

11.2.2 Kok-Ing Diversion Canal

(1) Design concept and Criteria

(a) Hydraulic condition

Basic hydraulic design dimensions and formula are follows.

Basic design dimension

Maximum design discharge Kok-Ing diversion canal	140 cu.m/s
Kok intake water level	NWL388.00 m M.S.L
Outlet water level of Ing river	NWL 363.500 m M.S.L

Hydraulic formula

Manning's formula is applied in canals

Flow condition Uniform flow

$$\text{Manning's formula } Q = A \times V \times R^{2/3} \times S^{1/2} / n$$

Where Q; Discharge (cu.m/s)

V; Velocity (m/s)

A; Flow area (sq.m.)

R; Hydraulic Radius $R = A/P$ (m)

S; Gradient of canal bed

n; Coefficient of roughness in open canal of concrete canal lining $n=0.016$
culvert, siphon and tunnel $n=0.015$

Siphon loss

Siphon loss consists of friction loss, inlet transition loss, outlet transition loss and trash rack loss.

$$h_f = (nV / R^{2/3})^2 \times L + (f_i + f_o + f_t) \times V^2 / 2g$$

Maximum flow velocity

Earth lining canal (in case of clay) $V_{max}=1.00$ m/s

Concrete lining canal ($t < 10$ cm) $V_{max}=1.80$ m/s (USBR standard)

($t > 18$ cm) $V_{max}=3.00$ m/s

R.C canal & R.C pipe

$V_{max}=3.00$ m/s

Froude number

$F_d < 0.7$

Free board

Concrete lining canal $F_b > 0.05d + h_c + (0.05 \dots 0.15)$ m

Culvert, tunnel $d/r = 1.60$ (Circular and horse shoe type)

d : Water depth (m)

Mean Hydraulic Gradient

As hydraulic mean gradients of Kok-Ing diversion canal are supposed as follows.

Hydraulic heads is appropriately enough for canal design.

Kok diversion canal Head = $388.00 - 363.50 - (\text{Intake loss} + 4 \text{ siphon losses}) = 20$ m

Gradient slope = $20 / 54,500 = 1 / 2,700$

Composition of bed gradient

Kok-Ing diversion canal consists of about 39 km open canal, 7 km culvert and 8.5 km tunnel. Mean gradient of Kok-Ing diversion canal would be designed less than 1/2,700. Hydraulic gradient and water head in each case is shown in Table 11.2.2(1)-3. Hydraulic energy in following cases is enough. Gradient would be decided topographic condition, velocity and cost into conditions.

Table 11.2.2 (1)-3 Hydraulic Gradient and Water Head in each Cases

Canal	Length (m)	Case-1		Case-2		Case-3	
		Gradient	Head(m)	Gradient	Head(m)	Gradient	Head(m)
Open canal	39,000	1/3,000	13.00	1/5,000	7.80	1/10,000	3.90
Culvert	7,000	1/3,000	2.30	1/2,500	2.80	1/2,000	3.50
Tunnel	8,500	1/3,000	2.85	1/2,500	3.40	1/2,000	4.25
Total	54,500		18.15		14.20		11.65

(b) Open Canal

Canal Type and Lining

The purpose of Diversion canal is to be safely and speedily to convey the diverted water to Ing river. Canal velocity is requested more than 1.0 m/s based on the hydraulic energy and lining is also requested to protect the canal erosion and to maintenance of canal. Open canal type would be applied for trapezoid concrete lining type by the reason of widespread in Thailand, with technical, economical and constructional experience.

Lined open canals are classified into three types with, which is shown in Table 11.2.2 (1)-2. Though trapezoid concrete lining type requires much spoils bank volume and land acquisition area, construction cost is low.

Table 11.2.2 (1)-4 Land Acquisition Width and Excavation Volume in Open Canal Types

(In case of Q=140 cu.m/s, S=1/5,000, Water depth D=3.85m and excavation depth H=9.55m)

Canal type	Lining	Side slope	Width sq.m/m	Excavation Volume cu./m	Cost
Trapezoid type	Placing thin concrete	1:1.5 (2.0)	70	315	Low
Trapezoid type	Pre-cast concrete block	1:0.5 (1.0)	65	290	Medium
Rectangular type	Reinforced concrete	1:0.0	65	310	More

Longitudinal gradient of canal slope

Relating with canal velocity and cross section, canal section with steep slope shows high velocity in small section and increases the excavation depth. Canal longitudinal slope would be generally decided taking followings into consideration.

- Purpose of canal and lining condition

- Required water level at turn out
- Total energy and arrangement of canal type
- Topographical condition
- Balance of earthwork volume (Excavation and filling volume)
- Hydraulic most effective cross section, Allowable velocity

This diversion canal is excavated type under the ground, and has no turnouts except for associated project. Longitudinal slope is decided as $S=1/5,000$ in open canal and $S=1/2,500$ in culvert and tunnel taking hydraulic conditions including total energy from Kok to Ing river into consideration. The canal dimensions are shown in Table 11.2.2 (1)-4.

Longitudinal gradients and velocity in open canal is shown in Table 11.2.2 (1)-5 and detail is shown in 11.2.2 (1)-8.

Table 11.2.2 (1)-5 Longitudinal Gradients and Velocity in Open Canal

Gradient	$d = 3.00m$		$d = 3.50m$		$d = 3.85m$		Remarks
	W(m)	V(m/s)	W(m)	V(m/s)	W(m)	V(m/s)	
I/3,000	18.60	2.02	13.70	2.11	11.10	2.16	
1/5,000	24.50	1.61	18.40	1.70	15.00	1.74	$V_{max} < 1.8$
I/7,000	29.30	1.39	22.00	1.47	18.40	1.51	
1/10,000	35.20	1.18	26.70	1.25	23.30	1.30	$H < 23 \text{ m}$

Where: Water depth (m) W: Bottom width V: Velocity (m/s)

Free board

Free board (Fb) and lining height (Hc) of canal would be employed 0.70m and 4.50 m, respectively. In case of flood or miss operation of gates, discharge of 189 cu.m/s, which is 1.35 times of design capacity, can flow with in free board.

(c) Culvert

Culvert Section

The culvert covered by backfill is used for deep excavation portion, which excavation depth is over 15 meter. Culver canal type would be applied for concrete horseshoe type reinforced by steel bar taking earth/hydraulic pressure and economical conditions into consideration. Culver canal is generally classified as Table 11.2.2 (1)-6.

Table 11.2.2 (1)-6 Land Acquisition Width and Excavation Volume in Culvert Types

In case of $Q=140 \text{ cu.m/s}$, $S=1/2,500$ and water surface 15m under ground level

Canal type (Reinforced concrete)	Water Depth	Size $H*B*rows$	Excavation Width	Excavation Volume	Cost
Rectangular type	3.85 m	$4.55*3.85*6$	72 m	790 cu.m	High
Circular type	7.20 m	$D=9.00 \text{ m}$	57 m	640 cu.m	Medium
Horse shoe type	7.00 m	$D=8.70 \text{ m}$	56 m	620 cu.m	Medium

Longitudinal gradient of culvert canal

Longitudinal gradient of culvert is designed with more rapidly velocity than open canal to reduce cross section. Longitudinal slope of culvert is decided as $S=1/2,500$ taking hydraulic conditions including total energy from Kok to Ing river into consideration.

Longitudinal Gradients and Velocity in culvert is shown in Table 11.2.2 (1)-7 and detail calculations are shown in Table 11.2.2 (1)-9 and 10.

Table 11.2.2 (1)-7 Longitudinal Gradients and Velocity in Culvert

Gradient	Rectangular		Circular		Horse shoe		Remarks
	W(m)	V(m/s)	D(m)	V(m/s)	D(m)	V(m/s)	
I/2,000	21.40	1.70	8.60	2.83	8.40	2.80	
I/2,500	23.10	1.57	9.00	2.61	8.70	2.57	
I/5,000	32.10	1.13	10.20	2.01	10.00	1.99	

Where D: Diameter (m) W: Bottom width V: Velocity (m/s) Culvert cross section

Culvert section with diameter 8.70 m and water depth of 7.00 m is selected taking water velocity into consideration. The dimensions of canal section are as follows.

Discharge Q(cu.m/s)	Diameter (m)	Water depth d(m)	Flow area A(sq.m)	Coefficient Roughness n	Longitu Slope	Velocity V(m)	Remarks
140.00	8.70	7.00	54.56	0.015	1/2,500	2.57	

Table 11.2.2(1)-8 Hydraulic Dimension in Open Cnal (Gradient & Section)

Lining	L/S	b m	d m	z	A sqm	P m	R m	n	S	V m/s	Q cum/s	Hc m	Remarks
KOK-ING	Q=140 cum/s												
Conc.Lining	1/5000	15.00	3.850	1.50	79.98	28.88	2.77	0.016	0.00020	1.743	140.0	4.55	
Culvert	1/2500	8.70 (2r)	7.000	-	54.30	41.59	1.31	0.015	0.00040	2.564	140.0	8.70	
ING-YOT	Q=175 cum/s												
Conc.Lining	1/5000	20.00	3.795	1.50	97.50	33.68	2.89	0.016	0.00020	1.80	175.0	4.55	
Culvert	1/2500	9.50	7.500	-	63.99	21.98	2.91	0.015	0.00040	2.72	173.9	9.50	

Lining	L/S	b m	d m	z	A sqm	P m	R m	n	S	V m/s	Q cum/s	Hc m	Remarks
KOK-ING	Q=140m ³ /s												
Conc.Lining	1/3000	11.10	3.85	1.50	64.97	24.98	2.60	0.016	0.00033	2.16	140.20		
	1/5000	15.00	3.85	1.50	79.98	28.88	2.77	0.016	0.00020	1.74	139.42		
	1/7000	18.40	3.85	1.50	93.07	32.28	2.88	0.016	0.00014	1.51	140.85		
	1/10000	22.30	3.85	1.50	108.09	36.18	2.99	0.016	0.00010	1.30	140.13		
	1/3000	13.70	3.50	1.50	66.33	26.32	2.52	0.016	0.00033	2.11	140.15		
	1/5000	18.40	3.50	1.50	82.78	31.02	2.67	0.016	0.00020	1.70	140.76		
	1/7000	22.00	3.50	1.50	95.38	34.62	2.75	0.016	0.00014	1.47	140.02		
	1/10000	26.70	3.50	1.50	111.83	39.32	2.84	0.016	0.00010	1.25	140.29		
	1/3000	18.00	3.00	1.50	67.50	28.82	2.34	0.016	0.00033	2.01	135.85		
	1/5000	24.50	3.00	1.50	87.00	35.32	2.46	0.016	0.00020	1.61	140.26		
	1/7000	29.30	3.00	1.50	101.40	40.12	2.53	0.016	0.00014	1.39	140.55		
	1/10000	35.20	3.00	1.50	119.10	46.02	2.59	0.016	0.00010	1.18	140.32		

Lining	L/S	b m	d m	z	A sqm	P m	R m	n	S	V m/s	Q cum/s	Hc m	Remarks
ING-YOT	Q=175m ³ /s												
Conc.Lining	1/3000	15.00	3.795	1.50	78.53	28.68	2.74	0.016	0.00033	2.23	175.37		
	1/5000	20.00	3.795	1.50	97.50	33.68	2.89	0.016	0.00020	1.80	175.05		
	1/7000	24.10	3.795	1.50	113.06	37.78	2.99	0.016	0.00014	1.55	175.39		
	1/10000	29.20	3.795	1.50	132.42	42.88	3.09	0.016	0.00010	1.33	175.49		
	1/3000	17.70	3.50	1.50	80.33	30.32	2.65	0.016	0.00033	2.18	175.49		
	1/5000	23.40	3.50	1.50	100.28	36.02	2.78	0.016	0.00020	1.75	175.40		
	1/7000	28.00	3.50	1.50	116.38	40.62	2.87	0.016	0.00014	1.51	175.36		
	1/10000	33.88	3.50	1.50	136.96	46.50	2.95	0.016	0.00010	1.28	175.88		
	1/3000	23.70	3.00	1.50	84.60	34.52	2.45	0.016	0.00033	2.07	175.49		
	1/5000	31.00	3.00	1.50	106.50	41.82	2.55	0.016	0.00020	1.65	175.55		
	1/7000	36.80	3.00	1.50	123.90	47.62	2.60	0.016	0.00014	1.41	175.10		
	1/10000	44.20	3.00	1.50	146.10	55.02	2.66	0.016	0.00010	1.20	175.11		

Table 11.2.2 (1)-9 Hydraulic Dimensions in Culvert (Gradient & Section)

1) Hydraulic Section		d/2r=1.60--1.61	d/r=0.80--0.84	V<3.00m/s	Qn/(I^0.5 * r^(8/3))			R	V1	Q	d
d/2r	$\alpha = A/r^2$	P/r	$\beta = R/r$	$\beta^{(1/2)}$	$\beta^{(2/3)}$	$\alpha \beta^{(2/3)}$	I (slope)	r	m/s	m3/s	m
Q=100m ³ /s											
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	100.00	0.015	1/2700	0.000370	3.90
0.82	2.9324	4.7805	0.6134	0.7832	0.7219	2.1170	100.00	0.015	1/2800	0.000357	3.89
0.84	2.9924	4.8871	0.6123	0.7825	0.7211	2.1578	100.00	0.015	1/2900	0.000345	3.89
Q=125m ³ /s											
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	125.00	0.015	1/2900	0.000345	4.29
0.82	2.9324	4.8871	0.6123	0.7825	0.7211	2.1578	125.00	0.015	1/3100	0.000323	4.28
0.84	3.0524	4.9937	0.6112	0.7818	0.7203	2.1986	125.00	0.015	1/3200	0.000313	4.28
Q=140m ³ /s											
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	140.00	0.015	1/2000	0.000500	4.18
0.82	2.9324	4.7805	0.6134	0.7832	0.7219	2.1170	140.00	0.015	1/2100	0.000476	4.18
0.84	2.9924	4.8871	0.6123	0.7825	0.7211	2.1578	140.00	0.015	1/2200	0.000455	4.19
* 0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	140.00	0.015	1/2500	0.000400	4.36
* 0.82	2.9324	4.7805	0.6134	0.7832	0.7219	2.1170	140.00	0.015	1/2600	0.000385	4.36
* 0.84	2.9924	4.8871	0.6123	0.7825	0.7211	2.1578	140.00	0.015	1/2700	0.000455	4.19
Q=160m ³ /s											
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	160.00	0.015	1/2000	0.000526	4.35
0.82	2.9324	4.7805	0.6134	0.7832	0.7219	2.1170	160.00	0.015	1/2000	0.000500	4.36
0.84	2.9924	4.8871	0.6123	0.7825	0.7211	2.1578	160.00	0.015	1/2100	0.000476	4.37
Q=175m ³ /s											
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	175.00	0.015	1/2600	0.000385	4.77
0.82	2.9324	4.7805	0.6134	0.7832	0.7219	2.1170	175.00	0.015	1/2700	0.000370	4.77
0.84	2.9924	4.8871	0.6123	0.7825	0.7211	2.1578	175.00	0.015	1/2900	0.000345	4.80
* 0.84	2.9924	4.8871	0.6123	0.7825	0.7211	2.1578	175.00	0.015	1/2500	0.000400	4.67

Table 11.2.2 (1)-10 Hydraulic Dimensions in Kok-Ing Culvert

$Q=140 \text{ m}^3/\text{s}$

Rectangular type		b m	Section z	P m	n	I (slope)	A sq. m	R m	V m/s	Q cum/s
3.85		21.40 H=4.55 B=3.60*6	0.00	67.60	0.015	1/2000	0.0000500	82.39	1.22	1.70 140.14
3.85		23.10 H=4.55 B=3.85*6	0.00	69.30	0.015	1/2500	0.0000400	88.94	1.28	1.57 140.04
3.85		25.80 H=4.55 B=3.70*7	0.00	79.70	0.015	1/3000	0.0000333	99.33	1.25	1.41 140.02
3.85		32.10 H=4.55 B=4.00*8	0.00	93.70	0.015	1/5000	0.0000200	123.59	1.32	1.13 140.13
		$d/2r=1.60$		$d/r=0.80$		$V < 3.00 \text{ m/s}$		$Qn/(I^{0.5}*r^{(8/3)})$		
Circular type		$d/2r$	$\alpha = A/r^2$	P/r	$\beta = R/r$	$\beta^{(1/2)}$	$\beta^{(2/3)}$	$\alpha \beta^{(2/3)}$	Q m^3/s	I (slope)
0.80	2.6943	4.4286	0.6084	0.78	0.718	1.9435	140.00	0.015	1/2000	0.0000500
0.80	2.6943	4.4286	0.6084	0.78	0.718	1.9435	140.00	0.015	1/2500	0.0000400
0.80	2.6943	4.4286	0.6084	0.78	0.718	1.9435	140.00	0.015	1/3000	0.0000333
0.80	2.6943	4.4286	0.6084	0.78	0.718	1.9435	140.00	0.015	1/5000	0.0000200
		$d/2r=1.60$		$d/r=0.80$		$V < 3.00 \text{ m/s}$		$Qn/(I^{0.5}*r^{(8/3)})$		
Horse shoe		$d/2r$	$\alpha = A/r^2$	P/r	$\beta = R/r$	$\beta^{(1/2)}$	$\beta^{(2/3)}$	$\alpha \beta^{(2/3)}$	Q m^3/s	r m
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	140.00	0.015	1/2000	0.0000500
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	140.00	0.015	1/2500	0.0000400
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	140.00	0.015	1/3000	0.0000333
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	140.00	0.015	1/5000	0.0000200

(3) Design by JICA

(a) Siphon

Location and Length of Siphon

Four siphons are placed at Kok basin diversion canal to cross under existing big river. Inverted siphons with covering of 1 or 1.5 m earth is buried under the riverbed. Proposed water level, riverbed level and length of siphons are shown in Table 11.2.2 (3)-5. In a case of Lao river with one existing weir at down stream, riverbed level is higher than water level of diversion canal.

Table 11.2.2 (3)-5 Water level , River Bed Level and Length of Siphon

No.	Siphon name	Station	Water Level	River bed level	Length (m)	Remarks
S-1	Nam Mea Kou	1+160.475	387.54	386.7	140.50	
S-2	Nam Mea Lao	3+619.675	386.30	387.3	218.00	
S-3	Huai Mae Hang	9+ 8.475	384.37	382.1	168.00	
S-4	Nam Mae Sakoen	11+685.405	383.03	382.4	198.00	
	Total length				724.50	

Cross section

The section of siphon is usually applied with about 1.5 times velocity of open canal one's to reduce cross sectional area. Dimensions on siphon is shown in Table 11.2.2 (3)-6

Table 11.2.2 (3)-6 Dimensions on Siphon

Discharge	Width (m)	Height (m)	Rows	Flow area	Coefficient Roughness	Velocity	Remarks
Q(cu.m/s)	W(m)	H(m)	4	A(sq.m)	n	V(m)	
140.00	3.60	3.60	4	51.84	0.015	2.70	

Foundation

Foundation of siphon would be applied for direct foundation except Nam Mae Hang siphon based on drilling investigation.

- Nam Mae Kon N value at foundation N=18 to 20 Sandy Soil (SM) Direct foundation
- Nam Mae Lao N=28 to 32 Clay soil (CH) Direct foundation
- Nam Mae Hang N= 8 to 24 Clay soil (CH) Direct/Pile found.
- Nam Mae Sakoen N=15 to 45 Clay soil (CH) Direct foundation

(b) Detail hydraulic calculation

Detail hydraulic calculations are shown in Table 11.2.2 (3)-7 to17 and results of calculation is shown in Database Maps.

(c) List of structures

Structure lists are shown in Table 11.2.2 (3)-8 to 22.

(d) Quantity

Quantities are shown in Table in 11.2.2 (3)-23 to 26

(e) Spoil bank volume and area

Calculation of spoils bank volume and area are shown in Table 11.2.2 (3)-27 to 28 and location of spoil bank area is shown in Data Base Map.

Table 11.2.2 (3)-7 Hydraulic Computation of Kok-Ing Diversion Canal (1/11)

Station (KM)	Structure	Q_{req} (m^3/s)	b (m)	d (m)	H_c (m)	H (m)	L.S. var	S.S. var	A (m^2)	R (m/s)	V (m/s)	h_v	Draught, Head Losses (m) of	FSL. E.G.L.	BL. E.L.	Top Conc. Lining E.L.	TBL. E.L.	Remark				
0+045 Beginning of Approach Channel	140.00 141.348	230.00	4.000	-	var 1: 750,000	1: 2.0	0.019	932,000	3.840	0.149	0.001		355,000	0.000		388,000	384,000	- 391,000				
0+400 End of Approach Channel	140.00 141.348	230.00	4.000	-	var 1: 750,000	1: 2.0	0.019	932,000	3.840	0.149	0.001				388,000	384,000	- 391,000					
0+725 Beginning of Concrete Lined Canal (Reach 1)	140.00 139.412	15.00	3.650	4.55	5.35 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155		225,000	0.045	0.045	387,755 387,600	383,750 383,300	389,500			
0+950 Overcut/tube	140.00 139.412	15.00	3.850	4.55	5.35 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155			387,710	387,555	383,705	388,255	389,500			
1+019.575 Beginning of Nam Mae Kon Siphon	140.00 139.412	15.00	3.850	4.55	5.35 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155						387,696 387,541	383,691 383,241	389,500		
1+40.000 Design Section of Siphon								0.016	51,840	0.900	2.701	0.372	140,500	0.668	0.750				387,455 387,491	383,491 383,500	389,500	
1+160.475 End of Nam Mae Kon Siphon	140.00 139.412	15.00	3.850	4.55	very 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155		178,525	0.036	0.036						
1+339 Overcut/tube	140.00 139.412	15.00	3.850	4.55	very 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155			386,910	386,755	382,905	387,455	389,500			
1+593 Highway No.1232 Bridge, 11.00 m. Width	140.00 139.412	15.00	3.850	4.55	very 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155		386,899	386,791	382,941	387,444	389,500				
1+604 Overcut/tube	140.00 139.412	15.00	3.850	4.55	very 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155		211,006	0.042	0.042						
2+113 Overcut/tube	140.00 139.412	15.00	3.850	4.55	very 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155			386,857	386,702	382,852	387,402	389,500			
2+4528 Overcut/tube	140.00 139.412	15.00	3.850	4.55	very 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155		386,790	0.116	0.116						
2+729.500 Drain Culvert 3-2,000 m. (Nam Mae Ham)	140.00 139.412	15.00	3.850	4.55	very 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155		201,500	0.040	0.040						
3+000 Station of Changing of TBL. E.L.	140.00 139.412	15.00	3.850	4.55	very 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155		345,000	0.069	0.069						
3+070 Overcut/tube	140.00 139.412	15.00	3.850	4.55	very 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155			386,672	386,517	382,667	387,217	389,500			
3+105 Overcut/tube	140.00 139.412	15.00	3.850	4.55	very 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155			386,632	386,477	382,627	387,177	389,500			
3+231 Overcut/tube	140.00 139.412	15.00	3.850	4.55	very 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155			35,000	0.007	0.007					
3+500 End of Sheet 1 & Beginning of Sheet 2	140.00 139.412	15.00	3.850	4.55	very 1:	5,000	1: 1.5	0.016	79,944	2.769	1.743	0.155		386,557	386,402	382,552	387,107	389,512				

Table 11.2.2 (3)-8 Hydraulic Computation of Kok-Ing Diversion Canal (2/11)

Station (KM)	Structure	Q_{avg} (m^3/s)	Q_{max} (m^3/s)	b (m)	d (m)	H_c (m)	H (m)	L.S. (m)	S.S. (m)	n	A (m^2)	R (m)	V (m/s)	h_v (m)	Distance, Head Losses (m) ΔH	Height of FSL Calc. Provide E.G.L.	Top Conc Lining El.	TBL. Remark					
3+619.675	Beginning of Nam Ma Lao Siphon	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	119.675	0.024	386.454	386.299	382.449	385.999	392.000	
3+637.675	Design Section of Siphon	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	51.840	0.000	2.701	0.372	218.000	0.451	9.900	385.554	385.399	381.549	386.099	392.000
3+637.675	End of Nam Ma Lao Siphon	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.522	385.367	381.517	386.067	391.000	
4+000	Station of Changing of TBL El	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.495	385.340	381.490	386.040	390.884	
4+052	Overbrake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.512	385.357	381.507	386.057	390.956	
4+137.500	Overbrake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.495	385.340	381.490	386.040	390.884	
4+152	Overbrake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.495	385.340	381.490	386.040	390.884	
4+440	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.494	385.279	381.429	385.979	390.629	
4+552	Overbrake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.495	385.249	381.399	385.949	390.501	
4+557.500	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.495	385.248	381.398	385.948	390.496	
4+911	Overbrake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.495	385.205	381.355	385.905	390.316	
4+990	Overbrake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.495	385.248	381.398	385.948	390.496	
5+037	Overbrake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.342	385.187	381.337	385.887	390.241	
5+664	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.342	385.035	381.185	385.735	389.596	
5+674	Overbrake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.188	385.035	381.183	385.733	389.598	
6+133	Overbrake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.096	384.941	381.091	385.641	389.201	
6+520	Station of Changing of TBL El	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.019	384.864	381.014	385.564	389.200	
6+540	Station of Changing of TBL El	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			385.015	384.860	381.010	385.560	389.880	

Table 11.2.2 (3)-9 Hydraulic Computation of Kok-Ing Diversion Canal (3/11)

Station (Km.)	Structure	Q_{des} (m^3/s)	b (m)	d (m)	H_c (m)	H (m)	L.S.	S.S.	a	A	R	V	h_v (m)	Distance, Head Losses (m) of ΔH	Height FSL. at E.L.	Top Conc E.L.	Living E.L.	TBL.	Remark			
6+632 Overtake		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.6	0.016	79.984	2.769	1.743	0.155			384.597	384.842	380.092	385.542	389.850
6+638 Highway No.1232 Bridge, 11.00 m. Width		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.596	384.841	380.591	385.541	389.850
6+740 Station of Changing of TBL. El.		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
6+850.500 Overtake		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
6+960 Station of Changing of TBL. El.		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
7+000 End of Sheet 2 & Beginning of Sheet 3		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
7+987 Overtake		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
8+155 Highway No.1173 Bridge, 11.00 m. Width		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
8+200 Station of Changing of TBL. El.		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
8+240 Station of Changing of TBL. El.		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
8+330 Overtake		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
8+411 Overtake		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
8+487 Roadway Bridge, 4.00 m. Roadway Width		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
8+819.700 Overtake		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
9+008.475 Beginning of Hui-Mae Hsi Siphon		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
9+119.700	Design Section of Siphon 4-3.60x3.60 m.	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850
9+176.475 End of Hui-Mae Hsi Siphon		140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			384.576	384.821	380.571	385.521	389.850

Table 11.2.2 (3)-10 Hydraulic Computation of Kok-Jing Diversion Canal (4/11)

Station (KM)	Structure	Q_{out} (m^3/s)	b (m)	d (m)	H_c (m)	H (m)	L.S.	S.S.	α	A (m^2)	R	V	h_v	Distance, Head Losses (m)	Height of ΔH	FSL. Calc.	BL. Provide E.G.L.	Top Conc. Lining	TBL.	Remark		
9+30.500	Overtake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	133.500	0.027	0.027	383.450	379.600	384.150	387.000
9+33.9	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155				383.578	379.573	384.123	387.000
9+42.4	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.69	1.743	0.155				285.000	0.057	0.057	
9+42.7	Overtake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.69	1.743	0.155				383.571	383.366	384.066	387.000
10+09.4	Overtake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.69	1.743	0.155				383.457	379.482	384.032	387.000
10+49.450	Overtake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.69	1.743	0.155				383.520	383.365	379.515	384.065
10+50.0	End of Sheet 3 & Beginning of Sheet 4	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.69	1.743	0.155				383.405	383.251	379.401	383.951
10+59.500	Overtake	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.69	1.743	0.155				383.405	383.252	379.402	383.952
11+00.8	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.69	1.743	0.155				383.407	383.252	379.402	383.952
11+18.0	Station of Changing of TBL. El	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.69	1.743	0.155				383.500	0.001	0.001	
11+62.1024	Equation - Ahead	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.69	1.743	0.155				383.200	0.034	0.034	
11+63.405	Beginning of Nam Mae Sakorn Siphon	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.69	1.743	0.155				383.151	379.301	383.851	387.000
11+63.405 End of Nam Mae Sakorn Siphon	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.69	1.743	0.155				383.306	383.149	379.299	383.849	
12+281.120 End of Concrete Lined Canal (Reach 1)	140.00	139.412	15.00	3.850	4.55	very	1:	5.000	1: 1.5	0.016	79.984	2.69	1.743	0.155				383.266	383.111	379.261	383.811	
12+291.120 Inlet of Tunnel No.1	140.00	140.006	-5.50	6.198	H=7.50	-	1:	2.500	-	0.015	55.757	2.585	2.511	0.321				383.045	379.193	383.743	386.000	
14+000 End of Sheet 4 & Beginning of Sheet 5	140.00	140.006	-5.50	6.198	H=7.50	-	1:	2.500	-	0.015	55.757	2.585	2.511	0.321				381.496	381.175	379.977	382.477	

$\Delta W.S. = 0.250 \text{ m}$

$\Delta W.S. = 0.249 \text{ m}$

Table 11.2.2 (3)-11 Hydraulic Computation of Kok-Ing Diversion Canal (5/11)

Station (K.M.)	Structure	Q_{ds} (m^3/s)	b (m)	d (m)	H_C (m)	H (m)	I.S. (m)	S.S. (m^2)	a (m)	R (m/s)	V (m/s)	h_v (m)	Distance, Head Losses (m)	Height of FSL.	BL.	Top Coat	TBL.	Lining El.	Remark				
15+520.604	Outlet of Tunnel No.1	140.00	140.006	3.850	6.198	H=7.30	-	1:	2.500	-	0.015	55.757	2.511	0.321			380.968	380.647	374.449	381.949	$\Delta W.S. = 0.042 \pm$		
15+545.604	Beginning of Cut & Cover Conduit	140.00	141.023	3.850	7.000	H=4.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349			380.954	380.605	373.605	382.305	395.000	
16+565	End of Cut & Cut Conduit	140.00	141.023	3.850	7.000	H=6.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349			380.968	380.647	374.449	381.949	$\Delta W.S. = -0.035 \pm$	
16+600	Beginning of Concrete Lined Canal (Reach 2)	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1:	1.5	0.016	79.984	2.769	1.745	0.155			34.000	0.161	0.161		
17+126.604	Overside	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1:	1.5	0.016	79.984	2.769	1.743	0.155			380.025	380.150	376.300	380.850	389.000
17+130.104	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1:	1.5	0.016	79.984	2.769	1.743	0.155			380.020	380.045	376.195	380.745	386.367
17+300	End of Sheet 5 & Beginning of Sheet 6	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1:	1.5	0.016	79.984	2.769	1.743	0.155			3.500	0.001	0.001		
17+73.604	Roadway Bridge, 7.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1:	1.5	0.016	79.984	2.769	1.743	0.155			380.199	380.044	376.194	380.744	386.330
17+793.604	Overside	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1:	1.5	0.016	79.984	2.769	1.743	0.155			380.076	379.921	376.071	380.621	384.500
18+400.604	Overside	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1:	1.5	0.016	79.984	2.769	1.743	0.155			50.000	0.010	0.010		
19+740	Station of Changing of TBL. El.	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1:	1.5	0.016	79.984	2.769	1.743	0.155			607.000	0.121	0.121		
20+320	Station of Changing of TBL. El.	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1:	1.5	0.016	79.984	2.769	1.743	0.155			379.945	379.790	375.940	380.600	384.500
20+580.604	Overside	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1:	1.5	0.016	79.984	2.769	1.743	0.155			1.359.396	0.268	0.268		
20+968.604	Highway Bridge, 11.00 m. Roadway Width (Hs)	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1:	1.5	0.016	79.984	2.769	1.743	0.155			379.677	379.522	375.672	380.222	384.500
21+000	End of Sheet 6 & Beginning of Sheet 7	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1:	1.5	0.016	79.984	2.769	1.743	0.155			379.461	379.306	375.456	380.006	387.000

Table 11.2.2 (3)-12 Hydraulic Computation of Kok-Ing Diversion Canal (6/11)

Station (KM)	Structure	Q_{out} (m^3/s)	b (m)	d (m)	H _c (m)	H (m)	I.S.	S.S. 1: 1.5	n	A (m^2)	R (m)	V (m)	b_V (m)	Distance, Head Losses (m) ΔL	FSL. of Calc. Provide E.G.L.	BL. Top Conc. Lining El.	BL. Top Conc. TBL. El.	Remark	
21+240 Station of Changeing of TBL. El.	140.00 139.412	15.00	3.450	4.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155		379.377	379.222	375.572	379.922	388.350
21+4937.604 Overchute	140.00 139.412	15.00	3.450	4.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155		379.257	379.082	375.232	379.782	391.402
21+560 End of Concrete Lined Canal (Reach 2)	140.00 139.412	15.00	3.450	4.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155		379.239	379.078	375.228	379.778	391.500
21+489 Beginning of Cut & Cover Conduit	140.00 141.023	7.000	H=8.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349			379.138	378.789	371.789	370.459	-
22+023.604 Asphalt Road to Ban Dol Ngam	140.00 141.023	H=4.35	7.000	H=8.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349		349.604	0.380			
23+191.604 Nam Ma Tat	140.00 141.023	H=4.35	7.000	H=8.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349		378.758	378.409	371.409	380.109	-
24+560 End of Sheet 7 & Beginning of Sheet 8	140.00 141.023	H=4.35	7.000	H=8.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349		253.000	0.161	0.101		
24+783.968 Equation - Back	140.00 141.023	H=4.35	7.000	H=8.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349		1.308.396	0.523	0.323		
24+724.562 Equation - Ahead	140.00 141.023	H=4.35	7.000	H=8.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349		378.134	377.785	370.785	379.485	-
26+139.777 End of Cut & Cover Conduit	140.00 141.023	H=4.35	7.000	H=8.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349		283.968	0.114	0.114		
26+164.777 End of Tunnel No.2	140.00 140.006	H=5.50	6.198	H=7.50	-	1:	2.500	-	0.015	55.757	2.585	2.511	0.221		378.020	377.671	370.671	379.371	-
28+000 End of Sheet 8 & Beginning of Sheet 9	140.00 140.006	H=5.50	6.198	H=7.50	-	1:	2.500	-	0.015	55.757	2.585	2.511	0.321		378.020	377.671	370.671	379.371	-
31+500 End of Sheet 9 & Beginning of Sheet 10	140.00 140.006	H=5.50	6.198	H=7.50	-	1:	2.500	-	0.015	55.757	2.585	2.511	0.321		377.454	377.105	370.105	378.805	-
31+523.254 Cut off Tunnel No.2	140.00 140.006	H=5.50	6.198	H=7.50	-	1:	2.500	-	0.015	55.757	2.585	2.511	0.321		376.000	1.400	1.400		
32+062.254 Roadway Bridge, 4.00 m Roadway Width	140.00 139.412	15.00	3.850	4.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155		34.000	0.139	0.139		
32+430.254 Overchute	140.00 139.412	15.00	3.850	4.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155		375.155	375.000	371.150	375.700	388.000
32+530 Station of Changeing of TBL. El.	140.00 139.412	15.00	3.850	4.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155		374.840	370.989	375.549	377.358	

Table 11.2.2 (3)-13 Hydraulic Computation of Kok-Ing Diversion Canal (7/11)

Station (K.M)	Structure	Q_{eff} (m^3/s)	b	d	H_C (m)	H	I.S.	S.S.	n	A	R	V	h_V	Distance, Head Losses (m)	Height of ΔH	F.S.L.	E.L.	Top Conc Lining El.	T.B.L.	Remark
32+8.67-254	Drain Culvert 1-ft-1.00 m.	140.00	139.412	15.00	3.850	4.35	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	487.254	0.097	0.097		
																374.893	374.738	370.888	375.338	376.238
32+9.60	Inlined Drop (w/s)	140.00	139.412	15.00	3.850	4.35	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	92.246	0.019			
																374.874	374.719	370.868	375.419	376.219
32+9.60	Inlined Drop (d/s)	140.00	139.412	15.00	3.850	4.35	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	0.000	0.000	4.194		$\Delta W.S = 4.194 \text{ m}$
																370.680	370.525	366.675	371.225	372.025
33+0.35	Drain Culvert 2-ft-1.00 m.	140.00	139.412	15.00	3.850	4.35	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	575.000	0.115	0.115		
																370.565	370.410	366.560	371.110	371.910
33+7.67-254	Roadway Bridge 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.35	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	232.254	0.046	0.046		
																370.519	370.364	366.514	371.064	371.864
33+8.95	Drain Culvert 2-ft-1.00 m.	140.00	139.412	15.00	3.850	4.35	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	127.746	0.026			
																370.493	370.338	366.488	371.038	371.838
34+4.65	Roadway Bridge 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.35	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	570.000	0.194	0.194		
																370.299	370.144	366.294	370.844	371.644
35+0.00	End of Sheet 10 & Beginning of Sheet 11	140.00	139.412	15.00	3.850	4.35	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	135.000	0.027	0.027		
																370.272	370.117	366.267	370.817	371.617
35+0.09-994	Equation - Back	140.00	139.412	15.00	3.850	4.35	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	9.994	0.002	0.002		
35+0.21-074	Equation - Ahead	140.00	139.412	15.00	3.850	4.35	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	370.270	370.115	366.265	370.815	371.615
35+4.912-028	E.C. 27 (Beginning of Alternative Alignment)	140.00	139.412	15.00	3.850	4.35	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	290.054	0.038	0.038		
																370.212	370.057	366.207	370.757	371.557
35+5.25	End of Concrete Lined Canal	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	212.972	0.043	0.043		
																370.169	370.014	366.164	370.714	378.900
35+5.54	Begging of Cut & Cover Canal	140.00	141.023	r=4.35	7.000	H=6.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349	29.000	0.095	0.095		
																370.074	369.725	362.725	371.425	-
36+4.24-038	Equation - Back	140.00	141.023	r=4.35	7.000	H=6.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349	870.038	0.348	0.348		
36+4.54-347	Equation - Ahead	140.00	141.023	r=4.35	7.000	H=6.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349	365.726	369.377	362.377	371.077	-
36+5.87-253	Huk Kang	140.00	141.023	r=4.35	7.000	H=8.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349	32.906	0.013	0.013		
																371.747	0.151	0.151		
36+9.66	End of Cut & Cover Conduit	140.00	141.023	r=4.35	7.000	H=8.70	-	1:	2.500	-	0.015	53.887	2.667	2.617	0.349	365.562	369.213	362.213	370.913	-
37+0.00	Beginning of Concrete Lined Canal	140.00	139.412	15.00	3.850	4.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	34.000	0.161	0.161		$\Delta W.S = -0.033 \text{ m}$
																369.401	369.246	365.396	369.946	377.560

Table 11.2.2 (3)-14 Hydraulic Computation of Kok-Ing Diversion Canal (8/11)

Station (K.M.)	Structure	Q_{ave} (m ³ /s)	b (m)	d (m)	H_C (m)	H (m)	L.S.	S.S. a	A (m ²)	R (m)	V (m)	h_V	Distance, Head Losses (m) of ΔH	FSL. E.L.	Top Conc. Lining E.I.	Remark						
37+114.233	Overbank (Final Pump)												114.233	0.023								
37+114.233	Roadway Bridge, 15.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1: 5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	369.378	369.223	366.373	369.923	377.107			
37+133.253	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1: 5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	19.000	0.004						
38+525	Station of Changeing of E.L.	140.00	139.412	15.00	3.850	4.55	very	1: 5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			369.219	365.369	365.919	377.042		
38+507.253	Roadway No.1,74 Bridges, 11.00 m. Width	140.00	139.412	15.00	3.850	4.55	very	1: 5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			369.159	368.984	365.134	369.684	375.000	
38+500	End of Sheet 11 & Beginning of Sheet 12	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	177.47	0.004	0.004				
40+133.253	Roadway Bridge, 7.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			369.135	368.980	365.130	369.680	370.480
40+210	Drain Culvert 3-dia.1.00 m.	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			175.000	0.035	0.035		
40+224.253	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			369.100	368.945	365.095	369.645	370.445
40+228.253	Drain Culvert 1-dia.1.00 m.	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			1.593.253	0.327	0.327		
40+235.253	Drain Culvert 3-dia.1.00 m.	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			368.773	368.618	364.4763	369.313	370.118
40+275	Drain Culvert 3-dia.1.00 m.	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	76.747	0.015	0.015				
40+354.253	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			368.738	368.603	364.753	369.303	370.103
40+447.253	Roadway Bridge, 7.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			368.735	368.600	364.750	369.300	370.100
41+002.253	Drain Culvert 1-dia.1.00 m.	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			4.000	0.001	0.001		
41+052.253	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			368.754	368.599	364.749	369.299	370.099
41+121.253	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			46.747	0.009	0.009		
41+141.253	Roadway Bridge, 7.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			368.745	368.590	364.740	369.290	370.090
41+212.253	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			289.253	0.058	0.058		
41+297.253	Roadway Bridge, 7.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			368.587	368.52	364.682	369.232	370.032
42+000	End of Sheet 12 & Beginning of Sheet 13	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			368.610	368.465	364.605	369.155	369.955
42+121.253	Drain Culvert 1-dia.1.00 m.	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			555.000	0.111	0.111		
42+182.253	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			319.000	0.064	0.064		
42+252.253	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			178.747	0.036	0.036		
42+322.253	Roadway Bridge, 7.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			368.399	368.244	364.394	368.744	
42+400	End of Sheet 13 & Beginning of Sheet 14	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			141.253	0.028	0.028		
42+472.253	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			365.571	368.216	364.366	368.916	369.716
42+542.253	Roadway Bridge, 7.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			324.000	0.079	0.079		
42+612.253	Drain Culvert 1-dia.1.00 m.	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155			368.292	368.137	364.287	368.857	369.637

Table 11.2.2 (3)-15 Hydraulic Computation of Kok-Ing Diversion Canal (9/11)

Station (Km)	Structure	Q_{dis} (m^3/s)	Q_{des} (m^3/s)	b	d	H_c (m)	H (m)	I.S.	S.S.	n	A	R	V	h_v	Distance (m)	ΔL (m)	Head Losses (m) of ΔH	FSL. of Provide E.G.L.	El.	Top Conc. Lining El.	TRI.	Remark	
42+585.253	Drain Culvert 2-dia 1.00 m. (Huu Tui Boat)	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	20.020	0.010	0.010	368.127	364.277	368.827	368.627	
42+587.253	Roadway Bridge 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	12.000	0.002	0.002	368.280	368.125	364.275	368.825	
42+591.253	Drain Culvert 1-dia 1.00 m.	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	364.000	0.073	0.073	368.207	368.032	364.202	368.752	
43+021.253	Drain Culvert 2-dia 1.00 m. (Huu Tui Khue)	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	368.195	0.040	0.040	368.190	364.190	368.740	369.540	
43+457.253	Drain Culvert 2-dia 1.00 m. (Huu Tui)	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	20.000	0.042	0.042	368.102	367.998	364.148	368.698	
43+529.253	Roadway Bridge 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	60.000	0.012	0.012	368.102	367.998	364.148	368.698	
43+481.253	Drain Culvert 1-dia 1.00 m.	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	22.000	0.046	0.046	368.107	367.998	364.148	368.698	
43+487.253	Drain Culvert 2-dia 1.00 m. (Huu Tui)	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	24.000	0.005	0.005	368.102	367.998	364.148	368.698	
43+537.253	(Huu Tui)	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	368.102	0.046	0.046	368.107	367.998	364.148	368.698	
44+177.253	Roadway Bridge 7.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	356.900	0.071	0.071	368.102	367.998	364.148	368.698	
44+467.253	Overburden	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	340.000	0.068	0.068	368.102	367.998	364.148	368.698	
44+515.253	Overburden	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	356.900	0.071	0.071	368.102	367.998	364.148	368.698	
44+529.253	Overburden	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	367.998	0.046	0.046	368.102	367.998	364.148	368.698	
44+530.250	Station of Changing of TBL. E.	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	367.958	0.046	0.046	368.102	367.998	364.148	368.698	
45+200	Station of Changing of TBL. E.	140.00	139.412	15.00	3.850	4.55	5.35	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	33.253	0.007	0.007	367.907	367.652	363.802	368.352	
45+229.253	Overburden	140.00	139.412	15.00	3.850	4.55	5.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	244.747	0.049	0.049	367.751	367.506	363.746	368.206
45+230.250	Overburden	140.00	139.412	15.00	3.850	4.55	5.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	74.000	0.015	0.015	367.751	367.506	363.746	368.206
45+237.253	Overburden	140.00	139.412	15.00	3.850	4.55	5.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	367.751	0.015	0.015	367.751	367.506	363.746	368.206
45+297.253	Overburden	140.00	139.412	15.00	3.850	4.55	5.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	66.000	0.013	0.013	367.751	367.506	363.746	368.206
45+373.253	Overburden	140.00	139.412	15.00	3.850	4.55	5.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	367.751	0.015	0.015	367.751	367.506	363.746	368.206
45+467.253	Overburden	140.00	139.412	15.00	3.850	4.55	5.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	367.751	0.015	0.015	367.751	367.506	363.746	368.206
45+491.253	Overburden	140.00	139.412	15.00	3.850	4.55	5.35	very	1:	5.000	1: 1.5	0.016	79.984	2.769	1.743	0.155	18.000	0.004	0.004	367.751	367.506	363.746	368.206

Table 11.2.2 (3)-16 Hydraulic Computation of Kok-Ing Diversion Canal (10/11)

Station (KM)	Structure	Q_{des} (m^3/s)	b (m)	d (m)	H_c (m)	H (m)	L.S. 1:	S.S. 1:	A (m^2)	R (m)	V (m^3/s)	h_v (m)	Distance, Head Losses (m) ΔH	FSL. of E.G.L.	E.L.	BL.	Top Conc.	TBL.	Remark	
43+500	End of Sheet 13 & Beginning of Sheet 14	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155	103.747	0.022	367.697	367.542	363.892	368.242 / 372.540
44+72.253	Roadway Bridge, 7.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155	472.259	0.094				
44+98.023	Overcut	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.002	367.693	367.448	363.598	368.148 / 372.500
45+115.253	Overcut	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.002	367.601	367.446	363.596	368.146 / 372.500
46+217.253	Overcut	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155	135.000	0.027	367.542	367.387	363.537	368.087 / 372.500
46+500	Station of Changing of TBL. El.	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.045	367.497	367.342	363.492	368.042 / 372.500
47+137.253	Overcut	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.032	367.523	0.127	0.127	
47+500	Station of Changing of TBL. El.	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.032	367.370	367.215	363.365	367.915 / 373.233
47+940.853	Highway No.1020 Bridge, 11.00 m. Width	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.008	367.205	367.050	363.200	367.730 / 373.660
48+000	Station of Changing of TBL. El.	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.008	367.147	367.042	363.192	367.742 / 373.650
48+500	Station of Changing of TBL. El.	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.015	367.297	367.142	363.292	367.842 / 373.650
48+677.253	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.092	460.853	0.092		
49+000	End of Sheet 14 & Beginning of Sheet 15	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.120	600.000	0.120		
49+323	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.007	367.197	367.042	363.192	367.742 / 373.650
50+000	Station of Changing of TBL. El.	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.007	366.907	365.057	363.072	367.622 / 370.080
50+023.253	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.007	366.597	366.842	362.922	367.512 / 369.714
50+507.253	Roadway Bridge, 4.00 m. Roadway Width	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.095	474.000	0.095		
52+500	End of Sheet 15 & Beginning of Sheet 16	140.00	139.412	15.00	3.850	4.55	very	1:	5.000 1: 1.5	0.016	79.984	2.769	1.743	0.155		0.399	1.992.747	0.399	366.296	366.141 / 362.291

Table 11.2.2 (3)-17 Hydraulic Computation of Kok-Ing Diversion Canal (11/11)

Station (KM)	Structure	Q_{rec} (m^3/s)	b (m)	d (m)	H _c (m)	H (m)	L.S. (m)	S.S. (m)	n	A (m^2)	R (m)	V (m)	h_v (m)	Distance, Head Losses (m) of ΔH	Height of FSL of E.G.L.	Head Losses (m) of ΔL	Living El.	Top Conc El.	TBL	Remark		
52+750	End of Can., Lined Canal & Inclined Drop (W/S)	140.00	139.412	15.00	3.550	4.55	5.35	1:	5,000	1:1.5	0.016	79.94	2.769	1.743	0.155	250.000	0.050	366.246	366.091	366.241	366.791	569.000
52+750	Inclined Drop (W/S) & Beginning of Earth Canal	140.00	140.34	30.00	3.900	-	-	1:	8,000	1:2.0	0.025	147.420	3.107	0.932	0.046	0.000	5.008	361.238	361.192	357.292	-	569.000
35+332.233	End of Earth Canal at Nam Mae Loy	140.00	140.34	30.00	3.900	-	-	1:	8,000	1:2.0	0.025	147.420	3.107	0.932	0.046	0.323	0.323	360.915	360.869	356.969	-	569.000

Table 11.2.2(3)-18 Canal Length and numbers of structures in Kok-Ing & Ing-Yot Diversion Canal

Canal & Structures	Type	Shape	Size	Unit	Numbers or Length			Total	Remarks
					Reach				
					1	2	3		
1.Lined open canal	Concrete Lining	Trapezoid	W=15.00m,H=4.55	m	10,753	5,360	19,707	35,820	
2.Unlined open canal	Earth Lining	Trapezoid	W=30.00m	m	-	-	2,582	2,582	
3.Culvert	Re.concrete	R.C Horse shoe		m	-	5459	1345	6804	
4.Siphon	Inverted	R.C box	3.60m*3.60m*5	m	725	-	-	725	
5.Drop	Inclined Check drop			Nos.	-	-	2	2	
6.Check	With slide gate	R.C Rectangular		Nos.	1	1	2	4	
7.Turnout	Gravity	R.C Pipe		Nos.	-	-	4	4	
	Pumping	R.C Slab		Nos.	6	2	2	10	
8.Drain culvert									
Type-1	R. C Box	Rectangular		Nos.	1	-	-	1	
Type-2	R.C Pipe			Nos.	-	-	12	12	
9.Overchute				Nos.	29	5	12	46	
10.Bridge									
Type-1	Highway bridge	R.C Slab	W=11.0m	Nos.	3	1	2	6	
Type-2	Road way bridge	R.C Slab	W= 7.0m	Nos.	7	2	18	27	
Type-3	Farm road bridg	R.C Slab	W=4.00m	Nos.	10	6	14	30	
	O&M bridge	R.C Slab	W=4.00m	Nos.	4	0	0	4	
11.Sand trap				Nos.	1	1	1	3	

Reach-1 STA. : 0+725.000~ 12+281.199

Reach-2 STA. : 15+320.604~ 26+139.777

Reach-3 STA. : 31+557.254~ 55+332.253

Canal Length and numbers of structures - ING-YOT Diversion Canal

Canal & Structures	Type	Shape	Size	Unit	Numbers		Total	Remarks
					Reach			
					1	2		
1.Lined open canal	Concrete Lining	Trapezoid	W=20.00m,H=4.55	m	1,476	-	1,476	
2.Culvert	Re.concrete	R.C Horse shoe		m	360	285	8807	9452
3.Siphon	Inverted	R.C box	3.60m*3.60m*5	m	-	185		185
4.Sand trap				Nos.	1	1		3

Reach-1 STA. : 0+724.2500~ 2+560.00

Reach-2 STA. : 4+560.00~ 13+836.952

Table 11.2.2 (3)-19 Kok-Ing Diversion Canal Length

STA	Canal Type	Reach/No.	Length (m)					Remarks
			OpenCanl	Culvert	Siphon	Structure	Tunnel	
0 + 725.000								
	Open Canal	Reach-1	294.975					
1 + 19.975								
	No.1 Siphon	Nam Mae Kon			140.500			
1 + 160.475								
	Open Canal	Reach-1	2459.200					
3 + 619.675								
	No.2 Siphon	Nam Mae Lao			218.000			
3 + 837.675								
	Open Canal	Reach-1	5170.800					
9 + 8.475								
	No.3 Siphon	Huai Mae Han			168.000			
9 + 176.475								
	Open Canal	Reach-1	2365.827					
11 + 542.302								
	Equation	Reach-1	0.000					eq=78.722
11 + 621.024								
	Open Canal	Reach-1	64.381					
11 + 685.405								
	No.4 Siphon	Nam Mae Sakon			198.000			
11 + 883.405								
	Open Canal	Reach-1	397.715					
12 + 281.120								
	Tunnel	No.1						3039.484
15 + 320.60								
	Culvert	Reach-2			1279.396			
16 + 600.00								
	Open Canal	Reach-2	5360.000					
21 + 960.000								
	Culvert	Reach-2			4179.777			
26 + 139.777								
	Tunnel	No.2						5417.477
31 + 557.254								
	Open Canal	Reach-3	1402.746					
32 + 960.000								
	Drop	Reach-3						0.000
32 + 960.000								
	Open Canal	Reach-3	2049.994					
35 + 9.994								
	Equation	Reach-3	0.000					eq=11.080
35 + 21.074								
	Open Canal	Reach-3	503.926					
35 + 525.000								
	Culvert	Reach-3			899.038			
36 + 424.038								
	Equation	Reach-3			0.000			eq=130.309
36 + 554.347								
	Culvert	Reach-3			445.653			
37 + 0.000								
	Open Canal	Reach-3	15750.000					
52 + 750.000								
	Drop	No.2						0.000
52 + 750.000								
	Open Canal	Reach-3	2582.253					
55 + 332.253								
Total			38401.817	6803.864	724.5	0.000	8456.961	54387.142

Table 11.2..2 (3)-20 List of Structures(1/3)

1. Open Canal-Concrete Lining Canal

Reeach	STA(m)		Length (m)	Type	Discharge (m3/s)	Section (m)	Remarks
	from	to					
Reach-1	0 + 725.000	1 + 19.975	294.975	Trapezoid	140.00	W=15.0,H=5.35	
	1 + 160.475	3 + 619.675	2459.200	Trapezoid	140.00	W=15.0,H=5.35	
	3 + 837.675	9 + 8.475	5170.800	Trapezoid	140.00	W=15.0,H=5.35	
	9 + 176.475	11 + 542.302	2365.827	Trapezoid	140.00	W=15.0,H=5.35	
	11 + 542.302	11 + 621.024	0.000	Trapezoid	140.00	W=15.0,H=5.35	Eq = -78.722m
	11 + 621.024	11 + 685.400	64.376	Trapezoid	140.00	W=15.0,H=5.35	
	11 + 883.400	12 + 281.120	397.720	Trapezoid	140.00	W=15.0,H=5.35	
	Sub Total		10752.898				
Reach-2	16 + 600.00	21 + 960.00	5360.000	Trapezoid	140.00	W=15.0,H=5.35	
	Sub Total		5360.000				
Reach-3	31 + 557.254	32 + 960.000	1402.746	Trapezoid	140.00	W=15.0,H=5.35	
	32 + 960.000	35 + 9.994	2049.994	Trapezoid	140.00	W=15.0,H=5.35	
	35 + 9.994	35 + 21.074	0.000				Eq = -11.080m
	35 + 21.074	35 + 525.000	503.926	Trapezoid	140.00	W=15.0,H=5.35	
	37 + 0.000	52 + 750.000	15750.000	Trapezoid	140.00	W=15.0,H=5.35	
	Sub Total		19706.666				
Total			35819.564			W=30.0,d=3.90	

2. Open Canal-Earth Lining Canal

Reach-3	52 + 750.000	55 + 332.253	2582.253	Trapezoid	140.00	W=15.0,H=5.35

3. Culvert

CLT-1	15 + 320.60	16 + 600.00	1279.396	RC Horse Shoe	140.00	H=8.70m
CLT-2	21 + 960.00	26 + 139.777	4179.777	RC Horse Shoe	140.00	H=8.70m
	Sub Total		5459.173			
CLT-3	35 + 525.000	36 + 424.038	899.038	RC Horse Shoe	140.00	H=8.70m
CLT-4	36 + 424.038	36 + 554.347	0.000	RC Horse Shoe	140.00	H=8.70m
CLT-5	36 + 554.347	37 + 0.000	445.653	RC Horse Shoe	140.00	H=8.70m
	Sub Total		1344.691			
Total			6803.864			

4.Sihon

S-1	1 + 160.475	1 + 19.975	140.500	R.C Box	140.00	3.60*3.60*4	Nam Mae Kon
S-2	3 + 619.675	3 + 837.675	218.000	R.C Box	140.00	3.60*3.60*4	Nam Mae Lao
S-3	9 + 176.475	9 + 8.475	168.000	R.C Box	140.00	3.60*3.60*4	Huai Mae Hang
S-4	11 + 685.405	11 + 883.405	198.000	R.C Box	140.00	3.60*3.60*4	Nam Mae Sakoen
Total			724.500				

5.Drop

D-1	32 + 960.000			R.C Inclined	140.00	$\Delta H=2.55m$
D-2	52 + 750.000			R.C Inclined	140.00	$\Delta H=5.05m$

Table 11.2.2 (3)-21 List of Structures (2/3)

6. Weir/Check Structure

Name	No.s.	STA(km)	Type		Remarks
Check	CH-1	11+680	With radial gate		
	CH-2	21+960	With radial gate		
	CH-3	37+114	With radial gate		
	CH-4	46+115	With radial gate		
Check drop	CD-1	32+960	With stop log gate		
	CD-2	52+750	With stop log gate		

7. Turn Out

Name	Area	STA(km)	Type	Irrigation. (rai)	Discharege (cum/s)	Remarks
TOT- 1	Kok-1	2+183.000	Pump	920	0.230	
TOT- 2	Kok-1	2+528.000	Pump			
TOT- 3	Kok-2	4+137.500	Pump	1,880	0.470	
TOT- 4	Kok-2	5+298.000	Pump			
TOT- 5	Kok-2	6+632.000	Pump			
TOT- 6	Kok-3	10+999.500	Pump	740	0.190	
TOT- 7	Tak-1	17+793.604	Pump	460	0.120	
TOT- 8	Tak-2	21+960.000	Pump	7,000	1.750	
TOT- 9	Ing-1	32+860.000	Gravity	7,940	1.990	
TOT-10	Ing-2	36+587.253	Pump	8,600	2.150	
TOT-11	Ing-3	37+000.000	Gravity	3,200	0.800	
TOT-12	Ing-4	41+450.000	Gravity	4,390	1.100	
TOT-13	Ing-5	42+500.000	Gravity	3,140	0.790	
TOT-14	Ing-6	46+115.253	Pump	7,530	1.880	
Total				45,800	11.470	

8. Drain Culvert

Name	STA(km)	Type	Size		Remarks
DC- 1	2+729.500	RC Box	2.0*2.0*3		Nam Mae Hang
DC- 2	32+867.254	RC Pipe	ϕ 1000*1		
DC- 3	33+535.000	RC Pipe	ϕ 1000*2		
DC- 4	33+895.000	RC Pipe	ϕ 1000*2		
DC- 5	40+210.000	RC Pipe	ϕ 1000*3		
DC- 6	40+228.253	RC Pipe	ϕ 1000*1		
DC- 7	40+275.000	RC Pipe	ϕ 1000*3		
DC- 8	41+502.253	RC Pipe	ϕ 1000*1		
DC- 9	42+535.253	RC Pipe	ϕ 1000*1		
DC-10	42+961.253	RC Pipe	ϕ 1000*1		
DC-11	43+021.253	RC Pipe	ϕ 1000*2		
DC-12	43+457.253	RC Pipe	ϕ 1000*2		
DC-13	43+481.253	RC Pipe	ϕ 1000*1		

Table 11.2.2 (3)-22 List of Structures (3/3)

9. Overchute

Name	STA(km)
OVC-1	0+950.000
OVC-2	1+339.000
OVC-3	1+604.000
OVC-4	2+183.000
OVC-5	2+528.000
OVC-6	3+070.000
OVC-7	3+105.000
OVC-8	3+251.000
OVC-9	4+052.000
OVC-10	4+137.500
OVC-11	4+592.000
OVC-12	4+811.000
OVC-13	4+900.000
OVC-14	5+037.000
OVC-15	5+298.000
OVC-16	5+674.000
OVC-17	6+133.000
OVC-18	6+632.000
OVC-19	6+850.500
OVC-20	7+987.000
OVC-21	8+282.500
OVC-22	8+530.000
OVC-23	8+811.000
OVC-24	8+889.700
OVC-25	9+505.500
OVC-26	9+927.000
OVC-27	10+094.000
OVC-28	10+494.500
OVC-29	10+999.500
OVC-30	17+124.604
OVC-31	17+793.604
OVC-32	18+400.604
OVC-33	20+580.604
OVC-34	21+937.604
OVC-35	32+309.254
OVC-36	37+114.253
OVC-37	44+617.253
OVC-38	44+955.253
OVC-39	45+235.253
OVC-40	45+307.253
OVC-41	45+373.253
OVC-42	45+391.253
OVC-43	45+980.253
OVC-44	46+115.253
OVC-45	46+277.253
OVC-46	47+137.253

10. Bridge

10-1 High Way Bridge W=11.00m

	Name	STA(km)	H.W No.	Type
HB-1	H/W Bridge	1+393.000	No.1232	R.C Slab
HB-2	H/W Bridge	6+638.000	No.1232	R.C Slab
HB-3	H/W Bridge	8+156.000	No.1173	R.C Slab
HB-4	H/W Bridge	20+968.604	No.1152	R.C Slab
HB-5	H/W Bridge	38+307.253	No.1174	R.C Slab
HB-6	H/W Bridge	47+960.853	No.1020	R.C Slab

10-2. Road Way Bridge W=7.00--4.00m

	Name	STA(km)	R/W No.	Type
RB- 1	R/W Bridge	4+440.000		R.C Slab
RB- 2	R/W Bridge	4+597.500		R.C Slab
RB- 3	R/W Bridge	5+664.000		R.C Slab
RB- 4	R/W Bridge	8+887.000		R.C Slab
RB- 5	R/W Bridge	9+639.000		R.C Slab
RB- 6	R/W Bridge	9+924.000		R.C Slab
RB- 7	R/W Bridge	11+008.000		R.C Slab
RB- 8	R/W Bridge	17+130.104		R.C Slab
RB- 9	R/W Bridge	17+743.604		R.C Slab
RB-10	R/W Bridge	32+086.254		R.C Slab
RB-11	R/W Bridge	33+767.254		R.C Slab
RB-12	R/W Bridge	34+865.000		R.C Slab
RB-13	R/W Bridge	36+704.253		R.C Slab
RB-14	R/W Bridge	37+133.253		R.C Slab
RB-15	R/W Bridge	40+224.253		R.C Slab
RB-16	R/W Bridge	40+224.253		R.C Slab
RB-17	R/W Bridge	40+564.253		R.C Slab
RB-18	R/W Bridge	40+947.253		R.C Slab
RB-19	R/W Bridge	41+821.253		R.C Slab
RB-20	R/W Bridge	42+141.253		R.C Slab
RB-21	R/W Bridge	42+597.253		R.C Slab
RB-22	R/W Bridge	43+229.253		R.C Slab
RB-23	R/W Bridge	44+177.253		R.C Slab
RB-24	R/W Bridge	45+972.253		R.C Slab
RB-25	R/W Bridge	48+677.253		R.C Slab
RB-26	R/W Bridge	50+033.253		R.C Slab
RB-27	R/W Bridge	50+507.253		R.C Slab

10-3. Farm Road Bridge W=4.00m

30

10-4. O&M Road Bridge W=4.00m

4

Table 11.2.2 (3)-23 Quantities(1/4)

Kok-Ing Diversion Canal(1/3)
km. 0+725.00 to km. 12+281

Reach-1 (From BP to No.1Tunnel)
Kok basin L=11.478 m

Items	Spec	Unit	Open Canal L=11,478m	Culvert L=0m	Siphon			Struture & Restoration			Quantity	Remarks
					No.1	No.2	No.3	No.4	Total	Name	Spec	
Site Clearing	rai		729	-	-	-	-	-	-	Bridge		
Stripping	cu.m	193,000	-	-	-	-	-	-	-	Highway	W=11.0m	Nos. 3
Excavation	Soil	cu.m	1,874,000	-	9,360	12,960	9,780	9,800	41,900	Road way	W=7.0m	Nos. 7
	Rock	cu.m	0	-	-	-	-	-	-	Farm road	W=3.0m	Nos. 10
Compacted Fill 95%	cu.m	240,000	-	8,230	10,350	7,980	7,120	33,680	-	O/M road	W=4.0m	Nos. 4
Disposal soil L=2 km	cu.m	1,827,000	-	1,130	2,610	1,800	2,680	8,220	-	Overchute	R.C	Nos. 29
Laterite Compacted	cu.m	17,470	-	107	107	107	107	428	-	-	-	
Rip rap	cu.m	-	625	625	940	625	940	2,815	Drainage Culvert	R.C	Nos. 1	
Sodding	sq.m	244,000	-	-	-	-	-	-	R.C pipe	Nos.	-	
Sand drain with w.h & valve	ea.	11,770	-	-	-	-	-	-	-	-	-	
Concrete Lining S=1:1.5	cu.m	53,260	-	-	-	-	-	-	-	Turn-out	Pipe	Nos. 6
Lean C.	cu.m	-	223	354	270	321	1,168	-	-	-	-	
Reinforced	cu.m	-	2,750	4,570	3,375	4,116	14,811	-	Check Structure	Gate	Nos. 1	With spillway
Form work Lining	sq.m	188,300	-	-	-	-	-	-	-	-	-	
Structure	sq.m	-	3,100	5,240	3,835	4,704	16,879	-	Restoration work			On the culvert
Reinforcing bar	ton	-	330	548	405	494	1,777	-	Highway			
Concrete Joint	ea.	3,930	-	-	-	-	-	-	Road way			
Elastic Filler t=2cm	sq.m	-	118	210	141	190	659	-	Canal			
Water stop Type B	m	-	215	375	255	335	1,180	-	River			
Trash rack	kg	-	21,000	21,000	21,000	21,000	84,000	-	Detour river			
Safety facility	Fence,rope,addi	m	23,000	-	-	-	-	-	road			
U-flume	300*300	m	23,000	-	-	-	-	-	-	-		
Tree plantation @3.00m	noose	7,670	-	-	-	-	-	-	Land acquisition	ha	120	
Steel Pipe,ladder	m,ea.	24eq.	-	-	-	-	-	-	Compensation paddy	ha	120	
Sand trap	L=36m H=1.0m	L.S	1									

Table 11.2.2(3)-24 Quantities (2/4)

Reach-2(From end of No.Tunnel to No2 Tunnel)
km. 15+320.60 to km. 26+197.79 Tak basin L=10,819 m

Items	Spec	Unit	Culvert No.1 L=1279.40m L=5,360m	Open Canal L=4179.77m	Total	Structures & others				Remarks
						Name	Spec	Unit	Quantity	
Site Clearing	rai	rai	40	418	160	618	Bridge			
Stripping	cum	cum	32,000	119,000	128,000	279,000	Road way	W=7.0m	Nos	1
Excavation	cu.m	cu.m	636,200	1,581,000	3,233,000	5,450,200	Farm road	W=3.0m	Nos	6
Rock	cu.m	cu.m	33,500	0	170,200	203,700	O/M road	W=4.0m	Nos	0
Compacted Fill 95%	cu.m	cu.m	557,600	155,000	3,010,300	3,722,900				
Disposal soil	cu.m	cu.m	144,100	1,545,000	520,900	2,210,000	Overchute	R.C	Nos	5
Laterite	cu.m	cu.m	1,830	8,710	6,230	16,770				
Rip rap	cum	cum	-	-	-	0	Drainage Culvert	R.C	Nos	-
Sodding	sq.m	sq.m	-	205,000	-	205,000	R.C pipe	Nos	-	
Sand drain with w.h & valve ea.	ea.	ea.	-	5,360	-	5,360				
Concrete Lining S=1:1.5	cum	cum	-	31,400	-	31,400	Turn-out	Pipe	Nos	2
Lean Conc.	cum	cum	1,410	-	4,600	6,010				
Reinforced Conc.	cum	cum	34,350	-	129,220	163,570	Check Structure	Gate	Nos	1
Form work Lining	sq.m	sq.m	-	87,940	-	87,940				
Structure	sq.m	sq.m	6,655	-	22,700	29,355	Restoration work			
Reinforcing bar	t	t	4,122	-	15,510	19,632	Highway			
Concrete Joint	ea.	ea.	-	1,785	-	1,785	Road way			
Elastic Filler t=2cm	sq.m	sq.m	-	-	-	-	Canal			
Water stop Type B	m	m	-	-	-	-	River			
Trashrack	kg	kg	-	-	-	-	Detour	river	Nos.	3
Safety facility Fence,rope,Jaddr	m	m	-	10,720	-	10,720	Road	road	Nos.	6
U-flume 300*300 nos	nos	nos	-	10,720	-	10,720				
Tree plantation @3.00m nos	nos	nos	-	3,580	-	3,580	Land acquisition	ha	110	
Steel Pipe,ladder m,ea.	m,ea.	m,ea.	-	11ea.	-	11ea.	Compensation paddy	ha	220	O-100m,C-300m
Sand trap L=36m H=1.0m L.S	L.S	L.S	-	1	-	1	Plantation	ha	10	Teak

Table 11.2.2 (3)-25 Quantities (3/4)

1. Open canal

2. Culvert No.1

Kok-Ing Diversion Canal (3/3-1) Ing basin

km. 31+557.25 to km. 55+332.253

Km.31+557.25 to km.35+525.00

Km.35+525.00 to km.37+000.00

L= 3,958.74m

Km.37+000.00 to km.52+750.00

L= 1,344.69m

L=15,750.00m

Km.52+750.00 to km.55+332.25

L= 2,582.25m

L= 2,582.25m

1. Open canal L= 3,958.74m

2.Culvert No.1 L= 1,344.69m

3.Open canal Lined L=15,750.00m

4.Open canal Unlined L= 2,582.25m

Items	Spec	Unit	Ing basin			River Training Mae Loi	Total	Drop structures		Remarks
			Open Canal	Culvert No.1	Open Canal			No.1 Drop	No.2 Drop	
Site Clearing	rai	rai	281	34	1,115	188	15	1,633		
Stripping	cu.m	cu.m	65,000	27,200	264,000	89,000	7,220	452,420		
Excavation	Soil	cu.m	650,000	499,800	2,267,000	707,000	155,600	4,279,400	9,705	19,410
	Rock	cu.m	0	26,300	0	0	0	26,300	0	0
Compacted Fill 95%	cu.m	94,000	411,600	395,000	474,000	77,800	1,452,400	8,040	16,080	
Disposal soil L=6 km	cu.m	621,000	141,700	2,136,000	322,000	85,020	3,305,720	1,665	1,665	3,330
Laterite Compacted	cu.m	6,350	2,120	25,600	4,090	1,350	39,510	140	140	280
Rip rap	cu.m	-	-	-	-	-	-	-	-	410
Sodding	sq.m	69,400	-	287,800	132,930	20,600	510,730	164	164	
Sand drain with w.h & valve	ea.	3,970	-	15,750	-	-	19,720	0	0	
Concrete Lining S=1:1.5	cu.m	19,701	-	79,820	-	-	99,521			
	Lean Conc.	cu.m	-	1,480	-	-	1,480	160	160	320
	Plain concrete	cu.m	-	-	-	-	0	140	140	280
	Reinforced Conc	cu.m	-	34,520	-	-	34,520	1,550	1,550	3,000
Form work Lining	sq.m	64,940	-	258,380	-	-	323,320			
	Structure	sq.m	-	6,840	-	-	6,840	1,900	1,900	3,800
Reinforcing bar	t	-	4,142	-	-	-	4,142	186	186	348
Concrete Joint	ea.	1,220	-	5,250	-	-	6,570			
Elastic Filler t=2cm	sq.m	m	-	-	-	-	0	65	65	130
Water stop Type B	Type B	m	-	-	-	-	0	123	123	246
Trash rack	kg	-	-	-	-	-	0			
Safety facility	Fence,rope	m	7,920	-	31,500	-	-	39,420		
	U-flume 300*300	m	7,920	-	31,500	-	-	39,420		
	Tree plantation @3.00m	nos	2,640	-	10,500	-	-	13,140		
Steel Pipe,ladder	m,ea.	8ea.	-	32ca.	-	-	56m	56m	56m	112m
Bulk gate	set	-	-	-	-	-	4	4	4	8
Sand trap	L=36m H=1.0m	L.S	1	-	-	-	1			

Table 11.2.2 (3)-26 Quantities (4/4)
 Kok-Ing Diversion Canal (3/3-2)
 Ing basin
 km. 31+557.25 to km. 55+332.253

1. Open canal
 Km.31+557.25 to km.35+525.00 L= 3,958.74m
 Km.35+525.00 to km.37+000.00 L= 1,344.69m
 2. Culvert No.1
 Km.37+000.00 to km.52+750.00 L=15,750.00m
 3. Open canal Lined Km.52+750.00 to km.55+332.25 L= 2,582.25m
 4. Open canal Unlined Km.52+750.00 to km.55+332.25 L= 2,582.25m

Structures & others		Unit	Ing basin		Total	Remarks
Name	Spec		Open Canal Lined	Culvert No.1		
Bridge						
Highway	W=11.0m	Nos	-	-	2	2
Road way	W=7.0m	Nos	4	-	14	18
Farm road	W=3.0m	Nos	4	-	10	14
O/M road	W=4.0m	Nos	-	-	-	0
Overchute	R.C	Nos	1	-	11	12
Drainage Culver R.C		Nos	-	-	-	0
R.Cpipe	D=1.00m*1rows	Nos	1	-	5	6
	D=1.00m*2rows	Nos	2	-	2	4
	D=1.00m*3rows	Nos	-	-	2	2
Turn-out	Pipe	Nos	2	-	4	6
Check Struture	With gate	Nos	1	2	-	3
Restoration work						
Highway	Nos.		0		0	0
Road way	Nos.		5		5	5
Canal	Nos.		2		2	2
River	Nos.		2		2	2
Detour	River	Nos.	2	5	7	Temporary
	Road	Nos.	4	5	16	25
Land acquisition	ha	50	10	180	40	280
Compensation	Paddy	ha	40	40	160	30
	Plantation	ha	10	10	10	10
						Orchard, teak

Table 11.2.2 (3)-27 Spoil Bank Volume and Area (1/2)

Kok-Ing Canal (1/2)

Reach	Canal Type	STA(km) From To	Length (m)	Earth work volume('1000m ³)			Proposed Area & Volume		
				Stripping	Excavation	Fill	No.	Area (ha)	Height (m)
1	Open	0+725	12+281	193	1,875	240	1,828		H=390.5-389.5
1-1	Open	From B.P to Kok-Lao siphon		120 ^{m3/m} *2895 ^m =			347	1	1.0
		0+725	3+620	2895			2	4	40
							3	37	370
							51	510	510
		S.Total							
1-2	Open	From Kok-Lao to Nam Mae Hang Siphon		150 ^{m3/m} *5380 ^m =			807	4	1.5
		3+620	9+000	5,380			5	35	525
							38	570	1,080
		S.Total							
1-3	Open	From Nam Mae Hang Siphon to Kok-Ing No.1 Tunnel		Eq =78.72 1828-(347+807)=			674	6	1.5
		9+000	12+281	3,203			7	10	225
							8	7	150
							9	18	105
							50	270	-do-
							139	750	-do-
								1,830	
		S.Total		1,828					
		Total		11,478					

Table 11.2.2 (3)-28 Spoil Bank Volume and Area (2/2)

Kok-Ing · Canal (2/2)

2	15+321	26+140	10,819	Kok-Ing No.1 Tunnel to Kok-Ing No.2 Tunnel
2-1 Culvert	From Kok-Ing No.1 Tunnel to end of culvert			
15+321	16+600	1,279	32	669
2-2 Open	From end of culvert to Huai Tin Non			
16+600	18+600	2,000	119	1581
			250 $m^3/m * 2000^m =$	155
Open	Huai Tin Non to BP of culvert			
18+600	21+960	3,360	1350-500=	1,045
S.Total				1,545
2-3 Culvert	21+960	26+140	4,180	128
Total			10,819	3,403
3	31+557	55+332	23,634 Eq = -141	From Kok-Ing No.2 Tunnel to end of canal
3-1 Open	31+557	35+525	3,957 Eq = -11	
3-2 Culvert	35+525	37+000	1,345 Eq = -130	65
3-3 Open	37+000	48+000	11,000	650
Open	48+000	55+332	7,332	94
Total			23,634	869

11.2.3 Ing Weir

(1) Design Concept and Criteria

(a) Diversion Weir and Intake Site

It is proposed that the Ing diversion weir is constructed at the upstream of the confluence with the Lao River, and that an intake structure is provided at 100 m upstream of the proposed weir on the right bank. The diversion weir site and surrounding area lower than EL. 364 m is remained as uncultivated area of 500 ha and have a large retardation effect against flood from the tributaries as well as the Ing River.

(b) Concept of Structural Design

It is required to preserve the current regulating function not only for flood control but also for the existing natural environment. Also, this function is necessary to be effectively utilized for taking water from the Ing River and the diverted water of the Kok river.

Whilst, during the dry season, there is scarce water resources and the farmers have desired water for irrigation use. Furthermore, it is possible to enhance freshwater fishery by storing river water flow in the reservoir at the end of the wet season.

Based on the mentioned basic consideration for facilities, the design water level of the gate is studied to enable farmers to use stored water for irrigation in the surrounding area and enhance fishery during the dry season.

There will be possible impact on fish migration when the gates are closed. Therefore, it is necessary to design the diversion weir with fish-way.

(c) Design Water Levels for Diversion Weir and Intake Structure

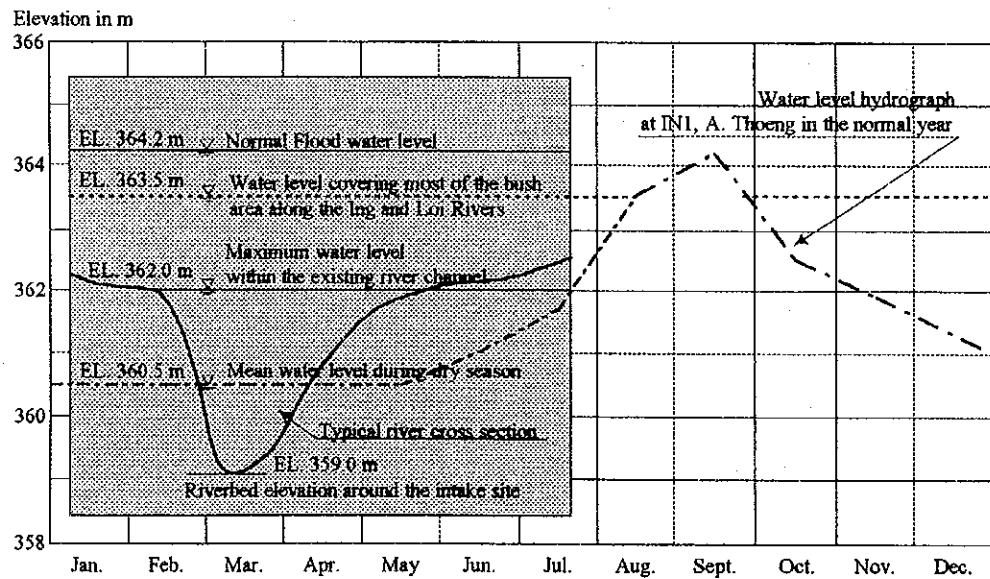


Figure 11.2.3-1 Water Level Hydrograph at Ing Diversion Weir Site

Setting the design water level at EL. 363.5 m, the river water level is required to be controlled, excluding the peak wet season from August to September. Due to this change of river water level in

the upstream of the Ing diversion weir, the existing bush or reed areas will be inundated through a year.

The environmental study of the Team J/V indicated that there is no rare and endangered animals and species in the wet lands along the Ing river, and that the creation of ponds during the dry season will provide a habitat area for fishes and an opportunity of water use for farmers living in the upstream reaches.

Consequently, the water level of EL. 363.5 m is applied for design of the proposed diversion weir and an intake gates.

Design flood water level of EL 368.9 m is proposed based on hydraulic analysis for the design flood discharge of 760 cu.m/s with a probability of once in 100 years. The crest elevation of concrete weir and flood embankment is set at EL. 370.4 m, adding free board of 1.5 m to the aforesaid design flood water level.

(d) Gate type of diversion weir

The Team J/V proposed a rubber gate with a span length of 90 m in the Interim Report and afterwards selects the steel slide gates with four (4) leaves in the draft Final Report, since it is identified that the existing rubber gates in Thailand are sometimes broken by the inhabitants due to water allocation problems and that it is subject to smooth closing of gates, though the rubber gate have an advantage on cheaper construction cost and simple operation.

However, the objective of the diversion weir is to control the river water level at EL 363.5 m for about two (2) months at the beginning and end of the wet season and it is low possibility that the rubber gate is broken due to water allocation problems. The appropriate number of spans will solve the second problems above-mentioned.

The JICA Study Team recommends adopting the rubber gate type for diversion weir.

(e) Layout and conditions of the diversion weir and intake structures

The proposed diversion weir comprises; a) concrete weir with two (2) rubber gates, b) three (3) types of fish-way, c) a bridge structure connecting the right and left riverbanks for operation and maintenance, and d) river structures such as revetment and riverbed protection works.

The proposed intake structures consists of; a) a silting basin, b) an intake tower and gate(s), c) flood embankment surrounding intake tower, and d) river structures such as revetment and riverbed protection works.

It is designed to provide the rubber gate of two (2) spans with an unit span length of 32 m and the bridge structure laid out at the downstream of the rubber gates.

A silting basin is planned to be provided between the existing river channel of the Ing and the intake tower, in order to deposit the river sand with a grain size of more than 0.3 mm to be conveyed by the Ing River and the diverted water.

Slide steel gate is selected from the advantage on accurate operation comparing with the tender-gate type, in order to strictly control the amount of the diverted water according to fluctuating river water level. Size and number of gates are determined taking into account economical and operational view points.

Such river structures as revetment and riverbed protection works are planned to provide at

downstream of the diversion weir, inlet portion of the silting basin and in front of the intake tower.

(2) Review of Structural Design Made by the Team J/V

Through exchanging the design concept and criteria, the following differences are identified:

Table 11.2.3-1 Comparison of Main Features designed by Team J/V and JICA Study Team

Main Features	Team J/V	JICA Study Team
1) Ing Diversion Weir a) Weir site b) DWL c) DFWL d) Type of gates e) No. of gates f) Width of weir g) Fish-way	5 km upstream of the existing bridge EL. 363.5 EL. 368.21 m Fixed wheel gate 12.5 m @ 4 nos. 57.5 m Provided	Same location EL. 363.5 m EL. 368.9 m Rubber gate 4.8 m x 32 m @ 2 nos. and 5 m x 3.5 m @ 1 no. 66 m Three types: ladder, vertical slot and slope types
2) Ing Intake a) Intake structure site b) Design Intake W.L. c) Width of silting basin d) Width of Intake e) Type of Gate f) No. of gates	Same location of the diversion weir EL. 363.5 m 65 m with a length of 300 m 27.6 m Roller gate 6 m @ 4 nos.	Same location EL. 363.5 m 230 m with a length of 415 m 77.5 m Fixed wheel gate 5 m@2 nos., 10 m@4 nos., and 12 m @ 1 no.

Through the review of study made by the Team J/V, it is concluded that the concept of design applied to the study is reasonable, but further consideration about sedimentation and gate types are required to be given in the next stage of the Project.

(3) Design by JICA Team

The Ing diversion weir has been designed on the basis of the mentioned consideration and conditions. Figures 11.2.3-2 to -5 show the general layout plan and profile of the Ing intake structures by means of non-conventional design method applying the design flow velocity of 0.2 m/s in the silting basin and 0.8 m/s at the intake gates. The main feature of the structures is given as follows:

Ing Diversion Weir

- Catchment area : 4,400 km²
- Design flood discharge : 760 cu.m/s with a probability of once in 100 years
- Flood water level : 368.9 m
- Width of weir : 66.0 m
- Sill elevation : 358.7 m
- Crest elevation : 370.4 m
- Gate type : Rubber gate
- Gate size : 2 nos. with 32.0 m (width) and 4.8 m (height)

Ing Intake

• Flood water level	:	368.9 m
• Design water level for intake gate	:	363.5 m
• Design discharge	:	175 cu.m/s
• Width of intake	:	77.5 m
• Width of silting basin	:	230 m
• Sill elevation	:	360.0 m
• Crest elevation	:	370.4 m
• Gate type	:	Fixed wheel gate
• Gate size	:	1 no. with 12.0 m (width) and 2.0 m (height) 4 nos. with 10.0 m (width) and 2.0 m (height) 2 nos. with 5.0 m (width) and 2.0 m (height)

11.2.4 Ing-Yot Diversion Canal

(a) Hydraulic condition

Basic hydraulic design dimensions and formula are follows.

Basic design dimension

- Maximum design discharge Ing-Yot diversion canal	175 cum/s
- Ing intake water level	NWL 363.50 m M.S.L
- Yao flood control dam	NWL 320.00 m M.S.L

Hydraulic formula

Manning's formula is applied in canals and flow condition is designed as uniform flow

$$\text{Manning's formula} \quad Q = A \times V \quad V = R^{2/3} \times S^{1/2} / n$$

Maximum flow velocity and free board are same as description of Kok-Ing diversion canal.

Hydraulic Gradient

Hydraulic gradients of Ing-Yot diversion canal are applied same value as Kok-Ing diversion canal. Hydraulic heads is appropriately enough for canal design.

- Open canal with Lining	1/5,000
- Culvert	1/2,500

(b) Open Canal

Canal Type and Lining

Open canal type would be applied for trapezoid concrete lining type by the reason of widespread in Thailand, with technical, economical and constructional experience.

Longitudinal gradient of canal slope

Relating with canal velocity and cross section, canal section with steep slope shows high velocity in small section and increases the excavation depth. Canal longitudinal slope would be generally decided taking followings into consideration.

- Purpose of canal and lining condition
- Required water level at turn out
- Total energy and arrangement of canal type
- Topographical condition
- Balance of earthwork volume (Excavation and filling volume)
- Hydraulic most effective cross section, Allowable velocity

This diversion canal is excavated type under the ground, and has no turnouts. Longitudinal slope is decided as $S=1/5,000$ for open canal and $S=1/2,500$ for culvert and tunnel taking hydraulic

conditions. The canal dimensions are shown in Table 11.2.4-2

Longitudinal gradients and velocity in open canal is shown in Table 11.2.4-4.

Table 11.2.4-4 Longitudinal Gradients and Velocity in Open Canal

Gradient	D=3.00m		d=3.50m		d=3.795m		Remarks
	W(m)	V(m/s)	W(m)	V(m/s)	W(m)	V(m/s)	
I/ 3,000	23.70	2.07	17.70	2.18	15.00	2.23	
1/ 5,000	31.00	1.65	23.40	1.75	20.00	1.80	$V_{max} = 1.80$
I/ 7,000	36.80	1.41	28.00	1.51	24.20	1.55	
1/10,000	44.20	1.20	33.90	1.28	29.10	1.33	

Where d: Water depth (m) W: Bottom width V: Velocity (m/s)

Free board

Free board (Fb) and lining height (Hc) of canal would be employed 0.70m and 4.50 m, respectively.

In case of flood or miss operation of gates, discharge of 237 cu.m/s, which is 1.35 times of design capacity, can flow with in free board.

(c) Culvert

Culvert Section

The culvert covered by backfill is used for deep excavation portion, which excavation depth is over 15 meter. Culver canal type would be applied for concrete horseshoe type reinforced by steel bar taking earth/hydraulic pressure and economical conditions into consideration. Culver canal is generally classified as Table 11.2.4-5.

Table 11.2.4-5 Land Acquisition Width and Excavation Volume in Culvert Types

In case of Q=140 cu.m/s, S=1/2,500 and water surface 15m under ground level

Canal type (Reinforced concrete)	Water Depth	Size H*B*rows	Excavation Width	Excavation Volume	Cost
Rectangular type	3.85 m	4.55*3.85*6	72 m	790 cu.m	High
Circular type	7.20 m	D=9.00 m	57 m	640 cu.m	Medium
Horse shoe type	7.00 m	D=8.70 m	56 m	620 cu.m	Medium

Longitudinal Gradient of Culvert

Longitudinal gradient of culvert is designed with more rapidly velocity than open canal to reduce cross section. Longitudinal slope of culvert is decided as S=1/2,500 taking hydraulic conditions including total energy from Kok to Ing river into consideration.

Longitudinal Gradients and Velocity in culvert is shown in Table 11.2.2.4-6 and Table 2.4.-7.

Table 11.2. 4-6 Longitudinal Gradients and Velocity in Culvert

Gradient	Rectangular		Circular		Horse shoe		Remarks
	W(m)	V(m/s)	D(m)	V(m/s)	D(m)	V(m/s)	
I/ 2,000	21.40	1.70	8.60	2.83	8.40	2.80	
1/ 2,500	23.10	1.57	9.00	2.61	8.70	2.57	
I/ 5,000	32.10	1.13	10.20	2.01	10.00	1.99	

Where D: Diameter (m) W: Bottom width V: Velocity (m/s)

Culvert section with diameter 8.70 m and water depth of 7.00 m is selected taking water velocity into consideration. The dimensions of canal section are as follows.

Discharge Q(cu.m/s)	Diameter (m)	Water depth d(m)	Flow area A(sq.m)	Coefficient Roughness n	Longitu .Slope	Velocity V(m)	Remarks
140.00	8.70	7.00	54.56	0.015	1/2,500	2.57	

(d) Siphon

Location

Lao siphon with capacity of 175 cu.m/s is placed at down stream of tunnel to cross under Lao river. Inverted siphons with covering of 1 or 1.5 m earth is buried under the riverbed. Trash rack would be provided for maintenance and safety in front of inlet of siphon. And bridge for maintenance road would also provided.

- LengthL=185 m (No.4+845 to 5+030)
- Water level381.44 m.M.S.L River bed level384.6 m.M.S.L

Cross section

The section of siphon is usually decided with about 1.5 times velocity of open canal one to reduce cross section area, without hydraulic restriction. Siphon type would be applied for circular type because of large section. D=8.25m, V=2.70 m/s

Loss Head

Loss head by siphon consist of transition loss, trash rack loss, friction loss, bend loss and Inlet-outlet loss. Total head loss is calculated as 0.85m.

(e) Detail hydraulic calculation

Diversion canal length and detail hydraulic calculations are shown in Table 11.2.4-8 and 9. Results of calculation is shown in Data Base Map

(f) Quantity

Quantities are shown in Table in 11.2.4-10

(g) Spoil bank volume and area

Calculations of spoil bank volume and area are shown in Table 11.2.4-11 and location of spoil bank area is shown in Data Base Map.

Table 11.2.4-7 Hydraulic Dimensions in Ing-Yot Culvert

$Q=175 \text{ m}^3/\text{s}$

Rectangular type		d m	b m	Section z	P m	n	I (slope)	A sq.	R m	V m/s	Q cum/s						
3.795		26.50	H=4.55 B=3.80*7	0.00	79.63	0.015	1/2000	0.0000500	100.57	1.26	175.16						
3.795		29.90	H=4.55 B=3.75*8	0.00	90.62	0.015	1/2500	0.0000400	113.47	1.25	175.76						
3.795		33.00	H=4.55 B=3.70*9	0.00	101.31	0.015	1/3000	0.0000333	125.24	1.24	175.57						
3.795		41.80	H=4.55 B=3.90*11	0.00	125.29	0.015	1/5000	0.0000200	158.63	1.27	175.04						
		$d/2r=1.60$		$d/r=0.80$	$V<3.00 \text{ m/s}$		$Qn/(I^{0.5}*r^{(8/3)})$										
$d/2r$	$\alpha=A/r^2$	P/r	$\beta=R/r$	$\beta^{(1/2)}$	$\beta^{(2/3)}$	$\alpha \beta^{(2/3)}$	Q m^3/s	n	I (slope)	r m	A sq. m	R m	V1 m/s	Q m^3/s	d m		
Circular type																	
0.80	2.6943	4.4286	0.6084	0.78	0.718	1.9435	175.00	0.015	1/2000	0.0000500	4.65	4.70	59.517	2.859	3.003	178.74	7.52
0.80	2.6943	4.4286	0.6084	0.78	0.718	1.9435	175.00	0.015	1/2500	0.0000400	4.85	4.90	64.690	2.981	2.762	178.66	7.84
0.80	2.6943	4.4286	0.6084	0.78	0.718	1.9435	175.00	0.015	1/3000	0.0000333	5.02	5.05	68.711	3.072	2.572	176.75	8.08
0.80	2.6943	4.4286	0.6084	0.78	0.718	1.9435	175.00	0.015	1/5000	0.0000200	5.53	5.55	82.991	3.377	2.122	176.11	8.88
Horse shoe																	
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	175.00	0.015	1/2000	0.0000500	4.54	4.55	59.408	2.791	2.955	175.55	7.28
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	175.00	0.015	1/2500	0.0000400	4.74	4.75	64.745	2.914	2.720	176.11	7.60
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	175.00	0.015	1/3000	0.0000333	4.90	5.00	71.740	3.067	2.569	184.33	8.00
0.80	2.8696	4.6785	0.6134	0.7832	0.7219	2.0716	175.00	0.015	1/5000	0.0000200	5.40	5.40	83.678	3.312	2.095	175.30	8.64

Table 11.2.4-8 Diversion Canal Length of Ing Yet Diversion Canal

STA	Canal Type	Reeach/No.	Length (m)					Remarks
			OpenCanl	Culvert	Siphon	Structure	Tunnel	
0 + 724.250								
	Open Canal	Reach-1	1475.750					
2 + 200.000								
	Culvert	Reach-1		360.000				
2 + 560.000						2000.000		
4 + 560.000								
	Culvert	Reach-2		285.000				
4 + 845.000								
	Siphon	Nam Mae Lao			185.00			
5 + 30.000								
	Culvert	Nam Mae Lao		8806.952				
13 + 836.952								
Total			1475.750	9451.952	185	2000.000	0	13112.702

Table 11.2.4-9 Hydraulic Computation of Ing-Yot Diversion Canal

Station (KM)	Structure	Q_{out} (m^3/s)	b (m)	d (m)	H_C (m)	H (m)	L.S. -	S.S. -	n	A (m^2)	R (m)	V (m/s)	h_y (m)	Distance, ΔL (m)	Head Losses (m)	Height of ΔH FSL. Provide E.G.L.	'BL'	Living El.	Top Conc TBL.	Remark		
0+030.750	Beginning of Approach Channel	175.00	174.216	230.00	4.000	-	very	1:	700.000	1.20	0.016	952.000	3.840	0.183	0.002	363.502	363.490	359.500	-	370.100		
0+031.5	End of Approach Channel	175.00	174.216	230.00	4.000	-	very	1:	700.000	1.20	0.016	952.000	3.840	0.183	0.002	363.501	363.499	359.499	-	370.100		
175.000	Inlets Structure 10-12/06x2.00 m. Fixed Wheel Gates															340.000	0.480	0.327		$\Delta W.S. = 0.399 \text{ m}$		
0+355	Beginning of Concrete Lined Canal	175.00	175.018	20.00	3.795	4.50	very	1:	5.000	1.15	0.016	97.503	2.895	1.795	0.164			363.264	363.100	359.305	363.805	370.100
2+200	End of Concrete Lined Canal	175.00	175.018	20.00	3.795	4.50	very	1:	5.000	1.15	0.016	97.503	2.895	1.795	0.164	1,445.000	0.289	0.289				
2+230	Beginning of Cut & Cover Conduit	175.00	175.093	r=4.75	7.550	H=9.300	-	1:	2.500	-	0.015	64.373	2.913	2.720	0.377			362.975	362.811	359.016	363.516	370.100
2+560	End of Cut & Cover Conduit	175.00	175.093	r=4.75	7.550	H=9.300	-	1:	2.500	-	0.015	64.373	2.913	2.720	0.377			362.871	362.494	354.944	364.444	-
2+590	Inlet of Tunnel No.1	175.00	174.981	r=5.45	6.692	H=8.175	-	1:	2.500	-	0.015	65.807	2.817	2.659	0.360			350.000	0.132	0.132		
3+500	End of Sheet 1 & Beginning of Sheet 2	175.00	174.981	r=5.45	6.692	H=8.175	-	1:	2.500	-	0.015	65.807	2.817	2.720	0.377			362.739	362.362	354.812	364.312	$\Delta W.S. = 0.317 \text{ m}$
4+530	Outlet of Tunnel No.1	175.00	174.981	r=6.45	6.692	H=8.175	-	1:	2.500	-	0.015	65.807	2.817	2.659	0.360			30.000	0.017	0.017		$\Delta W.S. = 0.008 \text{ m}$
4+550	Beginning of Cut & Cover Conduit	175.00	175.093	r=4.75	7.550	H=9.500	-	1:	2.500	-	0.015	65.807	2.817	2.720	0.377			362.722	362.362	355.670	363.845	-
4+845	Beginning of Niam Mae Lao Siphon	175.00	175.093	r=4.75	7.550	H=9.500	-	1:	2.500	-	0.015	64.373	2.913	2.720	0.377			91.000	0.364	0.364		
5+030	End of Niam Mae Lao Siphon	175.00	175.093	r=4.75	7.550	H=9.500	-	1:	2.500	-	0.015	65.807	2.817	2.659	0.360			362.946	361.586	354.894	363.069	-
7+000	End of Sheet 2 & Beginning of Sheet 3	175.00	175.093	r=4.75	7.550	H=9.500	-	1:	2.500	-	0.015	64.373	2.913	2.720	0.377			361.817	361.440	353.820	363.390	$\Delta W.S. = 0.032 \text{ m}$
10+500	End of Sheet 3 & Beginning of Sheet 4	175.00	175.093	r=4.75	7.550	H=9.500	-	1:	2.500	-	0.015	64.373	2.913	2.720	0.377			360.515	360.138	352.588	351.188	$\Delta W.S. = 0.554 \text{ m}$
13+365.652	End of Cut & Cover Conduit and Inlet of Ing-Yot Tunnel (Tunnel No.2)	175.00	175.093	r=4.75	7.550	H=9.500	-	1:	2.500	-	0.015	64.373	2.913	2.720	0.377			357.780	357.403	349.853	359.353	-