

			TaDI	C7-7-7-11310	-43 ABC	INCOULD U	T TOURT A	THE RESERVES OF THEOREMENT A CONTACT (1)	(11)					
		Samiling Denth	Unit Weisht	Absorption	Ultra Sonic	Velocity	Young ratio	Poisson	U.C.S	Petrographic	Boi	Boring Core Condition	ų	Performed
Location	Borchole No.	mater a grant march	( a/cm	Weight (%)		Vs(km/s)	(Gpa)	Ratio	(kgf/cm <sup>2</sup> )	Examination	Form. Name	Geology	Rock Class.	Ъу
	Ash Pridate	30.60 - 30.80	2.63		5.87	2.91	59.8	0.34	506.3	Granite	PTR	Granite	сW	Thai side
the state of the second st	DUNDATE TO A	63.00 - 63.30	275		5.73	2.81	51.2	0.37	937.4	-		Tuff	Ð	Thai side
	DUNDAL PLAN	00.00 - 00.00 66.60 - 66.90	2.70		5.00	3.20	63.7	0.18	367.7	(Micro)diorite		Diorite	НЭ	Thai side
	Triver 1 criderin	37.10 - 37.40	2.62		6.48	2.95	65.6	0.37	953.5	(Meta)basalt	An	Basalt	Η	Thai side
Kok-ing re- induce	T-AT MONITAL	AS 30. AS 50	2.76		6.16	3.08	6.69	0.33	1,212.2			Basalt	Ð	Thai side
	DENVELTED T	63 M - 63 30	2.77	1	6.34	3.54	83.8	0.27	2,784.0	Dacite porphyry		Porphyry	H	Thai side
	Duren i	50.05 - 50.25	2.72	1	6.34	3.06	66.0	0.35	445.0		P2	Marble	No.	Thai side
Kok lež vo / hube:		30.00 - 30.60	2.79		6.29	3.35	81.6	0.30	836.9	Slate	PIR	Shale	CH B	Thai side
		132.60 133.30	271	0.42	5.52	3.14	1.78	0.26	32.1		P3	Andesite	ъ	JICA side
	Puttoria X	142 00 - 142 30	2.71	0.06	6.04	2.99	64.8	0.34	307.8	Andesite		Andesite	СM	JICA side
	PUBLA <	143 20 - 143 60	2.76	0.03	6.21	3.11	71.0	0.33	590.3	Andesite		Andesite	GM	<b>JICA side</b>
	DHRIA 5	148.40 149.00	2.76	0.03	6.54	2.73	57.4	0.39	685.2	Andesite		Andesite	Ч	JICA side
	NAAPERO'	50.45 - 50.65	2.69	,	3.66	2.29	32.9	0.19	229.1		CPab	Shale	E	Thai side
		05.50 - 96.00	2.63		4.75	2.64		0:30	566.4	(Meta-)sandstone	TRhf	Sandstone	H	Thai side
	DEKADICE	114 55 - 114.80	272		4.50	2.57	45.4	0.26		1		Sandstone	HO	Thai side
	DIMANNES	119.55 - 120.00	2.73		5.41	2.92	60.0	0.29	1,983.4	1		Sandstone	ا بم	Thai side
		42.00 - 42.25	2.68		5.71	2.77	55.6	0.35	983.0	Meta-sandstone	TRbf	Sandstone	Ϋ́	Thai side
	Derahi.	52 50 - 52 80	254	1	6,19	3.94	91.7	0.18	467.0	1		Sandstone	CH	Thai side
	Sugar.	48.50 - 48.80	2.55	1	4.08	2.27	33.5	0.28	228.1	1		Sandstone	Š	Thai side
	Fighter	67.50 - 67.80	1991		5.72	2.91	59.9	0.33	1,069.8	Granite porphyry	PIRgr	Granite porphyry	р Д	Thai side
		100.75 110.00	271		5.08	2.09	33.1	0.40	418.0	Slate	~	S.s.& shale alt.	CH	Thai side
	DUPRED	126.50 - 126.65	2.70		3.12	1.89	23.7	0.22	247.2	Slate		S.s.& shale alt.	м О	Thai side
		45.10-45.35	273		3.35	1.76	22.1	0.31	248.0		CPnb	Shale	CH	Thai side
	TOPPT 16 C	45.40 - 45.60	2.72		3.42	1.75	22.0	0.32	47.8	-		Shale	CH	Thai side
	DHRLIK 5	73.20 - 73.35	2.70		3.21	1.76	21.5	0.29	174.2	Slate		Slate	CM	Thai side
	DEPT-16.5	160.20 - 160.80	2.74	0.35	4.00	2.04	30.1	0.32	65.8	Slate		Slate	ß	JICA side
	DHR1-16.5	183.40 - 184.00	2.75	0.07	3.98	2.44	39.2	0.20	404.7	Slate		Slate	Н	JICA side
	DHRI-16.5	188.10 - 188.60	2.76	0.19	4.95	2.81	54.9	0.26	<u>123.8</u>	Slate		S.s.& shale alt.	S.	JICA side
	DERI-16.0	157.30 - 157.50	2.69	         	5.30	2.32	40.0	0.38	65.3	Slate (with s.s.)	CPab	S.s.& shale alt.	GM	Thai side
	DHRI-18.0	165.60 - 166.00	2.67	0.04	5.67	3.13	60.9	0.28	287.2	Sandstone		Sandstone	Ŋ	JICA side
	DBRJ-18.0	185.60 - 186.00	2.65	0.03	5.86	3.01	63.3	0.32	1,173.3	Sandstone		Sandstone	B	JICA side
	DHR1-18.0	196.30 - 197.00	2.68	0.04	5.70	2.62	50.3	0.37	<u>678.8</u>	Sandstone		Sandstone	S	JICA see
	<b>DHR1225</b>	189.50 - 189.90	2.77	0.13	4.22	2.55	43.7	0.21	177.0	Slate	CPab	S.s.& shale alt.	E	JICA side
	DIRN 22.5	190.40 - 191.00	2.73	0.06	5.33	2.36	42.0	0.38	101.4	Slate		S.s.& shale alt.	Ð	JICA side
	DHRI 22 \$	194.00 - 194.60	2.73	0.10	4.30	2.48	42.0	0.25	406.4	Slate		Slate	M	<b>JICA side</b>
	DHBV 22.5	201.00 - 201.40	2.70	0.14	4.12	2.43	39.3	0.23	174.1	Sandstone		Sandstone	CH	JICA side

Table 11.2.2-23 The Results of Laboratory Test (1)

Table 11.2.2-24 The Results of Laboratory Test (2)

Location	Borehole No	Sampling Depth [Unit Weight] Absorption Ultra Sonic Velocity	Unit Weight	Absorption	Ultra Sonic V	elocity	Young ratio	Poisson	U.C.S	Petrographic	Bc	Boring Core Condition	ion	Performed
TOCHENIN	TOOLETING INO.	(E)	(g/cm <sup>2</sup> )	Weight (%)	Vp(km/s)	Vs(km/s)	(Gpa)	Ratio	(kgf/cm <sup>*</sup> )	Examination	Form. Name	Geology	Rock Class.	γď
big-Vot No.2 hinnel	DHBJ 26.0	258.00 - 259.00	2.78	0.02	6:30	3.29	79.3	0.32	531.0	Dacite	PTRv	Dacite	CH-B	JICA side
	DHBI-26.0	265.00 - 266.00	2.75	0.03	5.89	3.00	65.7	0.33	1,098.4	Tuff		Tuff	CH-B	JICA side
	DHRI-26.0	270.00 - 271.00	2.80	0.04	2.11	3.14	66.1	0.20	566.4	Tuff		Tuff	СН	JICA side
	DHBI 26.0	276.00 - 277.00	2.77	0.06	3.76	2.42	37.1	0.15	820.6	Tuff		Tuff	CH	JICA side
	DHBU 33.0	181.50 - 181.80	2.71		4.25	2.73	48.4	0.15	888.1	Tuff(Marble)	TRM	Theff	сM	Thai side
	DHBJ-33.0	198.30 - 198.60	2.74	1	5.42	3.31	74.1	0.18	1.229.0	(Meta-)tuff	•	Tuff	СН	Thai side
	DHB1-33.0	273.00 - 274.00	2.67	0.22	3.81	2.48	37.1	0.13	776.1	Tuff		Tuff	СН	JICA side
	DHBU-33.8	289.00 - 290.00	2.72	0.04	5.36	2.59	49.2	0.35	650.5	Tuff		Tuất	CH	JICA side
	DHBI 33.0	296.00 - 297.00	2.66	0.13	4.69	2.68	48.0	0.26	1,150.3	(Silicified) tuff		Tuff	СН	JICA side
	DEB46SP	57.20-57.50	2.72		6.49	2.56	50.2	0.41	2,007.8		TRpI	Limestone	CH	Thai side
	DEBAKSP	71.50 - 71.75	2.69		6.51	3.42	82.5	0.31	1,101.5	Limestone		Limestone	сM	Thai side
	DHB46SP	89.25 - 89.50	2.72	1	6.53	2.58	51.2	0.41	772.2	1		Limestone	сM	Thai side
	DEBSOSP	77.30 - 77.60	2.69		5.50	3.07	64.6	0.27	181.4	(Meta-)sandstone	TRhf	Sandstone	CM	Thai side
Ing-Yot No.2 tunned (197)	DHA-1	- 27.5	. 1	1	1	1	1	1	1,523.4	}	TRpn	Tuff	CH	Thai side
	DHB-7	52.0	-				· •		1,978.3		TRpi	Limestone	B	Thai side
	DEB	48.0	1	1	1	1	1	1	1,267.9	-	TRhf	Tuff	CH	Thaî side
Ing-Yot No.2 tunnet ('96)	DHC-1	29.5				1		1	1,032.0		TRpn	Siltstone	CH-B	Thai side
(south route)	DAC 2	64.5			1			1	271.3		nus3	Sandstone	ថ	Thai side
* Unit weight (Bulk S.G.) = W(dry) / Volume	(dry) / Volume													

\* Poisson's ratio, GPa =  $1.0197 \times 10^{4}$  kg/cm<sup>2</sup>

\* U.C.S. : Uniaxial compressive strength, in case of getting two data at the same sample, higher strength data is adopted.

Tensile strength (by Brazilian test), DHBJ22.5 (194.0-194.6 m) : 97.9 kgf/cm<sup>2</sup>, DHBJ26.0 (270.0-271.0 m) : 227.4 kgf/cm<sup>2</sup>
 Point load strength (by point load test), DHBJ22.5 (194.0-194.6 m) : 18.5 kgf/cm<sup>2</sup>, DHBJ26.0 (270.0-271.0 m) : 10.0 kgf/cm<sup>2</sup>

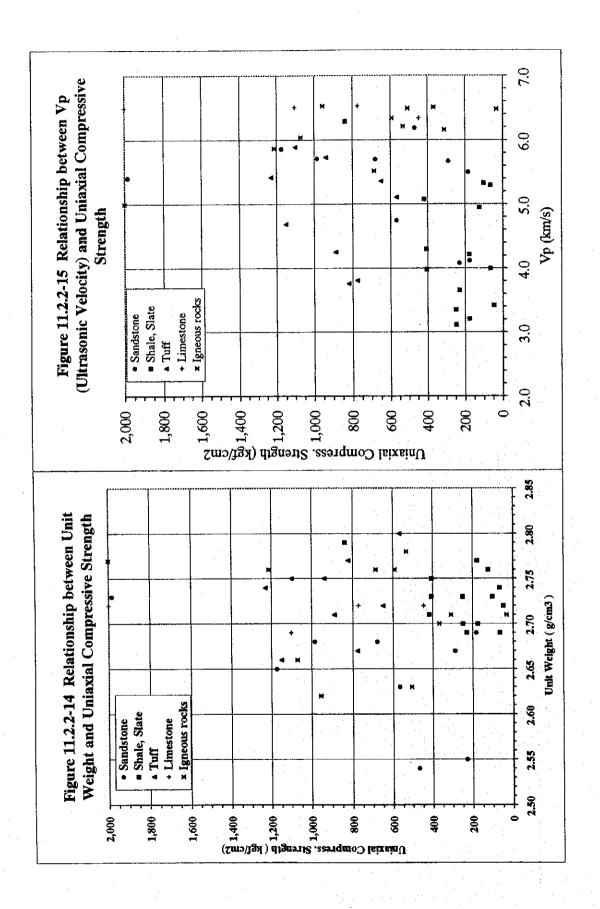
Intender (A)         Control (A) <thcontrol (a)<="" th=""> <thcontrol (a)<="" th=""></thcontrol></thcontrol>		;	011	1 Iten Scein Valority	ory lest Velocito	ID-5111 1CS	r lest	Short	Long	as (	Gamma (	щ	<b>Boring Core Condition</b>	lition
Districtive interventing         State         Sta	Location	Borehole No.	Sampling Depth		Vs/fm/s)	- 14	Vs/tm/s)	(ohm/m)	(ohm/m)	(m)	(ed-)	Form. Name	Geology	Rock Class
MARIENTING         GIOD GAD         STD         Description           DISCRETTING         FOUN GAD         GIO         230			30 60 - 30 80	5.87	10 2	╋╌		510	130	-135	38	MIA	Granite	ъ М
Totactivity:         Constraints         Constraints <thconstraints< th=""> <thconstraints< th=""></thconstraints<></thconstraints<>	South Front South	DHKRITI-JSP	63.00 - 63.30	5.73	2.81	1	1	885	905×	-180	61		Tuff	CH
MULTION         3710. 710. 610. 610         646         293 <t< td=""><td></td><td>DHKENTL-ISP</td><td>66.60 - 66.90</td><td>5.00</td><td>3.20</td><td>1</td><td>1</td><td>1</td><td>1</td><td></td><td>1</td><td></td><td>Diorite</td><td>Ð</td></t<>		DHKENTL-ISP	66.60 - 66.90	5.00	3.20	1	1	1	1		1		Diorite	Ð
(HEREFLY)         (S.10)         (S.14)         (S.1	The No.2 Vinnel	DHKBJT2.	37.10 - 37.40	6.48	2.95	1	ļ	1	: 1	1		An	Basalt	CH
MARTIFAL         G.0.6. G.3.0         G.4         3.54 <th< td=""><td>(B. Linnite)</td><td>DHRENT2-1</td><td>45.30 - 45.50</td><td>6.16</td><td>3.08</td><td></td><td>1</td><td></td><td>1</td><td></td><td>1</td><td></td><td>Basalt</td><td>Н</td></th<>	(B. Linnite)	DHRENT2-1	45.30 - 45.50	6.16	3.08		1		1		1		Basalt	Н
Diricity		DHKBT2 1	63.00 - 63.30	6.34	3.54	1	1	1	l	1	1		Porphyry	CH
Ministry         Distry         Distry <thdistry< th=""> <thdistry< th=""> <thdistry< <="" td=""><td>he No.3 tunnel</td><td>T DHKB1</td><td>50.05 - 50.25</td><td>6.34</td><td>3.06</td><td>1</td><td>1</td><td>I</td><td>1</td><td>!</td><td>1</td><td>P2</td><td>Marble</td><td>No.</td></thdistry<></thdistry<></thdistry<>	he No.3 tunnel	T DHKB1	50.05 - 50.25	6.34	3.06	1	1	I	1	!	1	P2	Marble	No.
Dright, for the first of the first			30.00 - 30.60	1 6230	3.35						3	PTR	Shale	CH-B
DiBAGE         14.0.0.142.0         6.04         2.05         3.41         150         700         12         Andelic           DiBAGE         14.0.0         153         14.0         151         3.01         2.00         3.01         5.0         3.01         5.0         3.01         5.0         3.01         5.0         3.01         5.0         3.01         5.0         3.01         5.0         3.01         5.0         3.01         5.0         3.01         5.0         3.01         5.0         3.01         5.00         3.01         5.00         3.01         5.00         3.01         5.00         3.01         5.00         3.01         5.00         3.01         5.00         3.01         5.00         3.01         5.00         3.01         5.00         3.01         5.00         3.01         5.00         3.01         5.00         3.01         5.01         5.00         5.010         5.01         5.010 <th<< td=""><td></td><td></td><td>132.60 - 133.30</td><td>5.32</td><td></td><td>3.68</td><td>2.96</td><td></td><td></td><td>380</td><td>55</td><td>B3</td><td>Andesite</td><td>CM</td></th<<>			132.60 - 133.30	5.32		3.68	2.96			380	55	B3	Andesite	CM
Difficition         14.30-14.660         6.21         3.11         6.12         3.23         14.60         600         52         Addition           Difficition         Difficition         0.53         2.73         4.97         2.79         3.00         1.01         3.1         1.1         1.1         1.1         2.		DIRAC	142.00 - 142.30	6.04	2.99	5.66	3.41	1550	780	300	15		Andesite	Ğ
1444         Diprot         64         2.37         4.97         2.97         5.00         4.00         5.5         5.44         2.94         5.94         5.94         5.94         5.94         5.94         5.94         5.94         5.94         5.94         5.94         5.94         5.940         5.94 <th< td=""><td></td><td>DHRI45</td><td>143.30 - 143.60</td><td>6.21</td><td>3.11</td><td>6.12</td><td>3.28</td><td>1450</td><td>800</td><td>320</td><td>22</td><td></td><td>Andesite</td><td>СM</td></th<>		DHRI45	143.30 - 143.60	6.21	3.11	6.12	3.28	1450	800	320	22		Andesite	СM
Table         Title         State         State <th< td=""><td></td><td>TURKS</td><td>148.40 - 149.00</td><td>6.54</td><td>2.73</td><td>4.97</td><td>2.97</td><td>500</td><td>400</td><td>400</td><td>55</td><td></td><td>Andesite</td><td>CM</td></th<>		TURKS	148.40 - 149.00	6.54	2.73	4.97	2.97	500	400	400	55		Andesite	CM
Midolity         153         264          500         200         -115         36         That           DiffoD137         114357         114357         114357         114357         114357         1143         31         310	A. W. P. S. L. L. L. L. L. L.	I DHANDI	\$0.45 - 59.65	3.66	2.29	1		1		1		CPab	Shale	CH
Diskatisy         11435-11440         450         277          620         320         -115         41           Diskatisy         119555-12000         541         2.22           200         275         35           Diskatisy         119555-12000         541         2.22 <t< td=""><td></td><td>DEGADICE</td><td>02.50 - 96.00</td><td>4.75</td><td>2.64</td><td></td><td>         </td><td>18 18 18</td><td>250</td><td>-115</td><td></td><td></td><td>Sandstone</td><td>Ð</td></t<>		DEGADICE	02.50 - 96.00	4.75	2.64		       	18 18 18	250	-115			Sandstone	Ð
Dilevidis         119:55 - 120:00         541         2.92		DHKADISP	114.55 - 114.80	4.50	2.57		1	620	320	-115	41		Sandstone	HO
Mir.ADA         #Zetor         Zetor<		DH&AD(SP	119.55 - 120.00	5.41	2.92	1	1	>1000	>400	-75	35		Sandstone	æ
Diprivation         52:00-52:00         6.19         394		TOTATE	42.00 - 42.25	5.71	2.77							TRM	Sandstone	СM
Difference         48.50         4.06         2.27             TRence           Difference         67.50         57.2         2.91          2.00         1250         35         >-00         PTRence           Difference         105.75         110.00         5.03         5.72         2.91          2         2           2         2		DH7AD1	52.50-52.80	6.19	3.94	1		1		1			Sandstone	ΗÐ
THRUS         67.30         57.3         2.91          1330         1350         351         200         778           DHRS         106.75         100.75         5.08         2.09           20         30         178           DHRS         126.75         3.12         1.89           20         30         176         60         778           DHRS         126.00         5.08         3.12         1.76          20         30         176         60         778           DHRS         126.01         5.06         3.12         1.76          20         30         176         60         73           DHR5         3         3.10         1.75          20         3.25         176          20         20         175         60         73           DHR5         3         3.10         1.75          23         2.41         2.35         2.45         1.36         60         73           DHR5         3         3.10         1.5         2.41         2.36         2.43         1.3         2.43         1.3	d Nn 2 tunnel	DHB0.6	48.50 - 48.80	4.08	2.27			1	1	Ţ	1	TRpn	Sandstone	CM
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		TOTAL STATE	67.50 - 67.80	5.72	2.91			1350	1250	ا الا الا	Š Š	PTRU	Granite porphyry	ዉ
135.50135.501361.892530-14565CPab $45.10$ $45.35$ $3.35$ $1.76$ $22$ $23$ $25$ $150$ $73$ $65$ CPab $45.10$ $45.60$ $3.42$ $1.76$ $22$ $22$ $25$ $100$ $75$ $73$ $73.20$ $73.35$ $3.21$ $1.76$ $23$ $210$ $75$ $120$ $66$ $73$ $73.20$ $73.35$ $3.21$ $1.76$ $233$ $10$ $12$ $25$ $62$ $CPab$ $183.40$ $180.00$ $3.98$ $2.44$ $4.08$ $2.79$ $222$ $23$ $10$ $12$ $25$ $62$ $CPab$ $183.40$ $188.60$ $4.95$ $2.81$ $4.71$ $2.68$ $100$ $15$ $12$ $63$ $CPab$ $183.40$ $189.60$ $4.95$ $2.31$ $4.62$ $3.07$ $223$ $23$ $10$ $72$ $25$ $55$ $55$ $CPab$ $155.60$ $155.60$ $5.67$ $3.11$ $2.59$ $8.27$ $100$ $75$ $70$ $75$ $70$ $165.60$ $165.00$ $5.67$ $3.01$ $3.11$ $2.59$ $500$ $40$ $35$ $45$ $CPab$ $155.60$ $150.00$ $5.73$ $2.28$ $4.71$ $2.95$ $56$ $57$ $47$ $70$ $196.30$ $197.00$ $5.33$ $2.43$ $5.30$ $2.84$ $5100$ $70$ $55$ $47$ <			109.75 - 110.00	5.08	1817			18		1601 1001	8	CPab D	S.s.& shale alt.	HO
45.10 - 45.35 $1.76$ $25$ $3.0$ $-145$ $65$ $C7ab$ $73.20 - 73.35$ $3.42$ $1.75$ $23$ $25$ $-150$ $75$ $73$ $73.20 - 73.35$ $3.21$ $1.76$ $23$ $25$ $-100$ $75$ $73$ $73.20 - 73.35$ $3.21$ $1.76$ $23$ $2.83$ $10$ $12$ $2.5$ $62$ $C7bb$ $183.40 - 184.00$ $3.96$ $2.04$ $4.08$ $2.79$ $2.22$ $2.83$ $10$ $15$ $12$ $66$ $183.10 - 186.00$ $3.96$ $2.44$ $4.08$ $2.79$ $2.25$ $2.8$ $10$ $15$ $12$ $65$ $133.40 - 184.00$ $3.96$ $2.32$ $2.81$ $4.71$ $2.68$ $10$ $15$ $12$ $65$ $62$ $135.60 - 166.00$ $5.67$ $3.11$ $2.59$ $82$ $10$ $-70$ $75$ $55$ $C7bb$ $165.60 - 166.00$ $5.67$ $3.01$ $3.11$ $2.59$ $82$ $10$ $-70$ $75$ $55$ $C7bb$ $165.60 - 166.00$ $5.67$ $3.01$ $3.11$ $2.59$ $82$ $10$ $-70$ $75$ $55$ $C7bb$ $165.60 - 166.00$ $5.70$ $2.62$ $4.79$ $2.59$ $50$ $82$ $10$ $77$ $70$ $165.60 - 166.00$ $5.33$ $2.22$ $4.71$ $2.59$ $50$ $90$ $40$ $75$ $70$ $195.60 - 186.00$ $5.33$ $2.36$ $4.30$ $2.43$ <		DHB88P	126.50 - 126.65	3.12	1.89	1		1			1		S.s.& shale alt.	СM
45.40 - 45.60 $3.42$ $1.75$ $$ $23$ $25$ $-150$ $73$ $7$ $73.20 - 73.35$ $3.21$ $1.76$ $$ $7$ $15$ $100$ $75$ $7$ $160.20 - 160.80$ $4.00$ $2.04$ $4.36$ $2.83$ $10$ $12$ $2.25$ $62$ $183.10 - 186.60$ $3.98$ $2.44$ $4.08$ $2.79$ $2.2$ $28$ $10$ $15$ $12$ $66$ $183.10 - 186.60$ $3.96$ $2.31$ $4.71$ $2.68$ $10$ $15$ $12$ $65$ $62$ $157.30 - 157.50$ $5.30$ $2.31$ $4.62$ $3.07$ $2.79$ $2.7$ $2.8$ $10$ $75$ $62$ $157.30 - 157.50$ $5.30$ $2.32$ $2.31$ $4.62$ $3.07$ $2.5$ $10$ $75$ $65$ $165.60 - 166.00$ $5.67$ $3.11$ $2.59$ $82$ $10$ $-70$ $75$ $65$ $165.60 - 166.00$ $5.67$ $3.01$ $3.11$ $2.59$ $82$ $10$ $-70$ $75$ $65$ $165.60 - 166.00$ $5.70$ $2.22$ $4.79$ $2.94$ $70$ $70$ $70$ $75$ $7$ $185.60 - 166.00$ $5.70$ $2.68$ $3.01$ $2.59$ $70$ $70$ $70$ $75$ $7$ $185.60 - 166.00$ $5.70$ $2.68$ $3.01$ $2.59$ $70$ $70$ $70$ $75$ $7$ $185.60 - 196.00$ $5.33$ $2.24$ $4.71$ $2.95$ $70$ $50$ $95$ $47$		FIDHBJ-16.5	45.10 - 45.35	3.35	1.76			22	100	-145	65	CPub	Shale	CH
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		DERLIGS	45.40 - 45.60	3.42	1.75	1		ន	3	-150	73		Shale	СН
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		DHBJ-16.3	73.20 - 73.35	3.21	1.76	1	.1	4	15	-100	75		Slate	CM
133.40 - 184.003.98 $2.44$ $4.08$ $2.79$ $2.2$ $2.8$ $-10$ $66$ 138.10 - 139.604.95 $2.31$ $4.71$ $2.66$ $10$ $15$ $12$ $63$ 157.30 - 157.305.30 $5.30$ $2.32$ $$ $-28$ $10$ $-70$ $75$ 165.60 - 165.005.67 $3.11$ $2.59$ $8.2$ $10$ $-70$ $75$ $CPab$ 165.60 - 186.005.67 $3.11$ $2.59$ $8.2$ $10$ $-70$ $75$ $CPab$ 185.60 - 186.005.70 $2.62$ $4.79$ $2.84$ $40$ $8$ $-55$ $47$ 185.60 - 186.005.70 $2.62$ $4.79$ $2.84$ $40$ $8$ $-55$ $47$ 185.60 - 186.005.70 $2.65$ $4.79$ $2.98$ $500$ $40$ $35$ $45$ $CPab$ 185.60 - 196.005.70 $2.65$ $2.84$ $>1000$ $70$ $180$ $72$ $CPab$ 190.40 - 191.005.33 $2.36$ $4.71$ $2.95$ $70$ $50$ $-95$ $54$ 201.00 - 201.40 $4.12$ $2.43$ $5.30$ $2.66$ $250$ $150$ $0$ $55$ $54$ 201.00 - 201.40 $4.12$ $2.43$ $5.30$ $2.66$ $250$ $150$ $0$ $55$ $54$		DHREAGS	160.20 - 160.80	4.00	2.04	4.36	2.83	10	12	55	62		Slate	CM
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		DHB)-16.3	183.40 - 184.00	3.98	2.44	4.08	2.79	22	28	-10	99		Slate	CH
157.30-157.30         5.30         2.32          28         10         -25         55         CPab           165.60-166.00         5.67         3.13         4.62         3.07         25         10         -70         75         75           185.60-186.00         5.67         3.01         3.11         2.59         82         10         -70         75         75           185.60-186.00         5.70         2.62         4.79         2.84         40         8        55         47           185.60-186.00         5.70         2.62         4.79         2.84         500         40         35         45         CPub           189.50-189.90         4.22         2.55         4.90         2.98         500         40         35         45         CPub           190.40-191.00         5.33         2.36         4.37         2.98         700         70         180         72         CPub           201.00-201.40         4.12         2.43         5.30         2.66         250         19         0         55         45         CPub           201.00-201.40         4.12         2.43         5.30         70         50		DHBJ-16.5	183.10 - 188.60		2.81	4.71	2.68	10	15	12	8		S.s.& shale alt.	CM
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		DHNLING T	157.30 - 157.50	<b>!</b>	2:32			121	9	-25	55	CPab	S.s.& shale alt.	СM
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		DHBI 18.0	165.60 - 166.00		3.13	4.62	3.07	R	10	0%-	75		Sandstone	CM
196.30         5.70         2.62         4.79         2.84         40         8         -55         47           180.50         4.22         2.55         4.90         2.96         500         40         35         45         CPnb           180.50         5.33         2.35         4.90         2.96         500         40         35         45         CPnb           190.40         191.00         5.33         2.36         4.71         2.96         70         70         70         72         76           190.40         194.00         194.00         4.12         2.48         4.71         2.95         70         90         95         54         70           201.00         201.40         4.12         2.43         5.30         2.66         250         150         0         55         54         70		DFDR-18.0	185.60 - 186.00	5.86	3.01	3.11	2.59	82	10	-190	45		Sandstone	Ð
180.50         4.22         2.55         4.90         2.98         500         40         35         45         CPnb           190.40         191.00         5.33         2.36         4.85         2.84         >1000         70         180         72         CPnb           190.40         191.00         5.33         2.36         4.85         2.84         >1000         70         180         72         72           201.00         194.00         312         2.43         5.30         2.66         250         150         0         55         54         72         72         72         72         72         72         72         72         72         72         72         72         72         73         73         73         73         73         73         73         73         73         73         73         73         73         74         73         73         74         73         73         73         74         74         74         74         74         74         74         74         74         74         74         74         74         74         74         74         74         74         74		DHRL18.0	196.30 - 197.00	5.70	2.62	4.79	2.84	4	8	-55	47		Sandstone	QM O
190.40 - 191.00     5.33     2.36     4.85     2.84     >1000     70     180     72       194.00 - 194.60     4.30     2.48     4.71     2.95     70     50     -95     54       201.00 - 201.40     4.12     2.43     5.30     2.66     250     150     0     55			189.50 - 189.90	4.22	2.55	100.4	2.98	1005	     	35	154	G B P P P	S.s.& shale alt.	B
194.00 - 194.60         4.30         2.48         4.71         2.95         70         50         -95         54           201.00 - 201.40         4.12         2.43         5.30         2.66         250         150         0         55		DUREDDS	190.40 - 191.00	5.33	2.36	4.85	2.84	>1000	202	180	72		S.s.& shale alt.	Ð
201.00-201.40 <b>4</b> .12 2.43 5.30 2.66 250 150 0 55		DHPJ-22-3	194.00 - 194.60	4.30	2.48	4.71	2.95	2	50	26	54		Slate	СM
		DHBL22.5	201.00 - 201.40	4.12	2.43	5.30	2.66	250	150	0	55		Sandstone	E
				-										
		•												

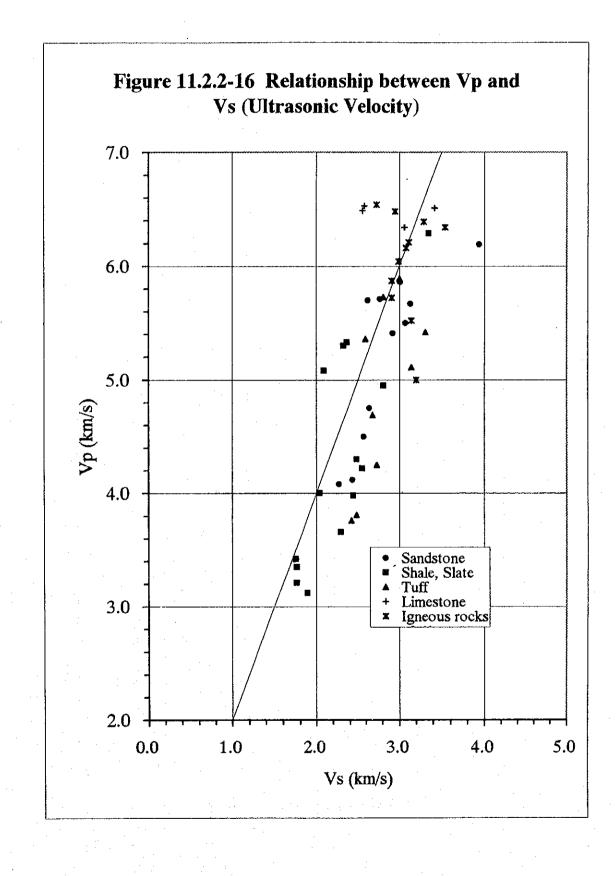
Table 11.2.2-26 Correlation of Results between Laboratory Test and In-situ Test (2)	t In-situ Test Short Long SP Gamma Boring Core Condition	Sonic Logging Resistivity Resistivity (mv) (cps)	avs) Vp(krnds)   Vs(krnds) (ohnu/m) (ohnu/m)   Form. Name Geology   Rock Class.	0 6.08 3.18 >10000 >10000 100 37 PTRv Dacite CH-B	0 5,99 3.31 9000 >10000 60 25 1 Tuff CH-B	t 5.40 3.20 3100 4000 35 50 Tut Tut CH	4.25 3.14 2000 1000 50 45 Tuff	 	1 1 1700 1200 -70 38 Tuff CH	3 5.42 3.11 4000 >5000 165 32 10tf CH	5.40         3.00         2000         2000         230         35         1	3 5.32 3.13 3000 4000 400 400 23		2 600 230 70 10 Limestone CM	850	
2.2-26 Correlation of Results bet	Laboratory Test	Sampling Depth Ultra Sonic Velocity	Vp(km/s) Vs(km/s)	3.29	265.00 - 266.00 5.89 3.00 5	271.00 5.11 3.14	277.00 3.76 2.42	181.80 4.25 2.73	198.30 - 198.60 5.42 3.31	- 274.00 3.81 2.48	290.00 5.36 2.59	297.00 4.69 2.68	- 57,50		۰.	
Table11.		Location Borehole No. Sa		Main Yor No. 2 tuninel Science DHBP 26.0 Science 25	TMR1260				DHR1.31.0			DHBJ-35.0			EDIHB46SP	

	Table11.2	2-27 Correlation of P - wave Velocity by Different Measurement Method (1)	<u>a of P - wi</u>	nve Veloc	ity by Di	ifferent <b>N</b>	<u>Aeasuren</u>	ient Met	hod (1)			
			Laboratory Test	rry Test	In-situ Test	Test		Seismic Survey	Survey	Å	Boring Core Condition	
Location	Borehole No.	Sampling Depth	Ultra Sonic Velocity	: Velocity	Sonic Logging	ogging	Index for	RFR	RFL	3		10
		(m)	Vp(km/s)	Vs(km/s)	Vp(km/s)	Vs(km/s)	Cracking	Vp(km/s)	Vp(km/s)	Form. Name	Geology	Rock Class.
Kok-Ing No.1 tunnel	DHKBUTLISP	39.60 - 39.80	5.87	2.91	•	i	1		>2.5	PTR	Granite	сW
	DHIKBUTI-ISP	63.00 - 63.30	5.73	2.81	1	1	1	1	>2.5		Tuff	CH
	DHKBUTH-ISP	66.60 - 66.90	5.00	3.20		-	1	1	>2.5		Diorite	CH
Kok-Ing No.2 tunnel	DEIKBUT2-1	37.10 - 37.40	6.48	2.95	1	1			1	٩n	Basalt	СН
(B-J-route)	DHKBUZA	45.30 - 45.50	6.16	3.08	1	1	1	1	1		Baselt	EB
	DRIKB/T2-1	63.00 - 63.30	6.34	3.54	1	1		-	1		Porphyry	CH
Kok-Ing No.2 tunnel	DEIKBI	50.05 - 50.25	6.34	3.06			-		>2.3	P2	Marble	ß
	DHKBZ	30.00 - 30.60	6.29	3.35					>23	PTR	Shale	CH-B
	DHB14.5	132.60 - 133.30	5.52	3.14	3.68	2.96	0.67			P3	Andesite	CM
	DEBUAS	142.00 - 142.30	6.04	2.99	5.66	3.41	0.94				Andesite	CM
	DHB14.5	143.30 - 143.60	6.21	3.11	6.12	3.28	0.99	1			Andesite	W
	DRB04.5	148.40 - 149.00	6.54	2.73	4.97	2.97	0.76	1	1		Andesite	CM
Ing-Yet NoZ. tunned addt	DESADI	59.45 - 59.65	3.66	2.29		1	ł	(2.5)	>2.4	CPub	Shale	CH
	DH6AD1SP	95.50 - 96.00	4.75	2.64		1	1	(2.7)	>2.8	TRM	Sandstone	CH
	DH6AD1SP	114.55 - 114.80	4.50	2.57	1	+	1	(2.7)	>2.8		Sandstone	Œ
	DH6ADISP	119.55 - 120.00	5.41	2.92	1	1		(2.7)	>2.8		Sandstone	æ
	DH7AD1	42.00 - 42.25	5.71	2.77		1		(4.6)	>2.1		Sandstone	N N N
	DETADI	52.50 - 52.80	6.19	3.94	1	1		(4.6)	>2.1		Sandstone	CH
Ing-Yot No.2 Inund	DHB0.6	48,50 - 48,80	4.08	2.27					>2.9	TRpn	Sandstone	CM
	DHBISP	67.50 - 67.80	5.72	2.91				(4.7)	>2.7	PTRgr	Granite porphyry	Ē
	DEBOSP	109.75 - 110.00	5.08	2.09				3.1		CPB	S.s.& shale alt.	CH
	DHBSSP	126.50 - 126.65	3.12	1.89				3.2	1		S.s.& shale alt.	CM
	DHBJ-16.5	45.10 - 45.35	3.35	1.76		- - -	1	3.3		CPB1	Shale	E E
	DRBI-16.5	45.40 - 45.60	3.42	1.75	I	1	1	3.3	1		Shale	CH
	DUBJ-165	73.20 - 73.35	3.21	1.76		1	1	3.4	1		Slate	CM
	DHBU-16.5	160.20 - 160.80	4.00	2.04	4.36	2.83	1.09	3.7	ï		Slate	CM
	DHBJ-165	183.40 - 184.00	3,98	2.44	4.08	2.79	1.03	3.8	!		Slate	CH
	DHBI-18.5	188.10-188.60	4.95	2.81	Ē	2.68	80	8. 8. 8.			S.s. & shale alt.	W
	DHBU-18.0	157.30 - 157.50	5.30	2.32	1		1	3.6	1	CPub	S.s.& shale alt.	CM
	DHRJ-18.0	165.60 - 166.00	. 2.67	3.13	4.62	3.07	0.81	3.7	1		Sandstone	CM
	DHBI-18.0	185,60-186.00	5.86	3.01	3.11	2.59	0.53	3.8	í		Sandstone	CH
	DHRUIS	196.30 - 197.00	51	50	23 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1	282	20 20 20 10 20	3.8			Sandstone	NO
	DUBU 22.5	189.50 - 189.90	4.22	2.55	6.9	2.98	1.16	4.7		CPab	S.s. & shale ait.	CH
	DHBV 22.5	190.40 - 191.00	5.33	2.36	4.85	2.84	16.0	4.7	1		S.s. & shale alt.	CH
	DHBU 22.5	194.00 - 194.60	4.30	2.48	4.71	2.95	1.10	4.8	1		Slate	CM
	DHBV 225	201.00 - 201.40	4.12	2.43	5.30	2.66	1.29	4.8	1		Sandstone	CH

\* Index for cracking : Vp of field (or Vp of Logging) / Vp of core \* Seismic survey, RFL : Reflection seismic survey, RFR : Refraction seismic survey

\* Vp in parentheses shows that of projected borehole on survey line.





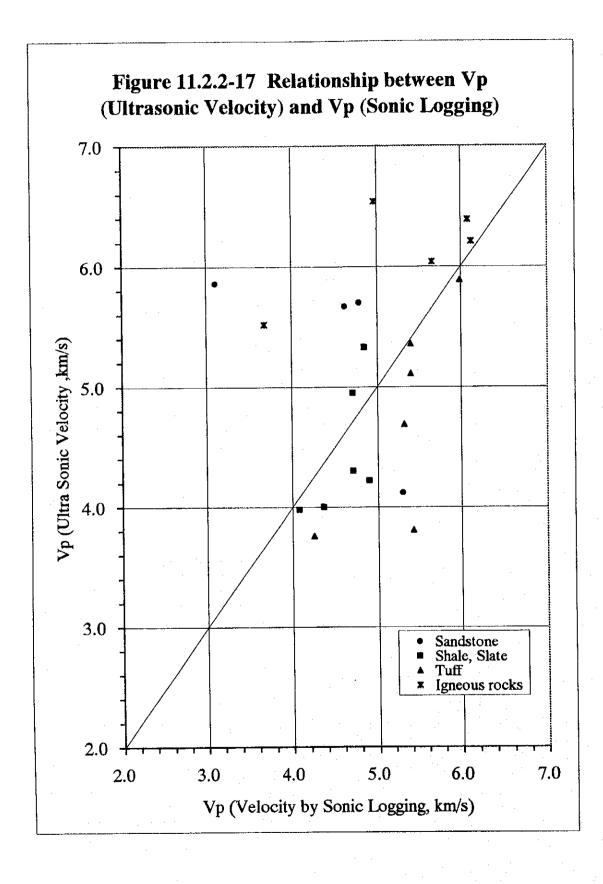


	Table 11.2.2-29	Results (	of Refra	sults of Refraction Prospecting Survey (P-wave Velocity)	urvey (P-1	wave Velo	city)	
I ine Name	Toration	Line Length	ength	Survey Line	Vp (P-w	Vp (P-wave velocity,	, km/sec)	Geological formation
ANTENT ATTAT	TOC8110T	(m)		Number	1st layer	2nd layer	<b>3rd layer</b>	OCOLOGICAL LULIMATION
SKIT-1-1	Kok-Ing No.1 tunnel inlet (main)	400		A-1 to A-4	0.3 - 0.4	0.8 1.3	2.6-3.5	Qt, Jv
SKIT-1/1	Kok-Ing No.1 tunnel inlet (sub)	400		B-1 to B-4	0.3 - 0.4	1.3 - 1.9	2.4 - 3.7	Qt, Jv
SKIT-1-2	Kok-Ing No.1 tunnel outlet (main)	1,000		C-1 to C-9	0.3 - 0.4	0.6 - 1.3	2.1-3.7	Qt, PTR, Jv
SKIT-1/3	Kok-Ing No.1 tunnel outlet (sub)	300		D-1 to D-3	0.3 - 0.4	1.0 - 1.7	2.7 - 3.4	Qt, PTR, Jv
SKIT-1/4	Kok-Ing No.1 tunnel outlet (sub)	400		E-1 to E-4	0.3 - 0.4	1.1 - 1.5	2.4 - 3.9	Qt, PTR, Jv
SKI-1, SKIT-2	Kok-Ing No.2 tunnel inlet (main)	4,800						
(SKIT-2/1RR)	_		200	G-1 to G-6	0.4	0.7 - 0.8	1.1 - 1.4	Qt, P3
			360	G-7 to G-10	0.3 - 0.4	0.7 - 0.9	1.4 - 1.8	Qt, P3
			1,085	G-11 to G-20	0.3 - 0.4	1.1 - 1.5	2.2 - 2.8	Qt, P3
			435	G-21 to G-24	0.4	1.0 - 1.1	1.7	Qt, P3
			2,160	G-25 to G-44	0.3 - 0.5	1.1 - 1.9	2.2 - 4.4	Qt, P3, P2, Bs
SKIT-2/2RR	Kok-Ing No.2 tunnel inlet (sub)	500		SKITA-1 to AKITA-5	0.3 - 0.4	1.2 - 1.9	2.2 - 2.5	Qt, P3, P2, PTRgr
SKIT-3/1RR	Kok-Ing No.2 tunnel outlet (main)	800		F-1 to F-8	0.3 - 0.4	0.7-1.6	2.3 - 3.4	Qt, PTR, (Bs)
SKIT-3/2RR	Kok-Ing No.2 tunnel outlet (sub)	500		SKITB-1 to AKITB-5	0.3 - 0.4	1.2 - 1.5	2.3 - 2.9	Qt, PTR
Line IY	Ing-Yot No.1 tunnel (main)	1,925						
			1,155	LineIY-1 to LineIY-11	0.3 - 0.4	0.6 - 1.1	1.9 - 4.5	Qt, ms3, TRpn
			770	LineIY-12 to LineIY-18	0.3 - 0.5	3.3 - 4.8	-	Qt, ms3, TRpn
SB0(Main)	Ing-Yot No.2 tunnel inlet (main)	3,100		SB0-1 to SB0-28	0.3 - 0.5	0.5 - 1.0	1.7 - 3.4	TRpn, TRhf, PTRv, PTRgr
SB0(SubA)	Ing-Yot No.2 tunnel inlet (sub)	500		SB0-A1 to SB0-A5	0.4-0.5	0.7 - 1.2	2.2 - 3.0	TRpn
SB0(SubB)	Ing-Yot No.2 tunnel inlet (sub)	500		SB0-B1 to SB0-B5	0.3 - 0.4	0.9 - 1.2	2.3 - 3.1	PTRv
SB0(SubC)	Ing-Yot No.2 tunnel inlet (sub)	600		SB0-C1 to SB0-C6	0.3 - 0.4	0.7 - 1.1	2.5 - 4.1	TRhf, PTRv
S2B0(Main)	Ing-Yot No.2 tunnel inlet (main)	1,100		S2B0-1 to S2B0-11	0.4 - 0.5	0.7 - 1.2	2.0 - 4.0	TRpn, PTRv, PTRgr
S2B0(Sub)	Ing-Yot No.2 tunnel inlet (sub)	500		S2B0-A1 to S2B0-A5	0.3 - 0.4	0.7 - 0.9	2.7 - 4.3	TRpn, PTRv, PTRg
SAd1(Main)	Ing-Yot No.2 tunnel Adit No.1(main)	1,000		SAd1-1 to SAd1-9	0.3 - 0.5	0.6 - 1.1	1.7 - 3.8	Qt, CPhk
SAd1(Sub)	Ing-Yot No.2 tunnel Adit No.1(sub)	500		SAd1-S1 to SAd-S5	0.4	0.6 - 0.8	1.8 - 3.5	Qt, CPhk
SAd2-RFR1	Ing-Yot No.2 tunnel Adit No.2(main)	400		SAd2-1 to SAd2-4	0.3 - 0.4	1.0 - 1.6	2.4 - 3.7	Qt, CPhk
SAd3-RFR1	Ing-Yot No.2 tunnel Adit No.3(main)	500		SAd3-A1 to SAd3-A5	0.3 - 0.4	0.8 - 1.3	2.1 - 2.4	Qt, CPnb
SAd3-RFR2	Ing-Yot No.2 tunnel Adit No.3(sub)	500		SAd3-B1 to SAd3-B5	0.3 - 0.4	0.9 - 1.3	2.3 - 2.4	Qt, CPnb
SAd4-RFR2	Ing-Yot No.2 tunnel Adit No.4(main)	600		SAd4-A1 to SAd4-A6	0.3 - 0.4	0.8 - 1.5	2.3 - 2.6	CPhk
SAd4-RFR1	Ing-Yot No.2 tunnel Adit No.4(sub)	650		SAd4-B1 to SAd4-B6	03-04	1.1 - 1.9	2.5 - 3.6	CPhk
SAd5-RFR1	Ing-Yot No.2 tunnel Adit No.5(main)	300		SAd5-A1 to SAd5-A3	0.3 - 0.4	1.2 - 1.4	2.4 - 3.0	TRhf
SAd5-RFR2	Ing-Yot No.2 tunnel Adit No.5(sub)	500		SAd5-B1 to SAd5-B5	0.3 - 0.4	0.9 - 1.5	2.4 - 3.9	TRhf

-	Table 11.2.2-30	<b>Results of Ref</b>	Table 11.2.2-30 Results of Refraction Prospecting Survey (P-wave Velocity)	urvey (P-v	vave Velo	city)	-
		Line length	Survey line	Vp (P-w	Vp (P-wave velocity, km/sec)	km/sec)	Geological formation
Line name	Location	(II)	number	1st layer	2nd layer	<b>3rd</b> layer	COUNTRY TO THE TO THE
SAd6-RFR1	Ing-Yot No.2 tunnel Adit No.6(main)	500	SAd6-A1 to SAd6-A5	0.3 - 0.4	0.9 - 1.2	2.4 - 2.8	TRhf
SAd6-RFR2	Inc-Yot No.2 tunnel Adit No.6(sub)	500	SAd6-B1 to SAd6-B5	0.3 - 0.4	0.8 - 1.6	2.3 - 2.6	TRhf
SAd7-RFR1	Inc-Yot No.2 tunnel Adit No.7(main)	400	SAd7-A1 to SAd7-A4	0.3 - 0.4	1.1 - 1.4	2.1-3.1	Qt, TRhf, (TRpl)
SAd7-RFR2	Ing-Yot No.2 tunnel Adit No.7(sub)	500	SAd7-B1 to SAd7-B5	0.3 - 0.4	1.0 - 1.5	2.1 - 2.4	Qt, TRhf
SE49-RFR1	Ing-Yot No.2 tunnel outlet(main)	800	SB49-A1 to SB49-A7	<b>0.3 - 0.4</b>	1.1 - 1.7	2.3 - 3.9	Qt, TRpl, TRhf
SB49-RFR2	Ing-Yot No.2 tunnel outlet(sub)	600	SB49-B1 to SB49-B6	0.3	1.4 - 1.8	3.0-3.3	Qt, TRpl, TRhf
SKI-B20(Main)	Kok- Ing tunnel south route(main)	1,035	SKI-M1 to SKI-M9	0.3 - 0.4	1.6 - 1.9	2.7 - 3.5	Qa, Qi
E	Kok- Ing tunnel south route(sub)	345	SKI-S1 to SKI-S3	0.3 - 0.4	1.6 - 1.7	2.9 4.0	Qa, Qî
SB0(Man)	Ing-Yot No.1 tunnel (main)	066	SB0-M1 to SB0-M18	0.4 - 0.5	0.6 - 1.4	3.1-53	Qt, ms3, TRpn
SB0(Sub)	Inc-Yot No.1 tunnel (sub)	495	SB0-S1 to SB0-S9	0.4 - 0.5	1.0 - 1.6	31-5.6	Qt, ms3, TRpn
NV X	Yao dam - dam axis	440	NY-A1 to NY-A8	0.3 - 0.4	0.7 - 1.2	2.4 - 3.3	TRhf
NY-B	Yao dam - left saddle	220	NY-B1 to NY-B4	0.3 - 0.4	0.5 - 1.3	2.6-3.4	TRhf
NY-C	Yao dam - cross section	385	NY-CI to NY-C7	0.4 - 0.5	1.1 - 1.4	32 4.0	TRhf
* Dense colour a	* Dense colour area shows Vp (P-wave velocity) of 4.0 km/sec	n/sec		•	:		č

SKI-1 and SKIT-2 line correspond to a series of survey line. SKIT-2 line is located on the inlet of Kok-Ing No.2 tunnel, and survey line for Kok-Ing No.2 tunnel is called as SKIT-2/1RR line.

\* SKIT-3/1RR line was called as SKIT-3 at the initial survey stage.

\* SB0 (Main, SubA-C) line at the Ing-Yot tunnel inlet and SKI-B20 (Main, Sub) line at the south route are correspond to canceled route.

\* Low velocity layers are found out following survey line.

SKIT-1/4 : width 5 m (survey point (sp.) 305-315)

Line IY : width 5 m (Vp=2.0 km/sec, sp.150-155), width 5 m (Vp=2.4 km/s, sp.925-930)

SB0 (Main) : width 5 m (sp. 2,550-2,555), width 15 m (sp. 2,580-2,590), width 10 m (sp. 3,015-3,025)

S2B0 (Main) : width 20 m (Vp=1.6 km/sec, sp.140-160)

SAd1 (Main) : width 10 m (Vp=1.1 km/sec, sp.50-60, width 10 m (Vp=1.3 km/sec, sp.270-280), width 5 m (Vp=1.3 km/sec, sp.790-795), width 10 m (Vp=2.3 km/sec, sp.790-795), width 10 m (Vp=2.3 km/sec, sp.270-280) width 5 m (Vp=1.4 km/sec, sp.790-795), width 10 m (Vp=2.4 km/sec, sp.270-280) width 5 m (Vp=1.4 km/sec, sp.790-795), width 10 m (Vp=2.4 km/sec, sp.270-280) width 5 m (Vp=1.4 km/sec, sp.790-795), width 10 m (Vp=2.4 km/sec, sp.270-280) width 5 m (Vp=1.4 km/sec, sp.790-795), width 10 m (Vp=2.4 km/sec, sp.270-280) width 5 m (Vp=1.4 km/sec, sp.790-795), width 10 m (Vp=2.4 km/sec, sp.270-280) width 5 m (Vp=1.4 km/sec, sp.270-280) width 5 m (Vp=1.4 km/sec, sp.790-795), width 10 m (Vp=2.4 km/sec, sp.270-280) width 5 m (Vp=1.4 km/sec, sp.270-280) w sp.905-915)

SAd1 (Sub): width 5 m (Vp=1.1 km/sec, sp.L210-215), width 5 m (Vp=1.1 km/sec, sp.R135-140)

SAd4-RFR1 : width 10 m (sp.165-175)

SAd1 (Sub), high speed layers (3rd layer) is found out line point R200-250 (Vp=3.5 km/sec). In case of the 3rd layer shows Vp=1.8-2.1 km/sec excluding the above high speed layer.

- SAd5 (Sub), the thickness of 1st layer at the right side shows 18.0 m.
- SB49 (Main), line point 0-40, 350-600 show 2-layer structure. High speed layer (3rd layer) is found out line point 220-330 (Vp=3.9 km/sec). In case of the above high speed
  - layer, 3rd layer shows Vp=2.3-3.3 km/sec.
- \* SB0 (Main) by RID, line point 130-255, 375-495, 605-880 show 2-layer structure.
  - \* SB0 (Sub) by RID, line point 90-205, 420-440 show 2-layer structure.
    - \* NY-A by RID, line point 0-60, 155-285 show 2-layer structure. \* NY-B by RID, line point 80-125 shows 2-layer structure.
      - \* NY-C by RID, line point 0-35, 170-235 show 2-layer structure.

	Table11.2.2-31 Results 0	ts of Ref	lection <b>P</b>	rospectin	of Reflection Prospecting Survey (	Thckness	(Thckness of Velocity Layer)	y Layer)	
		Line Length	ength	Thickness of E	Thickness of Each Layer (m)	Thickness from GL. (m)	om GL. (m)	Geological formation	Performed
Line Name	Location	5	(II)	1st layer	2nd layer	1st layer	2nd layer		by
A STATE OF A	Keledne No 1 tunnel inlet (main)	400		0 - 3.7	4.0 - 15.0	0 - 3.7	4.9 - 18.0	Qt, Jv	Thai side
CUTT 1/1	Kob-Ind No 1 tunnel inlet (sub)	400		1.4 - 4.0	2.3 - 16.4	1.4 - 4.0	4.7 - 18.9	Qt, Jv	Thai side
SULT 1.0	Volt Ind No. 1 turnel outlet (main)	1.000		1.0 - 9.0	5.0 - 25.0	1.0 - 9.0	6.6 - 34.2	Qt, PTR, Jv	Thai side
2-1-1 MG	Volt fine No.1 tunnel outlet (sub)	300		1.2 - 5.3	3.3 - 18.0	1.2-5.3	7.7 - 20.3	Qt, PTR, Jv	Thai side
5/1~1/2/	NOK-HIG INUL HUMMED CARDE (202)	400		1.4 - 4.0	7.5 - 14.0	1.4 - 4.0	10.7 - 16.8	Qt, PTR, Jv	Thai side
SM1-1/4	NOK-ING NO.1 tunnel ocuret (acc)	4.800							Thai side
SMI-L SMI-Z	NOK-ING INO.2 IMPRISTING INGEL (INGEN)	2224	100	0.4 - 3.3	3.0-11.0	0.4 - 3.3	5.3 - 12.2	Qt, P3	Thai side
(SINT/2-TINC)			360	0.5 - 2.3	3.5 - 9.3	0.5 - 2.3	4.7 - 10.7	Qt, P3	Thai side
			1.085	0.8 - 2.5	9.9 - 17.2	0.8 - 2.5	11.2 - 18.9	Qt, P3	Thai side
			435	0.2 - 1.4	4.3 - 6.8	0.2 - 1.4	5.1 - 7.7	Qt, P3	Thai side
			2,160	0.4 - 3.7	6.9 - 19.0	0.4-3.7	8.5 - 21.2	Qt, P3, P2, Bs	Thai side
SETTODRE	Kok-Ino No.2 tunnel inlet (sub)	500		1.0 - 5.0	3.5 - 19.0	1.0 - 5.0	6.5 - 20.0	Qt, P3, P2, PTRgr	Thai side
CICHT 2/100	Kok-Ino No.2 hunel outlet (main)	800		1.3 - 7.0	9.8 - 25.2	1.3 - 7.0	13.0 - 28.0	Qt, PTR, (Bs)	Thai side
COCT 2/20D	Vob-Ing No 2 tunnel outlet (sub)	500		1.0 - 6.5	12.5 - 20.0	10-6.5	15.5 - 26.0	Qt, PTR	Thai side
NNA-LING	Inc. Vot No 1 tunnel (main)	1.925							Thai side
			1.155	0 - 4.3	0 - 11.5	0 - 4.3	1.4 - 13.7	Qt, ms3, TRpn	Thai side
			770	1.0-8.5	1	1.0 - 8.5	1	Qt, ms3, TRpn	Thai side
AN PAULOES	Inc. Vot No.2 tunnel inlet (main)	3.100		0 - 13.0	0 - 14.5	0 - 13.0	3.5 - 17.0	TRpn, TRhf, PTRv, PTRgr	Thai side
CD076-AV	Inc. Vot No 2 tunnel inlet (sub)	500		0 - 4.5	. 0 - 10.5	0 - 4.5	2.0 - 12.5	TRpn	Thai side
CDA/CHUN	The Vot No 2 tunnel inlet (sub)	500		1.0 - 14.0	0-11.0	1.0 - 14.0	4.0 - 13.0	PTRv	Thai side
Concologic Son/Site	Inc. Vot No 2 tunnel inlet (sub)	909		0 - 8.0	0 - 13.0	0 - 8.0	4.5 - 15.5	TRhf, PTRv	Thai side
SOBOM SIL	Ino-Yot No.2 tunnel inlet (main)	1,100		0-8-0	2.0 - 15.5	0 - 8.0	4.0 - 19.5	TRpn, PTRv, PTRgr	Thai side
STRUKIA	Ing-Yot No.2 tunnel inlet (sub)	500		0 - 16.0	0 - 11.0	0 - 16.0	4.0 - 16.5	TRpn, PTRv, PTRg	Thai side
SAd1(Main)	I Ing-Yot No.2 tunnel Adit No.1(main)	1,000		0 - 4.0	4.0 - 17.0	0 - 4.0	5.0 - 17.0	Qt, CPhk	Thai side
CART/Shiky	Inc-Yot No.2 tunnel Adit No.1(sub)	500		0.5-5.0	3.0 - 12.0	0.5 - 5.0	5.0 - 12.5	Qt, CPhk	Thai side
CAND DID1	Ino-Yot No.2 tunnel Adit No.2(main)	400		1.0 - 5.0	5.0 - 19.5	1.0 - 5.0	6.5 - 21.0	Qt, CPhk	Thai side
SAA2 PED-	Ing-Yot No.2 tunnel Adit No.3(main)	500		0 - 4.5	9.0 - 16.5	0.4.5	11.5 - 18.5	Qt, CPab	Thai side
SAAD PEDO	Inc-Yot No.2 tunnel Adit No.3(sub)	500		0 - 4.0	6.0 - 21.0	0 - 4.0	9.0 - 23.0	Qt, CPnb	Thai side
COLO VEVO	Inc-Yot No.2 tunnel Adit No.4(main)	600		0 - 4.5	3.5 - 16.0	0-4.5	7.0 - 20.0	CPhk	Thai side
SANA DEPT	Inc-Yot No.2 tunnel Adit No.4(sub)	650		0 - 7.5	2.5 - 19.5	0-7.5	4.0 - 22.5	CPhk	Thai side
SAd5 RPR1	Ing-Yot No.2 tunnel Adit No.5(main)	300		0.5 - 5.0	4.0 - 19.0	0.5 - 5.0	5.5 - 22.0	TRhf	Thai side
SAAS REPO	Ino-Vot No.2 tunnel Adit No.5(sub)	500		0 - 18.0	1.0 - 20.5	0 - 18.0	2.0 - 34.0	TRhf	Thai side
Name and a state									

1.1.2.1	Starter Starter		
		3	

Table11.2.2-32 Results of Reflection Prospecting Survey (Thckness of Velocity Layer)

		Line Length	Thickness of I	Thickness of Each Layer (m)	Thickness from GL. (m)	om GL. (m)	Colorised formation	Performed
Line Name	Location	(m)	1st layer	2nd layer	1st layer	2nd layer	Ueological Ionination	by
SAd6-RFR1	Ing-Yot No.2 tunnel Adit No.6(main)	500	0.5 - 4.5	2.0 - 19.0	0.5 - 4.5	3.5 - 20.5	TRhf	Thai side
SAd6-RFR2	Ing-Yot No.2 tunnel Adit No.6(sub)	500	0 - 8.5	5.0 - 18.0	0 - 8.5	5.0 - 23.0	TRhf	Thai side
SAd7-RFR1	Ing-Yot No.2 tunnel Adit No.7(main)	400	1.0-4.0	5.5 - 19.0	1.0 - 4.0	8.0 - 22.5	8.0 - 22.5   Qt, TRhf, (TRpl)	Thai side
SAd7-RFR2	Ing-Yot No.2 tunnel Adit No.7(sub)	500	0 - 7.5	8.5 - 24.0	0 - 7.5	8.5 - 26.0	Qt, TRhf	Thai side
SB49-RFR1	Ing-Yot No.2 tunnel outlet(main)	800	1.0 - 10.0	5.0 - 34.0	1.0 - 10.0	9.5 - 38.0	Qt, TRpl, TRhf	Thai side
SB49-RFR2	Ing-Yot No.2 tunnel outlet(sub)	600	0 - 24.0	0 - 23.5	0 - 24.0	3.5 - 29.0	Qt, TRpl, TRhf	Thai side
SKI-B20(Main)	Kok- Ing tunnel south route (main)	1,035	1.0-3.3	9.3 - 24.7	1.0 - 3.3	11.0 - 26.7	Qa, Qt	Thai side
SKI-B20(Sub)	Kok- Ing tunnel south route(sub)	345	0.7 - 2.3	18.0 - 25.5	0.7 - 2.3	19.0 - 27.7 Qa, Qt	Qa, Qt	Thai side
SB0(Main)	Ing-Yot No.1 tunnel (main)	066	0 - 6.0	0 - 10.7	0-6.0	3.0 - 15.3	3.0 - 15.3   Qt, ms3, TRpn	Thai side
SB0(Sub)	Ing-Yot No.1 tunnel (sub)	495	1.0 - 7.0	0-19.0	1.0 - 7.0	2.5 - 22.8	Qt, ms3, TRpn	Thai side
NY A	Yao dam - dam axis	440	1.0 - 8.5	0 - 18.8	1.0 - 8.5	4.0 - 25.7	TRhf	Thai side
NY-B	Yao dam - left saddle	220	2.0 - 7.8	09.8	2.0 - 7.8	3.7 - 17.2	TRhf	Thai side
NY C	Yao dam - cross section toward dam axi	385	0 - 5.6	0 - 10.8	0-5.6	0.6 - 13.2	TRhf	Thai side

SKI-1 line, survey point (sp.) 1,060-1,130 has not data for existing of river flow.

SKI-1 line, sp.0-700 is found out as 4-layer structure. The 4th layer shows Vp=2.3-2.5 km/sec, thickness of 3rd layer 11.6-19.8 m, thickness from GL of 3rd layer 21.7-29.4 m \* SKI-1 line, high speed layers (3rd layer) are found out sp.3,060-3,170 (Vp=3.8 km/sec), 3,390-3,500 (Vp=3.7 km/sec), 3,500-3,610 (Vp=4.4 km/sec). In case of excluding the above high speed layer, 3rd layer shows Vp=2.2-2.9 km/sec.

\* IY line, sp.325-450, 650-665, 1,155-1,925 show 2-layer structure. The 3rd layer shows Vp=3.0-4.8 km/sec excluding sp.0-155.

\* SB0 (Main) line, sp. 865-895, 2,075-2,170, 2,730-2,870 3,025-3,100 show 2-layer structure. The thickness of 1st layer of sp. 2,075-2,170, 3,025-3,100 show

13.0 m, 5-10 m, respectively.

\* SB0 (SubA), sp.L115-250, R15-45, 240-250 show 2-layer structure.

SB0 (SubB), sp.L115-250, R70-250 show 2-layer structure. The thickness of !st layer at the right side shows 14.0 m.

\* SB0 (SubC), sp.R65-300 shows 2-layer structure.

S2B0 (Main), high speed layer (3rd layer) is found out sp.485-840 (Vp=3.8-4.0 km/sec).

S2B0 (Sub), sp.150-250 shows 2-layer structure, high speed layer (3rd layer) is found out sp.R30-145 (Vp=4.1-4.3 km/sec). The thickness of 1st layer of sp.R150-250 shows SAd1 (Main), high speed layers (3rd layer) are found out sp.385-515 (Vp=3.5-3.6 km/sec), 855-1,000 (Vp=3.8 km/sec). In case of excluding the above high speed layer, the 3rd layer shows Vp=1 7-2.8 km/sec.

	T anoth	TaDIC	Victor 2010 And the Flevation 600 - 0 m Level (unit km/sec)	along the Eleva	Vn along the Flevation 600 - 0 m Level (unit km/sec)	Level (unit km/s	sec)		Vp at the Tunnel	
Line Name	(m)	EL.600	EL.500	EL.400	EL.300	EL.200	EL.100	EL.0	Invert Level (Im/s)	ocoucy
SKTT BET	1 200		-	3.8 - 4.1	4.0 - 4.3	4.1 - 4.8		•	3.8	Jv
SKIT2-RPL)	1,000	•		,	1	•	1	-		Bs, P3, PTR
SBOMain	4.500		3.0 - 4.2	3.1 - 4.4	3.3 - 4.6	3.4 - 4.8	4.0 - 4.9	11 S 1 S 1	3.2 - 4.5	CPhk
SBOCSuby	006	3.2 - 3.6	3.3 - 3.8	3.5-4.1	3.9 - 4.5	4.1 - 4.8	-		4.3	CPhk
S2B0(Main)	1.600		,	3.8 - 4.4			E1 0.5	56-7.7	4.0 - 4.7	TRH, PTRV
S2B0(Sub)	806	•	4.8 5.8	5.6 6.0	12 E 9	6.6 7.3			6.7	TRhf
S2B0-RFL1	1,100	,	4.3 - 4.5	4.4 - 5.6	47 60	1.1.66	53-68	5.5-6.9	4.9	TRhf, (CPhk)
S2BO-RFL2	800	1	2.2 - 3.0	2.9 - 3.6	3.3 4.1	3.7 - 4.5	•		3.5	CPhk
SB8-RFL1	006	•	F	2.9 - 3.5	3.4 - 4.0	4.3 5.4	-	•	3.3	CPhk, CPnb, CPdm
SBIOCEM	500	-	3.7 - 3.8	3.8 - 4.1	4.0 - 4.6	4.4 - 4.9	<b>3.6</b> 5.0	4	3.9 - 4.3	CPhk, CPhb
SBUDOWY	600		3.2 - 3.9	3.6 - 4.4	4.1-4.9	5.2-5.6	5.6 5.9	•	3.8	CPab
SB10/E	006		3.4 - 3.5	3.8-4.0	4.1 - 4.8		•	,	4.2	CPnb
SAd2.RFL2	1.300	-	1.9 - 3.1	2.2-3.5	2.8 - 4.0	3.7 - 4.5	-	•	•	CPhk, TRpl, (Qt)
SB16(Man)	1.000	-	2.6 - 3.1	2.8 3.4	3.1 - 3.7	3.4 - 4.1	3.7 - 4.2	3.8 4.3	3.3	CPab
SBL6(Sub)	906		3.3 - 3.4	3.5 - 3.7	3.6 - 3.9	3.9 - 4.1	-	-	3.6	CPab
SAd3-RFL1	006		2.3 - 2.8	2.5-3.2	3.2 - 3.6	3.6 - 3.9		•		CPub
SB17(Main)	1.000	2.5-3.1	3.1-3.5	3.8 - 4.0	4.1 - 4.3	.1	- -	,	4.1	CPab
SB17(Sub)	700	2.8 - 3.6	3.2 - 3.9	3.8 - 4.2	4.2 - 4.7	05 11 11	9.6 5.0	•	4.2	CPab
SB21(Main)	1,100		4.2 - 4.5	4.5-4.7	40 50		<b>11231537</b>	•	4.8	CPub
SB21(Suth)	700		3.4 - 3.6	3.8 - 4.2	1 42 52	5.0-54	1		1	CPnb
SB35(Main)	2,000		2.3 - 2.7	2.6 - 3.0	2.8-3.1	2.9 - 3.1		•	2.7 - 3.0	TRM
SB35(Sub)	800		2.6 - 2.7	2.7 - 2.8	2.9 - 3.1	3.0 - 3.2		1	3	TRhf
SAd7-RFL1	1,600	•	•	3.6 - 4.5	3.9 - 4.9	144 52	<b>4</b> .6 5.6	4.0 5.6	'	TRhf, TRpi
SB46(Main)	<b>006</b>	•	2 <b>-</b> -	3.2 - 4.6	3.5 - 4.9	11 319 H 512	42 54	4.4.55	4.5	TRhf, TRpi
SB48(Main)	1,100	-	•	3.1 - 3.8	3.9 - 4.6	14:5-5:4	•	1	3.6 - 4.3	TRM
SB48(3ub)	800	•		3.1-4.7	35 50	4.0-5.5	4.6 - 5.8	1	4.9	TRMf, (TRpl)
SB40-KFL1	1,500			-	3.8 - 4.7	40 52	4 5 4	49.59	3.9	TRhf, TRpi
* Dense colo	ur area shows	· Vp (P-wave v	* Dense colour area shows Vp (P-wave velocity) of 5.0 km/sec or more.	cm/sec or more		· · · ·	•			
* SKITY-BF	1 snew line	has not record	• SKITY-BET 1 survey line has not record as for velocity counter line.	counter line.						

Table 11.2.2-33 Results of Reflection Prospecting Survey (P-wave velocity)

Table 11.2.2-33 Results of Reflection Prospecting Survey (P-wave velocity) \* SKIT2-RFL1 survey line has not record as for velocity counter line.

		JUB I		T TO CHINGAN	T TIME AN INT	autor of the state				
╞	Length		νp	along the Eleva	tion 600 - 0 m	Vp along the Elevation 600 - 0 m Level (unit km/sec)	sec)	1	Vp at the Tunnel	Geology
Line Name	°(E	EL.600	EL.500	EL.400	EL.300	EL.300 EL.200	EL.100	EL.0	Invert Level (km/s)	
SB46(Main) 9	8			3.2 - 4.6	3.5-4.9	2:5-6:8	1 <b>1</b> 2 3 4	1.52.24	4.5	TRhf, TRpl
Left side of survey point 150	150			3.2 - 3.5	3.5 - 3.9	3.9 - 4.4	4.2 - 4.7	4.4 - 4.9		TRhf
Right side of survey point 220	M 220		•	3.7 - 4.6	3.7 - 4.6 4.2 - 4.9		50-54	5.1-5.5	-	TRpl
SB48(Sub) 8	808	-	-	3.1 - 4.7	<b>35 5.0</b>	11 4 0 5 2 11	11 X 0 2 X 11	-	4.9	TRhf, (TRpl)
Left side of survey point 100	8	•	•	3.1 - 3.2	3.5 - 3.8	4.0-4.4	3.6-51	L	1	TRhf
Right side of survey point 220	220	,	ţ	4.6 - 4.7	4.9 5.0	5455	5.6 - 5.8		-	TRpi

		Table 11.2.2-34 Results of Reflection Prospecting Surv	ction Prospecting Survey (Characteristics of Analyzed Section)
Line Name	Length (m)	General Description	Description around Tunnel Location
SKITL-RH.J	1,200	Velocity contour lines show syncline feature around survey point (sp.) 440, and two clear discontinuities are found out at sp.300 (SSW-dip 70°) and sp.950 (NNE-dip 60°).	Tunnel location is situated on wing (NNE direction) of syncline feature as layer structures, and those around tunnel location show SSW-dip 40°.
SKITLANEL	1,000	Clear anticline feature is found out at sp.320, and whole discontinuities shows SEE-dip with gradient 50-80°.	Tunnel location is situated at the area of dominant discontinuities with SEE-dip.
SB0(Mam)	4,500	Velocity contour lines show both syncline feature around sp.980, sp.2,170 and sp.3,950 and anticline feature at sp. 4,300-4,500. Two clear discontinuities are found out at sp.2,200 (NNE-dip 60°) and sp.4,000 (SSW-dip 70°).	Layer structures along the tunnel line are flat or gentie gradient (less than 10° dip) for the most part, excluding existing of discontinuity (sp.2,100-2,600 (NNE-dip 10-15°)).
SB0(Sub)	006	Velocity contour lines show gentle syncline feature at sp.700-900. Feature of discontinuities can be classified NNW-dip at the NNW direction of survey line and SSE-dip at the SSE direction of that, respectively, and clear discontinuity is found out around sp.700 (SSE-dip $70-80^{\circ}$ ).	Tunnel location is situated in the distribution area of discontinuities, and layer structures around tunnel location show flat or gentle gradient.
S2B0(Main)	1,600	Velocity contour lines show syncline feature at sp.1,350-1,600. In this case, it is inferred that the range of TRhf shows high Vp in comparison with that of CPhk.	Layer structures along the tunnel line show flat or gentle gradient (less than 10° dip) for the most part, excluding distribution area of discontinuities.
(97S)082S	006	Velocity contour lines show both syncline feature around sp.250 and gentle anticline feature around sp.670. Vp of this survey line are characterized by presence of high velocity in comparison with those of other survey line.	Layer structures at the tunnel location show gentle gradient with SSE-dip 5- 10°.
S2B0-RFI-1	1,100	Contour lines show high velocity at the south-direction of survey line, and clear discontinuity is found out around sp.450 (SEE-dip 65°).	Layer structures at the tunnel location show SSE-dip 15-20°.
S2B0-KH.2	800	Velocity contour lines show flat or gentle gradient for the most part, and clear discontinuity is found out around sp.450 (SSE-dip $60-65^{\circ}$ ).	Tunnel location is situated in the distribution area of discontinuities, which show SSE-dip 70° approximately.
SB8 RHL1	006	Velocity contour lines show both syncline feature from EL 400 to EL 300 at sp.0-200 and gentle anticline feature at sp.230-400.	Layer structures at the tunnel location show flat or gentle gradient (less than 10° dip).
SB10(Ext)	200	Velocity contour lines show anticline feature at sp.330-550, and clear discontinuity is found out at sp.50-150 (NWW-dip 65-70°).	Layer structures along the tunnel line show flat or gentle gradient (less than SEE-dip $5^{\circ}$ ).
SB10(W)	600	Velocity contour lines show anticline feature from EL 500 to EL 230 around sp.250. Feature of discontinuities can be classified N-dip at the S direction of survey line and S-dip at the N direction of that, respectively.	Layer structures at the tunnel location show S-dip 15° approximately.
* In the above to	able, the direct	* In the above table, the direction and dip as for discontinuity etc. mean apparent that.	

	Ľ	Table 11.2.2-35 Results of Reflection Prospecting Survey (Characteristics of Analyzed Section)	y (Characteristics of Analyzed Section)
Line Name	Length (m)	General Description	Description around Tunnel Location
SB10(E.E)	006	Syncline and anticline features on a large scale of velocity contour lines are hardly recognizable. Two clear discontinuities are found out at sp.E200 (SSW -dip 45°) and sp.E'300 (NNE-dip 60°).	Layer structures at the tunnel location show gentle gradient with NNE-dip 5- 10°.
SA42.RFL2	1,300	Velocity contour lines show syncline features, which is inferred to be ascribed to existing of thick diluvial deposits or weathered rock zone, at sp.400-1,200. Layer structures along the survey line show flat or gentle gradient with NNE-dip 5-10°. Especially, layer structures of sp.1,000-1,300 show monotonous feature.	
SB16(Main)	1,000	Velocity contour lines show monotonous feature, and Vp of this survey line is characterized by presence of low velocity in comparison with those of other survey lines. Gradient of discontinuities shows steep gradient (70-90°).	Layer structures at the tunnel location show NW-dip 15-20°.
SB16(Sub)	006	Velocity contour lines show anticline feature around sp.480, and two clear discontinuities are found out at sp.0-200 (NNE-dip 45-60°) and sp.450-500 (SSW-dip 70°). Velocity of this survey line shows higher than those of SB16 (Main), suggesting existing of anisotropic characteristic in base rock.	Layer structures at the tunnel location show almost flat or gentle gradient.
1.143 SA43 RFL1	006	Velocity contour lines show remarkable anticline feature, which is inferred to be ascribed to existing of base rock at the shallow depth, at sp.750-900. Layer structures along the survey line show flat or gentle gradient with NNE-dip 5-10°.	
SB17(Main)	1,000	Velocity contour lines show monotonous feature, and two clear discontinuities are found out at/around sp.150-200 (NWW-dip 55°) and sp.700(SEE-dip 60-70°).	Layer structures at the tunnel location show NWW-dip 20-25°.
SB17(Sub)	700	Velocity contour lines have monotonous gentle gradient, which signify to rise toward SSW direction.	Layer structures at the tunnel location show flat or gentle gradient with SSE- dip 5°, and discontinuities (SSE-dip 60-70°) are recognized around tunnel
SB21(Main)	1,100	Velocity contour lines show monotonous feature, which signify almost flat or gentle gradient. Two clear discontinuities are found out at/around sp.250 (SEE-dip 80°) and sp.600-650 (NWW-dip 70°).	Tunnel location is situated between two discontinuities, and layer structures show steep gradient with NWW-dip 55-60°.
SB21(Sub)	200	Velocity contour lines show anticline feature at sp.350-400. Clear discontinuity is found out at sp.500-550 (SSW-dip 75°), and syncline feature as layer structure is recognized at the SSW direction of that.	
SB35(Meih)	2,000	Velocity contour lines show both syncline feature at sp.450-600 and anticline feature at sp.1,550-1,650. Vp of this survey line is characterized by presence of low velocity in comparison with that of other survey lines. Three clear discontinuities are found out around sp.400 (NW-dip 85°), sp.600 (SE-dip 60°) and sp.1,500 (SE-dip 70-75°).	Layer structures along the tunnel line show flat or gentle gradient (less then 20°), excluding around the above discontinuities, where shows steep gradient (dip 50- 70°, approximately).

Table 11.2.2-36 Results of Reflection Prospecting Survey (Characteristics of Analyzed Section)	General Description Central Description around Tunnel Location	Velocity contour lines show monotonous feature, which signify almost flat or gentle gradient. Discontinuity is found out around sp.200 (SSW-dip 50°), and layer structures show NWW-dip at the deep portion (EL 400-200) of sp.400-800	Velocity contour lines show anticline feature at sp.250-350 and sp.950-1,300. Layer structures along the survey line show complex fold feature , which are remarkably recognized at/around sp.250-500 (N-dip 50-60°, sp.500-650 (S- dip 50-60°) and sp.1,00 (N-dip 55-60°), and these fold shapes are probably ascribed to the existing of discontinuities.	Velocity contour lines show high-speed feature at the NNE side from sp.220, Layer structures at the tunnel location show SSW-dip 15-20°. which probably involve existing of limestone. A number of discontinuities (NNE-dip) are found out at sp.0-300.	Velocity contour lines show both syncline feature around sp.200 and anticline Layer structures along the tunnel line show flat or gentle gradient, excluding feature around sp.400. SE-dip 30-40°). Clear discontinuity is found out around sp.500 (NW-dip 55-60°).	Velocity contour lines show high-speed feature at the SW side from sp.300- 350, which probably involve existing of limestone. Clear discontinuities are found out at sp.50-150 (SW-dip 60°) and sp.300-450 (NE-dip 40°).	Velocity contour lines show anticline feature at sp. 100-200 and sp. 700-850. Layer structures at the tunnel location show N-dip 20°, approximately. A number of discontinuities, which are complex with a variety of gradient direction. are find out along the survev line.
Table 11.2.2-36 Results of Reflection Pr	General Description	Velocity contour lines show monotonous feature, which si gentle gradient. Discontinuity is found out around sp.200 ( layer structures show NWW-dip at the deep portion (EL 4) 800	Vekocity contour lines show anticline feature at sp.250-350 Layer structures along the survey line show complex fold 1 remarkably recognized at/around sp.250-500 (N-dip 50-60 dip 50-60°) and sp.1,000 (N-dip 55-60°), and these fold sh ascribed to the existing of discontinuities.	Velocity contour lines show high-speed feature at the NNE side from sp.2. which probably involve existing of limestone. A number of discontinuities (NNE-dip) are found out at sp.0-300.	Velocity contour lines show both syncline feature around s feature around sp. 400.	Velocity contour lines show high-speed feature at the SW side from sp.300- 350, which probably involve existing of limestone. Clear discontinuities are found out at sp.50-150 (SW dip 60°) and sp.300-450 (NE-dip 40°).	Velocity contour lines show anticline feature at sp. 100-200 and sp.700-85 A number of discontinuities, which are complex with a variety of gradient direction, are find out along the survey line.
	Length (m)	800	1,600	005	1,100	800	1,500
	Line Name	SB35(Sub)	SAD-RFLI	SB46(Main)	SE48(Main)	SB48(Sub)	SB49-RH.1

Z, No. ΰ . f 5

	DH - 1 (L = 50.0 m, G	G.L.(EL.) 321.5)	
	Location: Right abutment	along the dam axis	
G	eological Condition	Rock Class.	Condition
Depth	Geology	Depth	Rock Class.
0 - 1.5 m	Soil	0 - 1.5 m	D
1.5 - 7.0 m	Shale interbedded with s.s.	1.5 - 5.0 m	CL
7.0 - 14.0 m	Shale	5.0 - 6.0 m	CL - CM
14.0 - 18.0 m	Sandstone	6.0 - 10.0 m	CL
18.0 - 50.0 m	Tuff	10.0 - 13.0 m	D - CL
		13.0 - 18.0 m	CL
N value, 1.0 m 16		18.0 - 20.0 m	СМ
		20.0 - 22.0 m	CL - CM
		22.0 - 23.3 m	CM
		23.3 - 42.0 m	CM - CH
	. · · · · · · · · · · · · · · · · · · ·	42.0 - 43.0 m	CL - CM
		43.0 - 48.4 m	СМ
		48.4 - 49.1 m	CL
	· .	49.1 - 50.0 m	CM

# Table 11.2.2-37 Summary of Drilling Results at the Yao Flood Control Dam (1)

· · · · · · · · · · · · · · · · · · ·	DH - 2 (L=80.0 m, G.L Location: River portion al	المتفسيفان الالتبار فتقاسك كالمتحد والمستعد والمتعاد	· · · · · · ·
G	eological Condition	Rock Class.	Condition
Depth	Geology	Depth	Rock Class.
0 - 6.1 m	Soil	0 - 6.1 m	D
6.1 - 52.0 m	Tuff	6.1 - 12.8 m	D - CL
52.0 - 55.0 m	Sandstone	12.8 - 13.0 m	CL
55.0 - 57.4 m	Shale	13.0 - 13.7 m	CL - CM
57.4 - 59.0 m	Sandstone	13.7 - 14.0 m	D - CL
59.0 - 80.0 m	Sandstone interbedded with sh.	14.0 - 22.0 m	CL
	-	22.0 - 23.0 m	CL-CM
		23.0 - 39.0 m	CL
		39.0 - 52.0 m	СМ
		52.0 - 55.0 m	CM - CH
		55.0 - 57.4 m	CL - CM
· · ·		57.4 - 60.0 m	CM
1		60.0 - 61.0 m	CL
	· .	61.0 - 68.8 m	СМ
		68.8 - 75.2 m	CL - CM
		75.2 - 79.0 m	CM
		79.0 - 80.0 m	CM - CH

· · · ·	DH - 3 (L=60.0 m, G.L.	(EL) 295.8)	
	Location: Left abutment alo	ng the dam axis	
Ge	ological Condition	Rock Class.	Condition
Depth	Geology	Depth	Rock Class.
0 - 4.0 m	Soil	0 - 4.0 m	D
4.0 - 18.0 m	Shale	4.0 - 6.0 m	D-CL
18.0 - 44.0 m	Sandstone	6.0 - 7.7 m	CL
44.0 - 48.4 m	Shale	7.7 - 8.0 m	D - CL
48.4 - 51.0 m	Sandstone	8.0 - 8.2 m	CL
51.0 - 60.0 m	Sandstone interbedded with sh.	8.2 - 14.0 m	D - <u>CL</u>
		14.0 - 18.0 m	CL - CM
N value, 1.0 m - 20		18.0 - 21.0 m	СМ
2.0 m - 21		21.0 - 22.2 m	CM - CH
3.0 m - 26	- · · · · · · · · · · · · · · · · · · ·	22.0 - 33.2 m	CL - CM
		33.2 - 35.6 m	СМ
		35.6 - 36.6 m	CL
		36.6 - 44.3 m	CM - CH
		44.3 - 48.8 m	CL
	and the second	48.8 - 50.8 m	СМ
	· · · · ·	50.8 - 60.0 m	CL - CM

	DH - 4 (L=50.0 m,	G.L.(EL) 330.8)	
	Location: Left abutmer	nt along the dam axis	
(	Seological Condition	Rock Class	. Condition
Depth	Geology	Depth	Rock Class.
0 - 5.0 m	Soil	0 - 10.0 m	D
5.0 - 37.0 m	Shale	10.0 - 11.0 m	D - CL
37.0 - 50.0 m	Sandstone	11.0 - 13.0 m	D
		13.0 - 15.5 m	D - CL
N value, 1.0 m - 17		15.5 - 34.0 m	D
2.0 m - 24		34.0 - 35.0 m	CL
3.0 m - 21		35.0 - 37.2 m	. CM
4.0 m - 33		37.2 - 39.0 m	CL-CM
		39.0 - 39.5 m	СМ
		39.5 - 43.2 m	CL - CM
		43.2 - 43.8 m	СМ
		43.8 - 45.0 m	CL
		45.0 - 48.6 m	CM - CH
		48.6 - 50.0 m	CL - CM

# Table11.2.2-38 Summary of Drilling Results at the Yao Flood Control Dam (2)

· · · · · · · · · · · · · · · · · · ·	DH - 5 (L=30.0 m, G.L	(EL) 328.4)	
	Location: Left side me	untain arca	
G	eological Condition	Rock Class.	Condition
Depth	Geology	Depth	Rock Class.
0 - 3.3 m	Soil	0 - 6.0 m	Soil
3.3 - 15.0 m	Shale	6.0 - 7.0 m	D - CL
15.0 - 16.0 m	Sandstone	7.0 - 9.0 m	D
16.0 - 30.0 m	Shale interbedded with s.s.	9.0 - 10.0 m	D - CL
		10.0 - 15.4 m	CL
N value, 1.0 m - 12		15.4 - 16.1 m	CL
2.0 m - 14		16.1 - 16.5 m	CM
3.0 m - 37		16.5 - 23.3 m	CL
		23.3 - 27.0 m	CM
		27.0 - 29.0 m	CL - CM
		29.0 - 30.0 m	CM - CH

	DH - 6 (L=30.0 m, G.I	L.(EL) 315.9)	
······································	Location: Left side me	ountain area	
Geo	logical Condition	Rock Class.	Condition
Depth	Geology	Depth	Rock Class.
0 - 3.0 m	Soil	0 - 3.5 m	D
3.0 - 30.0 m	Sandstone	3.5 - 9.0 m	CL
		9.0 - 18.2 m	CL - CM
N value, 1.0 m - 10	•	18.2 - 20.5 m	СМ
2.0 m - 14		20.5 - 23.1 m	CL - CM
3.0 m - 10/0	1	23.1 - 23.9 m	СМ
A A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR AND A CONTRA		23.9 - 24.1 m	D
		24.1 - 25.5 m	CM - CH
		25.5 - 26.0 m	CL
		26.0 - 26.8 m	CM
		26.8 - 28.0 m	CL - CM
1		28.0 - 28.3 m	CM - CH
		28.3 - 28.5 m	CL - CM
		28.5 - 29.0 m	CM - CH
		29.0 - 29.5 m	CL
		29.5 - 30.0 m	СМ

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		Geology	; ;	Roz	Soil	Nor	Soil	Shale	Sandstone	Sandstone	Sandstone	Sandstone	Sandstone	Sandstone	Sandstone	Sandstone	S.s., Shale	Shale	Shale, S.s.	Sandstone	Sandstone	Sandstone														
	DH-3 (EL_295.8)	L.		OUS	ous	23	76.5	22.2	18.2	15.4	15.5	19.6	175	17.5	15.9	16.0	15.4	15.4	15.4	16.7	16.7	5.7	6.5	2.5	2.2	2.7	3.0	4.5	44	4,4	5.3	5.0	5.9	6.6	6.6	
	DH-3	k (cm/sec)		impervious	impervious	1.2×10 <sup>-2</sup>	9.9×10 <sup>-1</sup>	2.9×10 <sup>-1</sup>	2.4×10 <sup>-4</sup>	2.0×10 <sup>-4</sup>	2.0×10 <sup>-4</sup>	2.6×10 <sup>+</sup>	2.3×10 <sup>-4</sup>	2.3×10 <sup>-1</sup>	2.1×10 <sup>-1</sup>	2.1×10 <sup>-1</sup>	2.0×10 <sup>-1</sup>	2.0×10 <sup>-1</sup>	2.0×10"	2.2×10 <sup>-1</sup>	2.2×10 <sup>-1</sup>		:		1	-	1	1	1	-	ł	1		-		* G.W.L.: GL-13.0 m (24/7/98)
		Depth	ĥ				;	5.0	6.0	7.0	8.0	9.0	10,0	11.0	12.0	13.0	14.0	15.0	16.0	17.0	18.0	21.0	24.0	27.0	30.0	33.0	36.0	39.0	42.0	45.0	48.0	51.0	54.0	57.0	60.0	: GL-13.0
am (1)		Testing Depth	From	1.3	2.3	3.3	4.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0	11.0	12.0	13.0	14.0	15.0	16.0	17.0	18.0	21.0	24.0	27.0	30.0	33.0	36,0	39.0	42.0	45.0	48.0	51.0	54.0	57.0	* G.W.L
trol D	[		.	-					Ļ L	<u> </u>		[ _				Σ						[		Г.,		E	CH	X		. <u> </u>	X			Γ	सि	ĺ
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ie Yao Fl		Geology	Country .	Soil	Soil	Soil	Tuff	Tuff	Tuff	Tuff	Tulf	Tuff	Tuff	Tuff	Tuff S.s.	S.s., Shale	Shale, S.s.	Sandstone	Sandstone	Sandstone	Sandstone	Sandstone	Sandstone	Sandstone												
Fest at th	DH-2 (EL.283.5)			40.8	1,530.8	286.9	286.9	37.8	21	9.5	62.5	88.5	103.8	7.5	1.6	<b>5.</b> 8	9.4	8.0	9.3	4.6	18.5	4.6	4.6	4.6	6.3	22.2	2.2	27.8	1.6	1.5	1.5	27.8	37.1	46.4	50.5	
Lugeon [	DH-2 (		K (cm/sec)	5.3×10	2.0x102	3.7×10	3.7×10 <sup>-3</sup>	4.9×10 <sup>-1</sup>	2.7×10 <sup>3</sup>	1.2510	8.1×10 <sup>-4</sup>	$1.2 \times 10^{-3}$	1.4×10 <sup>-3</sup>	9.7×10 <sup>3</sup>	$2.1 \times 10^{3}$				1.2×10 <sup>-1</sup>	6.0×10 <sup>-5</sup>	2.4×10-4	6.0×10 <sup>-5</sup>	6.0×10 <sup>-3</sup>	6.0×10 <sup>-3</sup>	8 2~10 <sup>-3</sup>	2.9×10 <sup>-4</sup>	1	3.6×10 <sup>-1</sup>	1	1	:	3.6×10 <sup>-1</sup>	4.8×10 <sup>-1</sup>	6.0×10 <sup>-4</sup>	6.6×10 <sup>-4</sup>	(86/1/61)
.39 Results of Lugeon Test at the Yao Flood Control Dam (1)		┝	Γ					00	10.0	12.0	13.0	15.0	16.0	18.0	21.0	24.0	27.0	30.0	33.0	36.0	39.0	0.04	45.0	48.0	005	240	57.0	60.08	63.0	0.99	69.0	72.0	75.0	78.0	80.0	3L-3.2 m
		Testing Depth	From	3.0	4.0	0.9	2.0	202		00	120	130	15.0	16.0	18.0	21.0	74.0	27.0	0.05	33.0	36.0	0.05	0.04	45.0	18.0		54.0	57.0	0.05	0 69	0.99	0.69	0.4	75.0	0.82	* G.W.L.: GL3.2 m (197798)
11.2.2	L	ـــــــــــــــــــــــــــــــــــــ		L +-		1	<u> </u>					<u> </u>	<u> </u>		<u> </u>	<u> </u>	L T	]	L.,	1. -	]	L า	1	1	Ļ	Ļ	<u>]</u>	.	Ŀ	1	. I	Ļ	1	<u>]</u> .	<u> </u>	].
<b>Table 11.2.2-39</b>			Rock Class.	٩	U					1			DWCH	HO-WO	HU-WC	CM-CH	E-NC	HU-WU		NO NO													:			
			Geology	Sail	Shale .	Shale	Shale	Challe	OBAIN CL-1-0-1	Chale, 0.5.	Canusumer			14 14		Tuff								and an and	OII VAUAC			÷								
	A11 1 A11 A11 A	(01170010	7	2121	5 7	120.2	9.00	0.00	120.9	13.2	1.0/	0.0	0.0	<b>t</b> 0		4		0 / 2		3				Jugeon Value	ingenea Lager	y Lugeon test				÷		• .				
		T-HIM	k (cm/sec)	1 0110-3	1.0X10	0.0X10	1./X10 1.7.10 <sup>-3</sup>	1.2X10	L. /XLU	1.7×10	9.9X10	4.3X10	4.3X10	1			201.00	8./X10	0.1710	1			(06/0/07)	* ic coefficient of permeabury, Lu: Lugeon vanc	* Lugeon value: thin ligures snow converted Lageon value;	dense figures show Lugcon value by Lugton test										
			T		╉	+	╉		╉		·	+	+	0.12	0.00	0.00		+	╉	10.04	40.0		ш-т/.2 Ш	cal of pera	lue: thin 1)	res show L										
		i	Lesting Lieptin	LIOH		╉	+	┥	╡		+	-	╉	╉	╈	╉	+	╉	╉	╉	╉	4/.0	06/0/07 m (7/1/20 m (70/0/20)	Lic coeffici	Lugeon va	dense figu					÷					· .
			ſ	7[	ſ	ſ	1	1			<u> </u>	1	1	<u> </u>	1	1	1	<u> </u>		<u> </u>	1	<u> </u>	• •	• •	÷		•									•.
																											• .								1	

l Dam (2)		
Flood Contro		
est at the Yao	EL-328.4)	
Table 11.2.2-40 Results of Lugeon Test at the Yao Flood Control Dam (2)	DH-5 (EL.328.4)	
Table 11.2.2-40 F		

Rock Class.

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k (cm/sec)

Testing Depth

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DH-6 (EL 315.9)

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\* G.W.L.: GL-2.0 m (10/7/98)

CLCM, CM-CF С С

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		DH-4	DH-4 (EL.330.8)					2-HG
Testing	Testing Depth	V (cm/tec)	. I	Ganhow	Bock Class	Testing	Testing Depth	h-(rm(sec)
From	To	* (vanov)	1	(Simo)	TAUL CHANGE	From	To	* (www.cr)
13		3.1×10 <sup>-3</sup>	235.4	Soil	D	2.3	1	1.2×10 <sup>-4</sup>
2.3	-	1.7×10 <sup>-3</sup>	133.1	Soil	D	3.3		1.1×10 <sup>-4</sup>
3.3	Ì	1.2×10 <sup>-3</sup>	92.3	Soil	Ð	4.0	-1	9.9×10 <sup>-4</sup>
4.3		1.4×10 <sup>-3</sup>	106.9	Soil	A	5.0	1	8.0×10 <sup>-4</sup>
5.0		1.2×10 <sup>-3</sup>	91.5	Soil	Ð	6.0	1	1.2×10 <sup>-3</sup>
6.0	Ì	1.2×10 <sup>-3</sup>	91.5	Shale	٩	7.0	1	1.1×10 <sup>-3</sup>
7.0	1	1.0×10 <sup>-3</sup>	78.5	Shale	A	8.0	1	1.1×10 <sup>-3</sup>
8.0	;	9.9×10 <sup>-1</sup>	76.5	Shale	Á	9.0	1	9.7×10 <sup>-4</sup>
9.0		8.8×10 <sup>-4</sup>	68.0	Shale	D	10.0	1	8.8×10 <sup>-4</sup>
10.0		8.8×10 <sup>-4</sup>	67.3	Shale	Δ	10.0	12.0	3.2×10 <sup>-4</sup>
11.0	-	8.0×10 <sup>-1</sup>	61.2	Shale	D-CL	12.0	15.0	2.5×10 <sup>-4</sup>
12.0	-	7.3×10 <sup>-1</sup>	56.1	Shale	D	15.0	18.0	1
13.0	1	6.7×10 <sup>-1</sup>	51.8	Shale.	Ω	18.0	21.0	1
14.0		6.5×10 <sup>+</sup>	50.2	Shale	D-CL	21.0	24.0	1
15.0	-	6.1×10 <sup>-1</sup>	46.9	Shale	D-CL	24.0	27.0	1
16.0		5.7×10 <sup>-4</sup>	44.0	Shale	Ω	27.0	30.0	1
17.0		5.6×10 <sup>+</sup>	43.2	Shale	ġ	* G.W.L.	* G.W.L.: GL-10.0 m (2/8//98)	m (2/8//98)
18.0	<b>!</b>	5.7×10 <sup>4</sup>	44.2	Shale	Ð			
19.0		5.4×10 <sup>+</sup>	41.8	Shale	Q			
20.0	1	4.6×10 <sup>-4</sup>	35.2	Shale	9			
21.0		5.3×10 <sup>-1</sup>	40.8	Shale	Q			•
22.0		4.7×10 <sup>-1</sup>	36.2	Shale	٩			
23.0		4.5×10 <sup>-1</sup>	34.6	Shale	۵			
24.0		3.8×10	29.2	Shale	Ð			
25.0	-	4.5×10	34.6	Shale	۵			
26.0		5.2×10 <sup>-4</sup>	39.9	Shale	Q			
27.0		5.2×10 <sup>-1</sup>	39.9	Shale	۵			
28.0		1.0×10 <sup>-3</sup>	80.0	Shale	D			
29.0	-	1.0×10 <sup>-3</sup>	80.0	Shale	٩			
30.0	1	1.0×10	80.0	Shale	Q			
31.0	-	1.0×10 <sup>-3</sup>	80.0	Shale	Q			
32.0	-	1.1×10 <sup>-3</sup>	86.2	Shale	A			
33.0	1	1.1×10 <sup>-3</sup>	86.2	Shake	٩			
34.0		$1.1 \times 10^{-3}$	86.2	Shale	Q			
34.0	35.0	1.6×10 <sup>-4</sup>	12.3	Shale	CL	41.0	44.0	2.4×10 <sup>-4</sup>
35.0	38.0	1.9×10 <sup>-4</sup>	14:2	Shale, S.s.	CLCM CM	44.0	47.0	2.9×10 <sup>-4</sup>
38.0	41.0	1.9×10 <sup>-4</sup>	14.2	Sandstone	CL-CM, CM	47.0	50.0	2.9×10 <sup>-4</sup>
			<continue th="" to<=""><th><continue left="" sheet="" side="" the="" to=""></continue></th><th>cet&gt;</th><th>* G.W.L</th><th>: GL -23.0</th><th>* G.W.L.: GL-23.0 m (24/6//98)</th></continue>	<continue left="" sheet="" side="" the="" to=""></continue>	cet>	* G.W.L	: GL -23.0	* G.W.L.: GL-23.0 m (24/6//98)

41.0	44.0	2.4×10 <sup>-4</sup>	18.1	Sandstone	CL, CL-CM, CM
44.0	47.0	2.9×10 <sup>-4</sup>	22.6	Sandstone	CI, CM-CH
47.0	<b>50.0</b>	2.9×10 <sup>-4</sup>	22.6	Sandstone	CL-CM, CM-CH
* G.W.L	.: GL-23.0	* G.W.L.: GL-23.0 m (24/6/98)			

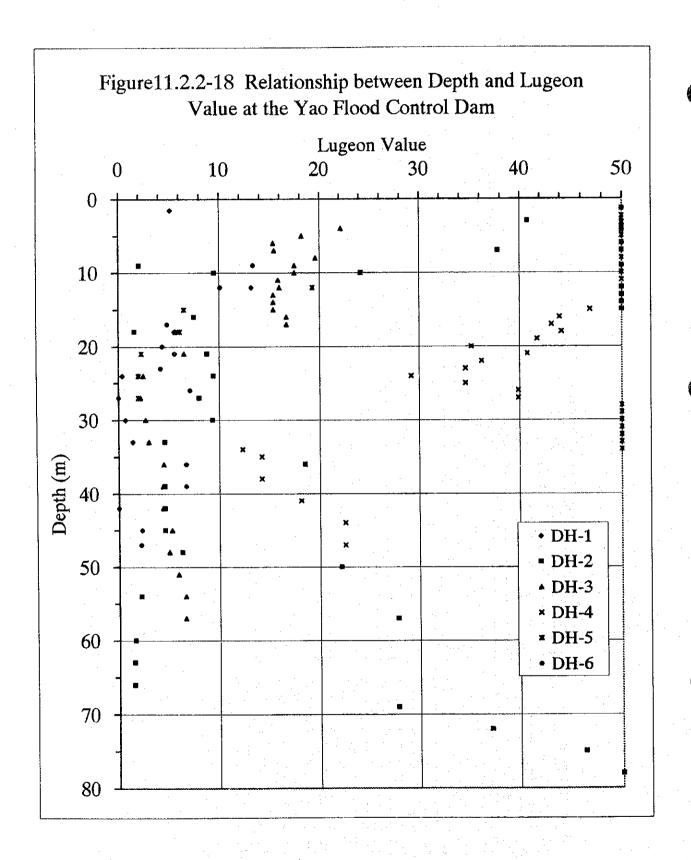


Table11.2.2-41 Results of Test Pitting and Augerhole Drilling at the Proposed Borrow Area

	1 auto1.2.2.4	-+T NCOULD VI		רפר ד זווווע מ	Semeral violandance and Summer 1951					
Pit No.	Depth (m)	USCS		Pit No.	Depth (m)	USCS	Ŀ	Pit No.	Depth (m)	USCS
TP.A1	0 - 4.0	ML		A.1	0 - 2.5	ML	A	A.31	0 - 2.1	ML
TP.A4	0 - 4.0	ML		A.2	0 - 2.1	GM	A	A.32	0 - 2.1	ML
TP.A5	0-2.0	ML		A.3	0-2.5	ML	A	.33	0 - 2.8	· ML
	2.0 - 4.0	GM		A.4	0 - 1.8	ML	A	A.34	0 - 2.3	ML
TP.A8	0-4-0	ML		A.5	0 - 1.5	ML	Α	A.35	0 - 2.4	ML
TP.A11	0-2.0	GM		A.6	0 - 2.2	ML	A	A.36	0 - 1.8	ML
TP.A12	0-2.0	ML	-	A.7	0 - 4.0	ML	A	.37	0 - 1.2	ML
<b>TP.A15</b>	0 - 4.0	ML		A.8	0 - 1.8	ML	A	A.38	0 - 2.7	ML
TP.A16	0 - 4.0	ML		6'V	0 - 2.0	ML	A	A.39	0 - 2.2	ML
TP.A17	0-4-0	ML	•	<b>A.</b> 10	0 - 2.0	ML	A	<b>A.</b> 40	0 - 2.0	ML
TP.A19	0-4-0	ML	* .	A.11	0 - 1.7	GM	A	A.41	0 - 1.7	SM
TP.A22	0-4-0	ML	•	<b>A</b> .12	0 - 3:0	ML	A	A.42	0 - 2.1	ML
TP.A24	0 - 4.0	ML		A.13	0 - 2.3	ML	Y	.43	0 - 1.8	ML
TP.A27	0-4.0	ML		A.14	0-3.0	ML	Y	A.44	0 - 2.3	ML
TP.A28	0-4-0	ML		A.15	0 - 2.5	ML	A	A.45	0 - 1.2	ML
TP.A30	0 - 4.0	ML		A.16	0 - 2.1	ML	A	A.46	0 - 2.1	ML
TP.A33	0-2.0	ML	۰.	A.17	0 - 3.0	ML	A	A.47	0 - 1.5	ML
	2.0 - 4.0	SM		A.18	0 - 1.5	ML		A.48	0 - 2.2	ML
TP.A36	0 - 4.0	ML		A.19	0 - 2.3	ML	A	.49	0 - 2.6	ML
TP.A38	0-4-0	ML		A.20	0 - 1.5	ML	A	A.50	0 - 1.5	ML
TP.A41	0-40	SM		A.21	0 - 2.5	ML	V	A.51	0 - 1.5	ML
TP.A45	0-4.0	ML		A.22	0 - 1.1	ML	A	52	0 - 1.5	ML
TP.A47	0 - 4.0	ML		A.23	0 - 3.0	ML	Y	A.53	0 - 1.0	SM
TP.A51	0-4.0	ML		A.24	0 - 2.0	ML	A	A.54	0 - 2.1	ML
TP.A53	0 - 4.0	SM		A.25	0 - 1.0	ML	A	A.55	0 - 4.0	ML
TP.A55	0 - 4.0	ML		A.26	0 - 2.0	ML	<b>V</b>	A.56	0 - 2.0	ML
TP.A57	0 - 1.5	ML		A.27	0 - 2.5	ML	<	A.57	0 - 1.5	ML
	1.5 - 4.0	GM	•	A.28	0 - 2.2	ML				
				A.29	0 - 2.1	ML				
				A.30	0 - 1.5	ML				

\* USCS: Unified soil classification system

\* ML: Inorganic silts and very fine sands, rock flour, silty or clayey fine sands, or clayey silts, with slight plasticity.

GM: Silty gravels, gravel-sand-clay mixtures. SM: Silty sands, sand-silt mixtures.

Sample	Sampling	Atter	tterberg Limits (%)	(%)		Grad	Gradation (% Passing)	ssing)		uscs
	Depth	TT.	PL.	PL.	#3/4	#4	#10	#40	#200	Group
TP.A5	2.0 - 4.0 m	30.2	27.3	2.9	100.0	58.4	43.3	24.4	19.1	GM
TP.A12	0 - 4.0 m	36.1	26.3	9.8	100.0	- 9°66	1.66	94.6	86.8	ML
TP.A16	0 - 4.0 m	38.9	32.8	6.1	100.0	87.9	84.5	83.2	81.8	ML
TP.A17	0 - 4.0 m	38.5	31.8	6.7	100.0	78.2	70.5	59.3	50.7	ML
TP.A28	0 - 4.0 m	41.8	30.0	11.8	100.0	92.1	85.4	80.1	77.1	ML
TP.A30	0 - 4.0 m	46.6	37.1	9.5	100.0	84.7	73.9	63.9	58.4	ML
TP.A33	0 - 2.0 m	48.3	30.4	17.9	8		100.0	96.5	89.8	ML
	2.0 - 4.0 m	29.9	26.0	3.9	100.0	91.7	84.5	60.9	44.3	SM
TP.A38	0 - 4.0 m	33.8	29.7	4.1	100.0	98.4	96.7	84.7	67.5	ML
TP.A41	0 - 4.0 m	29.3	27.1	2.2	100.0	90.8	78.6	55.0	37.1	SM
TP.A53	0 - 4.0 m	36.7	32.4	4.3	100.0	90.2	81.7	57.8	43.6	SM
	* USCS. Hnified soil classification sys	ation system		-						

Table 11.2.2-42 Results of Soil Test at the Proposed Borrow Area

\* USCS: Unified soil classification system

\* ML: Inorganic silts and very fine sands, rock flour, silty or clayey fine sands, or clayey silts, with slight plasticity.

GM: Silty gravels, gravel-sand-clay mixtures. SM: Silty sands, sand-silt mixtures.

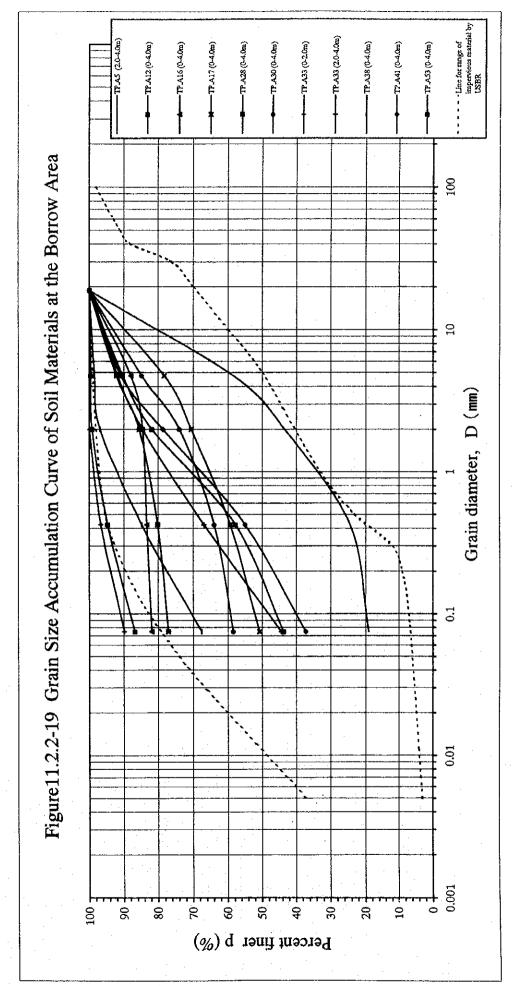


		Table 11.	2.2-43 R	.2.2-43 Results of Water Quality Analysis	water (	<b>Juanty A</b>	nalysis			:
			ST.1	r.1	ST.2	1.2	ST.3	.3	ST.4	4
			DHB	DHBJ 26.0	Pangtham	tham	Phusang waterfall	waterfall	Phusang river	g river
		ppmepm	uudd	epm	bpm	epm	ppm	epm	ppm	epm
Hq		1	7.6	1	7.7		7.6	1	7.4	1
Conductivity	micromho/cm		570.0		450.0		200.0		510.0	3 9 9
Temperature		1			22.2		27.5		24.5	1
Chloride	<u>cı</u>	0.02820	1.9	0.05	1.1	0.03	0.7	0.02	0.7	0.02
Bicabonate Alkalinity	CaCO <sub>3</sub>	0.01998	236.0	4.72	197.0	3.94	234.0	4.68	76.0	1.52
Sulfate	$So_4^{2-}$	0.02082	28.0	0.58	5.0	01.0	4.0	0.08	2.5	0.05
Nitrate	Z	1	0.02 or less		0.7		0.0		0.3	
Calcium	Ca <sup>2+</sup>	0.04990	33.0	1.65	74.0	3.69	69.0	3.44	19.0	0.95
Magnesium	Mg <sup>2+</sup>	0.08224	4.1	0.34	2.9	0.24	11.5	0.95	4.1	0.34
Potassium	$\mathbf{K}^{+}$	0.02558	0.4	0.01	0.4	10:0	1.4	0.03	1.5	0.04
Sodium	Na <sup>+</sup>	0.04350	84.0	3.65	2.9	0.13	7.0	0.31	6.8	030
* nnm · narts ner milion (mo/liter)		* enm · conivalent ner million	valent ner m	nillion						

Table 11 2 2.43 Decults of Water Analysis

\* ppm : parts per milion (mg/liter), \* epm : equivalent per million \* ST.1 (DHBJ 26.0) : aquifer water, ST.2 (Pangtham) : water from limestone cave, ST.4 (Phusang river) : river water in front of waterfall

# Geological Relationship between Tunnel and Phu Sang Waterfall

Geological condition of the section from STA.7+050 to STA.10+000 consists of the CPnb formation in Carboniferous-Permian age which is characterized by foliated dark gray slate interbedded with sandstone. Overburden condition shows 120 to 340 m in thickness and rock facies indicate medium hard to hard but somewhat breakable along bedding plain of the slate.

Geological condition from STA.7+050 to STA.10+000 consists of the CPnb formation characterized by foliated dark gray slate interbedded with sandstone. According to the drilling data, the geological condition shows sandstone and slate as follows.

Drilling Depth	Soil	Sandstone	Shale, slate	Phyllite
120 m	7.0 m	56.9 m	54.6 m	1.5 m

Classification of Geological Condition of Borehole No. DHB-5

The section from STA.10+000 to STA.11+200 is located on the northern part of the heated groundwater area (Phu Sang spring area). This spring has 27.5° C (river water is 24.5° C) water temperature and 498 micro-s/cm in conductivity.

The results of TEM prospecting reveal the existence of extremely low resistivity (5 to 10 ohm-m or less) from which it is inferred that cracks of basement rock at this area may be partly filled up by the above heated water.

These resistivity values may support the idea that geological condition of this area is derived from marine sediments.

Furthermore, their thermal origin is presumed to be related to the igneous rocks (granite or porphyry), which is continued for a great depth at a deeper portion, and some faults located around this section may be regarded as a passage of the heated groundwater.

In addition, this heated groundwater is characterized by rich in calcium according to the results of water quality analysis.

In accordance with the water pressure test at the drilling hole No.DHB5, the result shows the very low permeability from 1.3 to 1.8 Lugeon Value (Refer Table 11.2.2-13 Results of Lugeon Test (2) and following summary table), so that leakage of water during tunnel excavation will be judged to be small.

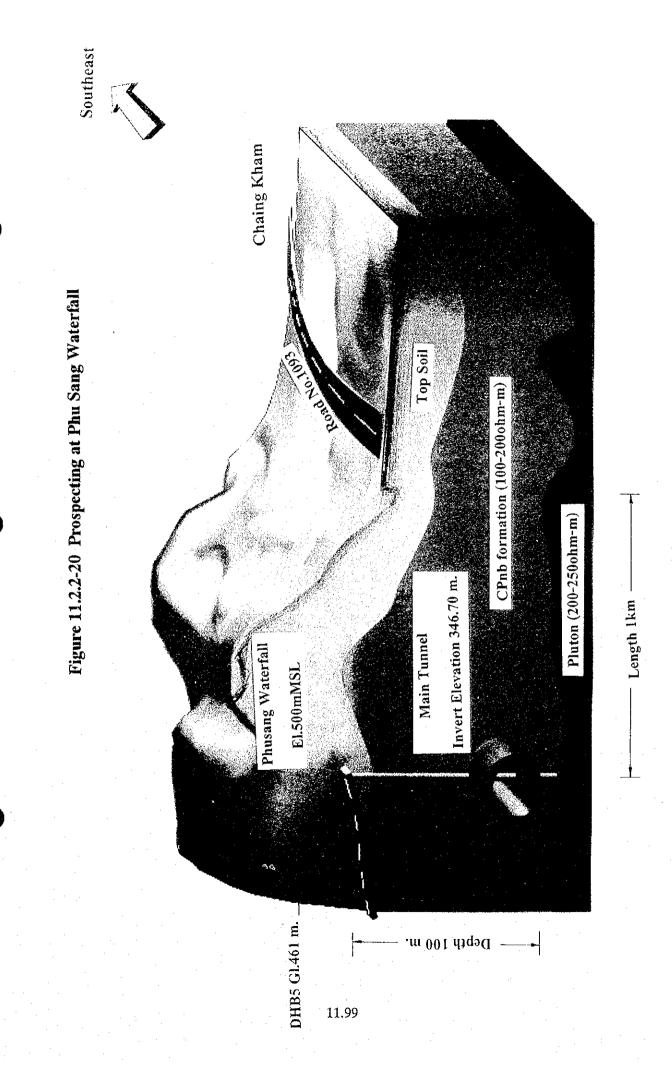
	+	4 - F				
Elevation of Borehole		G.H.461 m				
Testing Depth from G.H.(m)	105 - 110	110 - 115	115 - 120			
Testing Elevation	E.L.356 - 351	E.L.351 - 346	E.L.346 - 341			
Max. Water Pressure (kgf/cm <sup>2</sup> )		15.4				
Lugeon Value	1.5	1.8	1.3			
Water Table (G.Hm)		-3.2 m				
Testing Date		June 26, '96				
Geological Period		Paleozoic				
Geological Age	C	arboniferous-Perm	ian			
Name of Geological Formation		Nam Bong				

#### **Results of Lugeon Test at Borehole No. DHB-5**

Boring Core Facies	Sandstone, Slate	Slate	Slate
Rock Class	CM, CL	CM	CH

Taking the whole geological information into consideration, it is inferred that tunnel alignment which passes around drilling hole No.DHB-5 location is situated on the outer area of the zone strongly affected by heated groundwater because that is located on the outside of remarkably low resistivity area.

The prospecting drawing around tunnel, drilling hole No.DHB-5 and the Phu Sang water fall are shown in Figure 11.2.2-20.



### **Comments for Additional Geological Investigation**

For confirmation of geological conditions in detail at/along the sites of each project facility, the following additional geological investigations should be performed prior to the detail design stage. The required additional geological investigation items, investigation points and drilling depths (survey length) etc. are shown in Table 11.2.5-1 to 11.2.5-5 and Figure 11.2.5-1 respectively.

#### (1) Kok Intake

Along the Kok intake axis and on the cross section (apron portion), at least 4 drilling investigations with in-situ test (standard penetration test) are required to confirm the geological conditions (bearing capacity) of foundation.

#### (2) Kok-Ing Diversion Canal

Along the Kok-Ing diversion canal route, drilling investigation should be performed for confirmation of geological condition at points of 1,000 m interval at least. The in-situ test (standard penetration test) accompanied with drilling should be performed for confirmation of bearing capacity of foundation. Furthermore, the drilling investigation should be also performed at the planning locations of facility such as the highway bridge.

\*Drilling investigation for foundation at the siphon facility have already been carried out up to this stage.

On the occasion of drilling investigation, if the geological condition of foundation is composed of thick sand layer or poor ground condition, in-situ test (the case of former is permeability test and that of the latter is lateral loading test (LLT)) should be performed together with drilling. Furthermore, laboratory test (physical test by grain size analysis, liquid limit test and plastic limit test etc.) by using of core sample should also be performed.

#### (3) Kok-Ing No.1 Tunnel

Along the Kok-Ing No.1 tunnel route, the following geological conditions in detail should be confirmed by the additional geological investigation, e.g. drilling investigation and geophysical prospecting survey (TEM, electromagnetic prospecting survey), prior to the detail design stage. Especially, electromagnetic prospecting survey is to be carried out along the whole section.

Confirmation of geological conditions around the tunnel inlet and outlet

These sections correspond to a shallow overburden condition and are necessary to confirm geological condition.

- Clarification of rock facies of Jv formation (rhyolite and tuff formation) and fault feature located around STA.1+260

As for JV formation, there is no drilling data at present.

## (4) Kok-Ing No.2 Tunnel

Along the Kok-Ing No.2 tunnel route, the following geological conditions should be confirmed by additional geological investigation such as drilling survey and geophysical prospecting survey (TEM, electromagnetic prospecting survey). Especially, electromagnetic prospecting survey is to be carried out along the whole section.

Confirmation of geological condition around the tunnel inlet and outlet

- These sections show a shallow overburden condition and it is necessary to confirm geological condition. Especially, around the tunnel inlet, the existence of limestone has been clarified by the performed drilling survey.
- Clarification of fault condition at the middle section of tunnel
- Confirmation of geological condition in detail of basalt lava and intrusion

#### (5) Ing Diversion Weir

Along the axis of the Ing diversion weir and intake facility, at least 7 drilling investigations with in-situ test (standard penetration test) are required to confirm the geological conditions (bearing capacity) of foundation.

#### (6) Ing-Yot Diversion Canal

Along the Lao diversion canal route, drilling investigation should be performed for confirmation of geological condition at points of 1,000 m interval at least. The in-situ test (standard penetration test) accompanied with drilling should be performed for confirmation of bearing capacity of foundation. Furthermore, the drilling investigation should also be performed at the planning locations of facility such as the siphon facility etc. At present, there is no geological investigation data along the Lao diversion canal route.

On the occasion of drilling investigation, if the geological condition of foundation is composed of thick sand layer or poor ground condition, in-situ test (the case of former is permeability test and that of latter is lateral loading test (LLT)) should be performed together with drilling. Furthermore, laboratory test (physical test by sieving test and Atterberg test etc.) by using of core sample should be also performed.

#### (7) Ing-Yot No.1 Tunnel

Along the Ing-Yot No.1 tunnel route, drilling investigation, seismic survey (refraction prospecting survey) and geophysical prospecting survey (TEM, electromagnetic prospecting survey) are required in order to confirm the geological conditions and lithological characteristics. Especially, electromagnetic prospecting survey is to be carried out along the whole section. At present, there is no geological investigation data along the Ing-Yot No.1 tunnel route.

#### (8) Ing-Yot No.2 Tunnel

Along the Ing-Yot No.2 tunnel route, the following geological conditions need to be clearly confirmed by additional geological investigation such as drilling survey, including geophysical logging test, and geophysical prospecting survey (TEM and TDEM, electromagnetic prospecting survey). In addition, on the occasion of drilling survey at the fault zone, the inclined drilling is of great use in confirming the scale of fault or fracture zone.

Confirmation of geological condition around tunnel inlet

These sections show a shallow overburden condition and it is necessary to confirm geological condition.

Clarification of lithological characteristics of basement rocks at the section between STA.0+800 and STA.3+250

It is necessary to confirm rock facies at the contact between porphyry (granite porphry) and PTRv formation. In addition, the rock facies of the TRhf formation should also be clarified.

Confirmation of geological condition and the scale of fault and fractured zone at the section from STA.3+140 to STA.3+250 section and around STA.7+000

It is required to confirm the detail geological condition, including permeable characteristic, of the above fault and fractured zone because they show clear large-scale fault features and are likely to affect tunnel construction.

Confirmation of hydrogeological mechanism of the heated groundwater around the Phu Sang spring area and proper assessment of the effects of tunnel construction

The results of the electromagnetic prospecting survey (TEM) and drilling revealed that the thermal origin may be related to the igneous rocks (granite or porphyry), which are continued to a great depth in the deeper portion, and some faults located around this section may be regarded as the passage for the heated groundwater. However, clear identification and solution of these problems should be considered in detail based on the additional investigation from the hydrogeological viewpoint, for example drilling investigation and electromagnetic prospecting survey (TEM) by grid method as setting for investigation lines, including detailed groundwater quality tests etc. Furthermore, drilling holes for investigation should be use as observation well to monitor fluctuation of water level and quality both under natural condition and tunnel construction. In addition, in advance of tunnel construction, the preceding drilling (pilot drilling) will suppose to check the existence of heated groundwater discharge

Checking of lithological condition of CPnb (Nam Bon) formation and CPhk (Huai Krai) formation

These formations are recognized along the long section of 20 km or more in tunnel length and show uniform rock facies, as a whole, of foliated slate interbedded with sandstone. Additional drilling and electromagnetic prospecting survey (TEM) are required to confirm the situation of presumed fault and fractured zone at/around the major river course such as the Huai Sai, Huai Herak and Hai Bong.

Problem of groundwater discharge from deeper depth in the PTRv formation around the existing drilling DHBJ26

Drilling of DHBJ26 revealed the existence of excellent confined aquifers, which may be formed along fissure situated in PTRv formation (tuff and dacite formation), at the deeper depth from 276 m. Additional drilling and electromagnetic prospecting survey (TDEM) is required to confirm the geological condition and scale of fault and fractured zone related to groundwater discharge. Furthermore, in advance of tunnel construction, the preceding drilling (pilot drilling) will suppose to check groundwater discharge from deeper.

Problem of groundwater discharge from the TRpl formation (limestone formation) of the Doi Pha Deang mountain around STA.28+500 to STA.30+100 section.

At the limestone formation and adjacent PTRv and TRhf formation, supplemental electromagnetic prospecting survey (TDEM) and several drillings, including the inclined drillings, are required for confirmation of geological condition (rock facies of limestone and contact condition of formations) and the existence of limestone cave. In this case, the electromagnetic prospecting survey (TDEM) should be applied as point sounding method around tunnel alignment because of difficult line setting by the rugged topographical condition. Furthermore, in advance of tunnel construction, the preceding drilling (pilot drilling) can be used to check groundwater discharge from limestone cave.

Confirmation of fault zone observed by TDEMB line 30.0

Supplementary geophysical prospecting survey (TDEM survey) and several drillings are required for confirmation of geological condition, rock facies and fault zone at/around this area.

Confirmation of geological condition of the TRhf (Huai Fak) formation

This formation, which is composed of sandstone and tuff interbedded with shale, are recognized over a distance of approximately 16.0 km long along the tunnel alignment. Additional drilling is required for confirmation of geological condition and the existence of fault at/around the major river course such as the Yean river.

Confirmation of geological condition around the highest mountain area (STA.38+000 to STA.45+000 section)

The geophysical prospecting survey (TDEM survey) is required to confirm the boundary line between ms 5-3 formation and TRhf (Huai Fak) formation and the rock facies along the tunnel level. The check drilling is also required for correlation of results of geophysical prospecting survey. Required drilling depth of borehole should be reached at least 150 to 200 m in the fresh rock.

Problem of groundwater discharge from the TRpl formation (limestone formation) around STA 46+000 to STA 47+100 section and STA 49+900 to STA 50+500 section.

Additional geophysical prospecting survey (TEM survey) and drilling, including the inclined ones, are required for clarification of geological condition and the existence of limestone cave. Furthermore, in advance of tunnel construction, the preceding drilling (pilot drilling) is need to check groundwater discharge from limestone cave.

Confirmation of geological condition around tunnel outlet

These sections show a shallow overburden condition and it is necessary to confirm geological condition.

## (9) Yao Flood Control Dam

At the Yao flood control dam, additional drilling investigations accompanying with lugeon test are required to confirm the geological condition in detail and permeable characteristics of dam foundation. At this site, the seismic survey (refraction prospecting survey) had already been performed in 1998. The required quantities for drilling are as follows.

- Along the dam axis: 5 holes in total (hole location of the left abutment should be planned in a dense pattern.)
- At the upstream and downstream of dam base : 6 holes in total (3 holes at the upstream and downstream, respectively)
- Along the spillway axis : 4 holes in total
- Along the diversion tunnel axis : 3 holes in total
- At the thin ridge between spillway and diversion tunnel : 2 holes

At the left abutment of dam, geophysical prospecting survey (TEM, electromagnetic prospecting survey) should be also performed to clarify the geological condition because there is a possibility of the existence of a large-scale fault zone on.

Furthermore, for embankment material of dam, soil tests should be performed in detail. Required test items and quantities, including test pitting at the proposed borrow site, are as follows.

Material	Test Item	Sample	Remarks
Test pitting		30 pits	At the proposed borrow site
Impervious	Physical test	20 samples	
material	Dynamic test	10 samples	
Semi-pervious	Physical test	20 samples	
material	Dynamic test	10 samples	
· · · · · · · · · · · · · · · · · · ·	Physical test and rock test	10 samples	
Pervious material	Dynamic test	5 samples	Soil test for pervious material should be performed by large-scale testing using excavation material of tunnel
	Rock test	10 samples	
Dilton - cotonial	Physical test	10 samples	
Filter material	Dynamic test	5 samples	

In this case, testing items for physical, dynamic and rock test are as follows.

- Physical test : specific gravity of soil particle, field water content, grain size analysis, liquid limit, plastic limit etc.
- Dynamic test : compaction, permeability, consolidation, shear strength (by tri-axial compression test) etc.
- Rock test : specific gravity and water absorption, compressive strength, stability, abrasion resistance