

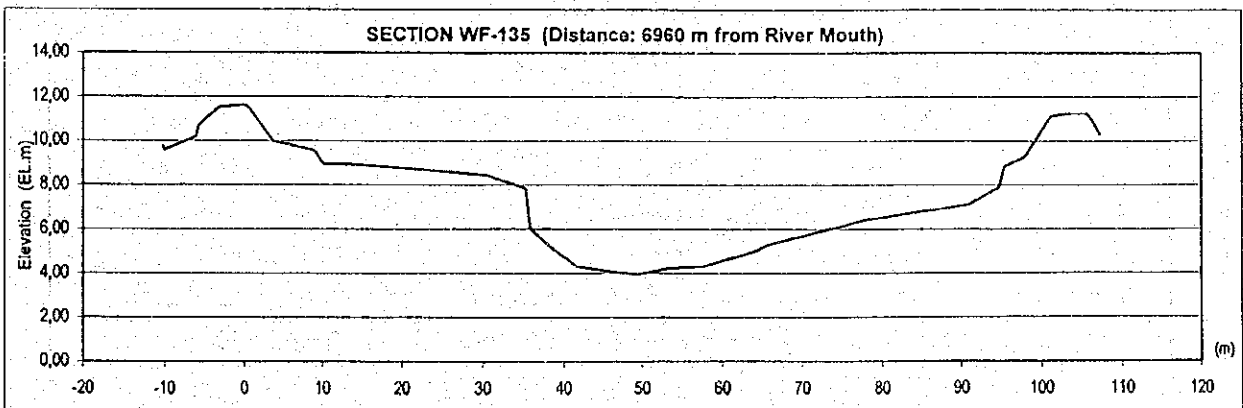
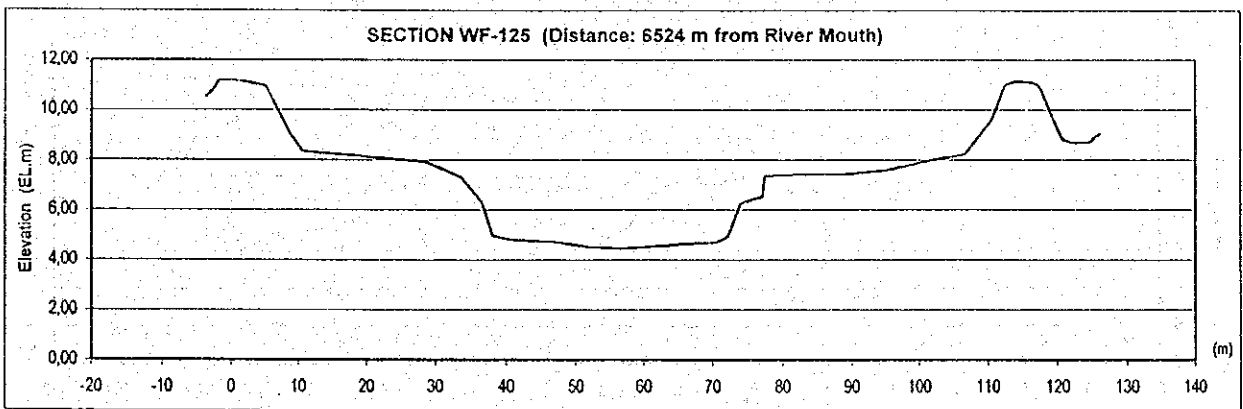
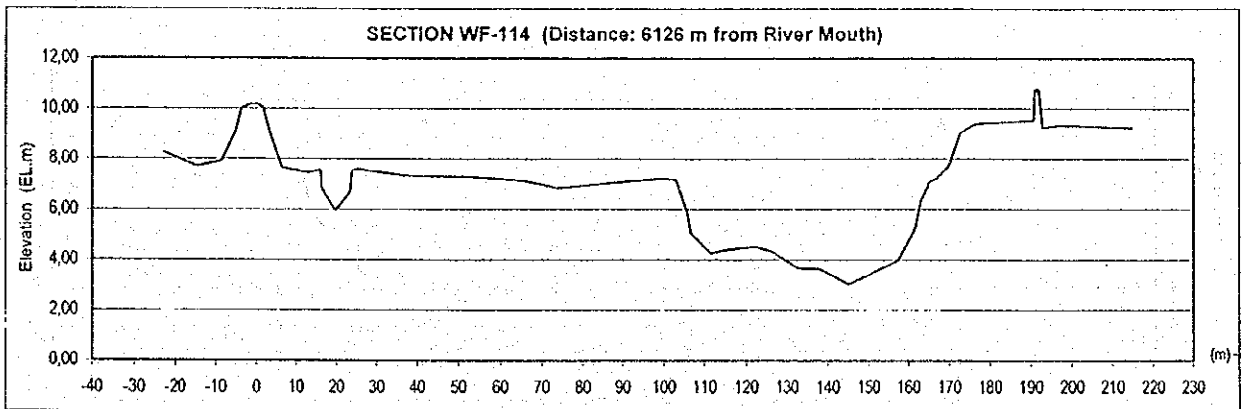
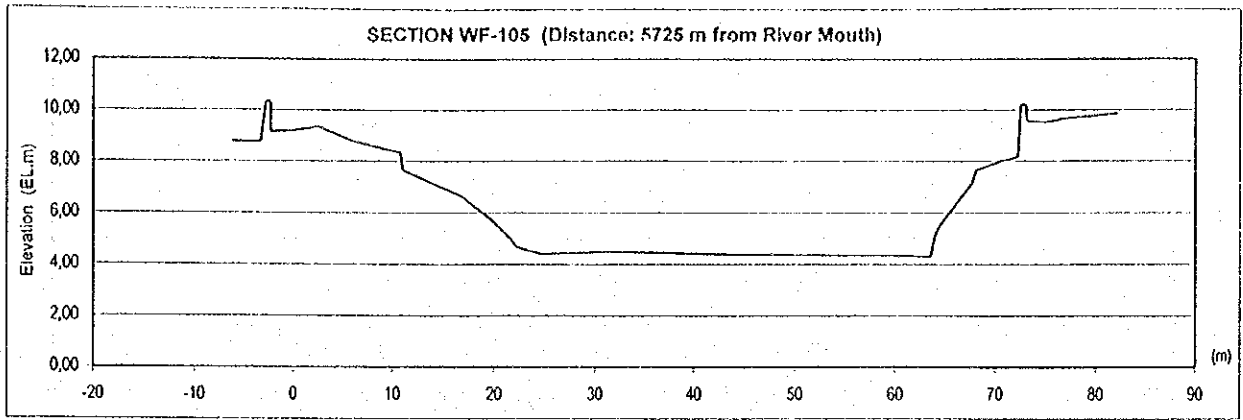
2.1.3 Garang River

(1) River Cross Sections

The typical cross sections of Garang River are shown in the following figures.

(2) River Flow Capacity

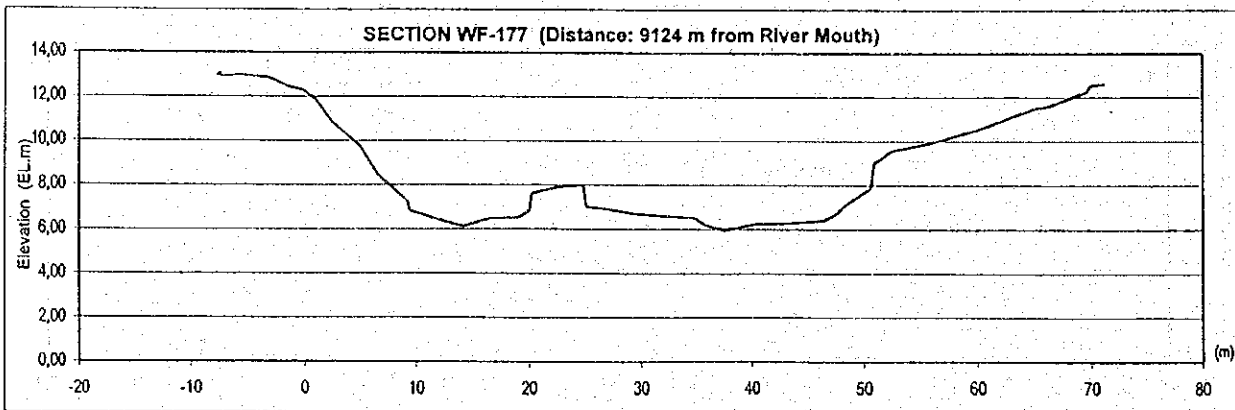
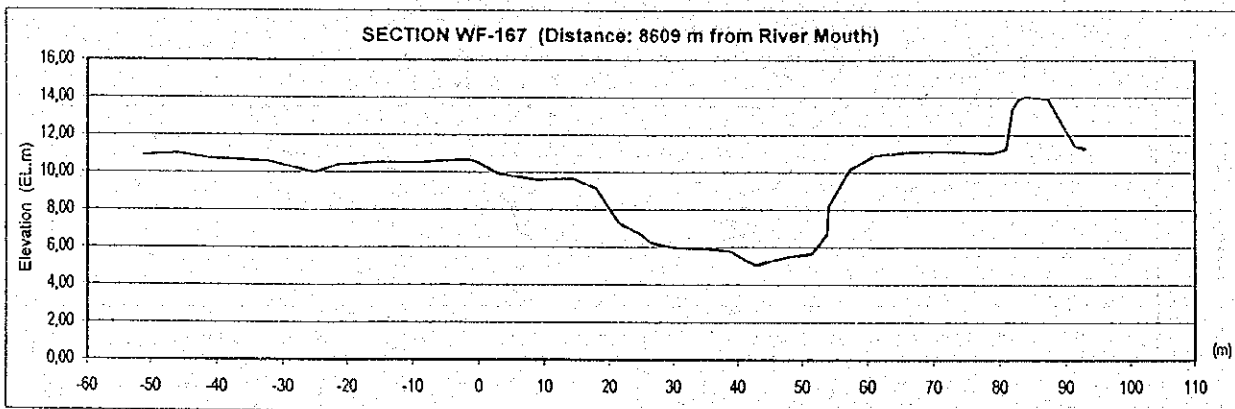
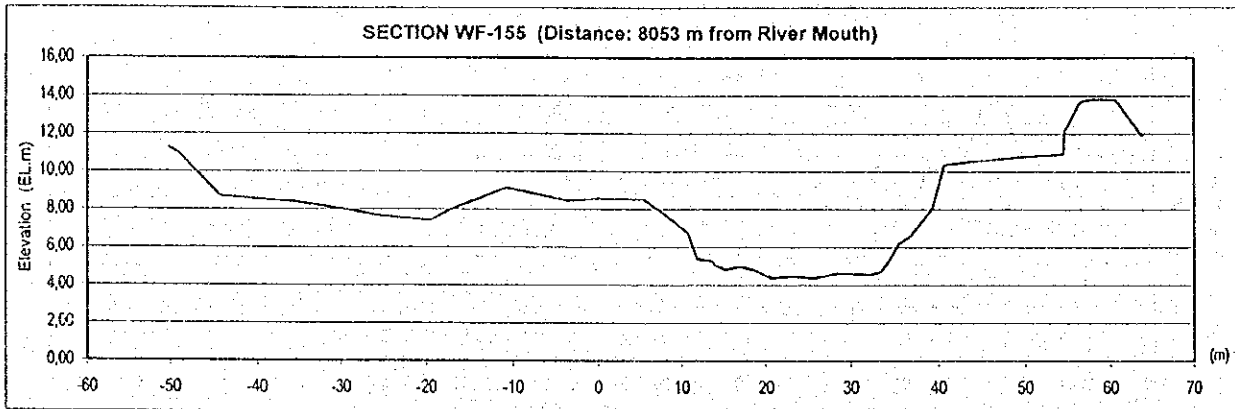
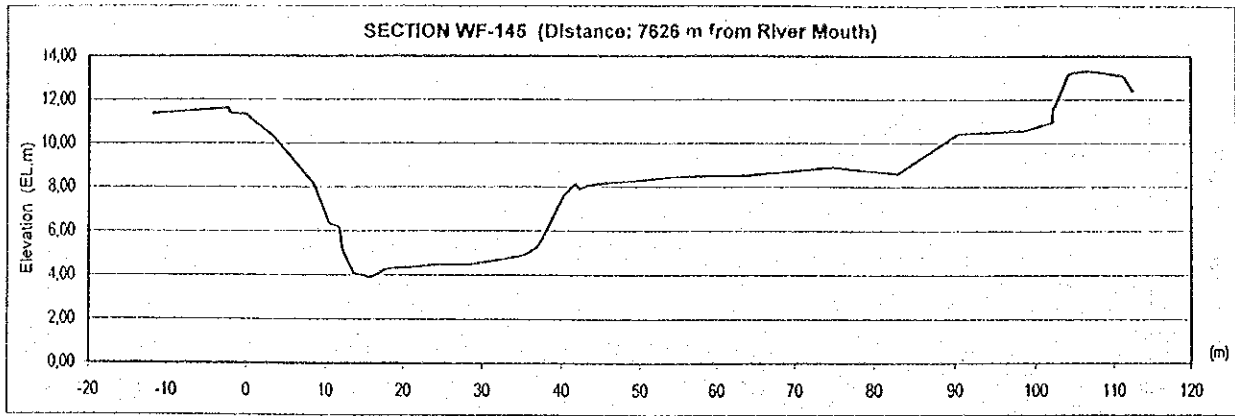
The flow capacity of channel was obtained based on the water level profile under several discharges. The calculation was done for the discharge of 300 m³/s, 500 m³/s, 700 m³/s, 900 m³/s, 1,000 m³/s, 1,200 m³/s. And, the water flow profiles and the chart of the flow capacity are shown in the following sheets.



THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

JAPAN INTERNATIONAL COOPERATION AGENCY

Fig.



THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

Fig.

JAPAN INTERNATIONAL COOPERATION AGENCY

24	WF-123	11.792	655.5	4.832	131.2	1.831	0.035	1200	32.3	2.66E-01	5.03E-04	238.01	15.428
25	WF-124	11.772	593.4	4.781	120	2.022	0.035	1200	30.9	2.95E-01	6.22E-04	291.44	17.072
26	WF-125	11.662	462.1	5.048	96.3	2.597	0.035	1200	32.8	3.69E-01	9.54E-04	471.92	21.724
27	WF-126	11.662	426.8	4.407	135.5	2.811	0.035	1200	51.6	4.28E-01	1.34E-03	578.75	24.057
28	WF-127	11.845	513.3	4.133	124.7	2.338	0.035	1200	49.9	3.67E-01	1.01E-03	408.87	20.221
29	WF-128	11.98	648	4.49	130.3	1.852	0.035	1200	39.1	2.79E-01	5.67E-04	249.59	15.798
30	WF-129	12.038	739.1	5.194	133.6	1.624	0.035	1200	38.4	2.28E-01	3.59E-04	182.73	13.518
31	WF-130	11.905	476.5	1.837	522.4	2.519	0.035	1200	29.5	5.94E-01	3.45E-03	621.72	24.934
32	WF-131	11.849	384.2	4.271	206	3.124	0.035	1200	45.5	4.83E-01	1.73E-03	721.92	26.869
33	WF-132	12.257	762.5	3.15	169.5	1.574	0.035	1200	30.7	2.83E-01	6.57E-04	202.83	14.242
34	WF-133	12.291	791.4	2.827	247.7	1.515	0.035	1200	37.4	2.88E-01	7.05E-04	195.2	13.971
35	WF-134	12.077	442.7	4.122	126.2	2.711	0.035	1200	41.7	4.27E-01	1.35E-03	550.09	23.454
36	WF-135	12.191	458.7	4.561	213.4	2.616	0.035	1200	72	3.91E-01	1.11E-03	495.39	22.257
37	WF-136	12.262	458.4	3.945	98.9	2.618	0.035	1200	58.2	4.21E-01	1.35E-03	520.77	22.82
38	WF-137	12.471	535.2	3.339	218	2.242	0.035	1200	89.7	3.92E-01	1.23E-03	403.81	20.095
39	WF-138	12.522	509.2	4.492	122.6	2.356	0.035	1200	72.5	3.55E-01	9.18E-04	404.02	20.1
40	WF-139	12.645	597.9	5.364	285.8	2.007	0.035	1200	61.8	2.77E-01	5.26E-04	276.26	16.621
41	WF-140	12.752	770.9	5.736	134.8	1.557	0.035	1200	61.6	2.08E-01	2.89E-04	162.52	12.748
42	WF-141	12.703	605	4.467	130.5	1.984	0.035	1200	59.1	3.00E-01	6.55E-04	286.82	16.936
43	WF-142	12.546	406.6	4.684	307.5	2.951	0.035	1200	86.4	4.36E-01	1.36E-03	624.86	24.997
44	WF-143	12.221	285.6	5.499	94.8	4.202	0.035	1200	73.1	5.72E-01	2.23E-03	1200.66	34.651
45	WF-144	12.134	255.7	5.758	117.3	4.694	0.035	1200	56.2	6.25E-01	2.62E-03	1475.51	38.412
46	WF-145	12.949	418.7	3.249	290.8	2.866	0.035	1200	46.9	5.08E-01	2.09E-03	665.83	25.804
47	WF-146	12.5	278.4	5.49	138.3	4.311	0.035	1200	36.2	5.88E-01	2.35E-03	1264.65	35.562
48	WF-147	13.083	406.9	4.781	143.9	2.949	0.035	1200	42.4	4.31E-01	1.32E-03	619.86	24.897
49	WF-148	12.793	301.6	6.391	71.3	3.978	0.035	1200	50.3	5.03E-01	1.63E-03	1023.77	31.996
50	WF-149	12.785	281.2	5.505	174.2	4.268	0.035	1200	58	5.81E-01	2.30E-03	1238.38	35.191
51	WF-150	12.876	280.7	5.682	124.2	4.275	0.035	1200	41.5	5.73E-01	2.21E-03	1229.58	35.065
52	WF-151	13.283	354.3	5.69	64.5	3.387	0.035	1200	33.4	4.54E-01	1.38E-03	771.22	27.771
53	WF-152	13.323	355.2	5.495	79.8	3.379	0.035	1200	26.5	4.60E-01	1.44E-03	776.64	27.868
54	WF-153	13.487	396.1	6.341	65.3	3.029	0.035	1200	40.9	3.84E-01	9.58E-04	595.29	24.398
55	WF-154	13.644	454.2	4.948	117.8	2.642	0.035	1200	45.8	3.79E-01	1.01E-03	491.76	22.176
56	WF-155	13.788	521.6	3.487	218.5	2.301	0.035	1200	51.8	3.94E-01	1.23E-03	419.07	20.471
57	WF-156	13.317	297.6	5.556	84	4.032	0.035	1200	54.5	5.47E-01	2.02E-03	1102.03	33.197
58	WF-157	13.663	356.7	5.84	164.8	3.364	0.035	1200	56.1	4.45E-01	1.32E-03	754.53	27.469
59	WF-158	13.975	471.1	3.848	399.6	2.547	0.035	1200	50.2	4.15E-01	1.32E-03	497.1	22.296
60	WF-159	13.764	345.9	5.263	134.5	3.469	0.035	1200	48.6	4.83E-01	1.61E-03	830.45	28.817
61	WF-160	13.83	336.6	5.097	145.8	3.565	0.035	1200	59.6	5.04E-01	1.78E-03	886.38	29.772
62	WF-161	13.788	313.3	5.49	101.8	3.83	0.035	1200	32	5.22E-01	1.86E-03	998.33	31.596
63	WF-162	13.881	312.1	6.045	69.5	3.845	0.035	1200	56.4	5.00E-01	1.65E-03	974.39	31.215
64	WF-163	14.004	321.3	6.435	89.4	3.734	0.035	1200	52.3	4.70E-01	1.43E-03	900.13	30.002
65	WF-164	14.469	505	5.204	117.7	2.376	0.035	1200	38	3.33E-01	7.67E-04	391.14	19.777
66	WF-165	14.416	433.5	3.555	324.1	2.768	0.035	1200	39.6	4.69E-01	1.73E-03	602.82	24.552
67	WF-166	14.345	382.2	4.372	291.4	3.14	0.035	1200	23.9	4.80E-01	1.69E-03	723.86	26.905
68	WF-167	14.416	383.8	5.38	127	3.126	0.035	1200	45.1	4.31E-01	1.27E-03	659.62	25.877
69	WF-168	14.708	537.2	4.168	102.3	2.234	0.035	1200	44.5	3.50E-01	9.12E-04	372.29	19.295
70	WF-169	14.446	354.9	5.367	101.8	3.381	0.035	1200	55.1	4.66E-01	1.49E-03	783.89	27.998
71	WF-170	14.618	387.3	4.804	229	3.098	0.035	1200	53.4	4.52E-01	1.45E-03	683.07	26.136
72	WF-171	14.701	391	5.321	151.7	3.069	0.035	1200	55	4.25E-01	1.24E-03	647.75	25.451
73	WF-172	14.864	440.4	4.44	220	2.725	0.035	1200	49.5	4.13E-01	1.25E-03	542.34	23.288
74	WF-173	14.955	449.9	4.667	309.2	2.667	0.035	1200	63.1	3.94E-01	1.12E-03	511.03	22.606
75	WF-174	14.987	426.9	3.797	465.9	2.811	0.035	1200	52.6	4.61E-01	1.63E-03	608.15	24.661
76	WF-175	15.288	688.8	5.128	198.1	1.742	0.035	1200	51.1	2.46E-01	4.20E-04	211.27	14.535
77	WF-176	15.206	535.2	6.161	99.9	2.242	0.035	1200	41.9	2.89E-01	5.45E-04	329.27	18.146
78	WF-177	15.121	443.9	6.615	90.9	2.703	0.035	1200	49.3	3.36E-01	7.21E-04	467.34	21.618
79	WF-178	15.365	587.6	1.816	220.3	2.042	0.035	1200	55	4.84E-01	2.31E-03	410.37	20.257
80	WF-179	15.483	656.6	6.543	122.9	1.828	0.035	1200	58	2.28E-01	3.34E-04	214.4	14.642

H-QHYO

NO	D-NAME	H	Q	NO	D-NAME	H	Q	NO	D-NAME	H	Q
1	WF-100	9.4	0	2	WF-101	9.4	0	3	WF-102	9.4	0
		7.1	300			7.934	300			7.976	300
		7.8	500			8.38	500			8.461	500
		8.51	700			8.928	700			9.031	700
		9.03	900			9.429	900			9.549	900
		9.3	1010			9.691	1010			9.819	1010
		9.4	1200			9.95	1200			10.111	1200
4	WF-103	9.4	0	5	WF-104	9.4	0	6	WF-105	9.4	0
		8.03	300			8.072	300			8.107	300
		8.554	500			8.616	500			8.659	500
		9.137	700			9.202	700			9.243	700
		9.664	900			9.728	900			9.769	900
		9.937	1010			10	1010			10.04	1010
		10.251	1200			10.319	1200			10.363	1200
7	WF-106	9.4	0	8	WF-107	9.4	0	9	WF-108	9.4	0
		8.131	300			8.165	300			8.231	300
		8.694	500			8.758	500			8.871	500
		9.294	700			9.35	700			9.49	700
		9.834	900			9.868	900			10.032	900
		10.112	1010			10.132	1010			10.308	1010
		10.453	1200			10.454	1200			10.664	1200
10	WF-109	9.4	0	11	WF-110	9.4	0	12	WF-111	9.4	0
		8.223	300			8.256	300			8.337	300
		8.833	500			8.885	500			9.048	500
		9.409	700			9.471	700			9.72	700
		9.897	900			9.966	900			10.309	900
		10.14	1010			10.211	1010			10.609	1010
		10.424	1200			10.507	1200			11.029	1200
13	WF-112	9.4	0	14	WF-113	9.4	0	15	WF-114	9.4	0
		8.387	300			8.43	300			8.446	300
		9.135	500			9.222	500			9.251	500
		9.837	700			9.968	700			10.009	700
		10.455	900			10.632	900			10.685	900
		10.771	1010			10.972	1010			11.032	1010
		11.222	1200			11.472	1200			11.544	1200
16	WF-115	9.4	0	17	WF-116	9.4	0	18	WF-117	9.4	0
		8.463	300			8.473	300			8.45	300
		9.281	500			9.294	500			9.254	500
		10.05	700			10.064	700			10.014	700
		10.735	900			10.751	900			10.693	900
		11.088	1010			11.105	1010			11.044	1010
		11.61	1200			11.629	1200			11.565	1200
19	WF-118	9.4	0	20	WF-119	9.4	0	21	WF-120	9.4	0
		8.501	300			8.525	300			8.54	300
		9.339	500			9.37	500			9.391	500
		10.128	700			10.163	700			10.188	700
		10.838	900			10.877	900			10.905	900
		11.206	1010			11.246	1010			11.277	1010
		11.761	1200			11.805	1200			11.84	1200
22	WF-121	9.4	0	23	WF-122	9.4	0	24	WF-123	9.4	0
		8.515	300			8.555	300			8.549	300
		9.363	500			9.397	500			9.383	500
		10.157	700			10.187	700			10.167	700
		10.872	900			10.898	900			10.873	900
		11.242	1010			11.267	1010			11.239	1010
		11.801	1200			11.826	1200			11.792	1200
25	WF-124	9.4	0	26	WF-125	9.4	0	27	WF-126	9.4	0
		8.553	300			8.563	300			8.589	300
		9.38	500			9.356	500			9.382	500
		10.157	700			10.105	700			10.124	700
		10.859	900			10.783	900			10.794	900
		11.222	1010			11.134	1010			11.141	1010
		11.772	1200			11.662	1200			11.662	1200
28	WF-127	9.4	0	29	WF-128	9.4	0	30	WF-129	9.4	0
		8.642	300			8.701	300			8.76	300
		9.473	500			9.556	500			9.615	500
		10.244	700			10.343	700			10.401	700
		10.939	900			11.052	900			11.11	900
		11.3	1010			11.42	1010			11.477	1010
		11.845	1200			11.98	1200			12.038	1200

31	WF-130	9.4	0	32 WF-131	9.4	0	33 WF-132	9.4	0
		8.73	300		8.723	300		8.793	300
		9.559	500		9.542	500		9.702	500
		10.321	700		10.293	700		10.529	700
		11.009	900		10.969	900		11.275	900
		11.364	1010		11.319	1010		11.661	1010
		11.905	1200		11.849	1200		12.257	1200
34	WF-133	9.4	0	35 WF-134	9.4	0	36 WF-135	9.4	0
		8.804	300		8.79	300		8.876	300
		9.723	500		9.645	500		9.747	500
		10.555	700		10.432	700		10.54	700
		11.304	900		11.143	900		11.254	900
		11.692	1010		11.512	1010		11.623	1010
		12.291	1200		12.077	1200		12.191	1200
37	WF-136	9.4	0	38 WF-137	9.4	0	39 WF-138	9.4	0
		8.85	300		8.955	300		9.096	300
		9.749	500		9.888	500		10.003	500
		10.565	700		10.726	700		10.82	700
		11.299	900		11.479	900		11.554	900
		11.678	1010		11.868	1010		11.933	1010
		12.262	1200		12.471	1200		12.522	1200
40	WF-139	9.4	0	41 WF-140	9.4	0	42 WF-141	9.4	0
		9.118	300		9.183	300		9.151	300
		10.048	500		10.126	500		10.091	500
		10.888	700		10.974	700		10.935	700
		11.644	900		11.738	900		11.696	900
		12.035	1010		12.133	1010		12.089	1010
		12.645	1200		12.752	1200		12.703	1200
43	WF-142	9.4	0	44 WF-143	9.4	0	45 WF-144	9.4	0
		9.17	300		9.18	300		9.191	300
		10.066	500		10.023	500		10.025	500
		10.87	700		10.756	700		10.741	700
		11.594	900		11.4	900		11.36	900
		11.967	1010		11.727	1010		11.671	1010
		12.546	1200		12.221	1200		12.134	1200
46	WF-145	9.4	0	47 WF-146	9.4	0	48 WF-147	9.4	0
		9.306	300		9.248	300		9.366	300
		10.283	500		10.14	500		10.368	500
		11.148	700		10.92	700		11.25	700
		11.923	900		11.608	900		12.039	900
		12.322	1010		11.96	1010		12.444	1010
		12.949	1200		12.5	1200		13.083	1200
49	WF-148	9.4	0	50 WF-149	9.4	0	51 WF-150	9.4	0
		9.403	300		9.402	300		9.451	300
		10.349	500		10.348	500		10.415	500
		11.161	700		11.159	700		11.237	700
		11.873	900		11.869	900		11.953	900
		12.234	1010		12.229	1010		12.315	1010
		12.793	1200		12.785	1200		12.876	1200
52	WF-151	9.4	0	53 WF-152	9.4	0	54 WF-153	9.4	0
		9.47	300		9.499	300		9.603	300
		10.51	500		10.544	500		10.666	500
		11.415	700		11.452	700		11.586	700
		12.22	900		12.258	900		12.404	900
		12.632	1010		12.671	1010		12.823	1010
		13.283	1200		13.323	1200		13.487	1200
55	WF-154	9.4	0	56 WF-155	9.4	0	57 WF-156	9.4	0
		9.637	300		9.696	300		9.65	300
		10.732	500		10.815	500		10.673	500
		11.681	700		11.783	700		11.546	700
		12.525	900		12.644	900		12.314	900
		12.957	1010		13.085	1010		12.704	1010
		13.644	1200		13.788	1200		13.317	1200
58	WF-157	9.4	0	59 WF-158	9.4	0	60 WF-159	9.4	0
		9.731	300		9.826	300		9.79	300
		10.816	500		10.968	500		10.889	500
		11.748	700		11.949	700		11.831	700
		12.573	900		12.82	900		12.664	900
		12.994	1010		13.265	1010		13.089	1010
		13.663	1200		13.975	1200		13.764	1200
61	WF-160	9.4	0	62 WF-161	9.4	0	63 WF-162	9.4	0
		9.845	300		9.888	300		9.975	300
		10.951	500		10.978	500		11.076	500
		11.896	700		11.904	700		12.005	700
		12.73	900		12.719	900		12.818	900
		13.155	1010		13.133	1010		13.23	1010
		13.83	1200		13.788	1200		13.881	1200

64	WF-163	9.4	0	65	WF-164	9.4	0	66	WF-165	9.4	0
		10.007	300			10.072	300			10.043	300
		11.129	500			11.301	500			11.269	500
		12.078	700			12.339	700			12.302	700
		12.911	900			13.255	900			13.212	900
		13.334	1010			13.722	1010			13.675	1010
		14.004	1200			14.469	1200			14.416	1200
67	WF-166	9.4	0	68	WF-167	9.4	0	69	WF-168	9.4	0
		10.135	300			10.199	300			10.277	300
		11.299	500			11.367	500			11.504	500
		12.295	700			12.364	700			12.55	700
		13.177	900			13.247	900			13.477	900
		13.626	1010			13.697	1010			13.95	1010
		14.345	1200			14.416	1200			14.708	1200
70	WF-169	9.4	0	71	WF-170	9.4	0	72	WF-171	9.4	0
		10.259	300			10.313	300			10.367	300
		11.421	500			11.507	500			11.571	500
		12.413	700			12.526	700			12.596	700
		13.288	900			13.426	900			13.502	900
		13.734	1010			13.884	1010			13.963	1010
		14.446	1200			14.618	1200			14.701	1200
73	WF-172	9.4	0	74	WF-173	9.4	0	75	WF-174	9.4	0
		10.437	300			10.505	300			10.538	300
		11.666	500			11.74	500			11.773	500
		12.712	700			12.791	700			12.825	700
		13.637	900			13.721	900			13.755	900
		14.109	1010			14.195	1010			14.228	1010
		14.864	1200			14.955	1200			14.987	1200
76	WF-175	9.4	0	77	WF-176	9.4	0	78	WF-177	9.4	0
		10.627	300			10.616	300			10.628	300
		11.919	500			11.888	500			11.873	500
		13.018	700			12.971	700			12.935	700
		13.992	900			13.931	900			13.874	900
		14.489	1010			14.42	1010			14.353	1010
		15.288	1200			15.206	1200			15.121	1200
79	WF-178	9.4	0	80	WF-179	9.4	0				
		10.716	300			10.737	300				
		11.995	500			12.037	500				
		13.09	700			13.152	700				
		14.063	900			14.146	900				
		14.561	1010			14.656	1010				
		15.365	1200			15.483	1200				

RYUKA NOU

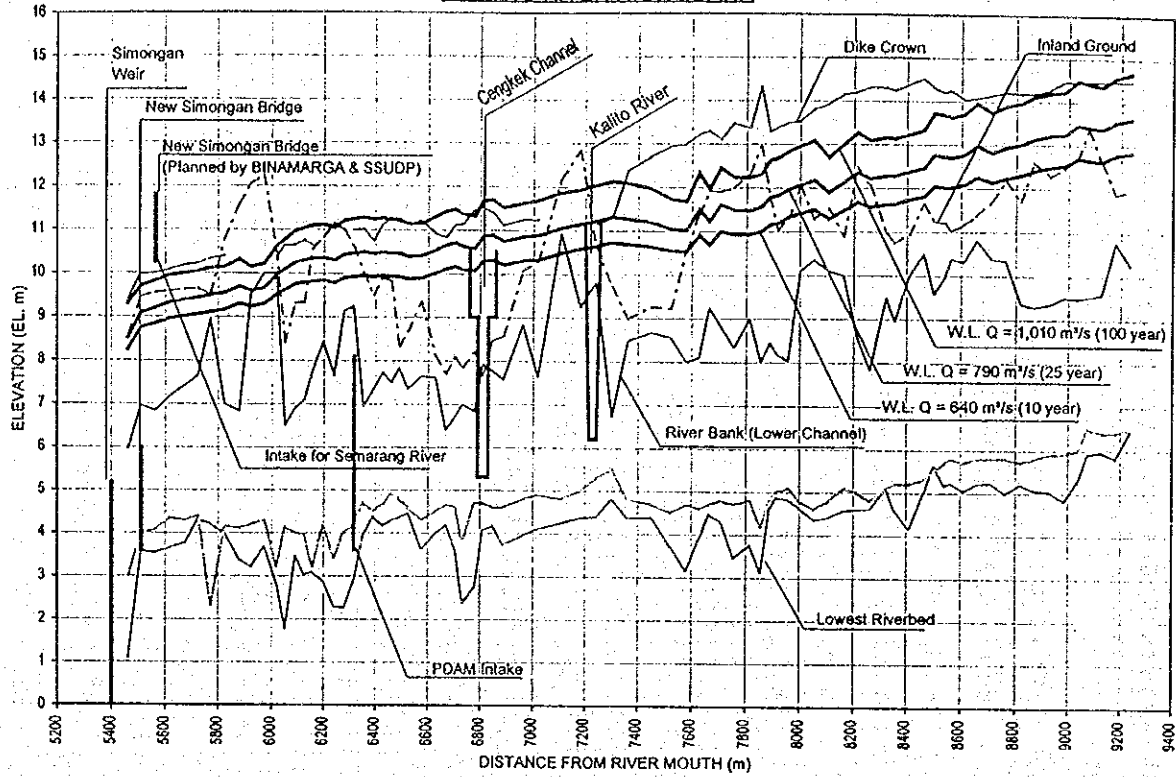
RYOKU HYO

Freeboard = 1.0 m

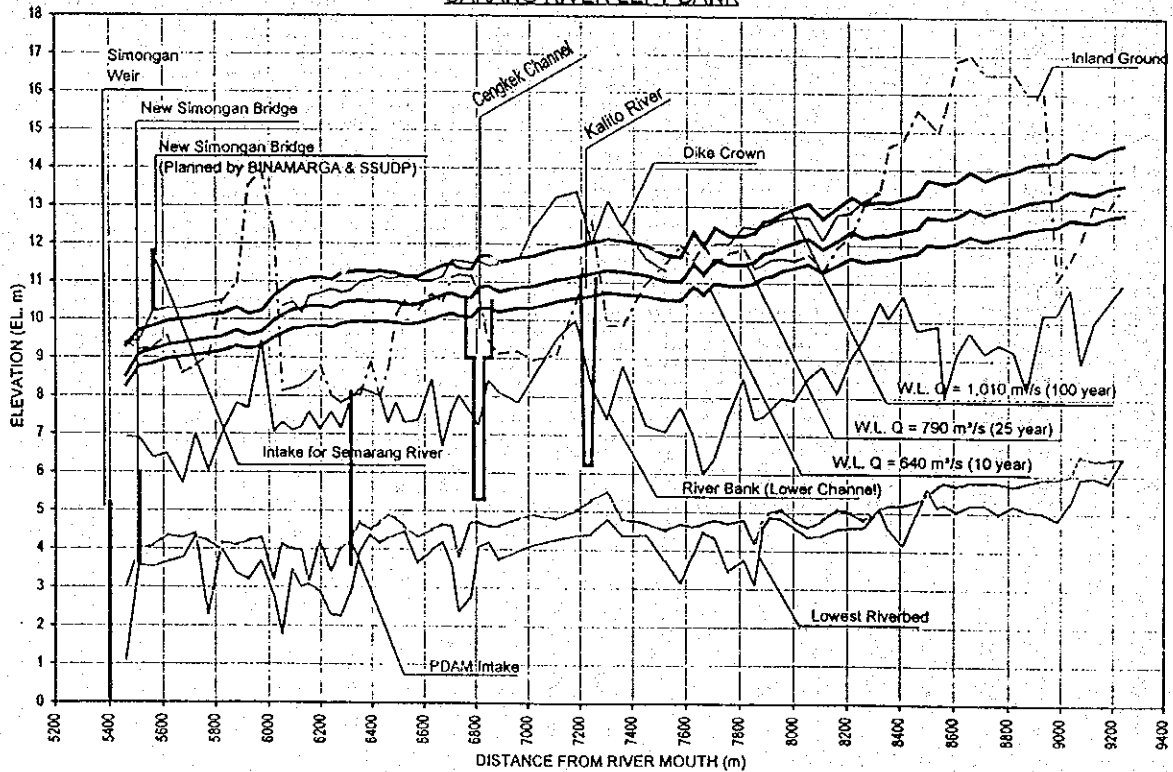
PAGE 18

NO	D-NAME	H	Q	NO	D-NAME	H	Q	NO	D-NAME	H	Q
1	WF-100	9.45	1301.1	2	WF-101	9.43	900.4	3	WF-102	9.42	847.9
4	WF-103	9.42	804.3	5	WF-104	9.77	916.5	6	WF-105	9.53	806
7	WF-106	9.84	902.3	8	WF-107	9.46	740.4	9	WF-108	10.83	1294.5
10	WF-109	11.7	2255.6	11	WF-110	11.8	2224.1	12	WF-111	10.5	969.2
13	WF-112	10.34	860.8	14	WF-113	9.46	560.1	15	WF-114	9.41	539.1
16	WF-115	9.61	581.4	17	WF-116	9.68	596.1	18	WF-117	9.79	637.6
19	WF-118	9.71	589.9	20	WF-119	9.76	594.2	21	WF-120	10	649.8
22	WF-121	9.74	590.7	23	WF-122	10.15	690	24	WF-123	10.07	673.5
25	WF-124	10.1	684.2	26	WF-125	10.11	701.3	27	WF-126	10.34	761.8
28	WF-127	9.91	609.2	29	WF-128	9.83	565.9	30	WF-129	10.11	622
31	WF-130	10.04	622.2	32	WF-131	10.46	747.2	33	WF-132	10.53	700.1
34	WF-133	10.43	667.8	35	WF-134	10.46	707.4	36	WF-135	10.52	694.6
37	WF-136	11.38	923	38	WF-137	12.25	1128.4	39	WF-138	11.83	979.4
40	WF-139	12.48	1147	41	WF-140	9.9	447.5	42	WF-141	11.35	806
43	WF-142	11.77	951.2	44	WF-143	11	772.8	45	WF-144	11.02	787.1
46	WF-145	11.31	739.7	47	WF-146	11.22	784.1	48	WF-147	10.94	625.9
49	WF-148	12.45	1081.4	50	WF-149	12.28	1026.8	51	WF-150	11.45	756.9
52	WF-151	11.5	719.9	53	WF-152	11.55	723.1	54	WF-153	11.7	726.3
55	WF-154	11.65	693	56	WF-155	11.66	672.7	57	WF-156	11.7	738
58	WF-157	11.79	709.6	59	WF-158	11.86	680.5	60	WF-159	12.04	747.9
61	WF-160	12.39	815.5	62	WF-161	13.23	1037.2	63	WF-162	13.25	1015.7
64	WF-163	13.52	1061.2	65	WF-164	13.3	910.3	66	WF-165	13.28	915.9
67	WF-166	13.25	917.5	68	WF-167	13.03	848.5	69	WF-168	13.07	809.1
70	WF-169	13.14	864.3	71	WF-170	13.21	849.7	72	WF-171	13.18	826.1
73	WF-172	13.19	800.2	74	WF-173	13.2	784.8	75	WF-174	13.45	831.7
76	WF-175	12.2	547.9	77	WF-176	12.3	572.1	78	WF-177	12.41	596.9
79	WF-178	12.7	624.9	80	WF-179	12.6	596.8				

GARANG RIVER RIGHT BANK



GARANG RIVER LEFT BANK



THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

Fig.

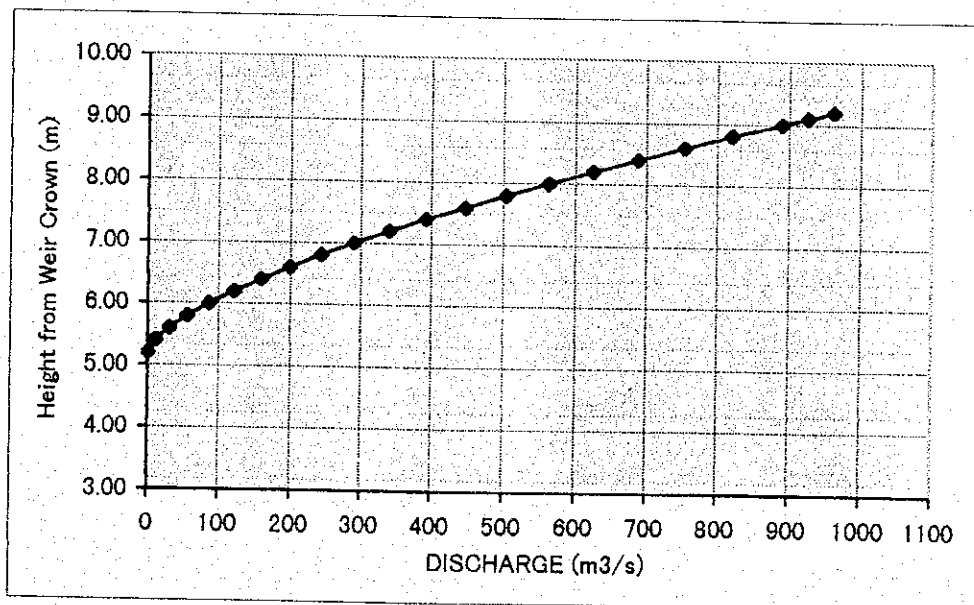
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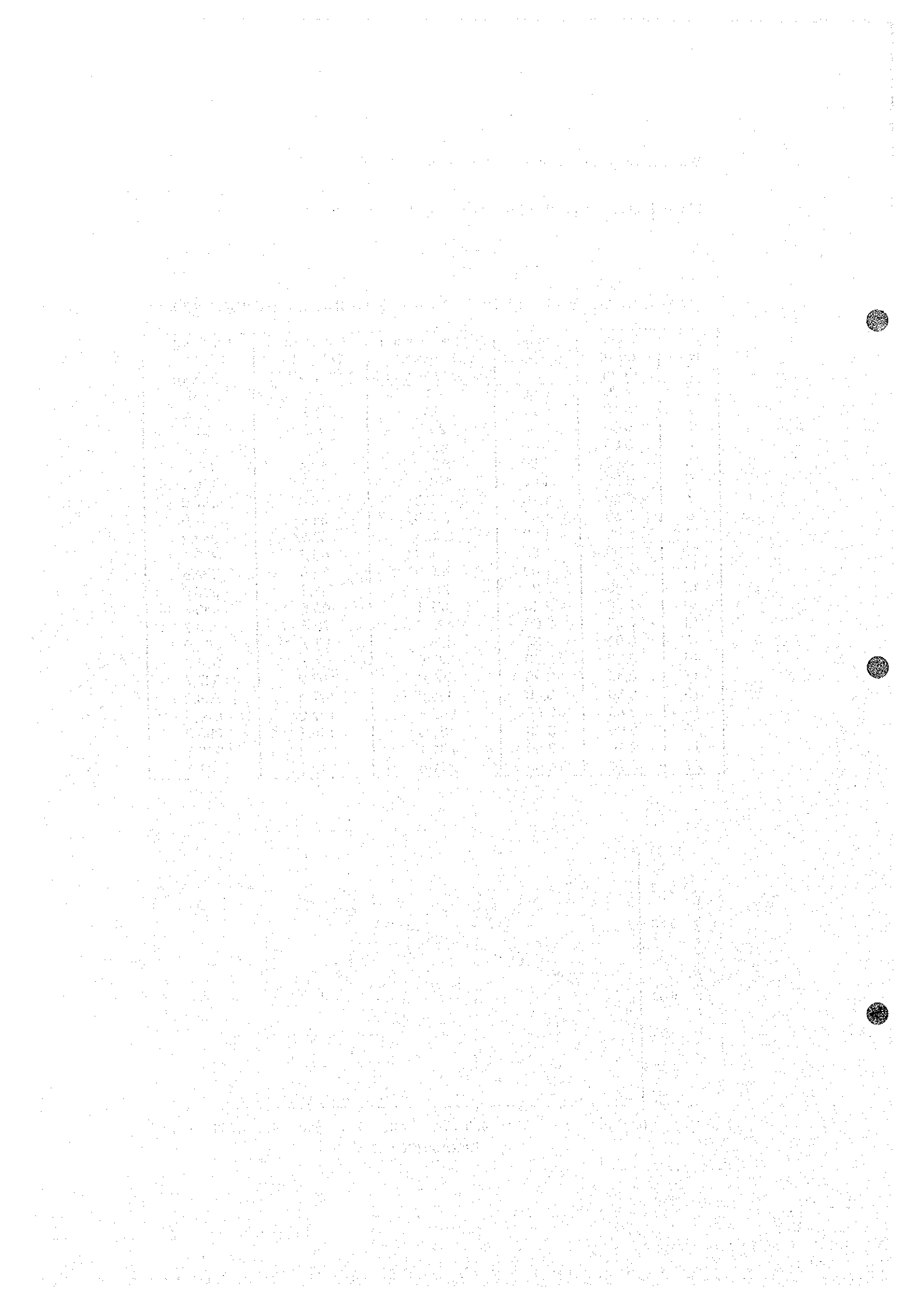
(3) Water Level and Discharge at Existing Simongan Weir

Flood discharge capacity of the weir was estimated as follows:

Table 3.1.1 WATER LEVEL-DISCHARGE RELATION AT SIMONGAN WEIR

No.	Water Level EL(m)	Head $h=H-5.2$ (m)	Center Portion Q_1 (m ³ /s) $=1.57*64.6*h^{1.5}$	Side Portion Q_2 (m ³ /s) $=1.8*10.4*h^{1.5}$	Discharge $Q=Q_1+Q_2$ (m ³ /s)
1	5.20	0.00	0.0	0.0	0.0
2	5.40	0.20	9.1	1.7	10.7
3	5.60	0.40	25.7	4.7	30.4
4	5.80	0.60	47.1	8.7	55.8
5	6.00	0.80	72.6	13.4	86.0
6	6.20	1.00	101.4	18.7	120.1
7	6.40	1.20	133.3	24.6	157.9
8	6.60	1.40	168.0	31.0	199.0
9	6.80	1.60	205.3	37.9	243.2
10	7.00	1.80	244.9	45.2	290.1
11	7.20	2.00	286.9	52.9	339.8
12	7.40	2.20	331.0	61.1	392.0
13	7.60	2.40	377.1	69.6	446.7
14	7.80	2.60	425.2	78.5	503.7
15	8.00	2.80	475.2	87.7	562.9
16	8.20	3.00	527.0	97.3	624.3
17	8.40	3.20	580.6	107.2	687.7
18	8.60	3.40	635.8	117.4	753.2
19	8.80	3.60	692.8	127.9	820.6
20	9.00	3.80	751.3	138.7	890.0
21	9.10	3.90	781.1	144.2	925.3
22	9.20	4.00	811.4	149.8	961.1





2.2 Design Riverbed and Channel Hydraulics

The design riverbed profiles of West Floodway and Garang River are determined based on the following considerations.

(1) West Floodway

Fig. 2.2.1 shows the change of riverbed profile between 1991 and 1997. Distinctive changes are observed as the riverbed aggradation in the river mouth area and bed degradation in the midstream and upstream. The riverbed of the river mouth is raised by about 1.0 m from the previous riverbed. However, this sedimentation does not extend to the offshore seabed as can be seen from Fig. 2.2.2.

The existing riverbed in the midstream and upstream is lowered by about 0.5 m. This is due to the cutting off the sediment flow by Simongan Weir. Remarkable riverbed degradation due to the local scouring is found as well in immediately downstream portions of three bridges. As to the riverbed gradient, a flat or rather gentle slope except the reverse bed slope of river mouth area, is formed.

Taking the said existing riverbed profile into account, the design riverbed is studied through the comparison of the following three (3) alternatives.

Alternative	Riverbed Elevation at River Mouth	Design Riverbed Gradient	Riverbed Elevation at Simongan Weir
Case-1	EL. -2.00	Level to 1/2,650	EL. -0.67
Case-2	EL. -2.50	Level to 1/2,650	EL. -1.17
Case-3	EL. -3.00	Level to 1/2,650	EL. -1.67

As for the design elevation of floodplain, the height of 3.0 to 3.5 m from the design riverbed is employed to avoid frequent flood inundation of floodplain as shown in Fig. 2.2.4. With this design height, the floodplain will not be submerged under the flood of 2-year return period or more for the whole channel stretches except the lowermost portion near the river mouth. This proposed ground elevation is almost the same height as that of existing floodplain.

Based on the above riverbed profiles and channel cross sections (schematically shown in Fig. 2.2.3), the flood water level profiles for the above alternatives are estimated as shown in Fig. 2.2.4. The freeboard between the underside of each bridge

girder and the high water level is also estimated as follows:

Alternative	Name of Bridge	Underside elevation of Bridge Girder	Water Level	Freeboard
Case-1A	North Ring Road. Br.	EL. 2.52 m	EL. 1.41 m	1.11
	Railway Bridge	EL. 3.50 m	EL. 3.32 m	0.18
	National Road Bridge	EL. 4.14 m	EL. 3.65 m	0.49
Case-2A	North Ring Road. Br.	EL. 2.52 m	EL. 1.10 m	1.42
	Railway Bridge	EL. 3.50 m	EL. 2.98 m	0.52
	National Road Bridge	EL. 4.14 m	EL. 3.33 m	0.81
Case-3A	North Ring Road. Br.	EL. 2.52 m	EL. 0.85 m	1.67
	Railway Bridge	EL. 3.50 m	EL. 2.64 m	0.86
	National Road Bridge	EL. 4.14 m	EL. 2.98 m	1.16

Case-1A:

Of the three alternatives the highest water level is obtained. It is almost the same elevation as the existing floodwall crest in the river stretches upstream from North Ring Road Bridge. Further, the freeboard between the water level and girders of Railway Bridge and National Road Bridge are rather small of 18 cm and 49 cm, respectively. As the results, the raising work of floodwall with big height and raising of two bridges are necessary. The impact on the existing river structures by channel excavation is negligible.

Case-2A:

The water level lower than the existing floodwall crest is obtained for the whole river stretch. The freeboard between water level and said bridge girders are 52 cm and 81 cm. The channel excavation is moderate with little impact on river structures.

Case-3A:

The lowest water level is obtained. However, channel excavation will affect most existing river structures and bridge foundations to a great deal. Further, the channel maintenance at river mouth will be difficult due to the heavy future sedimentation.

Judging from these advantages/disadvantages of each alternatives, Case-2A is preferred as the optimum river bed profile. As the results, the optimum longitudinal channel profile proposed is given as shown in Fig. 2.2.5.

- (2) Garang Rive (Simongan Weir to Confluence with Kreo River)

Comparing the current riverbed profile in 1997 with that in 1991, there is no big changes in overall riverbed profile except the locally scoured portions found in riverbed profile in 1997 as shown in Fig. 2.2.1. This is caused by an excessive sand mining activity. Therefore, the design riverbed gradient of 1/1,250, which was adopted as the stable riverbed slope in the F/S, is still applicable.

There are two (2) alternatives conceived as to what riverbed elevation is employed for the bottom of new Simongan Weir. The design riverbed profiles of each alternatives are summarized in the table below.

Alternative	Riverbed Elevation at Simongan Weir	Design Riverbed Gradient	Head of Hydraulic Drop *3
Case-1B	EL. +1.50 *1	1/1,250	1.5 m
Case-2B	EL. +3.00 *2	1/1,250	-

- *1 This is the average elevation of existing riverbed at Simongan Weir whose riverbed has been extremely lowered by local scouring.
- *2 This is the elevation of the point 0.6 m lower than the original riverbed at Simongan Weir.
- *3 Case-1B requires a hydraulic drop with the head of 1.5 m, while no hydraulic drops for Case-2B.

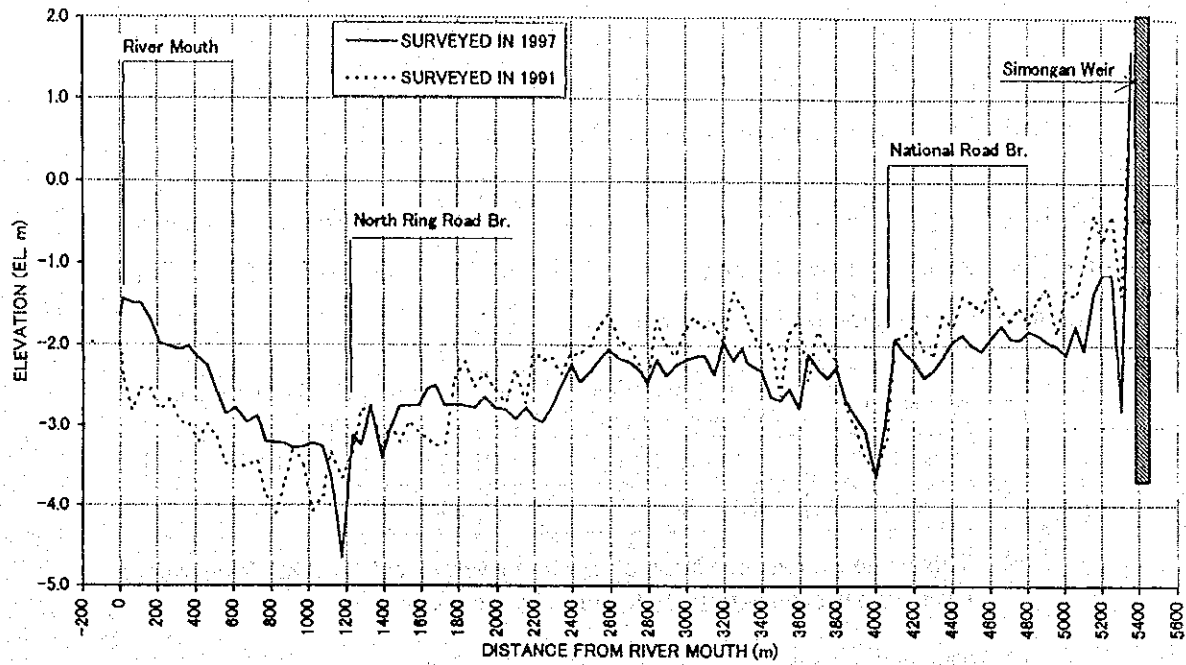
For these two cases, the flood water level profiles are estimated by non-uniform flow calculation and compared in Fig. 2.2.6.

The water level of Case-2B becomes about 2 m higher than that of Case-1B in the downstream stretches. Accordingly, the floodwall in this area can not confine the high flood level within a required freeboard level. This means that more raising of the existing floodwalls along the main river and its tributaries are required, resulting in increase of flood damage potential in the area.

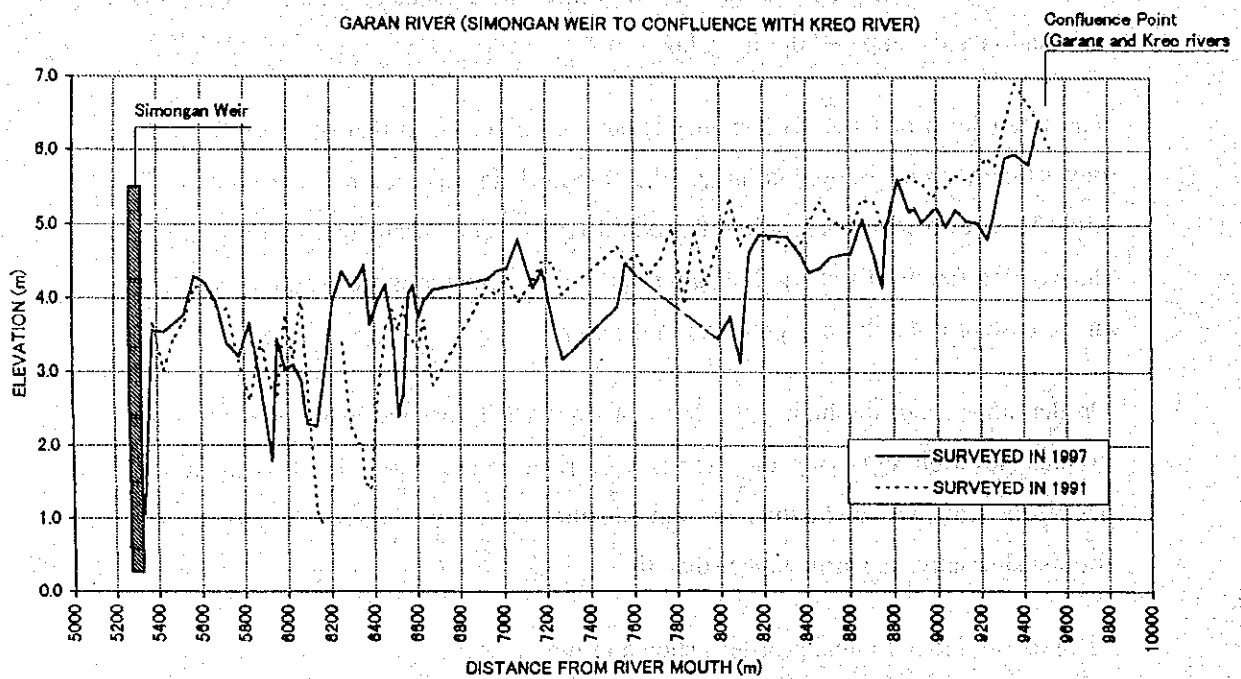
On the other hand, the high water level of Case-1B is lowered below the average ground elevation satisfying the premises of river improvement for Garang River. Therefore, Case-1B can be the most suitable alternative, even though the project cost for this alternative is a little higher than the.

The proposed longitudinal profile is shown in Fig. 2.2.7.

WEST FLOODWAY (RIVER MOUTH TO SIMONGAN WEIR)



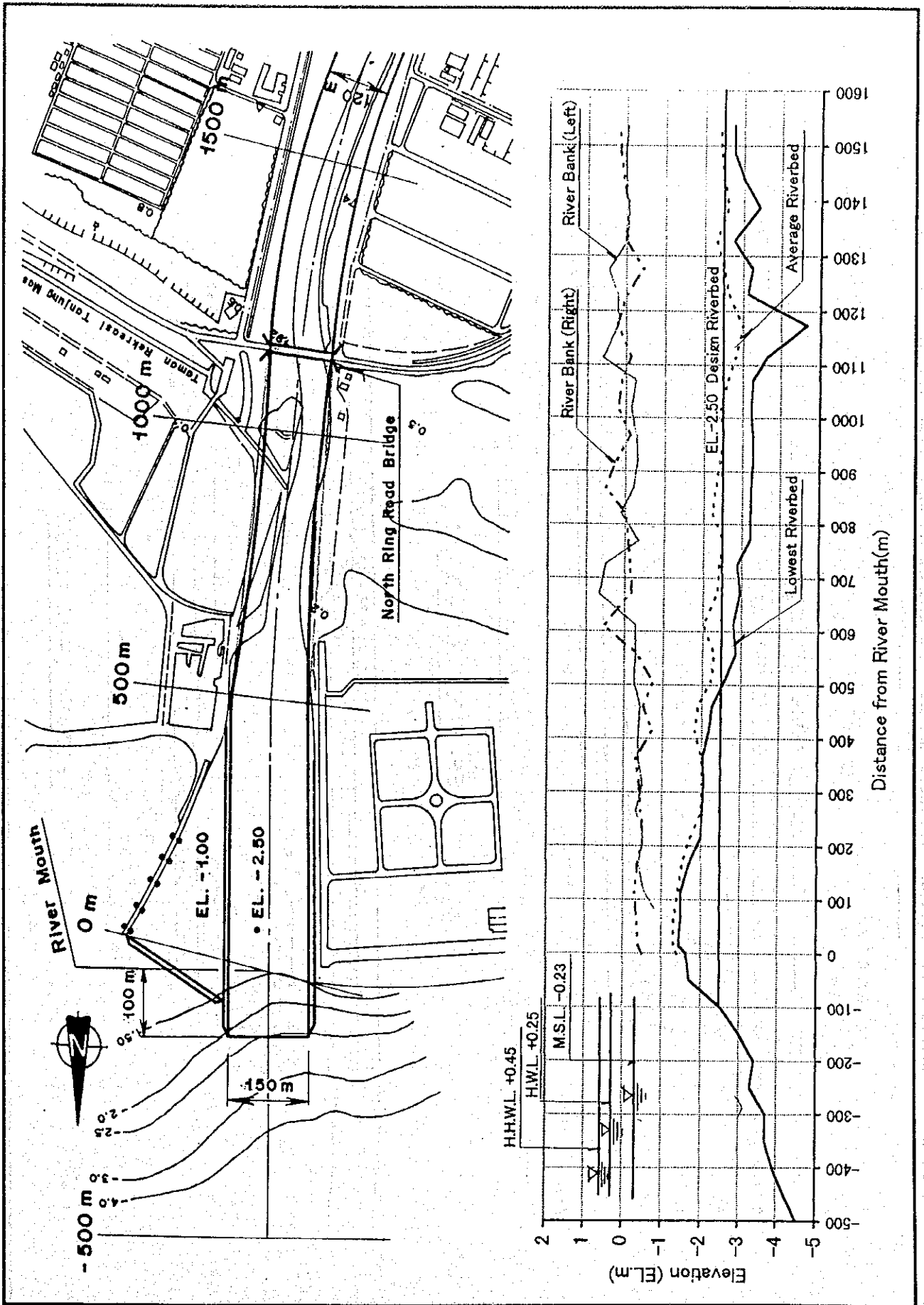
GARAN RIVER (SIMONGAN WEIR TO CONFLUENCE WITH KREO RIVER)



THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

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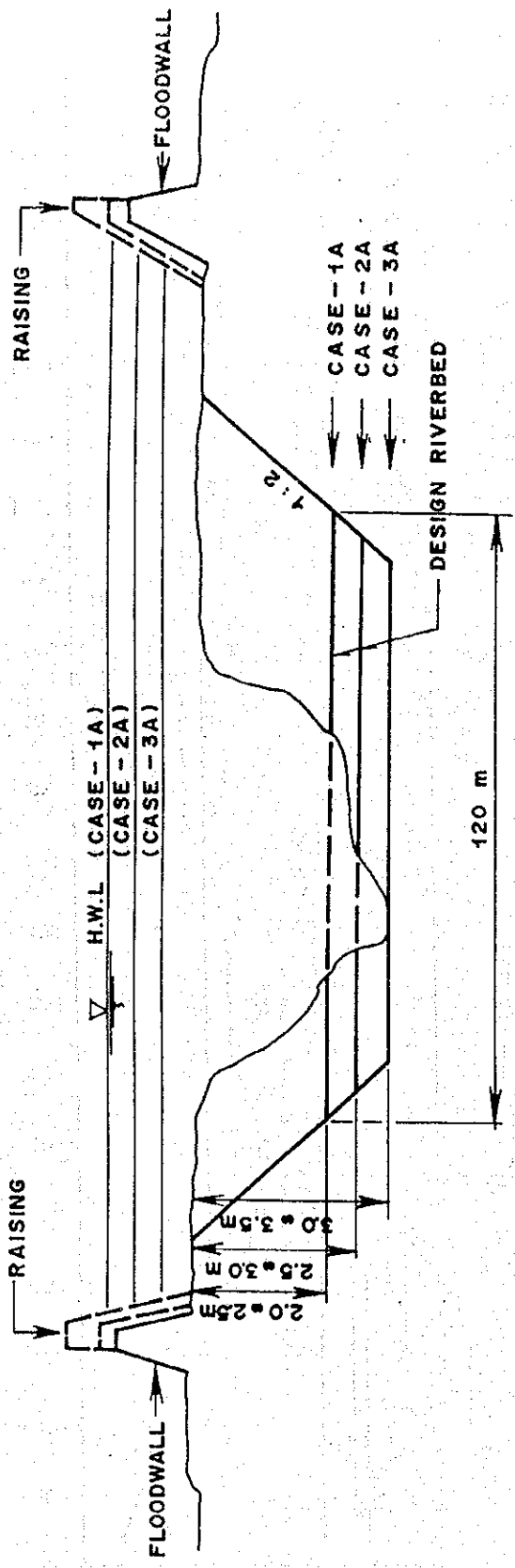
Fig. 2. 2. 1



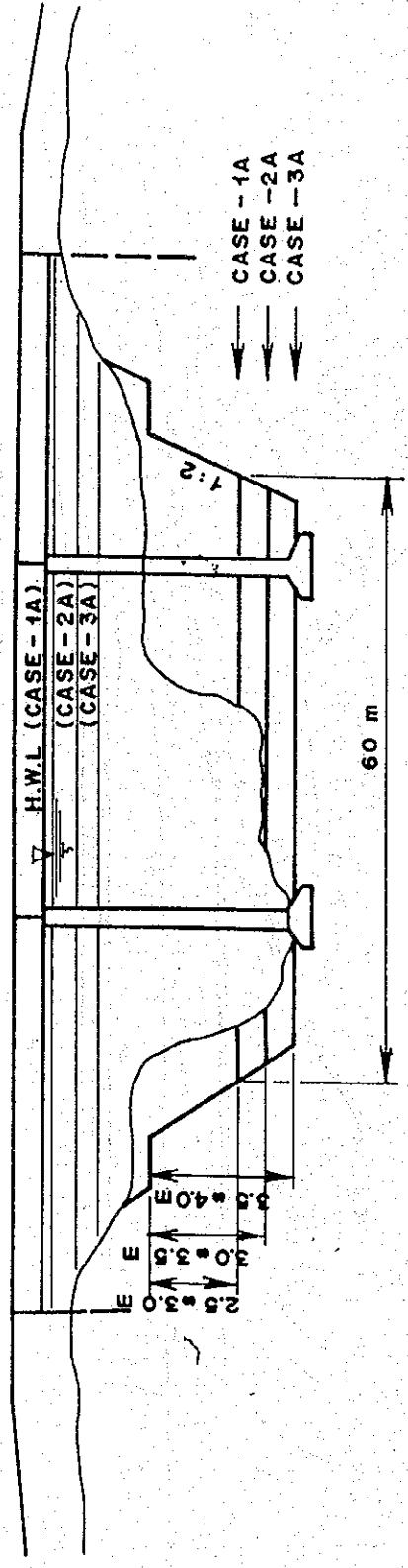
THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

Fig. 2. 2. 2

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SECTION 500 to 3400



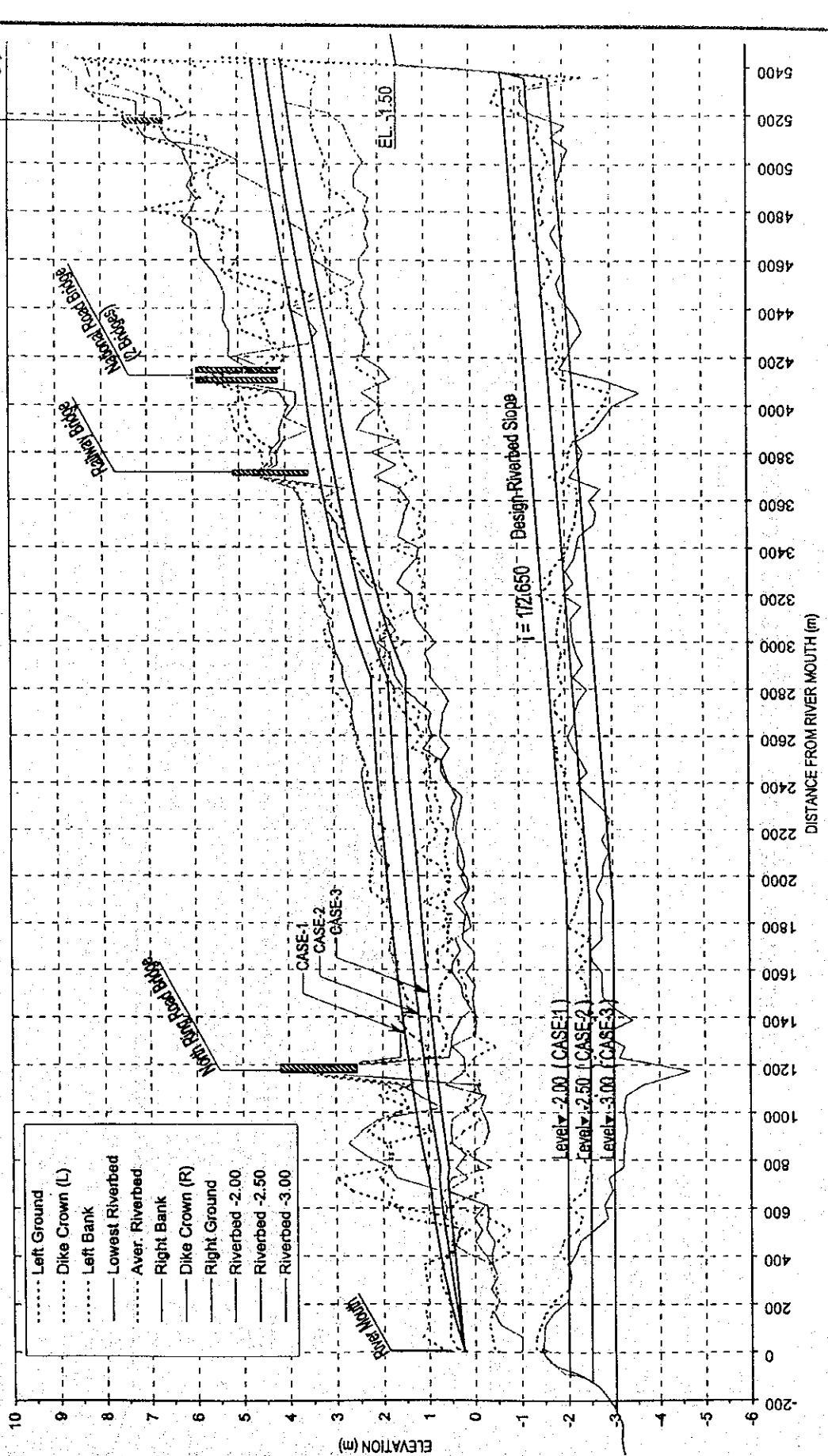
SECTION 3400 to 5200

THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

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Fig. 2.2.3

LONGITUDINAL PROFILE OF WEST FLOODWAY CHANNEL



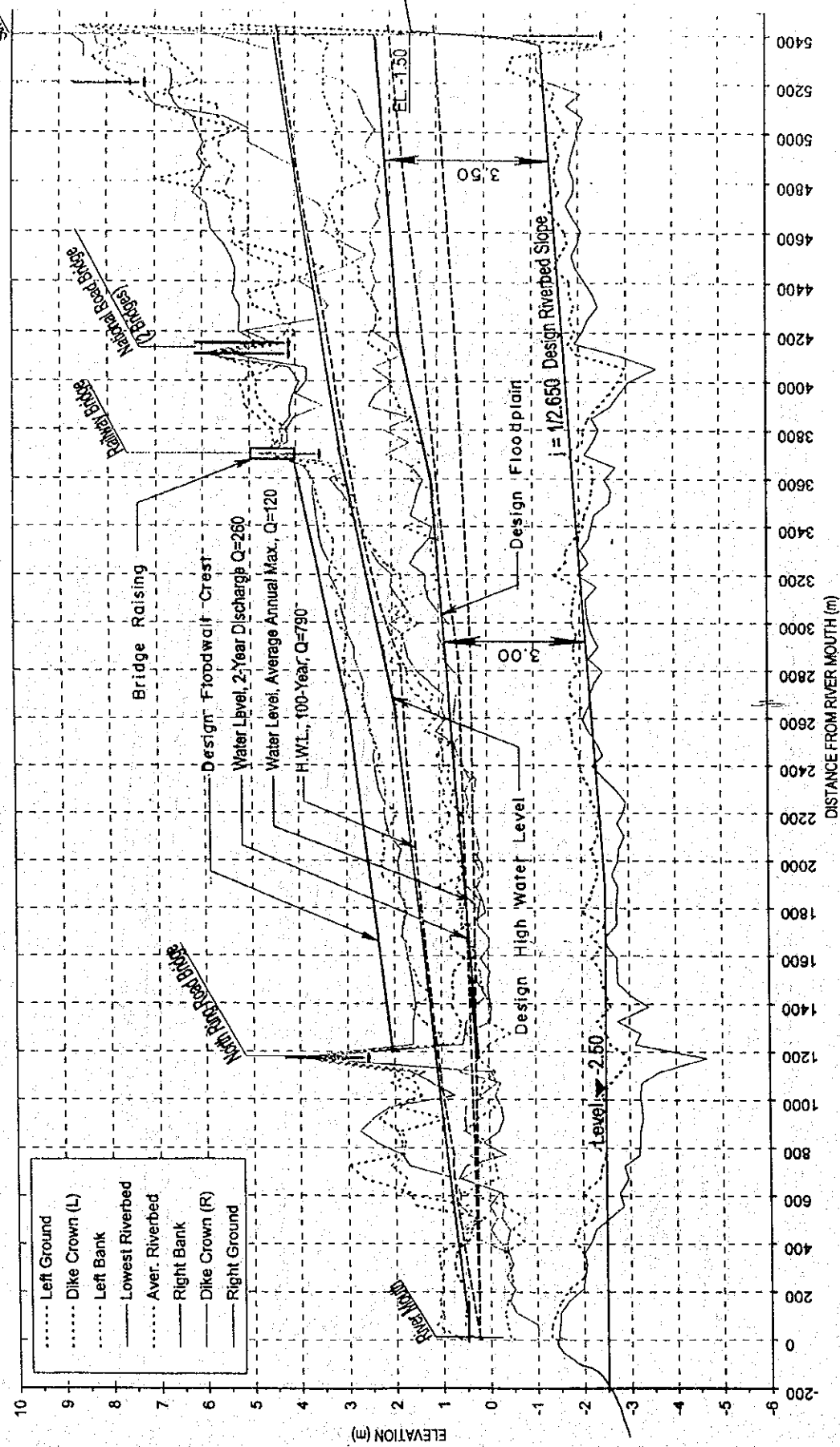
.....	Left Ground
.....	Dike Crown (L)
.....	Left Bank
.....	Lowest Riverbed
.....	Aver. Riverbed
.....	Right Bank
.....	Dike Crown (R)
.....	Right Ground
.....	Riverbed -2.00
.....	Riverbed -2.50
.....	Riverbed -3.00

THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

Fig. 2. 2. 4

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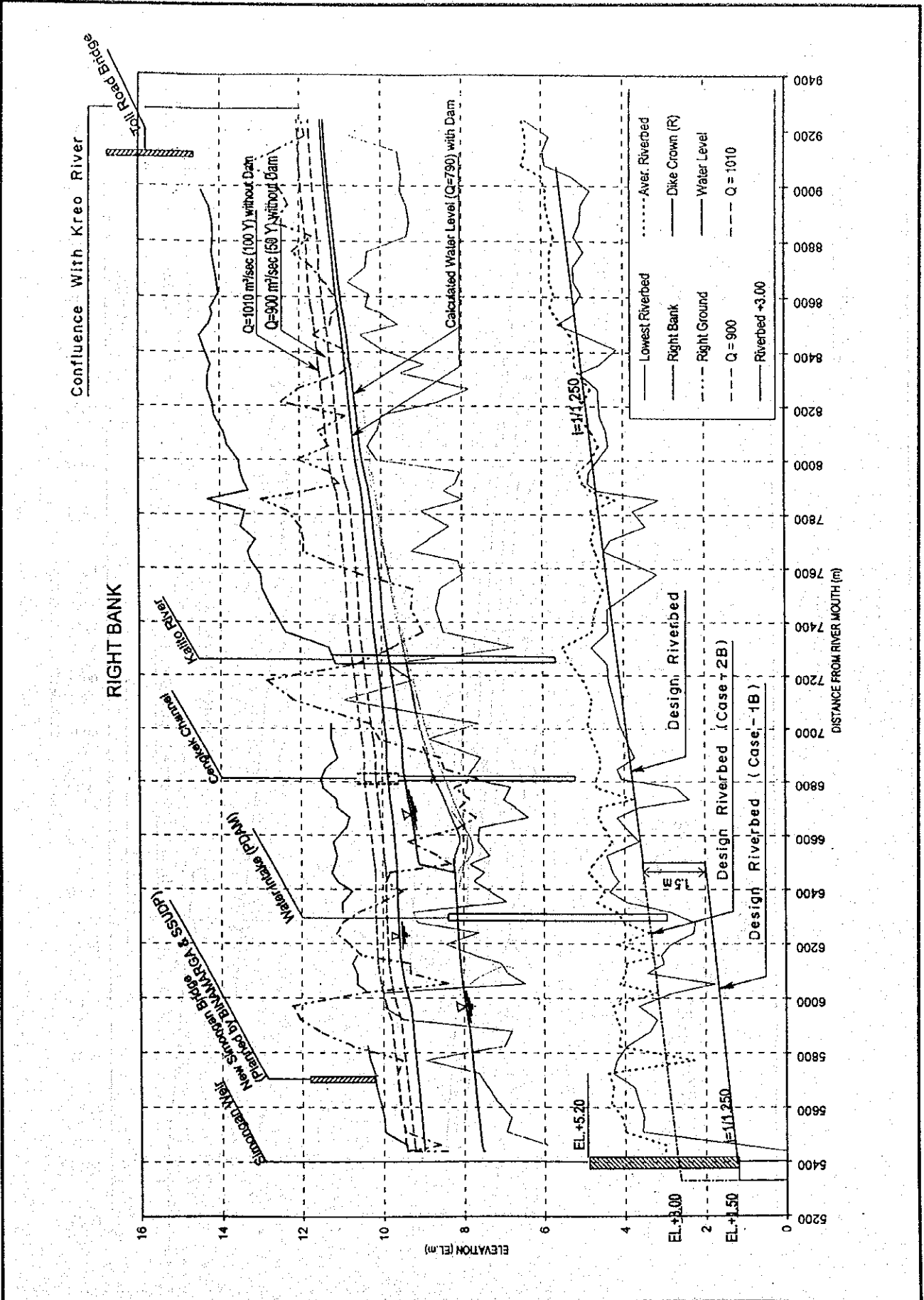
LONGITUDINAL PROFILE OF WEST FLOODWAY CHANNEL



THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

Fig. 2. 2. 5

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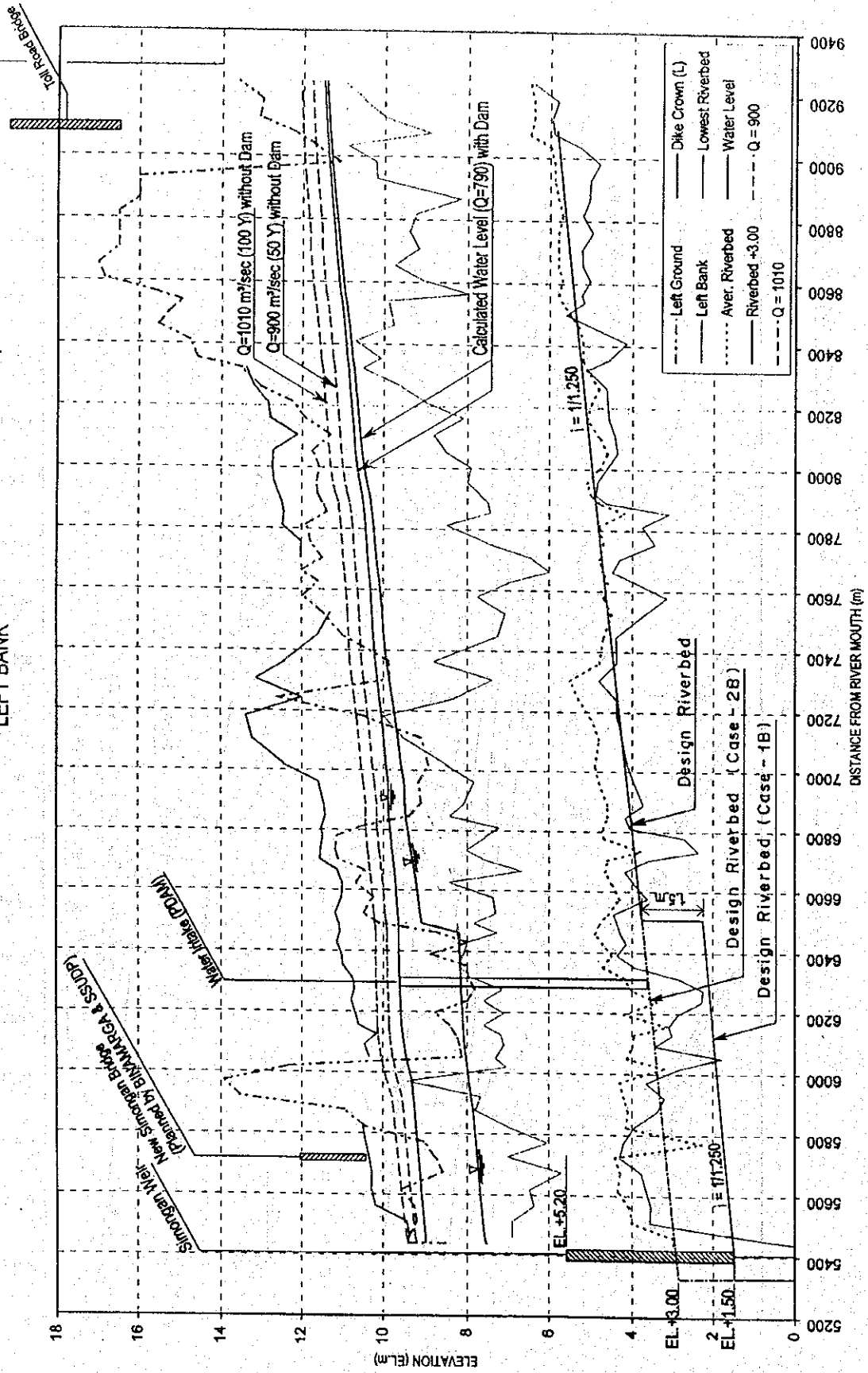
THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

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Fig. 2. 2. 6 (1/2)

LEFT BANK

Confluence With Kreo River

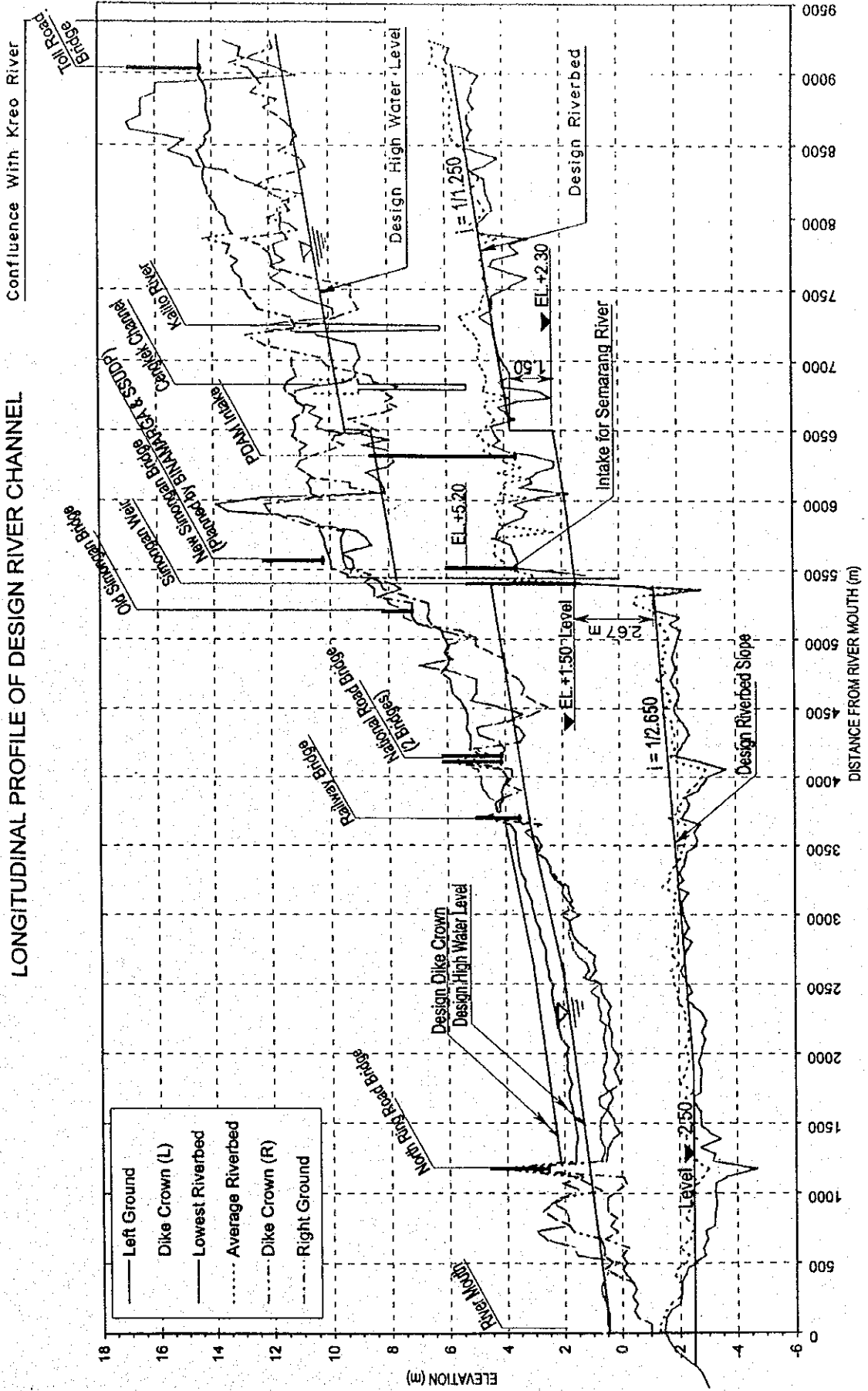


THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

Fig. 2. 2. 6 (2/2)

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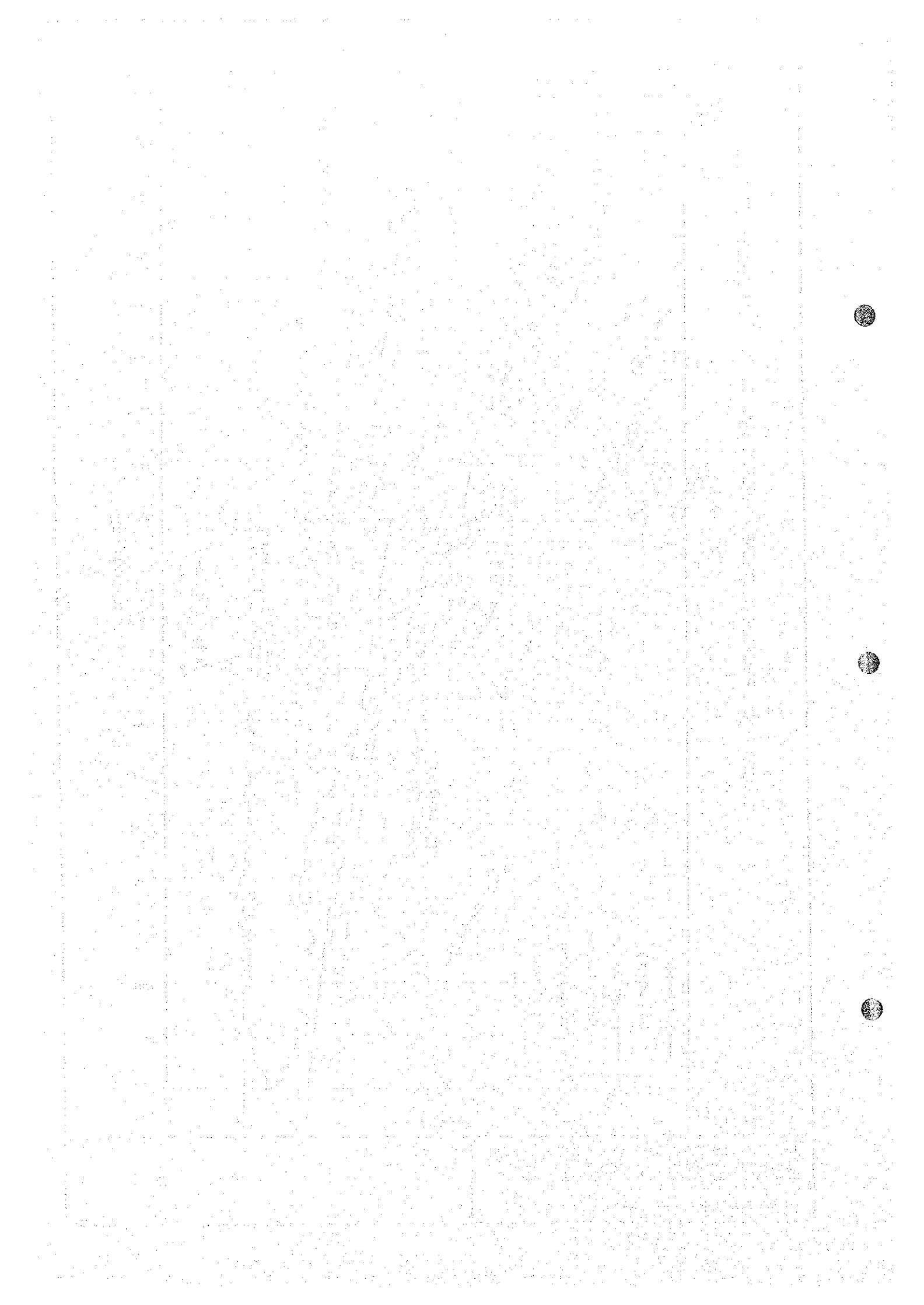
LONGITUDINAL PROFILE OF DESIGN RIVER CHANNEL



THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

JAPAN INTERNATIONAL COOPERATION AGENCY

Fig. 2. 2. 7



2.3 River Hydraulics on Design Channel

Water level profile was calculated for the design river channel as mentioned below.

2.3.1 Conditions on Calculation

(1) Uniform Flow Calculation

In principle, the design high water level profile is set based on the uniform flow calculation. This method is commonly applied for the river stretch of which water level is not affected by tide. As a uniform flow calculation method, the following Manning's Formula is used.

$$Q = \frac{1}{n} \times I^{1/2} \times R^{2/3} \times A$$

where;

- Q : design discharge (m³/s)
- n : Manning's roughness coefficient
- I : gradient of river bed
- R : hydraulic radius (m)
- A : flow area (m²)

(2) Non Uniform Flow Calculation

For the river channel where water level is influenced by the downstream water level, non-uniform flow method is employed to compute the water surface profile. The calculation equation is presented as follows:

$$\left\{ H_2 + \frac{D_2 \left(\frac{Q_2}{A_2} \right)^2}{2g} \right\} - \left\{ H_1 + \frac{D_1 \left(\frac{Q_1}{A_1} \right)^2}{2g} \right\} = h_e$$

$$h_e = \frac{1}{2} \left\{ \frac{N_1^2 \cdot Q_1^2}{A_1^2 \cdot R_1^{4/3}} + \frac{N_2^2 \cdot Q_2^2}{A_2^2 \cdot R_2^{4/3}} \right\} \times \Delta X$$

Using Iida's Formula, coefficients; D, N and R are expressed below.

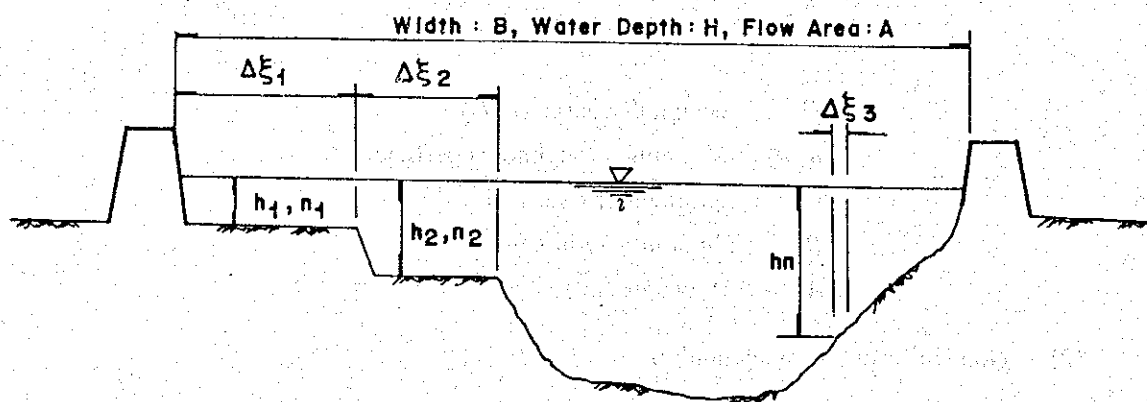
$$D = \alpha \cdot \frac{A^2 \int_0^B \frac{h^3}{n^3} d\xi}{\left(\int_0^B \frac{h^{5/3}}{n} d\xi \right)^3}, \quad N = \frac{\int_0^B h^{5/3} d\xi}{\int_0^B \frac{h^{5/3}}{n} d\xi}, \quad R = \left(\frac{1}{A} \int_0^B h^{5/3} \right)^{3/2}$$

where,

- H : elevation of water level (m)

- h_e : difference in water level between two sections
- g : acceleration of gravity (9.8 m/s^2)
- Q : discharge (m^3/s)
- A : flow area (m^2)
- ΔX : distance between two cross sections (m)
- D : coefficient for correction
- N : equivalent roughness coefficient for the whole cross sections
- R : equivalent hydraulic depth for the whole cross sections
- n : Manning's roughness coefficient for each cross section
- α : energy coefficient (1.0)
- B : river width subject to computation.

Suffix denotes the number of cross sections from downstream to upstream.



CHANNEL CROSS SECTION

(3) Roughness Coefficient

For the uniform and non-uniform flow calculation, the following Manning's roughness coefficient are used based on the recommended figures in "Flood Control Manual".

Low Water Channel (excavated)	0.030
Low Water Channel (existing)	0.033
Flood Plain (excavated) *1	0.035
Flood Plain (existing)	0.040
Channel with Lining (narrow channel)	0.025

*1 The flood plain here is referred to the bottom portion of high water channel.

(4) Design Tidal Level at River Mouth

The design tidal levels at the river mouth are determined based on the tidal data observed at Semarang Harbor. Since the tidal data observed in the past have been affected by land subsidence in the low lying area, the most recent data of April 1997 to August 1997, which are considered less affected, are used for the tidal analysis.

Kind of Water Level	Elevation (TTG)
Highest High Water Level (HHWL)	EL. +0.45 m
Mean High Water Level (MHWL)	EL. +0.25 m
Mean Sea Level (MSL)	EL. -0.23 m
Mean Low Water Level (MLWL)	EL. -0.70 m
Lowest Low Water Level (LLWL)	EL. -0.90 m

For the non-uniform flow calculation in the event of flooding, the mean high water level of EL. +0.250 m is used as the starting water level at the river mouth.

Table MAXIMUM AND MINIMUM VALUE OF TIDAL LEVEL IN THE LAST FIVE MONTHS

Months Date	April, 1997		May, 1997		Jun. 1997		July, 1997		August, 1997	
	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
1	176	118	184	100	189	106	162	114	174	118
2	174	105	182	94	184	109	162	106	178	124
3	170	99	188	96	174	112	164	112	182	122
4	176	95	176	100	168	110	156	105	180	120
5	170	105	166	107	172	116	162	110	176	123
6	174	96	160	110	177	126	169	117	166	121
7	164	109	162	121	180	129	178	116	162	-
8	160	114	152	117	180	121	182	124	158	120
9	135	115	160	123	181	120	174	113	170	114
10	143	116	166	128	184	116	176	115	166	117
11	141	112	171	120	183	118	169	108	178	105
12	154	110	168	116	177	112	176	123	174	107
13	166	107	178	103	184	111	167	108	180	99
14	164	82	179	100	182	113	172	122	170	91
15	168	77	180	100	182	112	168	118	173	104
16	167	102	175	100	177	124	164	115	102	102
17	160	94	169	100	174	120	158	112	164	108
18	156	91	165	96	178	120	158	108	160	116
19	160	94	164	105	173	119	155	108	153	112
20	161	111	153	104	172	117	170	109	149	116
21	159	122	157	110	174	116	165	102	142	115
22	159	122	153	111	175	118	168	111	152	114
23	154	132	160	115	188	117	169	112	159	119
24	154	125	167	110	187	124	170	112	165	111
25	152	126	173	120	190	120	170	115	166	122
26	164	126	174	116	188	119	177	112	164	116
27	169	129	178	122	192	113	170	120	171	117
28	179	123	182	108	179	112	185	116	167	112
29	188	118	187	108	176	119	-	-	169	116
30	179	102	186	104	-	-	-	-	172	113
31	-	-	194	104	-	-	-	-	170	119
Average	163	109	171	109	180	117	168	113	165	114
Max. Value	188	-	194	-	192	-	185	-	182	-
Min. Value	-	77	-	94	-	106	-	102	-	91
Average										
-										
188.2										
94.0										

Note :

TIDAL DATA ** APRIL 1997 **

Unit : cm

TIME DATE	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	Aver.	Max.	Nin.	Difference	
1	121	123	132	141	146	146	146	146	144	139	138	138	140	150	162	171	176	176	172	168	154	140	127	118	146	176	118	58	
2	117	121	127	139	145	146	146	144	140	134	130	130	130	139	150	163	172	174	169	162	150	134	119	105	141	174	105	69	
3	99	98	105	116	124	133	136	135	130	124	118	116	118	126	136	148	161	169	170	167	157	143	127	111	132	170	98	72	
4	98	95	98	110	114	124	134	138	135	132	127	121	121	127	137	150	164	172	176	176	172	161	146	130	136	176	95	81	
5	116	106	105	97	117	126	133	139	140	140	134	123	120	124	132	142	154	163	169	170	169	161	147	132	136	170	97	73	
6	116	104	96	109	104	112	120	129	134	138	137	132	126	123	130	139	148	160	166	171	174	172	164	150	136	174	96	78	
7	137	123	114	116	109	114	123	128	130	131	133	130	125	124	126	131	140	150	157	162	164	164	159	152	135	164	109	55	
8	142	131	122	122	114	118	126	131	136	139	138	138	138	136	136	136	141	147	153	158	160	160	157	154	139	160	114	46	
9	148	139	129	118	116	115	118	123	127	128	131	131	130	128	126	127	128	130	130	134	135	133	130	130	129	148	115	33	
10	125	122	120	126	118	116	118	120	124	130	131	136	140	140	143	143	144	143	139	138	140	140	133	128	132	144	116	28	
11	128	130	129	118	126	126	124	124	127	124	126	130	136	138	141	141	141	139	133	126	121	114	114	112	128	141	112	29	
12	110	114	115	124	121	123	126	128	127	125	130	132	138	144	148	152	154	152	145	136	126	118	112	110	130	154	110	44	
13	109	111	116	122	127	129	132	133	122	130	130	133	140	148	158	164	166	162	154	144	132	120	110	107	133	166	107	59	
14	105	106	112	94	128	133	138	140	140	138	138	140	140	141	148	157	164	160	148	132	118	104	93	82	129	164	82	82	
15	77	79	86	112	104	109	112	114	116	116	112	115	122	132	144	155	165	168	168	160	148	134	120	106	124	168	77	91	
16	102	102	104	102	122	133	138	140	141	137	134	132	132	138	147	157	164	167	166	162	152	138	124	110	135	167	102	65	
17	98	94	96	97	110	120	128	134	134	130	126	126	128	132	142	149	156	160	160	155	148	136	124	110	129	160	94	66	
18	100	93	91	97	104	111	120	127	132	132	128	125	124	128	135	144	152	156	156	154	146	137	135	122	127	156	91	65	
19	101	95	94	112	104	110	116	124	127	128	125	123	123	127	135	144	152	158	160	159	154	147	137	126	128	160	94	66	
20	118	111	111	124	116	122	128	133	135	136	135	130	130	134	141	146	152	157	160	161	160	155	148	139	137	161	111	50	
21	132	126	122	126	127	130	132	136	142	144	143	138	138	136	140	147	153	158	159	156	152	147	140	134	140	159	122	37	
22	127	122	122	154	130	133	138	143	147	147	146	144	142	146	153	157	159	159	159	156	150	146	144	142	144	159	122	37	
23	143	149	153	126	152	150	148	145	145	147	147	144	142	144	146	148	149	152	153	152	151	144	138	132	146	153	126	27	
24	127	126	125	130	130	136	142	146	150	150	152	150	151	152	152	154	154	154	154	154	150	144	138	135	144	154	125	29	
25	132	128	128	134	134	138	141	144	146	149	150	150	151	151	152	151	149	146	142	140	138	133	128	126	141	152	126	26	
26	126	126	126	128	128	134	138	142	144	148	152	154	158	160	162	164	163	160	156	152	147	142	136	132	145	164	126	38	
27	129	129	129	132	132	134	136	138	140	144	146	150	154	159	164	168	169	168	163	156	150	144	138	132	146	169	129	40	
28	130	130	131	133	133	135	136	138	141	142	144	144	144	144	144	144	144	144	144	144	146	146	146	147	147	179	123	56	
29	123	129	134	146	146	146	146	149	150	151	148	152	158	167	176	183	186	184	174	163	148	134	126	118	153	188	118	70	
30	114	110	121	133	133	137	137	136	134	131	131	134	142	151	162	171	177	179	173	164	144	124	110	102	140	179	102	77	
Average																									137	164	109	55	
Max.																										188			
Nin.																												77	

TIDAL DATA ** MAY 1997 **

Unit: cm

TIME DATE	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	Aver.	Max.	Min.	Difference	
1	100	102	109	120	132	141	142	142	139	134	133	133	138	150	165	175	184	184	178	168	154	134	114	100	140	184	100	84	
2	94	96	103	112	123	134	143	144	142	138	135	133	135	142	153	164	175	182	182	176	165	149	130	113	140	182	94	88	
3	100	96	102	110	120	132	143	149	150	146	142	140	143	146	155	166	175	184	188	184	176	163	147	129	145	188	96	92	
4	112	102	100	103	116	126	135	143	142	140	138	136	138	142	149	157	165	172	176	176	172	163	152	139	141	176	100	76	
5	126	113	107	108	114	122	131	140	146	148	146	143	140	141	144	142	154	160	164	166	164	158	150	141	140	166	107	59	
6	130	120	112	110	113	118	126	133	140	145	148	146	144	142	145	148	151	154	157	160	159	156	152	146	140	160	110	50	
7	139	131	125	122	121	125	131	138	146	152	148	160	162	162	159	159	154	152	150	150	150	148	141	138	144	162	121	41	
8	132	125	120	117	117	120	124	128	134	139	143	146	149	151	152	152	150	148	145	142	140	136	133	130	136	152	117	35	
9	128	126	124	123	124	126	129	132	135	140	144	148	152	156	158	160	159	156	154	150	146	142	136	132	141	160	123	37	
10	130	128	128	128	130	132	134	136	139	142	145	149	153	158	162	165	166	164	162	157	152	145	137	132	145	166	128	38	
11	130	130	130	131	133	136	140	142	145	148	150	154	158	163	167	170	171	170	166	158	148	136	127	120	147	171	120	51	
12	116	116	120	123	126	131	138	140	140	141	143	146	149	154	161	165	168	168	163	154	143	133	123	116	141	168	116	52	
13	112	112	114	122	128	135	142	147	150	152	154	155	159	163	168	173	176	178	175	170	158	118	106	103	145	178	103	75	
14	105	111	123	133	139	145	150	152	152	149	150	152	157	166	171	174	179	172	162	149	132	114	104	100	143	179	100	79	
15	100	105	117	128	142	150	150	152	152	152	154	152	156	166	176	180	179	176	169	158	144	125	112	105	146	180	100	80	
16	100	107	112	126	139	150	156	154	154	152	150	150	154	160	166	173	175	175	170	159	143	127	113	102	144	175	100	75	
17	100	100	106	118	132	144	150	150	149	146	144	144	146	151	159	164	169	165	161	154	146	128	113	104	139	169	100	69	
18	96	98	103	112	123	133	143	147	147	144	139	142	142	146	152	156	164	165	162	156	146	136	122	110	137	165	96	69	
19	105	107	114	112	134	147	154	159	156	152	145	142	145	151	155	161	164	163	162	153	140	127	116	106	140	164	105	59	
20	104	101	110	117	128	140	145	150	153	150	149	145	147	150	151	151	152	152	151	146	140	133	123	116	138	153	101	52	
21	110	108	114	123	131	140	148	157	156	156	152	149	150	150	155	155	152	151	149	144	138	131	123	116	140	157	108	49	
22	111	112	115	120	128	134	143	149	152	153	159	152	151	150	150	151	150	147	144	143	138	130	126	122	139	159	111	48	
23	117	115	116	122	128	137	146	154	158	160	160	156	153	152	152	149	146	144	141	137	134	127	118	115	139	160	115	45	
24	112	110	112	118	125	132	140	151	158	164	167	167	167	164	164	164	160	156	152	148	143	137	130	127	145	167	110	57	
25	126	122	121	122	128	136	147	156	164	169	173	176	174	171	170	168	165	159	152	144	137	130	124	120	148	176	120	56	
26	119	119	116	116	119	126	135	144	152	157	163	169	171	173	174	174	172	167	160	152	145	140	133	130	147	174	116	58	
27	130	131	132	130	130	134	140	147	154	159	164	168	173	177	178	178	178	174	166	151	138	129	124	122	150	178	122	56	
28	122	126	132	133	133	135	140	147	152	157	162	166	171	177	180	182	182	180	170	150	132	119	111	108	149	182	108	74	
29	112	117	123	129	134	136	140	144	146	148	150	156	165	176	184	187	186	183	174	161	146	130	117	108	148	187	108	79	
30	106	112	118	127	138	142	144	144	148	150	153	156	162	169	178	184	186	186	180	170	156	132	114	104	148	186	104	82	
31	104	110	120	136	141	150	154	154	156	158	160	161	167	173	182	190	194	192	186	178	163	145	128	113	155	194	104	90	
Aver.																									143	172	108	63	
Max.																										194			
Min.																											94		

TIDAL DATA ** JUN 1997 **

Unit : cm

TIME DATE	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	Aver.	Max.	Min.	Difference		
1	106	112	119	129	141	154	163	165	163	160	160	161	164	168	174	181	186	189	187	179	167	150	133	119	155	189	106	83		
2	109	108	115	125	138	150	161	170	170	166	161	158	159	162	165	170	177	184	184	180	171	158	142	126	155	184	108	76		
3	116	112	117	122	134	149	162	170	174	174	170	165	163	164	165	165	167	171	173	173	169	161	146	130	155	174	112	62		
4	118	110	112	117	125	137	150	161	168	169	169	165	162	160	158	158	158	159	160	160	156	150	143	134	148	169	110	59		
5	125	117	116	119	126	136	145	154	164	170	172	171	169	166	164	162	160	158	157	155	152	148	144	139	150	172	116	56		
6	134	128	126	128	132	140	148	155	164	170	175	177	176	175	173	170	166	162	158	154	150	146	142	138	154	177	126	51		
7	134	130	129	129	134	141	147	154	162	167	173	178	180	180	179	176	172	166	158	151	145	138	133	130	154	180	129	51		
8	128	126	124	125	130	138	147	154	160	166	170	175	177	180	180	180	178	174	164	152	141	132	125	121	152	180	121	59		
9	121	123	124	126	130	138	145	154	156	162	168	174	179	181	182	182	180	175	165	153	143	134	126	120	152	182	120	62		
10	116	118	121	124	130	137	147	156	162	167	170	174	179	182	184	184	182	179	170	158	146	135	125	120	153	184	116	68		
11	118	120	124	128	137	144	152	158	162	165	165	165	164	168	172	176	177	176	176	176	163	148	123	114	147	183	118	65		
12	112	112	118	124	130	135	141	147	152	156	158	160	164	168	172	176	177	176	172	163	148	134	123	114	147	177	112	65		
13	111	114	120	128	136	144	152	157	162	164	165	168	170	175	178	182	184	183	179	171	157	140	126	116	153	184	111	73		
14	113	115	121	128	137	147	154	159	162	165	166	168	172	175	177	180	182	180	176	168	157	142	127	117	153	182	113	69		
15	112	114	118	124	132	143	152	159	163	164	166	167	168	173	177	180	182	181	182	179	174	165	141	130	155	182	112	70		
16	124	124	124	130	141	151	161	168	170	168	168	168	169	171	174	176	177	177	174	168	159	148	137	128	156	177	124	53		
17	121	120	124	130	141	153	164	172	174	170	165	160	159	159	162	165	168	168	166	162	154	146	135	126	153	174	120	54		
18	120	121	126	134	144	157	168	176	178	175	170	167	164	164	165	168	168	168	166	160	154	145	136	126	155	178	120	58		
19	119	120	125	132	143	152	162	168	173	172	168	165	161	159	158	157	157	156	154	151	145	138	130	123	150	173	119	54		
20	117	116	120	128	136	146	156	164	170	172	172	170	168	165	164	160	158	155	152	148	144	138	131	125	149	172	116	56		
21	119	116	116	121	128	136	147	157	164	172	174	174	171	168	166	164	161	157	154	150	146	140	134	130	149	174	116	58		
22	124	120	118	123	131	140	149	157	164	171	175	176	175	172	170	167	162	156	150	146	140	134	128	124	149	176	118	58		
23	121	118	117	120	128	140	150	158	165	173	180	185	188	188	186	182	176	169	161	155	149	142	136	131	155	188	117	71		
24	130	128	126	124	126	132	142	151	158	164	172	180	184	187	185	180	174	168	158	149	145	140	134	130	153	187	124	63		
25	130	130	130	130	132	136	144	150	157	164	170	176	184	188	190	190	186	178	168	156	142	133	125	120	155	190	120	70		
26	119	120	122	125	126	128	137	145	151	155	162	169	176	184	187	188	185	180	172	160	147	135	128	127	151	188	119	69		
27	126	128	134	139	143	147	165	162	168	172	174	176	179	185	190	192	190	186	178	163	147	130	118	113	159	192	113	79		
28	112	115	119	126	133	138	141	143	149	152	152	156	162	167	171	174	179	178	173	165	152	136	124	118	147	179	112	67		
29	119	120	128	140	150	157	162	164	161	162	156	154	153	160	166	172	174	176	173	165	152	136	124	118	154	176	119	57		
30																														
Average																									152	180	117	63		
Max.																										192				
Min.																												106		

TIDAL DATA ** JULY,AUGUST 1997 **

	September			August			July		
	Max	Min	Differ.	Max	Min	Differ.	Max	Min	Differ.
1	163	128		174	118	56	162	114	48
2	172	122		178	124	54	162	106	56
3	163	116		182	122	60	164	112	52
4	174	122		180	120	60	156	105	51
5				176	123	53	162	110	52
6				166	121	45	169	117	52
7				162	-	-	178	116	62
8				158	120	38	182	124	58
9				170	114	56	174	113	61
10				166	117	49	176	115	61
11				178	105	73	169	108	61
12				174	107	67	176	123	53
13				180	99	81	167	108	59
14				170	91	79	172	122	50
15				173	104	69	168	118	50
16				102	102	0	164	115	49
17				164	108	56	158	112	46
18				160	116	44	158	108	50
19				153	112	41	155	108	47
20				149	116	33	170	109	61
21				142	115	27	165	102	63
22				152	114	38	168	111	57
23				159	119	40	169	112	57
24				165	111	54	170	112	58
25				166	122	44	170	115	55
26				164	116	48	177	112	65
27				171	117	54	170	120	50
28				167	112	55	185	116	69
29				169	116	53	-	-	-
30				172	113	59	-	-	-
31				170	119	51	-	-	-
32				162	114	48	-	-	-
Aver.				165	114	51	168	113	55
Max.				182			185		
Min.					91			102	

2.3.2 West Floodway

(1) Water Level Profile

Since West Floodway is a tidal river of which riverbed slope is almost flat in the lower reaches, the steady uniform flow calculation is not applicable. Then, the non-uniform flow calculation presented in "Hydraulic Criteria" is applied to estimate the water level and the flow velocity of river channel.

Using the river cross-sections and longitudinal profile of the channel determined in the basic design, non-uniform flow calculation was conducted. When the design flood discharge of 790 m³/s flows in the river channel, the water level and the flow velocity are calculated as shown in the following calculation sheets. The water level profile calculated and flow velocity are illustrated as well.

WEST FLOODWAY, STEADY NON-UNIFORM FLOW (LEVEL-.2.5,1/2650) b = 50 WF.75-UP
BASIC DATA

KUKAN-SU =13 ALPHA = 10 QO = 790.00 M3/S HO = .250 M ZO = .2500 M

JCO = 0 KEY = 0 IPT = 0

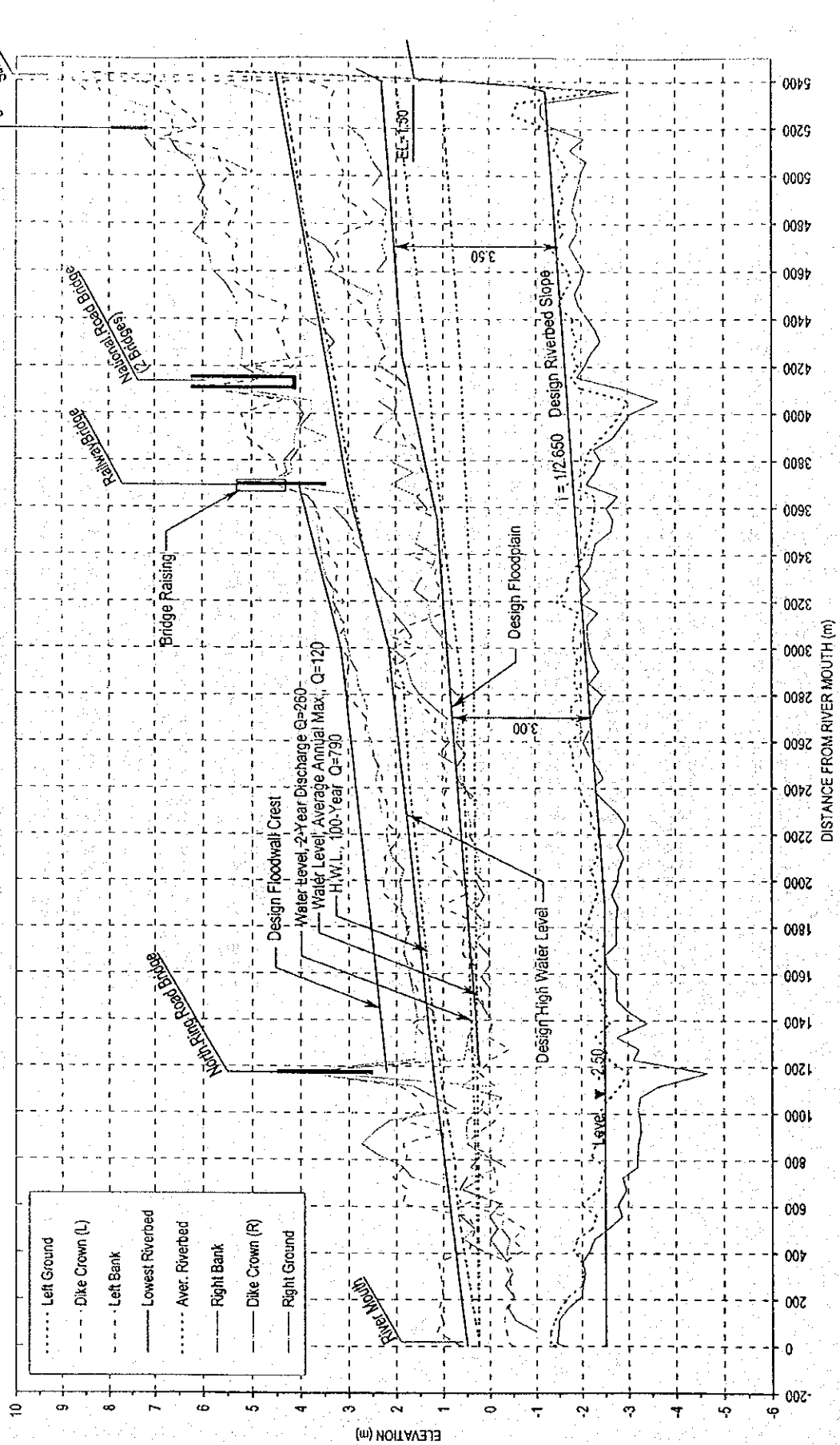
KUKAN DATA

DANMEN NO.	BUNKATSU SUU	DANMEN KEIJO	LOSS TYPE	SODO KEISU	KUKAN KYOR(M)	KASYO KOOBA(1/I)	RAKUSA (M)	RYUNYU RYO(M3/S)
1 WF-9 -WFO	9	2 1	0	0.0324	413.7	999999	0	0
2 WFO - WF5	5	2 1	0	0.031	258.96	999999	0	0
3 WF5 - WF14	9	2 1	0	0.0307	442.71	999999	0	0
4 WF14 -WF21	7	2 1	0	0.0306	371.14	999999	0	0
5 WF21 -WF29	8	2 1	0	0.0306	401.9	999999	0	0
6 WF29 -WF39	10	2 1	0	0.0308	509.15	2650	0	0
7 WF39 -WF47	8	2 1	0	0.0317	399.23	2650	0	0
8 WF47 -WF59	12	2 1	0	0.0317	600.23	2650	0	0
9 WF59 -WF63	4	2 1	0	0.031	200.01	2650	0	0
10 WF63 -WF69	6	2 1	0	0.0308	300.9	2650	0	0
11 WF69 -WF75	6	2 1	0	0.0305	305.77	2650	0	0
12 WF75 -WF95	20	2 1	0	0.0309	1006.84	2650	0	0
13 WF95 -WF99	4	2 1	0	0.0309	199.6	2650	0	0

NO.	H	A	R	V	N	Q	DX	FROUD	IE	Z	H-Z
WF-9 -WFO	.250'	427.63	2.635	1.847	0.0324	790	0	0.3621	9.85E-04	-2.5	2.75
+ 45.97	.300'	435.73	2.681	1.813	0.0324	790	45.97	0.3523	9.27E-04	-2.5	2.8
+ 91.93	.347'	443.26	2.724	1.782	0.0324	790	45.97	0.3435	8.77E-04	-2.5	2.847
+ 137.90	.392'	450.48	2.765	1.754	0.0324	790	45.97	0.3355	8.32E-04	-2.5	2.892
+ 183.87	.434'	457.26	2.803	1.728	0.0324	790	45.97	0.3282	7.93E-04	-2.5	2.934
+ 229.83	.474'	463.69	2.84	1.704	0.0324	790	45.97	0.3216	7.58E-04	-2.5	2.973
+ 275.80	.512'	470.74	2.864	1.678	0.0324	790	45.97	0.375	7.27E-04	-2.5	3.012
+ 321.77	.550'	478.97	2.854	1.649	0.0324	790	45.97	0.3566	7.02E-04	-2.5	3.05
+ 367.73	.586'	485.83	2.864	1.626	0.0324	790	45.97	0.3402	6.83E-04	-2.5	3.085
+ 413.70	.620'	491.6	2.864	1.607	0.0324	790	45.97	0.3254	6.67E-04	-2.5	3.119
WFO - WF5	.620'	491.64	2.864	1.607	0.031	790	0	0.3253	6.10E-04	-2.5	3.119
+ 51.79	.654'	497.78	2.864	1.587	0.031	790	51.79	0.3162	5.95E-04	-2.5	3.154
+ 103.58	.688'	503.48	2.864	1.569	0.031	790	51.79	0.3077	5.82E-04	-2.499	3.187
+ 155.38	.720'	508.74	2.864	1.553	0.031	790	51.79	0.2998	5.70E-04	-2.499	3.219
+ 207.17	.752'	513.59	2.864	1.538	0.031	790	51.79	0.2925	5.59E-04	-2.499	3.251
+ 258.96	.782'	518.01	2.883	1.525	0.031	790	51.79	0.2857	5.45E-04	-2.499	3.282
WF5 - WF14	.692'	390.21	2.827	2.025	0.0307	790	0	0.3912	9.67E-04	-2.499	3.191
+ 49.19	.746'	397.86	2.827	1.986	0.0307	790	49.19	0.3795	9.30E-04	-2.499	3.246
+ 98.38	.798'	405.17	2.827	1.95	0.0307	790	49.19	0.3688	8.97E-04	-2.499	3.298
+ 147.57	.848'	411.96	2.875	1.918	0.0307	790	49.19	0.3593	8.48E-04	-2.499	3.347
+ 196.76	.894'	418.3	2.926	1.889	0.0307	790	49.19	0.3507	8.03E-04	-2.499	3.393
+ 245.95	.938'	424.21	2.975	1.862	0.0307	790	49.19	0.3429	7.64E-04	-2.499	3.437
+ 295.14	.979'	429.75	3.022	1.838	0.0307	790	49.19	0.3359	7.29E-04	-2.499	3.478
+ 344.33	1.018'	434.97	3.067	1.816	0.0307	790	49.19	0.3294	6.98E-04	-2.499	3.517
+ 393.52	1.055'	439.9	3.11	1.796	0.0307	790	49.19	0.3234	6.70E-04	-2.499	3.554
+ 442.71	1.091'	444.56	3.152	1.777	0.0307	790	49.19	0.3178	6.44E-04	-2.499	3.59
WF14 -WF21	1.091'	444.59	3.152	1.777	0.0306	790	0	0.3178	6.44E-04	-2.499	3.59
+ 53.02	1.128'	449.91	3.179	1.756	0.0306	790	53.02	0.3127	6.18E-04	-2.499	3.627
+ 106.04	1.164'	455.09	3.206	1.736	0.0306	790	53.02	0.3078	5.97E-04	-2.499	3.663
+ 159.06	1.198'	460.12	3.231	1.717	0.0306	790	53.02	0.3032	5.78E-04	-2.499	3.697
+ 212.08	1.232'	465.01	3.256	1.699	0.0306	790	53.02	0.2989	5.60E-04	-2.499	3.73
+ 265.10	1.264'	469.76	3.279	1.682	0.0306	790	53.02	0.2948	5.44E-04	-2.499	3.763
+ 318.12	1.295'	474.4	3.302	1.665	0.0306	790	53.02	0.2909	5.28E-04	-2.499	3.794
+ 371.14	1.325'	478.93	3.324	1.65	0.0306	790	53.02	0.2872	5.14E-04	-2.499	3.824
WF21 -WF29	1.326'	478.95	3.324	1.649	0.0306	790	0	0.2872	5.14E-04	-2.499	3.824
+ 50.24	1.354'	483.8	3.331	1.633	0.0306	790	50.24	0.284	5.02E-04	-2.498	3.852
+ 100.47	1.381'	488.63	3.339	1.617	0.0306	790	50.24	0.2809	4.91E-04	-2.498	3.88
+ 150.71	1.408'	493.43	3.346	1.601	0.0306	790	50.24	0.2778	4.80E-04	-2.498	3.907
+ 200.95	1.435'	498.19	3.353	1.586	0.0306	790	50.24	0.2749	4.69E-04	-2.498	3.933
+ 251.19	1.460'	502.91	3.359	1.571	0.0306	790	50.24	0.2721	4.59E-04	-2.498	3.959
+ 301.42	1.486'	507.61	3.366	1.556	0.0306	790	50.24	0.2693	4.50E-04	-2.498	3.984
+ 351.66	1.510'	512.27	3.372	1.542	0.0306	790	50.24	0.2666	4.40E-04	-2.498	4.008
+ 401.90	1.534'	516.91	3.378	1.528	0.0306	790	50.24	0.264	4.32E-04	-2.498	4.032
WF29 -WF39	1.534'	516.92	3.378	1.528	0.0308	790	0	0.264	4.37E-04	-2.498	4.032
+ 50.92	1.559'	521.87	3.323	1.514	0.0308	790	50.92	0.2637	4.38E-04	-2.479	4.038
+ 101.83	1.583'	526.87	3.271	1.499	0.0308	790	50.92	0.2633	4.39E-04	-2.46	4.043
+ 152.74	1.608'	531.91	3.222	1.485	0.0308	790	50.92	0.2628	4.40E-04	-2.44	4.048
+ 203.66	1.632'	536.99	3.175	1.471	0.0308	790	50.92	0.2622	4.40E-04	-2.421	4.054
+ 254.58	1.657'	542.11	3.131	1.457	0.0308	790	50.92	0.2616	4.40E-04	-2.402	4.059
+ 305.49	1.681'	547.25	3.089	1.444	0.0308	790	50.92	0.261	4.40E-04	-2.383	4.064
+ 356.41	1.706'	552.43	3.049	1.43	0.0308	790	50.92	0.2602	4.39E-04	-2.364	4.069
+ 407.32	1.730'	557.63	3.011	1.417	0.0308	790	50.92	0.2595	4.38E-04	-2.344	4.074
+ 458.24	1.754'	562.86	2.974	1.404	0.0308	790	50.92	0.2586	4.37E-04	-2.325	4.079
+ 509.15	1.778'	568.1	2.939	1.391	0.0308	790	50.92	0.2578	4.36E-04	-2.306	4.084
WF39 -WF47	1.778'	568.12	2.94	1.391	0.0317	790	0	0.2578	4.61E-04	-2.306	4.084
+ 49.90	1.790'	533.91	2.924	1.48	0.0317	790	49.9	0.275	5.26E-04	-2.287	4.077
+ 99.81	1.802'	500.04	2.908	1.58	0.0317	790	49.9	0.2943	6.04E-04	-2.268	4.071
+ 149.71	1.816'	466.45	2.892	1.694	0.0317	790	49.9	0.3162	7.00E-04	-2.249	4.065
+ 199.62	1.830'	433.13	2.875	1.824	0.0317	790	49.9	0.3414	8.18E-04	-2.231	4.061
+ 249.52	1.845'	399.9	2.856	1.975	0.0317	790	49.9	0.3708	9.68E-04	-2.212	4.057
+ 299.42	1.861'	366.89	2.836	2.153	0.0317	790	49.9	0.4054	1.16E-03	-2.193	4.054
+ 349.33	1.876'	333.9	2.812	2.366	0.0317	790	49.9	0.4471	1.42E-03	-2.174	4.051
+ 399.23	1.890'	300.76	2.783	2.627	0.0317	790	49.9	0.4985	1.77E-03	-2.155	4.045

WF47 -WF59	1.890*	300.77	2.783	2.627	0.0317	790	0	0.4985	1.77E-03	-2.155	4.045
+ 50.02	1.990*	307.52	2.88	2.569	0.0317	790	50.02	0.4791	1.62E-03	-2.136	4.126
+ 100.04	2.079*	312.95	2.968	2.524	0.0317	790	50.02	0.4636	1.50E-03	-2.118	4.197
+ 150.06	2.161*	317.36	3.05	2.489	0.0317	790	50.02	0.4509	1.41E-03	-2.099	4.26
+ 200.08	2.237*	320.96	3.127	2.461	0.0317	790	50.02	0.4402	1.33E-03	-2.08	4.316
+ 250.10	2.307*	323.88	3.2	2.439	0.0317	790	50.02	0.4311	1.27E-03	-2.061	4.368
+ 300.11	2.374*	326.24	3.271	2.422	0.0317	790	50.02	0.4232	1.21E-03	-2.042	4.416
+ 350.13	2.436*	328.12	3.339	2.408	0.0317	790	50.02	0.4164	1.17E-03	-2.023	4.46
+ 400.15	2.496*	329.58	3.405	2.397	0.0317	790	50.02	0.4104	1.13E-03	-2.004	4.501
+ 450.17	2.554*	330.66	3.47	2.389	0.0317	790	50.02	0.4051	1.09E-03	-1.985	4.539
+ 500.19	2.609*	331.42	3.533	2.384	0.0317	790	50.02	0.4004	1.06E-03	-1.967	4.576
+ 550.21	2.662*	331.88	3.596	2.38	0.0317	790	50.02	0.3962	1.03E-03	-1.948	4.61
+ 600.23	2.714*	332.08	3.659	2.379	0.0317	790	50.02	0.3925	1.01E-03	-1.929	4.642
WF59 -WF63	2.714*	332.08	3.659	2.379	0.031	790	0	0.3925	9.65E-04	-1.929	4.642
+ 50.00	2.763*	333.12	3.706	2.372	0.031	790	50	0.3887	9.43E-04	-1.91	4.673
+ 100.00	2.811*	333.98	3.751	2.365	0.031	790	50	0.3852	9.22E-04	-1.891	4.702
+ 150.01	2.858*	334.68	3.797	2.36	0.031	790	50	0.382	9.04E-04	-1.872	4.73
+ 200.01	2.904*	335.24	3.841	2.357	0.031	790	50	0.3791	8.87E-04	-1.853	4.757
WF63 -WF69	2.904*	335.24	3.841	2.357	0.0308	790	0	0.3791	8.76E-04	-1.853	4.757
+ 50.15	2.949*	336.28	3.887	2.349	0.0308	790	50.15	0.3754	8.57E-04	-1.834	4.783
+ 100.30	2.993*	337.27	3.93	2.342	0.0308	790	50.15	0.3718	8.39E-04	-1.816	4.809
+ 150.45	3.036*	338.22	3.971	2.336	0.0308	790	50.15	0.3683	8.23E-04	-1.797	4.833
+ 200.60	3.079*	339.13	4.007	2.329	0.0308	790	50.15	0.365	8.09E-04	-1.778	4.857
+ 250.75	3.121*	340.03	4.038	2.323	0.0308	790	50.15	0.3617	7.97E-04	-1.759	4.879
+ 300.90	3.162*	340.91	4.059	2.317	0.0308	790	50.15	0.3586	7.87E-04	-1.74	4.902
WF69 -WF75	3.162*	340.91	4.059	2.317	0.0305	790	0	0.3586	7.71E-04	-1.74	4.902
+ 50.96	3.198*	338.52	4.007	2.334	0.0305	790	50.96	0.3648	7.96E-04	-1.721	4.918
+ 101.92	3.235*	336.06	3.947	2.351	0.0305	790	50.96	0.3712	8.24E-04	-1.701	4.936
+ 152.88	3.274*	333.57	3.883	2.368	0.0305	790	50.96	0.3777	8.55E-04	-1.682	4.956
+ 203.85	3.314*	331.04	3.817	2.386	0.0305	790	50.96	0.3843	8.88E-04	-1.663	4.976
+ 254.81	3.355*	328.51	3.751	2.405	0.0305	790	50.96	0.391	9.23E-04	-1.644	4.999
+ 305.77	3.399*	325.98	3.685	2.423	0.0305	790	50.96	0.3978	9.60E-04	-1.624	5.023
WF75 -WF95	3.399*	325.98	3.685	2.423	0.0309	790	0	0.3978	9.85E-04	-1.624	5.023
+ 50.34	3.453*	329.04	3.713	2.401	0.0309	790	50.34	0.3926	9.57E-04	-1.605	5.058
+ 100.68	3.506*	331.94	3.739	2.38	0.0309	790	50.34	0.3878	9.32E-04	-1.586	5.092
+ 151.03	3.557*	334.72	3.764	2.36	0.0309	790	50.34	0.3833	9.08E-04	-1.567	5.124
+ 201.37	3.606*	337.37	3.788	2.342	0.0309	790	50.34	0.379	8.87E-04	-1.548	5.155
+ 251.71	3.655*	339.91	3.811	2.324	0.0309	790	50.34	0.375	8.66E-04	-1.529	5.184
+ 302.05	3.702*	342.34	3.833	2.308	0.0309	790	50.34	0.3713	8.48E-04	-1.51	5.212
+ 352.39	3.748*	344.68	3.854	2.292	0.0309	790	50.34	0.3677	8.30E-04	-1.491	5.239
+ 402.74	3.793*	346.93	3.874	2.277	0.0309	790	50.34	0.3644	8.14E-04	-1.472	5.265
+ 453.08	3.836*	349.09	3.894	2.263	0.0309	790	50.34	0.3612	7.98E-04	-1.453	5.29
+ 503.42	3.879*	351.18	3.912	2.25	0.0309	790	50.34	0.3582	7.84E-04	-1.434	5.314
+ 553.76	3.921*	353.19	3.93	2.237	0.0309	790	50.34	0.3553	7.70E-04	-1.415	5.337
+ 604.10	3.963*	355.13	3.947	2.225	0.0309	790	50.34	0.3526	7.57E-04	-1.396	5.359
+ 654.45	4.003*	357.01	3.964	2.213	0.0309	790	50.34	0.35	7.45E-04	-1.377	5.38
+ 704.79	4.043*	358.83	3.98	2.202	0.0309	790	50.34	0.3475	7.34E-04	-1.358	5.401
+ 755.13	4.082*	360.59	3.996	2.191	0.0309	790	50.34	0.3451	7.23E-04	-1.339	5.421
+ 805.47	4.120*	362.29	4.011	2.181	0.0309	790	50.34	0.3428	7.13E-04	-1.32	5.441
+ 855.81	4.158*	363.95	4.025	2.171	0.0309	790	50.34	0.3406	7.03E-04	-1.301	5.46
+ 906.16	4.195*	365.55	4.039	2.161	0.0309	790	50.34	0.3385	6.93E-04	-1.282	5.478
+ 956.50	4.232*	367.1	4.053	2.152	0.0309	790	50.34	0.3365	6.84E-04	-1.263	5.495
+ 1,006.84	4.268*	368.62	4.066	2.143	0.0309	790	50.34	0.3346	6.76E-04	-1.244	5.513
WF95 -WF99	4.268*	368.62	4.066	2.143	0.0309	790	0	0.3346	6.76E-04	-1.244	5.513
+ 49.90	4.304*	370.07	4.079	2.135	0.0309	790	49.9	0.3327	6.68E-04	-1.226	5.529
+ 99.80	4.338*	371.49	4.091	2.127	0.0309	790	49.9	0.331	6.60E-04	-1.207	5.545
+ 149.70	4.373*	372.86	4.103	2.119	0.0309	790	49.9	0.3293	6.53E-04	-1.188	5.561
+ 199.60	4.407*	374.2	4.115	2.111	0.0309	790	49.9	0.3276	6.45E-04	-1.169	5.576

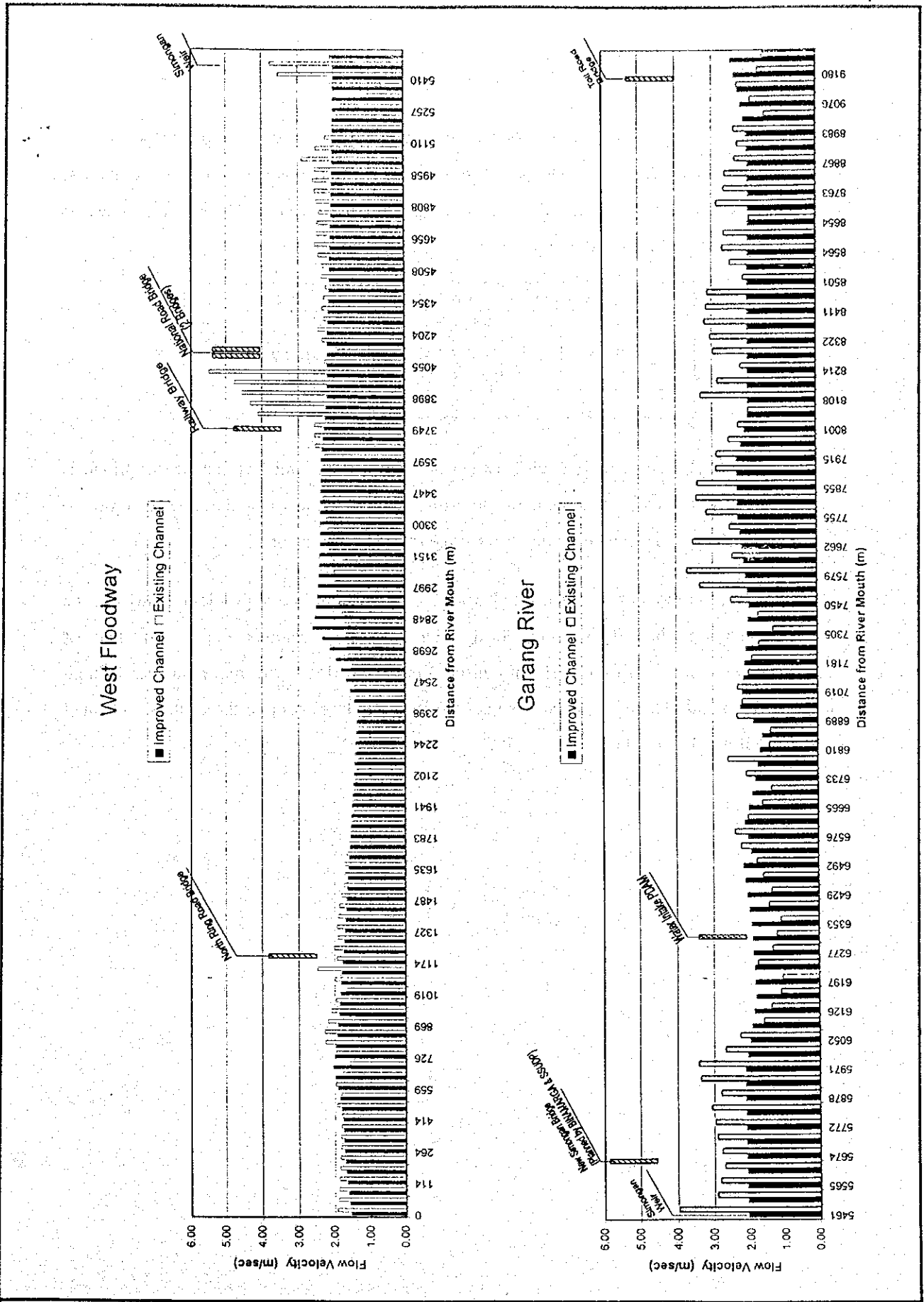
LONGITUDINAL PROFILE OF WEST FLOODWAY CHANNEL



THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

Fig.

JAPAN INTERNATIONAL COOPERATION AGENCY



THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

Fig.

JAPAN INTERNATIONAL COOPERATION AGENCY

(2) Water Level Rise by Bridge Pier

In connection with the bridge raising and construction of new piers, the piers of Railway Bridge may induce a rise in water level in the upstream channel. So, the rise of water level is estimated by using D'Aubuisson's formula. The result is shown in the table below together with the calculation conditions.

Calculation Condition		Result
Q	790 m ³ /s	$\Delta h = 0.11 \text{ m}$
H ₁ , B	4.8 m, 3.0 m x 2	
b ₁ , b ₂	80.0 m, 74.0 m	
C ²	0.81	

The D.H.W.L in the stretch between Railway Bridge and National Road Bridge is determined with a tolerance of more than 0.11 m against calculated water level, so the D.H.W.L can confine the water stage raised by bridge piers.

Also, the piers of National Road Bridge may cause the same problem. However, the upstream channel from the bridge has a bigger channel depth than that of downstream. This channel can confine the design flood with more than 1.5 m high freeboard. Therefore, even if some rise in water level occurs, the upstream channel will not be affected.

(3) Pumping Station near North Ring Road Bridge and Water Level of West Floodway

To solve the drainage problem in Tanah Mas residential area which lies along the right bank of West Floodway (Drainage area : 127 ha), Semarang City formulated drainage system improvement including pump drainage into West Floodway. This pumping station is located at the lower end of Bulu River near the North Ring Road Bridge as shown in the following drawing. (Currently, Bulu River is connected to West Floodway by a box culvert laid under North Ring Road) According to the drainage plan, a pumping station with the total pump capacity of 3.0 m³/s has been proposed as follows:

	Number and Capacity of Pump			Pump Operation
1	1.4 m ³ /s	2 units	Sub total 2.8 m ³ /s	Rainy season only
2	0.1 m ³ /s	2 units	Sub total 0.2 m ³ /s	Dry and Rainy seasons
3	Total		3.0 m ³ /s	

To know the hydraulic impact on the flood flow in West Floodway, the Study Team estimated a rise in water level by non-uniform flow calculation. The calculation results are presented in the following calculation sheets. The estimated rise is as small as 5 mm which is negligible. Therefore, the Study Team judged that there is no hydraulic impact on the main river flow. The results are presented in the following calculation sheets.

** INPUT DATA ** PUMPING STATION Q=3.0 t/m3

* BAISIC DATA *

KUKAN-SU = 17 ALPHA = 1.00 QO = 793.00 M3/S HO = .250 M ZO = -2.500 M

JCO = 0 KEY = 0 IPT = 0

* KUKAN DATA *

DANMEN NO.	BUNKATSU SUU	DANMEN KEIJO	LOSS TYPE	SODO KEISU	KUKAN KYORI (M)	KASYO KOUBAI (1/1)	RAKUSA (M)	RYUNYU RYO (M3/S)
1	WF-9 -WFO	9	2 1	0	0300	413.70	999999.00	.000
2	WFO - WF4	4	2 1	0	0310	208.96	999999.00	.000
3	WF4 - WF14	10	2 1	0	0307	492.71	999999.00	.000
4	WF14 -WF21	7	2 1	0	0306	371.14	999999.00	.000
5	WF21 -WF29	8	2 1	0	0306	401.90	999999.00	.000
6	WF29 -WF39	10	2 1	0	0311	509.15	2650.00	.000
7	WF39 -WF42	3	2 1	0	0317	149.23	2650.00	.000
8	WF42 -WF53	11	2 1	0	0317	550.00	2650.00	.000
9	WF53 -WF59	6	2 1	0	0317	300.00	2650.00	.000
10	WF59 -WF63	4	2 1	0	0312	200.01	2650.00	.000
11	WF63 -WF69	6	2 1	0	0310	300.90	2650.00	.000
12	WF69 -WF72	3	2 1	0	0307	155.77	2650.00	.000
13	WF72 -WF73	1	2 1	0	0305	50.00	2650.00	.000
14	WF73 -WF75	2	2 1	0	0305	100.00	2650.00	.000
15	WF75 -WF76	1	2 1	0	0300	50.00	2650.00	.000
16	WF76 -WF95	19	2 1	0	0310	956.84	2650.00	.000
17	WF95 -WF99	4	2 1	0	0310	199.60	2650.00	.000

* KEIJO DATA *

KUKAN	KEIJO	BO (R)	M1	N1	B1	B2	HP (B3)	M2	N2
1	2 1	150.000	2.000	2.000	50.000	40.000	2.000	2.000	.001
		150.000	2.000	2.000	10.000	10.000	2.200	2.000	2.000
2	2 1	150.000	2.000	2.000	10.000	10.000	2.200	2.000	2.000
		115.000	2.000	2.000	9.000	10.000	2.500	2.000	2.000
3	2 1	115.000	2.000	2.000	9.000	10.000	2.500	2.000	2.000
		115.000	2.000	2.000	9.000	5.000	2.700	2.000	2.000
4	2 1	115.000	2.000	2.000	9.000	5.000	2.700	2.000	2.000
		115.000	2.000	2.000	8.000	6.000	3.000	2.000	2.000
5	2 1	115.000	2.000	2.000	8.000	6.000	3.000	2.000	2.000
		115.000	2.000	2.000	9.000	25.000	3.000	2.000	2.000
6	2 1	115.000	2.000	2.000	9.000	25.000	3.000	2.000	2.000
		115.000	2.000	2.000	10.000	48.000	3.000	2.000	2.000
7	2 1	115.000	2.000	2.000	10.000	48.000	3.000	2.000	2.000
		115.000	2.000	2.000	6.000	18.000	3.000	2.000	2.000
8	2 1	115.000	2.000	2.000	6.000	18.000	3.000	2.000	2.000
		58.000	2.000	2.000	10.000	13.000	3.200	2.000	2.000
9	2 1	58.000	2.000	2.000	12.000	15.000	3.200	2.000	2.000
		58.000	2.000	2.000	7.000	8.000	3.300	2.000	2.000
10	2 1	58.000	2.000	2.000	7.000	8.000	3.300	2.000	2.000
		58.000	2.000	2.000	7.000	4.000	3.400	2.000	2.000
11	2 1	58.000	2.000	2.000	7.000	4.000	3.400	2.000	2.000
		58.000	2.000	2.000	10.000	7.000	3.500	2.000	2.000
12	2 1	58.000	2.000	2.000	10.000	7.000	3.500	2.000	2.000
		50.000	1.000	1.000	4.000	4.000	3.500	.500	.500
13	2 1	50.000	1.000	1.000	4.000	4.000	3.500	.500	.500
		50.000	1.000	1.000	4.000	4.000	3.500	.500	.500
14	2 1	50.000	1.000	1.000	4.000	4.000	3.500	.500	.500
		50.000	2.000	2.000	4.000	5.000	3.500	2.000	2.000
15	2 1	50.000	2.000	2.000	4.000	5.000	3.500	2.000	2.000
		50.000	2.000	2.000	8.000	6.000	3.500	2.000	2.000
16	2 1	50.000	2.000	2.000	8.000	6.000	3.500	2.000	2.000
		50.000	2.000	2.000	8.000	6.000	3.500	2.000	2.000
17	2 1	50.000	2.000	2.000	8.000	6.000	3.500	2.000	2.000
		50.000	2.000	2.000	8.000	8.000	3.500	2.000	2.000

* LOSS DATA *

KUKAN LOSS TYPE FL1 FL2

NO.	H	A	R	V	N	Q	DX	FROUD	IE	Z	H-Z
WF-9 -WFO	.250	494.56	1.967	1.603	0300	793.00	.00	3638	.9386E-03	-2.500	2.750
+ 45.97	.293	497.55	2.041	1.594	0300	793.00	45.97	3551	.8831E-03	-2.500	2.793
+ 91.93	.334	499.47	2.114	1.588	0300	793.00	45.97	3475	.8359E-03	-2.500	2.834
+ 137.90	.372	500.57	2.189	1.584	0300	793.00	45.97	3408	.7947E-03	-2.500	2.872
+ 183.87	.408	500.95	2.265	1.583	0300	793.00	45.97	3348	.7581E-03	-2.500	2.908
+ 229.83	.442	500.73	2.344	1.584	0300	793.00	45.97	3293	.7251E-03	-2.500	2.942

+ 275.80	.474	499.99	2.425	1.586	.0300	793.00	45.97	.3242	6948E-03	-2.500	2.974
+ 321.77	.505	498.78	2.511	1.590	.0300	793.00	45.97	.3193	6667E-03	-2.500	3.004
+ 367.73	.534	497.17	2.601	1.595	.0300	793.00	45.97	.3147	6402E-03	-2.500	3.034
+ 413.70	.562	495.21	2.696	1.601	.0300	793.00	45.97	.3103	6151E-03	-2.500	3.061
WFO - WF4	.562	495.24	2.696	1.601	.0310	793.00	.00	.3103	6566E-03	-2.500	3.061
+ 52.24	.584	470.55	2.692	1.685	.0310	793.00	52.24	.3267	7288E-03	-2.500	3.083
+ 104.48	.608	445.81	2.687	1.779	.0310	793.00	52.24	.3451	8138E-03	-2.499	3.107
+ 156.72	.633	420.97	2.681	1.884	.0310	793.00	52.24	.3658	9156E-03	-2.499	3.133
+ 208.96	.661	395.99	2.673	2.003	.0310	793.00	52.24	.3893	1039E-02	-2.499	3.160
WF4 - WF14	.661	395.91	2.673	2.003	.0307	793.00	.00	.3894	1019E-02	-2.499	3.160
+ 49.27	.717	403.48	2.728	1.965	.0307	793.00	49.27	.3781	9549E-03	-2.499	3.216
+ 98.54	.769	410.40	2.780	1.932	.0307	793.00	49.27	.3683	9002E-03	-2.499	3.268
+ 147.81	.818	416.81	2.829	1.903	.0307	793.00	49.27	.3594	8527E-03	-2.499	3.317
+ 197.08	.864	422.79	2.875	1.876	.0307	793.00	49.27	.3514	8109E-03	-2.499	3.364
+ 246.35	.908	428.40	2.920	1.851	.0307	793.00	49.27	.3442	7739E-03	-2.499	3.407
+ 295.63	.950	433.68	2.962	1.829	.0307	793.00	49.27	.3375	7408E-03	-2.499	3.449
+ 344.90	.989	438.67	3.003	1.808	.0307	793.00	49.27	.3314	7110E-03	-2.499	3.488
+ 394.17	1.027	443.40	3.042	1.788	.0307	793.00	49.27	.3257	6840E-03	-2.499	3.526
+ 443.44	1.063	447.89	3.080	1.771	.0307	793.00	49.27	.3204	6594E-03	-2.499	3.562
+ 492.71	1.098	452.17	3.116	1.754	.0307	793.00	49.27	.3155	6368E-03	-2.499	3.597
WF14 - WF21	1.098	452.20	3.117	1.754	.0306	793.00	.00	.3154	6325E-03	-2.499	3.597
+ 53.02	1.135	456.74	3.145	1.736	.0306	793.00	53.02	.3109	6127E-03	-2.499	3.633
+ 106.04	1.169	461.15	3.171	1.720	.0306	793.00	53.02	.3066	5942E-03	-2.499	3.668
+ 159.06	1.203	465.40	3.197	1.704	.0306	793.00	53.02	.3026	5771E-03	-2.499	3.702
+ 212.08	1.236	469.50	3.222	1.689	.0306	793.00	53.02	.2987	5612E-03	-2.499	3.735
+ 265.10	1.268	473.47	3.246	1.675	.0306	793.00	53.02	.2951	5464E-03	-2.499	3.766
+ 318.12	1.299	477.32	3.270	1.661	.0306	793.00	53.02	.2917	5326E-03	-2.499	3.797
+ 371.14	1.329	481.05	3.292	1.648	.0306	793.00	53.02	.2884	5196E-03	-2.499	3.827
WF21 - WF29	1.329	481.07	3.292	1.648	.0306	793.00	.00	.2884	5195E-03	-2.499	3.827
+ 50.24	1.358	487.43	3.277	1.627	.0306	793.00	50.24	.2853	5092E-03	-2.498	3.857
+ 100.47	1.387	493.88	3.263	1.606	.0306	793.00	50.24	.2822	4989E-03	-2.498	3.885
+ 150.71	1.415	500.37	3.249	1.585	.0306	793.00	50.24	.2792	4887E-03	-2.498	3.914
+ 200.95	1.443	506.91	3.236	1.564	.0306	793.00	50.24	.2761	4787E-03	-2.498	3.941
+ 251.19	1.470	513.50	3.225	1.544	.0306	793.00	50.24	.2731	4687E-03	-2.498	3.968
+ 301.42	1.496	520.14	3.213	1.525	.0306	793.00	50.24	.2701	4590E-03	-2.498	3.994
+ 351.66	1.522	526.81	3.203	1.505	.0306	793.00	50.24	.2671	4494E-03	-2.498	4.020
+ 401.90	1.547	533.52	3.193	1.486	.0306	793.00	50.24	.2642	4400E-03	-2.498	4.045
WF29 - WF39	1.547	533.53	3.193	1.486	.0311	793.00	.00	.2642	4544E-03	-2.498	4.045
+ 50.92	1.572	536.92	3.167	1.477	.0311	793.00	50.92	.2636	4536E-03	-2.479	4.051
+ 101.83	1.596	540.33	3.143	1.468	.0311	793.00	50.92	.2630	4526E-03	-2.460	4.056
+ 152.74	1.621	543.76	3.119	1.458	.0311	793.00	50.92	.2623	4515E-03	-2.440	4.061
+ 203.66	1.645	547.20	3.095	1.449	.0311	793.00	50.92	.2617	4503E-03	-2.421	4.066
+ 254.58	1.669	550.65	3.073	1.440	.0311	793.00	50.92	.2610	4490E-03	-2.402	4.071
+ 305.49	1.693	554.11	3.051	1.431	.0311	793.00	50.92	.2603	4477E-03	-2.383	4.076
+ 356.41	1.717	557.57	3.029	1.422	.0311	793.00	50.92	.2597	4463E-03	-2.364	4.081
+ 407.32	1.741	561.04	3.009	1.413	.0311	793.00	50.92	.2589	4449E-03	-2.344	4.086
+ 458.24	1.765	564.52	2.989	1.405	.0311	793.00	50.92	.2582	4434E-03	-2.325	4.090
+ 509.15	1.789	568.00	2.969	1.396	.0311	793.00	50.92	.2575	4418E-03	-2.306	4.095
WF39 - WF42	1.789	568.02	2.969	1.396	.0317	793.00	.00	.2575	4590E-03	-2.306	4.095

*** WEST FLOODWAY , STEADY NON-UNIFORM FLOW (LEVEL, -2.5, 1/2650) b=50 wf75-up

PAGE = 3

NO.	H	A	R	V	N	Q	DX	FROUD	IE	Z	H-Z
+ 49.74	1.807	555.49	3.086	1.428	.0317	793.00	49.74	.2582	4557E-03	-2.287	4.094
+ 99.49	1.825	542.90	3.219	1.461	.0317	793.00	49.74	.2586	4510E-03	-2.268	4.093
+ 149.23	1.842	530.24	3.371	1.496	.0317	793.00	49.74	.2586	4447E-03	-2.250	4.092
WF42 - WF53	1.842	530.25	3.371	1.496	.0317	793.00	.00	.2586	4447E-03	-2.250	4.092
+ 50.00	1.855	507.63	3.340	1.562	.0317	793.00	50.00	.2713	4913E-03	-2.231	4.086
+ 100.00	1.869	485.24	3.308	1.634	.0317	793.00	50.00	.2851	5446E-03	-2.212	4.081
+ 150.00	1.884	463.10	3.275	1.712	.0317	793.00	50.00	.3002	6059E-03	-2.193	4.078
+ 200.00	1.901	441.18	3.241	1.797	.0317	793.00	50.00	.3167	6770E-03	-2.174	4.076
+ 250.00	1.920	419.49	3.206	1.890	.0317	793.00	50.00	.3348	7597E-03	-2.155	4.075
+ 300.00	1.940	397.97	3.169	1.993	.0317	793.00	50.00	.3548	8573E-03	-2.136	4.076
+ 350.00	1.962	376.73	3.131	2.105	.0317	793.00	50.00	.3770	9722E-03	-2.118	4.080
+ 400.00	1.987	355.72	3.091	2.229	.0317	793.00	50.00	.4016	1109E-02	-2.099	4.085
+ 450.00	2.014	334.94	3.049	2.368	.0317	793.00	50.00	.4293	1274E-02	-2.080	4.094
+ 500.00	2.044	314.37	3.005	2.522	.0317	793.00	50.00	.4605	1475E-02	-2.061	4.105
+ 550.00	2.077	294.02	2.957	2.697	.0317	793.00	50.00	.4961	1722E-02	-2.042	4.119
WF53 - WF59	2.089	298.93	2.889	2.653	.0317	793.00	.00	.4939	1719E-02	-2.042	4.132
+ 50.00	2.185	304.24	2.988	2.607	.0317	793.00	50.00	.4770	1586E-02	-2.023	4.208
+ 100.00	2.271	308.46	3.081	2.571	.0317	793.00	50.00	.4631	1481E-02	-2.004	4.275
+ 150.00	2.350	311.83	3.169	2.543	.0317	793.00	50.00	.4515	1396E-02	-1.986	4.335
+ 200.00	2.423	314.51	3.255	2.521	.0317	793.00	50.00	.4416	1324E-02	-1.967	4.390
+ 250.00	2.492	316.63	3.338	2.504	.0317	793.00	50.00	.4330	1264E-02	-1.948	4.440
+ 300.00	2.558	318.27	3.420	2.492	.0317	793.00	50.00	.4255	1211E-02	-1.929	4.486
WF59 - WF63	2.558	318.27	3.420	2.492	.0312	793.00	.00	.4255	1173E-02	-1.929	4.487
+ 50.00	2.620	320.64	3.475	2.473	.0312	793.00	50.00	.4188	1131E-02	-1.910	4.530
+ 100.00	2.680	322.75	3.530	2.457	.0312	793.00	50.00	.4128	1093E-02	-1.891	4.571
+ 150.01	2.737	324.64	3.583	2.443	.0312	793.00	50.00	.4073	1060E-02	-1.872	4.609
+ 200.01	2.792	326.32	3.635	2.430	.0312	793.00	50.00	.4022	1029E-02	-1.853	4.646
WF63 - WF69	2.792	326.32	3.635	2.430	.0310	793.00	.00	.4022	1015E-02	-1.853	4.646
+ 50.15	2.851	330.87	3.638	2.397	.0310	793.00	50.15	.3965	9867E-03	-1.835	4.685
+ 100.30	2.907	335.29	3.640	2.365	.0310	793.00	50.15	.3912	9601E-03	-1.816	4.723
+ 150.45	2.962	339.61	3.641	2.335	.0310	793.00	50.15	.3862	9356E-03	-1.797	4.759
+ 200.60	3.015	343.82	3.641	2.306	.0310	793.00	50.15	.3815	9128E-03	-1.778	4.793
+ 250.75	3.067	347.92	3.640	2.279	.0310	793.00	50.15	.3770	8916E-03	-1.759	4.825
+ 300.90	3.117	351.94	3.639	2.253	.0310	793.00	50.15	.3728	8718E-03	-1.740	4.857
WF69 - WF72	3.117	351.94	3.639	2.253	.0307	793.00	.00	.3728	8550E-03	-1.740	4.857
+ 51.92	3.120	325.38	3.707	2.437	.0307	793.00	51.92	.3980	9758E-03	-1.720	4.841
+ 103.85	3.119	298.71	3.778	2.655	.0307	793.00	51.92	.4267	1129E-02	-1.701	4.819
+ 155.77	3.108	271.87	3.841	2.917	.0307	793.00	51.92	.4601	1333E-02	-1.681	4.789
WF72 - WF73	3.108	271.87	3.841	2.917	.0305	793.00	.00	.4601	1316E-02	-1.681	4.789
+ 50.00	3.184	275.68	3.888	2.877	.0305	793.00	50.00	.4508	1259E-02	-1.662	4.846

WF73 -WF75	3.184	275.68	3.888	2.877	.0305	793.00	.00	.4508	.1259E-02	-1.662	4.846
+ 50.00	3.297	295.39	3.900	2.685	.0305	793.00	50.00	.4252	.1092E-02	-1.643	4.941
+ 100.00	3.393	314.90	3.867	2.518	.0305	793.00	50.00	.4031	.9720E-03	-1.625	5.018
WF75 -WF76	3.393	314.90	3.867	2.518	.0300	793.00	.00	.4031	.9404E-03	-1.625	5.018
+ 50.00	3.462	326.72	3.770	2.427	.0300	793.00	50.00	.3938	.9037E-03	-1.606	5.068
WF76 -WF95	3.462	326.72	3.770	2.427	.0310	793.00	.00	.3938	.9649E-03	-1.606	5.068
+ 50.36	3.515	329.60	3.796	2.406	.0310	793.00	50.36	.3889	.9393E-03	-1.587	5.102
+ 100.72	3.567	332.35	3.822	2.386	.0310	793.00	50.36	.3844	.9157E-03	-1.568	5.135
+ 151.08	3.617	334.98	3.846	2.367	.0310	793.00	50.36	.3802	.8938E-03	-1.549	5.166
+ 201.44	3.666	337.50	3.869	2.350	.0310	793.00	50.36	.3762	.8735E-03	-1.530	5.196
+ 251.80	3.713	339.92	3.891	2.333	.0310	793.00	50.36	.3724	.8546E-03	-1.511	5.224
+ 302.16	3.760	342.24	3.912	2.317	.0310	793.00	50.36	.3689	.8370E-03	-1.492	5.251
+ 352.52	3.805	344.48	3.932	2.302	.0310	793.00	50.36	.3655	.8205E-03	-1.473	5.278
+ 402.88	3.849	346.63	3.952	2.288	.0310	793.00	50.36	.3623	.8050E-03	-1.454	5.303
+ 453.24	3.893	348.71	3.970	2.274	.0310	793.00	50.36	.3593	.7905E-03	-1.435	5.327

*** WEST FLOODWAY , STEADY NON-UNIFORM FLOW (LEVEL, -2.5, 1/2650) b=50 wf75-up

PAGE = 4

NO.	H	A	R	V	N	Q	DX	FROUD	IE	Z	H-Z
+ 503.60	3.935	350.71	3.989	2.261	.0310	793.00	50.36	.3564	.7768E-03	-1.416	5.351
+ 553.96	3.977	352.64	4.006	2.249	.0310	793.00	50.36	.3537	.7638E-03	-1.397	5.373
+ 604.32	4.018	354.51	4.023	2.237	.0310	793.00	50.36	.3511	.7516E-03	-1.378	5.395
+ 654.68	4.058	356.32	4.039	2.225	.0310	793.00	50.36	.3486	.7400E-03	-1.359	5.416
+ 705.04	4.097	358.08	4.055	2.215	.0310	793.00	50.36	.3462	.7290E-03	-1.340	5.437
+ 755.40	4.136	359.78	4.070	2.204	.0310	793.00	50.36	.3439	.7185E-03	-1.321	5.457
+ 805.76	4.174	361.42	4.084	2.194	.0310	793.00	50.36	.3417	.7086E-03	-1.302	5.476
+ 856.12	4.212	363.02	4.099	2.184	.0310	793.00	50.36	.3396	.6991E-03	-1.283	5.494
+ 906.48	4.249	364.57	4.112	2.175	.0310	793.00	50.36	.3376	.6901E-03	-1.264	5.512
+ 956.84	4.285	366.08	4.126	2.166	.0310	793.00	50.36	.3356	.6815E-03	-1.245	5.530
WF95 -WF99	4.285	366.08	4.126	2.166	.0310	793.00	.00	.3356	.6815E-03	-1.245	5.530
+ 49.90	4.323	368.68	4.128	2.151	.0310	793.00	49.90	.3332	.6714E-03	-1.226	5.548
+ 99.80	4.359	371.25	4.130	2.136	.0310	793.00	49.90	.3308	.6617E-03	-1.207	5.566
+ 149.70	4.395	373.78	4.132	2.122	.0310	793.00	49.90	.3285	.6524E-03	-1.188	5.583
+ 199.60	4.430	376.29	4.133	2.107	.0310	793.00	49.90	.3263	.6435E-03	-1.169	5.600