

Figure 2.24 VLF Result -Hoa Thuong (HTVLF1)

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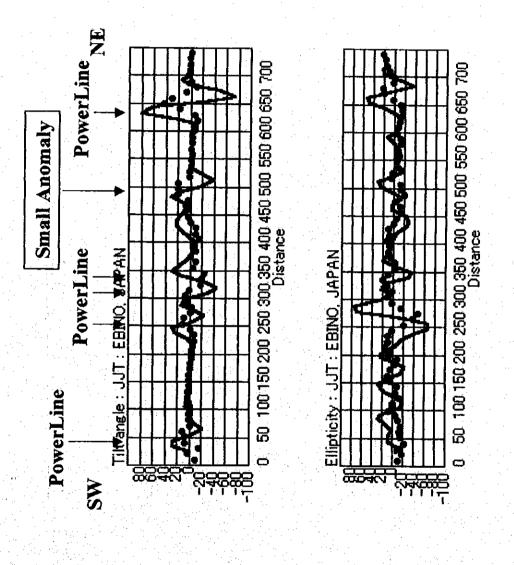


Figure 2.25 VLF Result -Hoa Thuong (HTVLF2)-

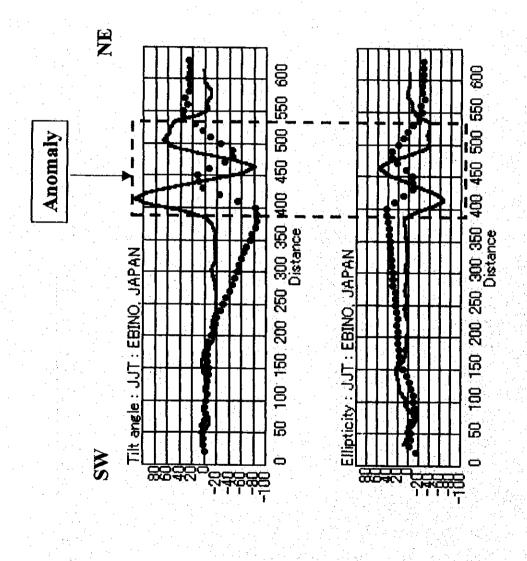
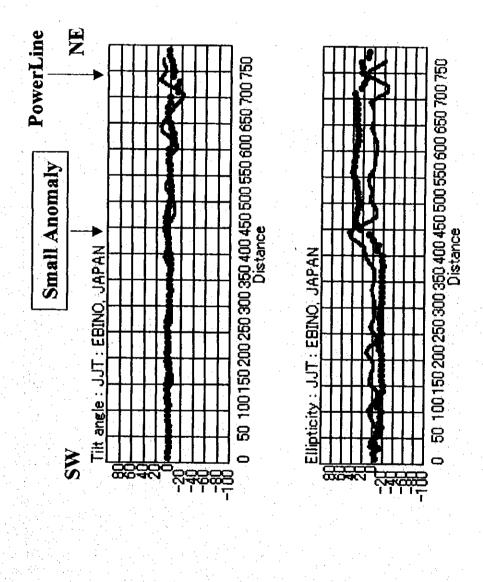


Figure 2.26 VLF Result -Dong Bam(DBVLF1)-



VLF Result -Dong Bam(DBVLF2)-Figure 2.27

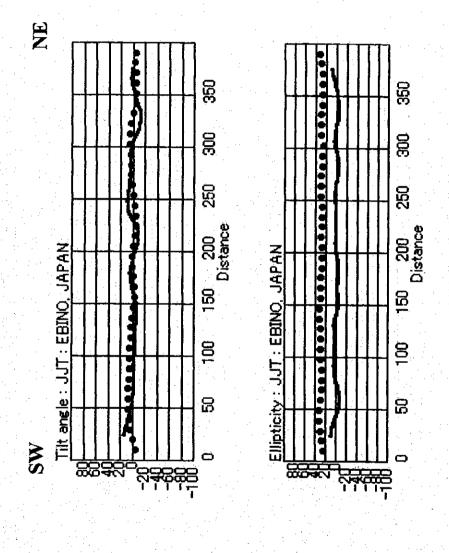
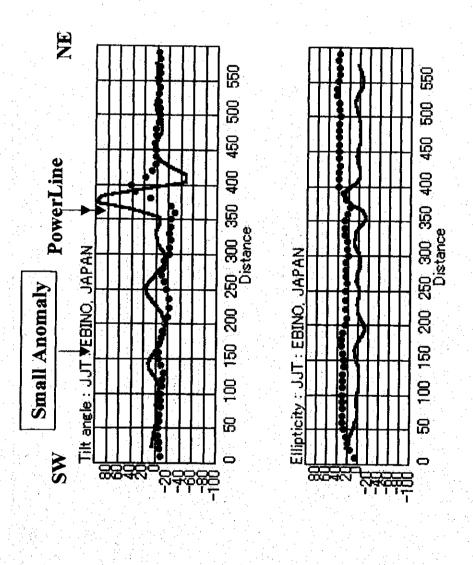


Figure 2.28 VLF Result -Thinh Duc (TDVLF1)



VLF Result -Thinh Duc (TDVLF2) Figure 2.29

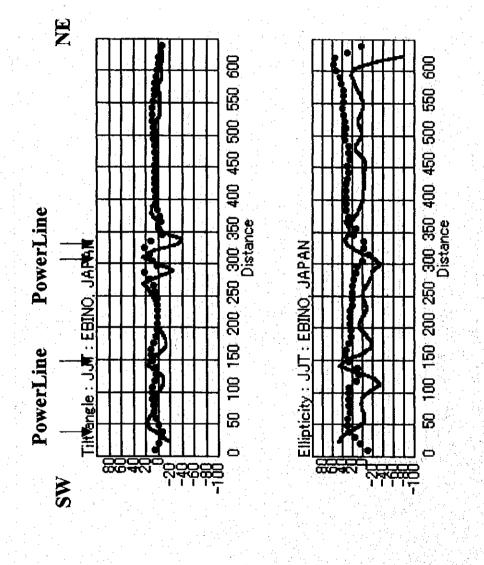


Figure 2.30 VLF Result -Nam Tien (NTVLF1)-

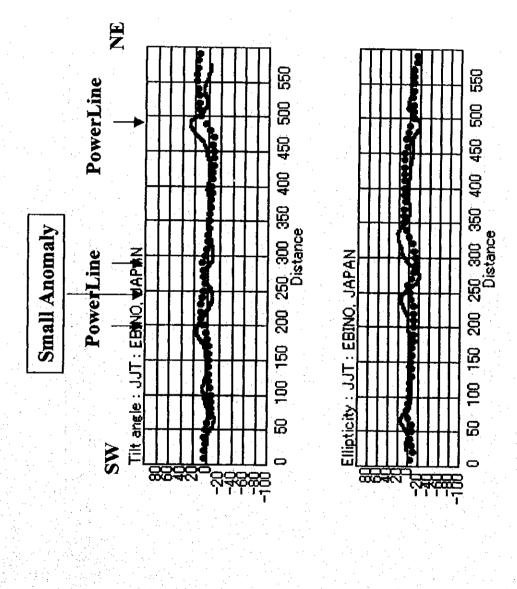


Figure 2.31 VLF Result -Nam Tien (NTVLF2)-

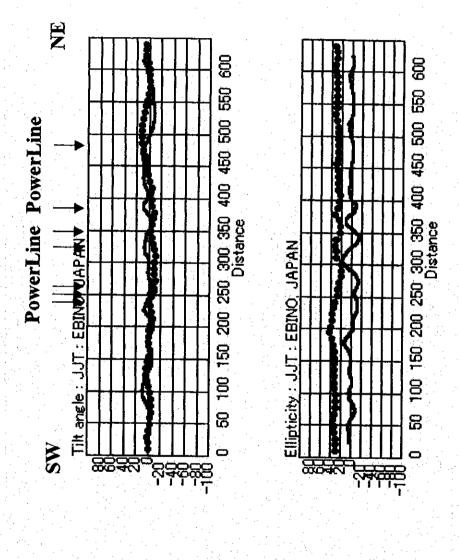
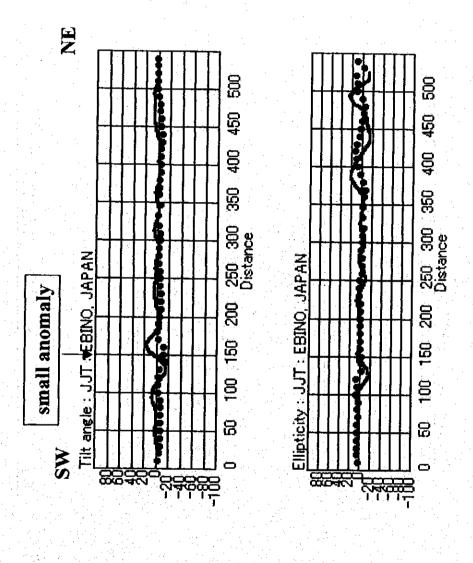
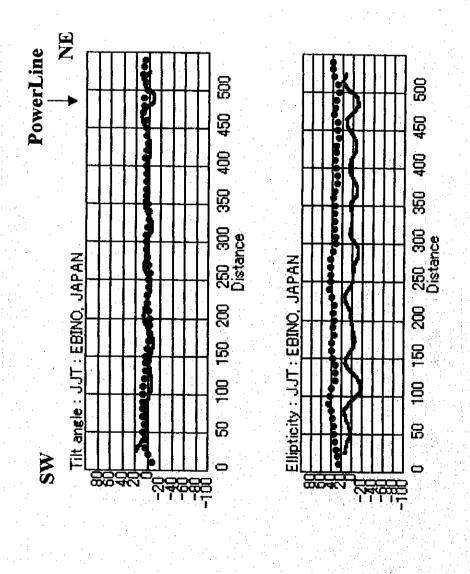


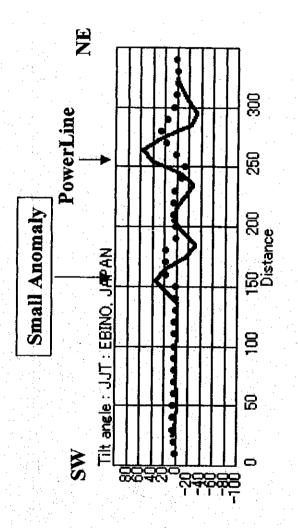
Figure 2.32 VLF Result -Nam Tien (NTVLF3)-

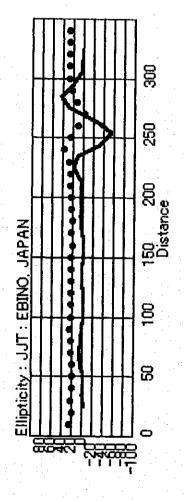


VLF Result -Yen Thang (YTVLF1)-Figure 2.33



VLF Result -Yen Thang (YTVLF2)-Figure 2.34





VLF Result -Yen Thang (YTVLF3)-Figure 2.35

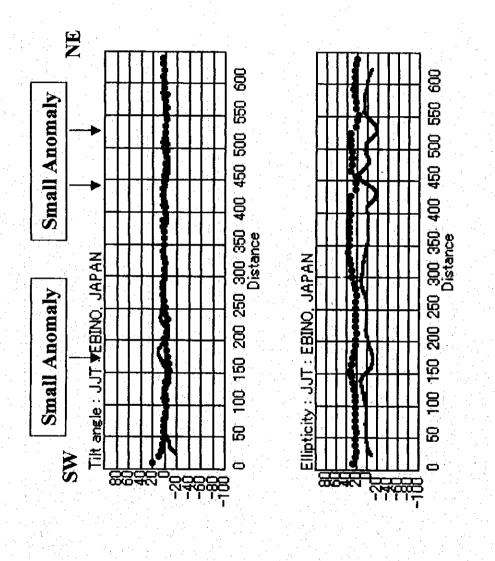
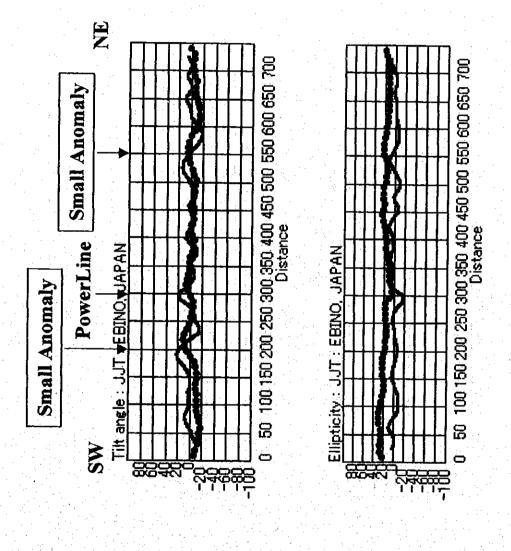


Figure 2.36 VLF Result -Yen Thang (YTVLF4)-



VLF Result -Quang Son (QSVLF)-Figure 2.37

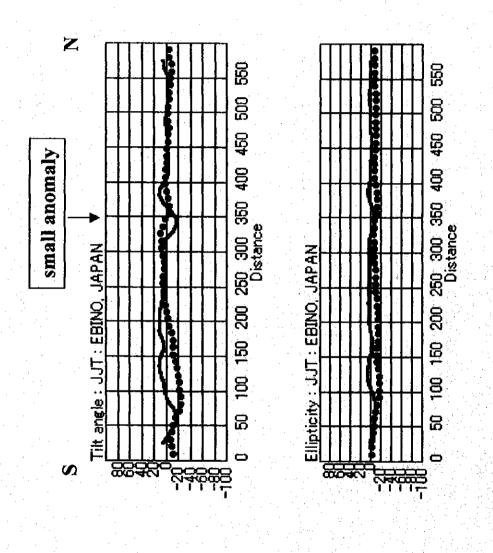
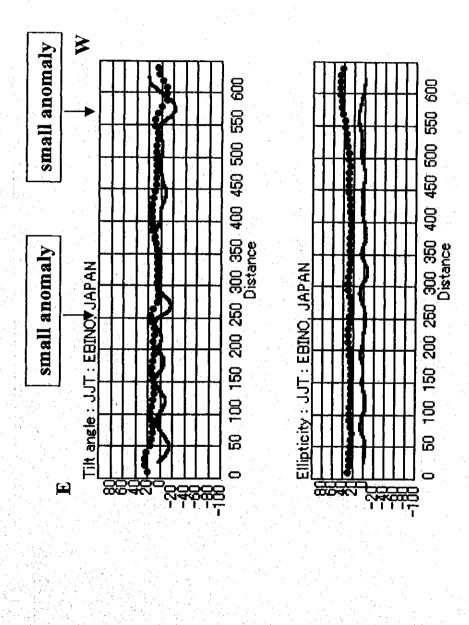
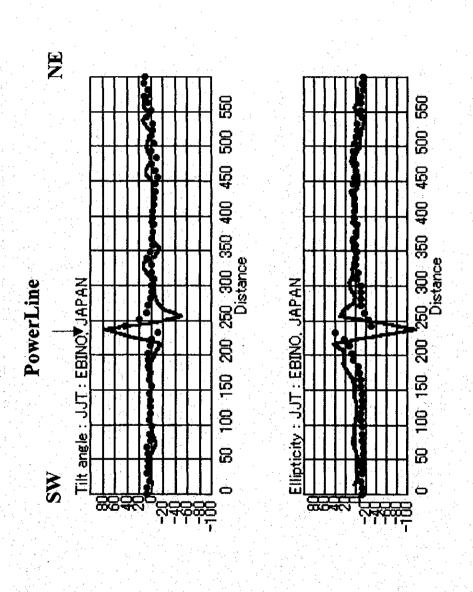


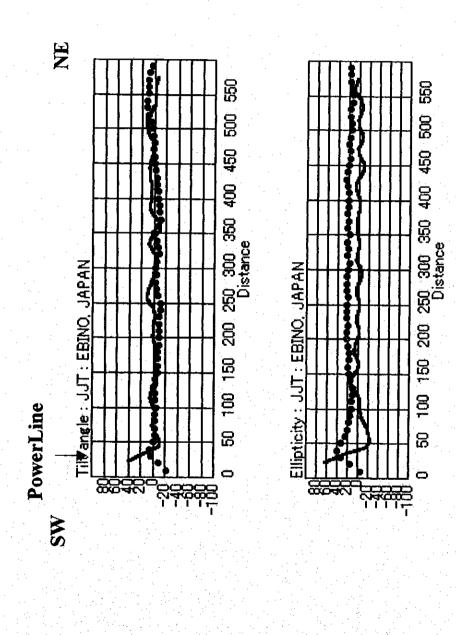
Figure 2.38 VLF Result -Dong Phong (DPVLF1)



VLF Result -Dong Phong (DPVLF2)-Figure 2.39



VLF Result -Vinh Thanh (VTVLF1)-Figure 2.40



VLF Result -Vinh Thanh (VTVLF2)-Figure 2.41

# CHAPTER 3

**PUMPING TEST** 

#### CHAPTER 3 PUMPING TEST

### 3.1 Methodology

Pumping tests were carried out at the test wells to obtain aquifer constants. The tests were performed after installation of casing/screen pipes and well development. The pumping test is comprised of three (3) types of test; viz. step-drawdown test, continuous drawdown test, and recovery test. The step-drawdown test was conducted prior to the continuous pumping test. Four (4) steps with pumping duration of four (4) hours for each step were conducted in each step-drawdown test. The duration of continuous pumping test was 2,880 minutes (48 hours). The recovery test was started just after the continuous pumping test for a duration of 720 minutes (12 hours).

During a well development work at JICA-1 in Dong Bam, Thai Nguyen, the land near the well sank and the neighboring houses were slightly damaged. The Study Team investigated immediately after the incident, then supervised the contractor to stop the well development work. The incident happened after two (2) days from the starting of well development. The discharge rate was about 900  $\ell$ /min. The Study Team decided not to perform further well development and pumping test at JICA-1 well to prevent expansion of the damages. Therefore, detailed aquifer evaluation based on pumping test is not available at JICA-1 well.

## 3.2 Step-Drawdown Test

The results of step-drawdown test at test wells are tabulated in Table 3.1. It is noted that the four (4) steps of step-drawdown test could not be carried out at JICA-3 well (Nam Tien, Thai Nguyen) and JICA-13 well (Trung Le, Ha Tinh), because the wells yielded small amount of water so that only two (2) steps' drawdowns were able to be measured.

Based on the test, a specific capacity value of each step was obtained, then aquifer loss coefficient (B) and well loss coefficient (C) were computed. In practice, the drawdown at a well consists of the aquifer loss and the well loss. Jacob (1947) stated that well loss is proportional to some power of the discharge exceeding the first power and approaching the second, so that the total drawdown  $s_w$  is given by:

$$s_w = BQ + CQ^n \tag{3.1}$$

where B is the aquifer loss coefficient, C is the well loss coefficient, and n is a constant greater than one. In the Study, the n value is assumed to be 2.

Well efficiency of each pumping step was also calculated and average well efficiency of each well is obtained. The well efficiency can be defined as the percentage of  $(BQ / s_w)$  for a specified duration of pumping.

Graphical interpretation of step-drawdown test at each test well is presented from Figures 3.1 to 3.14.

The results show that the values of aquifer loss coefficient B at JICA-3 (Nam Tien), JICA-4 (Thinh Duc), and JICA-8 (Van Thang) are higher, within a range from 1.0E-2 to 1.0E-1 day/m<sup>2</sup>. This is because the aquifers consist of sandstone with less permeability. The B values of JICA-5 (Quang Son) and JICA-6 (Yen Thang) wells are also higher even the aquifer consists of limestone. This can be explained that the porous space in fractured limestone is filled with clayey materials, that may reduce permeability of the aquifer.

The values of well loss coefficient C take a wider range of distribution. Small values of C in a range between 1.0E-7 and 1.0E-8 day<sup>2</sup>/m<sup>5</sup>, indicating smaller drawdown caused by the well structure, were obtained from JICA-2 (Hoa Thuong), JICA-7 (Dong Phong), JICA-9 (Thieu Hung), and JICA-10 (Dinh Tuong) wells. The C values of JICA-5 (Quang Son) and JICA-6 (Yen Thang) wells are greater, showing the drawdown caused by unit discharge is greater due to the well structure.

The performance of a well can be evaluated from the well efficiency value. If the total drawdown is equal to the drawdown caused by aquifer loss, the well efficiency is 100 %. The test wells of JICA-4 (Thinh Duc) and JICA-7 (Dong Phong) have more than 90 % in well efficiency. Lower well efficiency values below 60 % were obtained from JICA-2 (Hoa Thuong), JICA-11 (Vinh Thanh), JICA-12 (Duc Yen), JICA-14 (Thieu Do), and JICA-15 (Trung Le).

The relationship between discharge rate Q and drawdown s is plotted on a log-log graph. If the Q-s curve is vended upward, the Q value at the turning point is called "critical discharge rate" of the well. It can be said that the discharge rate above the turning point may not suitable for continuous pumping. For example at JICA-2 well (Hoa Thuong), the drawdown curve of the step-drawdown test became almost stable in each step until step-3 ( $Q_3$ 51,080 m³/day), however, the curve in step-4 ( $Q_4$ 51,440 m³/day) was not stabilize within the duration of 240 minutes. Therefore, the Q-s curve is vended at step-3 and the Q-s plot at step-4 is

plotted above the extended portion of the linear line between step-1 and step-3. Such critical discharge rates are found at wells of JICA-5 (Quang Son, Q5259.2 m³/day), JICA-6 (Yen Thang, Q5172.8 m³/day), JICA-14 (Thieu Do, Q51425.6 m³/day), and JICA-15 (Trung Le, Q5259.2 m³/day).

# 3.3 Continuous Pumping Test and Recovery Test

The results of continuous pumping test and recovery test are summarized in Table 3.2. The values of transmissivity are obtained by Cooper-Jacob method, Their method, and Recovery method. The values of storativity are obtained by Cooper-Jacob method and Their method.

Cooper-Jacob method uses a semi-log plot of drawdown s versus the logarithm of time t. The plots usually form a straight line, and the transmissivity T can be computed by obtaining the drawdown difference  $\Delta s$  per log cycle of t. Storativity (or storage coefficient) S is computed by obtaining  $t_0$ ; the value of  $t_0$  can be obtained by projecting the straight line of semi-log plots to s50.

Theis method uses a log-log plot of drawdown s versus time t. The log-log type curve of W(u) versus 1/u is prepared to find a matching point of superposition on the drawdown curve to obtain S and T. Usually the match point is found by manually graphic method, however, in this Study, a compute code called "AQUITEST" was used to obtain S and T values by automatic curve fitting.

Recovery method is similar to Cooper-Jacob method, using a semi-log plot of residual drawdown s' versus time ratio t/t'. From the straight portion of the plots,  $\Delta s'$  per log cycle of t/t' can be obtained, then T is computed.

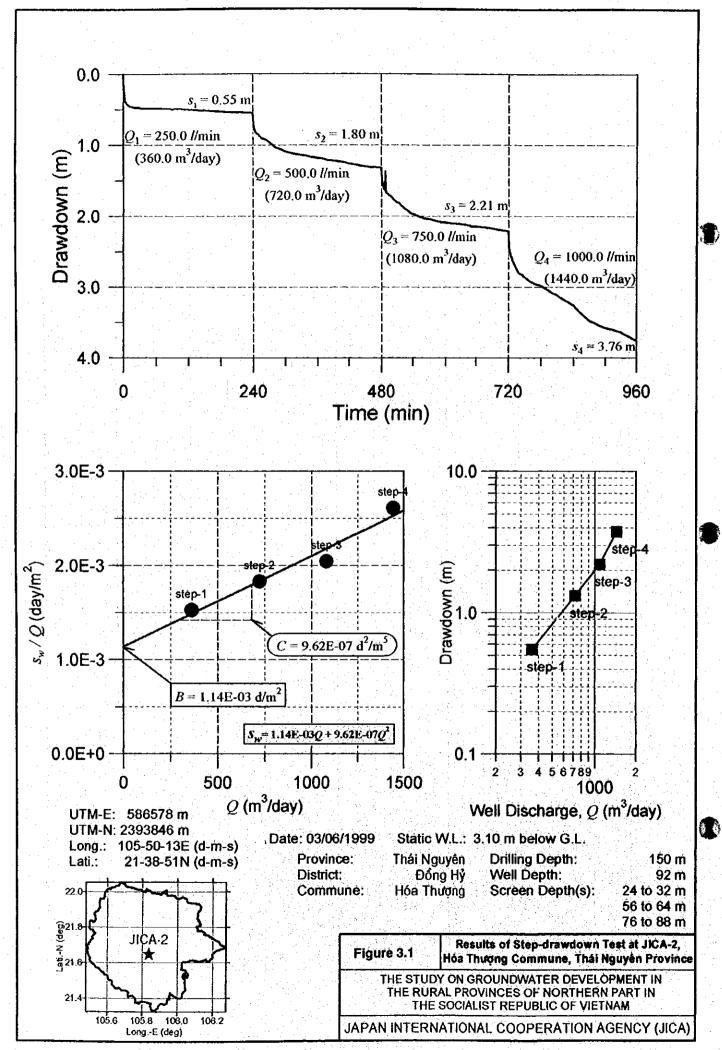
The results of continuous pumping test and recovery test by Cooper-Jacob method and Recovery method are shown in Figures 3.15 to 3.28. The results of continuous pumping test analysis by Theis method are shown in Figures 3.29 to 3.42. It is noted that the time-drawdown curves of JICA-5 (Quang Son), JICA-9 (Thieu Hung), and JICA-14 (Thieu Do) wells show a leaky type confined aquifer, so that Hantush method was applied to obtain aquifer parameters.

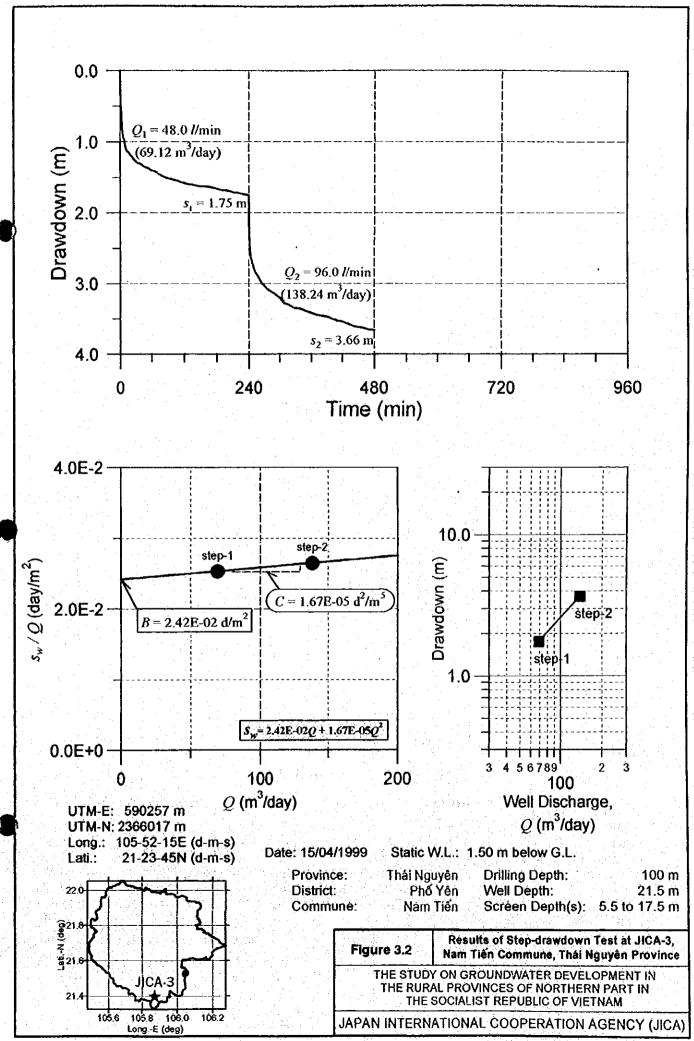
Table 3.1 Results of Step-Drawdown Test at JICA Test Wells

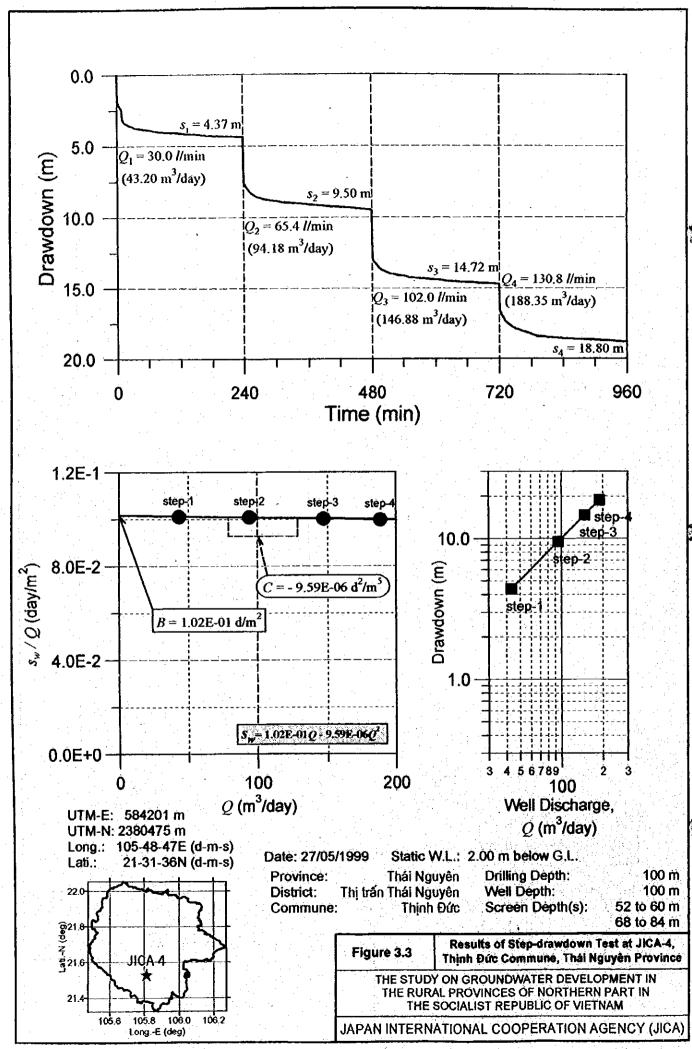
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Test Well	District	3-WILD	N-MTO	Drilling	Well	Soreen	Date(dd/mm/yy)	O1(m³/day)	02(m <sup>3</sup> /day)	Q3(m³/day) Q4(m³	04(m³/day)	Aquifer Loss	Well Loss	Average Well
Š	Province	Ê	æ	Depth (m)	Oepth (m)	Depth(a) (m)	Statio Water Level (m below G.L.)	s1(m) So1(m²/day)	s2(m) So2(m²/day)	s2(m) So3(m²/day)	e4(m) So4(m² / day)	Coefficient B (d/m²)	Coefficient C (d²/m²)	Efficiency (%)
	Đông Bám													
JICA-1	Đồng Hỳ Thời Nguyễn	587420	2389687	92	92	40 to 72	•		•	:		1	ı	
	Hoa Thượng					24 to 32		360.00	720.027	1080,00	1440.00			
JICA-2	Edng HV	586578	2393846	150	92	56 to 64	03/06/1989	0.55	1,80	2,21	3.78	1,145-03	9.62E-07	54.90
	Thái Nguyên					70 to 88	3.10	654.55	400.00	488.89	382.98			
	Nam Tiến							69,12	138.24	1	1			
JICA-3	Phơ Yên	590257	2366017	90	21.5	5.5 to 17.5	15/04/1989	1,75	3,66		,	2,425-02	1,675-05	93,49
	Thái Nguyên						1.50	39.50	37.77	1	1			
	Thinh Đức	2				8 to 18	:	43.20	94,19	146.88	188.35		-	
1CA-4	Thi trấn Thái Nguyên	584201	2380475	8	8	52 to 60	27/05/1998	4.37	8,50	14,72	13.80	1,025-01	-9.59E-06	101.48
	Thái Nguyên					88 to 84	2.00	9.89	9.91	90.6	10.02			
	Quang Son							86.40	172,80	259,20	345.60	ı		
JICA-5	Thi tran Tam Elep	592553	2228660	150	120	72 to 116	05/03/1988	9.00	15.20	21.90	43.00	7,44E-02	1,06E-04	78.20
	Ninh Bình						10.80	10.60	11.37	11.84	8.04			
	Yen Thang					78 to 84		57.60	115,20	172.80	230,40			
JICA-6	Yen Mo	600941	2220065	130	136	92 to 104	17/03/1990	10,87	22,89	35.77	54,97	1.695-01	2.745-04	81.77
. '	Ninh Bình			•		124 to 132	1.23	5.30	5.03	4.83	4.19			
	Dong Phong							432.00	964,00	1296,00	1728.00			
JICA-7	Nho Ouan	577817	2246829	120	130	92 to 126	23/05/1999	2,07	4.56	6,49	8.54	4,96E-03	4.01E-08	99,26
	Ninh Bình						0.60	208.70	188.47	200.00	202.34			
	Van Tháng					-		158,40	271,54	475,20	633.60			
JICA-8	Nông Cống	265030	2170050	<u>\$</u>	120	90 to 119	05/02/1999	9,83	20.98	41,60	56.53	5,80E-02	5.486-05	74.95
	Thanh Hoa	: -					5.70	16.11	12,94	11.42	11.21			
15	Thiệu Hưng		•	:				352.80	705.60	1058.40	1411,20			
JICA-9	Thiệu Hoá	671655	2199306	2	25	32 to 48	10/02/1990	2.40	4,55	7,12	10,01	5.795-03	9,14E-07	85,65
	Thanh Hos	: :					4:00	147.00	155.08		140.96			
	Djrih Tuðing			٠		23,2 to 39,2		432,00	984,00	-	1728.00			
JICA-10	Yen Onh	568421	2207260	27.2	91.2	47.2 to 63.2	10/04/1999	1.26	3.03	4.92	7.04	2,635-03	8,735-07	74.81
	Thanh Hoa						<b>98</b>	342.86	286.09	263.47	245.45			
	Vinh Thanh			. !				362,00	734,40	1123.20	1512.00			
JICA-11	Vinh Loc	564793	2210122	₹	 2	32 to 48	7.55	184.62	149 68	9.80	1427	33896-03	3.905-05	95,43
	Dúc Yên	1.						108.00	216,00	324.00	432.00			
JICA-12	OUC Tho	563705	2048152	961	2	20 to 26	06/03/1999	1,38	3,24	6.11	9.27	9.36E-03	2.82E-05	57.50
	Hà Tinh					84 to 100	2.90	79.41	66.67	53.03	46.60			
	Trung Lê		1.7					12.96	25,92	•	•	-		
JICA-13	Dúc Tho	566783	2046329	8	8	58 to 82	08/04/1999	2,56	14.60	1	•		ı	ı
	HA Tinh				1		2.60	5.06	1.78	•				
	Thiệu Đô					- 1 - 1 - 1		475,20	950,40	1425,60	1900.80			
JICA-14	Thiệu Hoa	572185	2197515	2	<del></del>	18 to 50	29/03/1999	2,08	4,21	7.01	13.67	3.006-03	1.886-06	59,75
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JICA-15	Ede Tro	587146	2046557	2	₹	95 of 91	2.48	0.86	08.1	3,09	6.93	6.695-03	6,615-05	47.16
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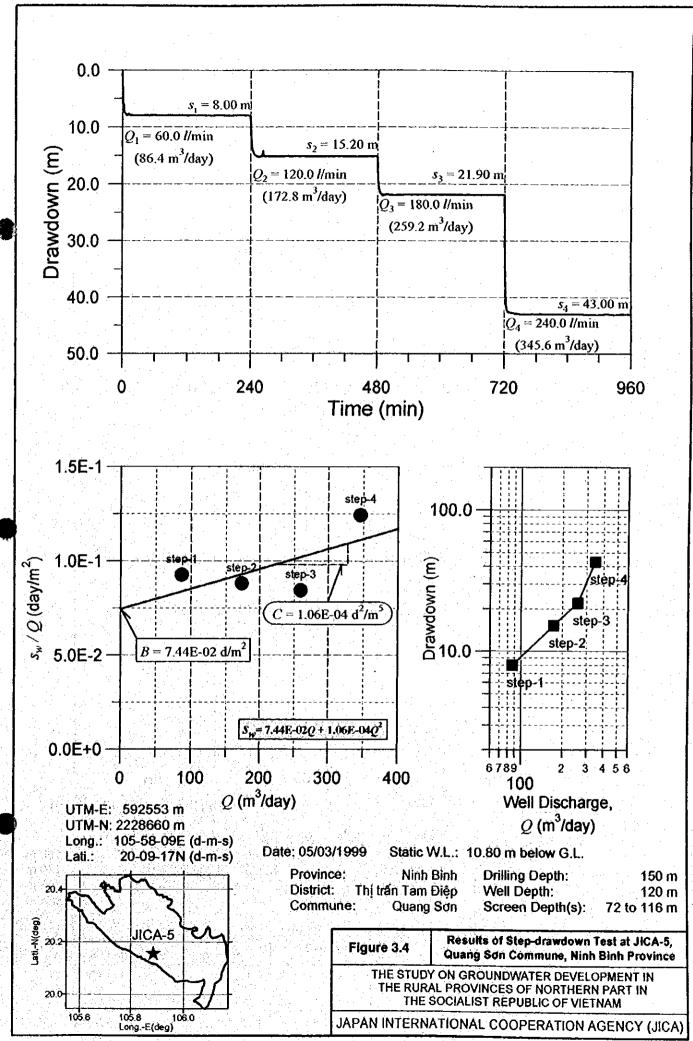
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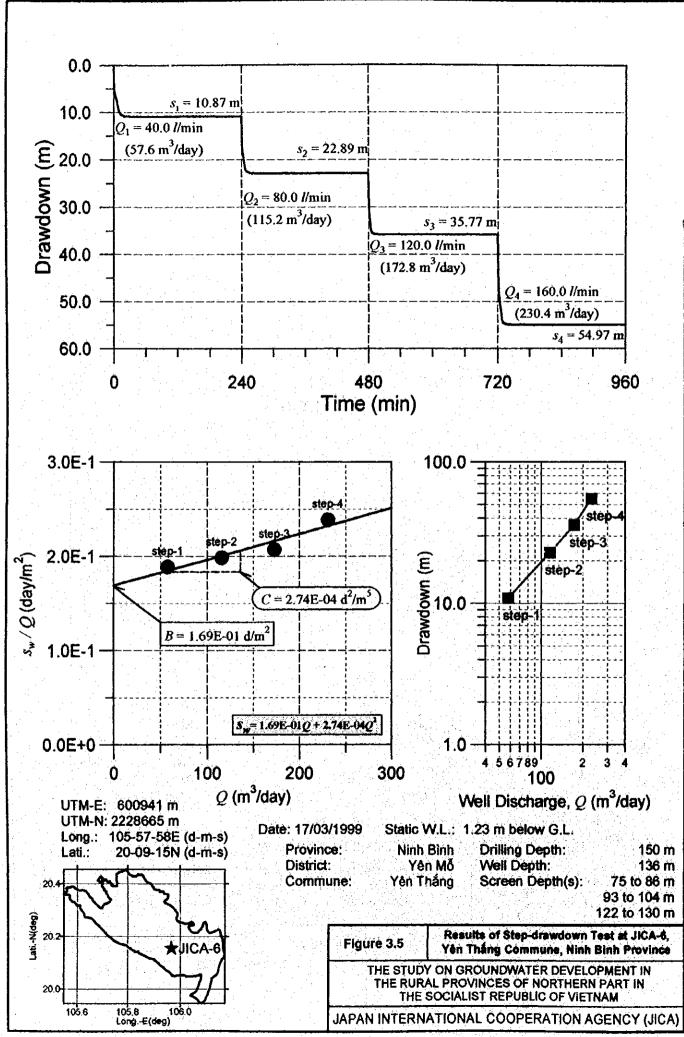
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	Thai Nguyên					76 to 88								30.00	200	1000		3/C-1/5	40,00	2020
	Nam Tien							2												
<b>₽-43</b> 5	Phó Yen	590267	2386017	8	21.6	6.5 to 17.5	12.0	16/04/1999	1,90	13824	4.75	29.10	24.00	2.00F+00	7.095-01	22.8	1 CRF-LOO	A 48FaA	20.43	2245.00
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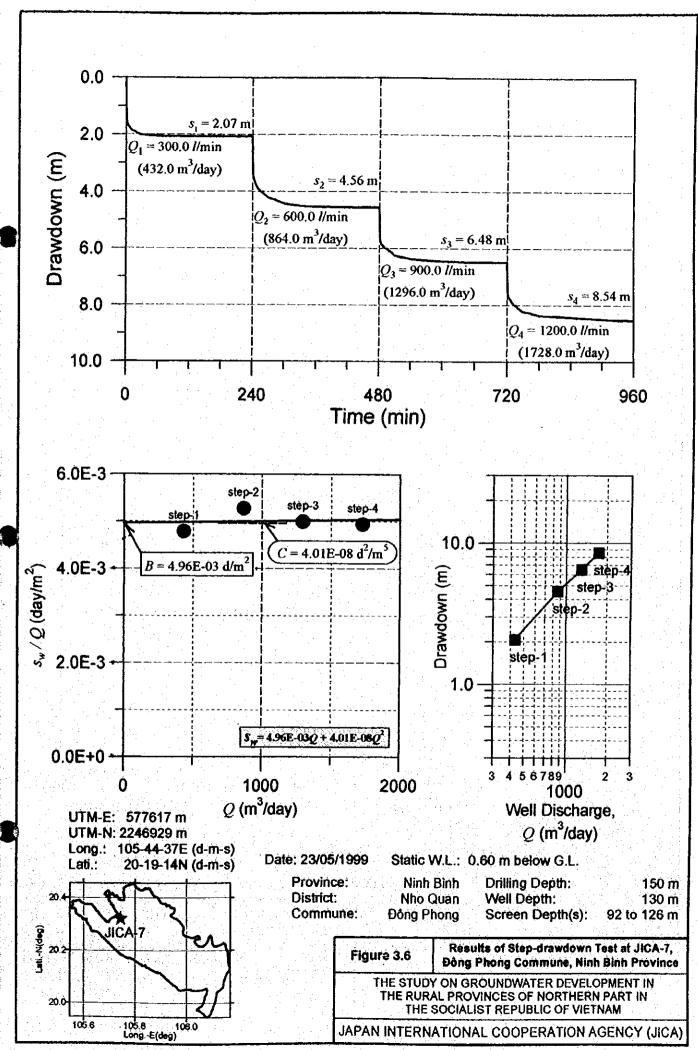


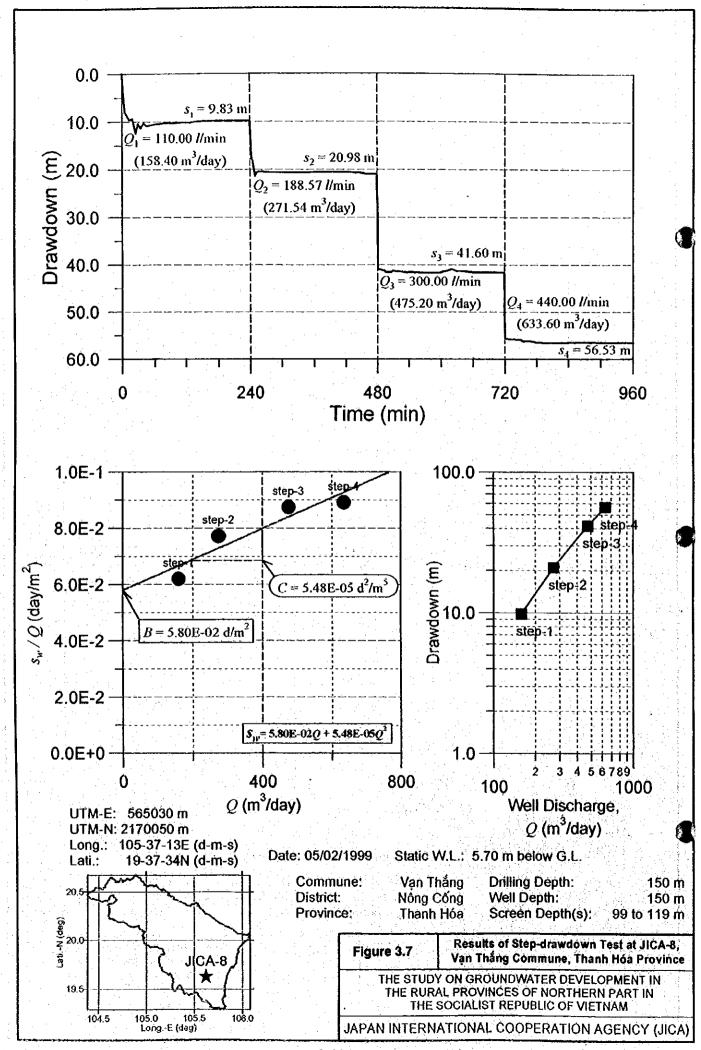


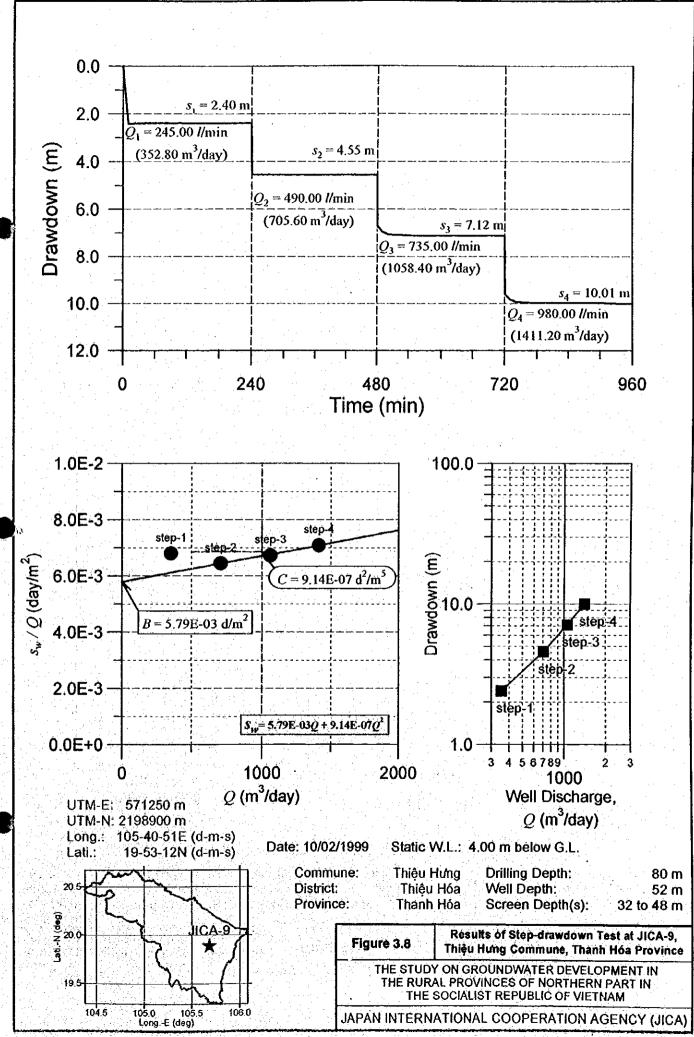


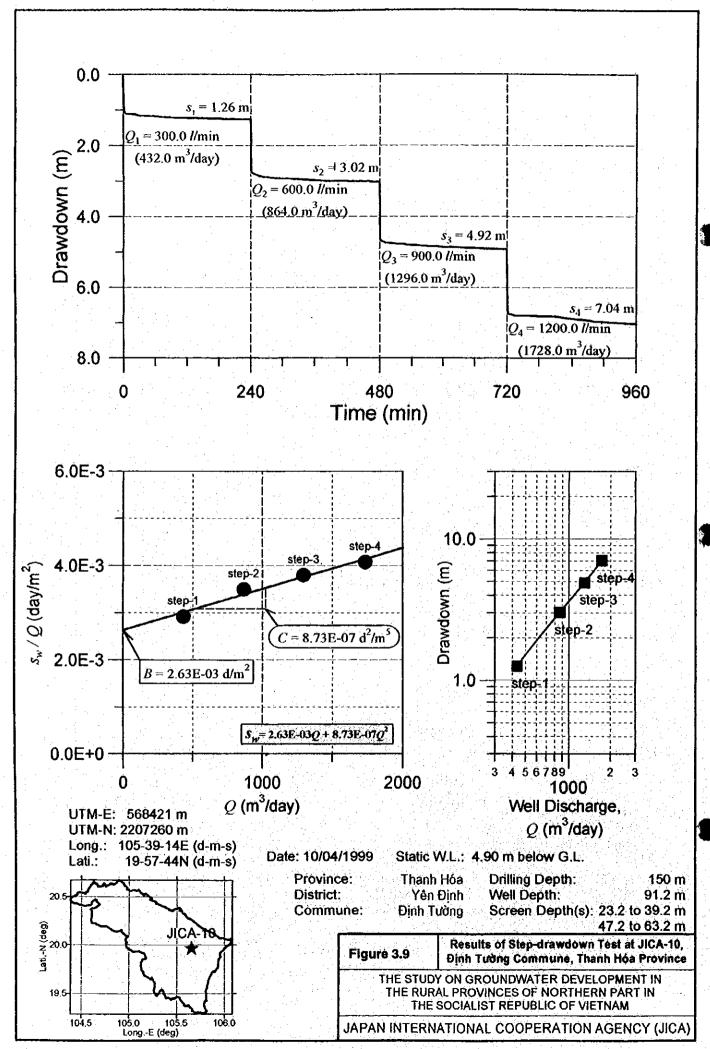


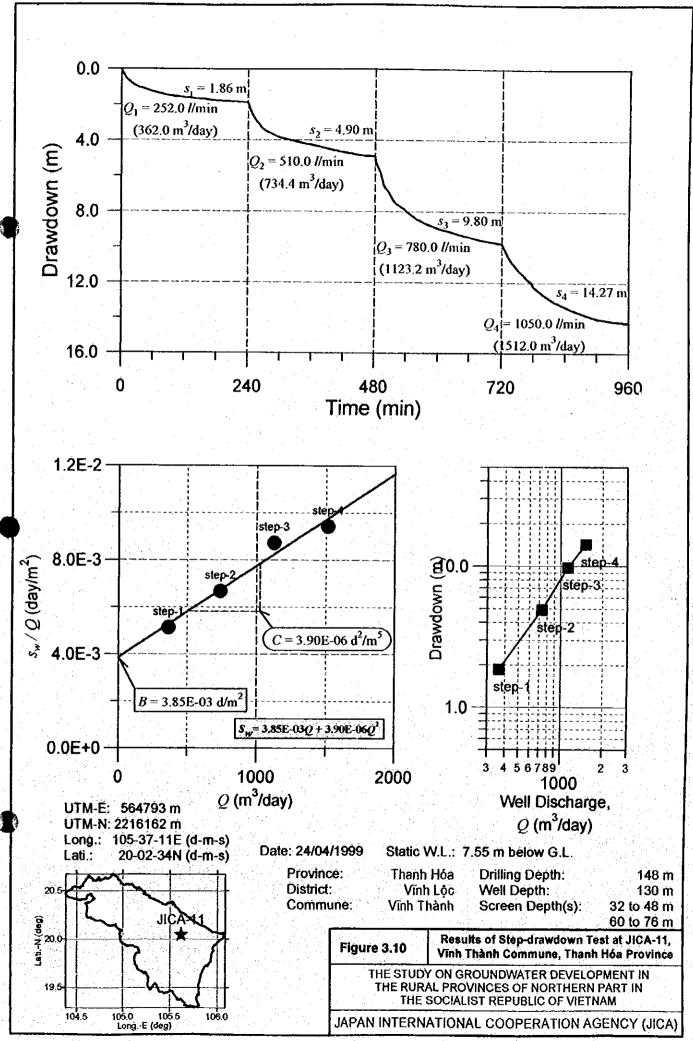


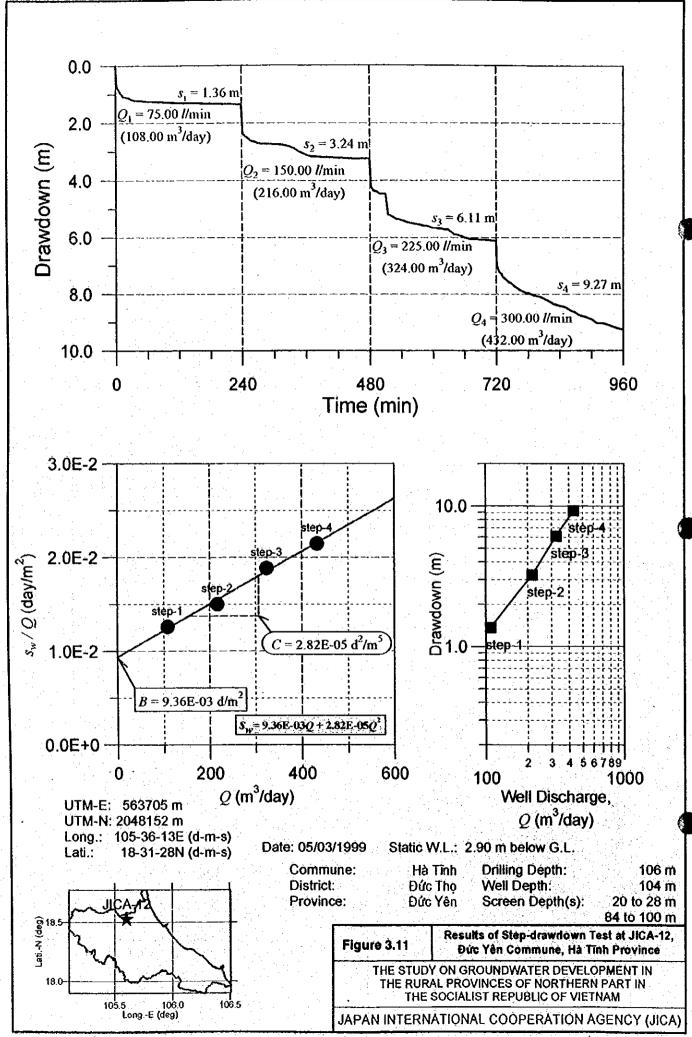


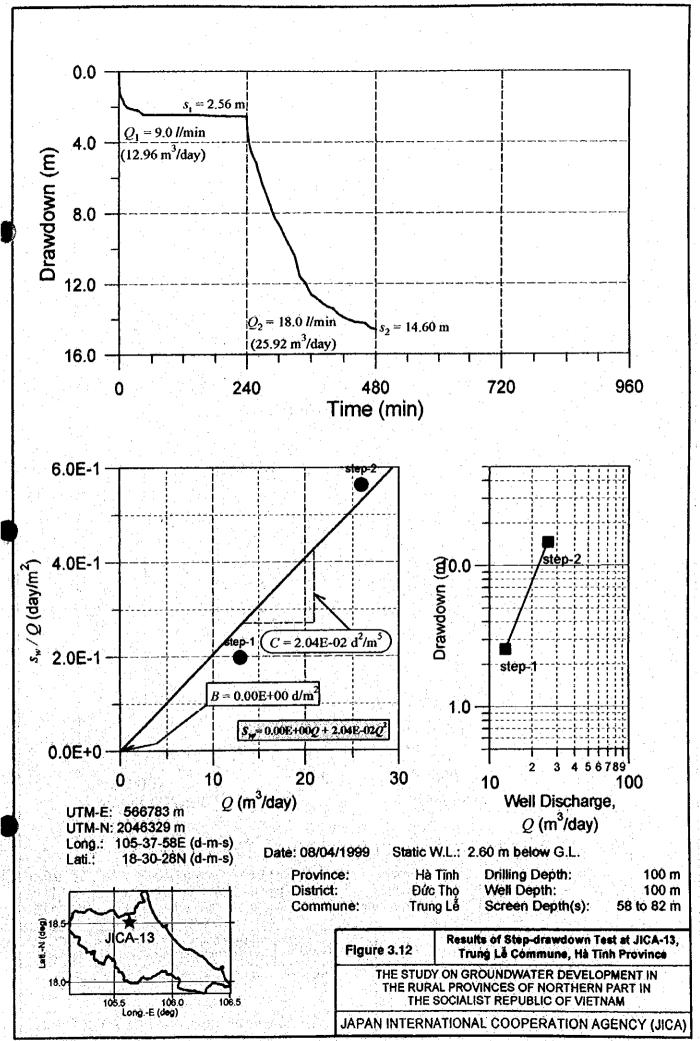


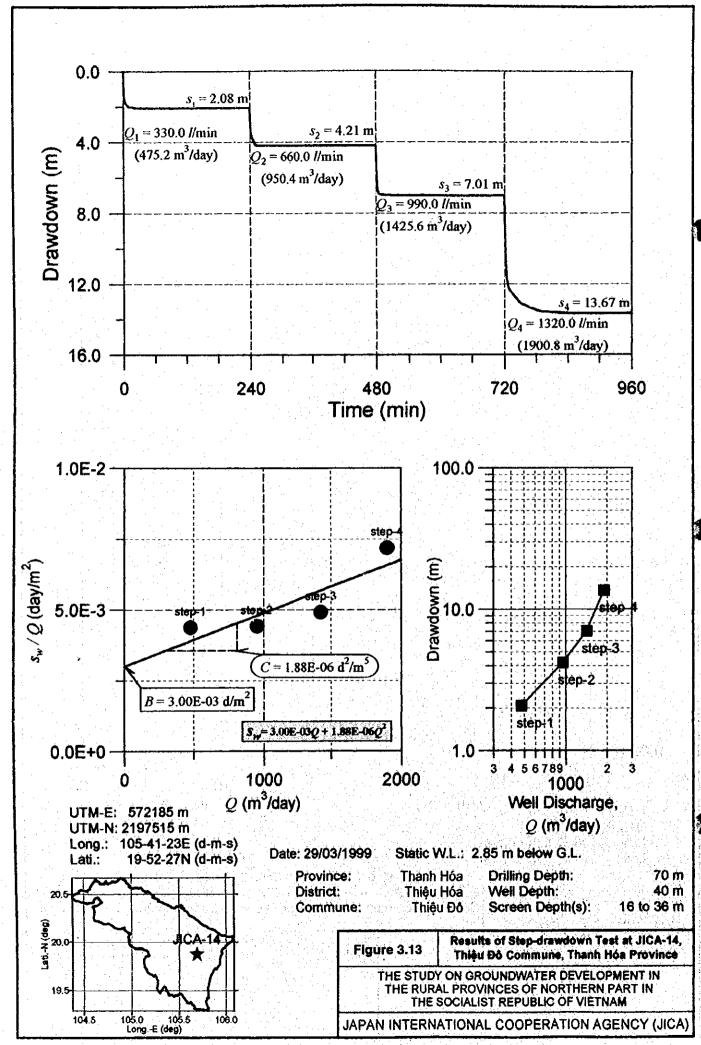


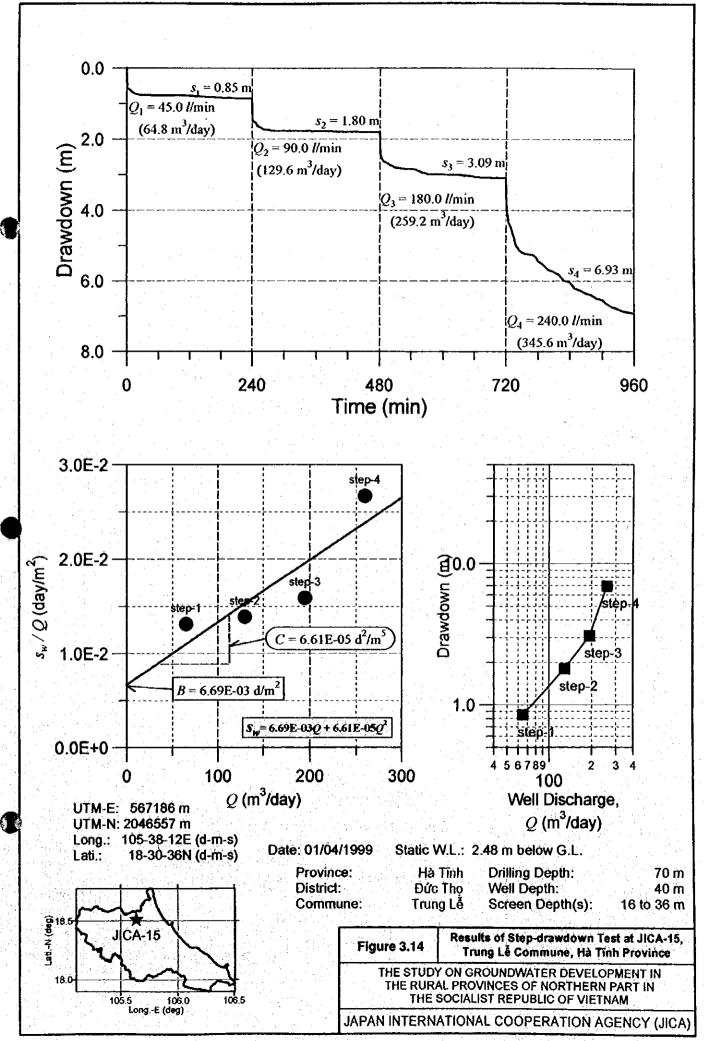


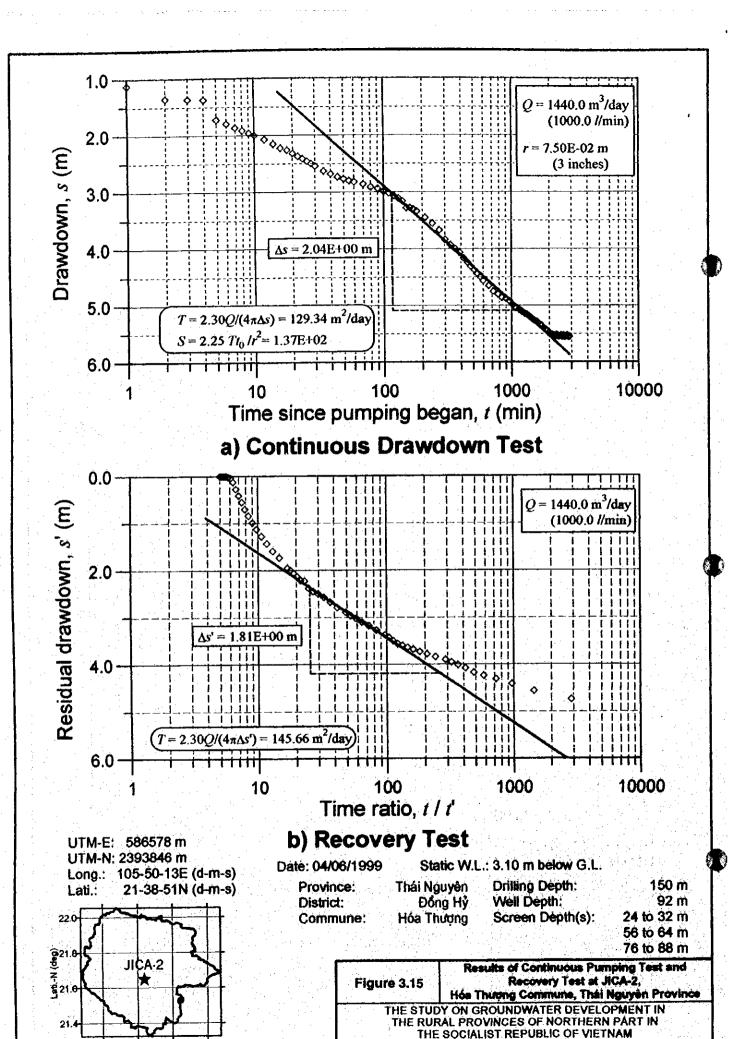












JAPAN INTERNATIONAL COOPERATION AGENCY (JICA)

105.8

Long - (deg)

106.0

