P/S LOAD AT CLOSURE SPAN 4
OF FRAME 5 (WHOLE STRUCTURE)

ob No: Designed by: Checked by: Date: January 23, 2000

#### **CLOSURE PRESTRESS LOAD AT SPAN 4**

							<del></del>	
MEMB	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z

#### **LOADS**

#### LOAD 1: PRESTRESS FORCE AT CLOSURE SPAN 4

#### PRESTRESS LOAD

95 108 FORCE 10868 ES -2.005 EM -2.005 EE -2.005

96 107 FORCE 21736 ES -2.005 EM -2.005 EE -2.005

97 106 FORCE 32604 ES -2.005 EM -2.005 EE -2.005

98 105 FORCE 43472 ES -2.005 EM -2.005 EE -2.005

99 104 FORCE 48906 ES -2.005 EM -2.005 EE -2.005

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2	1	1	marki di Lin					
			-0.17	-5.92	0	0	0	
		2	0.17	5.92	0	0	0	-11
	,	2	-0.18	-5.91	0	0	0	11
•		(a. 11 a. 11 a	0.18	5.91	0	0	0	-3
	1	3	-0.18	-5,91	0	0	0	3
		4	0.18	5.91	Ō	Ŏ	ő	-59
4	1		-0.13	-5.91	0	0		100
		5	0.13	5.91	0	0	0	59 -82
5		\$	-0.2	-5.91			gen a	4000
		6	0.2	5.91	0	0	0	82 -10
6			0.10					e di Certi
		6 7	-0.19 0.19	-5.91 5.91	0	0	0	10 -130
		7 8	-0.2 0.2	-5.91 5.91	0	0	0	130
	, it					, and the same	· ·	-150
8	1	8 9	-0.21 0.21	-5.92 5.92	0	0	0	150
					· Š		0	-171
9		9 10	-0.18 0.18	-5.91 5.91	0	0	0	171
			V.16	( ) ( ) ( ) ( ) ( ) ( ) ( ) ( )	, , , , , , , , , , , , , , , , , , ,	0	0	-192
10	1	10	-0.18	-5.92	0	. <u>o</u>	0	192
		<b>11</b>	0.18	5.92	0	0	0	-213
$\mathbb{H}_{\mathbb{R}^n} : \mathbf{H} \to$	1	!!	-0.16	-5.92	0	0	0	100
		12	0.16	5.92	0	0	0	-233
12	1	12	-0.21	-5.91	0	0	0	233
		13	0.21	5,91	0	• • • • • • • • • • • • • • • • • • •	0	-254
13	1	13	0.15	-5.91	0	0	0	254.
		14	-0.15	5,91	0	0	0	-272.
14	1	14	0.17	-5,91	0	0	0	272.
		15	-0.17	5.91	0	0	0	-289.
15	1.	15	0,14	-5.91	0	0	0	289.
		16	-0.14	5,91	0	0	0	-307.
16	1	16	0.16	-5,92	0	0	0	307.
		17	-0.16	5.92	0	0	Ŏ	-325.
17	1	17	0.13	-5.91	0	0	0	325.
		17 18	-0.13	5.91	Ö	ŏ	ŏ	-343.
18	1	18	0.13	-5.92	0	0		
18	ewist of a second	19	-0.13	5.92	ő	0	0	343. -360.
19		10						
		19 20	0.2 -0.2	-5.92 5.92	0	0	0	360.9 -378.6
20							\$ 120 St 40	Property and the
		20 21	0.17 0.17	-5.91 5.91	0.	0	0	378.
						展览有知 的		-402
21		21 22	0.02 -0.02	5.93 - 5.93	0	0.	0	402.
			보는 경우가 목표를	5.93	· ·	Ü	Ó	-414
22		22 23	-264.39	-66.56	0	0	0	-2921.6
		문화 시작하다 그	264.39	66,56	0	0	0	2788.0
23		23 24	-265.3 265.3	-63.14 63.14	0	0	0	-2788.2

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мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
24	1	24 25	-265,38 265,38	-62.94 62.94	0	0	0	-2534.76 2345.2
25	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	25 26	-265,3 265.3	-62.78 62.78	. 0	0 0	0	-2345.21 2156.1
26	1	26 27	-265,4 265.4	-62.77 62.77	0		0	-2156.2 1967.2
27	1 1	27 28	-265.47 265.47	-62.73 62.73	0	0	0	-1967.1 1778.2
28		28 29	-265.37 265.37	-62.86 62.86	0		0	-1778.2 1588.9
29		29 30	-265,38 265.38	-62.93 62.93	0		and the second second	
30	1	30 31	-265.32 265.32	-63.11 63.11			1.5	
31	. 1964 - 1964 - 1964 1964 - 1964 - 1964 1964 - 1964 - 1964	31 32	-261.44 261.44	-77.64 77.64			24 7 7 7 7	
32		32 33	-261.45 261.45	-77.65 77.65			and the second of the second of the second	
33		33 34	-261.45 261.45	-77.65 77.65			for the second control of the second	4.5
34	1	34 35	-261.4 261.4	-77.65 77.65				
35	1	35 36	-261.46 261.46	-77.64 77.64		) i	化二氯化甲基甲基苯甲基甲基	and the second s
36		36 37	-261.41 261.41	-77.65 77.65		) )	and the second of the second of the second	) 149. ) 421
37	1	37 38	-261,39 261.39	-77.66 77.66		The second second	) }	) 421. ) -576.
38	1	3 <b>8</b> 39	-261.43 261.43	-77.64 77.64				) 576. ) -732.
39	1	39 40	-261.37 261.37	-77.64 77.64		0		732. 0 -1003.
40		40 41	-261.48 261.48	-77.62 77.62				0 10 0 -1275
41		41 1 41 42	-261.35 261.35	-77.65 77.65				0 1275 0 -1547
4:		1 42 43	-261.41 261.41	-77.68 77.68				0 1547 0 -1819
4:	3 3	1 43 44	-261.46 261.46				the contract of the contract o	0 1819 0 -2091
4	4	1 44 45	-261.46 261.46			0		0 2091 0 -2363
4	5	1 45 46				0		0 2363 0 -2639
4	6	1 46 47	-256.7 256.7		barrar in in	0. 0	0	0 2639 0 -2916

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мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ү	MOM-Z
47	1	47 48	•256.67 256.67	-92.31 92.31	0	0	0	2915.82 -3192.75
<b>48</b>		4 <b>8</b> 49	-256.59 256.59	-92.3 92.3	0	0	0	3192.63 -3469.99
49	1	49 50	-256.54 256.54	-92.28 92.28	0	0		3469.98 -3746.88
50	.1	50 51	-256.54 256.54	-92.26 92.26	0	0	0	3747.03 -4024.06
51		51 52	-256.73 256.73	-92.15 92.15	0	0	0	4024.07 -4300.74
52	1	52 53	-256.73 256.73	-91.96 91.96	0	0	0	4300,71 -4668.82 4668.8
53		53 54	-257.91 257.91	-88.66 88.66 210.34	0	(	0	-4846.21 6939.08
		54 55 55	-394.03 394.03 -391.21	-210.34 -210.34 -215.13	0	C.	0	-6517.44 6517.6
		56 56	391.21 -391.08	-215.13 215.49	0		0	-5654.14 5654.06
57		57 57	391.08 -391.01	-215.49 215.74	0		0	-5005.57 5005.65
58		58 58	391.01 -390.92	-215.74 215.74	0		) 0	-4356.05 4356.08 -3706.84
59		59 59 60	390.92 -390.99 390.99	-215.74 215.84 -215.84	0	(		3706.98 -3057.32
60		60 61	-391.08 391.08	215.6 -215.6	0		) ) 0	
61		61 62	-391.05 391.05	215.48 -215.48	0		o 0 O 0	2408.6 -1759.92
62		62 63	-391.13 391.13	215.04 -215.04	0		0 0 0	and the second s
63 81		63 64	-402.53 402.53	193.31 -193.31	0		) 0 ) 0	
64		64 65	-402.47 402.47	193,32 •193,32		the state of the s	0 0	and the second second
6:		65 66	-402.49 402.49	193.24 -193.24			0 0 0	917.25
66		66 67	-402.53 402.53	193.46 -193.46	0		0 0 0	1594.21
2. 19862		67 68	-402.47 402.47	193.11 -193.11			0 0	2270.23
- 1		68 69	-402,52 402,52	193.36 -193.36	0		0 0	2947.17
6	<b>9</b>	1 69 70	-402.52 402.52	193.1 -193.1		and the second second	0 0	

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мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
70		70 71	-402.45 -402.45	192.96 -192.96	0	0		
71		71	-402.51 402.51	193.21 -193.21	Ó 0		and the second second second	3
72	.1	72 73	-402.52 402.52	193.11 -193.11	0		the state of the s	3
73	1	73 74	-402.48 402.48	193.46 -193.46	0		the state of the s	
74		74 75	-402.48 402.48	193.2 -193.2	0		) )	and the second second
75		75 16	-402,5 402.5	193,27 -193,27	0	and the second of the second	) ()	and the second of the second o
. 76		76 77	-402.53 402.53	193.4 -193.4			and the second of the second	) -7104,41 ) 7781,84
77		1 77 78	-412.61 412.61	170,84 -170,84	0			7781.59 8294.3
78		1 78 79	-412.65 412.65	170.45 -170.45	0		and the second second	0 -8294.45 0 8806.09
79		1 79 80	-412.75 412.75	169,98 -169,98				0 -8806.68 0 9317.47
80		1 80 81	-412.8 412.8	170.19 -170.19	(			0 -9317.28 0 9829.33
81		1 81 82	412.71 412.71	170.16 -170.16			the second of the second	0 -9828,54 0 10340,89
82		l 82 83	-412.74 412.74	170.1 -170.1				0 -10339.77 0 10851.82
83		1 83 84	-412.66 412.66	170.54 -170.54				0 -10851.51 0 11363.35
84		1 84 85	-412.57 412.57	170.85 -170.85		9		0 -11363.46 0 12047.67
.85		1 85 86		175.86 -175.86		0 0		0 -12047.96 0 12399.81
80		1 86 87		81.9 -81.9		0 0		0 -40904.2 0 41069.7
8	7	1 87 88				0	0	0 -41069.8 0 41458.8
8	8	1 88 89	1130.05	-97.21		<b>o</b>	0	0 -41459.1 0 41753.5
8	9	1 89 90	-1130.02			0		0 -41753.1 0 42051.2
9		1 90 91	1129.98			0	0 0	0 -42051.3 0 42348.1
9		1 .91 92		-97.88		0	0	0 -42348.8 0 42646.0
	2	. 1				0 0	0	0 42647 0 42942.5

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MEMB	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ч	MOM-Z
93		93 94	-1130.07 1130.07	96.64 -96.64	0	0	0	-42944.41 43239.62
94	1	94 95	-1129.96 1129.96	96,97 -96,97	0	0	0	-43239.7 43536.53
95		95 96	9734.31 •9734.31	33.79 -33.79	0	0	0	-21746.29 21805.2
96	1	96 97	20602.32 -20602.32	34.46 -34.46	0	0	0	-14,04 4,13
97 98		97 98	31470.28 -31470.28	33,31 -33,31	0	0	0 0	21786.97 -21859.98
<b>70</b>		98 99 99	42338.34 -42338.34 47772.3	34.36 -34.36 34.28	0	0	0	43650.24 -43742.99
100		100	47772.3 47772.29	-34.28 -33.25	0 0	0	0	54639.63 -54687.24
101		101 101	-47772.29 -47772.1	-33.25 32.58	0	0	0	54686.28 -54655.6 54656.36
204		102 204	-47772.1 -79.53	-32.58 261.77	0	0	0	-54600.99 2457.71
205	1	205 205	79.53 -79.53	-261.77 258.87	0	0	0	-2065,42 2066,66
206		206 206 207	79.53 -79.53 79.53	-258.87 258.99 -258.99	0 0	0	0	-901.57 901.5
207	1	207 208	-79.53 79.53	257.76 -257.76	0	0	0	-264.08 -263.54 652.62
210		210 211	266.59 -266.59	148.78 -148.78	0	<b>0</b> 0	0	-2600.88 2822.83
211		211 212	266.59 -266.59	149.14 -149.14	0	0 0	0	-2823.62 3718.64
21 <b>2</b>		212 213	266.59 -266.59	149.09 -149.09	0	0 0	0	-3718.7 4613.5
213		213 214	266.6 -266.6	148.86 -148.86	0 0	0 0	0 0	-4613.85 4836.91
216		216 217	-181.12 181,12	730.19 -730.19	0	0 0	0 0	26037.38 -24945.2
217 36 43 14 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3		217 218	-181,15 181,15	726.07 -726.07	0 	0	0	24945.99 -19499.92
219		218 219 219	-181.14 -181.14 -181.14	726.11 -726.11 719.26	0	0	0	19499.93 -14053.94
239		219 220 209	-181.14 181.14 -130.94	-719.26 -719.26 583.77	0.	0	0	14045.42 -12970.65
240		240 240	130.94 -0.1	-583.77 0	0	0	0	676.88 2096.04
		241	0.1	0	0	Ō	ŏ	0

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мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ч	MOM-Z
241	1	209 242	128.07 -128.07	-504.24 504.24	0			
242		242 243	0.08 -0.08	0.01 -0.01	0			
243	1	21 <i>5</i> 244	-70.04 70.04	637.79 -637.79	(		) (	
244		1 244 245	-0.05 0.05	-0.01 0.01	and the second of the second			10.01 0
245		1 215 246	79.09 -79.09	-904.38 904.38	and the second second second	T		0 -3054.89 0 -1240.92
246		1 246 247	-0.03 0.03	0 0	the state of the s			0 -0.01 0 -0.01
247		1 221 248	-366.18 366.18	97.83 -97.83				0 -5581.46 0 6046.15
248		1 248 249	-0.12 0.12	0.01 -0.01		0		0 0,01 0 0.01
249		1 221 250	360 -360	83.31 -83.31		0	0 / A   D   A   B   A   B   B   B   B   B   B   B	0 6294.08 0 -5898.33
250		250 251	0.07 -0.07	0,03 -0.03		0	0	0 0.05 0 0.01
264		1 264 265	-583.77 583.77	130.92 -130.92		0	0	0 1899.72 0 -722
265		1 265 266	-583.77 583.77	130.92		0	0	0 722 0 1240.51
266		1 266 267	-583.77 583.77	94.61		0	0	0 -1240.49 0 1382.34
267		1 267 268	-583.77 583.77	37.		0	0	0 -1382.3 0 1438.3
268		1 268 269	-583.77 583.77	-6.1	3	0	0	0 -1438.3 0 1429.03
269		1 269 270		-37.9	1	0	0	0 -1429.07 0 1372.09
270	•	1 270 271	-583.7	7 -59.9	3	0	0	0 -1372.00 0 1282.1
27		1 271 271 272	-583.7	7 -78.1	2	0	0	0 +1282.1 0 1164.9
27	2	1 272	-583.7	7 -105.6		0	0	0 -1164.9 0 1006.4
27		273	-583.7	7 -117.2	29	0	0	0 -1006.4 0 830.4
27	74	1 274	-583.7	7 -118.0	)5	0 7	0	0 -830.4 0 653
2:	75	275 1 275	; -5 <b>8</b> 3.7	7 -109	53	0	0	0 -653 0 489
2	76	270 1 270	5 -583.1	-95.	78	0	0	D -489
		27		95.	78	0	0 se	0 345.4

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MEMB LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ч	мом-г
277 1	277 278	•583,77 583,77	-79.81 79.81	0	0	and the second of the second	-345.43 225.71
278 1	278 279	-583.77 583.77	-63,79 63.79	0	0		-225.71 130.04
279 1	279 280	-583.77 583.77	-49.11 49.11	0	0		-130.04 56.37
280. 1	280 281	-583.77 583.77	-36.61 36.61	0	0		-56.37 1.46
281	281 282	-583.77 583.77	-26.65 26.65	0	0		-1.46 -38.5
282 1	282 283	-583.77 583.77	-16.78 16.78	0	0	0	38.5 -63.67
283 1	283 284	-583.77 583.77	-10.04 10.04	0	0	0	63.67 -78.73
284	284 285	-583.77 583.77	2.26 -2.26	0	0	the second secon	78.74 -75.35
285 1	285 286	-583.77 583.77	8.62 -8.62	0	0	0	75.35 -58.11
286	286 287	-583.77 583.77	9.82 -9.82	0	0	0	58.11 -38.47
287	287 288	-583.77 583.77	8.37 -8.37	0	0	0	38.47 -21.73
288	288 289	-583.77 583.77	5.96 -5.96	0	0	0	21.73 -9.81
289	289 290	-583,77 583,77	3,76 -3.76	0	0	0	9.81 -2.29
290 1	290 291	-583.77 583.77	-2 -2	0 110 0 110 110 110 110 110 110 110 110		0	2.29 1.71
291 to 100 to 10	292	-583.77 583.77	0.78 -0.78		0	0	-1.71 3.26
<b>292</b> X (1) 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	292 293	-583.77 583.77	0.05 -0.05	0	0	0	-3.26 3,37
293 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	294		-0.3 0.3	0	0	0	-3.37 2,76
1 (1.5) (1.5	295	-5 <b>83</b> .77 583.77	-0.41 0.41		0	0	-2.76 1.94
	296	-583.77 583.77	-0.38 0.38	0	0	0	-1.94 1.18
296 1	297	-583,77 583,77	-0.29 0.29	0	0	0	+1.18 0.59
297 1	297 298	-583.77 -583.77	-0.2 0.2	0	0	0 0	-0.59 0.2
298	298 299	-583,77 583,77	-0.11 0.11		0	0	-0.2 -0.02
299	299 300	-583.77 583.77	-0.05 0.05	0	0	0	0.02 -0.13

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мемв	LOAD NODE	AXIAI.	SHEAR-Y	SHEAR-Z	TORSION	мом-ч	мом-г
300	1 30 30		-0.01 0.01		) )		
301	30		0.01 -0.01	and the second of the second	) 0 ) 0		
302	1 30		0.02 -0.02		0 0		the state of the s
303	1 30 30		0.02 -0.02	4 - 1 - 4	0 0 *:	the second second	0.1 -0.07
304	30 30	infativities.	-0.01		0 0 0	0	-0.04
305	6 - 10 - 30 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 1	5 -583.77 6 583.77	-0.01	Material (	0	0	-0.01
306	30 30	583.77	-0.01		0 0 0	0	0.01
307 308	30		-0.01 -0.01 0.01		0	0	0.02
310		9 583.77	-0.01 128.05		) )	0	
7, 12 (1) 10 (2) (1) (2) 2 (1) (3) (1) (3) (1)	기원 (소리는 기회원 기계원 <b>)</b> 기원 : 기교회 (기원 기원 기계원	1 -504.24 1 504.24	-128.05 128.05		0 0		-685.96
312		2 -504,24 2 504,25	-128.05 92.12		0 0	0	-1236.02
313			-92.12 35.7 -35.7		0 0 0 0	0	-1374,35
314		.5 504.24 16 -504.24	-7.2 7.2		0	0	-1427.97
315	: 1	16 504.24 17 -504.24	-38,54 38,54	2.467	0 0		-1417.24
316	3 ( ) ( ) ( ) ( ) ( )	17 504.24 18 -504.24	-60.21 60.21		0 0 0 0		
317	$g \sim g^{-1} + i g$ . $1 < i < j < 3$	8 504.24  9 -504.24		and the second second	0	and the second of the second o	the second of the second of
318	33	9 504.24 20 -504.24		The state of the s	0 0 0		
319	Server of the contribute ${\cal F}$	20 504.24 21 -504.24	-116.37 116.37		0 0		
320		21 504.24 22 -504.24	-116.92 116.92		0		
321		22 504.24 23 -504.24	-108,36 108,36		0 0 0 0	0	482.12
322		23 504.24 24 -504.24	-94.66 94.66		0	0	340.13
323		24 504.24 25 -504.24	-78.82 78.82		0	2.1	-340.13 221.9

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### CLOSURE PRESTRESS LOAD AT SPAN 4

МЕМВ	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-у	MOM-Z
324	1	325 326	504.24 -504.24	-62.94 62.94	(		0	-221.9 127.49
325	1	326 327	504,24 -504,24	-48.41 48.41	(		0	-127,49
326		327	504.24	-36.05		)	0	54.86 -54.86
327		328 328	-504.24 504.24	36.03 -26.21			0	0.78 -0.78
328	1	329 329	-504.24 504.24	26.21 -16.47	0	0	0	-38.53
		330	-504.24	16.47	0	0	0	38,53 -63,24
<b>329</b>		330 331	504.24 -504.24	-9.82 9.82	0		0	63.24 -77.98
330	1	331 313	504.24 -504.24	2.3 -2.3	0	the state of the s	0	77.98 -74.53
331	1	313 333	504.24 -504.24	8.56 -8.56	0		0	74.53 -57.42
332	1	333 334	504.24 +504.24	9.72 -9.72	0		0	57.42
333		334	504.24	8.28	0	0	0	-37.97 37.97
334		335 335	-504.24 504.24	-8.28 5.88	0		0	-21.42 21.42
335		336 336	-504.24 504.24	-5.88	0	Ó	0	-9.65
eried by a di Herri Alba is		337	-504.24	3.71 -3.71	0	0	0 0	9.65 -2.23
336		337 338	504.24 -504.24	1.97 -1.97	0	0	0	2.23 1.71
337		338 339	504.24 -504.24	0.76 -0.76	0	0	0 0	-1.71 3.23
338		339 340	504.24 -504.24	0.05 -0.05	0	0	0	-3.23 3.33
339		340 341	504.24 -504.24	-0,3 0.3	0	0 0	0	-3.33
340		341	504.24	-0.41	0	0	0	2.73 -2.73
8. 65 (1) 3. 65 (1) 3. 64 (1) 3. 64 (1)		342 342	-504.24 504.24	0.41 -0.38	0 0	0	0	1.92
342		343	-504.24	0.38	0	0	0	-1.92 1.16
		343 344	504.24 -504.24	-0.29 0.29	0	0	0	-1.16 0.58
343		344 345	504.24 -504.24	-0.19 0.19	0	0	0	-0.58 0.2
344	1	345 346	504.24 -504.24	• •0.11 0.11	0	0	0	-0.2 -0.03
345.	i	346 347	504,24 -504.24	-0.05 0.05	0	0	0	0.03
346	1	347	504.24	-0.01		0	0	-0.13 0.13
		348	-504.24	0.01	0	0	0	-0.15

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мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ч	мом-2
347	1	348 349	504,24 -504,24	0,01 -0.01	(	- A		
348	1	349 350	504.24 -504.24	0.02 -0.02	(	and the second second		0.13 0 -0.1
349	1	350 351	504.24 -504.24	0.02 -0.02	( ) ( )	A STATE OF THE STA		0.1 0 -0,06
350		351 352	504.24 -504.24	0.01 -0.01				0.06 0 -0.03
351		352 353	504.24 -504.24	0.01 -0.01				0.03 0 -0.01
352	1 1	353 354	504.24 -504.24	0.01 -0.01			7	0 0.01 0 0,01
353		354 332	504.24 -504.24	0.01 -0.01			0	9 -0.01 0 0.02
354		332 355	504.24 -504.24	0,01 -0.01			0	0 -0.02 0 0.03
356		356 357	-637.79 637.79	70.05 -70.05		•	0	0 918.39 0 -288.4
357		357 358	-637.79 637.79	-70.05		)	0	0 288.4 0 761.47
358		358 360	-637.79 637.79	49.17 -49.17			0	0 -761.46 0 835.17
359	• • • • • • • • • • • • • • • • • • •	360 361	-637.79 637.79	16.43 -16.43		0	0	0 -835.15 0 859.75
360		361 362	-637.79 637.79	-8.34 8.34		0	0	0 -859.73 0 847.17
361		362 363	-637.79 637.79	-26.34 26.34		0	0	0 -847.17 0 807.61
362		363 364	-637.79 637.79	38,69		0	0	0 -807.62 0 749.55
363	1,	364 365	-637,79 637,79	48.77		Ó	0	0 -749.55 0 676.38
364		365 366	-637.79 637.79	63.67		0	0	0 -676.38 0 580.85
365		366 367	-637.79 637.79	69.6	and the second of the second	0	0	0 -580,85 0 476,44
366		367 368	637.79	69.22		0		0 476.44 0 372.6
367		368 369	-637.79 637.79	63.69		0	0	0 -372.6 0 277.06
368		369 370	-637.79 637.79	55.32		0	0	0 -277,06 0 194,07
369		370 371	-637.79 637.79	45.82		0	0	0 -194.07 0 125.34
370		371 372	-637.79 637.79			0 0	0	0 -125.34 0 70.74

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мемв	LOAD NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
371	1 372 373	-637.79 637.79	-27.85 27.85	0	C		-70.74 28.97
372	1 373 374	-637.79 637.79	-20.6 20.6	0	0	the second secon	-28.97 -1.94
373	1 374 375	-637.79 637.79	-14.86 14.86	0	and the second of the second o		1.94 -24.23
374	1 375 376	-637.79 637.79	-9.21 9.21	0			24.23 -38.05
375	1 376 377	-637.79 637.79	+5.37 5.37	0			38.05 -46.11
376	1 377 359	-637.79 637.79	1.58 -1.58	0			46.11 -43.73
377	1 359 379	-637.79 637.79	5.13 -5.13	0	and the second second		43.73 -33.48
378	1 379 380	-637.79 637.79	n like ya Likin	0		and the second second	33.48 -22.01
1941	1 380 381	-637.79 637.79	4.84 -4.84	0	0	0	22.01 -12.32
380	1 381 382		3.42 -3.42	0		0	12.32 -5.48
381	1 382 383	-637.79 637.79	2.15 -2.15	0	C	0	5.48 -1.19
382	1 383 384	-637.79 637.79	1.13 -1.13	0		0	1.19
383 384	1 384 385 1 385	-637.79 637.79 -637.79	0.43 -0.43 0.02	0		0	-1.07 1.92 -1.92
385	386	637.79	-0.02 -0.18	0	C	0	1.96
386	387	637.79	0.18	Ö		0	1.59
387	388 1 388	637.79	0.24	0	the second secon	0	1.11 -1.11
388	389 1 389	637.79 -637.79	0.22 -0.17	0	0	0	0,67 -0.67
389	390 1 390	637,79 -637,79		0 20 20 20 20 20 20 20 20 20 20 20 20 20	0	0	0,33 -0,33
390	391	637.79	-0.06	0	0	0	0.11 -0.11
391	392 1 392	637.79 -637.79	0.06	0	0		-0.02 0.02
392	393 1 393	637,79		0		0	-0.08
393	394 1 394		0.01 10.0	0	Ŏ	0	-0.09 0.09
	395		-0.01				

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## CLOSURE PRESTRESS LOAD AT SPAN 4

	мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ч	мом-2
	394	1	395 396	-637,79 637,79	0.01 -0.01	0		0 0	0.08 -0.06
	395	1	396 397	-637.79 637.79	0.01 -0.01	0	and the second second	0 0	0.06 -0.04
	396		397 398	-637.79 637.79	0.01 -0.01	0		0 0	0.04 -0.02
	397		398 399	-637,79 637,79	0.01 -0.01	0	and the second second	0 0	0.02 -0.01
	398		399 400	-637.79 637.79	0.01 -0.01	0	and the second of the second	0 0	0.01 0
	399		400 378	-637,79 637.79	0	0		0	0.01
	400	1	378 401	-637.79 637.79	0	0		0 0	-0.01 0.02
	402		402 403	904.38 -904.38	79.08 -79.08	0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0	1122,24 -409,9
	403		403 404	904.38 -904.38	79.08 -79.08	0		0	409.9 777.62
	404		404 406	904.38 -904.38	56.73 -56.73	0 0		) ) )	-777.6 862.8
	405		406 407	904.38 -904.38	21.54 -21.54	0. 0		0	-862.77 895.15
	406		407 408	904.38 -904.38	-5.22 5.22	0		0	-895.16 887.4
	407	2019/13 3019/13/13	408 409	904,38 -904.38	-24.71 24.71	0		)	-887.42 850.42
	408		40 <del>9</del> 410	904.38 -904.38	-38.17 38.17	0		) ) 0	-850.42 793.22
	409		410 411	904.39 -904.39	49.25 49.25	0			+793.22 719.37
	410		411 412	904.39 -904.39	-65.93 65.93	0	raka (1914) Nama	0	-719,37 620.5
	411		412 413	904.38 -904.38		0		) ) (	-620.5 511.2
	412		413 414	904.39 -904.39	•73.11 73.11	0			-511.2 401.54
	413		414	904.38 -904.38	-67.68 67.68	0		3000	-401.54 300.04
	414		415 416	904.38 -904.38	-59.07 59.07	0.		) ) (4)	-300.04 211.43
ve de G	415		416 417	904,38 -904,38	′-49.14 49.14		( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( )		-211.44 137.72
	416		417 418	904.39 -904.39	-39.21 39.21	0		) ) 0	-137.72 78.91
45-35 1-3-	417	1	418 419	904,38 -904.38	-30.13 30.13	0		) )	-78.91 33.71

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МЕМВ	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-у	MOM-Z
418		419 420	904.38 -904.38	-22.42 22.42	0	0	0	-33,71 0.08
419		420 421	904.39 -904.39	-16.27 16.27	0.	0	0	-0.08 -24.34
420	1	421 422	904.39 -904.39	-10,21 10.21	0	0	0	24.34 -39.65
421	1	422 423	904.38 -904.38	-6.06 6.06	0	0	0	39.65 -48.75
422		423 405	904.39 -904.39	1.48 -1.48	0	0 0	0	48.75 -46.54
423	1	405 425	904.38 -904.38	5.36 -5.36	0	0	0	46.54 -35.82
424		425 426	904.38 -904.38	6.08 -6.08	0	0 0	0 0	35.82 -23.66
425	1	426 427	904.38 -904.38	5.17 -5.17	0 0	0 0	0	23.66 -13.33
426	14	427 428	904.38 •904.38	3.67 -3.67	0	0	0 0	13,33 -6
427	1	428 429	904.38 -904.38	2.31 -2.31	0	0	0	6 -1.37
428		429 430	904.38 -904.38	1.22 -1.22	0	0	0	1.37 1.08
429 430		430 431	904.38 -904.38	0.47 -0.47	0	0	0	-1.08 2.02
431		431 432 432	904.38 -904.38	0.03 -0.03	0	0	0	-2.02 2.08
432		433 433	904.38 -904.38 904.38	-0.19 0.19 -0.25	0	0	0	1.7
433		434 434	-904.38	0.25 -0.24	0	0	0	-1.7 1.2
434		435 435	-904.38 904.38	0.24	Ō	0	0	-1.2 0,73
報酬を 1000年 (2004年) 435日 (2004年)		436 436	-904.38 904.38	0.18 -0.12	o O	0	0	-0.73 0.36
436		437 437	-904.38 904.38	0.12 -0.07	0	0	0	-0,36 0,12 -0,12
437		438 438	•904,38 904,38	0.07 -0.03	0	Ŏ O	0	-0.02 -0.02
438	1	439 439	-904.38 904.38	0.03	0	0	o O	-0.08 -0.08
439		440 440	-904.38 904.38	0.01 0.01	0	0	o o	-0.09 0.09
440		441 441	-904.38 904.38	-0.01 0.01	0	0	0	-0.08 0.08
		442	-904.38	-0.01	Ò	0	Ô	-0.06

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мемв	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-2	TORSION	мом-ч	MOM-Z
441	1	442 443	904.38 -904.38	0.01 -0.01	0 0		) 0 ) 0	0.06 -0.04
442		443 444	904.38 -904.38	0.01 -0.01	0		0 0	
443		444 445	904.38 -904.38	0.01 -0.01	0	and the second s	) ) 0	
444	1	445 446	904.38 -904.38	0.61 -0.01	0		0	0
445	1	446 424	904,38 -904.38	0	0	and the second second	0 0 0	0
446	ļ	424 447	904,38 -904,38	0 0	0	A STATE OF THE STA	0 0 0	The state of the s
448	1	448 449	-97.83 97.83	366.16 -366.16	0		0	and the second second
449		449 450	-97.84 97.84	366.16 -366.16	0		0 0 0	
450		450 452		267.05 -267.05	0	and the second of	) ) 0	and the second of the second of the second of
451		452 453	97,84	111.1 -111.1			0	3857.44
452		453 454		-7.89 7.89	0		0 0	3845.62
453		454 455	97.83	-95.1 95.1	Ò		0 0 0	3703.03
454		455 456	97.84		0		0	3469.72
455		456 457	97.84	205.75	0		0 0	3161.09
456		457 458 458	97.84	282.36	0		0 0 0	2737.52
457		459	97.84				0 0	2264.17
458 459		459 460 460	97.84		0		0 0 0	1785.51
		461	97.83	297.06			0 0	1339.92
460 461		461 462 462	97.84	260.44	C		0 0 0 0	949.26
		463	97.84	217.54			0	622.96
462 463		463 464 464	97.84	174.25	0		0 0 0 0	361.59
464		465 465	97.84	134.49	(		0 0	159.85
404		466 466					0 0	

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МЕМЕ		LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	465	1	466 467	-97.84 97.84	-73,41 73,41	0	0	0	-9.06 -101.06
	466	1	467 468	-97.83 97.83	-46.52 46.52	0 0	0	0	101.06 -170.83
	467	1	468 469	-97.84 97.84	-28.09 28.09	0	0		
	468	1	469 451	-97.84 97.84	5.63 -5.63	0	0	0	212.96 -204.52
	469		451 471	-97. <b>8</b> 4 97.84	23.16 -23.16	0	0	0	204.52 -158.19
	470	1	471 472	-97.84 97.84	26,6 -26,6	0	0	0	158.19 -104.99
	471	1	472 473	-97.84 97.84	22.75 -22.75	0	0	0	104.99 -59.49
	472		473 474	-97.84 97.84	16.23 -16.23	0	0	0	59.49 -27.02
	473	1	474 475	-97,84 97.84	10.28 -10.28	0	0	0	27,02 -6.46
	474		475 476	-97.84 97.84	5.48 -5.48	0	0	0	6.46 4.49
	475 476		476 477	-97.84 97.84	2.15 -2.15	0	0	0	-4,49 8.8
	477		477 478 478	-97.84 97.84 -97.84	0.16 -0,16	0	0	0	•8.8 9.13
	478		479 479	97.84 -97.84	-0.81 0.81 -1.11	0	0	0	-9.13 7.52
	479		480 480	97.84 -97.84	-1.04	0	0	0	-7.52 5.3
	480		481 481	97.84 -97.84	1.04	0	0	0	-5.3 3.23
	481	1	482 482	97.84 -97.84	0,8 -0,54	0	0	0	-3.23 1.63 -1.63
	482	1	483 483	97.84 -97.84	0.54 -0.31	0	0	0	0.55
	483		484 484	97.84 -97.84	0.31 -0.14	0	0	0	-0.06 0.06
	484	1	485 485	97. <b>8</b> 4 -97.84	0.14 -0.03	0	o o	0	-0.34 0.34
	485		486	97.84 -97.84	0.03	0	Ŏ	0	-0.41 0.41
	486		487	97,84 -97,84	-0.02 0.04	0	ŏ	0	-0.36 0.36
	487		488	97.84 -97.84	-0.04 0.05	0	0	0	-0.27
			489	97.84	-0.05	Ŏ	ò	ŏ	-0.18

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МЕМВ	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y		MOM-Z
488	1	489 490	-97.84 97.84	0,04 -0.04	0	and the second second	the second second	0	0.18 -0,1
489		490 491	-97.84 97.84	0.03 -0.03	0	1 4 5 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	the state of the s	0	0.1 -0.0
490	1	491 492	-97.84 97.84	0,02 -0.02	0 0	and the second of the second		0	0.03 0.01
491	1	492 470	-97.84 97.84	0.02 -0.02	0	and the second section in the second	0 0	0 0	-0.0 0.0:
492	1	470. 493	-97.84 97.84	0.02 -0.02	0		and the second second second	0	-0.0: 0.00
494	1	494 495	-83.31 83.31	359.94 -359.94	0	2. 1	0 0	0 0	5358.4 -2119.2
495		495 496	-83.31 83.31	359.94 -359.94	0	Annual Control of the	0 0	0	2119.24 3279.3
496		496 498	-83.31 83.31	261.87 -261.87	0	The state of the s	0 0	0 0	-3279,4: 3672.1:
497		498 499	-83.31 83.31	107.69 -107.69	0	the safe of the fact that the	0 0	0 0	-3672.1 3833.5
498	) 	499 500	-83.31 83.31		0	the state of the s	0 0	0 0	-3833.4 3818.4
499	1	500 501	-83.31 83.31		0		0 0	0	-3818.4 3674.0
500	1	501 502	-83.31 83.31		0	and the second s	0 0	0 0	-3674.0 3440.1
501	1	502 503	-83,31 83,31		0		0 0	0	-3440.11 3131.8
502	1	503 504	-83.31 83.31				0 0	0	-3131.8 2710.5
503	1	504 505	-83.31 83.31		C		0	0	-2710.5 2240.
504	1	50 <b>5</b> 50 <del>6</del>	-83.31 83.31		and the second second		0	0	-2240.5 1765.7
505		506 507	The second second				0	0	-1765.7 1324.2
506	1	507 508				and the second of the second	0	0	-1324.2 937.
507		508 509	a				0	0	-937. 614.4
508	144 - 144 -	509 510		172.34			0	0	-614.4 355.9
509		311	83,31	132.93	laska nyayê <b>(</b> Diskara bi diskara Diskara bi bi b		0	0	-355.9 156.5
510		511 512	83.31	99.29		医试验剂体	0	0	-156.5 7.6
511	1	512 513		-72.44 72.44			0	0	-7.6 -101.0

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MEMB	LOAD	NODE	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	мом-ү	MOM-Z
512		1 513 514	-83.31 83.31	-45.83 45.83	0		and the second second	101.02 -169.76
513		1 514 515	-83.31 83.31	-27.61 27.61		7		169.76 -211.18
514		1 515 497	-83.31 83.31	5.7 -5.7	0			211.18 -202.62
51 <b>5</b>		1 497 517		23.01 -23.01			) 0 ) 0	202.62 -156.6
516		1 517 518		26.37 -26.37	0		) ) 0	
517		1 518 519		22.53 -22.53			) 0 ) 0	
518		1 519 520		16.07 -16.07			) )	58.8 -26.67
519		1 520 521	-83.31 83.31	10.17 -10.17			) ) 0	26.67 -6.34
520		1 521 522	83.31	5.41 -5.41	0			
521		I 522 523	83,31	2.12 -2.12	0	•	)	-4.49 8.73
522		1 523 524	83.31	0.16 -0.16	0		) 0	-8.73 9.04
523		1 524 525		-0.8 0.8	0		0	-9.04 7.44
524		1 525 526	83.31	-1.1 1.1	0	•	)	
525		1 526 527 1 527	83.31	-1.03 1.03	0			-5.24 3.19 -3.19
526 527		528 1 528	83.31	-0.79 0.79 -0.53	0	•	0	1.61 -1.61
528		529 1 529	83.31	0.53 -0.3	0		)	0.55 -0.55
529		530 1 530	83.31	0.3 -0.14	0		0	-0.06 0.06
530		531 1 531	83.31	0.14	Ŏ		) 0	-0.34 0.34
531		532 1 532	83.31	0.03	0		0	-0.4 0.4
532		533 1 533	83.31	-0.02 -0.02	0		0	-0.36 0.36
533		534 1 534		-0.04 0.05	0	•	) 0	-0.27 0.27
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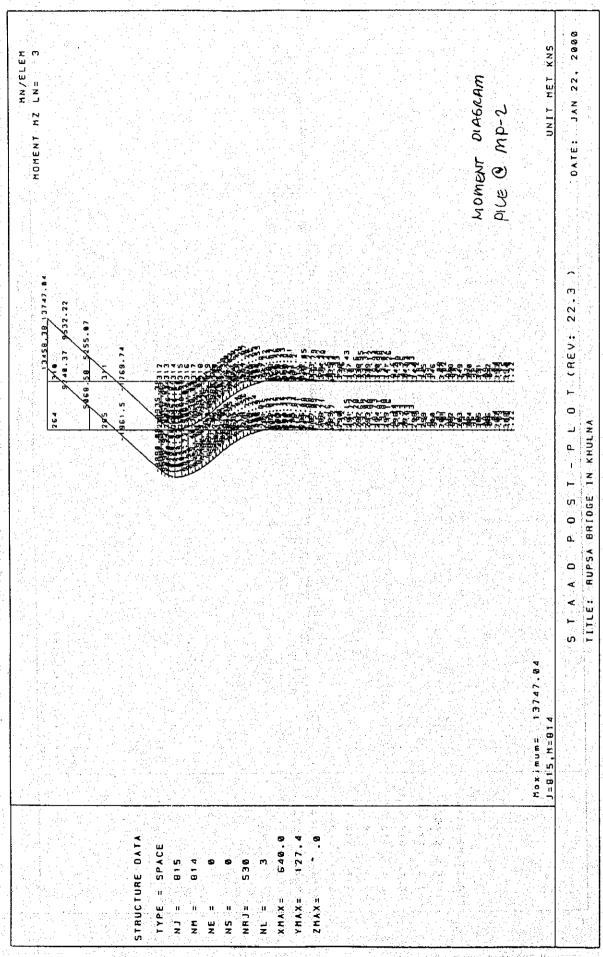
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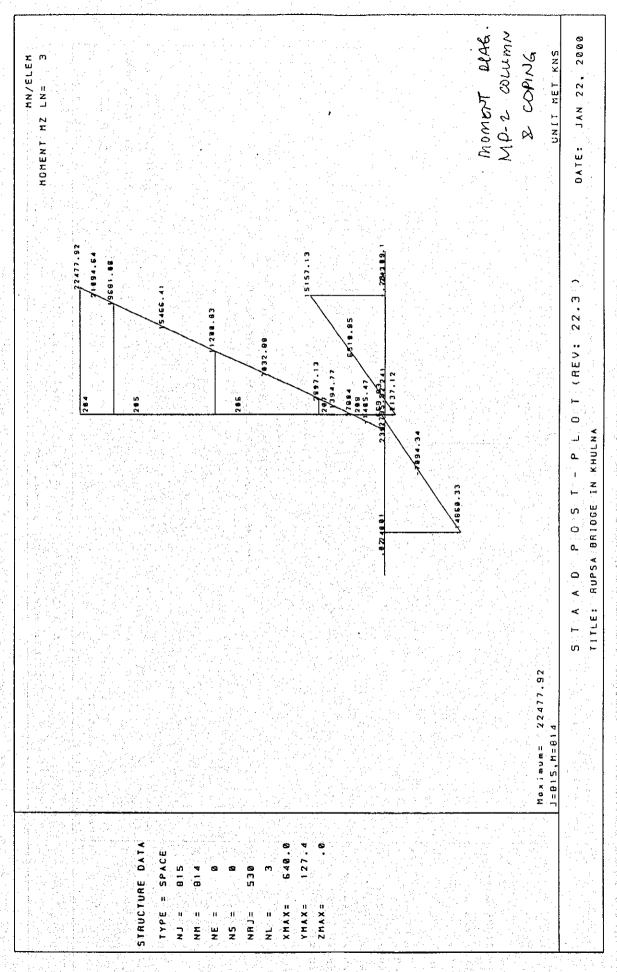
PRESTRESS LOAD

OF FRAME 5 (WHOLE STRUCTURE)





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