8.267 8.267 m ³		
$V_2 = -\frac{\pi}{4} \times 0.50^2 \times (4.00 + 7.826 + 1.00) \times 6.00 \times 2 = -30.221$ TOTAL V = 8.267 8.267 m ³		
TOTAL V = 8.267 8.267 m ³		
	TOTALV = 8.267	8.267 m ³
	""一个""我们的,我看到我们的时间,我们的一个人,就是我们的一样,就是我们的一样的,我 <u>我们也不是一样的,这个一样的,我们</u>	
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E OF 120 (WET STONE MASOWRY TYPE)	CALCULATION	A CONCRETE(TYPE-C1)	V = 2.20 m 3/10.0m x 142,25 = 31.295 31.295 m3	(R=138)	· GRAUFL BEDDING	(1) 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	V=0.70 m3/10,0m x 142,25 = 9,958 9,958 m3		- FORH (H < 4.0 m)		A = 10.83 m3/10.0m X 142.25 = 150.057 150.057m2		. REINTORCING BAR		W = 0,10 th/20m x 142,25 = 1,423 142	JOINT FILLER	A = 0.22 m / 100m x 142.25 = 3.130 3.130m	· · · · · · · · · · · · · · · · · · ·	
REVETWENT FOR SIDE SLOPE OF	BASE CONCRETE.	WF. 1632 + 1.5m~ WF. 166732.0m					SOO CONCRETE TYPE C1	200 300	010 @ 300			400	100	BASE CONCRCETE	SCALE OF STATE OF STA				
* *	TYPE OF WORK	OCATION							00	00G	100								

	RESULT		 27.149 m3			11. 372 m				183.711 4				J+8151		•	39.291 m2				
THE THOUSE STATE STATE STONE HAS OURY TYPE)	CALCULATION	· CONCRETE CTYPE-CI)	V= 1.80 m3/0,0m x 150.83 m =27.149 2	¥)	. GRAUEL REDDING	V=0.75 m3/10,0m x 150.83 m = 11.312 1		· FORH (H< 4.0m)		A = 12,18 m = /10,0m x 150:83m = 183,711 1		- REINFORCING BAR		W = 0.094 +f/10,0m x 150.83m = 1418	· JOINT FILLER		A= 2,605 m=10,0 x ×150.83 m =39,291 3	1			
70 70 70 40 10 10 10 10 10 10 10 10 10 10 10 10 10	TYPE OF WICHK TY O'CH, OFTE	1					GRAVEL PAVEMENT 30 JOINT FILLER 1*10		013 1		GRAVEL BEDDING / 100 300 100 150		TOP CONCRETE								

OF 1:2,0 (WET STONE KMSONRY TYPE) CALCULATION RESINT		CONCKEICITTE	V= 1.605 m3/ place x 9 places = 14.445 14.445m3	GAAVEL BEDDING	V = 0,639 m3/place x 9 places = 5,751 5,751 m3	FORM (H < 4.0 m)		= 10,703 m3/place x 9 places = 96.327 96.327 m3		REINTOROING BAR		= 0,097 +f place x 9 places = 0.873 o.873 +f		JOINT FILLER	A = 2.691 m2/place x 9 ylaces = 24.219 24.219 m2				
REVETHENT FOR SIDE SLOPE	DKK: FARTITION WALL	LOCATION: WF. 163L + 1.5m ~ WF. 166L + 52.0m				20 200 20	JOINT FILLER 1-10 IELASTIC MATERIAL)	000000000000000000000000000000000000000	210 300	S S S S S S S S S S S S S S S S S S S	1-8	W 100 NOT LEVEL TO THE TOTAL T	SCALE D				,我们就是这个人,我们就是这个人,我们就是我们的一个人,我们就是这个人,我们就是我们的一个人,我们也会会看到了一个人,我们也会会看到这些人,我们就是我们的一个人, 我们就是我们的一个人,我们就是我们		

	ers.				:											٠.			
	RESULT			3.854 m3			1,704 m3		25.694m2			0.204tf	•		5,382 m²				-
20 CWET STONE MASONRY TYPE)			·CONCRETE (TYPE-CI)	V=1.927 = 3.854	. 1	-GRAVEL BEDDING	V= 1.852 "/place × 2places = 1.704	-FORM (H<4.0m)	A = 12.847 m2/place x 2places = 25.694		· REINFORCING BAR	W = 0.102		JOINT FILLER	A=2.691 ">place x 2 places = 5,382		「		
REVETMENT FIRE STOP OF 1:2.	TYPE OF WORK: END WALL	LOCATION: WF. 1834 +1.5m ~ WF. 760L + 32.0m						91	7	20 0 0 10 0 300 0 0 0 0 0 0 0 0 0 0 0 0 0		SOO SOO	18			10. 11. 11. 11. 11. 11. 11. 11. 11. 11.			

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RESULT		76.743m2	28.725m ³	3.918+f	65.022 m					
CALCULATION	70742	CONCRETE (TYPE C-1)	GRAVEL BEDDING FORM (HC4.0m)	1	JOINT TILLER				· 1. (1) ·	
TYPE OF WORK:	LOCATION:									