ob No.: Designed by: Checked by: Date: January 22, 2000

иемв	LOAD NOD	E AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
2 1 T	LOADS						
		OP CABLE PRESTRESS					
1000	LOAD 1: DUE TO 1	OF CURE INESTRESS					
	MEMBER	•	ES	EM	EE		
				0.035	0.93		
ng Project	7 39 71 103 135 167	5,434.20 10,868.40	0.938 0.938	0.93 <b>8</b> 0.938	0.938		
	8 40 72 104 136 168 9 41 73 105 137 169	16,302.60	0.938	0.938	0,938		
	10 42 74 106 138 170	27,171.00	0.938	0.938	0.938		
	11 43 75 107 139 171	32,605.20	0,938	0.938	0.938		
	12 44 76 108 140 172	43,473.60	0.938	0.938	0.93 <b>8</b> 1.021		
	13 45 77 109 141 173 14 46 78 110 142 174	54,342.00 65,210.40	1.021	1.021	1.188		
	15 47 79 111 143 175	76,078.80	1.357	1.357	1.357		
	16 48 80 112 144 176	86,947.20	1,526	1,526	1.526		
	17 49 81 113 145 177	92,381.40	1.696	1,696	1.696		
	1# 50 #2 114 146 178	97,815,60	1.866	1.866 2.035	1, <b>8</b> 66 2,035		
	19 51 83 115 147 179 20 52 84 116 148 180	103,249.80 108,684.00	2.035 2.340	2.340	2.340		
	21 53 85 117 149 181	108,684.00	2:340	2.340	2.340		
	22 54 86 118 150 182	108,684.00	2.340	2,340	2.340		
	23 55 87 119 151 183	108,684.00	2.340	2,340	2,340		4.0
	24 56 88 120 152 184	103,249,80	2,035 1, <b>866</b>	2.035 1. <b>866</b>	2.035 1,866		
	25 57 89 121 153 185 26 58 90 122 154 186	97,815.60 92,381.40	1.696	1.696	1.696		
k in the	27 59 91 123 155 187	86,947.20	1.526	1.526	1.326		
	28 60 92 124 156 188	76,078.80	1.357	1.357	1.357		
in Majita N	29 61 93 125 157 189	65,210.40	1.188	1.188	1.188		
	30 62 94 126 158 190	54,342,00 43,473,60	1.021 0.938	1.021 0.938	1.021 0.93 <b>8</b>	네고 날 때	
Š. V	31 63 95 127 159 191 32 64 96 128 160 192	32,605.20	0.938	0.938	0.938		
	33 65 97 129 161 193	27,171,00	0.938	0.938	0.938		
	34 66 98 130 162 194	16,302.60	0.938	0.938	0.938		
	35 67 99 131 163 195	10,868.40	0.938	0.938	0.938 0.938		
	36 68 100 132 164 196	5,434.20	0.938	0.938	0.93		
	LOAD 2 : DUE TO	BOTTOM CABLE PREST	RESS				
	11 62 05 177 150	10,868.40	-1.830	-1,830	-1.830		
	31 63 95 127 159 32 64 96 128 160	21,736.80	and the second second	-1.839	-1.830		
	33 65 97 129 161	32,605.20		-1.\$30	-1.830		
2.	34 66 98 130 162	43,473.60		-1.830	-1.830		
	35 67 99 131 163	48,907.80		-1.830 -1.830	-1.830 -1.830		
	36 68 100 132 164 37 69 101 133 165	48,907,80 48,907,80	4.00	•1.830	-1.830		
	38 70 102 134 166	48,907.80		-1,830	-1.830		
4 1.75	39 71 103 135 167	48,907.80		-1.830	-1.830		
	40 72 104 136 168	48,907.80			-1.830	and the first of the second of the second	
	41 73 105 137 169	43,473.60	and the second of the second		-1,830 -1,830		
	42 74 106 138 170 43 75 107 139 171	32,605.20 21,736.80		the state of the s	-1, <b>83</b> 0 -1, <b>83</b> 0	the state of the s	
	44 76 108 140 172	10,868.40		The state of the s	-1.830		
	1 202	21,736.80			-1.017		
	2 201	21,736.80			-1.830 -1.830	Control of the Contro	
	3 200	27,171.00 32,605.20			-1.830 -1.830		
	4 10 193 199 5 9 194 198	32,603.20 38,039.40		The second of the second		and the second of the second	
	6 TO \$ 195 TO 197	43,473.60	and the second second	and the state of t			
	11 192	27,171.00	and the second second	and the state of t	and the second second	2004	
1000	6 12 i9i	16,302.60					
	13 190	5,434.20	-1.830	-1,915	-2.000		

ob No.; Designed by: Checked by: Date: January 23, 2000

мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ч	MOM-2
	3	9 5 4.	12 222 28	12 212 24				
		2	17,223.38 -17,223.38	-13,712.62 9,323.52	0.00 0.00		0.00 0.00	
							0,00	-23,137.85
<b>2</b>	3	2 3	17,230.62 -17,230.62	-9,302,79 459.81	0.00	0.00	0,00	23,137,81
			117,250,02	437.81	0.00	0.00	0.00	-42,844.52
3	3	3	22,664.04	-465.09	0.00	0.00	0,00	52,788.99
		•	-22,664.04	465.09	0.00	0.00	0.00	-54,843.15
	3	4	28,098.21	-465.10	0,00	0.00	0.00	64,787.27
		5	-28,098.21	465.10	0.00		0.00	-66,835.91
	3	5	33,532.33	-465.40	0.00	0.00		
		6	-33,532.33	465.40	0.00	0.00	0.00	76,779.27 -78,795.05
					Popular San Page 1999			10,753.05
6	3	6	38,967.25 -38,967.25	-464.95 464.95	0.00	0.00	0.00	88,740.03
75						0.00	0.00	-90,687.52
7	3	7	44,401.52	-465,74	0.00	0.00	0.00	85,590.55
			-44,401.52	465.74	0,00	0.00	0.00	-87,223.96
	3	8	49,835.18	-465,43	0.00	0.00	0.00	82,126.79
		9	-49,835.18	465.43	0.00	0.00	0.00	-83,690.12
- In Market 6	3	9	49,835.11	-464.82	0.00	0.00	0.00	60 646 00
		10	-49,835.11	464.82	0.00	0.00	0.00	68,646.09 -70,155.82
10	3	20						
The Name of		10 11	55,269,72 -55,269.72	-465.43 465.43	0.00	0,00 0,00	0.00	50,017.71
							0.00	-51,488.08
11	3	11	55,269.19	<b>-465,19</b>	0.00	0,00	0.00	36,446.92
		12	-55,269.19	465.19	0.00	0,00	0,00	-37,895.14
12	3	12	55,270.25	-465.29	0,00	0.00	0,00	7,811.73
		13	-55,270.25	465.29	0,00	0.00	0.00	-9,263.39
13	3	13	55,293,47	-1,021.68	0.00	0.00	0,00	25 221 05
		14	-55,293.47	1,021.68	0.00	0.00	0.00	-25,331,95 22,413,57
14	3	14	4,467.02	715 41				
		15	4,467.02	-716.41 716.41	0.00	0.00 0.00	0.00	22,193.51 -24,359.11
							0.00	-24,359,11
15		15 	71,606,04 -71,606,04	-717.88	0.00	0.00	0.00	-78,872.01
			71,000.04	717.88	0.00	0.00	0,00	76,977.19
16	3	16	82,474.34	-719.65	0,00	0.00	0.00	-106,418,60
		17	-82,474,34	719.65	0.00	0.00	0,00	104,518.10
17	3	17	\$7,907.45	-719.34	0.00	0.00	0.00	-128,515.60
		18	-87,907.45	719,34	0.00	0.00	0.00	126,582.70
18	3	18	93,343.26	-719,48	0.00			
14 14 14 15 15 15 15 15 15 15 15 15 15 15 15 15		19	-93,343.26	719.48	0.00	0.00	0.00	-152,428,80 150,452.90
e ( . KC) 19				1.3	1-26			150,452.50
4. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	3	19 20	98,776.23 -98,776.23	-716,55 716,55	0.00	0.00	0.00	-178,041.30
n di Saka Tangan Tili dali. Kacamatan Sakamatan				710.33	0.00	0.00	0,00	176,018,50
20	3	20	104,209.80	-713.23	0.00	0.00	0.00	-220,225.10
		21	-104,209.80	713.23	0.00	0.00	0.00	217,433.60
21	3	21	104,201.20	-656.22	0.00	0.00	0.00	-217,433.70
		22	-104,201.20	656,22	0,00	0.00	0.00	216,101.80
22		22	102,318.30	233.17		1.	er i kalabya sa	
		23	-102,318,30	-233,17	0.00	0.00 0.00	0.00	-244,964,40 245,380,10
	100.6			and the same of th			0.00	245,380.10
		23 24	102,322,40 -102,322,40	313.66 -313.66	0.00	0.00	0.00	-245,379,80
			-1 <b>74,346,76</b>	-313.50	0,00	0.00	0,00	246,406,00
		a Aline British III (1976) Julien <u>Anna mala</u> nia						

ob No.: Designed by: Checked by: Date: January 23, 2000

мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
24	i swapina katao Pangana atao	24	96,888,79	318,29	0,00	0.00	0.00	-202,198.80
		25	-96,888.79	-318.29	0.00	0.00	0.00	202,886.70
25.	3	25 26	91,455.53 -91,455.53	322.56 -322.56	0.00	0,00	0,00 0,00	-175,297.10 175,932.00
26	3	26	86,020.42	322.61	0.00	0.00	0,00	-150,085.30
		27	-86,020.42	-322.61	0,00	0,00	0.00	150,663.20
27	3	, <b>27</b> .	\$0,586.02	323.38	0.00	0.00	0.00	-126,666.50
		28	-80,586.02	-323.38	0.00	0.00	0.00	127,205.00
28	3	28	69,718.53	321.20	0.00	0.00	0,00	-97,761.02
		29	-69,718.53	-321,20	0.00	0.00	0.00	98,300.38
29	3	29	-6,354.19	317.07	0.00	0.00	0.00	4,931.40
	Andrew State (1997) The Mark State (1997)	27 30	6,354.19	-317.07	0.00	0.00	00,0 00.0	+,931.40 +3,950.62
			arienden die	yan paramet		的复数形式		
30	3	30	47,981,48	314.43	0.00	0,00	0.00	-51,525.58
		31 - 143	<b>-47,981.48</b>	-314.43	0.00	0,00	0.00	52,197.83
31	3	31	47,972.99	-36.96	0.00	0.00	0.00	-17,604.31
er spirit in the		32	47,972.99	36. <del>96</del>	0.00	0.00	0,00	17,185.30
32	3	32	47,973.15	-36.38	0.00	0.00	0.00	12,901.06
		33	47,973.15	36.38	0.00	0.00	0.00	-13,291.33
#79 To			that o					
33	3	33 34	53,407.33 -53,407.33	-37.07 37.07	0,00 0,00	0,00	0,00	38,277,94 -38,671.10
						<b>商进入民员</b>		30,071.10
. 34	3	34	53,408.24	-37,55	0.00	0.00	0.00	68,754.99
		35 1 (1) (1) (1) (1)	-53,408,24	37.55	0.00	00,00	0.00	-69,100.61
35	3	35	53,407.77	-37.57	0,00	0.00	0,00	84,141.60
		36	-53,407.77	37.57	0.00	0.00	0,00	-84,422.23
36	3	36	47,973.64	-35.82	0.00	0,00	0.00	\$9,521.03
		37	-47,973.64	35.82	0.00	0.00	0.00	-89,714.94
		•	19 590 24					
37	3	37 38	42,539,34 -42,539.34	-38,73 38,73	0.00	0.00	0.00 0.00	94,808.46
					eri — Poletingija Oranjan <sub>del</sub> objekt			
38	3	38	42,539.08	-36.14	0.00	0.00	0.00	94,897.15
		39	-42,539.04	36,14	0.00	0,00	0.00	-94,955,45
39	3	39	47,973.64	-37.82	0.00	0.00	0.00	89,861,67
		40	-47,973.64	37.82	0.00	0,00	0.00	-89,921.53
40	. i i i i i i i i i i i i i i i i i i i	40	53,407.29	-37,19	0,00	0,00	0.00	\$4,824,68
		41	-53,407.29	37.19	0.00	0.00	0,00	-\$4,803.09
			a production of					
41	3	41 42	53,408.61	-37.43	0.00	0.00	0.00	69,758.86
			-53,408.61	37.43	0.00	0,00	0,00	-69,677.27
42	3	42	53,407.77	-35.87	0.00	0,00	0,00	39,591.44
Ty cycle Alich		43	-53,407.77	35.87	0.00	0,00	0.00	-39,460,60
43	3	43	47,973.29	-36.62	0.00	0,00	0,00	14,475.50
i sakata	a de la	4	47,973.29	36,62	0,00	0.00	0,00	-14,347,86
10.3 (11.2)								
. 44	3	44 45	47,973.26 -47,973.26	-37.23 37.23	0.00	0.00	0.00 0,00	-15,737, <b>80</b> 15, <b>892.3</b> 5
								15,472.35
45	3		47,985.26	-388.77	0.00	0.00	0.00	-50,485.95
1.01.0		46	-47,985.26	388,77	0.00	0.00	0.00	49,589.14
46	3	46	-6,350.28	-393.16	0.00	0.00	0.00	5,\$\$5.24
							-,	V, VVV

ob No.: Designed by: Checked by: Date: January 23, 2000

МЕМВ	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-у	MOM-Z
47	<b>3</b>	47	69,722.22	-394.97	0,00	0.00	0,00	-96,142.2
		48	-69,722.2 <u>2</u>	394.97	0,00	0.00	0,00	95,382.9
48	3	48	80,590,93	-398.30	0.00	0.00	Δ.00	124 936 6
		49	-80,590,93	398.30	0.00	0.00	0.00	-124,826.6 124,069.3
49	3	49	86,025.35	-396,42	0,00	0.00	0.00	140,000
		50	-86,025.35	396.42	0.00	0.00	0.00 3.00	-148,066,7 147,274.2
						3 2 2 2 2 4 3		
50	3	50 51	91,459.47 -91,459.47	-397,48 397,48	0.00	0.00	0,00	-173,120.5
			V., 1	377.46	0.00	0.00	0.00	172,275.5
51	3.	51 (	96,893.19	-393.18	0.00	0.00	0.00	-199,865.0
		52	-96,893,19	393,18	0.00	0.00	0.00	198,970.0
52	3	52	102,327.00	-388,46	0.00	0,00	0.00	-243,177.0
		53	-102,327.00	388,46	0.00	0.00	0.00	241,880.70
			100 900 10					
53		53 54	102,322.10 -102,322.10	-307,54 307,54	0.00 0.00	0.00	0.00	-241,880.40
1350					0.00	0.00	0.00	241,333.40
54	3	54	101,921.40	252,77	0.00	0.00	0.00	-244,792.30
		55	-101,921.40	-252.77	0.00	0.00	0.00	245,327.30
55	3	55	101,926.20	338.41	0.00	0.00	0.00	-245,327.20
		. 56	-101,926.20	-338.41	0.00	0.00	0.00	246,610.40
56	76 - 3 - 3	56	96,492.15	747.67	9.00			
		57	•96,492.15	343.67 -343.67	0,00	0.00	0.00	-202,403.60 203,276.60
							0.00	203,170.00
<b>57</b>	િક્ષ કુલ કુલ <b>ક</b> ુલ કુલ કુલ કુલ કુલ કુલ કુલ કુલ કુલ કુલ ક	57	91,058.00	348,33	0.00	0.00	0.00	-175,687.40
erda (1)	No.	58	-91,058.00	-348.33	0.00	0.00	00,00	176,497.90
58	3	58	\$5,623.23	348,63	0.00	0.00	0.00	-150,650.80
		59	<b>-8</b> 5,623.23	-348.63	0.00	0,00	0.00	151,398.80
59	<b>.</b>	59	80,188,98	348.20	0.00	0,00	0.00	122 400 00
		60	-80,188.98	-348.20	0.00	0,00	0.00 0.00	-127,400.30 128,096.60
							Property of	
	3 4 9 6 <b>3</b> -	60 61	69,321.12 -69,321.12	346.31 -346.31	0,00 0,00	0,00	0.00	-98,653.86
	20.5			-540.51		0.00	0.00	99,334.62
61	3	61	-6,751.72	343.46	0.00	0.00	0.00	3,896.63
7.01.37		62	6,751.72	-343.46	0,00	0.00	0.00	-2,834.78
62	3	62	47,583.79	339.66	0.00	0,00	0.00	<b>-5</b> 2,639. <b>8</b> 3
	y diwo iki iliyata Nasarin iliyota	63	-47,583,79	-339,66	0.00	0,00	0.00	53,424.36
63								Talanta .
	3	63 64	47,575.17 -47,575.17	-33.62 33.62	0.00	0.00	0.00	-18,829.47 18,446.26
						<b>V.</b>	0.00	10,440.20
. 4	3	64	47,574.89	-33,50	0,00	0,00	0.00	11,640.01
161 (F) 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		65	-47,574,89	33.50	0.00	0.00	0.00	-12,010.51
65	3	65	53,009.29	-33.04	0.00	0.00	0.00	36,996.13
professor (1995) Hard Mary (1995)		66	-53,009.29	33.04	0.00	0.00	0.00	-37,370.41
66	3	44	53,010.42					
		66 67	-53,010.42	-33,65 33,65	0.00 0.00	0.00 0.00	0.00	67,455.65 -67,781.84
				Array Million			0.00	-07,781.04
67	3 ×	67	53,009.18	-33,21	0.00	0.00	0.00	82,824.39
286 A. A.		65	-53,009.18	33.21	0.00	0,00	0.00	-83,082.07
68	3	68	47,574,28	-33.51	0,00	0.00	0.00	<b>\$8,179,61</b>
		69	-47,574.88	33.51	0,00	0.00	0.00	<b>-88</b> ,350.32
69	3	48	43 140 40					
4 North Control		69 70	42,140.69 -42,140.69	-34,79 34.79	0.00	0.00	0,00	93,444,51
	194 Jan 186			T	<b>7.27</b>	V.VV	0.00	-93,514.68

Date: January 23, 2000

мемв	LOAD	NODE	AXIAL	sı	HEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
						A AA	0.00	0.00	93,511.27
70	3	7	and the second second	11.96 11.96	-30.55 30.55	0,00	0.00	0.00	-93,558.55
		The state of the s							00 263 00
71	3	7		75,43	-33.91	0,00	0.00 0.00	0.00	88,461.08 -83,488.88
		7.	2 –47,5	/3.43	33.91	0,00			
72	3	7	7.1.4	09.24	-33.08	0,00	0.00	0.00	83,391.85
		. ( At <b>7</b>	3 -53,0	09.24	33.08	0.00	0.00	0.00	-83,342.26
73	3			10.14	-34.49	0.00	0.00	0.00 0.00	68,298.83 -68,194.43
			4 -53,0	10.14	34.49	0.00	0.00	0.00	<b>~39,177.73</b>
74	3	7	74 53,0	09.14	-33.45	0.00	0.00	0.00	
		and the second second		09.14	33.45	0,00	0.00	0.00	-37,969.88
10 10 10 10 10 10 10 10 10 10 10 10 10 1	3		75 47,5	75.34	-34.07	0,00	0.00	0.00	12,983.76
75			4.5	75,34	34.07	0.00	<ul> <li>* ** ** ** ** ** ** ** ** ** ** **</li> </ul>	0.00	-12,856.16
			16 27	75.58	-33.74	0.00	0.00	0.00	-17,229.11
76	3			75.58 75.58	33.74	0.00	41	0.00	and the state of t
ting til sampa fyriger. Frankliger Stock				dia di	and a second	6.00	00,0	0.00	-51,961.63
77	3	1 May	4 1 4	587.53 587.53	-407.56 407.56	0.00	transfer to the contract of	0.00	and the second of the second of the second
To a final section of the section of			agawaya Walayayayayay	garana.					
	3	the state of the s	and the second of the	747.78 747.78	-411.36 -411.36	0.00 0.00		0.00	
			79 6,	747,78	711.30				
79	3		4 NO 1 NO 1	324.93	-414.74	0.00	the state of the second state of the second	0,00 0.00	
			<b>8</b> 0 - <b>69</b> ,	324.93	414.74	0.00	) 0.00		V V V
80		•	80 80,	193.01	-417.57	0.00	and the second of the second	0.00	
			81 -80,	193.01	417.57	0.00	) 0.00	0.00	125,180,00
81		3	B1 85,	627.20	-416.91	0.00	0.00	0.0	
•				627.20	416.91	0.00	) 0.00	0.0	148,276,50
			82 91	061.89	<b>-4</b> ]6,76	0.00	0.00	0.0	174,123,50
**************************************	e i na aliente de la composition de la Composition de la composition de la co	3	97 PF 1	061,89	416.76	0.0		0.0	0 173,171.60
				405 t#	-412.40	0.0	0.00	0.0	0 -200,760.50
83		3	Annual Control of the	,495.87 ,495.87	412.40				The state of the s
			(a) (1) (b)				A A A	0.0	0 -243,966.50
. 84		3		,929.50 ,929.50	-407.30 407.30	and the second of the second o	the state of the s		
1	<b>5</b>	3		,924.60	-321,11				
			<b>\$</b> 6 -101	,924.60	321.11	<b>10.0</b>			
<b>8</b> 4	6	<b>3</b>		726,50	641.27				and the state of t
			87 -102	,726.50	-641.27	0.0	o 0.00	0.0	0 230,350.80
	7	3	\$7 102	2,734.80	716.47				
				2,734.80	-716,47		) <b>e</b> 0.00	) 0.(	0 233,107.00
			<b>81</b> 9'	7,301.66	720.85	j 0.0	0.00	) 0.(	0 -128,900.40
	•	3		7,301.66	-720.85	and the state of t	420	the control of the co	
							),0 0,0	0.0	00 -163,294.80
	9	3		1,868,08 1,868.08	725.13 -725.13	and the second of the second of	The state of the second	N 40	
				ded de				나마를 하하셨다.	
10 July 10 July 10 S	ю,	3		6,432,99	725.3 725.1	State to the second of the	Annual Control of the		
			91 -	6,432.99	-725.3				
n en de la verifica. La companya de la co	91	3	171.4	0,998,94	725.0	2. S. S. S. Landell, Phys. Lett. 16, 116	00 0.0	and the first the same	00 -117,250.10
			97 -8	0,998,94	-725.0	3 0.	00 0.0	o .	00 119,076.00
	92	3	92 7	0,130,02	722.9	1 0.	00 0.0	and the first state of the state of the	-89,634.83
				0,130.02	-722.9		0.0	0 0.	00 91,452.16
	who say we are also	and the second second	فياحم وجياسين بدند					The second second second	

ob No.; Designed by: Checked by: Date: January 23, 2000

MEMB	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
93	3	93	-5,941,96	721.05	0.00	0.00	0.00	11,77
	大学 禁。	94	5,941.96	-721.05	0.00	0.00	0.00	-9,58
94	3	94	48,393.29	717.14				
		95	-48,393.29	717.14 -717.14	0.00 0.00	0.00	0.00	-45,897
					0.00	0.00	0.00	47,823
95	3	95	48,362.69	388,05	0.00	0.00	0.00	-13,230
		<b>%</b>	-48,362.69	-388.05	0.00	0.00	0.00	14,336
96	3	96	48,362.53	3 <b>88</b> .16	0.00	0.00	0.00	
		97	-48,362.53	-388.16	0.00	0.00	0.00	15,741
			a salah di Salah			1	0.00	-14,621
67	and the latest of							
97	•	97 98	53,796.65 -53,796.65	387.58	0.00	0.00	0.00	39,612
			-55,750.05	-387.58	0.00	0.00	0.00	-38,494
98	3	98	53,797.68	388.34	0.00	0.00	0.00	68,571
	Length (Comment	99	-53,797.68	-388.34	0.00	0.00	0.00	-67,413
99	3	<b>~</b>	62.205.01					H 12 (4)
		99 100	-53,796.01 -53,796.01	. 387.14 -387.14	0.00	0.00	0.00	82,45
			,//0,0,	701.14	0.00	0.00	0,00	-81,22
100	160 × 15 3	100	48,362.69	388.36	0.00	0.00	0.00	86,324
	e de journe de la 18 et la journe de la 18	101	-48,362.69	-388.36	0.00	0.00	0.00	-85,007
101	3	101	42,928.32	387,29	0.00			ji firma karista. Tanan salah
		102	-42,928,32	-387.29	0.00 0.00	0.00	0.00 0.00	90,107
						0.00	0.00	-89,323
204		204	372,20	1,844,37	0.00	0.00	0.00	22,477
		205	-372.20	-1,844,37	0.00	0.00	0.00	-19,691
205	3	205	372,20	1,873.18	0.00	0.00	0.00	10.40
egeneral e de		206	-3 <i>7</i> 2.20	-1,873.18	0.00	0.00	0.00	19,681 -11,250
204								
206	•	206 207	372.20 -372.20	1,873.96	0.00	0.00	0.00	11,249
		-20	-372.20	-1,873.96	0.00	0.00	0,00	-2,817
207	3	207	372.21	1,869.81	0.00	0.00	0.00	2,797
arene kaj li jud		208	-372,21	-1,869.81	0.00	0.00	0.00	-17.
210	3	210	<b>-1.77</b>					
		210	8.77	375.25 -375.25	0.00	0,00 0,00	0.00	2,103.
						• • • • • • • • • • • • • • • • • • • •	0.00	•1,5 <b>23</b> .
211	3	211	-5.81	398.09	0.00	0.00	0.00	1,510.
K. F. F. Mar.		212	8.81	-398.09	0.00	0.00	0.00	878.
212	3	212	-8.81	397.87	0.00	0.00	0.00	
	e de la companya de l	213	8.81	-397.87	0.00	0.00	0.00 0.00	-877.1 3,264.0
414								3,204.
213	3	213 214	-8.81	398.61	0.00	0.00	0,00	-3,256.
		• 333	3.81	-398.61	0.00	0.00	0.00	3,874.
216		216	445.26	-778,73	0.00	0.00	0.00	-10,242
18 - 18 July 1		217.	-445.26	778.73	0.00	0.00	0.00	9,063.0
217	3	217	445.27				and the second of the	
		218	445,27	-774,19 774,19	0.00 0.00	0.00	0.00	-9,069.1
					0.00	0.00	0.00	3,262.7
218	g system 3 d	218	445.26	-774.25	0,00	0.00	0,00	-3,262.4
Mary 1	, w.c	219	-445,26	€ ; <b>774.25</b>	0.00	0.00	0,00	-2,544.5
219	3	219	445.27	-776.27				
集造章		220	-445,27	776.27	0.00	0,00	0,00	2,548.7
						V.VV	0.00	-3,700.5
239	3	209	-936.88	3,269.03	0.00	0.00	0.00	669,6
savey. The		240	936.88	-3,269.03	0.00	0.00	0,00	14,860.3
240	3	240	0.28	-0.02	0,00	0.00	0.00	-0.0

ob No.: Designed by: Checked by: D a.t.e.: January 23, 2000

at Arman da								<del> </del>
мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-у	мом-г
241	3	209 242	936.41 -936.41	-3,641.25 3,641.25	0.00 0.00	0.00 0.00	0.00 0.00	-2,137,12 -15,157,13
242	3	242 243	-0.57 0.57	-0.17 0.17	0.00	0,00 0.00	0.00 0.00	-0,23 -0.10
243	3	215 244	-202.58 202.58	1,133.35 +1,133.35	0.00 0.00	0.00 0.00	0,00 0,00	2,246,17 3,138,17
244	3 3	244 245	0.57 -0.57	-0.01 0.01	0.00 0,00	0.00 0.00	0.00 0.00	0.04 0.02
245	3	215 246	195.33 -195.33	-1,124.54 1,124.54	0.00 0.00	0.00 0.00	0.00 0.00	-2,212.26 -3,128.34
246	3	246	-0.35	0.08	0.00	0.00	0.00	0.08
247	3	247 221	0.35 392.54	-0.08 -2,029.17	0.00	0.00	0,00	0.07 -3,309.65
248	3	248 248	-392,54 -0.33	2,029 17 -0.04	0.00	0.00	0,00 0,00	-6,32 <b>8</b> .28
249		249 221	0.33 -381.66	0.04 1,583.92	0.00	0.00	0.00	0.03 1,557.52
250		250 250	381.66 -0.61	-1,5 <b>8</b> 3.92 0.02	0.00	0.00	0.00 0.00	5,966.71 0.04
264	3	251	0.61 -3,269.00	-0.02 2937.34	0.00	0.00	0.00	0.04 13,458.38
265		265 265	3,269.00 -3,269.02	937.34 937.34	0,00	0.00	0.00	-5,068.59 5,068.58
		266 266	3,269.02 -3,269.02	-937.34 678.05	0.00	0.00	0.00	8,890.48
266		267	3,269.02	-678.05	0.00	0.00	0.00	9,899.53 -9,898.92
267		267 268	-3,269.01 3,269.01	268.37 -268.37	9.00	0.00	0.00	10,294.94
268		269	-3,269.03 3,269.03	<b>-43.13 43.13</b>	0.00	0,00	0.00	-10,295.06 10,224.70 -10,224.87
269		269 270	-3,269.02 3,269.02	-270.24 270.24	0.00	0,00 0,00	0.00	9,814,73
270		270 271	-3,269.02 3,269.02	-427.69	0.00 0,00		0.00 0.00	-9,814.77 9,169.45
271		271 272	-3,269.04 3,269.04	-557,59 557,59		0,00 0.00	0.00 0.00	-9,169,44 8,329.87
- <b>272</b>		272 273	-3,269.02 3,269.02	-754.51 -754.51	0.00 0.00	0.00 0.00	0.00	-8,329,85 7,195.81
273	3	273 274	-3,269.03 3,269.03	-837.97 837.97	0,00	0.00 0.00	0.00 0.00	-7,195.90 5,937.37
274		274 275	-3,269.03 3,269.03	-843.52 843.52	0.00 0.00	0.00	0.00 0.00	-5,937.36 4,671.00
275	3 ************************************	275 276	-3,269.00 -3,269.00	-782.75 782.75		0.00 0.00	0.00 0.00	-4,671.0 3,496.3
276		276 277	-3,269.01 3,269.01	684.54 684.54	0.00 0.00	0.00 0.00	0.00 0.00	-3,496,36 2,469.30
and the second second	544	war and the state of the state			and the second section of the second	and the community file and a second	the server as a server of the server of	and the state of the control of the state of

ob No.: Designed by: Checked by: Date: January 23, 2000

MEMB	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
277		277 278	-3,269.03 3,269.03	-570.49 570.4 <del>9</del>	0,00 0,00	0,00 0,00	0,60 0.00	-2,469,30 1,613.58
278	3	27 <b>8</b> 279	-3,269.03 3,269.03	-455.99 -455.99	0.00 0.00	0.00 0,00	0.00 0.00	-1,613.55 929.73
279		279 280	-3,269.01 3,269.01	-351.14 351.14	0.00 0.00	0.00 0.00	0,00 0,00	-929.72 403.24
280	3	280 281	-3,269.02 3,269.02	-261.79 261.79	0,00 0.00	0,00 0,00	0.00 0.00	-403.24 10.81
281	3	281 282	-3,269.02 3,269.02	-190,59 190,59	0.00 0.00	0.00	0.00 0.00	-10.80 -274,81
282	3	282 283	-3,269.03 3,269.03	-120.13 120.13	0.00 0.00	0.00 0.00	0,00 0.00	274.82 -454.76
283	3	283	-3,269.00	-71.94	0,00	0.00	0.00	454,76
284	3	284 284	3,269.00 -3,269.03	71.94 15.98	0.00	0.00	0.00	-562,45
285	3	285 285	3,269.03 -3,269.01	-15.98 61.49	0.00	0.00	0.00	562.46 -538.33
286	3	286 286	3,269.01 -3,269.02	-61.49 70.13	0.00	0.00	0.00 0.00	538,33 -415.21
287		287 287	3,269.02 -3,269.02	-70.13	0.00	0.00	0.00	415.21 -274.88
288		288	3,269.02	59.79 -59.79	0.00 0.00	0.00	0.00 0.00	274.88 -155.27
289		288	-3,269.01 3,269.01	42.56 -42.56	0.00 0.00	0.00 0.00	0,00 0,00	155.27 -70.16
		289 290	-3,269.03 3,269.03	26,89 -26.89	0.00	0,00 0,00	0,00 0.00	70.16 -16.40
290		290 291	-3,269.01 3,269.01	14.28 -14.28	0.00 0.00	0.00 0.00	0.00 0.00	16.40 12.15
291		291 292	-3,269,02 3,269,02	5,57 -5.57	0.00 0.00	0.00 0.00	0.00 0.00	-12,15 23,28
292		292 293	-3,269.01 3,269.01	0.38 -0.38	0.00	0.00 0.00	0,00 0,00	-23,28 24.02
293		293 294	-3,269.02 3,269.02	-2.14 2.14	0.00 0.00	0.00 0.00	0,00 0,00	-24.02 19.73
294		294 295	-3,269.02 -3,269.02	-2.92 2.92	0.00	0.00 0.00	0.00 0.00	-19.73 13.88
<b>295</b> [		295 296	-3,269.02 3,269.02	-2.72 2.72	0.00	0.00 0.00	0.00 0.00	-13.88 8.44
296		296 297	-3,269.02 3,269.02	-2.10 2.10	0.00	0.00 0.00	0,00 0,00	-8.44 4.23
297		297 29 <b>8</b>	-3,269.02 3,269.02	-1.40 1.40	0.00	0.00 0.00	0.00 0.00	-4.23 1,43
291		29 <b>1</b> 299	-3,269.01 3,269.01	-0.80 0.80	0,60 0.00	0.00 0.00	0.00 0.00	-1.43 -0.17
299	3	299 300	-3,269.02 3,269.02	-0,36 0.36	0.00 0.00	0.00 0.00	0.00 0.00	0.17 -0.90

ob No.: Designed by: Checked by: Daie: January 23, 2000

мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ч	MOM-Z
300	3	300	•3,269,0 <b>2</b>	-0.09	0.00	0.00	0.00	0.90
		301	3,269,02	0.09	0.00	0.00	0.00	-1.07
301	3	301	-3,269.02	0,06	0.00	0.00	0.00	1,07
		302	3,269.02	-0.06	0.00	0.00	0.00	-0.95
302	3	302	-3,269,02	0.12	0.00	0.00	0.00	0.95
		303	3,269.02	-0.12	0.00	0.00	0.00	-0.71
303	3	303	-3,269.02	0.12	0.00	0.00	0.00	0,71
303		304	3,269.02	-0.12	0.00	0.00	0.00	-0.46
204		204	1 260 02		0.00	0.00		
304		304 305	-3,269.02 3,269.02	0.11 -0.11	0.00 0.00	0.00	0.00 0.00	0,46 -0,25
			2 240 02	31 Mary 13 (4)		0.00	• • •	
305	3	305 306	-3,269.02 3,269.02	0.0 <b>8</b> -0.0 <b>8</b>	0.00	0.00 0.00	0.00	0.25 -0.09
306	3	306 307	-3,269.02 3,269.02	0.06 -0.06	0.00	0.00	0.00 0.00	0.09 0,04
307		307	-3,269.02	0.05	0.00	0.00	0.00	-0.04
		308	3,269.02	-0.05	0.00	0,00	0.00	0.14
308		308	-3,269.02	0.05	0,00	0.00	0.00	-0.14
		309	3,269.02	-0.05	0.00	0.00	0.00	0.22
310		3 310	3,641.23	936.63	0.00	0.00	0.00	13,747.04
3.0		311	-3,641.23	-936.63	0.00	0.00	0.00	-5,255.07
				1 2 3 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		4.00		
311		3 311 312	3,641.23 -3,641.23	936,64 -936.64	0.00 0.00	0.00 0.00	0,00 0,00	5,255,07 8,935,38
			Styling 2 s				g folgskert.	
312		3 312 314	3,641.24 -3,641.24	674.91 -674.91	0.00	0.00 0.00	0.00	-8,935.75 9,958.62
				riemār giene				
313		3 314	3,641,22 -3,641,22	262.94 -262.94	0.00 0.00	0.00 0.00	0.00	-9,959.2 <b>8</b> 10,363.20
			化氯化氯化	100			$\mathcal{N}_{\mathcal{A}}(h, s, s, h, \mathcal{M})_{\mathcal{A}}$	
314		3 315 316	-3,641.26 -3,641.26	49.36 49.36	0.00 0.00	0.00 0.00	0.00 0.00	-10,363,64 10,297.68
			er dynasty vite					
315	1.04	3 316 317	3,641.20 -3,641.20	-278.17 278.17	0.00	0.00	0.00	-10,297.61 9,887.07
			A su D, t :					
316		317	3,641.23	-436.31	0.00	0.00	0.00	-9,887.23
		318	-3,641.23	436.31	0.00	0,00	0.00	9,238.07
317	in the five five t	3 318	3,641.25	-567.05	0,00	0.00	0.00	-9,238.25
		319	-3,641.25	567.05	0.00	0.00	0,00	8,391.96
318			3,641.22	-764.15	0,00	0.00	0.00	-8,392.04
		320	-3,641.22	764.15	0.00	0,00	0.00	7,249.04
319			3,641.24	- <b>84</b> 7,36	0.00	0.00	0.00	-7,249.04
		321	-3,641.24	847.36	0,00	0.00	0.00	5,980.25
320		3 a 20 321	3,641.24	-851.92	0.00	0.00	0.00	-5,980.26
		322	-3,641.24	<b>\$</b> 51.92	0.00	0.00	0.00	4,703.80
321		3 22	3,641.24	-789.91	0.00	0.00	0.00	-4,703.81
		323	-3,641.24	789.91	0.00	0.00	0.00	3,519,76
322		3 323	3,641.22	-690.29	0.00	0.00	0.00	-3,519.74
		324	-3,641.22	690,29	0.00	0.00	0.00	2,484.67
323		. (1.5> . (1.5. (1.5. (1.5. ) 3	3,641.22	-574.92	0,00	0.00	0.00	-2.484.66
		325	-3,641.22	574.92 574.92	0.00	and the second of the second o	0.00	1,622.28
State of the second		<u> 1814 - Racijis</u>				rein gerrana diere		

ob No.: Designed by: Checked by: Date: January 23, 2000

мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-у	MOM-Z
324	3	325	3,641.27	-459.19	0,00	0,00	0.00	1 633 33
		326	-3,641.27		0.00	0,00	0.00	-1,622.27 933.28
325	3	326	3,641,24	-353,34				4 8 7 8 3
	aj lieta elektriko (j. 17. 18. julija - Listonija II., 18. julija izatera (j. 18. julija izatera (j. 18. julija izatera (j. 18. julija i	327	3,641.24	353.34	0.00	0.00 0.00	0.00	-933.27 402.92
724								102.52
326	3	327 328	3,641,22 -3,641,22	-263.17 263.17	0.00	0.00	0.00	-402.93
	ARTA Grant		********	205.17	0,00	0.00	0,00	7,78
327	3	328	3,641.24	-191.36	0.00	0.00	0.00	-7.79
		329	-3,641.24	191.36	0,00	0,00	0.00	-279.64
328	3	329	3,641.26	-120.30	0.00	0.00	0.00	279.64
		330	-3,641.26	120,30	0.00	0.00	0.00	460.46
329	3	330	3,641.23	-71,78	0.00	0.00		
	学的 化二二烷 氨酰二二烷	331	3,641.23	71.78	0.00 0.00	0.00	0.00 0.00	460,46 -568,43
770				14 (534)/15	and section for			500.43
330		331 313	3,641.23 -3,641,23	16.70 -16.70	0,00	0.00	0.00	568,43
			به	-10.70	0.00	0.00	0.00	•543.6J
331	3	313	3,641.24	62.40	0.00	0.00	0,00	543.61
		333	-3,641.24	-62.40	0,00	0.00	0.00	-419.00
332	<b>3</b> .	333	3,641.23	70,95	0.00	0.00	0.00	419.00
		334	-3,641.23	-70,95	0.00	0.00	0.00	-277.20
333	3	334	3,641,23	60.41	0.00	0.00	0.00	277,20
		335	-3,641.23	-60.41	0.00	0.00	0.00	-156.42
334	3	335	3,641.23	42,94				
		336	3,641.23	42,94	0.00 0.00	0.00	0.00	156.42 -70.54
							0.00	-70,34
335	3	336 337	3,641.26 2,641.26	27.09	0.00	0,00	0.00	70.54
			-3,641.26	-27.09	0.00	0.00	0.00	-16.33
336	3	337	3,641.23	14,37	0.00	0.00	0.00	16.33
		338	-3,641.23	-14.37	0,00	0.00	0.00	12.43
337	3	338	3,641.24	5,58	0.00	0,00	0.00	-12.43
		339	-3,641.24	-5.58	0.00	0,00	0.00	23.60
338	3	339	3,641.24	0.76				
		340	-3,641.24	0.35 -0.35	0.00	0,00 0,00	0.00 0.00	-23.60
								24,31
339	3	340 341	3,641.24 -3,641.24	-2.19	0.00	0.00	0.00	-24.31
			-3,041.24	2.19	0.00	0,00	0.00	19,94
340	3	341	3,641,24	-2.96	0.00	0.00	0.00	-19.94
排法法		342	-3,641,24	2.96	0.00	0.00	0.00	14,02
341	3	342	3,641,24	-2.76	0.00	0.00	0.00	14.00
		343	-3,641.24	2.76	0.00	0.00	0.00	-14.02 8,51
342		747	2 641 22			Maria (A		
	Barina in	343 344	3,641,23 -3,641,23	-2.12 2.12	0,00	0.00	0.00 0.00	-8.51
				wild fitter?	erren de la <del>de la de</del> la del Grando de la dela dela dela dela dela dela del		0.00	4.26
343	1 1 <b>3</b>	344	3,641.23	-1.42	0.00	5.90	0.00	-4,26
		345	-3,641.23	1.42	0.00	0.00	0,00	1.43
344	3 3	345	3,641.23	-0.81	0.00	0.00	0.00	-1,43
		346	-3,641.23	0.81	0.00	0.00	0.00	-0.19
345	3	346	3,641.24	A 74				
		347	-3,641.24	-0.36 0.36	0,00 0.00	0,00 0,00	0,00 0,00	0.19
ander Ger							0,00	-0.92
346	3	347 348	3,641,24	-0.09	0.00	0.00	0.00	0.92
down and the	reserve to the second		-3,641.24	0.09	0.00	0.00	0.00	-1.09

ob No.: Designed by: Checked by: Date: January 23, 2000

мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ч	мом-г
347	- 3.	348	3,641.23	0.06	0.00	0.00	0.00	1.09
		349	-3,641.23	-0,06	0,00	0,00	0,00	-0.96
348	77 ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	349	3,641.24	0,12	0.00	0.00	0,00	0.96
		350	-3,641.24	-0.12	0.00	0.00	0.00	-0.72
349	<b>.</b>	350	3,641.24	0.13	0.00	0.00	0.00	0.72
		351	-3,641.24	-0.13	0.00	0.00	0,00	-0.47
350		351	3,641.23	0.11	0.00	0.00	0.00	0.47
		352	-3,641.23	-0.11	0.00	0,00	0.00	-0.26
351	3.1	352	3,641,24	0.08	0,00	0,00	0.00	0.26
		353	-3,641.24	-0.0	0.00		0.00	-0.09
352	3	353	3,641.24	0.06	0.00	0.00	0.00	0.09
		354	-3,641.24	-0,06	0.00		0,00	0.04
74 jan 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	3	354	3,641.24	0.05	0.00	0.00	0,00	-0.04
		332	-3,641.24	-0.05	0.00	0,00		0.15
354	3	332	3,641.24	0.05	0.00	0.00	0.00	-0.15
		355	-3,641.24	-0.05	0.00	0,00	2.5	0,22
356	3	356	-1,133.34	202.68	0,00	0.00	0.00	2,836.87
		357	1,133.34	-202.68	0.00	0.00		-1,042,93
357	3		-1,133.34	202.68	0.00	0.00	0.00	1,042.93
		358	1,133,34	-202.68	0.00	0.00	0.00	1,931.96
358	· 6	358	-1,133.37	146.82	0.00	100	and the second of the second of the second	-1,931.74
		360	1,133.37	-146.82	0,00	0.00	0,00	2,146.96
359	3		-1,133.35	58,36	0.00		and the second second	-2,146.74
		361	1,133.35	-58.36	0.00	0,00	0,00	2,229.73
360	3	and the second second	-1,133.35	-9.23	0.00	The second secon		-2,229.95
		362	1,133.35	9.23	0,00	0.00	0.90	2,212.28
361	3		-1,133.35	-58.00 58.00	0.00 0.00		to the second	-2,212.3 <b>8</b> 2,122.24
		363	1,133.35	38,00	te Arlandi Sil		•	4,144.44
362	3		-1,133,35	-92.12	0.00	and the second second	the state of the s	-2,122.19
		364	1,133.35	92.12		0.00	0.00	1,981.43
363	3		-1,133,34	-120.11	0.00	and the state of t		-1,981.41
		365	1,133.34	120.11	0,00	V.W	0.00	1,799,26
364	3				0.00			
	Mariana Nasaran	366	1,133.37	162.71	0,00	0.00	0.00	1,553.69
363	3				0.00			-1,553.69
		367	1,133.35	180,74	0,00	0.00	0.00	1,281.57
366	3		and the second s		0.00			the second of the second of
		368	1,133.31	[81.95	0.00	0,00	0,00	1,008.00
367	3				0.00			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		369	1,133.37	168,85	0,00	0.00	0.00	754.35
368	3							-754,35
		370	1,133.36	147.69	0.00	0.00	0.00	532.65
369	3							
		371	1,133,33	123.09	0,00	0.00	0.00	348.02
370	3							
		372	1,133.32	98.39	0.00	o da como de Calabora A grafa da Calabora	0,00 (10 %) (82)	200.51

ob No.: Designed by: Checked by: Date: January 23, 2000

МЕМВ	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-у	MOM-Z
371	3	372	-1,133.32	-75.81	0.00	0,00	0.00	-200,
		373 ×	1,133.32	75.81	0,00	0.00	0.00	86,9
372	3	373	-1,133.36	-56.52	0.00	0.00	0.00	-86,5
		374	1,133,36	56.52	0.00	0.00	0.00	2.3
373	3	374	-1,133,34	41.17	0.00	0.00	0.00	-2.3
		375	1,133.34	41.17	0.00	0.00	0.00	-59.
374	3	375	-1,133,34	-25.97	0.00	0,00	0.00	59,2
		376	1,133,34	25.97	0,00	0.00	0.00	-98.0
375	3	376	-1,133.34	-15.58	0,00	0.00	0.00	98,(
		377	1,133.34	15.58	0.00	0.00	0.00	-121.3
376	<b>3</b>	377	-1,133.33	3.40	0.00	0.00	0.00	121,2
		359	1,133.33	-3.40	0.00	0.00	0,00	-116.0
377	3	359	-1,133.35	13.22	0.00	0.00	0.00	116 (
		379	1,133.35	-13.22	0.00	0.00	0.00	116.0 -89.5
378	3	379	•1,133.35	15.10	0.00	0.00	0.00	89.:
		380	1,133.35	-15.10	0,00	0.00	0.00	-59.2
379	3	380	-1,133.33	12.88	0,00	0.00	0.00	59.2
		381	1,133.33	-12.88	0.00	0.00	0.00	-33.4
380	3	381	+1,133.33	9.17	0.00	0.00	0.00	33.4
	ur. Salata	382	1,133.33	-9.17	0.00	0.00	0.00	-15,1
381	3	382	-1,133,34	5.80	0.00	0.00	0.00	15.1
		383	1,133.34	-5.80	0.00	0.00	0.00	-3.5
382	3	383	-1,133.36	3.08	0.00	0,00	0.00	3.5
		384	1, 133,36	-3.08	0,00	0.00	0,00	2.6
383	3	384	-I,133.34	1.21	0.00	0.00	0.00	-2.6
		385	1,133.34	-1.21 ·	0.00	0.00	0.00	5.0
384	3	3 <b>8</b> 5 386	-1,133,35	0.09	0.00	0.00	0.00	-5.0
			0.00 1,133.35	-0.09	0.00	0.00	0.00	5.1
385	3	386 387	-1,133,35	-0.46	0.00	0.00	0.00	-5.1
		Note that he	1,133.35	0.46	0.00	0.00	0.00	4.2
386	3	387 388	-1,133.35	-0.63	0.00	0.00	0.00	-4.2
		n, and	1,133.35	0.63	0.00	0.00	0.00	2.9
387	9 3 3	3## 389	-1,133.35 1,133.35	-0.59 0.59	0.00	0.00	0.00	-2.9
		to the state of	1,133.33	0,37	0.00	0.00	0.00	1.8
388	ffilia (n. 1915). Seagar (n. 1915).	3 <b>8</b> 9	-1,133,35 1,133,35	-0.45 0.45	0.00	0.00	0.00	-1.83
	-50 f	rijas virtis elijasiks	was figure 5 h		0.00	0.00	0.00	0.9
389	3 74 f	390 391	•1,133.35 1,133.35	-0.30 0.30	0.00	0.00	0.00	-0.9
		a nama ngabatan	1,193.35	0.30	0.00	0.00	0.60	0.3
390	<b>3</b> .	391 392	-1,133.35	-0.17	0.00	0.00	0.00	-0.31
	was in the	ji wasansi kata Ma	1,133.35	0.17	0.00	0.00	0,00	-0.04
391	3	392	-1,133,35 946 1,133,35	-0.08	0.00	0.00	0.00	0.04
	we like	• • • • • • • • • • • • • • • • • • •	10 to	0.08	0.00	0.00	0,00	-0.19
392	. A., 1€, <b>3</b>	393 194 394	-1,133,34	-0.02	0.00	0.00	0.00	0.19
	Soft Filt		4) 1,133.34 -000	0.02	0.00	0,00	0.00	-0.23
393	3	394 395	-1,133.34	0.01	0.00	0,00	0.00	0.23
Maria de la Maria Maria de Carta de Maria	89.0	373	1,133,34	-0.01	8.00	0.00	0.00	-0.20

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мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-у	мом-г
394	3	395	-1,133,34	0.03	0.00	0.00	0.00	0.20
		396	1,133.34	-0.03	0,00	0.00	0,00	-0.15
395	3	396	-1,133,34	0.03	0,00	0.00	0.00	0.15
		397	1,133.34	-0.03	0.00	0,00	0.00	-0.10
396	3	397 398	-1,133,34 1,133,34	0.02 -0.02	0.00	0.00 0.00	0.00	0,10 -0,05
397	3	398	-1,133.34	0.02	0.00	0.00	0.00	0.05
		399	1,133,34	-0.02	0.00	-0.00	0.00	-0.02
398	3	399	-1,133,34	0.01	0.00	0.00	0,00	0.02
		400	1,133,34	-0.0t	0.00	0.00	0.00	0.01
399	3	400 378	-1,133,34 1,133,34	0.01 -0.01	0,00	0,00 0,00	0.00	-0.01 0.03
					e Herring in	West States		
400		378 401	-1,133.34 1,133.34	0.01 -0.01	0.00	0.00 0.00	0.00 0.00	-0.03 0.05
402	3	402	1,124,54	195.25	0.00	0.00	0.00	2,832.81
		403	-1,124.54	-195.25	0.00	0.00	0.00	-1,046.88
403	3	403	1,124.54	195.25	0,00	0.00	0.00	1,046,85
		404	-1,124,54	-195.25	0.00	0.00	0.00	1,943.41
404	3	404 406	1,124.55 -1,124.55	139.43 -139.43	0.00 0.00	0.00	0.00 0.00	-1,943.54 2,157.02
405	3	406	1,124.56	51.57	0.00	0.00	0.00	-2,157,10
		407	-1,124.56	-51.57	0.00	0,00	0.00	2,238.65
406		407 408	1,124.55 -1,124.55	-15.17 15.17	0,00 0.00	0.00 0.00	0.00	-2,238.76 2,219.56
407	3	408	1,124.55	-63.68	0.00	0.00	0.00	-2,219.67
	- 불통이왕 1 - 1일 강남 1개	409	Market Artist Control			0.00	0.00	2,127.09
408	3 miles	The second secon		-97.21		0.00	0.00	-2,127.17
		410		医现象性睫状	0.00		0.00	1,983.71
409	3	410			44	0.00	0.00 0.00	-1,983.79 1,798.48
410	3	411	1,124.56		in visit (1967)	0.00	0.00	-1,798.49
		412				0.00	0.00	1,550.83
411	3	The state of the s				0.00	0.00	-1,550.81
		413	-1,124.54	183,11	0.00	0.00	0.00	1,277.09
412	3	413 414		The second secon		the second of th	0,00	-1,277.09 1,002.67
				7 July 4 A				
413		414 415			and the second of the second	The second of the second	0,00 0,00	-1,002.67 748.74
414	•	415	1,124:54	-147.79	0.00	0.00	0.00	-748.74
		416	-1,124.54				0.00	527.18
415	3						0.00	-527,17
		417		$F_{ij} = \{ e_{ij} \in \mathbb{R} \mid i \in \mathbb{N} \}$		0.60	0.00	342.94
416	3	417 . 41 <b>8</b>					0.00 0.00	-342,93 195,97
417		418			THE ALLOW	ja naturaja r	0.00	-195.97
		419		75.15		and the state of t	0.00	*193,97 **3.09
ri <u>aan</u> seed ah in seed ah	and the state of the state	a marangan arawan bari	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1					a ja otoj setneni

ob No.: Designed by: Checked by: Date: January 23, 2000

мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ч	мом-2
418	<b>3</b>	419 420	I,124.55 -I,124.55	-55,82 55,82	0,00 0,00	0,00 0,00	0.00 0.00	-83,07 -0,82
419	3	420	1,124.56	<del>-4</del> 0,46	0,00	0,00	0.00	0,83
		421	-1,124.56	40,46	0.00	0,00	0.00	-61.70
420	3	421 422	i,124.55 ÷l,124.55	-25,30	0.00	0.00	0.00	61.69
				25.30	0,00	0.00	0.00	+99.80
421	3	422 423	1,124.55 -1,124.55	-14,95 14.95	0.00 0.00	0.00 0.00	0.00 0.00	99.79 -122.34
422	3	423	1,124.54	3.86	0.00	0,00	0.00	122,33
		405	-1,124.54	-3.86	0.00	0.00	0.00	-116.65
423	3	405 425	1,124.56	13.52	0.00	0.00	0.00	116.64
			-l,124.56	•13.52	0.00	0.00	0.00	-89.68
1. See al. 15. <b>424</b> 15. See asset 1. See	i (1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	425 426	1,124.54 -1,124.54	15.27 -15.27	0.00 0.00	0.00	0.00 0.00	<b>89.68</b> -59.19
425	3	426	1,124.55	12.95	0,00	0.00	0.00	59.19
		427	-1,124.55	-12,95	0,00	0.00	0,00	-33.30
426	3	427 428	1,124,55 -1,124,55	9.18	0,00	0.00	0.00	33.30
427				-9.18	0.00	0.00	0.00	-14.94
		428 429	1,124.54 -1,124.54	5.78 -5.78	0,00 0,00	0.00	0,00 0,00	14.94 -3.37
428		429	l,124.54	3.05	0.00	0.00	0.00	3.37
		430	-1,124.54	-3.05	0.00	0.00	0.00	2.74
429	3	430 431	1,124.55 -1,124.55	1.17 -1.17	0,00 0,00	0.00	0.00	-2.74
					0.00	0.00	0.00	5,10
430	3	431	l,124.54	0.06	0.00	0.00	0.00	-5.10
		432	-1,124.54	-0.06	0.00	0,00	0,00	5.23
	3 2 2 3 3 4 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4	432 433	1,124.55 -1,124.55	-0.48 0.48	0.00 0.00	0,00 0,00	0.00 0.00	-5.23 4.27
432	3	433	1,124,55	-0.64	0,00	0.00		
		434	-1,124,55	0.64	0.00	0.00	0.00 0.00	-4.27 3.00
433	3	434	1,124,54	-0.59	0.00	0.00	0,00	-3.00
		435	-1,124.54	0.59	0.00	0,00	0.00	1.81
434 43.886		435	1,124.55 -1,124.55	-0.46 0.46	0,00 0,00	0,00 0,00	0.00 0.00	-1,8 i 0,90
435	19. januar (j. 18. j 18. januar (j. januar (j. 18. januar (j. januar (j. 18. januar (j. 18. januar (j. 18. januar (j. 18. januar (j	436	1,124.55	-0.30	0.00	0.00	0.00	-0.90
		437	-1,124.55	0.30	0,00	0.00	0.00	0.30
436	(a) (a) (b) (b) (b) (b) (b) (b) (b) (b) (b) (b	437	1,124.55	-0.17	0.00	0.00	0.00	-0.30
		438	-i,124,55	0,17	0.00	0.00	0.00	-0.04
1977 - 1978 - 1979 - 1970 - 19		438 439	1,124.55 -1,124.55	-0.06 0.08	0.00 0.00	0.00 0.00	0.00 0.00	0.04 -0.20
	3	€ 439	1,124,54	-0.02	0.00	0.00		
		440	-1,124,54	0.02	0.00	0.00	0,00 0,00	0.20 -0.23
439		440	1,124.55	0.01	0.00	0.00	0.00	0.23
		41	-1,124.55	-0.01	0.00	0.00	0,00	-0.21
440	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	441 442	1,124.54 -1,124.54	0,03 -0.03	0.00 0.00	0.00 0.00	0.00 0.00	0.21
							V.W	-0.15

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мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ч	MOM-Z
441	3	442	1,124.54	0.03	0.00	0,00	0,00	0,15
		443	-1,124.54	-0.03	0.00	0.00	0,00	-0.10
					0.00	0.00	0.00	0.10
442	3	443 444	1,124.55 -1,124.55	0.02 -0.02	0,00 0,00	0.00 0.00	0.00	-0.05
	A CONTRACTOR							
443	3	444 445	1,124.55 -1,124.55	0.02 -0.02	0,00	0,00	0.00	0.05 -0.02
		<b>497</b>	1,124.55		4,00			
444	3	445	1,124.55	0.01	0.00	0.00	0.00	0.02
		446	-1,124.55	-0.01	0.00	0.00	0.00	0.01
. 445	3	446	1,124.55	0.01	0.00	0.00	0.00	-0.01
		424	-1,124.55	-0.01	0,00	0.00	0.00	0.03
446	3	424	1,124,55	0.01	0.00	0.00	0.00	-0.03
		447	-1,124.55	-0.01	0.00	0.00	0.00	0.05
448	3	448	2,029.17	-392.51	0.00	0.00	0.00	-5,737.81
		449	-2,029.17	392.51	0.00	0.00	0.00	2,186.55
440		449	2,029.17	-392,51	0.00	0.00	0.00	-2,186.55
449	3	450	2,029.17	392.51	0.00	0.00	0.00	3,741.46
						0,00	0.00	2 742 61
450	3	450 452	2,029.20 -2,029.20	-282.83 282.83	0.00	0.00	0.00	3,741.51 -4,169.00
451	3	452 453	2,029.18 -2,029.18	-110.89 110.89	0.00	0.00 0.00	0.00 0.00	4,169.00 -4,338.06
452	3	453		20,39	0.00	0.00	0.00	3 4,337.98
		454	-2,029.18	-20.39	,0.00	0,00	0.00	4,309.79
453	3			115,39	0.00	0.00	0.00	4,309.73
		455	-2,029.16	-115.89	0.00	0.00	0.00	-4,137.88
454	3	455	2,029.19	182.13	0.00	0.00	0.00	4,137.77
		456	-2,029.19	÷1 <b>82</b> .13	0.00	0.00	0.00	-3,866.08
455	3			236.90	0.00		the second control of	
		457	-2,029.17	-236.90	0.00	0,00	0.00	-3,511.92
456	3		and the second of the second	319,48	0.00	0.00		The state of the s
		451	-2,029.20	-319.48	0.00	0.00	0.00	-3,033.59
457	3	451	2,029.16	354,36	0.00	0.00	0.00	3,033.60
		455	-2,029.16	-354,36	0.00	0.00	0.00	-2,502.6
458	3	459	2,029,17	356.35	0.00	0,00	0.00	2,502.67
	14.45	460	Walter and the second	-356.35	0.00	0,00	0.00	-1,968.54
459		460	2,029.18	330.46	0.00	0.00	0,00	1,961.54
		46	and the second second second	-330.46	0.00	0,00	and the first of t	the state of the s
			200			0.00	0.00	1,473.10
460		l 46		288.84 -288.84	0.00			er and the first term of the second
						$\mathbb{R}[\mathbb{R}^n] \cdot \mathbb{R}[\mathbb{R}^n]$		
461	400	46: 46:	4.7 , 74	240,58 -240,58	0.00			and the first transfer of the con-
	*							
462		1.00	and the second second	192.18	0.00		to fit to the same of the fit of the con-	and the control of th
		46	-2,029.17	-192.18	0.00	0.00	0.00	-390.75
463					0.00	- 9 7 × 11 v 1 · · · · · · ·	and the contract of the first of the contract of the	at the first form of the first
		46	-2,029.18	-147.89	0.00	0.00	0.00	-164.64
464		3 46	5 2,029.17	110.16	0.00	5 ↔ 0.00	0.00	168.83
		46	6 -2,029.17	5 A 4 A 5 A 5 A 5 A 5 A 5 A 5 A 5 A 5 A	0.00	0.00	0.00	
e <u>llandin, della ella</u>								

ob No.: Designed by: Checked by: Date: January 23, 2000

MEMB	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ү	MOM-Z
465	1		2 22 42	1.3			i di peri	
403		466 467	2,029,18 -2,029,1\$	\$0,12 -\$0,12	0,00 0,00	0.00	0.00	3.47
			2,025,10	-40.12	V,W	0,00	0.00	116.83
466	3	467	2,029.20	50.40	0.00	0.00	0.00	-116,83
		468	-2,029.20	-50,40	0.00	0.00	0,00	192,52
467		Taylor Barrier	2.22.2					
467	3	468 469	2,029,17 -2,029,17	30.09 -30.09	0,00	0,00	0.00	-192.52
			-2,023.11	+30.05	0.00	0.00	0.00	237.74
468	3	469	2,029.18	-6.94	0.00	0.00	0.00	-237.74
		451	-2,029.18	6.94	0.00	0,00	0.00	227.39
		보상하는 사람						
469	n vita j	451 471	2,029.18 -2,029.18	-26.08 26.08	0.00	0.00	0.00	-227.39
				20.08	0.00	0,00	0.00	175,29
470	3	471	2,029.17	-29.67	0.00	0.00	0.00	-175.28
		472	-2,029,17	29,67	0,00	0.00	0.00	115,98
471			2 000 17				salis il di	
471	3	472 473	2,029.17 -2,029.17	-25.26 25.26	0.00	0.00	0.00	-115.98
			-	5.10	V.V0	0.00	0.00	65.46
472	3	473	2,029.17	-17.96	0.00	0.00	0.00	-65.46
		474	-2,029.17	17.96	0.00	0.00	0,00	29.53
473	3	474	2,029.18	-11.34	0,00	0.00	0.00	-29.53
		475	-2,029.18	11.34	0.00	0.00	0.00	-29.33 6.85
		y contraction.						
474	. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	475	2,029.17	-6,01	0.00	0.00	0.00	-6,85
		476	-2,029.17	6.01	0.00	0.00	0.00	-5.19
475	3	476	2,029.17	-2.34	0.00	0,00	0.00	5.19
		477	-2,029.17	2.34	0.00	0.00	0.00	-9.86
and the second		en geral de la j <u>er</u> a						
476	3	477 478	2,029.18 -2,029.18	-0.15	0.00	0.00	0,00	9.86
			2,02	0.15	0.00	0.00	0.00	-10,16
477	. 3	478	2,029,17	0.91	0.00	0.00	0.00	10.16
		479	-2,029,17	-0.91	0.00	0.00	0.00	-8.34
478	3	479	2,029.19	1.24	0.00	0.00	200	
		480	-2,029,19	-1.24	0.00	0.00	0,00 0,00	8,34 -5,86
그리아를 살았다.			Very state of the second					-5.00
479	3	480	2,029.18	1,15	0.00	0.00	0,00	5.86
		481	-2,029,18	-1,15	0.00	0.00	0.00	-3,56
480	3	481	2,029.18	0.89	0.00	0.00	0,00	3.56
		482	-2,029.18	0.19	0.00	0.00	0,00	-1.78
481	Jess T							
	3	482 483	2,029.18 -2,029.18	0.59 -0.59	0,00 0,00	0,00 0,00	0.00	1.78
				•		0.00	0.00	-0.60
482	3	483	2,029.17	0.34	0.00	0.00	0,00	0.60
A Section of		484	-2,029.17	-0.34	0.00	0.00	0.00	. 0.08
483	3	484	2,029.18	0.15	0.00			
		485	-2,029.18	-0.15	0.00	0.00 0.00	0,00 0,00	-0,08 0,38
n de jarozzak eta 190 Nordan eta 190								0.30
484	3	485	2,029.18	0,04	0.00	0,00	0.00	-0,38
		486	-2,029.18	-0.04	3.5 1.5 1.0,00	0,00	0.00	0.45
485	3	486	2,029,18	-0.03	0.00	6,00	0.00	0.45
		487	-2,029.18	0.03	0,00	0.00	0.00	-0.45 0.40
				ente recentificação de la compansa d				
416	3	487	2,029.18	-0.05	0.00	0.00	0.00	-0.40
		481	-2,029.18	0.05	0,00	0.00	0.00	0.30
487	3	488	2,029.18	-0.05	0,00	0,00	0.00	-0.30
	projekty se Ografia. Kan Sakaratan Alima	489	-2,029.18	0.05	0.00	0.00	0.00	0.20
<u> </u>			2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			ting Maria		

ob No.: Designed by : Checked by : Date: January 23, 2000

мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ч	MOM-Z
488	3	489	2,029.18	-0.04	0.00	0.00	0.00	-0,20
		490	-2,029.18	0.04	0.00	0.00	0.00	0.11
489	3	490	2,029,18	-0.03	0.00	0.00	0.00	-0.11
		491	-2,029.18	0.03	0.00	0.00	0.00	0.04
490	3	491	2,029.18	-0.03	0,00	0.00	0.00	-0.04
		492	-2,029.18	0.03	0.00	0.00	0.00	-0.02
491	3	492	2,029.18	-0.02	0.00	0.00	0.00	0.02
		470	-2,029.18	0.02	0.00	0.00	0,00	-0.06
492	3	470	2,029.18	-0.02	0.00	0.00	0,00	0,06
		493	-2,029,18	0.02	0.00	0.00	0.00	-0,09
494	3	494 495	-1,583,92 1,583,92	-381,74 381,74	0.00 0.00	0.00	0.00	-5,395,76 1,978,70
			1,000.52					
495	3	495 496	•1,583.91 1,583.91	-381,74 381.74	0,00 0.00	0.00	0.00	-1,978.72 -3,707.23
					premie Adam i nije. Posleda premie			
496	3	496 498	-1,583.92 1,583.92	-274.80 274.80	0.00 0.00	0.00	0,00	3,707.13 -4,116.14
		医多种 海森區				۸.00	0.00	
497	3	498 499	-1,583.92 1,583.92	-106.12 106.12	0.00	0.00 0.00	0.00	4,116.14 -4,272.66
498		499	-1,583.92	22.03	0.00	0.00	0.00	4,272,71
***		500	1,583.92	-22.03	0.00	0.00	0.00	-4.237.39
499	3	500	-1,583.87	115.25	0,00	0.00	0,00	4,237.35
		501	1,583.87	-115.25	0.00	0.00	0.00	
500	3	501	-1,583.90	180,02	0.00	0.00	0.00	4,062.45
		502	1,583.90	-180.02	0.00		0.00	-3,790.77
501	3	502	-1,583.93	233.34	0.00	0,00	0,00	3,790.81
		503	1,583.93	-233.34	0.00	0.00	0.00	-3,439.60
502	3	503	-1,583.92	313.62	こうしんがく しんじょん		0.00	3,439.61
		\$04	1,583,92	-313.62	0,00	0,00	0,00	-2,968.30
503	3	504	-1,5\$3.91	347,37	5 1 35 H 1 1 1 3	4.5 -	0.00	2,968.28
		505	1,583,91	-347,37	0.00	0.00	0.00	-2,446.61
						0.00		
504		505 506	-1,583,88 1,583,88	348,92 -348,92	0.00 0.00	the first of the control of the con-	0.00 0.00	2,446,60 -1,922,82
505		506	+1,583.92		0.00		0,00	
303		507	1,583.92		0.00		0.00	
506		507	-1,583.91	282.41	0.00	0.00	0.00	1,437.61
		508	1,583.91				0.00	
507		508	-1,583.94	235.12	0.00	0.00	0.00	1,013.91
		509	1,583.94				0.00	
508		3 509	-1,583.92	187.73	0.00	0.00	0.00	661,22
		510	1,583.92				0.00	
509	erro Busculari. Na seria	3 510	-1,583.90	144,40	0.00	0.00	0.00	379.68
		511	1,583.90					
510	1	511	-1,5#3.93	107,53	0.00	0.00	0.00	163.17
		. 512	1,583.93				0.00	and the state of t
511		3 512	-1,583.93	78.16	0.00	0,00	0.00	1.98
	n en jan saterija. Europagini regenar	513	1,583.93			0.00	0.00	
<u> </u>	<u> se samatan tinggata</u> .		<u> </u>	<u>ar jang biki</u>	n well to be on	s pred greete	160 116 50 L	

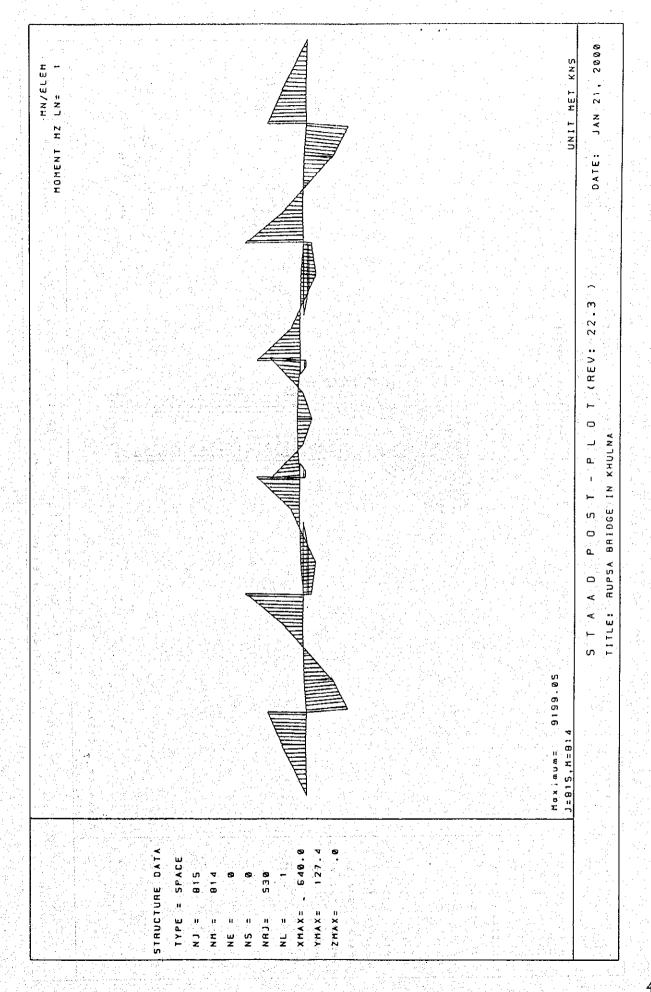
ob No.: Designed by: Checked by: Date: January 23, 2000

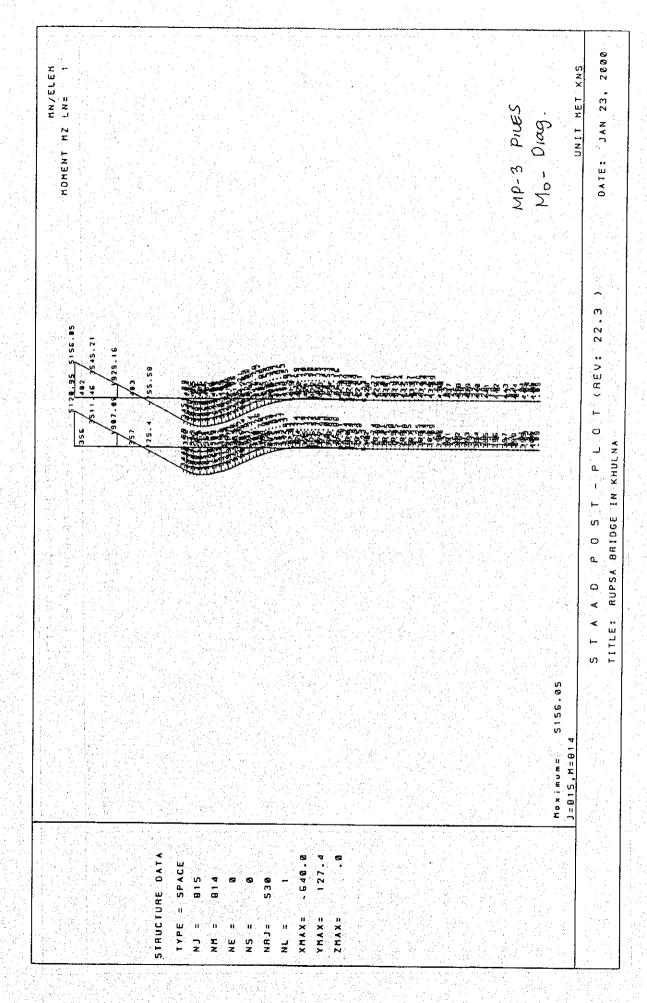
мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-у	MOM-Z
512	3	513 , 514	-1,583,91 1,583,91	49,13 -49,13	0,00	0.00	0.00	-115.15
			1,343.91	77.13	0.00	0.00	0.00	188,75
513	1. a 1. j . <b>3</b> .	514 515	+1,583.91 1,583.91	29.30 -29.30	0.00 0.00	0.00 0.00	0.00 0.00	-1 <b>88.7</b> 5 232,61
514	3	515	1,583.92	-6.84	0.00	0.00	0.00	222.
		497	1,583.92	6,84	0.00	0,00	0.00 0.00	-232.61 222.28
<b>515</b>	3	497 517	-1,583,92 1,583,92	-25.50 25.50	0.00	0,00	0.00 0.00	-222.28 171.22
\$16	3	517	-1,583.91	-28,99	0.00			
		518	1,583.91	28.99	0.00	0.00	0,00 0,00	-171.22 113.22
517	3	518	-1,583.91	-24.67	0.00	0.00	0.00	-113,22
		519	1,583.91	24.67	0.00	0.00	0,00	63.86
518	3	519	-1,583.92	-17.54	0.00	0,00	0.00	-63.86
		520	1,583.92	17.54	0.00	0,00	0.00	28.78
519	3	520	-1,583.91	-11.07	0.00	0.00	0,00	-28.78
		521	1,583.91	11.07	0.00	0.00	0.00	6.65
520	3	521	-1,583.92	-5.87	0.00	0.00	0.00	-6.65
		522	1,583.92	5.87	0.00	0.00	0.00	-5.08
521	3	522	-1,583.92	-2.28	0.00	0,00	0.00	5.08
		523	1,583.92	2.28	0.00	0.00	0.00	-9.64
522	3	523	-1,583.91	-0.14	0.00	0.00	0.00	9.64
		524	1,583,91	0.14	0.00	0.00	0.00	-9.92
523	7. 3. 3.	524 525	-1,583.91 1,583.91	0.89 -0.89	0.00 0.00	0.00	0.00	9.92 ~8.14
524			1 687 01					
	3	525 526	-1,583.91 1,583.91	1,21 -1,21	0.00 0.00	0.00	0,00 0,00	8.14 -5.72
525	3	526	-1,583.92	1.12	0.00	0.00	0.00	5,72
		527	1,583.92	-1.12	0.00	0.00	0.00	-3.47
526	3	527	-1,583.91	0.87	0.00	0.00	0.00	3.47
		528	1,583.91	-0,87	0.00	0.00	0.00	•i.74
527	3	52 <b>8</b> 529	-1,583.92	0.58	0.00	0.00	0.00	1.74
		<b>327</b>	1,583.92	+0.5\$	0.00	0.00	0.00	-0,58
528	e de la filosofia de la filoso Esta de la filosofia de la filo	529	-1,583.92	0.33	0.00	0.00	0.00	0.58
		530	1,583.92	-0.33	0,00	0.00	0.00	0.08
529	3	530	-1,583.92	0.15	0.00	0.00	0.00	-0.08
		531	1,583.92	-0.15	0.00	0.00	0.00	0.37
530	3	531	-1,583.92	0.04	0.00	0.00	0.00	-0.37
		532	1,583.92	-0.04	0,00	0.00	0.00	0.44
531	3	532	-1,583.92	-0.03	9.00	0.00	0.00	-0.44
		533	1,583.92	0.03	0,00	0.00	0.00	0,39
532	3	533	-1,583.92	-0.05	0.00	0.00	0.00	-0.39
		534	1,583.92	0.05	0.00	0.00	0.00	0.29
533	.3	534	-1,583,92	-0.05	0.00	0.00	0.00	-0,29
		535	1,583.92	0.05	0.90	0,00	0.00	0.19
534	3	535	-1,583.92	-0.04	0.00	0.00	0.00	-0.19
		536	1,583.92	0.04	0.00	0.00	0.00	0.10
		38 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	<u> </u>		err op i i itis	e jihan sa jash	nika jawa Milia Al	

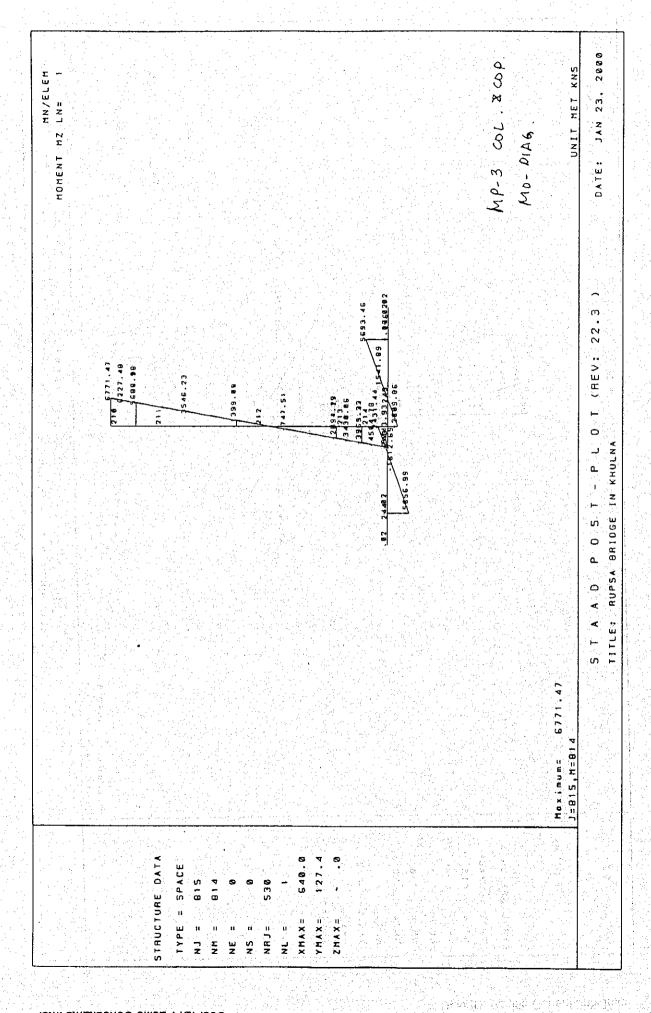
oh No.: Designed by :	Checks	dhu ID	a i c ; January 23, 1600
ink No.			
			<del>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</del>

The state of the s								
мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
535		536	-1,583,92	-0.03	0.00	0,00	0.00	-0.10
333		537			0,00		and the second second	0.04
536		537	-1,583.92	-0.03	0,00	0,00	0,00	-0.04
330		538			0,00	and the second		
537		538	-1,583.92	-0.02	0,00	0.00	0.00	0,02
331		516		and the second second	and the second of the second			
		516	-1,583.92	-0.02	0.00	0.00	0,00	0.06
538	•	539			4.0			

# SHRINKAGE LOAD OF FRAME 5 (WHOLE STRUCTURE)







DATE: JAN 23, 2000	A D P O S T - P L O T (REV: 22.3) Hupsa bridge in Khulna	S T A A TILE:
UNIT HET KNS		Neximums 2631.14 J=815,N=814
Mo - 01AG.		
MP-4 COL, 2 COP		
	24.001 24.858, 3 1571.49 14.85.35 1477.1	
	28 · 36 · 36 · 37 · 37 · 37 · 37 · 37 · 37	
	38 98 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
IN LATECA		

ob No.: Designed by: Checked by: Date: January 23, 2000

#### SHRINKAGE LOAD

MEMB	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z

LOADING

Load 1 SHRINKAGE LOADS

1 TO 6 197 TO 202 STRAIN -.000434

7 TO 12 31 TO 36 167 TO 172 191 TO 196 STRAIN -.00028

13 TO 30 173 TO 190 45 TO 62 141 TO 158 37 TO 44 - 159 TO 166 77 TO 94 109 TO 126 STRAIN -.00034

63 TO 76 95 TO 100 103 TO 108 127 TO 140 STRAIN -.00029

101 TO 102 STRAIN -.000216

ob No.: Designed by: Checked by: Date: January 23, 2000

MEMB	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
1		1 2	-2,04 2.04	•76.99 76.99	0.00 0.00	0.00 0.00	0.00	0.0
				70.33	0.00	0.00	0.00	-153,90
2	1	2	-2.34	-76.95	0.00	0.00	0.00	153,97
		3	2,34	76.95	0.00	0.00	0.00	-461.92
3		3	-2.48	-76.95	0.00	0.00	0,00	461.91
		4	2.48	76.95	0.00	0.00	0.00	-769.85
enter de la companya								
		5	-2.14 2.14	-76.95 76.95	0.00	0.00	0.00	769.84
				.0.55	0.00	0.00	0.00	-1,077.81
5	1	5	-2.42	-76.96	0.00	0.00	0.00	1,077,78
			2.42	76.96	0.00	0.00	0.00	-1,385.75
6	1	6	-2.52	-76.93	0.00	0.00	0.00	1,385.75
		7	2.52	76.93	.0.00	0.00	0.00	-1,693.67
7						and the second of		
		7 8	-2.29 2.29	-76.91 76.91	0.00	0.00	0.00	1,693.75
					0.00	0.00	0.00	-1,963.10
8		8	-2.18	-76.95	0.00	0.00	0.00	1,963.17
		9	2.18	76,95	0.00	0.00	0.00	-2,232.56
9	1	9	-2.13	-76.96	0.00	0.00	0.00	2 727 67
		10	2.13	76.96	0.00	0.00	0.00	2,232.52 -2,502.07
10								and the second of the
10		10 11	-2.18 2.18	-76.96 76.96	0,00 0,00	0.00	0.00	2,502.02
				70.50	0.00	0.00	0.00	-2,771.50
11		11	-2.38	-76.93	Ö. <b>0</b> 0	0.00	0.00	2,771.47
		12	2.38	76.93	0.00	0.00	0.00	-3,040.94
12		12	-2.57	-76.98	0.00	0.00	0.00	3,040.87
		l <b>3</b>	2.57	76.98	0.00	0.00	0.00	-3,310.40
13				0.141	A whigh a			
		13 14	2.18 -2.18	-76.98 76.98	0.00	0.00	0.00	3,310.42
					0.00	<b>V.00</b>	0.00	-3,541.31
14		14	2.05	-76.91	0.00	0.00	0.00	3,541.41
		15	-2.05	76.91	0.00	0.00	0.00	-3,772.23
15	1	15	2.22	-76.95	0.00	0.00	0.00	3,772.38
		16	-2.22	76.95	0.00	0.00	0.00	4,003.18
16							i Mariana	fate and
		16 17	2.36 -2.36	-76.85 76.85	0.00	0,00	0.00	4,003.11
					0.00	0.00	0.00	-4,234.34
17		17	2.42	-76.95	0.00	0.00	0.00	4,234.19
		18	-2.42	76.95	0.00	0.00	0.00	-4,465.14
18		18	2.02	-76.93	0.00	0.00	0.00	4,465.18
		19	-2.02	76.93	0.00	0.00	0.00	-1,696.08
	e i việu bi			9.24				
19		19 20	1,99 -1.99	-77,00 77,00	0.00 0.00	0.00	0.00	4,696.13
PAR S.	n i jaren 1 de. Similaria i Ser			Too To <b>相性</b> The trapped to	0.00	0.00	0.00	-4,927.01
20	1	20	1,93	-76.97	0.00	0.00	0.00	4,927.10
	9 (00.3)	21	-1.93	76.97	0.00	0,00	0.00	-5,235.01
21	1	21	1.10	-77.07	0.00	0,00	0.00	6 22 4 02
Jahren J		22	-1.10	77.07	0.00	0.00	0.00	5,234.93 -5,389.06
			i e e v					
22	1	22 23	-1,223.06	-86.75	0.00	0.00	0,00	-5,897.75
a1.07 - F		23	1,223.06	86.75	0.00	0.00	0.00	5,723.74
23	1	23	-1,223.43	-71,83	0.00	0.00	0.00	-5,723.07
		24	1,223,43	71.83	0.00	0.00	0.00	5,434.10

ob No.: Designed by: Checked by: Date: January 23, 2000

-5,434.14 5,220.24 -5,220.16	er alle view of a fill for						
-5,220,16	0,00	0.00	0.00	-70,84	-1,223.60	24	24
	0.00	0.00	0,00	70.84	1,223,60	25	
£ 000 0 °	0,00	0.00	0,00	-69.90	-1,223.61	25	25
5,008.85	0.00	0.00	0.00	69.90	1,223.61	26	
-5,008.75	0.00	0.00	0.00	-70.07	-1,223.70	26	26 1
4,797.36	0.00	0.00	0.00	70.07	1,223.70	27	
-4,797.43 4,585.98	0.00 0.00	0.00	0.00	-70.01 70.01	-1,223.43 1,223.43	27 28	27
-4,585,93 4,373,26	0.00	0.00 0.00	0.00 0.00	-70.47 70.47	-1,223.58 1,223.58	28 29	28
-4,373.48	0.00	0.00	0,00	-70.98	-1,223,29		
4,159.74	0.00	0.00	0.00	70.98	1,223.29	29 30	1 1 29 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
4,159.56	0.00	0.00	0.00	-71.57	-1,223.48	30	30 Jan 1
3,943.90	0.00	0.00	0.00	71.57	1,223.48	31	
-3.943.73	0.00	0.00	0.00	-139,02	-1.217.68	31	31
3,456.94	0.00	0.00	0.00	139.02	1,217.68	32	
-3,456.91	0.00	0.00	0.00	-139.00	-1,217.47	32	<b>32</b> 1
2,970.31	0,00	0.00	0.00	139.00	1,217.47	33	
-2,970.30	0,00	0.00	0.00	-139.03	-1,217.67	33	33
2,483.64	0.00	0.00	0.00	139.03	1,217.67	34	
-2,483.62 1,997.35	0.00 0.00	0.00 0.00	0.00	-138.99 138.99	-1,217.81 1,217.81	34 35	
		된 개발가 되었다.					特特的
-1,997.32 1,510.88	0.00	0.00 0.00	0.00 0.00	-139.02 139.02	-1,217.59 1,217.59	35 36	1 (1945) <b>35</b> (1946) <b>1</b>
		0.00					
-1,510.90 1,024.57	0.00 0.00	0.00	00.00 00.00	-139.02 139.02	-1,217.72 1,217.72	36 37	36
-1,024.64	0.00	0.00	0.00	-139.02	-1,217.44	37	37
746.64	0.00	0.00	0.00	139.02	1,217,44	38	
-746.61	0.00	0.00	0.00	-138.95	-1,217.11	38	38 1
468,85	0.00	0.00	0.00	138.95	1,217.11	39	
-468.89	0.00	0.00	0.00	-139.02	-1,217.65	39	39 1
-17.47	0.00	0.00	0.00	139.02	1,217.65	40	
17.44	0.00	0.00	0.00	-138.99	-1,217.57	40	40
-503.68	0.00	0.00	0.00	138.99	1,217.57	41	
503,72 -989.96	0.00	0.00	0.00	-138.98	-1,217.76	41	41 · 1 · 1
989.95 -1,476.29							42
1,476,25 -1,962.66	0.00 0.00	0.00	0.00	A Company of the Comp		43 44	43
	0.00	0.00	0.00	\$ 0, \$ 5e	to the second state of the second		
1,962.63 -2,449.11	0.00	0.00	0.00	-139.02 1 <b>3</b> 9.02	1,217.44	45	
2,449.09	0.00	0.00	0.00	<i>-2</i> 06 13	-1 20R 43	1000	
-3,067.48	0,00	0.00	0.00	206.13	1,208.43	46	
3,067.49	0.00	0.00	0.00	-206.92	-1.208.07	46	er i per til de i gjer danse. Hij i gjer <b>46</b> for de joe en s
-3,688.30	0.00	0.00	0.00	206.92	1,208.07	47	
	0,00 0,00 0,00 0,00 0,00 0,00 0,00	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	138.98 -139.01 139.01 -139.02 139.02 -139.02 -206.13 206.13	1,217.76 -1,217.53 1,217.53 -1,217.31 -1,217.31 -1,217.44 1,217.44 -1,208.43 1,208.43	42 43 43 44 44 45 45 46	

ob No.: Designed by; Checked by; Date: January 23, 2000

MEMB		LOAD	NODE	AXIAL '	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	47		1 47	-1,207,74	-207.31	0.00	0.00		
	· · · ·		48	1,207.74	207.31	0.00	0.00	0.00	3,688.33 -4,310.46
	48		,						1,510.10
	40	erija ing pilati Propinsi di Kara	1 48 49	-1,207,63 1,207,63	-207,7] 207,71	0.00 0.00	0.00	0.00	4,310.50
	٠.,			禁门 医乳毒毒素	20,,,,	0.00	0.00	0.00	<b>-4,933,8</b> 1
	49		1 49	-1,207.82	-207.68	0.00	0.00	0.00	4,933.86
			50	1,207.82	207,68	0.00	0,00	0.00	-5,557.25
	50		1 50	-1,207.80	-207.71	0.00	0.00	0.00	5,557.28
医圆线片			51	1,207.80	207.71	0.00	0,00	0.00	-6,180.78
	51		1 51	-1,207.67	-206,84	0,00	0.00		
Property of	. 4.		52	1,207.67	206.84	0.00	0,00	0.00	6,180.92 -6,801.79
	52								5,001.77
	32		1 52 53	-1,208.30 1,208.30	-206,02 206,02	0.00 0.00	0.00	0.00	6,801,95
					200,02	0.00	0.00	0.00	-7,626.46
	53		J 53	-1,210.61	-190.59	0.00	0.00	0.00	7,626.54
			54	1,210.61	190.59	0.00	0.00	0.00	-8,007.85
	54	Take (TA)	1 54	-1,933.37	9.86	0.00	0.00	0.00	1.101.63
il ayalı			55	1,933.37	-9.86	0.00	0.00	0.00	-1,191.62 1,211.40
	55			1 010 40					
rain de en la compaña de l La compaña de la compaña d			1 35	-1,932.47 1,932.47	34,15 -34,15	0.00 0.00	0.00	0.00	-1,210.91
						<b></b>	0.00	0.00	1,347.68
	56		56	-1,932.74	35,65	0,00	0.00	0.00	-1,347.49
			<b>57</b>	1,932.74	-35.65	0.00	0.00	0.00	1,454.45
y Army	57	753	57	-1,932.49	36.87	0.00	0.00	0.00	-1,454.41
			58	1,932.49	-36.87	0.00	0.00	0.00	1,564.89
	58	- 1	58	-1,932.45	36.86	0,00	0.00		15 E 4 74 F
		83	59	1,932.45	-36.86	0.00	0.00 0.00	0.00	-1,565.09 1,675.72
	"								1,075.72
	59		59 60	-1,932.45 1,932.45	36.85 -36.85	0.00	0.00	0.00	-1,675.68
				1,752,15	30.03	0.00	0.00	0.00	1,786.46
e dan kar	60	(1) 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	60	-1,932.82	36.27	0.00	0.00	0,00	-1,786.34
10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			61	1,932.82	-36.27	ე.00	0.00	0.00	1,895.27
i di sa sana di	61	1.0	61	-1,932.61	35.62	0.00	0.00	0,00	-1,895.22
		0.05/1973	62	1,932.61	-35.62	0.00	0.00	0.00	2,002.23
	62		62	-1,932.60	34,36	0.00			
			63	1,932.60	-34,36	0.00 0.00	0.00 0.00	0.00	-2,002.16 2.105.35
				化复数放客层				0.00	2,105.35
	63	I	63	-1,931.51 1,931.51	-72.25	0.00	0.00	0.00	-2,105.35
			64	16,165,1	72.25	0.00	0.00	0.00	1,852.30
	54	gr y . 1	64	41,931.75	72.21	0.00	0.00	0.00	-1,852.26
			65	1,931.75	72.21	0.00	0.00	0.00	1,599.39
90 a sec (	55	0.3 4 1	65	-1,931.52	-72,26	0.00	0.00	0.00	1 600 06
	d Da	1000	66	1,931.52	72.26	0.00	0.00	0.00	-1,599.36 1,346.54
	C.A.			1021 61				ngini ng ng	
			66 67	-1,931.51 1,931.51	-72.26 72.26	0.00 0.00	0.00	0.00	-1,346.52
						0.00	0.00	0.00	1,093.78
30 30 5 6	5 <b>7</b>	i i	67	-1,931.56	-72.22	0.00	0.00	0.00	-1,093.73
		ombilionis Longo en s	. in the firm <b>68</b> in	1,931.56	72.22	0.00	0.00	0.00	841.12
6		way I	68	-1,931.71	-72.24	0.00	0,00	0.00	241.07
			69	1,931.71	72.24	0.00	0.00	0.00	-841,07 588,47
	Q	i filozofia (2005) Viktorio (2016)	69	1 021 40	e (Se la				
다 : 생기에서, " 그는 생각 없습니다			69 70	1,931,49 1,931,49	-72.21 72.21	0.00 0.00	ó,00 0.00	0,00	-588.39
						0.00	0.00	0.00	444.15

ob No.; Designed by: Checked by: Date: January 23, 2000

MEMB		LOAD	NODE	AXIAL _	SHEAR-Y	SHEAR-Z	TORSION	мом-у	MOM-Z
	70	1	70	-1,931.47	-72.40	0.00	0.00	0.00	444.27
			71	1,931.47	72.40	0.00	0.00	0,00	299.64
	71	1	71 72	-1,931.60 1,931.60	-72,24 72.24	0,00	0.00 0,00	0,00 0.00	-299.75 47.20
	72	1	72	-1,931.64	-72.26	0.00	0.00	0.00	47.20
			73	1,931.64	72.26	0.00	0.00	0.00	-205.41
	73	1	73 74	-1,931.68 1,931.68	-72.25 72.25	0.00	0.00 0.00	0.00 0.00	205.38 -457.99
			74	1,931.51	-72.25	0.00	0.00	0.00	457.98
	74		75	1,931.51	72.25	0.00	0.00	0.00	-710.60
	75	1	75	1,931.60		0.00	0,00	0.00	710.60
			76	1,931.60	72.25	0.00	0.00	0.00	-963.26
	76	1		-1,931.65 1,931.65	-72.25 72.25	12 0.00 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.00	0.00 0.00	963.27 -1,215.98
	77	1	77	-1,924.70	-178.94	0.00	0.00	0.00	1,215.98
			78	1,924.70		0.00	Ö.00	0.00	-1,752.80
	78	1	7 <b>8</b> 79	-1,924.46 1,924.46		0.00 0.00	0,00 0,00	0.00 0.00	1,752.79 -2,293.53
	79		79	-1,924.63		0.00	0,00	0.00	2,293.52
r nami Likinan	′′		80	1,924.63		0.08	0.00	0,00	-2,836.27
	80	1	80	-1,924.32		0.00	0.00	0.00	2,836.26
i kata (pr. ). Primber			81	1,924.32		0.00	0.00	0.00	-3,380.95
	81	1	81 82	-1,924.37 1,924.37		0.00	0.00 0.00	0.00 0.00	3,380.99 -3,925.67
	82		82	-1,924.39		0.00	0.00	0.00	3,925.71
			83	1,924.39	181.51	0.00	0,00	0.00	4,470.52
	83	1	83 84	-1,924,51 1,924.51		0.00	0.00 0.00	0.00	4,470.48 -5,011.56
	84	el d'allanda Hallanda de la companya de la compa	84	-1,924.68		0.00	0.00	0.00	5,011.52
			85	1,924.68		0,00	0.00	0.00	-5,727.14
	85		85 86	-1,926.87 1,926.87		0.00 0.00	0.00 0.00	0.00 0.00	5,727,13 -6,035. <b>8</b> 4
				× 3.		0.00	0.00		4,235.37
i de la compaña de la comp La compaña de la compaña d	86		86 87	-2,116.47 2,116.47	-153.36	0.00	0.00	0.00 0.00	-3,927.71
	87	1	87	-2,114.36		0.00	0.00	0.00	3,927.82
			. 88	2,114.36		0.00	0.00	0,00	-3,204.61
	88	1	88 89	-2,114.23 2,114.23		0.00	0.00	0.00	3,204.70 -2,657.47
	89	1	89	-2,114,15	i 183.24	0.00	0.00	0.00	2,657.63
			90	2,114.15		0.00	0,00	0.00	-2,106.25
	90	1	90 91	-2,114.09 2,114.05		00,0 00.0	0.00 0.00	0.00 0.00	2,106,26 -1,555,09
	0.								
	91		91 92	-2,114.10 2,114.10		0.00	0.00 0.00	0,00 0.00	1,555.08 -1,003.74
	92	1	92	-2,114.18		0,00	0.00	0.00	1,003.79
			93	2,114.18	-182.49	0.00	0.00	0.00	-454.79