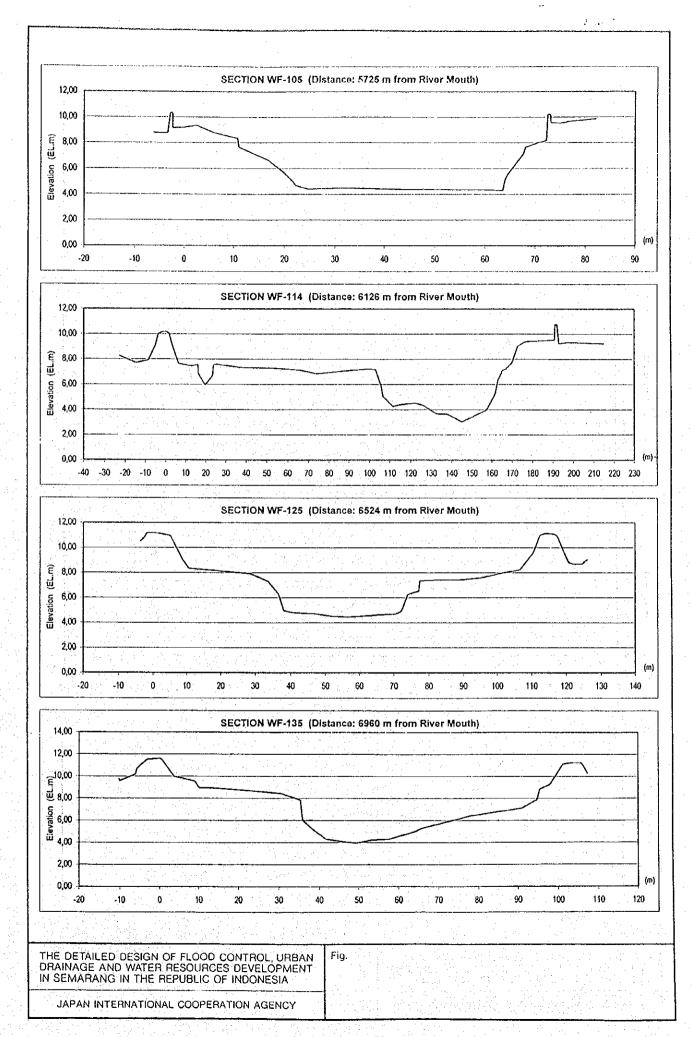
2.1.3 Garang River

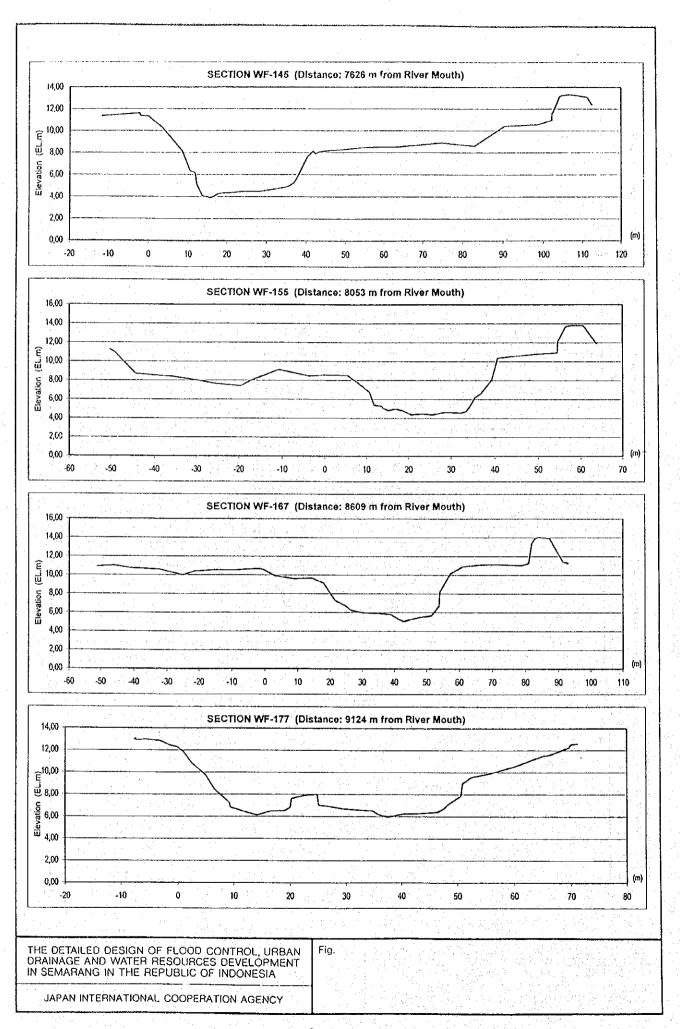
(1) River Cross Sections

The typical cross sections of Garang River are shown in the following figures.

(2) River Flow Capacity

The flow capacity of channel was obtained based on the water level profile under several discharges. The calculation was done for the discharge of 300 m³/s, 500 m³/s, 700 m³/s, 900 m³/s, 1,000 m³/s, 1,200 m³/s. And, the water flow profiles and the chart of the flow capacity are shown in the following sheets.





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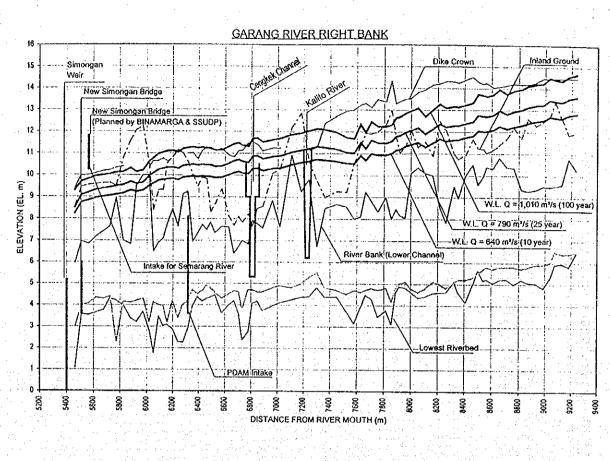
24	WF-123	11 702	***	4.000									
		11.792	655.5	4.832	131.2	1.831	0.035	1200	32.3	2.668-01	5.03E-04	238.01	15.428
25	₩F-124	11,772	593,4	4,781	120	2.022	0.035	1200	30.9	2.95€-01	6.22E-04	291.44	17.072
25	WF-125	11.662	462,1	5,048	96.3	2.597	0,035	1200	32,8	3,69E-01	9.54E-04	471.92	21.724
27	WF-126	11,662	426.8	4.407	135.5	2.811	0,035	1200	\$1.6	4.28E-01	1.34E-03	578,75	24.057
28	WF-127	11.845	513.3	4.133	124.7	2.338	0.035	1200	49.9	3,67E-01	1.01E-03	408.87	20,221
29	WF-128	11.98	648	4.49	130,3	1.852	0.035	1200	39.1	2.79E-01	5.67E-04	249.59	15.798
30	WF-129	12.038	739,1	5.194	133,6	1.624	0.035	1200	38.4	2.28E-01	3.59E-04	182.73	13.518
31	WF-130	11.905	476.5	1.837	522.4	2.519	0.035	1200	29.5	5.94E-01	3,45E 03	621,72	24.934
32	WF-131	11.849	384.2	4,271	206	3,124	0.035	1200	45.5	4.83E-01	1.73E-03	721.92	26.869
33	WF 132	12.257	762.5	3.15	169.5	1.574	0.035	1200	30.7	2.83E-01	6.57E 04	202.83	
34	WF-133	12.291	791.4	2,827	247.7	1,515	0.035	1200	37.4	2.88E-01	7.05E-04	195.2	14,242
35	WF-134	12.077	442.7	4.122	126.2	2.711	0.035	1200					13.971
36	WF-135	12.191	458.7	4.561	213.4	2.616			41.7	4.27E-01	1.36E-03	550.09	23.454
37	WF-136	12.262	458.4	3.945	98.9	2.618	0.035	1200	72	3.91€-01	1.11E-03	495.39	22.257
38	WF-137	12,471					0.035	1200	58.2	4.21E-01	1.35E 03	520.77	22.82
39		12.522	535.2	3.339	218	2.242	0.035	1200	89.7	3.92€-01	1.23E-03	403.81	20.095
	WF-138		509.2	4.492	122.6	2.356	0.035	1200	72.5	3.55E 01	9.18E-04	404,02	20.1
40	WF-139	12,645	597.9	5.364	285.8	2.007	0.035	1200	61.8	2.77E-01	5.26E-04	276.26	16.621
41	WF-140	12.752	770.9	5.736	134.8	1.557	0.035	1200	61.6	2.08E-01	2.89E-04	162.52	12.748
42	WF-141	12.703	605	4.467	130.5	1.984	0.035	1200	59.1	3.00E-01	6.55€ 04	286.82	16.936
43	WF-142	12.546	406.6	4.684	307.5	2.951	0.035	1200	86.4	4.36E-01	1.36E-03	624.86	24,997
44	WF-143	12.221	285.6	5.499	94.8	4.202	0.035	1200	73.1	5.72E-01	2.23E-03	1200.66	34.651
45	WF-144	12.134	255.7	5,758	117.3	4.694	0.035	1200	56.2	6.25E-01	2.62E-03	1475.51	38.412
46	WF-145	12.949	418.7	3,249	290.8	2.866	0.035	1200	46.9	5,08E-01	2.09E-03	665.83	25.804
47	₩F-146	12.5	278.4	5.49	138.3	4.311	0.035	1200	36,2	5.88E-01	2.35E 03	1264.65	35.562
48	WF-147	13.083	406.9	4.781	143.9	2.949	0.035	1200	42.4	4.31E-01	1.32E-03	619.86	24.897
49	WF-148	12.793	301.6	6.391	71.3	3.978	0.035	1200	50.3	5.03E-01	1.63E-03		
50	₩F-149	12,785	281,2	5,505	174.2	4.268	0.035	1200	50.3 58	5.81E-01	2.30E-03	1023.77	31.996
51	WF-150	12.876	280.7	5.682	124.2	4.275	0,035	1200	41,5			1238.38	35.191
52	WF-151	13.283	354.3	5.69	64.5	3.387		1200		5.73E-01	2.21E 03	1229.58	35.065
53	WF-152	13.323	355.2	5.495	79.8	3.379	0.035		33.4	4.54E-01	1.38E 03	771.22	27.771
. 54	WF-153	13,487	396.1	6,341	66.3		0.035	1200	26.5	4.60E-01	1.44E 03	776.64	27.868
55	WF-154	13,644	454.2			3.029	0.035	1200	40.9	3,84E-01	9.58E-04	595.29	24.398
				4.948	117.8	2.642	0.035	1200	45.8	3.79E 01	1.01E 03	491.76	22.176
56	WF-155	13.788	521.6	3.487	218.5	2.301	0.035	1200	51.8	3.94E-01	1.23E-03	419.07	20.471
57	WF:156	13.317	297.6	5.556	84	4.032	0.035	1200	54.5	5.47E-01	2.02E-03	1102.03	33,197
58	WF-157	13,663	356.7	5.84	164.8	3.364	0.035	1200	56.1	4.45E-01	1.32E 03	754,53	27,469
59	WF-158	13.975	471.1	3.848	399.6	2.547	0.035	1200	50.2	4.15E-01	1.32E-03	497.1	22.296
60	WF-159	13.764	345.9	5.263	134.5	3.469	0,035	1200	48.6	4.83E-01	1.61E-03	830.45	28.817
61	WF-160	13.83	336.6	5.097	145.8	3.565	0.035	1200	59.6	5.04E-01	1.78E 03	886.38	29.772
52	WF-161	13.788	313.3	5.49	101.8	3.83	0.035	1200	32	5.22E-01	1.86E 03	998,33	31.596
63	₩F-162	13.881	312.1	6.045	69.5	3.845	0.035	1200	56.4	5.00E-01	1.65E-03	974.39	31.215
64	WF-163	14.004	321.3	6,435	89.4	3.734	0.035	1200	52.3	4.70E-01	1.43E-03	900.13	30.002
65	₩F-164	14.469	505	5.204	117.7	2.376	0.035	1200	38	3.33E-01	7.67E 04	391.14	19.777
66	WF-165	14.416	433.5	3.555	324.1	2.768	0.035	1200	39.6	4.69€-01	1.73E-03	602.82	24.552
67	WF-166	14.345	382.2	4.372	291.4	3.14	0.035	1200	23.9	4.80E-01	1.69E-03	723.86	26.905
58	WF 167	14.416	383.8	5.38	127	3.126	0.035	1200	45.1	4.31E-01	1.27E-03	669.62	25.877
69	WF-168	14.708	537.2	4,168	102.3	2.234	0.035	1200	44.5	3.50E-01	9,12E-04	372.29	19.295
70	WF-169	14,446	354.9	5,367	101.8	3.381	0.035	1200	55.1	4.66E-01	1.49E-03	783.89	27,998
71	WF-170	14.618	387.3	4.804	229	3.098	0.035	1200	53.4	4.52E-01	1.45E-03		
72	WF-171	14.701	391	5,321	151.7	3.069	0.035	1200	55			683.07	26.136
73	WF-172	14,864	440.4	4,44	220	2.725	0.035	1200	49.5	4.25E-01	1.24E-03	647.75	25.451
74	₩F-173	14.955	449.9	4.667	309.2	2.723				4.13E-01	1.25E-03	542.34	23.288
75	WF-174	14.987	426.9	3.797	465.9		0.035	1200	63.1	3,94E-01	1.128-03	511.03	. 22.606
76	WF-175	15.288	688.8	5.128	198.1	2.811	0.035	1200	52.6	4.61E-01	1.63E-03	608,15	24.661
77	WF-176	15.206	535.2			1.742	0.035	1200	51.1	2.46E 01	4.20E-04	211.27	14.535
78	WF-177	15.121	443.9	6.161 6.615	99.9 90.9	2.242	0.035	1200	41.9	2.89E 01	5,45E-04	329.27	18.146
79	WF-178	15.365	587.6				0.035	1200	49.3	3.36E-01	7.21E-04	457.34	21.618
80				1.816	220.3	2,042	0.035	1200	55	4.84E-01	2.31E 03	410.37	20.257
au.	WF-179	15.483	656.6	6.543	122.9	1.828	0.035	1200	58	2.28E-01	3.34E-04	214.4	14.642

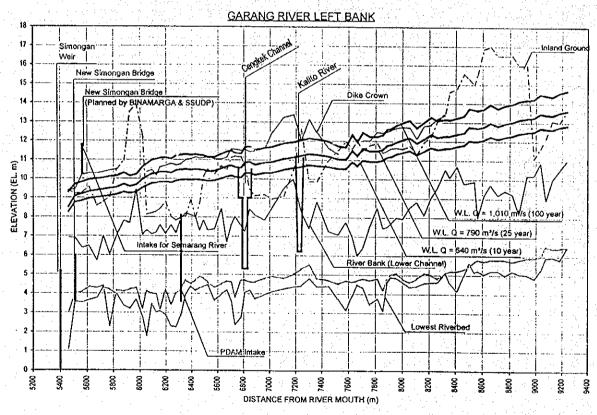
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NO .	D NAME	Н	· · · · · · · · · · · · · · · · · · ·	NO D-NAME	н .	Q	NO D-NAME	н	Q
1	WF-100	9.4	. 0 .	2 WF-101	9.4	0	3 WF-102	9.4	0
•	100	7.1 7.8	300 500	2 111-101	7.934	300	3 WF-102	7.976	300
		8.51	700		8.38 8.928	500 700		8,461 9.031	500 700
		9.03 9.3	900 1010		9.429 9.691	900 1010	And the second second	9,549 9.819	900 1010
· · · .		9.4	1200		9.95	1200		10.111	1200
. 4	WF-103	9.4	0	C HE LOA	9.4	0	- 11- 44-	9.4	0
•	111,102	8.03	300	5 WF-104	8.072	300	6 WF 105	8.107	300
:		8.554 · 9.137	500 700		8.616 9.202	500 700		8.659 9.243	500 700
		9.664 9.937	900 1010		9.728 10	900 1010		9.769 10.04	900
		10.251	1200		10.319	1200		10.363	1010 1200
7	WF-106	9.4	0	0.05.107	9.4	0		9.4	0
	116-100	8.131	300	8 WF-107	8.165	300	9 WF-108	8.231	300
15		8.694 9.294	500 700		8.758 9.35	500 700		8.871 9.49	500 700
* .		9.834 10.112	900 1010		9.868 10.132	900 1010		10.032 10.308	900 1010
		10.453	1200		10.454	1200		10.664	1200
10	WF-109	9.4	. 0	11 WF-110	9.4	0	to be see	9.4	0
	203	8.223	300	11 111-110	8.256	300	12 WF 111	8.337	300
		8.833 9.409	500 700		8.885 9.471	500 700		9.048 9.72	500 700
		9.897 10.14	900 1010		9.966 10.211	900 1010		10.309 10.609	900 1010
		10.424	1200		10.507	1200		11.029	1200
13	WF-112	9.4	0	14 WF-113	9.4	0	15 165 114	9.4	0
		8.387	300	14 #1-115	8.43	300	15 WF-114	8.446	300
la de		9.135 9.837	500 700		9.222 9.968	500 700		9.251 10.009	500 700
1		10.455 10.771	900 1010		10.632 10.972	900 1010		10.685 11.032	900 1010
		11.222	1200		11.472	1200		11.544	1200
16	W r∙115	9.4	0	17 WF-116	9.4	0	18 WF-117	9.4	0
		8.463 9.281	300 500		8.473 9.294	300 500		8.45	300
	* 1	10.05 10.735	700 900		10.064	700		9.254 10.014	500 700
		11.088	1010		10.751 11.105	900 1010		10.693 11.044	900 1010
	O Million	11.61	1200		11.629	1200		11.565	1200
NO '	D-NAME	H	Q	NO DINAME	н	Q	NO D-NAME	н	Q
19	WF-118	9.4	0	20 WF-119	9.4	0	21 WF 120	9.4	0
		8.501 9.339	300 500		8.525 9.37	300 500		8.54 9.391	300 500
		10.128 10.838	700 900		10.163 10.877	700 900		10.188	700 900
		11.206 11.761	1010 1200		11.246 11.805	1010 1200		10.905 11.277	1010
		9.4	0			0		11.84	1200
22	WF-121	•		23 WF-122	9.4		24 WF-123	9.4	0
		8.515 9.363	300 500		8.555 9.397	300 500		8.549 9.383	300 500
		10.157 10.872	700 900		10.187 10.898	700 900		10.167 10.873	700 900
		11.242 11.801	1010 1200		11.267 11.826	1010 1200		11.239 11.792	1010 1200
		9.4	0		9.4	0		9.4	0
25	WF-124	8.553	300	26 WF-125	that is a first of		27 WF-126	a Maria	1.1
		9.38	500		8.563 9.356	300 500		8.589 9.382	300 500
		10.157 10.859	700 900		10.105 10.783	700 900		10.124 10.794	700 900
		11.222 11.772	1010 1200		11.134 11.662	1010 1200		11.141 11.662	1010 1200
		9.4	0		9.4	0		9.4	0
28	WF-127	8.642	300	29 WF-128			30 WF-129		
		9.473	500		8.701 9.556	300 500		8,76 9,615	300 500
		10.244 10.939	700 900		10.343 11.052	700 900		10,401 11.11	700 900
		11.3 11.845	1010 1200		11.42 11.98	1010 1200		11.477 12.038	1010 1200
	4.0				11.70			12.030	1200

	21	U# 100	9.4	0		9.4	0		9.4	0
	31	WF-130	8.73 9.559	300 500	32 WF-131	8.723	300	33 WF-132	8.793	300
			10.321 11.009	700 900	4.	9.542 10.293 10.969	500 700 900		9.702 10.529	500 700
			11.364 11.905	1010 1200		11.319 11.849	1010 1200		11.275 11.661 12.257	900 1010 1200
			9.4	0		9.4	0		9.4	0
	34	WF-133	8.804	300	35 WF-134	8.79	300	36 WF-135	8.876	300
			9.723 10.555	500 700		9.645 10.432	500 700		9.747 10.54	500 700
		1. 11.	11.304 11.692	900 1010		11.143 11.512	900 1010		11.254 11.623	900 1010
			12.291	1200		12.077	1200		12.191	1200
	37	WF-136	9.4 8.85	300	38 WF-137	9.4	0	39 WF-138	9.4	0
			9.749 10.565	300 500 700		8.955 9.888 10.726	300 500	•	9.096 10.003	300 500
			11.299 11.678	900 1010		11.479 11.868	700 900 1010		10.82 11.554	700 900
			12.262	1200		12.471	1200		11.933 12.522	1010 1200
	40	WF-139	9.4	0 1 44 1 44 12	41 WF-140	9.4	0	42 WF-141	9,4	0
	1.5		9.118 10.048	300 500		9.183 10.126	300 500		9.151 10.091	300 500
			10.888 11.644	700 900		10.974 11.738	700 900		10.935 11.6 96	700 900
			12.035 12.645	1010 1200		12.133 12.752	1010 1200		12.089 12.703	1010 1200
	43	WF-142	9.4	0	44 WF 143	9.4	0	45 WF-144	9.4	0
			9.17 10.066	300 500		9.18 10.023	300 500	40 Wr-144	9.191 10.025	300 500
			10.87 11.594	700 900		10.756 11.4	700 900		10.741 11.36	700 900
			11.967 12.546	1010 1200		11.727 12.221	1010 1200		11.671 12.134	1010 1200
			9.4	0		9.4	0		9.4	0
3	46	WF-145	9.30 6 10.283	300 500	47 WF-146	9.248	300	48 WF-147	9.366	300
	i yiri		11.148 11.923	700 900		10.14 10.92 11.608	500 700 900		10.368 11.25	500 700
			12.322 12.949	1010 1200		11.96 12.5	1010 1200		12.039 12.444 13.083	900 1010 1200
	31 July 10 July		9.4	0		9.4	0		9.4	0
	49	WF-148	9.403	300	50 WF-149	9.402	300	51 WF-150	9.451	300
			10.349 11.161	500 700		10.348 11.159	500 700		10.415 11.237	500 700
			11.873 12.234 12.793	900 1010 1200		11.869 12.229	900 1010		11.953 12.315	900 1010
			9.4	0		12.785 9.4	1200		12.876 9.4	1200 0
	52	WF-151	9.47	300	53 WF-152	9,499	300	54 WF-153	9.603	300
			10.51 11.415	500 700		10.544 11.452	500 700		10.666 11,586	500 700
			12.22 12.632	900 1010		12.258 12.671	900 1010		12.404 12.823	900 1010
			13.283	1200		13,323	1200		13.487	1200
	55	WF-154	9.4 9.637	300	56 WF-155	9.4	300	57 WF-156	9.4	0
			10.732 11.681	500 700		9.696 10.815 11.783	300 500 700		9.65 10.673 11.546	300 500 700
			12,525 12,957	900 1010		12.644 13.085	900 1010		12.314 12.704	900 1010
			13.544	1200		13.788	1200		13.317	1200
	58	WF-157	9.4	0	59 WF 158	9.4	0	60 WF-159	9.4	0
			9.731 10.816	300 500		9.826 10.968	300 500		9.79 10.889	300 500
			11.748 12.573	700 900	introduce (1965). Graffings for the	11.949 12.82	700 900		11.831 12.664	700 900
			12.994 13.663	1010 1200		13.265 13.975	1010 1200		13.089 13.764	1010 1200
	61	WF-160	9.4	0	62 WF-161	9.4	0	63 WF-162	9.4	0
			9.845 10.951	300 500	III -101	9.888 10.978	300 500	03 ML-105	9.975 11.076	300 500
			11,896 12,73	700 900		11.904 12.719	700 900		12.005 12.818	700 900
			13.155 13.83	1010 1200		13.133 13.788	1010 1200		13.23 13.881	1010 1200
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		9.4	0		9.4	0				
64	WF-163		· · · · · · · · · · · · · · · · · · ·	65 WF-164	3.4		66 WF-165	9.4	0	
		10.007 11.129	300 500		10,072	300		10.043	300	
		12,078	700		11.301 12.339	500 700		11.269 12.302	500 700	
		12.911	900		13.255	900	7	13.212	900	
		13.334 14.004	1010 1200		13.722 14.469	1010 1200		13.675	1010	
						1200		14.416	1200	
67	WF-166	9.4	0	68 WF-167	9.4	0	co ur ico	9.4	. 0	
	200	10.135	300	00 111-107	10.199	300	69 WF-168	10.277	300	
		11.299 12.295	500		11.367	500		11.504	500	
		13,177	700 900		12.364 13.247	700 900		12.55 13.477	700	
		13.626	1010		13.697	1010	**	13.95	900 1010	
		14.345	1200		14.416	1200		14.708	1200	
70	WE'LCO	9.4	0		9.4	0		9.4	0	
70	WF-169	10.259	300	71 WF-170	10.313	300	72 WF-171			
	14.0	11.421	500		11.507	500		10.367 11.571	300 500	
		12.413 13.288	700 900	1.	12.526	700		12.596	700	
		13.734	1010		13.426 13.884	900 1010		13.502 13.963	900 1010	
		14.446	1200		14.618	1200		14.701	1200	
	*	9.4	0		9.4	0		9.4	0	1.
73	WF-172	10.427	200	74 WF-173	Marie y		75 WF 174		4 2 4	3 1 1
		10.437 11.666	300 500		10.505 11.74	300 500		10.538 11.773	300	
		12.712	700	(1) (A) (A)	12.791	700		12.825	500 700	
		13.637 14.109	900 1010		13.721 14.195	900 1010	The second secon	13.755	900	
200	1.0	14.864	1200		14.955	1200		14.228 14.987	1010 1200	1.1
		9.4	. 0		9.4	0		9,4	0	
76	WF-175	10.627	200	77 WF-176	The second second	rise a Brigini	78 WF-177	<i>3.</i> 4		Maria 1
		11.919	300 500		10.616 11.888	300 500		10.628 11.873	300	
	The transfer	13.018	700		12.971	700		12.935	500 700	
		13.992 14.489	900 1010		13.931 14.42	900 1010	The first section of the section of	13.874	900	
	. 13. 1 	15.288	1200		15,206	1200	ALL STATES	14.353 15.121	1010 1200	1
		9.4	0		9.4	0				
79	WF-178	10.716	300	80 WF-179	10.707					7.7.
		11.995	500		10.737 12.037	300 500				
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55 58	WF-154 WF-157	11.65 11.79	693 709.6	56 WF-155 59 WF-158	11.66	672.7	57 WF-156	11.7	738	er George
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THE DETAILED DESIGN OF FLOOD CONTROL, URBAN DRAINAGE AND WATER RESOURCES DEVELOPMENT IN SEMARANG IN THE REPUBLIC OF INDONESIA

Fig.

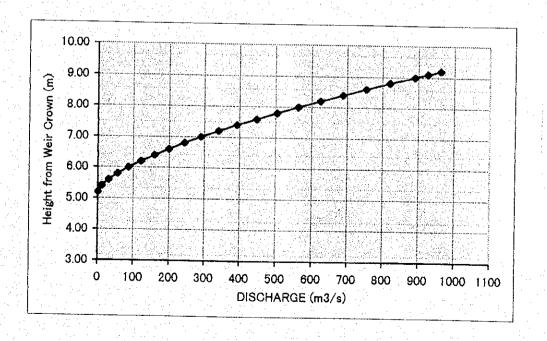
JAPAN INTERNATIONAL COOPERATION AGENCY

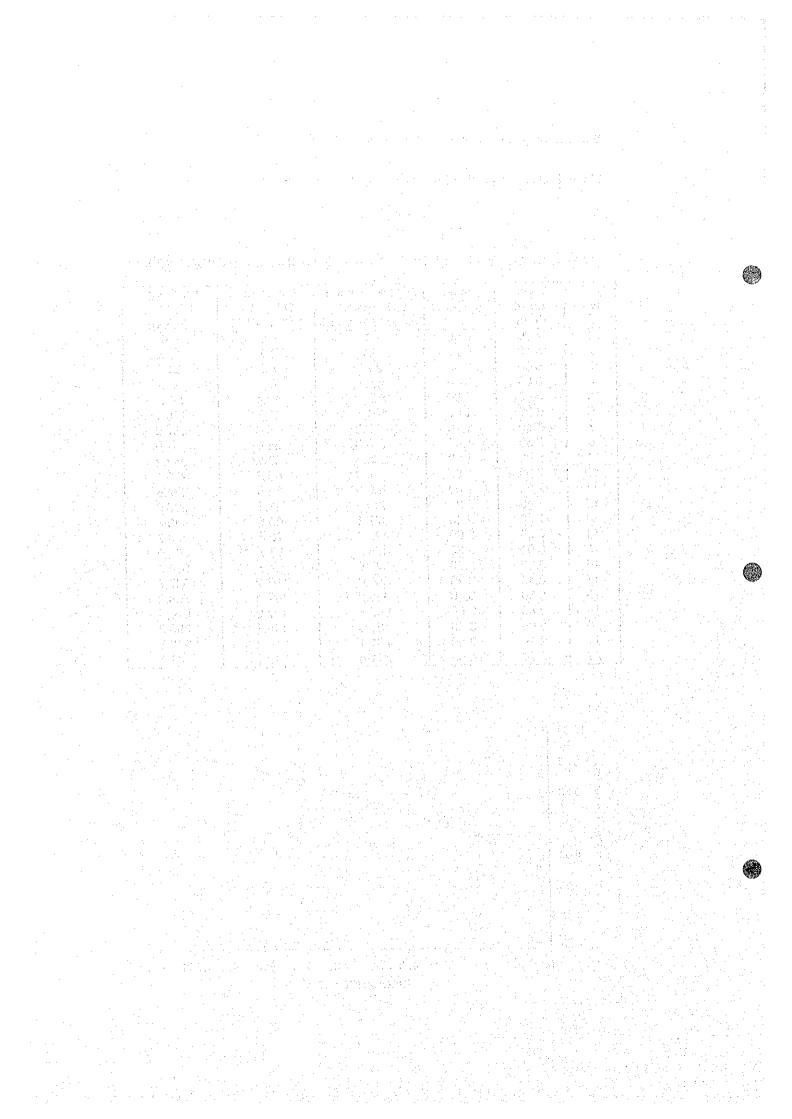
(3) Water Level and Discharge at Existing Simongan Weir

Flood discharge capacity of the weir was estimated as follows:

Table 3.1.1 WATER LEVEL-DISCHARGE RELATION AT SIMONGAN WEIR

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2.2 Design Riverbed and Channel Hydraulics

The design riverbed profiles of West Floodway and Garang River are determined based on the following considerations.

(1) West Floodway

Fig. 2.2.1 shows the change of riverbed profile between 1991 and 1997. Distinctive changes are observed as the riverbed aggradation in the river mouth area and bed degradation in the midstream and upstream. The riverbed of the river mouth is raised by about 1.0 m from the previous riverbed. However, this sedimentation does not extend to the offshore seabed as can be seen from Fig. 2.2.2.

The existing riverbed in the midstream and upstream is lowered by about 0.5 m. This is due to the cutting off the sediment flow by Simongan Weir. Remarkable riverbed degradation due to the local scouring is found as well in immediately downstream portions of three bridges. As to the riverbed gradient, a flat or rather gentle slope except the reverse bed slope of river mouth area, is formed.

Taking the said existing riverbed profile into account, the design riverbed is studied through the comparison of the following three (3) alternatives.

Alternative	Riverbed Elevation at River Mouth	Design Riverbed Gradient	Riverbed Elevation at Simongan Weir
Case-1	EL2.00	Level to 1/2,650	EL0.67
Case-2	EL2.50	Level to 1/2,650	EL1.17
Case-3	EL3.00	Level to 1/2,650	EL1.67

As for the design elevation of floodplain, the height of 3.0 to 3.5 m from the design riverbed is employed to avoid frequent flood inundation of floodplain as shown in Fig. 2.2.4. With this design height, the floodplain will not submerged under the flood of 2-year return period or more for the whole channel stretches except lowermost portion near the river mouth. This proposed ground elevation is almost the same height as that of existing floodplain.

Based on the above riverbed profiles and channel cross sections (schematically shown in Fig. 2.2.3), the flood water level profiles for the above alternatives are estimated as shown in Fig. 2.2.4. The freeboard between the underside of each bridge

girder and the high water level is also estimated as follows:

Alternative	Name of Bridge	Underside elevation of Bridge Girder	Water Level	Freeboard
	North Ring Road, Br.	EL. 2.52 m	EL. 1.41 m	1.11
Case-1A	Railway Bridge	EL. 3.50 m	EL. 3.32 m	0.18
	National Road Bridge	EL. 4.14 m	EL. 3.65 m	0.49
	North Ring Road, Br.	EL. 2.52 m	EL. 1,10 m	1.42
Case-2A	Railway Bridge	EL. 3.50 m	EL. 2.98 m	0.52
	National Road Bridge	EL. 4.14 m	EL. 3.33 m	0.81
Case-3A	North Ring Road, Br.	EL. 2.52 m	EL. 0.85 m	1.67
	Railway Bridge	EL. 3.50 m	EL. 2.64 m	0.86
	National Road Bridge	EL.4.14 m	EL. 2.98 m	1.16

Case-1A:

Of the three alternatives the highest water level is obtained. It is almost the same elevation as the existing floodwall crest in the river stretches upstream from North Ring Road Bridge. Further, the freeboard between the water level and girders of Railway Bridge and National Road Bridge are rather small of 18 cm and 49 cm, respectively. As the results, the raising work of floodwall with big height and raising of two bridges are necessary. The impact on the existing river structures by channel excavation is negligible.

Case-2A:

The water level lower than the existing floodwall crest is obtained for the whole river stretch. The freeboard between water level and said bridge girders are 52 cm and 81 cm. The channel excavation is moderate with little impact on river structures.

Case-3A:

The lowest water level is obtained. However, channel excavation will affect most existing river structures and bridge foundations to a great deal. Further, the channel maintenance at river mouth will be difficult due to the heavy future sedimentation.

Judging from these advantages/disadvantages of each alternatives, Case-2A is preferred as the optimum river bed profile. As the results, the optimum longitudinal channel profile proposed is given as shown in Fig. 2.2.5.

(2) Garang Rive (Simongan Weir to Confluence with Kreo River)

Comparing the current riverbed profile in 1997 with that in 1991, there is no big changes in overall riverbed profile except the locally scoured portions found in riverbed profile in 1997 as shown in Fig. 2.2.1. This is caused by an excessive sand mining activity. Therefore, the design riverbed gradient of 1/1,250, which was adopted as the stable riverbed slope in the F/S, is still applicable.

There are two (2) alternatives conceived as to what riverbed elevation is employed for the bottom of new Simongan Weir. The design riverbed profiles of each alternatives are summarized in the table below.

Alternative	Riverbed Elevation at Simongan Weir	Design Riverbed Gradient	Head of Hydraulic Drop *3
Case-1B	EL. +1.50 *1	1/1,250	1.5 m
Case-2B	EL. +3.00 *2	1/1,250	<u>-</u>

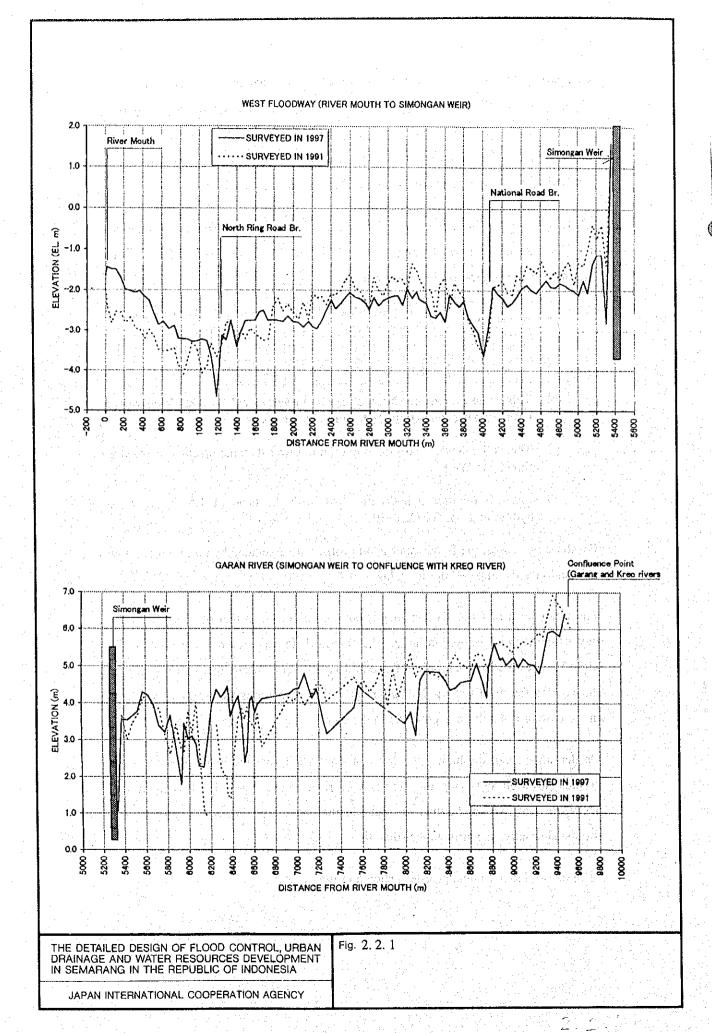
- *1 This is the average elevation of existing riverbed at Simongan Weir whose riverbed has been extremely lowered by local scouring.
- *2 This is the elevation of the point 0.6 m lower than the original riverbed at Simongan Weir.
- *3 Case-IB requires a hydraulic drop with the head of 1.5 m, while no hydraulic drops for Case-2B.

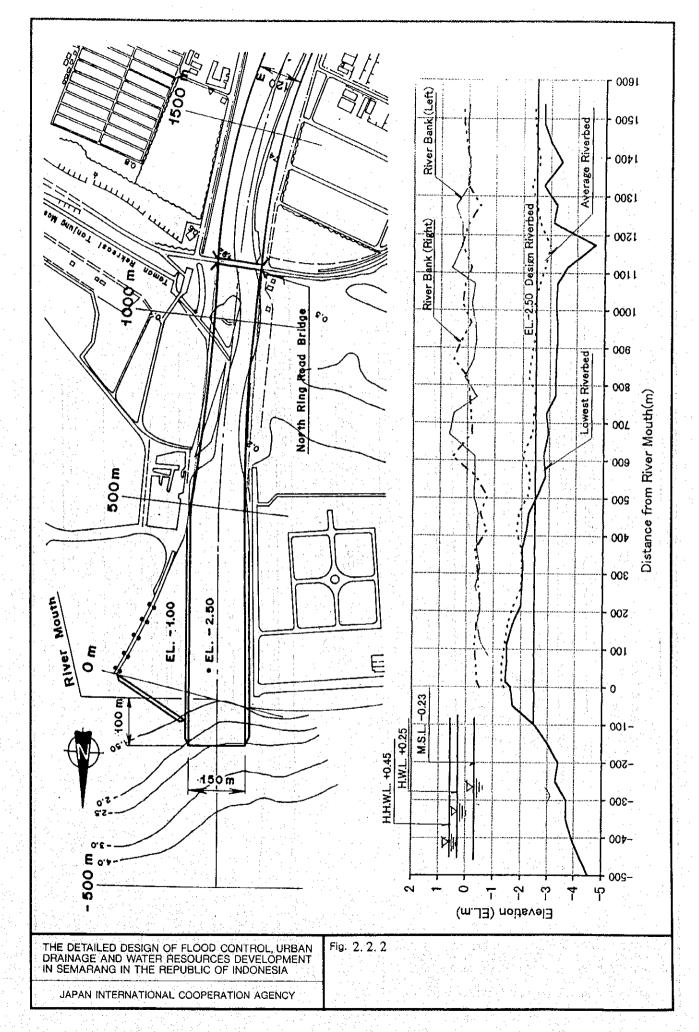
For these two cases, the flood water level profiles are estimated by non-uniform flow calculation and compared in Fig. 2.2.6.

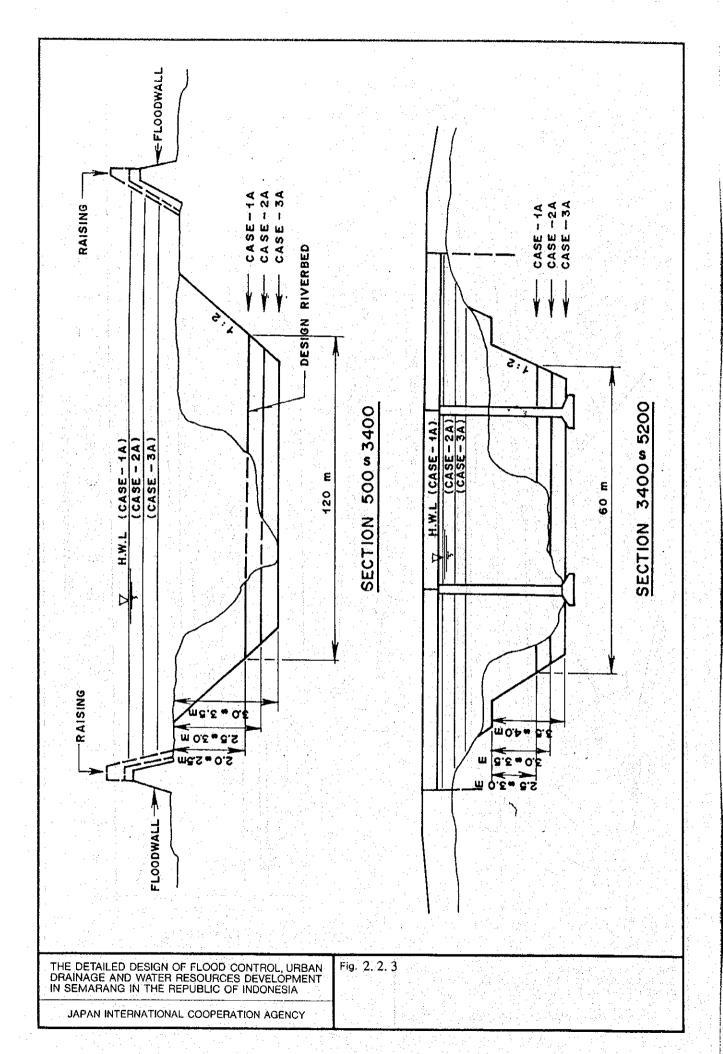
The water level of Case-2B becomes about 2 m higher than that of Case-1B in the downstream stretches. Accordingly, the floodwall in this area can not confine the high flood level within a required freeboard level. This means that more raising of the existing floodwalls along the main river and its tributaries are required, resulting in increase of flood damage potential in the area.

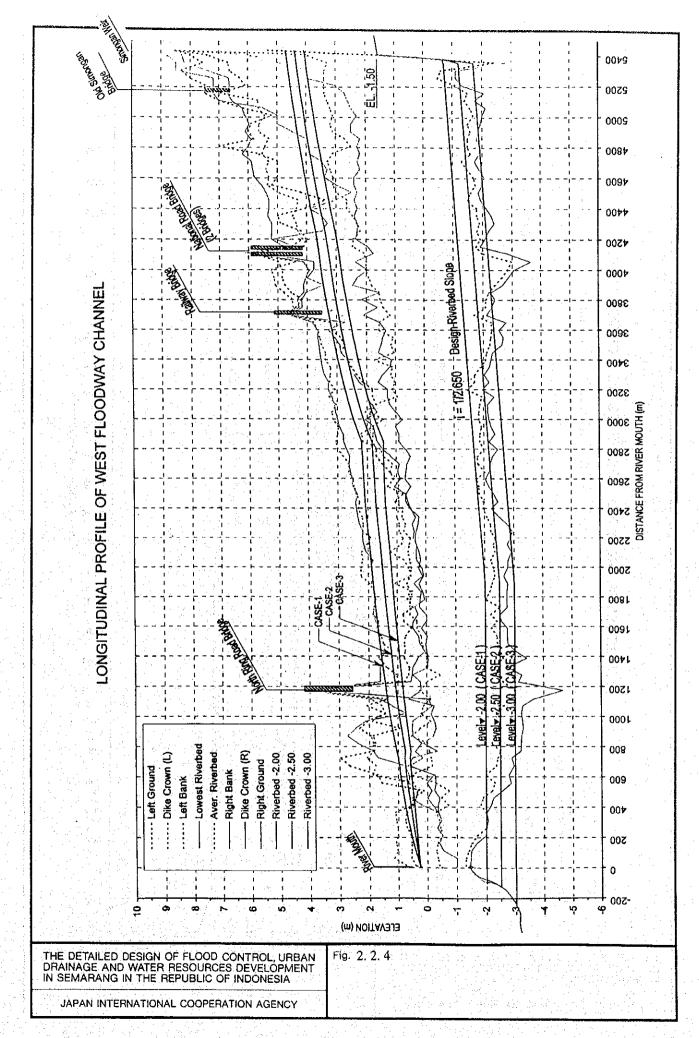
On the other hand, the high water level of Case-1B is lowered below the average ground elevation satisfying the premises of river improvement for Garang River. Therefore, Case-1B can be the most suitable alternative, even though the project cost for this alternative is a little higher than the.

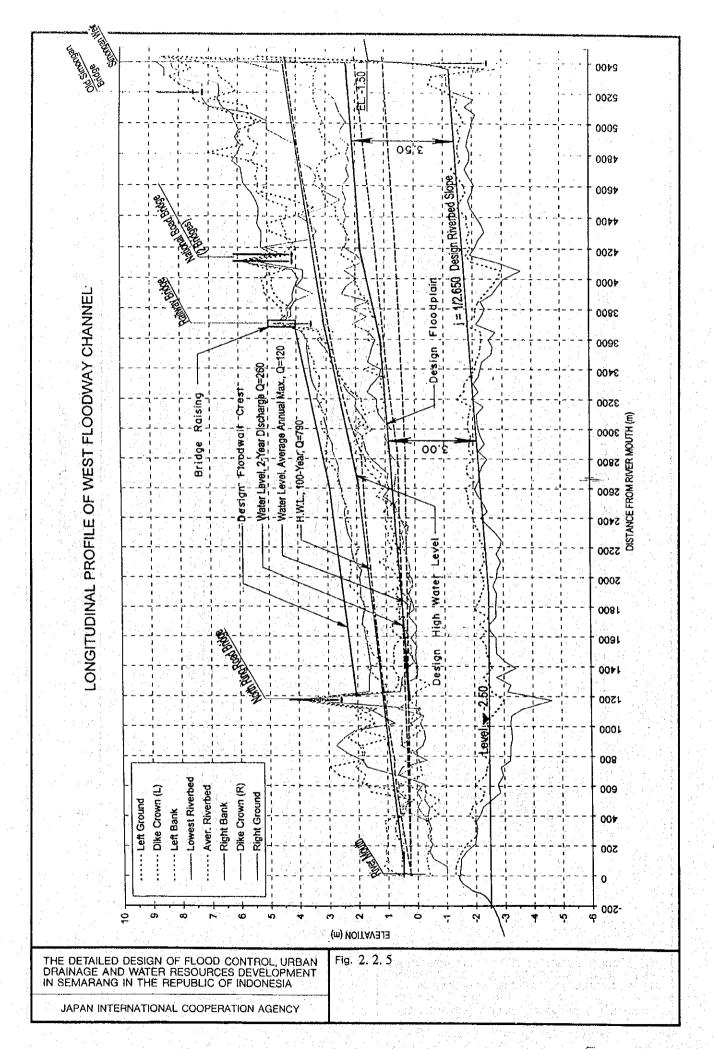
The proposed longitudinal profile is shown in Fig. 2.2.7.

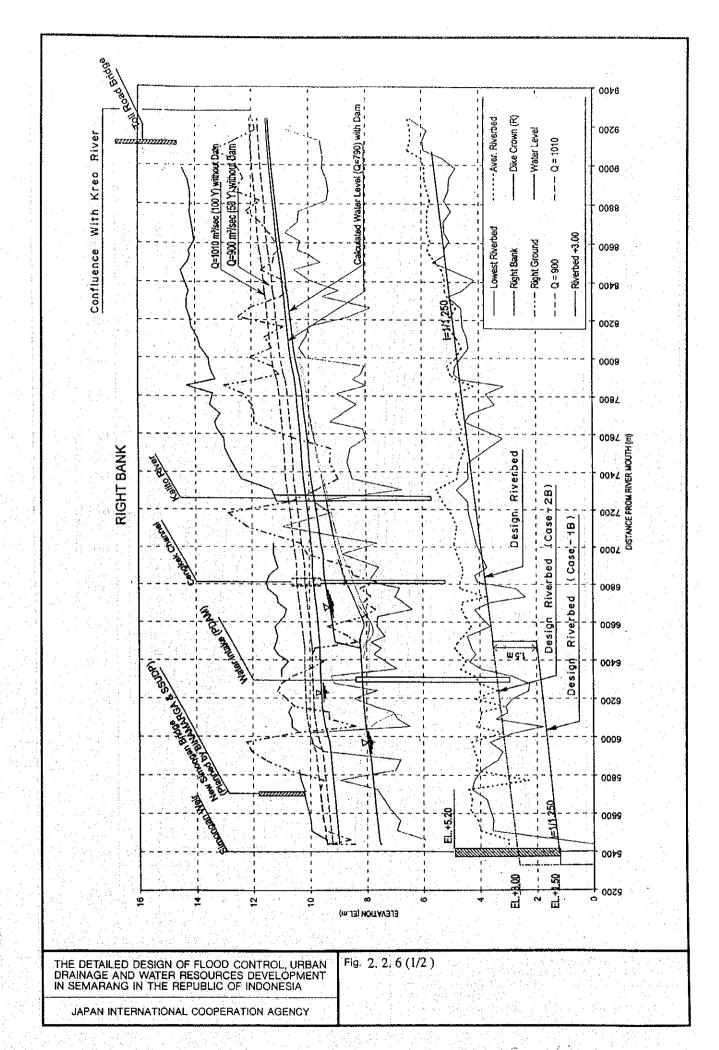


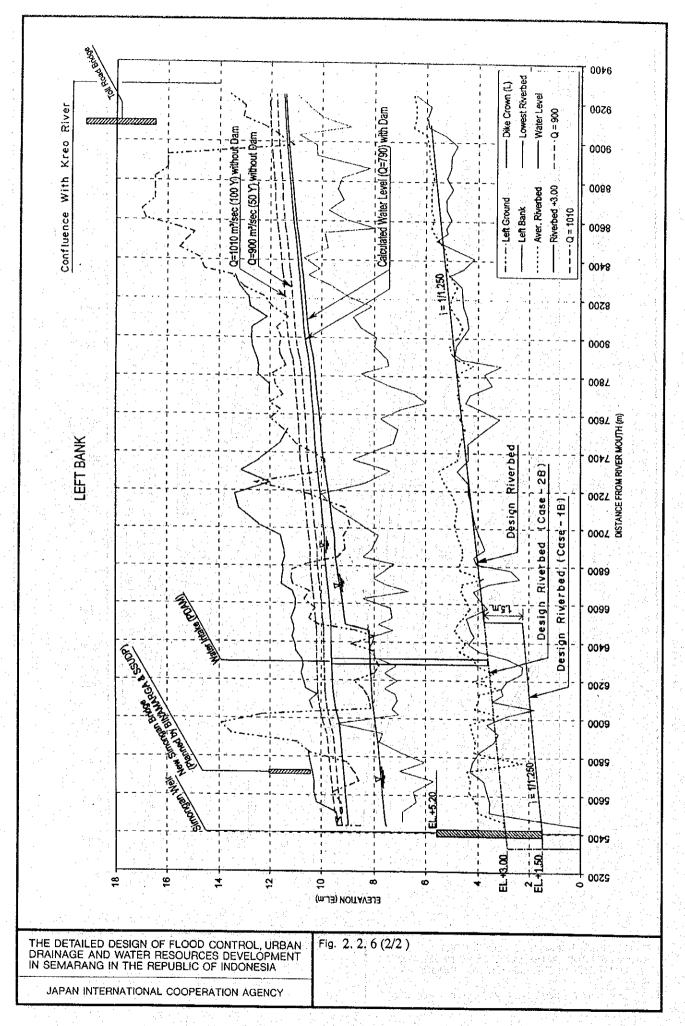






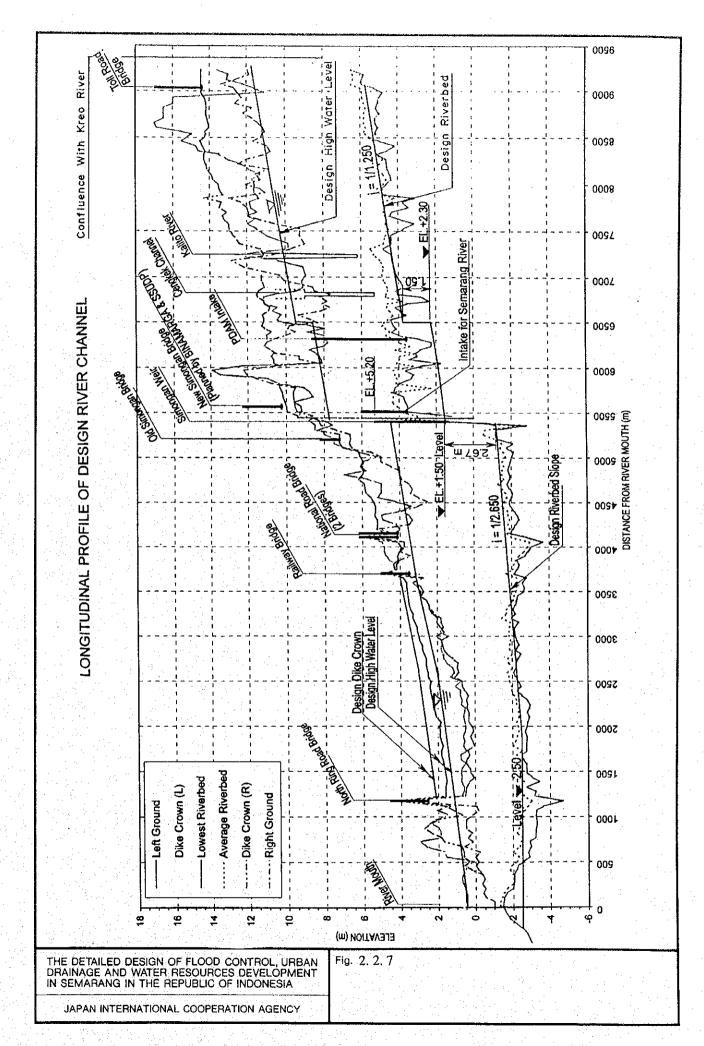


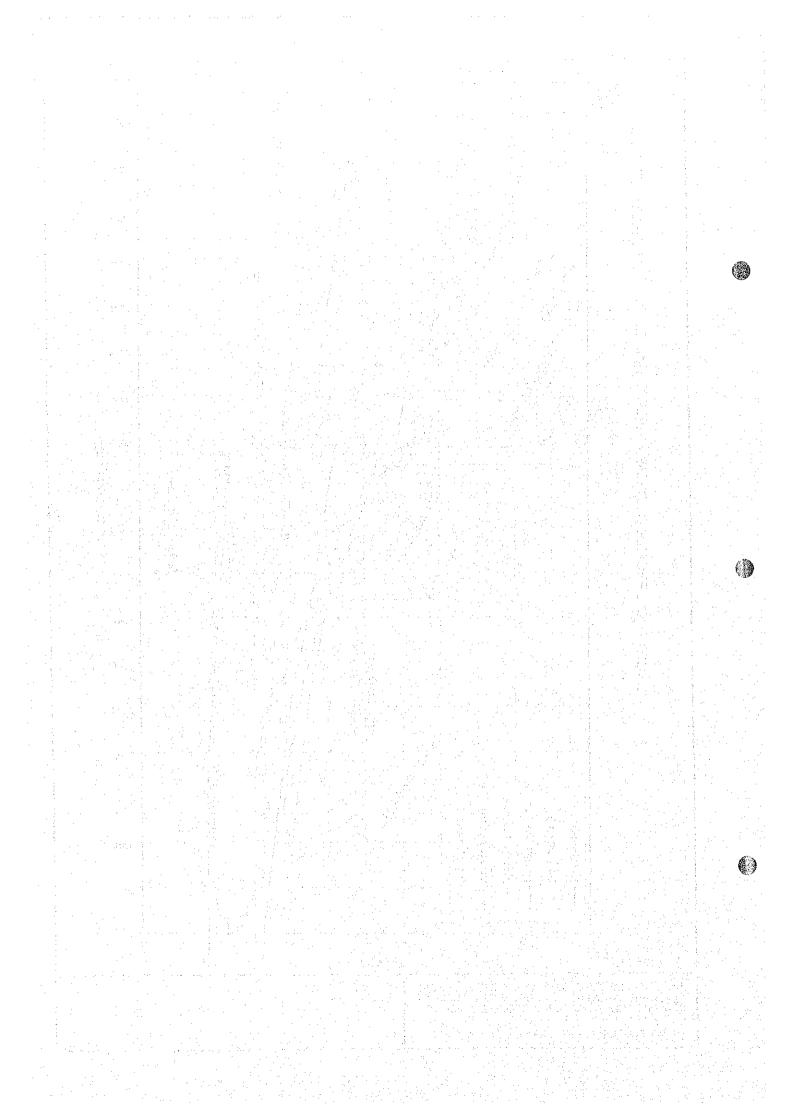




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2.3 River Hydraulics on Design Channel

Water level profile was calculated for the design river channel as mentioned below.

2.3.1 Conditions on Calculation

(1) Uniform Flow Calculation

In principle, the design high water level profile is set based on the uniform flow calculation. This method is commonly applied for the river stretch of which water level is not affected by tide. As a uniform flow calculation method, the following Manning's Formula is used.

$$Q = \frac{1}{n} \times I^{1/2} \times R^{2/3} \times A$$

where:

Q: design discharge (m³/s)

n: Manning's roughness coefficient

I : gradient of river bed

R: hydraulic radius (m)

A: flow area (m²)

(2) Non Uniform Flow Calculation

For the river channel where water level is influenced by the downstream water level, non-uniform flow method is employed to compute the water surface profile. The calculation equation is presented as follows:

$$\left\{H_2 + \frac{D_2}{2g} \left(\frac{Q_2}{A_2}\right)^2\right\} - \left\{H_1 + \frac{D_1}{2g} \left(\frac{Q_1}{A_1}\right)^2\right\} = h_e$$

$$h_{e} = \frac{1}{2} \left\{ \frac{N_{1}^{2}}{A_{1}^{2}} \frac{Q_{1}^{2}}{R_{1}^{4/3}} + \frac{N_{2}^{2}}{A_{2}^{2}} \frac{Q_{2}^{2}}{R_{2}^{4/3}} \right\} \times \Delta X$$

Using Iida's Formula, coefficients; D,N and R are expressed below.

$$D = \alpha \cdot \frac{A^2 \int_0^B \frac{h^3}{n^3} d\xi}{\left(\int_0^B \frac{h^{5/3}}{n} d\xi\right)^3} , \quad N = \frac{\int_0^B h^{5/3} d\xi}{\int_0^B \frac{h^{5/3}}{n} d\xi} , \quad R = \left(\frac{1}{A} \int_0^B h^{5/3}\right)^{3/2}$$

where,

H: elevation of water level (m)

he: difference in water level between two sections

g: acceleration of gravity (9.8 m/s²)

Q: discharge (m³/s) A: flow area (m²)

 ΔX : distance between two cross sections (m)

D: coefficient for correction

N: equivalent roughness coefficient for the whole cross sections

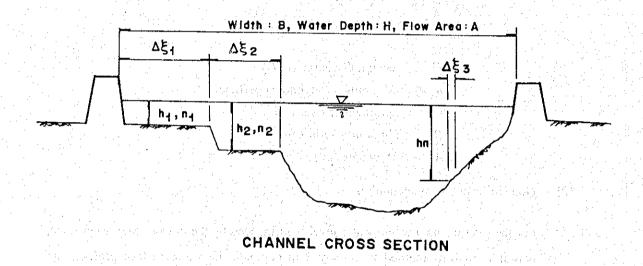
R: equivalent hydraulic depth for the whole cross sections

Manning's roughness coefficient for each cross section

a: energy coefficient (1.0)

B: river width subject to computation.

Suffix denotes the number of cross sections from downstream to upstream.



(3) Roughness Coefficient

For the uniform and non-uniform flow calculation, the following Manning's roughness coefficient are used based on the recommended figures in "Flood Control Manual".

Low Water Channel (excavated)	0.030
Low Water Channel (existing)	0.033
Flood Plain (excavated) *1	0.035
Flood Plain (existing)	0.040
Channel with Lining (narrow channel)	0.025

^{*1} The flood plain here is referred to the bottom portion of high water channel.

(4) Design Tidal Level at River Mouth

The design tidal levels at the river mouth are determined based on the tidal data observed at Semarang Harbor. Since the tidal data observed in the past have been affected by land subsidence in the low lying area, the most recent data of April 1997 to August 1997, which are considered less affected, are used for the tidal analysis.

Kind of Water Level	Elevation (TTG)
Highest High Water Level (HHWL)	EL. +0.45 m
Mean High Water Level (MHWL)	EL. +0.25 m
Mean Sea Level (MSL)	EL0.23 m
Mean Low Water Level (MLWL)	EL070 m
Lowest Low Water Level (LLWL)	EL090 m

For the non-uniform flow calculation in the event of flooding, the mean high water level of EL, +0.250 m is used as the starting water level at the river mouth.

Table MAXIMUM AND MINIMUM VALUE OF TIDAL LEVEL IN THE LAST FIVE MONTHS

		<i>.</i>	٧.																													Average	1	188.2	94.0
. 1997	Min.	118	124	122	120	123	121	I	120	114	117	105	107	66	91	104	102	108	. 116.	112	116	115	114	119	111	122	116	117	112	116	113	119	114	3	94
August	Max.	174	178	182	180	176	166	162	158	170	166	178	174	180	170	173	102	164	160	153	149	142	152	159	165	166	164	171	167	169	172	170	165	182	•
. 1997	Min.	114	106	112	105	110	117	116	124	113	115	108	123	108	122	118	115	112	108	108	109	102	111	112	112	115	112	120	116	1	1	ı	113	•	102
July .	Max.	162	162	164	156	162	169	178	182	174	176	169	176	167	172	168	164	158	158	155	170	165	168	169	170	170	177	170	185		1	1	168	185	1
1997	Min.	106	109	112	110	116	126	129	121	120	116	118	112	111	113	112	124	120	120	119	117	116	118	117	124	120	119	113	112	119	ı	ı	117	1	106
Jun .	Max.	189	184	174	168	172	177	180	180	181	184	183	177	184	182	182	177	174	178	173	172	174	175	188	187	190	188	192	179	176	1	-	180	192	•
1997	Min.	100	94	96	100	107	110	121	117	123	128	120	116	103	100	100	100	100	96	105	104	110	111	115	110	120	116	122	108	108	104	104	109		94
May. 1997	Max.	184	182	188	176	166	160	162	152	160	166	171	168	178	179	180	175	169	165	164	153	157	153	160	167	173	174	178	182	187	186	194	171	194	t
1997	Min.	118	105	66	95	105	96	109	114	115	116	112	110	107	82	77	102	94	91	94	111	122	122	132	125	126	126	129	123	118	102		109	•	77
April. 1997	Max.	176	174	170	176	170	174	164	160	135	143	141	154	166	164	168	167	160	156	160	161	159	159	154	154	152	164	169	179	188	179	•	163	188	
Months	Date	-	2	က်	4	5	9	2	80	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Average	Max Value	Min. Value

Note:

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		Max.	176	174	170	176	170	174	164	160	148	144	141	154	166	164	168	167	160	156	160	161	159	159	3	2 2	70.	40	169	179	188	179		164	188
`.		Aver	146	141	132	136	136	136	135	139	129	132	128	130	133	129	124	135	129	127	128	137	140	144	34:	444	147	641	146	147	153	140		137	
		23	118	105	111	130	132	150	52	<u>₹</u>	130	28	112	110	107	8	106	110	13	13	126	8	ਲ	142	3	3 8	9 5	75	132	23	118	102		\$14(3)	
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		20	154	150	157	172	169	174	164	160	135	2	121	126	132	118		152	148	146	154	160	152	150	2	2 5	2	74		146	148	144			
	. 4	19	168	162	167	176	170	171	162	158	134	138	126	136	44	33	160	162	155	154	159	161	156	156	<u>ک</u>	2 3	3	20	156	159	163	164			
		18	172	169	170	176	169	166	157	153	130	139	133	145	154	148	168	166	160	156	160	160	159	+	-	40.	747	200	163	168	174	173			-
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	*	16	176	172	161	164	154	148	5	141	128	144	141	154	166	164	165	164	156	152	152	152	153	159	24 :	6 5	24.	20	169	179	188	177			
	997 *	15	171	163	148	150	142	139	131	136	127	2	141	152	164	157	155	157	149	44	4	146	147	157	2	2	<u></u>	Š	88	176	186	171			
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	*	12	140	130	118	121	120	126	125	138	130	1	136	138	140	-	122	132	128	124	123	8	38	142	74.	2	5	200	15	152	167	142			
	ATA	1	138	130	116	121	123	132	130	138	131	136	130	132	133	2	115	132	126	125	123	33	138	4	4 2	2 5	3	40	22	152	158	134			
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		8	144	140	130	135	140	134	130	136	127	124	127	127	122	140	116	7	훒	132	127	33	142			2 3	40	44	140	141	151	134			
		7	146	144	135	138	139	129	128	131	123	120	124	128	133	2	114	140	134	127	124	133	136	143	2	2			138	138	150	136			
		9	146	146	136	25	133	120	133	126	118	118	124	126	132	138	112	138	128	120	118	128	132	138	5	4	4	22	136	36	149	137	- 22		
		2	146	146	133	124	126	112	114	118	115	116	126	123	129	133	109	133	120	11	110	122	130	133	200	2 3	2 2 7	45	134	135	146	137			
		4	146	145	124	114	117	104	109	114	116	118	126	121	127	128	104	122	110	104	104	116	127	130	152	3	45	971	132	133	146	133			
		9	141	139	116	10	97	109	116	122	118	126	118	124	122	8	112	102	97	97	112	124	126	<u>5</u>	2	3	ر ا	22	132	133	146	133			
		2	132	127	105	86	105	96	114	122	129	120	129	115	116	112	98	104	96	91	94	111	122	122	2	2 3	871	8	129	131	134	121			
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		0	121	117	සි	88	116	116	137	142	148	125	128	110	109	1	77	102	88	3	101	118	132	127	3	17,	132	9	129	130	133	114			
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	Difference	84	88	92	76	59	50	41	35	37	38	<u>بن</u>	52	75	79	80	75	69	69	99	52	64	84	45	57	29	28	56	74	79	82	90	83		
Unit: cm	Min.	100	94	96	190	107	110	121	117	123	128	120	116	103	160	901	100	100	96	105	101	108	111	115	110	120	116	122	108	108	10,4	104	108		76
	Max.	184	182	188	176	166	160	162	152	160	196	171	158	178	179	180	175	169	165	164	153	157	159	160	167	176	174	178	182	187	186	194	172	194	
	Aver.	140	140	145	141	140	140	144	136	141	145	147	141	145	143	146	144	139	137	140	138	140	139	139	145	148	147	150	149	148	148	155	143		
:	23	100	113	129	139	141	146	138.	130	132	132	120	116	103	100	105	102	104	110	90	116	116	122	115	127	120	130	122	108	108	104	113			
- 1	22	114	130	147	152	150	152	141	133	136	137	127	123	106	5	112	113	113	122	116	123	123	126	118	130	124	133	124	111	117	114	128			4
	21	134	149	163	163	158	156	144	136	142	145	136	133	118	114	125	127	128	136	127	133	131	130	127	137	2	40	129	119	130	132	145	-		
	20	154	165	176	172	<u>7</u>	129	148	140	46	152	148	143	158	132	1. 44	143	146	146	140	140	138	138	134	143	137	145	138	132	146	156	163			
	19	168	176	184	176	166	160	150	142	150	157	158	154	170	149	158	159	154	156	153	146	144	143	137	148	144	152	151	150	161	170	178			
	18	178	182	188	176	164	157	150	145	154	162	166	163	175	162	169	170	161	162	162	151	149	144	141	152	152	160	166	170	174	180	186	-		
	17	184	182	184	172	160	154	152	148	156	164	170	168	178	172	176	175	165	165	163	152	151	147	144	156	159	167	174	180	183	186	192			
	16	184	175	175	165	154	151	154	150	159	166	171	168	176	179	179	175	169	164	164	152	152	150	146	160	165	172	178	182	186	186	194			
** //	15	175	164	166	157	142	148	159	152	160	165	170	165	173	174	180	173	164	156	9	151	155	151	149	164	168	174	178	182	187	184	8			
1997	14	165	153	155	149	144	145	159	152	158	162	167	161	168	171	176	166	159	152	155	151	155	150	152	164	02	174	178	180	20	178	182			
** MAY	13	150	142	146	142	141	142	162	151	156	158	163	154	<u>1</u> 8	196	99	8	151	146	5	150	150	150	152	164	171	173	177	111	176	169	173		ia, Legi	
	12	138	135	143	138	140	144	162	149	152	153	158	149	159	157	156	154	146	142	145	147	150	151	153	167	174	17	173	171		162	167			
DATA	11	133	133	140	136	143	146	160	146	148	149	154	146	155	152	152	120	144	142	42	145	149	152	156	167	176	169	168			156	161			
TIDAL	10	133	135	142	138	146	148	148	143	144	145	150	143	154	150	154	150	144	139	45	149	152	159	160	167	173	163	164	162	55	153	160			
F	6	134	138	146	140	148	145	152	139	140	142	148	141	152	149	152	152	146	141	152	150	156	153	160	164	169	157	159	157	148	150	158			
	8	139	142	150	142	146	140	146	134	135	139	145	140	150	152	152	154	149	147	156	153	156	152	158	158	164	152	154		146	148	32			
	7	142	144	149	143	140	133	138	128	132	136	142	140	147	152	152	154	150	147	159	150	157	149	154	151	156	144	147	147	144	144	154			
	. 9	142	143	143	135	131	126	131	124	129	134	140	138	142	150	150	156	150	143	154	145	148	143	146	140	147	135	140	64	₹	144	15			
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	4	132	123	120	116	114	113	121	117	124	130	133	126	128	139	142	139	132	123	34	128	131	128	128	125	128	119	130	133	중	138	Ξ	- 4		
	3	120	112	110	103	108	110	122	117	123	128	131	123	122	133	128	126	118	112	112	117	123	120	122	118	122	116	130		- 1	127	136	14		
	2	109	103	102	100	107	112	125	120	124	128	130	120	114	123	117	112	106	3	114	110	114	115	116	112	121	116	132			118	22			
	1	102	96	96	102	113	120	131	125	126	128	130	116	112	111	105	107	100	86	107	101	108	112	115	110	12	119	131	126	117	112	110			
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· · · · · · · · · · · · · · · · · · ·	Cart	Min.	106	108	112	110	116	126	129	121	120	116	118	112	111	113	112	124	120	120	113	116	116	118	117	120	119	113	112	119		117		106
		Max.	189	184	174	169	172	177	180	180	182	184	183	177	184	182	182	177	174	178	173	172	174	9/1	188	190	188	192	179	176		180	192	
\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		Aver.	155	155	155	148	150	154	5	152	152	153	152	147	153	153	155	156	153	155	150	149	149	149	3 5	155	151	159	147	154		152		
		23	119	126	130	134	139	138	33	2	120	120	118	114	116	117	130	128	126	126	133	125	8	124	131	2 2	127	113	138					
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	TA **	12	164	159	163	162	169	176	8	111	179	179	175	164	170	88	168	169	129	2	161	168	Ξ.	2 5	188	28	176	179	162	153				
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	TIDAL	10	160	161	170	69	172	175	173	2	168	170	59	158	165	166	166	168	165	170	168	172	7	9	180	1/2	162	174	152	156				
	₣	6	160	166	174	169	22	170	167	99	162	167	<u>.</u>	35	20	1	164	168	130	175	172	172	172	<u> </u>	173	2	155	172	152	162				
		8	163	170	174	168	164	164	162		156	162	158	152	- +			170	174	178	173	120	164	104	165	157	151	168	149	161				
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		9	163	161	162	150	145	148	147	147	145	147	<u>‡</u>	141	152	2 5	152	161	164	168	162	156	147	94.	150	4	137	165	141	162		-		:
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in section of the State of the		*************************************	141	138	134	125	126	132	134	130	130	130	137	130	136	137	132	141	141	144	143	136	128	131	128	132	126	143	133	150				
		3	129	125	122	117	119	128	129	125	126	124	128	124	128	128	124	130	130	134	132	128	121	3	120	3 8	125	139	126	140				:
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		DATE	1	2	3	4	2	9	7	œ	6	0	=	12	13	4-	15	16	17	8	19	20	2	27	23	25	26	27	28	29	30	Average	Max	Min.
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TIDAL DATA ** JULY, AUGUST 1997 **

5	9	Septembe	r		August			July	
	Max	Min	Differ.	Max	Min	Differ.	Max	Min	Differ.
1	163	128		174	118	56	162	114	48
2	172	122		178	124	54	162	106	56
3	163	116		182	122	60	164	112	52
4	174	122		180	120	60	156	105	51
5				176	123	53	162	110	52
6				166	121	45	169	117	52
7				162	•	-	178	116	62
8				158	120	38	182	124	58
9				170	114	56	174	113	61
10				166	117	49	176	115	61
11	2.1 1			178	105	73	169	108	61
12				174	107	67	176	123	53
13				180	99	81	167	108	59
14				170	91	79	172	122	50
15				173	104	69	168	118	50
16				102	102	0	164	115	49
17				164	108	56	158	112	46
18				160	116	44	158	108	50
19	, , , , ,			153	112	41	155	108	47
20				149	116	33	170	109	61
21			10 10 11 11 11 11 11 11 11 11 11 11 11 1	142	115	27	165	102	63
22				152	114	38	168	111	57
23				159	119	40	169	112	57
24				165	111	54	170	112	58
25				166	122	44	170	115	55
26				164	116	48	177	112	65
27				171	117	54	170	120	50
28				167	112	55	185	116	69
29				169	116	53		1	
30				172	113	59			
31				170	119	51		_	-
32				162	114	48		3 (1) 1	. -
Aver.				165	114	51	168	113	55
Max.				182			185		
Min.					91			102	

2.3.2 West Floodway

(1) Water Level Profile

Since West Floodway is a tidal river of which riverbed slope is almost flat in the lower reaches, the steady uniform flow calculation is not applicable. Then, the non-uniform flow calculation presented in "Hydraulic Criteria" is applied to estimate the water level and the flow velocity of river channel.

Using the river cross-sections and longitudinal profile of the channel determined in the basic design, non-uniform flow calculation was conducted. When the design flood discharge of 790 m³/s flows in the river channel, the water level and the flow velocity are calculated as shown in the following calculation sheets. The water level profile calculated and flow velocity are illustrated as well.

KUKAN SU =13

ALPHA = 10

Q0 = 790.00 M3/S

HO = .250 M

ZO = -2.500 M

JCO = 0

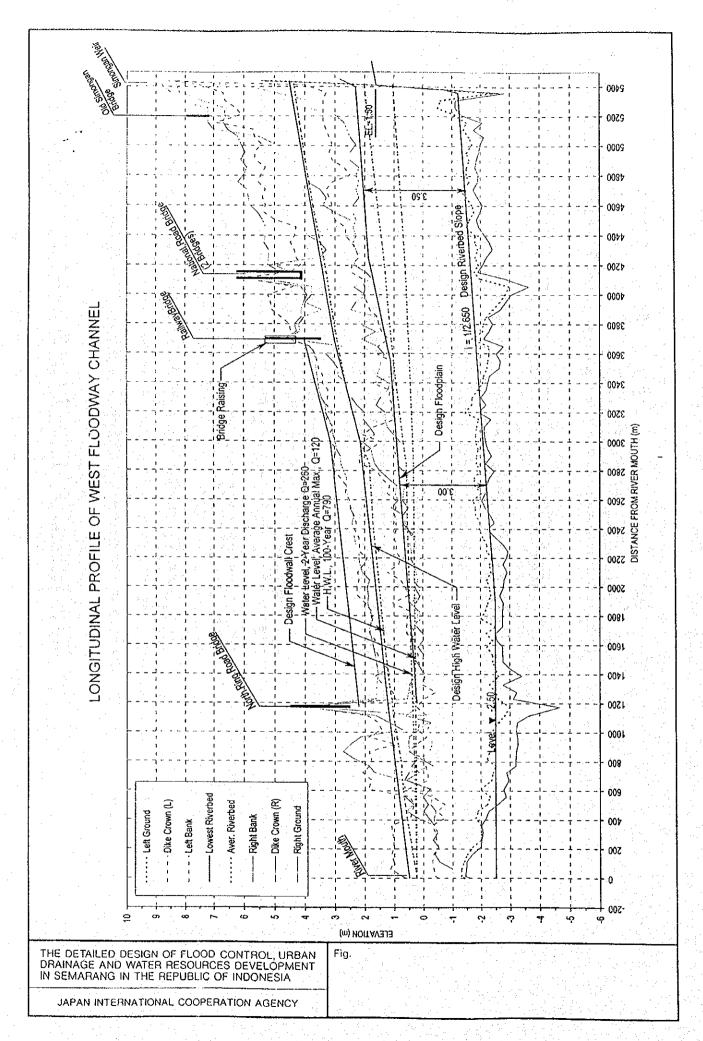
KEY ≈ 0

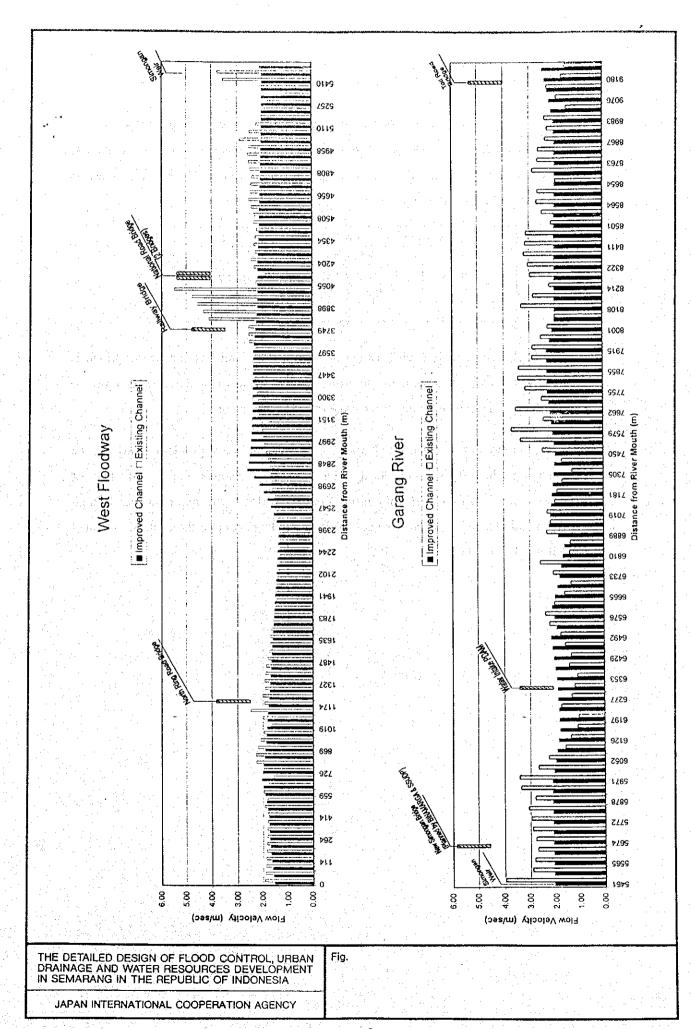
EY ≈ 0 IPT = 0

KUKAN	DAT	A
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DANMEN NO.	BUNKATSU SUU	DANMEN KEIJYO	LOSS TYPE	SODO KEISU	KUKAN KYORI(M)	KASYO KOOBAI(1/I)	RAKUSA (M)	RYUNYU RYO(M3/S)	Marie Zakaj		
LUCO MEO	•	9 1	•	0.0004	4127	000000				14 14 14 14 14 14 14 14 14 14 14 14 14 1	
1 WF-9 -WF0 2 WF0 - WF5	9 5	2 1	0	0.0324	413.7	999999	0	. 0	and the state of		
3 WF5 - WF14	9	2 1 2 1	0	0.031	258.96	999999	0	0	1, 154 (Entro)		•
			0	0.0307	442.71	999999	0	0			1000
4 WF14 -WF21	7	2 1	. 0	0.0306	371.14	999999	0	0			
5 WF21 - WF29	8	2 1	. 0	0.0306	401.9	999999	0	0			
6 WF29 - WF39	10	2 1	. 0	0,0308	509.15	2650	0	0			•
7 WF39 - WF47	8	2 1	0	0.0317	399.23	2650	0	0		445.4	
8 WF47 -WF59	12	2 1	. 0	0.0317	600.23	2650	. 0	0	*	4	•
9 WF59 -WF63	: 4	2 1	0	0.031	200.01	2650	0	0			
10 WF63 -WF69	6	2 1	. 0	0.0308	300.9	2650	0	0			
11 WF69 -WF75	6	2 1	0	0.0305	305.77	2650	0	0	일 사람들	Adam Commence	
12 WF75 -WF95	20	2 1	U	0.0309	1006.84	2650	0	. 0			
13 WF95 - WF99	4	2 1	0	0.0309	199.6	2650	0	0	A SERVICE	e galacije.	. 4.
			100								4.6
NO.	н	Δ	R	(, y .	N		DX	FROUD	1 C	7	цт
no.	to the state of	. 1				Q	VA.	TROOD	i iE	3.73 Z	ΗZ
WF-9 -WF0	.250	427.63	2.635	1.847	0.0324	790	0	0.3621	9.85E-04	2.5	2.75
+ 45.97	.300	435.73	2.681	1.813	0.0324	790	45.97	0.3523	9.27E-04	2.5	2.73
+ 91.93	,347	443.26	2.724	1.782	0.0324	790	45.97	0.3435	8.77E-04	2.5	2.847
+ 137.90	.392	450.48	2.765	1.754	0.0324	790	45.97	0.3355	8.32E-04	-2.5	2.892
+ 183.87	.434	457.26	2.803	1.728	0.0324	790	45.97	0.3282	7.93E-04	2.5	2.934
+ 229.83	474	463.69	2.84	1.704	0.0324	790	45.97	0.3216	7.58E-04	2.5	2.973
+ 275.80	.512	470.74	2.864	1.678	0.0324	790	45.97	0.375	7.27E-04	.2.5	3.012
+ 321.77	.550	478.97	2.864	1.649	0.0324	790	45.97	0.3566	7.02E-04	-2.5	3.012
+ 367.73	.586	485.83	2.864	1.626	0.0324	790	45.97	0.3402	6.83E-04	-2.5	3.085
+ 413.70	.620	491.6	2.864	1.607	0.0324	790	45.97	0.3254	6.67E-04	2.5	3.119
WFO - WF5	.620	491.64	2.864	1.607	0.031	790	. 0	0.3253	6.10E-04	2.5	3.119
+ 51.79	.654	497.78	2.864	1.587	0.031	790	51.79	0.3162	5.95E-04	2.5	3.154
+ 103.58	.688*	503.48	2.864	1.569	0.031	790	51.79	0.3077	5.82E-04	2.499	3.187
+ 155.38	.720	508.74	2.864	1.553	0.031	790	51.79	0.2998	5.70E-04	2.499	3.219
+ 207.17	.752	513.59	2.864	1.538	0.031	790	51.79	0.2925	5.59E-04	2.499	3.251
+ 258.96	.782	518.01	2.883	1.525	0.031	790	51.79	0.2857	5.45E-04	2.499	3.282
WF5 - WF14	.692	390.21	2.827	2.025	0.0307	790	0	0.3912	9.67E-04	2.499	3.191
+ 49.19	.746	397.86	2.827	1.986	0.0307	790	49.19	0.3795	9.30E-04	2.499	3.246
+ 98.38	.798	405.17	2.827	1.95	0.0307	790	49.19	0.3688	8.97E-04	2.499	3.298
+ 147.57	.848	411.96	2.875	1.918	0.0307	790	49.19	0.3593	8.48E-04	2.499	3.347
+ 196.76	894	418.3	2,926	1.889	0.0307	790	49.19	0.3507	8.03E-04	2.499	3.393
+ 245.95	.938	424.21	2.975	1.862	0.0307	790	49.19	0.3429	7.64E-04	2.499	3.437
+ 295.14	.979*	429.75	3.022	1.838	0.0307	790	49.19	0.3359	7.29E-04	-2.499	3.478
+ 344.33	1.018	434.97	3.067	1.816	0.0307	790	49.19	0.3294	6.98E-04	-2.499	3.517
+ 393.52	1.055	439.9	3.11	1.796	0.0307	790	49.19	0,3234	6.70E-04	2.499	3.554
+ 442.71	1.091	444.56	3.152	1.777	0.0307	790	49.19	0.3178	6.44E-04	-2.499	3.59
WF14 WF21	1.091	444.59	3,152	1.777	0.0306	790	0	0.3178	6.40E-04	2,499	3.59
+ 53.02	1.128	449.91	3.179	1.756	0.0306	790	53.02	0,3127	6.18E-04	2.499	3.627
+ 106.04	1.164*	455.09	3,206	1.736	0.0306	790	53.02	0.3078	5.97E-04	2.499	3.663
+ 159.06	1.198	460.12	3.231	1.717	0.0306	790	53.02	0.3032	5.78E-04	2.499	3.697
+ 212.08	1.232	465.01	3.256	1.699	0.0306	790	53.02	0.2989	5.60E-04	2,499	3.73
+ 265.10	1.264*	469.76	3.279	1.682	0.0306	790	53.02	0.2948	5.44E.04	-2.499	3.763
+ 318.12	1.295	474.4	3.302	1.665	0.0306	790	53.02	0.2909	5.28E-04	2.499	3.794
+ 371.14	1.326*	478.93	3.324	1.65	0.0306	790	53.02	0.2872	5.14E-04	2.499	3.824
WF21 WF29	1.326	478.95	3.324	1.649	0.0306	790	0	0.2872	5.14E-04	2.499	3.824
+ 50.24	1.354	483.8		1.633	0.0306	790	50.24	0.284	5.02E-04	-2.498	3.852
+ 100.47	1.381	488.63	3.339	1.617	0.0306	790	50.24	0.2809	4.91E-04	2.498	3.88
+ 150.71	1.408*	493.43	3.346	1.601	0.0306	790	50.24	0.2778	4.80E-04	-2.498	3.907
+ 200.95	1.435	498.19	3.353	1.586	0.0306	790	50.24	0.2749	4.69E-04	2.498	3.933
+ 251.19	1.460	502.91	3.359	1.571	0.0306	790	50.24	0.2721	4.59E-04	2.498	3.959
+ 301.42	1.486	507.61	3,366	1.556	0.0306	790	50.24	0.2693	4.50E-04	2.498	3.984
+ 351.66	1.510	512.27	3.372	1.542	0.0306	790	50.24	0.2666	4.40E-04	2.498	4.008
+ 401.90	1.534	516.91	3.378	1.528	0.0306	790	50.24	0.264		2.498	4.032
WF29 -WF39	1.534	516.92	3.378		0.0308	790	0	0.264		-2.498	4.032
+ 50.92	1.559	521.87	3.323	1.514	0.0308	790	50.92	0.2637		-2.479	4.038
+ 101.83	1.583	526.87	3.271	1.499	0.0308	790	50.92	0.2633		-2.46	4.043
+ 152.74	1.608	531.91	3.222	1.485	0.0308	790	50.92	0.2628		-2.44	4.048
+ 203.66	1.632	536.99	3.175	1.471	0.0308	790	50.92	0.2622		-2.421	4.054
+ 254.58	1.657	542.11	3.131	1.457	0.0308	790	50.92	0.2616		2.402	4.059
+ 305.49	1.681*	547.25	3.089	1.444	0.0308	790	50.92	0.261		2.383	4.064
+ 356.41	1.706	552.43	3.049	1.43	0.0308	790	50.92	0.2602		2.364	4.069
+ 407.32	1.730	557.63	3.011	1.417	0.0308	790	50.92	0.2595		2.344	4.074
+ 458.24	1.754	562.86	2.974	1.404	0.0308	790	50.92			2.325	4.079
+ 509.15	1.778*	568.1	2.939	1.391	0.0308	790	50.92	0.2578		-2.306	4.084
WF39 WF47	1.778	568,12	2.94	1.391	0.0317	790				2.306	4.084
+ 49.90	1.7901	533.91	2.924	1.48	0.0317	790		0.275		2.287	4.077
+ 99.81	1.802	500.04	2.908	1.58	0.0317	790		0.2943		2.268	4.071
+ 149.71	1.816	466,45	2.892		0.0317	790		0.3162		2.249	4.065
+ 199.62	1.8301	433.13	2.875	1.824	0.0317	790		0.3414		2.231	4.061
+ 249.52	1.845	399.9	2.856		0.0317	790				2.212	4.057
+ 299.42	1.861	366.89	2.836		0.0317	790		0.4054		2.193	4.054
+ 349.33	1.876	333.9	2.812		0.0317	790				2.174	4.051
+ 399.23	1.890	300.76	2.783	2.627	0.0317	790	49.9	0.4985	1.77E-03	2.155	4.045
			30 S (1)			1.00		100	grand and the second	and the second	1.15

WF47 -WF59	1.890	300.77	2.783	2.627	0.0317		790	٥	0.4005	1 775 00	0.155	
+ 50.02	1.990	307.52	2.88	2.569	0.0317		790	0 50.02	0.4985	1,77E-03	2.155	4.045
+ 100.04	2.079*	312.95	2.968	2.524	0.0317		790	50.02	0.4791 0.4636	1.62E-03	2.136	4.126
+ 150.06	2.161*	317.36	3.05	2,489	0.0317		790	50.02	0.4509	1.50E-03	2.118	4.197
+ 200.08	2.237	320,96	3.127	2.461	0.0317		790	50.02	0.4402	1.41E-03 1.33E-03	2.099	4.26
+ 250,10	2.307	323.88	3.2	2.439	0.0317		790	50.02	0.4311	1.33E 03	2.08	4.316
+ 300.11	2.374	326.24	3.271	2.422	0.0317		790	50.02	0.4232	1.27E-03 1.21E 03	2.061	4.368
+ 350.13	2.436	328.12	3,339	2,408	0.0317		790	50.02	0.4252	1.17E 03	-2.042	4.416
+ 400.15	2.496	329.58	3.405	2.397	0.0317		790	50.02	0.4104	1.17E-03	∙2.023 •2.004	4.46
+ 450.17	2.554*	330.66	3.47	2.389	0.0317		790	50.02	0.4051	1.09E-03	-1.985	4.501
+ 500.19	2.609°	331.42	3,533	2.384	0.0317		790	50.02	0.4004	1.06E-03	-1.967	4,539
+ 550.21	2.662	331.88	3,596	2.38	0.0317	1.	790	50.02	0.3962	1.03E 03	-1.948	4.576
+ 600.23	2.714	332.08	3.659	2.379	0.0317		790	50.02	0.3925	1.03E-03	·1.946 ·1.929	4.61
WF59 -WF63	2.714	332.08	3.659	2,379	0.031		790	0	0.3925	9.65€.04	-1.929	4.642
+ 50.00	2,763	333.12	3.706	2.372	0.031		790	50	0.3887	9.43E-04	1.929	4.642
+ 100.00	2.811	333.98	3.751	2,365	0.031		790	. 50	0.3852	9.22E-04	-1.891	4.673
+ 150.01	2.858	334.68	3.797	2.36	0.031		790	50	0.382	9.04E-04	1.872	4.702
+ 200.01	2.904	335.24	3.841	2.357	0.031		790	50	0.3791	8.87E-04	·1.853	4.73
WF63 -WF69	2.904	335.24	3.841	2.357	0.0308		790	- 0	0.3791	8.76E-04	1.853	4.757
+ 50.15	2.949*	336.28	3.887	2.349	0.0308	· .	790	50.15	0.3754	8.57E-04	1.834	4.757 4.783
+ 100.30	2.993*	337.27	3.93	2.342	0.0308		790	50.15	0.3718	8.39E-04	·1.816	4.763
+ 150.45	3.036*	338.22	3.971	2.336	0.0308	٠.	790	50.15	0.3683	8.23E-04	-1.797	4.833
+ 200.60	3.079	339.13	4.007	2.329	0.0308		790	50.15	0.365	8.09E-04	-1.778	4.857
+ 250.75	3.121	340.03	4.038	2.323	0.0308		790	50.15	0.3617	7.97E 04	1.759	4.879
+ 300.90	3.162*	340.91	4.059	2.317	0.0308		790	50.15	0.3586	7.87E-04	-1.74	4.902
WF69 WF75	3.162	340.91	4.059	2.317	0.0305	:	790	0	0.3586	7.71E-04	1.74	4.902
+ 50.96	3.198*	338.52	4.007	2.334	0.0305	11.11	790	50.96	0.3648	7.96E-04	1.721	4.918
+ 101.92	3.235*	336.06	3.947	2.351	0.0305	· · · · · .	790	50.96	0.3712	8.24E-04	1.701	4.936
+ 152.88	3.274	333.57	3.883	2.368	0.0305		790	50.96	0.3777	8.55E-04	1.682	4.955
+ 203.85	3.314*	331.04	3.817	2.386	0.0305	4	790	50.96	0.3843	8.88E-04	-1.663	4.976
+ 254.81	3.355	328.51	3.751	2.405	0.0305	100	790	50.96	0.391	9.23E-04	1.644	4.999
+ 305.77	3.399	325.98	3.685	2.423	0.0305		790	50.96	0.3978	9.60E-04	1.624	5.023
WF75 WF95	3.399*	325.98	3.685	2.423	0.0309	: 1	790	0	0.3978	9.85E-04	-1.624	5.023
+ 50.34	3.453*	329.04	3.713	2.401	0.0309		790	50.34	0.3926	9.57E-04	1.605	5.058
+ 100.68	3.506	331.94	3.739	2.38	0.0309		790	50.34	0.3878	9.32E 04	1.586	5.092
+ 151.03	3.557*	334.72	3.764	2.36	0.0309	74 T	790	50.34	0.3833	9.08€-04	1.567	5.124
+ 201.37 + 251.71	3.606*	337.37	3.788	2.342	0.0309	100	790	50.34	0.379	8.87E-04	1.548	5.155
+ 302.05	3.655° 3.702°	339.91	3.811	2.324	0.0309	- 24	790	50.34	0.375	8.66E-04	1.529	5.184
+ 352.39	3.748	342,34 344,68	3.833	2.308	0.0309	1.5	790	50.34	0.3713	8.48E-04	-1.51	5.212
+ 402.74	3.793	346.93	3.854 3.874	2.292	0.0309		790	50.34	0.3677	8.30E-04	1.491	5.239
+ 453.08	3.836*	349.09	3.894	2.277 2.263	0.0309	- 11.7	790	50.34	0.3644	8.14E-04	1.472	5.265
+ 503.42	3.879	351.18	3.912	2.25	0.0309 0.0309	. i	790	50.34	0.3612	7.98E-04	1.453	5.29
+ 553.76	3.921	353.19	3.93	2.237	0.0309	Sec. 2	790 790	50.34	0.3582	7.84E-04	1.434	5.314
+ 604.10	3.963	355.13	3.947	2.225	0.0309	110	790	50.34	0.3553	7.70E 04	1.415	5.337
+ 654,45	4.003	357.01	3.964	2.213	0.0309	41.14	790	50.34	0.3526	7.57E-04	1.396	5.359
+ 704.79	4.043	358.83	3.98	2.202	0.0309	. 11.12	790	50.34 50.34	0.35	7.45E-04	1,377	5.38
+ 755.13	4.082	360.59	3.996	2.191	0.0309	f North	790	50.34 50.34	0.3475 0.3451	7.34E-04 7.23E-04	-1.358	5.401
+ 805.47	4.120	362.29	4.011	2.181	0.0309	200	790	50.34	0.3451		1.339	5.421
+ 855.81	4.158	363.95	4.025	2.171	0.0309		790	50.34	0.3426	7.13E 04 7.03E 04	-1.32 -1.301	5.441
+ 906.16	4.195	365.55	4.039	2.161	0.0309	1.0	790	50.34	0.3385	6.93E-04		5.46
+ 956.50	4.232	367.1	4.053	2.152	0.0309	4000	790	50.34	0.3365	6.84E-04	1.282 1.263	5.478
+ 1,006.84	4.268	368.62	4.066	2.143	0.0309	走 经	790	50.34	0.3346	6.76E-04	1.244	5.495 5.513
WF95 WF99	4.268*	368.62	4.066	2.143	0.0309		790	0.54	0.3346	6.76E-04	1.244	5.513
+ 49.90	4.304*	370.07	4.079	2.135	0.0309	2 / 1	790	49.9	0.3327	6.68E-04	1.226	5.529
+ 99.80	4.338	371.49	4.091	2.127	0.0309		790	49,9	0.331	6.60E-04	1.207	5.545
+ 149.70	4.373*	372.86	4.103	2.119	0.0309		790	49.9	0.3293	6.53E-04	1.188	5.561
+ 199.60	4.407*	374.2	4.115	2.111	0.0309	. 11.	790	49.9	0.3276	6.45E-04	1.169	5.576
		The state of				, 417°	47.7	5. J. M.	. 441.		R1202	9.570
						200			4			
		- 1			医连续性	54. J.		100	,		4.35.45	
			e detail						`			





(2) Water Level Rise by Bridge Pier

In connection with the bridge raising and construction of new piers, the piers of Railway Bridge may induce a rise in water level in the upstream channel. So, the rise of water level is estimated by using D'Aubuisson's formula. The result is shown in the table below together with the calculation conditions.

Calcul	ation Condition	Result
Q	790 m ³ /s	
H ₁ B	4.8 m, 3.0 m x 2	$\Delta h = 0.11 \text{ m}$
b_1 , b_2	80.0 m, 74.0 m	
C^2	0.81	

The D.H.W.L in the stretch between Railway Bridge and National Road Bridge is determined with a tolerance of more than 0.11 m against calculated water level, so the D.H.W.L can confine the water stage raised by bridge piers.

Also, the piers of National Road Bridge may cause the same problem. However, the upstream channel from the bridge has a bigger channel depth than that of downstream. This channel can confine the design flood with more than 1.5 m high freeboard. Therefore, even if some rise in water level occurs, the upstream channel will not be affected.

(3) Pumping Station near North Ring Road Bridge and Water Level of West Floodway

To solve the drainage problem in Tanah Mas residential area which lies along the right bank of West Floodway (Drainage area: 127 ha), Semarang City formulated drainage system improvement including pump drainage into West Floodway. This pumping station is located at the lower end of Bulu River near the North Ring Road Bridge as shown in the following drawing. (Currently, Bulu River is connected to West Floodway by a box culvert laid under North Ring Road) According to the drainage plan, a pumping station with the total pump capacity of 3.0 m³/s has been proposed as follows:

	Number and Capacity of Pump	Pump Operation		
1	1.4 m ³ /s 2 units Sub total 2.8 m ³ /s	Rainy season only		
2	0.1 m ³ /s 2 units Sub total 0.2 m ³ /s	Dry and Rainy seasons		
3	Total 3.0 m ³ /s			

To know the hydraulic impact on the flood flow in West Floodway, the Study Team estimated a rise in water level by non-uniform flow calculation. The calculation results are presented in the following calculation sheets. The estimated rise is as small as 5 mm which is negligible. Therefore, the Study Team judged that there is no hydraulic impact on the main river flow. The results are presented in the following calculation sheets.

** INPUT DATA **

PUMPING STAION Q=3, 0 t/m3

* BAISIC DATA *

KUKAN-SU = 17 ALPHA = 1.00 Q0 = 793.00 M3/S H0 = .250 M Z0 = -2.500 M

JC0 = 0 KEY = 0 IPT = 0

* KUKAN DATA *

DA	NMEN NO.	BUNKATSU SUU	DANMEN KE I JYO	LOSS TYPE	SODO Keisu	KUKAN Kyori (M)	KASYO KOOBAT (1/1)	RAKUSA (M)	RYUNYU RYO (M3/S)
1 WF	9 -WF0	9	2 1	. 0	. 0300	413, 70	999999, 00	.000	00
2 WF) - WF4	. 4	2 1	0	0310	208, 96	999999.00	. 000	00
3 WF	1 - WF14	10	2 1	0	. 0307	492.71	999999.00	000	. 00
4 WF	4 -WF21	7	2 1	0	. 0306	371.14	999999.00	.000	.00
5 WF	21 -WF29	8	$\bar{2}$ i	0	0306	401.90	999999.00	000	00
6 WF	9 -WF39	10	2 1	0	.0311	509.15	2650.00	000	őő
7 WF:	39 -WF42	3	2 1	0	. 0317	149. 23	2650, 00	000	.00
8 WF	12 -WF53	11	2 1	0	0317	550.00	2650.00	.000	ŎŎ
9 WF:	3 -WF59	6	2 1	Õ	0317	300, 00	2650, 00	000	.00
10 WF:	59 -WF63	4	2 1	Ō	. 0312	200, 01	2650, 00	. 000	őő
11 WF	3 WF69	6	2 1	0	0310	300, 90	2650, 00	. 000	. 00
12 WF	9 -WF72	3	2 1	0	. 0307	155, 77	2650, 00	.000	.00
13 WF	72 -WF73	1	2 1	0 .	0305	50.00	2650, 00	000	.00
14 WF	73 -WF75	2	2 1	0	0305	100.00	2650.00	000	ŏŏ
15 WF	75 -WF76	1	2 1	0	. 0300	50.00	2650.00	000	00
16 WF	76 -WF95	. 19	2 1	0	0310	956. 84	2650.00	000	. ŏŏ
17 WF	5 -WF99	4	2 1	0	. 0310	199. 60	2650, 00	000	őő
-						a agricultural for	The second second		The fighter of

* KEIJYO DATA *

KUKAN	KEIJYO	80 (R)	M 1	N1	B 1	B2	HP (B3)	M2	N2
1 1	2 1	150, 000	2. 000	2.000	50,000	40, 000	2.000	2. 000	. 001
:		150,000	2.000	2.000	10.000	10, 000	2, 200	2.000	2.000
. 2	2 1	150,000	2.000	2,000	10,000	10,000	2. 200	2,000	2, 000
. '	- to 1	115, 000	2.000	2,000	9,000	10,000	2, 500	2.000	2. 000
3	2 1	115,000	2,000	2.000	9,000	10,000	2, 500	2,000	2.000
1.00		115, 000	2,000	2,000	9,000	5, 000	2, 700	2. 000	2.000
4	2 1	115.000	2.000	2,000	9, 000	5. 000	2.700	2,000	2.000
100	144 00 00 00	115, 000	2.000	2,000	8.000	6,000	3.000	2.000	2.000
. 5	2 1	115, 000	2.000	2,000	8,000	6.000	3,000	2.000	2. 000
	44 1534	115, 000	2.000	2.000	9,000	25. 000	3.000	2.000	2.000
. 6	2 1	115, 000	2. 000	2,000	9.000	25. 000	3.000	2.000	2.000
٠		115, 000	2.000	2,000	10,000	48, 000	3,000	2.000	2.000
7	2 1	115, 000	2.000	2,000	10.000	48. 000	3, 000	2.000	2,000
	100	115. 000	2,000	2,000	6.000	18,000	3.000	2,000	2.000
8	2 1	115, 000	2,000	2,000	6.000	18.000	3, 000	2,000	2.000
	ile e	58, 000	2.000	2. 000	10.000	13.000	3. 200	2,000	2. 000
9	2 1	58, 000	2.000	2,000	12,000	15.000	3, 200	2,000	2.000
	1.0	58, 000	2.000	2, 000	7. 000	8.000	3, 300	2,000	2.000
10	2 1	58, 000	2.000	2.000	7, 000	8, 000	3.300	2,000	2.000
		58, 000	2.000	2,000	7. 000	4, 000	3, 400	2,000	2, 000
11	2 1	58, 000	2,000	2,000	7, 000	4.000	3.400	2,000	2.000
1.2		58, 000	2,000	2,000	10,000	7. 000	3.500	2,000	2.000
12	2 1	58, 000	2,000	2,000	10,000	7, 000	3.500	2,000	2,000
	4.5	50, 000	1.000	1, 000	4. 000	4, 000	3. 500	. 500	500
13	2 1	50, 000	1,000	1.000	4, 000	4, 000	3, 500	. 500	. 500
		50,000	1.000	1.000	4. 000	4.000	3, 500	. 500	. 500
14	2 1	50, 000	1.000	1, 000	4, 000	4, 000	3, 500	. 500	500
		50,000	2.000	2, 000	4, 000	5,000	3. 500	2,000	2.000
15	2 1	50, 000	2.000	2,000	4,000	5,000	3. 500	2,000	2.000
100	100	50.000	2.000	2,000	8, 000	6.000	3.500	2,000	2,000
16	2 · 1	50, 000	2.000	2.000	8.000	6,000	3. 500	2.000	2.000
		50, 000	2.000	2,000	8, 000	6.000	3. 500	2.000	2.000
. 17	. 2 1	50, 000	2.000	2,000	8, 000	6, 000	3, 500	2,000	2.000
	•	50.000	2.000	2. 000	8, 000	8, 000	3, 500	2.000	2.000

* LOSS DATA *

KUKAN LOSS TYPE FL1 FL2

*** WEST FLOODWAY , STEADY NON-UNIFORM FLOW (LEVEL, -2. 5, 1/2650) b=50 wf75-up DX FROUD ΙĒ 1. 967 2. 041 2. 114 2. 189 2. 265 2. 344 494. 56 497. 55 499. 47 500. 57 -2. 500 -2. 500 -2. 500 -2. 500 -2. 500 -2. 500 2. 750 2. 793 2. 834 2. 872 2. 908 2. 942 WF-9 -WF0 250 1.603 . 0300 . 9386E~03 793.00 3638 + 45.97 793, 00 793, 00 793, 00 793, 00 793, 00 . 293 45. 97 45. 97 45. 97 45. 97 . 8831E-03 . 8359E-03 . 7947E-03 . 7581E-03 1. 594 1. 588 1. 584 . 0300 . 0300 . 0300 3551 91.93 . 334 3475 3408 3348 + 137.90 . 372 + 183, 87 + 229, 83 408 442 500. 95 500. 73 1. 583 1. 584 . 0300 . 7251E-03

NO. + 49.74 + 99.49 + 149.23 WF42 -WF53 + 50.00 + 100.00 + 150.00 + 200.00 + 250.00	H A 1.807 555.49 1.825 542.90 1.842 530.24 1.842 530.25 1.855 507.63 1.869 485.24 1.884 463.10 1.901 441.18 1.920 419.49 1.940 397.97 1.962 376.73 1.987 355.72 2.014 334.94	2. 425	0300 75 0300 75 0300 75 0300 75 0300 75 0310 75 0310 75 0310 75 0310 75 0310 75 0307 75 0306 75 0306 75 0306 75 0306 75 0306 75 0306 75 0306 75 0306 75 0306 75 0306 75 0306 75 0307 75 0311 75 0311 75 0311 75 0311 75 0311 75 0311 75 0311 75 0311 75 0317 7	Q DX 93. 00 49. 74 93. 00 49. 74 93. 00 49. 74 93. 00 50. 00 93. 00 50. 00 93. 00 50. 00 93. 00 50. 00 93. 00 50. 00 93. 00 50. 00 93. 00 50. 00 93. 00 50. 00 93. 00 50. 00 93. 00 50. 00 93. 00 50. 00 93. 00 50. 00 93. 00 50. 00	3267 3451 3658 3893 3894 3781 3683 3594 3514 3442 3375 3214 3257 3204 3155 3154 3109 3066 3026 2987 2987 2981 2917 2884 2853 2822 2792 2761 2771 2671 2642 2636 2630 2623 2617 2610 2603 2597 2589 2580 2580 2617 2610 2603 2617 2610 2603 2617 2610 2623 2636 2630 2623 2617 2610 2603 2597 2589 2589 2589 2589 2589 2589 2589 2589 2589 2589 2589 2589 2589 2589 2580	6948E-03 6667E-03 6667E-03 6151E-03 6566E-03 7288E-03 8138E-03 9156E-03 1039E-02 1019E-02 9549E-03 8527E-03 8109E-03 7408E-03 710E-03 6840E-03 6368E-03 6127E-03 5464E-03 5771E-03 5512E-03 5195E-03 5195E-03 4887E-03 4496E-03 4590E-03 4590E-03 4544E-03 4456E-03 4546E-03 4546E-03 4546E-03 4590E-03 6848E-03 687E-03	-2. 500 -2. 500 -2. 500 -2. 500 -2. 500 -2. 500 -2. 500 -2. 500 -2. 499 -2. 498 -2. 498 -2. 498 -2. 498 -2. 498 -2. 498 -2. 498 -2. 306 -2. 306 -2. 306 -2. 306 -2. 306 -2. 306 -2. 306 -2. 306 -2. 306 -2. 306 -2. 306 -2. 3080 -2. 250 -2. 251 -2. 212 -2. 193 -2. 174 -2. 155 -2. 136 -2. 174 -2. 155 -2. 136 -2. 193 -2. 174 -2. 155 -2. 118 -2. 199 -2. 080	4, 076 4, 086 4, 085 4, 094
+ 250.00 + 300.00 + 350.00 + 450.00 + 450.00 + 550.00 + 550.00 + 550.00 + 100.00 + 150.00 + 250.00 + 250.00 + 250.00 + 100.00 + 150.01 + 100.00 + 150.01 + 100.00 + 150.01 + 100.00 + 150.01 + 100.00 + 150.01 + 1	1. 901 419, 49 1. 940 397, 97 1. 962 376, 73 1. 987 355, 72 2. 014 334, 94 2. 044 314, 37 2. 077 294, 02 2. 089 298, 93 2. 185 304, 24 2. 271 308, 24 2. 271 308, 24 2. 271 308, 24 2. 350 311, 83 2. 423 314, 51 2. 492 316, 63 2. 558 318, 27 2. 558 318, 27 2. 620 320, 64 2. 680 322, 75 2. 737 324, 63 2. 792 326, 32 2. 792	3. 206 1. 890 3. 169 1. 993 3. 131 2. 105 3. 091 2. 229	0317 7: 0317 7: 0317 7: 0317 7: 0317 7: 0317 7: 0317 7: 0317 7: 0317 7: 0317 7: 0317 7: 0317 7: 0317 7: 0317 7: 0312 7: 0312 7: 0312 7: 0312 7: 0312 7: 0310 7:	93. 00 50, 00 93. 00 50, 15 93. 00 51, 92 93. 00 51, 92 93. 00 50, 00	4016 4293 4605 4961 4939 4770 4631 4515 4416 4330 4255 4255 4188 4128 4073 4022 4022 3965 3912 3862 3815 3770 3728 3980 4267 4601	.4447E-03 .4447E-03 .4447E-03 .4913E-03 .5059E-03 .6770E-03 .8573E-03 .9722E-03 .1109E-02 .1274E-02 .1719E-02 .1719E-02 .186E-02 .1396E-02 .131E-02 .1093E-02 .1093E-02 .1093E-02 .1093E-02 .1058E-03 .9365E-03 .9365E-03 .9365E-03 .9316E-03 .8718E-03 .8718E-03 .8718E-03 .8718E-03 .8718E-03 .8718E-03 .8718E-03 .8718E-03 .8750E-03 .9758E-03 .1129E-02 .1316E-02	-2. 155 -2. 136 -2. 118 -2. 099	4. 076 4. 076 4. 076 4. 080 4. 081 4. 103 4. 113 4. 133 4. 208 4. 416 4. 438 4. 530 4. 440 4. 488 4. 688 4. 723 4. 85 4. 85 4. 85 4. 85 4. 85 4. 85 4. 85 4. 85 4. 85 4. 85 4. 88

®

WF73 -WF75												
+ 50.00 + 50.00 WF75 -WF76 + 50.00 WF76 -WF95 + 50.36 + 100.72 + 151.08 + 201.44 + 251.80 + 302.16 + 352.52 + 402.88	3. 184 3. 297 3. 393 3. 462 3. 462 3. 515 3. 567 3. 666 3. 713 3. 760 3. 805 3. 849	275. 68 295. 39 314. 90 326. 72 326. 72 329. 60 332. 35 334. 98 337. 50 339. 92 342. 24 344. 48 346. 63	3, 888 3, 900 3, 867 3, 867 3, 770 3, 770 3, 796 3, 822 3, 846 3, 869 3, 891 3, 912 3, 932 3, 952	2. 877 2. 685 2. 518 2. 518 2. 427 2. 426 2. 386 2. 367 2. 350 2. 333 2. 317 2. 302 2. 288	. 0305 . 0305 . 0305 . 0300 . 0300 . 0310 . 0310 . 0310 . 0310 . 0310 . 0310 . 0310	793. 00 793. 00	50, 00 50, 00 50, 00 50, 00 50, 36 50, 36 50, 36 50, 36 50, 36 50, 36	. 4508 . 4252 . 4031 . 4031 . 3938 . 3938 . 3889 . 3844 . 3802 . 3762 . 3724 . 3689 . 3655	. 1259E-02 . 1092E-02 . 9720E-03 . 9404E-03 . 9649E-03 . 9393E-03 . 9157E-03 . 8938E-03 . 8735E-03 . 8546E-03 . 8205E-03	-1. 662 -1. 643 -1. 625 -1. 625 -1. 606 -1. 587 -1. 568 -1. 549 -1. 530 -1. 511 -1. 492 -1. 473	4, 846 4, 941 5, 018 5, 068 5, 068 5, 102 5, 135 5, 166 5, 196 5, 224 5, 251 5, 278	
+ 453, 24	3, 893					793.00	50. 36	3623	8050E-03	-1. 454	5, 303	٠
T 400, 24	3, 893	348. 71	3. 970	2. 274	. 0310	793. 00	50, 36	3593	: 7905E~03	-1. 435	5, 327	
*** WEST FL	OODWAY ,	STEADY NON	-UNIFORM FL	OW (LEVEL,	-2. 5, 1/26	50) b=50 i	wf75~up	PA	GE = 4			
NO.	Н	Α	R	v	. N	0	DX	FROUD	ΙE	Z	H-Z	
+ 503. 60	H 3. 935	A 350. 71	R 3, 989	y 2, 261	N 0310	. i.	18	* . * . *	Substitution of the	Z -1 416		
+ 503, 60 + 553, 96	H 3. 935 3. 977					793, 00	50. 36	3564	7768E-03	Z -1. 416	5. 351	
+ 503. 60		350.71	3, 989 4, 006	2. 249	0310	793, 00 793, 00	50. 36 50. 36	3564 3537	7768E-03 7638E-03	-1.397	5. 351 5. 373	
+ 503, 60 + 553, 96 + 604, 32	3. 977 4. 018	350. 71 352. 64 354. 51	3. 989 4. 006 4. 023	2. 249 2. 237	.0310 .0310	793, 00 793, 00 793, 00	50. 36 50. 36 50. 36	3564 3537 3511	. 7768E-03 . 7638E-03 . 7516E-03	-1. 397 -1. 378	5. 351 5. 373 5. 395	
+ 503, 60 + 553, 96 + 604, 32	3. 977 4. 018 4. 058	350, 71 352, 64 354, 51 356, 32	3. 989 4. 006 4. 023 4. 039	2. 249 2. 237 2. 225	. 0310 . 0310 . 0310	793, 00 793, 00 793, 00 793, 00	50. 36 50. 36 50. 36 50. 36	3564 3537 3511 3486	. 7768E-03 . 7638E-03 . 7516E-03 . 7400E-03	-1. 397 -1. 378 -1. 359	5. 351 5. 373 5. 395 5. 416	
+ 503. 60 + 553. 96 + 604. 32 + 654. 68 + 705. 04	3. 977 4. 018 4. 058 4. 097	350, 71 352, 64 354, 51 356, 32 358, 08	3. 989 4. 006 4. 023 4. 039 4. 055	2. 249 2. 237 2. 225 2. 215	.0310 .0310 .0310 .0310	793, 00 793, 00 793, 00 793, 00 793, 00	50. 36 50. 36 50. 36 50. 36 50. 36	3564 3537 3511 3486 3462	.7768E-03 .7638E-03 .7516E-03 .7400E-03 .7290E-03	-1. 397 -1. 378 -1. 359 -1. 340	5. 351 5. 373 5. 395 5. 416 5. 437	
+ 503. 60 + 553. 96 + 604. 32 + 654. 68 + 705. 04 + 755. 40	3. 977 4. 018 4. 058 4. 097 4. 136	350, 71 352, 64 354, 51 356, 32 358, 08 359, 78	3. 989 4. 006 4. 023 4. 039 4. 055 4. 070	2. 249 2. 237 2. 225 2. 215 2. 204	.0310 .0310 .0310 .0310	793. 00 793. 00 793. 00 793. 00 793. 00 793. 00	50. 36 50. 36 50. 36 50. 36 50. 36 50. 36	3564 3537 3511 3486 3462 3439	.7768E-03 .7638E-03 .7516E-03 .7400E-03 .7290E-03 .7185E-03	-1. 397 -1. 378 -1. 359 -1. 340 -1. 321	5. 351 5. 373 5. 395 5. 416 5. 437 5. 457	
+ 503. 60 + 553. 96 + 604. 32 + 654. 68 + 705. 04 + 755. 40 + 805. 76	3. 977 4. 018 4. 058 4. 097 4. 136 4. 174	350, 71 352, 64 354, 51 356, 32 358, 08 359, 78 361, 42	3, 989 4, 006 4, 023 4, 039 4, 055 4, 070 4, 084	2. 249 2. 237 2. 225 2. 215 2. 204 2. 194	.0310 .0310 .0310 .0310 .0310 .0310	793, 00 793, 00 793, 00 793, 00 793, 00 793, 00 793, 00	50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36	3564 3537 3511 3486 3462 3439 3417	.7768E-03 .7638E-03 .7516E-03 .7400E-03 .7290E-03 .7185E-03 .7086E-03	-1. 397 -1. 378 -1. 359 -1. 340 -1. 321 -1. 302	5. 351 5. 373 5. 395 5. 416 5. 437 5. 457 5. 476	
+ 503. 60 + 553. 96 + 604. 32 + 654. 64 + 705. 04 + 755. 40 + 805. 76 + 856. 12	3. 977 4. 018 4. 058 4. 097 4. 136 4. 174 4. 212	350, 71 352, 64 354, 51 356, 32 358, 08 359, 78 361, 42 363, 02	3. 989 4. 006 4. 023 4. 039 4. 055 4. 070 4. 084 4. 099	2. 249 2. 237 2. 225 2. 215 2. 204 2. 194 2. 184	.0310 .0310 .0310 .0310 .0310 .0310	793, 00 793, 00 793, 00 793, 00 793, 00 793, 00 793, 00 793, 00	50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36	3564 3537 3511 3486 3462 3439 3417 3396	. 7768E-03 . 7638E-03 . 7516E-03 . 7400E-03 . 7290E-03 . 7185E-03 . 7086E-03 . 6991E-03	-1. 397 -1. 378 -1. 359 -1. 340 -1. 321 -1. 302 -1. 283	5. 351 5. 373 5. 395 5. 416 5. 437 5. 457 5. 476 5. 494	
+ 503. 60 + 553. 96 + 604. 32 + 654. 68 + 705. 04 + 755. 40 + 805. 76 + 866. 12 + 908. 48	3. 977 4. 018 4. 058 4. 097 4. 136 4. 174 4. 212 4. 249	350. 71 352. 64 354. 51 356. 32 358. 08 359. 78 361. 42 363. 02 364. 57	3. 989 4. 006 4. 023 4. 039 4. 055 4. 070 4. 084 4. 099 4. 112	2. 249 2. 237 2. 225 2. 215 2. 204 2. 194 2. 184 2. 175	.0310 .0310 .0310 .0310 .0310 .0310 .0310	793. 00 793. 00 793. 00 793. 00 793. 00 793. 00 793. 00 793. 00 793. 00	50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36	3564 3537 3511 3486 3462 3439 3417 3396 3376	. 7768E-03 7638E-03 . 7516E-03 . 7400E-03 . 7290E-03 . 7185E-03 . 7086E-03 . 6991E-03	-1. 397 -1. 378 -1. 359 -1. 340 -1. 321 -1. 302 -1. 283 -1. 264	5. 351 5. 373 5. 395 5. 416 5. 437 5. 457 5. 476 5. 494 5. 512	
+ 503. 60 + 553. 96 + 604. 32 + 654. 68 + 705. 04 + 755. 40 + 805. 76 + 856. 12 + 906. 48 + 956. 84	3. 977 4. 018 4. 058 4. 097 4. 136 4. 174 4. 212 4. 249 4. 285	350. 71 352. 64 354. 51 356. 32 358. 08 359. 78 361. 42 363. 02 364. 57 366. 08	3. 989 4. 006 4. 023 4. 039 4. 055 4. 070 4. 084 4. 099 4. 112 4. 126	2. 249 2. 237 2. 225 2. 215 2. 204 2. 194 2. 184 2. 175 2. 166	.0310 .0310 .0310 .0310 .0310 .0310 .0310 .0310	793. 00 793. 00 793. 00 793. 00 793. 00 793. 00 793. 00 793. 00 793. 00	50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36	3564 3537 3511 3486 3462 3439 3417 3396 3376 3356	.7768E-03 .7638E-03 .7516E-03 .7516E-03 .7290E-03 .7185E-03 .7086E-03 .6991E-03 .6901E-03 .6815E-03	-1. 397 -1. 378 -1. 359 -1. 340 -1. 321 -1. 302 -1. 283 -1. 264 -1. 245	5. 351 5. 373 5. 395 5. 416 5. 437 5. 457 5. 476 5. 494 5. 512 5. 530	
+ 503.60 + 553.96 + 604.32 + 654.68 + 705.04 + 755.40 + 805.76 + 856.12 + 906.48 + 956.84 WF95 - WF99	3. 977 4. 018 4. 058 4. 097 4. 136 4. 174 4. 212 4. 249 4. 285 4. 285	350. 71 352. 64 354. 51 356. 32 358. 08 359. 78 361. 42 363. 02 364. 57 366. 08	3. 989 4. 006 4. 023 4. 039 4. 055 4. 070 4. 084 4. 099 4. 112 4. 126 4. 126	2. 249 2. 237 2. 225 2. 215 2. 204 2. 194 2. 184 2. 175 2. 166 2. 166	.0310 .0310 .0310 .0310 .0310 .0310 .0310 .0310 .0310	793. 00 793. 00	50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36	3564 3537 3511 3486 3462 3439 3417 3396 3376 3356	7768E-03 7638E-03 7516E-03 7516E-03 7290E-03 7185E-03 7086E-03 6991E-03 6815E-03 6815E-03	-1. 397 -1. 378 -1. 359 -1. 340 -1. 321 -1. 302 -1. 283 -1. 264 -1. 245 -1. 245	5. 351 5. 373 5. 395 5. 416 5. 437 5. 457 5. 476 5. 494 5. 512 5. 530 5. 530	
+ 503. 60 + 553. 96 + 604. 32 + 654. 68 + 705. 04 + 755. 40 + 805. 76 + 856. 12 + 906. 48 + 956. 84 WF95 - WF99 + 49. 90	3. 977 4. 018 4. 058 4. 097 4. 136 4. 174 4. 212 4. 249 4. 285 4. 323	350. 71 352. 64 354. 51 356. 32 358. 08 359. 78 361. 42 363. 02 364. 57 366. 08 368. 68	3, 989 4, 006 4, 023 4, 039 4, 055 4, 070 4, 084 4, 099 4, 112 4, 126 4, 128	2. 249 2. 237 2. 225 2. 215 2. 204 2. 194 2. 184 2. 175 2. 166 2. 166 2. 151	. 0310 . 0310 . 0310 . 0310 . 0310 . 0310 . 0310 . 0310 . 0310 . 0310	793. 00 793. 00	50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 49. 90	3564 3537 3511 3486 3462 3439 3417 3396 3376 3356 3356 3356	. 7768E-03 7638E-03 7516E-03 7400E-03 7290E-03 7185E-03 7086E-03 6991E-03 6815E-03 6815E-03 6714E-03	-1. 397 -1. 378 -1. 359 -1. 340 -1. 321 -1. 302 -1. 283 -1. 264 -1. 245	5. 351 5. 373 5. 395 5. 416 5. 437 5. 457 5. 476 5. 494 5. 512 5. 530	
+ 503. 60 + 553. 96 + 604. 32 + 654. 68 + 705. 04 + 755. 40 + 805. 76 + 856. 12 + 906. 48 + 956. 84 WF95 - WF99 + 49. 90 + 99. 80	3. 977 4. 018 4. 058 4. 097 4. 136 4. 174 4. 212 4. 249 4. 285 4. 323 4. 359	350. 71 352. 64 354. 51 356. 32 358. 08 359. 78 361. 42 363. 02 364. 57 366. 08 366. 08 368. 68 371. 25	3, 989 4, 006 4, 023 4, 039 4, 055 4, 070 4, 084 4, 099 4, 112 4, 126 4, 126 4, 130	2. 249 2. 237 2. 225 2. 215 2. 204 2. 194 2. 184 2. 175 2. 166 2. 166 2. 151 2. 136	.0310 .0310 .0310 .0310 .0310 .0310 .0310 .0310 .0310 .0310	793. 00 793. 00	50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36	3564 3537 3511 3486 3462 3439 3417 3396 3376 3356	7768E-03 7638E-03 7516E-03 7516E-03 7290E-03 7185E-03 7086E-03 6991E-03 6815E-03 6815E-03	-1. 397 -1. 378 -1. 359 -1. 340 -1. 321 -1. 302 -1. 283 -1. 264 -1. 245 -1. 245	5. 351 5. 373 5. 395 5. 416 5. 437 5. 457 5. 476 5. 494 5. 512 5. 530 5. 530	
+ 503. 60 + 553. 96 + 604. 32 + 654. 68 + 705. 04 + 755. 40 + 805. 76 + 856. 12 + 906. 48 + 956. 84 WF95 - WF99 + 49. 90	3. 977 4. 018 4. 058 4. 097 4. 136 4. 174 4. 212 4. 249 4. 285 4. 323	350. 71 352. 64 354. 51 356. 32 358. 08 359. 78 361. 42 363. 02 364. 57 366. 08 368. 68	3, 989 4, 006 4, 023 4, 039 4, 055 4, 070 4, 084 4, 099 4, 112 4, 126 4, 128	2. 249 2. 237 2. 225 2. 215 2. 204 2. 194 2. 184 2. 175 2. 166 2. 166 2. 151	. 0310 . 0310 . 0310 . 0310 . 0310 . 0310 . 0310 . 0310 . 0310 . 0310	793. 00 793. 00	50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 50. 36 49. 90	3564 3537 3511 3486 3462 3439 3417 3396 3376 3356 3356 3356	. 7768E-03 7638E-03 7516E-03 7400E-03 7290E-03 7185E-03 7086E-03 6991E-03 6815E-03 6815E-03 6714E-03	-1. 397 -1. 378 -1. 359 -1. 340 -1. 321 -1. 302 -1. 283 -1. 264 -1. 245 -1. 226	5. 351 5. 373 5. 395 5. 416 5. 437 5. 457 5. 457 5. 494 5. 512 5. 530 5. 548	