| • | Design | wediby : | Che | cked by : | Da | te ; | January 23, 21 | 00 |
|--|---------|------------|------------------------|---------------|--------------|--------------|----------------|-------------|
| | | | TEMPER | ATURE LO | DADS | | | |
| MEMB | LOAD | NODE | AXIALİ | SHEAR,Y | SHEAR-Z | TORSION | MOM-Y | Мом |
| 432 | | 433 | 3,545,66 | -2.30 | | | | |
| 432 | | 434 | -3,545.66 | 2.30 | 0.00 | 0.00 0.00 | 0.00 0.00 | 15. 10 |
| nego de la contra en la contra e En la contra en la co | 2 | 433 | -2,239.51 | 1.45 | 0,00 | 0,00 | 0.00 | 9. |
| a a la contra d | 3 | 434 433 | 2,239,51 -84,40 | -1.45 | 0.00 | 0.00 | 0.00 | -6. |
| | | 434 | -54.40 84.40 | 0,01 -0.01 | 0,00 | 0.00 | 0.00 0.00 | 0. -0. |
| 433 | 1 | 434 | 3,545,66 | -2.14 | 0.00 | 0.00 | 0.00 | •10. |
| | | 435 | -3,545.66 | 2.14 | 0.00 | 0.00 | 0.00 | •10. |
| | . 2 | 434 | -2,239,50 | 1.35 | 0.00 | 0.00 | 0.00 | 6. |
| | 3 | 435 434 | 2,239.50 | -1.35 0.01 | 0.00 | 0,00 | 0.00 | -4 |
| | | 434 | 84.40 | -0.01 | 0.00 | 0.00 | 0.00 | 0. |
| | | | | | | | | |
| 434 | 영상 방송 문 | 435 436 | 3,545,67 | -1.65 1.65 | 0.00 | 0,00 0,00 | 0.00 | -6 |
| | 2 | 435 | -2,239.50 | 1.04 | 0.00 | 0.00 | 0.00 | 3. 4 |
| | | 436 | 2,239.50 | -1.04 | 0.00 | 0.00 | 0.00 | -2. |
| | 3 | 435 | -84,40 84,40 | 0.01 -0.01 | 0.00 0.00 | 0.00 | 0.00 | 0. |
| | | 420 | 64.4V | -0.01 | 0.00 | 0.00 | 0.00 | -0. |
| 435 | 1 | 436 | 3,545,67 | -1.10 | 0.00 | 0.00 | 0.00 | -3. |
| | 2 | 437 436 | -3,545.67 -2,239.50 | 1.10 0.69 | 0.00 0.00 | 0.00 | 0.00 | 1. |
| | | 437 | 2,239.50 | -0.69 | 0.00 | 0.00 0.00 | 0.00 0.00 | 2. -0. |
| 가 있다. 가 가 가 있다. 가 있는 것은 것 같아요. | 3 | 436 | -84.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0. |
| | | 437 | 84.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0. |
| 436 | | 437 | 3,545.67 | -0.63 | 0.00 | 0.00 | 0,00 | -1, |
| | | 438 | -3,545.67 | 0.63 | 0.00 | 0.00 | 0.00 | - 0. |
| | 2 | 437 438 | -2,239.50 2,239.50 | 0.40 -0.40 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | 0. 0. |
| | 3 | 437 | -84.40 | 0.00 | 0.00 | 0.00 | 0.00 | Ŭ. |
| | | 438 | 84.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.0 |
| 437 | 1 | 438 | 3,545.67 | -0.28 | 0.00 | 0.00 | 0.00 | 0. |
| ann a feile | 2 | 439 438 | -3,545.67 -2,239.50 | 0.28 | 0.00 | 0.00 | 0.00 | -0. |
| | | 438 | 2,239.50 | 0.18 -0,18 | 0,00 0,00 | 0.00 0,00 | 0.00 0.00 | -0. 0. |
| | 3 | 438 | -84.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0. |
| | | 439 | 84.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0. |
| 438 | 1 | 439 | 3,545.67 | -0.07 | 0,00 | 0.00 | 0.00 | O. |
| | | 440 | -3,545.67 | 0.07 | 0.00 | 0.00 | 0.00 | -0, |
| | 2 | 439 440 | -2,239.50 2,239.50 | 0,04 -0.04 | 0.00 | 0.00 0.00 | 0.00 0.00 | -0. |
| | 3 | 439 | -84.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0. 0. |
| | | 440 | 84.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0. |
| 439 | 1 | 440 | 3,545.66 | 0.05 | 0.00 | 9.00 | 0.00 | Q. |
| | | 441 | -3,545,66 | -0.05 | 0.00 | 0.00 | 0.00 | -0. |
| | 2 | 440 441 | -2,239.50 2,239.50 | -0.03 0.03 | 0.00 | 0.00 | 0.00 | -0. |
| | 3 | 440 | -84.40 | 0.00 | 0.00 | 0.00 0.00 | 0.00 0.00 | 0. 0.(|
| | | 441 | 84.40 | 0.00 | 0,00 | 0.00 | 0.00 | 0.(|
| 440 | 1 | 441 | 3,545.67 | 0.09 | 0.00 | 0.00 | 0.00 | |
| | | 442 | -3,545.67 | -0,09 | 0.00 | 0.00 | 0.00 0.00 | 0. -0. |
| | 2 | 441 | -2,239.50 | -0.06 | 0,00 | 0.00 | 0.00 | -0.4 |
| | 3 | 442 441 | 2,239.50 -84.40 | 0,06 | 0,00 | 0.00 | 0.00 | 0 |
| | | 442 | -54.40 84.40 | 0.00 | 0.00 | 0.00 0.00 | 0.00 0.00 | 0.0 0.0 |
| | | | | | | | | |
| 441 | | 442 443 | 3,545.67 -3,545.67 | 0.10 -0.10 | 0.00 | 0.00 | 0.00 | 0. |
| | 2 | 442 | -2,239.50 | -0.06 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | -0. -0_ |
| | | 443 | 2,239.50 | 0.06 | 0.00 | 0,00 | 0.00 | 0 |
| | 3 | 442 | | 0,00 | 0.00 | 0.00 | 0.00 | 0.0 |

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| b Ne. : | Desi | gned by : | Cъ | ocked by : | D. | 1e ; | January 23, | 2000 |
|--|---|--|-----------------------|---------------------------|---|--|--|-----------------------------------|
| | | | TEMPER | ATURE LO | DADS | | | |
| MEMB | LOAD | NODE | AXIAL | SHEAR-Y | SHEAR-Z | TORSION | MOM-Y | MON |
| 442 | 1 | 443 | 3,545.67 | 0.05 | 0.00 | 0,00 | 0.00 | 0 |
| | 水道 からな 流り き へい いい | 444 | -3,545.67 | -0.08 | 0.00 | 0.00 | 0,00 | -0. |
| | 2 | 443 | -2,239,50 | -0.05 | 0.00 | 0.00 | 0.00 | -0 |
| | - - | 444 443 | 2,239.50 -84,40 | 0.05 | 0.00 | 0.00 | 0,00 | 0 |
| | | 444 | -84,40 84,40 | 0.00 | 0.00 | 0.00 | 0.00 0.00 | 0. 0. |
| Creek 443 M | 1 | 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 | 3,545.67 | 0.06 | 0.00 | 0.00 | | e de la composición Perspectos |
| s yandigi Q | | 445 | -3,545.67 | -0.06 | 0.00 | 0.00 | 0.00 0.00 | 0. |
| | 2 | 444 | -2,239.50 | -0.04 | 0.00 | 0.00 | 0.00 | -0. -0. |
| | | 445 | 2,239.50 | 0.04 | 0.00 | 0.00 | 0.00 | 0. |
| | 3 | 444 | -84.40 | 0.00 | 0.00 | 0,00 | 0.00 | 0 |
| | | 445 | \$4.40 | 0.00 | 0.00 | 0,00 | 0.00 | 0. |
| 444 (A) | 19 (4.9) 1 (4.9) 24 (2.9) (4.9) | 445 | 3,545.67 | 0.05 | 0.00 | 0.00 | 0.00 | 0. |
| 부분 전 가지는 것 있는 가 전 가지 가지 않는 것 | 2 | 446 445 | -3,545.67 | -0.05 | 0.00 | 0.00 | 0.00 | 0. |
| | | 446 | -2,239.50 2,239.50 | -0.03 0.03 | 0.00 | 0.00 | 0,00 | -0. |
| | 64-1.1 3 1.4 | 445 | -84.40 | 0.03 | 0.00 | 0.00 | 0.00 | -0. 0. |
| 9 M - 1 | | 446 | 84.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0. |
| n. 120 1 445 | | 446 | 3,545.67 | 0.04 | 0.00 | 0.00 | 0.00 | |
| $f = \{0, \dots, n\}$ | 0 | 424 | 3,545.67 | -0.04 | 0.00 | 0.00 | 0.00 | -0. |
| $\{1, \dots, N_{n}\} \in \{1, \dots, N_{n}\}$ | 0 (<u>2)</u> 2) - | 446 | -2,239.50 | -0.03 | 0.00 | 0.00 | 0,00 | 0. 0.(|
| | | 424 | 2,239.50 | 0.03 | 0.00 | 0.00 | 0.00 | -0 (|
| | 3 | 446 | -84.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.0 |
| | | 424 | 84.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.0 |
| 446 | 1 | 424 | 3,545.67 | 0.04 | 0.00 | 0.00 | 0.00 | -0. |
| | | 447 | -3,545.67 | -0.04 | 0.00 | 0.00 | 0.00 | 0.1 |
| | 2 | 424 447 | -2,239.50 2,239.50 | -0.03 | 0.00 | 0.00 | 0.00 | 0.0 |
| | 3 | 424 | -84.40 | 0.03 0.00 | 0.00 | 0.00 0.00 | 0.00 | -0.1 |
| | | 447 | 84.40 | 0.00 | 0.00 | 0.00 | 0.00 0.00 | 0.0 0.0 |
| 448 | | 448 | -1,091,74 | 194.23 | 0.00 | 0.00 | 0.00 | |
| al astronomica de la | | 449 | 1,091.74 | -194.23 | 0.00 | 0.00 | 0.00 | 2,717.1 |
| Stern Stern | - 2 | (k. d 448 | 689.79 | -122.32 | 0.00 | 0.00 | 0.00 | -1,714.3 |
| | | 449 | -689.79 | 122.32 | 0.00 | 0.00 | 0,00 | 612.7 |
| | 1977 - 1 977 - 1977 1978 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - 1977 - | 448 996 449 | 22.89 -22.89 | -8.35 8.35 | 0.00 | 0.00 | 0.00 | -118.2 |
| | | | | | 0.00 | 0.00 | 0.00 | 43.1 |
| 4 49 | | 449 450 | -1,091.74 | 194.23 | 0.00 | 0.00 | 0.00 | 971.0 |
| | 2 | 449 | 1,091.74 689.79 | -194.23 -122.32 | 0.00 0.00 | 0.00 | 0.00 | 1,938.4 |
| | | 450 | -689.79 | 122.32 | 0.00 | 0.00 0.00 | 0.00 | -612.7 |
| | 2 S 3 | 449 | 22.89 | -8,35 | 0.00 | 0.00 | 0.00 | -1,223,5 -43,1 |
| | | 450 | -22.89 | 8.35 | 0.00 | 0.00 | 0.00 | -82.0 |
| 450 | | 450 | -1,091.74 | 138.85 | 0.00 | 0.00 | 0.00 | -1,938.3 |
| | | 452 | 1,091.74 | -138.85 | Ó.00 | 0.00 | 0.00 | 2,146.4 |
| | 2 | 450 | 689,78 | -87.48 | 0.00 | 0.00 | 0,00 | 1,223.5 |
| · 新闻的名词称" 同节" 中国 1997年——————————————————————————————————— | 938 (1997) 1938 (1997) 1938 (1997) | 452 | -689.78 | 87.48 | 0.00 | 0.00 | 0.00 | 1,354,8 |
| | | 450 452 | 22.89 -22.89 | -5.99 5.99 | 0.00 0.00 | 0.00 0.00 | 0.00 | 82.0 -91.0 |
| 1. | | All Your St | | | | | | - ,1.0 |
| 14 (1985) 451 1987 (1986) - 1987 (1987) | 가는 것 - 가지가 성장 전 사람 - 1 | 452 · · · · · · · · · · · · · · · · · · · | -1,091.74 1,091.74 | 51,85 -51,85 | 0.00 | 0.00 | 0.00 | -2,146.48 |
| | 2 | 452 | 689.79 | -31.85 | 0.00 0.00 | 0.00 0.00 | 0.00 | 2,223.96 |
| use data in the first of the | | (8),8 (453 | -689.79 | 32.56 | 0.00 | 0.00 | 0.00 | 1,354.71 |
| | 3 | 452 | 22.89 | -2.27 | 0.00 | 0.00 | 0.00 | -1,-03.03 |
| | na fa de selo Guide enve | 453 | -22.89 | * 2.27 | 0.00 | 0,00 | 0.00 | 94.45 |
| | 1 | 453 | -1,091.73 | -14.13 | 0.00 | 0.00 | 0.00 | -2,224.00 |
| | | 454 | 1,091.73 | 14.13 | 0.00 | 0,00 | 0.00 | 2,202.56 |
| | 2 | 453 | 689.78 | 9.15 | 0.00 | 0.00 | 0.00 | 1,403.70 |
| | 2000 - 1997 - 2000 - 2000 1998 - 201 3 - 2010 | 454 | 689.78 | -9.15 | 0.00 | 0.00 | 0.00 | -1,390.08 |
| | 3 | 453 454 | 22.89 -22.89 | 0.55 | 0.00 | 0.00 | 0,00 | 94.48 |
| | | | -44.07 | -0.55 | 0.00 | 0.00 | 0.00 | -93.66 |
| | | メンクス かんそうし かいたいかい | | 5 1.1 2.1 A. 1997 M. 1997 | a second de la 1973 en la secondada | e a la subsectión de la companya de | and the second | |

Pacific Consultants International of Japan, Third Floor, Bldg # 47 DDC Center, Mokhali, Dhaka1212

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Designed by ;

Checked by I

1.1.

January 23, 2000

| MEMB | LOAD | NODE | AXIAL | SHEARY | SHEAR-Z | TORSION | MOM-Y | MOM-2 |
|------------------------|--|--------------|--------------------|-------------------|--------------|-----------------|---|----------------------|
| | | e i pare aut | | | | ren de tet grae | 1997 - 1998 - 1997 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - | |
| 453 | 1 | 454 | -1,091.74 | -62.26 | 0.00 | 0.00 | 0.00 | -2,202.5 |
| | 2 | 455 | 1,091.74 | 62.26 | 0.00 | 0.00 | 0.00 0.00 | 2,108.95 1,390.09 |
| | 4 | 454 455 | 689.78 -689.78 | 39.50 -39.50 | 0.00 | 0.00 | 0.00 | -1,330.94 |
| | 1 | 454 | 22.89 | 2.61 | 0.00 | 0.00 | 0.00 | 93.60 |
| | | 455 | -22.89 | -2.61 | 0.00 | 0.00 | 0.00 | -89,70 |
| | | 455 | -1.091.75 | -95,53 | 0.00 | 0.00 | 0.00 | -2,108.9 |
| 454 | ele Maria de la secono de la se | 455 | 1,091,75 | 95.53 | 0.00 | 0.00 | 0.00 | 1,965,5 |
| | 2 | 455 | 689.79 | 60,44 | 0.00 | 0.00 | 0.00 | 1,330.9 |
| | | 456 | -689.79 | -60.44 | 0.00 | 0.00 | 0.00 | -1,240.3 |
| | 3 | 455 | 22.89 | 4.03 | 0.00 | 0.00 | 0.00 | 89.7 |
| | | 456 | -22.89 | -4.03 | 0.00 | 0.00 | 0.00 | -83.7 |
| 455 | 1 | 456 | -1.091.73 | -122.83 | 0.00 | 0.00 | 0.00 | -1,965.5 |
| ette statue | | 457 | 1,091.73 | 122.83 | 0.00 | 0.00 | 0.00 | 1,781.1 |
| | 2 | 456 | 689.79 | 77.68 | 0.00 | 0.00 | 0.00 | 1,240.3 |
| | | 457 | -689.79 | -77.68 | 0.00 | 0.00 | 0.00 | -1,123.8 |
| | 3 | 456 457 | 22.89 -22.89 | 5.20 -5.20 | 0.00 0.00 | 0.00 | 0.00 0.00 | 83.7 -75.9 |
| | | •••• | -44.07 | -3-20 | 0.00 | | | |
| 456 | 1 | 457 | -1,091.74 | -163.83 | 0.00 | 0.00 | 0.00 | -1,781,1 |
| | | 458 | I 091.74 | 163.83 | 0.00 | 0.00 | 0.00 | 1,535.3 |
| | 2 | 457 | 689.78 | 103,49 | 0.00 | 0.00 | 0.00 | 1,123.9 |
| | | 458 | -689.78 | -103,49 6.96 | 0.00 | 0.00 | 0.00 | -968. 75.9 |
| | 3 | 457 458 | 22.89 -22.89 | -6.96 | 0.00 | 0.00 | 0.00 | -65.4 |
| | | 460 | -1,091.74 | 190.00 | 0.00 | 0.00 | 0.00 | -1,535 |
| 457 | | 458 459 | 1,091,74 | -180.82 180.82 | 0.00 | 0.00 | 0.00 | 1,264.0 |
| | . 2 | 458 | 689.78 | 114.18 | 0.00 | 0.00 | 0.00 | 968. |
| | | 459 | -689,78 | -114.18 | 0.00 | 0.00 | 0.00 | -797 |
| | 3 | 458 | 22.89 | 7.69 | 0.00 | 0.00 | 0.00 | 65. |
| | | 459 | -22.89 | -7.69 | 0.00 | 0.00 | 0.00 | -53,9 |
| 458 | 1 | 459 | -1,091.74 | -181.16 | 0.00 | 0.00 | 0.00 | -1,264.0 |
| | | 460 | 1,091.74 | 181,16 | 0.00 | 0.00 | 0.00 | 992. |
| | 2 | 459 | 689.78 | 114.36 | 0.00 | 0.00 | 0.00 | 797. -625. |
| | | 460 459 | -689,78 22,89 | -114.36 7.72 | 0.00 | 0.00 | 0.00 0.00 | -623. 53. |
| (회원의 전원의) 41 관리 전문의 | | 460 | (| -7.72 | 0.00 | 0.00 | 0.00 | -42. |
| 459 | | 460 | -1,091.74 | -167.56 | 0.00 | 0.00 | 0.00 | -992, |
| 4.17 | | 461 | 1,091.74 | 167.56 | 0.00 | 0.00 | 0.00 | 740. |
| | 2 | 460 | 689,79 | 105.75 | 0.00 | 0.00 | 0.00 | 625. |
| | | 461 | -689.79 | -105.75 | 0.00 | 0.00 | 0.00 | -467. |
| | 3 | 460 | 22.89 -22.89 | 7.14 -7.14 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | 42. -31. |
| | | 461 | | | 0.00 | 0.00 | 0.00 | - 16- |
| 460 | 1 | 461 | -1,091.74 | -146.15 | 0.00 | 0,00 | 0.00 | -740. |
| | 2 | 462 461 | 1,091.74 689.78 | 146.15 92.22 | 0.00 | 0.00 | 0.00 | 521 467 |
| | 승규는 물통 것 | 462 | -689.78 | -92.22 | 0.00 | 0.00 | 0.00 | -328. |
| | 3 | 461 | 22,89 | 6.23 | 0.00 | 0.00 | 0.00 | 31. |
| | | 462 | -22.89 | -6.23 | 0.00 | 0.00 | 0.00 | -22. |
| 461 | 1 | 462 | -1,091.74 | -121.51 | 0.00 | 0.00 | 0.00 | •521. |
| | | 463 | 1,091.74 | 121.51 | 0.00 | 0.00 | 0.00 | 339. |
| | 2 | 462 | 689.79 | 76.67 | 0.00 | 0.00 | 0.00 | 328. |
| | | 463 | -689.79 | -76.67 | 0.00 | 0.00 | 0.00 | -213. |
| | 3 | 462 | 22.89 | 5,19 | 0,00 | 0.00 | 0.00 | 22. |
| | | 463 | -22.89 | -5.19 | 0.00 | 0.00 | 0.00 | -14 |
| 462 | 1 | 463 | -1,091.74 | +96.89 | 0.00 | 0,00 | 0.00 | -339 |
| | | 464 | 1,091.74 | 96.89 | 0.00 | 0.00 | 0.00 | 194 |
| | 2 | 463 | 689.79 | 61.12 | 0.00 | 0.00 | 0.00 | 213 |
| | (1) A. 1984 A. 199 | | | | | 0.00 | 0.00 | -122 |
| | 3 | 464 463 | -689.79 22.89 | -61.12 4.14 | 0.00 | 0.00 | 0.00 | •122 14 |

Pacific Consultants International of Japan, Third Floor, Bidg # 47 DDC Center, Mokhali, Dhaka1212

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eb No. :

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Designed by :

Checked by :

January 23, 2000

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Date :

TEMPERATURE LOADS

| MEMB | LOAD | NODE | AXIAL | SHEAR-Y | SHEAR-Z | TORSION | MOM-Y | мом |
|--|-----------------------------|------------|--------------------|----------------|---|--------------|--------------|------------|
| 463 | 1 (1 | 464 | -1,091.74 | -74,42 | 0.00 | 0.00 | 0,00 | -194. |
| | | 465 | 1,091.74 | 74.42 | 0.00 | 0.00 | 0.00 | 82. |
| | 2 | 464 | 689,79 | 46.94 | 0.00 | 0.00 | 0.00 | 122. |
| | | 465 | -689.79 | -46,94 | 0.00 | 0,00 | 0.00 | -51. |
| | 3 | 464 | 22.89 | 3.18 | 0.00 | 0.00 | 0.00 | 8. 3. |
| | e di tabi se | 465 | -22.89 | -3.18 | 0.00 | 0.00 | 0.00 | • • |
| 464 | | 465 | -1,091,74 | -55.32 | 0.00 | 0.00 | 0.00 | -82. |
| | | 466 | 1,091,74 | 55.32 | 0.00 | 0.00 | 0.00 | 0. |
| | 2 | 465 | 689.79 | 34.89 | 0.00 | 0.00 | 0.00 | 51, |
| | | 466 | -689.79 | -34.89 | 0.00 | 0.00 | 0,00 | 0 |
| | 3 | 465 | 22.89 | 2.37 | 0.00 | 0.00 | 0.00 | 3. |
| | | 466 | -22.89 | -2.37 | 0.00 | 0.00 | 0.00 | -0. |
| | | 466 | -1,091.74 | -40,13 | 0.00 | 0.00 | 0.00 | 0. |
| 465 | | 467 | 1,091.74 | 40.13 | 0.00 | 0.00 | 0.00 | -60 |
| 98 - 199 - 199 - 199 | 2 | 466 | 689.78 | 25.30 | 0.00 | 0.00 | 0.00 | -0 |
| | | 467 | -689.78 | -25.30 | 0.00 | 0.00 | 0.00 | 38 |
| | 1 - 3 - 📜 | 466 | 22.89 | 1.72 | 0.00 | 0.00 | 0,00 | 0 |
| | | 467 | -22.89 | -1.72 | 0.00 | 0.00 | 0.00 | 2 |
| | | | | | | 0.00 | A 00 | |
| 466 | 1 | 467 | -1,091.74 | -25.13 | 0.00 | 0.00 | 0.00 0.00 | 60 -98 |
| | | 468 467 | 1,091.74 689.78 | 25.13 15.83 | 0.00 | 0.00 | 0.00 | -38 |
| | 2 | 468 | -689.78 | -15.83 | 0.00 | 0.00 | 0.00 | 62 |
| | 84.38 .3 C | 467 | 22.89 | 1.08 | 0.00 | 0.00 | 0.00 | -2 |
| | | 468 | -22.89 | -1.08 | 0,00 | 0.00 | 0.00 | 4 |
| 1997년 1월 1997년 1월 1997년 1997년 1월 1997년 br>1월 1997년 1월 19 | | | | | Mercelander og blev som Fra Standard og blev som | | | |
| 467 | , 1 | 468 | -1,091.74 | -14,90 | 0.00 | 0.00 | 0.00 | 98 -120 |
| | | 469 | 1,091,74 | 14.90 9.38 | 0.00 0,00 | 0.00 0.00 | 0.00 | -62 |
| | 2 | 468 469 | 689,78 -689,78 | -9.38 | 0.00 | 0.00 | 0.00 | 76 |
| | 3 3 | 468 | 22.89 | 0.64 | 0.00 | 0.00 | 0.00 | -4 |
| | | 469 | -22.89 | -0.64 | 0.00 | 0.00 | 0.00 | 5 |
| 468 | 1 | 469 | -1,091.74 | 3.72 | 0.00 | 0.00 | 0.00 | 120 |
| | | 451 | 1,091.74 | -3.72 | 0.00 | 0.00 | 0.00 | -115 |
| | ୁ 🤆 👌 🖞 | 469 | 689.79 | -2,36 | 0.00 | 0.00 | 0.00 | -76 |
| | di shakariki ili. N | 45] | -689.79 | 2.36 | 0.00 | 0.00 | 0.00 | 72 |
| | 1 3 4 8 5 5 5 5 5 | 469 | 22.89 | -0.16 | 0.00 0.00 | 0.00 | 0.00 0.00 | -5 4 |
| g av star star star | | 451 | -22.89 | 0.16 | 0.00 | | 0.00 | |
| 469 | | 451 | -1,091.74 | 13.30 | 0.00 | 0.00 | 0.00 | 115 |
| | | 471 | 1,091,74 | -13.30 | 0.00 | 0.00 | 0.00 | -88 |
| 하는 것 같 같 | 2 | 451 | 689.79 | -8.40 | 0.00 | 0.00 | 0.00 | -72 |
| | | 471 | -689.79 | 8.40 | 0.00 | 0.00 | 0.00 | \$5 |
| 위에 있는 것이 있는 것이 있다. 1월 18일 - 19일 - 1 | 3 | 451 | 22.89 | -0.57 | 0.00 | 0.00 | 0.00 0.00 | 4 |
| | | 471 | -22.89 | 0.57 | 0.00 | 0.00 | 0.00 | , |
| 470 | | 471 | -1,091.74 | 15.05 | 0.00 | 0.00 | 0.00 | 88 |
| ena na filia a 🗼 | | 472 | 1,091.74 | -15.05 | 0.00 | 0.00 | 0.00 | -58 |
| w phatairtí a fr | 2 | 471 | 689.78 | -9.50 | 0.00 | 0.00 | 0.00 | -55 |
| | 건설 관계 가슴 | 472 | -689.78 | 9.50 | 0.00 | 0.00 | 0.00 | 36 |
| | 3 | 471 | 22.89 | -0.64 | 0.00 | 0.00 | 0.00 | -3 |
| | | 472 | -22.89 | 0.64 | 0.00 | 0.00 | 0.00 | 2 |
| 491 | | 472 | -1,091,74 | 12.78 | 0.00 | 0.00 | 0.00 | 58 |
| - 471 - 15- 93 | | 473 | 1,091.74 | -12.78 | 0.00 | 0.00 | 0.00 | -32 |
| | 2 | 472 | 689,79 | -8.07 | 0,00 | 0.00 | 0.00 | -36 |
| | | 473 | -689,79 | 8.07 | 0,00 | 0.00 | 0.00 | 20 |
| | 3 | 472 | 22.89 | -0.55 | 0.00 | 0.00 | 0.00 | -2 |
| 2年代,任太王元(19 18月1日—1943年 | | 473 | -22.89 | 0.55 | 0.00 | 0.00 | 0.00 | 1 |
| | | 473 | -1,091.74 | 9.07 | 0.00 | 0,00 | 0.00 | 32 |
| 472 | | 474 | -1,091.74 | -9.07 | 0.00 | 0.00 | 0.00 | -14 |
| 64 | 2 | 473 | 689.79 | -5.72 | 0.00 | 0.00 | 0.00 | -20 |
| | | 474 | -689.79 | \$.72 | 0,00 | 0.00 | 0.00 | 9 |
| | 8 - S | 473 | 22.89 | -0,39 | 0.00 | 0.00 | 0.00 | -1 |
| | | 474 | -22.89 | 0.39 | 0.00 | 0,00 | 0.00 | 0 |

Pacific Consultants International of Japan, Third Floor, Bldg # 47 DDC Center, Mokhali, Dhaka1212

| p, : | Detign | <u></u> | <u></u> | ecked by : | - <u> </u> | <u>té;</u> | January 23, 20 | ~~ |
|---|--|------------|--------------------|---------------|--------------|--------------|----------------|--|
| | | | TEMPER | ATURE LO | DADS | | | |
| MEMB | LOAD | NODE | AXIAL | SHEAR-Y | SHEAR-Z | TORSION | MOM-Y | MO |
| 473 | 1 | 474 | -1,091.74 | 5.71 | 0.00 | 0,00 | 0.00 | 1 |
| | | 475 | 1,091.74 | -5.71 | 0.00 | 0.00 | 0.00 | • |
| | 2 | 474 475 | 689.79 -689.79 | -3.60 3.60 | 0.00 | 0.00 0.00 | 0,00 0,00 | |
| | 3 | 474 | 22.89 | -0.24 | 0.00 | 0.00 | 0.00 | • |
| | | 475 | -22.89 | 0.24 | 0.00 | 0.00 | 0.00 | |
| 474 | 1 | 475 | -1,091,74 | 3.02 | 0.00 | 0.00 | 0.00 | |
| | | 476 | 1,091.74 689.78 | -3.02 | 0.00 0.00 | 0.00 | 0.00 0.00 | |
| | 2 | 476 | -689.78 | -1.91 1.91 | 0,00 | 0.00 | 0.00 | |
| | 3 | 475 | 22.89 | -0.13 | 0.00 | 0.00 | 0.00 | |
| | | 476 | -22.89 | 0.13 | 0.00 | 0.00 | 0.00 | |
| 475 | | 476 | -1,091.74 | 1.17 | 0.00 | 0,00 | 0.00 | |
| | | 477 | 1,091.74 | -1.17 | 0.00 | 0,00 | 0.00 | 141-14 |
| | siya ing 🕇 lang | 476 477 | 689.79 -689.79 | -0.74 0.74 | 0.00 0.00 | 0.00 0.00 | 0,00 0,00 | |
| | | 476 | 22.89 | -0.05 | 0.00 | 0.00 | 0.00 | |
| | un de la parte de la parte 1973 - La companya de la parte 1973 - La companya de la parte | 477 | -22.89 | 0.05 | 0.00 | 0.00 | 0.00 | |
| 476 | 1 | 477 | -1,091,74 | 0.07 | 0.00 | 0.00 | 0.00 | |
| | | 478 | 1,091.74 | -0.07 | 0.00 | 0.00 | 0.00 | |
| | 2 | 477 478 | 689.79 -689.79 | -0.04 0.04 | 0,00 0,00 | 0.00 | 0.00 0.00 | |
| | 3 | 477 | 22.89 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | | 478 | -22.89 | 0.00 | 0.00 | 0,00 | 0.00 | |
| 477 | $\frac{1}{2}$ | 478 | -1,091.74 | -0.47 | 0.00 | 0.00 | 0.00 | |
| | | 479 | 1,091,74 | 0.47 | 0.00 | 0.00 | 0.00 | с. К. |
| हाओं कि दुख्यां के के जन्म संस्थित के सामग्र | 2 | 478 479 | 689.78 -689.78 | 0.30 -0.30 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | . i. 1994 - |
| | 3 | 478 | 22.89 | 0.02 | 0.00 | 0.00 | 0.00 | |
| | | 479 | -22.89 | -0.02 | 0.00 | 0.00 | 0.00 | |
| 478 | | 479 | -1,091.74 | -0.63 | 0.00 | 0.00 | 0.00 | |
| | 2 | 480 479 | 1,091.74 689.79 | 0.63 0.40 | 0.00 0,00 | 0.00 0.00 | 0.00 | in ag |
| | | 480 | -689.79 | -0.40 | 0.00 | 0.00 | 0.00 | |
| | 3 | 479 | 22.89 | 0.03 | 0.00 | 0.00 | 0.00 | |
| | | 480 | -22.89 | -0.03 | 0.00 | 0.00 | 0.00 | |
| 479 | 1 | 480 | -1,091.74 | -0.58 | 0.00 | 0.00 | 0.00 | |
| | | 481 | 1,091.74 | 0.58 | 0.00 | 0.00 | 0.00 | |
| | 2 | 480 481 | 689.78 -689.78 | 0.37 -0.37 | 0.00 0.00 | 0,00 0,00 | 0.00 0.00 | an an Seo tao |
| | 3 | 480 | 22.89 | 0.02 | 0.00 | 0.00 | 0.00 | |
| | | 481 | -22.89 | -0.02 | 0.00 | 0.00 | 0.00 | |
| 480 | 1 | 481 | -1,091.74 | -0.45 | 0.00 | 0,00 | 0.00 | |
| | | 482 481 | 1,091.74 689.78 | 0.45 | 0.00 | 0.00 | 0.00 | |
| | 2 | 481 | -689.78 | 0,28 -0.28 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | |
| | 3 | 481 | 22.89 | 0.02 | 0.00 | 0.00 | 0.00 | |
| | | 482 | -22.89 | -0.02 | 0.00 | 0.00 | 0.00 | |
| 481 | 1 | 482 | -1,091.74 | -0.30 | 0.00 | 0.00 | 0.00 | |
| | | 483 | 1,091.74 | 0.30 | 0,00 | 0.00 | 0,00 | |
| | 2 | 482 483 | 689.79 -689,79 | 0.19 | 0.00 | 0.00 | 0.00 | |
| | 3 | 483 482 | -089,79 | -0.19 0.01 | 0,00 0.00 | 0.00 0.00 | 0.00 | |
| | and a second br>Second second | 483 | -22.89 | -0.01 | 0,00 | 0,00 | 0.00 | |
| 482 | | 483 | -1.091.74 | -0.17 | 0.00 | 0.00 | 0.00 | |
| | 가지, 2013년 1월 12년 역사 1일 - 1913년 1월 12년 | 484 | 1,091.74 | 0.17 | 0.00 | 0.00 | 0.00 | |
| | 2 | 483 | 689,79 | 0.11 | 0.00 | 0.00 | 0.00 | |
| | 3 | 484 483 | -689.79 22.89 | -0.11 0.01 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | |
| 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - | an tha an the state of the stat | 484 | -22.89 | -0.01 | 0.00 | 0.00 | 0.00 | |

| ob No. : | : , , , i haa | algned by : | | and and have | le le | le i stati | | |
|---|---|-------------|-----------------------|---------------|--------------|--------------|---------------|----------------|
| | | NCHOS DY : | na si aka ta | ecked by : | Hara ta Ar | | January 23, 2 | 000 |
| | | | TEMPER | ATURE LO | DADS | | | |
| MEMB | LOAD | NODE | ÂXÎAL | SHEAR-Y | SHEAR-Z | TORSION | MOM-Y | МОМ |
| 483 | 1 | 484 | -1,091.74 | -0.08 | 0.00 | 0.00 | 0.00 | 0.0 |
| | | 485 | 1,091.74 | 0.08 | 0.00 | 0.00 | 0,00 | -0.1 |
| | 2 | 484 | 689,79 -689,79 | 0.05 | 0,00 | 0.00 | 0.00 | -0.0 |
| | 3 | 484 | -089.79 | -0.05 0.00 | 0,00 | 0.00 | 0.00 | 0.1 |
| | | 485 | -22.89 | 0.00 | 0.00 | 0,00 | 0.00 | 0,0 |
| | | | | a attraction | | 0.00 | 0.00 | 0.0 |
| 484 | 1 | 485 | -1,091.74 | -0.02 | 0.00 | 0.00 | 0.00 | 0.1 |
| | | 486 | 1,091.74 | 0.02 | 0.00 | 0.00 | 0.00 | -0.2 |
| | 2 | 485 486 | 689.78 -689.78 | 0.01 | 0.00 | 0.00 | 0.00 | -0.1 |
| $= - \kappa_{\mu} (k_{\mu}) + (k_{\mu} - k_{\mu}) + (k_{\mu} -$ | 3 | 485 | 22.89 | -0.01 0,00 | 0,00 0.00 | 0.00 | 0.00 | 0,1 |
| | · 문양 전 11 년 11 년 · 제품: | 486 | -22.89 | 0.00 | 0.00 | 0.00 | 0.00 0.00 | -0.0 |
| | | | | | | 0.00 | 0.00 | 0.0 |
| 485 | 1 | 486 | -1,091,74 | 0.01 | 0.00 | 0.00 | 0.00 | 0.2 |
| | | 487 | 1,091.74 | -0.01 | 0.00 | 0.00 | 0.00 | -0.2 |
| | 2 | 486 | 689.78 | -0.01 | 0.00 | 0.00 | 0.00 | -0.1 |
| george (sp. 1945). | 3 | 487 486 | -689.78 22,89 | 0.01 | 0.00 | 0.00 | 0.00 | 0.1 |
| | | 480 | -22.89 | 0.00 0.00 | 0.00 | 0.00 | 0.00 | -0.0 |
| | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.0 |
| 486 | 1 | 487 | -1,091.74 | 0.03 | 0.00 | 0.00 | 0.00 | 0.2 |
| na se por se anno 1978. An factoria de la trace | | 488 | 1,091.74 | -0.03 | 0.00 | 0.00 | 0.00 | -0.1 |
| | 2 | 487 | 689.78 | -0.02 | 0.00 | 0,00 | 0.00 | -0,1 |
| | | 488 | -689.78 | 0,02 | 0.00 | 0.00 | 0.00 | 0.1 |
| | 3 | 487 | 22.89 | 0.00 | 0.00 | 0.00 | 0.00 | -0.0 |
| | | 488 | -22.89 | 0.00 | 0.00 | 0.00 | 0,00 | 0.0 |
| 487 | 1 | 488 | . 1,091.74 | 0.03 | 0.00 | 0.00 | | |
| | | 489 | 1,091.74 | -0.03 | 0.00 | 0.00 | 0.00 | 0.1 |
| | 2 | 488 | 689.78 | -0.02 | 0.00 | 0.00 | 0.00 0,00 | -0.10 -0.10 |
| Read States | | 489 | -689,78 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3 | 488 | 22.89 | 0.00 | 0.00 | 0.00 | 0.00 | -0.01 |
| | | 489 | -22.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 488 | | 489 | -1,091.74 | 0.07 | • • • | | | e Sante |
| 2.00 | | 407 | 1,091.74 | 0.02 -0.02 | 0.00 | 0.00 | 0.00 | 0.10 |
| | 2 | 489 | 689.78 | -0.02 | 0.00 0.00 | 0.00 0.00 | 0.00 | -0.05 |
| | | 490 | -689.78 | 0.01 | 0.00 | 0.00 | 0.00 0.00 | -0.06 |
| | 3 | 489 | 22.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| en de l'Arrie de la celegi. Aux d'Arren de Rome | | 490 | -22.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | | | | | | | |
| 489 | $1_{\mathcal{K}} \rightarrow 1_{\mathcal{K}}$ | 490 | -1,091.74 | 0.02 | 0.00 | 0.00 | 0.00 | 0.05 |
| | 2 | 491 | 1,091,74 | -0.02 | 0.00 | 0.00 | 0.00 | -0.02 |
| | 1995 - 1 995 | 490 491 | 689.79 -689.79 | -0.01 0.01 | 0.00 | 0.00 | 0.00 | -0.03 |
| 이번 영국 소리 | | 490 | 22,89 | 0.00 | 0.00 0.00 | 0.00 | 0.00 | 0,01 |
| | | 491 | -22.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | | | | | | 0.00 | 0.00 |
| 490 | 1 | 491 | -1,091.74 | 0.01 | 0,00 | 0.00 | 0.00 | 0.02 |
| | | 492 | 1,091.74 | -0.01 | 0.00 | 0.00 | 0.00 | 0.01 |
| | 2 | 491 | 689.78 | -0.01 | 0.00 | 0.00 | 0.00 | -0.01 |
| | | 492 | -689.78 | 0.01 | 0.00 | 0.00 | 0.00 | -0.01 |
| | 1998 - 199 8 - 1997 | 491 | 22.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | 492 | -22.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 491 | 1 + 1 + 1 | 492 | -1,091.74 | 0.01 | 0.00 | 0,00 | 0.00 | |
| | | 470 | 1,091.74 | -0.01 | 0.00 | 0,00 | 0.00 0.00 | -0.01 |
| 化学型数据中心分子的 | 2 | 492 | 689.78 | -0.01 | 0,00 | 0.00 | 0.00 | 0.03 |
| | | 470 | -689.78 | 0.01 | 0.00 | 0.00 | 0.00 | -0.02 |
| | 3 | 492 | 22.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0,00 |
| | t Asia (Fisher) | 470 | -22,89 | . 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | | | | | | | |
| 492 | - 69 a 1 | 470 | -1,091,74 | 0.01 | 0.00 | 0.00 | 0.00 | -0.03 |
| | | 493 | 1,091.74 | -0.01 | 0.00 | 0.00 | 0.00 | 0,05 |
| | 4 | 470 493 | 689.78 -689.78 | -0.01 | 0.00 | 0.00 | 0.00 | 0.02 |
| 요즘 영화 영화 | | 493 470 | -087.78 22.89 | 0.01 0.00 | 0.00 | 0.00 | 0.00 | -0.03 |
| 이 물건 가지? | 영양 아이 아이아 | 493 | -22.89 | 0.00 | 0.00 | 0,00 | 0.00 | 0.00 |
| | | 174 | | 0,00 | 0,00 | 0.00 | 0.00 | 0.00 |

Pacific Consultants International of Japan, Third Floor, Bldg.# 47 DDC Center, Mokhali, Dhaka1212

•

ob No.

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Checked by :

Designed by :

Date :

• January 23, 2000

TEMPERATURE LOADS

| MEMB | LOAD NODE | AXIAL | SHEAR-Y | SHEAR-Z | TORSION | MOM-Y | МОМ |
|------------|----------------|-----------------------|-------------------|--------------|--------------|--------------|---|
| 494 | 1 494 | 1,356.35 | 202,81 | 0.00 | 0.00 | 0.00 | 2,919.6 |
| | 495 | -1,356.35 | -202,81 | 0.00 | 0.00 | 0.00 | -1,092.0 |
| and a Twee | 2 494 | -856,85 | -128.25 | 0.00 | 0.00 | 0.00 | -1,841.9 |
| | 495 | 856.85 | 128,25 | 0.00 | 0.00 | 0.00 | 688.0 |
| | 3 494 495 | -42.95 42.95 | -9,04 9,04 | 0,00 | 0.00 0.00 | 0.00 | -133.6 52.2 |
| | | | | | | | |
| 495 | 1 495 496 | 1,356.35 -1,356.35 | 202,81 -202.81 | 0,00 0,00 | 0.00 | 0.00 0.00 | 1,092,0 1,955.0 |
| | 2 495 | -856.85 | -128.25 | 0.00 | 0.00 | 0.00 | -688.0 |
| | 496 | 856.85 | 128.25 | 0.00 | 0.00 | 0.00 | -1,233. |
| | 3 495 | -42.95 | -9.04 | 0.00 | 0.00 | 0.00 | -52. |
| | 496 | 42.95 | 9.04 | 0.00 | 0.00 | 0.00 | -83. |
| 496 | 1 496 | 1,356.35 | 145.98 | 0.00 | 0.00 | 0.00 | -1,955. |
| | 498 | -1,356.35 | -145.98 | 0.00 | 0.00 | 0.00 | 2,174. |
| | 2 496 | -856.85 | -92.41 | 0.00 | 0.00 | 0.00 | 1,233. |
| | 498 | 856.85 | 92.41 | 0.00 | 0.00 | 0.00 | -1,371. |
| | 3 496 498 | -42.95 42.95 | -6.56 6.56 | 0,00 0,00 | 0.00 0.00 | 0,00 0.00 | 83. -93. |
| | | | | | | | ere e di e più la contra di Stato di anti- |
| 497 | 1 498 | 1,356.36 | 56.61 | 0.00 | 0.00 | 0.00 | -2,174 |
| | 499 | -1,356.36 | -56.61 | 0.00 | 0.00 | 0.00 | 2,259 |
| | 2 498 499 | +856.85 856.85 | -36.00 36.00 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | 1,371 -1,425 |
| | 3 498 | -42.95 | -2.67 | 0.00 | 0.00 | 0.00 | 93 |
| | 499 | 42.95 | 2.67 | 0.00 | 0.00 | 0.00 | -97 |
| 498 | 1 499 | 1,356.35 | -11.37 | 0.00 | 0.00 | 0.00 | -2,259 |
| | 500 | -1,356.35 | 11.37 | 0.00 | 0.00 | 0.00 | 2,242 |
| | 2 499 | -856.85 | 6.90 | 0.00 | 0.00 | 0.00 | 1,425 |
| | 500 | 856.85 | -6.90 | 0.00 | 0.00 | 0,00 | -1,415 |
| | 3 499 500 | -42.95 42.95 | 0.30 -0.30 | 0.00 0.00 | 0.00 0.00 | 0.00 | 97 -96 |
| 400 | 600 | 1,356.36 | -60.95 | 0,00 | 0.00 | 0.00 | -2,242 |
| 499 | 1 500 501 | •1,356.36 | 60,95 | 0.00 | 0.00 | 0.00 | -2,242 |
| | 2 500 | -856.86 | 38.23 | 0.00 | 0.00 | 0.00 | 1,414 |
| | Geo. 501 | 856.86 | -38.23 | 0.00 | 0.00 | 0.00 | -1,357 |
| | 3 500 501 | -42.95 42.95 | 2.47 -2.47 | 0,00 0,00 | 0.00 0.00 | 0.00 0.00 | 96 -92 |
| | 100 | 42,73 | - 4.4 7 | | v.vv | | |
| 500 | 1 501 | 1,356.35 | -95.27 95.27 | 0.00 0.00 | 0.00 0.00 | 0,00 0.00 | -2,151 |
| | 2 502 2 501 | -1,356.35 -856.86 | 59.92 | 0.00 | 0,00 | 0.00 | 2,009 1,357 |
| | 502 | 856.86 | -59.92 | 0.00 | 0.00 | 0.00 | -1,267 |
| | 3 501 | -42.95 | 3.98 | 0.00 | 0.00 | 0.00 | 97 |
| | SO2 | 42.95 | -3.98 | 0.00 | 0.00 | 0.00 | -87 |
| 501 | 1 502 | 1,356.36 | -123.57 | 0,00 | 0.00 | 0.00 | -2,009 |
| | 503 | -1,356.36 | 123.57 | 0.00 | 0.00 | 0.00 | 1,823 |
| | 2 502 | -856.85 | 77.79 | 0,00 | 0.00 | 0.00 | 1,267 |
| | 503 3 502 | 856.85 -42.95 | -77,79 5.23 | 0,00 0,00 | 0.00 | 0.00 0.00 | -1,150 81 |
| | 503 | 42.95 | -5.23 | 0.00 | 0.00 | 0,00 | -79 |
| 607 | | 1 Act - | 160.00 | 6 6 6 | á na | e | 14 |
| 502 | 1 503 504 | 1,356.37 -1,356.37 | -166.25 166.25 | 0.00 0.00 | 0,00 0.00 | 0.00 0.00 | •1,823 1,574 |
| | 2 503 | -856.85 | 104.78 | 0,00 | 0.00 | 0.00 | 1,150 |
| | 504 | \$56.85 | -104.78 | 0.00 | 0.00 | 0.00 | -993 |
| | 3 503 | -42.95 | 7.12 | 0.00 | 0.00 | 0.00 | 79 41 |
| | 504 | 42.95 | -7.12 | 0.00 | 0.00 | 0.00 | -68 |
| 503 | 1 504 | 1,356.35 | -184.22 | 0.00 | 6,00 | 0,00 | -1,574 |
| | 505 | -1,356.35 | 184,22 | 0.00 | 0.00 | 0.00 | 1,298 |
| | 2 504 505 | -856.85 856.85 | 116.14 -116.14 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | 99. -819 |
| | 3 504 | -42.95 | 7,93 | 0.00 | 0.00 | 0.00 | -91 |
| | 505 | 42,95 | -7,93 | | 0,00 | 0.00 | -56 |

| b N6, 1 | | Desig | med by : | Ch | cked by : | Da | te : | January 23, 2 | 1000 |
|--|--|---------------------------------------|--------------|---------------------------------------|-------------------|--------------|--------------|---------------|----------------|
| | | | | TEMPER | ATURE L | DADS | | | |
| | MEMB | LOAD | NODE | AXIAL] | SHEAR-Y | SHEAR-Z | TORSION | MOM-Y | MOM |
| | 504 | 1 | 505 | 1,356.35 | -185.10 | 0.00 | 0,00 | 0.00 | •1,298.3 |
| | | | 506 | -1,356,35 | 185,10 | 0,00 | 0.00 | 0.00 | 1,020.7 |
| | - N | 2. | 505 | -856,86 | 116.74 | 0.00 | 0.00 | 0.00 | 819.3 |
| 9 - E | e per l'estre | 1 | 506 505 | 856.86 -42.95 | -116.74 8.01 | 0,00 | 0,00 0,00 | 0.00 | -644 |
| | | | 506 | 42.95 | -8.01 | 0.00 | 0,00 | 0.00 | 56. -44. |
| | 505 | 1 | 506 | 1,356.36 | -171.56 | 0.00 | 0.00 | 0.00 | -1,020. |
| PERALA SPECIAL | | | 507 | -1,356.36 | 171.56 | 0.00 | 0.00 | 0.00 | 763.4 |
| | | 2 | 506 | -856.85 | 108.22 | 0,00 | 0.00 | 0.00 | 644. |
| e di g | | | 507 | 856.85 | -108.22 | 0.00 | 0.00 | 0.00 | -481.5 |
| d Atio | | 3 | 506 507 | -42.95 42.95 | 7.44 | 0,00 0,00 | 0.00 | 0.00 | 44.5 -33.4 |
| | | | | | | 0,00 | 0.00 | 0.00 | |
| | 506 | 1 | 507 | 1,356.35 | -149.88 | 0.00 | 0.00 | 0,00 | -763.4 |
| 24.992 24.992 | | | 508 | -1,356.35 | 149.88 | 0.00 | 0.00 | 0.00 | 538.6 |
| et de l | | 2 | 507 508 | -856.85 | 94,56 -94,56 | 0.00 | 0.00 | 0,00 | 481.9 |
| | | 3 | 508 | 856.85 | -94.36 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | -340.0 33.4 |
| uri de la Naciona | | | 508 | 42.95 | -6.52 | 0.00 | 0.00 | 0.00 | -23.6 |
| ing Sing i Tanàng | | | | | | | | | |
| | 507 | | 508 509 | 1,356.35 | -124.79 124.79 | 0,00 0.00 | 0.00 | 0.00 | -538.6 |
| 89,44 | 1999 - | 2 | 508 | -856.86 | 78.75 | 0.00 | 0.00 | 0.00 | 351.4 340.0 |
| | | | 509 | 856.86 | -78.75 | 0.00 | 0.00 | 0,00 | +221.9 |
| Profession Calific S | | 3 | 508 | -42.95 | 5.44 | 0,00 | 0.00 | 0.00 | 23.6 |
| (***) {***, -1, | | | 509 | 42.95 | -5.44 | 0.00 | 0.00 | 0.00 | -15.4 |
| an di b | 508 | 1 | 509 | 1,356.35 | -99.65 | 0.00 | 0.00 | 0.00 | -351.4 |
| | | | 510 | -1,356.35 | 99.65 | 0.00 | 0.00 | 0.00 | 201.9 |
| 54 534 19 5 1 | | 2 | 509 | -856.85 | 62.90 | 0.00 | 0.00 | 0.00 | 221.9 |
| in C | | | 510 | 856,85 | -62.90 | 0.00 | 0.00 | 0.00 | -127.5 |
| store - | | 3 | 509 510 | -42.95 42.95 | 4.35 -4.35 | 0.00 | 0.00 | 0.00 | 15.4 |
| | | | | · · · · · · · · · · · · · · · · · · · | | 0.00 | 0.00 | 0.00 | •8.9 |
| n da Geologia | 509 | 1 | 510 | 1,356.35 | -76.66 | 0.00 | 0.00 | 0.00 | -201.9 |
| | | | 511 | -1,356.35 | 76.66 | 0.00 | 0.00 | 0.00 | 86.9 |
| 25 Ø ¹⁴ | | 2 | 510 511 | -856.85 856.85 | 48.39 -48.39 | 0,00 | 0.00 | 0.00 | 127.5 |
| | | 3 | 510 | -42,95 | 3,35 | 0.00 0,00 | 0.00 0.00 | 0.00 | -55.0 |
| ing Alai | 김 나는 것을 | | 511 | 42.95 | -3.35 | 0.00 | 0.00 | 0.00 | 8.9 -3.9 |
| | 510 | | 611 | 36 336 1 | 67.00 | 0.00 | 0.00 | | |
| R. (| 310 | • | 511 512 | 1,356.35 | -57.09 57.09 | 0.00 | 0.00 | 0.00 | -86.9 |
| 연수가 | | 2 | 511 | -856.85 | 36.05 | 0.00 | 0.00 | 0.00 | 1.2 55.0 |
| an sei Station | | | 512 | 856.85 | -36.05 | 0.00 | 0.00 | 0.00 | -0,9 |
| 01.9 (11.9) | | 3 | S11 | -42.95 | 2.50 | 0.00 | 0.00 | 0.00 | 3.9 |
| | an an an | | 512 | 42.95 | -2.50 | 0.00 | 0.00 | 0.00 | -0.1 |
| | 511 | 1 | 512 | 1,356.35 | -41.50 | 0.00 | 0.00 | 0.00 | -1.2 |
| | | | 513 | -1.356.35 | 41.50 | 0.00 | 0.00 | 0.00 | -60.9 |
| 3135 6515 (| | 2 | 512 | -856.86 | 26.21 | 0.00 | 0.00 | 0.00 | 0.9 |
| | | 3 | 513 | \$56.86 | -26.21 | 0.00 | 0.00 | 0.00 | 38.3 |
| 1.9 | | | 512 513 | -42,95 42.95 | 1.83 -1.83 | 0.00 | 0.00 | 0.00 0.00 | 0.1 |
| S €. | | | | | | | | 0.00 | 2.5 |
| | 512 | 1 | 513 | 1,356.36 | -26.08 | 0.00 | 0,00 | 0.00 | 60.9 |
| | | en al anti- a la companya di seria | 514 | -1,356.36 | 26.08 | 0.00 | 0.00 | 0,00 | -100,1 |
| 3.2.2 | (d) | N 4 (| \$13 \$14 | -856.85 856.85 | 16.48 -16.48 | 0.00 | 0.00 | 0.00 | -38.38 |
| | | 3 1 | 513 | -42.95 | 1.15 | 0.00 | 0.00 0,00 | 0.00 | 63.10 -2.51 |
| NG ALT BRID | e de la composition Constanta de | | 514 | 42.95 | 4 -1,15 | 0.00 | 0.00 | 0.00 | 4.3 |
| | | | | | | | | | 1.57 |
| | 513 | 1 | \$14 414 | 1,356.36 | -15.55 | 0.00 | 0.00 | 0.00 | 100.11 |
| | | 2 | 515 514 | -1,356.36 -856.85 | 15.55 9.84 | 0.00 0.00 | 0.00 0.00 | 0.00 | -123.4 |
| | Č. | . | - 515 | 856.85 | -9.84 | 0.00 | 0.00 | 0.00 | -63.10 77.8 |
| | | s | 514 | -42.95 | 0.69 | 0.00 | 0.00 | 0.00 | -4.30 |
| an a | | N | 515 | 42.95 | -0.69 | 0.00 | 0.00 | 0.00 | 5.3 |

| 1.1.1 | Designed | l by s |
|-------|----------|--------|

ob No.

Checked by :

January 23, 2000

Date :

| | | | TEMPERA | ATURE LO | DADS | | | |
|--|----------------------|-------------|--------------------------|-----------------|--------------|--------------|--------------|------------------|
| мемв | LOAD | NODE | AXIAL | SHEAR-Y | SHEAR-Z | TORSION | MOM-Y | MOM-Z |
| 514 | | 515 | 1,356.36 | 3,64 | 0.00 | 0,00 | 0.00 | 123,45 |
| | | 497 | -1,356.36 | -3.64 | 0,00 | 0,00 | 0.00 | -118.00 |
| | 2 | 515 | -856.85 | -2.28 | 0.00 0,00 | 0.00 | 0.00 0.00 | -77.85 |
| | | 497 515 | 856.85 -42.95 | 2,28 -0,15 | 0.00 | 0,00 | 0.00 | 74.43 •5.34 |
| | с с с с | 497 | 42.95 | 0.15 | 0.00 | 0.00 | 0.00 | 5.12 |
| 515 | 1 | 497 | 1,356.35 | 13.55 | 0.00 | 0.00 | 0.00 | 118.00 |
| | | 517 | -1,356.35 | -13.55 | 0,00 | 0.00 | 0.00 | -90,92 |
| | 2 | 497 | -856.85 | -8.54 | 0.00 | 0.00 | 0.00 | -74,43 |
| | | 517 | 856.85 | 8.54 -0.58 | 0.00 0.00 | 0.00 0.00 | 0,00 0.00 | 57.36 -5.12 |
| | 3 | 497 517 | -42.95 42.95 | 0.58 | 0.00 | 0.00 | 0.00 | 3.96 |
| 516 | | 517 | 1,356.35 | 15.40 | 0,00 | 0.00 | 0.00 | 90.92 |
| 1910 1917 - 1917 - 1919 | | 518 | -1,356.35 | -15.40 | 0.00 | 0.00 | 0.00 | -60.13 |
| | 2 | 517 | -856.85 | -9 71 | 0.00 | 0.00 | 0.00 | -57.36 |
| | | 518 | 856.85 | 9.71 | 0.00 | 0.00 | 0.00 | 37.94 |
| | 3 3 1 | 517 | -42.95 | -0.67 | 0.00 | 0.00 | 0,00 0.00 | -3.96 |
| | | 518 | 42.95 | 0.67 | 0.00 | 0.00 | | 2.62 |
| 517 | | 518 | 1,356.35 | 13.11 | 0.00 | 0.00 | 0.00 | 60.13 |
| an 1999. Ng taong | | 519 518 | -1,356.35 -856.86 | -13.11 -8.27 | 0,00 0.00 | 0.00 0.00 | 0.00 0.00 | -33.92 -37.94 |
| | an an tha 🕈 an a | 518 | 856.86 | 8.27 | 0.00 | 0.00 | 0.00 | 21.41 |
| | 3 | 518 | -42.95 | -0.57 | 0.00 | 0.00 | 0.00 | -2.62 |
| | | \$19 | 42.95 | 0.57 | 0.00 | 0.00 | 0.00 | 1.48 |
| 518 | 1 | 519 | 1,356.35 | 9.32 | 0,00 | 0.00 | 0.00 | 33.92 |
| | | 520 | -1,356.35 | -9.32 | 0.00 | 0.00 | 0.00 | -15.29 |
| | 2 | 519 520 | -856.85 856.85 | -5.88 5.88 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | -21.41 9.65 |
| | 3 - 1 - 3 - 1 | 519 | -42.95 | -0.41 | 0.00 | 0.00 | 0.00 | -1.48 |
| | | 520 | 42.95 | 0.41 | 0.00 | 0.00 | 0.00 | 0.67 |
| 519 | 1. 1. 1. 1. 1. | 520 | 1,356.36 | 5.88 | 0.00 | 0.00 | 0.00 | 15.29 |
| | | 52 1 | -1,356.36 | -5.88 | 0.00 | 0,00 | 0.00 | -3.53 |
| | 2 | 520 | -856.85 856.85 | -3.71 3.71 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | -9.65 2.24 |
| | 3 | 521 520 | -42.95 | -0.26 | 0.00 | 0.00 | 0.00 | -0.67 |
| | | 521 | 42.95 | 0.26 | 0.00 | 0.00 | 0.00 | 0.16 |
| 520 | 1 | 521 | 1,356.35 | 3.12 | 0.00 | 0.00 | 0.00 | 3.53 |
| | | 522 | -1,356.35 | -3.12 | 0.00 | 0.00 | 0.00 | 2.70 |
| | 2 | 521 | -856.85 | -1.97 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | -2.24 +1.70 |
| | 3 | 522 521 | \$56.85 -42.95 | .1,97 -0.14 | 0.00 | 0.00 | 0.00 | -0.16 |
| | | 522 | 42.95 | 0.14 | 0.00 | 0.00 | 0.00 | -0.11 |
| 521 | 1 | 522 | 1,356,35 | 1.21 | 0.00 | 0.00 | 0.00 | -2.70 |
| | | 523 | -1,356.35 | -1.21 | 0.00 | 0.00 | 0.00 | 5.12 |
| | 2 | 522 | -856.85 | -0,76 | 0.00 | 0.00 | 0.00 | 1.70 |
| | 3 | 523 522 | 856.85 -42.95 | 0.76 -0.05 | 0.00 0.00 | 0.00 0,00 | 0.00 0.00 | -3.23 0.11 |
| | | 523 | 42,95 | 0.05 | 0.00 | 0.00 | 0.00 | -0.22 |
| 522 | анала 1993 г. – Т | 523 | 1,356.35 | 0.08 | 0,00 | 0.00 | 0.00 | -5,12 |
| | Start, N | 524 | -1,356.35 | -0.08 | 0.00 | 0.00 | 0.00 | 5.27 |
| | 2 | 523 | -856.86 | -0.05 | 0.00 | 0.00 | 0.00 | 3.23 |
| | | 524 | 856.86 | 0.05 | 0.00 | 0.00 | 0.00 | -3.32 |
| | 3 | 523 524 | -42.95 42.95 | 4 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 | 0.22 -0.23 |
| | | | 1,356.35 | | | | 0.00 | |
| 523 | | 524 525 | -1,356.35 | -0.47 0.47 | 0.00 | 0.00 0.00 | 0.00 | -5.27 4.32 |
| | 2 • | 524 | -856.85 | 0.30 | 0.00 | 0.00 | 0.00 | 3.32 |
| | | 525 | 856.85 | -0.30 | 0,00 | 0.00 | 0.00 | -2.73 |
| | 3 3 - | 524 | -42.95 42.95 | 0.02 | 0.00 | 0.00 0.00 | 0.00 | 0.23 |
| | | 525 | 42.33 | -0,02 | 0.00 | V.00 | 0.00 | -0.19 |

Pacific Consultants International of Japan, Third Floor, Bldg.# 47 DDC Center, Mokhali, Dhaka1212

ob No. Date : Designed by Checked by : January 23, 2000 **TEMPERATURE LOADS** MEMB LOAD NODE AXIAI. SHEAR-Y SHEAR-Z TORSION MOM-Y MOM-Z 524 1 525 1,356.36 -0.64 0.00 0.00 0.00 -4.32 526 -1,356.36 0.64 0.00 0.00 0.00 3.04 2 525 -856.86 0.40 0.00 0.00 0.00 2.73 526 856.86 -0.40 0.00 0.00 0.00 -1.92 3 525 -42,95 0.03 0.00 0.00 0.00 0.19 526 -0.03 42.95 0.00 0.00 0.00 -0.13 525 526 1 1.356.35 -0.60 0.00 0.00 0.00 -3.04 527 1,356.35 0.60 0.00 0.00 0.00 1.84 2 526 -856,85 0.38 0.00 0.00 0.00 1,92 527 856.85 -0.38 0.00 0.00 0.00 -1.16 3 \$26 -42.95 0.03 0.00 0.00 0.00 0.13 527 42.95 -0.03 0.00 0.00 0.00 -0.08 \$26 1 527 1.356.36 -0.46 0.00 0.00 0,00 -1.84 528 -1.356.36 0.46 0.00 0.00 0.00 0.92 2 527 -856.85 0.29 0.00 0.00 0.00 1.16 528 856,85 -0.29 0.00 0.00 0.00 -0.58 -3 527 -12.95 0.02 0.00 0.00 0.00 0.08 528 42.95 -0.02 0.00 0.00 0,00 -0.04 527 1 528 1,356.35 -0.31 0.00 0.00 0.00 -0.92 529 -1,356.35 0.31 0.00 0.00 0.00 0.31 2 528 -856.85 0.19 0.00 0.00 0.00 0.58 $^{*}C$ 529 856.85 -0.19 0.00 0.00 0,00 -0 20 3 528 -42.95 0.01 0.00 0.00 0.00 0.04 529 42.95 -0.01 0.00 0.00 0.00 -0.01 528 I 529 1,356.36 -0.18 0.00 0.00 0.00 -0.31 \$30 -1.356.36 0.18 0.00 0.00 0.00 -0.04 ų. 2 529 -856.85 Õ.11 0.00 0.00 0.00 0.20 245 530 \$56.85 -0.11 0.00 0.00 0.00 0.03 3 529 42.95 0.01 0.00 0.00 0.00 0.01 $\gtrsim 100$ 530 42.95 -0.01 0.00 0.00 0.00 0.00 529 1 530 1 356 35 -0.08 0.00 0.00 0.00 0.04 \$31 -1.356.35 0.08 0.00 0.00 0.00 -0.20 2 530 -856.85 0.05 0.00 0.00 0.00 -0.03 531 856.85 -0.05 0.00 0.00 0.00 0.13 3 530 -42.95 0.00 0.00 0.00 0.00 0.00 531 42.95 0.00 0.00 0.00 0.00 0.01 530 1 531 1,356.36 -0,02 0.00 0.00 0,00 0.20 532 -1,356.36 0.02 0.00 0.00 0,00 -0.24 2 531 -856 85 0.01 0.00 0.00 0.00 -0.13 532 856.85 -0.01 0.00 0.00 0.00 0.15 3 531 -42.95 0.00 0.00 0.00 0.00 -0,01 532 42.95 0.00 0.00 0.00 0,00 0.01 531 1 532 1 356 35 0.01 0.00 0.00 0.00 0.24 \$33 -1,356.35 0.01 0.00 0.00 0.00 -0.21 2 532 -856.85 -0.01 0.00 0.00 0.00 -0.15 533 856.85 0.01 0.00 0.00 0.00 0.13 3 532 -42.95 0.00 0.00 0.00 0.00 -0 01 533 42.95 0.00 0.00 0.00 0.00 0.01 532 j 533 1,356.35 0.03 0.00 0.00 0.00 0.21 \$34 -135635 -0.03 0.00 0.00 0.00 -0.16 2 533 -856.85 -0,02 0.00 0.00 0.00 -0.13 534 856:85 0.02 0.00 0.00 0,10 0.00 3 533 -42.95 ,0.00 0.00 0.00 0.00 -0.01 534 42.95 0.00 0.00 0,00 0.00 0.01 533 1 534 1,356.35 0.03 0.00 0.00 0,00 0.16 535 1,356.35 -0.03 0.00 0.00 0.00 -0.10 2 534 -856.85 -0.02 0.00 0.00 0.00 -0.10 535 856.85 0.02 0.00 0.00 0.00 0.06 'n 534 42.95 0.00 0,00 0.00 0.00 -0.01 535 42.95 0.00 0.00 0.00 0.00 0.00

Pacific Consultants International of Japan, Third Floor, Bldg.# 47 DDC Center, Mokhali, Dhaka 1212

Checked by :

ob No. :

Designed by 1

TEMPERATURE LOADS

Date :

January 23, 2000

| MOM-Z | MOM-Y | TORSION | SHEAR-Z | SHEAR-Y | AXIAL | NODE | LOAD | MEMB |
|-------|-------|---------|---------|---------|-----------|------|-------------------|-------|
| 0.10 | 0.00 | 0.00 | 0,00 | 0.02 | 1,356.35 | \$35 | | 534 |
| -0.06 | 0,00 | 0.00 | 0,00 | -0.02 | -1,356.35 | 536 | la segui de la ca | +66 |
| -0.06 | 0.00 | 0.00 | 0.00 | -0.01 | -856.85 | 535 | | |
| 0.03 | 0.00 | 0.00 | 0.00 | 0.01 | 856.85 | 536 | 4 | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -42.95 | 535 | 3 | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0,00 | 42.95 | 536 | | |
| 0.06 | 0.00 | 0.00 | 0,00 | 0.02 | 1,356.35 | \$36 | 1 | \$35 |
| -0.02 | 0.00 | 0.00 | 0.00 | -0.02 | -1,356.35 | 537 | | |
| -0.03 | 0.00 | 0.00 | 0.00 | -0.01 | -856.85 | 536 | 2 | |
| 0.01 | 0.00 | 0.00 | 0.00 | 0.01 | 856.85 | 537 | na keto di Esper | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -42.95 | \$36 | 3 | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.95 | \$37 | | |
| 0.0 | 0.00 | 0.00 | 0.00 | 0.01 | 1,356.35 | 537 | 1 | 536 |
| 0.0 | 0.00 | 0.00 | 0.00 | -0.01 | -1,356.35 | \$38 | | |
| -0.0 | 0.00 | 0.00 | 0.00 | -0.01 | -856.85 | 537 | 2 | |
| -0.0 | 0.00 | 0.00 | 0,00 | 0.01 | 856.85 | 538 | | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -42.95 | 537 | 3 | |
| 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | 42.95 | 538 | | |
| -0.0 | 0.00 | 0.00 | 0.00 | 0.01 | 1,356.35 | 538 | ı - | 537 |
| 0.0. | 0.00 | 0.00 | 0.00 | -0.01 | -1,356.35 | 516 | | |
| 0.0 | 0.00 | 0.00 | 0.00 | -0.01 | -856.85 | 538 | 2 | |
| -0.0 | 0.00 | 0.00 | 0.00 | 0.01 | 856.85 | 516 | 그는 바람이 가지 않는 | |
| 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | -42.95 | 538 | 3 | |
| 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | 42.95 | 516 | | |
| -0.0 | 0.00 | 0.00 | 0.00 | 0.01 | 1,356.35 | 516 | | 538 |
| 0.0 | 0.00 | 0.00 | 0.00 | -0.01 | -1,356.35 | 539 | de la Alactería | |
| 0.0 | 0.00 | 0.00 | 0.00 | -0.01 | -856.85 | 516 | 2 | |
| -0.0 | 0.00 | 0,00 | 0.00 | 0.01 | 856.85 | 539 | 1977년 18일 | |
| 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | -42.95 | 516 | 3 | |
| 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | 42.95 | 539 | | ••• X |

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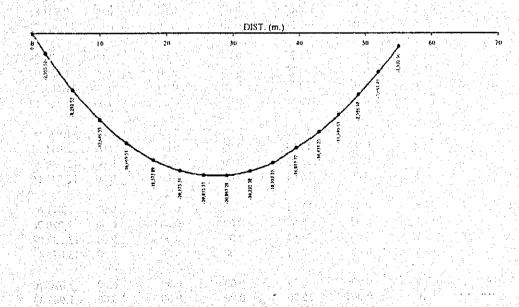
Pacific Consultants International of Japan, Third Floor, Bldg.# 47 DDC Center, Mokhali, Dhaka1212

MAX + MOMENT ENVELOP @ SPAN 1 OF BOX GIRDER SUPERSTRUCTURE

MAX POS. LL MOMENT ENVELOP @ SPAN 1 (DUE TO COMBINED SIDEWALK & LANE LOAD)

| Impact Factor, | | 5.244/(1.+38.11) | | 14.10 % | | |
|----------------------|-------|------------------|-----------|--|-----------|------------|
| NODE | : S | IDEWALK | EQUIV | ALENT LANE I | LOAD | TOTAL |
| NODL | 1 5 | SW | <u>P</u> | <u>la de Wilder </u> | IMPACT | LL+1 |
| | | | | | | |
| | 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 2 | -281,38 | -520.01 | -1,823.66 | -330.47 | -2,955.52 |
| | 3 | -781.02 | -1.521.39 | -5,061.85 | •928.27 | -8,292.53 |
| | 4 | -1,196.50 | -2,280.37 | -7,754.69 | -1,414.99 | -12,646.55 |
| | 5 | -1,527.82 | -2,842.79 | -9,901.85 | -1,797.05 | -16,069.51 |
| | 6 | -1,774.99 | -3.219.12 | -11,503.78 | -2.076.00 | -18,573.89 |
| | 7 | -1,938.00 | -3,423.30 | -12,560.26 | -2,253.75 | -20,175.31 |
| | 8 | -2,011.00 | -3,460.95 | -13,037.08 | -2,326.30 | -20,835.33 |
| | .9 | -2,020.76 | -3,420.95 | -13,096.53 | -2,329.04 | -20,867.28 |
| | 10 | -1,965.45 | -3,262.50 | -12,738.25 | -2,256.18 | -20,222.38 |
| | 11 | -1,845.79 | -3,066.12 | -11,962.27 | -2,119.07 | +18,993.25 |
| | 12 | -1,661.60 | +2,510.85 | -10,768.78 | -1,872.49 | -16,813.72 |
| | 13 | -1,412.94 | -2,251.61 | -9,157.91 | -1,608.79 | -14,431.25 |
| | 14 | -1,148.70 | -1,987.74 | -7,444.22 | -1,329.95 | -11,910.61 |
| | 15 | -836.93 | -1,718.85 | -5,424.02 | -1,007.18 | -8,986.98 |
| | 16 | -477.96 | -1,445.33 | -3,097.55 | -640.57 | -5,661.41 |
| | 17 | -71.56 | -1,167.57 | -463.80 | +230.03 | +1,932.96 |
| territum de la secol | | ちょうした たいせい たいいう | | and the second | | |

MAX POS. MOMENT ENVELOP @ SPAN 1



Pacific Consultants International of Japan, Bldg #47, DDC Center, Third Floor, Mokhali, Dhaka1212

Designed by: Checked by:

Date : 01-Dec-99

Note : Load 1 : Sidewalk Live Load, w = 5.26 KN/m Load 2 : Uniform Lane load, w = 34.09 KN/m.

lob No.

ſ

MAX POS. LL MOMENT ENVELOP @ SPAN 1 (DUE TO SIDEWALK & UNIFORM LANE LOAD)

| [MIN M | LOAD | NODEL | 12 - 6 3/1 - 1 | en se de la sectoria de la se Sectoria de la sectoria de la sectori | | n (ng sanga) (ng sanga) Tanàna amin'ny tanàna mandritry (ng sanga) (ng | 93983 - 65 1997 - 1998 | |
|---------|---|---|---|---|----------------|---|---------------------------|---|
| MEMB | LOAD | NODE | Ρ-ΛΧΙΛΙ | SHEAR-Y | SHEAR Z | TORSION | MOM Y | MOM-Z |
| | | | | | | | | |
| | | | 0,00 | | 0.00 | 0.00 | 0,00 | 0.00 |
| | | 2 | 0.00 | | 0.00 | 0.00 | 0.00 | 281.39 |
| | 2 | 1 | and the process of the second s | 945.93 | 0.00 | 0.00 | 0.00 | -0.0] |
| | | 2 | 0.00 | -877.75 | 0.00 | 0.00 | 0.00 | 1,823.65 |
| | | | | | a el 16 e Sere | ada sa ar | | |
| 2 | 1997 | 2 | 0.00 | 135.43 | 0.00 | 0.00 | 0.00 | -281.38 |
| | | 3 | 0.00 | -114,39 | 0.00 | 0.00 | 0,00 | 781.03 |
| | . | 2 | 0.00 | 877.73 | 0.00 | 0.00 | 0.00 | -1,823.66 |
| | | 3 | 0.00 | -741.37 | 0.00 | 0.00 | 0.00 | 5,061.83 |
| | | | | | | | | |
| 3 |), e e 1 | 3 | 0.00 | 114.39 | 0.00 | 0.00 | 0.00 | -781.02 |
| | | 4 | 0.00 | -93.35 | 0.00 | 0.00 | 0.00 | 1,196.52 |
| | 2 | 3 | 0.00 | 741.32 | 0.00 | 0.00 | 0.00 | -5,061.85 |
| | | 4 | 0.00 | -604.96 | 0.00 | 0.00 | 0.00 | 7,754.53 |
| | an an an a' | | | | | | | |
| 4 | 1 (d. 1 .) | 4 | 0.00 | 93.35 | 0.00 | 0.00 | 0.00 | -1,196.50 |
| | | 5 | 0.00 | -72-31 | 0.00 | 0.00 | 0.00 | 1,527.85 |
| | 2 | 4 | 0.00 | 605.00 | 0.00 | 0.00 | 0.00 | -7,754.69 |
| | 人の読みたい。 | 5 | 0.00 | -468.64 | 0.00 | 0.00 | 0.00 | 9,901.75 |
| | | en al construction Carlos de la construction | | | | | | 7,701.75 |
| 5 | 1 | 5 | 0.00 | 72.31 | 0.00 | 0.00 | 0.00 | -1,527.82 |
| | 11.5.5.5 | 6 | 0.00 | -51.27 | 0.00 | 0.00 | 0.00 | 1,775.01 |
| | 2 | 5 | 0.00 | 468.62 | 0.00 | 0.00 | 0.00 | -9,901.85 |
| | | 6 | 0.00 | -332.26 | 0.00 | 0.00 | 0.00 | 11,503.72 |
| | | یا ایرانیک ایران مراجع | يى ھېچىد ئىل يەرىپ بارىكى ھىلار كىلى | | | | | 11,29.2,74 |
| 6 | 1 | 6 | 0.00 | 51.27 | 0.00 | 0.00 | 0.00 | -1,774.99 |
| | | 7 | 10.00 J | -30.23 | 0.00 | 0.00 | 0.00 | 1,938:00 |
| | 2 | 6 | 0.00 | 332.22 | 0.00 | 0.00 | 0.00 | -11,503.78 |
| | | 7 | 0.00 | -195.86 | 0.00 | 0.00 | 0.00 | 12,560.17 |
| | | | | | | | | 12,200,17 |
| 7 | 111 | 7 | 0.00 | 30.25 | 0.00 | 0.00 | 0.00 | +1,938.00 |
| | | 8 | 0.00 | -11.84 | 0.00 | 0.00 | 0.00 | 2,011.61 |
| | 2 | 7 | 0.00 | 195.92 | 0.00 | 0.00 | 0.00 | +12,560.26 |
| | | 8 | 0.00 | -76.61 | 0.00 | 0.00 | 0.00 | 13,037.00 |
| | | | | | | | 0.00 | 1.5,0.17.00 |
| 8 | 1 | 8 | 0.00 | 11.81 | 0.00 | 0.00 | 0.00 | -2,011.60 |
| | | 9 | 0.00 | 6.60 | 0.00 | 0.00 | | a activity of the call of |
| | 2 | 8 | 0.00 | 76.62 | 0.00 | 0.00 | 0.00 | 2,020.76 |
| | | 9 | 0.00 | 42.69 | 0.00 | 0.00 | 0.00 | 13,096.48 |
| | | | | | | 0.00 | 0.00 | 10,070.40 |
| 9 | 1 | 9 | 0.00 | -6.59 | 0.00 | 0.00 | 0.00 | -2,020.76 |
| | | io | 0.00 | 25.00 | 0.00 | 0.00 | 0.00 | 1,965.44 |
| | alar ang sa | | | | | | ••••• | ی اور در مرکز اور در /b> |
| | | | a da an tara tara tara tara tara tara tara | | di Pade de | alle datas | i estatorio i di | |

Pacific Consultants International of Japan, Bldg# 47, DDC Center, Third Floor, Mokhali, Dhaka 1212.

THE STUDY ON THE CONSTRUCTION OF THE BRIDGE OVER THE RIVER RUPSA IN KHULNA, PHASE-2 Dob No. : Determined by : Date : 01-Dec-99

Note: Load 1 : Sidewalk Live Load, w = 5.26 KN/m Load 2 : Uniform Lane load, w = 34.09 KN/m.

 $\{ \{ i,j\} \in \{i,j\} \}$

MAX POS. LL MOMENT ENVELOP @ SPAN 1 (DUE TO SIDEWALK & UNIFORM LANE LOAD)

| N ALL AND | | NORP | DAVIA | OT TO A DOM N | ing an stand | | | |
|-----------|------------------------|---------------------------------------|--------------|----------------|--------------|--------------|---|-------------------------|
| MEMB | LOAD | NODE | P-AXIAL | SHEAR-Y | SHEAR-Z | TORSION | MOM-Y | MOM-Z |
| | 2 | 9 | 0.00 | -42.74 | 0.00 | 0.00 | IN 1111 | 15 002 25 |
| | | 10 | 0.00 | 162.05 | 0.00 | 0,00 | 0.00 | -13.096.53 |
| | | | | 102.02 | 0.00 | 0,00 | 0.00 | 12,738.19 |
| 10 | 1 | 10 | 0.00 | -25.00 | 0.00 | 0.00 | 0.00 | -1,965.45 |
| | | 11 | 0.00 | 43.41 | 0.00 | 0.00 | 0.00 | 1,845.76 |
| | 2 | 10 | 0.00 | -162.03 | 0.00 | 0.00 | 0.00 | -12,738.25 |
| | | $1 \le n$ | 0.00 | 281.34 | 0.00 | 0.00 | 0.00 | 11,962.24 |
| | | | | 문문문문 | | | | |
| <u>1</u> | 1 | - 11 | 0.00 | -43.41 | 0.00 | 0.00 | 0.00 | -1,845.79 |
| | | 12 | 0.00 | 61.82 | 0.00 | 0.00 | 0.00 | 1,661.59 |
| | 2 | 1 | 0.00 | -281.33 | 0.00 | 0.00 | 0.00 | -11,962.27 |
| 같은 동생 | | 12 | 0.00 | 400.65 | 0.00 | 0.00 | 0.00 | 10,768.98 |
| | e Carl | | | | | | | |
| 12 | 1 | 12 | 0.00 | -61.83 | 0.00 | 0.00 | 0.00 | -1,661.60 |
| | | 13 | 0.00 | 80.24 | 0,00 | 0.00 | 0.00 | 1,413.02 |
| | 2 | 12 | 0.00 | -400.61 | 0.00 | 0.00 | 0.00 | -10,768.78 |
| 문화된 | | 13 | 0.00 | 519.92 | 0.00 | 0.00 | 0.00 | 9,157.65 |
| 10 | | | | | | | | |
| 13 | 1 | 13 | 0.00 | -80.22 | 0.00 | 0.00 | 0.00 | -1,412.94 |
| | ` | 14 | 0.00 | 96.00 | 0.00 | 0.00 | 0.00 | 1,148.73 |
| | 2 | 13 | 0.00 | -520.03 | 0.00 | 0.00 | 0.00 | -9,157.91 |
| | | 14 | 0.00 | 622.30 | 0.00 | 0.00 | 0.00 | 7,444.19 |
| 14 | 1 | 14 | 0.00 | -96.03 | 0.00 | 0.00 | 0.00 | 1.1.0 -0. |
| 17 | | 15 | 0.00 | - 20.0.5 | 0.00 | 0.00 0.00 | 0.00 | -1,148.70 |
| | 2 | 13 | 0.00 | -622.29 | 0.00 | 0.00 | 0.00 | 836.93 -7,444.22 |
| | | 15 | 0.00 | 724.56 | 0.00 | 0.00 | 0.00 | -7,444.22 - 5,424.25 |
| | | | | 121.50 | 0.00 | 0.00 | 0,00 | 2,424.20 |
| 15 | 1 | 15 | 0.00 | -111.79 | 0.00 | 0.00 | 0.00 | -836.93 |
| | | 16 | 0.00 | 127.57 | 0.00 | 0.00 | 0.00 | 477.93 |
| | 2 | 15 | 0.00 | -724.40 | 0.00 | 0.00 | 0.00 | -5,424.02 |
| | | 16 | 0.00 | 826.67 | 0.00 | 0.00 | 0.00 | 3,097.70 |
| | | | | | | | a da sera da sera. A sera da s | |
| 16 | 1 | 16 | 0.00 | -127.60 | 0.00 | 0.00 | 0.00 | -477.96 |
| | | 17 | 0.00 | 143.38 | 0.00 | 0.00 | 0.00 | 71.48 |
| | 2 | 16 | 0.00 | -826.71 | 0.00 | 0.00 | 0.00 | -3,097.55 |
| | | 17 | 0.00 | 928.98 | 0.00 | 0.00 | 0.00 | 463.57 |
| | | · · · · · · · · · · · · · · · · · · · | | | | | | |
| 17 | 1 | 17 | 0.00 | -143.37 | 0.00 | 0.00 | 0.00 | -71.56 |
| | | 18 | 0.00 | 159.15 | 0.00 | 0.00 | 0.00 | -382.15 |
| | 2 | | 0.00 0.00 | -929.31 | 0.00 | 0.00 | 0.00 | -463.80 |
| | af séal Se la state | 18 | 0.00 | 1,031.58 | 0.00 | 0.00 | 0.00 | -2,477.23 |
| 1 | | | | 한 것은 말한 것이 없어? | | | | And Andrews and |

Pacific Consultants International of Japan, Bldg# 47, DDC Center, Third Floor, Mokhali, Dhaka 1212

THE STUDY ON THE CONSTRUCTION OF THE BRIDGE OVER THE RIVER RUPSA IN KHULNA; PHASE-2 No.: Designed by: Date : 01-Det-99

Note : Load 1 : Sidewalk Live Load, w = 5.26 KN/m Load 2 : Uniform Lane load, w = 34.09 KN/m.

Job No

l

MAX POS. LL MOMENT ENVELOP @ SPAN 1 (DUE TO SIDEWALK & UNIFORM LANE LOAD)

| | | S. Oak | | 18 an 17 3 | $\partial [A, W, U]$ | | | |
|-------------------|--|--------|--|------------|----------------------|--|-------|------------|
| MEMB | LOAD | NODE | P-AXIAL | SHEAR-Y | SHEAR-Z | TORSION | MOM-Y | MOM-2 |
| | | | | | | e e e a tradición. A las tradiciónses | | |
| 18 | 1 | 18 | 0.00 | -159,14 | 0.00 | 0.00 | 0.00 | 382.13 |
| ta e | | 19 | 0.00 | 174.92 | 0.00 | .0,00 | 0.00 | -883.22 |
| | 2 | 18 | 0.00 | -1,031,19 | 0.00 | 0.00 | 0.00 | 2,477.17 |
| | | 19 | 0.00 | 1,133.46 | 0.00 | 0.00 | 0.00 | -5,724.14 |
| | | | | | | | | |
| 19 | 1 | 19 | 0.00 | -174.91 | 0.00 | 0.00 | 0.00 | 883.19 |
| | | 20 | 0.00 | 190.69 | 0.00 | 0.00 | 0.00 | -1,431.62 |
| | 2 | 19 | 0.00 | -1,133.49 | 0.00 | 0.00 | 0.00 | 5,724.12 |
| | | 20 | 0.00 | 1,235.76 | 0.00 | 0.00 | 0.00 | -9,278.29 |
| | | | | | | | | |
| 20 | 1 | 20 | 0.00 | -190.69 | 0.00 | Ga (ag 0.00) | 0.00 | 1,431.60. |
| | | 21 | 0.00 | 211.73 | 0.00 | 0.00 | 0.00 | -2,236.45 |
| | 2 | 20 | 0.00 | -1,235.87 | 0.00 | 0.00 | 0.00 | 9,278.38 |
| | | 21 | 0.00 | 1,372.23 | 0.00 | 0.00 | 0.00 | -14,494 34 |
| | an a | | | | | | | |
| 21 | 100 | 21 | 0.00 | -211.71 | 0.00 | 0.00 | 0.00 | 2,236.43 |
| | | 22 | 0.00 | 222.23 | 0.00 | 0.00 | 0.00 | -2,670.46 |
| | 2 | 21 | 0.00 | -1,372.08 | 0.00 | 0.00 | 0.00 | 14,494 49 |
| | | 22 | 0.00 | 1,440.26 | 0.00 | 0.00 | 0.00 | -17,306.95 |
| in the set of the | All the second | | and the second | * + | | | | |

Pacific Consultants International of Japan, Bldg# 47, DDC Center, Third Floot, Mokhali, Dhaka 1212

THE STUDY ON THE CONSTRUCTION OF THE BRIDGE OVER THE RUPSA RIVER IN KHULNA, PHASE-2 Designed by ::: Checked by ;

Joh No 🔅

| 1 | | () (| | ///C. L | ANE LU | л <i>р</i> , г = | 292,4 KI / | Y) | | |
|--------------------|---------|------------------|---------------------|-----------------------|-------------------|---|---|--|--|-----------------|
| N | 1EMB | FY/FZ | DIST | ĹD | MZ/MY | DIST | LD | ΓX | DIST | LD |
| 1 | MAX | 260.01 | 0.00 | 1 | 0.01 | 0.00 | 7 | | | |
| | | 0.00 | 0.00 | 40 | 0.00 | 2.00 | 40 | .00 C | 0.00 | 31 |
| | MIN | 9.42 | 2.00 | 60 | -520.01 | 2.00 | | | an a | |
| | | 0.00 | 2.00 | 27 | 0.00 | 2.00 | 27 | 00 T | 2.00 | 3,3 |
| 2 | MAX | 260.01 | 0.00 | 1 | -18.84 | 0.00 | 60 | | na Xanan An Angel | |
| | | 0.00 | 0.00 | 40 | 0.00 | 4.00 | 40 | .00 C | 0.00 | 37 |
| | MIN | -38.84 | 4,00 | 2 | -1,521.39 | 4.00 | 2 | | | |
| | | 0.00 | 4.00 | 27 | 0.00 | 4.00 | 27 | .00 T | 4.00 | 39 |
| 3 | MAX | 247.14 | 0.00 | 3 | -56.51 | 0.00 | 60 | | | |
| | | 0.00 | 0.00 | 40 | 0.00 | 4.00 | 40 | .00 C | 0.00 | 33 |
| | MIN | -64.36 | 4.00 | 6 | -2,280.37 | 4.00 | 6 | | | |
| | | 0.00 | 4.00 | 27 | 0.00 | 4.00 | 27 | .00 T | 4.00 | 34 |
| 4 | MAX | 221.73 | 0.00 | 7 | -94.18 | 0.00 | 2 | | | |
| 1 | TAD DV | 0.00 | 0.00 | 40 | -24.18 | 0.00 4.00 | 60 40 | 00.0 | 0.00 | |
| in e su Line su | MIN | -89.35 | 4.00 | | -2,842.79 | 4.00 | 40 | .00 C | 0.00 | 37 |
| | | 0.00 | 4.00 | 27 | 0.00 | 4.00 | 10 27 | .00 T | 4.00 | 39 |
| | | | | | | | | | | |
| 5 | MAX | 196.93 | 0.00 | 11 | -131.86 | 0.00 | 60 | | | |
| | | 0.00 | 0.00 | 40 | 0.00 | 4.00 | 40 | .00 C | 0.00 | - 2 33 - |
| 1.1 | MIN | -113.57 | 4.00 | 14 | -3,219.12 | 4.00 | 14 | | | |
| | | 0.00 | 4.00 | 27 | 0.00 | 4.00 | 27 | .00 T | 4.00 | 34 |
| 6 | МАХ | 172.94 | 0.00 | 15 | -169.53 | 0.00 | 60 | | | |
| | | 0.00 | 0.00 | 40 | 0.00 | 4.00 | 40 | .00 C | 0.00 | 33 |
| | MIN | -136.80 | 4.00 | 18 | -3,423.30 | 4.00 | 18 | | 0.00 | |
| | | 0.00 | 4.00 | 27 | 0.00 | 4.00 | 27 | .00 T | 4.00 | 34 |
| 7 | MÁX | 149.98 | 0.00 | 19 | -207.21 | 0.00 | 60 | | | |
| | | 0.00 | 0.00 | 40 | 0.00 | 3.50 | 40 | .00 C | 0.00 | 35 |
| | MIN | -153.44 | 3.50 | 21 | -3,462.30 | 2.92 | 21 | .00 C | 0.00 | |
| | | 0.00 | 3.50 | 27 | 0.00 | 3.50 | 27 | .00 T | 3.50 | 31 |
| 8 | MAX | 122.50 | ባ ባባ | 22 | 540.17 | 0.00 | 10 | an a | | |
| 0 | IVICT.A | 133.58 | 0.00 0.00 | 22 40 | -240.17 | 0.00 | 60 40 | | 0.00 | •0 |
| | MIN | -174.43 | 3.50 | 25 | 0.00 -3,459.58 | 3.50 | 40 | .00 C | 0.00 | 30 |
| | | 0,00 | 3.50 | 27 | 0.00 | 0.58 3.50 | 22 27 | .00 T | 2 50 | 16 |
| | | 0.00 | | | 0.00 | 0.00 | 41 | .001 | 3.50 | 46 |
| 9 | MAX | 112.94 | 0.00 | 26 | -273.14 | 0.00 | 60 | | | |
| | | 0.00 | 0.00 | 40 | 0.00 | 3.50 | 40 | .00 C | 0.00 | 35 |
| | MIN | -189.15 | 3.50 | 14 M 1 | -3,420.95 | 0,00 | 25 | | | |
| | | 0.00 | 3.50 | 27 | 0.00 | 3.50 | 27 | .00 T | 3.50 | 31 |
| 1.1 | | jah sa kata dege | t gest ter en trans | and the second second | | - 19 - 19 - 19 - 19 - 19 - 19 - 19 - 19 | 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - | and the second second | and the second second | 98 N 1 1 1 1 |

MAX. POS. LL MOMENT ENVELOP @ SPAN 1 (DUE TO CONC. LANE LOAD, P = 292.4 KN)

Pacific Consultants International of Japan, Bldg, #47, DDC Center, Third Floor, Mokhali, Dhaka 1212

12/1/99

Date

Designed by Checked by :

Job No

Dale : 12/1/99

MAX. POS. LL MOMENT ENVELOP @ SPAN 1 (DUE TO CONC. LANE LOAD, P = 292.4 KN)

| MI | EMB | FY/FZ | DIST | LD | MZ/MY | DIST | LD | FX | DIST | LD |
|-----|------------------|----------|--|--|------------------|------------|--------------------|---------|------|---|
| | <u></u> | . | an a | | | <u> </u> | الم من تعريف الم | <u></u> | | المیں بینی کے اور |
| 01 | MAX | 98.56 | 0,00 | 29 | -295.81 | 3.50 | 1 | | | |
| | | 0.00 | 0.00 | 40 | 0.00 | 3.50 | 40 | 00 C | 0.00 | 25 |
| | MIN | -207.22 | 3.50 | 32 | -3,236.21 | 0.58 | 29 | | | |
| | | 0.00 | 3.50 | 27 | 0.00 | 3,50 | 27 | 00 1 | 3.50 | .26 |
| | | | | | | | | | | |
| 11 | MAX | 80.94 | 0.00 | 33 | -182.42 | 3.50 | 1 | | | |
| | | 0.00 | 0.00 | 40 | 0.00 | 3.50 | 40 | 00 C | 0.00 | 35 |
| | MIN | -219.50 | 3.50 | 14 C 14 | -3,066.12 | 0.00 | 32 | | | |
| | | 0.00 | 3.50 | 27 | 0.00 | 3.50 | 27 | .00 T | 3,50 | 31 |
| | | 20.03 | 0.00 | | 70.04 | 2.40 | | | | |
| 12 | MAX | 69.04 | 0.00 | 36 | -69.04 | 3.50 | 40 | .00 C | 0,00 | 25 |
| |) mí | 0.00 | 0.00 | 40 | 0.00 | 3.50 | | .000 | 0.00 | 23 |
| | MIN | -234.03 | 3.50 | 39 | -2,747.89 | 0.29 | 36 27 | - 00 Τ | 2.50 | |
| | 이가 다니다. 이야마 전 | 0.00 | 3.50 | 27 | 0.00 | 3.50 | 27 | .00 T | 3.50 | 26 |
| 13 | MAX | 55.14 | 0.00 | 40 | 37.48 | 3.00 | 5 | | | |
| 1.5 | IVLAA | 0.00 | 0.00 | 40 | 0.00 | 3.00 | 40 | .00 C | 0.00 | 40 |
| | MIN | -243.47 | 3.00 | 40 | -2,510.85 | 0.00 | 39 | | 0.00 | |
| | NITIA | 0.00 | 3.00 | 27 | 0.00 | 3.00 | 27 | .00 T | 3.00 | 45 |
| | | 0.00 | 3.00 | | 0.00 | | * • | .001 | | ••• |
| 14 | MAX | 46.04 | 0.00 | 43 | 301.26 | 3.00 | 14 | | | |
| | | 0.00 | 0.00 | 40 | 0.00 | 3.00 | 40 | .00 C | 0.00 | 39 |
| | MIN | -251.81 | 3.00 | and the second second | | 0.00 | 42 | 연물문문 | | |
| | | 0.00 | 3.00 | | 0.00 | 3.00 | 27 | .00 T | 3.00 | 51 |
| | | | | 10 | | | | | | |
| 15 | MAX | 37.94 | 0.00 | 46 | 680.86 | 3.00 | 19 | | | |
| | | 0.00 | 0.00 | 40 | 0.00 | 3.00 | 40 | .00 C | 0.00 | 52 |
| | MIN | -259.35 | 3.00 | 48 | -1,987.74 | 0.00 | 45 | | | |
| | | 0.00 | 3.00 | 27 | 0.00 | 3 (2) | 27 | .00 T | 3,00 | 17 |
| | | | | | | | | | | |
| 16 | MAX | .30.71 | 0.00 | 49 | 1,133.21 | 3.00 | - 22 | | | |
| | | 0.00 | 0.00 | 40 | 0.00 | 3.00 | 40 | .00 C | 0.00 | ંગું કો |
| | MIN | -266.10 | 3.00 | 51 | -1,718.85 | 0.00 | 48 | | | |
| | | 0.00 | 3.00 | 27 | 0.00 | 3.00 | 27 | T 00. | 3.00 | 41 |
| | | | | | | | | | | |
| 17 | MAX | 24.19 | | | 1 A. 2 A. 2 M. 2 | 6 g (a) an | 그는 사람은 소문을 가지 않는 것 | | | |
| | | 0.00 | | | | | | .00 C | 0.00 | 35 |
| | MIN | -272.25 | | | 그 같은 것 같은 것 같아요 | | 2.32 | | | |
| | | 0.00 | 3.00 | 27 | 0.00 | 3.00 | 27 | T 00. | 3.00 | 31 |
| 18 | MAX | 18.21 | 0.00 | 55 | 2,181.49 | 3.00 | 28 | | | |
| 10 | IVLAA | 0.00 | 1.1 A State 1.1 | (1) A. | | | 1. 1 X 1 K 1 | .00 C | 0.00 | 26 |
| | MIN | -277.87 | | | | | | | 0.00 | 20 |
| | 1417714 | 0.00 | 1. T. 1. M. | | | | a sha dhe a she m | .00 T | 3.00 | 51 |
| | | 0.00 | | | | 2.00 | | | | |

Pacific Consultants International of Japan, Bldg. #47, DDC Center, Third Floor, Mokhali, Dhaka 1212

Designed by : Date 12/1/99

MAX. POS. LL MOMENT ENVELOP @ SPAN 1 (DUE TO CONC. LANE LOAD, P = 292.4 KN)

Job No

| ME | ν́В | FY/FZ | DIST | LD | MZ/MY | DIST | LD | FX | DIST | LD |
|------|---------|---------|------|----|----------|-------------|-----------|---------------------------------------|----------|---------|
| | ta Nara | | | | | un en de la | i de pare | 1. * 1. ¹ . ¹ . | - | |
| 19 : | MAX 🚲 | 12.77 | 0.00 | 58 | 2,757.50 | 3,00 | 30 | | | |
| | | 0,00 | 0.00 | 40 | 0,00 | 3.00 | 4() | .00 C | 0.00 | 14 |
| | MIN 👘 | -282.99 | 3,00 | 60 | -886.46 | 0.00 | 57 | | | |
| | | 0,00 | 3.00 | 27 | 0.00 | 3,00 | 27 | .00 T | 3,00 | 49 |
| | | | | | | | | | | |
| 20 | MAX | -32.39 | 0.00 | 1 | 3,565.25 | 4,00 | 32 | | | |
| | | 0.00 | 0.00 | 40 | 0.00 | 4.00 | 40 | .00 C | 0.00 | 19 |
| | MIN | -282.98 | 4:00 | 60 | -602.78 | 0.00 | 60 | | | |
| | | 0.00 | 4.00 | 27 | 0.00 | 4.00 | 27 | .00 T | 4.00 | 33 |
| | | | | | | | | | | |
| 21 | MAX | -32.40 | 0.00 | 1 | 3,982.74 | 2.00 | 33 | | | e en la |
| | | 0.00 | 0.00 | 40 | 0.00 | 2.00 | 40 | .00 C | 0.00 | 36 |
| | MIN | -283.00 | 2.00 | 60 | 529.14 | 0.00 | 60 | | | |
| | | 0.00 | 2.00 | 27 | 0.00 | 2.00 | 27 | .00 T | 2.00 | 38 |

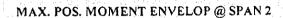
Pacific Consultants International of Japan, Bldg. #47, DDC Center, Third Floor, Mokhali, Dhaka 1212

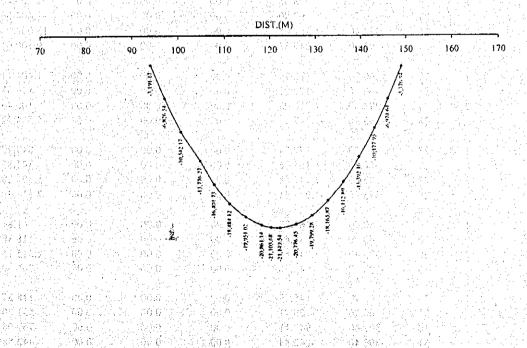
MAX + MOMENT ENVELOP @ SPAN 2 OF BOX GIRDER SUPERSTRUCTURE

THE STUDY ON THE CONSTRUCTION OF THE BRIDGE OVER THE RIVER RUPSA IN KHULNA, PHASE-2 Job No. Designed by : Checked by : 12/4/99

MAX. POS. LL MOMENT ENVELOP @ SPAN 2 (DUE TO COMBINED SIDEWALK & LANE LOAD)

| NODE | SIDEWALK | EQUIVA | LENT LANE/L | ,OAD | TOTAL |
|------|------------------------|------------------------|-------------|-----------|-----------|
| NODE | SW | e la P olatev (| W | IMPACT | £L+1 |
| | | | | | |
| 30 | ふかた かっと あっとう いたからなか かた | -2.000.27 | •767.08 | -305.45 | -3.191.1 |
| 31 | -531.24 | +2.227.19 | -3.442.33 | -625.78 | -6.826.5 |
| 32 | -952.80 | -2.459.95 | -6.176.20 | -953.22 | -10.542.1 |
| 33 | -1.310.58 | -2.733.25 | -8.493.30 | -1.239.14 | 13.776.2 |
| 34 | -1.603.47 | -2.935.06 | -10.392.19 | -1,471.01 | -16.401.7 |
| 35 | -1,831.86 | -3.123.74 | -11.873.22 | -1.655.30 | -18.484.1 |
| 36 | -1.996.12 | -3.233.42 | -12.936.69 | -1.784.79 | -19,951.0 |
| 37 | -2.095.27 | -3.317.08 | -13.583.39 | -1.865.40 | -20,861.1 |
| 38 | ·2.123.46 | -3.329.59 | -13.763.92 | -1,886.71 | -21,103.6 |
| 39 | +2.130.35 | -3.322.99 | -13.805.62 | -1,890.58 | -21.149.5 |
| 40 | | -3.249.26 | -13.577.97 | -1.857.32 | -20.776.4 |
| 41 | -1.989.07 | -3.149.31 | -12.890.49 | -1.770.41 | -19.799.2 |
| 42 | -1,821.85 | -2,911,91 | +11.807.45 | -1.624.66 | -18,165.8 |
| 43 | -1.590.06 | -2,774.47 | -10.304.65 | -1,443.62 | -16,112.8 |
| . 44 | | -2.510.17 | -8,385.50 | -1,202.62 | -13,392 |
| 45 | 사람이 가장하는 사람이 나라 있다. | -2,277.55 | -6,048,22 | -918.96 | -10,177.9 |
| 46 | | -2.052.07 | -3.713.41 | -636.37 | -6.974.6 |
| 40. | -165.13 | +1,822.03 | -1.070.51 | -319.27 | -3.376.9 |





Pacific Consultants International of Japan, Bldg.#47, DDC Center, Third Floor, Mokhali, Dhaka 1212

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| and the second | TRUCTION OF THE BRIDGE SA IN KHULNA, PHASE-2 |
|--|---|
| Job No. : Designed by : | Checked by : Date 02-Dec-99 |

341

Note: Load 1 : Sidewalk Live Load. w = 5.26 KN/m. Load 2 : Uniform Lane Load, w = 34.09 KN/m.

1.六美。

MAX POS. LL MOMENT ENVELOP @ SPAN 2 & 4 (DUE TO SIDEWALK & UNIFORM LANE LOAD)

| MEMB | LOAD | NODE | P-AXIAL | SHEAR-Y | SHEAR-Z | TORSION | MOM-Y | MOM-Z |
|--|--|--|---|---|--|---|--------|------------|
| | | 2. an 191 | | | | an a | | |
| 22 | | 22 | 60.70 | 271.76 | 0.00 | 0.00 | 0.00 | 4.888.49 |
| | | 23 | -60.70 | -261.24 | 0.00 | 0.00 | 0.00 | -4.355.53 |
| | 2 | 22 | 393.39 | 1.761.10 | 0.00 | 0.00 | -0.01 | 31.682.23 |
| | | 23 | -393.39 | -1.692.92 | 0.00 | Ö.Ó0 | 0.01 | -28.227.94 |
| | | | | | | e Participation - Alignation D'Alignation - Alignation | | |
| ં 23 ્ | 1 | 23 | 60.70 | 261.22 | 0.00 | 0.00. | . 0.00 | 4.355.51 |
| | | 24 | -60.70 | -240.18 | 0.00 | 0.00 | 0.00 | -3.352.73 |
| ين اليا. بر ما كان المان | 2 | 23 | 393.40 | 1.692.96 | 0.00 | 0.00 | -0.01 | 28.228.31 |
| | | 24 | -393.40 | -1.556.60 | 0.00 | 0.00 | 0.01 | -21.728.89 |
| | | | en de la compañía de Compañía de la compañía de la compañí | | 0.00 | 0 00 | 0.00 | |
| 24 | alaste sil∎ Da Altaria | 24 | 60.70 | 240.19 | 0.00 | 0.00 | 0.00 | 3.352.71 |
| n i par de la su Polo de la sub- | | 25 | -60.70 | -224.41 | 0.00 | 0.00 | 0.00 | -2.655.86 |
| | 2 | 24 | 393.40 | 1,556.76 | 0.00 | 0.00 | -0.01 | 21,729.31 |
| | | 25 | -393.40 | -1,454.49 | 0.00 | 0.00 | 0.00 | -17.212.29 |
| | | • * | 60.70 | 224.36 | 0.00 | 0.00 | · 0.00 | 2.655.80 |
| 25 | | 25 | -60.70 | -208.58 | 0.00 | 0.00 | 0.00 | -2.006.40 |
| | | 26 | 393.40 | 1.453.79 | 0.00 | 0.00 | 0.00 | 17,211.47 |
| | 2 | 25 26 | -393.40 | -1.351.52 | 0.00 | 0.00 | 0.00 | -13,003.87 |
| | | 20 | -373.40 | -1.501.52 | 0.00 | 0.00 | 0.00 | -15,005.07 |
| 26 | 1 | 26 | 60.70 | 208.68 | 0.00 | 0.00 | 0.00 | 2,006.40 |
| 20 | | 20 | -60.70 | -192.90 | 0.00 | 0.00 | 0.00 | -1,404.06 |
| | 2 | | 393.40 | 1,351.65 | 0.00 | 0.00 | 0.00 | 13,002.36 |
| | 2 | 27 | -393.40 | -1,249.38 | 0.00 | | 0.00 | +9.100.61 |
| | | • | | | | | | |
| 27 | 1.1 | 27 | 60.70 | 192.79 | 0.00 | 0.00 | 0.00 | 1.404.11 |
| | | 28 | -60.70 | -177.01 | 0.00 | 0.00 | 0.00 | -849.33 |
| | 2 | - とうと かいえい しょう | 393.40 | 1.250.03 | 0.00 | | 0.00 | 9.100.46 |
| an a | | 28 | -393.40 | -1,147.76 | 0.00 | 0.00 | 0.00 | -5.504.22 |
| | | | | | | | | |
| 28 | | 28 | 60.70 | 177.04 | 0.00 | 0.00 | 0.00 | 849.27 |
| | | 29 | -60.70 | -161.26 | 0.00 | 0.00 | 0.00 | -341.83 |
| | | 2 28 | 393.40 | 1,147.68 | 0.00 | 0.00 | 0.00 | 5,504.28 |
| | | 29 | -393.40 | -1,045.41 | 0.00 | 0.00 | 0.00 | -2,215.30 |
| | | | | | | | | |
| 29 | | 1 29 | 1.1.1 | | 0.00 | | 0.00 | 341.81 |
| | n an | 30 | 1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1. | | | | 0.00 | 118.38 |
| este se le Proposition de la | | 2 29 | | the second se | | | 0.00 | 2,215.15 |
| | | 30 | -393.40 | -942.58 | 0.00 | 0.00 | 0.00 | 766.90 |
| | | | | | 0.00 | 0.00 | 0.00 | -118.37 |
| 3(|) | 1 30 | A second seco | | and the second | | 0.00 | 531.20 |
| | | 31 | | | Additional of the second se Second second sec | the second se | 0.00 | -767.08 |
| | | 2 30 | | | | (a) An an an array of the second s Second second s Second second se | 0.00 | |
| | | 31 | -393.40 | -840.84 | 0.00 | , v.ov | 0.00 | J,442.JO |
| | | and the second secon Second second | 바이다 가슴이 있는 것이 있는 것이다. 바이다 가슴이 있는 것이 같이 있는 것이 있는 것 같이 있는 것이 같이 있는 것이 있는 것 | | an a state of the state of the | 1.15月代月4日(1月1月) 建341 | | |

Pacific Consultants International of Japan, Bldg. #47, DDC Center, Third Floor, Mokhali, Dhaka 1212

Job No. : Designed by : Checked by : Date 02-Dec-99

Note: Load 1 : Sidewalk Live Load, w = 5.26 KN/m. Load 2 : Uniform Lane Load, w = 34.09 KN/m.

MAX POS. LL MOMENT ENVELOP @ SPAN 2 & 4 (DUE TO SIDEWALK & UNIFORM LANE LOAD)

| | | | the second s | | ······ | <u></u> | | |
|---|--------------------------|----------|--|---------|--|---|--------------|--|
| MEMB | LOAD | NODE | P-AXIAL | SHEAR Y | SHEAR-Z | TORSION | MOM-Y | MOM-Z |
| | | | 40 70 | 120.20 | <u>.</u> | 0.00 | 0.00 | |
| 31 | | 31 | 60.70 | 129.70 | 0.00 | 0.00 | 0.00 | -531.2 |
| in pi | | 32 | -60.70 | -111.29 | 0.00 | 0.00 | 0.00 | 952.9 |
| | 2 | 31 | 393.40 | 840.94 | 0.00 | 0.00 | 0.00 | -3.442.3 |
| | ta la stricta Alterna | 32 | -393.40 | -721.62 | 0.00 | 0.00 | 0.00 | 6.176.7 |
| 32 | | 32 | 40 70 | 111 44 | 0.00 | 0.00 | 0.00 | 052.9 |
| 34 | 1 | 33 | 60.70 -60.70 | -93.03 | 0.00 | 0.00 | 0.00 0.00 | -952.8 1.310.5 |
| | 2 | 32 | 393.40 | 721.50 | 0.00 | 0.00 | 0.00 | A set of the set of th |
| it en la ser Général estat | ti i d | 33 | -393.40 | -602.19 | and the second | A set of the set of | 0.00 | -6.176.2 |
| | | | -393.40 | -002.19 | 0.00 | 0.00 | 0.00 | 8.492.7 |
| 33 | 1 | 33 | 60.70 | 92.79 | 0.00 | 0.00 | 0.00 | -1.310.5 |
| | | 34 | -60.70 | •74.38 | 0.00 | 0.00 | 0.00 | 1,603.0 |
| | 2 | 33 | 393.40 | 601.68 | 0.00 | 0.00 | 0.00 | -8.493.3 |
| | 4 | 34 | -393.40 | -482.36 | 0.00 | 0.00 | 0.00 | 10,390.2 |
| 1111 | 지 전 | | | -482.50 | 0.00 | | 0.00 | 10,390.2 |
| 34 | 1 | 34 | 60.70 | 74.39 | 0.00 | 0.00 | 0.00 | -1,603.4 |
| 94 | | 35 | -60.70 | -55.98 | 0.00 | 0.00 | 0.00 | 1,831.6 |
| | 2 | 34 | 393.40 | 482.13 | 0.00 | 0.00 | 0.00 | -10.392.1 |
| | | 35 | -393.40 | -362.82 | 0.00 | 0.00 | 0.00 | 11,870.2 |
| | | | -575.40 | -502.02 | 0.00 | 0.00 | 0.00 | 11,070.2 |
| 35 | i i | 35 | 60.70 | 56.04 | 0.00 | 0.00 | 0.00 | -1,831.8 |
| | | 36 | •60.70 | -37.63 | 0.00 | 0.00 | 0.00 | 1,995.7 |
| Skie stati | 2 | 35 | 393.40 | 362.52 | 0.00 | 0.00 | 0.00 | -11,873.2 |
| | े हो 🖈 | 36 | -393.40 | -243.20 | 0.00 | 0.00 | 0.00 | 12,933.5 |
| | | | | | | 0.00 | 0.00 | |
| 36 | 1 | 36 | 60.70 | 37.50 | 0.00 | 0.00 | 0.00 | -1,996.1 |
| | | 37 | | -19.09 | 0.00 | 0.00 | 0.00 | 2,095.2 |
| | 2 | | 393.40 | 243.31 | 0.00 | 0.00 | 0.00 | -12.936.6 |
| | | 37 | -393.40 | -124.00 | 0.00 | 0.00 | 0.00 | 13,578.8 |
| | | | | | | | | |
| 37 | | 37 | 60.70 | 19.54 | 0.00 | 0.00 | 0.00 | -2,095.2 |
| | | 38 | -60.70 | -9.02 | 0.00 | 0.00 | 0.00 | 2,123.8 |
| 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - | 2 | | 393.40 | 122.93 | 0.00 | 0.00 | 0.00 | -13,583.3 |
| | | 38 | -393.40 | -54.75 | 0.00 | 0.00 | 0.00 | 13,759.0 |
| | <u>.</u> | | | | | | | i Alix Ali |
| 38 | ់ | 38 | 60.70 | 8.84 | 0.00 | 0.00 | 0.00 | -2,123.4 |
| | | 39 | -60.70 | 1.68 | 0.00 | 0.00 | 0.00 | 2,130.5 |
| | 2 | 38 | 393.40 | 55.24 | 0.00 | 0.00 | 0.00 | -13,763.9 |
| | | 39 | -393.40 | 12.94 | 0.00 | 0.00 | 0.00 | 13,805.6 |
| | | | | | | | | |
| 39 | ា | 39 | 60.70 | -1.74 | 0.00 | 0.00 | 0.00 | -2,130.3 |
| | | 40 | -60.70 | 20.15 | 0.00 | 0.00 | 0.00 | 2,092.0 |
| | 2 | | 393.40 | -10.70 | 0.00 | 0.00 | 0.00 | -13,805.6 |
| 1.1.1 | 9 C. K.G., | 40 | -393.40 | 130.02 | 0.00 | 0.00 | 0.00 | 13,559.9 |

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| lob No | Designed by : | Checked by : | Date | 02-Dec-99 |
|----------|--------------------------|--------------|------|--|
| 100 140. | <u>le recent a train</u> | | | •••••••••••••••••••••••••••••••••••••• |

Note: Load I : Sidewalk Live Load. w = 5.26 KN/m.

Load 2 : Uniform Lane Load, w = 34.09 KN/m.

MAX POS. LL MOMENT ENVELOP @ SPAN 2 & 4 (DUE TO SIDEWALK & UNIFORM LANE LOAD)

| ИЕМВ | LOAD | NODE | P-AXIAL | SHEAR-Y | SHEAR-Z | TORSION | MOM-Y | MOM-Z |
|--|---|---|---------|--|--|---|-------|-----------|
| | 5 A. | , AL | 60.70 | -20.18 | 0.00 | 0.00 | 0.00 | -2.091.9 |
| 40 | | 40 41 | -60.70 | 38.59 | 0.00 | 0.00 | 0.00 | 1.989.1 |
| | 2 | 40 | 393.40 | -130.93 | 0.00 | 0.00 | 0.00 | -13,557.9 |
| | 4 | 40 41 | -393.40 | 250.24 | 0.00 | 0.00 | 0.00 | 12.891.6 |
| | | 41 | 60.70 | -38.58 | 0.00 | 0.00 | 0.00 | -1.989.0 |
| 41 | | 41 | -60.70 | 56.99 | 0.00 | 0.00 | 0.00 | 1.821.7 |
| | 2 | We have been a set of the set of | 393.40 | -249.58 | 0.00 | 0.00 | 0.00 | -12.890.4 |
| | - | 42 | -393.40 | 368.89 | 0.00 | 0.00 | 0.00 | 11.807.9 |
| 42 | 1 | 42 | 60.70 | -57.05 | 0.00 | 0.00 | 0.00 | -1.821.8 |
| 14 44 4 19 19 19 19 19 19 19 19 19 19 19 19 19 1 | - | 43 | -60.70 | 75.46 | 0.00 | 0.00 | 0.00 | 1.589.9 |
| | | | | | | | | |
| | 2 2 | 42 | 393.40 | -369.94 | 0.00 | 0.00 | 0.00 | -11.807.4 |
| | 4 | 43 | -393.40 | 489.25 | 0.00 | 0.00 | 0.00 | 10,304.1 |
| 43 | | 43 | 60.70 | -75.44 | 0.00 | 0.00 | 0.00 | -1.590.0 |
| 43 | | 44 | -60.70 | 93.85 | 0.00 | 0.00 | 0.00 | 1,293. |
| | | 2 43 | 393.40 | -488.80 | 0.00 | 0.00 | 0.00 | -10.304.0 |
| | | 44 | -393.40 | 608.11 | 0.00 | | 0.00 | 8,385. |
| 44 | |] 44 | 60.70 | -93.86 | 0.00 | 0.00 | 0.00 | -1,293. |
| | | 45 | -60.70 | 112.27 | | 그는 가장 가는 것 같은 것은 것을 가지 않는 것 | 0.00 | 933. |
| | | 2 44 | 393.40 | -608.20 | 그는 정말 수 있는 것이 있는 것이 없다. | and the start of the second | 0.00 | -8.385. |
| | | 45 | | 727.51 | A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 | 0.00 | 0.00 | 6,047. |
| 45 | 17 A. | 1 45 | 60.70 | •112.25 | 0.00 | 0.00 | 0.00 | •933. |
| | | 46 | | and the second | A statistic set of the statistic set o | 0.00 | 0.00 | 572. |
| | | 2 45 | | | and the second | 0.00 | 0.00 | -6,048 |
| | | 46 | | and the second | 0.00 | 0.00 | 0.00 | 3,712. |
| 46 | , | 1 46 | 60.70 | -128.02 | 0.00 | 0.00 | 0.00 | -572 |
| | | 47 | -60.70 |) 143.80 | 0.00 | 0.00 | 0.00 | 165. |
| | | 2 46 | 393.40 | -830.45 | i 0.00 | 0.00 | 0.00 | -3,713 |
| | | 47 | -393.40 |) 932.72 | 2 0.00 |) 0.00 | 0.00 | 1,068 |
| 4 | | 47 | 60.70 |) -143.84 | 0.00 | | 0.00 | -165 |
| | N | 48 | | | | | | |
| | | 2 4 | | | | | | -1,070 |
| | | 48 | -393.4(| 0 1,034.70 |) 0.00 |) 0.00 | 0.00 | -1,880 |
| | 8 | 1 41 | 8 | -159.6 | 8 0.0 | 0.00 | 0.00 | 289 |
| | r i i i i i i i i i i i i i i i i i i i | 4 | | | | | | -792 |

Pacific Consultants International of Japan, Bldg. #47, DDC Center, Third Floor, Mokhali, Dhaka 1212

| THE STUDY ON THE CONS | | en a en altra de la companya de la c |
|-------------------------|--------------|---|
| Job No. : Designed by : | Checked by : | Date 02-Dec-99 |

Note: Load 1 : Sidewalk Live Load, w = 5.26 KN/m. Load 2 : Uniform Lane Load, w = 34.09 KN/m.

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MAX POS. LL MOMENT ENVELOP @ SPAN 2 & 4 (DUE TO SIDEWALK & UNIFORM LANE LOAD)

| MEMB | LOAD | NODE | P-AXIAL | SHEAR-Y | SHEAR-Z | TORSION | MOM-Y | MOM-Z |
|------|---------------------------------------|------|---------|-----------|---------|---------|------------------------|------------|
| | | | | | | | | |
| | 2 | | 393.40 | +1.035.21 | 0.00 | 0.00 | 0.00 | 1.878.52 |
| | | 49 | -393.40 | 1.137.48 | 0.00 | 0.00 | 0.00 | -5.136.91 |
| | · · · · · · · · · · · · · · · · · · · | | | | | | | |
| 49 | | 49 | 60.70 | -175.41 | 0.00 | 0.00 | 0.00 | 792.31 |
| | | 50 | -60.70 | 191.19 | | 0.00 | 0.00 | -1.342.19 |
| | 2 | 49 | 393.40 | -1.136.73 | 0.00 | 0.00 | 0.00 | 5.135.25 |
| | | 50 | -393.40 | 1.239.00 | 0.00 | 0.00 | 0.00 | -8.698.98 |
| | | - 0 | | | | | | |
| 50 | 1 | 50 | 60.70 | -191.18 | 0.00 | 0.00 | 0.00 | 1.342.06 |
| | | 51 | -60.70 | 206.96 | 0.00 | 0.00 | 0.00 | -1.939.32 |
| | 2 | 50 | 393.40 | +1,238.52 | 0.00 | 0.00 | 0.00 | 8.698.95 |
| | | 51 | -393.40 | 1.340.79 | 0.00 | 0.00 | 0.00 | -12,567.51 |
| 51 | 1 | 51 | 60.70 | -206.99 | 0.00 | 0.00 | 0.00 | 1.020.10 |
| | | 52 | -60.70 | 222.77 | 0.00 | 0.00 | 0.00 | 1,939.18 |
| | 2 | 51 | 393.40 | -1.341.02 | 0.00 | 0.00 | 5. 14 (1997) 10 (1997) | -2.583.78 |
| | | 52 | -393.40 | 1,443.29 | 0.00 | | 0.00 | 12,568.70 |
| | | 22 | -373.40 | 1,443,29 | 0.00 | 0.00 | 0.00 | -16.744.79 |
| 52 | 1 | 52 | 60.70 | -222.71 | 0.00 | 0.00 | 0.00 | 2,583.64 |
| | | 53 | -60.70 | 243.75 | 0.00 | 0.00 | 0.00 | -3.516.63 |
| | 2 | 52 | 393.40 | -1,443.36 | 0.00 | 0.00 | 0.00 | 16.744.62 |
| | | 53 | -393.40 | 1,579.72 | 0.00 | 0.00 | 0.00 | -22,790.96 |
| | | | | | | | | |
| 53 | 1 | 53 | 60.70 | •243.70 | 0.00 | 0.00 | 0.00 | 3.516.60 |
| | | 54 | -60.70 | 254.22 | 0.00 | 0.00 | 0.00 | -4.014.56 |
| | 2 | 53 | 393.40 | -1.580.11 | 0.00 | 0.00 | 0.00 | 22.790.24 |
| | | 54 | -393.40 | 1.648.29 | 0.00 | 0.00 | 0.00 | -26.019.00 |
| | | | | | | | | |

Pacific Consultants International of Japan, Bldg. #47, DDC Center, Third Floor, Mokhali, Dhaka 1212

Job No

Checked by:

12/2/99 Date :

534

MAX. POS. LL MOMENT ENVELOP @ SPAN2 (DUE TO CONC LANE LOAD, P =292.40 KN)

| мемв | FY/FZ | DIST | LD | MZ/MZ | DIST | LD | ГХ | DIST | LD |
|----------------------|---|--------|--|--|--------------|--|--------------------------|------|----------------------------------|
| | | (4×0) | | 40.9420 | eg wer | | 14.1.1 | | |
| 22 MAX | 286.13 | 0.00 | | 4,533,16 | 0.00 | 34 | | | |
| | 0.00 | 0.00 | <u>19</u> | 0.00 | 0.00 | 34 | 52.43 C | 0,00 | 3 |
| MIN | 11.52 | 2.00 | 90 | 196.19 | 2.00 | 1 | | | |
| | 0.00 | 2.00 | 39 | 0.00 | 0.00 | 18 | 7.01 C | 2.00 | 9 |
| 3 MAX | 286.14 | 0.00 | n di 1976. Pri si 1 | 4.134.26 | 0.00 | | | | |
| 5 11/17 | 0.00 | 0.00 | 1.9 | 0.00 | 0.00 | 35 | 10022000-0 11.50110-0 | 0.00 | |
| MIN | -9.37 | 4.00 | 3 | | 4.00 | | 52.43 C | 0.00 | 3 |
| 141114 | 0.00 | • 4.00 | 39 | the second second | 0.00 | 3 | 7.01 C | 4.00 | 9 |
| | | | 가 가 주지 지수는 제 관리 | | | | 1.91 X | 7.00 | |
| 4 MAX | 281.40 | 0.00 | 4 | 3,366.73 | 0.00 | 38 | | | |
| | 0.00 | 0.00 | 19 | · | 0.00 | -34 | 52.43 C | 0.00 | 3 |
| MIN | -14.36 | 3.00 | 6 | | 3.00 | 6 | | | |
| an Natara. Nation | 0.00 | 3.00 | 39 | and the second | 3.00 | 27 | 7.01 C | 3.00 | 9 |
| | 1997 - 1 1997 - 199 | | | | | | | | |
| 25 MAX | 276.27 | 0.00 | 7 | 2.821.86 | 0.00 | 40 | | | |
| | 0.00 | 0.00 | 19 | 0.00 | 0.00 | 34 | 52.43 C | 0.00 | 3 |
| MIN | -19.82 | 3.00 | 9 | -1.051.88 | 3.00 | 9 | | | |
| | 0.00 | 3.00 | 39 | 0.00 | 3.00 | 27 | 7.01 C | 3.00 | 9 |
| | | (r, r) | | | | 1995 A. | | | |
| 26 MAX | 270.62 | 0.00 | 10 | 2.307.92 | 0.00 | 43 | | | |
| | 0.00 | 0.00 | | 0.00 | 0.00 | 34 | 52.43 C | 0.00 | 3 |
| MIN | -25.77 | 3.00 | 12 | -1.296.91 | 3.00 | 12 | | | |
| | 0.00 | 3.00 | 39 | 0.00 | 3.00 | .27 | 7.01 C | 3.00 | 9 |
| 27 MAX | 264.53 | 0.00 | 13 | 1.830.43 | 0.00 | 46 | | | |
| | 0.00 | 0.00 | e de la seconda de la second | 0.00 | 0.00 | and the second | \$2.42 C | 0.00 | |
| MIN | -32.30 | 3.00 | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | -1.536.63 | | 34 | 52.43 C | 0.00 | 3 |
| IVITIN | 0.00 | 3.00 | 39 | and the second | 3.00 3.00 | 15 | 2010 | 7 00 | • |
| | 0.00 | 5.00 | 76 | 0.00 | 3.00 | 2 7 | 7.01 C | 3.00 | 9 |
| 28 MAX | 257.78 | 0.00 | 16 | 1.394.74 | 0.00 | 49 | | | |
| | 0.00 | 0.00 | 19 | 0.00 | 0.00 | 34 | 52.43 C | 0.00 | 3 |
| MIN | -39.39 | 3.00 | 18 | -1.770.85 | 3.00 | 18 | | | |
| | 0.00 | 3.00 | 39 | 0.00 | 3.00 | 27 | 7.01 C | 3.00 | , - - - - - |
| | | A A A | | | | | | | |
| 29 MAX | 250.37 | 0.00 | | 1,008.44 | 0.00 | and the second second second | | | |
| | 0.00 | 0.00 | and the second | 0.00 | 0.00 | | 52.43 C | 0.00 | 3 |
| MIN | -47.31 | 3.00 | 11 A. | -2,000.27 | | 21 | | | |
| | 0.00 | 3.00 | 58 | 0.00 | 3.00 | 27 | 7.01 C | 3.00 | 9 |
| 30 MAX | 242.41 | 0.00 | 22 | 678.08 | 0.00 | 58 | | | |
| | 0.00 | 0.00 | | 0.00 | 3.00 | | 52.44 C | 0.00 | |
| MIN | -55.87 | 3.00 | | -2,227.19 | 3.00 | 19 24 | 22.44 U | 0.00 | 3 |
| 141714 | 0.00 | 3.00 | 45 | | 3.00 | and the second second second | 7 01 0 | 1 00 | |
| | 0.00 | 3.00 | 4) | 0.00 | 3.00 | 45 | 7.01 C | 3.00 | 9 |

Pacific Consultants International of Japan, Bldg.#47, DDC Center, Third Floor, Mokhali, Dhaka1212

| ob No. | | VER TH | ang sa sa sa sa | | Checked by : | | | Date: 1 | 2/2/99 |
|---------------------|---|-----------------|-------------------|---------------------------|--------------|--------------------------|--|----------------------------|-------------------|
| | | | | | | | <u></u> _ | | 2/2/99 |
| | M | AX. POS | 5. LL M | OMEN | T ENV | ELOP | @ SPAN | 12 | |
| ni seriit Anna S | | (DUE | тосо | NC LANE | LOAD, P | =292.40 | KN) | | |
| | <u> </u> | | | | | | | | |
| MEMB | FY/FZ | DIST | LD | MZ/MZ | DIST | LD : | FX | DIST | LD |
| 31 MAX | 233.32 | 0.00 | 25 | 409.14 | 0.00 | 64 | | | |
| | 0.00 | 0.00 | 57 | 0.00 | 3.50 | 57 | 52.43 C | 0.00 | 37 |
| MIN | -65.56 | 3.50 | 27 | -2.437:30 | 3.21 | 27 | 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1 | 0.00 | 37 |
| | 0.00 | 3.50 | 7 | 0.00 | 3.50 | 45 | 7.01 C | 3.50 | 90 |
| 32 MAX | 223.47 | 0.00 | 10 | 171.10 | 0.00 | | | | |
| ar maa | 0.00 | 0.00 | 28 57 | 174.18 | 0.00 | 71 | | | |
| MIN | -79.56 | 3.50 | 31 | 0.00 -2.733.25 | 3.50 | 57 | 52.43 C | 0.00 | 37 |
| | 0.00 | 3.50 | 45 | -2.7 <u>33.25</u> 0.00 | 3.50 | 31 | | | |
| | 0.00 | 0.00 | | 0.00 | 3.50 | 45 | 7.01 C | 3.50 | 90 |
| 33 MAX | 209.21 | 0.00 | 32 | 26.83 | 0.00 | 83 | | an din Ang Ang Ang Sala | |
| | 0.00 | 0.00 | 57 | 0.00 | 3.50 | - 85 - 57 | 52.43 C | 0.00 | |
| MIN | -90.99 | 3.50 | 34 | -2.903.79 | 2.92 | 34 | 92.43 C | 0.00 | 37 |
| | 0.00 | 3.50 | 45 | 0.00 | 3.50 | 45 | 7.01 C | 3.50 | 90 |
| | | | | | | | 7.01 C | 5.50 | 90 |
| 4 MAX | 197.56 | 0.00 | 35 | -20.48 | 0.00 | 90 | | | |
| | 0.00 | 0.00 | 57 | 0.00 | 3.50 | 57 | 52.43 C | 0.00 | 37 |
| MIN | -107.04 | 3.50 | 38 | -3.123.74 | 3.50 | -38 | | 0.00 | |
| | 0.00 | 3.50 | 45 | 0.00 | 3.50 | 45 | 7.01 C | 3.50 | 90 |
| | | | | | | | | | |
| 35 MAX | 181.30 | 0.00 | 39 | -60.78 | 0.00 | 90 | | | |
| | 0.00 | 0.00 | 57 | 0.00 | 3.50 | 57 | 52.43 C | 0.00 | 37 |
| MIN | -119.51 | 3.50 | 41 | -3,219.56 | 2.92 | 41~ | | | |
| | 0.00 | 3.50 | 45 | 0.00 | 3.50 | 45 | 7.01 C | 3.50 | 90 |
| 6 MAX | 160.61 | 0.00 | | | | n an Allanda Allandar | | | |
| | 168.61 | 0.00 | 42 | -100.53 | 3.50 | 1 | | | |
| MIN | 0,00 -i36.51 | 0.00 | 57 | 0.00 | 3.50 | 57 | 52.43 C | 0.00 | 37 |
| ALLEN . | 0.00 | 3.50 3.50 | · · | -3.317.08 | 3.50 | 45 | • • • • | | |
| | 0.00 | 0.00 | 45 | 0.00 | 3.50 | 45 | 7.01 C | 3.50 | 90 |
| 7 MAX | 151.57 | 0.00 | 46 | -88.05 | 2.00 | | | | |
| | 0.00 | 0.00 | 57 | 0.00 | 2.00 | 57 | 52.43 C | 0.00 | |
| MIN | -145.38 | 2.00 | 47 | -3,329.59 | 2.00 | 47 | J2:43 C | 0.00 | 37 |
| | 0.00 | 2.00 | 45 | 0.00 | 2.00 | 45 | 7.01 C | 2.00 | 90 |
| | | ананан Хатар | | - 19 9 - 19 | | | | | |
| 8 MAX | 143.49 | 0.00 | 48 | -75.49 | 2.00 | 1 | an di ta | | |
| | 0.00 | 0.00 | 57 | 0.00 | 2.00 | 57 | 52.43 C | 0.00 | 37 |
| MIN | -153:36 | 2.00 | The Carlos of the | -3.329.42 | 0.00 | 47 | | | |
| | 0.00 | 2.00 | 45 | 0.00 | 2.00 | 45 | 7.01 C | 2.00 | 90 |
| 9 MAX | 134,56 | 0.00 | دم | 53.57 | | | | | |
| ~ 191717 | 0.00 | 0.00 | 50 57 | -53.57 0.00 | 3.50 | 1 - 1 - 1 | | | |
| | - 19 - 19 - 19 - 19 - 19 - 19 - 19 - 19 | | 2 2 - | | 3.50 | 57 | 52.43 C | 0.00 | 37 |
| MIN | -166.42 | 3.50 | 52 | -3,322,99 | 0.00 | 49 | 48. 2 A | | 1. 1. 1. 1. A. A. |

have failed Pacific Consultants International of Japan, Bldg #47, DDC Center, Third Floor, Mokhali, Dhaka1212

Job No.

.

Designed by

Date : 12/2/99

MAX. POS. LL MOMENT ENVELOP @ SPAN2 (DUE TO CONC LANE LOAD, P =292.40 KN) 法国际公司 化磷酸盐 医白白素

24

| | | | <u>a a taa a</u> | | | | | | |
|---------------------------------------|--|--------------|--|--|--|--|----------------------|---------------------|--------------|
| МЕМВ | FY/FZ | DIST | LD | MZ/MZ | DIST | LD | FX | DIST | LD |
| | | 0.00 | | . | 5 E.N | | | | |
| 40 MAX | 121.74 | 0.00 0.00 | 53 57 | -31.67 0.00 | 3.50 3.50 | 57 | 52.43 (* | 0.00 | 37 |
| N ALXI | 0.00 | | | -3.237.18 | 0.58 | 53 | 92.49 C | 0.00 | |
| MIN | -183,16 0.00 | 3.50 3.50 | 56 45 | 0.00 | 3.50 | -15 | 7.01 C | 3.50 | 90 |
| | 0.00 | 0.00 | | 0.00 | 5.50 | | 7.01 C | 0.00 | <i>,</i> ,,, |
| 41 MAX | 105.08 | 0.00 | 57 | -9 75 | 3.50 | 1 | | | |
| | 0.00 | 0.00 | 57 | 0.00 | 3.50 | 57 | 52.43 C | 0.00 | 37 |
| MIN | -195.34 | 3.50 | 59 | | 0.00 | * 56 | | Hand V | |
| | 0.00 | 3.50 | 45 | 0.00 | 3.50 | 45 | 7.01 C | 3.50 | 90 |
| | | | | | | | | | |
| 42 MAX | 93.07 | 0.00 | 60 | 18.88 | 3.50 | 9 | | | |
| | 0.00 | 0.00 | 57 | 0.00 | 3.50 | 57 | 52.43 C | 0.00 | 37 |
| MIN | -210.77 | 3.50 | 63 | -2.939.21 | 0.58 | 60 | | | |
| | 0.00 | 3.50 | 45 | 0.00 | 3.50 | 45 | 7.01 C | 3.50 | 90 |
| | e ng | | | | | | | | |
| 43 MAX | 77.94 | 0.00 | 64 | 151.05 | 3.50 | 23 | | | |
| | 0.00 | 0.00 | 57 | 0.00 | 3.50 | 57 | 52.43 C | 0.00 | 37 |
| MIN | 221.56 | 3.21 | 66 | -2.774.47 | 0.00 | -63 | | | |
| | 0.00 | 3.50 | 45 | 0.00 | 3,50 | 45 | 7.01 C | 3.50 | 90 |
| | | 신하는 | | $\{i_{1}, \cdot\}$ | | | | | |
| 44 MAX | 67.38 | 0.00 | | | 3.50 | 30 | | | |
| | 0.00 | 0.00 | and the second | 0.00 | 3,50 | and the second | 52.43 C | 0.00 | 37 |
| MIN | -234.72 | 3.50 | the second s | the second second second second | 0.29 | 67 | | | |
| | 0.00 | 3.50 | 45 | 0.00 | 3,50 | . 45 | 7.01 C | 3.50 | 90 |
| | | 0.00 | | | • •• | | | | |
| 45 MAX | 54.69 | 0.00 | | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 3.00 | 35 | 52.43 C | 0.00 | 37 |
| MIN | 0.00 | 0.00 | | 0,00 •2,277,55 | 3.00 0.00 | 57 70 | 22. 4 3 € | 0.00 | 31 |
| MIN | -243.51 0.00 | 3.00 3.00 | | | 3.00 | | 7.01 C | 3.00 | 90 |
| | 0.00 | 3.00 | | 0.00 | 5.00 | | See Letter | 5.00 | 70. |
| 46 MAX | 46.08 | 0.00 | 74 | 946.81 | 3.00 | 40 | | | |
| | 0.00 | 0.00 | and the second | - アントレン かたいきょう | 3.00 | 57 | 52.43 C | 0.00 | 37 |
| MIN | •251.60 | 3.00 | | | | 1.1.1 | | | |
| | 0.00 | 3.00 | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | and the second | e da la serie de la serie d | in the state of the state | 7.01 C | 3.00 | 90 |
| | | | | | | | | | |
| 47 MAX | 38.35 | 0.00 | 77 | 1.322.22 | 3.00 | 44 | | | |
| | 0.00 | | | 0.00 | | and the second | 52.43 C | 0.00 | 37 |
| MIN | | | 79 | -1.822.03 | | | | $(1,1) \in \{0,1\}$ | |
| | 0.00 | 3.00 | 45 | 0.00 | 3.00 | 45 | 7.01 C | 3.00 | 90 |
| 48 MAX | 31.26 | 0.00 | | 1,748.63 | | 48 | | | |
| | 0.00 | | | 이 없는 것이 아파지 않아? | and the second | | 52.44 C | 0.00 | 37 |
| MIN | and the second | | 82 | and the second second second | | | | | |
| · · · · · · · · · · · · · · · · · · · | 0.00 | 3.00 |) 45 | and the second | | 1.1.1 | 7.01 C | 3.00 | 90 |
| | | | | | | | | | |

Pacific Consultants International of Japan, Bldg.#47, DDC Center, Third Floor, Mokhali, Dhaka1212

OVER THE RIVER RUPSA IN KHULNA, PHASE-2 Designed by: Date: 12/2/99

Job No. :

| MAX. POS. LL MOMENT ENVELOP @ SPAN2 (DUE TO CONC LANE LOAD, P =292.40 KN) | | | | | | | | | |
|--|---------------|------|----|-----------|------|----|-------------|----------------------------|---------------------------|
| мемв | FY/FZ | DIST | LD | MZ/MZ | DIST | LD | FX | DIST | LD |
| | | 0.00 | | | | | | an contra de | |
| 49 MAX | 24.73 | 0.00 | | 2.217.95 | 3.00 | 51 | | | |
| | 0.00 | 0.00 | 57 | 0.00 | 3.00 | 57 | 52.43 C | 0.00 | 37 |
| MIN | -271.68 | 3.00 | 85 | -1.342.24 | 0.00 | 82 | | | · · · · |
| | 0.00 | 3.00 | 45 | 0.00 | 3.00 | 45 | 7.01 C | 3.00 | 90 |
| 50 MAX | 18.81 | 0.00 | 86 | 2.724.68 | 3.00 | 54 | | | |
| | 0.00 | 0.00 | 57 | 0.00 | 3.00 | 57 | 52.43 C | 0.00 | |
| MIN | -277.34 | 3.00 | | -1.091.56 | 0.00 | 85 | 52.45 C | 0.00 | 37 |
| | 0.00 | 3.00 | 45 | 0.00 | 3.00 | 45 | 7.01 C | 3.00 | 90 |
| | | | | | | | | | |
| 51 MAX | 13.26 | 0.00 | 89 | 3.263.10 | 3.00 | 56 | | n in Argentante. Ngjara | |
| | 0.00 | 0.00 | 57 | 0.00 | 3.00 | 57 | 52.43 C | 0.00 | 37 |
| MIN | -280.87 | 3.00 | 90 | -834.36 | 0.00 | 88 | | | |
| | 0.00 | 3.00 | 45 | 0.00 | 3.00 | 45 | 7.01 C | 3.00 | 90 |
| 52 MAX | -6.26 | 0.00 | | | | | | | 1997 - 199 1997 - 1997 |
| JZ MAA | -0.20 0.00 | 0.00 | | 4,023.41 | 4.00 | 59 | | | |
| MIN | | 0.00 | 57 | 0.00 | 4.00 | 57 | 52.44 C | 0.00 | 37 |
| WHIN | -280.88 | 4.00 | 90 | -378.71 | 0.00 | 90 | te takining | | |
| | 0.00 | 4.00 | 45 | 0.00 | 4.00 | 45 | 7.01 C | 4.00 | 90 |
| 53 MAX | -6.26 | 0.00 | 1 | 4,418.77 | 2.00 | 60 | | | |
| | 0.00 | 0.00 | 57 | 0.00 | 2.00 | 57 | 52.43 C | 0.00 | 37 |
| MIN | -280.83 | 2.00 | 90 | 212.57 | 0.00 | 1 | | 0.00 | |
| | 0.00 | 2.00 | 45 | 0.00 | 2.00 | 45 | 7.01 C | 2.00 | 90 |
| | | | | 0.00 | 00 | | 1.01 C | 4.UU | <u>;</u> 90 |

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