The Study on Urban Drainage and Sesserage System for HCMC JICA -- PCHCM Supporting Report : Appendix C

8. Hydrodynamic Modeling of Drainage Pipe System

The existing drainage pipe system in Ho Chi Minh City is large and complex networks. Furthermore the outlets of the drainage pipe system are affected by the tidal time varying water levels.

Thus, for consideration of the drainage pipe network and the hydraulic condition at the outlet, MOUSE, developed by Danish Hydraulic Institute (DHI), can be applied to modeling

(1) Modeling for the Drainage Areas in the Study Area

At the Master Plan stage, there are 3 main purposes for the modeling activity.

- 1) Construct the main drainage pipe network database
- 2) Assess the flow capacity of the main drainage pipes
- 3) Calibration against records of inundated areas during the 1994 flood

Consequently, the modeling shall be concentrated on the main drainage pipes having an equivalent or a larger area of cross-section than that of ϕ 600 mm pipe.

a) Boundary Conditions

Dry-weather flow

Unit wastewater discharge, which is 170 l/day/person for urban district and 140 l/day/person for rural district, is applied to the boundary condition for the calibration.

Rainfall

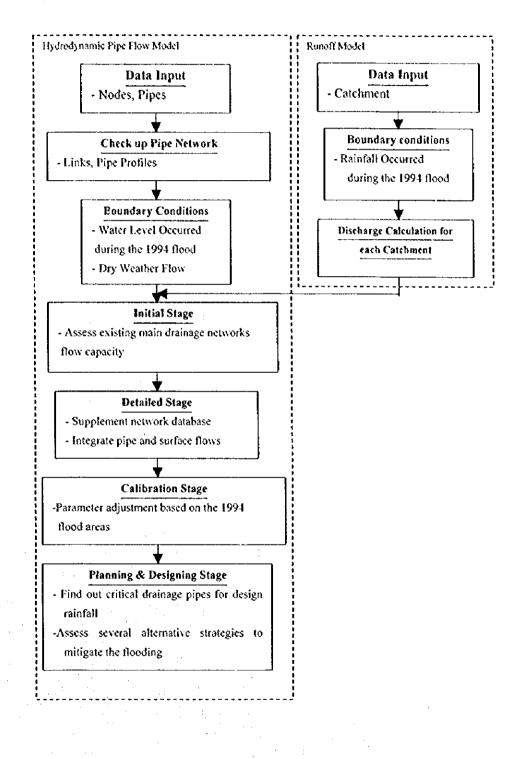
The rainfall time series occurred on June 28^{th} , 1994 will be applied to the boundary condition for the calibration. The rainfall started at 7:00 on June 28, 1994 and continued for 24 hours.

Water Level at the Outlets

The water level at the Phu An station, corresponding to the rainfall time series, is applied to the boundary condition of the water level at the outlet into the Saigon River, the Tau Hu-Ben Nghe, the Doi-Te and the Nhieu Loc-Thi Nghe canals.

b) Procedure for Modeling

A general idea of modeling procedure is shown as the flow chart below.



Supporting Report : Appendix C

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Essentially, MOUSE consists of 2 components as shown:

* MOUSE Runoff Model :	Compute surface runoff for each catchment. The Catchment is linked to the specified network node (i.e. manhole) of the Pipe Flow Model.
* MOUSE Hydrodynamic Pipe Flow Model :	Compute the drainage network flows based on the runoff discharge calculated by the Runoff Model.

a) General Description of Modeling

Surface Runoff Model

The model computes the runoff discharge for each catchment. The resulting runoff from the catchment is computed on the basis of the specified time of concentration and the runoff coefficients.

Hydrodynamic Pipe Flow Model

The model is a computational tool for simulations of unsteady flows in pipe networks with alternating free surface and pressurized flow conditions. The computation is based on an implicit, finite difference numerical solution of basic 1-D, free surface flow equations (Saint Venant). The implemented algorithm provides efficient and accurate solutions in multiply connected, branched and looped pipe networks.

The computational scheme is applicable to vertically homogeneous flow conditions which occur in low-lying pipes, often pressurized main pipes, affected by the varying water level at the outlet.

Both subcritical and supercritical flows are treated by means of the numerical scheme which adopts according to the local flow conditions. Naturally, flow features such as backwater effects and surcharges are precisely simulated.

Moreover, a advanced technique using this model can simulate the street flooding when the overflow from the node surmounts the inflow capacity of the node.

b) Required Data for Modeling

Required data for modeling are shown in the table below.

Runoff Model	Hydrodynamic	Pipe Flow Model
Catchment	Node (i.e. manhole)	Pipe
Area	- Boltom Elevation	- Linkage
		(upstream node and
		downstream node)
- Concentration Time	- Shape	- Cross-section
- Runoff Coefficient	- Dimension	- Upstream and
		Downstream Invert
		Elevation
	- Ground Elevation	- Manning Number

c) Boundary Conditions for Modeling

These models support the following time-variable boundary conditions for simulation:

Runoff Model	Hydrodynamic Pipe Flow Model
- A Rain Hydrograph	- Dry Weather Flow (wastewater from household)
	- Water Levels in the Outlets
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9. CALCULATION ON STORAGE REQUIREMENT

Flood Plain Storage along Daihan Canal

Improvement plan of Daihan canal has been proposed such that the proposed canal sections can drain 5-year rain water in 24 hours. In such a case, inundation is expected to occur along the flood plain of Daihan canal. An analysis has been carried out on flood plain storage along Daihan canal for 5-year return period and is presented in Fig. C.9.1. Flood plain storage volume, V_s (m³) along any reach is calculated as:

$$V_s = (V_i + V_f) - V_c$$

where:

 V_i = Inflow volume (m³) from main channel of upper reach; V_f = Lateral inflow volume (m³) from contributing sub-catchment along the reach in consideration and

C -19

 $V_o = Outflow$ volume (m³) from main channel of the reach in consideration.

Average specific storage volume and area (considering a 30 cm inundation depth) are calculated to be 29,800 m^3/km^2 and 99,300 m^2/km^2 respectively.

Specific Storage Volume due to Urbanization

According to future (2020) landuse plan prepared by Urban Planning Institute of Ho Chi Minh City, rapid urbanization is expected in the North Eastern zone. To keep future runoff (under future landuse condition) same as present runoff (under existing land use condition), storage pond (non-structural measure through landuse regulation) is proposed for the rapidly urbanizing catchments. Required specific storage volume due to increase in urbanization has been estimated. Overland flow runoff hydrographs for 5 and 10 year return periods have been constructed for five landuse conditions for a unit catchment area of 1.0 km² and are presented in Fig. C.9.2. Required specific storage volume ($m^3/s/km^2$) as a function of increase in runoff coefficient for four categories of urbanizations, with reference to agricultural land, have been calculated and the results are plotted as shown in Fig. C.9.3. For ease in application, two equations have been proposed for 5 and 10 year return periods :

$V = 76852 \text{ x } (\Delta \text{C})^{0.76112}$ V = 85679 x (\Delta \text{C})^{0.76201}	5-year return period
$V = 85679 \text{ x} (\Delta C)^{0.76201}$	10-year return period

where:

V = required specific storage volume (m³/s/km²) and AC = increase in runoff coefficient by urbanization.

10. STRENGTHENING MONITORING NETWORK ON METEO-HYDROLOGY

Proposed Rainfall Stations

In the Study area, there exists only one automatic type rainfall station at Tan Son Nhat where short duration rainfall data is available. There exist six more rainfall stations in and around the Study area which are of manual type and where, only daily rainfall data are available. This posed a great difficulty in performing a detailed analysis on rainfall distribution over the Study area that could support in carrying out a better runoff analysis and developing a better hydrodynamic model. To have a more uniform distribution with smaller representative areas, five new automatic type rainfall stations are proposed to be installed within the Study area. It is also proposed that the existing six rainfall stations shall be updated from manual to automatic type. Locations of the proposed rainfall stations are shown in Fig. C.10.1. It can be seen that areas of Thiessen polygons with the proposed rainfall stations are much smaller and more uniformly distributed than those with the existing rainfall stations.

Proposed Water Level Stations

There exists no water level station along any of the canals in the Study area. This posed a great difficulty in carrying out a detailed analysis on discharge and water level along the canals as well setting up boundary conditions and calibration for hydrodynamic model development. To overcome this difficulty, nine new automatic type water level stations are proposed to be installed along the canals that best represents the hydrologic system. Among them, six water level stations are proposed in the Western canal system and three water level stations are proposed in the Eastern canal system. Locations of the proposed water level stations are shown in Fig. C.10.2.

NFALL STATIONS
Table C.1.1 INVENTORY ON RAINFALL STATIONS
Table C.1.1

							Turne of Data
2		Station	Date of	Elevation	Geographic Co-ordinates	Method of Measurement	man to white
2	Same N	Location	Establishment	(EL. m)	Latitude Longitude	Automatic Manual	Short Duration Daily
				_			;
	Tan Son Nhat (Tan Son Hoa)	Dist. Tan Binh	5161	\$	10°48' 106°41'	X	~
6	Hor Mon	Dist. Hoc Mon	1973	10	10°53' 106°36'	×	×
• •		Die Binh Chank	1977		10°45' 106°34'	×	*
n	רכ אומום צרמו					>	×
4	Binh Chanh	Dist. Binh Chanh	1977		10.40 100.34	c	
~	5 Nha Be	Dist. Nha Be	1977	-	10"40' 106"44"	×	×
, 		-					-
Ģ	6 Ha Tien Cement	Dist. 9	1963		10*50' 106*41'	×	×
,	Factory					-	
٢	I and San	Dist. Thuan An	0861		10*53 106*49'	× .	X
	100 8007						

Table C.1.2 INVENTORY ON WATER LEVEL STATIONS

<u>ö</u>	Station		Location	Date of	Geographic	Geographic Co-ordinates	Method of Measurement	leasurement
	Матс	River Name	Chainage (km)	Establishment	Latitude	Latitude : Longitude	Automatic	Manual
	Thu Dau Mot	Saigon	107.78 km from East Sea Mouth or 40.41 km from Phu An station	9961	10°58	.66.301		×
	Phu An	Saigon	67.36 km from East Sea Mouth or 27.22 km from Nha Be station	21 61	10°47'	106°43'	×	
r.	Nha Bv	Nha Be	40.14 km from East Sca Mouth	1977	10°40'	106°46'	×	
4	Bicn Hoa	Dong Nai	88.57 km from East Sca Mouth or 48.44 km from Nha Be station	1960	10°56'	106°49'	*	
\$	5 Ben Luc	East Vam Co (Vam Co Dong)	67.42 km from East Sca Mouth or 42.64 km from Phu An station	606 t	10*38	106*29		×

Implementation agency of all stations : Southern Region Hydro Meteorological Center, Ho Chi Minh City

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BAR CHART OF COLLECTED DATA ON RAINFALL Table C.1.3

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Date Source - Ho Chi Minh City Statistical Office

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Table C.1.4 BAR CHART OF COLLECTED DATA ON WATER LEVEL

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Data Source - Southern Region Hydro Meteorological Center, Ho Chi Minh City

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1	Amount Date	Amount	Date	Amount	Date	Amount :	Date	Amount	Date	Amount	Date	Amount	Date
1973		7 30.0	0/11 0										
1974	75.6 27/09	20.0	0. 20/05										
1975			•	-		••••				95.2	21/10		
1976	81.0 29/10	· 	•	• •		• · · ·		 -		116.3	16/08		
1977		99.6	ز 13/09	83.2	17/07	109.8	29/08	89.4	11/20	95.5	27/06		
1978	·	••		130.4	01/90	144.3	15/09	90.5	11/04	158.5	01/60	170.0	01/60
6261	Ē		, 	126.2	16/06	68.2	14/09	58.2	27/04	129.2	01/50	81.0	29/08
1980		\$ 85.5		88.0	18/05	75.0	01/08	83.5	19/05	120.5	15/05	175.0	15/05
1981				101.1	27/07	58.3	26/07	87.7	12/07	154.5	29/06	103.5	04/09
982				82.7	07/04	52.4	04/04	46.5	14/06	168.1	60/80	114.0	21/05
1983				101.5	11/08	122.0	20/09	63.9	30/09	70.3	24/06	116.1	10/08
1984	÷	20.6	08/10	82.0	12/07	66.3	12/10	71.4	26/07	96.0	60/90	84.0	16/10
1985				61.7	25/07	•	•	66.1	01/05	101.0	10/10	94.0	08/00
1986				84.0	24/06	100.5	17/06	90.1	11/05	100.6	13/09	146.0	18/05
1987	÷	:		97.2	02/11	• •	•	58.8	12/06	115.8	03/10	60.0	01/20
988				87.6	25/11	-		`•	•	108.0	03/10	70.0	11/50
980			24/04	117.1	16/10	105.9	25/05	• •	٩	100.1	18/08	120.0	01/80
0661		· .	: -	99.3	08/11	74.6	17/08	•	•	46.8	20/07	115.0	04/10
1661				83.2	06/06	84.8	26/05	- •	•	49.5	17/05	70.4	27/07
1992			• .	92.9	21/06	96.7	23/05	129.3	21/08	98.8	18/07	68.0	21/08
1993	: .		.	83.5	26/10	169.9	06/06	93.3	16/10	79.1	03/09	82.0	02/09
1994			04/09	62.3	18/10	184,5	28/06	1961	28/06	124.6	28/06	159.0	28/06
1995				92.3	01/11	58.3	30/06	79.9	26/08	98.4	29/09	105.5	26/08
9661		• .		94.0	14/10	62.3	14/10	79.3	26/09	67.4	21/05	104.5	20/08
1997			3 21/07	72.0	02/11	73.5	28/10	66.5	04/11	50.0	16/09	0.111	20/08
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Table C.3.1 ANNUAL MAXIMUM DAILY RAINFALLS

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Data Source : Southern Region Hydro Mcteorological Center, Ho Chi Minh City Daily : From 7:00 P.M. to 7:00 P.M.

Table C.3.2 ANNUAL MAXIMUM RAINFALLS AT TAN SON NHAT

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	(min.)	(min)	(min.)	(min.)	(min)	(mia)	Amount	Date	(hrs.)	(hrs.)	(hrs)	(hrs.)	Amount	Date
1952	26.5	27.6	29.8	31.0	31.4	32.8	44.2	06/10	51.4	70.4	76.3	113.4	113.4	20/10
1953	20.0	31.0	42 2	45.8	52.7	56.3	58.8						106 5	28/05
1954	30.6	42.4	62.6	82.0	93.7	94.5	95.3	-	l I	-			110.6	26/09
1955	26.0	38.0	36.8	45.2	50.2	55.6	60.8	06/11	72.1	· ·			87.8	06/11
1956	25.2	37.0	45.0	45.4	45.6	45.7	45.8	15/11		1			70 2	06/09
1957	28.0	36.0	48.0	53.8	57.4	64.4	68.6	22/09]				71.6	22/09
1958	23.2	50.3	50.8	50.8	51.8	51.8	52.4						52.4	30/06
1959	40.3	\$0.0	60.0	70.0	79.0	79.0	79.0	30/06					87.0	16/08
1960	27.6	36.6	37.6	37.9	38 2	383	38.5	01/04					93.0	20/06
1961	28.0	40.6	50.6	51.0	53.8	55.0	55.0	06/07	68 5				72.0	25/07
1952	22 1	31.8	48.2	53.4	68.0	71.6	74.3	12/09	86.8	116.1			154.6	30/05
1963	25.7	410	48.0	55.5	59.4	68 2	73.0	19/06					86.9	19.06
1964	37.5	59.0	83.7	89.3	90.8	92.8	92.8	13/06					101.5	13.06
1965	34.0	49.0	61.6	68.1	75.0	76.5	78.3	30/04					825	27/06
1966	28.7	47.5	73.0	85.0	95.0	112.8	116.2	17/08		• • •		. 	116.7	17/08
1967	35.0	520	12.5	80.0	89.3	90.0	91.5	03/05	100.6				107.5	03/05
1968	25.0	38.7	50.0	57.5	61.0	62.0	63.0	27/04	74.6	93,4			1129	17/09
1969	30.7	514	62.1	770	803	80.3	80.3	26/10	1.111		• • •		81.5	26/10
1970	41.2	50 7	70.5	72.5	72.7	73.0	73.0	30/06	81.2	• • • • • • •		· -	87.5	17/06
1971	30.0	52.0	74.0	78.7	86.0	87.5	83.0	31/05		• · · ·			91.8	31/05
1972	29.0	40.0	52.0	55.0	58.0	58.5	59.5	12/05	73.0	77.8			77.8	25/06
1973	45.0	74.0	81.0	81.8	82.0	82.0	82.0	01/10			1 · · ·		89.6	11/07
1974	30.0	36.5	58.0	66.0	72.0	72.5	73.0	27/09			ł		75.6	27/09
1975	25.8	32.1	41.0	54.5	66.0	71.3	80.5	20/10	1.1	-	· · ·		83.4	20/10
1976	36.5	49.5	67.0	75.0	79.0	79.9	80,9	29/10			1.1		83.4	29/10
1977	310	38.6	610	61.0	65.6	65.6	67.8	13/09		· · · ·	· •		86.6	07/10
1978	31 2	43.8	67.9	75.2	106.7	137.4	144.5	09/10	• - • - •	• • •			176.9	10/10
1979	34.0	51.5	85.0	92.0	92.0	93.0	93.2	04/05					93.6	02/05
1980	23.4	46.7	61.2	78.6	81.7	86.7	92.0	18/05	95.4				94.5	18/05
1981	34.2	712	761	1.114.3	116.1	116.1	116.9	09/07	- 2007 I				99.8	29.06
1982	32.3	57.0	62.2	62.8	64.9	65.1	66.9	19/10			· ·		110.8	03/09
1983	27.2	47.7	96.3	98.9	117.0	118.6	127.3	10/08			· ·		130.7	10/08
1984	28.8	36.4	41.5	51.7	56.6	62.0	61.2	25/07				1.1	65.7	25/07
1985	29.4	42.0	50.5	55.7	60.4	64.4	727	09/10				1	mi	10/10
1985	34.2	41.7	46.5	46.5	47.5	51.1	51.6	24/09	'	1	1	1.1.1	92.5	23/06
1987	44.6	68.0	83.1	83.7	88.6	- 91.9	93.5	11/06	913		1.14		94.9	11/06
1987	28.8	40.3	45.1	45.1	48.8	49.5	49.5	02/10					63.6	07/11
1988	19.4	36.0	48.0	43.0	61.0	61.3	73.2	12/10	1		1 ·	ł	89.5	12/10
1939	50.0	69.5	76.6	78.1	78.2	78.2	84.2	03/09	97.4	• •	1	1 ·	84.3	29/09
	37.8	60.9	68.3	68.3	109.8	112.6	112.7	09/10	<u> </u>	· · •·		· ·	13.1	09/10
1991 1992	28.7	58.1	65.7	67.7	13.7	75.9	81.7	21/08	98.1	98.7		1	99.9	21/08
1992	35.4	527	59.8	61.5	65.4	65.9	69.0	03/08			1		89.5	03/08
		845	94.1		106.4	106.7	103.8	23/08	116.3	154.1	188.8	205		28/06
1994	37.6		73.5	75.0	76.0	86.5	88 2	06/08	110.3	124.	100.0	200	953	04/08
1995	37.6	65.6	705	70.5	72.0	72 5	88 2	21/05	93.7			· ·	91.6	21/05
1996	25.6	475		86.0	98.3	99.5	111,0	04/07	1			1 · ·	94.6	30/10
1997	29.5	57.4	77.5	80.0					<u> </u>	<u> </u>				
Maximun	n 50.0	84.5	96.3	114.3	117.0	137.4	144.5	9/10/78	116 3	154.1	188.8	3 205	3 176.9	10/10/78

Short and long duration rainfall : Amount represents annual maximum rainfall for a single rainfall event. Daily rainfall : Amount represents annual maximum rainfall for compound rainfall (single or multiple rainfall events on same day).

Data Source : Southern Region Hydro Meteorological Center, Ho Chi Minh City Daily : From 7.00 P.M. to 7.00 P.M.

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PROBABLE MAXIMUM RAINFALL DEPTHS AT TAN SON NHAT

Table C.3.3

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Time				Prot	bable Rainf	Probable Rainfall Depths for Different Return Periods	or Differen	t Return Pe	riods	· · ·		
(minutes)	1-Yr.	1.5-Yr.	2-Yr.	3-Yr.	5-Yr.	10-Yr.	20-Yr.	25-Yr.	30-Yr.	50-Yr.	70-Yr.	100-Yr.
15	18.82	27.70	30.06	32.80	35.86	39.70	43.39	44.56	45.51	48.16	49.90	51.74
30	24.91	41.74	46.21	51.42	57.21	64.50	71.49	73.71	75.51	80.53	83.83	12.73
45	31.94	53.15	58.78	65.34	72.64	81.82	90.63	93.42	95.69	102.03	106.18	110.57
60	33.39	57.72	64.18	17.17	80.09	90.62	100.73	103.93	106.54	113.81	118.57	123.61
06	34.92	62.64	70.00	78.57	88.12	100.12	111.63	115.28	118.25	126.53	131.96	137.70
120	35.65	64.74	72.72	82.00	92.34	105.33	117.79	121.75	124.96	133.92	139.80	146.01
180	37.12	67.75	75.88	85.36	95.91	109.17	121.88	125.92	129.20	138.34	144.34	150.68
360	47.26	77.89	83.72	90.50	98.06	111.42	124.22	128.29	131.60	140.81	146.85	153.24
daily	51.09	83.58	92.22	102.27	113.47	127.54	141.03	145.31	148.80	158.50	164.86	171.59

Note: Calculated by applying Gumbel's distribution method using collected data from 1952 to 1997.

Data Source : Southern Region Hydro Meteorological Center, Ho Chi Minh City.

 Table C.4.1
 PROBABLE MAXIMUM WATER LEVELS BY STATION

Unit. EL. m (Mui Nai)

Unit: EL. m (Mui Nai)

Poit FL m (Mui Nai)

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Station				Probable	Maximum	Water Level	for Differe	nt Return P	eriods			
) 0-Yr.	15-Yr.	2-Yr.	3-Yr.	5-Yr.	10-Yr.	20-Yr.	25-Yr.	30-Yr.	50-Yr.	70-Ye.	100-Yr.
23 D. M.	1 23	127	1.28	1 29	1.31	132	1.34	1.35	135	1 36	1.37	1.38
The Dae Met			(1 20)		(1 23)	(1 25)	(127)		1			(1 30)
	1 32	1.40	1.42	1.45	1.48	1.51	1.54	1.56	1.56	1.59	1 60	1.62
Phy An			(1.35)		(1.41)	(1.44)	(1.47)					(1.57)
			<1.35>	····	<1.41>	<1.44>	<1.16>			<1.49>		<1.52>
	1 40	1.47	1.48	1 50	1.53	1 56	1.58	1.59	1 60	162	1 63	1.65
Nha Be			(1.32)		(1.41)	(1.46)	(151)					(1 60)
Bien Hoa	1 30	1 55	1.62	1.69	1.78	1.89	1.92	2 0 2	2 0 5	2.12	2.17	2 22
Benluc	1.08	1 22	1.26	1 30	1.34	1.40	1.46	1.48	1.49	1.53	1.56	1.59

Table C.4.2 PROBABLE MINIMUM WATER LEVELS BY STATION

Station				Probable	Minimum V	Vater Level	for Differen	nt Return P	eriods			
	1.0-Yr.	15-Yr.	2-Yr.	3-Yr.	5-Yr.	10-Yr	20-Yr.	25-Yr.	30-Yr.	50-Yr.	70-Yr.	100-Yr.
	-1.76	-1.97	-2.05	-2 12	-2 20	-2 29	-239	-2.42	-2.44	-2 51	-2 56	-2.60
Tha Dau Mot			(-2 18)		(-1.99)	(-1.87)	(-1.76)					(-1.53)
	-1 80	-2.03	-209	-2.15	-2.23	-2.33	-2.42	-2.45	-2.48	-2 54	-2 59	-2.63
Phu An	· · · · · · · ·		(-2.23)		(-2.04)	(-1.92)	(-1.80)					(-1.55)
	· — · · · ·		<-2.16>		<-2.27>	<-233>	<-2 37>		1	<-2.43>		<-2.45>
13 B.	-1.98	-2.17	-2.22	-2 28	-2 35	-2.43	-2.51	-2.54	-2 56	-2.61	-2.65	-2 69
Nha Be			(-2.42)	· · •	(229)	(-2.15)	(-2.06)			(1.87)		
Bien Hoa	-1 35	-1 55	-1.61	-1.67	-3.74	-1 83	-1.92	-1.94	•1.96	-2.02	2.06	-2.11
Ben Luc	-1.47	-1.56	1 58	-1.61	-1.64	-1.67	-1.71	1.72	-1.73	-1.75	-1.77	-1.79

1.48 : Calculated by the Study Team applying Gumbel's distribution method using collected data from 1960 to 1997, depending upon station. Data Source : Southern Region Hydro Meteorological Center, Ho Chi Minh City.

(1.41): The Hydrological Sub-Institute HCMC, 1990; Using Gumbel's method.

<1.41> : Asian Development Bank, 1998; Data ranges from 1960 - 1991.

Table C.4.3 REFERENCE WATER LEVELS BY STATION

Station			Reference Wa	iter Levels		
	Recoreded Historical	High Water Level	Design Flood Level	Mean Water Level	Low Water Level	Recorded Historical
	Righest WL	(HWL)	(DFL)	(MWL)	(LWL)	Lowest WL
Tho Dau Mot	1 38	1 29	1 22	0.32	-2.08	-2 34
Phu An	1.54	1.43	1.31	0 24	-2.11	-2.4 i
Nha Be	1.67	1.49	1.36	0.17	-2 25	-2 57
Bien Hoa	2.02	1.65	1 50	0,66	-163	-1 87
Ben Luc	1.54	1 27	1.12	0.32	-1 59	-1.70

Nore : Calculated by the Study Team using collected data from 1960 to 1997, depending upon station MWL : Data for Phua An ranges from 1993 to 1997 (hourly data) and for other stations, estimated from correlations of mean water levels. Data Source : Southern Region Bydro Meteorological Center, Ho Chi Minh City.

Criteria for Reference Water Levels

Highest WL HWL = High Water Level DFL = Design Flood Level MWL = Mean Water Level LWL = Low Water Level Lowest WL : Recorded historical maximum water level : Average of annual maximum water levels : Average of monthly maximum water levels for the months August to November : Average of daily mean water levels : Average of annual minimum water levels : Recorded historical minimum water level

Table C.4.4

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PROBABLE MAXIMUM WATER LEVELS BY REACH

Unit. EL. m (Mui Nai)

Reach				Probable	Maximum	Water Level	l for Differe	nt Return P	eriods			
• • • • • • • • • • • • • • • • • • •	1.0-Yr.	1.5-Yr.	2-Yr.	3-Yr.	5-Yr.	10-Yr.	20-Yr.	25-Yr.	30-Yr.	50-Yr.	70 -Y 1.	100-Yr.
Reach 1	1.33	1.42	1.44	1.47	1.50	1.53	1.57	1.58	1.59	1.62	1.63	1.65
Reach 2	1.38	1.48	1.51	1.55	1.58	1.63	1.67	1.69	1.70	1.73	1.75	1.27
Reach 3	1.32	1.53	1.58	1.65	1.72	1.81	1.89	1.92	1.94	2.00	2.01	2 09
Reach 4	1.33	1.42	1.41	1.47	1.50	1.53	1.57	1.58	1.59	1.62	1.63	1.65
Southern Boundaries	1.38	1.48	1.51	1.55	1.58	1.63	1.67	1.69	1.70	1.73	1.75	1.77

 Table C.4.5
 PROBABLE MINIMUM WATER LEVELS BY REACH

Unit:	EL.	m (Mui	Nai)
- CHUC		*****		

Reach				Probable	Mioimum V	vater Level	for Differen	nt Return P	eriods		_	
	1.0-Yr.	1.5-Yr	2-Yr	3-Yr.	5-Yr.	10-Yr.	20~¥7.	25-Yr.	30-Yr.	50-Yr.	70-¥r.	100-Yr.
Reach 1	-1.80	-2.02	-2.08	-2.15	-2 23	-2.32	-2.42	-2.45	-2.47	-2.54	2 58	-2.63
Reach 2	-1.94	-2.14	-2.19	-2 26	-2 32	-2.41	-2.49	-2.52	-2.54	-2.60	-2.64	-2.63
Reach 3	-1.85	-2.06	-2.12	-2.19	-2 26	-2.35	-2.44	-2.47	-2.50	-2 56	-2.60	-2.65
Reach 4	-1.80	-2.02	-2.08	-2.15	-2 23	-2.32	-2.42	-2.45	-2.47	-2.54	-2.58	-2.63
Southern Boundaries	-1.94	-2.14	-2.19	-2.26	-2 32	-2.41	-2.49	-2.52	-2.54	-2.60	-2.64	-2 68

Table C.4.6 REFERENCE WATER LEVELS BY REACH

Unit: EL. m (Mui Nai)

Reach			Reference Wa	ter Levels		
	Recoreded Historical Highest WL	High Water Level (HWL)	Design Flood Level (DFL)	Mean Water Level (MWL)	Low Water Level (LWL)	Recorded Historical Lowest WL
Reach I	1.56	1,45	1.32	0.23	-2,11	-2,40
Reach 2	1.75	1.52	1.39	0.27	-2.12	-2.42
Reach 3	1.94	1.61	1.47	0.54	-1.78	-2.04
Reach 4	1.56	1.45	1.32	0.23	-2.11	-2.40
Southern Boundaries	1.75	1.52	1.39	0.27	-2.12	-2.42

Reach 1: From confluence point of Rach Ba Hong with Song Saigon to

confluence point of Kinh Te with Song Saigon (33.97 km).

Reach 2: From confluence point of KinhTe with Song Saigon to

confluence point of Song Muong Chuoi with Song Nha Be (27.83 km).

Reach 3 : From confluence point of Song Saigon with Song Nha Be to

(northern) confluence point of Song Tac with Song Dong Nai (26.33 km).

Reach 4 : From confluence point of Kinh Te (and Kinh Ben Nghe) with Song Saigon to

confluence point of Rach Ba Goc with Song Ben Luc (15.00 km).

Southern Boundaries : The southern boundaries of Rach Can Giuoc, Rach Ba Lao etc. flowing towards the south.

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Zone

	Zone		chment		archment
Ð	Area (km2)	iD -	Area (km2)	ID I	Area (km2)
				NIL	333
	. 1	NI	1987	N12	6.60
			17 87	8.13	4 2 5
				814	5 6 9
	ľ			N21	11 67
	. 1			N 2 2	643
				N 2 3	11 24
				N24	\$ 32
				N 2 5	10.98
N	13618		:	1	11 19
	:		207 57	N 2 6	
		N 2	20131	N 27	7,43
				N 28	13.93
			:	N 2 9	6 32
			1	N 2 10	5 \$1
			1	8211	5.71
				N 2 1 2	4.89
			ł	N213	6 8 9
	1	Na	8 7 5	Na	875
•				cn	7 54
	-		1	ci2	3.55
		C1	31 67	C13	5 87
			• •	C14	7 58
			•	C15	1 7.0
		C 2	5.14	C 2	514
	:		1	C31	, 586
	;		1 0000	C32	4 72
	1	C 3	20 22	C33	3.77
		ł	•	C34	5 88
с	106 41			C.41	184
		I		C 4 2	2 83
		1	÷	C 43	3.41
	1	ł	1	C 4 4	
		C 4	; 41.50		
		1	1	C 4 5	5 24
		1	:	C46	751
			1	C 4 7	664
	:	J		C.48	10 86
		C a	4 91	Ca	<u>, 491</u>
	1	Cb	1 28	<u>C b</u>	128
		C	- 168	Ce	1.65
		1	:	W.LE	9.68
				W12	5.14
	÷	1		W13	4 73
		1		W.14	8 62
		ł	i	W-1 5	8 20
		i	1	W16	3 20
w	72 91	W1	72 91		
		1		<u>W17</u>	3.70
		1		WIB	6 04
		1	:	W19	095
				W 1 10	0 2 1
	:			ŵ i u	8 5
	•			W112	13.50

ID .	Area (km2)	iD	Asea (km2)	JÐ	Area (km2)
				SLI	2 68
				\$12	4 04
		\$1	14 33	\$13	4 3 8
				\$14	196
	:			\$15	1 27
				\$21	2 40
		\$2	15 65	\$22	196
				\$23	2 85
	:			\$ 2 4	8.45
	1		, ,	\$31	217
s	8174			S 3 2 S 3 3	2 32
			ł	533	5 75
	ļ	\$3	34.51	535	431
			1	\$3.6	4 3 4
	•	Í	4	\$3.7	6 45
				\$38	4 38
	-	\$4	2 36	5.4	2 36
	:	55	2 23	\$ 5	2 2 3
		S a	3.46	Sa	3.46
		56	3 86	Sb	3 85
		Sc	(533	Sc	533
		SE I	1 98	SE 1	1 198
	1	SE 2	2 60	58.2	2 60
		SE 3	1 92	SE 3	1.92
		SE.4	7.80	SE 4.1	5.40
	1		1	SE.4.2	2 40
		SE 5	3 83	SE.5	3 83
	1	SE 6	5.10	SE 6	5.10
		SE7	14 58	SE 7.1	8 39
	;			SE 81	<u>6 20</u> 2 77
	•	SE 8	11.33	SE 8 2	8 56
SE	11936	}	+	SE 9.1	7.45
		SE 9	21.11	SE 9 2	626
	1 1		1	SE 9 3	7 3 8
	1			SE 101	7 57
		SE 10	24 88	SE 10 2	11.43
			· · · ·	SE 103	5.88
	1	SE a	3 67	SE a	367
		SEb	1 516	SE b	5 16
	ļ	SEc	; 182	SE c	1.82
		SE 🕹	1 30	SEd	1 30
	:	SE e	277	SEe	277
		SEF	9.52	SEI	9.52
		NET	3 32	NE 1	3 32
	-	NE 2	9.53	NE 2 1 NE 2 2	4.75
		NE 3	1 7.15	NE 3	7.15
	•	NE 4	2 65	NE 4	2 65
		<u> </u>	,	NE S.I	10.12
NE	64 91		; ,	NE 52	4.72
		NE 5	34.38	NE 53	3.16
				NE 5.4	1017
			1	NESS	6 21
		NE a	3.76	NE a	3 76
		NEB	2 50	NE b	2 50
		NEc	1 62	NE c	- 162
· ·				To	al 58151
	· · · · · · · · · · · · · · · · · · ·				

Catchment

Sub-Calchment

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Measurement : GIS database Scale = 1/10,000

 Table C.6.2
 EXISTING LAND USE AREAS BY SUB-CATCHMENT (1/2)

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Zone	Catchment	S	ub-Catch	ment	· · · · · ·			aciduse Ar	ca by Categ	200 0.0	21			Runoff
-	ID	- ID		Area (km2)	Com :	Ind.			Low R.	Inst	Green	Agn	Water	Coefficient
		NLI		3.33	0.00,	0.13	0.00	0 22		0.00	0.00	2.96	0.01	0.44
		81.2		6.60	0.00	016	0.00	1.79	0.00	0.00	0.00	4.60	0.05	0.50
	N.1	81.5	· · · · ·	4 25	0.00	0.00	0.00	0.37	0.00	0.00	0.00	3.82	0.06	0.43
-		N14	- · · · ·	5.69	0.00	0.00	0.00	0.22	0.00	0 00	0.00	5.26	0 22	0.43
		N21		11.87	0.00	0 08	0.00	3.39	0.00	0.00	0.00	8 00	0.00	0.50
		N22		613	ŏ.00`	0.00	0.00	1.53		0.00	0.00	4 50	0.00	0,49
Northern Zone		823	• ·· · ·	····· H 24	0.00	0.00	0.00	2 32	0.00	0.11	0.00	8.60	0.01	0.47
S		N 2.4		532	0.60	0.05	0.01	···-ID	0.00	0.15	0.00	3.84"	0.05	0.49
E I		N 23	• · · ·	10.98	0.001	1011		6.87	0.00	0 22	000	8 50	0.11	0.48
D I		N 2 6		1119	- 0.00 ⁺	0 56	2 59	0.29	0.00	6 67	0.00	0.82	0.23	0.66
臣	N.2	N2.7		7 48	0.00*	6 18	0.89	1.28	0.00		0.00	3.93	0.05	0.55
.?		N 2 8		13.93	0.00	0 35	3.03	2.05	0.00	0.59	0.21	7.55	0.13	0 56
4.		N.2.9		6 32	0.00	0 19	0.00	134		0 02	0.00	4.47	010	0.50
		N 2 10 -	· · • ·	3.54	0.00	ō 20	0.00		0.00	0.00	0.00	4.06	0.11	0.49
		N 2 IT		5.71	- 000	0.01	1.36	0.24	0.00	0.64	0.00	2 89	0.57	0.59
		N 2 12			0.00	0.03	0.58	0.52	0.00	0.01	0.00	3.52	0 23	0.51
		N.2.13		6.89	0.05	0.07	1.64	0.13	0.00	- 131		3.21	0.26	0.58
	Na	Na		8.75	0.00	0.06	0.00	2.09	0.00	0.02	0.00	6.45	0.12	0.48
		СП		7.54	0.06	0.28	5.61	0.00	0.00	1.45	0.05	0.00	0.08	0.13
		C12		3.55	0.11	0.01	2 34	0.00	0.00	0.70	0.08	0.00	0.08	
	C.I	C.I.3		3.87	0.36	0.01	4.13		0.00	112	0.12	0.00	0.10	0.75
		CIA T	• • • • • • •	7.58	0.33	0.36	4.49.	0.00	0.00	1.69	0.56	0.00	0.12	0.72
		ci s		7.13	0.05	0.18	3.79	0,00	0.00	0.50	0.24	0.06	0.12	
	C2	C 2		5.14	0.01	0.15	- 3.41	0.00	0.00	0.01	0.00	0.08		0.78
		03.1		5,86	0.04	0.63	4.88	0.00	0.00	-0.04	0.00	0.95	0.37	0.74
		032		····· 4.72	0.00	0.49	2.82	0.10	0.00	- δ.09	0.21	0.83	0.20	0.80
õ	C.3	C33		3.77	0.00	0.15	193	0.00	0.00	0.07	6.00	1.24	0.33	0.69
્રુ		C3.1		5.88	0.00	610	····· 0.27	0.00	0.00	0.00	60.0	431	0.21	0.69
12		CT		184	0.00	010	0.63	0.00	0.00	0.03	0.00	0.56	0.21	
Central Zone		C42		288	0.00	-053	0.00	0.00	0.00	0.01	0.00	2.66	0.19	0.74
5		C 4 3		3,41	0.00	0.00	0.00		0.00	0.00	0.00	2 50	0.19	
O D		C.4.4		3.11	0.00	0.01	0.07	0.21	0.00	0.00	0.00	2.58	0.24	0.48
	C.4	C.4 5		5.24	- 0.31	0.51		0.00	0.00	0.00	0.00	0.44	0.44	0.45
		C.4.6		7,51	0.31	0.38	4.62	0.02	0.00	0.99	0.01	0.14	0.47	0,79
		C.4.7		6.64	0.14	0.16	4 28	0.01	0.00	0.72	- 0.01	0.62	0.69	0.75
		C.4.8	• • • •	10.86	0.14	0.92	4.71	0.69		0.81		0.95	1.68	0.76
	<u>Ca</u>	C a		4.91	0.00	0.92	1.06	0.00	0.00	0.06		3,62	0,15	0.75
	СЪ	<u>c.</u>		1.28	0.00	0.32	0.72	0.00		0.05	0.00	0.08	0.15	0.51
	Ce	Ce		1.68	0.48	0.10	0.00	0.00	0.00	0.03	0.12	0.00	0.0	0.60
*** * * ****		WIL	aa	9.65	0.01	0 27		0.76	0.00	0.17	0.00	1.41		
	I	W.1.2		9.68 3.T4	0.01	0.00	3.96	0.76	0.00	0.00	0.00	4.44	0.06	0.61
	1	W.1.3	-	4,73	0.00	0.00	0.00	0.50	0.00	0.00	0.00	4.58	0.06	0.44
2		w.T4		8.62	0.00	0.00	0.00	1.88	0.00	0.00	0.00 0.00	4 52 6.60	0.09	0.42
б	1	W1.3		8.02	0.00	0.01	0.02	0.68	0.00	0.00	0.00	137	0.03 0.11	0.47
Western Zone		W.16		3 20	0.00	0.04	0.03	0.84	0.00	0.02			0.03	0.44
E S	W.I	WIT		3.70	0.00	0.02	0.60	0.04	00.0	0.00		2.84	0.05	0.54
š	1	W.1.8	· · · -· ·	6.04	- 0.00 ⁺	001	0.00	0.04	0.00	0.00	0.00	5.33	0.13	0.41
Ň	1	W.19		0.99	0.00	0.06	0.00	0.05	0.00	0.00	0.00	6.72	0.15	0.41
_		W.1.16		0.99	0.00	0.00	0.09	0.00	0.00	0.00	0.60	0.05	0.10	0.33
		with	:	8.83	0.00			135	0.00	0.00	0.00	6,75	0.13	
	1.1.1	W.T.12	•••••	13.50	0.00	0.00	0.46			0.03		11.64	0.63	0,49
• ••• ••• •••	<u>}</u>	511		2.68	0.00			0.39		0.03	0.00			
	1	512		2.68	E	0.00	0.00			0.00		2 (9	0 20	0.49
č	S.1	\$13			0.00	000	0.00	0.34	1		0.00	3 39	0.30	0.47
Ñ	3.1		<u>.</u>	4.38	0.00	000		0.07		0.00		3,86	0.43	0.47
F	1	\$ 1.4		1.96	0.00	0.00	0.00	0.00		0.00		1.81	0.15	0.45
ğ	J	\$ 1.5		1 27	0.00	0.00	0.00	0.04		0.01	•	1.06	0.16	0.49
琂		S 2.1		2.40	0.00	0.00	0.00	0.26		0.60	000	1 88	0 26	0 50
	S 2	\$ 2 2		1%	0.00	0.00	0.03	0.40		0.00	0.00	1.41	0.11	0.50
, N														
Southern Zone	31	\$ 2 3 \$ 2 4		2.85	0.00	0.00	0.00 0.00	0.14		0.60		233	0.38	0.49

Table C.6.2

5.2 EXISTING LAND USE AREAS BY SUB-CATCHMENT (2/2)

Zoac	Catchment	- Sub-Ca	chment					ca by Catej	tóry (km	2)			Runoff
		10	Area (km2)	Com.	Ind		Med R ;	LowR	Inst.	Green	Agri	Water	Coefficien
		531	217	0.00	0.00	0.00	0 67	0.00	0.00	0.00	133	0.15	0.5
		\$32	2 32	0.00	0.00	0.00	0.13	0.60	0.02	0.00	3.94	0.21	۵.4 ۱
		\$ 3.3	4 79	0 00 ji	0.00	0.00	0.60	0.00	T0.13]	0.00	3 33	0.72	
Ų.	\$3	\$ 3.4	5.73	0.00	0.60	0.00	0.30	0.00	0.00	0.00	4.91	0.54	···· ð.
Southern 2000	33	\$35	4.33	0.00	0.00	0.00	0.08	0.00	0.01	Ō.00	3 76	0.45	Ŭ.
4		\$ 3.6	434	0.00	0.00	0.00	0.73	60.6	0.04	0.00	2.97	0.60	ŭ
Ę		\$3,7	6.45	0.00	0.00	0.00	0 23	0.00	0.00	0.00	5.63	0.60	D
Š.		\$38	4.38	0.00	0.00	0.00	0.57	0.00°	0.00)	0.00	3.20	0.61	····· 6
2	5.4	S.4	236	0.00	0.81	0.00	0.60	0.00	0.00	0.00	0.82	0.14	0
5	55	5.5	223	0.00	0.18	0.00	0.00	0.00	0.00	0.00	.96	0.09	0
	50	5.2	3.46	0.00	2.03	0.00	0.24	0.00	0.00	0.00	1.04	0.16	0
	55	5.6	3.86	0.00	0.14	0.00	0.10	0.00	0.18	0.00	3.19	15.0	0
	S.c	S.c	5 33	0.00	- 0.14	0.00	0.92	0.00	0.12	0.00	3.89	0 26	0
	NE.1	NE.I	332	000	0.01	0.00	0.53	0.00	0.00	0.00	2.73	0.05	σ – 1
	NE2	NELL	4 78		0.03	0.00	88.0	0.00	0.05	0.00	3.79	10.0	to
9		NE 2 2	4.73	0.00	0.00	0.00	1.01	0.00	0.00	0.00	3.66	0.07	0
North-Eastern 2006	NE 3	NE 3	7.15	0.00	0.02	0.00	2.02	0.00	0.35	0.00	4,69	0.06	0
3	NE.4	NE.4	2.65	0.00	0.18	0.00	1.01	0.00	0 28	0.00	<u> </u>	0.01	o
Ę	NE 5	NE.S.T	10.12	0.00	0.08	0.00	0.34		0.00	0.00	9.68	0.02	5t
3	1	SE32	4.72	···· 0.00 ¹	0.16	0.00	0.58	0.00	0.00	0.00	3.91	0.03	0
3		NE 5.3	3.16	0.00	0.55	0.00	0.27	0.00	0.03	0.00	2 26	. 0.04	· · · · a
ł.		NE 3.4	10.17		0 23	0.00	121	100.00 ·····	··· 0.47	0.00	\$ 20	0.03	a
ಕ್ಷ		NE 3.3	6 21		0.00	0,00	0.70	0.00	0.48		4.87	0,17	1
ž	NE a	NE a	3.76		0.03	0.00	0.14	0.00	0.02	0.00	3.42	0.15	16
	NEB	NE 6	2 50	0.00	0.07	0.00	0.08	0.00	0.02		2.28	0.06	
	NEC	NE c	1.62			0.00			0.00		0.83	0.30	1
	SE.	ISE I	1.95	0.00	0.04	1 0.00	0.18	0.00	0.00	0.00	1.68	0.08	
	SE 2	SE 2	260		0.03				0.00	0.00	2 33	80.0	
	SE 3	SE 3	19		0.01				0.00		1.60	0.19	•
		SEAT	5.40						0.00		3.92	0.21	
	SE.4	SE.42	2.40		0.00				0.00		1.98	0.13	
	SE 3	ISE 5	3.8				1		0.00	• •	3.18	0.07	
	5E.6	SE.6	3.10			5 C	•		0.08	0.00	- 424	0.13	
ų		SE.7.1	8.3		0.12	-	,		0.04		6.83	0.17	
5	\$E.7	SE.7.2	6.20			0.00	0.74	0.00	0.12	° ° 0.00'	4.79	0.36	; ·)
South-Eastern Zone	65.0	SEBI	2.7						0.00		2 63	0.06	
Ę	SE.8	SE32	8.5			1			0.00		7.25	0 28	1
ы К	1	SE 9.1	7,4	5 0.00	0.02	0.00	<u>, is</u>	0.00	0.36	0.00	5.76	0.12	:
Б Ц	SE.9	SE92	62	6 0.00	0.00	00.6	of 11 (0.3)	0.00	0.00	0.00	5.73	0.22	7
Ł		SE 9.3	7.3	8 0.00	0.00	0.00	0.62	0.00	0,00	0.00	6.51	0.2	5
ğ		SELIO	7.5	7 0.00	0.00	0.00	0.00	0.00	0.08	0.00	6.68	0.8	
Ň	SE.10	SE.10.2	0.4	3 0.00	0.60	<u>, </u>	0.6	0.00	0.00	, <u>0.00</u>	9.85	0.9	st
		SE 10 3	5.8	8 0.00	0.00	0.00	0.2	0.00	0.00		5.02	0.4	3
	SE a	SE a	3.6	7 0.00	0.00	0.00	5. 1.05	0.00	0.00	0.00	1.83	0.7:	5
	SE 6	SEB	3.1	6 0.00	0.00	0.00	5, 1.00	0.00	0.00	0.00	3.99	0.1	,,
	SEc	SEc	1.8	2 0.00	0.00				0.00	; 0.00	1.62	0.0	
	SE d	SEI	T.5							4		0.1	
	SE.e	SEe	2.7							1	2.51	0.20	
	SEL	SET	9.5		1						•	0.1	
	4	Total (ki							24 12	-	330.65	25.0	
		Percent	~1										

Com. : Commercial Areas Ind. : Industrial Areas High R. : High Residential Areas Inst. : Institutional Areas Green : Green Spaces Agri. : Agricultural Areas

Med. R. : Medium Residential Areas

Low R. : Low Residential Areas

Water : Water Bodies

Data Source : Urban Planning Institute, Ho Chi Minh City (UPL, HCMC) Calculation : GIS database : Inner City : Scale = 1/10,000 Outer City : Scale = 1/25,000

Zene	Catchment	Sut	-Catchmeat		• • • •	r	anduse Are-	a by Categ	ory (Lin2)			Runoff
	ID	מ	Area (kn		Ind.	High R .		Lov R.	Inst.	Green	Agri	Water	Coefficient
	1	NII		33 0.00	0.90	0.00	0.12	0.06	0.00	1.51	0.72	0.01	031
	N.I	N.1 Ž		60 0.00	2 07	60.00	0.64	0 23	0 26	2.18	1.17	0.05	0.57
	49.1	80.3	- 4	25 0.66		0.00	0.88	0.09	0.07	191	1 20	0.06	
		N.1.4		69 0.00	0.00	0.00	1.52	0.00	0.00	1.09	2 87	0.55	0.48
	r	N21	n	67 0.00	0.07	0.00	2 58	1.85	0.00	2 87	431	000	0.45
	1	N 2 2		43 0.00	0.00	0.00	0.41	0.65	0.13	0.19	5.05	0.00	0.44
Northern Zone		N 2 3		24 0.00	1 83	1.54	0.67	0.40	0.08	2.03	4.68	0.01	0.54
Ň		N 2.4		32 0.00	1.00	1.821	0.70	0.00	0 00	1.74	0.00	0.03	0.64
E		N.2.5	10	.98 0.00	0.08	4 39	2.30	0.58	0.18	2.13	1.19	0.14	0.63
<u>S</u>		N.2.6		19 0.00		3.15	0.00	0.00	7.14	0.49	0.00	0 2 5	0.66
Ę	N 2	N 2.7		48 0.00		3.74	0.29	0.65	1.70	1.04	0.00	0.03	0.6
ž		N 2 8		93 0.00		6.49	2 2 5	1 86	1.18	1.98	0.00	0.13	0.67
		N29		32 0.00		0.001	1.66	0.70	0.26	3 32	0.00	0.10	0.49
		N 2 10		54 0.00		0.00	1.52	6.00	0.00	2.52	0.00	0.11	0.37
		N.2.11		.71 0.00		2 29,	1.70	0.00	0.25	0.91	0.03*	0.57	0.70
		N.2.12		89 0.00		1 23	2.03	0.00	0.11	1 24	0.04	0.23	0.63
		N213		.89 D.00		5.15	0.23	0.00	0.16	1.09	0.00	0.28	0.72
	Na	Na		75 0.00		0.00	4.02	0.00	0.43	3.91	0.00	0.12	0.52
		CH		31 0.00		5.96'	0.00	0.00	1.47	0.01	0.00	0.05	0.76
		C12		33 0.00		3.16	0.00,	0.00	0.00	0.29	0.00	0.10	5.17
	C.I	C.13		87 0.00		5.38	0.00	0.00	0.11	0.13	0.00	0.05	0.79
		<u>C.14</u>		58 0.00		5.61	0.00	0.00	1.09	0.76	0.00	<u>σ.</u> Ω	0.72
		°C.1.5		0.00		6.15	0.00	0.00	0.46	0.51	0.00	0.30	0.78
	C.2	<u>C2</u>		0.00		4.47	0.00	0.00	0.00	0 30	0.00	0.37	0.78
		C.3.1		.86 0.00			0.00	0.00	0.00	0.15	0.00	0.07	
e د	C3	C.3.2		72 0.00		3.36	0.00	0.00	0.00	1.16	0.00	0.20	
ŝ		C33		0.00		3.42	0.00	0.00	0.02	0.00	0.00	0.33	0.82
Ň		C.3.4		5.88 0.00		4.18	0.00	0.00	0.00	1.40	0.04	0.21	0.69
Central Zone		C.4.1		.84 0.00		1.31	0.00	0.00	0.00	0.01	0.00,	0,52	1
E.		C.42		88 0.00			0.93	0.00	0.00	0.61	0.00	0.19	
പ്		°C.4.3		3.41 0.00			2 56	0.00	0.00	0.74	0.00	0.13	0.53
	C.4	C.4.4		3.11 0.00			0.62	0.00	0.71	0.96	0.53	024	
		C43		5.24 0.00		2.77	0.00	0.00	2.03	0.00	0.00	0.11	
		C.4.6		7.31 0.00			0.01	0.00	3.07	0.71	00.0	0.17	
		C.4.7		5.64 0.00			0.00	0.00	2.75	0.10	0.00	0.69	
		C.4.8		0.86 0.00		3.67	0.55	0.29	3.28	1.03	0.00;	1,68	
	C a	Са		1.91 0.00			0.00	0.00	0.07	2 65	0.00	0.13	
	С.Б	-C.b		28 0.00			0.00	0.00	0.00	0.42	0.04	0.08	1
	C.c	<u>С.</u> с		1.68 0.00		· · · · ·	0.00	0 .00	1.53;	0.11	0.000	0.04	
		W.L1		9.68 0.00			0.58	0.28	0.38	2 26	0.01	0.06	
		W.1.2	•	5.14 0.00			060	0.41	0.00	0.19	3.88	0.06	
•		W13		4.73 0.00			0.00	0.68	0.00	0.00	4,56	0.09	
č		W.1.4		8.62 0.00			1.61	0.62	0.15	4.13	0.07	0.03	
Ň		W.15		8.20 0.00			0.16	0.84	0.99	0.93	1.62	0.11	
Western Zone	W.I	W.16		3.20 0.00			0.33	0.00	0.01	0.69	0.00,	0.0	
. E		.W.I.7		3.70 0.00	•		1.69	0.45	0.03	0.51	0.01	0.10	
es/	ļ ·	W.1.8	1.1.1. .	6.04 0.00			0.49	0 21	0.00	0.00	5.20	0.1	
3	1	W.19		0.99 0.00			0.00	0.00	0.00	0.15	0.00	0.10	
-	1	W.1.10		0.27 0.00			0.00	0.00	0.00	0.02	0.00	0.1	
	i i i	W.LEE		8.85 0.0			1 25	0.07	0.87	2.34	1.92	030	
		W.1012		3:30 1 0.00	1		1.48	0.69	0.37	1.75	724	0.6	
		511		2 68 0 0			0.92		0.00	0.66	0.65	0.20	
2		\$12		4.04 0.0			0.99		0.00	1.06	1.62	03	
Southern Zone	S .1	\$.1.3		4 38 0.0			0.85	0.00	0.21	1.26	1.19	0.4	
12		S.1.4	1	1.96 0.0			0.60	0.00	0.00	0.00	[8]	Ø.):	
en -		S1.5		1.27 0.0			0.00	0.00	0.00	0.05	1.06	0.10	
÷		\$21		2.40 0.0			0.58	0.07	0.00	1.49	0.00	0 20	
	S 2	\$ 2 2		1.96 0.0			0.85	0.00	0.51	0.49	0.00	0.1	
· •				A A # 2 A # 2		A 50	0 57	0.00	0.00	11.32°	0.58	0.3	8 01
So		\$23 \$24		2 85 0.0 8.45 0.0			1.55	0.07	0.00	0.61	4.67	0.6	

Table C.6.3 FUTURE (2020) LAND USE AREAS BY SUB-CATCHMENT (1/2)

8

\$

Zone	Catchinent	Sub-Catch	ment				Landuse A	rea by Cat	igory (km	2)			Runot
2.V.	C treasient		Area (km2)	Cera.	Ind	Ibgh R	Med.R.	Low R.	Test	Green	Agn	Water	Coefficient
	L	331	217	0.00	0.00	0.9	0 39	012	0.12	0.10	0.00,	0.13	0.71
		\$32	232	0.00	0.00	T.73	0.00	0.00	0.00	0.38	0.00	0.21	0.74
:	1	\$33	4.79	0.00	0.00	1.77	0.62	1 56	0.00	0.11	0.00	6.72	0.74
		\$3.4	5,75	0.00	- 0 60 ⁺	0 38 [†]	7.13	0.01	0.22	2.47	0.00	0 \$4	0 56
Southern Zone	\$3	3.13	4.31	0.00	65.6	1.00	1765	0.07	0.13	1 38	0.00	0.45	0.60
Ň	1	\$36	4.34	0.00	ō.00	0.00	233	0 33	0.00	1.08	0.00	0.60	660
Ε		\$ 17	6.45	- ō.60	0.00	0.00	2.15	0.00	0.05	3.05	0.00	0.60	0.54
2		\$ 3 8	4.38	0.00	0.00	6 00	2 33	031	0.23	0.90	0.00	(6.0	0.65
H H	5.4	5.4	2 36	0.00	1 04	0 26	0.00	0.00	0.09	0.84	0.00	0.14	0.67
ъ	5 5	\$.5	2 23	0.00	0.61	0.49	0.00	0.00	0.00	1.04	0.00	0.09	0.60
	51	Sa	3,46	0.00	2.75	0.00	0.00	· ·	0.00	0.55	0.00	0.16	0.81
	55	55	3.85	0.00	0.92	0.47	0.00		0.23	2.00	0.00	ō 24	0.57
	Sc	Se	5.33	0.00	LB	0.00	0 27		0.00	2 26	0.00	0.26	0.36
	NE.1	NE.1	3.32	0.00	0.17	0.00	1.46		0.00	1.34	0.00	0.03	
	NE 2	NE21	- 3.78		0.00	0.00	3.70			0.04	0.00	0.64	0.68
õ	NE Z	NE 2 2	4.75		0.00	0.26				0.85	0.62	0.07	0.62
North-Eastern Zone	NE 3	NE 3	7,15		0.17	1.33	1.63		2 62	0.82		0.06	0.64
N	NE.4	NE.4	2.65	0.00	0.00					0.17		0.01	0.73
E,		NE 5.1	10.12		1.09		0.00		1	3.32	0.00	0.02	0.53
វ័ន	i i	NE 3.2	4.72		1.98	0.00	0.17		0.32	1 57	0.00	0.03	0.63
ណ៍	NE.5	NE33	3.16	f	17	072	0.00			0.25	0.00	0.04	0.79
÷	1	NE 3.4	10.17		0.88		134		1.97	3.97	0.00	0.03	0.54
5	· ·	NESS	6.2	1	1.6	•	0.36	1	•	3.52	0.00	0.17	
Z	NE a	NE a	3.76	•	0.21		1.32		•	1.65	,	0.15 0.06	
	NE b	NE b	250		0.00	,	1		• •			0.00	
	NEC	NE ¢	1.62		0.47	1			•	0.92		0.00	1
	SE 1	ise.1	1.99		0.00	4	ł.		•			0.00	
	SE 2	SE 2	26		0.00		•					0.0	
	\$E.3	SE 3 SE 4.1	5.4		0.00							0.2	
	SE.4	SE.4.1	2.4										
	SE 3	SE 5	38										
	SE 6	SE 6	5.1					,					
**		SE 7.1	83		f				•		1	4	
Ĕ	SE.7	SE 7.2	62									03	
Z		SEBI	2.7					1 0.0X	5 <u>0.00</u>	1.70	0.00	0.0	8 0.46
South-Eastern Zone	\$E.8	SE 8 2	85	6 0.00	2 26	0.00	1.0	0.40	0.08	4.52	0.00	0.2	B 0.55
ste		SE.9.1	7.4	6 0.63	<u>1 I R</u>	1.69	F <mark>. 1.0</mark>	6 0.3	s <u>i 0.5</u> 0	2 01	0.00	0.1	2 0.65
ដ	SE 9	5892	62	6 0.00	0.0X	1.29	0.5				0.00		
Ē		SE 9.3	7.3	8 0.00	0.0	0.00	3.5	2 0.0					
T T		SE 10.1	1.5	7 0.00	000	<u> </u>							
Š	SE.10	SE 10.2	- <u> </u>	3 0.00									
		SE 10.3	5.8						1				
	SE a	SE.a	3.6										
	<u>- 5E.6</u>	SED	3.1									•	
	SEC	SEc	1.3										
	2E.9	SEd	13			1							
	SE e	SE ¢	2.7										
	SET	SET	9.3						· ·				1
	· · · · · · · · · · · · · · · · · · ·	Total (km)					-						
		Percent (ରୀ [™] 169.0	01 0.3	5***********	5, 23.0	3, 14.8	9 4.1	6 9.1	27.2	9 9.9	7, 11, 14, 3	41 · · · · · · · ·

FUTURE (2020) LAND USE AREAS BY SUB-CATCHMENT (2/2) Table C.6.3

Com : Commercial Areas

Inst : Institutional Areas Green 1 Green Spaces

Ind. : Industrial Areas

Agril : Agricultural Areas Water : Water Bodies

High R. : High Residential Areas Med R. : Medium Residential Areas Low R. : Low Residential Areas

Data Source : Urban Planning Institute, Ho Chi Minh City (UPI, HCMC) Calculation : GIS database : Inner City : Scale = 1/25,000 Outer City : Scale = 1/25,000

췖

Item No.	Aain Landuse Group	Sub-Group for Landuse Category	Sub-Group for Landuse Category (as in original GIS database by UPI, HCMC)		Run off Coefficient	ų
		Existing Landuse	Future Landuse (2020)	Normal Range	Hydrological Applied by JICA Sub-Institute. Study Team HCMC*	Applied by Study Te
1	Commercial Areas	Services, Commerce	Commerce, Services	0.70 - 0.90	0.80	0.80
		Industrial Area	Industrial Area (Existing)			
		Ware House	[Industrial Area (Planned)	0.70 - 0.60	000	08.0
7	Industrial Arcas		Ware House		^ /··>	~~~~
			Garbage Treatment Site (Planned)			
,		Residential (Inner City)	Inner City	0 20 - 0 00	0.80	0.80
s,	High Residential Areas	en en anter en anter anter a la companya de la comp	Suburban Residential Town (Planned)	0.10 - 0.10	20.2	20.0
4	Medium Residential Arcas	Residential (Suburban)	Suburban Residential Area (Planned)	0.50 - 0.70	09.0	0.70
s	Low Residential Areas		Existing Residential Area (Suburban)	0.30 - 0.50	0.40	0.60
		Administrative Office	City Center			
	•	Education	District Center			
		Health Care	Center of an Area			
;	- -	Social Culture, Sports	Culture, Education			
		Military	Tourism	040-040	050	0.60
Þ	Insulutional Areas	Preservative Works	Military	0000 - 0100	>	222
	-	Religion				
		Transportation Stations				
		Public Works				
		Technical Works				
r	Current Constant	Green Park	Green Park (Planned)	010-030	02.0	0.30
•	Orecti Spaces	Cemetary	Ecological Forestry			
20	Agricultural Areas	Agriculture	Agriculture	0.10 - 0.60	0.15	0.40
6	Water Bodies	River, Canal	River, Canal			1.00

CRITERIA FOR RUNOFF COEFFICIENT BY LAND USE CATEGORY Table C.6.4

轡

* : "Research the drainage capacity and measure for the inner area of Ho Chi Minh City"; Hydrological Sub-Institute of HCMC; 1989

URBANIZATION AND RUNOFF COEFFICIENTS Table C.6.5

7	one	Catel	ment	Existin	gLandu	se Area (km?)		Future (2	020) I a	nduse Area (kir	2)		Runoff C	tasiodfso	
ID .	Area	10	Area	Urbanize	J	Non-Urban	ized	Urbaniz	eđ	Non-Urba	ized	Catche	nent	2 e	6 č
	(km2)		(km2)	Catchment	Zone	Catchment	700e	Catchment !	Zone	Calchment :	Zone	Existing	Future	Existing	Future
nin en pr		NI	19 R7	2 8 8		16 98		6 85		13 01		0 45	0.51		
N	136.18	N 2	107 57	41 54	46 60	66 03	89 58	68 81	BO 35	38 75	55 83	0 53	0 60	0.52	0.55
		Na	B 75	2 17		6 58		4 68		4 06		0 48	0 52		
		C L	3167	29.76		191		29 59		2 07		0.75	0 76		
		C 2	\$ 14	381	ł	133,		4 4 7		0.67		0.74	0 78	1	
		C 3	20 22	12 41		781		16 67		3 56		0.67	074]	
C	106 41	C ł	41.50	25 6)	75 38	15 89	31 03	32 45	87 56	9.05	15 85	0.70	0 70	070	072
		C a	4 91			3 17		2 10		2 81		0.51	0.53	1	
		Сь	1 28) 13		016		0.75		0.54		0 80	0.64	1	
		Cτ	1.68	1.52		0 16		1 53		0 15		0.66	0 59	.[
w	72 91	WI	72.9)	14 39	14 39	58 52	58 52	33 62	33 62	39 29	39 29	0.45	0.56	0.45	0.55
		51	1433	0 87		13.46		371		10 62		0.47	0.52	1	
		52	15 66			14 13		5 12		10 54		0.48	0.51	1	
		\$3	34.51			30.97		20.96		13 55		0.50	0.63	.[
		54	236					139		0.07		0.68	0 6		
s	8174	55	- 223	4	11 38	2 05	70 36	110		113	42 26	0.46	0.60	0.00	0 59
		Sa.	3.40			1 20		2 75	•	071		074	01		
	•	· - ·	•	4		3 4 4		162		2 24	2	0.47	05		
		56	38	1		415		2 81	1	2 52		0.50	0.5	1	
	<u>.</u>	50				2 78	· · · · · · · · · · · · · · · · · · ·	193	• • • • •	1 39		0.46	05	+	
	1 V	NET	1 333]		8 51	1	1 02		0.47	06	1	
		NE 2	95			7 56	,	6 25	÷	0.89	1	0 50	06	1	
		NE 3	71						1		ţ	0.57	07	,	
NE	64 93	NE 4	26	· · · · · · · · · · · ·	32.35			1 ··· - · · · · ·	1 44.2	8 0 18 12 92		0.45	05	0.97	: 0.59
		NE 5	343	1 · · · · ·		29 25		21.46	1	1 79	-	0.44		- 1	
		NE a	37	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		357		197				0 44	2° 2. 04	1	:
		NED	25		•	2 34	•	102	7	1.4	•	0 66		-	
	·	NE.C	16			113		095		0.61	T	0.46			
		SE 3	19	· • · · · · · · · · · ·		1.75	1	0.98	i	100	1	0.44	11 P P P P P P	· 1	
		5E 2	26	1	•	2 39		1.7	Ţ	0.88		0.44	•••	1	
		SE 3	19		-	1 78	-	169	` •	0 2	1	· · · · · · · · · ·	• • • • • •	1	
		. <u>SE 4</u>	78			6.25	-	2 2	-	55	1	0.49	• • • • • • • • • • • • • • • • • • • •	1	
		58.5			-	32	-	2.5	•	13	7	0.46			
		SE 6	51		-	4 30		43:	•	070	•	0.46	 A 1997 		
		SE 7	14 5	8 2 43		12 1	1	83		62	1	0 48			
SE.	119 35	SE 8		B 100	. 13 5	4 10.2	105.8							0.40	0.5
		SE 9	211	2.52		18.59	₹.	114	6	95		0.45		· · ·	
		SE K	241	S 0.95	ŀ	23 8	?:	7.4	<u>o</u> '	17.4	•	0.46	÷		
		SE a	30	7 169)	25	7_	23	9	12	8.	0 63	• · · · • ·	1	
		5E b	5.9	15 1 00)	410	6	40	ı'	<u></u>	s.	0.48			
		SE e	11	2 010		16	6	00	o .	18	2	0.44		-1	
		SE d	1.	04	۲ <u>.</u>	08	6	0 4	9	03	Ľ,	0.56	5 0	62	
		SE e	2	00)	27	1	0.0	0	27	7	0.46		-	÷ .
		SE I	9	52 0.4	2	9.1	L.	19	2	76	01	0.4	20	38	
	Total	Azea (km	2) 581	51 173	66	407	85	339	81	241	70	_			
		Percent (70	14	58.	41	41	56		1		

Urbacized Non-Urbanized Sub-Total of commercial, industrial, residential and institutional areas Sub-Total of green spaces, agricultural areas and water bodies

Data Source : Urban Planning Institute, Ho Chi Minh City (UPL HCMC) Measurement : GIS database Inner City => Scate = 1/10,000 (for existing landuse) and 1/25,000 (for future landuse) Outer City => Scate = 1/25,000 (for both existing and future landuse) Measurement : GIS database

Draunake i Catchmont	nent Nub-	Sub-Catchment	Runofl'Pount	Point								Details	of Runoff	Details of Runoff Calculation by Kational Formula	T by Kalio	nal Form	9						
Area		Area	9	ANA.	U U	٦ د	(min) Vr(m	Vs) by Sey	ment	(km) Lr (km)		umulative	s Tr (min	Cumulativ	e To (min) 1 for 5-5	Cumulative Tr (min Cumulative Ta (min): I for 5-yr (mm/hr) I for 10-yr (mm/hr)	1 for 10-y	տ (աա/ու)	¢ Ó	r 5-yr (m3/s	On for 3-vr (m3/s) On for 10-vr (m3/s)	7E) 22
				-	Ex. Fut. (k	m) Ex	(km) Ex Put Ex Fut		-	Segment - Cumulative		F.x.	Fut.	Ex	Put	Ä	Fut	ă	Fu	-	μ.	Ex	ž
	C C Z	11 67 N	A G N	11.67	0.48 3	47	001 -	0		0.97	126.0		ล		12	1	40.0		8.0 STS	8.0	•	<u>3</u>	
		•		18.10	0.47	: +	1	. 6	Ĺ		2.65		3		16.		35.4		39.4 0.94	40	-		8
		,	0.07	2013	05.0	•		0		8	6.74	Í	171		51 		20.7		12.6 0.9	16.0		-	5
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		101	10 07	CC 8/	0.40	1.	i 	o	÷		17.45	† '	e70}	•	ä				0.20	8.9 0.83	°	đ	Ĩ
		<u> </u>	12			2 16	121		1	. 011	3.10	•	12	•	52	Ļ	5.61		213 0.98	86.0		5	•
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	3	4.7	12	19.55	0.55	-	! +		:		20.8	i I	5				14.3		15.6	80	3		
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	× ×	6.04	N B	8	0 44	<u> </u> 	74			4.90	8.4	-	17		34		16.8		18.3	0.98			5
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. '			¥1.E	50.28	0.57	,	 - - 				15.97		Å		11.		20		9.5 0.87	0.87	53	ا	2
	W.1.10	0.1	0.27 W.I.P	20.55	0.57	: ; [ð - 	<u> </u>	18	17.15		669		760		() 30		9.0 0.87	0.87	3	ן 	•
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				2	0.46		:	ć	-	¥	2 V	-	841		910		70		7.7	0.83	¢	-	

PEAK RUNOFF CALCULATION FOR OUTFLOW FROM DAIHAN CANAL (ALTERNATIVE 1) Table C.6.6

C = Runoff coefficient, Lr = Inter length, Tr = inter time, Vr = Plow velocity, Lr = Flow tength, Tr = Flow time Tr & Trime of concentration; I = Rainfull intensity, f = Areal reduction factor, Qr = Peak runoff Note : It is assumed that outflow from Kach Daihan will be discharged into Rach Tham Luong - Rach Ben Cat system.

Uranake Catchment	nt Sub-Catchment	nt Kuñolf Point	Long																2 C. L.		1 0 - 1 m J	i
		L	Area	- -	-	1, (min)	Vr (m/s) by Se	Segment	لية (km)		Cumulative	Tr (mm) C	Cumulative Tr (min) Cumulative Tr (min) 1	(r (mm)) 1	(or S-yr (mm/hr))		뒤	<u>-</u>	사 호 주	Ch tor X-vr (m.Vs) - Ch to		
•				Fix Fut	~	FAL FUL	A A	ł	Vegment Cum	Cumulative I		Fut	Ex.	Ful.	F.K	Ϋ́u. f	EX 1	Fut.	Ē	Fut.	N.	۶ļ
		2 14 2 E	1.	ļ	1			┞	. 80	10.7	-	8		12		45.6	-	51.0: 0.4	\$	3	-	2
;	•						0	035	2.25	5 85		167		232		2.7	. :	26.9 0.9	4	8		8
					1			ł	4 17 1	10.21	1.	375		440	-	13.4		14.6 0.9	-	8		<u>8</u>]
	-+				, r	2		<u>+</u> -	10	10		2		50.	•	19		213 0.9	*	9		2
	• •		1		-	3			64 1	50		i.	+	11	∔ } {	14.2		15.5 0.96	Ŷ	\$		4
			2					1	-	10.01		375	-	3		13.4		14.6 0.8	-	8		2
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			6.99	2								197	1	ĝ				8.2 0.84	4	2		*
	•		8					-		18				112		27.2		24.7 0.97		3		
	W.1.4	20.0			-					10.93		240		940	-	7.5		8.2 0.83	0	- 18		~
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C = Runoff coefficient, Li = Inier length, Ti = Inier times. Vi = Flow velocity, Li = Flow length; Tr = Flow time Tic = Time of concentration; 1 = Rainfail intensity. Li = Areal reduction factor; Op = Peak runoff

Note : It is assumed that outflow from Kauh Dailven will be discharged into Rach Tham Luong - Rach Ben Cat system :

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Min (5, 16) Display (2, 16	Amb. Fix. Ford Disgmant Community 1.35 35 30 0.33 2.04 0.35 1.47 100 0.37 0.30 0.37 0.40 0.35 3.47 100 0.37 0.30 0.37 0.36 0.37 3.47 100 0.37 0.37 0.36 0.37 0.36 0.35 0.37 0.37 0.36 0.37 0.36 0.37 0.37 0.37 0.37 0.36 0.37 0.36 0.37 0.37 0.37 0.37 0.34 0.36 0.37 0.36 0.37 0.37 0.37 0.34 0.36 0.37 0.36 0.37 0.37 0.31 0.37 0.36 0.37 0.36 0.37 0.31 0.33 2.34 0.35 0.36 0.37 0.31 0.33 2.34 0.36 0.36 0.31 0.31 0.31	Bur Fa		- -		ů	•••	
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PEAK RUNOFF CALCULATION BY RATIONAL METHOD (1/2) Table C.6.8

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9/2 SL2 266/SE2A 2.66/10 (arc) (arc) 0.27 0.60 2.66 1.7 2.66 1.7 2.66 1.7 2.66 1.7 2.66 1.7 2.66 1.7 2.66 1.7 2.66 1.7 2.66 1.7 2.66 1.7 2.66 1.7 2.66 1.7 2.66	3	\$	30.01 0.94		
NF.3 SF.3 Vec With A		37 4.	53 X 0.00	11 22	
SEA Stat And Stead		-4 14	30.5 0.04		
SE SE 2.40 SER4.8 7.80 0.90 0.44 0.40 0.40 2.05 5.45 2.27 2.46 2.91 3.021 <		513	31.3 0.4%	×	2
NEA NEA NAT[SEAA Net] UNO 2.41 1.11 1.11 4.10 2.42 1.11 3.11 3.11 3.12 3.11		21.0	21 0 0 07		
SEA SEA <td></td> <td>÷ Zi</td> <td>37.3 0.00</td> <td></td> <td></td>		÷ Zi	37.3 0.00		
RE7 NB7.1 K.20[SE/A X.90 (0.66) (3.5) (100) (3.5) 0.40 0.50 1.50 1.41 2.51 1.91 2.43 30.0 SE73 SE71 Z77 (SE/A Z79 (SE/A Z79 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z77 (SE/A Z76 (SE/A Z77 (SE/A Z76 (SE/A		- 4	20.7:0.98		
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[44] [27.12]					-
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N.1 N.12 600 N.1.8 N.13 425 N.1 C N.14 560 N.1.0 N.21 1160 N.2.0 N.22 643 N.2.0 N.22 1124 N.2.0 N.20 N.20 N.20 N.20 N.20	03 048 0.55 17 0.47 0.52 87 0.46 0.51 0.7 0.50 0.48 3. 10 0.50 0.48 3. 10 0.50 0.47 3. 10 0.50 0.47 3.	<u>8</u>	┊╸┧╸┥╸╽╌┤╶┼╴┤	3.38 3.61 3.61 3.61						22	20.02		1		• •
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NI.3 425/NI.C NI.4 500/LID N2.1 110/N2.A N2.2 11.24/N2.A N2.4 5.22 N2.D N2.4 5.22 N2.D N2.5 10.08/N2.D2 N2.5 10.08/N2.D2	17 0.47 0.52 87 0.46 0.51 67 0.50 0.48 3.4 10 0.50 0.47 133 0.49 0.52	8	╺╺┥╸╽╌┥╶╁╴					I.			11 5 0 0				-1
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N21 1167 N2A N22 640 N2B N25 114 N2C N2A 114 N2C N2A 1098 N2D2 N2D2	67 0.50 0.48 3. 10 0.50 0.47 131 0.49 0.50	8	╏╌┥╌╂╴╏				345				20.4 0.44		1		e
N.2.2 640 N.2.6 N.2.5 1124 N.2.6 N.2.4 N.2.6 N.2.4 10,08 N.2.02 N.2.6 10,08 N.2.02	10 0.50 0.47 .33 0.49 0.50					-	111	111 8	0.5 50.5		0 99 9	80	76 76	<u></u>	ž
N23 1128 N26 N23 532 N26 N28 1098 N201 N25 1098 N202	33 0.49 0.50			168			130			49.2	49.2 C		1		<u>ک</u>
N.2.5 1.24 N.2.6 N.2.6 5.32 N.2.6 N.2.5 10.08 N.2.02 N.2.5 10.08 N.2.02	53 0.49 0.52		-	97		ļ	1831	ĺ	ł		0 14.66	11 160	11.		2
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4 80 N 21	00 681 0.53 0.59		0.15	25	21.48 89	173	Š	874	6.4 7.2		а б х	1			3
C N OA Y	in states and		ľ	2.61	24.09 1035		1135	\$ S	57 64	6.4	110	0.81 9	97 122	:90 1	2

Table C.6.9 PEAK RUNOFF ALONG BEN DA-BA HONG AND THAM LUONG-BEN CAT CANALS WITHOUT INUNDATION

C = Runoff coefficient, L= Inlet length; T: = Inlet time; Vr = Flow velocity; Lr = Flow length; T: = Priow tume; T: = Time of concentration; I = Rainfall intensity; f = Area' reduction factor; Or = Peak runoff

DESIGN DISCHARGES OF THE CANALS BY RATIONAL METHOD (1/2) Table C.6.10

					İ	т	L	r	The second second second second second second second second second second second second second second second se	- 4, 9 P	DAY R.P.	Reduction	5 11 10	30-41.2
Area	(D Area	01 10	Name	Area (m)	< <	Area Coefficient /hm2)	(m)	(II/8)	(minutes)		(mmhr)	Factor	(m)(n)	(m3/s
1	5 2	ត្			1	111 011	101	550			61.5	\$0	ล	
						į	1			2	20.5	50	2	
	- 7	10 87 C.N	- Kach Ben Da - Rach Ba Hong *	19.87					9	i	20.5	80	57	
						İ				0.4	152	10 0		
	_	-	-	,			10.7	2				3	3	
-		_			-		50	2		1				
		-		14 41	14.4 N.2B	1	191	8	3					:
uc		in z si				29.33 0.50	- 8	80	77				e i	
_					.	4.65 0.52	2 40	940	381	15.3:	16.7	80	¢	
			- K 10 (News 1	50	ŀ	000 1860	3.34	0.30	220	15.4	16.K	*	Ā	
		5			-	16.821 0.57	\$ 1	50.0	454	13.0.	14.2	0.80	3	
		_		LA FA		Į.	i,	0.15	4		11.7	0.24	8	
	N.2 107	07.57 C-N.3	Num Tham wong						701		¥9	0.83	8	1
-		·				L	-	010	200		21.3	24.0	\$	
		ς Ζ	Rach Ben Cat	11.86						14 71		80	7	
					•	÷				ł	×	0 %1	3	l
		_			N 2H			5	ŝ				8	
		23	Kinh Tham Luong	107.57		00.68 0.59	5.2		3					
					_	107.57 0 60	2.61	0.35	1068		0.0	0.81	3	
1	ł	ļ			- -	7.54 0.76	0.55	S .1	84.	213	75.4	50	8	
					-			120	2	1	101	80	ġ	
	-			-		ł	1			1	17.6	.00	1.6	
	รี 	31 67 0-01	Rach Nhieu Loc - Rach Thi Nghe	79'IC							14.5	100	1.01	ì
					-	24.54 0.76	- Z Z	5.0	ŧ	10.07			+	
					CIE - 3	1.67 0.76	2.15	0.70	27%	20.7		170		
-		C UT UT 1	. March Con. Con., Rach Tail Vam Tat	5.14	C.2.A	5,14 0.78	2.06	0.40	116	48.5	54,3	š	ŝ	
-						X 0 XX	2.26	8	2	1.17	8.67	860	8	
								20	00	55.4:	3	0.0	112	
	C3 20	20.22	NACT LAN FOR + NACT LO COM				1.1	940	2	325	36.1	56.0	112	
1		•				Ì	5			5 C	47.6	860	4	ļ
		_	날씨는	22			2		1441		12.14	30	2	
		3 0		01.10	(~)	ł						1000		
		ပိုပ	ž	2.82	2.85 C 4.A2			3	1					1
_				54		3,41 0.62	\$	8		} 	2			-
		100	Nach Ba Lun		C.4.A4	6.52) 0.58	3.18	0.40	TT.		2	0.95		
	- 	41.50				36.71 0.71	3.02	040	360	15.8	17.2	80	117	
					. ⊺ ر	L	40	0.40	427		15.0	0.88	17.	
		ŝ	Kinh Doi - Kinh Te	17.19			6	0.40	\$		12.8	78.0	117	
				-		1			127	0		0.85	117	
		_	ł		C*C					ł		0.07		
			.Kach Tan Phu	80.6	× . ×	80 80	8							ļ
			-				5	+ ₹		l				
				41.76	W.LO			90			0.01		ŝ	+
		- 	Ninh Chua - Rach Nuoc Len		ST M	8.42 0.52	2.20	0.00	211		29.7	5		
					W 1.01	76.36 0.57	4.49	0.40	3 8		1.1	8	ŝ	
- •			C. Buck March	120	3	3.20 0.69	200	010	167	34.7	38.7	8	71 	
	¥.: 7	7. 91 L.Y.					12	970	112		1	0.58	- 6	
		3	Kach Chus - Kach Nuoc		1	ł			YFL	× 91	12.81	0.98		
15		N S S	Rec	50.9	6.04 W. EZ									1
			1 •		W.E	7.02 0.50	1.36	940	402		2.5	8.0	4	
	••••	C-W.4	4 Nong Ban Luc	60'A0	W.L.F.	50.55 0.57	811	640	760	() %	0.0	0.87	\$	
	• •	-	-		0	19.41 0.57	1 85	0.40	837	7.5	5 .3	0.85	3	
	- ;	C-WS	5 Song Can Give	1672		7 01 04	- 1 - 20	040	016		2.7	0.83	- ¢\$	

Can al improvement plan for Rach Ben Ban Hong has been proposed considering inundation in the upper fuo classifier and at transfig bioms N.2.A, N.2.B, N.2.C and N.2.D1 and 24 mD4s responsed considering inundation. Design (Screen through main channel at transfig bioms N.2.A, N.2.B, N.2.C and N.2.D1 and 24 mD4s responsed considering inundation. Design (Screen through main channel at transfig bioms N.2.A, N.2.B, N.2.C and N.2.D1 and 24 mD4s responsed considering inundation. Design (Screen through main channel at transfig bioms N.2.A, N.2.B, N.2.C and N.2.D1 and 24 mD4s responsed considering inundation. Design (Screen through main channel at transfig bioms N.2.A, N.2.B, N.2.C and N.2.D1 and 24 mD4s respectively.
 Canal improvement plan for Kinh Chua has been proposed considering inundation. Design (Screen through main channel are different runoff points. under inundation condition.
 Canal improvement plan for Kinh Chua has been proposed considering inundation. Design (Screen through main channel for lengths of 0.25 and 31.1.4 m along resches W1.1.0 are 12 and 14 mJ/s respectively.
 Canal improvement plan for Kinh Chua has been proposed considering inundation. Design (Screen through main channel for lengths of 0.25 and 31.1.4 m along resches W1.1.0 are 12 and 14 mJ/s respectively.
 The design discharges along Xinh Chua (Rooff points W1.1.9 and W1.1.C.1), as shown in this table represent total discharges through main channel for lengths of 0.25 and 31.1.4 m along resches W1.6.1 are 12 and 14 mJ/s respectively.

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DESIGN DISCHARGES OF THE CANALS BY RATIONAL METHOD (2/2) Table C.6.10

9

Urannago	Catchment	ž				LUNDIN F	"	Kunoff	MOILS LIGHT SAV	, ,		1.0	Calification Internance			
Area Area	א פ	Area (km2)	Q	Name	([m2)	D Are (ma)	-	Coefficient	(km) (m/s)	Vatocity (m/s)	Concentration (minutes)	S-Yr. K.P. 1 (mm/hr)	5-Yr. K.P. 1 10-Yr. K.P. (mm/hr) (mm/hr)	Reduction Factor	5-Yr. R.P. (m3/s)	(m3/s) (m3/s)
┢		-				 < 12 	2.68	0.57	2.54	040	137	8.14	7.64		181	
		<u>.</u>	C-N.I Kach the Lao			101.2	6,1	0.53	2.51	9 0	242	23.7			ิล	
8	S.1	14.33				S.1.82	4.38	0.5	4.6	040	217	26.3	28.7	0.99	17	
		<u>ر</u>				1.83	6,33	0.52	87	0.40	303	0'61			17	
•• ••		Ŭ	C-S.I Kuch Ballao	·····	14.30	S.LC	14.33	0.52	61.1	0.40	a c	16.9:			34	
L		ľ	L	Lev Kiko	13.70 S.2.AI	2 1	4	0.48	202	0,40	158	36.6	40.6		12:	
			Kach One		8	52.25	8	50	8	0.40	150	36.4	42.9		12-	
	225	2.8 8.9				2.0	7.21	0.52	13	940	218	262	28.6	860	8	
		<u>ں</u>	C-S.3 Reach Ong Lon - Kinh Cay Kho	Carly KCro	19. EI	210	15.66	639	- I	040	359	16.2	17.6		8	
L UJ		ľ				5. A	2.17	0.71	1.57	0.40	121	40.1		W.0	20	ľ
		ي	C-Sco Kech Kor-Kech Tom+:	Kech Tom + Song Muong Chuoi		19.0.5	84	E S	5	940	ĥ	5.5		8	2	204 1 1 1
		Ċ	C-S.6 RACH They Ties		1 × 1	S 3. B2	24	1420	10	0.00	3	0.0		18.0		1
			Ī.		5 75 2 3 83	1 83	- 22 -	0.56	35	040	20	10.7			1.1	
	S.	 			530	10	10.33	0.65	56	940	100	19.61	18.9	i.	-25	
		<u>0</u>	C-S.5 Kach Roi - Kach Tom - 1	Kach Tom - Song Muang Chuoi	, A	S 3 DI	23.68	0.65	2.63	04.0	242	133	14.5	i	52	°
		<u> </u>	C.S.S. Phune Khim River	and a second second second second second second second second second second second second second second second	6.45	53.02	6.45	7	14	9	259	222	24.1	80	211	
	-	Ċ	Rach Roi - Rach Tom -	Sone Muone Chuoi	34.51 5.3.2	3.6	34.51	0.63	1	040	3		12.1	1	2	ð
[<i>X</i>		236 C S 9	Rach Cwu Kinh		· 2.36 S.4.A		2.36	0.67	- 55.7	940	101	41.1	48.2	3	5	
12		2 23 C-S 10	(Kach AP3		2 23 N.5 A	5 A	2.23	990	- 93	9	116	48.5	543	1	8	
Г	╞	1 12 CAF	Kach One		3.3215	3.32 NE LA	3.32	0.57	. 85°E	0.40	170	34.0	37.9		18	
	ł					NEZA	4 78	0.68	2.57	0.0	12	33.61	37.4	86.0	g	
	NE2 9	9,43 C.NE.2	NE.2 Rech Co Due		. 6 .	NE.2.B	0.5	590	520	9	264	-217	23.7	6.0	9	
	C NN	110	VEA Rech Thu Due		1212	7.15 NE 3.A	Ĩ.	190	4 .	940	3	35.8	A.S.	80	1	
	1		2 64 C.NEA Rech Towns Tho		2 65 1	2 65 NE 4.A	265	120	217 :	9	[4]	40.2	2.14	0.00	7	
	L	+	6		-	NESAL	101	0.42	- 56.6	2.33	3	0.0	4 23	64.0	3	S
						NE.5.A2	4	0.46	121	2.80	62	00	89.2	8.0	4	8
	NE.5 DA	34.38 C-NE.5	Kach Nhu	m - Kach Cau - Kach Go Cong	34.38	E.B	8	\$ 1 0	8	7	85	63.2	1.0	30	.8	2
10					<u>.</u>	ES.C	28.17	0.45	26	6.7	*		1	8	12	6 <u></u>
					<u></u>	NE.S.DI	34.3%	045	Į	5.0	378	15.4	16 8	80	133	₹ <u>₹</u>
ž	┞	10	SK. 1 - Kech Binh Khanh		3, 1	SELA 1	<u>3</u> -	80	2.32	0	12	544	0.05	0.10	12	
12	24.2	2.60 C SE 2	Rech Co T		0.0	NE 2.A	2 60	0.65	101	9	1817	48.1	18.CS	30	8	
13	-	1.v2/C-SE 3	Kach Da		1.92 %	SE3.A	1.92	0.80	- 06.4	0.40	205	27.4	30.5	\$	2	
Ľ		5			1	SEA.	5.40	0,43	5.41	0.40	8	28.6	6.15	84:0	:81	
7	NE.4	7.80 C-SEA	SEA NACE CLORE ONE TO		N De /	NE 4.B	3	4	2.05	9	582	202	51.9	440	2	
18	L	3.8J C-SE.5	SE.5 Rach Muong		3.83 SES.A	ESA	183.5	0.65	-	040	121	33,61	37.3	3	ສ	
17	SE 6	0			S 01 S	SEAA	0	080		9 0	263	21.4	23.7	8 0	72	
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ň	20.0			Lay - Kach Die Unit - Kach Ong Men		SEXB	1.33	0.53	4	0.40	336	17.2	18.8	0.96	27.	
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	-					NE9C	21.11	0.56	2.83	0.40	442	13.3	14.6	40	-15	
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ŝ	SE.10 24	24,88 C-SE.11	SE.11 Tao Ruver		597.65	SE.IO.B	19.00	0.52	4.08	80	\$15	13.51	14.7	30	35	3.5
		-			1						100	5				

• Canal improvement plan for Yach Go Cong has been proposed considering construction of on-site storing to pool to reduce peak runoff due to mpid urbanization such that discharges under existing landure condition can be kept. The design discharges along Reach Go Cong shown in this table represent discharges under existing landure condition.

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RESULTS OF HYDRODYNAMIC MODELING (1/2)
Table C.7.2

Availability Domine Type Dimension Synthetic formula Bank (Church) 10 10 Availability Synthetic formula Bank (Church) Bank (Church) Bank (Church) Bank (Church) Bank (Church) Bank (Church) Bank (Church) Control (Church) Bank (Church) Control (Church) <th>Matrix Matrix <th>anal 1</th> <th>Drainaur</th> <th>Carohimeni</th> <th></th> <th>Runoff</th> <th>Design Discharge</th> <th>-</th> <th>Proposed</th> <th></th> <th>Secnario 1: Constant Water Level Boundary Condition</th> <th>Constant</th> <th>Vater L</th> <th>evel Bour</th> <th>ndary Cor</th> <th>dition</th> <th>-</th> <th>NC NC</th> <th>charlo 2: 1</th> <th>Dynamic Dynamic</th> <th>Water</th> <th>CVCI DOL</th> <th>Scenario 2: Dynamic Water Level Boundary Condition</th> <th>ngition</th> <th></th>	Matrix Matrix<	anal 1	Drainaur	Carohimeni		Runoff	Design Discharge	-	Proposed		Secnario 1: Constant Water Level Boundary Condition	Constant	Vater L	evel Bour	ndary Cor	dition	-	NC NC	charlo 2: 1	Dynamic Dynamic	Water	CVCI DOL	Scenario 2: Dynamic Water Level Boundary Condition	ngition	
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וח דוצ. ליטי שחם אוככ עכוא Note: A +ve discharge indicates flow direction from PID simulation is the same as assumed flow direction, as show A -we free board at point W.J.B represents depth of inundation along the flod plain of Kinh Chua. The discharges at runoff points NE.5.B. NE.5.C. NE.5.D1 and SE.10.C are for existing landuse condition. The shaded portion represents designed condition.

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Level Boundary Condition	10-Year Return Period	. Free Board Discharge (m3/s)	m) (m) + +	0.46	55 izeo	4	0.42	0.40. 213	0.50 57	9	0.47 38	0.401 111	0.55	0.53 39	0.53 43	0.53 103	0.49	0.45 240	0.451 79	0.40	6.03	0.50	140	0.54	0,481 45	0.55 77	0.55 169	0.51 27		0.48	0,44 48	10+0	46 0.48 275 150
Scenario 2: Dynamic Water Level B	5-Year Return Period	W.L. Free Board Discharge (m3/s)] (EL	0.461 18 -27	1.39 0.42 55 - 35	1.38 0.46 22	1 39 0.42 40 59	1 39 0.40 210 -125	76.1	1.37 0.50 0.10	1,32 0,471 37 99 1	1 29 0.40 109 -173	0.55 13 -17 3	0.53	42 -55	1.38 0.53 102 -181	1.38 0.491 188 -3.36	1.38 0.451 2.38 -426	1,35	1.19 0.40 383 -651	1.56 0.55 1.4	1.4% 0.50 121	1.47 0.43 132 -153 1		1.39 0.48 48 73	77 35	- 0.55 16k -136 1	1 44 0.51 238	1.47 0.40 21 31	1.48 0.48 35 - 7	1.47 0.44	. 47 0.40 106 -142	1.45 0.481 204
Level Boundary Condition	10-Year Return Period	W.L. Free Board Discharge (m3/s)	(m) (m)		_		1.391 0.42 9 -21	0.40 26		1.39. 0.48 1 - 8	1.39. 0.451 +74		2	1,411 0.51 26			1.40 0.47 -103	0.44		1.39 0.40 0.41	0.43 127	0.40 162	1.48 0.42 7.0	0.531	0.4N 11	0.54	1.32 0.55 126	0.49	1.47 0.40 6 -22	0.48 35	40	040	**
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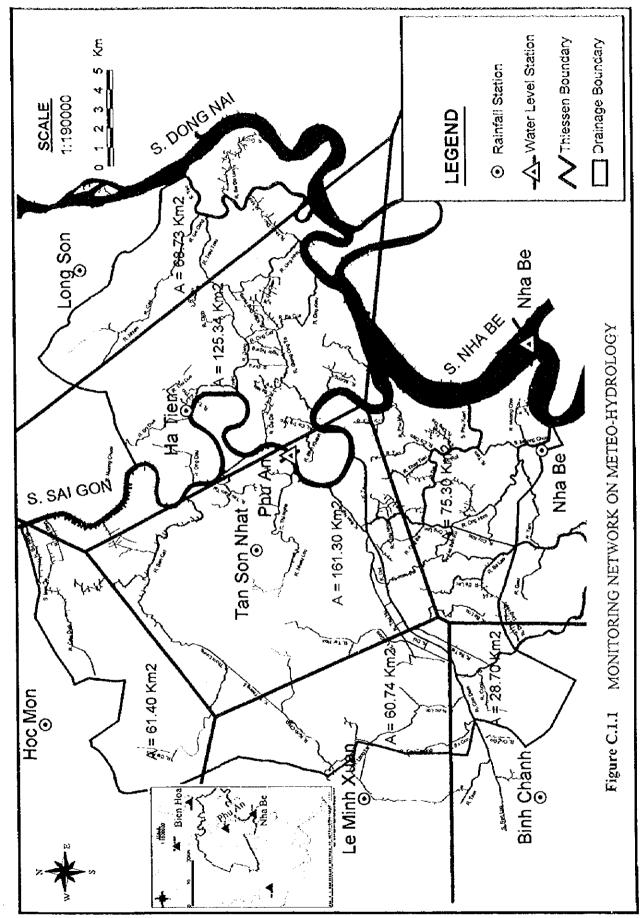
RESULTS OF HYDRODYNAMIC MODELING (2/2) Table C.7.2

Note: A +ve discharge indicates flow direction from HD simulation is the same as assumed flow direction, as shown in Fig. C.37 and vice versa. A -ve free board at point W.1.B represents depth of inundation along the flod plain of Kinh Chua. The discharges at runoff points NE.5.B, NE.5.C, NE.5.D1 and SE.10.C are for existing landuse condition. The shaded portion represents designed condition.

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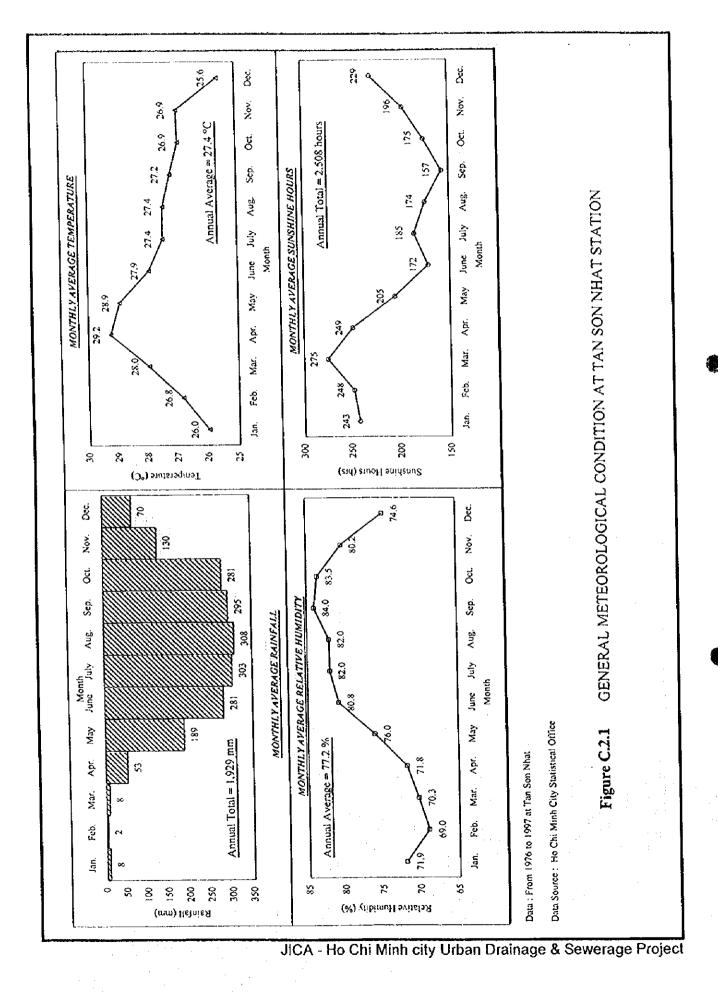
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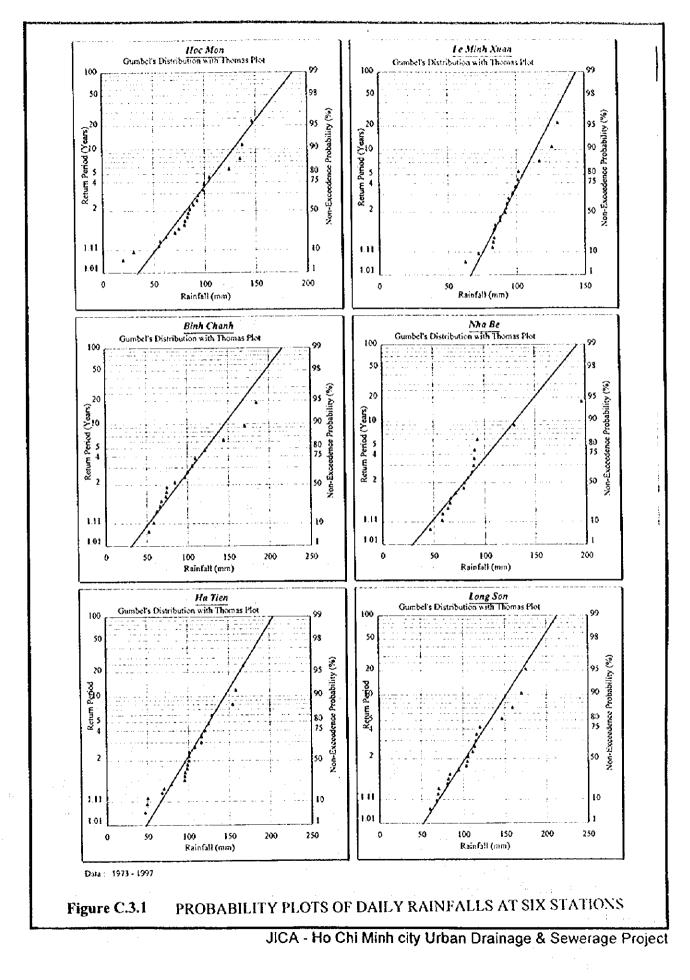
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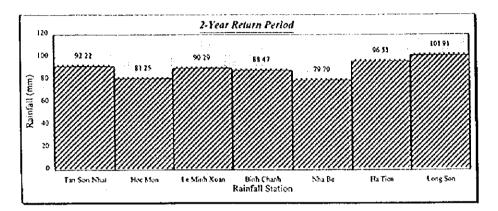
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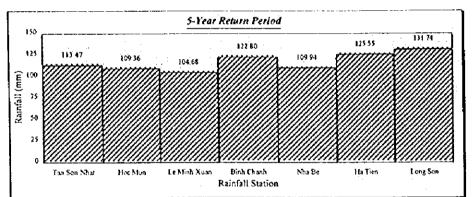
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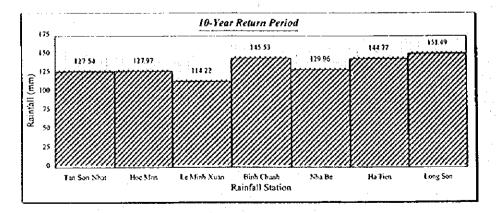


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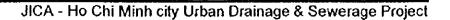
Probable Rainfalls : Calculated applying Gumbel's distribution method Basin Mean : Estimated applying Thiesen Polygon method Duta : 1552 - 1997 for Tan Son Nhat and 1993 - 1997 for other stations

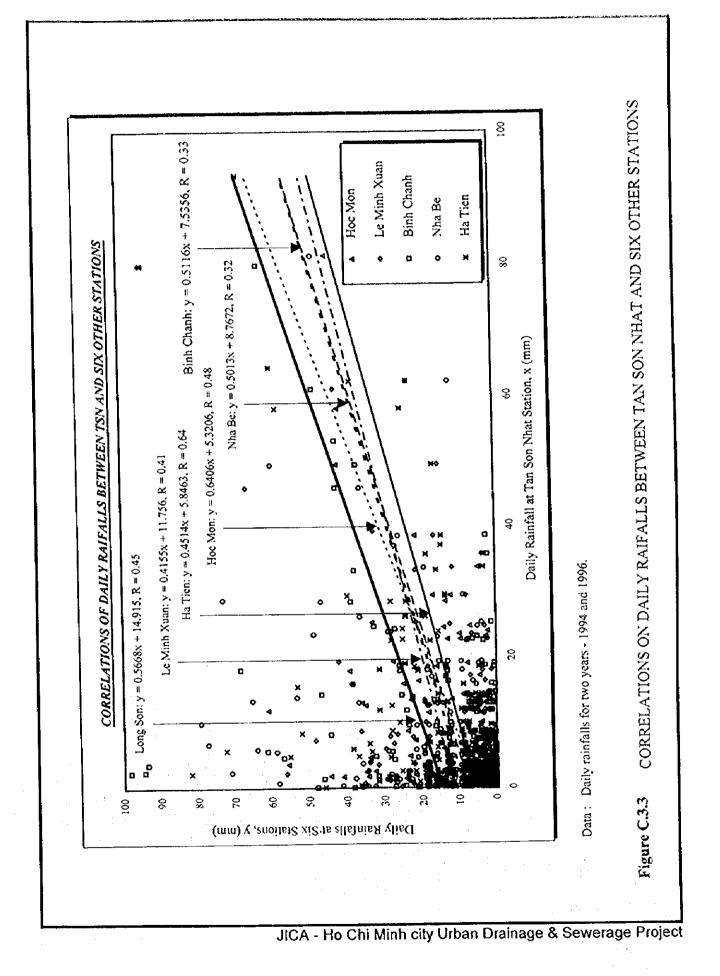


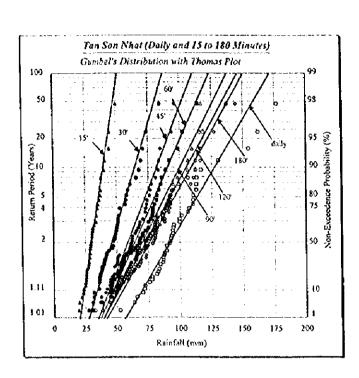




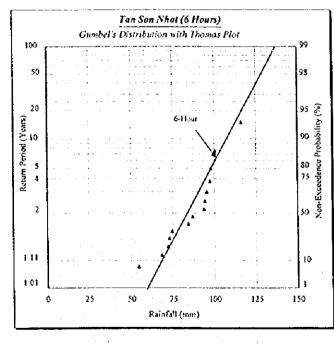
PROBABLE MAXIMUM DAILY RAINFALLS Figure C.3.2







Data : 1952 - 1997 = 46 years



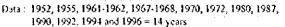
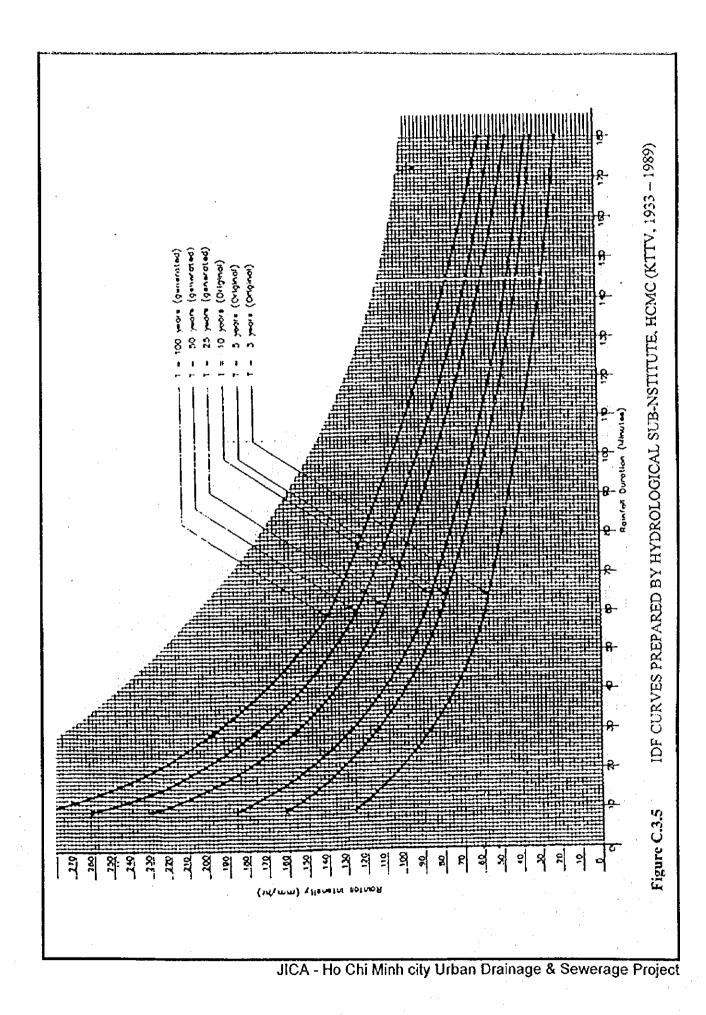


Figure C.3.4 PROBABILITY PLOTS OF MAXIMUM RAINFALLS AT TAN SON NHAT

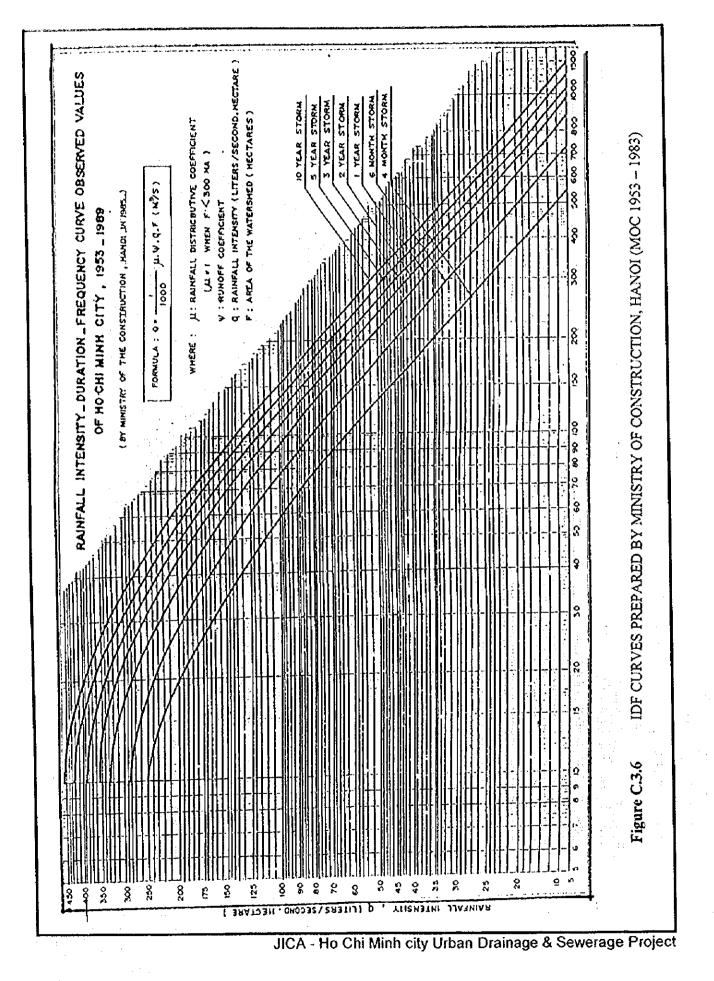


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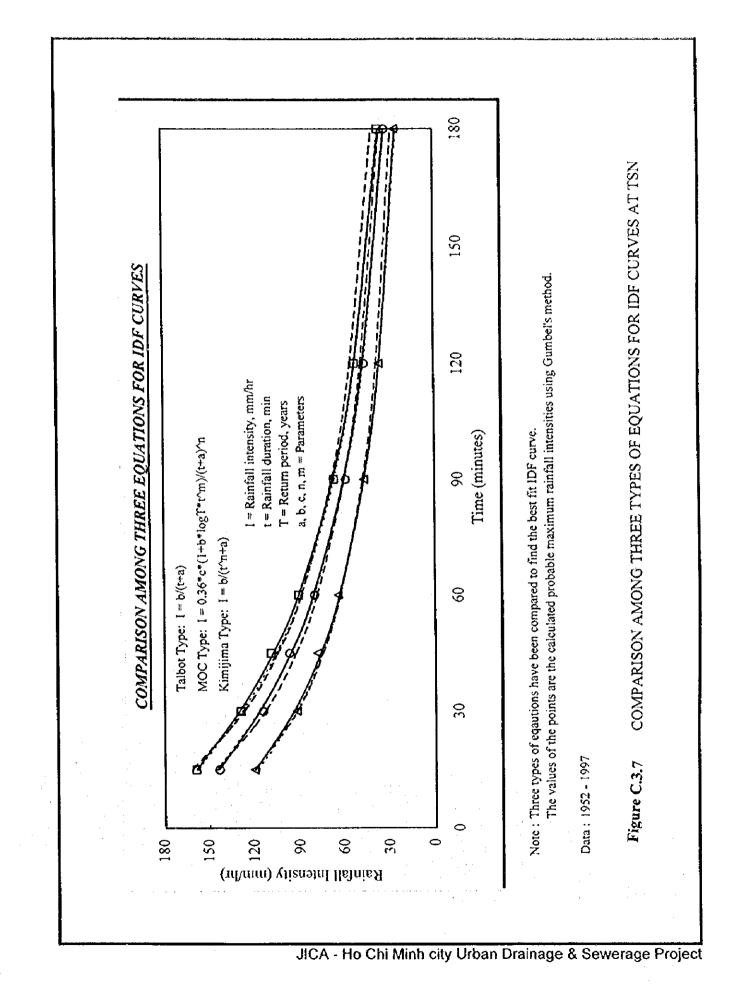


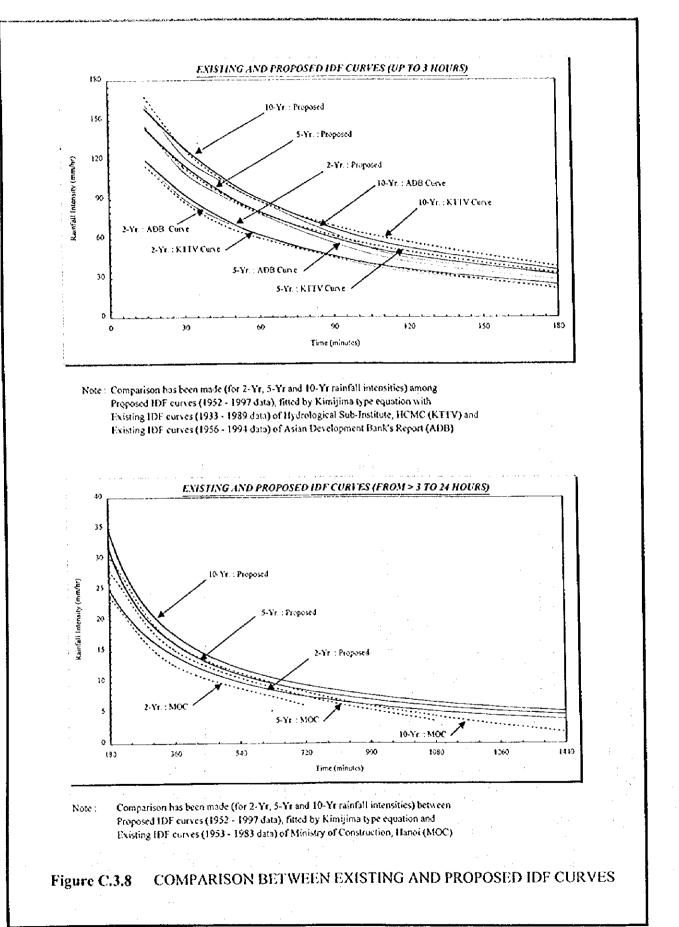
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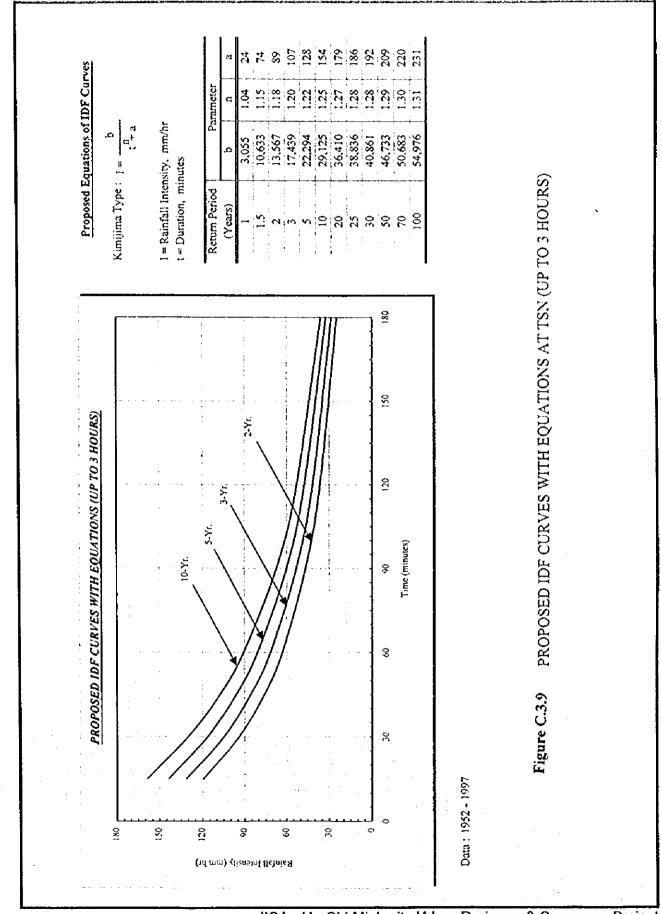


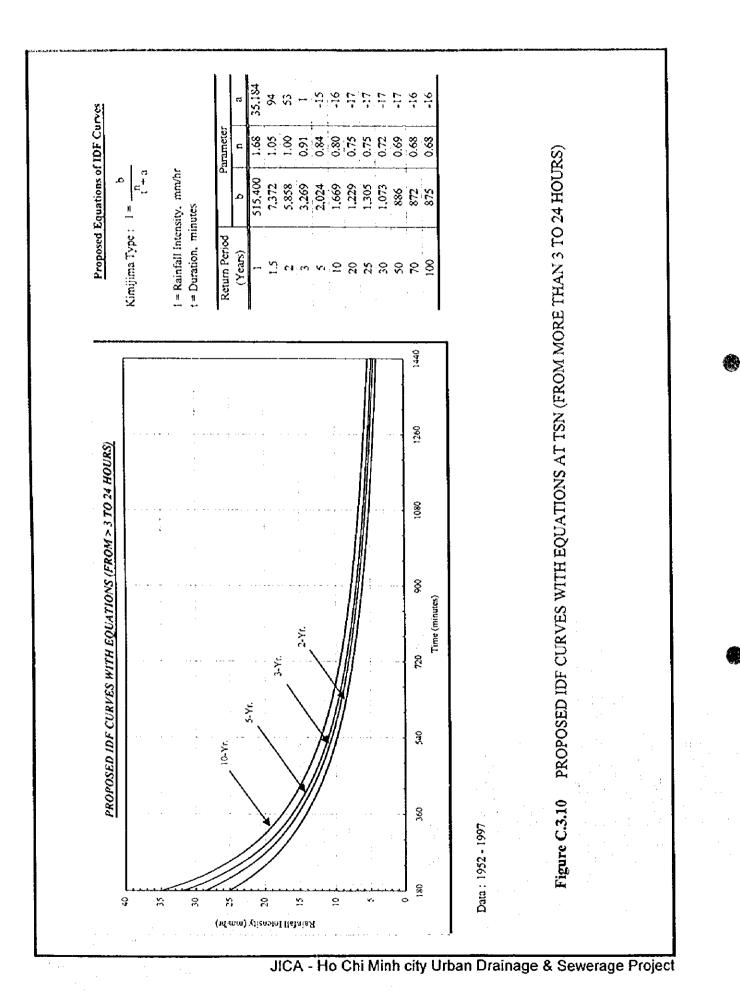


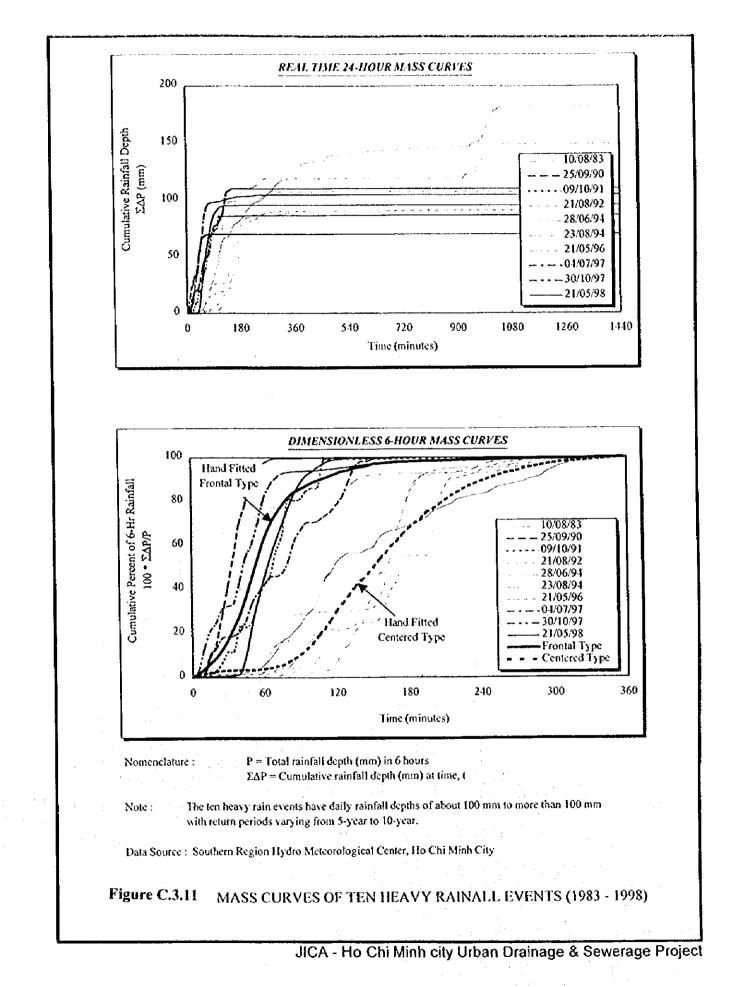


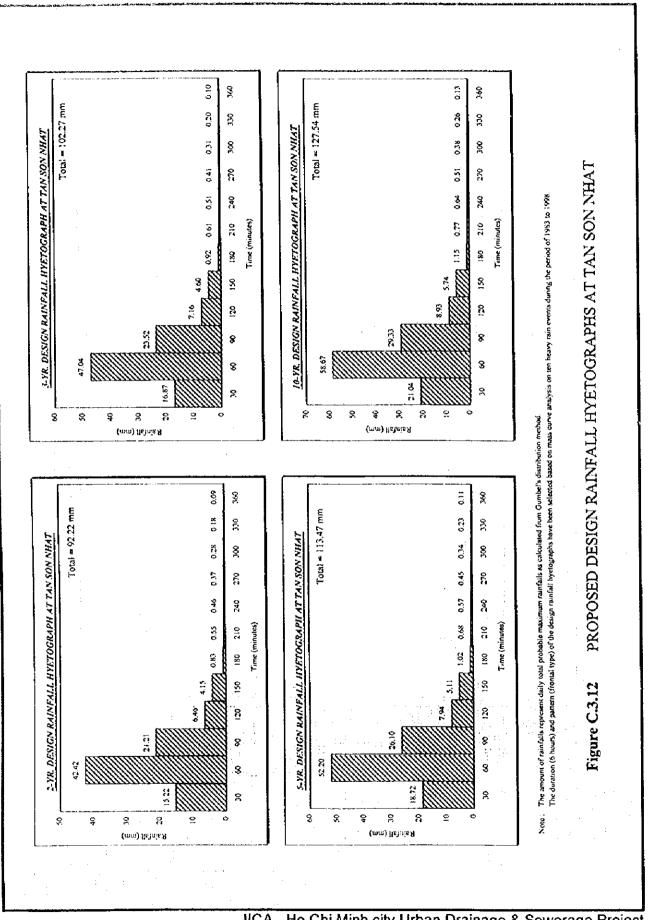




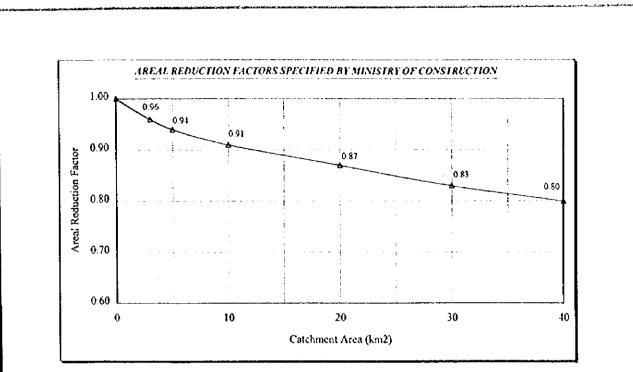




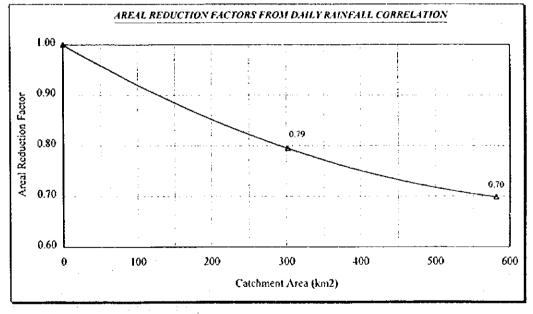




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Note : Ministry of Construction (MOC) only specifies the values, not the smooth line.

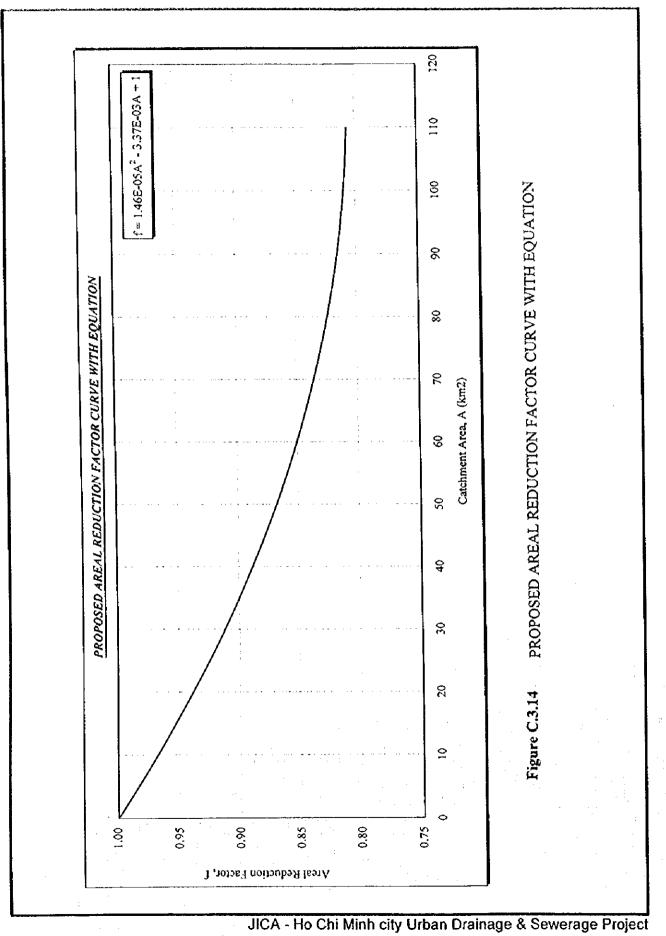


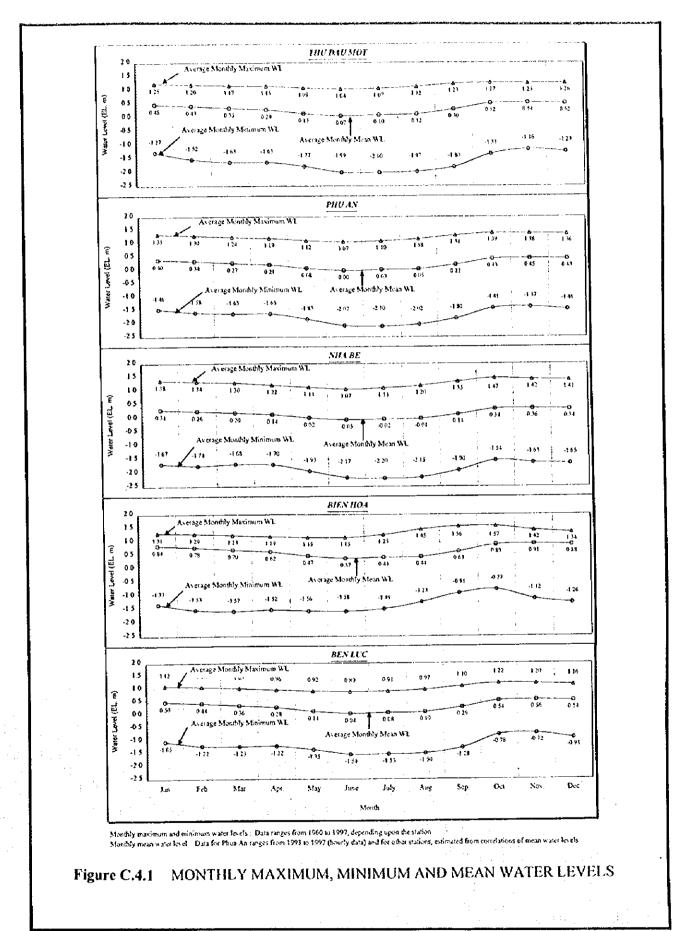
Note 1

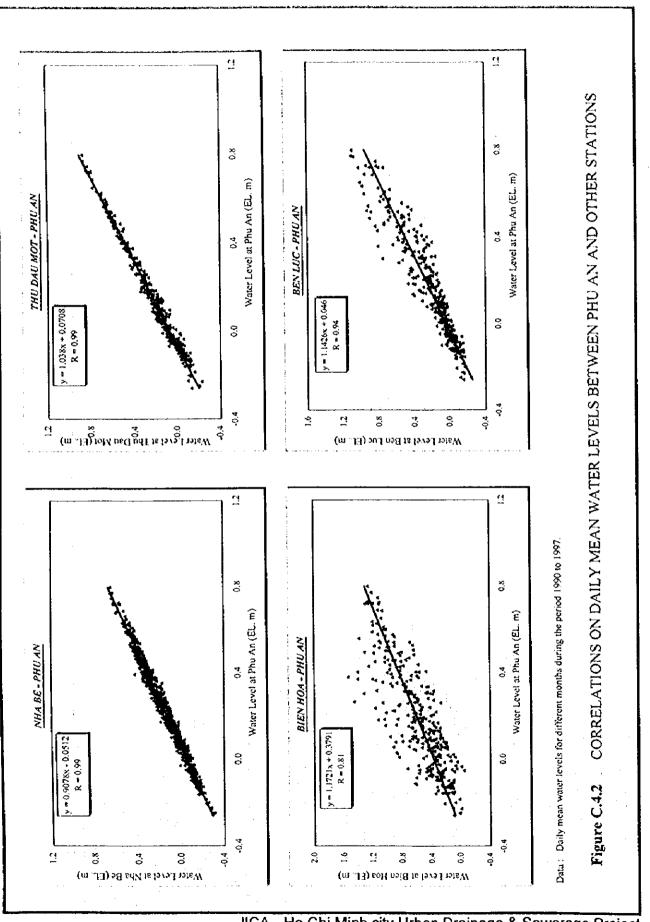
Investgated by the JICA Study Team using Thiessen Polygons of seven stations and

daily rainfall conclutions between Tan Son Nhat and other six stations based on 1994 & 1996 rainfall data

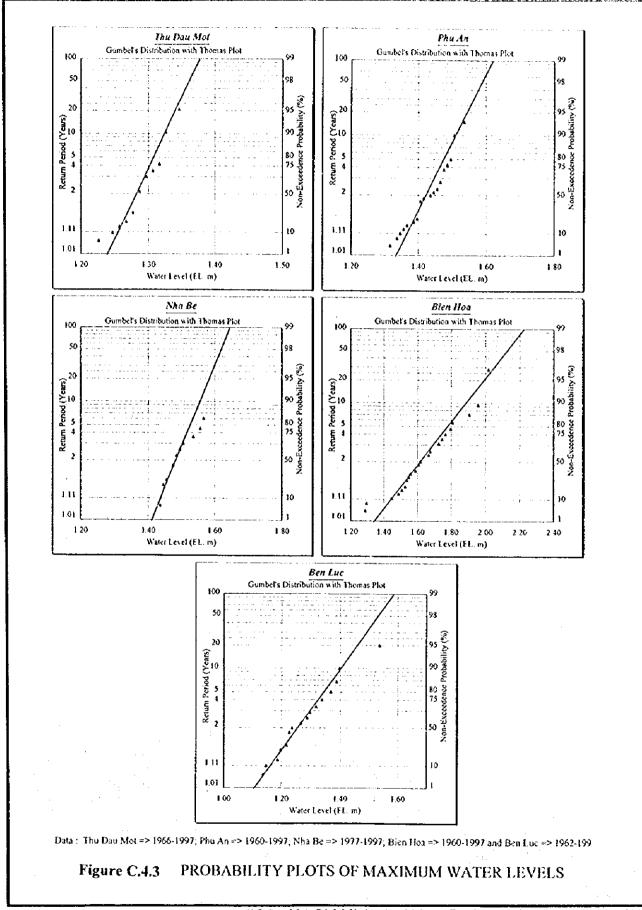
Figure C.3.13 AREAL REDUCTION FACTORS SPECIFIED BY MOC AND CALCULATED FROM DAILY RAINFALL CORRELATIONS BY JICA

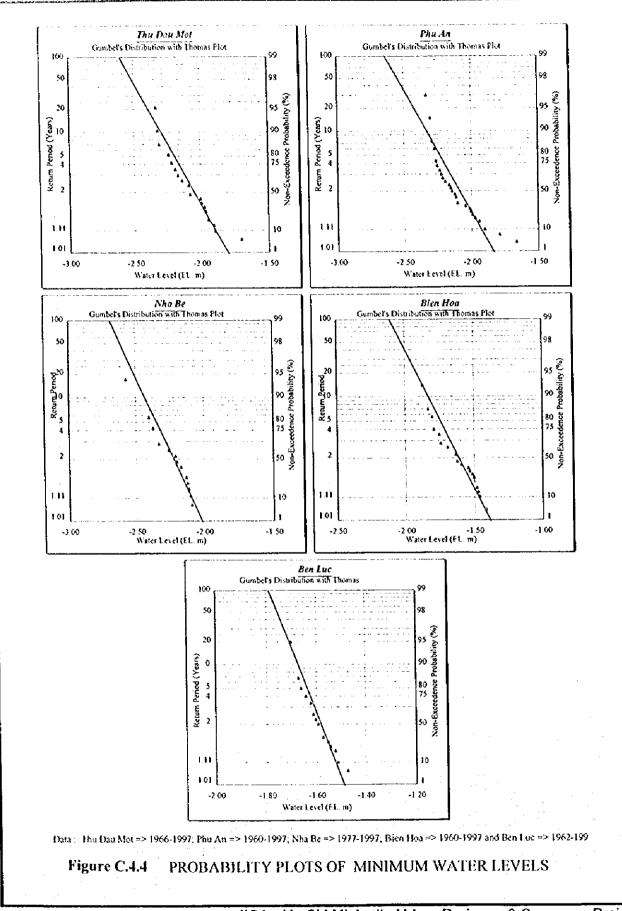


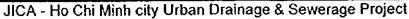


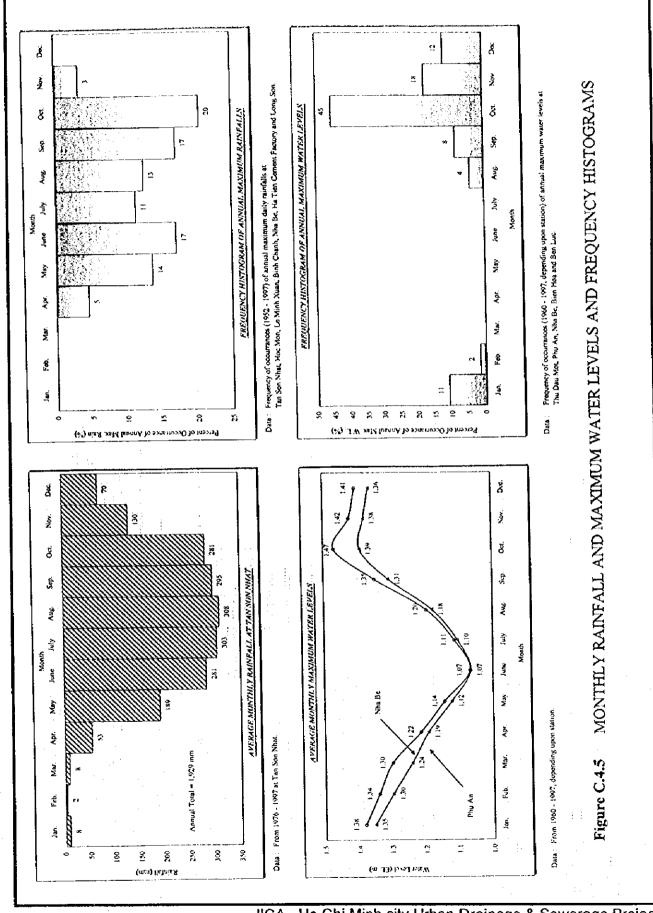




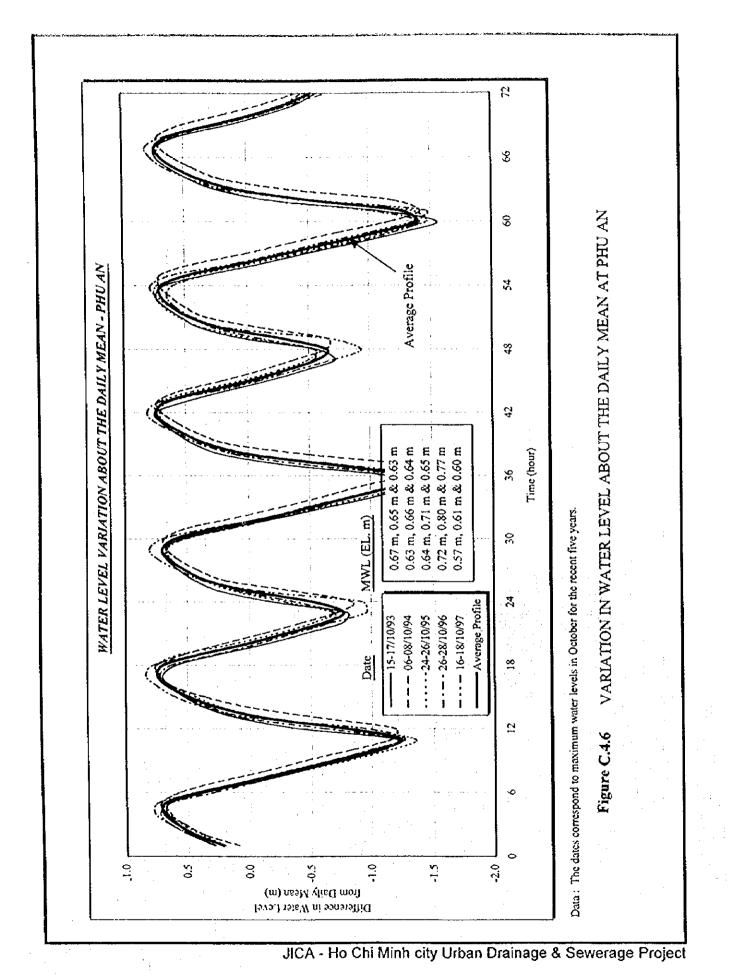






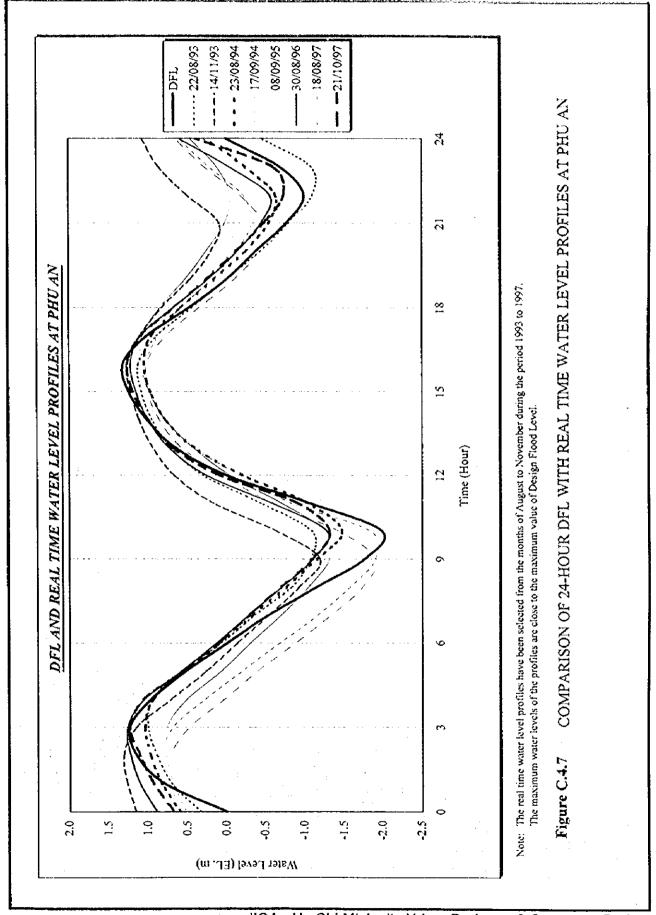


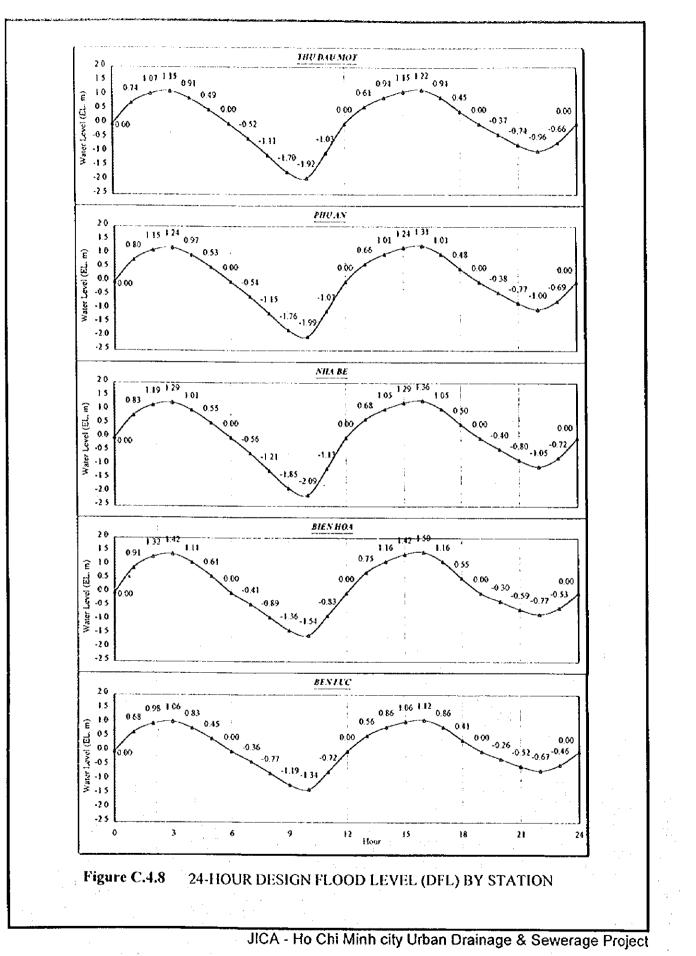
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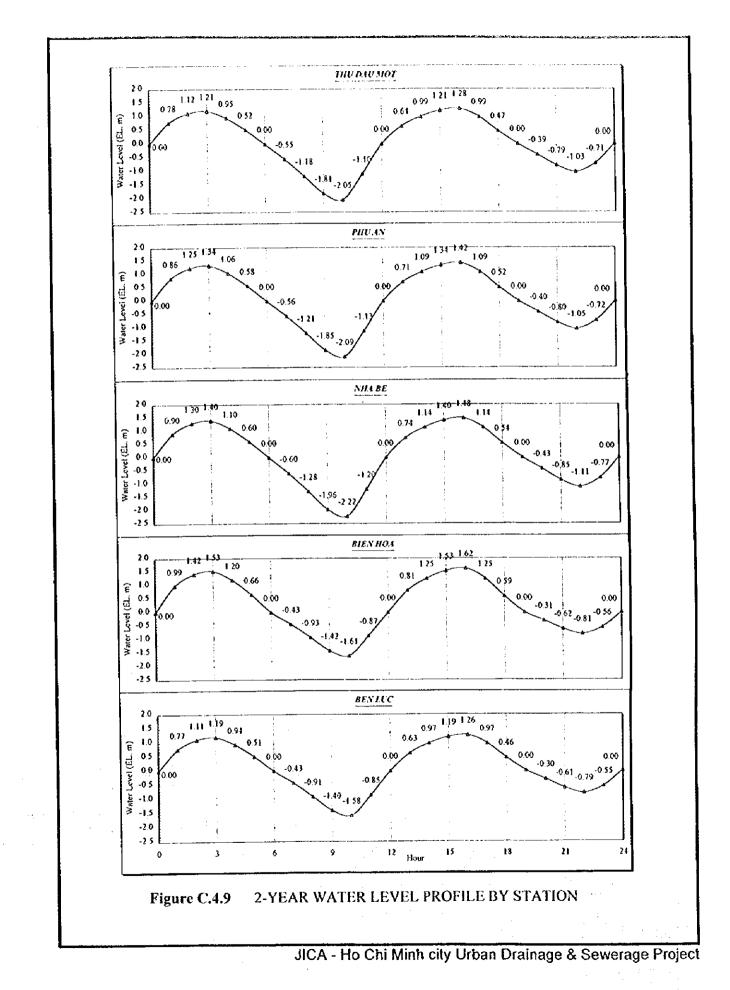




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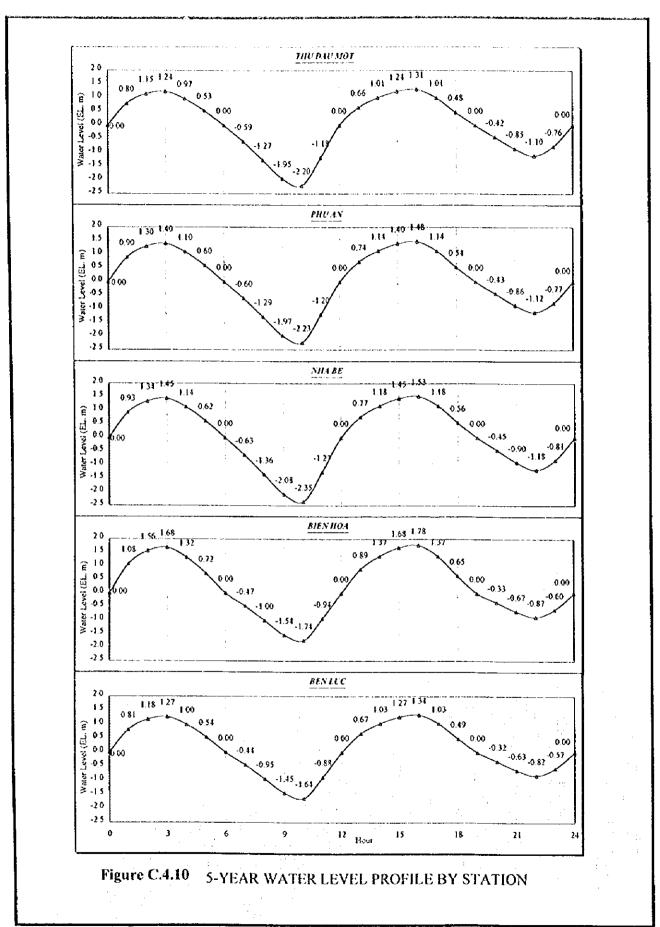
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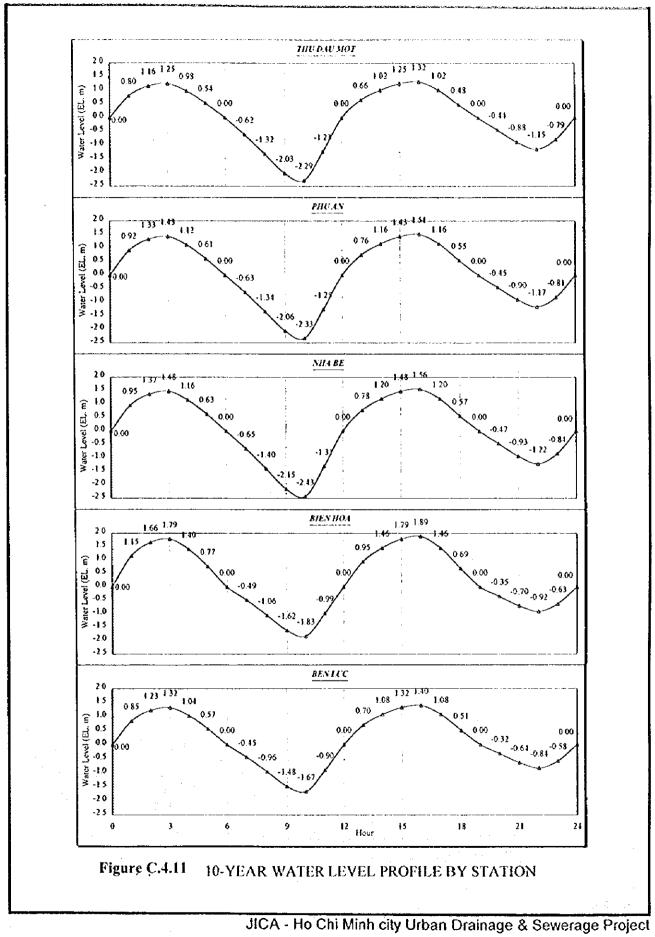


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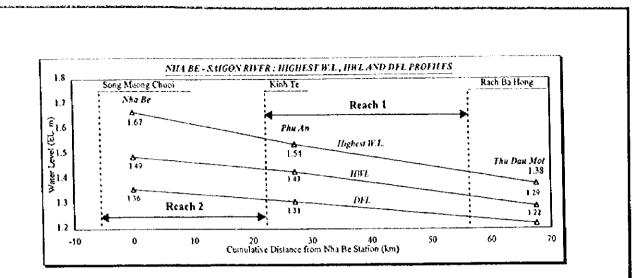
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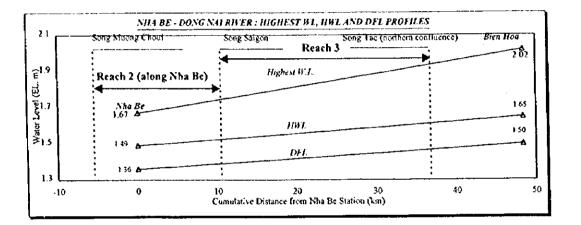
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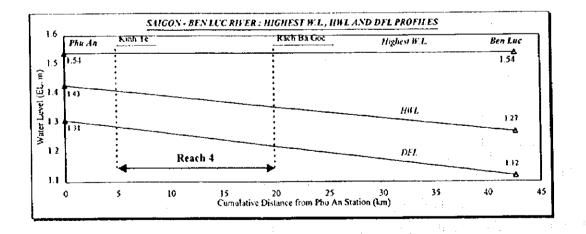


Figure C.4.12 LONGITUDINAL WATER LEVEL PROFILES

