GE2. WATER PRESSURE TEST DATA

List of Borehole Water Tests (1)

				Average I	ugeon Valu	<u> </u>	and the second sector between	
Depth (m)	M98-1	M98-2	M98-3	M98-4	M98-5	M98-6	M98-7	M98-8
					k= 5x10 ⁻⁵			
					to 1x10 ⁻²			
2-7	128	112	68	5	cm/sec	8	41	38
5 10	110	65	13	0.		1	78	41
10 15	79	36	7	11	1	1	105	19
15 - 20	42	0	4	9	0	1	4	1
20 – 25	8	1	6	0	0	1	0	9
25 – 30	11	1	5	0	0	0	0	11
30 – 35	14	9	1	Į.		1]	0	32
35 ~ 40	12	- 1	1	1		0	1	9
40 – 45	11	0	3	1	1	0		4
45 – 50	9	2	0	2		2	0	46
50 - 55	15	0	0	2		2	0	2
55 - 60 60 - 65	18	ol	0		Ì	- 1	\frac{1}{2}	1
65 ~ 70	20 0	0	,	1		- ']	\ \	0
70 – 75	Ϋ́	ŏl	1	•		'1	ň	U
75 ~ 80		ŏ	il				ň	
80 - 85	ļ	ŏĺ	ŏl	ł		}	ŏ	
85 - 90	Í	ŏ	ŏ			l	ől	
90 - 95	l	o]	ó		j		o	
95 - 100		0	0				0	

List of Borehole Water Tests (2)

				Average L	ugeon Valu			
Depth (m)	M98-9	M98-10	M98-11	M98-12	M98-13	M98-14	M98-15	M98-16
			k= 5x10 ⁻²					
į į			to 6.2x10					
			cm/sec.					
2 7	20	20		1	27	53	68	105
5 10	9	54	241	1	24	1	75	35
10 — 15	4	10	1	43	19	2	14	34
15 - 20	0	5	2	1	24	1	5	13
20 25	8	2	0	1	1	0	20	3
25 - 30	5	4	0	3	2	0	24	13
30 - 35						0	0	28
35 - 40						0	0	1
40 - 45						0	. 0	i
45 ~ 50						0 0	5 0	2
50 - 55 55 - 60						1	0	1
60 - 65						i i	0	Ö
65 - 70						il	ŏ	ő
70 - 75	ļ					ö	ŏ	Ĭ
75 - 80						ŏ	ŏ	
80 - 85		į				ŏ	ŏ	
85 - 90						0	0	
90 - 95						0	0	
95 - 100						0	o	
100 - 105					ł	0	Ì	
105 110						0		
110 115						0		
115 - 120	j					0		
120 - 125				Ì		0		j
125 - 130 130 - 135						0		
135 - 140						ő		
140 - 145]			ő		
145 - 150						ő		
150 155					1	ő		
155 - 160						ŏ		
160 - 165						ŏ	į	
165 - 170						ŏ]
170 - 175						o		
175 - 180						0		

List of Borehole Water Tests (3)

				Average Lu	ugeon Valu	6	
Depth (m)	M98-17	M98-18	M98-19	M9820	Qs-1	Qs-2	
		-		k= 2x10 ⁻²			
ļ				to 6x10 ⁻³			ļ
				cm/sec.			ĺ
2 7	74	73	40,		84	8	
5 10	22	49	9	5	68	33	
10 15	23	18	5	1	33	0	
15 ~ 20	23	4	8	12	29	2	ļ
20 – 25	25	0	214	11	3	2	Ì
25 - 30 J	6	1	14	0	36	1	
30 – 35	7	İ	129		43	3	ł
35 – 40	1		5		35	1	Í
40 - 45	0		18		32	1	
45 - 50	3 2 0		0		7	1	
50 - 55	2		0			2	
55 - 60	익		1	1			
60 - 65			0			2	
65 - 70	İ		0	ļ		2	
70 - 75 75 - 80				1		24 3	
75 - 80 80 - 85			ļ		· ·	5 5	
85 ~ 90	ļ	•				4	
90 - 95	1			1		3	
95 - 100						12	

Hole Inclination (a): Dain Axis (Right Bank, Dam Cress) Dia, of Hole: 76 m/m				
2): 0.73 ction (Lu) lue lue a {lit/min/m} 3 3 4 4 0 45 50 min/m)	n Axis (Right E	Bank, Dam Crest)	Dia, of Hole:	
(min/m)	 	90 degrees	Packer Type:	Mechanical
ction (Lu) a luc luc luc luc luc luc luc luc luc luc	ncter (pd) : 1x	(10"×0";	Date:	3/December/1998
ction (Lo.) 10 m 10		Groundwater level		0.73
	c to hole mouth		pth of test section	(Langth of section (La)
10 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)				ε
2 {	eading of flow	/ meter		ulation of Lugeon value
7. (min/m)	3 -	3		s)-Pr [kg(/cm2], q=0-/Lr {li/min/m}
	1.		·	9 91= 17.3
. 40 45 (min/m)	41,340	i		Ġ
; 40 45 (min/m)	41,475			.
; 40 45 (min/m)		-	74•	440
; 40 45 (min/m)	029 41,646	:		#.C
; 40 45 (min/m)	193 41,/32	 	2 5	
; 40 45 (min/m)	0.00	ļ	<u> </u>	Ť
; 40 45 (min/m)		:	9	
; 40 45 /min/m)				
; 40 45 /min/m)	42,168	_	∞ ∞/)°	
; 40 45 /min/m)		<u> </u>	1	
; 40 45 /min/m)		-	1 1 1 1 1 1 1	
; 40 45 /min/m)			nss	
. 40 45 /min/m) n2			. i	
; 40 45 /min/m)				\
; 40 45 /min/m) n2	3	3. 3.	_	
, 40 45 /min/m)		,		
Water Injection Ratio (q : lit_Imin/m)	3 8	3	n 0	5 20 25 30 35 40 45
(Lo+L) [kg/cm2] (2) Lugeon value: (128) Lu' (Lo+L) [kg/cm2] (2) Lu' (Lo+L) [kg/cm2] (2) Lu'			¥	ter Injection Ratio (q : lit./min/m)
(Lo+L) [kg/(cm2] n= v Lugeon value: (128) Lu' Citical Pressure: >2.2 kg/(cm2	Н			
na 12 Critical Pressure: >2.2 kgl/cm2	*(Lo+L) [kg(/cm;			(128)
		S.ft	n Critical Press	ure: >2.2 kgt/cm2
	rater should be con	ntinued for at least 10	numbles under the specified be just previous one minute	pressure, after the injection rate per minute
Injection of water should be continued for at least 10 nimutes under the specified pressure, after the injection rate per minute senter within 90 % to 110 % of the injection rate in the tist previous one minute.				

Water Pressure Test

Hole Inclination (a): 90 degrees Packer Type: Machanical	Location:	on:	Dam A	Dam Axis (Right Bank, Dam Crest)	ght Bar	ik, Dan	Crest	_	Dia. of Hole:	76	m/m	
Date Application Elemento	Hole I	nclinati	(a) no	·		8	degrees		Packer Type:	Mechanic	ja.	
Circulton EL	Frictic	on Loss	per met	(<u>A</u>	X	OX L	<u>;</u>		Date:	4/December	1998	
Price kings from pressure gauge to Depth of test section Described mouth: (La)	Ground	clevation	E		£	Ground	vater lev	Ę	N.	Gauge h	reight (La):	1
Parchole mount: (L)= 7.76 m Cil. (L)= 5 m to (L)= 10 m S m S m	P.PC.	gth from	pressure	gauge to		;	,	o tito	: 		ngth of rection	<u>3</u>
Paid Paid	borchol	e mouth;	3	7.76		Cr - (L	1		10 ([v]= 10	æ	5	£
Page Pag			Rea	ling of	flow m	refer			Calc	ulation of Lu	geon value	
Writing 10-00 10-055 12-00 12-11 12-22 12-00 12-11 12-22 12-00 12-11 12-22 12-00 12-11 12-22 12-00 12-20	Caugo P.		Pu2_	E.	Ž	P.5	9A.	Pu7	1- 1(-)-(-)1	(Constant)		استرمانها
1	THE STATE OF	1		3	1	10.00	Ī		- 10 (MAN MAN MAN MAN MAN MAN MAN MAN MAN MAN	יניאוויאפארון זיינים		TIME IN
1	E L	-	۱×	(V) 22		77 /1						
2 49,540 51,734 56,100 57,539 59,412	<u>.</u>							1				
3 49,619 51,889 56,220 58,023 59,578 59,578 59,678 59,689 59,789 50,621 58,245 59,758	1,	40 540					-	İ				
4 49,697 32,019 56,445 38,231 39,578 5 49,775 22,106 56,621 38,386 59,663 6 49,853 22,218 56,999 88,322 59,326 7 7 8 20,013 22,505 57,138 58,984 59,925 8 20,013 22,505 57,138 58,984 59,925 10 50,108 52,900 57,138 58,984 59,925 11 10 50,108 52,900 57,485 59,100 60,100 11 10 50,108 52,900 57,485 59,100 60,100 11 10 50,108 52,900 57,485 59,100 60,100 12		49,619					Ī	1				
S		40.00					Ī					
6 9 9 53 52 23 18 54,795 58,532 57,366 57,99 58,632 59,736 57 58,632 59,736 57,99 58,632 59,736 59,7	s'u	12,0			į,				2 5		1.6	
10 20,013 52,505 56,575 58,684 59,525 56,575 58,684 59,525 56,575 58,684 59,525 56,575 58,684 59,525 59,146 59,14	i	200								,	<u>.</u>	
# 50,0013 52,006 57,138 58,844 59,925	ا اه	40.03	0770						\$			
10 50,156 52,550 57,214 59,000 60,106 10 10 10 10 10 10 10	×	5003	50, 50,				1		-			
10 50,168 52,999 57,485 59,160 60,109		8008	52,750					1				
11 12 2 2 2 3 3 3 3 3 3	2	50.168	52.90									
12	_ 											
13	2		İ						_			
14	.51				ļ							
15- 0-1 0-2 0-4	7		Ī	ĺ								
Total Oct	15			: :			Ĩ				٦	
Average Qo-1 (Qo-2) (Qo-2) (Qo-3) (Qo-4) (Qo-2) (Qo-4) (Qo-2) (Qo-1) (Qo-1) (Qo-1) (Qo-1) (Qo-1) (Qo-2) (Qo	Total	3	3	3	3,	3	3	ð,			i.	
Note : Injection of water should be continued for at least 10 minutes under the specified pressure, after the mjoction rate per minute Note : Injection of water should be continued for at least 10 minutes under the specified pressure, after the mjoction rate per minute Note : Injection of water should be continued for at least 10 minutes under the specified pressure, after the mjoction rate per minute Note : Injection of water should be continued for at least 10 minutes under the specified pressure, after the mjoction rate per minute Note : Injection of water should be continued for at least 10 minutes under the specified pressure, after the mjoction rate per minute Note : Injection of water should be continued for at least 10 minutes under the specified pressure, after the mjoction rate per minute Note : Injection of water should be continued for at least 10 minutes under the specified pressure, after the mjoction rate per minute Note : Injection of water should be continued for at least 10 minutes under the specified pressure, after the mjoction rate per minute Note : Injection of water should be continued for at least 10 minutes under the specified pressure, after the mjoction rate per minute Note : Injection of water should be continued for at least 10 minutes under the specified pressure, after the mjoction rate per minute Note : Injection of water should be continued for at least 10 minutes under the specified pressure, after the mjoction rate per minutes Note : Injection of water should be continued for at least 10 minutes under the mjoction of water should be continued for at least 10 minutes under the mjoction of water should be continued for at least 10 minutes under the mjoction of water should be continued for at least 10 minutes under the mjoction of water should be continued for at least 10 minutes under the should be continued for at least 10 minutes under the should be continued for at least 10 minutes under the should be continued to the should be	≣	۶	2	5	٠,	į,	Ţ	Š				
Friction Loss (Pr) = pr (Lo + L.) [kg/cm2] Loss (Pr) = pr (Lo + L.) [kg/cm2] Loss (Pr) = pr (Lo + L.) [kg/cm2] Loss (Pr) = pr (Lo + L.) [kg/cm2] Loss (Pr) = pr (Lo + L.) [kg/cm2] Loss (Pr) = pr (Lo + L.) [kg/cm2] Loss (Loss (Lo + L.) [kg/cm2] Loss (Loss	Average lst /m.s	j š	3 9	36	3 5	3	3 3	ò	۰	55	5. 5.	Ą
Priction Loss (Pr) = pr(Lo + Lo) [kg/lcm2] Name Lageon value : (110) Laterate Friction Loss (Pr) = pr(Lo + Lo) [kg/lcm2] Name Lageon value : (110) Laterate Laterate Pressure Pr	450					12:32	Ī		•			•
]ຮ [ຊ	E					0.83	T		*	ater Injection Kal	o (q : lit/min/	Ê
: 2	Frage	1 6 1 E			2/cm2/] }		Inoron val		, m 1	
[2]]		<u> </u>	i.	5			ě	,			kg/cm2	
1	Remark	S: Al7	24 OL L5	/cm2, pr	SSurce	No Dia	Ziji.					
1 1				-								
SCHOOL WHOM WE'RE 110 WE'N THE INJECTION THE IN THE DUST PREVIOUS ONE MINNIE	Note:	Ілуестюг	of water	bluots	be contin	ucd for a	if least 1	0 minute	es under the specified	pressure, after th	e myection rate	per minute
		֓֡֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜										





Hole No.: M98-1 Location: Dam Axis (Right Bank, Dam Crest)	natio	Friction Loss per meter (pt): 1x10*x04m;	0.73 m Ground clevation : El. m Groundwater level (on (La) Pripe length from pressure gauge to (La) m Porepole mouth; (La) = 9.34 m (CL. (La) =	Reading of flow n	Guege P. Pol. Pol. Pol. Pol. Pol. Pol. Pol. P	Shart time 15:15 15:30 15:45 16:00 16:15	03(1) 3,600 000	2 98,416 99,192 454 2,298	3 98,473 99,287 583 2,448	5 98.584 99.873 713 7.001 4,180	99,575 969 2,896	99,671 1,099 3,045	99,767 1,228 3,194	20,000	6/6/5 CA+'C CDD' 6C6'KK 700'0K 17		. 12.	
3/14 76 m/m	Mechanical	8/December/1998	Gauge height (La):	(Langth of section (L)	Calculation of Lugeon value	P=P++0.1(sin(2)1.+1.1)-P* [kg//cm2], q=0-/1.0 [ii/m.n/m]		3.4 q2= 22.84 4.0 c3= 30.22	1 P S									•	1
nge: a. of Hole:	cker Type:	ite:	ž	Section (LA)= 15		Pu+0,1(sin(a)1	r.	2,5	7	χ.,	2 5		L_ ≘	ÇW	∞ >}	3 t i	ni:	10 50	\$5
Dam Axis (Right Bank, Dam Crest) Dia, of Hole:		lx10°x0'm: Date:	Groundwater tevel (Ls): Nil	Depth of (est section S CL.)= 15		PuS Pu6 Rv7 PuPu+0.1(sin(a))		81,236 82,492 P2*			81,700 82,087 81,815 82,747	82,803	82,036 82,862	82,912 m2	30,040	2 31	9 5:	3 m	!

Water Pressure Test

4/14

Dia. of Hole: Stage:

9

Friction Loss per meter (p.) :				•					4	
l and many	ž Ž	:: ই ট	- [1×10×0			Date:	17/December/1998	1,1998	
Ground elevation: EL	: EL		ε	Groundwater level ([1,4);	vater leve	3	EX	Gauge	Gauge height (La):	0.73 درس
Pipe length from pressure gauge to	pressure	ලා පුරිගේහි			ă	pth of te			ength of	Length of section (Lu)
borehole mouth: (L.)=	3	9.34 m		GL . (LL)=		14.5 m	20	£		5.5 m
	Reac	Reading of flow meter	Пож п	cter			Calc	Calculation of Lugeon value	ugeon v	pluc
Gauge P. Pol	Pu2	P.B	7.	ጉራ	Pub	Pv7				
(Agl/cms)	4	~		7	4	1	P=Po+0.1(sin(a)[+1.2)-Pr [kgt/cm2],	2)-P* [kgt/cm2		q=Q-/L [livmin/m]
Start time 15:15	15:30	15:45	16:00	16:15	16:30	16:50	12.	~		10.4
O(min) 98,290	99,000	300	200	3,060	201	6,250	2	3.9	- -	7.4
		:	14.	Ş	\$206	6.321	ž.	4		4.03
		į	2.298	8	5,312		P4#	7.2		27.1
_		i_	1,448	4.057	5,418		*	73		24.0
4 98.528		713	2.60	4.186	5.524			8		6.93
_			2746	4.320	5,639		-24			13.0
98,638		•	2,896	4.452	5,73	•	•		,	
2 98 694		. ,	3.045	4.584	5.841		٥			
8 98.750		1.22x	1			•	7			
_		_	٠.	4 847	6083		w			
ı					•	•			•	
			•) }	ł	110		ν,	
2:	ĺ	!	-		Ī		oi s	•	٠,	
	İ	1	į		İ	į	uns	<i>(</i> -		
	-	;	Ï		Ī	į	231	٦		
	!					ĺ		!		
200	5	ě	3	2	2	S	64 2;8	Ö		
<u>.</u>	ş	3,8	403	91.	9	216	 .v.			
2	ô	S	ò	0.5	Š	0]			
٠	Š	128.5	1403	9,16,6	8	71.6	0	15 20	ห ห	35 40 45 50
Finals own 15:25	15:40	15:55	16:10	16:25	16:40	17:00		Water Inication Basis /o : 1: Water	. 0/0/6	ir /min/m)
(P) 0.70	1.93	3.43	4.61	3.61	2.34	1.08	:			,
Friction Loss (Ps) = pr(Lu	7) d = (+ L.) [kgf/cm2	gf/cm2]		1	:	Lugeon value :	ue: (42)	Ē	
					MAIN'SCIT	1	Critical Pressure:			kgf/cm2
Remarks :								l		
- 1.										
Note: Injection	inn 90	r snould	5 CORT	יוסכן זפריים ביוסיקיים	n rate in	ואר יכאן נואר יכאן	injection of water should be continued for all least LV minutes under the specified pressure, after the injection rate per minute «ettles within 40 % to 110 % of the injection rate in the just previous one minute	pressure, atter	the myed	ion rate per m

0 0 8 r 0 0 4 5 5 4 10 Water Pressure in Agfem?

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.

Invected by : A. Gill

Prepared by: A. Hamid & Azhar

ô ဝ

ુ ş

Total Lie

፫

§ 4

Lugeon value:

Remarks: Due to very high loss of water, pressure did not developed beyond 7 kg//cm2.

Friction Loss (Pr) = pr(Lo + Lo) (kgl/cm2)

Hole No.:	M98-1	Stage:	5/14	-
Location:	Dam Axis (Right Bank, Dam Crest)	Dia. of Hole:	101 m/m	_
Hole Inclination (a)	tion (a): 90 degrees	Packer Type: Mechanical	Mechanical	_
Friction Los	Friction Loss per meter (pv): 1×10° ×0"":	Date:	1/January/1998	- ,

1	EL LAC	(4)			ï		Date:	1/	0000	
Friction Loss per meter (pv) . IXIV XV	į	כוכו ואי	×	ХÞ					1/January/ 1998	
Ground elevation: EL	ion : EL		E	Groundwater level (L.)	ater leve	<u>(</u>	Σij	П	Gauge height (La): 0.73	ε
Pipe length from pressure gauge to	om pressu	ire gauge 10	٠		Ā	pth of re	Depth of rest section	i	Length of section (L.)	Ī
horehole mouth: (Ls)=	<u>1</u>	9.30 m		Ct (L)-	ļ	20 m	to (La)= 25	E	5. B	Ì
	, X	Reading of flow meter	Now m	eter			ථ	Culati	Calculation of Lugeon value	
Gauge P. Pol.		3	Z	7.05	P.V	P.7				
(tref/cms)		7	2	^	4	_	P=Po+0.1(sin(a)Lr	<u>.</u>	P=Po+0.1(sin(a)Li+Lj)-Pr [kgt/cm2], q=O-/Lj [ii/min/m]	_
Start tothe 11:	11:35 11:4k	12:00	12:13	12:35	12:47	13:00		33		
O(mm) 37,970	70 38,120	38,410	38,910	39,610	40,130			6.2		
		9 38,450	38,970	39,657	4,16			0.8		
	78,167		39,028					11.4	44= 11.8	
	06 38,191	38,530	780,60	39.75	40,232			7,2	45 = 9,5	
4 38,017	117 38,213		39,146		40,266			0.0		
5 38,028		119,86 3	39,205		10,301		2	3,2	q7≈ 3.8	
,	39 38,260	159'88 09	39,265		40,335					
7 38,049	49 38,282		35,33		0,770		<u>ရ</u>	١		۳
8 38,059	59 38,305		39,386		\$ \$ \$	050	م در		1	Ö
9 38,070	70 38,328	38,771		40,037	40,43X	90.06	тэ. 20		·: \	
10 38,080	80 38,351	38,812	39,500	40,08	40,473	40,689	181		·. \	
= - = -		-	İ	i	1	1	ni Q		٥	
- 2 -	 	-	į	i			11c		·.	
: ::	-			_	-		4	'	· .	
<u> </u>	-	1					nf) 1	•	•	
Total	12	╄	Ş	3	ş	ે	7,E			_
<u>.</u>	110 231	5	96	474	143	189	c			
Average Out		-	Ö	Ŷ	ô	0-7	,			:
lk/men 11	23.1	40.2	20	47.4	78.3	18.0	0	61	3456739	2
I I was denied	11:45 11:58	12:10	12:23	12:45	12:57	13:10	-	Water I	Water Injection Ratio (q : lit/min/m)	
(P) 0.03	3 0.14	0.43	16.0	65.0	0.31	0.0				
Friction Loss (Pr) = pr(Ls + Ls) [kgUcm2	(Pr) = pr(₹ ? *	g(/cm2]		а	ż	Lugeon value:	alue:		
					\$	3	Critical Pressure	CSUTC:	7.1 kgt/cm2	ı

Water Pressure Test

Hote Inclination (a): 90 degrees Packer Type: Mechanical	Date Date	1 1 1 1 1 1 1 1 1 1	Hote Inclination (a): 90 degrees Packer Type: Mechanical		Location: I	Jam A	Dam Axis (Right Bank, Dam Crest)	cht Ban	k, Dam	Seal Seal		Dia. of Hole:	إي		101	m/m		ŀ
The page to a graph of test section and the pa	The gauge to a Groundwater level (La). Nil Gauge beight (La): 0.73 The gauge to a Groundwater level (La). Nil Gauge beight (La): 0.73 The gauge to a groundwater level (La). Nil Gauge beight (La): 0.73 The gauge to a groundwater level (La). Nil Gauge beight (La): 0.73 The gauge to a groundwater level (La). The groundwater level (La) the groundwater level (La) the groundwater level (La). The groundwater level (La) the groundwater level (La) the groundwater level (La) the groundwater level (La) the groundwater level (La). The groundwater level (La) the groundwater level (La). The groundwater level (La) the groundwater level (La) the groundwater level (La). The groundwater level (La) the groundwater level (La) the groundwater level (La) the groundwater level (La) the groundwater level (La). The groundwater level (La) the groundwat	The control of the	Friction Loss per meter (pp.): 1 1 1 1 1 1 1 1 1 1	Hole Incl.	inatio	(e) u			8	degrees		Packer Ty	ä	Σ	echanical			
Sign	B. 20 m Groundwater level (L.) Nii Gauge beight (L.) 0.73 m	B. 20 m Groundwater level (L.) Nii Gauge height (L.) 0.73 m	Depth of testing in the control (La)	Friction L	d ssor	cr mete	 สั		ф	<u>ا بر</u>		Date:		2/381	nua:7//199			
S.90 m CL(L.) = 25 m to (L.) = 30 m Length of section (L.) = 6 m to (L.) = 30 m Calculation of Lugeon value S.90 m CL(L.) = 25 m to (L.) = 30 m Calculation of Lugeon value S. 10	S.90 m CL(L.) E-ph of test section S.90 m CL-engin of section (L.)	S.90 m CL(L.) E-ph of test section S.90 m Cl(L.) S. m O(L) E-ph of test section Cl. m O(L) E-ph of test section Cl. m O(L) E-ph of test section Cl. m O(L) E-ph of test section Cl. m O(L) E-ph of test section Cl. m O(L) E-ph of test section Cl. m O(L) E-ph of test section O(L) O	Pipe length from pressure pauge to Rechold test section (La) = 8.90 m (CL(La) = 25 m to (Lb) = 30 m 5 m (SL(La) = 5 m to (Lb	Ground eter	vation	E	ľ	Г	Ground	ater leve	(<u>r</u>	Ź		-	Gauge here); } }		1 E
Pal Pal	Pal Page P	Parading of flow meter Parading of flow me	'US 	Pipe length	from 5	ressure	gauge to			1	ph of te	st section		┝	Mus.	h of sectic		1
No. Ped. P	Reading of flow meter Reading of flow meter Reading of flow meter Reading of flow meter Reading of flow meter 1	Reading of flow meter Reading of flow meter Reading of flow meter Reading of flow meter Pal	<u> </u>	borehole m	owth: (ż	8.90	F	يا. ال	i	25 m	±(₹) 01	8,	ΙE		s		
Pal	Pol	Pol. Poz.	 			Read	ing of	flow m	eter				Cate	ulation	of Luga	on value		3
11-45	11-45 11:551 12:10 12:25 12:40 12:55 12:10 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 45,100 45,20	11-45 11:551 12:10 12:25 12:40 12:55 12:10 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,100 46,8710 45,10	, 			. F.2	3,	3 c	3, 4	3 4	_	Parpose 1/ci	(a)(a)	4) *d*(*)		0.1	i/min/mi	
\$45,545 \$45,740 \$45,100 \$45,100 \$45,750 \$45,450 \$45,750 \$45,450 \$45,750 \$45,450 \$45,750 \$45,450 \$45,750 \$45,450 \$45,750 \$45,45	45,366 45,710 46,170 47,700 48,410 48,510 773 48,426 45,928 77,700 48,426 45,928 77,700 48,426 45,928 77,700 48,426 45,928 77,700 48,426 45,928 77,700 48,426 45,928 77,700 48,426 45,928 77,721 48,728 45,729 45,72	45,366 45,710 46,170 47,700 48,410 48,510 PP= 6.4 q2= 7.2 q3= 10.9	45,345 45,710 46,120 46,170 45,170 48,410 48,910 75 48,425 48,938 75 49,238 47,730 48,436 48,938 75 49,238 47,730 48,436 48,938 75 49,238 47,730 48,436 48,938 75 49,025 75 49,025 75 49,025 45,307 47,006 47,820 48,936 48,936 75,940 48,932 45,230 45,230 47,230 48,932 45,230 45	┸		35	12:10	12.0	2.5	12.55		Α.	1= 3	`•		4.7	•	
45,519 45,746 46,246 46,928 47,750 48,456 48,938 PPa 819 qpa 10.9 45,451 45,745 46,4250 46,928 47,750 48,456 48,996 45,451 45,719 46,720 48,720 48,572 49,025 45,525 45,525 46,420 47,288 48,001 48,081 48,721 49,043 45,525 45,525 46,520 47,288 48,001 48,081 49,112 45,526 45,529 46,520 47,288 48,001 48,081 48,713 49,141 45,520 46,520 46,626 47,244 48,181 48,773 49,141 45,500 46,626 47,434 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,544 48,181 48,773 49,141 45,500 46,620 47,734 47,734 48,181 48,773 49,141 45,500 46,620 47,734 47,734 48,181 48,773 49,141 45,500 46,620 47,734 47,734 48,181 48,773 49,141 45,500 46,620 47,734 47,734 48,181 48,773 49,141 45,500 46,620 47,734 47,734 48,181 48,773 49,141 45,500 46,620 47,734 47,734 48,181 48,773 49,141 45,500 46,620 47,734 47,734 48,181 48,773 49,141 45,500 46,620 47,734 47,734 48,181 48,773 49,141 45,500 46,620 47,734 47,734 48,181 48,773 49,141 45,500 46,620 47,734 47,734 48,181 48,773 49,141 45,500 46,620 47,734 47,734 48,181 48,773 49,141 45,500 46,620 47,734 48,181 48,773 49,141 45,500 46,620 47,734 48,181 48,773 49,141 45,500 46,620 47,734 48,181 48,773 49,141 45,500 46,620 47,734 48,181 48,773 49,141 45,500 46,620 47,734 48,181 48,181 45,500 46,620 47,734 48,181 48,173 49,141 45,500 46,620 47,734 47,734 48,181 48,173 49,141 45,500 46,700 47,734 47,734 48,181 48,173 49,141 45,500 46,700 47,734 47,734 48,181 48,181 48,181 45,500 47,734 47,734 48,181 48,181 48,181 48,181 48,173 49,141 45,50	45,431 45,746 46,246 46,938 47,736 48,456 48,938 PPa 83 9 43 8 10.9 45,431 45,835 46,432 47,000 47,000 47,000 48,857 49,003 45,505 45,835 46,432 47,237 47,000 48,637 47,0	45,431 45,746 46,246 46,938 47,730 48,436 48,938 PPa 819 qa 10.9 45,431 45,835 46,432 47,000 47,220 48,512 48,900 45,431 45,835 46,432 47,200 48,512 48,900 45,431 45,835 46,432 47,200 48,512 47,940 48,512 48,900 45,525 45,926 46,573 47,281 48,121 48,723 49,113 45,525 45,926 46,573 47,281 48,121 48,723 49,113 45,520 46,520 47,281 48,121 48,723 49,113 45,520 46,520 47,281 48,121 48,723 49,113 45,520 46,520 47,281 48,121 48,723 49,113 45,520 46,520 47,281 48,121 48,723 49,113 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,520 47,724 47,724 48,181 48,773 49,114 45,520 46,727 47,724 47,724 48,181 48,773 49,114 45,520 46,727 47,724 47,724 48,181 48,773 49,114 45,520 46,727 47,724 48,181 48,773 49,114 45,520 46,727 47,724 48,181 48,773 49,114 45,520 46,727 47,724 48,181 48,773 49,114 45,520 46,727 47,724 48,181 48,773 48,181 48,174 47,520 47,724 47,724 48,181 48,773 48,174 47,520 47,724 47,724 48,727 47,724 48,727 48,724 48,727 47,724 48,727 48,727 48,727 48,727 48,727 48,727 48,727 48,727 48,727 48,727 48,727 48,727 48,727 48,727 48,727 48,728 47,729 48,727 48,728 47,729 48,727 48,728 47,729 48,727 48,728 47,729 48,727 48,728 47,729 48,727 48,728 47,729 48,727 48,728 47,729 48,727 48,728 47,729 48,727 48,728 47,729 48,727 48,728 47,729 48,727 48,728 47,729 48,728		-		5,710	8.13	46,870	47 700		48,910			4	8			
45,453 45,733 45,732 45,700 47,700 47,700 48,901 Pate 113 quee 14,2 45,456 45,1819 45,735 46,460 47,720 48,501 48,507 49,034 45,501 45,202 45,203 45,203 47,204 48,771 45,000 48,503 49,033 45,502 45,503 46,504 47,724 47,724 48,713 49,141 45,500 46,003 46,003 47,724 47,724 48,713 49,141 45,500 46,003 46,003 47,724 47,724 48,713 49,141 45,500 46,003 46,003 47,724 47,724 48,713 49,141 45,500 46,003 46,003 47,724 47,724 47,724 48,713 49,141 45,500 46,003 46,003 47,724 47,	45,423 45,735 45,302 47,006 47,820 48,907 P4* 11.3 q4* 14.2 45,456 45,191 94,572 47,006 48,572 49,003 45,526 45,285 46,412 47,127 48,000 48,572 49,003 45,526 45,287 45,286 47,217 48,000 48,627 49,121 45,500 46,626 47,217 43,000 46,626 47,244 48,181 48,773 49,141 45,500 46,620 47,244 48,181 48,773 49,141 45,500 46,620 47,244 48,181 48,773 49,141 45,500 46,620 47,734 47,586 48,727 48,181 48,773 49,141 45,500 46,020 46,626 47,734 48,181 48,773 49,141 45,500 46,020 46,620 47,734 48,181 48,773 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 46,020 47,734 48,181 48,773 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,586 48,727 49,141 45,500 46,020 47,734 47,734 48,181 48,777 49,141 45,500 46,020 47,734 47,734 48,181 48,777 49,141 45,500 46,020 47,734 47,734 48,181 48,777 49,141 45,500 46,020 47,734 48,181 48,777 49,141 45,500 46,020 47,734 48,181 48,777 49,141 45,500 46,020 47,734 48,181 48,777 49,141 45,500 46,020 47,734 48,181 48,777 49,141 45,500 46,020 47,734 48,181 48,777 49,141 45,500 46,020 47,734 48,181 48,777 49,141 45,500 46,020 47,734 48,181 48,181 48,777 48,181 48,181 45,500 46,020 47,734 48,181 48,18	45,453 45,735 46,302 47,006 47,820 48,907 P4* 11.3 q4* 14.2 45,456 45,191 96,473 47,006 48,572 49,029 45,526 45,825 46,466 47,221 74,006 48,572 49,029 45,526 45,528 45,528 45,220 47,206 48,572 49,029 45,526 45,529 46,520 47,249 48,181 48,773 49,142 45,500 46,626 47,434 48,181 48,773 49,141 45,600 46,626 47,434 48,181 48,773 49,141 45,600 46,620 47,734 47,249 48,181 48,773 49,141 45,600 46,620 47,734 47,249 48,181 48,773 49,141 45,600 46,620 47,734 47,249 48,181 48,773 49,141 45,600 46,620 47,734 47,249 48,181 48,773 49,141 45,600 46,620 47,734 47,249 48,181 48,773 49,141 45,600 46,620 47,734 47,249 48,181 48,773 49,141 45,600 46,620 47,734 47,249 48,181 48,773 49,141 45,600 46,620 47,734 47,249 48,181 48,773 49,141 45,600 46,620 47,734 47,249 48,181 48,773 49,141 45,600 46,620 47,734 47,734 48,181 48,773 49,141 45,600 47,734 47,734 48,181 48,773 49,142 45,600 47,734 47,734 48,181 48,18			419	45,746			47,750					٠,	8			
45,486 45,319 46,319 47,127 47,281 48,280 48,286 48,290 P5= 8.7 q5= 12.0 45,528 45,228 45,228 45,228 48,039 48,537 49,025 45,528 45,292 45,228 48,280 48,039 49,033 45,528 45,292 45,282 47,391 48,181 48,773 49,141 45,500 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 42,242 48,181 48,773 49,141 45,600 46,039 46,628 47,34 47,240 48,181 48,773 49,141 45,600 46,039 46,628 47,34 47,240 48,181 48,773 49,141 45,600 46,039 46,628 47,34 47,240 48,181 48,773 49,141 45,600 46,039 46,628 47,34 47,181 48,773 49,141 45,600 46,039 46,628 47,34 47,181 48,773 49,141 45,600 46,039 46,628 47,34 47,181 48,773 49,141 45,600 46,039 46,628 47,34 47,181 48,181 48,773 49,141 45,600 46,039 46,628 47,34 47,181 48,181 48,773 49,141 45,600 46,039 46,628 47,34 47,181 48,	45,486 45,315 46,315 47,127 47,248 48,296 48,296 45,284 45,285 46,412 47,287 47,287 47,287 49,025 45,528 45,228 46,529 47,281 48,289 49,033 45,528 45,228 46,529 47,281 48,789 49,039 45,528 45,298 46,529 47,281 48,789 49,039 45,528 47,249 48,789 49,112 48,789 49,112 48,789 49,112 48,789 49,113 49,789 49,113 49,789 49,113 49,789 49,113 49,789 49,113 49,789 49,113 49,789 49,113 49,789 49,113 49,789 49,113 49,789 49,113 49,789 49,113 49,789 49,113 49,789 49,113 49,789 49,113 49,789 49,789 49,113 49,789 49	45,486 45,831 46,332 47,376 47,880 48,596 48,596 45,832 46,523 46,423 47,137 47,940 48,596 45,832 46,523 46,423 47,137 47,940 48,596 46,520 45,232 46,523 47,243 48,089 49,083 45,524 45,524 46,523 47,243 48,181 48,789 49,112 48,789 49,112 48,789 49,113 48,789 49	8 6 5 8	-		45,783	46,302		47,820	48,501		Ω.		<u>.</u>	8			
45,505 46,412 47,287 47,940 48,577 49,003 48,003 49,003 45	45,505 46,412 47,157 47,940 48,577 49,003 40,003 40,003 40,003 40,003 45,502 46,503 47,203 46,606 47,203 46,606 47,203 46,606 47,203 46,602 47,203 46,502 47,203 46,502 47,203 46,502 47,203 46,573 47,203 46,502 47,203 46,502 47,203 46,502 47,203 46,502 47,203 46,502 47,203 47	45,505 46,412 47,157 47,940 48,577 49,003 46,64 47,217 47,940 48,577 49,003 46,657 47,240 48,577 49,003 46,658 47,217 48,003 46,658 47,217 48,003 46,628 47,217 48,003 46,628 47,241 48,778 49,112 48,112 48,	8 8 8 8	:		45,819			47,880	45.546 0.454		اتم		ا جا	3 .			
45,525 45,825 46,456 47,218 48,000 48,007 49,003 49,003 49,003 45,522 45,954 45,220 45	45,520; 45,822 46,450 47,217 43,000 48,027 49,034 45,228 45,229 46,520 47,288 48,001 48,039 49,113 10 45,522 45,924 46,520 47,288 48,121 48,723 49,114 10 45,522 45,924 46,520 46,620 47,289 48,222 48,818 48,713 49,141 10 48,914	45,520; 45,822 46,450 47,217 43,000 48,027 49,034 45,522 45,524 45,522 45,524 45,522 45,524 45,522 45,524 45,523 45,121 43,000 46,525 45,524 45,724 43,181 43,773 49,141 45,500 46,529 45,729 45,220 45,229 45,220 45,229 45,220 45,229 4	8 6 5 8	-		45,855			8,7	8. 		α.		Ŋ	ģ			
45,528, 45,528, 45,520 47,288 48,061 48,088 99,083 45,522 45,524 46,527 47,261 48,121 48,728 99,112 45,500 46,029 46,622 47,734 47,280 48,242 48,181 48,113 45,600 46,029 46,622 47,734 47,280 48,242 48,181 48,113 45,600 46,029 46,622 47,734 47,280 48,242 48,181 48,113 45,600 46,029 46,622 47,734 47,280 48,242 48,181 48,113 45,600 46,029 46,622 47,734 47,280 48,242 49,200 45,600 46,029 46,622 47,734 47,280 48,242 49,200 45,600 46,029 46,622 47,734 47,280 48,242 49,200 45,600 46,029 46,622 47,734 47,280 48,242 49,200 45,600 46,029 46,622 47,734 47,280 48,242 49,200 45,600 46,029 46,622 47,734 47,280 48,242 49,200 45,600 46,029 46,622 47,734 47,280 48,242 49,200 45,600 46,029 46,024 47,734 47,280 48,242 49,200 46,600 46,029 46,024 47,734 47,280 48,242 49,200 45,600 46,029 46,024 47,734 47,280 48,242 49,200 46,600 46,029 47,734 47,280 48,242 49,200 46,600 46,029 47,734 47,280 48,242 49,200 46,600 46,029 47,734 47,280 48,242 49,200 46,600 46,029 46,020 47,734 47,280 48,242 49,240 48,242 49,240 48,242 49,242	45,528 45,928 45,928 45,021 43,088 49,083 45,529 45,529 47,288 48,001 48,088 49,083 45,520 46,020 46,026 47,524 48,181 48,718 49,112 45,500 46,020 46,026 47,544 48,181 48,718 49,141 45,500 46,020 46,026 47,544 48,181 48,718 49,141 45,500 46,020 46,020 47,544 48,181 48,718 49,141 45,500 46,020 46,020 47,544 48,181 48,718 49,141 45,500 46,020 46,020 48,242 48,181 48,718 49,141 45,500 46,020 46,020 48,242 48,181 48,718 49,141 45,500 46,020 46,020 48,181 48,718 49,141 45,500 46,020 46,020 48,181 48,718 49,141 45,500 46,020 46,020 48,181 48,718 49,141 45,500 46,020 46,020 48,020 48,181 48,718 49,141 45,500 46,020 46,020 48,020 48,181 48,718 49,141 45,500 46,020 46,020 48	45,528 45,928 45,928 47,928 48,001 48,089 49,083 45,529 45,289 45,280 48,181 48,789 49,112 45,500 46,029 46,626 47,541 48,181 48,718 49,141 45,600 46,029 46,626 47,544 48,181 48,718 49,141 45,600 46,029 46,626 47,544 48,181 48,718 49,141 45,600 46,029 46,626 47,544 48,181 48,718 49,141 45,600 46,029 46,626 47,546 48,242 48,181 48,718 49,141 45,600 46,029 46,626 47,546 48,242 48,181 48,718 49,141 45,600 46,029 46,626 47,546 48,242 48,181 48,718 49,141 45,600 46,029 46,626 47,546 48,181 48,718 49,141 45,600 46,029 46,626 47,546 48,181 48,718 49,141 45,600 46,029 46,626 47,546 48,181 48,718 49,141 45,600 46,029 46,626 48,181 48,718 49,141 45,600 46,020 46,020 47,744 47,140 46,02 46,020 45,600 46,020 47,744 47,140 46,02 46,020 45,600 46,020 46,020 47,744 47,140 46,02 46,020 45,600 46,020 46,020 47,141 41,041 45,600 46,020 46,020 47,141 41,041 45,600 46,020 46,020 47,141 41,041 45,600 46,020 47,744 47,140 46,02 46,020 45,600 46,020 46,020 47,141 41,041 45,600 46,020 46,020 47,141 41,041 45,600 46,020 47,744 47,141 41,041 45,600 46,020 47,744 47,141 47,041 45,600 46,020 47,744 47,141 47,041 45,600 46,020 47,744 47,141 47,041 45,600 46,020 47,744 47,141 47,041 45,600 46,020 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,141 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041 45,600 47,744 47,041	<u> </u>			45,892			8,00	48,637	49,054	Δ.		٠,	- P			
\$5552 45,904 46,573 47,344 48,181 48,773 49,112 75,500 46,020 46,	5,555 (45,964 46,573 47,346 48,121 48,773 49,112 75,576 49,112 75,576 46,000 46,025 47,244 48,181 48,773 47,244 48,181 48,773 47,244 48,181 48,773 47,244 48,181 48,773 47,244 48,181 48,773 47,244 48,181 48,773 47,244 47,244 48,181 48,773 47,24 48,773 47,24 48,773 47,24	5,555 (45,964 46,573 47,346 48,121 48,773 49,112 75,000 46,020 47,346 48,118 48,773 47,346 48,118 48,773 47,346 48,118 48,773 47,346 48,118 48,773 47,346 48,118 48,773 47,346 48,118 48,773 48,564 48,723 48,564 48,723 48,564 48,723 48,564 48,723 48,564 48,723 48,564 48,723 48	7 45,552 45,964 46,573 47,361 48,121 48,773 49,112 10 49,112 10 45,570 46,620 46,620 46,620 47,540 48,181 48,773 49,141 49,770 49,141 4			45,928			48 06	48,688								
5,576 46,000 46,626 47,434 44,181 48,777 49,141 55,500 46,000 46,626 47,204 44,181 48,777 49,141 55,500 46,000 46,628 47,206 48,202 48,818 49,170 15 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5,576 46,000 46,626 47,434 48,181 48,777 49,144 52,500 46,620 47,434 48,181 48,777 49,144 52,500 46,632 47,500 46,632 47,500 48,500 46,632 47,500 48,	5,576 46,000 46,626 47,343 48,181 48,777 48,144 55 500 46,600 46,626 47,340 48,181 48,777 48,144 55 500 46,000 46,620 47,340 48,202 48,818 49,710 55 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	S 45,776 46,000			45,964			48,121	48,728		2		ļ				•
5,500 46,503 46,582 43,750 48,232 48,818 49,170 57 8 7 7 10 46,734 49,818 49,170 57 8 7 7 10 46,734 47,590 48,320 48,864 49,200 51 8 7 7 10 40 40,20 5 50 50 50 50 50 50 50 50 50 50 50 50	5,600 46,039 46,632 47,506 48,242 48,818 49,170 55 8 7 7 6 6 6 7 7 6 47,724 42,818 49,170 55 8 7 7 6 7 7 6 47,724 42,818 49,170 55 8 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	5,600 46,039 46,632 47,510 48,736 49,170 55 8 7 7 5 6 46,734 49,110 55 8 7 7 5 6 46,734 49,110 55 8 7 7 5 6 46,734 49,110 55 8 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	9 45,600 46,635) 47,556 48,242, 48,818 49,170 51 8 8 10 45,622 46,632 47,556 45,242 48,818 49,170 51 8 8 11	i ,		96,000			48.181	8,77		Z						
5 (507) 46,774 (47.754) 45,7540 43,007 (48.864) 49,200 126 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5 (200 46,077) 46,774 5724 57250 43,907 43,907 43,900 25 7 7 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	5 (gizz 46,072) 46,754 5/1540 49,202 48,864 49,202 46, 69,202 46, 69,202 46, 69,202 46, 69,202 46, 69,202 46, 69,202 46, 69,202 47,00 40,202 48, 602 49,202 48, 602 49,202	10 45,622 46,724 47,744 47,7540 43,002 48,864 49,200 26 7 10 10 10 10 10 10 10	_		46,039			48,24.	48,818		113,		`.				
1.50 1.20	Color Colo	Color Colo	13			5,07	4.7.4	ر ار	\$ 	28.85 29.			_	:				
1. 1. 1. 1. 1. 1. 1. 1.		Col. Col. Col. Col. Col. Col. Col. Col.	13	= :	İ		1	1	Ī	-	İ	gi ©	_	9 .				
Color Colo	Col. 1 Col. 2 Col. 3 Co	Coll Coll Coll Coll Coll Coll Coll Coll	Total 25-7 30.2 50.4 71.0 60.2 60.2 70.0 70.4 11.5 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0	12	 	!		-	Ī	Ī	Ĭ	911) 545	·-					
Cal Cal Cal Cal Cal Cal Cal Cal Cal Cal	Cal Cal Cal Cal Cal Cal Cal Cal Cal Cal	Cal Cal Cal Cal Cal Cal Cal Cal Cal Cal	10 Cal		i		Ì	1	Ī	1		223						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.1 O.2 O.3 O.4 O.5 O.4 O.5 O.7 O.4 O.7 O.7 O.7 O.7 O.7 O.7 O.7 O.7 O.7 O.7	Col. Col. Col. Col. Col. Col. Col. Col.	Total Co.1 Co.2 Co.3 Co.4 Co.5 Co.5 Co.5 Co.5 Co.5 Co.5 Co.5 Co.5	1.14	i	!	į		Ī		1	u	}					
237 362 544 710 602 454 250 0 1 15 20 25 30 35 40 45 25.7 36.2 544 71.0 60.2 36.3 12.00 17.0 12.00 17.0 12.00 17.0 12.00 17.0 17.0 17.0 17.0 17.0 17.0 17.0 1	237 : 362 544 710 602 454 720 $\frac{2}{10}$ $\frac{1}{10}$ 237 : 362 544 710 602 454 720 $\frac{2}{10}$ $\frac{1}{10}$ 11 127	╀	1	í	7	1	Т	2	3									
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.1. 02. 03. 04. 05. 05. 06. 07. 0.0. 07. 0.0. 0.0. 07. 0.0. 07. 0.0. 0.0	0-1	Number Out O	:	4	362	3	5	-	Å	8							
23.7 36.2 54.4 71.0 60.2 45.4 29.0 0 5 10 15 20 25 30 35 40 45 11:55 12.08 12.20 12.35 12.50 13.05 0.26 11:55 12.08 12.20 12.35 12.50 12.30 12.30 3.1 1.09 0.20 1.51 1.09 0.0.3 0.26 3.2	23.7 36.2 54.4 71.0 60.2 45.4 29.0 0 5 10 15 20 25 30 35 40 45 11.55 12.08 12.25 12.35 12.59 13.20 Water Injection Ratio (q : Ili_min/m) 30.17 0.40 0.50 1.51 1.09 0.53 0.25 Sas (Ps) = pr(La + L.) [kg/tcm2]	23.7 36.2 54.4 71.0 60.2 45.4 29.0 0 5 10 15 20 25 30 35 40 45 11.55 12.08 12.20 12.35 12.59 13.20 Water Injection Ratio (q : Il_min/m) 30.17 0.40 0.50 1.51 1.09 0.63 0.26 30.08 (Pr) = pr(La + L.) [kg/tcm2]	Number 13.5 13.08 12.20 12.35 12.50 13.5	Ļ.	į	Ö		,	ે	ŝ	6	•				l	l	1
11-55 12-08 12-20 12-35 12-50 13-00 13-20 13-	11-55 12-08 12-20 12-35 12-35 13-30 0.17 0.40 0.50 1.51 1.09 0.63 0.26 0.8 Pr Lo + Lo [kg/cm2] Lugeon v Critical Pr	11-55 12-08 12-20 12-35 12-35 13-30 0.17 0.40 0.50 1.51 1.09 0.63 0.26 0.8 Pr = Pr (Lo + Lo) [kg/cm2]	11:55 12:98 12:39 12:39 12:39 12:39 13:39 13:39 Water Injection Ratio (q : liu/min/m)	`	3.7	33.2			50.2	45.4	29.0	_	n		8 8	ĸ	ħ	8
0.17 0.40 0.90 1.51 1.09 0.63 0.26 3xs (Pt) = pr(Lo + L.) [kg/cm2]	0.17 0.40 0.90 1.51 1.09 0.63 0.26 See (Pe) = Pe(Le + Le) [kg/cm2] See Critical Pe	0.17 0.40 0.90 1.51 1.09 0.63 0.26 338 (Pt) = Pt (Lo + Lo) [kg/tcm2]	Friction Loss (Ps) = pr(Ls + Ls) [kg/lcm2]	Ļ	\$3.1	5	•	12.35	12:50				3	Acer for	Choo Resid	(o - lit./m	(w/c)	
ons (Ps) = pr(Ls + Ls) [kg/cm2]	ons (Ps) = pr(Lo + Lo) [kg/cm2]	ons (Ps) = pr(Lo + Lo) [kg/cm2]	Friction Loss (Pr) = pr(Lu + Lu) [kg/lcm2] us us Critical Pressure: (3.1) Lui Remarks: Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minutes.	H	71.0	0.40	060	1,51	8		0.26						`	
v - Critical Pressure: 6.4	v - Critical Pressure: 6.4	v - Critical Pressure: 6.4	Remarks: Kemarks: Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minutes.	Friction Lo	SS (P.)	* P.(L	5	st/cm2]		44			con va	 20	33	3		
			Kemarks: Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minu							2			tion! Pre	33mVc:	6.4	kgC/cm2		
				Kemarks:														1

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.

[Prepared by: A. Humid]

Hole No.:	M98-1	Stage:	7/14	웊
Location:	Dam Axis (Right Bank, Dam Crest)	Dia. of Hole:	101 m/m	ሷ
Hole Inclination (a)	tion (a): 90 degrees	Packer Type: Mechanical	Mechanical	£
Friction Loss	Friction Loss per meter (p): 1x10 x0 x0 x1;	Date:	3/January/1998	Ë
				l

CL - (L) = 30 m to (L) = 35 m	Color Colo	چ چ	Ground elevation; EL.	13		E	Groundwater level (L.):	vater leve	$\frac{2}{3}$	Z	Gauge beight (La): 0.73 m
7.50 m Ci(L) = 30 m to (L) = 35 m 5 m 5 m	7.50 m CL(L)= 30 m ading of flow meter N-3 10 m ading of f	딅	id woj	Tall Se	gauge to			Å	o the	:	
Pay Pad	Pay Pad	Ě	1) He	4	7.50	=	CL - (L	-	30	35	5
PA1. PG2 PG3 PG4 PG5 PG5	Pal. Pal.			Read	ing of	flow m	eter			Calculati	on of Lugeon value
1	12:30 12:43 12:55 13:00 13:31 13:45 14.45 15:45 13:45	_		P.2	3		3	3	Pu7		
12:30 12:45 13:45 13:46 13:25 13:48 13:25 13:48 13:45 13:4	12:30 12:45 12:55 13:08 13:30 13:45 13:45 12:49 14:40 12:40 12:55 13:08 13:45 13:45 12:40 12:4			4	7		,	4	-	P=Pu+0.1(sin(a)ಓ+ಓ)-P»	[kgf/cm2], q=Q=/Lu [lit/min/m]
50,990 57,900 58,610 P2= 67 q2= 8.5 50,990 57,900 58,640 P3= 91. q3= 12.3 57,000 58,100 58,727 P4= 10.4 qq= 18.8 P5= 17.1 P4= 18.8 P7= 18.8 P4= 18.8 P5= 17.1 P4= 18.8 P7= 18.8 P5= 17.1 P4= 18.8 P5= 17.1 P4= 18.8 P5= 17.1 P4= 18.8 P5= 17.1 P4= 18.8 P5= 17.1 P4= 18.8 P5= 17.1 P5= 17.1 P4= 18.8 P5= 17.1 P5=	A	L	2:30	12-43	12:55	13-0x	13:20		13:45		
57,004 57,966 58,644 P2= 9.1 q3= 12.3 57,004 57,966 58,648 P4= 10.4 q4= 18.8 57,7120 58,032 53,667 P6= 5.8 q6= 17.1 57,705 58,1467 58,767 P6= 5.8 q6= 17.1 57,705 58,1467 58,767 P6= 5.8 q6= 17.1 57,705 58,1467 58,707 P6= 5.8 q6= 17.5 57,704 58,307 58,906 P2= 9 P7= 1.8 q7= 7.9 57,704 58,577 58,907 P6= 5.8 q6= 17.5 57,704 58,577 58,907 P6= 5.8 q6= 17.5 57,704 58,577 58,907 P6= 5.8 q6= 17.5 57,704 58,577 58,907 P6= 5.8 q6= 17.5 57,704 58,577 58,907 P6= 5.8 q6= 17.5 57,704 58,577 P6= 5.8 q6= 17.5 57,704 58,577 P6= 5.8 q6= 17.5 57,704 58,577 P6= 5.8 q6= 17.5 57,704 58,577 P6= 5.8 q6= 17.5 57,704 58,577 P6= 5.8 q6= 17.5 57,704 58,907 P6= 5.8 q6= 17.5 57,704 58,907 P6= 5.8 q6= 17.5 57,704 58,577 P6= 5.8 q6= 17.5 57,704 58,577 P6= 5.8 q6= 17.5 57,704 58,577 P6= 5.8 q6= 17.5 57,704 58,577 P6= 5.8 P6= 5.8 57,704 58,577 P6= 5.8 57,704 58,577 P6= 5.8 57,704 58,577 P6= 5.8 57,704 58,577 P6= 5.8 57,704 58,577 P6= 5.8 57,704 P6= 5.8 57,704 P6= 5.8 57,704 P6= 5.8 57,704 P6= 5.8 57,704 P6= 5.8 57,704 P6= 5.8 57,704 P6= 5.8 58,704 P6=	H4454 59,703 55,281 56,001 57,004 57,966 58,644 P5-44,497 54,746 55,474 56,177 57,120 58,003 28,668 P5-44,499 53,474 55,474 55,474 57,120 58,100 28,100 P5-44,499 53,474 55,474 56,177 57,120 58,100 S3,777 P5-44,532 54,002 56,170 57,290 58,100 58,100 P7-45,52 54,002 56,280 57,290 58,100 58,407 58,807 P7-45,52 54,017 55,546 56,280 57,290 58,290 58,290 58,490 5		_	_	55,220	55,950			58,610		
57,120 58,032 38,688 P4= 10.4 q4= 18.8 57,205 58,105 53,777 P6= 5.8 q6= 17.1 57,205 58,105 53,777 P6= 5.8 q6= 17.1 57,205 58,205 58,807 P7= 3.8 q7= 7.9 57,7448 58,305 58,807 P7= 3.8 q7= 7.9 57,7448 58,305 58,807 P7= 3.8 q7= 7.9 57,7448 58,305 58,807 P7= 3.8 q7= 7.9 57,751 58,507 58,906 P7= 2.8 P7= 2.8 57,751 58,507 58,906 P7= 2.8 57,751 58,507 P7= 2.8 58,752 P7= 2.8 58,753 P7= 2.8 58,755 P7= 2.8 5	H,477 54,746 55,342 56,117 57,120 58,032 58,688 P4= H,479 54,746 55,342 56,117 57,120 58,032 58,688 P4= H,450 54,748 55,478 55,428 57,205 58,100 58,777 P6= H,520 54,978 55,485 56,280 57,290 58,167 58,777 P7= H,522 54,917 55,546 56,487 57,488 58,300 58,487 H,522 54,917 55,548 56,487 57,748 58,300 58,487 H,523 54,917 55,548 56,487 57,748 58,497 H,524 56,491 55,747 56,747 57,771 58,597 58,966 H,677 55,045 55,771 56,747 57,771 58,297 58,966 H,677 55,045 55,771 56,747 57,771 58,297 58,966 H,677 55,045 55,771 56,747 57,771 58,297 58,966 H,678 56,890 57,814 58,475 59,005 H,524 0,22 0,24 0,24 0,25 0,24 0,27 0,27 0,27 0,27 0,27 0,27 0,27 0,27				55,281						
57,205 58,100 53,727 75	HA 499 59,778 55,400 50,207 57,205 58,100 53,777 PG= 14,514 54,402 55,220 57,205 58,107 58,777 PG= 14,522 54,022 55,230 57,203 58,107 58,207 PP= 14,522 54,027 55,240 57,556 58,207 58,407 PP= 14,527 54,027 56,487 57,744 58,407 58,806 PP= 14,527 55,007 55,404 58,407 58,404 58,407 58,806 15,507 55,007 56,808 57,814 58,507 58,906 FP= 16,507 55,007 55,807 57,814 58,777 59,707 58,906 FP= 18,507 55,007 55,007 55,806 57,814 58,777 59,007 FP= 18,507 55,007 56,806 57,814 58,777 59,007 FP= 18,507 55,007 55,007 55,007 55,007	_			55,342		57,120				
57,250 58,167 58,767 Pcs 5.8 qcs 13.5 57,250 58,235 58,807 Prz 3.8 qcs 13.5 57,548 58,370 58,886 Fr 9 Fr	10	<u>x</u>			55,404		57,205				
57,280 58,235 58,807 5	H4533 54,877 55,572 56,390 57,340 58,223 58,807 P7- H4522 54,947 55,574 56,487 57,468 58,370 58,887 H4528 55,000 55,710 56,685 57,7644 58,439 58,926 H458 55,000 55,710 56,685 57,7644 58,439 58,926 H458 55,000 55,710 56,685 57,764 58,439 58,926 H458 55,000 55,710 56,685 57,764 58,439 58,926 H458 55,000 55,710 56,685 57,764 58,439 58,926 H458 55,000 55,710 56,685 57,764 58,439 58,926 H458 56,710 56,780 57,771 56,7	Ÿ			55.465	56,298					
57,448 58,303 58,847 57,548 58,370 58,886 57,548 58,370 58,806 57,771 58,507 58,906 57,771 58,507 59,005 57,771 58,507 59,005 57,814 58,575 59,005 58,575 59,005 58,575 59,005 58,575 59,005 58,575 59,005 58,575 59,005 58,575 59,005 58,575 59,005 58,575 59,005 58,575 5	H. 552 54.917 55.587 56.487 57,464 58.303 58.947 H. 570 44,677 55.045 57,705 58,705 58,806 H. 607 55.045 55,710 56,828 57,764 58.479 58,806 H. 607 55.045 55,771 56,787 57,731 58,907 58,906 H. 607 55.045 55,771 56,787 57,731 58,907 58,906 H. 602 55,087 55,833 56,830 57,814 58,573 59,003 H. 603 604 605 605 604 605 604 605 605 604 605 605 605 605 605 605 605 605 605 605	-			55.526	56.390		58,235			
57,556 58,370 58,886 10 10 10 10 10 10 10 1	4,570 54,954 55,548 56,585 57,556 58,370 58,886 10 4,528 55,000 55,710 56,685 57,644 58,549 58,370 58,886 10 56,685 57,644 58,549 58,370 58,986 10 56,685 57,644 58,570 58,900 57,710 56,685 57,644 58,577 57,710 56,777 57,710 58,577 58,200 58,710 58,577 58,200 58,710 58,577 58,200 58,710 58,577 58,700 58,571 58				55,587	56,487		58,303	58,847		
57,644 58,439 58,926 Fig. 8 Fig. 9 F	4,588 55,000 55,710 56,685 57,644 58,439 58,926 m2 9 4,607 55,045 55,771 56,777 57,771 58,507 58,906 m2 9 4,625 55,045 55,771 56,777 57,771 58,507 58,906 m2 9 4,625 55,047 55,771 56,800 57,814 58,577 59,005 m2 9 4,625 50,047 55,800 57,814 58,577 59,005 m2 9 4,627 50,800 57,814 58,577 59,005 m2 9 4,627 50,800 m2 9 4,6	_	500		55,648			58,370		9	
57,731 58,507 58,966 52,07 59,005 52,534 59,005 59	44,607 55,045 55,771 56,787 57,721 58,596 58,966 46,621 55,087 55,087 55,087 55,087 57,721 58,577 59,005 57,81 58,577 59,005 57,81 58,577 59,005 57,81 58,577 59,005 57,81 58,577 59,005 57,81 5	X	<u>88</u>		55,710		57,644			21	-
57814 58,575 59,005 24 7	Color Colo	Y			55.771		57,72		58,966	- œ	• 6
Color Colo	Col. Col.				55,803	26,890				184	
Control Cont	Control Cont	1	 		Ī			1		in 6.	-
Cost Cost	Out Que Constitution Constitution	1	<u> </u>	<u> </u>	-	-	-		į	216	
Co-5 Co-6 Co-7	Out Out Out Out Out Out Out Out Out Out	1	<u>.</u> i	!	1		-	:		223 A	
Out Out	Out Out Out Out Out Out Out Out Out Out	•	-	i	-		:	!	!	M 1	
RS4 675 395 0 0 1 2 2 2 30 35 40 45	185 427 613 940 854 675 395 7 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 5 0 1 0 0 1	۲	Н	2	3		1	3	0	c4 -	
Qu-5 Qu-6 Qu-7	Out Out Out Out Out Out Out Out Out Out	_	-	ţ,	613		_	675	305	- ·	
		L	⊢	2.4	3		3,	វូ	0-7	ł	
13:30 13:43 13:55	12:40 12:53 13:05 13:18 13:50 13:43 13:55 0.12 0.61 1.25 2.91 2.41 1.52 0.53 0.06 (P) = pr(Lo + Lo) [kgt/cm2] 11 1.52 0.53 0.1 11 1.52 0.53 0.1 1.52 0.53	_	-	12.7	61.3		85.4	67.5	39.5	2	20 25 30 35 40 45
2.41 1.57 0.53 Lugeon v	0.12 0.61 1.25 2.91 2.41 1.57 0.53 oss (Ps) = ps(Lo+Lo) kgt/cm2 11			12-53	13:05	13-1X	13:30	13:43	13.55	Water It	lection Ratio (o : lit./min/m)
Lugeon value: (14)	oss (Ps) = pv(Lo+Lo) [kg/lcm2] 11 14 Cnical Pressure: 9.1	٥	7	197	1.25	2.91	2.41	1.57	0.53		(m.) h) on m. (m.)
•• Critical Pressure: 9.1	or or Critical Pressure: 9.1	3	* (Pr) =	ۼ	* (J.	(f/cm2)		-	:	Lugeon value:	
	מי							Ē		Critical Pressure:	

Note: Insection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute senter within 90 % to 110 % of the injection rate in the just previous one minute.

[Prepared by: A. Humid & Azhor

Water Pressure Test

Location	ä	Dam Axis (Right Bank, Dum Crest)	xis (Riy	zht Ban	k, Dun	Crest		Dia, of Hole:	101	m/m	
Hole I	Hole Inclination (a):	(e) u.	•		8	90 degrees		Packer Type:	Mechanical		
Frictio	1.0SS	Friction Loss per meter (p.) :	3. 3.	1	1×! (f*×C+*)!	ä		Date:	4/January/1999	8	
Ground	Ground elevation: EL	13		E	Groundwater level (L.)	aler 'cw	3	NI	Gauge height (La):	(L.):	0.73
Pipe len	gth from	Pipe length from pressure gauge to	gauge lo	-		Δ	cpth of te	Depth of test section	guar ₁	Length of section (L.)	3
borehok	borehole mouth: (L.)=	(1)	7.50 m		CL . (L)=		35 m	m ro (L₄)= 40	ε	. 5	: £
		Read	ing of	Reading of flow meter	eter			Calcu	Calculation of Lugeon value	on value	
Gauge P.	Po! 1	-Pa2.	. P.	3.0	. <u>P</u> .€	P.0	Po7	P=Po+0.3(sin(a)L+La)-Pe [kg/km2]. O=O=.La [ii/min/m])-Pelket/cm2).	omOmOL s like	/min/ml
E P	2500	12:12	12:25	×	12:50	13:03	13:15		#10	6,7	
O(min)	10	េ	67.100	67.800	08.630	P	69 830				
,			67.158	67.875	68 691			2			
.7	66,350		67.217	67,951	68,752	69,418		P4=			
	66,375		67,275	68,027	68,813	69,463	69,905	PS= 9.4		•	
. 4	66,398		67,334	68.103	68.874	69,507		-5 <u>4</u>			
	66.423		67.392	68179	68.930	69.551		2		5.0	
.9	66.448		67,450	68255	68.997	69,595					
7	66.472		67.508	68,331	69,058	69,639		٤			
	66,497	97,000	67.567	68,409		69,683		7	€.		
6	66,520	796.98	67,625	88		69,727	70,057	_	•		
2	66,545	67,008	67,683	195'89	69 242	69,772	70,082	731			
≓ ;			-	Ì		İ		ni S			
77		1						31			
2	j						ļ	• s			
7		i					į	al j			
1.5								, tr 1			
Total	6	5	3	ò	3	Š	6				
Ξ	245	408	583	761	612	44.	252	 d		•	
Average		2-0	0-3	40	5-0	Š	0-7			ł	ł
MUMM	24.5	40.8	58.3	76.1	61.2	44.2	25.2	- -	22 23 23 23	S S	\$ \$ S
Final time	04:31	12.22	12-35	12.48	13:00	13:13	13:25	3	Water Initial Date of the Contractor		í
(A)	62.0	0.64	1.29	2.18	1 42	0.75	0.25				2
Friction	Pr (Pr	Friction Loss (Pr) = pr (Lo + Lo) [kgf/cm2]	3	f/cm2]		CII	•	Lugeon value :	le: 12	17.5	
	•		•			?	- 1	Critical Pressure:	-	kot/cm2	
Remarks :	ا		l		ŀ						
1			1	1	10		- F	Transferred of section 8 world has solved for a level () secultar trades the second of averages after the second of	200		
	*	thin 90	017019	10%	inicolio	n rate in	Je in	injection of water product of commodates in the initial of the investment of the previous one minute	Actoric, and the	mjernom tak	

	Hole No.:	ا پر		M98-1				_	Stage:		9/14		Hole No.:	ا يو:	2	M98-1	
	Location:		Oam A:	ris (Ri	ght Bar	Dam Axis (Right Bank, Dam Crest)	Crest	_	Dia. of Hole:	ا	101 m/m		Location:	•	Dam Axis (Right B	is (Rig	
	Hole Inclination (a):	clinatio	(a)	•		8	90 degrees	_	Packer Type:	ij	Mechanical		Hole I	Hole Inclination (a):	n (a):	ı	
	Friction Loss per meter (pv):	3 889	er met	ã ħ		1×10'×0''''	:		Date:	5/	5/January/1999		Frictio	Friction Loss per meter (P.) :	er meter	ا ق	٦
	Ground elevation: EL.	evation	림		E	Cround	Groundwater level (14)	(<u>3</u>	N.1		Gauge height (L):); 0.73 в	Cround	Ground elevation: EL	E.	E	ا۔ا
	Pipe length from pressure gauge to	E Gal	pressure	gauge to			۵	epth of t	Depth of test section		Length of section (L.)	ction (Lu)	Pipe Kr	Pipe length from pressure gauge to	ressure g	auge to	
	borchole mouth: (Le)=	mouth:	3	7.50 m		GL - (L)=		F 유	10 ([v]=	45 n	S	£	borehol	borehole mouth: (Ls)=	ا	7.50 m	
			Read	ing of	Reading of flow meter	leter				Calculat	Calculation of Lugeon value	lue			Readi	Reading of flow	ð
	Campon P.	3	5.4	3 '	1 2	3, ~	94. 4	7 4	P=Po+0,1(sin(*4-(**)***](e)	P=Po+0.1(sin(a)L+L2)-P* [kgf/cm2], q=O-/L2 [liVmin/m]	[liVmin/m]	Cauge P, (kg/cm)	1e -	P ₁₂	5,7	3.2
	of Land	01:61	13:25	13:40	100	14:10	14:25			5.1	q1= 4.3		Shart time	15:00	15:12	15:25	3
	-			10,050			~ .				42a 7.6	90	(mm)	13,540	13,965 1		0,5
	7,0	2 5 2 5 3 8	8,8	3 S	26,05	5 2	20,00	\$ \$ \$ \$ \$ \$		12.1		ç vç	27	13.046		14.547	3,5
	<u></u>			86,212		87,602						90	. n			14.594 15,17	15,17
	!!		85,807	86,265		87,662					q6= 8.4	47	4.			14.642	15,2
	<u>ب</u>			86.319	86,983		-		2	. 2.	4.	•	.	13,728	8.	90	Ž
(۱۰	2 %	8 28	86.428	87.128	87,73	88,513	88,613	! <u>-</u>				- · ·				12
GE	8			86,481	87,201	87,893			71	···	•		 				5.4
32	٥			86,534	87.276	87.951				· .			۽ اِه	93			Α
- 3	2:		(2)	OKC OK	Ş Ş	10,88	94,88 8	90,00	•	•			2.5	8	À À		ļ
8		Ī		Ī	Ī	-	Ī	ļ	ui si O v	~			: <u>'</u> 2	İ	i	<u>-</u> -	١
	<u> </u>	Ħ						; į	wss: u 4	•] [2]		i		ij
	3	Ī	-		1	į	:	-	14 1 40				2 4		-	$\dot{\uparrow}$	
	Τ.	╈	3	3	Š		Ş	0.7	C4 3]\$,				Total		Š	3	3
		217	32	3	2	S	419	122	W.	-			Tj.	122	-	-	Š
	<u>. </u>	ð	ş	_	j	3	3	40) , >	:	3	, ;	Avente	ઢ	<u> </u>	-	3
			2			•	41.9		>	2	כר אל כד אז כו	2	hit/min	27.7	40.4	7.79	2
	(A)	22.50	1 20	124	2.24	1.43	0.75	0.22	_	Water	Water Injection Ratio (q : lit./min/m)	(m/min/m)	(PP)	0.37	4		
	17	OSS (P.)	2)	3	(/cm2)		*		Lugeo	Lugeon value:			Friction	riction Loss (Pr) = pr (Lo + Lo) [kgU/cm2	\$ (<u>}</u>	3	Ę
							¥.	ď.	Critic	Critical Pressure:	>12 kgf/cm2	2					
	Remarks:												Remarks:	 «			
	·	-		٠.								,					
	Note: In	njection.	of water	should t	oc contin	ued for a	at least li	O menute	Injection of water should be continued for at least 10 minutes under the specified	scified pressi	Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute and an additional for the injection and in the just previous one minute.	rate per minute	Note:	Injection of water should be con	of water's	hould be	8 0
	Prepared by Azbor / Hamid	2	42.50						Inspected by : Farhat M. Shah	v Farhat	M. Shah		Prepar	Prepared by: Azhor / Hamid	/Zhor/	Hamid	<u>.</u>
					,								_				

Water Pressure Test

Hole Inclination (a): 90 degrees Packer Type: Mechanical Mec														
를 이 1번 위 등 1 1분 중인인증	Location	Ë.	Dam A	xis (Ri	ght Ban	k, Dam		_	Dia. of He	ا چ	101	١		- 1
이 배우를 다 살았다.	Hole I	clinatic)n (a):			8	degrees		Packer Ty	إ	Mechan	tical		
	Friction	i ssori u	er met	cr (p.) ;	l	О× b	ٳ		Date:		10/Januar	6061/		- 1
	Ground	cievation	E		Γ	Ground	aler lev	3	2	=	Caupe	height (La):	0.73	1
	Pipe len	gth from	pressure	gauge to				cpth of te	est section		3	ength of secti	(m) w	
1 2 2 2 3 1 1 1 1 1 1 1 1 1	borehole	mouth:	į	7.50	_	<u>5</u>		45 m	±(σ') οι	i I		8	ε	
			Res	ling of	Now m	eter				Colcu	lation of L	urcon valu	Ų	
\$1810	Gauge P.	Pel	P42	١ '	3	P-5	8	P.7						١.
	(kg(/cm))	-	4	ı	2	-	4		P-P-0.1(s	n(a)[_+)-Pr [kgt/cm2		livmin/m	
	Nat lime	15:00		15:25	15:38	15:50	16:03	- 1	<u>.</u>					
	Semina Semina	U-5.51			15,018	300	16,190		Α.					
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		13,618			12,071	15,678	16,233							
1 12 13 1 1		2,0			15,122	15,726	16,276							
1 1 1 1 1 1 1 1 1	<u>د</u> .	17,674			15,174	5,7	2.5							
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	_	13.70			15,225	15.820	16,362		ጁ					
1 1 1 1 1 1 1 1 1	v	7.7X			5 2 40	15 R6R	16.403		Α					
1 12 131 16 15	٠	1.7				15.016	16.445							
1 1, 13171 e 15		2			1	. 8	7.4							
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	. ~	ď				2		6 OK	7				~	Γ.
1 12 131 1 e 15 1 1	į,	1,00				y v	, V		ш				\;	
1 12 13 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.ie	8			Š	2	6.5) já			`	?	
1 12 13 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	:=		Ì		}	1	2					\	٠.,	
The latest the latest terms of the latest term		Ī	į	İ	Ī	-	-					'	٠.	
i i i i i i i i i i i i i i i i i i i	1		İ	ļ	İ		1		N)			•		
1 12 13 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3,3	į	į		ļ		1	1	•					-
1 12 13 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		T :					Ĭ		n m					
i vertition e 15 e i i	Lon	2	5	5	5	ž	ź	Ġ						
1131me 15 1 1	! <u>=</u>	į	\$) ?	3	} {	3 8	į		-				_
		ŀ	Ç	(1	Ľ	Z	-	0					٦
131m = 15 1	, ,	7.7.	9	0	-	Š	ç		_	1 2	27		-	2
TT 6 15 1 1	French tom	15:10	15.22	18-35		9.45	6.13	1		3				;
1 - 15 1	3	0.37	0.77	š	33	1.07	7	1		ř	er injection k	m/m; (d : m/m	Ē	
. 15 1	Friction	(gs (P)	- D(L	3	Cm23		ā	i	Luck	non volu				
15 1 1							\$	ì	Ü	ical Pressu				
1 6	Kemarks													1
		Injection	of water	Should t	ocontin	ued for	r Icasi 1	O minute	s under the s	ימכניווכת מ	ressure, after	the injection r	ate per m	ΙĒ

Hote No.: M98-1	Stage:	11/14	Hole No.
Location: Dam Axis (Right Bank, Dam Crest)		Dia, of Hole: 101 m/m	Location
Hole Inclination (a): 90 degrees		Packer Type: Mechanical	Hole Inc
Friction Loss per meter (pt): 1×10 ⁴ ×0 ^{1,11} ;	. Date:	13/January/1999	Friction

Pipe length from pressure gauge to berehole mouth. (Lober 7,00 r Courge P. Pol. P. 2. Pol. P. 2. Pol. P. 2. Pol. Pol. Pol. Pol. Pol. Pol. Pol. Pol	20	10 10 10 10 10 10 10 10 10 10 10 10 10 1	S 23 24 2 8 8 4	4 #[점등성상상성성상	50 m P-7 P-7 12:18 34,912 34,912 35,016 35,016 35,018 35,118	Depth of rest section 50 m to (La)= 55 m Calculation P _{0.7} 1 P=P=0.1 (sin(a)L'+L)-P ₁ [kg 12.18 13.4560 13.4563 14.963 15.4563 16.566 17.418 18.718 19.818 10.	Calculation of Lugcon value Calculation of Lugcon value Calculation of Lugcon value P=P=+0.1(sin(a)L=Lu)-Pr {kgl/cm2}, q=Ou/Lu {lil/min/m} P1 = 5.2 q2 = 11.4 P2 = 7.5 q2 = 11.4 P3 = 9.5 q2 = 11.4 P3 = 9.5 q4 = 19.8 P5 = 8.7 q5 = 10.4 P6 = 6.9 q6 = 13.3 P7 = 4.8 q7 = 10.3
원 [7.00 adding of P.3 adding of P	100 10 10 10 10 10 10 10 10 10 10 10 10	S 23242884	\$ 18 2 7 11 8 2 11 8 3 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	E	10 (L/) = 55 m	of Luggon value
7et 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	22,170 22,170 22,170 22,170 22,170 22,230 11,32,583 11,32,583 11,32,584 12,555	10 10 11:38 13:00 33:120 33:120 33:120 33:120 33:120 33:120 33:39:49:49:49:49:49:49:49:49:49:49:49:49:49	2 23242884			Calculation -Po-0.1(sin(a)L-L.)-Pr [kg PL= 5.2 PL= 5.2 PL= 5.2 PL= 5.2 PL= 6.9 PL= 6.9 PL= 6.9 PL= 4.8	of Lugcon value flom2], q=Q=,Lu [li\/min\/m] q2= 11.4 q2= 11.4 q3= 14.3 q4= 15.8 q6= 15.3 q7= 10.3
Pet 1 11:00 31,000 31,046 31,046 31,093	7 20 32,170 32,240 40 32,312 11 32,383 17 32,484 17 32,484	, P.4. 10 10 13,030 13,130 13,210 13,394 13,494				-Po-0.1(sin(a)L/-L.)-Pr [8g P1	f/cm2], q=Q_d/La [liv/min/m] q1= 8.6 q1= 8.6 q2= 11.4 q3= 14.3 q4= 19.8 q5= 11.3 q7= 10.3
31,000	7 22,170 32,240 4 32,340 10 32,383 17 32,484 17 52,583	10 35,050 35,050 35,050 35,500 45,600				**Pe**********************************	### ##################################
31,000 31,046 31,046 31,037	22,112 20,172 20,170 20,170 20,130 20	35,030 35,030 35,030 35,230 35,398 35,398			12:18 74,860 74,963 35,016 35,016 35,118 35,170		
31,000 31,046 31,093 31,137	10 32,170 77 32,240 74 32,340 71 32,454 72 52,55	33,030 33,130 33,230 33,398 33,398			74,867 74,947 74,967 75,016 75,118 75,170		
31,046 31,093 31,137	6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	33,230 33,398 34,484 54,684 56,684			24,912 24,963 25,016 35,016 35,118 17,25 1	į.	
31,093		5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5			25.25.25.25.25.25.25.25.25.25.25.25.25.2	ŀ	
31,137		55 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5			35,016 35,016 35,118 35,170		
		33,39% 33,494 33,594			35,066 35,118 35,130 125,23		
4 31,180 31,747	•	33,494	2,690 477,4		35,118 35,170 15,221		
5 31,223 31,804	•	33.591	2,77		55.72 157.72	0 0	
31,264	2 32 596				25,25 27,25	2 2	
7 31,305 31,918	32.666	33,692	34,855		14 271	2	
8 31,346 31,975			¥ 937	35,723			
9 31,387 32,032			35,019		35,324	э., ж	
10 31,428 32,088	32,884	8,00	35,102	35,856	35,75	131	
11			1	i	:	0 i	
	1	-	Ì	i	Ī	, o	
		-		-		4	
	:		İ		i	18 18 20 1	
Total 0.1	33	38	38	3.8	် ဝိ	M'sic	
3	╁╌	j	Š	3	ď		
	1	8	¥2.2	9.6	51.5	0 5 10 15	20 25 30 35 40 45 50
占	2 11:35	¥4.	12.03	12:16	12 13	Wufer Inte	Water Interlion Batio (o . N. (m.o/m)
(Pr) 0.94 1.64	2,58	16.4	3.40	2.25	1,35		
Friction Loss (Pr) = pr(La + L.) [kg(/cm2,	*\(\gamma\+0	g(/cm2)		3	-	Lugeon value:	(15) Lu '
				3	:	Critical Pressure:	9.5 kg/cm2

Note: Impection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just pressure one minute.

Prepared by: Azhor / Hamid

Water Pressure Test

Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st Friction Loss per meter (p) 1st 1st Friction Loss per meter (p) 1st		•				,	•						
	Tega Tiga	٠	Eg D	ž.	F C	ž D	Š	_	Dia. of Hole:	76	m/m		- 1
	Hole l	nclinatio	(a) EC	Ī	ı	8	degrees		Packer Type:	Mechanic	*;		- 1
<u> </u>	Frictio	n Loss	oct me	(A)	- 1	ox,	ij		Date:	28/January/	6661		
 	Ground	elevation	: EL		E	Ground	vater lev	e (L):0	50.30	Gauge N	cight (La):	0.73	1
	Pipe len	gth from	pressure	Sauge Ic				cpth of te	est section	3	oth of section	٤	
 	horehok	mouth:	<u>-</u>	7.00		CL - (L	l	55				E	
 			Rea	ding of	flow m	eter			Calcu	lation of Luy	geon value		ı
	George P.		204	£M4	3	PuS.	Pub	/W.					
	(kgf/cmJ)	1	4	7	0	7	4	-	P=P-+0.1(sin(a)[_+1	PP [kgC/cm2],		i/mm/m]	_
	Start Irms	L.	15.13		15:40	15.54	16:06	1	Pt= 5.9	9			
	O(min)						76,820		Ē				
73,075 73,395 74,086 75,100 76,371 76,948 77,559 75,000 77,544 74,545 75,195 76,250 77,101 77,544 74,545 75,195 76,250 77,101 77,518 75,495 74,206 75,295 76,411 77,137 77,571 75,955 74,240 75,526 74,340 75,526 74,340 75,524 77,325 77	-	2.05					76,884		£				
	64	27,075					76,948		P4=				
		73,092					77,010		ŗ				
~ ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		73,112					77.074		P.6.				
~ ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	:	5							2				
	1	1 1 1					1		!				
	: ^	1, 12					17.00			•			
		Š					1		i				r
		7							įω:	۴.		_	
	. 01	12.12					14),]B				
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~						•				s.,			
	12		-	ļ				ĺ	•				_
	-				1		-	ŀ	_				
<del></del>			!	i		Ī	ĺ	i					
<del>   - </del>	,×		İ	Ī									
<del>  - </del>  -/ -/ -/ -/ -/ -	ē	ã	3	7	Į	Š	Ş	Ş					
<del> </del>	×	Š	ŝ	7	ğ	õ	93	5					
<del></del>	Avelage	l	5 0	Ç	Ş	Ş	9	0.7	•				1
<del></del>	it/min		S	7.7	ş		62.6	42.9	'n	:: 8	S S	₹	8
T 8 12 1 1	Finnsh tum	15:10		15:35	15.50	16:04	16:16			And and and an order	21, 27, 27, 4	1	
도 본	(4)	0.24	- 56	3.32	4.87	3.51	2.16	1.03		ci migazina Par		(m)	
[2 ]	Friction	Loss (Pv	7)	+1.0[k	g(cm ² )		2	3	Lugcon valu		3		
[ <b>2</b> ]]							i				ket/cm2		
1	Kemark	. ا											Į.
1 1													
certies within 90 % to 110 % of the injection rate in the just previous one minute	Note:	Injection	of wate	rshould	be contin	ned for a	l least 1	U minute	s under the specified pr	ressure, after the	aniection rai		- 18
	_	3											É

Ho	Hole No.:	~	M98-1				Stage:			13/14			Hole No.:		M98-1			ŀ	Stage:		14/14			i
3	Location:	Dam Ax	is (Rig	ht Bank	Dam Axis (Right Bank, Dam Crest)	[ <u>3</u> 2	Dia, o	Dia, of Hole:		76	m/m		Location:	Ī	Dam Axis (Right Bunk, Dam Crest)	eht Bunk	Dam Cr	ନ୍ଧ	Dia, of Hole:	ole:	92	m/m		ı
HOH	Hole Inclination (a):	ion (a):			90 degrees	្រី	Packer	Packer Type:	Ψ	Mechanical		1	Hole Inclination (a):	nation (a	ë		90 degrees	gl	Packer Type:	ا پيز	Mechanical	- Jac		1
Fric	Friction Loss per meter (Pr) :	per mete	۱ <u>څ</u>	ı	1×10 ×0,***		Date		30/3a	30/January/1999	8		Friction L	oss per n	Friction Loss per meter (p.) :		1×10*×01"	1	Date:	0	02/February/1999	6661/		1
[5	Ground elevation : E1.	. E.	l l E		Groundwater level (L.); GL.	r level (L		50.30 m	F	Gauge height (La):	1	0.73 m	Ground clevation: EL	ation : EL		Ŭ E	oundwater	Groundwater level (Ls): GL-	Н	50.3 m	Gauge	Gauge height (La);	0.73 m	
<u>ا</u>	Pine breath from pressure gauge to	n pressure s	Value 10	Γ		200		1	_	Fengl	Length of section (Lu)	[3	P.pe length	from press	Pipe length from pressure gauge to		;		Depth of test section			(LL) Length of section (LL)	ا ( <u>3</u>	·
. 4	horehole mouth: (I 4)=	•	7.00 m		5	!	=(vT) on w		٠ ٤		v	E	horehole mouth: (Ls)=	(e):	7.00 m		OL- (C)	હ	=( <b>-1</b> ) o u	2		8	ε	7
		Read	ng of fi	3	ř		_		rulation	Calculation of Lugeon value	on value				Reading of flow meter	flow me	1			Calcula	tion of Lu	Calculation of Lugeon value		T
Consta	7 -	3 .	3 .	3 5		Pub Pu7	_	Pa-Pa-0 1(sin(a)[.+[.]-Pr.]kgf/cm2].	L)-Prika	ļ	Monday	nin/ml	(kg/km)	Pol. Po2.	. P.	ž 5	3 r 3 4	2 - 1 2 - 1	P=Po+0.1(5	P=Po+0.1(sin(a)L++Ls)-P+ [kgf/cm2],	* [kgf/cm2].	q=0-/L [¼/min/m]	Vmin/m]	
(willow)	1 (cm)	1-	15:40	+	16:05	16:17 16:29		P1= S	5.0	` <b>.</b>	8.6		ш	11:45 11:57	57 12:10	2:52	12:34 12:	12:46 12:58			Ĭ			
<u>ြင်</u>	匚	11,82×			<u> </u>		8		6.6	25	13.0		U(mm) 7,9	74.5 7.980	7,974.5 7,980.8 7,981.0 7,981.3 7,988.1 7,988.6 7,988.7	7,981.37	7,988.1 7,980	7,988.6 7,988.7		P2= 9.1		45 0.002		
<u>'</u> .c	1.313	368	2 764	13,8381	14.972.14	14,910 15,648	\$ 50 50 50 50 50 50	- 6	و ج	9 8			2 7.9	74.5 7,98	7,974.5 7,980.8 7,981.0 7,982.5 7,988.1	7,982.5	988.1 7,98	7,988.6 7,988.7						
	200	2022					Ĝ.		3.1	5			0.	74.5 7,980	7,974.5 7,980.8 7,981.0 7,983.7 7,983.1 7,988.6 7,988.7	7,983.7	988.1 7.98	8.6 7,988.7		P5= 12.1	•	45= 0.004		
4	11.441	12,087					<b>%</b>		6.7	ġ.	17.8		4 7,9	74.5 7.98	7,974.5 [7,980.8] 7,981.1 [7,984.5] 7,988.1 [7,988.6 7,988.7	7,984.517	988.1 7,98	8.6 7,988.7		P6-		90- 0-002 		
., .,		21.53				15,166 15,833	ខ្លួន	7	8,4	2.5			0.0	7074 5 7 980	7,980.9 7,981.1 7,985.9 7,988.2 7,988.7 7,988.7	7.985.9	988.2 7.98	8.7 7.988.7						
	288	1273	13.268 1	14/4/4	15,465 15		8.5	2				_		74.5 7,980	7,974.5 7,980.9 7,981.1 7,986.2 7,988.2 7,988.7 7,988.7	7,986.2 7,	988.2 7,98	8,7 7,988.7	••					محصمه
. !	۱ ا	12,348	13,351				ζ <u>ι</u>	_	,	•			2.0	7,974.5 7,980	7,974.5 7,980.7 7,981.1 7,986.6 7,988.2 7,988.7 7,988.7	7,000	988.4 7,78	0 1 1 000 1	7W.	<b>#</b> ~				
<u> </u>	11,655	12,413	13,434	86.2	21 828,21	15,422 16,017	nyî C C	<b>∞</b> 1	<u>,</u>				1_	7,974.5 7.980	7,980.9 7,981.2 7,987.4	7,987.4	7,988.3 7,988.7	X.7 7.988.7	)]]]] 					
							f ai		8				= :	1			1	 		-				
0	2	Ì	<u> </u>	Ī	- 	<u> </u>	) I	~	<b>₽</b>				13.5	<u> </u> 		İ			ארנו איר					
_		+	:	<u>-</u> -		÷	, E31,	4 (					1 1	<u> </u>			<u> </u>		914 4 %					
, <b>*</b>			1		1		. T	- ·					-1	+	_L	7		-+	15;1				- 4	
₽ :	7 7	3	3	38	38	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \					-		, 	38	3 8	}	5.2	) 6 6	M					
		3 2	100	-	╁╴	Г	.].						Vestage	١.	┞	Ş	L:	H	o 	ı				
in James	·	8		<del>, -</del> -		26.	_	0 5	10 15 20 25		30 35 40 45	5 50	1st/min 0	- [	- 1	8	_1			0 0.1 0.2	0.3 0,4 0,	0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9	 60 S	
Tar.	l.	5 15.37	15:50		16:15	16:27 16:39	2	*	Vater Injec	Water Injection Ratio	(q:lit/min/m)		귀	4	_	12-22	.+	ᆛ		Water	Injection Ra	Water Injection Ratio (q : ilt./min/m)	(E/2	
(A)	01 1 10	2.52	4.25	5.52	3.08 2	2.44 1.2x	_		•					0.00	000	4	000	3.0		•		,		
Frici	Friction Loss (Pr) = pr(Lo + Ls) [kgVcm2	مر) م= (۰	. L.) [kg	/cm2]		2		Lugeon value:	]e:		Į,		Friction	5 (Pr) 1 P	Friction Loss (Pr) = Pr(Lo + Lv) [kgt/cm2]	g(/cm2]				Ingeon value:		3		
	•					į	1	Critical Pressure:	asure:	<b>≯</b> 9.6	kgf/cm2							3		Critical Pressure	5	kgt/cm2		T
Ken	Remarks:												Remarks:											
												_												
Noge :		on of water	Should by	Continue	ed for at k	ntm 10 mm	utes under	Injection of water should be continued for at least 10 minutes under the specified	1 pressure,	after the 10	Injection of water should be continued for at teast 10 minutes under the specified pressure, after the injection rate per minute	per minute	Note: Iny	ection of w	Injection of water should be continued for at least 10 minutes under the specified settles within 90 % to 110 % of the injection rate in the just previous one minute	be continue	ed for at lea	as to mout	es under the previous or	specified pres seminate	Sourc, After I	Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.	te per minul	Ü
Į,	S Contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of	A LIVE		W DC 118.	meet real to	11 MI 11 MI	1	forected by . Earlist M. Shah	N. Sept.	App.		_	Prepared	5V AZ	Prepared by : Azhor / Hamid	و.[			Inspected	Inspected by: M. Suga	uga			
57	Prepared by: Azhor/ Humid	AZDOL	of Early				3	יוני היי		Citate		1				ا								1

#### Water Pressure Test

Stage:	Dia, of Flole:	Packer Type:	Date:	EN.	Depth of test section	m to (La)= 10	D		reretti.k(Sin(a).	2	P. 73	<b>2</b> 2	2 2		<u> </u>	100 100/J							, ,	<b>1</b> "1	v moseon v	Critical P	. Due to high water loss all stages could not be completed Equipment condition unsatisfactory. Test had to be stopped three times due to	Injection of water should be continued for at least 10 minutes under the specific settles within 40 % to 110 % of the intection rate in the tust previous one minuteriles.	Inspected by :
	Sank)	90 degrees	0,221;	Groundwater level (L1):	Deptho	GL - (L) = 5		Pu6   Pu7		4:40	1				-		-		<u> </u>  -		ફ જુ	2 Ome Om2	-		IA7	<b>97</b>	Remarks : Due to high water loss all stages could not be completed Equipment condition unsatisfactory. Test had to be stopped	or at least 10 min	
	Dam Axis (Right Bank)		1×1 @ ×0721:	m Grou			flow meter	2 . 3.	1 2 2	24,300	24,436	24.502	24.700	24,699	24,831	24,898	 		-		2 & 3	\$ 0 \$ 0	13:20	O.4h	(/cm2)		il stages could lisfactory. Tes	c continued f	1
M98-2	D _{um} A	;(e)	meter (p.) :		sure gauge to	6.89 m	ading of	_P.2	ē	1,	20,224 20,300		20,001	20,855	20,982	21,23	C. L. P. C. L. L. L. L. L. L. L. L. L. L. L. L. L.				245 248	0-2	┵	Н	3x] (~1 + ~1) ×		h water loss a ondition unsa	water should t	-h., he Cha
Hole No.:	Location:	Hole Inclination (a):	Friction Loss per meter (p.) :_	Ground elevation: El.	Pipe length from pressure gauge to	borehole mouth: (La)=	#	₹.	10.01	18.930	2 19,002 20,	19,143	0. 001		19,413	19,547	17,014			15.	- - - - - - - - - - - - - - - - - - -		╁	0.49	Fretion Loss (Pr) = pr(Ln + Lr) [kgf/cm2]		Equipment o	1	Oraniera hu Chaha Ma Chah
Ť	ጃ	Ĭ	ជ	[5]	<u> ۽</u>		L.	<u> 3</u>	(chrotala)	<u>  5.</u>				· · · · ·		0 5	- F	<u> </u>	3,2	 	Total	Ľ	12	a)	<u> </u>		<u>x</u>	Nor	<u>ا</u> مُ
1/20	76 m/m	Mechanical	17/December/1998	Cauge height (La): 0.86 m	Length of section (L.)	: -	Cafculation of Lugeon value		Pare-U.I(sin(a)Li+L.)-rr (kgi/cmi), qa.Q/Li (n/mn/m)	q2= 29.5	1 100	190	# QD	ı						9	\		15 20 25 30 35 40 45 50	Water Injection Ratio (q : lit/min/m)	: (112) Lu'			U minutes what the specified pressure, after the injection rate per minute. The tust neevitus one minute	
Stage:	Dia. of Hole:	Packer Type:	Date: 1	Nii		m to (La)= 7 m	Culcula		P=Fe+0.1(sin(s)Li+L.)>. n::	17.	P2=	ž:	9 5	· L	_	y ∞		ni su o vo			NeW	]	0 2 10	Water	Lugeon value:	Chical Pressure		10 moutes under the specified pre-	action with different
			-	evel (Lu):	Depth of test section			Po7				;	:		<u>.</u>	1 !	1		-	1	0	<u>د</u> و			K. 1977			E	1616
	Bank)	90 degrees	1×10*×0;;	Groundwater les		( <u>C</u>	ļ.	3. 8.	1		<u> </u>	<u> </u>			<u> </u>		-	;   ;		<u> </u>	ટ	30	+				l/cm2.	Injection of water should be continued for at least	CCHOL IGH
	Dam Axis (Right Bank)		1×1¢				Ž	Pa4 Pa5	1	+	1	<u>  !</u> 	1	i		<u>! :</u> 	-		!	-	3	9	+	╀	cm2]		2 and 2 kg	continue.	MIN IN
M98-2	Jam Ax	ł	.l	E	on same	7.50 m	ing of fi	3	1		1	- 1	1	Ī		! [	<u>:</u> !		<u>-</u> -	· :	3	3	$\dagger$	╁	L Ikgt		1kgf/cm.	should be	
_	-	(a) co	xr mete	멾	pressure s	. <u>3</u>	Read	7.7	-	12,040	12,197	2,480	<u>8</u>	i					i	:	38	╂	147.5	2	<u>و</u> - ۵		leaked at	of water	
. '	on:	Hole Inclination (a):	Friction Loss per meter (p):_	Ground elevation : EL.	Pipe length from pressure gauge to	borehole mouth: (L.)=		ž		25	11.383	11.506	3	089	11,751	11,870	11,92%			-	38		S	ᆫ	Friction Loss (Pv) = Pr(L+L)  kg//cm2]	•	Kemarks : Packer leaked at tkgfrem2 and 2 kgfrem2.		A VI O BY ON BUILDING STREET
Hole No.:	Location:	Hole I	Frictio	Dawor	S S	orehol		Casego P.	(Mycm)	O(mm)	- 0	'n	٩¦.	n 0	۲, «	\a\;	2,=	12	ב;.		<u>.</u>	Avenge	W/W/	3	ğ		Сспат	Note:	

#### Water Pressure Test

76 m/m 2/20

Mechanical

1

()

Friction Loss per meter (tp)   Lyl f xQ ²⁷⁷¹   Date   18/December/1998   Experiment elevation: EL   m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater level (LJ)   Log f m   Groundwater le			· (a)		•		۱							l	l
0.86 m (Ground Mile) (Juge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge P. (Junge		Frictio	n Loss	per met	cr (v):		o, vo	ä		Date:	¥	%Decen	nbcr/199	~	
Pipe len   Pipe len	98'0	Ground	clevation	: EL		Γ	Ground	ster leve	Ŝ	Z		ð	Gauge height (La):	1	9%¢ ==
(Gauge P. (Gauge P. (Aglema)) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema) (Aglema)	cetion (L.)	1 8 E	nor) que	pressure	ot agueg			<u>مٌ</u>	pth of re	st section			Chytho	(L) notices of section (L)	ব
10 (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P. (Amge P.	. E 5	borehok	e mouth:	Ĵ	689		5	t	E ا	=(**) 0)	10		i	. E	
(Gwgg P. (Gwgg P. (Agrons)) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (Agrons) (A	alue	_		Reac	ling of	flow m	eter				Calcut	ation of	Legeon	vasuc	
### (Actions)   (Actions)		Cauge P.	Ľ	5	5	Ž,	3	3	_						
	(L. (lit/min/m)	(Agtions)	-	4	2.5	1				P=Po+0.1(5	i(a)(*)(a)(i	-P. [kg0c	m2j, 9	7.C [ii/ii]	o/m/
W(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)  V(min)		Start time								۰			5	13.7	
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		(min)		20,100		24,300	į			۸.			45	24.9	
2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4						24,367				۵.			Ĝ	19.6	
10 11 12 12 13 14 15 15 15 15 15 15 15 15 15 15 15 15 15		~			20,398	24,436		į	į	۵.			44	13.3	
4 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 -		m.	19,143		20,494	24,502		İ		۵.	<b>.</b>		ş		
40 45 50 113 113 114 114 115 115 115 115 115 115 115 115		4:				24.568	1		-	۵.	<b>.</b>		95		
40 45 50 11. 11. 11. 13. 14. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15	-1	w.	_		į	24,633	İ		İ	O.,			<b>6</b>		
10 11 11 12 12 13 14 14 15 14 15 15 15 15 15 15 15 15 15 15 15 15 15		•	19,346		•	24.699		į	ļ						
40 45 50 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70th 11.70		7	19,413			24,766	Ì			2					
10 10 11 11 11 11 11 11 11 11 11 11 11 1		æ. !	19,480		į	24,831	1	İ	İ	ζu					<b>W</b>
10 _ 10 _ 11		•	19,547		-	24,898		ļ	Ī	20) (13)					
11. 12. 12. 13. 14. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15		<u>ප</u>	19,614		1	2. 8.	j			181					
40 45 50 113-113-1144-1144-1144-1144-1144-1144-1		=:	1	Ţ	1	Ī		Ī	į	ni :					
14 14 16 16 16 16 16 16 16 16 16 16 16 16 16		2,5		İ		Ī	Ī		Ī	nu:					
15. Total III.  18. Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Average Av		31.5					İ	Ī	Ī	3531			,		
Total  II.  Average Average Average III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min  III./min		. <u> </u>		1	•			-	İ	4 i		8	١		
40 45 50 Information of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control		F	2	Ś	S	2	ž	4	Ś	) { C-\$	<u>.</u>				
40 45 50 ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING THE ILITHING			3	245	Į	\$	}		<u>`</u>	M		•			
10/m) House un house in per minuite Per minuite Per minuite Percount	7	Average	_	0	Ö	ैं	Q 3	<b>†</b>	ှိ	0		1			]
American (Ps) Frection Frection Remark Remark Remark Remark Prepare		LI J. TRIO		124.5	0.00	Ş		-	1	_	'n	ä	и Х	33 53	\$\$ \$\$
Nemark Nemark Note:		Pinah lim		•		13:20					Water	1000	o Datio (a	· lie /min/m)	
Frection Remark Ite per minute Note:	:/ww/m/	(b)	0.49	10.	1.00	0.46							2	(m. /m. /m. /	
Remark Ité per minute Note :	•	Fretion	Loss (Pr	- P(L	31 (~1 +	t/cm2]		TAIL .	:	3	con value			Ľu,	
Remark is per minute Note:	ĩ.							î		Ö	Ixeal Pressur			kgUcm2	
Noie :		Kemark	s : Due to	high wa	er loss a	II stages	could no	i be com	plered						
Note:	-	<b>-</b>	redniba	100 III	esun voc	risiacior.	e S	1000	noddor	nice times	Dane to both	10 all	avery nose		
Note															
	on rate per minute			ithin 90	should in	be contan	ued for a imjection	it least 10 a rate in t	) minute the just (	s under the previous one	specified pr	essure, af	ier the mje	ction rate po	r minuk
		Prepar	cd by:	Farhat	M. Sha	عِ				Inspected	bv: M. 5	Suga			

Hole No.:	M98-2	Stage:	3/20	Hole No.:
Location:	Dam Axis (Right Bank)	Dia, of Hole:	76 m/m	Location:
Hole Inclination (a):	(a): 90 degrees		Packer Type: Mechanical	Hole Inclinat
Friction Loss per	Friction Loss per meter (pv): 1×10°×01**1:	Date:	20/December/1998	Friction Loss

Hole Inclination (a):   90 degrees   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packer Type: Machanical   Packe	Dam Axis (Right Bank)   1   90 degrees	1 2 6	76 m/m  Mechanical  Course heigh (La): 0.86 m  Course heigh of section (La).  5 m  5 m  on of Lugeon value  kg/cm2, q=0.42 [li/min/m]  q1 9.9  q2 16.8  q3 23.7  q4 14.1  q4 26 8.0
Mechanical December/1998  Cauge height (La): 0.86  The construction (La): 5 m  Solution of Lugeon value  [kg//cm2], q=Q-/La [iit/min/m]  q1= 9.9  q2= 16.8  q4= 23.7  q4= 14.2  q5= 40.45  sycation Ratio (q: iit/min/m)  (36) Lu'  >6.3 kg//cm2  >6.3 kg//cm2  >6.3 kg//cm2	1   1   1   1   1   1   1   1   1   1	1 1 2 . 6	Mechanical   Cauge height (La): 0.86 m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m
Cauge height (La): 0.86   Cauge height (La): 0.86   Cauge height (La): 0.86   Cauge height (La): 0.86   Cauge height (La): 0.86   Cauge height (La): 0.86   Cauge height (La): 0.86   Cauge height (1.87)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (1.88)   Cauge height (	refer (pr): 1x10f xQ ^[vr] :  m Groundwater level (La)  6.81 m GL_ (La)= 10  6.81 m GL_ (La)= 10  7 1 15.10 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.20  13.10 15.2	1 1 2 6	Councer/1998  Cauge height (L.): 0.86 m  Longli of section (L.) 5 m  End Lugeon value  \$2 m
Genge heigh (La): 0.86  Length of section (La).  5 m  5 m  6 or of Lugeon value  (kg//cm2], q=O_m/L [lit/min/m]  q1= 9.9  q2= 16.8  q3= 23.7  q4= 14.2  q5= 8.0  q6= q7=  q7= q7=  (30  Lu'  >6.3  kg//cm2  >6.3  kg//cm2	ading of Row meter  P.3 P.4 P.5 P.4 P.5 P.6 P.7 P.5 P.4 P.5 P.6 P.7 P.4 P.5 P.6 P.7 P.5 P.6 P.5 P.6 P.7 P.6 P.5 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.6 P.7 P.7 P.7 P.7 P.7 P.7 P.7 P.7 P.7 P.7	1 2 6	Cauge height (L.): 0.86 m  Length of section (L.)  5 m  5 m  5 m  6 m  6 m  7 m  7 m  7 m  7 m  7 m  7
Length of section (L.),   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S	CL. (L) = 10   Depth of	<u> </u>	Length of section (Lu).  5 m  5 m  5 m  6 m  5 m  7 m  7 m  8 m  8 m  9 m  9 m  9 m  9 m  9 m  9
S m   S m	6.81 m GL(L)- 10  ading of flow meter  Pro. Ped. Ped. Ped. Ped. Ped. 13:10  38.000 39.270 40.130  38.228 39.504 40.207  38.228 39.5720 40.207  38.289 39.5720 40.209  38.589 39.5720 40.329  38.589 39.5720 40.329  38.589 39.5720 40.329  38.589 39.5720 40.329  38.589 39.5720 40.329  38.589 39.5720 40.329	m to (L)= 15 m Calculation P=P=0.1(sin(s)L+U)-P-1 P1= 2.0 P2= 4.3 P2= 6.3 P3= 6.3 P4= 4.6 P5= 2.1	5 m  5 m  5 m  6 m  7 m  8 m  8 m  9 m  9 m  1 m  1 m  1 m  1 m  1 m  1
(kg//cm2), q=O/L [ii/min/m] (kg//cm2), q=O/L [ii/min/m] q2= 16.8 q3= 23.7 q4= 14.2 q5= 8.0 q6= q7= q7= 15 20 25 30 35 40 45 nyoction Ratio (q: itt/min/m) (36) Lu' >6.3 kg//cm2	ading of flow meter  7 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Calculation (*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-(*) 1.97-	kg/cm2, q=O=/Lugeon value  kg/cm2, q=O=/Lu [ii/min/m]  q1
[kg/cm2], q=Q/Ls [lit/min/m] q1= 9.9 q2= 16.8 q3= 23.7 q4= 14.2 q4= 14.2 q5= 8.0 q6= q5= 9.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6= q5= 1.0 q6	4 7 7 8 8 6 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8	Pared 1 (sin(a) L+L).Pr Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Practical Pr	kg/cm2, q=O=/L_ [ii/min/m] q1= 9.9 q2= 16.8 q2= 23.7 q4= 14.1 q6= 8.0 q6= q7=
41= 9.9 42= 16.8 43= 14.2 45= 80 46= 9.9 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80 45= 80	13:04 13:16 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45 13:45	P	41 9.9 42 16.8 43 13.7 45 80 47 80
42= 16.8 43= 2.3.7 44= 14.2 45= 8.0 46= 47= 47= 47= 47= 47= 47= 47= 47=	36,220 34,000 39,770 40,130 36,391 38,225 39,436 40,167 36,391 38,228 39,504 40,207 36,473 38,374 39,573 40,230 36,473 38,497 39,402 40,234 36,4726 38,516 39,770 40,338 36,811 38,828 39,807 40,465 36,899 38,980 39,937 40,465		
43= 23.7 45= 14.2 45= 14.2 46= 97= 97= 15 20 25 30 35 40 45 15 20 25 30 35 40 45 15 20 25 30 35 40 45 15 20 25 30 35 40 45 15 20 25 30 35 80 45 15 20 25 30 35 80 45 15 20 25 30 35 80 45 15 20 25 30 35 80 45 16 20 20 30 30 30 40 45 17 20 20 30 30 40 45 18 20 20 30 30 40 45 18 20 20 30 30 40 45	36,311 38,125 39,436 40,167 36,473 36,473 38,238 39,473 40,230 36,239 36,473 39,473 40,230 36,473 36,473 39,473 40,234 36,472 36,473 39,772 40,382 36,813 38,880 39,937 40,465 36,889 38,880 39,937 40,465 36,899 38,980 39,937 40,465 36,899 38,980 39,937 40,465 36,899 38,980 39,937 40,465 36,899 38,980 39,937 40,465 36,899 38,980 39,937 40,465 36,899 38,980 39,937 40,465 36,899 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38		
94* 14.3 95* 8.0 97* 97* 15 20 25 30 35 40 45 sylveotion Ratio (q.: lit_/min/m) (36) Lut' >6.3 kg//em2	36,391 38,238 39,504 40,207 36,40,3207 36,473 38,274 40,220 36,558 38,497 39,647 40,234 36,726 40,338 36,726 40,338 36,899 38,798 40,428 36,899 38,980 38,997 40,465 36,899 38,980 38,997 40,465 36,998 38,990 38,997 40,465 36,998 38,990 38,997 40,465 36,998 38,990 38,997 40,465 36,998 38,990 38,997 40,465 36,998 38,990 38,997 40,465 36,998 38,990 38,997 40,468 38,990 38,997 40,498 38,990 38,990 38,998 38,990 38,990 38,998 38,990 38,990 38,998 38,990 38,990 38,998 38,990 38,990 38,998 38,990 38,990 38,998 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,990 38,99		
45= 8.0 46= 47= 47= 15 20 25 30 35 40 45 45 20 25 30 35 40 45 45 20 25 30 35 40 45 45 30 25 30 35 40 45 45 30 35 40 45	36,473 38,374 39,575 40,250 36,542 38,497 39,647 40,259 36,726 38,516 39,720 40,338 36,811 38,658 39,867 40,425 36,889 38,980 39,937 40,465 36,889 38,980 40,034 60,498		
90= 97= 97= 97= 97= 97= 97= 97= 97= 97= 97	26,558 38,497 39,647 40,234 36,625 38,516 39,720 40,338 36,726 38,736 39,720 40,338 36,839 38,930 39,937 40,465 36,899 38,930 39,937 40,465 36,899 38,930 39,937 40,465	P7=	• 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
47= 47= 5 20 25 30 35 40 45 6) (36) Lul >6,3 kg/(cm2 >6,3 kg/(cm2	36,642 34,516 39,720 40,338 36,726 34,730 39,792 40,382 36,811 34,588 39,867 40,425 36,889 38,980 39,937 40,465 36,889 38,980 40,604 40,468	P74	<b>8</b> /5
15 20 25 30 35 40 45 hydrotion Ratio (q : lit_min/m) (36) Lut' >6.3 kg/cm2	36,726 38,730 39,792 40,382 36,811 38,858 39,867 40,465 36,889 38,980 39,937 40,465 36,883 39,085 40,098	_	<b>V-7.</b>
15 20 25 30 35 40 45 hydrotion Ratio (q : lit/min/m) (36) Lu' >6.3 kg/cm2	36,899 38,980 39,937 40,462 36,989 36,980 39,937 40,465 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36,990 36		-
15 20 25 30 35 40 45 hyportion Ratio (q : lit/min/m) (36) Lu' >6.3 kg/cm2	36,983 39,085 40,004 40,498	90	
15 20 25 30 35 40 45 hydrotion Ratio (q : lit/min/m) (36) Lul >6.3 kg/cm2	20,700, 37,000, 40,000	 ζω	
15 20 25 30 35 40 45 hypothem Ratio (q: lit/min/m) (36) Lu' >6.3 kg/cm2		20 3/)	
15 20 25 30 35 40 45 hydrotion Ratio (q : lit_/min/m) (36) Lu' >6.3 kg/cm2	ביילים ביולים מסינה בייליה	81	
15 20 25 30 35 40 45 njection Ratio (q : lit/min/m) (36) Lui' >6.3 kg/cm2		•	•
15 20 25 30 35 40 45 hydrotion Ratio (q : lit_min/m) (36) Lut' >6.3 kg/cm2		<b>-</b>	·;
15 20 25 30 35 40 45 njection Ratio (q : lit_min/m) (36) Lu' >6,3 kg/cm2		4	
15 20 25 30 35 40 45 njection Ratio (q:lit_min/m) (36) Lu' >6,3 kg/cm2		m r	
15 20 25 30 35 40 45 njection Ratio (q:lit_/min/m) (36) Lu' >6.3 kg//cm2	90 90 90 20	· ·	-
15 20 25 30 35 40 45 hydrotion Ratio (q : lit/min/m) (36) Lu' >6.3 kg/cm2	742 1 186 703 349	, , , , , , , , , , , , , , , , , , ,	
njection Ratio (q : lit/min/m) (36) Lu' >6.3 kgt/cm2	0.2 0.3 0.4 0.5 0.6	2 20 25 20	20 25 30 35 40 45
(Po)         0.37         1.05         2.07         0.74         0.24         0.24         0.24         1.05         1.05         Lul         Value on value         (36)         Lul           Friction Loss (Pr) = pr (Lo + L.) [kg/cm²]         1.05         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00	13-14 13-26 13-40		
8.3 8.3 8.3	1.05 2.07 0.74	in the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of th	(m/mm/m) (d : m/mm/m)
×63	١.	Luecon value:	
	ä		
	offered agencies double and but dies to stone then me	withing discharge of parties	l
Kemiarks : 10 kgl/cm2 pressure could not built, due to more than maximum dischalge of pump.	13:14   13:20   3:40   13:55   1.05   2:07   0.74   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24   0.24	<del></del>	Water In. Lugeon value: Critical Pressure: tum discharge of pump.

#### Water Pressure Test

4/20 76

Dia. of Hole: Stage:

Dam Axis (Right Bank)

M98-2

Friction Loss per meter (p): 1x(0f x00 ²⁰¹ . Date: 22/December/1993  Ground elevation: EL. m Groundwater tree; (La): Nij Gauge beign (La): 0.366 m bereloit mouth; (La): 0.566 m Calculation of Luggeon value support of the length from pressure gauge to Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Luggeon value Section (La): 0.567 m Calculation of Calculation of Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.567 m Calculation (La): 0.57 m Calculation (La): 0.57 m Calculation (La): 0.57 m Calculation (La): 0.57 m Calculation (La): 0.57 m Calculation (La): 0.57 m Calculation (La): 0.57 m Calculation (La): 0.57 m Calculation (La): 0.57 m Calculation (La): 0.57 m Calculation (La): 0.57 m Cal	•			•										ı
Chound elevation   El.   m   Choundwater [Leve] (Le)    Nij   Chound elevation   El.   m   Choundwater [Leve] (Le)    Nij   Chound elevation   El.   Choundwater guys to   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of lest section   Deph of le	Frictio	n Loss ₁	oer met	(Å)		0 × 0	<u>;</u>		Date:	22/22	cember/19	88		ŀ
Pipe length from pressure gauge to   CL-	Ground	cicvation	급		E	Ground	vater lev	3			Caupe heig	(س)	0.86	F
Secretarian Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Content   Co	Pipe le	ngth from	pressure	უ ამიცმ	Ĺ		Δ	coup of			iğuər T	h of sectio	( <u>1</u>	
Rending of flow meter   Rending of flow meter   Calculation of Luggeon value   Calculation of Luggeon value   Calculation of Luggeon value   Calculation of Large   Pa   Pa   Pa   Pa   Pa   Pa   Pa   P	borehol	e mouth:	3	6.75	E	GL .(I	-	13				S	E	
Compress   Pal			Ren	ling of	now n	heter			Ü	alculation	n of Luge	on value		
1	Gevge P.	-	P.2	3,		P.S	9. 2.	Pa7						
1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5	kg(/cm)		4	-	ı	- 1	- 1	•		<b>一、</b> 个: •		- - - -	/min/m	
V(mm) 5,774-9 5,774-0 5,771-0 0         V(mm) 5,774-0 5,774-0 5,771-0 0         V(mm) 5,774-0 5,771-0 0         V(mm) 5,774-0 5,771-0 0         V(mm) 5,774-0 5,771-0 0         V(mm) 5,774-0 5,771-0 0         V(mm) 5,774-0 5,771-0 0         V(mm) 5,774-0 5,771-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 5,774-0 0         V(mm) 6,774-0 0         V(mm) 6,774-0 0         V(mm) 6,774-0 0	Start time	22	5			77	- [	- 1		7. 9.	E C			
1 5.785.5 5.799.2 5.815.3 5.846.2 5.880.9 5.889.9 77= 8.3 q= 0.25  5 7786.7 5.890.2 5.817.1 5.842.5 5.886.9 5.889.9 77= 8.3 q= 0.25  5 7786.7 5.890.7 5.882.4 5.896.3 5.883.7 5.890.2 77= 8.3 q= 0.23  5 7787.3 5.890.7 5.882.4 5.896.3 5.883.7 5.890.2 77= 8.3 q= 0.23  5 7787.3 5.890.7 5.882.2 5.890.9 5.890.7 5.882.8 5.890.2 7 7 5.789.1 5.820.9 5.870.1 5.870.2 5.890.7 5.890.7 5.890.7 5.890.7 5.890.7 5.890.9 5.800.9 5.870.0 5.885.6 5.890.2 7 2.890.7 5.890.7 5.890.7 5.890.7 5.890.9 5.800.9 5.800.9 5.800.9 5.800.0 5.885.6 5.890.2 7 2.890.7 5.890.7 5.890.7 5.890.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.800.9 5.80	() () ()	5,78	5,78,0	5,813.5	5,838.0	5,8620	5,875.0	5,888.9			4			
2 5,7766.7 5,801.7 5,817.1 5,824.6 5,865.9 5,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,889.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,899.8 7,8		5,785.5	5,799.2	5,815.3	800	5,863.4	5,880.0	S.849.3		ες ; ες ;	ę,			
3 5,7787.3 5,902.9 5,520.7 5,846.5 5,862.7 5,881.3 5,890.3 F75= 8.8 q5= 0.28 5,787.3 5,902.9 5,520.7 5,846.5 5,862.7 5,881.3 5,890.3 F75= 8.8 q6= 0.19 5,787.3 5,902.1 5,822.9 5,820.7 5,848.3 5,890.3 F75= 8.8 q6= 0.19 7 5,787.9 5,902.1 5,822.9 5,820.9 5,820.6 5,820.5 5,820.5 5,820.5 5,820.1 5,870.5 5,882.1 5,870.5 5,882.1 5,870.5 5,892.1 5,870.5 5,892.1 5,870.5 5,892.1 5,870.5 5,892.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,893.1 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,870.2 5,8	ا ا	5,786.1		5,617.1	5.842.5	5,864.9	5,880.9	5,889,8		80	40			
4 5/787.9 5,902.1 5,822.4 5,822.7 5,892.1 5,892.8 5,897.7 5,892.8 5,897.7 5,892.8 5,892.7 5,892.8 5,892.7 5,892.8 5,892.7 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,892.8 5,89	ا :	5, 86.7	5,801.7	5,818.9	5.844.6	5,866.3	5,881,8	5,890.3		87.8	Đ.			
\$ 5,778.5 5,905.3 5,822.4 5,825.5 5,825.1 5,874.2 5,889.1 7 10  \$ 5,788.5 5,905.3 5,822.4 5,825.0 5,872.0 5,889.1 7 10  \$ 5,789.1 5,806.4 5,822.4 5,825.1 5,872.4 5,885.5 5,892.1 10  \$ 5,799.1 5,806.4 5,822.1 5,872.1 5,874.8 5,885.5 5,892.1 10  \$ 5,799.1 5,806.4 5,822.1 5,872.1 5,874.8 5,883.5 5,892.1 10  \$ 5,799.1 5,806.1 5,827.1 5,874.8 5,883.4 5,893.5 10  \$ 5,799.1 5,806.1 5,827.1 5,874.8 5,883.4 5,893.5 10  \$ 5,799.1 5,806.1 5,827.1 5,874.8 5,883.4 5,893.5 10  \$ 5,799.1 5,806.1 5,827.1 5,874.8 5,883.4 5,893.5 10  \$ 5,799.1 5,806.1 5,829.1 5,872.2 5,838.4 5,893.5 10  \$ 5,799.1 5,806.1 5,829.1 5,872.2 5,838.4 5,893.5 10  \$ 5,799.1 5,806.1 5,809.1 5,872.1 5,874.8 5,883.4 5,893.5 10  \$ 5,799.1 5,806.1 5,809.1 5,807.1 5,874.8 5,883.4 5,893.5 10  \$ 5,799.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,809.1 5,	1	5,787.3	5,802.9	5,820.7	5,846.8	5,867.7	5,888	5,890.8		80 i	ģ			
6 5,788 5,805.3 5,802.4 5,825.9 5,870.6 5,885.6 5,892.1 7 5,789.1 5,800.4 5,825.9 5,870.6 5,885.6 5,892.1 8 7 5,789.1 5,800.4 5,825.9 5,870.6 5,887.1 5,872.9 5,885.6 5,892.1 10 5,790.8 5,800.7 5,800.7 5,887.1 5,872.2 5,888.4 5,893.5 5 5,892.1 10 5,790.8 5,800.7 5,800.7 5,887.1 5,872.2 5,888.4 5,893.5 5 5,892.1 10 5,790.8 5,800.7 5,800.7 5,892.1 5,872.2 5,888.4 5,893.5 5 5,892.1 10 5,790.8 5,800.7 5,800.7 5,892.1 5,872.2 5,888.4 5,893.5 5 5,892.1 10 5,892.1 5,872.2 5,888.4 5,893.5 5 5,892.1 10 5,892.1 5,872.2 5,888.4 5,893.5 5 5,892.1 10 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7 5,800.7	'n	5,787,9	5,864.1	5,877	2888		5,887.7	5,891.2		2.8	4/5	_		
7 5,799.1 5,806.4 5,823.0 5,873.0 5,883.0 5,892.1 10 5,790.1 5,809.1 5,879.4 5,893.5 5,893.6 5 5,893.6 5 5,893.6 5 5,893.8 5,799.8 5,899.9 5,893.0 5,899.1 5,879.4 5,899.3 5,899.9 5,899.1 5,879.4 5,899.3 5 5,893.8 5,899.9 5,899.1 5,879.2 5,888.4 5,899.3 5 5,893.8 5 5,899.3 5 5,899.8 5,899.9 5,899.1 5,879.2 5,888.4 5,899.3 5 5,899.8 5 5,899.8 5 5,899.8 5 5,899.8 5 5,899.8 5 5,899.9 5 5,899.8 5,899.9 5,899.1 5,879.8 5,899.9 5,899.1 5,879.8 5,899.9 5 5,899.8 5,899.9 5 5,899.8 5 5,899.8 5 5,899.8 5 5,899.8 5 5,899.9 5 5,899.8 5 5,899.8 5 5,899.9 5 5,899.8 5 5,899.8 5 5,899.9 5 5,899.8 5 5,899.8 5 5,899.9 5 5,899.8 5 5,899.9 5 5,899.8 5 5,899.9 5 5,899.8 5 5,899.9 5 5,899.8 5 5,899.9 5 5,899.8 5 5,899.8 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9 5 5,899.9	ø	5,788 5	5,805,3	5,824.2	5,850.9	5,870.6	5,884.7	5,891.7						
8 5,789.7 5,897.6 5,827.1 5,873.4 5,889.5 5,889.5 5,897.6 5,89.5 1,99.7 5,897.1 5,873.4 5,889.5 5,889.5 5,893.1 5,870.8 5,899.0 5,870.8 5,899.0 5,870.8 5,899.0 5,870.8 5,899.0 5,899.1 5,870.8 5,899.0 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,899.1 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.8 5,870.	1	5,789.1	5,806.4	5,825.9	5,853.0	5,872.0	5,885,6	5,892.1	<u></u>					,
9 5,790.2 5,808.7 5,829.3 5,837.1 5,878.8 5,893.5 5,893.1 5,879.2 5,888.8 4 5,893.5 5,893.1 5,879.2 5,808.8 4 5,893.5 5,893.1 5,879.8 5,809.1 5,879.2 5,808.8 4 5,893.5 5,879.8 5,809.1 5,879.1 5,879.2 5,809.1 5,879.2 5,809.1 5,879.2 5,809.1 5,879.2 5,809.1 5,879.2 5,809.1 5,879.2 5,879.1 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.2 5,879.	· •	5,789.7	5,807.6	5,827.6	5,855.1	5,873.4	5,886.5	5,892.6	_	8	7			
10 5,790.8 5,809.9 5,801.0 5,809.1 5,879.2 5,888.4 5,893.5 24 7 7 12 12 12 12 12 12 12 12 12 12 12 12 12	•	5,790.2	5,808.7	5,629.3	5,857.1		5,887.5	5,893,1	. «с шэ,	٠.				
11		5,790.8	5,809.9	5,831.0	5,859.1	5,876.2	5,838.4	5,893.5	181					
12   13   14   15   15   15   15   15   15   15	11	!			_	i		!	- 40					
Total Out Out Out Out Out Out Out Out Out Out	2	ļ	į	į	į			ļ		<u>`</u>				_
Total Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct   Oct	ב		· •		į	ا	_		. 4	·:				
15   10   10   20   20   30   30   30   30   30   3	ž									`				
Total Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out	1.5		,							•				
11.   5.9   11.5   17.5   21.1   14.2   9.4   4.6   7.5   1   14.5   9.4   9.4   9.5   1   1   1   1   1   1   1   1   1	Total	õ	g	3	į	Ş	ŝ	0						
Average   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Ou	Ä	ŝ	6 ::	17.5	27	14.2	4.0	4						_
1.05   1.19   1.75   1.20   1.75   1.20   1.75   1.20   1.75   1.20   1.75   1.20   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75   1.75	Average		0	0-3	ò	S.	8	0	]					
12-40   12-55   13-07   13-20   13-32   13-45   14-01   Water Injection Ratio (q : lit/min/m)	In Junia	0.50	1.19	1.75	23	1.42	8.0	0.46	0	1 0.2 0.3	0.4 0.5	0.0 0.7 0		
(Pp) 6.00 6.00 0.00 0.00 0.00 0.00 0.00 0.0	mal dam		12:55	13:07	13.20			1		Water Init	, cited acies	100	1	
rinction Loss (Pr) = pr(Lo+L.) [kg/cm2]	(B)	00.0	0.00	900	000	00.00		000					(m)	
(emarks :  (emarks :  Vote: Injection of water should be custimed for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.	notion	Los (Pr)	2)4	3	57/cm2]		1	,	Lugeon	alue:	4.0	3		
(emarks :  Voic : Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute  Settles within 90 % to 110 % of the injection rate in the just previous one minute							3	72		Texsure:	×12	kgC/cm2		
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute verifies within 90 % to 110 % of the injection rate in the just previous one minute	Cemark	ا ا												l
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute						÷								
THE WINDS WITH THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE	.: Jose	Injection	of water	Should !	be contin	ued for	of Jeast 1	D minute	s under the specif	ed pressur	c, after the st	nection rat	c per min	별

Note: Inscrion of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.

Prepared by : A. Hamid & Azhor Inspecified by: M. Suga

Hole No.:	M98-2		Stage:	5/20	훈
Location:	Dam Axis (Right Bank)	ht Bank)	Dia. of Hole:	76 m/m	Ĕ
Hole Inclination (a):		90 degrees	Packer Type: Mechanical	Mechanical	Ho
Friction Loss	Friction Loss per meter (ps) : 1x1 & x0 xm:	0* ×0**1:	Date:	24/December/1998	Fri
					Į

Hole No.	o O		M98-2			$\cdot$		Stage:	5/20			Hole No.:	 
Location:	ou:		Dam A	xis (Ri	Dam Axis (Right Bank)	K	_	Dia, of Hole;	92	m/æ		Location:	ë,
Hole I	Hole Inclination (a):	on (a):	·		8	90 degrees	_	Packer Type:	Mechanical	cəl	-	Hole I	Hole Inclinatio
Frictio	n Loss	Friction Loss per meter (p.) :_	: (১ চু		1×10 ×0121:	:	_	Date:	24/December/1998	er/1998		Friction	Friction Loss p
Ground	Ground elevation: EL	- EL		٤	Groundwater level (Ls):	vater leve	3	Nil	Gauge )	Gauge height (L2): 0.86	œ و	Ground	Ground elevation
Prpc ler	ath from	Pipe length from pressure gauge to	gauge to			ă	of to	Depth of test section	2	Length of section (La)		Pipe len	Pipe length from p
boreho	borehole mouth: (L.)=	3	7.50 m		( <u>1</u>	į	20 m	m to (Lo)= 25		S m		Dorchole	borchole mouth: (
		Read	Reading of flow meter	flow m	eter				Calculation of Lugeon value	geon value			
Company P.	Pet	Pa2	3,	7, ⊆	3,1	8. 4	Pe7	P=P+0 {(sin(s)].+[3).Pv{(kof/cm2]. c=O_f.Ju{lis/min/m}	)	o=O=/1.4 His/min		Gauge P.	₹ -
Ser less	. 6	1	\$21		150	2.5	22.2	P1= 3.3	,	pl= 0.1		New Ima	101:01
Cuma)	_	ı.	049.44	49.50	45 583	49,636	\$ 5	72- 63				Qmin	1.,
,~	49,351	49.378	49,446	49.50H		49,638	49,668					,	51,404
ام!	49,351	49,383	47,451		-	49,64						· ;	51,405
'n	49,352					49,644						r:	\$1,40
*	49,353					\$.54 74.5	49,673			96•		4	5,40
1	66						40.0	E/E				α·\	9,
9,0	49,154							,				• 1	2,40
\.	3			À		20,	200	<u></u>			 [	\! <u>.</u>	5
*	2	2,400		2	4,0		0/0/0	}; ◇				• •	3
i s	2	71.7	00.00	3 5		3,4		 درد				. •	
<b>\$</b>	χ. Σ.				070'4	8	, , , , , , , , , , , , , , , , , , ,	- { 			_	2	1
2	-	-	į	!	1	į	1	i s				::	1 :
<u> </u>			i	1	Ì	!	:	11.2 N				-	i
i, 2	-		ļ	į	:	1		4					:
15.			-		-	:		ຕີ 13 ພຸດ ຊີ້					i
Total	ैं	ç	3	Ş	3	Ş	ટે	1 -				Total	ō,
35.	9	43	53	9	45	_	ž	٠.			_	Ë	œ
Average	_:	6	3	3	ð		ò			,		Average	3
N.C.	9,0			9	Ç.		<u>``</u>		 4	6 7 8 5	 21 6	art/man	ĕ
Finesh tem	5		- 1	<u>?</u>	Ž	5 2	2 2 2	₩.	ter Injection Ra	Water Injection Ratio (g : Jit./min/m)		Kinah tem	¢-50
3	0,00	000	ĩ	0.01	0.01	00.0	3					Ē	000
Friction	Loss (P.	riction Loss (Pr) = pr(Lo + Lo) [kgf/cm2]	3	g//cm2]		Ξ	ī	Lugeon value:	ie: 1.1	ቷ		Friction	rication Loss (Pr)
						•	4	Critical Pressure:	ure: >12	kgf/cm2			
Kemarks	.;				•							Kemarks :	
_											_	_	

#### Water Pressure Test

Californ (a)   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Date   California Da		ş		č	10/ 21/	The Day	3		Die of Moles	ķ	ļ	
	3				200	111	2		יייייייייייייייייייייייייייייייייייייי	9	m/m	
	Hole Ir	ıclinati	( <del>a)</del> uo	•		8	degrees		Packer Type:	Mechani	15	
[ 2 6 경   도급발은	Friction	SSOT II	per met	: (એ) ડા		ig vo	<u></u>		Date:	24/Десешр	cr/1998	
등 현 교육 발문 :	Ground	clevation	: EL		П	Ground	vater lev	٦	27.80	Cauge	height (L.):	98.0
S = 2 E E E	Pipe len	gth from	pressure	gauge to			۵	cpth of to	ı		ength of section	1
도 일 및 유 · · · · · · · · · · · · · · · · · ·	Sorchole	mouth:	Ċ	6.80	£	0Q	i	ž. E	6	<u> </u> 	•	: . 8
<u> </u>			Reak	ling of	flow m	eter			Calc	ilation of Lu	ageon value	
물 발 음 · : : : : : : : : : : : : : : : : : :	Cauge P.	₹.		2	3:	3.		. P.7			,	
[ [ [ [ [ [ [ [ [ [ [ [ [ [ [ [ [ [ [	(renom)	1			ı		4	- 1	P=Pv+0.1(Sin(s)L+F	2)-Pr [kgf/cm2]	. q=0=/-0	/min/m}
e	Shrt lime	_1	=	٤					, d			
- B - 5 - 5 - 1.	Quin O	51,403		51,479					Σ.			
- B 6 5 8 1		\$						_	ŗ			
- B 5 5 8	· '	51,405							P4m	•		
- B 6 5 8	: n	94.4			3,				ŗ	_		
- B 6 5 6 1. 1	*	51,408			51,545				<u>\$</u>			
- B 5 5 8 1. I		51,407			55,15				7	_		
- B - E	•	51,408		51,500	51,559							
- B S S 2	_	\$1,409			51,565							
- B 6 5 - 5 - 2	∞,	51,409			51,570				Ž1		Ź	
- B E E S	φ :	51,410			51,576				93/3	,	<i>!</i> ,	
- B 6 5 8 1. 1	2:	51,411			51,581	51.617			-	ò		
- B 6 5 5 1. 1	3 5	1: ;	;		į		i	j	_	;		
- B = E		i	İ	İ	į	1	-		vn sin	<i>!</i> :		
- B 6 5 8 8 1		:	į	•	ļ	Ī		Ī	Ť			
- B - E - E - I. I		į		Ì		ļ	į					
- B 등 등 등 등   :	106	ä	S	S	Š	ž	Ş	S				
<u> 통통</u> 등 (관 )	≝	œ	ဥ	4	V	2	8	9				
<u>्राह्म</u> ह हि । ।	Avenge	Ö	0-2	5.00	Š	Ş	ŝ		•			]
सि⊒ ह   <del>है</del>	laf /m·m	8.0	2.0	4	5.		8		0,0 0.1 0.	2 0.3 0.4 0.	5 0.6 0.7 0.8	3 0.9 2.
∏ s l€	Finant term	16.20		16:44	16.55	17.0%	×1.7	05.71	-	or fortunation	-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	1
ਨ ਵਿੰ     '	(P)	0.00	0.00	0.00	0.01	0.00	0.00	000	•	e injection s		È
<del>  2</del>	Friction	Loss (Pr	7)24	+ L. [kg	2(/cm2]		4	*	Lugeon valu		ደ	
lê     '	_						2				kgC/cm2	
1 13	Kemarks	 										
1 13												
	ν ο ο	Injection	of water	r should t	Se contro	ned for	it least 1	O minute	s under the specified g	oressure, after th	he injection rate	c per mu
V 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	0				10.00	100	100	ž	ACAMOS CARC HIMMIC			

Note: Inscending water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles, within 90 % to 110 % of the injection rate in the just previous one minute. Prepared by: A. Hamid & Azhor

Hole No.:	M98-2		Stage:	7/20	Hole No.:
Location:	Dam Axis	Dam Axis (Right Bank)	Dia. of Hole:	m/m 92	Location:
Hole Inclination (a)	ttion (a)	90 degrees	Packer Type:	Packer Type: Mechanical	Hole Inclinati
Friction Lo	Friction Loss per meter (p.): 1×10°×01"	1×10+×0-71	Date:	25/December/1998	Friction Loss

Friction Loss per meter (pv):  x    ⁴ x  Ground elevation : EL m   Ground pressure gauge to   CL    borchole mount: (La) = 6.70 m   CL    Reading of flow meter   CL    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Reading of flow meter    Re	1×10,×0,11.		•	0000
ure gauge to 6.70 m cading of flow m			Date:	2)/December/1998
e Nor	Groundwater level (L.); GL-	ا (الم): د	JL. 27.80 m	Gauge height (L.): 0.86 m
6.70 m ading of flow m	۵	cpth of Ic	Depth of lest section	Length of section (L)
Reading of flow me	GL . (L.)-	8	35	e S
-	ter		Calculat	Calculation of Lugeon value
?	Pas Pas	Po7 .		
4 7 10	7 4		P=P++0.1(sin(a)L+1.1)-Pr	PaPa+0.1(sin(a)L+LJ)-Pr{kgf/cm2], q=O+/LJ {lit/min/m}
3:55 14:10 14:25 14:40	14:55 15:10	15-25		qi≖ 0.2
54,004 54,051 54,262 54,747 S	55,343 55,693	55,361		
54,005 54,068 54,302 54,807 5	55,378 55,709	55,866	P3= 9,4	43≖ 7.6
SA. 343 SA. 865	55,412 55,727		P4= 11.8	•
\$4,383 \$4,923	5,447 55,745	55,877		£5= 6.7
54 421 54,980	55,481 55,762			96= 3.5
54,148 54,460 55,039	_		77 3.9	97= 1.2
54,496 55,095	55,549 55,797			
54,012  54,182  54,533  55,149  5	55,581 55,815	55,90	10	
54,196 54,569 55,204	55,613 55,833	\$5,90	21	
\$4,212 54,605 55,260			οο, υ.১,	· <u>·</u>
54,015   54,226   54,641   55,314   5	55,677 55,868	55,921	)81	1
		į	ni o	_
		-	,,	
		:	4	
	1	:	111 . w	
20, 20	3	Š	71	
379 567	_	ફ	·	
ှ ရ	0-0 5-0	٥ ر	0	
37.9 56.7	33.4 17.5	6.0	0 7	3 4 5 6 7 8 9 10
14:05 14:20 14:35 14:50	15:05 15:20	15:35	Water !!	Water Injection Ratio (o : lit/min/m)
0.10   0.48   1.05   0	0.37 0.10	0,01		
Friction Loss (Pr) = pr(L+L) [kgf/cm2]	2	ì	Lugeon value:	8.5 Lu
	511	•	Critical Pressure:	>12 kgf/cm2

#### Water Pressure Test

Stage:

M98-2

Friction Loss per meter (pp): 1st(p ² xQ ² m ² .  Ground clevation: EL    Pipe length from pressure gauge to   Coundorder-level (LJ); GL- Z7.50 m   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation rate per minute   Calculation of value   Calculation rate in the jost   Calculation rate in the jost   Calculation rate in the jost   Calculation rate in the jost   Calculation rate in the jost   Calculation rate in the jost   Calculation rate per minute   Calculation rate in the jost   Calculation rate per minute   Calculation rate in the jost   Calculation rate per minute   Calculation rate in the jost   Calculation rate in the jost   Calculation rate in the jost   Calculation rate in the jost   Calculation rate in the jost   Calculation rate in the jost   Calculation rate in the jost   Calculation rate in the jost   Calculation rate in the jost   Calculation rate in the jost   Calculation rate   Calculation rate   Calculation rate		Hole Inclination (a)	on (B)	·		8	90 degrees		Packer Type:	Mex	Mechanical		
Fige length from pressure gauge to   Cround-nater level (Lu); CLL = 27,30 m   Cround elevation; EL   m   Cround-nater level (Lu); CLL = 27,30 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.36 m   Cauge bright (Lu)   0.37 m   Cauge bright (Lu)   0.37 m   Cauge bright (Lu)   0.37 m   Cauge bright (Lu)   0.37 m   Cauge bright (Lu)   0.37 m   Cauge bright (Lu)   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0.37 m   0	Frictio	ssor] u	per met	g (g	ı	g ×O,	Ë		Date:	27/Dec	cmber/19	86	ŀ
Pipe length from pressure gauge in   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test section   Dopht of test s	Ground	clevation	: EL.			Ground	rater lev	(2)	27.80	6	auge beight	(راز): ا	i I
CL)	Pipe len	ngth from	pressure	gange to			۵	cpth of t	est section		Length	of section	Ĵ
Calculation of Luggeon value   Calculation of Luggeon value   Calculation of Luggeon value   Calculation of Luggeon value   Calculation of Luggeon value   Calculation of Luggeon value   Calculation of Luggeon value   Calculation of Luggeon value   Calculation of Luggeon value   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   Calculation   C	borehol	e mouth:	3	6.73		GL - (L		35 m		£		S	E
Change P   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal			Reac	Jing of	flow m	cter			J	culntion (	or Lugeo	a value	
Comparison   105451   10-12   10-25   10-25   10-25   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12   11-12	Gauge F. (kef/cm.)	_ '	ğ. 4	3, 4	Z. 9	3,	3. 4	Pe7	P=P+0.1(sin(a)1.+	Jay Pe (ket)		átl c.∿_O	(w/wjw)
O(min) 2,952.0 62,856 62,902 63,166 63,700 64,061 72.4 65,70 64,101 72.4 65,00 62,852 62,902 63,106 64,105 74.1 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.4 11.9 67.1 11.9 67.4 11.9 67.1 11.9 67.2 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9 67.1 11.9	Ned In	1	1	10-25	10:3X	10:50	11:402	11.15	E	61	-	0.19	
1 2.842.8 62.860 62.972 63.214 63.772 64.057 64.163	O(min)					63,700	97,026	l٥		6.9	Ġ	8,0	
2 4 2.84.7 62.808 62.908 63.208 64.000 64.170 PS= 9.5 64.4 64.2 64.170 PS= 9.5 64.4 64.170 PS= 9.5 64.4 64.170 PS= 9.5 64.4 65.8 62.808 62.908 63.208 64.300 64.170 PS= 9.5 6.8 62.80  62.800 63.2013 64.208 64.000 64.181 PS= 9.5 64.8 62.808 63.003 64.208 64.000 64.181 64.188  10 2.881.4 62.885 63.003 63.871 63.803 64.100 64.181 64.180 PS= 9.5 64.80 64.100 64.181 64.180 PS= 9.5 64.100 64.181 64.180 PS= 9.5 64.100 64.181 64.180 PS= 9.5 64.100 64.181 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180 PS= 9.5 64.180	_i,					63,732	8,5	_		7.	S	Ž,	
4 2, 244.57 62,272 62,290 63,370 63,531 64,076 64,177 874 5.9 qoe 2.6 2,8 qoe 2.6 2,847.7 62,873 63,013 63,771 63,843 64,190 64,177 874 5.9 qoe 2.6 2,847.7 62,873 63,023 63,273 63,103 64,190 62,884 63,081 63,571 63,873 64,190 62,874 62,896 63,103 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193 64,193	i	2.545.5					8 8					5 4	
\$ 2,846.7 62,875 63,013 63,871 63,895 64,090 64,177 7 77a 3.9 q7a 0.8 47a 0.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4	4	2,845.7					3,6			) <u>s</u>	) <b>.</b>	9	
6 2.8477 (22.879 63.035 63.471 (52.899 64.103 64.188 12 10 1 10 1 10 1 10 1 10 1 10 1 10	'n	2,846.7				63,863	<b>2</b>		3	61		0.8	
7 2,343,7 62,832 63,028 63,520 63,920 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130 64,130	۰	2,847.7				63,895	\$,103	64,181			•		
8 2,840,6 (2,886, 63,081, 63,571, 63,598, 64,130, 64,199, 24, 24, 24, 24, 24, 24, 24, 24, 24, 24	,	2,348.7			63,520	63,927	64,116	_	•		1		
10 2,850,5 62,890 63,120; 63,623 63,900 64,143; 64,199 55 8 8 9 9 10 2,851,4 62,890 63,120; 63,75 64,018 64,157 64,199 55 8 9 10 2,851,4 62,890 63,120; 63,75 64,018 64,157 64,199 55 8 9 10 2,851,4 62,890 63,120; 63,75 64,018 64,157 64,199 55 8 9 10 2,851,4 62,890 63,120; 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,190 64,	•	2,849.6			63,571	63,958	2. 5.			1	: ۱		
10 2,851,4 62,896 63,126 63,675 64,018 64,157 64,199 25 7 9 9 1 1 1 1 2,851,4 62,896 63,126 63,675 64,018 64,157 64,199 25 7 9 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0	2,850.5	62,890			8,9	2.	2		/			
13	۹:	2,851.4	62,896			81018	64,157	<b>2</b> 8		: کې د			
13	= :			ļ			Ī		ci :	٠.			
15	2			1	-	!	Ī		SIU S				
10al   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out	5,2			į		ļ	Ī		4 4				
1044   Qu1   Qu2   Qu2   Qu3   Qu4   Qu3   Qu4   Qu3   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4   Qu4		ļ	1	İ	i i		Ī		41:				
18.   9.4   40   22.4   51.2   31.8   13.1   38   7   6   6   7   8   9   10   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0   10.0	Total	ઢ	Ş	ဂ	ર	ż	ş	o V	NEA				
Note :   Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute   Note :   Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute   Note :   Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute   Note :   Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute   Note :   Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute   Note :   Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute	Œ	I	94	77.7	212	313	Ē	Ä	۸				-
	Vector		Ö	3	3	3	3	ò			٠		,
Priction Loss (Pr) = pr(Lo + Lo) [kg/lcm2]   vs   respect to 10.00   0.10   0.19   0.00   0.10   0.19   0.00   0.10   0.19   0.10   0.19   0.00   0.10   0.19   0.10   0.19   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0.10   0	11/m	1	ı	,	3		- 1		•	n 1	o o	•	,
Friction Loss (Pt) = pt(Lo + Lo) [kgt/cm2]	3	Д.	ľ	91.0	3	32.0	000	000	<b>i</b> *	Vater Injects	On Pario (4	: Sit/min	Ê
Remarks:    Critical Pressure: 8.4 kg/cm2   Remarks:	Friedon	I oss (P.		17.7	1/cm2		3		En devet 1			7	
Kemarks:  Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles, within 30 % to 110 % of the injection rate in the just previous one minute.			<u>.</u>	<u> </u>			3	- 1	Oritical Pre		_	et/cm2	
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles, within 90 % to 1.10 % of the injection rate in the just previous one minute	Kemurk	.;							: :				
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute veitles within 90 % to 110 % of the injection rate in the just previous one minute.													
Thurs Act the IO TO THE INTERCTION FAIR THE DATE	Note :	Injection	of water	blook	De contin	ued for a	i keast 10	) minute	s under the specifie	J pressure, 1	atier the iny	ection rate	per minu
		*	2	9									



Insection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just pressure menute.

**A. Hamfid & Azhor**

Inspected by : A. Hamfid & Azhor**

	xis (Right Bank)	Dia, of Hole:	76 m/m	Location:	22	Dam Ax	Dam Axis (Right Bank)	Bank
ination (a)	90 degrees	Packer Type:	Mechanical	Hole Inc	Hole Inclination (a)	,		90 degrees
Friction Loss per meter (ps): 1x10*x0****	·O, _M ;	Date: 28	28/December/1998	Friction	Friction Loss per meter (pt) :	ster (p.) :	1	1×10+×0,411
Ground elevation: EL. m Grou	Groundwater level (L1): GL.	GL. 27.80 m	Gauge height (La): 0.86 m	Groundel	Ground elevation: EL.	Æ		Groundwater tevel
oj odnež a	Deptho		Length of section (La)	Pipe lengt	Pipe length from pressure gauge to	o agneg o		
٤	₹ (1)	a b(Ls)= 45 a	E	Dorehole n	borehole mouth: (Le)=	6.60 E	٥	<u>ئ</u>
Reading of flow me		Calcula	Calculation of Lugeon value		Ì	Reading of flow meter	low me	
Congge P. Pol Ph2 Pol. Pol Pub. (Agicons) 1 4 7 10 7	5 Pub Pu7	P=Pv+0,1(sin(a)Lv+L2)-P	P=P-+0.1(sin(s)L++L2)-P+[kgf/cm2], q=Q-/L2 [ligmin/m]	(hef/em)	Pul PuZ	₹.	3 2	2. 7 0. 4
11:10 11:22 11:35 11:47	12-00 12:15 12:27	P1≖ 3.9	000	Yeard front	15:30 15:42	200	łş	16:20 16:35
9,700.7 9,702.8 9,703.5	9,704,4 9,717.0 9,722.6 9,724.9	Ž,			1	77,555		1' '
9,700.7(9,702.8(9,703.5(9,703.5(9,71	9,705.5 9,717.5 9,722.8 9,724.9	P.7 9.9	43# 0.00	(		7 582		78,316 78,742
	9,700.0 9,718.0 9,72.0 9,724.9	2 8		7 6	7.00 ( 7.00)	7,610	300	
	0 708 8 0 710 7 0 703 6 0 704 0	2 %	300	. ·		2 4		
_	0 700 0 0 710 H 0 773 0 0 724 9	2		, ,		3 6	_	
_	9,711,1 9,720,4 9,724,2 9,724,9			. 9	: F	77.7		
_	9,712 2 9,721 0 9,724 4 9,724.9	10				77 746		
_	9,713.3 9,721.6 9,724.7 9,724.9			. 20		7.77		
9,700.7 9,702.8 9,703.5	9,714.4 9,722.2 9,725.0 9,724.9			0	• •	7,79		
0 8,700,7 9,702,8 9,703,5 9,715,5 9,722,8	2.8 9,725.2 9,724.9	81 .0		. 10	7,485.4 77,551	7,87	78,768	78,514 78,835
	: :	uj a			<u> </u>		<u> </u>	+
		nus.	-		-		<u>!</u> 	<u> </u>
14		231°		7		İ	<u> </u> 	<u> </u> 
				15			1	
3	3 _,	19,4		_	÷		3	30
0.0 0.0	2.6	1		<u>=</u>	8.4 63	222		Ĺ
0-2 0-3 0-4	9			Average	0-1	6-3	_	١
0.00	0.26	0.0 0.1 0.2 0	0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0	br/min	0.8 6.3	27.2	37.6	22.1 10.3
J 11:32 11:45 11:57	ᅱ	Water	Water Injection Ratio (o : lit./min/m)	Person terre	15:40 15:52	10:04		16:30 16:45
0.00 0.00 0.00 0.00 0.00 0.00	X 0.00 0.00			(a)	0.00	0.35	0.66	0.23 0.05
Friction Loss (Pr) = pr(Lo + Lo) [kgt/cm2]	:	Lugeon value:	(0.0) Lu'	Friction	Friction Loss (Pt) = pr(Lu + Lu) [kgt/cm2]	2 + [] [kgf	(/cm2)	
	A21 X.		9.9 kgf/cm2			•		
Remarks: Reverse flow for 7 seconds by decrea	sang from 7 to 4 kgf/	has by decreasing from 7 to 4 kg/cm2 and for 1 minutes to 1 kg/cm2	1 kgf/cm2.	Kemarks :				
:								
Note: Injection of water should be contained for at least 10 minutes under the specified pressure, after the injection rate per minute sentles within 90 % to 110 % of the injection rate in the just previous one minute.	se contanued for at least 10 minutes under the specified % of the injection rate in the just previous one minute	is under the specified pres- previous one manute	ure, after the injection rate per minute	Note: In	Injection of water should be continued for at least 10 recities within 90 % to 110 % of the injection rate in the	er should be	c continue	for at in
		Department No. C. Ches.	74 Ch. h	To the second	Description A Margin & Author	A	1	

#### Water Pressure Test

76

Dia, of Hole:

Stage:

per meter (p): 1x10²x0³x1?  Date: 29/December/1998  1:EL													
Ground clevation : EL.   m   Groundwater tevel (L.): GL.   27.30 m   Cauge height (L.):	FIGUR	on Loss	per met	er (p)	- 1	it vo	<u> </u>		Date:	29/Decei	mber/1998		
Pipe kingth from pressure gauge to   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test section   Depth of test s	Ground	elevation	.: EL.			Grounds	rater tev	دا ( <b>لـا</b> ): (	27.80	Ö	ge height (I	98'0 :("	١
Paraling of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row meter   Rading of Row   Rading of Row   Rading of Row   Rading of Row   Rading of Row   Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading of Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading Rading	Pipe le	ngth from	pressure	gange to		į	ı	epth of t	ļ	_	Length of	(سا) moi son	i
Reading of Row meter   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair   Pair	borehol	le mouth;	<u>;</u>	6.60		SL-(L		45 m		E		£ 3	
Campa P.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul.   Pul			Reak	ding of	flow m	eler			Calc	culation of	Lugeon v	ज्यात	
Cartiery   15.30   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   15.52   1	Case P		PuZ	Ped	3	3,	9	Po7					
View   15:30   15:42   15:43   16:10   16:35   16:48   16:20   16:35   16:48   16:48   16:30   15:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40   17:40	(wg//cm)			7	10	7	4	1	P=P=+0.1(sin(a)L++	L) P. [kg//cr		/L [lit/mir/	Ē
Q(mm)         7,477.0         77,488         77,585         77,377.2         78,293         78,772         78,823         72=         6.8         q2=         1.3           1         7,477.0         77,482         77,582         78,792         78,772         78,832         72=         9.5         q3=         5.4           2         7,478.0         77,692         78,016         77,902         78,702         77,803         78,702         78,702         77,803         78,702         78,703         77,803         78,903         78,803         78,803         78,803         78,803         78,803         77,703         77,703         77,703         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803         78,803 <td< td=""><td>Kent time</td><td></td><td></td><td></td><td>16:08</td><td>16:20</td><td>16:35</td><td>16:48</td><td>-12</td><td><u>o.</u></td><td></td><td>0.2</td><td></td></td<>	Kent time				16:08	16:20	16:35	16:48	-12	<u>o.</u>		0.2	
1 7,4779 77,492 77,592 77,594 78,316 78,742 78,833 79-8 9.5 9.5 9.5 9.5 75.5 75.5 75.5 75.5 75.	(Olmio)						78,732	78,829	23	80		5	
2 7,478.7 77,499 77,610 77,965 78,333 78,752 78,833 P4= 12.2 q4= 7.5  3 7,485.6 77,507 77,628 78,003 78,361 78,752 78,837 P5= 9.6 q5= 4.4  5 7,483.1 77,220 77,658 78,023 78,023 78,829 78,835 P7= 5.9 q5= 2.1  7,483.0 77,220 77,719 78,120 78,237 78,839 78,835 P7= 5.9 q5= 0.6  8 7,483.1 77,220 77,719 78,120 78,237 78,839 78,835 P7= 5.9 q5= 0.6  9 7,483.6 77,545 77,772 78,129 78,237 78,839 P8,23 P7= 5.9 q5= 0.6  10 7,483.4 77,251 77,227 78,129 78,231 78,839 P8,23 P8,23 P7= 0.6  11 7,485.4 77,251 77,257 78,124 78,231 78,835 P8,23 P8,23 P7= 0.6  12 10 7,483.4 77,251 77,272 78,129 78,237 78,835 P8,23 P7= 0.6  13 10 7,483.4 77,251 77,272 78,129 78,231 78,835 P8,23 P8,23 P7= 0.6  14 10 7,483.4 77,251 77,257 78,129 78,231 78,835 P8,23 P8,23 P7= 0.6  15 10 7,483.4 77,251 77,257 78,129 78,231 78,835 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23 P8,23	· <del></del>	7,17.9					78,742		£	'n		5.4	
3 7,47% 77.507 77,687 78,095 78,837 78,890 78,800 78,361 78,772 78,800 78,772 78,890 78,772 78,890 78,773 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 78,890 7	14	7.478.7					78,752		P4=	2.2		7.5	
4 7,480.4 77.513 77,667 78,044 78,396 78,773 78,893 78,793 78,893 78,793 78,893 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793 78,793	67	7,479.6				78.361	78,762		ž	9		4.4	
\$ 7,481.3 77,520 77,693 78,092 78,497 78,783 78,896  6 7,482.1 77,520 77,719 78,121 78,793 78,895 78,895  8 7,483.8 77,530 77,772 78,129 78,473 78,895  9 7,483.6 77,546 77,799 78,221 78,473 78,885  10 7,483.4 77,551 77,727 78,206 78,514 78,895  10 7,483.4 77,551 77,727 78,206 78,514 78,895  10 7,483.4 77,551 77,727 78,206 78,514 78,895  10 7,483.4 77,551 77,727 78,206 78,514 78,895  10 7,483.4 77,551 77,727 78,206 78,514 78,895  10 7,483.4 77,551 77,727 78,206 78,514 78,895  10 7,483.4 77,551 77,727 78,206 78,514 78,895  10 7,483.4 77,551 77,727 78,206 78,514 78,895  10 7,483.4 77,551 77,727 78,206 78,514 78,895  10 7,483.4 77,551 77,727 78,206 78,514 78,895  10 7,483.4 77,551 77,727 78,206 78,514 78,895  10 7,483.4 77,551 77,727 78,206 78,514 78,895  10 7,483.4 78,514 77,521 78,704 78,704  10 7,483.4 77,521 78,704 78,704  10 7,483.4 77,521 78,704 78,704  10 7,483.4 77,521 78,704 78,704  10 7,483.4 77,521 78,704  10 7,483.4 78,704  10 7,483.4 78,704  10 7,483.4 78,704  10 7,483.4 78,704  10 7,483.4 78,704  10 7,483.4 78,704  10 7,483.4 78,704  10 7,483.4 78,704  10 7,483.4 78,704  10 7,483.4 78,704  10 7,483.4 78,704  10 7,483.4 78,704  10 8,78 8,78 78,704  10 8,78 8,78 78,704  10 8,78 8,78 78,704  10 8,78 8,78 78,704  10 8,78 8,78 78,704  10 8,78 8,78 78,704  10 8,78 8,78 78,704  10 8,78 8,78 78,704  10 8,78 8,78 78,704  10 8,78 8,78 78,704  10 8,78 8,78 78,704  10 8,78 8,78 78,704  10 8,78 8,78 78,704  10 8,78 8,78 8,78 8,78 8,78 8,78 8,78 8,7	. 4	7,480.4				78,384	78,773		<b>*</b> 92	ang.		2.1	
6 7,482,1 77,525 77,719 78,126 78,429 78,793 78,846 10 10 7,483.0 77,546 78,128 78,429 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,24 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249 78,249	, <b>ن</b>	7,481.3	F	77.693		78.407	78.783	78.843	2	6.		9.0	
7 7,483,0 77,533 77,726 78,135 78,435 78,844 78,845    10	· •	7,482.1		•		78 429	78,793					•	
8   7,483,8   77,559   77,772   78,159   78,852   78,855   56   8   9   7,484,6   77,596   77,792   78,131   78,855   56   8   9   7,484,6   77,595   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,525   77,5		7 483 0				78.450	78.804				,		
9 7,484 6 77,546 77,799 78,231 78,855 78,855 51 78,855 10 7,485 4 77,551 77,557 78,328 78,855 51 78,855 10 7,485 4 77,551 77,557 78,328 78,855 51 78,858 51 78,551 77,551 77,557 78,558 51 78,858 51 78,551 77,551 77,557 78,558 51 78,551 78,552 78,553 78,855 51 78,551 78,551 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78,552 78	·, ¤	7 483 8				7	7 8 8		•	ľ	8		٢
10   7,4854   77,551   77,852   78,513   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,853   78,85	ه ه 	7 7 7 7		•		10,0	70 07		-	:}	\		
12	· · <u>· ·</u>	7.485.4				78,514	78.83		-	1			
12					2					Θ.			
13			ĺ	: :					1 21				
14	ü						ij	Ì	nsn			•	
15   Q-1   Q-2   Q-3   Q-4   Q-5   Q-6   Q-7   \frac{22}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{29}   \frac{2}{20}   \frac{2}{29}   \frac{2}{29}   \frac{2}{2}   \frac{2}{2}   \frac{2}{2}   \fra	7				ĺ	-			91 ⁴				
18,	2								ונו טיי				
Average   Q=1   Q=2   Q=2   Q=3   Q=4   Q=5   Q=6   Q=7   Q=7   Q=1   Q=2   Q=3   Q=4   Q=5   Q=4   Q=5   Q=4   Q=5   Q=4   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5   Q=5		33	3:	3 (	3,5	3,5	3 5	ر م	· ··				
Human   0.8   6.3   27.2   27.6   22.1   10.3   2.9   0   1   2   3   4   5   7   8		L	,	,			,	,					٦
Friction Loss (P.) = pr(La+La) [kg/cm2]   10:30   10:45   10:30   10:45   10:30   10:45   10:30   10:45   10:30   10:45   10:30   10:45   10:30   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10:45   10	, i		, ,	;	Š	ŝ	5	, 0	-	,-		× ×	2
(P ₂ ) 0.00 0.02 0.35 0.06 0.23 0.05 0.00 Water injection Kaito (q : It./min/ Friction Loss (P ₂ ) = p ₁ (L ₄ + L ₂ ) [kgf/cm ² ]	Fundah Lim	L	ı	10.00	16:18	16:30	16:45	16.5x					,
Friction Loss (Pt) = pr(Lu + Lu) [kgf/cm2]  Veraits:  Kemarks:  Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate in the just previous one minute.	à	1	ľ	0.35	8.0	0 23	0.05	800	*	ater injection	i Called	(m/m/m)	
Kemarks:  Kemarks:  Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate within 90 % to 1 10 % of the injection rate in the just previous one minute.	Friction	Loss (Pr	7.) ă = <	] [3]	g(cm2)		]	1	Lugeon va			_	
Kemarks:  Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate settles within 90 % to 1 to % of the injection rate in its just previous one minute.							3	-1	Critical Pre			Cm2	
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate settles within 90 % to 1 to % of the injection rate in the just previous one minute.	Kemark	] :;											
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate seriles within 90 % to 1 to % of the injection rate in the just previous one minute.													
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate settles within 90 % to 110 % of the injection rate in the just previous one minute.													
Note: Injection of water should be continued for all least 10 minutes under the specified pressure, after the injection rate settles within 90 % to 110 % of the injection rate in the just previous one minute.													
	 200	2000 S	iot water	should Fro 110	oc contin	ued for a	icast <u>.</u> nrete in	D manute De just	s under the specified previous one minute	pressure, aft	er the injects	on rate per	Ě
Presumed by . A library & Arbor	Dren	2	1	3	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4				Inchested by 1 5		ŀ		١

Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calculation of Calc	cer Type: Mechanical Hole Inc  27.30 m Gauge height (La): 0.86 m Ground el  27.30 m Gauge height (La): 0.86 m Ground el  27.30 m Gauge height (La): 0.86 m Ground el  Calculation of Largeon value Gauge Pape length  Calculation of Largeon value Gauge Pape length  Calculation of Largeon value Gauge Pape length  P1
Date: 30/December/1998  CL- 27.80 m Guuge height (La): 0.86 m  statestion  to (La) = 55 m  to (La) = 55 m  Calculation of Lugeon value  P-P+0.1(sin(a)L+La)-P+ [kgf/cm2], q=O/L-{lit/min/m}]  P2m 6.9 q2m 0.04  P2m 6.9 q2m 0.04  P2m 9.9 q2m 0.06  P2m 9.9 q2m 0.06  P2m 9.9 q2m 0.06  P2m 9.9 q2m 0.06  P2m 9.9 q2m 0.06  P2m 9.9 q2m 0.09  P2m 9.9 q2m 0.09  P2m 9.9 q2m 0.09  P2m 9.9 q2m 0.09	Date: 30/December/1998  CL- 27.80 m Gauge height (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat section (La): 0.86 m cat secti
CL- 27.80 m   Gauge height (La): 0.86 m   Ground	CL- 27.80 m   Cauge height (La): 0.86 m   Ground
California   Langth of section (Lu)   Proper length	Calculation of Lugeon value   S m   Dorchole
Calculation of Lugeon value   Cauge P.	Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calc
P=Pe+0.1(sin(s)L++L)-P+[kgf/cm2], q=O_w/L_{1}[i/min/m]   O_web P_1   O_web P_2   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3   O_web P_3	P=Pe+0.1(sin(s)L++L)-P+[kgf/cm2], q=O_wL_L [it/min/m]   O(min/m)   O(min/m)   P2= 6.9 q2= 0.04   O(min/m)   P3= 9.9 q2= 0.08   O(min/m)   P4= 12.9 q2= 0.08   O(min/m)   P5= 6.9 q5= 0.08   O(min/m)   P6= 6.9 q6= 0.04   O(min/m)   P7= 10 q6= 0.04   O(min/m)   P7= 10 q6= 0.04   O(min/m)   P7= 10 q6= 0.04   O(min/m)   P7= 10 q6= 0.04   O(min/m)   P7= 10 q6= 0.04   O(min/m)   P7= 10 q6= 0.04   O(min/m)   P7= 11 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 12 q6= 0.04   O(min/m)   P7= 13 q6= 0.04   O(min/m)   P7= 14 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P7= 15 q6= 0.04   O(min/m)   P
P1 a 3.9 q1 a 0.01 View by p2 a 6.9 q2 a 0.04 View by p3 a 0.08 View by p3 a 0.08 View by p5 a 9.9 q5 a 0.08 View by p5 a 9.9 q5 a 0.08 View by p7 a 3.9 q5 a 0.00 View by p7 a 3.9 q5 a 0.00 View by p7 a 3.9 q5 a 0.00 View by p7 a 3.9 q5 a 0.00 View by p7 a 3.9 q5 a 0.00 View by p7 a 3.9 q5 a 0.00 View by p7 a 3.9 q5 a 0.00 View by p7 a 3.9 q5 a 0.00 View by p7 a 3.9 q5 a 0.00 View by p7 a 3.9 q5 a 0.00 View by p7 a 3.9 q5 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7 a 0.00 View by p7	P1 a 3.9 q1 a 0.01  P2 a 6.9 q2 a 0.04  P3 a 6.9 q2 a 0.04  P3 a 12.9 q4 a 0.09  P5 a 12.9 q4 a 0.09  P5 a 12.9 q4 a 0.09  P5 a 12.9 q4 a 0.09  P5 a 12.9 q4 a 0.09  P5 a 12.9 q4 a 0.09  P5 a 12.9 q4 a 0.09  P5 a 12.9 q4 a 0.09  P5 a 12.9 q4 a 0.09  P5 a 12.9 q4 a 0.09  P5 a 12.9 q4 a 0.09  P5 a 12.9 q4 a 0.09  P5 a 12.9 q4 a 0.09  P6 a 12.9 a 1.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7 a 12.0  P7
P3 9.9 43 0.08 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2	White Pressure in high course in high control of the high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course in high course i
P4* 12.9 44* 0.00 7.2 P5** 0.00 P6** 0.00 P6** 0.00 P6** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7** 0.00 P7**	Prince 12.9 quantum (Prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12.9 prince 12
P6= 6.9 q6= 0.04 P7= 3.9 q7= 0.00	Water Injection Ratio (q : Itt/min/m)  Lugeon value: 0.1 Lu
20 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000 dy 0,000	Water Injection Ratio (q : 1it/min /m)  Lugeon value: 0.1 Lu
01 20	10 e e e e e e e e e e e e e e e e e e e
	Water Injection Ratio (q : 1it/min/m)  Lugeon value: 0.1 Lu  Friction  Friction  Friction  Friction
	2 2 2 0.0 6.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0 Water Injection Ratio (q : lit/min/m)  Lugeon value: 0.1 Lu
ssure in	Mater Injection Ratio (q : lit/min/m)  Lugeon value : 0.1 Lu
0 N 4 N 6	0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0  Water Injection Ratio (q : lit/min/m)  Lugeon value : 0.1 Lu
in in in in in in in in in in in in in i	Water Injection Ratio (q : lit/min/m)  Lugeon value : 0.1 Lu
Water Pressure in 13 - 13 - 13 - 13 - 13 - 13 - 13 - 13	Lugeon value: 0.1 Lu
Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet Picsourie in Mailet	

#### Water Pressure Test

	Hole Inclination (a)   90 degrees   Packer Type:   Mechanical		ë		Dam A	Dam Axis (Right Bank)	ht Bar	3		Dia, of Hole:		26	E/E		
		Hole In	clinatic	(g) L(			8	degrees		Packer Type		1echanica	_		
[ 2 5 월 14 일 16 일 1		Friction	Loss	SCI DC	(å)		OX b	ë		Date:	31/0	ocember/	1998		
		Ground	levation	3			Ground	vater lev	(1)		E	Gauge he	Eht (La):	98.0	
		Proc leny	th from	pressure	gauge K			٦	epth of t	ction	ŀ	3	th of sectio	(~1)	1
4 2 E E		borehole	mouth:	3	7.60	_	GL - (T	Ļ	.	!	!		8	£	i I
L		L		Reac	ling of	flow m	cter				Calculatio	a of Lug	on value		
E E E	E E E	Care Pa	₹.	72	3,	2 :	3,	8.	/ed:	, , , ,	4 4	i i		1 m/ m/ m/ m/ m/ m/ m/ m/ m/ m/ m/ m/ m/	
E :	E :	î j	-	•		2	- 1	•		Peretti (Sinta	~	'gr/cm-1.		E	
ê :	ê :		2	14.12	14:25	4	2. S.	Š			D.	7			
3 8 5 8 6	: · · · · · · · · · · · · · · · · · · ·		2,953.64	7,955.3	7,955.9	7 956 0	7,956,8	7.58	7.5	6	6.9	42			
3 8 5 8 8	1	~.	0.55	7,955.3	7,955.9	7,956.0	7,956.8	7,936.8	7,956.8	2	6.6	ò			
8 8 8	8 5 3	:	2,953.6	2,955.3	7,955.9	0,986,0	7,956.8	7,956.8	7,956.8	P4=	12.9	4			
8 8 8	8 S S	_	7,953.6	7,955.3	7,955.9	7,956.0	7,956.8	8,986,4	7,956.8	ž.	٥. د	ያ			
8 5	8 5 5 E		7.953.6	7.955.3	7,955.9	7,956.0	7,956.8	7,956.8	7,956,8	ş	6,9	୫			
8 5		. •	200	1 955.7	7 955 0	7 956 0	70%	7 956 8	7.956 K	2	3.9	6			
8 5 6	851 8 3	٥	7,953.6	7,955.3	7,955.9	7,956.0	7,956.8	7,956.8	7,956.8			•			
			200	200	V.60.	2000	000	0.0004,	0.000	_					_
1 1 2 8 5 5 8	851 8 5		0.000	3,5	7.000	2 0	2000	7,550 7,056 x	X 3 4 5 7	_					
8 5 6 6	1 1 2 5 E E S E		953.6	7,955.3		7,956.0	7,956.8	7,956.8	7,956.8	- 6 1,78					
: 1 3 5 5 8 5 .	1 3 8 5 5 8 5	_							i	l ńi • o					_
1 3 5 5 8 8	1 2 8 5 6 6	2			İ	-			İ	۰. ۱۱:e					-
1 3 5 5 6 6	; = 8 5 1 8 B	2	ļ					į		22.3 4					
3 5 5 5 8 6	3 5 5 6 8	4,	Ī	İ			İ		ļ						
S 5 3 .	<u>8 = 1                                  </u>	Tole.	į	3	3	Ş	3	Ş	1	(1) (1)					
8 5 8 6 .	8 5	¥	00	00	0.0	0.0	0.0	0.0		w.					
51 8 B	<b>511 8 8</b>	Average	ë		o G	ş	ŝ	ş	ċ	] •					-
<b>国</b> 8 号 .	<b>国</b>	ii/min	0.0		. 0	0.0	0	٥	0.0	0.0	0.1 0.2 0.3	0.4 0.5	0.6 0.7 0.	8 0.9 1	o.
<b>□8</b>   ₹   .	<b>□</b> 8	Pincells tem	14:10		14:35	ı	15:00	15:12			Water Inic	chon Ratio	(o . iii /mie	(É	
8 3 .	8 3	(b)	000	0.00	000	(10'0	0.00	0.00	0.00					ì	
물 .	urks :  Critical Pressure: >13  urks :  Injection of water should be continued for at least 10 minutes under the specified pressure, after the urestice within 90 ft. to 110 ft. of the injection are in the instrument one minute.	Friction	(Pr)	م).d=	+17)[k	rf/cm2}		1	**	Ingro	value:	0.0	፰		
울 .	를							3		Critical	Pressure:	<u></u>	kgC/cm2		
١.	ļ.,	Kemarks									:				•
١.	l														
		١.	nection	of water	- Provide	ar contra	oct for	I least 1	O minority	s under the spec	ofted pressur	c. after the	Insection rai	2 Oct 10	12

Hole No.: M98-2		Stage:	13/20	Hole No.: M98-2	2
Location: Dam A	Dam Axis (Right Bank)	Dia, of Hole:	76 m/m	Location: Dam,	Dam Axis (Right Bank)
Hole Inclination (a)	90 degrees	Packer Type: Mechanical	Mechanical	Hole Inclination (a)	90 degrees
Friction Loss per meter (ps): 1x10 xQ'nn	1×10*×0'**	Date:	2/January/1999	Friction Loss per meter (pt): 1x10°x0 ¹⁹⁷¹	: 1×10°×0'*7:
Ground elevation: El.	m Groundwater level (	L.): GL- 27.80 m	m Groundwater level (L.): GL- 27.80 m Gauge height (L.): 0,86 m	Ground elevation : EL. m	m Groundwater level (

4=0-/L) [lit/min/m]

-Pu+0.1(sin(a)L+L2)-Pr [kgf/cm2],

8.

. .

3

Reading of flow meter P.J. P.4 0.004 0.016 0.006 0.000 0.000 0.000

44444

5552555

2,939.5 3,939.5

3,933.8 3,937.8 3,938.5 3,939.5 3,939.5 3,939.5

3,930.9

Length of section (L)

Calculation of Lugeon value

E 59

60 m 10 (L)=

CL . (L)-

6.60 m

orehole mouth: (Ls)=

Pipe length from pressure gauge to

Depth of test section

<u>ع</u>

92

Dia. of Hole: Packer Type:

Stage:

14/20

Water Pressure Test

3/January/1999 Mechanical

Date:

#th from pressure gauge to	Pape lengi borehole r	in from	DICKNIE	Paure to	_		Ω	a Jo que	00,000		1	W
Pal   Paz   Pa   Paz   Pa   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz   Paz	borchole r					ļ				-	5	(ATT) LIGHT TO BEST TO
Reading of flow meter   Pal   Pa2   Pa3   Pa4   Pa5   Pa6   Pa7   Pa4   Pa5   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa6   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7   Pa7		mouth:	3	6.70		01 · (I				E		5 m
Pal   Pa2   Pa3   Pa4   Pa5   Pa6   Pa6   Pa6   Pa6   Pa7   Papa011			Read	ding of	flow m	eter			)	alculation	n of Luga	n value
4   7   10   7   4   1   10   7   4   1   10   10   10   10   10   10	Gauge P.	Pol	P.C	Fa3	3	2°S	P.66	Po7				
09-45   09-58   10-10   10-25   10-25   10-20   11-105     17-40-7   17-40-7   17-20   17-20   17-20   17-20   17-20     17-40-5   17-40-6   17-20   17-20   17-20   17-20   17-20     17-40-5   17-40-7   17-48   17-25   17-26   17-26   17-26   17-26     17-40-7   17-40-7   17-20   17-20   17-26   17-26   17-26   17-26     17-40-7   17-40-7   17-20   17-20   17-26   17-26   17-26     17-40-7   17-40   17-20   17-20   17-20   17-26   17-26     17-40-7   17-40   17-20   17-20   17-20   17-26   17-26     17-40   17-40   17-40   17-20   17-20   17-20     17-40   17-40   17-20   17-20   17-20   17-20     17-40   17-40   17-20   17-20   17-20   17-20     17-40   17-40   17-20   17-20   17-20   17-20     17-40   17-40   17-20   17-20   17-20     17-40   17-40   17-40   17-20   17-20     17-40   17-40   17-40   17-40     17-40   17-40   17-40   17-40     17-40   17-40   17-40   17-40     17-40   17-40   17-40   17-40     17-40   17-40   17-40   17-40     17-40   17-40   17-40   17-40     17-40   17-40   17-40   17-40     17-40   17-40   17-40   17-40     17-40   17-40   17-40   17-40     17-40   17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40   17-40   17-40     17-40	(kg/cms)	1	4	7	10	ŗ	4	_	P=Po+0.1(sin(a)	(L+LL)-Pr [k	g(/cm2], q	0.72 [5Vmi
7,743.5 7,746.7 7,748.4 7,751.0 7,756.0 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.	ш	\$5.0	S 53	П	! !	10:35	ı		=	3.9	-16	10.0
7,743,6 7,746,9 7,748,6 7,751,4 7,756.2 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,	O(min) 7	743.5	7.746.7	7,748,4	7.751.0	7,756.0	7,756.6	7,750.6	2	6.9	<b>4</b> 5	0.02
7,743,67,747,07,1748,87,751.97,756.37,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67,756.67	_	,743.6	7,746.9	7,748.6	7.751.4	7,756.2	7,756 6	7,756.6	Ş	6.6	63	8
7,743,7,777,11,7,748,9,7,722,3,7,756,4,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,756,7,7		743.6	7,747.0	7,748.8	7,751.9	7,756.3	7,756.6	7,756.6		12.9	4	0,10
7,443,7,772,2,7,749,1,7,752,8,7,756,4,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,7,756,6,		7.53.7	7,747.1	7,748.9	7,752.3	7,756.4	7,756.6	7,756.6		6'0	\$	0.02
7,443,8 7,747,2 7,749,3 7,753,2 7,756,5 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,	4	743.7	7,747.2	7,749.1	7,752.8	7,756.4	7,756.6	7,756.6		6.9	ģ	000
7,743.8 7,747.3 7,749.5 7,753.7 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.6 7,756.	2	743.8	7 747 2	7,749.3	7.753.2	7,756.5	7.756.6	7,756.6		3,9	20	800
7,743,8 7,747,3 7,749,7 7,754,2 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,	. 9	743.8	7.747.3	7,749,5	7 753 7	7,756.6	7.756.6	7,756.6				
7,743,9 7,747,4 7,749,9 7,754,7 7,756,7 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,	7 7	,743.B	7,747,3	7,749.7	7.754.2	7,756.6	7.756.6	7,756.6	2			
7,744,9 7,747,5 7,750,1 7,755,2 7,756,7 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,6 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,7 7,756,	_	743.9	7,747.4	7,749.9	7,754.7	7,756.7	7,756.6	7,756.6	_			
7,744.0 7,726.3 7,725.8 7,726.8 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.8 7,726.8 7,726.8 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.6 7,726.		,743.9	7,747.5	7,750.1	7,755.2	7,756.7	7,756,6	7,756.6	. « сш.			
0.05 0.09 0.04 0.05 0.00 0.00 0.00 0.00 0.00 0.00		744.0	7.747.6	7,750.3	7,755.8	7,756.8	7,756.6	7,756.6				
0.5   0.0   0.1   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2	=	;		ļ	ļ			į	l oi			
0-1 0-2 0-3 0-4 0-5 0-5 0-5 0-5 0-5 0-5 0-5 0-5 0-5 0-5	12	_		Ì		Ì			) (			
0-1 0-2 0-3 0-4 0-5 0-6 0-7 0-7 0-7 0-7 0-7 0-7 0-7 0-7 0-7 0-7	-	_							nss			
0-1 0-2 0-3 0-4 0-5 0-6 0-7 0-7 0-7 0-7 0-7 0-7 0-7 0-7 0-7 0-7	÷	1	1	İ		-	-		ng.			
0.5 0.9 1.9 4.8 0.8 0.0 0.0 W 1 0.5 0.0 0.0 W 1 0.5 0.4 0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	╀	2	Ş		2	ž	2	,	15;1			
041 Qu2 Qu3 Qu4 Qu5 Qu5 Qu7 005 009 000	•	0.5	0		4	9.0	0.0	<u>.                                    </u>	w			
0.05 0.09 0.19 0.48 0.08 0.00 0.00	Щ.	៊ី	7 0	0	0	S _m O	ទី	o 2	] •			
made and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second sec	4	50.0	0.00	0.19	0.48	90.0	0.00	000	000	1. 0.2 0.3	0.4 0.5 0	5 0.7 0.8 0.
09:55 10:08 10:20 10:33 10:45 11:00 11:15	Punish sens	00-55	10 OK	10:20	10:33	10:45	11:00	31.15		Water land	S Clark Contract	Water Industries Buch to 11st (minute)
(9) 0.00 0.00 0.00 0.00 0.00 0.00 0.00	Н	000	0.00	0.00	0.00	00'0	0.00	0.00		ofine some	CIVE PRINCE	(mannent t
Friction Loss (Ps) = pr(Lu + Lu) [kg/cm2] Lugeon value:	Friction	ON (Pr)	<u>بر</u> 1	1	g(/cm2)		3		Lugeon	value:	0.0	3
an on Critical Pressure:							3			Pressure:	۲ <u>۱</u> ۵	kgf/cm2

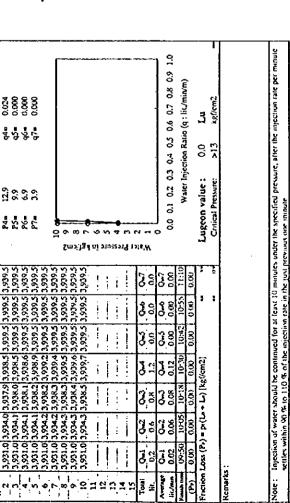
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute veriles within 90 % to 110 % of the injection rate in the just previous one minute.

Inspected by: Farhat M. Shah

Prepared by A. Hamid & Azhor

inspected by: Farhat M. Shah

Prepared by: A. Hamid & Azhor



Hole No.: Location:	M98-2 Dam Axis (Right Bank)	Stage: Dia, of Hole:	15/20 76 m/m	
Hole Inclination (a)	ion (a) 90 degrees	Packer Type: Mechanical	Mechanical	_
n Loss	Friction Loss per meter (pv): 1xt ff xQtm:	Date:	5/January/1999	

eter (pp): 13x10 ⁴ xQ ⁹⁷¹¹ Date: 5/8  m Groundwaler level (LJ): GL. 27,380 m  ne gauge to	Hole Inclination (a)	1 ~		90 des	8	90 degrees		Packer Type:	ا ا	Mechanical	į.	
m Groundwater level (La): GL- 27.80 m Gauge height (La): 0.86  6.70 m GL_l= 70 m to (La)= 75 m Length of section (La)  6.70 m GL_l= 70 m to (La)= 75 m Length of section (La)  6.70 m GL_l= 70 m to (La)= 75 m Length of section (La)  1.2.1 m to (La)= 70 m to (La)= 75 m Length of section (La)  1.2.2 m Length of section (La)  1.2.3 m Length of section (La)  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation of Lugeon value  Calculation value  Calculation of Lugeon value  Calculation value  Calculation of Lugeon value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value  Calculation value	, P	្តថ្ន	( <u>a</u>	1 I	OX j	11.		Date:		5/January/1	666	
6.70 m (cL.)= 70 m (c(L.)=  ding of flow meter    P3	Ground elevation: EL.	1		E	Ground	waler lev	<u>.</u>			Gauge		H
6.70 m GL(L) 70 m to (L) 2  Phy Py Py Py Py Py Py Py Py Py Py Py Py Py	press	Į	Sauge (c			Ω	epth of t	cst section		3	(山) ngth of section	
27, 570, 570, 570, 570, 570, 570, 570, 57	torehole mouth: (L)=		6.70	£	ם. ים		: 1	(o (Le)=		_	E 5	
Smo')gd ni stuezen 9 teta W	×	Ě	Jing of	flow n	refer				Calcula	tion of Lu	geon value	
Smo'lga' ai stuczen' a tera' W	Pal Pa	~		7.	PuS	P.6	Pu7					
Smo'lga' in succent neil W	. *	:	-	01	^	4	-	P=Pe+0.1(Si	P(a)L(+).	'r [kgf/cm2],	Q=O-/\-O=b	Ē
Smr3)gd ni succest sinw	11:55	12.0%	I	ŀ	l	ı	i	Δ,		•	1= 0.02	
Smothat in street 91 and 1844	7,662,4 7,667,2	27.2	7,670.5	7,675.0	7,683.5	7,088.1	0,169,7	P.		•		
Smo'lgå ei stuczen a tera W	<u> </u>	67.3	7,670.8	7,675.6	7,683.8	7,688.5	7,691.1	Þ.		or		
Smo'lga' in success? 1218W	7	67.4	7,671.1	7,676.3	7,684.2	7,688.8	7,691.2	ă.		σ		
Smo'dga'ni suszang tataW	7	67.5	7,671.4	7,677.1	7,684.6	7,689.0	7,691.3	ĸ		0		
Smr)ggl ni stuzzang neraW	7	67.6	7,671.7	7,677.9	7,685.0	7,689.2	7,691.4	æ		3		
Smo')gd ni suuzang setaW	7	57.8	7,672.0	7,878,7	7,685.4	7,689.4	2,69,7	Σ.		o		
Sm2)ga in success? 121W	2	62.9	7,672.3	7,679,5	7,685.8	7,689.6	7,691.6					
Smoothal oi success? The W	2.	68.0	7,672.6	7,680.3	7,686.1	7,689 8	7,691.7	0.				ſ
malgal ei suszeng netsW	3	3	767.9	7.681.1	7,686.5	7,690.1	7,691.8	21	••			
Dga ni suozzara neraW	?	83	7,673.7	7,681.8	7,686.9	7,690.3	7,691.9	us,	••			
l di suggest istaW	š	3	7,673.6	7,682.6	7,687.2	7,690.5	7,692.0	181	-		-	
0.3 0.4 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5		1		į	ا	ĺ	1	i ni	٠٠			
0.3 0.4 0.5 0.5 0.7 1.0 0.0 0.00 0.00 0.00 0.00 0.00 0.	į	i	1	į	i	į	;	11¢	<u>.</u>			
0.3 0.4 0.5 0.0 0.10 0.00 0.00 0.00 0.00 0.00 0	1	-		:		,	,	1551				_
0.31 0.44 0.45 0.45 0.77 0.71 0.71 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75		,	-				İ i	ng 1	,			
3.1   7.6   3.7   2.4   1.0   # 1   Q-3   Q-4   Q-5   Q-6   Q-7   Q.31   Q.76   Q.29   Q.20   0.10   12.30   12.48   3.10   13.23   u.00   0.00   0.00   0.00	2	'n	3	3	3	Ş	à	51 <b>1</b> ,				
0.3 0.4 0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	1	i cı	-	7.6	,,	2,0	0	~ ·			•	
0.31 0.76 0.37 0.24 0.10 (12:30 12:45 12:58 13:10 13:23 0.00 0.00 0.00 0.00 0.00	0	~	Ö	9 Z	Ş	Ŷ	0	0				1
(i 12:30 12:45 12:58 13:10 13:23 0.00 0.00 0.00	ď	12	0.31	0.76	0.77		0.10	õ	0.1 0.2	0.3 0.4 0.5	0.6 0.7 0.8 0.9	0
0.00 0.00 0.00 0.00 0.00	12:05	12:1H	12:30	12:45		_1	- 1		Water	Injection Rati	io (q : lit/min/m)	
	Ö	0.00	0,00	0.00	0.00	0.00	8					
						3	*	Š	ical Pressure		kgf/cm2	I
Critical Pressure: 8.7	l	ļ										

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 30 % to 110 % of the injection rate in the just previous one minute.

Prepared by: A., Humid & Azhor.

[Inspected by: Farhat M. Shah]

#### Water Pressure Test

Hote Inclination (a)   90 degrees   Packer Type: Mechanical	Location:	į		Dum A	xis (R	Dam Axis (Right Bank)	ık)		Dia, of Hole:		76	ш/ш	
per meter (pv): 1   1   1   1   1   1   1   1   1   1	Hole In	clinatio	(a) Ci			8	degrees		Packer Type:		chanical		
Propertion (EL.   m.   Groundwater [see] (LJ); GL.   27.80 m.   Gauge height (LJ); GL.   27.80 m.   Chauge height (LJ); GL.   27.80 m.   Chauge height (LJ); GL.   27.80 m.   Chauge height (LJ); GL.   27.80 m.   Chauge height (LJ); GL.   27.80 m.   Chauge height (LJ); GL.   27.80 m.   Chauge height (LJ); GL.   27.80 m.   Chauge height (LJ); GL.   27.80 m.   Chauge height (LJ); GL.   27.80 m.   Chauge height (LJ); GL.   27.80 m.   Chauge height (LJ); GL.   27.80 m.   Chauge height (LJ); GL.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.   27.80 m.	Friction	Loss	er met	( <u>a</u> )		10,00	,,,,		Date:	7/Jan	uary/19	8	
Proper length from pressure gauge to berth of Lesi section	Ground	levation	: EL		E	Ground	water lev	دا (ک)	27.80		Jauge heis	(P)	0.86
Parechole mount: (L)= 6.75 m   O(L.(L)= 75 m to (L)= 80 m   Calculation of Lupeon value	Pipe len	th from	pressure	gange (c	•		ı	epth of t	ction	-	2,1	h of section	(ساً) د
Reading of Row meter   Reading of Row meter   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of Largeon value   Calculation of	borehole	mourh: (	វ្នំ	6.75	E	<u>5</u> , (1	<b>.</b>		!	E		s	: :
Common   1			Reac	ting of	flow n	reter				alculation	of Luge	on value	
Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue   Continue	Course P.	P.	Pa2	3.	Ą	P.65	:	Pb7				,	
State   10:20   10:22   10:25   11:10   11:23   11:25   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:45   11:4	(KE(Icms)	-	4		2	ı	- 1	- 1		(*; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;		1	להישוש)
(wm) 8,135.9 (8,139.2 (8,142.2 (8,147.0 (8,139.7 (19.27))	_	10:30	10:42	10:55	=			1.4%		ų,	÷		
1 8,126.0 8,1322 (8,140.1 8,142.6 8,147.2 8,149.7 8,149.7 8,149.7 8,149.7 8,149.8 1,140.3 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,143.6 8,14		8,135.9	8,138.0	8,139.9	8,142.2	8,147.0	8,149,6	8,149.7		6.9	Ş		
1, 136.2   8, 138.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3   8, 140.3		3,136.0		8,140	8,142.6	8,147.2	8 149 7	8,149.7		66	9		
4 8.136.2 8.138.4 8.140.5 8.142.6 8.143.7 8.143.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.145.9 8.14		8,136,1	8,138.3	8,140,3	8 143.0	x,147.5	8,149.8	8 149.7		12.9	ş		
4 8,136.5 8,138.6 8,140.7 8,143.8 8,140.0 8,140.8 8 PG= 6.9 qG= 0.02 8 8,136.5 8,138.8 8,141.0 8,144.7 8,148.8 8,150.1 8,149.8 PT= 3.9 qG= 0.02 8 8,136.5 8,138.8 8,141.0 8,144.7 8,144.8 8,150.3 8,149.9 PT= 3.9 qG= 0.02 8 8,136.8 8,139.8 8,141.2 8,144.7 8,144.2 8,140.9 8,130.9 8,149.9 PT= 3.9 qG= 0.02 10 8,136.8 8,139.8 8,141.2 8,144.7 8,144.8 8,150.5 8,149.9 PT= 3.9 qG= 0.02 110 8,136.8 8,139.8 8,141.2 8,144.7 8,144.8 8,150.5 8,149.9 PT= 3.9 qG= 0.02 110 8,136.8 8,139.8 8,141.2 8,144.7 8,144.8 8,150.5 8,149.9 PT= 3.9 qG= 0.02 111	_	8,136.2	8,138.4	8,140.5	8 43.4	8,147.7	8,149.0	8,149,8		6.6	ò		
S   13.56. S   13.87 S   14.09 S   144.3 S   15.01 S   148.5 S   15.00 S   14.00 S   144.3 S   15.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S   14.00 S	-	8,136.3	8,138,6	8,140.7	8,143.8	8,148.0	8,150.0	8,149.8		6.9	ģ		
6 8,135.6 8,138.8 8,141.0 8,143.8 18,150.2 8,149.9 10		8,136.5	8,138.7	8,140.9	8,144,3	8,148.3	8,150.1	8,149.8		3,9	ò		
R. 1356, R. 1390, R. 1412, R. 1454, R. 1454, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R. 1450, R		8,136,6	8,138.8	8,141.0	8,144.7	8,148.5	8,150.2	8,149.9					
8 8.1356 98,1392 8,1343,8 1,4347,8 1,434,8 1,530,4 8,1303	<u>-</u>	8,136.7	8,139.0	8,141.2	8,145.3	8,148.8	8,150.3	8,149,9	_				
10   8,137,0 8,139,4 8,141,7 8,140,2 6,149,4 8,140,0 8,130,0 8,130,0   2,131,1 8,140,2 6,149,4 8,141,7 8,140,2 6,149,4 8,140,0 8,130,0   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1   2,131,1	∞'	8,73		8,141.5	8,145.7	8,149,1	x, 50 4	8,149.9	•				*****
12		700.1	7	0,141.7			0,000	7.001.0					
Total   Co.   1.0.2   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.   Co.		2	1				3	2					
13	-2	-				١	İ		ii s				r.a
13   14   14   2.0   2.0   2.4   2.6   1.0   0.3   2.5   1.0   0.3   2.5   1.5   0.0   0.1   0.2   0.3   0.4   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0	12	ĺ	Ī					Ĺ	102				
15   10   10   10   10   10   10   10	7	Ī	ĺ	!	-		اً		231 4				
Total   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Quality   Qualit	15	İ	Ī			İ	İ		415				
11.   1.4   2.0   4.5   2.6   1.0   0.3   0.4   0.3   0.4   0.3   0.4   0.5   0.4   0.3   0.4   0.5   0.4   0.5   0.4   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5	E S	ઢ	į,	3	3	3	3	ò	N				
Average   O+1   O+2   O+3   O+4   O+5   O+6   O+6   O+7   O+6   O+7   O+6   O+7   O+6   O+7   O+6   O+7   O+6   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+7   O+	Ξ	=	2	20	\$	2.6	- 1	٥	۸				
	Average	~ 0,	77.	7	9	0		6	3				<u>:</u>
Priction Loss (Pr) = pr(La + Lr) [kg/[cm2]	EL/10		:	3 5			2		3	7.7.	3	3	2.7
Friction Loss (Pr) = pr(Lo+Lo) [kg/(cm2] = 4 Critical Pressure: 9.5 kg/(cm2 Remarks:  Remarks:  Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute vertiles within 90 % to 110 % of the injection rate per minute.	1		2			Т.				Water Inject	on Ratio	(q : lit./min	Œ/
Remarks:  Remarks:  Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute vertiles within 90 % to 110 % of the injection rate per minute.	100					3		1	,		60	·	
Remarks:  Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute veilles within 90 % to 110 % of the injection rate per minute.			i i	<u> </u>	( all 1 )		2		Critical		) (2) (3)	kef/cm2	
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute within 90 % to 110 % of the injection rate in the just previous one minute	Remarks												
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute veiller within 90 % to 110 % of the injection rate in the just previous one minute													
within 90 % to 110 % of the injection rate in the just y		nyection	of water	planots	be confir	ned for	of least 1	0 minute	s under the speci	fied pressure,	After the	nyection rat	e per minute
		3	o uu	200					****	•			

			-	-	
Hole No.:	M98-2		Stage:	17/20	Floie No.:
Location:	Dam Ax	Dam Axis (Right Bank)	Dia. of Hole:	Dia. of Hole: 76 m/m	Location:
Hole Inclination (a)		90 degrees	Packer Type: Mechanical	Mechanical	Hole Inclination (a)
Friction Loss	per meter (p.) :	Friction Loss per meter (p): [x] f'x0'm:	Date:	14/January/1999	Friction Loss per met
	1		00 00	200 C 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0

	£			-		<u></u>							-	ſ							-					0.1.0				-7
\$	رات) 0.86	Length of section (L.)	5	n value		Q=O=/L> (BVmin/m)	900	0.11	0.25	0,15	80.0	0.05														0.7 0.8 0.5	(m/orm/ ij.		. 3	, magazina
14/January/1999	Gauge height (Lz):	Length		Calculation of Lugeon value				e e	45	<b>-</b> 5p	90	<b>-</b> 20														0.4 0.5 0.6	Water Infection Ratio (n - lit (min/m)		(0.1)	
14,	E		85 m	Calculatio		F=Fo+U.1(sin(a)Li+L2)-Fr {Kgt/cm2}, P1- 10							•		:	::	4	٠.		•						0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0	Water In		Lugeon value:	Critical Pressure
Date:	Groundwater level (L.): GL- 27.80 m	Depth of test section	m to (La)=											01	71	υ 3) Έ	18:	l ni	91:	nss	319	13	18,4	۸	>	0:0			Luge	Centre
	(1)	cbip of	80		_Pv7	1	14		8,661,196.6 1,199.8	1,190,1 1,197,0 1,200,0	1,200.3	1,200.5		0.102,1	202		3.102,1	:					6	2.5	o C	0.25	11.58	U UO	Å.	-:
	ater lev	Δ	3		P.	11.36	138.0 1.195.8	1,196,2	1,196.6	1,197.0	1,190.8 1,197.3	1,197.8	1,198.1	1,198.5	7.861		1,199,7			;	. :		3	3.0	ş	0.39	11:45	0.00	:	•
o v	Groundy		GL - (L	eter	٠.	7 1.	1.138.0	1,188,7	1,189.3	1,190.1	1,190.8	1,191.6	1,192.3			1,194.6	1,195.5	:	:				ટુ	7.5	Š	0.75	11:33	(K)(0		
×	Ε			flow m	3	2	13	1,176.5	1 1778	1,179.0	1,180.2	1,181.5	1,182.7	18:0	1.185.2	1,186.5	1,187.8	į					ş	12.5	3	33	11:20	0.00	(/cm2)	
 (§)		o) oSneR	3.80 m	Reading of flow meter	3	7	1.167.5	1,163.9 1,168.1 1,176.5	1,168 6	1,169	1,169.7	1,170.3	1,170.K	5.4.7	6.171,0.001,	1,172.5	1.53.1	ļ	!				3	2.6	ð	8	11:05	00.0	را الاها	
Ţ	13	Pipe length from pressure gauge to	3	Rend	P82	4 5	2,163,61,167,5	1,163.9	1,1642	1,164.6 1,169. 1,179.0	1,164.9	1,165.2	1,1655	1,165.7	166.0	1,166.3	1,1665 1,173.1	-	į	. !			3	5.0	Ö	0.20	10-52	00.0	Priction Loss (Pt) = pr (Lo + L.) [kgf/cm2]	
) E	1	_	-			7			1,160.2	1,003	1,1603	160.5	1,160.8		1,161.5	1,161.9	1,162.2		j				į	-7	3	0.21	10:40	00.0	٤	
Friction Loss per meter (p.): 1x1 ff xQ ^{m;}	Ground elevation: EL	gth from	harehole mouth: (Ls)=		P.	1	O(min) 1,160.1	ž	3	ž	Ĕ	Ē	Š	Ţ	Ž	3	.,	,	!			1	0	$\sim$	Ó,	0	ř	ō	Ś	

Note: Injection of water should be continued for at least 10 nitrates under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just prevaux one moute.

Prepared by: A. Hamid & Azhor

#### Water Pressure Test

Location:	ë.		Dam A	xis (Ri	Dam Axis (Right Bank)	ž		Dia. of Hole:	76		m/m		- 1
Hole In	Hole Inclination (a)	(m) uo	•		\$	90 degrees		Packer Type:	Mechanical	nical			
Friction	Sol	Friction Loss per meter (p.)	ر را را	×	1×10,×0,**1:	31.		Date:	27/January/1999	61/23	8		- 1
Ground	Ground elevation: EL	: EL.		E	Ground	valer lev	Groundwater level (L.); GL-	5L- 32,40 m	Gaug	e beig	Gauge height (La):	98.0	1 !
Pipe len	ուր from	Pipe length from pressure gauge to	gauge to			۵	epth of t	Depth of test section		Lengt	(will of section (Lu)	(m)	
borehole	borehole mouth: (La)=	3	4.10 m	E	GL -(L)-	1	85	m to ([)= 90	E	ř	S	E	
		Rea	Reading of flow meter	flow m	eter			Ö	Calculation of Lugeon value	2007	on value		
Cauge P.	164	Po2	3.	3.5	3.	<u>3</u>	Pu7	1/*/=;=/1 O O O				1	
(ALL)	Ī	,		3	,	,	1	יייייייייייייייייייייייייייייייייייייי	e e e e e e e e e e e e e e e e e e e				-
Nied Line		ž	ċ	,,,,,			Y:03						
(mm)	9,316.0	8,316.0 3,324.0	8,332.0	8,339.0	3,480	8,352.0	8,339.0 8,348.0 8,352.0 8,356.0	Ė	7	7			
	8,316,3	8,324,3	*,333.1	8,339,9	8,339,9 8,348,5	8,352,3	8,356.2	<u>.</u>	10.3	ģ			
۲۷.	8,316.8	8,316.8 8,325.0		8,340.6	8,348.9	8,352.7	8,352.7 8,356.5	P4	13.3	4			
۳,	8,317.5	8,325.5		8,741.5	8,334.0[8,341.5]8,349.5	8,353.0	8,353.0[8,356.7	<b>₽</b> \$4.	10.3	5	0.10		
4	8,317.9	8,317,9 8,326,1	8.334.6 8.342.2 8.349.9 8.353.5 8.357,1	8 342.3	8,349,9	8,353,5	8.357.1	₽6 <b>=</b>	7.3	90	0.07		
· v	81.18	2 30 K	A OST RIO FOR XIO SEE X	N X	200	K 151 R	K 353 R 4357 A	2		2			
. ,		1			2000				)	) •			
	100	X 727 K	7	7	3.1.2	3	3.5						
oc i	301.8	X 72 X O	X 3.76 A	X XX X	X 251 X	X 354 X	A 351 X 354 X X 258 X	2 6					_
	X 010 K	4 328 4	X 7.7.7	X 46.6	8 352 4	8 355 3	8 358 8						
: _	1201	8,328.0	, 137.	8 747 3	8 352.8	8.355.6	8.355.6 X.359.1	- 6 - 6 - 7 - 7					
				ļ'				10					
2:					1			i s					
!:	!		į	-			Ì						
3, 2	İ		į	!	İ			4					_
	İ	j	į	-	ĺ	ĺ		n n					
ē	Į	١	2	2	Ž	Į	ŝ	31s C1					_
2	, ,		, ,		) a	,	:	 M					
		,	,	ļ	Ç	ć	ļ	•		1			٦.
	53	200	ž	5	3 3	, ×	;	1000	01 02 03 04 05 05 07 08 00 10	Ç.	20.40	000	
4	7.77	Ŀ	ç	16.70		K > . Y							:
(-0)	1	L	á	000	1	5	Į.		Water Injection Katio (q : ht/min/m)	2	4: iit/mir.	Ê	
		$C_{\alpha}(\alpha_i,\alpha_i) = C_{\alpha_i}(\alpha_i) + C_{\alpha_i}(\alpha_i)$						T management	£ C	_	;		
		<u> </u>	ì	(4III-):		i 2	•	Colinal Designation		ء د	3		
Kemarks	1							Christian			7800		ı
Note :	Injection	of wale	should a	be confir	of pan	i lensi 1	O minute	Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute	d pressure, after	F.	jection rate	E Jod o	1 C

Friction Loss per meter (pv): 12x  Ground elevation: EL m  Pipe length from pressure gauge to borchole mouth: (La)w 4,15 m  Gauge P. Pul Reading of flow in Gauge P. Pul Pul Pul Pul Pul Pul Pul Pul Pul Pul	Friction Loss per meter (p): 1x    Ground elevation: EL   m     Pipe length from pressure gauge to	Friction  Ground Pipe leng Dorchole  Gwege P.  Gwege P.  Start time Of minip	Friction Loss per meter (p) : 1810
Friction Loss per Ground elevation : Pipe length from pr Dorehole mouth: (L Gouge P.   P41			99  In (La): 0.86 m  S m  S m  S m  S m  S m  S m  S m
Pipe length from pr Pipe length from pr borehole mouth: (I. Gweger: 1942	[S] [S] [S] [S]	[SIZ B] 10 C]2	[S]
Pipe length from pri borehole mouth: (L. Gauge P. Pri			
Governole mouth: (I.			
Gauge P. Put		10 0121	
Gauge P. 1942 Pa2 Pa3 (AgGens) 1 4 7	<u> </u>	<u> </u>	<u> </u>
(Agilem) 1 4 7			
	000	0000	0000
000000000000000000000000000000000000000	0.00	00'0	
888888888888888888888888888888888888888	000	0.00	00.00
888888888888888888888888888888888888888	0.00	000 000 000 000	0.00
888888888888888888888888888888888888888	000	0.00	0.00
88888888	000 000 000 000 000 000	0.00	000 000 4 N 0 V
8888888	000	000	000 000 000 000
888888	0000	0000	0.00
8888888	000	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	000 000 000 000 000 000 000
8888888	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00	000 000 000 000 000 000
888888	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	000 000 000 000 000 000 000 000 000 00
8888888	000 000 000 000 000 000 000 000 000 00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	000 000 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
888888	000 000 000 000 000 000 000 000 000 00	000 000 000 000 000 000 000 000 000 00	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
888888	000 000 000 000 000 000 000 000 000 00	000 000 000 000 000 000 000 000 000 00	8 8 9 9 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

## Water Pressure Test

20/20 92

Stage:

30/January/1999 Mechanical

Date:

Packer Type:___ Dia, of Hole:

90 degrees

Proceeding the from pressure gauge to a control of Lagran (La) = 100 m   Langth of section (La) = 100 m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S m   S									Official which in very (acr), one of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of		CAUSE NEIGHT (Aut)		3	E
Reading of flow meter   Reading of flow meter   Reading of flow meter   Calculation of I	og se	gth from	pressure	gauge to	_		۵	epth of t	icsi section		Length.	noites jou	Ĵ	
Reading of flow meter   Reading of flow meter   Reading of flow meter   Reading of flow meter   Reading of flow meter   Reading of flow meter   Reading of flow meter   Reading of flow meter   Reading of flow meter   Reading of flow meter   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Reading of flow   Read	orchol	e mouth: (	3	4.15	E	01-0		95 "	n to (1,)=	.		2		
Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Parameter   Para			Reac	ling of	flow n	reter				Calculati	on of Lugeo	yn value		İ
Umino   1,138,   1,041,   1,132,   1,131,   1,132,   1,134,   1,132,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,134,   1,13	Cauge F.		53, 4	,		3.	31.	1	-/- (V. BB	G (* 4.7. 100)**			1	
0(min) 7,138.8 7,941.8 7,942.8 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4	1	L	15	17:21	ŀ	_				1 ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (			(maxima)	
7,138.8 7,941.8 7,942.8 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,94	(aid)		7.941.8	7.942.8		7 943.4	11	10			1 1 7 6			
2 7,138.8 7,941.8 7,942.8 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,94		7.138.8	7.941.8	7.942.8		7,943.4	7,943.4				· C	000		
7 7,138.8 7,941.8 7,942.8 7,942.8 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,94	N	_	7.941.8	7.942.X	7.943.4	7,943.4	7,943.4	7.943.4			8	8		
4 7,138.8 7,941.8 7,942.8 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,94	ا س	7,138.8	7. X. 8	7,942.B	7,943.4	7,943,4	7,943.4	7,943.4			à	000		
5 7,138.8 7,941.8 7,942.8 7,942.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,94	4	7,138.8	7,941.8	7,942.8	7,943.4	7,943,4	1953.4	7,943,4			. 90	80		
6 7.1188 7,941.8 7,942.8 7,942.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943	s	7,138.8	7 941 X	7,942.8	7,943 4	4.5%	7,943.4	7.847.4			6	8		
7 71388 7,941.8 7,942.8 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.	۰	7,138.8	2,81.8	7,942,8	7,943,4	7,943.4	7,943.4				•			
8 7,138.8 7,941.8 7,942.8 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,94	~	7,138.8	7,941.8	7,942.8	7,943.4	7,943,4	7,943.4	7.943.4	2					
9 7,138.8 7,941.8 7,942.8 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,943.4 7,94		7.138.8	7.941.8			7,943.4	7,943.4	4.84.7	_					
10	•	7.138.8	7,941.8	7,942.8	7.963	7 23.4	7.943.4							
11   12   13   14   14   15   15   15   15   15   15	0	7,138.8	7.21.8	7,942.8	7.00.7	7,043,4	7,943.4	7 243.4	•					
12   13   14   15   15   15   15   15   15   15	1			:		:	!	:						
13	2	į	!				ĺ		31					
154	7	1	!	1			-	i	uss	•				
15   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Cal.   Ca	7		i		į	į		İ	234					
Total   Q-1   Q-2   Q-3   Q-4   Q-5   Q-6   Q-6   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-7   Q-	2								(1) (1)				-	
It.   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0	Total	3	Z	3	3	ટ	3	ģ	18,4				•	
Annete	Ē	0.0	00	0.0	0.0	0.0	00	0.0	- ·					
State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   Stat	Average	ੌਂ,	- -	S.	3	ð	Ŷ	ઠે	o '				]	
	lit/min		8	8	8	-1	8	8		0 0.1 0.2 0.	3 0,4 0,5 0,	6 0.7 0.8	0.9	_
finding Loss (Pr) = pr(La + L.) [kg/cm2]  ** 12 Critical Pressure: 0.0 La  Critical Pressure: >13 kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm2  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/cm3  kg/c	e i	L		17.20	7:37	- 1	<u> </u>	Š		Water In	jection Ratio (c	/uim/iii : p	Ē	
formarks:    Critical Pressure: 0.0 Ltd   Critical Pressure: 5.13 kg/cm.2		3	3	3		00%	3	3	·		•			
Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemarks:  Kemark	5	3	3	÷ ₹	E/CH		3	7	Î	con value :		3		
Kemarks:  Note: Injection of water-should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute veitle within 50 % of 110 % of the injection rate in the just previous one minute.			į			•	2	ŗ		tical Pressure:		kgf/cm2		
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute verther within 50 dt 110 dt of the injection rate in the just previous one minute.	Kemark	:												ı
1   3														
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute within 90 % to 110 % of the injection rate in the just previous one minute.														
A Line A P. Author	l	Injection	of water	hould !	be contain	ned for	it least 10	D minute	s ander the s	specified pressu	are, after the un	jection rate	per min	쏲
			5						100000	2 74				1



Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.

Prepared by: A. Hamid & Azhor

0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0 Water Injection Ratio (q : lit,/min/m)

Lu kgf/cm2

0.0 >13

Lugeon value: Critical Pressure:

 Freezion Losso (Pr) = pv (La + L.) {kg/cm2}
 11:55
 11:55
 11:55
 11:55

 (Pr) | 0.00
 0.00
 0.00
 0.00
 0.00
 0.00

 Friction Losso (Pr) = pv (La + L.) {kg/cm2}
 ***
 ***
 ***

Water Pressure Test

Hole No.: M98-3 Stage: 1/20	Hole No.: M98-3	Stage: 2/20	
Location: Dam Axis (Right Bank) Dia. of Hole: 76 m/m	Location: Dam Axis (	Dam Axis (Right Bank) Dia, of Hole: 76 m	m/m
Hote Inclination (a): 90 degrees Packer Type: Mechanical	Hole Inclination (a):	90 degrees Packer Type: Mechanical	
Friction Loss per meter (pp): 1x10*x0**** Date: 28/November/1998	Friction Loss per meter (pt) :	1×10 ×0": Date: 30/November/1998.	
Ground elevation: EL m Groundwater level (LJ): NIN Gauge beight (LJ):	0.96 m Ground elevation: EL m	Groundwater level (L.): Nill Gauge height (L.)	и (Гд): 1.00 m
are gauge to Depth of test section	Pipe length from pressure g	Depth of text section	Length of section (L.)
7 B	m hole mouth: (Ls)= 3.80 m	GL.(L) = 5 m to (L) = 10 m	E
Reading of flow meter	Reading of flow meter	meter Calculation of Lugeon value	n value
Compge P. Pal Pa2 Pa3 Pa4 Pa5 Pa6 Pa7 P=Pa0.1(sin(a)L+L)→P [kgf/cm2], q=Q-√L[11/min/m]	Cougge Pt.   Pt.2   Pt.3   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   Pt.4   P	Po5   Po6   Po7   7 4 1   P=Po+0.1(sin(a)[+L_u)-Pv [kgUcm2],	q=Q-/L [lit/min/m]
1.5	11:55 12:07	12:4k 13:00 13:12 PI= 1.8	8:1
6.0	U(min) 65,406 65,538 66,189 66,930	U 08,085 68,833 69,225 P2* 4.8 Q2**	5,9
28,494 58,805	65,619 66,310	68,222 68,912 69,256 P4= 10.2	18.5
23. 58,504 58,915 45# 58,515 45# 64# 40#	3 05,434 05,649 05,370 07,229 4 65,443 65,677 66,430 67,310	0 (82,360) 68,988 (69,287) P6* 4.7 q6*	7.6
\$8.527	65,706 66,487	68,428 69,027 69,303 P7= 1.8	ň
5 58.537	65,765 66,600	68,563 69,099	
28,556	65,477 65,795 66,663	68,626 69,141 69,349	
98588	10 65,494 65,852 66,779 67,874	68,753 69,212 69,379	
11	-	<u> </u>	
	13	1 4	
34		n tr	
1 02 02 040 040 047	Total 0-2	3 3	
106 315	AMERICA 240	0.5 0.4 0.7	\$ 57 OF 31 OF
10.4 10.4 10.4 10.4 10.4 10.4 10.4 10.4	45 50 Int/min R.N 29,4 59	66.8 37.9 15.4	?
6	Final 12:05 12:17	12:58 13:10	q:lit/min/m)
	(%) 0.01 0.07 0.27 0.66	0.35   0.11   0.02	•
(8 <del>8</del> )	Friction Loss (Pr) = pr(Lo + Lo) [kgf/cm2]	Lugeon value: (13)	, a.
h Chileal Pressure: >-4.0 kgt/cm2		1	kgC/cm2
Remarks: Watertake at 2 kgl/cm2, was more than 100 Inf/min. And due to surfacial leach 3.0m distance from borchole, pressure test was stopped. At 4kgl/cm2, pressure could not builted.	issure test Kemarks : Water table is Nili,		
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute sends within 90 % to 110 % of the injection rate in the tust menuture mention.		Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute serties within 90 % to 110 % of the injection rate in the just previous one minute.	jection rate per minute
Prepared by: A. Hamid Inspected by: Raja Bashir	Prepared by: A. Humid	Inspected by: Raja Bashir & Azumi Gill	mi Gill

Hole No.:	M98-3	Stage:	3/20	Hole No.:
Location:	Dam Axis (Right Bank)	Dia of Hole:	76 m/m	Location:
Hole Inclination (a):	ion (a): 90 degrees	Packer Type: Mechanical	Mechanical	Hole Inclination
Friction Loss	Friction Loss per meter (pv): 1×10°×0'271:	Date:	2/December/1998	Friction Loss

1				Ε														F					_				7	S					1
	m/m	Cal	cr/1998	Gauge height (La): 1.00	Length of section (L.)	S	Calculation of Lugeon value		P=Pv=0.1(sin(a)\L+Ls).P* [kg(/cm2], q=0=/Ls [livmin/m]		q2= 3.6			45= 8.5		g7= 1.8												30 35 40 45		Water Injection Ratio (q : III./min/m)		<u>`</u>	kg0cm2
320	92	Mechanical	2/December/1998	Gauge		$\dashv$	ation of Lu		-P- [kgt/cm2].	•				•	•	•												25 20 23		r Injection Ka		(9.9)	
Stage:	Dia. of Hole:	Packer Type:	Date:	Nin	Depth of lest section	1.5	Calcul		*=Pv+O, I (sin(a){"+*Lu)	P1= 23					P6= 53	77 2.3		2	, m	2.3°	r- 811	ni sı O A	7 7		13) 0 64			0 5 10		Wate		Lugeon value:	Critical Pressure:
••		_		<u>(L</u> )	pth of Te	10 B		Pu7		S O	53,044	53,053	53,061	53,069	82,078	53,087	53,097	53.18	53,115	53,123	53,132	l	Ī		;	Ş	æ	6.7	B.8	15.18	0.01	í	2
	<b>₽</b>	90 degrees	¥	Groundwater level ([L)):	۵			ja j	*	14:57	52,7%6	52,811		52,862					-		53,039		Ì	1	Ì	3	153	940	25.3	15-07	0.08	1	2
	Dam Axis (Right Bank)	8	1×10,×0,,,,;	Ground	֓֞֝֟֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֓֡֓֡֓֓֡֓֡	CL . (L).	eter	₽.5		14.44				52,463	55,56	5,5 <u>4</u>	52.591	52,634	52,675	52,716	52,760	!	ļ	-	į	3	426	ુ	42.6	14:50	0.23		
	xis (Ri			E			flow m			14:35	81,078		2,73	21,860	51,921			52,105	52,165		\$2,289	ļ	1		İ	S	611	Ş	3	14:45	0.46	(/cm2)	
883	Dam A	•	g (g)		gauge to	3.80 m	Reading of flow meter	3	7	14:23					2,764	51,397	51,429	51,463	51,4%	51,529	51,561	İ		;	į	3	3	3	33.4	14:33	0.14	3.5	
		on (a):	oer met	.E.	pressure	,	j -	Puz	4	14:12			51,059		51,086	21,100		51,141	51,18	51,177	51,195	!	!	i	-	3	182	ر د د	18.2	14:22	0.04	4)× =	
ق	;;	Hole Inclination (a):	Friction Loss per meter (p/):	Ground elevation: EL.	Pipe length from pressure gauge to	hole mouth: (L.)		74. 14.	1	14:00	50,856	50.8%	50,905	50,914	50,92	50,932	<u>\$</u>	50.950	50,95	58.387	50,975	!	į	!	İ	Z		ថ្ង	- 68	14:10	0.01	Friction Loss (Pr) = pr(Lo + Lo) [kgf/cm2]	
Hole No.:	Location:	Hole Ir	Friction	Cround	Pipe km	hole mo		Courge P.	(Ag(/cma))	Start teme	U(mm)	-	4	,	4	'n.	•	7	æ	٥	2	= :	-  -  -	2 2		ē	Œ	Aven ge	it Smis	Frank tem	(P.)	Friction	

#### Water Pressure Test

		Inclination (a):   Step degree   Inclination (b):   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation (c)   Inclunation		Mechanical     December/1998     Gauge height (LJ): 1.00     Cauge height of section (LJ)     S m
	on Loss per meter (pp): 1x1 d ² xQ ¹⁷¹¹ Date: 3/December/1998  gib from pressure gauge to meter and coundwater level (L.): Nill Cauge beight (L.): 1.00  only (L.)= 3.80 m   CL. (L.)= 15 m   co. (L.)= 20 m   L. (L.)= 15 m   co. (L.)= 20 m   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Lugeon value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calculation of Value   Calcu	Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Cont		December/1998   Cauge height (La): 1.00   Cauge height (La): 1.00   Cauge height of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of Langua of
		Croundwater   EL		Gauge height (L.): 1.00  Longth of section (L.).  Some perfection of Lugeon value  (kgt/cm2), q=0/La [it/mis/m]  q1= 0.4  q2= 2.3  q3= 5.4  q4= 6.4  q6= 3.3  q7= 1.1
		Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part	(feat section to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La) = 20 m to (La)	Longth of section (Ln)
		Neading of flow meter   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Property   Propert	10 (L) = 20 m	S m   S m
		Pel   Pe2   Pe3   Pe4   Pe5   Pe0		
		Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Pal		kgt/cm2 , q=0/La [li/min/m] q1= 0.4 q1= 0.4 q2= 2.3 q3= 3.7 q4= 6.4 q5= 5.0 q5= 3.3 q7= 1.1
		16.17   16.28   16.79   16.50   17.62   17.13   17.02   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.13   17.1		q. = 0.4 q. = 0.4 q. = 0.4 q. = 0.4 q. = 0.4 q. = 0.4 q. = 0.4 q. = 0.4 q. = 0.1
		9, 95,221 59,266 59,701 59,908 60,230 60,545 55,252 59,580 59,715 59,907 60,206 60,545 59,527 60,206 60,545 59,527 60,206 60,545 59,527 60,206 60,545 59,527 60,206 60,545 59,527 59,527 60,206 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540 60,540	18.65m2 28.82.32.5	
		9.9.522 95.580 95.7719 95.9570 60.306 60.561 9.5.523 95.502 95.7716 95.967 60.3131 60.578 9.5.533 95.640 15.97714 60.028 60.036 60.504 9.5.537 95.647 15.9778 60.006 60.406 60.610 9.5.537 95.647 15.9806 60.100 60.406 60.645 9.5.538 95.640 95.840 60.100 60.406 60.645 9.5.541 95.640 95.840 60.126 60.436 60.605 9.5.541 95.640 95.840 60.126 60.648 60.605 9.5.541 95.640 95.884 60.228 60.593 60.677 	(m2)33.	
		59,523 59,575 59,776 59,907 60,331 60,578 59,575 59,776 59,907 60,336 60,294 59,773 60,396 60,396 60,396 50,596 59,597 60,396 60,396 50,596 59,597 60,396 60,396 50,596 59,597 60,396 60,396 60,396 59,597 59,597 60,396 60,390 60,496 60,590 59,597 59,590 60,490 60,490 60,490 60,490 59,599 59,590 60,491 60,491 60,591 59,590 59,590 60,491 60,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59,591 59	(m))3,	
		59,533 59,601 59,754 59,997 60,356 60,594 59,774 59,997 60,356 60,594 59,773 60,028 60,396 60,505 59,535 59,535 59,535 59,535 59,536 59,536 60,605 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59,537 59	Smo)lgs	- 1
		59,533   59,614   59,771   60,028   60,300   60,610     59,533   59,624   59,771   60,028   60,300   60,620     59,533   59,625   59,788   60,062   60,406   60,625     59,539   59,640   59,820   60,120   60,456   60,645     59,539   59,640   59,840   60,164   60,481   60,679     59,540   59,671   59,860   60,197   60,256   60,697     59,541   59,640   59,884   60,228   60,521   60,772     59,541   59,640   59,884   60,228   60,521   60,772     59,541   59,640   59,884   60,228   60,521   60,772     50,541   59,640   59,884   60,228   60,697     50,541   50,641   50,884   60,228   60,697     50,541   50,641   50,884   60,228   60,697     50,541   50,641   50,884   60,281   60,772     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,641   50,884   60,891   60,891     50,541   50,884   60,884   60,884   60,891     50,541   50,884   60,884   60,884   60,884   60,884     50,541   50,884   60,884   60,884   60,884   60,884     50,541   50,884   60,884   60,884   60,884   60,884     50,541   50,884   60,884   60,884   60,884   60,884     50,541   50,884   60,884   60,884   60,884   60,884     50,541   50,884   60,884   60,884   60	εξίςεπλ 2 Φ Φ Β	-
		\$9,533 \$9,635, \$9,788 \$0,002 \$0,406 \$0,605 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$0,505 \$	50 m2, 13, 15, 15, 15, 15, 15, 15, 15, 15, 15, 15	
		59,533 59,637 59,708 60,100 60,430 60,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50,430 50	5 0 0 to	-
		59,537 59,503 59,500 60,100 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60,450 60	Zm3')3;	
		59,238 57,654 57,624 60,125 60,430 60,505 55,540 59,541 59,860 60,137 60,565 60,695 59,541 59,860 60,137 60,265 60,695 59,541 59,860 60,137 60,265 60,695 59,541 59,607 59,884 60,228 60,521 60,722 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60,20 60	_ Сто')3;	
		595-30 59,500 59,800 60,197 60,505 60,695 59,540 59,560 59,804 60,298 60,593 60,712 60,291 60,712 60,291 60,712 60,291 60,712 60,291 60,712 60,291 60,712 60,291 60,712 60,291 60,712 60,291 60,712 60,201 60,712 60,201 60,712 60,201 60,712 60,201 60,712 60,201 60,712 60,201 60,712 60,201 60,712 60,201 60,712 60,201 60,712 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60,201 60	யാ,}இ	
		29,441 29,641 59,884 60,231 60,712 59,441 59,641 59,884 60,238 60,531 60,712 	131	0
		20 117 1183 320 251 167 167 167 167 167 167 167 167 167 16		
		2-1-2-2-2-2-2-2-2-2-2-2-2-2-2-2-2-2-2-2	ָנט ן	•••
		20. 00. 00. 00. 00. 00. 00. 00. 00. 00.		<b>.</b>
		20 12 20 10 10 10 10 10 10 10 10 10 10 10 10 10		
		9-1 0-2 0-3 0-4 0-5 0-6 0-6 0-6 0-6 0-6 0-6 0-6 0-6 0-6 0-6		
		0-1 0-2 0-3 0-4 0-5 0-6 0-5 0-6 0-17 143 320 251 167 0-1 0-1 0-2 0-4 0-5 0-6 0-6		
	- I - I - I - I - I - I - I - I - I - I	20 117 183 320 251 167 Q-1 Q-2 Q-3 Q-4 Q-5 Q-6	18 A	
<u> </u>	<u> </u>	On 00 00 00 000 000	١.	
<u> </u>	<u> </u>	E 25 C C C C C C C C C C C C C C C C C C	0	4 5 6 7 8 9
1 2 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1	2.0   11.7   18.3   32.0   25.1   16.7		
Tie   12   1		[£22] [£1:21] [6:46] [7:00] [7:23]		Injection Action (q : Incommon)
le 120 - 1	le 120 1	0.00 0.02 0.06 0.17 0.11 0.05	[]	
12 1	1.22	3		( <del>,</del> 43
122 1	122 1	1		00
1	1	Remarks:		
- 1	1	-		
- 1	1			



Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.

Prepared by: A. Hamid

[Inspected by: A. Gill

Water Pressure Test

9

Hole No.: M99-3 Suge: 5/20	Hole No.: M98-3 Stage: 6/20
Location: Dam Axis (Right Bank) Dia. of Hole: 76 m/m	Location: Dam Axis (Right Bank) Dia, of Hole: 76 m/m
Hole Inclination (a): 90 degrees Packer Type: Mechanical	Hole Inclination (a); 90 degrees Packer Type; Mechanical
Friction Loss per meter (p): 1x1 d'x0'mi: Date: 5/December/1998	Friction Loss per meter (p): 1xt0*x0*** Date: 7/December/1998
Ground elevation: EL. m Groundwater level (L.): Nill Gauge height (L.): 1.00 m	Ground elevation: EL m Groundwater level (L.): Nill Gauge height (L.): 1,00 m
rest section	Depth of tex section
(L.) = 20 m to (L.) = 25 m	(Ls)m 25 m to (Ls)= 30 m
Reading of flow meter Calculation of Lugeon value	flow meter
5 Pu6 Po7 A 1 P=Pu+0.1(sin(t	George P. 941 Pul. Pul. Pul. Pul. Pul. Pul. Pul. Pul.
3.3 q1*	15:59 16:10 16:22 16:32 16:45 16:59 Pl= 3.8 ql=
65,456 65,630 65,930 66,516 66,911 67,162	O(min) 80,088 80,279 80,531 81,006 81,776 82,271 52,508 P2= 6.7 q2= 4.3
66,956,67,166 P4 11.8	80.324 80.611 81.341 81.862 82.318 52.527 P4 11.5 04m
3 65,418 65,500 65,706 66,030 66,628 66,981 67,176 PS- 9.0 q5-	80,346 80,650 81,215 81,907 82,345 52,539 PS= 9.2 q5=
65.515 (65,731) 66,132 66,665 (67,007) 67,190 P6= 6.2 96=	80,364 80,689 81,288 81,956 82,373 52,552 P6- 6.6
65,531 65,757 66,184 66,703 67,033 67,206 P7= 3.3 q7=	80,389 80,728 81,361 82,004 82,399 52,566 P7= 3.8 q7=
6 (5),421 (5,53) (6,521) (6,741) (7,709) (7,709) (7,709)	5 80,132,8 80,401 81,421 82,103 82,442/ 52,555 1 80,401 81,401 81,410 82,465 82,405
8 65.476 65.835 66.340 66.816 67.113	80,452 80,845 81,579 82,150 82,432 52,611
65,423 65,591 65,860 66,392 66,853 67,140	80,885 81,654 82,199 82,510 52,626 52 8
11 00,420 05,000 05,000 00,443 00,001 07,100 07,473	מיניים שליים מיניים ודייום אדרים הגדים
	7 5 5 1 mmm. mmm. mmm. mmm. mmm. mmm. mmm
1.5	
70 00 70 70 70 70	1 0-1 0-2 0-3 0-4 0-5 0-6 0-7
19 150 257 513 375 255 117 0	164 214 393 721 470 267 135 0
Average On 1 (0.2) On 3 (0.4) On 3 (0.5) On 5 (0.7) O 1 2 3 4 5 6 7 8 9 10	23.
12 11 44 11:55 124M 12:18 12:29	15:5N 16:09 16:20 16:32 16:42 16:55
0.05 0.14 0.56 0.30	0.40 1.37 0.60 0.20
Frection Loss (Pr) = pr(Lu + LL) [kg/tcm2] •• 1. Lugeon value: (5.8) Lu'	(5.4)
v. v. Gritical Pressure: 9,2 kgl/cm2	A Chilical Pressure; 8.6 kg/fcm2
Remarks:	Remarks: For 3 minutes reverse running at find 1 kg/lem2 pressure.
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute	Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute
e injection rate in the just of	110 % of the injection rate in the just
Prepared by: A. Hamid & A. Gill Inspected by: M. Suga	Propared by: A. Hamid Inspected by: M. Suga

Hole No.:	M98-3		Stage:	02/2	Hote No.:
Location:	Dam Axis (Right Bank)	tight Bank)	Dia. of Hole:	76 m/m	Location:
Hole Inclination (a)		90 degrees	Packer Type: Mechanical	Mechanical	. Hole Inclinati
Friction Loss	Friction Loss per meter (pt): [x] of xQuar.	×10+×0+71	Date:	11/December/1998	Friction Loss

																													_	-			
76 m/m	Mechanical	11/December/1998	Gauge height (L.): 1.00 m	Length of section (L.)	S m	Calculation of Lugeon value		oʻ		42* 0.4				46■ 3.6		-	18			8.	_		•				3 4 5 6 7 8 9 10	The fact that the state of the fact that the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the	water injection state (q : itt/inition)		(0.8) [4,	9.6 kgt/cm2	
Dia. of.Hole:	Packer Type:	Date:	Nill	test section	10 (La)= 35	Calculat				2	2	P.4.		\$	P7= 4.3	0	2 2		× × ×	810	ni s	insi	23162	120	•						Lugeon value :	vy Critical Pressure:	Remarks: As reversal pressure 1 kg/lem2, the flow meter started reverse for 4 minutes.
동 	90 degrees		Groundwater level (LA):	Depth of	E 00		'Lnd' 94d	4	12:00	\$ 386 86.48	94,400	44	4.4	_	94,466	8	202,80	94,519	25.55	94,555 94,616		1 1	*		Ľ	09 691	_	17.8 6.4	12:10	0.10 0.01	3	3	moter started re
Right Bar	8	1×10+×0+11.	Ground	_	( <u>)</u>	v meter	PuS	- 1	11:36 11:48			93,226 94,025	93,29H 94,074			52 8 220				93,837, 94,400	  -	1	-	_	L	-	-	9 45.R	11:46 11:58	X 0.64	ন		m2, the flow
Dam Axis (Right Bunk)	ļ	3	E	gauge to	3.80 m	Reading of flow meter	P.A.	7 10	11:23			92,841 93,	92,862 93,3	92,885 93,379		92,930 93,523	92,952 93,602			93,035 93,4	<u>.</u>	!	<u> </u> 		3	240 740	-	24.0 74.9	11:35	0,18 1.68	Friction Loss (Pr) = pr(Ls + Ls) [kg(vcm2)		sure A kg//c
	ion (a):	per mete	13:u	n pressure s			7.2		11:14	92,751	92,753	92,754	92,756	27,78	22,761	92,763	92,765	92,767	22,770	27.71	Į	;	!	; ;	Z	20.X	ار ان	2.08	11.24	000	- P(12		versal pres
Location:	Hole Inclination (a):	Friction Loss per meter (p+) :	Ground elevation: EL	Pipe length from pressure gauge to	hole mouth: (Le)		Pol.		Lamba   1:00)	O(min), 92,745	92.745	92,745	92,745	92,745	92,745	92,745	92,745	92,745		. 92,745	1	!		1	3	0.2	Ė	0.02 min	11:10	000	on Loss (P		arks: Alm
ዿ	Š	Fric	ğ	Ä	ğ	L	Camps F.	(kg/km)	Start Land	충				1	٠ <u>,</u>	_	`	~	^	2		<u> </u>	3 3		100	ž	Average	In Junio	Figures Lores	3	Ē		

### Water Pressure Test

Stage:

M98-3

Friction Loss per meter (p)   184   20 dagrees   Packer Type: Mechanical   Priction Loss per meter (p)   184   20 m   Cooundwater level (La)   184   20 m   Cooundwater level (La)   184   20 m   Coundwater level (La)   25 m   184   20 m   Collection of Layeron value   Consider March (La)   25 m   Collection of Layeron value   Consider March (La)   25 m   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Collection of Layeron value   Colection of Layeron value   Collection of Layeron value   Collectio	Location:	::0		E	XIS (R)	Dam Axis (Right Bonk)	되		Dia. of Hole:	76 m/m
Friction Loss per meter (p)   154 (p² Ag ^{hrit}   Date : 12/December/1998	Hole h	nclinati	on (a):			8	degrees		Packer Type:	Mechanical
Fige length from pressure gauge to   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst section   Depth of Itst s	Frictio	a Loss	Per mei	(£)	- 1	р Б	;;			2/December/1998
Pipe tength from pressure gauge to   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth of trest section   Depth o	Ground	cievation	: EL		E	Ground	ater leve	<u>(</u>	NIN	
Reading of flow meter	Pipe len	gth from	pressure	Sange (c	-		ă	pth of te		l.
Reading of flow meter   Calculation of Lugeon value	hole mo	3	•	3.98		ot- (L	ļ		4	
National Control of Water Should be continued for at least 10 mounts, under the specified by a service of the control of water should be continued for at least 10 mounts, and the specified by a service of the control of water should be continued for at least 10 mounts, and the control of water in the just and the specified by a service of the control of water in the just by decreasing the pressure to 4 kg/cm2, the first pressure to 10 kg/cm2 and to 10 kg/cm2. The service of the control of water should be continued for at least 10 mounts and to 1 kg/cm2 and to 10 kg/cm2. The service of the control of water in the just of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the co			Read	Jing of	flow m	eter			Calculat	ion of Lugeon value
Vivinia   12:00   12:20   12:20   12:00   13:15   13:40   14:00   14:00   14:00   15:15   13:40   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14:00   14	Guaga P.	Ŀ	204	3	₹.5	P.5	9. 4	Po7	Partie les les les les les les les les les le	
V(min)         9129.2         9177.0         9173.0         9177.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0         9173.0<	Start teme	J_	1	1	200.52	13:12	9.5	14.00		
19129.2   9139.0   9139.7   9,326   10,255   10,286   664.7   P3= 10.8   q3= 10.5   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4= 13.2   q4	(X	<u> 1</u> 2	ľ	ŀ	0.77	1	IRS OF	2	2	
2 9129.5 9141.0 9140.2 9464 10.200 10.596 664.7 P5** 10.0 q** 13.2 4 9129.6 9142.9 9142.2 9488 10.243 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.565 10.56	<u>,</u> "				9,326		10,588	664.7	2-2-	
3 91224 9141.0 9141.2 9438 10,345 664.7 P5a 10.04 q5a 7.5 q6a 1.8 5 91225, 9142.0 9142.9 94572 10,386 10,644 664.7 P6a 7.8 q6a 1.8 q6a 1.8 q5a 10,297, 9123, 9142.9 94572 10,386 10,645 10,632 664.7 P6a 7.8 q6a 1.8 q6a 1.8 q7a 0.00 0.00 10,446 10,646 10,642 10,641 664.7 P7a 4.8 q6a 1.8 q7a 0.00 0.00 10,446 10,646 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,6	7	9129.3			\$		10,596	5.7	P4=	
4 9122.6 9142.8 942.8 942.8 942.8 10.642.8 10.642.8 664.7 PG= 7.8 q6= 1.8 q6= 1.8 1922.6 9142.0 9142.9 9577 10.346 10.625 10.629 10.640 10.647 10.648 10.647 10.648 10.647 10.648 10.647 10.648 10.647 10.648 10.647 10.648 10.647 10.648 10.648 10.647 10.647 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648 10.648	~	9129.4			9,498		10,605	664.7	ž.	
\$ 9129.7 9145.9 9147.4 9,457 10,428 10,623 664.7 7 10	4	9129.5			2,572		10,614	3.	<b>•</b> 9.	
6 91220, 9145, 91474 9,740 10,466 10,632 664.7 10 10 10 10,641 664.7 10 10 10,641 10,641 664.7 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,641 10,64	· .	9129.6					10,623	7.4%	2	
7 9129.9 9145.5 9150.0 928.4 10.504 10.641 664.7 10 10 10 10 10.542 10.550 10.641 664.7 10 10 10 10.542 10.542 10.668 664.8 10 10 10 10.542 10.668 664.8 10 10 10 10.542 10.668 664.8 10 10 10 10.542 10.668 664.8 10 10 10 10 10 10 10 10 10 10 10 10 10	, ,	9129,7					10,632	6.7		
8 9130.1 9146.5 9153.0 9906 10542 10,055 10,056 664.7 \$\frac{6}{2}\$ 9 9 9130.1 9140.5 9156.4 10,097 10,580 10,066 664.7 \$\frac{6}{2}\$ 8 8 9 9130.1 9147.0 9156.4 10,097 10,580 10,066 664.7 \$\frac{6}{2}\$ 8 9 9130.1 9147.0 9158.2 10,178 10,015 10,068 664.8 \$\frac{6}{2}\$ 8 9 9 9130.1 9147.0 9158.2 10,178 10,015 10,068 664.7 \$\frac{6}{2}\$ 8 9 9 9130.1 9147.0 9158.2 10,178 10,015 10,000 \$\frac{6}{2}\$ 9130.1 914.7 \$\frac{6}{2}\$ 9158.2 10,178 10,015 10,000 \$\frac{6}{2}\$ 9130.1 914.7 \$\frac{6}{2}\$ 9158.2 10,178 10,015 10,000 \$\frac{6}{2}\$ 9130.1 914.7 \$\frac{6}{2}\$ 9158.2 10,178 10,015 10,000 \$\frac{6}{2}\$ 9130.1 914.7 \$\frac{6}{2}\$ 9158.2 10,178 10,015 10,000 \$\frac{6}{2}\$ 9130.1 914.7 \$\frac{6}{2}\$ 9158.2 10,178 10,015 10,000 \$\frac{6}{2}\$ 9130.1 914.7 \$\frac{6}{2}\$ 9158.2 10,178 10,015 10,000 \$\frac{6}{2}\$ 9130.2 914.7 \$\frac{6}{2}\$ 9158.2 10,178 10,015 10,000 \$\frac{6}{2}\$ 9130.2 914.7 \$\frac{6}{2}\$ 9158.2 10,178 10,000 \$\frac{6}{2}\$ 9158.2 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,178 10,1	,	9129.8		9150.0	9,874		10,61	5.4.7		
9 91301, 91470, 9156.4 10,007 10,580, 10,668, 664.8 2 7 7 1 20.2 10,007 10,580, 10,048, 664.8 2 7 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	30	9129.9			96,	10,542	10,651	7.3		
10 9130.2 9147.6 9188.5 10,178 10,618 10,668 664.8 2 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	٠.	9130			10,097	0,580	0,000	3		•
2     1     2	2	200.2			FZ (01	10,615	10,668	8.		
13	:	ļ	i		ļ	į	Ī	ĺ	, , , , , , , , , , , , , , , , , , ,	
15	1:	Ì	Ī	Ī	-	İ	Ī	į	• ~ • ~ • • • • • • • • • • • • • • • •	
15	3	ļ	Ì	Ì	j	Ī	-	i	÷ 6	
10		ļ	İ	Ì	ļ	!	Ī		313	-
10	3	õ	ŝ	3	ઢ	3	8	6	I FA	
Average Qu1 Qu2 Qu2 Qu3 Qu4 Qu3 Qu0 Qu7 Qu2 Qu2 Qu2 Qu2 Qu2 Qu2 Qu2 Qu2 Qu2 Qu2	Ē	6	10.0	193	Š	Ş	¥7.0	0		
1.2   1.0   2.7   30.8   37.4   9   0.02   Water Injection Ratio (q : lit/min/m)   1.0   1.2   1.2   1.3   1.2   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3   1.3	Average	0	240	0-3	4.0	S	9	ટે	0 1 2	4 5 6 7 8 9
Friction Loss (Pt) = pt(Lo+Lo) [kg/km2]	HI/min	٥	_1	-1	ş	37.4	٦	0.0 0.0		nicotion Pario to Tit (min)
Friction Loss (Pr) = pv(Lo+Lr) [kg/cm2]   Lugeon value: 0.5 Lu  Semurks: by decreasing the pressure to 4 kg/cm2, the flow started reverse for 3 minutes and to 1 kg/cm2 for 7 minutes.  Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute received within 90% to 110% to 4 photo in the injection rate in the jump minutes.  Inspection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute per minute.  France of the injection rate in the jump previous view minute.  Inspection of water should be about the injection rate in the jump.  France of the injection rate in the jump.  France of the injection rate in the jump.  France of the injection rate in the jump.	LAUSH CLIM		П	П		9		14.10		(
Friction Loss (Pr) = pv(Lo + Lo) (kg/cm2		3	800	î	*	ŝ	660	3	1	•
Remarks: By decreasing the pressure to 4 kg/tcm2, the flow started reverse for 3 manutes and to 1 kg/tcm2 for 7 minutes.  Note: Injection of water should be contained for at least 10 minutes under the specified pressure, after the injection rate per minute certies within 90 % to 110 % of the injection rate in the just minute that a feature of the injection rate per minute that have a feature of the injection rate per minutes.	Friction	è,	<u>. 5</u>	₹ 3	g/cm2		3	3	Lugeon value:	0.5
Remarks: By decreasing the pressure to 4 kg/cm2, the flow started reverse for 3 minutes and to 1 kg/cm2 for 7 minutes.  Note: Injection of water should be contained for at least 10 minutes under the specified pressure, after the injection rate per minute earlier within 90 % to 110 % of the injection rate in the just enemanter flowers. A first the injection rate per minute for a flower of the injection rate of the injection rate of the minutes.							7	1	Critical Pressure:	F4 F4
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute equiles within 90 % to 110 % of the injection rate in the just previous one minute.  Parameted No. 1 & Least 4 & A shot	Kemark	by c	creasing	the press	ure to 4	kgt/cm2,	the flow	Started	reverse for 3 manutes and	to 1 kgt/cm2 for 7 minutes.
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.    Property A.   A.   A.   A.   A.   A.   A.   A.	-		-				-			
A Hamid & Ashor	Note :	Injection	of water	r should	be contin	ued for a	t least 10	minute	s under the specified press	sure, after the injection rate per min
	Prepare	. 24	Ę	3	3770				located by . Such.	Shark M





Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.

Prepared by: A. Humid.

Hole No.: M98-3	Location: Dam Axis (Right Bank)	Hole Inclination (a): 90 degrees	Friction Loss per meter (pt): 1 x1 8 xQ431;
Stage: 9/20	Dia. of Hole: 76 m/m	Packer Type: Mechanical	Date: 15/December/1998
Hole No.: M98-3	Location: Dam Axis (Right Bank)	Hole Inclination (a): 90 degrees	Friction Loss per meter (pt): 1x10'x0'm:

Ground		GL - (I	heter	3	7					32,78		٠.	32.78		32,801		32,803						3	9	3	•		3			reverse
E			Reading of flow meter	PhA	ខ	10.45	32,772	32,750 32,760 32,774	32,776	32,73	32,781	32,783	32,784	32,786	32,789		32,793						Ş	5	3:	13	1	0.00	(g(/cm2]		Remarks: From 10 kg/Jcm2 to 7 kg/Jcm2, reverse
	අ ක්රියේ ද	4.40 m	ding of	3	^	10-34	32,755	32,760	32,761	32,762	32,763	32,78	32,765	32,767	32,768		32,770						3	=	3:	J.		3	<u> </u>		cm2 to 7
n: EL	Pipe length from pressure gauge to	=(	Rea	P.2	4	10:23						32,753	37,75	32,755	32,756						_		Ş	~	3	10.22		0.17)	Friction Loss (Pr) = px(La + Ls) [kgUcm2]		/15×01 v
Ground elevation: EL.	ngth from	hole mouth: (L.)=		<b>.</b>		10-12		::		32,738	32,739	32,739	32,740	32,740	32,741	32,742	32,742						ē	v.	٦, ٥	_Ł	I.	200	5.53		ts: Fron
Ground	Pipe Ic	Note m		Gauge P.	(kg/cms)	Sterl tome	(wim)	7	ر ا	. !	4	Š	9	_	· 	<u>`</u>	2	Ξ	127	2	7	!	TOAL	Ë	Average			ξ	Frictio		Kemar
E		٦		_	_								-		_						_			_ 1	 o	_				1	
8.6	Length of section (Lu)	E			i/min/m]																				o.	νw)					mraules,
	of sectio	S	n value		<u></u>	4,0	<u>:</u>	6.3	0.0	\$	0.7	0													۲.	: In/m			3	kgf/cm2	m2 (or 5
Gauge height (L2):	L'Sength		Calculation of Lugeon value		P=P++0.1(sin(a)L+L+)-P*[kgs/cm2], q=0/L>[lit/min/m]	Ş	45	÷	<b>.</b>	Ş.	95	6		l										l	'n	Water Injection Ratio (q : lit_/min/m)			_	0.6	0 1 kg1/c
Ŝ			tion of		% [kg/cr										/									ĺ	ω 4	Injection					one san
	1	£.	Calcula		1,11	5.3	8	11.0	13.2	11.0	83	5.4		ļ		•	\	\							7	Water			Cugeon value:	Critical Pressure:	NG 4 manu
Ē	ig.				0.1(sin(a)	ä	2	Ş	44	ŗ	9	7		2	•	. 00	_		. O	4		71		)	•				100 day	Critical	wpear as
 	Depth of test section	E(77) 01			P=P	[2]	5	0	_	_	Ó	3	3	0	Zu S	ມ, <u>ງ</u>		υį	<b>3</b> 10	5\$3	14	13;	*.X	_		14	:1	_	3		led rever
Groundwater level (L.):	Spho	<del>6</del>		2º4.		17.26	17,580				2,580	<u>S</u> 2€	3 17,580	7 17,580	17,580				i 	:	<u>.</u>	:	0.7	٥	ò	7	+	300	•		eter star
Iwater le		G. (J.)-		₽86	7		2 17,550														<u> </u>	<u> </u>	Š	3	3.	Ļ	L	9	•	-	he Ilowm
8		ог. (	meter	1.5	-	16-50	17,302	22,71			т.	0 17,438	17,464	17,487					_	_	_	1	0.5		9		+	9	_		ұйст2, т
E	٥	E	f flow	7	2	16:35	J 16,720	0,7,91	_			26,5	3 17,018	070,71 €							_			512	3:	4	┙	5	kgf/cm2]		re to 4 kg
	c gauge	3.97 m	Reading of flow meter	3	_	5 16:20	16.350	36,380	_	_	2 16,475	502	16,538	2 26.568						i	_	!	3	3.4			4	2 0	3;		& pressu
7H: EL	Pipe length from pressure gauge to	÷	<u>#</u>			16:415	16,220	2 16,233		26,262	16,27	16,282	16232	3 16,302	16311	16,320		-	<u> </u>		į	İ	i õ	8			4	Š	Friction Loss (Pr) = pr(Lo + Lr) [kgf/cm2]		Remarks: By decreasing pressure to 4 kg/cm2, the flowmeter statted reverse reading 4 minutes and to 1 kg/cm2 for 5 minutes.
Ground elevation : El.	ngth from	hole mouth: (La)-		12		15:50	081 91 (	16,182	16.18	16,185	16,187	16,189	16.191	16.193	16.195				<u> </u>				1-	2	3	-1		8	9,300,0		us: By
Ground	P. P. B.	Tole m		C. C.	(kg0cm))	New High	O(min)		61		4	'n	۰	,	00		<u>'</u> ≘	=	17	.=	. 7	12	196	ĭ	- VALVE		5	3	Friction		Remark

Note: Injection of water abouid be continued for at least 10 minutes, under the specified pressure, after the injection rate per minute settles within 80 % to 110 % of the injection rate in the just previous one minute.

Prepared by: A. Hamid & Azhor

#### Water Pressure Test

Mechanical

Stage:
Dia. of Hole:
Packer Type:

10/20 76

()

Ground elevation: EL.  Pipe length from pressure gauge to hole mouth: (Lo) # 4.40 1  Reading of	P. P.	I									
ipe length fre			E	Groundwater level (L.):	ater leve	([.])	NE		Cauge he	Gauge height (La):	8
ole mouth: ()	m pressure	ලා පහිතෙනී :			۵	of to	Depth of test section		5	Length of section (L.)	3
	3	4.40 m	_	GL - (L)=		45 m	1	₹0 m		S	Ē
	Rea	Reading of flow meter	flow m	eter		+		Calculati	Calculation of Lugeon value	con value	
Gauge P. Pul	P.2	2	Ž	3.5	8.	Pe7					
(kgf/cms)		_	20	_	4	-	P=Po+0.1(sin(a)L+L>)-Pr [kgf/cm2],	145		9-0-/L {!it/min/m}	/min/m]
Start tome 10-12	12-01 21	10-34	10.45	10:57	11:10	11:22	ž	5.8	- <del>1</del> 6		
O(min) 32,737	37 32,750	32.759	32,772	32, 793	32,802	32,804	2	8,8	g		
_			32,774	32.78	32,802	32,804	Ę.	11.8	å	- 0.2	
2 32.738			32,776	32.795	32,802	32,804	P4=	14.8	440		
,			32,779	32,796	32,802	32,804	75	11.8	\$		
	٠,		32,781	32 797	32,802	32,80	8	89 89	95		
5 32,739		•••	72,783	32,798	32,803	32,88	2	5.8	-20		
		-	32,784	32,799	32,803	32.80					
7 37.740			12.786	32,800	12,803	32.804	2				
,				5	500	2 6	2 9	1			
,				8	508	200	9 . (C1	•			
				1	3	200	)8	_			
10. 34,742	25,726	n/,,,	ر در/پې	34.00	0	3	1 5	_			
	-		Ī	Ī	Ţ	Ī	)   2)   2)				
7.7		-		Ī	1		u.88				
- 4		į			Ī	ĺ					
. 52				Ī	1		191				
Total	<u>ئ</u>	3	Ş	3	ŝ	ò	 				
Fit. 5	Η		21	02	2	-	)				
ï	-	6.0	3	3,	Š	6	0.0	0.1 0.2 0	0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9	0.6 0.7 0.8	3 0.9 1.0
_	_1	_	7.7	•	22	٥		Water	Water Injection Paris (n · 13 /min/m)	A / Co. Lie /min	ĺ
ᆲ	ᅱ		10:55	φ 1	1:50	1:35					ì
(Pt) 0.00	0.00	000	0.00	000	000	900					
Friction Loss (Pr) = pr(La + Ls) [kgUcm2]	기 - (교)	S T	g(/cm2]		3	1	(008m)	Lugeon value:	0.5	,3	
					3	1	Ö	Critical Pressure:	12	kgt/cm2	
Remarks: From 10 kg/Jcm2 to 7 kg/Jcm2, reverse flow for 2 minutes.	om 10 kg/c	:m2 to 7 }	set/cm2	reverse	low for	2 minute	,				
	•		· •								
											ľ
Note: Inject	ion of water swithin 90	r should	Ne Contro	ened for a	i least t	D mindle The igst	Injection of water should be continued for at least 10 minutes under the specified preasure, after the injection rate per minute perites within 90 % to 110 % of the injection rate in the just previous one minute	crited press inute	ure, after the	injection rat	E Jod
							Transfer of trees to the				

9-3 Stage:	Dam Axis (Right Bank) Dia. of Hole:	90 degrees Packer Type:	ν): [×[ψ*κο ^{μηι;} Date:	m Croundwater level (L.); CL- 53.50	Δ.	m (L. (L.)	ı	3 Pud Pus Pus Part 1 P=Pu+0.1(sin(a)Lu+Lu)-Pa	12:00 12:15 12:30 12:45	43,960 44,020	43,969 44,025 44,038 4,006.6	43,977 44,030 44,060 4,006.6	43,983 44,034 44,062 4,006.6	43,989 44,038	43,995 44,042 44,064 4,007.0	44.007 44.050 44.067 4.007.5	44,012 44,054 44,069 4,007.5	44,018 44,057 44,071 4,008,0	1 3111		1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	20.00	28 5/ 14 1.4	0 5.8 3.7 1.4 0.1	12:10 12:25 12:40	00.0 0.00 0.00 0.00		es un Critical Pressure:	Remarks: From 4 kg/Cm2 to 1 kg/Cm2 reverse 110w 4 minutes.	Injection of water should be continued for at least 10 minutes under the specified pres- seriles within 90 % to 110 % of the injection rate in the just previous one minute	& Fachat
Hole No.: M98-3	Location: Dam	Hole Inclination (a):	Friction Loss per meter (p.) :	Ground elevation: EL.	Pipe length from pressure gauge to	hole mouth: (L.) = 3.80		Gauge P. Pul Pul Pol	Sian time 11:10 11:25 11:40	43,901	2 3 800 H 43 905 43 920	43,907	43,909	3,891.8 43,911	43,912	3 894.0 43.916 43.948	3,894.7 43,917		1.11	13	14 15 1	3		Average Ort Or2 Ord	11:20 11:35	(Pr.) 0.00 0.00 (vd.)	Friction Loss (Pr) = pr(Lo + L.) [kgf/cm2]		Remarks: From 4 kgf/cm2 to	Note: Injection of water show	Description of Land & Bother
11/20	76 m/m	Mechanical	24/December/1998	Gauge height (La): 1.00 m	Length of section (Lu)	5 m	Calculation of Lugeon value	Parkettem21 o=0(Laflit/min/m)	_		0.00 0.40 0.48			47 ■ 0.00			-							0,1 0,2 0,3 0,4 0,5 0,6 0,7 0,8 0,9 1,0	Water Injection Ratio (q : lit/min/m)		0.0	:: 12 kg/cm2		lies under the specified pressure, after the injection rate per minute at nevious one manife	7,011
Stage:	Dia. of Hole:	Packer Type:	Date:	.CL. 53.50 m	ŀ	m to (L/)= 55 m		Parpare 1 (singa) 1.48 3. Pr [kgf/cm2]	P1= 6.5	23 1	P3= 12.4	Ÿ.	P6.				u3,]	810	ii sii o w		14 ts			0.0 0.1 0.2			Lugeon value:	Critical Pressure:		ites under the specified pro-	Increased by the Contract
	ght Bank)	90 degrees	1×16 ×0 +11:	Groundwater level (LA):	Dephof	S (7)		PuS Pub Pa7	10-35 10:50 11:05	8,557.4 8,565.0 8,570.5	8,557,5 8,565.5 8,570.3	8.558.5 8.566.5 8.570.5	8,559.4 8,566.9 N,570.5	8,560.8 8,567.4 8,570.5	8,561,3 8,567.9 8,570.3	8,561.9 8,568.5 8,570.5	8.562.8 K 569.5 8.570.5	8,563.4 8,569.7 8,570.5				╀	7	0.00	- C	0.00 0.00 0.00	3	77		ued for at least 10 minute	INCCIDENT TORY OF THE PARTY
M98-3	Dam Axis (Right Bank)	n (a):	Friction Loss per meter (p.): 1x1	ε	arc gauge to	F	Reading of flow n	Pa2 P.3 Pa4	09-501 10:05 10:20	8523.0 8,525.2 8,530.8 8,557.4 8,565.0 8,570.5	8523.0 8,525.5 8,233.2 8,557.5 8,565.5 8,570.5	4523 8 8 5264 8 538 3 8 558 5 8 566.5 8 570.5	8524.0 8,526.8 8,540.0 8,559.4 8,566.9 8,570.5	8524.1 8,527.2 8,543.0 8,560.8 8,567.4 8,570.5	8524.1 8,527.6 8,545.0 8,561.3 8,567.9 8,570.5	8524.2 8.528.0 8.547.0 8.561.9 8.568.5 8.570.5	8524,4 8,528,8 8,553,0 8,562,8 8,569,5 8,570.5	8524.5 8,529.2 8,555.0 8,563.4 8,569.7 8,570.5				+-	6.0 -	0.2	200	0.00 0.00 0.00	Friction Loss (Pr) = pr(Lo + Lo) [kgf/cm2]			Injection of water should be continued for at least 10 minu-	A Clampa W. Carbar
ļ	1	Hole Inclination (a):	Loss p	Ground clevation: EL.	of from p	hole mouth: (Le)-		Compre P. Pol	2		851.0 0.11.0		8,521.0		8,521.0	8,52,0 0,12,0 0,12,0				į		3	ı	Average On 1	200	(Pr.) 0.00	(P) ssol w		Remurks :	Note: Injection of	Drang read ha

#### Water Pressure Test

ation:  c Inclination (a):  tion Loss per met mouth (Lo)  Read  no. 1	Dam Axis (Right Bank)  or (p): 1x19*x0*****  m Groundwate  gauge to  3.80 m G (L.)**  ing of flow meter  p.3 - P.4 - P.5 - P.  7 10 - 7 - P.  7 10 - 7 - P.  43,926 44,023 44,43,466 44,623 44,43,926 44,623 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,633 44,63	7000 m	of Hole e: 53.50  53.50  53.50  1.(L)=  P2.  P3.  P3.  P3.  P4.  P4.  P5.  P6.	E C C C C C C C C C C C C C C C C C C C
nclination  Loss per elevation: E gth from pre wth: (L)=	90	25 m 55	ker Type e:	2011 (La): 1.00  100
Loss per		55 m 55 m 57 m 12.30 12.45	53.50 ction (L)= P1= P2= P3= P3= P3= P3= P3= P3= P3= P3= P3= P3	r/1998 cight (L.): 1.00 mgh of section (L.). geon value q=0/L [it/min/m] tl= 0.10 fl= 0.36 fl= 1.16 fl= 0.74
gth from pre gth; (Lo)=  1. 11:10 13,890,4 3,890,8 43,890,8 43,891,0 43,891,0 43,890,8	n Groundw n GL. (L low meter P.4 10 7 12:15 12:00 43,990 44,020	Se m 55 m 55 m 6 m 6 m 6 m 6 m 6 m 6 m 6 m	53.50 (L) π (L) π 10.1(sin(a 17.2 17.2 17.2 17.2 17.2 17.2 17.2 17.2 17.2 17.2 17.2 17.2 17.2 17.2 17.2 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17	eigh (La): 1.00 ngth of section (La):  S m  Scon value  q=0,-(La [hi/min/m]]
gth from pre with: (L)= Ful. 1 1 11:10 3,890.6 43 3,890.8 43 3,890.8 43 3,890.8 43	10 CL - (L 10 7 10 7 12:00 12:15 43,960 44,020 43,965 44,020	Depth of u  55 m  55 m  6 Pe7  1 1 12:45  057 4,006.6	# 27 5 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	E 101 47070707
11:10 13:870.4 13:870.6 13:870.8 13:870.8 13:870.8 13:870.8 13:870.8 13:870.8 13:870.8	CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   CL - (L   C) - (L ) C))))))))))))))))))	55 m 6 Pe7 4 1 2:30 12:45 057 4,006.6	10 (La)=	101 573 57 57 57 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Fe1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10 P.4 P.5 10 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:00 12:0	Pe7 1 12:45 4,006.6	Calculat P=Pv+0.1(sin(a)L+1.2)-Pv P1= 6.4 P2= 12.4 P3= 12.4 P5= 12.4 P5= 12.4 P5= 12.4 P5= 12.4	eq
Pel 1 1 1 2 3 2 3 2 3 2 3 2 3 2 3 2 3 2 3 2	P.4 P.5 10 7 12:00 12:15 12:960 44,020 43,965 44,023	Pe7 1 12:45 4,006.6	P=Po+0.1(sin(a)).L+(1.2)-Py P1= 6.4 P1= 6.4 P2= 12.4 P2= 12.4 P4= 13.4 P5= 12.4 P5= 12.4 P6= 9.4	- 4 G G Z Z Z,
11:10 11:25 3,890.4 43,901 3,890.6 43,903 3,890.8 43,905 5,891.0 43,907		12:45	Parcett, (sin(a)), to 4 L. J. Fry Plan 6.4 Plan 12.4 Pran 12.4 Pran 12.4 Pran 12.4 Pran 12.4	- 4 G U Z U ,
3,890.6 43,903 3,890.8 43,903 3,890.8 43,905 3,891.0 43,907		142		
3,8%1.4 43,901 3,890.6 43,903 3,890.8 43,905 3,891.0 43,907		0.000 % 0.00.0		
2 3,890.8 43,905 3,891.0 43,907		A ACC & 1920 KK		
3 3,891.0 43,907	42 060 44 026	4 050 4 006 6		
2000		42 060 4 006 6		
21 20 1 20 1 2 1 2 2 1 2 2 1 2 2 2 2 2 2		44 062 4 006.6		66* 0.28
3.891.8 43.911		44.063 4.007.0		
3,892.5 43,912		44,064 4,007.0		
7 3,893.3 43,914		44,066 4,007.0	2	
t	44,007 44,050	44,067 4,007.5	•	
43,917			,	
10 3,895.4 43,919 43,953	44,018 44,057	44,071 4,008.0		
		1	•	
12	-		-	
13-		<u> </u>	551	
14			9 2	
		100	•	
- CV	} ×	77	, 0	
0 1 0	_	1	7 60 10 00	01 04 04 04 04 04 08 00 10
0.5	5.8 3.7	٠.		2
11:20	12:10 12:25	12:40 12:55	Water	Water Injection Ratio (q : lit/min/m)
(Pr) 0.00 0.00 0.01	0.02 0.01	0.00 0.00		
Friction Loss (Pr) = pr(Lo + L.) [kgt/cm2]	f/cm2]	3	Lugeon value :	
		1	Critical Pressure:	13 kg//cm2
Remarks: From 4 kgf/cm2 to 1 kgf/cm2 reverse flow 4 minutes.	Com2 reverse flo	w 4 minutes.		
Note: Injection of water should be continued for at least 10 minutes under the specified	e continued for a	it least 10 minute	s under the specified pres	Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute
0			1. S. W. S. W. S	-

Water Pressure Test

9

Stage:	Dam Axis (Right Bank) Dia. of Hole: 76 m/m	90 degrees Packer Type: Mechanical	1x10*x0**** Date: 28/December/1998	Groundwater level (L.); GL. 52.30 m Gauge beinht (La): 1.00 m	Depth of test section	(L)= 65 m to (L)=	2 P. .)- P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L. V.L.) - P. (\sin(a)\L.L.) - P. (\sin(a)\L.L.) -	1622 16:40 17:30 Pl= 6.3 ql= 6.70 66,720 66,720 66,720 72 9.3 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2 q2= 6.2	00,731 00,741 06,743 F3m 12.3 66,734 66,745 F5m 12.3 66,734 66,745 66,745 F5m 12.3	66,736 66,742 66,746 P6= 9.3 q6= 66,736 66,742 06,746 P7= 6.3 q7=	66,737 (66,745) 65,746 66,737 (66,745) 65,747 66,738 (66,747) 66,747 66,739 (66,747)	i i i i i i i i i i i i i i i i i i i	\$0.00 \$4.00	T	16:35 76:50	Lugeon value :	er an Critical Pressure: >15 kg/cm2	Author Sciacio Carlo	Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.	oob Inspected by : Farhat M. Shah
	Location: Dam Axis	Hole Inclination (a):	Friction Loss per meter (p.):	Ground elevation: EL. In	ressure ¿	hole mouth: (Le)= 3.30 m (GL.	Z -	10.4	61,630 61,644 61,667	61,632 61,648 61,672 61,632 61,649 61,674	7. 61,634 61,651 61,676 66,772 8. 61,635 61,654 61,683 66,716 9. 61,636 61,654 61,683 66,725 9. 61,636 61,658 61,683 66,725 10. 91,637 61,638 61,686 66,726		Total O-1 O-2 O-3 III. 9 17 24 34	0-1	15:40 15:52 16:04 1	n Loss (Pt) = pr(L, + L) [kgi	Percent County to Lafton Took American Section 5	Action 5: From 4 to 1 Agrical, 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to	Nute: Injection of water should be co	Prepared by: A. Hamid & Mabboob
13/20	Dia, of Hole: /o m/m	Packer Type: Mechanical	Date: 27/December/1998	GL. 53.50 m   Cauge height (L.): 1.00 m	Length of section	Calculation of Lureon value	P=P+0.1(sin(a)L+L)-Pr [kgt/cm2], q=0/L [liu/min/m]	P2 9,4 42 42 42 42 42 42 42 42 42 42 42 42 42	P4= 15.4 P5= 12.4	P6= 9.4 q6= P7= 6.4 q7=	Sm3/lg4n G \oldow \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \times \tim	5 jussel 1 25 0 N 4 W 40	Mark.	0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0	Water Injection Ratio (q : lit,/min/m)	9.0	Critical Pressure: >15 kg//cm2 -		s under the specified pressure, after the injection rate per minute previous one minute	Inspected by : Farhat M. Shah
M98-3	Location: Dam Axis (Kight Bank)	Hole Inclination (a): 90 degrees	Friction Loss per meter (pt): 1x10 x0 vn: I	Ground elevation: EL m   Groundwater level (L.); GL-	necessare gauge to Depth of Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual Annual An	moc mostry (Let) 4 0 m   CL - (Let) = 00 m   Reading of flow meter	Pn6 Pu7	54.837 54.857 54.892 54.952 55,016 55,044 5, 54.878 54.858 54.861 56.896 54.958 55,018 55,044 5,	54,865 54,902 54,966 55,021 54,868 54,907 54,972 55,024	4 54,839 54,871 54,914 54,978 55,027 55,046 5,051.5 5 54,839 54,878 54,915 54,948 53,029 55,071 55,045 5,051.5	54,880 54,931 54,932 55,038 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55,048 55	12	Total Out Qu2 Qu3 Qu4 Qu5 Qu6 Qu7 lit. 6 30 34 62 27 7 0.4	Average Out _Qu2Oud   Qu4 _Qu5   Qu6   Qu7   St.   Qu6   Qu7   St.   St.   St.   St.   St.   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other   Other	13:10 13:21 13:32 13:44 13:58 14:10 0.00 0.00 0.02 0.02 0.00 0.00	۰۰ ( الله الله الله الله الله الله الله ال	Remarks: From 4 to 1 kel/cm2, for 3 minutes in reverse flowing.		uld be continued for at least 10 minute 110 % of the injection rate in the just	Prepared by: A. Hamid

M98-3	Dam Axis (Right Bank)	- 1	1×10° ×01"	Groundwater level (L.); GL.	(c) - (d)	w meter		73,715 73,733 73,742	2,72	73,735 73,743	75,736 75,744	73,729 73,738 77,745 73,749	73,740 73,746	7747					23 00 05 00	5 16:10 16:25	0000 0000	# <b>1</b>		Of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of the party of th
•;	۵	Hole Inclination (a):	Friction Loss per meter (ps) :	ation : EL. m	Pipe length from pressure gauge to	Reading of	Pul. Pu2 Pu3 P	15:00 15:15 15:30 1; 73:200 73:201 73:202 73	73,701 73,703	73,701 73,705	25,55 107,55 207,55	.c7   907, c7   107, c7   007, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7   107, c7	13,70	73,700 73,701 73,714 73,				32	0-1-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0	15:25 15:40	0 00 0.00 0.00	Friction Loss (Pv) = pr(Lo + Lo) [kgf/cm2]		transition of passes should be continued for at least 10 montes under the s
Hole No.:	Location:	Hole Inch	Friction L	Ground elevation : EL	Pipe length from p		Gauge P. P	Start time 1		3 2	: 1	1	:	1.1	12	5. 4	- 1	79 E	O Average O		0 (2)	Friction Los	Remarks:	. 0532
15/20	76 m/m	Mechanical	29/December/1998	Gauge height (La): 1.00 m	Length of section (L.)	Calculation of Lugeon value	P=Po+0.1(sin(s)Lu+Lu>P* {kgi/cm2}, q=Qw/Lu [livminvm]	# 5 5		45 0.6	-66 -74		.0.	_	•				0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0	Water Injection Ratio (q : lit./min/m)	•	ie: 0.6 Lu ire: >15 kg/cm² -		ton 1. On security under the second and negative after the insection rule for minute
Stage:	Dia. of Hole:	Packer Type:	Date:	er level (L.); GL- 50.50 m	Ý					<b>4</b> 2	67 P6= 9.1 67 P7= 6.1		<b>г</b> ш.	, 18 ( (			12219		00			Lugeon value:		
	Dam Axis (Right Bank)	90 degrees	1×1 0° ×0.971:	m Groundwater level (L.	į	3	Pa4 Pu5 Pu6 Pa7		68,623 68,612		68,585 68,632 68,616 68,667 68,591 68,635 68,617 68,667	K19,83 8E6,83	88,64 68,621	68,611 68,647 08,622 68,669 68,616 68,650 68,624 68,669			į	\$ 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	3.	0 16:25 16:40	0.02 0.01 0.00 0.00	(/cm2)	Remarks: From 7 to 4 kg//cm2, for 3 minutes in reverse flowing.	
Hole No.: M98-3	Location: Dam Ax	Hole Inclination (a):	Friction Loss per meter (p/) :_	Ground elevation : EL.	ğ	hole mouth; (Le) A 3.34 m CL. Rending of flow meter	George P. Pol. Pol. Pol. Pol. Pol. Pol. Pol. P	15:10 15:25 15:40	68,493 68,525	68,470 68,496 68,529 68,471 68,499 68,534	68,473 68,503 68,538 68,474 68,506 68,542	68.508 08.546	68,513 68,554	68,480 68,517 68,562 68,480 68,517 68,562		i	.	Total O.1 .0-2 0.3	0.1 0.2 0.1	Newskitzen 15:20 15:35 15:50	0.00 0.01 0.01	Friction Loss (Pr) = pr(La + La) [kgl/cm2]	ks: From 7 to 4 kgl/cm2, fo	

#### Water Pressure Test

Hole No.:		-	M98-3					Stage:	16/20	ا	
Location:	::0		Dam A	xis (Ri	Dam Axis (Right Bank)	ठ		Dia. of Hole:	76	m/m	6
Hole I	Hole Inclination (a):	on (a):	•		8	90 degrees		Packer Type:	Mechanical	ical	
Frictio	Friction Loss per meter (pt):	per met	G (b)	- i	1×10°×0'"			Date :	30/December/1998	Der/1998	
Ground	Ground elevation : EL	1: Et		٤	Groundwater level (L.): GL.	vater lev	(L)	JL- 45.50 m	Gauge	Gauge height (L.):	, 00·1 :(c
P 196 lgr	Pipe length from pressure gauge	pressure	or aguage			1	epth of te		, i	ength of	Length of section (Lu)
hole mo	hole mouth: (Le)=			E	ر <u>ا</u>		75 m	10 (La)= 80	E	.	
			Reading of flow meter	flow rg	eter				Calculation of Lugeon value	^ นดอสีก	alue
Cauge F.	정.	Ŀ	3.	<b>3</b> 6	3,	9.	Pn7.	Complete to the second of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formula of the formul	I.A.B. (Lond)man		and a Historial
(Kg/cm)	- 8	, ,	Ŀ	2	, K	.	19	Place S	7	-	90
	ľ	l,	1	10	7 77	77.77	I۳	2	2.2		200
-	•					7 742		ដ	11.6	÷	9.2
c1	20,57							74	14,6		0.5
<u>.</u> ا	2,700	• •	•		•	75,743	•	ž.	11,6		2.2
₹,	2,78 00,100	-			•	17.		Ž.	9		
	00,1		_			۲, ۱ ۲, ۱		74	7.		0.0
o¦.	۲ ا ا				2 1	4	5,4	•			
\   	5 F	5, £	2,5	3,7,7	_						
					•	77.747					
<u>.</u> 02	700		_			73,747		1g1			
ˈ='	. !										
ᄓ				İ	-		į				
2			,	ĺ			Ī	52			
Ξ,		į	į	1				i i			•
2								61			
ě	3	g'	3	Į,	3,	3.	6	M			
<u>=</u>		٦	z,		,	^{<	- -		0 . 0 . 0	3	
of the last		3 6	} •	,	} &	, s	0	7.0	0.4.0 0.4.0	2	טיז מיז מיז מיז מיז מיז מיז מיז מיז מיז מ
1	L	1	Ľ	ŀ	L	16:25	١	*	Water Injection Ratio (q : lit_/min/m)	11: b) 01:17	(/mia/m)
E	L	ľ	L		<u>.                                    </u>	0.00	0.00				
Friction	riction Loss (P+) = pr(Lo + Lo) (kgf/cm2	7)4-(	3	8f/cm2]		3		Lugeon value :		Ē	_
						1	•	Critical Pressure:	:ssure: 8.7		kgf/cm2
Remarks :	ä										
									•	:	
Note:	Injection settles w	n of wate	76 to 110	be conti	nued for	at least I	O minute	Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.	d pressure, after	the inject	ion rate per minut
Prenu	. 24	4	Premared by . A Hamid & Mabboob	Mahbo	 چ			Inspected by Farhat M. Shah	arhat M. Sha	۽	

Hole No.: M98-3		Stage:	17/20	Hole Z
Location: Dam A	Dam Axis (Right Bank)	Dia, of Hole:	76 m/m	Scatio
Hole Inclination (a):	90 degrees	Packer Type: Mechanical	Mechanical	Hole In
Friction Loss per meter (pt) : 1x10'x0'm	: 1×10,×0,	Date:	1/January/1999	Friction

Hole No.:	9		X 38					Stage:		1//20	ļ	Ę	Hole No
Location:			Dam A	xis (Ri	Dam Axis (Right Bank)	췽		Dia, of Hole:		76 m/m	1	IJ	Cocution
Hole 1	Hole Inclination (a):	(a) (a):	•		8	90 degrees		Packer Type:	2	Mechanical	1	<b>3</b> .	Hole Inc
Frictio	sso_I uc	Friction Loss per meter (pt):	cr (p,) ;		1×10,×0,21	32		Date:	1/3	1/January/1999	j	ш	Friction
Cround	Ground elevation: EL	n: EL.		E	Ground	Groundwater level (LA); GL-	(1)	3L- 42.50 m	H	Gauge beight (La): 1.00	E	[O]	Ground ele
Pipe kg	mor) qua	Pipe length from pressure gauge to	gauge to			۵	epth of it	ction		Length of section (L.)		LĒ.	Pipe lengt
hole mo	hole mouth: (L.)	į	2.80 ₪	E	GL - (L)=	;	. E	80 m to (La)= 85	£	E S		<u>*</u>	hole mouth
		ı	Reading of flow meter	No.	eter			Calc	ulatio	Calculation of Lugeon value		L	
Orega P.	Ξ,	3	3.	3	3	Γ,	Pu7.			(1)		[0]	Gauge P.
(hediome)	- 8	4 5	15/2	2 2	20.02	4 0	50	rareto, i (sinta)Liti	֝֝֟֝֜֝֝֝֝֓֜֝֝֟֝ ֓֓֓֓֞֓֞֞֞֞֓֓֞֞֞֜֞֞֜֞֞֜֞֞֞֜֞֞֞֜֞֞֜֞֜֞֜֞֜	2	<del></del>	<u> </u>	(hg/cmu)
(Mmia)	1.	11.	1.	29.95	80.018	1~	ι~	2	8.3	92= 0.2		ľ	(Vmin)
<u>_</u>		79.921				80.054		5	11.3				, ,,
. 74	79,913					80,055	80,057		14.3				2.
	79,913								ņ				<u>.</u>
4	79,014							P6=	J.	q6= 0.3			~ -
8	200	79,925						2	ņ				×,
ا	200							,					•
۰. ¤	200	2 8	\$ \$ \$ \$	200	5 5	2 2 2 2 3 2 3 2 3 2 3 2 3 2 3 2 3 2 3 2	80.00	_ و ه تر	\			·	
	7007	0,000		000				 	/	_ . o	•	_	
2	7.9.7							181	· .				01
					.	į	!					<u> </u>	=
2			į	.	i	-	į	ארי				_	27
3	1		j		į		1						5
4 ×	1	:	1		;		-	14 13 Lo V					4 i
ļ	2	Ş	[2	2	ž	٤	ć	is.V				_ا_	Join 1
<u> </u>	'n	9 9	7	4	3	-2	63	\ \ -					<u>`</u> !
Average	Į,	73 8		ð,	3	ŝ	Ġ,	0.0 0.1 (	0.2 0.3	0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0		<u> </u>	Average
area (1)	_L						,	*	pler Inje	Water Injection Ratio (q : ht/min/m)		13	
	L	1		1		2	3					<u>L</u>	,
3				70'D	600	0,00	2	•				J:	] :
O.	Š	inction Loss (Pr) = Pr(La + La) [kgt/cm2]	3			3	•	Lugeon value:	 9	(0.5)		-	2017
						3	5	Critical Pressure:	'Sure;	9.() kgf/cm2	ļ		
Remarks :												Χ.	Kemarks :
_													
_												_	

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just prevains one minute.

Prepared by: A, Hamid

#### Water Pressure Test

Friction Loss per meter (pr) :   Friction Loss per meter (pr) :   Ground elevation : EL		1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1   1x1	90 degrees  [18] d' ×Q''''!  [Groundwater lev  [CL. (L.)=  [CL. (L.)=  [CL. (L.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R.)=  [CL. (R	Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Pod.   Po	10 2 E   10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3/19 (Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culation Culati		(La) m m m m m m m m m m m m m m m m m
Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per   Loss per	m m m m m m m m m m m m m m m m m m m	Ow met Co. 1   X   O   O   O   O   O   O   O   O   O	Coundwate (L. (L.)=  13:10   1   1   1   1   1   1   1   1   1	Depth Depth 285 131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,131 86,	Date:	3/January/199  Gauge hei  Ilculation of Luge 14.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7	99	(m/z)
Elevation: 1  This is a second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second	23.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3.95 m 3	Ow met 10 10 10 10 10 10 10 10 10 10 10 10 10	Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundwate   Coundw	Depth (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994) (L. 1994)	1): CL. 36.50 m of test section m to (La) = 90 Ca Ca Ca Ca Ca Ca Ca Ca Ca Ca Ca Ca Ca	Gauge hei	Eth ([L]): 1.1   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1	88 (a) [m/s]
Eth from pre Pul. (L) = 1   12:10   2   12:10   2   12:10   2   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12:10   3   12	3.95 m 3.95 m 1.05 of 11 12:40 86,020 8 86,020 8 86,030 8 86,030 8 86,030 8 86,030 8 86,030 8	6,007 8 6,007 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008 8 6,008	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	285 85 6 1 133 86,13 133 86,13 133 86,13 135 86,13 140 86,13 142 86,13 142 86,13 142 86,13	of test section  m to (L _D ) = 90  Ca  Ca  Ca  Ca  Ca  Ca  Ca  Ca  Ca  C	m     Long	20 m S m section (IL S m value S m value S m value 0.1 m 0.2 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5 m 0.5	(m/zi
Re, (L)   1   1   1   1   1   1   1   1   1	3.95 m Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fill Fing of fil	0w met Pp.4	5 5 5 5 8 5 4 8 5 4		10 ([L) = 90 ([L) = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L] = 90 ([L	m	S m con value 0.1 0.2 0.5 0.5 0.0 0.0 0.0 0.0 0.0	[ E
Pol. 12:10 86,0901 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,0001 88,00001 88	P.3	Pud 10-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	522854854		NAN-CORALCI	ulculation of Luga 4.7 (kg/cm2), 4.7 q1 10.7 q3 10.7 q3 10.7 q4 4.1 q4 4.2 q5 4.3 q5 4.4 q5	con value q=0/1. {!i/mi 0.1 0.5 0.5 0.6 0.0 0.0 0.0	[m/si
Ful Pu2. 1 4 12:10 12:25 86,000 86,000 86,001 86,000 86,002 86,010 86,002 86,011 86,002 86,011 86,002 86,011				1 _ <del>1</del> _ <b>!</b> _ <b>!</b>	NAME COOKICE	4.7 (kg/cm2), 4.7 (kg/cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (cm2), 4.7 (	q=O=/L-{lit/mi 0.1 0.2 0.5 0.5 0.6 0.1	(m/m)
12:10 12:25 86,000 86,000 86,001 86,009 86,002 86,010 86,002 86,010 86,002 86,010				_!-!	NAME COOKICI	(*L)-Pr [kg/cm2], 4.7 4.7 7.7 61 10.7 64 7.7 64 7.7 64 65 64 65 65 65 65 65 65 65 65 65 65 65 65 65	0.42 (30 min	(m)
86,000 86,009 86,001 86,008 86,001 86,009 86,002 86,010 86,002 86,010				! _ l	6	Ĭ.		[
86,000 86,008 86,001 86,008 86,002 86,009 86,002 86,010 86,002 86,010					9	Ĭ.		
86,001 86,008 86,001 86,009 86,002 86,010 86,002 86,011					Of S	Į.		ſ
86,002 86,009 86,002 86,010 86,002 86,011					9	į.		
86,002 86,010 86,002 86,011					ទ ;	į.		
86,002 86,011					2 3	Į.		
710 26 000 25					요 :	Î		
77000					,	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		
86,003 86,012					7			
86,004 86,013						`		_
8 86,004 86,014						· \		•
86,004 86,015						ė.		
86,005 86,016	200	8 760,04	8. 2. 8	8 0.140		•••		_
	- <u>-</u> -   	i	<u> </u>	<u> </u>	i 31	•••		_
	-	<del>-</del>	!	<u> </u>	-	•		
- 13-	1			<u> </u>	5 t			
	!	<u>,</u> 	<u> </u>	-				
2	2	2	ž	5	18.4 T			
÷	22		<u>:</u> _	:				
1.00	3	├	_	Ŀ	Γ	0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0	0,6 0.7 0,8 0	2.9
_	;;	- 1	- 1	L		Water Injuries Dutie	(m)	_
Prese time 12:20 12:35	12:50	2	1320	2 2	13:40	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	(d. , m., mm/m)	
(%) 0.00 0.00	0.01	0.02	0.01	0.00	2			
Friction Loss (Pr) = pr(Lo + Lo) [kgf/cm2]	( ) ( ) ( ) ( )	/cm2]		7	Lugeon value :	ratue: (0.2)	<u>.</u>	
				3	77 Critical Pressure:		kgf/cm2	
Kemarks :								

Hole No.:	Location: D	Hole Inclination (a):	Friction Loss per meter	Ground elevation: EL.	Pipe length from pressure g	hole mouth: (La)=	Readi	Guage P. Pal PuZ	(kgf/cms) 1 4	Shart time ON:10 ON:22	10,587 10,587 10,587		2 10,588 10,594		4 10.589 10,595					10,591	10.00,01 10,591 10,600		-172.	1 2 3		Total 0-1 0-2	
19/20	76 m/m	Mechanical	4/January/1999	Gauge height (La): 1.00 m	Length of section (Ls)	E	Calculation of Lugeon value		PaPo+0.1(sin(a)La+La)-Pr[kgt/cm2], q=O=/La[lit/min/m]				94 0.9	45 <b>≈</b> 0.5		47= 0.1				_	-	-	-				-
Stage:	Dia. of Hole:	Packer Type:	Date:	Groundwater level (L.): GL- 35.50 m		ı	Calculati		PaPo+0.1(sin(a)La+La)-Pr	Pl= 4.6	P2= 7.6	_	P4= 13.6		\$			or i	<b>о</b>	× × × × × × × × × × × × × × × × × × ×		•	ns:	531,	1 191 J. C4	7.M	
				(P):(	Apply of R	ء چ		P-7	1	14:20	91,373	01,367 91,373	91,367 91,374	91,374	91,369 91,375	91,375	91,376	375,18	91,377		91,378	Ī	i	:		ું.	
	<u>B</u>	90 degrees	:12.1	water lev		3		98	4	14:15	575,1240 91,366 91,373	191367	25.267				0,70	1 91,371	152,18	2,72	5,73			!		9, 1,	
	Dam Axis (Right Bank)	S	1×10 ×0191:	Ground		다.(단	meter	P.S	7	13:50	1 91,34K	91,294 91,342	91,241 91,250 91,265 91,299 91,345	2 2	22 249	91,313 91,352		2 91,358	92,126	91 363	5 91,365	-		į	i	ટુંજ	١
_	Axis (R		- 1	E	وا	E	Reading of flow meter	ž	2	13-35	91,240 91,248 91,260 91,290	2 27.28	2,29	91,304	2000		715,19	2775			91,336	1	-	1	<u> </u>	Ş.ê	1
M98-3	Dam		Friction Loss per meter (pv) :		Pipe length from pressure gauge to	3.95 m	ding o	67		13:23	91,26	91,240 91,249 91,262	97.10	91,250 91,267	91,251 91,269	91,253 91,272	91,254 91,275	1 97,277	91,279	2 282	91,284		1	!	-	3.	1
		Hole Inclination (a):	ĕ	3: EL	n bucsent			2	4	13-11	11,24	21.24	2,22	2,23				91,254	91,244 91,255	91,245 91,256	72,12	-			-	ွဲ •	ŀ
.; 9	:uo	nclinat	a Loss	Ground elevation: EL.	igth from	hole mouth: (L.s)=		2		13:00		9,240	91,24	91,241	25.55	24,24	91,243	25,74	2,24	91.24	91,246				i	ું કે. જ	,
Hole No.:	Location:	Hole I	Frictic	Spund	9 5	Note mc	L	Configuration Property (Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Property Configuration Propert	(Mathema)	A Line	(Amin)		7		4	'n	٥		87	٥	2	_			4. v	Total	
																		(	3I	32	, -	3	0				

### Water Pressure Test

Ē

Dia, of Hole: Packer Type:

Dam Axis (Right Bank)

M98-3

Stage:

20/20 2 Mechanical

90 degrees

Ground	Ground elevation; EL.	ᇤ		ε	Groundwater level (L.); GL.	rater leve	į	33.40 m	Gauge height (La): 1.00
e len	th from	Pipe length from pressure gauge to	gange to			ā	coth of t	Depth of test section	Length of section (L.)
tole mot	hole mouth: (La)		3.95 m	E	CL.(L)-		E \$6	lo(La)= 100 m	. S
		Reac	Reading of flow meter	flow rr	eter			Calculation of Lugeon value	Lugeon value
Guuge P.	P ₀ 1	Pu2	P.3		Pes	3	2		
(kgf/cm3)		4		10	7	4		P=Pu+0.1(sin(a)L+L2)-Pr [kgf/cm2],	Ġ
Start little	04:10	08:22	08:35	08:50	00-03	09:15		-I.	
O(min)	10,587	10592	10,000	10,620	10,650			2	42= 0.2
,	10,587	10,593	10,602		10,652			£	
74	10,588							P4	
, [	10.588			10,628				ĸ.	
' 4	10,589		10,607	10,631					
'n	10,589	10,5%	10,609	10,634				2	q7= 0.1
	10,500		10,611	10,618	10,659				
· ~	10,590			10,640	10,662		10,677	000	
.∞	10,590			10,643			10,677	Zu	
	10.591							. ao 13/J	-2.4
20	10,591	10,600	10,617	10,648	10,668	10,675	10,078	84	
=		Ī						•	
22 _.					ļ			٠,	
2	į	Ī		-	I			•	(A)
Ξ,		į		į	İ	Ī			
<u>د</u>	ŀ	į	,	J	į	7	ţ	218,	•
0 0 1	<u> </u>	} ∝	3~	3,8	3 ≃	3,5	<u>}</u> ~	, , ,	
Average	į	0	3	3	ŝ	ĝ	0	0.0 0.1 0.2 0.3 0.4	0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0
il Jmin	4.0	8.0		2.8	۲8	0,5			Weter Initialian Dailo to 11th India
french time	03-20	OK:32	_ [	9 8	ŝ	25.50	- 1		(maximum : 5) 2013
3	8	0.00	8	0	8	8	8		
riction	(P) 256	Friction Loss (Pr) = $pr(Lo + Lr) [kgf/cm2]$	₹ 3	gf/cm2}		3	3	Lugeon value: (0.	(0.2)
						•	-	Oritical Pressure:	.3 kg/cm2
Remarks:									
Note :	Injection	of water	r should	oc contra	ned for	al icasi l	O minute	Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute	er the injection rate per men
		5				1		Charles Based to the contract of	

0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0 Water Injection Ratio (q : lit/min/m)

| Total | Qu.1 | Qu.2 | Qu.3 | Qu.4 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 | Qu.5 |

Remarks:

Lu' kef/cm2

(0.2) 8.8

Lugeon value: Critical Pressure:

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.

Prepared by: A. Hamid.

Holc No.: M98-4		Stage:	1/14	Hole N
Location: Dam Axis (Left Bunk)	eft Bank)	Dia, of Hole:	76 m/m	Locatic
Hole Inclination (a):	60 degrees	Packer Type: Mechanical	Mechanical	Hole Ir
Friction Loss per meter (pt): 1×10"×0"";	0-×0,071;	Date:	11/January/1999	Frictio
Ground elevation : EL m	Groundwater level (I	J:CL. 4.50 m	m Groundwater level (L.): GL. 4.50 m Gauge height (L.): 0.70 m	Ground
Pipe length from pressure gauge to Depth of test section	Depth	Depth of test section	Length of section (La)	Pipe len
		4		

q=0,/L [lit/min/m]

26.4.28.4.4

44446

21.5 4.7 4.4 4.4 5.4 5.4

2222222

\$5,032 \$5,032 \$5,082 \$5,052 \$7,052

58.661

7) 57,246 57,489 57,060 38,020 58,57,526 57,305 57,305 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,205 57,

8, 8, 8, 17, 2, 8, 58,903

Calculation of Lugeon value

Depth of test section

GL · (L) = 2 to (L) = 7

Reading of flow meter

4.50 m

hole mouth: (L.) =

## Water Pressure Test

Hole Inclination (a):   60 degrees   Pecker Type:   Mechanical   Precision Loss per meter (p):   1x10 ² xQl ²¹¹¹   Date:   11/January/1999   Dia of Hole;   Type:   Mechanical   Precision Loss per meter (p):   1x10 ² xQl ²¹¹¹   Date:   11/January/1999   Dia of Loss per meter (p):   1x10 ² xQl ²¹¹   Date:   11/January/1999   Dia of Loss per meter (p):   1x10 ² xQl ²¹¹   Date:   11/January/1999   Dia of Loss per meter (p):   1x10 ² xQl ²¹¹   Date:   11/January/1999   Dia of Loss per meter   Date:   11/January/1999   Dia of Loss per meter   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   11/January/1999   Date:   1									Stage:		2/14		
Climation (a):   60 degrees	Locatic	Ę.		Dam A	sis (Le	f Bank			Dia, of Hole:		92	m/m	
1 Coss per meter (p)   1   1   1   1   2   2   3   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3   4   3	Hole Ir	clinatic	n (a):	,		8	degrees		Packer Type:	2	(echanica	1	
### Charleon of water should be continued for at least 10 minutes under the specifical broad at \$2.0 m   Chaupe height (LJ); CLL.	Friction	ו נאסטן וו	oer met	ct (b)	1×10	OX.	<u> </u>		Date:	11	/January/	8	
### (La)=  ### A±50 m   CL(La)=  ### Sending of flow meter   Calculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation of Lurgeon value   S n   Colculation   S n   Colculation of Lurgeon value   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colculation   S n   Colcul	Ground	elevation	E			Grounda	vater leve	);( <b>[]</b> );	7.50	**	Gauge he	(L):	0.70
New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year   New Year	Pipe lcm	gth from	pressure	gauge to			Ã	cpth of te			Ž,	th of section	3
Reading of flow meter   Reading of flow meter   1	hole mor	(1)	,	4.50		GL . (L		•	to (Le)=			S	£
Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul   Pul			Reac	ing of	flow m	eter			C	alculatio	n of Lug	eon value	
16600   16112   16123   16124   16136   17710   1710   1710   1711   16121   16123   16124   16136   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308   61308	Cauge F.	ŀ	Pu?	3, 4	ž 5	3,4	8 4	. Pa7 .	P=Po+0.1(sin(a)I	() *A (**) **	i e	3i} ~J/~O≖o	m/u/m
3,022 (3,022 (3,022) (3,042) (3,043) (3,044 (3,042) (3,044 (3,042) (3,044 (3,042) (3,044 (3,044) (3,044 (3,044) (3,044) (3,044 (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044) (3,044)	Zied Pitte		16:12	16.23	4	ı	XS:Q	17:10	Pla		•	00	•
3,021 (3,022) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045 (3,045) 63,045	O E	63.021	63,022	22.5	63.043			30,53	2	7.7	- 3		
3,021 (3,024 (5,031 (3,047 (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,108) (5,		63,021	63.023	63.030	63,045				73	7.7	3		
3,022 (3,025 (3,035) (3,049 (3,071 (5,089 (3,092 Pre 2,17	٠,	63,021	63,024	63.031	63,047		63,086		P4=	10.7	8		
3,022 (5,026 (5,002) (5,003) (5,003) (5,004) (5,003) (5,004) (5,002) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (5,003) (		63,022		63,033	63,049	63,07	63,086			7.7	Α.		
3,022 (3,025 (3,035) (3,035) (3,038) (3,038) (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092 (3,092	4	63,022		63,034	63,051		63,087			4.7	8-		
3,022 (3,025 (3,036 (3,036 (3,036 (3,037 (3,089 (3,092 (3,093 (3,036 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,093 (3,	٧.	520'59		63,035	63,053					1.7	Ģ		
3,022 (3,022 (3,032) (3,038) (3,038) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (3,039) (	9	63,022		63,036	63,056								
33,022 (3,027) (3,0306) (3,080) (3,081) (3,093) (3,093) (3,093) (3,092) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093) (3,093	,	63,022		63,038									
3,022 (3,023 (3,042 (3,042 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,092 (5,	∞	63.022		63.039					0.6	···			
201 O-2 O-3 O-4 O-5 O-6 O-7 O-5 O-6 O-7 O-7 O-6 O-7 O-7 O-6 O-7 O-7 O-7 O-7 O-7 O-7 O-7 O-7 O-7 O-7	ياه	6 6 6 6 7 6 7 8 8		9	63,062				8.0				
Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Colo		77000		3	3				7.0	٠.			
Solution of water should be continued for at least 10 minutes under the specified pressure, after the injection rate pressure, and the with the specified by the short of the specified by the specified pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure, after the injection rate pressure pressure, after the injection rate pressure pressure, after the injection rate pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure pressure press	- 2	-			-	Ī			./ 0.9				y.a
10   10   10   10   10   10   10   10	: :			ļ			Ī		5.0				
Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Colo	- 4	i	i	!		1	Ī	Ī	4.0				
1   6   13   21   17   10   10   10   10   10   10   1	12	Ī	i	:	Ī		1		3.0				
1   6   13   21   17   9   10   10   10   10   10   10   10	Tolai	ő	S.	3	3	ر ا	3,	0	2.0				
0.1   02   03   04   05   06   07   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	ِ آ	-	٥	2	7	2	•	-	0.1				-
16:10   6:22   16:31   2:14   15:54   17:04   17:20   0.0   0.3   1.0   1.5    16:10   16:22   16:31   16:42   16:54   17:04   17:20   0.0   0.0   0.0    16:10   16:22   16:31   16:42   16:54   17:04   17:20   0.0    16:10   16:20   16:20   16:20   17:04   17:20   17:04   17:20    17:10   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:20   16:	Average	- -	6	7	3	3	3	ò	] 8				
	The state of	101.91	16.22	16.31	44	95.91	170		0.0	S	2	1.5	55
cos (P.) = pr(Lo + L.) [kg(lcm2]	3	3	300	8	8	8	3						
COS60=0.868  COS60=0.868  COS60=0.10 % of the injection rate in the just previous one minute after the injection rate rates with 90% for 110% of the injection rate in the just previous one minute. A think 4 A short	Priction	Loss (P.	3	3	1/cm2		1	1	Lugeon	value:	(0.3)	Ē	
COS60=0.868 poctum of water should be continued for at least 10 minutes under the specified pressure, after the injection rate rates within 90 % to 110 % of the injection rate in the just previous one minute. I have been also also been also also been also also been also also been also also been also also been also also also also also also also also	_	•					3	ŧ	Critical E	Pressure:	5.7	kg(/cm2	6.07285-05
}	Remarks	<u>.</u>											
}				09SOO	998.0								
}													
	l	Injection	of water	should !	x contin	ued for	r least 1	O minute	s under the specif	fied pressur	c, siter the	injection rate	per mon
	Prena	24	4	N Pin	27kor				lacacrated by	Firhat V	A Shah		

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.

Inspected by: Farhat M. Shah

Prepared by: A. Hamid & Azhor

오

•

2

. .

۳ ۲۲

4 107 108 10.7 11-40 11-52 0.01

(Ps) 0.01 0.01 0.03 0.10 0.05 0.05 0.05

riction Loss (Pr) =  $p_1(L_0 + L_0)$  [kg0/cm2]

COS60=0.868

Cemarks:

3.53.8

218 405 21.8 405 21.8 40.5

2,2 2 4 2,2 4

Tor E

0-1 10.9

Lui kgf/cm2

8. (2. 6.

Lugeon value:

Critical Pressure:

10   10 (L) =   15   15   15   15   15   15   15	32.9 0.0 5.0 10.0 15.0 20.0 25.0	12.0   10.0   15.0   20.0   25.0
72,280 73,480 74,270 74,717 72,281 72,581 74,717 74,511 72,581 73,538 74,272 74,751 74,751 72,281 72,281 74,972 74,817 72,286 72,986 74,987 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72,986 72	19.0 37.2 77.2 100.8 76.6 53.2 32.0 000 000:10 000:22 000:34 000:45 000:57 00:00 00:40 00:20 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:00 00:	19.0 32.2 72.2 100.8 76.6 53.2 32.9 Williams (9.12) 0.05 0.14 0.05 1.29 0.75 0.05 0.05 0.05 0.05 0.05 0.05 0.05

Hole No.: M98-4		Sage:	5/14	Hole No.:	M98-4	
Location: Dam	Dam Axis (Left Bank)	Dia. of Hole:	76 m/m	Location:	Dum Axis (Left Bank)	fr Bank)
Hole Inclination (a):	60 degrees	Packer Type: Mechanical	Mechanical	Hole Inclination (a):		60 degree
Friction Loss per meter (p.)	p): 1×10+×0,***;	Date :	13/January/1999	Friction Loss per meter (pt): 1×10° ×Q1*71;	יו (א): און (מ) און (מ)	
Ground elevation: EL.	m Groundwater level (	Li): GL. 14.70 m	m Groundwater level (L.): GL. 14.70 m Gauge height (L.): 0.70 m	Ground elevation : EL. m Groundwater l	ε	Groundwater I
Pipe length from pressure gauge to		h of test section	Depth of test section	Pipe length from pressure gauge to	gauge to	

Length of section (

25 m

Depth of test section 20 m to  $(L_s)$ =

Reading of flow meter

hole mouth: (L.)=

Calculation of Lugeon value

?=P++0.1(sin(a)L+1.;>Pr [kgl/cm2],

:332333

22322

(a) 55,472 55,473 55,473 55,473 55,476 55,476 55,476 55,476 55,476 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,475 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,477 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,475 55,47

13/January/1999 Mechanical

Date:_

Packer Type: Dia. of Hole:

60 degrees

6/14 76

Stage:

Water Pressure Test

_	~		т	τ-									_		_													
1	ı	i			ë									ſ						~~.				1	20			
9		E			iVmin/r																							
	ğ	'n	valer.		3	00	0.0	0.2	9.0	0,2	0.0	0.0													??		·=	•
	o clar	•	Seon	ļ	Q		5.		¥.	5.	9	4															3	
Crusta Nations (T. A).	Length of section (L.s.)	i 	2		(/cm2)	•			-	-	-			ŀ											0		(0.1)	
-	+-		lation		-P. (kg																				'n		::	
		30	Calculation of Lugeon value		1	23	5.3	8	11.3	8.3	5.3	5			٠.	۵.									2		Lugcon value:	2
۶		1 0	ı		1(sin(a	ï	ξ.	χ	PA	P5*	9	2		l	_	•	_	٠.	4	D)	ir.	•	2		0,0		100 Str	
	) X	3) or 8			P=Po+0.1(sin(a)L+La).Pr [kgt/cm2], q=Q-/Lu [lit/min/m]									0	0	8	7.0	9	) V	. 4	ų,	2.0	2 6	9	_		L	
m of 25 - 10 th of party and management	Death of test section	8		Pu.7	-	17:55	10.576	10,676	929'01	10,676	10,676	10,676	10,676	10,676	10,676	10,676	10,676	1	i	İ		် ဝ	Ş	C O	18.05	C)	2	7
l and	Å	Y.	ı	9	4	17:44	_	0,676	19,676	10,676	1 9/9/01	10,676		10,676	10,676		10,677	i	<u>:</u> 	÷			-		17:54	000	3	
and an and		5		ш.		17:32	רו						_					1	!	÷	!  -	3	0	6		Н		
		님	ğ	Pos	~	1	ı=	7 10,666	9 10 667	10,668	2 10,669	4 10,670	10,671	7 10,673	9 10,674		3 10,676	1	-	<u> </u>	ļ	3;	+-	- 2		00°C		
١		£	Š	3	2	17:20	۱~	10,647	10,649	10,650	10,652			10,657	10,659		10,663	1	-	ĺ		3.8	j	8.	17:30	000	g/cm2	
	t aguez	4.50 m	Reading of flow meter	2	~	17:0	10.634	10,635	10,636	10,637	10,638	10,638	10,639	10,640	10,640	10,01	20,0	1				3,*	0.3	O.X	17:19	0.00	<u>\$</u>	
	Pipe length from pressure gauge to		Read	Pu2	4	6 57	0.630			10,630	10,630	10,630	10,631	10,631			10,632	:	Ť	i		3.	-	0.2	17.07	00:0	Priction Loss (Pr) = pr(Ln + Lu) [kg//cm2]	
Geound chambion . Et	E E	Ĵ		Pul	_	16:45	_			10,629	10,629	10,629		10,629			629'01	-	•	<u>!</u> !	<u> </u>	ë	乚	0.0	10-55	000	3	
200	ength	hole mouth: (Le).		L	ê	L.	Ľ	2	2	2	-	2	<u> </u>	2			2	•			-	_	┺		Ξ	Н	Š	
3	ğ	100		Cauge P.	(kg//cm)	Nart time	C(mim)	, <del>-</del>	-7		4	٧,	٥		∞	o'	≘ : —	<b>:</b> :	1:	3 2	'n	Total	Average	It! /mie	Protein tim	3	Ē	_
_	_	_									_			_	_			_										•
E					Ē									٢	_								٦	ć	}			
0.7	5	E			lit/min/									1									١					
heigh (La): 0.70	ength of section (L)	S	ngeon value		, q=0~(L)[lit/min/m]	0.0	0.0	0.0	0.	9	0.0	0													?		3	No.
l is	tige B	i	100.0		•	-	42	5	<u>.</u>	÷.	9	47												_		١	<b>⊢</b> .	•

COS60=0.868

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.

Prepared by: A. Hamid & Azhor

Inspected by: Furhat M. Shah

I.u.' kg/cm2

(0.1) 6.8

Lugeon value: Critical Pressure:

3 1

0.

(0.0) 8.3

Lugeon value: Critical Pressure

Triction Loss (Pv) = p+(Lo + Lu) [kgf/cm2]

COS60=0.868

00 8 6 0 8 4 8 9 1 0 0

M98-4 Stage:	Dam Axis (Left Bank) Dia. of Hole:	60 degrees Packer Type:	p): 1×10° ×01971; Date:	m Groundwater level (L.): GL	Depth of to	4.50 m   CL - (L)= 35 m to (L)=	meter	P.S. P.6	<u>ج</u>		31,420 31,457 31,462	31,377 31,425 31,459 31,463 31,470	31,432 31,461 31,466	31,436 31,462 31,467 31,472	31,446 31,465 31,470	31,397 31,449 31,466 31,471 31,475 8.0 31,400 31,454 31,467 31,472 31,476 2.0			0.4	, 0	44 12 12		1 18:46 13:5K 19:10	0.00	[kgf/cm2]	Revirse reading for few seconds by decredsing to	89)	inued for at least 10 minute he injection rate in the just	d & Azhor
Hole No.:	Location: Dar	Hole Inclination (a):	Friction Loss per meter (p): 1×10* ×01971:	Ground elevation : EL	Pipe length from pressure gauge to	hole mouth: (La)= 4.	Reading		184X) 18:12	0(min) 31,298 31,531 31, 1 31,300 31,334 31,	31,337	3 31,305 31,339 31,	31,345	31,348	8 31,316 31,353 31,	10 31,319 31,356 31, 10 31,321 31,358 31,		12	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			Average Out Out. O.	18:10 14:22	0 000 000	Friction Loss (Pr) = $pr(L_0 + L_0)$ [kgf/cm2]	Remarks:	COS60#0.868	Note: Injection of water she seriles within 90 % to	Prepared by: A. Hamid & Azhor
7/14	76 m/m	Mechanical	14/January/1999	Gauge height (L.): 0.70 m	Length of section (La)	£ %	Calculation of Lugeon value	Ò		0.5 0.5 0.5		45 0.2 46 0.1											1 1.5 2	,	0.7 Lu >11 kgf/cm2			Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute certies within 90.% to 110.% of the injection rate in the just previous one minute.	M. Shah
Stage:	Dia, of Hole:	Packer Type:	Date:	level (14): GL- 14.10 m	wor	m to (L/) ≈ 3.5 m	Calculat	P=Po+0.1(sin(a)[_++[_2]-Pr [kgl/cm2],	ī.	71 72 5.5	P4=	77. PS= 8.3	3	13	01 27	30.00		9 9			2 - 2		১ জ্ব	_	Lugeon value:	f for few second reversed run		rutes under the specified press ust previous one minute	Inspected by: Farhat M. Shah
	oft Bank)	60 degrees		Groundwater level (1)	1	GL - (L)- 30	neter	8 4	OX:17	19.761 19,	19,763 19,771	19,764 19,7	19 766 19 772	19,767 19,773	19,769 19,774 19,774	19,770 19,775					) 0 0 0 0 0 0	7-0 0-0 0-0	9E-MO 72:KO	0.00 0.00 0.00	3 \$	om 4kgf to 1kgf for fev		nued for at least 10 mir se injection rate in the j	
M98-4	Dam Axis (Left Bank)	on (a):	Friction Loss per meter (pt): 1×10°×Q1***	. EL m	ure pauge to	4.50 m	Reading of flow meter		07:42 07:54	19,660 19,688 19,722	19,664 19,693		19,000 19,090	19,674 19,704	19,676 19,707 19,748	19,680 19,712			1		3 5 3 5	-0-2	07:52 OR:04	0.00 0.00 0.00	Friction Loss (Pv) = $p_1(L_0 + L_1)$ [kgf/cm2]	From 7kgf to 4kgf and from 4kgf to 1kg	COS60=0.868	Injection of water should be continued for at least 10 minutes under the specified verties, within 90 % to 110 % of the injection rate in the just previous one minute	Prepared by: A. Hamid & Azhor
Hole No.:	Location:	Hole Inclination (a):	Friction Loss	Ground elevation : Ef.	Pipe length from	hole mouth: (L)		Conge P. Pal.		U(min) 19,631	2 19,635	3 19,637	12,03	6 19,642	7 C	٠,٥	3 =	្ត ដ	3 4		Total	].°	07:40	(%) 0.00	Friction Loss (Pr	Remarks:		Note: Injection	Prepared by :

#### Water Pressure Test

8 8/14

60 degree  Groundwater)  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)=  GL. (L.)		1					İ							
Friction Loss per meter (p): 1x10 ⁴ xQ ¹⁷⁷¹ Ground cievation: EL. m Groundwater level   Pipe length from pressure gauge to   CL. (L.)= 35    Note mouth: (L.)= 4.50 m CL. (L.)= 35    Note mouth: (L.)= 4.50 m CL. (L.)= 35    Note length from pressure gauge to   CL. (L.)= 35    Note mouth: (L.)= 1.20    Note: loger   Pal   P.Z.   P.Z.    Note: loger   Pal   P.Z.   P.Z.    Note: loger   Pal   P.Z.   P.Z.    Reading of flow meter   P.Z.    Note: loger   Pal   P.Z.    Reading of flow meter   P.Z.    Note: loger   Pal   P.Z.    Note: loger   Pal   P.Z.    Note: loger   Pal   P.Z.    Remarks:   Reading of flow meter   P.Z.    Remarks:   Reading of flow meter   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   Remarks:   Revire reading for few soo    Note: loger   P.Z.   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.   P.Z.    Remarks:   Revire reading for at least 10    Note: loger   P.Z.   P.Z.   P.Z.    Note: loger   P.Z.   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.    Remarks:   Revire reading for at least 10    Note: loger   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.    Remarks:   Revire reading for at least 10    Note: loger   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   Remarks:   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.    Remarks:   P.Z.   P.Z.   P.Z.    Remarks:   P.Z.	Hole Incli	inatio	;; ;;			ક	Segreta Segreta		Packer Type:	i	Mechanical			
Cround clevation: EL m Groundwater level ( Pipe length from pressure gauge to  Note mouth: (La)= 4.50 m GL-(La)= 35   Cauger   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Pal   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Cauger   Pal   Pal   Pal   Cauger   Pal   Pal   Cauger   Pal   Pal   Cauger   Pal   Pal   Cauger   Pal   Pal   Cauger   Pal   Pal   Cauger   Pal   Pal   Cauger   Pal   Pal   Cauger   Pal   Pal   Cauger   Pal   Cauger   Pal   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger   Pal   Cauger	Friction 1	oss p	ğ H	cr (p) :	1×10	QX	ä		Date:		14/January/1999	666		
Pipe length from pressure gauge to   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth   Depth	Ground ele	logies.	1		Γ	Sound Supplied	vaior ley		07 13 70	E	Gauge height (La):	ght (L.):	0.70	E
Solid mouth; (L)=   4.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   CL-(L)=   3.50 m   C				1 2 2			۱	1	Į۶		3	(L) notice of section (L)	3	
Reading of flow meter   Reading of flow meter   Cauge F. Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   Fa.   F	rige iengin			2 4 2 2		10.10		. E	( <u>1</u> )	. e	!	<b>.</b>	. 6	
L   -   -   -   -   -   -   -   -	THE HOUSE	1	1	Ting of	Sow III	٥		1	_	Calculat	Calculation of Lugeon value	eon value		
	L			-	7	V	Ş	6						
<u> </u>		<u> </u>		<u> </u>	. ≘	5, 1	3, 4		P=P++0.1(sin(a)L+L)-Pr [kgf/cm2],	(a)(-1,-1)(a)		q=O_/L>[livmin/m]	/min/m]	
Q(mm)         31,298         31,331         31,401         31,408         31,400         31,400         31,400         31,400         31,400         31,400         31,400         31,400         31,400         31,400         31,400         31,400         31,400         31,401         31,401         31,401         31,401         31,401         31,401         31,401         31,401         31,401         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402         31,402 </td <td>l</td> <td>9.5K</td> <td>18.12</td> <td>18:24</td> <td>S.</td> <td>18:48</td> <td></td> <td></td> <td></td> <td></td> <td>ò</td> <td></td> <td></td> <td></td>	l	9.5K	18.12	18:24	S.	18:48					ò			
1 11,000 31,334 31,371 31,415 31,456 31,456 31,466 31,466 31,430 31,339 31,377 31,425 31,439 31,459 31,469 31,466 31,466 31,309 31,349 31,349 31,439 31,439 31,449 31,466 31,466 31,466 31,309 31,349 31,349 31,439 31,449 31,449 31,466 31,466 31,319 31,319 31,339 31,439 31,449 31,449 31,466 31,470 31,319 31,339 31,349 31,449 31,449 31,469 31,470 31,319 31,339 31,349 31,449 31,449 31,469 31,470 31,319 31,339 31,349 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449 31,449			31,331		31,410	31,455					42.	5		
2 31,302 31,337 31,374 31,420 31,457 31,462 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463 31,463	<u> </u>		3,334											
2 11,205 31,339 31,371 31,425 31,459 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465 31,465	e4		31,337							_	*	, ,		
4 31,307 31,342 31,348 31,427 31,440 31,446 31,466 31,310 31,342 31,343 31,435 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446 31,446	اً		3,39		3,425						<u>.</u>			
\$ 11.309 31.345 31.432 31.4461 31.4466 31.466 31.466 31.466 31.466 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.467 31.46	4		31,342					٠.		r.	ė			
6   31,312   31,348   31,348   31,435   31,442   31,445   31,445   31,314   31,333   31,345   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,446   31,447   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472   31,472	ر د		31,345						2		#./\$ ⁻	7.0		
7   31,314   31,350   31,391   31,441   31,443   31,465   31,465   31,465   31,465   31,465   31,465   31,465   31,465   31,467   31,465   31,465   31,467   31,467   31,467   31,467   31,470   31,467   31,467   31,470   31,467   31,472   31,467   31,467   31,467   31,467   31,472   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,477   31,477   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467   31,467	9		31.348					31,472						
8	7		31,350					31,473	ا وو					
9 31,319 31,356 31,397 31,445 31,445 31,445 31,472 3  10 31,321 31,338 31,460 31,454 31,467 31,472 3  11 12	ŀ		31,353							•	\			
10   31,321 31,358 31,450 31,454 31,467 31,472 3	_	319	31,356							, o	*			
13		33	31,358								_		_	
12 ————————————————————————————————————	=						1		2.0	•				
Total Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100 Onl 100	2	! 		ļ				j	2 6	•				
14   10   10   10   10   10   10   10	2	1	Ì					İ	? :	••				
15   0-1   0-2   0-3   0-4   0-5   0-6   17   17     11	4	:	1											
	4	1	Ī			Ì	į	1	2	~-(				
Average Gu-1 Gu-2 Gu-3 Gu-4 Gu-5 Gu-6 Gu-6 Gu-6 Gu-6 Gu-6 Gu-7 Gu-7 Gu-7 Gu-7 Gu-7 Gu-7 Gu-7 Gu-7	<u> </u>	 ;;	3 8	3	3	3,-	3,5		2.0	•				
Note   Lipsetton of water should be continued for at least 10   Note   Lipsetton of water should be continued for at least 10   Note   Lipsetton of water should be continued for at least 10   Note   Lipsetton of water should be continued for at least 10   Note   Lipsetton of water should be continued for at least 10   Note   Lipsetton of water should be continued for at least 10   Note   Lipsetton of water should be continued for at least 10   Note   Lipsetton of water should be continued for at least 10   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Note   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rate in It   Lipsetton rat	4		,			ŀ		ŀ	0.7				_	
Friction Loss (P ₂ ) = pr(La + L ₂ ) {kg/cm2}   18:346   18:34   19:10   (P ₂ )   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.		 1 ;	;	٠	3	3	3,2	; 6	] 8 					
Friction Loss (Pr) = pr (La + La) [kg//cm2]	L.	Tē ĕ	13:22	<u>1</u>	L	1	_	19.22	00	0.5	0.1	ij	20	0
Friction Loss (P.) = pr(La + Lu) [kg/lcm2]  Remarks:  Revirse reading for few sect  COS60a0.868  Noie: Injection of water should be continued for at least 10  verifey within 90 % to 110 % of the injection rate in it	L	8	000	Ш		i _ l	0.00	00'0						
Remarks:  Revirse reading for few sect  COS60#0.868  Noie: Injection of water should be continued for at least 10  vertley within 90 % to 110 % of the injection rate in it	Friction Lo	S (P)	a) 0 =	¥ (3)	gf/cm2]		•	3		Lugeon value:	8.0	3		
Remarks:  Revirse reading for few secon COS60#0.868  Note: Injection of water should be continued for at teast 10 veriles within 90 % to 110 % of the injection rate in it.		-					•	3		Critical Pressure:	. >11	kgt/cm2		'
1 1	Remarks:				Revirse	reading	for few s	econds t	y decredsing t	10 4 & I kgG	/cm2			
1 1		-	COS60	0.868										
Settles within 30 % of 10 % of the injection rate in the		cction	of wate	rshould	be conti	rued for	at Icasi	10 minut	es under the sp	section pres	sure, after the	injection rat	ic per min	٤
	4	Š	3	0	1 20 02 1		100		MC WRIGHT	1	-			l
Prepared by: A. Hamid & Azhor	Prepared	 6	노	mid &	Azhor				Inspected by : Farhal M. Shan	y: Farha	M. Shan			-

Hole No.:	M98-4	Stage:	9/14	Hole N
Location:	Dam Axis (Left Bank)	Dia. of Hole:	76 m/m	Location
Hole Inclination (a):	tion (a); 60 degrees	Packer Type: Mechanical	Mechanical	Hole In
Friction Los	Friction Loss per meter (pt): 1×10°×01911	Date:	15/January/1999	Priction
	ŀ	1 3.Cr 12.50 m	Cause to in [1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1	The second

			E 0.70	ction (14)	E	45		(livminvm)		9		-		7.4						-								20				Ě	-
76 m/m	Mechanica!	15/January/1999	Gauge height (La):	(all of section (La)		Calmination of Luseon value		[kgt/cm2], q=O=/	41 0,3	975					• •			_	•	_								-	2	,	8.0	>11 kgi/cm;	
Dia. of Hole:	Packer Type:	Date:	1. 13.50 m		1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1	Г		P=Pa+0.1(sin(a)Li+Li)-Pr[kgt/cm2], q=Q-/Li [lit/min/m]	Pl= 2.2					FO = 0.2	P7= 2:2		10,0	0.6	0.0	2.0		0	7 : 04	3.0	50	0.1	00		3		Lugeon value:	Critical Pressure:	
	60 degrees	 	Occumulation land (La). Gr. 13.50		5 E		-1	P.7 4	OR:OD OR:12	41,640	1,62	4 2, 2,	2,63	25,6	240,	4,048	2,2	41,650	41,651	7 41,652 41,655	-	-			ટ	-1	0	1.2	0M:10	0.00 0.00		3	
Dam Axis (Left Bank)	9	riction Loss per meter (pt): 1×10°×019111	- Constant		1	- TOI	빏	7 0 3 v		7 41,590 41,624	41,595	41.59	1,603		41,612	41,615	41,619	5,62	41,627	2 41,632 41,647	!			<u> </u>  -  -	ઢ	42 23	Cave Oavs	4.2	4 07-46 07:58	003 000	kg(/cm2]		
Dam,	on (a):	per meter (pr)		10.1	GSurc B	_ ['	Kending	Pu2 Pu3	٦	41,512 41,547	41,515	41,518	41,520	41,522 41,562	45,53	41,528	41,521	41,534	41,537	41,540 41,582	:	1		1	200	28 35	Oav2 Oav3	Н	07-22 07:34	0.00 0.01	nction Loss (Pr) = pr(Lo + L.) [kgf/cm2]		
ocation:	iole inclination (a):	iction Loss		round cicyanon . E.	pe kngth Irom	ole mouth: (Le)		mage P. Pul.	00-CO			2 41,493	3 41,495	4 490	5 41,498	6 41.499	7 41,500	8 41,502	9 41 504	10 41,506	=======================================	12	<u> </u> ព	1	Total O.1	_	Average Onv1	1.7 January 1.7	U1:10	(94) 0:00	nction Loss (P	ļ	(cmarks :

#### Water Pressure Test

Hote Inclination (a):	Hole No.:	ا 		1 2 2 3		١							
Hote Inclination (a):   600 degrees   Packer Type:   Mechanical	Location	٠.		Sum A	is) (ic	Bunk			Dia, of Hol		76	m/m	
Principal Loss per mater (p)   1 k10 ⁴ x0 ^{4/11}   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/1999   Date : 15/Januaay/	Hole Incl	linatio	(E)	•		93	degrees		Packer Typ		cchanical		
Direction of levation: EL.   m   Groundwater level (LJ): GLJ.   13.80 m   Chape Neight (LJ): GLO.	Friction	Loss p	cr met	ار. الله تا		Š	اع		Date:	15,	January/1	8	
Pipe length from pressure gauge to hold end of the production of Langth of section (La)      Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page   Page	Ground ele	vation	Er.			Ground	rater levi	<u>(1</u>			Gauge Deir	1	0.70 m
Noie mouth (L)	Pipe lengt	from p	ressure	Sauge to			1	coth of	est section	ļ	Lens.	nor section	<u>.</u>
	hale mout	3		4.50		01-10	1	45 B	=( <b>₽</b> () 0)	e 05.		s	٤
<del></del>			Read	ing of	Now m	eter				Calculatio	n of Luge	on value	
<del></del>	Caute P.	Po!	F.2	3.	\$ .	ζ.	Pa6	7.4	0-P-4	(1) (4) (4) (4)		on Ond	(m/wiw)
- <del> </del>	(Authorna)	-	,		٦,		,		100				
	-+		17.	77./	Q.		- 11	- 11			÷ć		
	_		3		3			2 5			•		
	,	829	49,647		49,769						9		
	-	2,62	49,652	\$9,705	18/18	40 86							
	_	9,624	49,656	49,71	49,787	49,867					Ġ.		
	_	10.627	80,54	49,718	49,795	49,873					ç		
	_		49,663	49.725	49.804	49.880					<u>ę</u>		
	;		40.667	49.73	49.812	49.886							
		2,0	49 671	40.77	49 R21	49.893							
	;	5 67 5	49 676	49.744	49.829	49 900						į	
		X . 9	40,680)	40.750	49 838						,		
		640	40,684	40.757	49 846				_		• • •	\	
		}	}		2		_				\		
13	:	Ì	1	Ì	-				0.0		\ ::		
13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-   13-	1 :	-	İ	!		1			2.0	€.	•		
15	1		!	-	İ			!		••			
15   10   10   10   10   10   10   10	4	ì		i	1		İ		?	`,			
Total   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil   Quil	13			1					0.	,			
	Total	3	ð	3	3	3	3	3	20.	•			
Note :   Injection of water should be continued for at least 10 nitivites under the specified pressure, after the injection rate per miles within 87 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10 to 10		ĸ	42	\$	86	5	ĸ	3	0.1				
Viryin   2.2   4.2   6.4   8.6   6.1   3.3   2.2   0.0   0.5   1.0   1.5   2.2   0.0   0.0   0.5   1.0   1.5   2.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0	Averago	3	0.2	3	0	3	ŝ	ઠે	5				7
Function   17-10   17-22   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   17-34   1	ri /mio	6	4.2	9.9	8.6	9	'n	7.7	}	,	:	•	•
Finction Loss (Pr) = pr(Lo + Lo) {kg/cm2}	1	7.10	17.22	7:14	7.46	l .	L.	L	_	C.O.	2	7	á
Friction Loss (Pr) = pr(Lo + Lo) (kg/fcm2)	J.	S	100	ŝ	ē	l_	ā	80					
Remarks :   Coscout, 868   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results   Results					5		]		1,1196	on value :	1.5	Lu	
Komarks   COS60w0,868   Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per mit settles, within 87 to 110 97 of the injection rate per mit settles, within 87 to 110 97 of the injection rate in the just previous one minute.	rescion 4		3	<u> </u>	- Comp					cal Pressure:	7	kgf/cm2	
COS60=0.868 Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minutes, within 97 to 10 to 97 to the injection rate in the just previous one minute.	Remarks										: -		
COSGO-0,868  Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per mit settles within 9% to 110 of the injection rate in the just previous one minute.													
Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per min vertiles within 90 % to 110 % of the injection rate in the just previous one minute.			Š 8	9868									
A C1 - 1 4 6 Ambus	1	njection	of walc	r should	be contii	nued for	at least	O minut	es under the sp	ecified pressu	re, after the	injection rat	E 52

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % in 110 % of the injection rate in the just previous one minute.

Prepared by: A. Hamid & Azhor Inspection of Inspected by: Furbat M. Shah

COS60=0.868

Hole No.	M98-4	Stage:	11/14	
Location:	Dam Axis (Left Bank)	Dia, of Hole:	76 m/m	
Hole Inclination (s	ntion (a): 60 degrees	Packer Type:	Mechanical	
Friction Los	Priction Loss per meter (p.): 1×10° ×01*11:	Date:	16/January/1999	,

No.   CL. (L)	Hole Inclination (a): Friction Loss per meter (p): Ground elevation: EL	r (9)	1×1	OS CALL	Oteric	1 (L1):	60 degrees Packer Type:  P* xQ ^{1*71} : Date:  Groundwater level (L ₁ ): GL- 13.40 m Death of real section	., E	Mechanical 16/January/1999 Gauge height (12):	ary/1999 te beight (L2): 0.70 Length of section (L)	ε
Part	4	8	ا 1	J) - 70		£			on of Lune	5 m	
7	٦		3	P-5	Pu6	767			4		Γ
17.54    1460    14812    17.54    1460    14812    1480    14812    1480    14812    1480    14812    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480    1480			2	7	4	1	P=P=+0.1(sin(	**(J+J(*)	[kgf/cm2],	m/min/min/m	_
54,559   54,601   54,623   72= 5.2 q2= 0.8   55,555   54,601   54,625   54,601   54,625   54,603   54,625   54,603   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   54,625   5	-	:24	17:36	17:4K	(00:K1	18:12			5		
34,503   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   34,605   3	X.	Ž.	\$4.452	54,550	26				3. 3	_	
54,567   54,609   54,626   75.8   8.2   q5.8   1.1     54,577   54,613   54,626   75.8   5.2   q5.8   1.1     54,579   54,613   54,626   54,627   10.0     54,584   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628   54,628	χį	3 8	¥ 2	¥ 2 Ç 3	3 3				7 8		
54,579 54,613 54,620 PFe 5.2 qée 0.5 54,579 54,615 54,620 PFe 5.2 qée 0.5 54,579 54,618 54,620 PFe 5.2 qfe 0.1 54,579 54,618 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5.2 qfe 0.1 54,620 PFe 5	Ÿ	Ę	4	54.567	8				Ş		
54,579   54,615   54,625   54,627   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100	X	ž	54,490	54,573	\$4.613		-		Š		
54,589 54,628 54,627 9.0 54,528 54,622 54,627 9.0 54,607 54,623 54,623 8.0 54,607 54,623 54,623 8.0 54,607 54,623 54,623 8.0 54,607 54,623 54,623 8.0 55,607 54,623 54,623 8.0 55,607 54,623 54,623 8.0 55,607 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,623 54,62	Ż,	8		\$5.53	\$19,4				<u> </u>		
54,505 54,622 54,628 8.0 6.0 6.0 54,623 54,628 8.0 6.0 6.0 54,623 54,628 8.0 6.0 6.0 54,623 54,628 8.0 6.0 6.0 54,623 54,628 8.0 6.0 6.0 54,623 54,628 8.0 6.0 6.0 54,623 54,628 8.0 6.0 6.0 6.0 54,623 54,628 8.0 6.0 6.0 54,623 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628 54,628	X.	8		¥ 5	2 S						
54,607 54,628 54,628 70 54,607 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628 70 50,007 54,628 54,628	χĮ	8 4	X	ž ž	2.5		_				
5 54,607 54,628 54,628 7.0	X		54,537		\$4,625				Ġ.	<b>\</b>	
Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Colo	X	Ş	34.4		5,628				•	\	_
Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution   Solution	į	1	:		•	į	0,9	-			_
17.56   13.10   13.22   1.0   1.5   1.0   1.5   1.0   1.5   1.5   1.0   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5		:	!	i	!	İ	5.0	O,	1		
Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   Column   C	ŀ	ī	Ī	į	İ		4.0	/			_
O-5   O-6   O-7   2.0   O-7   2.0   O-7   2.0   O-7   2.0   O-7   0.0   O-7   0.0   O-7   0.0   O-7   0.0   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7	į	1			i	1	3.0	.\			
O-5   O-6   O-7   1.0   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7   O-7	o r	2	<u>\$</u> 5	3.5	3.5	<u>}</u> -	07 5				
5.7 2.7 0.3 0.0 0.0 0.5 1.0 1.5 0.0 0.02 0.02 0.02 0.0 1.5 0.02 0.02 0.00 0.02 0.00 0.02 0.00 0.02 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	c			ý	3	5-7	9:				
17:58   18:10   18:22   0.00   0.3   1.0   1.3   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0   1.0	, ^	8	9.4	\$7.	2.7	Ó	] ; 00	30	۽ ا		 וי
0.02   0.00   0.00	7	χ.	17:46	17:58	13:10	- 1	2	3	2	j	}
Lugeon value: 2.0	Ö	3	0.05	0.02	000	8			1	i	
us as Critical Pressure; >11	7	7	(f/cm2)		:	2	Luger	on value :	2.0	ន	
					2	3	Critic	nd Pressure:	ج ۲	kgf/cm2	1

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute verties within 90 % to 110 % of the injection rate in the just previous one minute

Prepared by: A. Hamid & Azhor

Revine reading for few seconds by decrecising to 4 & 1 kg/lcm2 COS60=0.868

### Water Pressure Test

Hole Inclination (a):			Commission (a):   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees   60 degrees	76 m/m  Mechanical  16/lanuary/1999  16/lanuary/1999  Couge beigh (L.): 0.70  Longth of section (L.)  Colculation of Lugeon value  1(L+L.)-Pr [kg/cm2], q=0/L [ii/miv/m]
			Climation (a);   Clo degrees   Climation (b);   Ix10 ⁴ xQ ¹⁹⁷¹ ;   Laboration   EL	Mechanical  16/January/1999  Gauge height (L.): 0.70  Gauge height (L.): 0.70  Length of section (L.)  alculation of Lugeon value  L+L.)-Pr {kg(vcm2], q=0/L.} [ii/miv/m]
			n Loss per meter (p): 1x10 ⁴ xQ ¹¹¹¹ :  elevation: EL	1,1999  eight (L.): 0,70  eight of section (L.).  5 m  geon value  q-0(1i(min/m)
			## Groundwater fever (LL)**C gbt from pressure gauge to ## Groundwater fever (LL)**C gbt from pressure gauge to ## GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E \$5 m and GL.*(L)**E	eigh (L.): 0.70  gh of serion (L.).  S m  geon value  q=0/L [it/miv/m]
			## Character gauge to ## Ch.—(L.)= SS m   Reading of flow meter   P.    ## A 7	2 160
			Reading of flow meter   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.   Pa.	165
			Reading of flow meter   Pa2   Pa3   Pa4   Pa2   Pa3   Pa4   Pa2   Pa3   Pa4   Pa2   Pa3   Pa4   Pa2   Pa3   Pa4   Pa2   Pa3   Pa4   Pa2   Pa3   Pa3   Pa4   Pa2   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3   Pa3	6.0
			Pa_1   Pa_2   Pa_3   Pa_4   Pa_2   Pa_4   Pa_2   Pa_4   Pa_2   Pa_4   Pa_3   Pa_4   Pa_4   Pa_4   Pa_4   Pa_5   Pa_4   Pa_5   Pa_4   Pa_5   Pa_4   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5   Pa_5	
			16:00 16:12 16:24 16:36 16:48 17:00 17:12 16:00:00:00:00:00:00:00:00:00:00:00:00:00	
60,028   60,028   60,018   60,228   60,228   60,329   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   60,328   6	38	38	60,023 60,028 60,118 60,202 60,273 60,329 60,362 60,034 60,074 60,125 60,209 60,273 60,339 60,363 60,034 60,074 60,125 60,209 60,273 60,339 60,340 60,034 60,074 60,125 60,209 60,228 60,339 60,340 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60,034 60	
<del></del>	<del></del>	<del></del>	60,228 60,333 60,366 60,229 60,340 60,346 60,229 60,343 60,373 60,329 60,346 60,373 60,329 60,346 60,373 60,315 60,348 60,373 60,315 60,348 60,377 60,316 60,348 60,377 60,316 60,348 60,377 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,378 60,316 60,348 60,348 60,316 60,348 60,348 60,316 60,348 60,348 60,316 60,348 60,348 60,316 60,348 60,348 60,316 60,348 60,348 60,316 60,348 60,348 60,316 60,348 60,348 60,316 60,348 60,348 60,316 60,348 60,348 60,348 60,316 60,348 60,348 60,348 60,316 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,348 60,	
	<del></del>	<del></del>	60,285 60,345 60,346 60,286 60,286 60,286 60,345 60,345 60,375 60,346 60,375 60,346 60,375 60,346 60,375 60,315 60,315 60,315 60,315 60,315 60,315 60,315 60,315 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60,316 60	8.2 43=
			60,229 60,346 60,358 60,279 60,234 60,279 60,245 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,326 60,361 60,384 80,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60,372 60	11.2
		<del></del>	60,229 60,346 60,370 (60,29) (60,346 60,372 (60,346 60,372 (60,346 60,372 (60,346 60,372 (60,346 60,345 (60,346 60,345 (60,346 60,346 60,346 (60,346 60,346 60,346 (60,346 60,346 60,346 60,346 (60,346 60,346 60,346 60,346 60,346 (60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,346 60,3	8.2 q5m
		<del></del>	60,229   60,346   60,372     60,304   60,345   60,345     60,315   60,345   60,345     60,315   60,345   60,347     60,326   60,341   60,347     60,326   60,341   60,347     60,326   60,341   60,347     60,326   60,341   60,347     60,326   60,341   60,347     60,326   60,341   60,347     60,32   60,341   60,347     60,32   60,341   60,347     60,33   60,341   60,347     60,33   60,341   60,347     60,33   60,341   60,347     60,34   60,341   60,341     60,35   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344     60,37   60,344	5.2
<del></del>		<del></del>	60,330+ 60,349 60,375     60,315 60,335 60,377     60,315 60,335 60,377     60,326 60,356 60,361     60,326 60,361 60,384 7.5     60,326 60,361 60,384 7.5     60,326 60,361 60,384 7.5     60,326 60,361 60,384 7.5     60,326 60,361 60,384 7.5     60,326 60,361 60,384 7.5     60,326 60,361 60,384 7.5     60,326 60,361 60,384 7.5     60,326 60,361 60,384 7.5     60,326 60,326 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60,327 60	2.2
<del></del>	<del></del>	<del></del>	60,3150 60,332 60,377 100, 60,315 60,378 60,379 94, 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,326 60,3	
<del></del>		<del></del>	60,315 60,335 60,345     60,320 60,361 60,384     60,320 60,361 60,384     60,320 60,361 60,384     60,320 60,361 60,384     60,320 60,361 60,384     60,320 60,361 60,384     60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320 60,320	
<del></del>			60,330   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   60,338   6	•••
<del></del>			60,326 60,361 60,384 7.1 	•
<del></del>	<del> </del>		Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Cont	<u> </u>
<del></del>	<del></del>	<del></del>	Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Cont	:/
<del></del>	<del></del>	<del></del>	Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Color   Colo	•
<del></del>	<del></del>	<del></del>	Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Construction   Cons	
<del>-1                                      </del>	<del>-1 1: 131  </del> - 15	<del>-1 1: 1:1</del> - 15	Que5   Queb   Que5   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2	
<del>' '                                    </del>	<del>' '                                    </del>	<del>' '                                    </del>	Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size   Size	7
<del>'                                      </del>	<del>'                                      </del>	<del>'                                      </del>	Ogy Ogy Ogy Ogy Ogy Ogy Ogy Ogy Ogy Ogy	
<del>: isl</del> e 15	<del>: isl</del> i - 19	<del>: isl</del> ie 15	5.3 2.2 0.0 1 16.58 17:10 17:22 0.02 0.03 0.00	
<del>ist (</del> - 15 )	<del>isl (</del> - 15	<del>isl (</del> - 15 )	1 5.58 17:10 17:22 0.02 0.01 0.00 0.0 10:10 17:22	
<del>21 (</del> - 19	<del>21 (</del> - 15	<del># 1</del> - 15	0.02 0.03 0.09 0.03 0.09	1.0
1 - 15 l	1 - 15 l	1 - 19 l	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
- 19	- 15	- 15	2 2	-
15 1	15 1	15 1	[4.1] [4.1]	17
3 1	3 1	3 1	Destable :	
			COS60=0.868	
				ecified pressure. After the injection rate per minute
THE PARTY WILLIAM THE REAL PROPERTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE P				ninute

(

Hole No.:	M98-4		Stage:	13/14	Hole No.:	M98-4	
Location:	Dam Axis	ım Axis (Left Bank)	Dia. of Hole:	76 m/m	Location:	Dam Axis (Left Bank)	Bank)
Hole Inclination (a):	1	60 degrees	Packer Type: Mechanical	Mechanical	Hole Inclination (a):		60 degre
Friction Loss per meter (	s per meter (ps): 13	(p.): 1×10+×0,27;	Date:	17/January/1999	Friction Loss	Friction Loss per meter (pt): IxI 0 x0119711	×0,1971:
Ground elevation : EL		Groundwater level	(L.):GL- 13.50 m	m (Croundwater level (L.): GL. 13.50 m Gauge height (L.): 0.70 m	Ground elevation	Ground elevation : El. m   Groundwater	roundwater

Length of section (

Calculation of Lugcon value

=(~T) O II 0/9 Depth of test section

Rending of flow meter

3

3

Pipe length from pressure gauge to

mouth: (L.)=

62444

P=Pu+0.1(sin(a)L1+L2)-Pr (kgf/cm2), q P1= 2.2 q1= q1= D2= 5.2 q2= q2= P2= 5.2 q3= P4= 11.2 q4= P6= 5.2 q5= P7= 2.2 q5= P7= 2.2 q5= P7= 2.2 q7=

66,192 66,203 66,192 66,204 66,194 66,205 66,196 66,205 66,196 66,205

65,911 65,968 65,914 65,914 65,914 65,917 6

\$5,873 \$78,83 \$7,85,83 \$7,85,83

65,869 65,870 578,23 578,23

00:80

66,190 66,145 66,190 66 66,000 66,150 66,192 66 66,000 66,150 66,190 66 66,007 66,101 66,190 66 66,007 66,107 66,190 66,190 66,170 66,110 66,170 66,201 66,201 66,201 66,201 66,202 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,120 66,1

65,922 65,988 6 65,924 65,993 6 65,927 65,998 6

icight (L.): 0.70 =	Croun	Ground elevation : EL	1; EL		ء	Groundw	aler Jeve	<u>[</u>	m Groundwater level (L.); GL 12.70 m	Cauge height (La): 0.70
ngth of section (ட்)	Pige 2	Pipe length from pressure gauge to	pressure	gauge to			ă	o qld	Depth of test section	Length of section (L.)
S 3	holen	nouth: (L)		4.50		ار <u>ا</u> ارا	Ļ	e5	hole mouth: (Ls)= 4.50 m (CL - (Ls)= 65 m to (Ls)= 70 m	
geon value			Read	Reading of flow meter	Now III	eter			Calcular	Calculation of Lugeon value
	Cauge P.	Pel	Pu2	ď	3	PuS Pu6 Pu7	8	Po7		
q=O=/L {livmin/m}	(kg0/cm3)	, p-4	4		9	۲.	4		P=P=0.1(sin(a)[L+[L)-P	1 P=Pu+0.1(sin(a)Lu+La)-Pr [kgUcm2], q=Ou/Lu [liumin/m]
11= 0.2	TI PAIS	Shart time 16:20 16:42 16:55 17:37 17:20	16:42	16:55	17:07	17:20	17:32 17:45	17:45	P1= 2.2	q1= 0.1
12. 0.6	Ē	U(min) 74,107 74,116 74,135 74,178 74,270 74,323 74,343	74,116	74,135	74,178	74,270	74,323	74,343		42= 0.3
1.0	,-	74,108	74,108 74,118 74,139 74,186 74,275 72,325	74.139	74,186	74,275	74,325	74,74		43= 0.8
74= 2.1	c1	74,108	74,108 74,120 74,144 74,195	74 144	74,195	74,280 74,327 74,344	74 327	74,744	_	94* 1.8
1.1		74 100	74,109 74,121 74,148 74,205 74,284	74.14%	74,205	74,784	74,329	74,345	75- 8.2	65-
16= 0.3	7	74,110	74,110 74,123 74,151 74,214 74,289 74,33	74,151	74.214	74,289	24,330	74,746		46■ 0.4
17= 0.2	<b>S</b>	111,47	74,125 74,155 74,222	74,155	74,222	74,295 74,332 74,396	74,332	74,396		47= 0.1
	: • = ! 	74.111	74 1111 74 126 74 160 74 2311 74 300 74 334 74 347	74 160	74.231	7.00	74.334	74 747		

E/E

8

Dia, of Hole: Packer Type:

Stage:

14/14

Water Pressure Test

17/January/1999

Date:

60 degrees

Mechanical

	ţ	•	•	~	-	~	••	••								V,	•					ĺ
	.1(sin(a)	ä	2,	Ļ	74	ζ	Ş	ż		l	_							_	9			
	Par Parto. 1									10.0	0	2 6	9 6	?	0.0	8.0	0.4	3.0	2.0	1.0	6	š
£	1	17.45	74,343	74,74	74,744	74,345	74,46	2,28	74,747	*	74,349	74,349	74,350		İ	İ	<u> </u>		٥ ا	7	S	
3	4	17:32	74,323	74,325	74,327	74,329	74,330	74,332	74,334	74,336	74,337	74,339	24,341	!					3	18	Š,	œ
3	7	17:20	74,270	74,275	74,280	74,284	74,289	74,295	7.00	200	74,310	74,315	74,320			į			ŝ,	50	Š	ç
3	10	17:07	74,178	74,186	74,195	74,205	74.2.4	74,22	74,231	74.241	74,250	74,260	74,268		!		Ī		3	8	3	0
3	7	16:55	74,135	74,139	74 144	74.148	74,151	74,155	74.160	74 10	74,168	74,171	74,175		   	-	Ī		3	9	3	•
70.	4	16:42	74,116	74,118	74,120	74,121	74,123	74,125	74,126	74.13	74,129	74,131	74,133	:	İ	ĺ	:	İ	3	17	ر د	
7		16:30	74,107	74,108	74,108	74 100	74,110	74,111	74,11	74 112	74,113	74,113	74,114			1		!	ã,	7	5	
<u>.</u>	/cm3/	Ė	(uim				4	S	ۍ:		.00	٠.	:0	=	'2			v.	130	ï,	2011	1

0.02 0.00 0.00 (Pr) 0.00 16:52 17:05 17:17 (Pr) 0.00 0.00 0.01 0.05 Friction Loss (Pr) = pr(Lo + Lo) [kg//cm2] 3.8 ۲ - ۵ ី ខ

50

3.

3

S

00

0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.

ð

ટુંત્ર

3.≅

2 <mark>ق</mark>

ą.

7.2 3.7

Lu' kgf/em2

(1.7)

Lugeon value: Critical Pressure:

20

ដ

2

S

0

ؾ

6.7

Lugeon value:

Critical Pressure

COS60=0,868

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute sertles within 40 % to 110 % of the injection rate in the just previous one minute.

Inspected by: Azim Gill

Prepared by: A. Hamid & Azhor

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute sertles within 90 % to 110 % of the injection rate in the just previous one minute. Inspected by : Azim Gill Prepared by: A. Hamid & Azhor

inction Loss (Pr) = pr (Lo + Lo) [kgf/cm2]

COS60=0.968

= 2 2 2 2 E GE2 - 37

# Permeability Test (Open End Constant Head Method)

1/5	430 mm	п.50 м	.47 m
Stage:	Dia. of Hole (2r):	Bottom of Casing:	Constant Head Level (GL. + h3): 4.47
		1.50 m	0.00 m
Hole No.: M98-5	Location: Dam axis (river)	Bottom of Hole (GL-h1):	Groundwater Level (GL-h2): 0.00 m
Hole	3	Bott	Š

	Date: 23 /February/1999	Calculation	-		Calculation Formula	6	หา		k : Coefficient of Permeability (cm/sec)	f Hole (cm)	ead (cm) :	when groundwater is Nill Hahlah3	when water found in the hole H=h2+h3	q : Constant Injection Rate into Hole	(cm3/sec)		21.5	H= 597	, mb	k= 9.562E-05					Permeability (k) =	9,56E-05 cm/sec	
!	Test Record Date	ow Meter	Volume of Flow (cm3)	0		700	( X	100		0 r: Radius of Hole (cm)	400 H; Water Head (cm);				009	300	009	400	400		300	400	300	300	Q= 8,100 cm3	q = 405 cm3/min	= 7 cm3/xcc
	(16:30)	Reading of Flow Meter	Reading (lier)	4,524.0	4,525.2	4,525,9	4,525.9	4,526.0	4,526.5	4,526.5	4,526.9	4,527.5	4,527.8	4,528.0	4,528.6	4,528.9	4,529.5	4,529.9	4,530.3	4,530.8	4,531.1	4,531.5		4,532.1			
	Start Time: (16:30	SEC.	(Jie)	٥	-	7	-	4	5	*	1	- R	٥	2	==	122	12	4	15	91	12	82	65	ន	Total	Average	

Finish Time: ( 16:50 )

A. Hamced	A. Hameed	K, Yano
Tested by:	Prepared by:	Inspected by:

# Permeability Test (Open End Constant Head Method)

2-0/141		1	Stage:	1	à	
Location: Dam axis (river)	ļ		Dia. of Hole (2r):	I	430	mm
Bottom of Hole (GL-h1):	2.50	٤	Bottom of Casing:	1	2.50	E
Groundwater Level (GL h2):	0000	E	Constant Head Level (GL. + h3):	(GL + h3):	4.47	E
Seat Time ( 18:10)		Te	Test Record	Date:	23 /February/1999	7/1999
	Reading of Flow Meter	Flow Met			Calculation	
Reading (liter)	(liter)	Volu	Volume of Flow (cm3)			
3,096,6	99		0			
3,096.8	6.8		200	Calculation Formula	ormula	
3.00	7.0		200	•	t	
3,097.3	7.3	ļ ļ	300	K = X	13	
3,09	7.5		200	}		
3,097.8	7.8		300	k : Coefficient of Permeability (cm/sec)	( Permeability	(cm/sec)
3,098.1	8.1		300	r: Radius of Hole (cm)	le (cm)	
3,098.3	8.3	1	200	H: Water Head (cm);	: (m)	
3,098.5	85		200	when groundwater is Nill		H=h1+h3
3,09	8.9		400	when water found in the hole H=h2+h3	nd in the hole h	H=h2+h3
3,099.1	9.1		200	q : Constant Injection Rate Into Hole	ction Rate Into	Hole
3,099.4	9.4		300		5)	(cm3/sec)
3,099.7	9.7		300			
3,100.0	0.0		38	ŀ	21.5	
3,100.3	0.3		300	ł	269	
3,100.7	0.7	   	000	f	4	
3,101.0	0.1		300	¥	5.359E-05	
3,101.2	1.2		200			
3,10	3,101.4		200			
3,101.7	1.7		300			
3,101.9	9.1		200			
		-0	5,300 cm3	Pem	Permeability (k)	Ħ
Average		5	265 cm3/min		5.36E-05 cm/sec	u/sec
		II	4 cm3/sec			

Finish Time: ( 18:30 )

A. Hamced	A. Hameed	K.Yano
Tested by:	Prepared by:	Inspected by:

#### Permeability Test (Open End Constant Head Method)

Hole No.: M98-5		Stage:	3/5		
Location: Dum axis (river)		Dia. of Hole (21):	430 mm	m <del>m</del>	
Bottom of Hole (GL h1):	3.50 m	Bottom of Casing:	3.50 m	E	
Groundwater Level (GL-h2): 0.00 m		Constant Head Level (GL. + h3): 5.61 m	5.61	E	

Test Record

Date: 24 /February/1999	Calculation			Calculation Formula	ŧ	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		k: Coefficient of Permeability (cm/sec)	r : Radius of Hole (cm)	H: Water Head (cm);	when groundwater is Nill H=h1+h3	when water found in the hole Mah2+h3	q : Constant Injection Rate into Hole	(cm3/scc)		7. 21.5	н. 913	q= 49	k= 0.0004587					Permeability $(k) =$	4.59E-04 cm/sec	
	low Meter	Volume of Flow (cm3)	0	5,400	4,600	4,200	4,100	2,200	2,200	2,700	300	2,500		4,200	2,300	3,700	2,300	1,200	2,800	3,500	3,500	2,700	2,400	O= 59,300 cm3	q = 2,965 cm3/min	= 49 cm3/sec
(9:10)	Reading of Flow Meter	Reading (liter)	3,970.0	3,975.4	3,980.0	3,984.2	3,988.3	3,990.5	3,992.7	3,995.4	3,995.7	ļ !	4,000.7	4,004,9	4,007.2	4,010.9	4,013.2	4,014.4	4,017.2	4,020.7	4,024.2	4,026.9	4,029.3			
Start Time: (9:10)	Lime	(min.)	0			3	1 -	· •	. 9		   	<u> </u>	2	11	12	ח	4	;   2	92	12	82		8	Total	Average	
		-					_	_	_			GF	: າ	. 3	o		•									

when groundwater is Nill HwhI+h3 when water found in the hole Hwh2+h3

17,800 18,000 17,700 17,700 18,100

r: Radius of Hole (cm) H: Water Head (cm); q : Constant Injection Rate into Hole

(cm3/sec)

r= 21.5 H= 903 q= 278 k= 0.0026027

17,400 5,400 15,200 15,100

7,162.0 7,180.0 7,197.7 7,215.4 7,233.5 7,233.5 7,233.5 7,234.2 7,294.2 7,309.3

Finish Time: (9:30)

A. Lanner	A. Humeed	K Yano
באכם טיי.	repared by:	semented by.

#### Permeability Test (Open End Constant Head Method)

Hole No.: M98-5  Location: Dam axis (river)  Bottom of Hole (GL h1): 4.5  Groundwater Level (GL b2): 0.0  Start Time: (11:00)  Reading (liter)  (min.)  7,037.0  7,072.7  7,072.7	Stage: 4/5	Dia. of Hole (2r): 430 mm	4.50 m Bottom of Casing: 4.50 m	0.00 m Constant Head Level (GL + h3): 4.53 m	Test Record  Date: 24 /February/1999		Volume of Flow (cm3)	0	17,600 Calculation Formula	18,100	1	00.01
	M98-5	Dam axis (river)	ļ	ı	:(11:00)	Readi		7,037.0			7.0	•

Finish Time: ( 11:20 )

20 Total

Permeability (k) = 2.60E-03 cm/sec

333,500 cm3 16,675 cm3/min 278 cm3/sec

입 a ..

14,700 15,800

15,500

7,324.5

A. Hamced	A. Hameed	V Van
rested by:	repared by:	penerged by:

# Permeability Test (Open End Constant Head Method)

\$/\$	430 mm	7.50 m	4.63 m		Calculation			nula	•			k : Coefficient of Permeability (cm/sec)			is Nill Health3	when water found in the hole H=h2+h3	on Rate into Hole	(cm3/sec)		21.5	1213	~ %	0.0002614					Permeability (k) =	2.61E-04 cm/sec	
İ	İ	j	el (Gt_ + h3):	č	IJ			Calculation Formula		K SSOL		k : Coefficient of Po	r: Radius of Hole (cm)	H: Water Head (cm);	when groundwater is Nill	when water found a	q : Constant Injection Rate into Hole			*	ŧ	ŀ	kв 0.0					Рсгле		•
Stage:	Dia, of Hole (2r):	Bottom of Casing:	Constant Head Level (GL + h3):	Test Record	Meter	Volume of Flow (cm3)			2,000	3,000	2,000	2,000	3,000	2,000	3,000	2,000	1,000	2,000	2,000	3,000	2,000	3,000	2,000	2,000	3,000	2,000	2,000	O= 45,000 cm3	q ≈ 2,250 cm3/min	⇒ 38 cm3/xec
M98-5	Location: Dam axis (river)	Bottom of Hole (GL-h1): 7.50 m	Groundwater Level (GL-h2): 0.00 m		( 11:30 ) Reading of Flow Meter	Reading (liter)	5,231.0	: :: !	5,235.0		5,240.0	5,242.0	5,245.0	5,247.0	5,250.0	5,252.0	5,253.0	5,255.0	5,257.0	5,260.0	5,262.0	5,265,0	5,267.0	5,269.0	5,272,0	5,274.0	5,276.0			
Hole No.:	Location:	Bottom of 3	Groundwate	į	Time	Elaosed (min.)	0	1	64	5	4	8	•	7	i s		2	=	12	   12 	. 4	2	1 2	12	18	161	200	Total	Average	

#### Water Pressure Test

		,	•					•			ì	•			
Location:	::0	Diam a	Dum axis (River)	၌	ĺ		•	Dia. o	Dia. of Hole:		ę	E/E		ŀ	
Hole 1	Hole Inclination (a):	on (a):	·		8	90 degrees		Packer	Packer Type:		Mechanical	ij			- 1
Friction	Friction Loss per meter (pt): 1x10 xQ1,111.	per met	تد ( <u>آم</u> ) ::	e X	Ç	اي		Date			25/February/1999	٧/1999		1	- 1
Ground	Ground elevation : EL.	19		E	Ground	vater leve	Groundwater level (L.); GL.	1	0.00 m		Gauge	Gauge height (La):	H	0.82	E
Pipe le	Pipe length from pressure gauge to	pressure	gauge to			Ā	Depth of test section	A Section		i	د ا	(L) noitos lo rigna.	00100	3	1
hole me	hole mouth: (L.)	•	4.60 m		GL - (L)		10 3	to (La) ≃	15 E	E .		49.1	E		ı
			Reading of flow meter	flow m	eter					alculat	Calculation of Lugeon value	seon va	a		
Consign P. (ket/kms)	104	P.C.	. Ped.	<b>7</b> . ≅	3.	<b>₹</b> 4	<del>ر</del> ة -	P. Posto.	J(Sin(a)	4-(-)-7	PaPo+0.1(sin(s)\(\frac{1}{2}\)-Pr \(\kappa \)(cm2).	a=O=/-O=o	L High	in/mi	
Start time	100	10-12	107.5	5	10.4	3	11.12		14	`=	•		*	•	
(mim)	1.2	Į₹	96 070	l»	8	l∞	26.197		3	4			5,0		
			<b>36.07</b> 0				86,197		Š	7.1			9.6		
C1			86,082			86,186			P4=	10.1			0.7		
'n	_					86,188			Ϋ́.	7.1		Ŀ	٥. 4		
₹		86,049	86,080	86.138	86.168	86,189	86,197		₽6	4.1			9		
Y	86.014					86.190			7	Ξ		-Z-0	00		
٠	86,016				86 172	86,192									
	86,018		86.099			86,193			١			ŀ			-
'∞	₩ 020					86.18	86,198	ζщ							
6	86.023					86,198		13,"]	- 00		•	•			
9	86,026	86,065		86,157	86,180		8,18	81			Ġ.	•			
Ξ.	i	!	-	į	!		!	ni s	•		٠.,	\			_
2		Ī	1	1		1	j	IT.	·		٠.	\			
ລຸ	-		ļ	ì			j	551	4	Υ.		•			
7				į	į	ļ	į	4	m	٠.	`				
15						١,		17]1							
Total	_	Ş	3	Š	3	ટ	ò	M			•			_	
Ξ		£;	2	X,	۶	- 1	r z								
A PARTE		Š	3	Ş	Š,	ĵ	ે		0	0.1 0.2	0,2 0,3 0,4 0,5 0,6 0,7 0,8 0,9	5 0,6 0,	.7 0.8	6.0	-
iii./min	2.2	. 1	3.2	3.4	~	•	┚			11/2-625		1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	1	,	
Pinish ter	10:10	10.22	10:35	10.46	10:SX		_ 1			A BIC	water injection saito (q : nc/missin)	M : 6 OIL		-	
(·d)	0.00	0,00	0.00	0.00	000	0.00	000								
Friction	Friction Loss (Pr) = $pr\{L_0 + L_0\}$ [kgt/cm2]	d) = (-	¥ ?	kf/cm2]		3	1		uo-3n	Lugeon value:	0.7	នឹ			
			•			1	ř		Circ	Critical Pressure:			ď		
Kemarks	.5											Ì			
Note:	Injection of water should be continued for at least 10 minutes under the specified	n of wate	r should	be confin	of poor	at icast 1	O minute	s under	the spec	red pre-	Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute	the anjectic	on rate	Ser Ban	13
									Ē						





A. Hameed A. Hameed

Tested by:
Prepared by:
Inspected by:

Hole No.:	M98-5		Stage:	2/4		Hole No.:
Location:	Dam axis (River)		Dia. of Hole:	76 m/m		Location:
Hole Inclination (a)	tion (a):	90 degrees	Packer Type:	Mechanical	1	Hote Inclin
Friction Loss	Friction Loss per meter (p): 1×10° ×04971:	0- ×01,471:	Date:	26/February/1999		Friction L
Ground elevation: EL.	£	Groundwater level (	Groundwater level (L.); GL. 0.00 m	Gauge height (La): 0.82	0.82 ш	Ground eleva

E/E

3/4 છ્

Stage:

Water Pressure Test

26/February/1999

Mechanical

Packer Type: Dia. of Hole:

90 degrees

ination (a):

Dam axis (River) M98-5

Date:

oss per meter (ps) : 1×10 ×01,971;

					•									
Gauge height (La): 0.82 m	હ	iround elevation: EL	vation :	1	£	7	Iroundw	arer leve	) ([]) (	m Groundwater level (LJ); GL- 0.00 m   Gauge height (LJ): 0.82 m	Gauge heig	ht (L.):	0.82	E
Length of section (Lu)	ġ.	e length	from pr	ipe length from pressure gauge to	ot agus			ద	pth of te	Depth of test section	on Length of section (Ls)	h of sectio	(۳۱) د	
	No.	e mouth	3	•	1.60 m	<u></u>	۲.	<u>.</u>	20 E	hole mouth: (La) 4.60 m GL - (La) 20 m to (La) 25 m		S	E	-
tion of Lugeon value				Readin	Reading of flow meter	Ow me	rter			Calculz	Calculation of Lugeon value	on value		
	3	Laugar Pul Po2	19	P62	P _t G	ž	PuS	Pu3 Pe4 Pu5 Peo	Pu7					
'r [kgf/cm2], q=O=/L [lit/min/m]	(Page	Ag(/cms)		4	-	20	7	4		I P=P++0.1(sin(a)[x+1.2)-P* [kg//cm2], q=O/L>[lit/min/m]	Pr [kg(/cm2], q	10-0-	Vm.n/m]	
91 0.0	Stan	1 time	×:00	14:12	artime 18:00 18:12 18:24	18:36	18:36 18:48		19:00			q1= 0.0		
92= 0.0	ਤੱ	min) 30.	02551	U(min) 301,123 501,124 501,12	1,124 BC	1,125	01,125B	4921,10	101,127	P. 4.1	ę,	8		
0.0		2	00001	01,12430	1,12430	1,125	01,125	01,126	101,127	2		9		
0.0	!	3	301,123	1,124,00	01,12430	421,10	01,125	01,126	101,127	_	45	00		
45= 0.0		<u>8</u>	01,123501,124	1,12430	1,124bo	1,1250	01 1253	01,126 <b>þ</b>	127	7.	\$	0.0		
	: "	8	827,	301,123501,124501,124	1,124 30	421,10	01,125B	01,126,001,127	101,127	P6. 4.1	90	000		
0.0 ■7₽		S S	301,123501,1245		01,124 30	1.125p	01,125β	25 201,126 201,127	101,127		47	0.0		-

Calculation of Lugeon value

20 B

15 m to (L1)= Depth of lest section

(L)-15

8.68

hole mouth: (L.)

Pipe length from pressure gauge to

P=Pu+0.1(sin(a)L+L2)-Pr [kgf/cm2],

1449441

244544 24444 24444

0 0,1 0,2 0,3 0,4 0,5 0,6 0,7 0,8 0,9 Water Injection Ratio (q : ht/min/m) 000100404 Water Pressure, in kgC/cm2 001.122 501,124 501,124 501,125 501,125 501,125 501,127 501,127 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,125 501,127 501,127 501,125 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,127 501,12 000 000 ဦင ો ડે.૦ 3.0) (0,0) 1.40 I S

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute sentes, within 90 % to 110 % of the injection rate in the just previous one minute.

Prepared by: A. Hamid & Azhor.

Inspected by: M. Suga. Prepared by: A. Hamid & Azhor

Lu kg/cm2

8 2

Lugeon value : Critical Pressur

inction Loss (Pr) = pr(Lr + Lr) [kgf/cm2]

0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9

ટ્રેલ્

3.0 g e

3

j

ૢૼ૾

Total lit.

Water Injection Ratio (q : lit/min/m)

3

99

Lugeon value:

Friction Loss (Pr) = pr(Lu + Lu) [kg0cm2]

Critical Pressur

Remarks:

Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute series, within 90 % to 110 % of the injection rate in the Just previous use minute.

Prepared by: A. Hamid & Azhor

Inspected by : M. Suga

GE2 - 41

27,00

3××××××××××

Water Pressure in kgi'cm?

Stage: 1/14	Dia. of Hole: 76 m/m	Packer Type: Mechanical	Date: 30/January/1999	Nii Gauge height (La): 0.73 m	st section (LL)	10 (L) = 7 m S m	Calculation of Lugeon value	)L++L)-Pr [kg0cm2], q=O-	1.5 -1.5	P3= 7.2 q2= 14.3	9,1	P6= 7.2 q5= 16.0 P6= 4.5 q6= 7.1	1.5 q7=	•	200	200	ui:	o sources	Pres	200	, M	0 5 10 15 20 25 30 35 40 45 50	Water Injection Ratio (q : lit_/min/m)	į	Lugeon value: (7.9) Lu'	3		Injection of water should be continued for at least 10 minutes under the specified pressure, after the unjection tate per minute settler within 90 % to 110 % of the injection rate in the just previous one minute.	Inspected by: M. Suga
Hole No.: M98-6	Location: Upstream Coffer Dam (Left Bank)	Hole Inclination (a): 90 degrees	Friction Loss per meter (p): 1×10 ×0 1111	Ground elevation: EL m Groundwater level (Ls):	ure gauge to	n (CL. (L.) 2 m	Reading of flow meter	. Pub. Pu7	10:12 10:25 10:36 10:48 11:00	O(min) 68,992 69,098 69,333 70,060 71,650 72,465 72,832 1	69,016 69,131 69,472 70,383 71,812 72,537	3 69,026 69,152 69,532 70,546 71,891 72,575 72,882 4 69,034 69,173 69,598 70,700 71,972 72,611 72,900	69,043 69,193 69,667 70,856 72,050 72,645	69,050 69,212 69,741 71,008	69,054 69,252 69,889 71,322 72,292 72,750	9 69,071 69,272 69,966 71,483 72,371 72,735 72,982		12	13		Total Q-1 Q-2 Q-3 Q-4 Q-5 Q-6 Q-7	0-1 0-2 0-3 0-4 0-5 0-6	2 10:35 10:46 10:58 11:10	(Pr) 0.00 0.02 0.28 1.38 0.36 0.07 0.02	Friction Loss (Pr) = pr (Lo + Lo) [kgf/cm2]		Kemarks	Note: Injection of water should be continued for at least 10 minutes under the specified settles within 90 % to 110 % of the injection rate in the just previous one minute	Prepared by: Fathat M. Shah
Stage: 4/4	Dia, of Hole: 76 m/m	Packer Type: Mechanical	Date: 27/February/1999	Ci . 0.00 m Gauner betoht (L.): 0.32 m	Ction Length of section	30	1	P=P=0.1(sin(a)L+L-P) [kg/cm2], q=O=/L-[livmin/m]	~4	P2= 4.1	P4= 10.1 q4=		P7= 1,1 q7=			13/38:		\$1ns	22317 4 c.	131	- C	0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1	Water Injection Ratio (q : lit_fmin/m)	3	Lugeon value: 0.0	Critical Pressure: >10 kg/cm2		se under the specified pressure, after the injection rate per minute needing one minute	Inspected by : M. Suga
Hole No.: M98-5	Location: Dam axis (River)	, disci	lier (pc) : 1×10° ×		o como en	25	ow meter	George F. Pol. 1922 Pt.3 Pol. Pick Pub. Pub. Pub. Pub. Pub. Pub. Pub. Pub.	OK:00 ON:12 ON:23 ON:35 ON:46 C	64,077 64,080 64,083 64,082 64,081	2 64.072 64.077 64.080 64.083 64.082 64.081 64.079	64,077 64,080 64,083 64,082 64,081	2 8	64,077 64,080 64,083 64,082 64,081	Q = 7	64,072 64,077 64,080 64,083 64,082 64,081	וון פינית באיתון פיניתים פיניתים הייתים				Total O.1 Q.2 Q.3 Q.4 Q.5 Q.6 Q.7	6 0-1 0-2 0-3 0-4 0-5 0-6	1847mm 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00'0 00'0 00'0 00'0 00'0 00'0	m Loss (Pr) = pr(Lo + Lu) [kgt/cm2] ***	Î	Remarks :	Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the	Prepared by: A. Hamid & Azbor

#### Water Pressure Test

**(**)

Hole No.: M98-6	Location: Upstream Coffer Dam (Left Bank)	Hole Inclination (a): 90 degrees	Friction Loss per meter (ps) : 1x104 xQ1271:	County absumption of 1
2/14	76 m/m	Packer Type: Mechanical	31/January/1999	Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Commit
Stage:	Dia. of Hole:	Packer Type:	Date:	17
Hole No.: M98-6	Location: Upstream Coffer Dam (Left Bank)	Hole Inclination (2): 90 degrees	Friction Loss per meter (p.): 1×104×Q1471;	() land abundance ()

Depth of test sect

Pipe length from pressure gauge to

hole mouth: (La)

Reading of flow meter

. Pal . P.2

Casage P.

31/January/1999 Mechanical

E/E

Dia. of Hole: Packer Type: Date:

Stage:

3/14 9

Water Pressure Test

(8)

Choung fevation : EL	Croundwater level (La):   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Care   Ca
m Groundwater Tevel (LJ):  4.43 m GL. (LJ)= 10 m  3-ding of flow meter  7 10 7 4 1  12 18/23 18/20 81,430 81,512 81,562  8 13.23 81,232 81,443 81,512 81,562  9 81,232 81,332 81,443 81,512 81,562  9 81,232 81,332 81,443 81,512 81,562  9 81,232 81,332 81,443 81,512 81,562  9 81,232 81,332 81,443 81,512 81,562  9 81,232 81,332 81,443 81,512 81,562  9 81,232 81,332 81,432 81,522 81,562  9 81,234 81,435 81,435 81,532 81,573  18 12.26 81,328 81,492 81,532 81,573  18 12.26 81,412 81,493 81,543 81,573  10 000 0.00 0.00  10 000 0.00 0.00  10 000 0.00 0.	Neight (La): 0.70 m   Ground elevation : EL   m   Groundwitter level (La):   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.   Fig.
m me gauge to 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4.43 m 4	Neight (La): 0.70 m   Oround clevation: EL   m
Cround cle mouth line from the first transfer for the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the first transfer from the	Neight ([La); 0,70 m   Company of section (La)   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig. 2 m   Fig.
1-1 1:	Neight ([L.])   0.70

ဋ

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute

settles within 90 % to 110 % of the injection rate in the just previous one minute

Prepared by: A. Hamid & Azhor

Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.

Inspected by: M. Suga

Prepared by: A. Hamid & Azhor

inspected by: M. Suga

કે જ

38

şş

3 %

ت. ت. و

3835

į ટ્રેફ્ટ

į

ŧ

ដង ឯង ៦

Hole No.:	M98-6	Stage:	4/14	_
Location:	Upstream Coffer Dam (Left Bank)	Dia. of Hole:	76 m/m	_
Hole Inclination (a)	ttion (a); 90 degrees	Packer Type: Mechanical	Mechanical	
Friction Los	Friction Loss per meter (p.): 1×10° ×01911:	Date:	01/February/1999	(

			0.73 m	(1)	a e			(m/min/h					-						-	•		_			]	8 9 10	(m/u)		_	
ш/ш 92	Mechanical	01/February/1999	Gauge height (Lz):	Length of section (La)		Calculation of Lugeon value		ġ	q1= 0.1	42- 0.3		-S	_	_												3 4 5 6 7	Water Injection Ratio (q : lit/min/m)		t: (0.7) Lu'	
Dia. of Hole:	Packer Type:	Date:	Groundwarer level (L.); CL 13,40 m	Denth of rest section	m to (La) = 20 m	Calcul			E :	27 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	P4-		-9.d	2	22	50 %	, iii.	× × × × × × × × × × × × × × × × × × ×		1 31 0 A	nss	Pre	12)			0			Lugeon value :	
Bank)	90 degrees		water level (L.)	Denh	35		Pno Pn7	4	20:02	87,285 87,337	H7 295	87.239	87,304	87,309 87,350	87,314	87,318	3/2	87,328 87,360	3,4	-	1	t z		Ľ	ş	3.	10:12	0.00	;	
Upstream Coffer Dam (Left Bank)	8	Friction Loss per meter (py): 1x10° x01411;	m Ground		( <u>;</u>	Now meter	P.4 P.5	4		87,108 87,210		87.138 87.230		87,158 87,244					0/4/Je 3/4/1	<u> </u>	-	-	i	S S		3.5	14	ш	f/cm2]	
Stream Coff	; (a)	r meter (p·) :		of abuse on	Page length from pressure gauge to bole mouth: (La)= 5.48 m	Reading of flow meter	Po2 Po3	7	09:24	87,005 87,030	, k				87,070	87.076	6 64 64	8 8	1/60'/8 170'/9			-	-	┡	16 67	0.2	-	_	Friction Loss (Pr) = pr(Lo + Lo) [kgf/cm2]	
·	Hole Inclination (a):	on Loss per	Ground elevation: EL	and from our	ripe length room pro Note mouth: (L.e.)=		. Pa1	7	00:00	50,905			966.98	8.82	86,997			8 8	3. ×.	-		-		j	ч	3	01-01	00.0	n Loss (Pr) =	
Location:	Hole	Fricti	Special	1	2 4 4 5 E		Compan P.	(veryon)	Sind lyme	U(min)	1,6	ļ-	4	   	5	7	≈	ماء	2¹:	= :	ļ	1	<u>'</u> 2	ğ	Ei.	Average	Franch Lim	٤	Friction	

#### Water Pressure Test

Location:	iuo	Costre	Upstream Coffer Dam (Left Bunk)	er Dan	) (Zeft	Bunk)		Dia, of Hole:		36	ш/ш	
Hole E	Hole Inclination (a):	on (a);	•		8	90 degrees		Packer Type:	Mec	Mechanical		
Frictio	n Loss	Friction Loss per meter (pt): 1×10" ×01011:	رة تا تا	ž	Ŏ,	ای		Date:	01/Feb	01/February/1999	666	
Ground	Ground elevation: EL	ı. EL.		E	Ground	Groundwater level (L.); GL.	);( <u>[</u> ]);	SL- 13.40 m	Ö	auge hei	Gauge height (La):	0.73 m
P pc ler	gth from	Pipe length from pressure gauge to	gauge to				epth of te	Depth of test section		303	(LI) not section (LL)	<u>(j</u>
hole mo	hole mouth: (L.)	ļ	4.44 m		3		20 m	m to (La)= 2.5	E		S	ε
			Reading of flow meter	flow m	ŗ			รับ เ	Calculation of Lugeon value	Luc.	on value	
Cauge P.	4. E		3.	4 C	3.4.	ð. 4	Pu7	P=P=+0.1(sin(s)L+L-)-P= [kef/cm2].	الكولاية والمردآ		a=O=/Lu (livmio/m)	(wiw)
Start time		15:12	15:25	15.37	15.50		16.14	P1= 2	4,1			
U(min)					80,				4.0	<b>8</b> 6	უ მ •	
· r	9.77	2,72	9 7	61.5	91 924	90.0	30,00	7	11.4	3 4		
'n	91,713			93	91,932			2	8,4	9		
4	91,713			91,840	91,940			98	5.4	ģ		
	91,714			91,849				2	7. 4	6		
۰,۰	91.719	91.739	2 2	9.869	\$ \$ \$	2, 29 2, 29 3, 4	2,087	2				
· œ	91,715			91,87x				ζü				
: إم	91,716			98,18	98,18						-	
2 =	01,11	0*/. X:	<u>,                                     </u>	74077	10/41/	18065.	267	d Gi			•	
:   		!	:									
Ξ.	1			ļ i	į		-	4 6				
4 7	-	!	<u> </u>	į	į		-	113 2 64 2 64 3 64				
Total	ઢ	ç	3	ş	3	3	ે					
Ξ	. 1	χ	Ę	- 1	۶	×	32	]				
Average	Τ.	7	3	3	Ş	j	3	0	2		, ,	9
TANK IN	3	_!	\$ \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \frac{1}{2} \\ \		200	L	1		Vater Injecti	on Ratio	Water Injection Ratio (q : Sit/min/m)	æ
3	3	I.	93	000	100	L						
Frection	£	Friction Loss (Pr) = pr(Lo + Ls)  kgt/cm2	]     	t/cm2		];		Lugeon value :		0.13	Ξ.	
	•		•			:	3			8,4	kgf/cm2	
Kemarks:	يّا											
Noic:	injectio	n of wate	phods	X Contra	iog loc	at Icast 1	0 minute	insction of water should be continued for at least 10 minutes under the specified pressure, after the specition rate per minute	1 pressure, 1	fiter the	injection rate	Ser mino
	sentes.	vithin 90	% to 110	% of the	injection	on rate in	che ose	centes within 90 % to 110 % of the injection rate in the just previous one minute				

Note: Injection of water should be continued for at least 10 minutes under the specified pressure, after the injection rate per minute settles within 90 % to 110 % of the injection rate in the just previous one minute.

Prepared by: A. Hamid & Azhor

Hole No.	0						•	5						•	,	•				
Location:	ion:	Upstre	Upstream Coffer		Dam (Left Bank)	Sank)	-	Dia. of Hole:	łole:		92	m/m		<b>-</b>	Location:	•	stream C	Upstream Coffer Dam (Left Bank)	lam (Left	Bank
Hok	Hole Inclination (a):	ion (8):	•		8	90 degrees		Packer Type:	 اقر اقر	Ψů	Mechanical				Hole Inclination (a):	) noiteni	;;		8	90 degrees
Fricti	sson no	Friction Loss per meter (ps) ;	cr (9) ::	i	×10-×01-11			Date:		2/Feb	2/February/1999	g			Friction Loss per meter (pt): 1×10°×0'***	oss per	meter (p	×	,0×	¥
8	Ground elevation: EL	m: EL		E	Groundwater level (L.); GL. 13.40 m	ater leve	( <u>5</u>	13.	40 m	_	Gauge beight (La):	:(سا) بر	0.73 m	<u></u>	Ground elevation: FL	vation : E	ی	E	Ground	Groundwater level (L
ă ă	ngth from	Pipe length from pressure gauge to	Sauge to			8	pth of te	Depth of text section	18	ļ.	Length	Length of section (L.)	(m)		Pipe length from pressure gauge to	from pres	sure gaug	0 0	· · · ·	Δ
Pop	note mouth: (L.s)=		4.70 m	E	3	1	E S	# to ( <b>1.</b> ) #	ı	ε.	,	۱.	E	-1	hole mouth: ( - s)=		4	4./0 m	10	S.
		χœ	Reading of flow meter	flow m	į		7		Š	ulation	Calculation of Lugeon value	n value			Ļ	-	Reading	Reading of flow meter	meter	•
Cauge P.	Z -	P.2	3 ,	7 O	<u>5</u> ~	₹ 4	ž -	'=P⊶0.1(	P=P0+0.1(sin(a)L1+L1)-P* {kg//cm2}.	2)-Pv [kg5,	/ст2]. ф	ڻ 1.	Vmin/m[	<del></del>	Cause P. (Agf/cm.)	a. `  ⊒ ~	24 24 27	~ ₹ 5	٠ ک	₹ 4
7	1	Ľ	10:33		10:57	11:10	11:33		P1= 2.4	` <b>•</b>	5	0.1	ı			16:45	16:57 17	17:UK 17:20	17:32	17:43
Q mm)			18,477	98,487	38.502		8,511			4	Ġ,				O(min) 1			_	27,11,972	
-:	98.460	_	7,47	98,488	2 25 28 28 28 28	28,508	28,511		4 × ×	<b>.</b>	3 6			•		11,850	28871 278,11	716,11 588,11	6/6/11 5	3,3
7,5	6,5	0.00	98,478	98,4971	2 3		1 2 89				5	9 5			7,5					12.001
 , 4	98.461		\$ \$	ő	9X 504		98,511		P6= 5.4		ģ				_					
'n	98,462		98,482	õ			98,511		P7= 2.4	-	7.6	0.0								
۱۰	26.462	2 98,474	98,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14,480 14	98,497	505.50	035.0	98,512	•							0,1	11,854	11,876 11,896 11,874 11	96 11,96 10,00	200	2,5
			98.48	Ö	\$ 8		98,512	zu.	Ţ,											
E ₂	98.463		98.480	ŏ			98,512	. 00 13/]\$	о.	•			-							
	98,464	4 98,476	98,487	202,8%	98.50	98,511	98,513	gal ni r- <	_					•	9 :	11,857	206,11	11,970	2	12,008
45	!	;	!	1	İ	-	:	חופ	<b>6</b>						<u>.</u> :21	!				<u> </u>
_		<u>.</u>					· ·									· ·	-			
Z :				-	:	ļ	i	if is to c	•						2 ¥	- i	<u> </u>	<u> </u>		1
2 3	ä	ã	Ş	3	3		ò	; ;₹.\	_						Τ.,	ð	╁╌	╀	╀	Ľ
  =		٥	9	<u>~</u>	۰,		, 74										8 21	*	'n	_
ži V	Ŀ	0.2	0.3	Ş	5.0	3	<u>`</u>		0.0 0.1 (	),2 0.3 (	3.4 0.5 C	,6 0,7 0	0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0	·		7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	200	2.0	3,0	ð
11/11	200	27.47	10.47	30-44	0.1	1.20	3		ž	ater Inject	Water Injection Ratio (q : lit/min/m)	im/hit: p	(m/v	-1.5	Pinish time	1-	-	. I		17:53
3	↓.		000	0.00	1	0.00	ŝ								ш	Ц	L.J	Н	Н	0.00
ξ. Σ	a Lons (F	15,	3:	g(/cm2)		;	1	3	Lugeon value:	ne:	0.3	ដី		<u>-</u>	Priction Loss (Pr) = pr(Lu + Lr) [kgs/cm2]	75 (Pr) = 1	1+1)	(kg//cm/	22	1
					i	7	=	U	Critical Pressure:	Nure:	114	kgf/cm2		<u>-</u>						2
Remarks	_ تو														Kemarks:					
Sofe.		Insection of water should be	pluods 1	De contin	a toj pon	1 Ican 16	FIRMIC	under th	specified :	pressure,	afier the re	gection ra	continued for at least 10 minutes under the specified pressure, after the injection rate per minute		Note: In	Injection of water should be continued for at least 10 mi	water sho	uld be con	of bound for	at keast
		the production of the production of the production of the control order of the production																		

#### Water Pressure Test

0

Hole Inclination (a):   90 degrees   Packer Type:   Mechanical	Location:	⊃l	pstrea	3	Upstream Cotter Dam (Lett Bank)				Dia. of Hole:	إن		۹	EI/EI	
The control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the	Hole Inclir	intion	Ë	ľ		8	degrees		Packer 1	Ş,		fechanic	al	
## Groundwater [cvet] (L.): CL. 13.40  ## Groundwater [cvet] (L.): CL. 13.40  ## Groundwater [cvet] (L.): 30 m to (L.):  ## Groundwater [cvet] (L.): 30 m to (L.):  ## Groundwater [cvet] (L.): 30 m to (L.):  ## Groundwater [cvet] (L.): 30 m to (L.):  ## Groundwater [cvet] (L.): 30 m to (L.):  ## Groundwater [cvet] (L.): Cl.): 30 m to (L.):  ## Groundwater [cvet] (L.): Cl.): Cl.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40  ## Groundwater [cvet] (L.): Cl. 15.40	Friction L	oss pc	r mela	:: ق تا		Ş	¥		Date:		/20	Sebruary	1000	
### Character gauge to ### Character	Ground elev	ation :	٦		E	Ground	rater lev	ارکا) :				Gauge h	cight (La):	0.75
Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol	Pipe tength (	rom pr	Ssur	gauge lo				epth of to	est section	li			igth of section	س(ات) س
Reading of flow meter   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol   Pol	hole mouth:	3		4.70		01-10		30 m	(L)		E		S	E
P.o.    P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.   P.o.			Read	ing of	flow m	eter				Ü	culatic	n of Lu	eon value	
16.40   16.57   17.04   17.05   17.343   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.3444   17.		-	27.	J	3 :	Pιδ	P46	Po7		* 7 . 7	4	10		**************************************
11,850   11,871   11,845   11,912   11,972   11,998   12,008   73= 11,850   11,872   11,872   11,899   12,008   74= 11,881   11,872   11,899   12,009   74= 11,881   11,872   11,899   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009   12,009	1	J.	16:57	, 7.mx	17.20	17.32	17.43			Planta)	4.5	rgycmzj,		i mana
11,850 11,872 11,885 11,973 11,979 12,009 Pa- 11,851 11,872 11,886 11,921 11,971 11,979 12,009 Pa- 11,852 11,873 11,886 11,921 11,980 12,000 12,000 Pro- 11,852 11,874 11,886 11,930 11,981 12,000 12,010 Pro- 11,853 11,875 11,894 11,940 11,981 12,000 12,011 Pro- 11,855 11,877 11,898 11,951 11,989 12,000 12,011 Pro- 11,855 11,877 11,898 11,951 11,989 12,000 12,011 Pro- 11,855 11,877 11,992 11,990 11,990 12,010 Pro- 11,855 11,877 11,992 11,990 11,990 12,010 Pro- 11,857 11,877 11,992 11,990 11,990 12,010 Pro- 11,857 11,877 11,992 11,990 11,990 12,010 Pro- 10,877 11,877 11,879 11,990 11,990 12,010 Pro- 10,877 11,877 11,879 11,990 11,990 12,010 Pro- 10,877 11,877 11,879 11,990 11,990 12,010 Pro- 10,877 11,877 11,870 11,990 11,990 12,010 Pro- 10,87	+-		187	11,833			11.9%	1		2	4	rer		
11,851 11,873 11,886 11,923 11,978 12,000 12,000 P5+8 11,852 11,874 11,888 11,925 11,978 12,000 12,010 P5+18 11,873 11,874 11,888 11,925 11,920 12,010 P5+18 11,873 11,874 11,982 11,980 12,010 12,010 P5+18 11,873 11,874 11,982 11,980 12,000 12,010 P7+18 11,875 11,876 11,989 11,981 12,013 12,013 11,875 11,876 11,978 11,978 11,979 12,000 12,013 11,875 11,875 11,974 11,975 12,000 12,013 11,875 11,875 11,874 11,970 11,977 12,000 12,013 11,875 11,875 11,874 11,970 11,977 12,000 12,013 18 2 1			2,8	11,845						Ş	4.0			
11,852 11,874 11,888 11,929 11,980 12,000 12,000 13,851 11,874 11,882 11,935 11,935 11,935 12,000 12,010 11,835 11,874 11,892 11,935 11,935 12,000 12,010 11,835 11,874 11,892 11,935 11,936 11,936 11,936 12,000 12,011 11,835 11,877 11,896 11,935 12,000 12,011 11,835 11,877 11,904 11,937 12,000 12,012 11,835 11,877 11,904 11,937 12,000 12,012 11,835 11,875 11,904 11,907 12,937 12,000 12,012 11,835 11,875 11,904 11,907 12,937 12,000 12,012 11,835 11,835 11,804 11,907 12,937 12,003 12,013 18 2			1,373	11,886			•	-		P4=	11,4	•		
11,855 11,874 11,892 11,935 11,982 12,000 12,010 P78 11,855 11,875 11,892 11,990 11,985 12,000 12,010 P78 11,855 11,875 11,896 11,990 11,985 12,010 12,011 11,855 11,877 11,896 11,991 11,990 12,010 11,855 11,877 11,899 11,991 11,992 12,001 12,011 11,855 11,877 11,992 11,994 11,992 12,001 12,012 11,894 11,992 12,007 12,012 11,894 11,992 12,007 12,012 11,894 11,992 12,007 12,012 11,894 11,994 11,994 11,994 12,001 12,012 12,013 11,894 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 11,994 1	-		1,874	11,888		-	-	•		8	8.4	•		
11,853 11,875 11,894 11,940 11,918 12,004 12,010 11,855 11,876 11,894 11,940 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11,951 11	. 4		1.874	11,892						P6.	4.	•		
11,854 11,876 11,996 11,944 11,987 12,005 12,011 11,855 11,477 11,989 11,953 11,1999 12,006 12,011 11,855 11,477 11,989 11,953 11,999 12,006 12,011 11,855 11,877 11,994 11,995 12,007 12,012 11,855 11,879 11,994 11,997 12,008 12,013 11,994 11,997 12,008 12,013 11,877 11,879 11,994 11,997 12,008 12,013 12,013 11,879 11,879 11,994 11,970 11,997 12,008 12,013 12,013 11,879 11,879 11,994 11,970 11,997 12,008 12,013 12,013 11,879 11,879 11,994 11,979 12,008 12,013 12,013 11,879 11,879 11,894 11,970 11,897 12,008 12,013 11,879 11,879 11,894 12,913 11,819 12,013 11,819 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 11,919 1	5		1,875	11,894			2004			ŗ,	4			
11,855 11,877 11,898 11,951 11,989 12,000 12,011 11,855 11,877 11,898 11,951 12,000 12,012 11,851 11,875 11,875 11,954 11,957 12,000 12,012 12,012 11,855 11,875 11,904 11,997 12,007 12,012 12,012 11,855 11,875 11,904 11,997 12,003 12,013 14,77 11,875 11,904 11,997 12,003 12,013 14,77 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,013 14,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,997 12,9	_		1,876	11,896				т.						
11,855 11,878 11,899 11,958 11,992 12,006 12,012 11,878 11,878 11,992 11,992 12,006 12,012 11,879 11,992 11,992 12,007 12,012 11,879 11,992 11,992 12,007 12,012 12,013 12,013 12,013 11,879 11,992 11,992 12,007 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12,013 12	_		1,17	11,898	_	-		-	-				ľ	
11,850 11,879 11,902 11,930 11,930 12,000 12,001 12,000 12,001 12,000 11,879 11,879 11,970 11,970 11,970 12,000 12,001 12,000 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12,001 12	:		1,878	83					ęw3			10	(	
11,857   11,954   11,957   11,957   12,010   12,011   15,01   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15,011   15	_		<b>.</b>	2					J8					
Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out			7,8/2 5/-	<u> </u>			30,21	·	ų ¢!		\;			
Co.1 Co.2 Co.3 Co.4 Co.5 Co.6 Co.7 With 3 Co.1 Co.1 Co.2 Co.3 Co.4 Co.5 Co.6 Co.7 With 3 Co.5 Co.6 Co.7 With 3 Co.1 Co.1 Co.2 Co.3 Co.4 Co.5 Co.6 Co.7 With 3 Co.5 Co.3 Co.4 Co.5 Co.6 Co.7 With 3 Co.5 Co.7 Co.7 Co.7 Co.7 Co.8 Co.7 Co.7 Co.7 Co.7 Co.7 Co.7 Co.7 Co.7	1 :	-	ŀ	1			: 		10		ę.			
Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out		· ;	!	-	İ			ĺ	1155		<u>.</u>			
Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out   Out			:	ļ	i	-			e l		•			
Out   Out   Out   Out   Out   Out   Out     7			;	İ	:		-	!	[ J >]	·	•			
7 8 21 58 25 10 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	╁	ŀ	3	3	Ş	3	Š	ે	18,4					
O ₀₋₁   O ₀₋₂   O ₀₋₃   O ₀₋₄   O ₀₋₆   O ₀₋₆   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O ₀₋₇   O	<u>.</u>		æ	7	×.	'n	2	. 5	`	Ĭ				
0.7   0.8   2.1   5.8   2.5   1   0.5	F.,	┞	3	0	Ι.	3	ð	2-0		0.0	0.2 0.	3 0.4 0.5	0.6 0.7	1,8 0.9 1,
10,55   17,07   17,18   17,30   17,42   17,53   18,04	-1	-	80	7.1		2.5	-				Water for	and deliver	(a) (b) (b)	\w/o;
0.00   0.00   0.01   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.			17:07	17·1×		17:42	17:53	1			א שוללו זוו	2		(m/m)
oss (Ps) = ps (Lu + Lu) (kgf/cm2) Lugeon value: 0.8  Lugeon value: 0.8  Lugeon value: 0.8	Н	Н	0.00	0.00	10'0	0.00	000	000						
u o Gritical Pressure: >11	Priction Los	(P.)	3	₹ ₹	gf/cm2]		1	ì	3	L uoali	alue:	0.8	ន	
Kemarks:	•						2		Ü	Sition! P	ressure:	7	kgf/cm2	
	Kemarks ;													