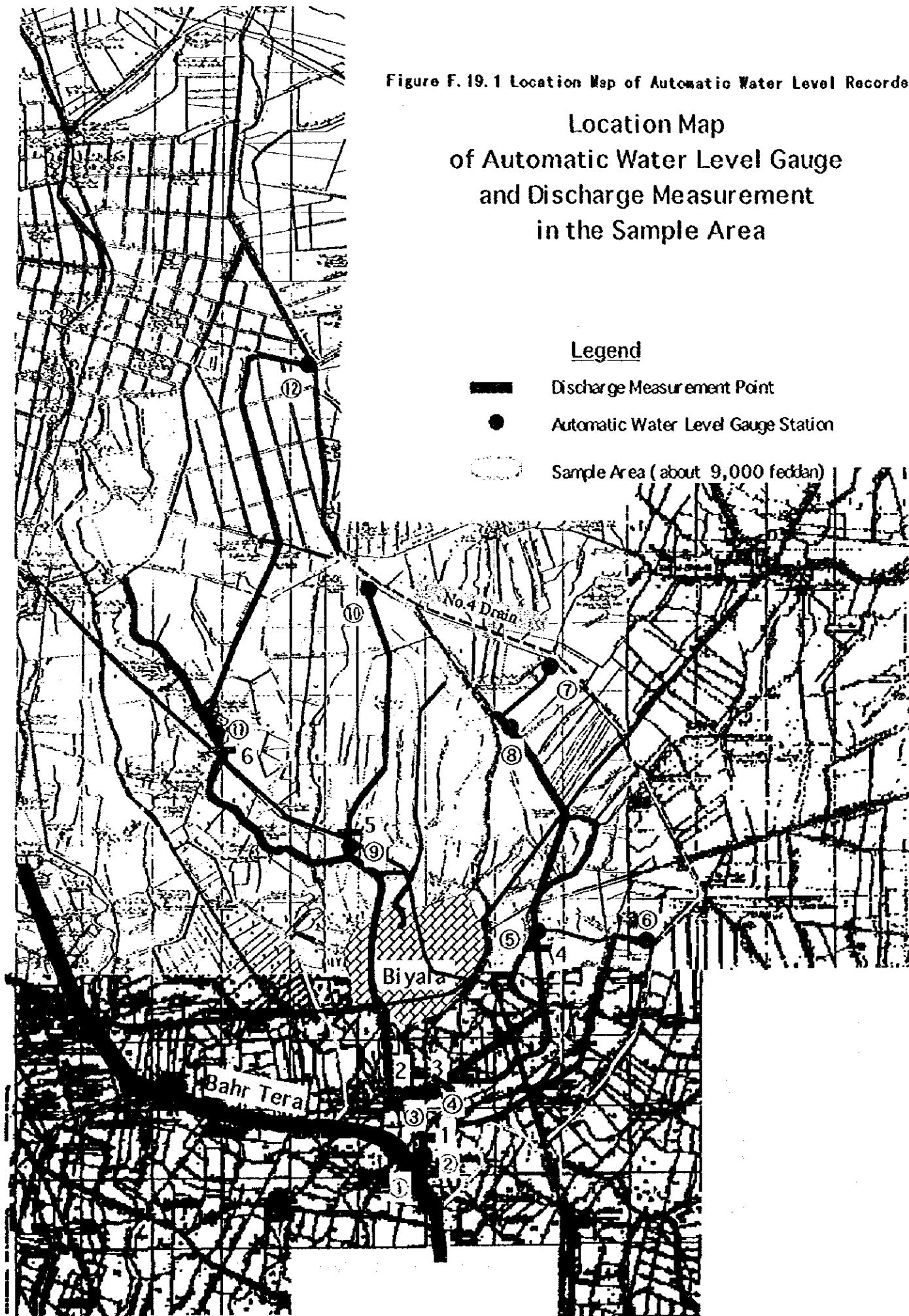


Figure F. 19. 1 Location Map of Automatic Water Level Recorders

Location Map
of Automatic Water Level Gauge
and Discharge Measurement
in the Sample Area

Legend

- Discharge Measurement Point
- Automatic Water Level Gauge Station
- Sample Area (about 9,000 feddan)



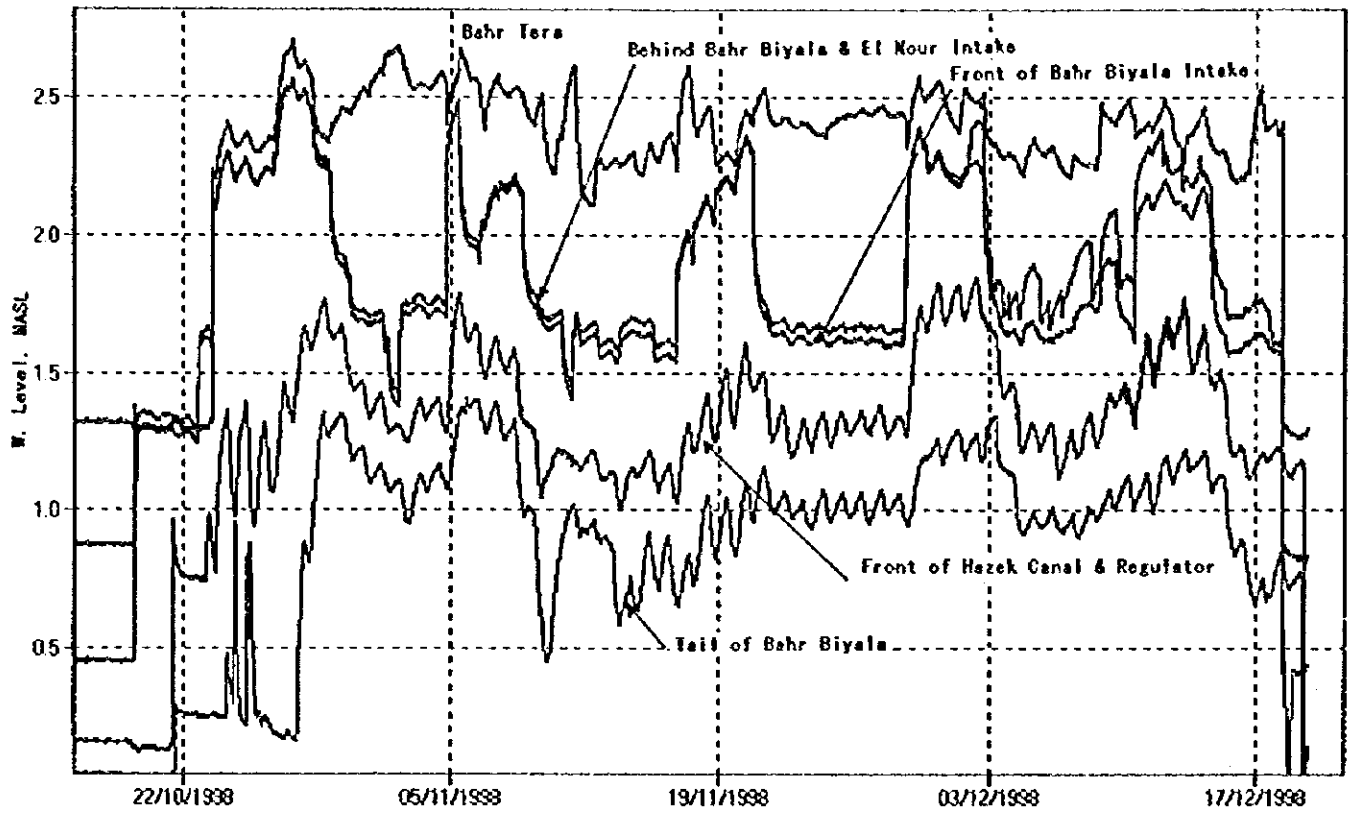


Figure F.19.3 Water Level Records for Bahr Biyala Related Canals

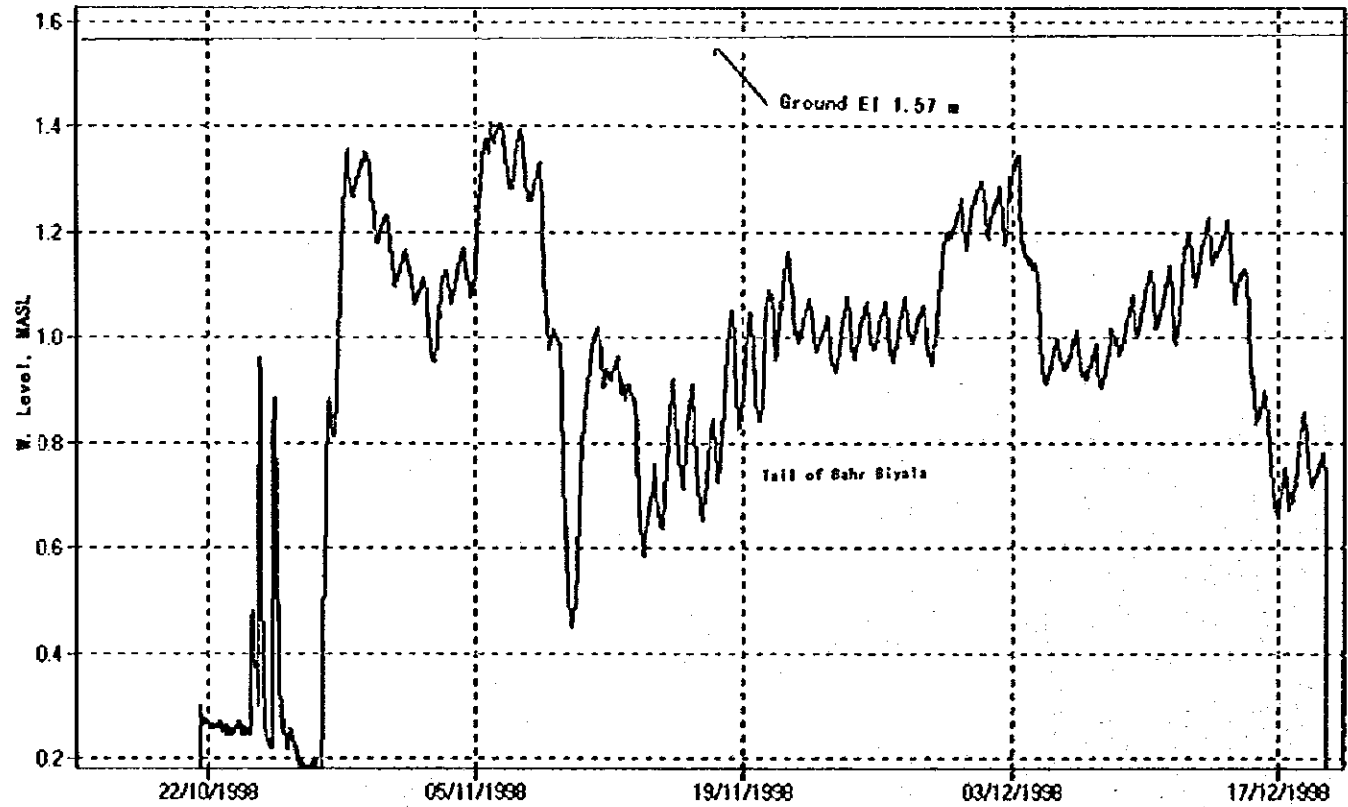


Figure F.19.4 Water Level Records at the Tail of Bahr Biyala

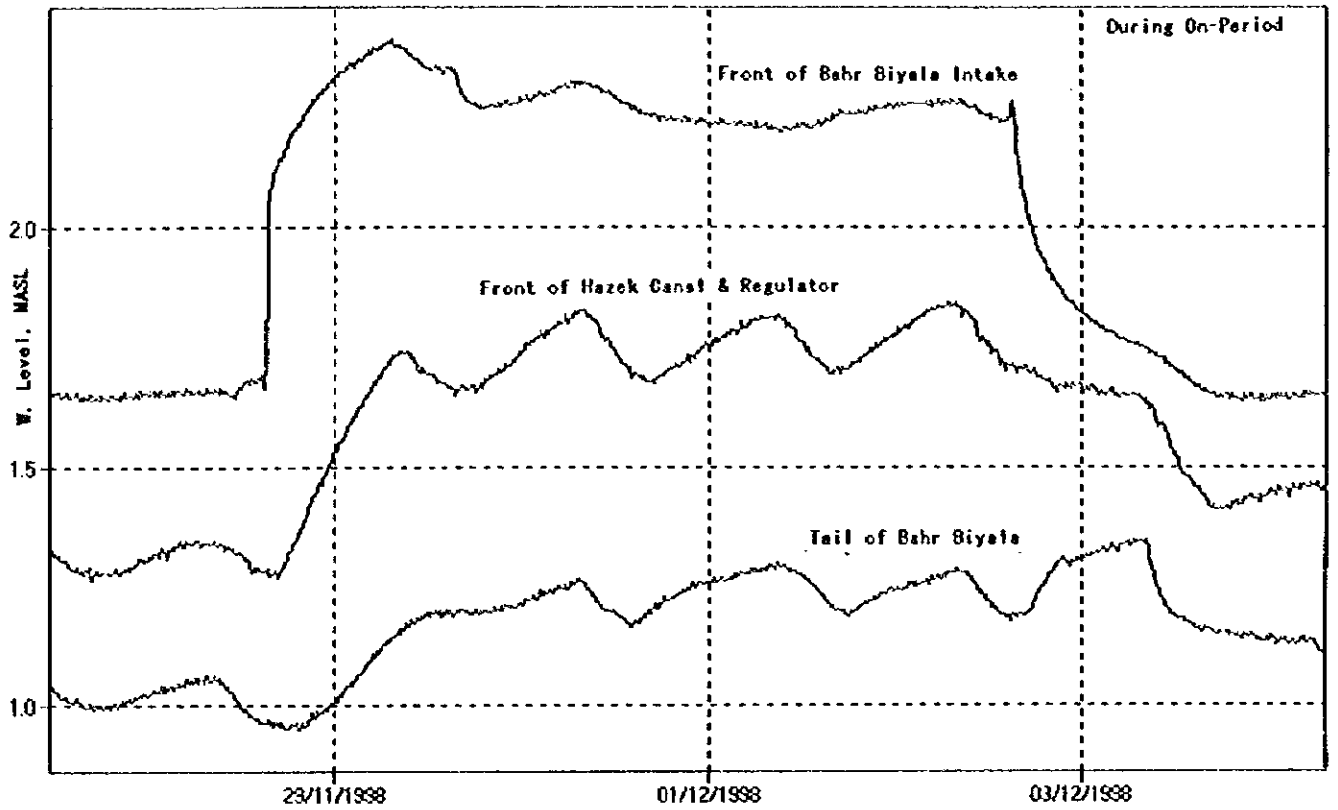


Figure F.19.5 Water Level Records for Bahr Biyal Canal during an On-period Only

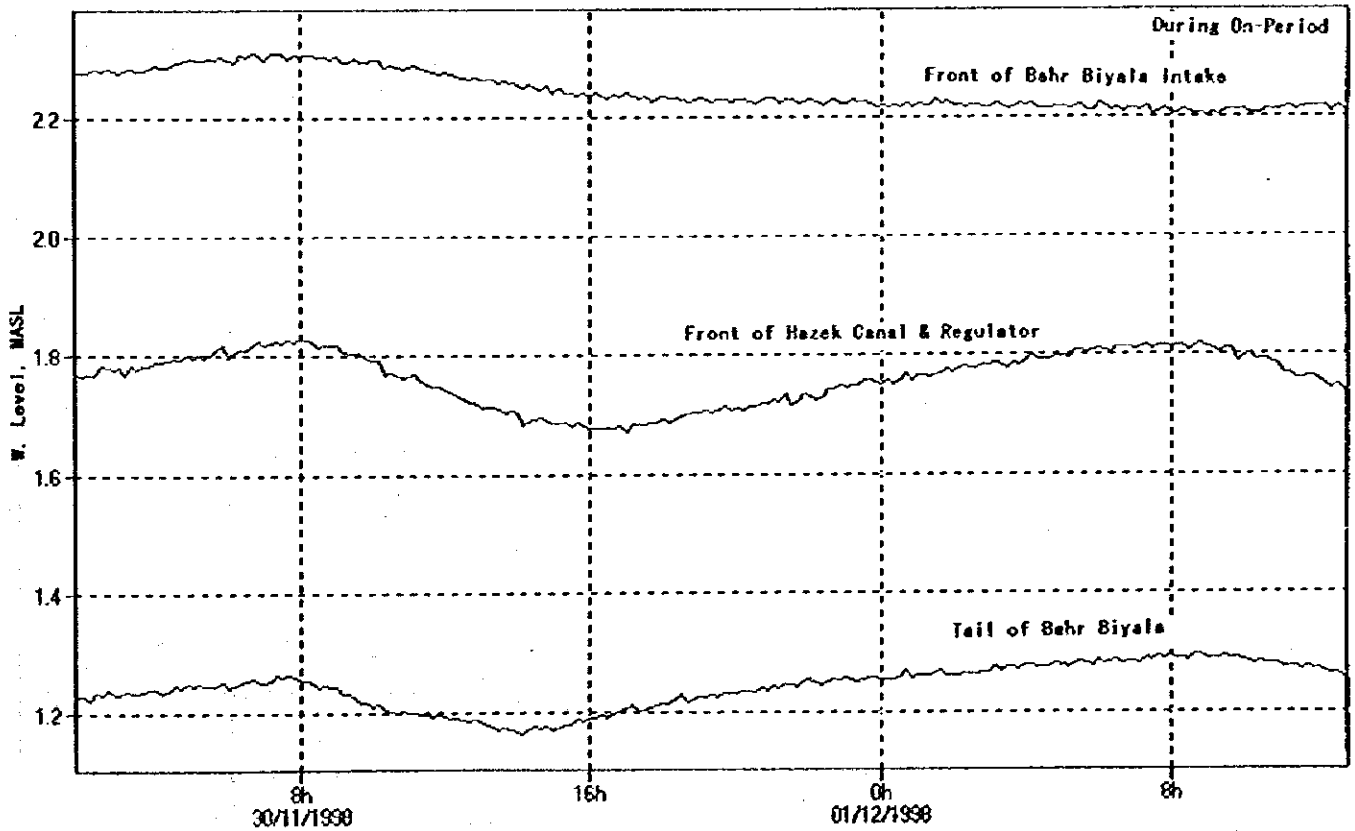


Figure F.19.6 Water Level Records for Bahr Biyal Canal during an On-period Only

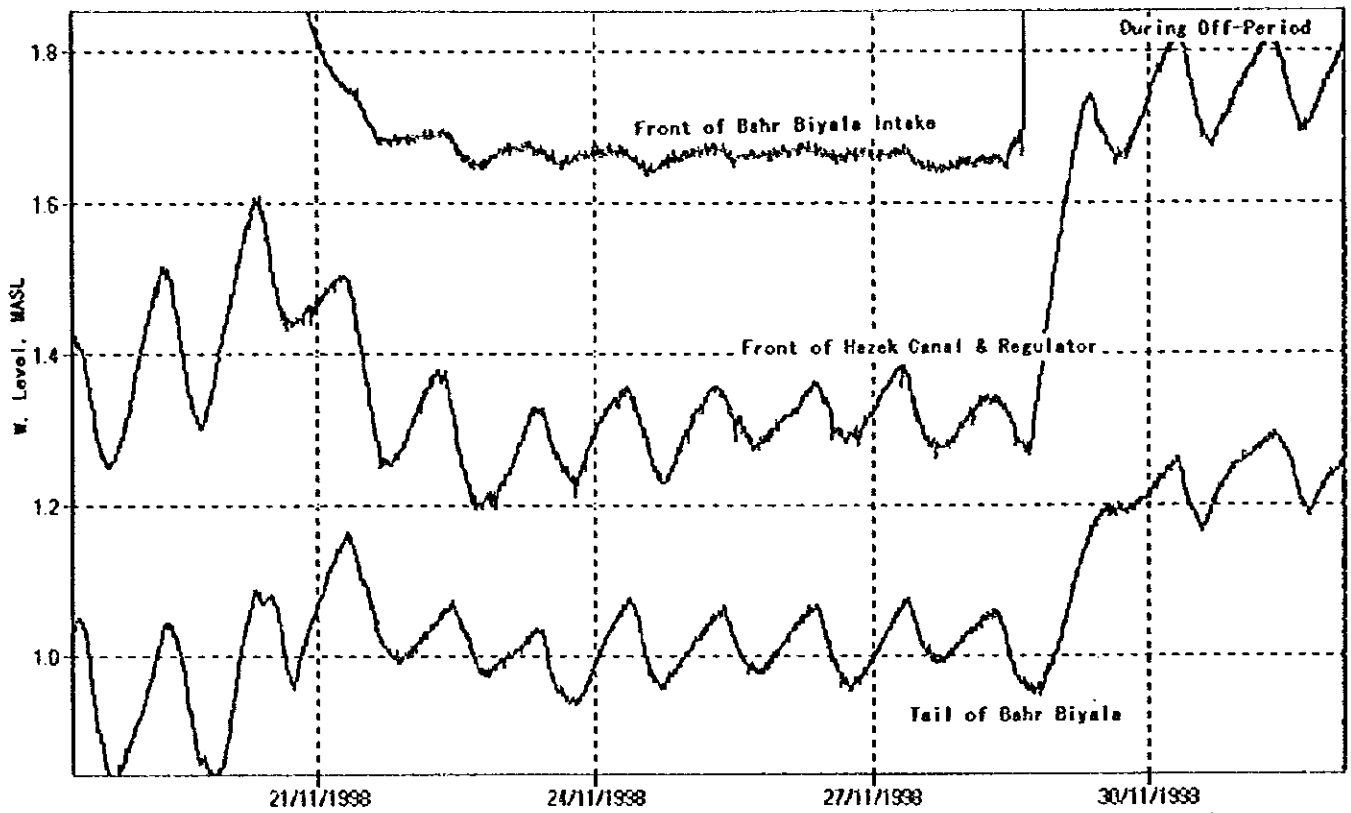


Figure F.19.7 Water Level Records for Bahr Biyal Canal during an Off-period Only

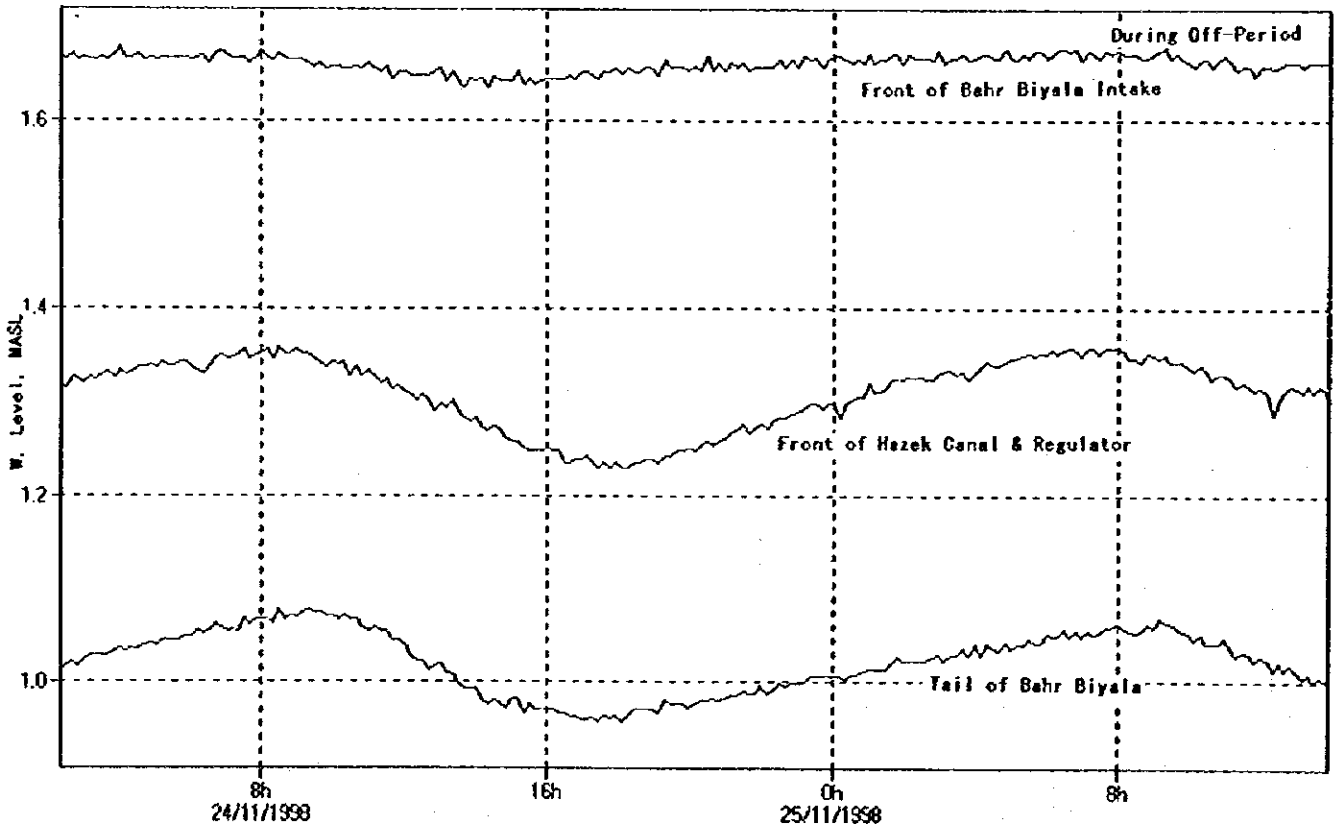


Figure F.19.8 Water Level Records for Bahr Biyal Canal during an Off-period Only

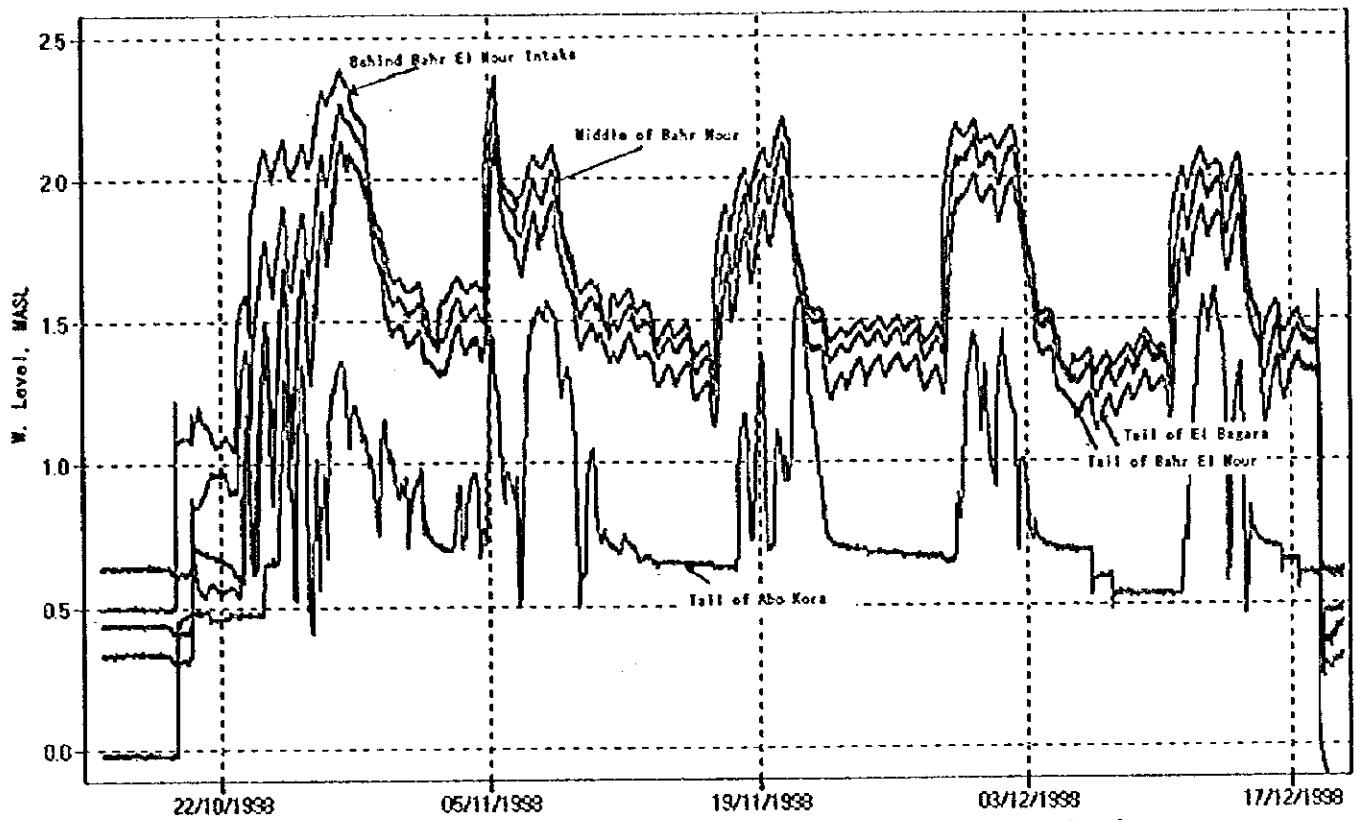


Figure F.19.9 Water Level Records for Bahr El Nour Related Canals

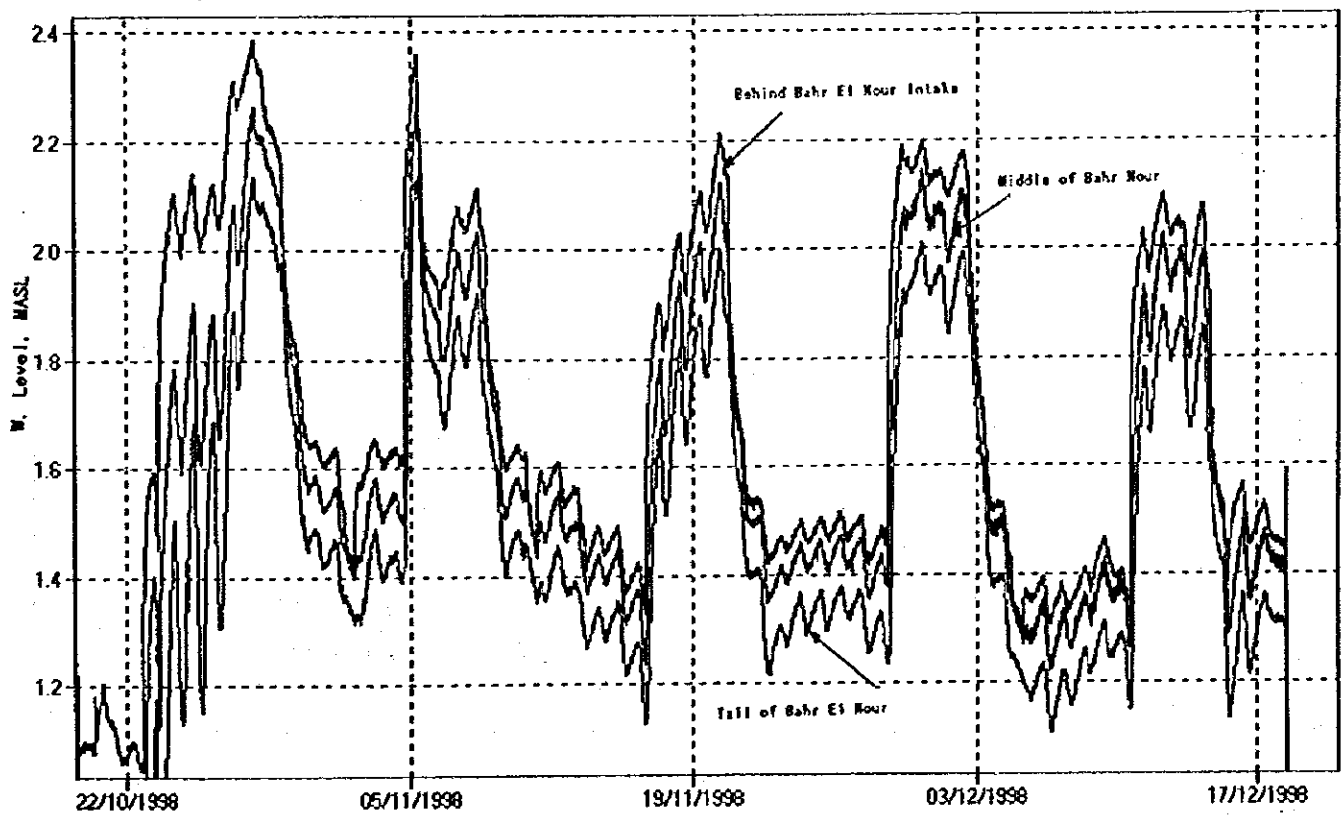


Figure F.19.10 Water Level Records for Bahr El Nour Canal

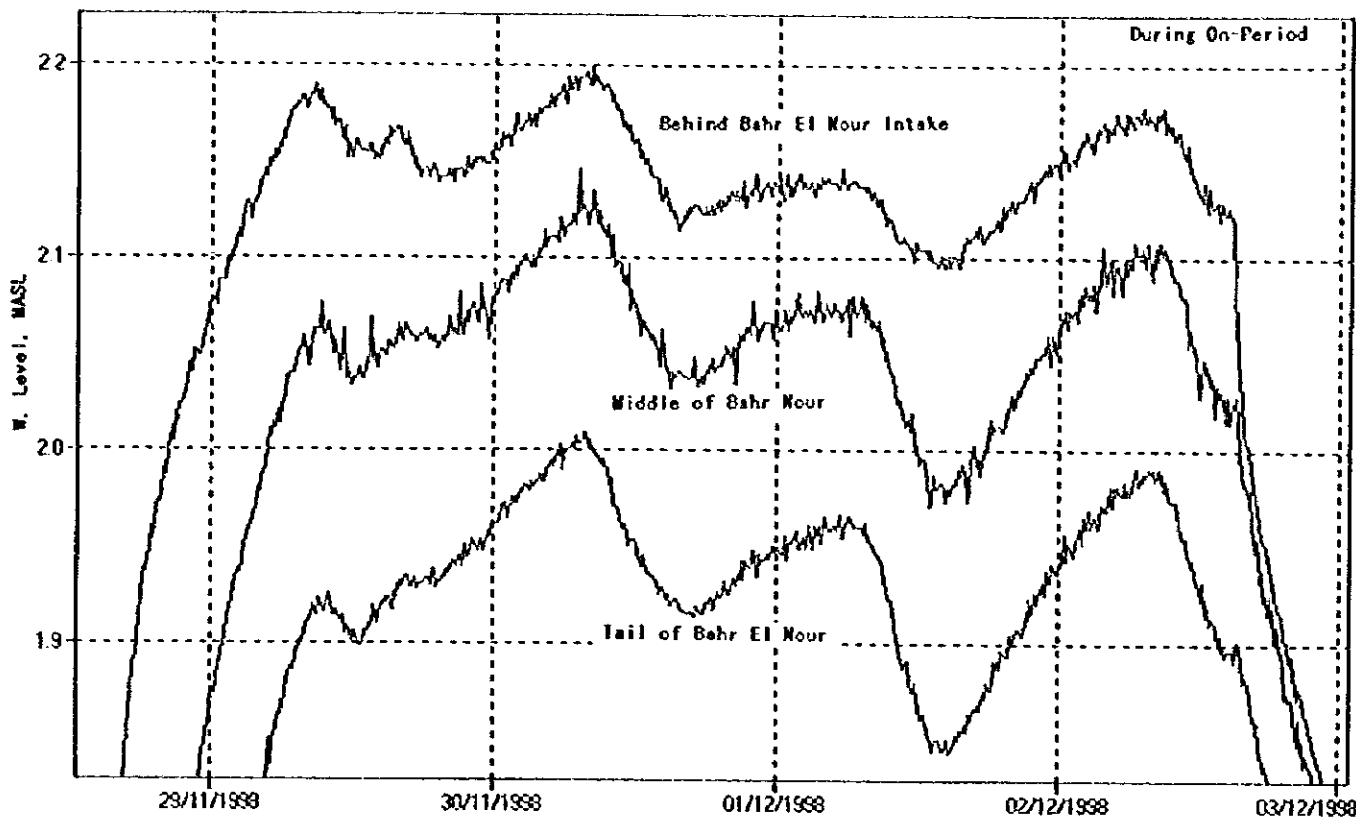


Figure F.19.11 Water Level Records for Bahe El Nour Canal during an On-period Only

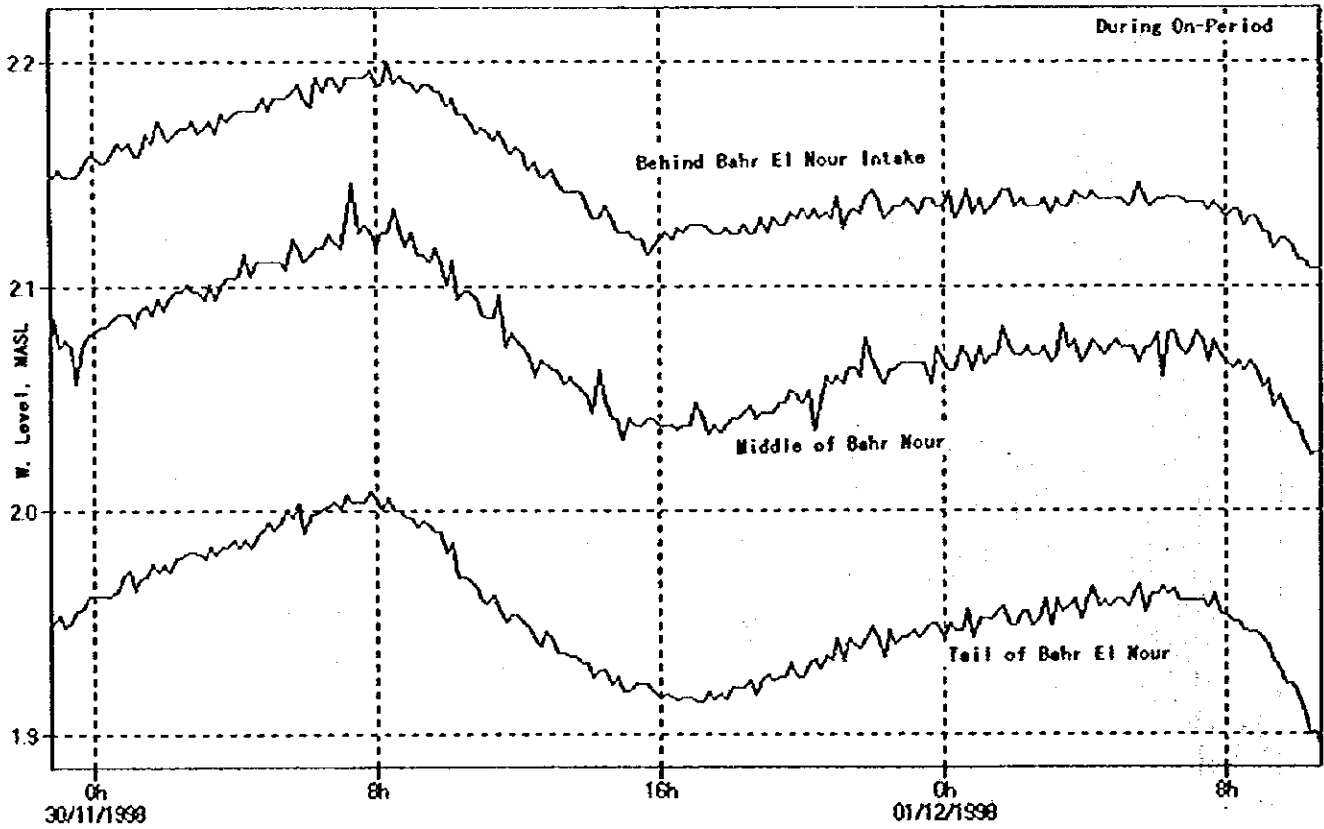


Figure F.19.12 Water Level Records for Bahe El Nour Canal during an On-period Only

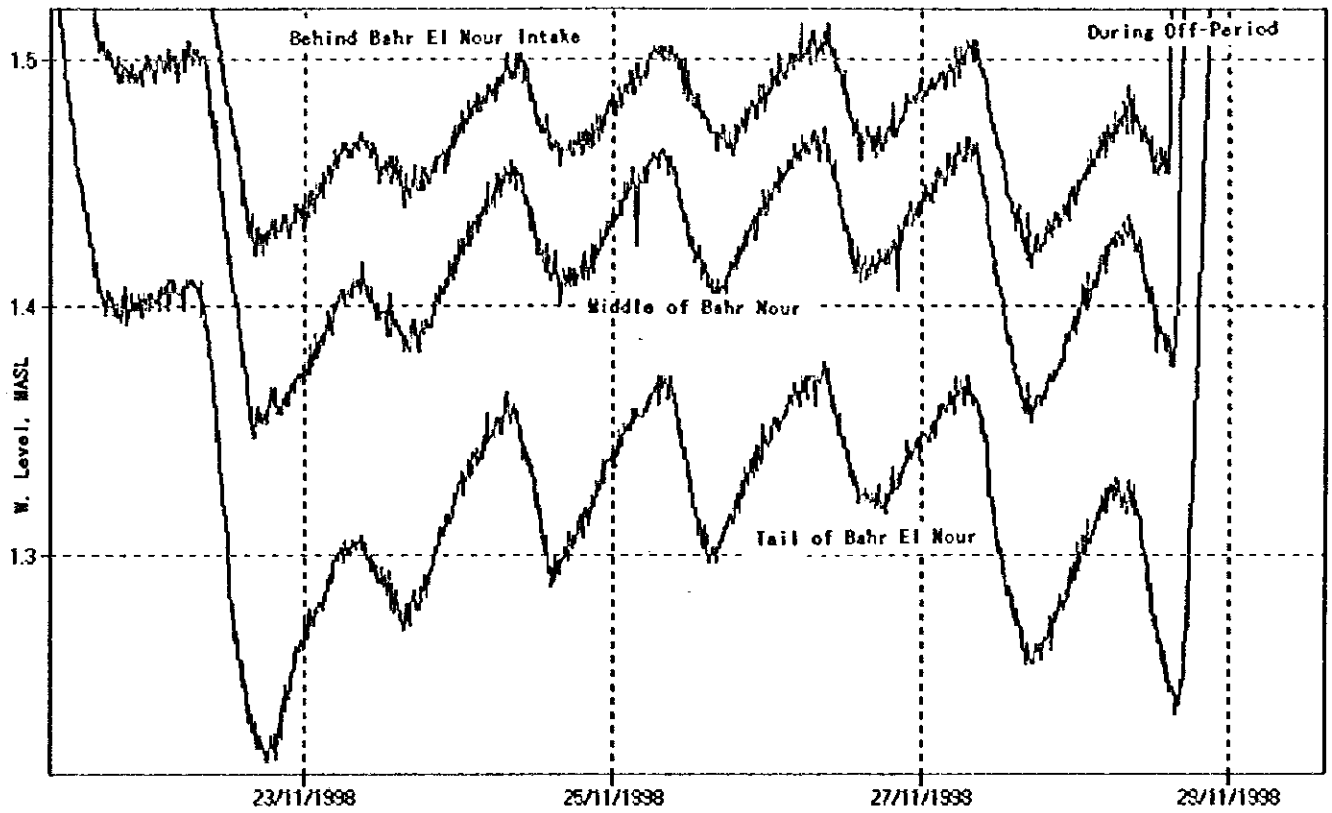


Figure F.19.13 Water Level Records for Bahe El Nour Canal during an Off-period Only



Figure F.19.14 Water Level Records for Bahe El Nour Canal during an Off-period Only

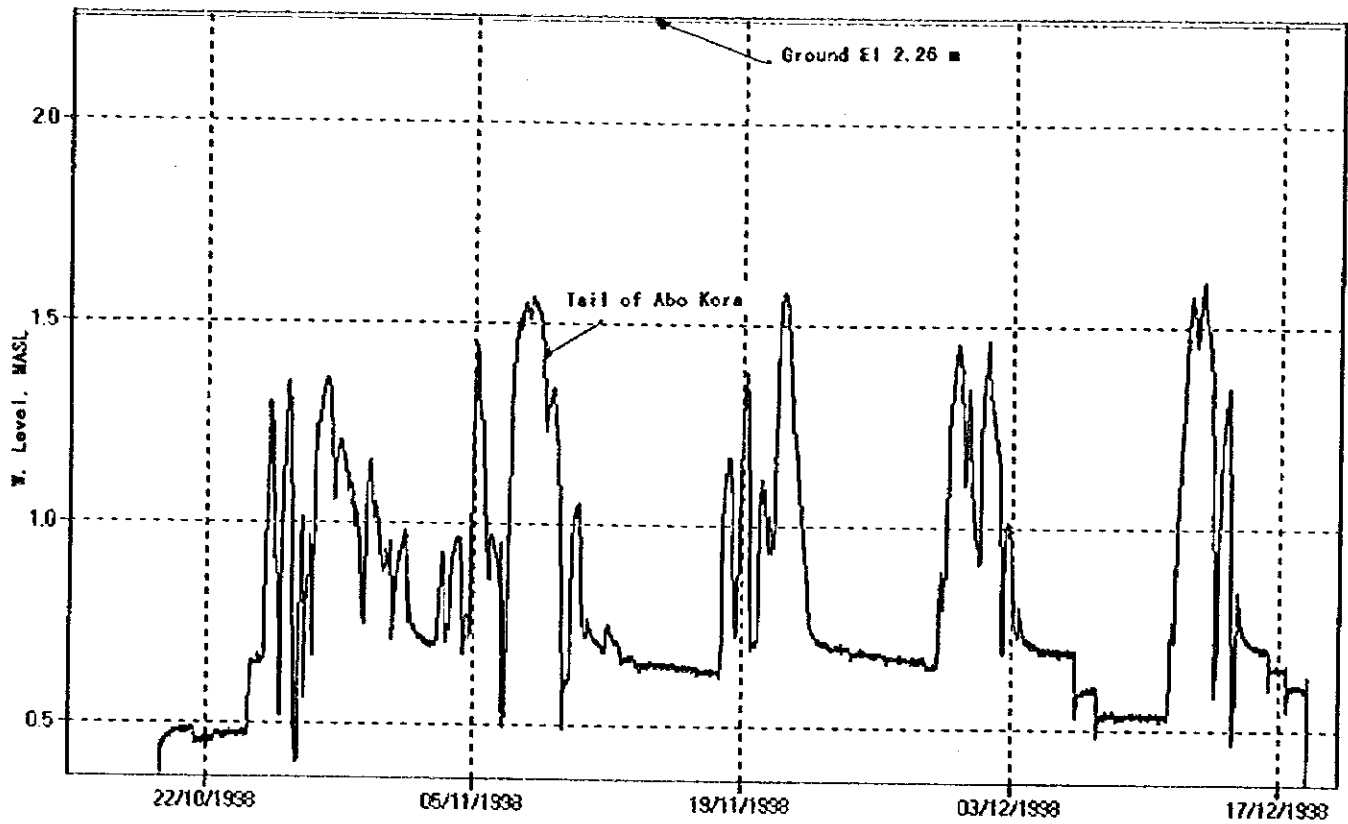


Figure F. 19. 15 Water Level Records at the Tail of Meska Abo Kora

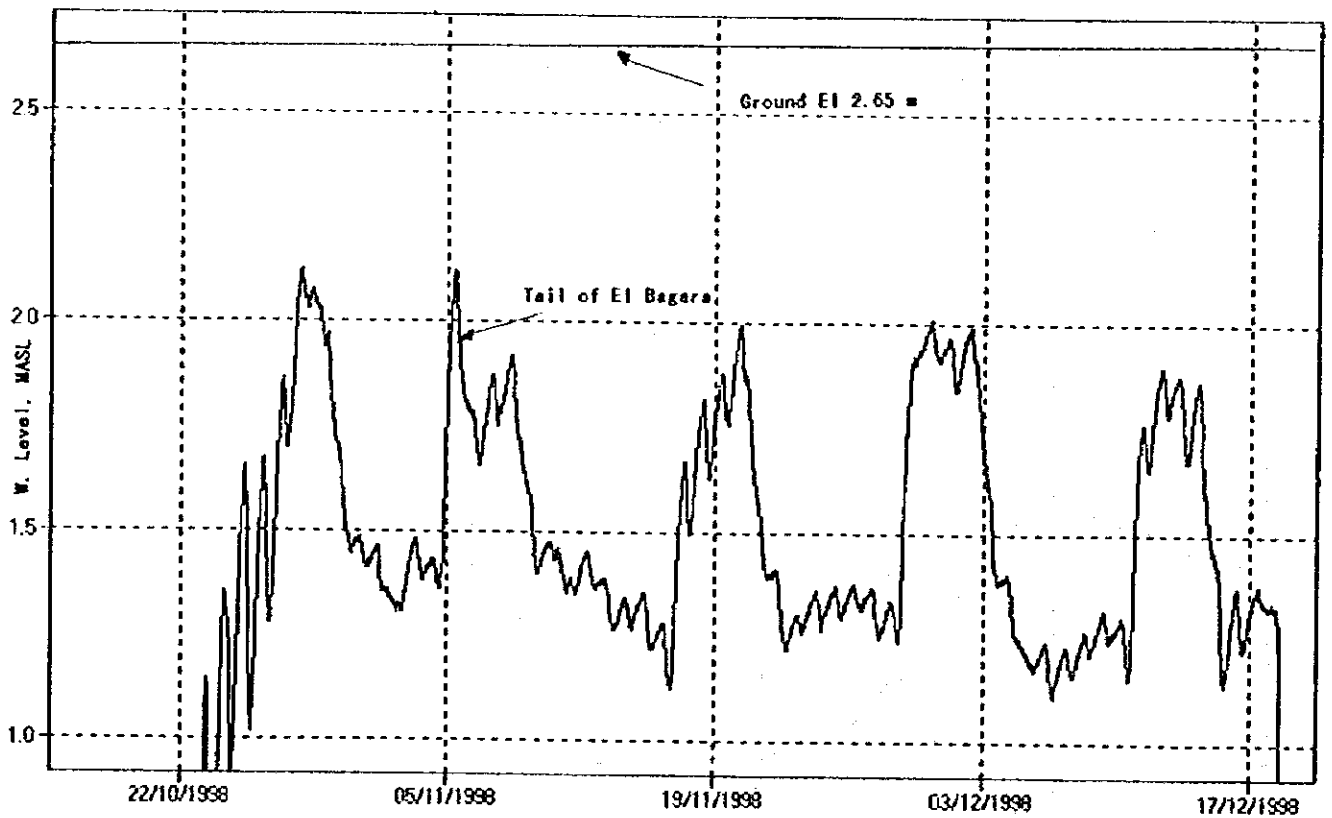


Figure F. 19. 16 Water Level Records at the Tail of Meska El Bagara

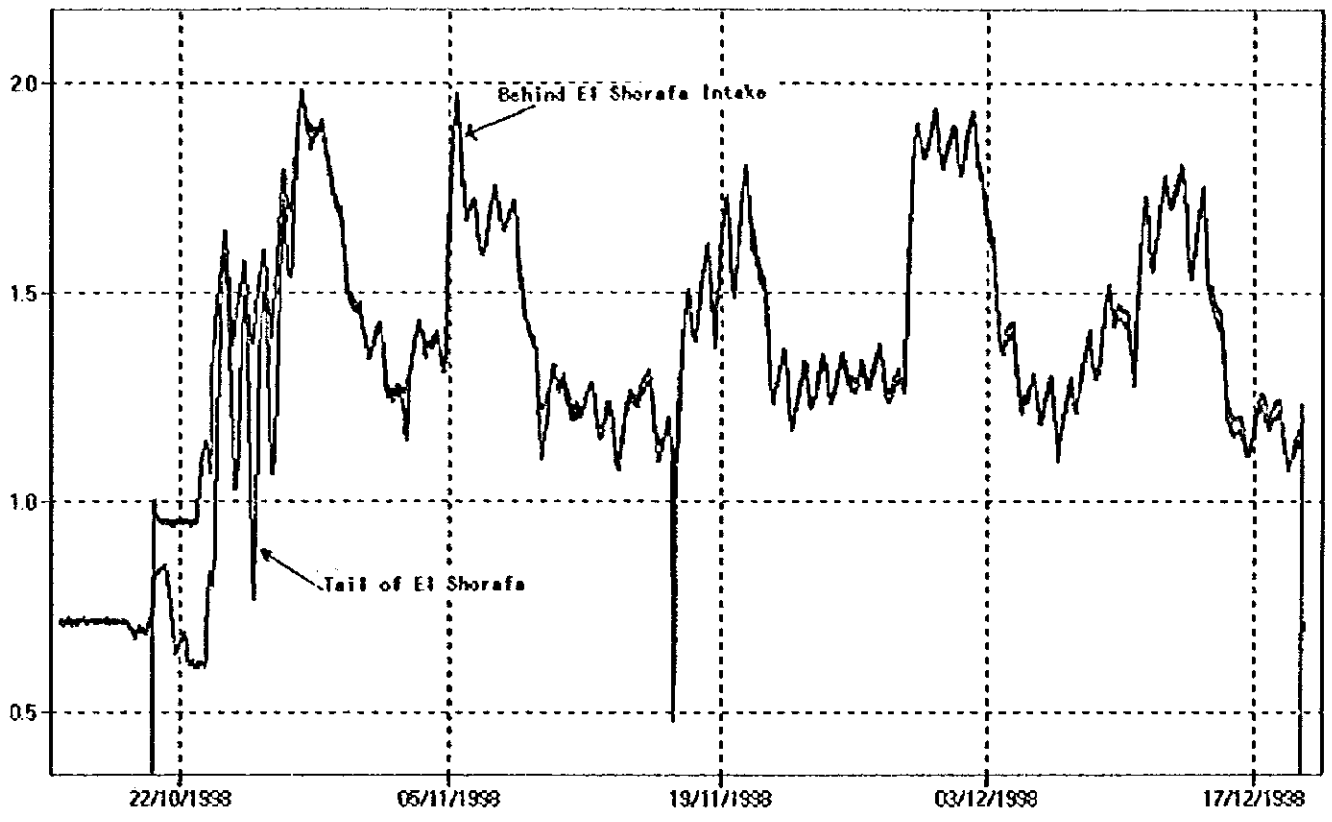


Figure F. 19. 17 Water Level Records for El Shorafa Canal

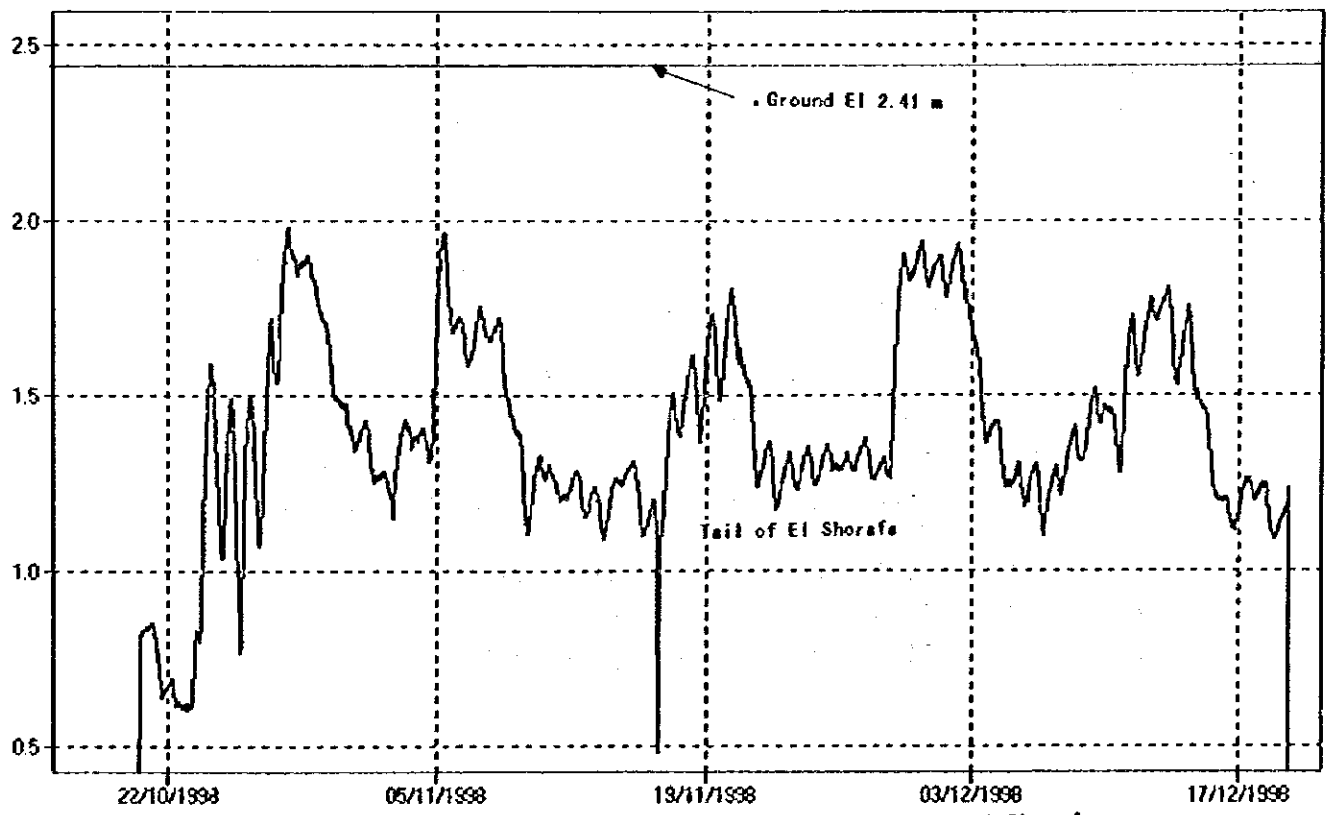


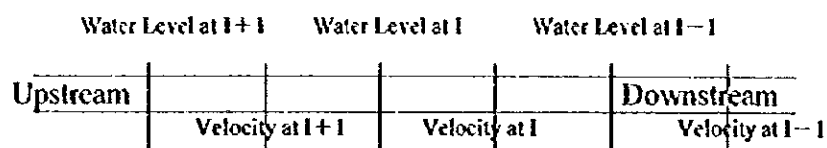
Figure F. 19. 18 Water Level Records at the Tail of El Shorafa

F.20 Unsteady Flow Simulation for Bahr Biyala Command Area

An unsteady flow simulation is carried out for Bahr Biyala command area. The objectives are; 1) to simulate the present conditions under rotational irrigation and to identify the problem incurred, and 2) to simulate the continuous flow to be introduced in future in line with one point lifting pump instead of current individual liftings and to verify the merit or otherwise identify the demerit accompanied if any.

F.20.1 Hydraulic Modeling of the Bahr Biyala Command Area

With reference to the topographic survey that had been carried out during Phase II survey, the Bahr Biyala command area is modeled. The model is composed of 327 meshes, including dummy nodes, each of which has both water level and velocity nodes as shown below;



There are 7 gates presently in the command area that had been undertaken in this simulation, and the dimensions are as below;

No.; From To	Name	Kind	Base El.m	Width	Number
38 → 90	El Agamy	Intake	1.035	2.0	1
37 → 65	Bahr El Nour	-do-	0.785	3.0	1
36 → 35	Bahr Biyala	-do-	1.100	2.0	2
28 → 187	Tahweelah B. Biyala	-do-	1.105	1.2	1
27 → 161	El Shorafa	-do-	-0.065	1.5	1
18 → 46	Hazek	-do-	-0.130	1.5	1
18 → 17	Biyala extension	Regulator	-0.135	1.5	1

With the introduction of the one-point lifting pump, the present Meskas will be buried (big ones will remain even in future), and the modeling is done by excluding the meshes that correspond to the Meskas. The modeling information is shown in the following tables and figures:

- Figure F.20.1 Simulation Model for the Present Condition (Case 1)
- Figure F.20.2 Simulation Model for the Plan (Meska Omitted) (Case 2)
- Figure F.20.3 Simulation Model for the Plan with Automatic Gate (Case 2A)
- Figure F.20.4 Simulation Model for the Plan with Automatic Gate (Case 2B4)
Automatic gate location is different from case 2A.
- Table F.20.1 Mesh Modeling Base Data (Present Condition) (7 sheets)
- Table F.20.2 Meska Dimensions (2 sheets)
- Table F.20.3 Mesh Modeling Base Data (the Plan) (3 sheets)

F.20.2 Simulation Case

Simulation study is carried out for the cases of; 1) present condition, 2) planned condition without automatic check gate (downstream water level constant gate), and 3) planned condition with the automatic check gate. The simulation period is to be 10 days in June that requires the maximum irrigation water. Also, minimum requirement is checked with the irrigation water of 1.02 cu.m/s at October. The water requirement and the case are as below;

Present; 8.69 cu.m/s (Max. only) (See Table F.18.3)

Planned; 6.16 cu.m/s (Max.)

1.02 cu.m/s (Min.) (See Table F.18.3)

Case	Irrigation	Meska	Check Gate	Q, cu.m/s	C'dition	Sim. Period
Case1	Rotation	As the present	No	8.69	present	10 days in July
Case2	Continuous	Abolished'	No	6.16	Planned	10 days in July
Case2'	Continuous	-do-	No	1.02	Planned	10 days in October
Case2A&2B	Continuous	-do-	Yes	6.16	planned	10 days in July

Note; * Large Meskas are to remain.

(1) Flow Input to the Model

There is a small mixing pumping station at the tail of Bahr Biyala. The pump lifts the drainage water from Drain No.4 into Bahr Biyala, and works 10 hours per day during peak period with a discharge of 1.0 cu.m/s (0.417cu.m/s per 24 hours). Therefore, in order to know the discharge from the intake of Bahr Biyala, this 1.0 cu.m/s (0.417 per day) discharge has to be subtracted from the discharges of 8.69 and 6.16 cu.m/s shown in above table;

Present (Case1);

from Bahr Biyala intake $(8.69 - 0.417) \times 2 = 16.546$ cu.m/s (first 5 days only)

from Bahr Biyala tail $1.0 \times 10/24 = 0.417$ cu.m/s (converted into 24 operation for the simplification)

Plan(in July, Case2);

from Bahr Biyala intake $6.16 - 0.417 = 5.743$ cu.m/s (continuous)

from Bahr Biyala tail $1.0 \times 10/24 = 0.417$ cu.m/s (converted into 24 operation for the simplification)

Plan(in October, Case2');

from Bahr Biyala intake 1.02 cu.m/s (continuous)

from Bahr Biyala tail 0.0 (no supply)

(2) Outflow from the Model

Outflow from the model is the pumping from Meskas and canals onto the fields by the farmers, and the pumping is modeled on basis of sine curve as shown below;

Present (Upstream, Case1);

$$\text{First 5 days; } Q = (1.0 + \text{SIN}((T-6) \pi / 12)) \times 1.7 \times 8.69 \times a / A$$

$$\text{Last 5 days; } Q = (1.0 + \text{SIN}((T-6) \pi / 12)) \times 0.5 \times 8.69 \times a / A$$

Present (Downstream, Case1);

$$\text{First 5 days; } Q = (1.0 + \text{SIN}((T-10) \pi / 12)) \times 1.7 \times 8.69 \times a / A$$

$$\text{Last 5 days; } Q = (1.0 + \text{SIN}((T-10) \pi / 12)) \times 0.5 \times 8.69 \times a / A$$

Where;

6 & 10; 4 (10-6) hours difference between up and downstream areas

1.7 / 0.5; adjustment factor

8.69; design outflow, cu.m/s

a; command area by the node concerned, feddan

A; total irrigation area of Bahr Biyala; 14,380 feddan

Whole command area for Bahr Biyala is divided into 2 areas as upstream and downstream, and the peak of the pumping is assumed, with reference to the field condition, to have 4 hours difference between the upstream and downstream. Adjustment factors 1.7 and 0.5 were decided in such way of; 1) With the factor of 1.7, high water levels in the canals within Bahr Biyala are to be almost equal at the last day of the first 5 days, and 2) With the factor of 0.5, canals within Bahr Biyala are to have almost 0 storage.

Plan (Upstream & Downstream, Case2, 2', 2A&2B);

$$\text{In July; } Q = (1.0 + \alpha \times \text{SIN}((T-6) \pi / 12)) \times 6.16 \times a / A$$

$$\text{In Oct; } Q = (1.0 + \alpha \times \text{SIN}((T-6) \pi / 12)) \times 1.02 \times a / A$$

Where;

6; the peak is to show up at noon with this 6

α ; maximum sine factor, 0.5 applied

6.16; design outflow in July, cu.m/s

1.02; design outflow in October, cu.m/s

a; command area by the node concerned, feddan

A; total irrigation area of Bahr Biyala; 14,380 feddan

Pumping pattern is assumed to be same between upstream and downstream areas, therefore only one pumping pattern is employed over the Bahr Biyala command area. Factor α is to be 0.5 in this study, which means maximum pumping shown at noon is 150% of the average and minimum pumping is 50% of the average.

(3) Roughness Coefficient

Roughness coefficient is estimated by using current measurement results done on Bahr Tera. The coefficient on Bahr Tera ranges between 0.024 and 0.028 (refer to Table F.17.4). With reference to the value, this simulation undertakes 0.03 taking into consideration poor maintenance condition than that of Bahr Tera.

(4) Automatic Gate Modeling

An automatic gate, downstream water level constant type, is modeled as; 1) there is a buffer of 0.05 m each at upstream and downstream of the gate, 2) when the downstream water level at the gate goes down 0.05 m, the gate starts opening with a speed of 1 cm/min, and 3) when the downstream water level goes up 0.05 m, the gate starts closing with a speed of 1 cm/min.

F.20.3 Simulation Results

(1) Case1 (Present Condition)

- Under present condition (rotational irrigation), it takes about 6 hours that the water discharged fills canals at upstream area of Bahr Biyala, while takes 24 hours or more to have the canals at downstream area of Bahr Biyala filled (see Figure F.20.5).
- Under present condition, water levels at downstream of Bahr Biyala fluctuates widely since discharge coming from upstream area cannot keep pace with the pumping done by farmers due to the time lag to reach. The low water level shown at the downstream area of Bahr Biyala makes it difficult to supply water into Meskas and canals branching from Bahr Biyala (refer to Figure F.20.5).
- Under present condition, water levels at tails of representative canals and Meskas fluctuate more widely than those shown in Figure F.20.5. Meska Rab El Fashool (No. 137) often dries up since enough water cannot be delivered into the Meska because of the fluctuation in Bahr Biyala canal (see Figure F.20.6).
- Present condition's hydrograph reveals that the water in Bahr El Nour canal starts reverse-flowing after the discharge from Bahr Biyala intake stopped. This is because that the Nour's capacity is relatively large comparing to other canals, therefore the reserved volume is easily withdrawn by Bahr Biyala (refer to Figure F.20.7).
- Present condition's hydrographs reveal that the water at around tail of Meskas and canals is flowing very unstable running forward and backward. Water management under this situation is very difficult, and the farmers would face difficulty to lift enough and stable water from the Meska (refer to Figure F.20.8).
- Present condition's hydraulic profile along Bahr Biyala fluctuates widely, giving difficulty to water management and making difficult to supply enough water to Meska and canals downward. While, Bahr Nour's hydraulic profile does not fluctuate so much because of the large capacity of the canal. After the discharge is stopped, the water level in Bahr Nour goes down quickly, and this can be explained by backward flow from Bahr El Nour into Bahr Biyala (Figures F.20.9 & F.20.10).
- Reservation in canals are at maximum such as; 230,000 cu.m in Bahr Biyala, 130,000 cu.m in Bahr El Nour, 35,000 cu.m in El Agamy, 230,000 cu.m in Meskas and canals other than aforementioned at upstream of Bahr Biyala, 140,000 cu.m in Meskas and canals other than aforementioned at downstream of Bahr Biyala, and as much as 270,000 cu.m will be lost by

burying Meskas accompanied with one-point lifting pump (see Figure F.20.11)

(2) Case2 (Continuous flow of max. 6.16 cu.m/s, Existing gates fully opened, Meska abolished)

- With the continuous flow of maximum of 6.16 cu.m/s, the water level fluctuates with a range of 0.4 m only, and this does not seem to create any noticeable problem. However, when looking into the water level at the tail of Bahr Biyala (No.3), the water level is gradually raising up. This is because that some Meskas from Bahr Biyala cannot in-taken enough water, maybe because of the high bed level elevation, so that excess water goes to the downstream of Bahr Biyala (see Figures F.20.12, F.20.13, F.20.14, F.20.15).
- Though the hydrographs do not give any problem, the hydrograph at the intake of Bahr Nour performs very uniquely, showing reverse sine curve to the others. This shows unstable flow at around the intake of Bahr El Nour, incurred by unevenness of the bed level there (Figure F.20.13).

(3) Case2' (Continuous flow of min. 1.02 cu.m/s, Existing gates fully opened & Operated, Meska abolished)

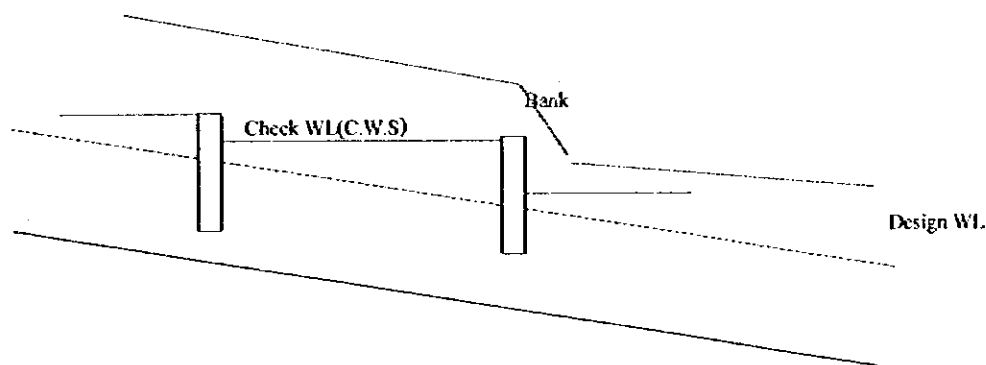
- First, a simulation was made with the continuous flow of 1.02 cu.m/s and existing gates fully opened. This case revealed that the water level at the downstream of Bahr Biyala were raising up as observed in Figure F.20.12 but very sharply. This was caused by the fact that Meskas and canals from Bahr Biyala could not take enough water since the water level in the Bahr Biyala remained low. This suggests that check gates be required.
- Secondary, with trial operations of the existing gates, several simulations were conducted. A simulation with the following gate operation revealed that the water level at the downstream of Bahr Biyala still did not stop raising up. This is because Meskas and canals from Bahr Biyala could not take enough water from Bahr Biyala because of the low water level in the Bahr Biyala. Also, since existing gate behaves as a gate keeping upstream water level constantly, the water level downstream of the gate often goes down quickly, making difficult that the farmers around take enough water (see Figures F.20.16, F.20.17, F.20.18, F.20.19).

No.:	Fr	to	Name	Opening, m
38	→	90	El Agamy	0.100
37	→	65	Bahr El Nour	0.060
36	→	35	Bahr Biyal	0.150
28	→	129	Tahweelah Bahr Biyala	Full open
27	→	119	El Shorafa	Full open
18	→	46	Hazek	0.060
18	→	17	Extension of Bhar Biyala	0.060

- Above results suggests that a automatic gate be required in order to raise water level in the Bahr Biyala during low water period of winter, so that Meskas and canals branching from Bahr Biyala can easily take enough water, and also to give enough water to downstream. This can be done with an automatic downstream water level control gate like Avio-Avis Gate.

(4) Case2A&2B (Continuous flow of max. 6.16 cu.m/s, With automatic checkgates, Meska abolished)

- Location of check gate is decided in considering; 1) the canal bank elevation and the profile, 2) flow variation, 3) boundary of maintenance, and so on.



- Two check gates are planned on Bahr Biyala and the locations are to be in between; mesh No.17 & No.18 and mesh No.28 & No.29, check WLs of which are El. 1.5 m and El. 1.9 m respectively (See Figures F.20.20, F.20.21).
- Check gate on Bahr El Nour could be installed either in between mesh No.55 and No.56 or the upstream of Bahr El Nour (in between mesh No.71 and No.56). The check WL is to be 2.0m. The former case is named Case2A and the latter Case2B (Figure F.20.22 and F.20.23).
- With the introduction of the gate keeping downstream water level constantly, the effect of pumping (outflow from the model) move to upstream area of the Bahr Biyala irrigation system. The water levels in the upstream of Bahr Biyala fluctuate within a range; 1.85 to 2.45 m at mesh No.29 to No.39, No.56 to No.65, and No.73 to No.78 for Case2A, and 1.85 to 2.60 m at mesh No.29 and No.39 for Case2B. The difference between the cases of Case 2A and 2B is not big with a mere 0.15 m only. Therefore, both cases are acceptable in terms of the simulation results but Case2A (check gate on Bahr El Nour is in the middle and not at the upstream) is preferred since the upstream is to have sluice gate (existing one) in order to measure the flow by using gate formula (see Figures F.20.24 to F.20.31).
- The hydrographs fluctuate periodically, and the flow at the intake of Bahr El Nour often goes backward. This would make difficult to measure the inflow volume into Bahr El Nour (Figure F.20.25 and F.20.29).
- The water level profile along Bahr Biyala does not give any problem, having enough water levels thanks to the downstream water level constant gate. The water level along Bahr El Nour does not give any problem either (see Figures F.20.26, F.20.27, F.20.30 and F.20.31).

Figure F.20.3 Simulation Model for the Plan (Meskas Omitted) with Automatic Check Gate (Case 2A)

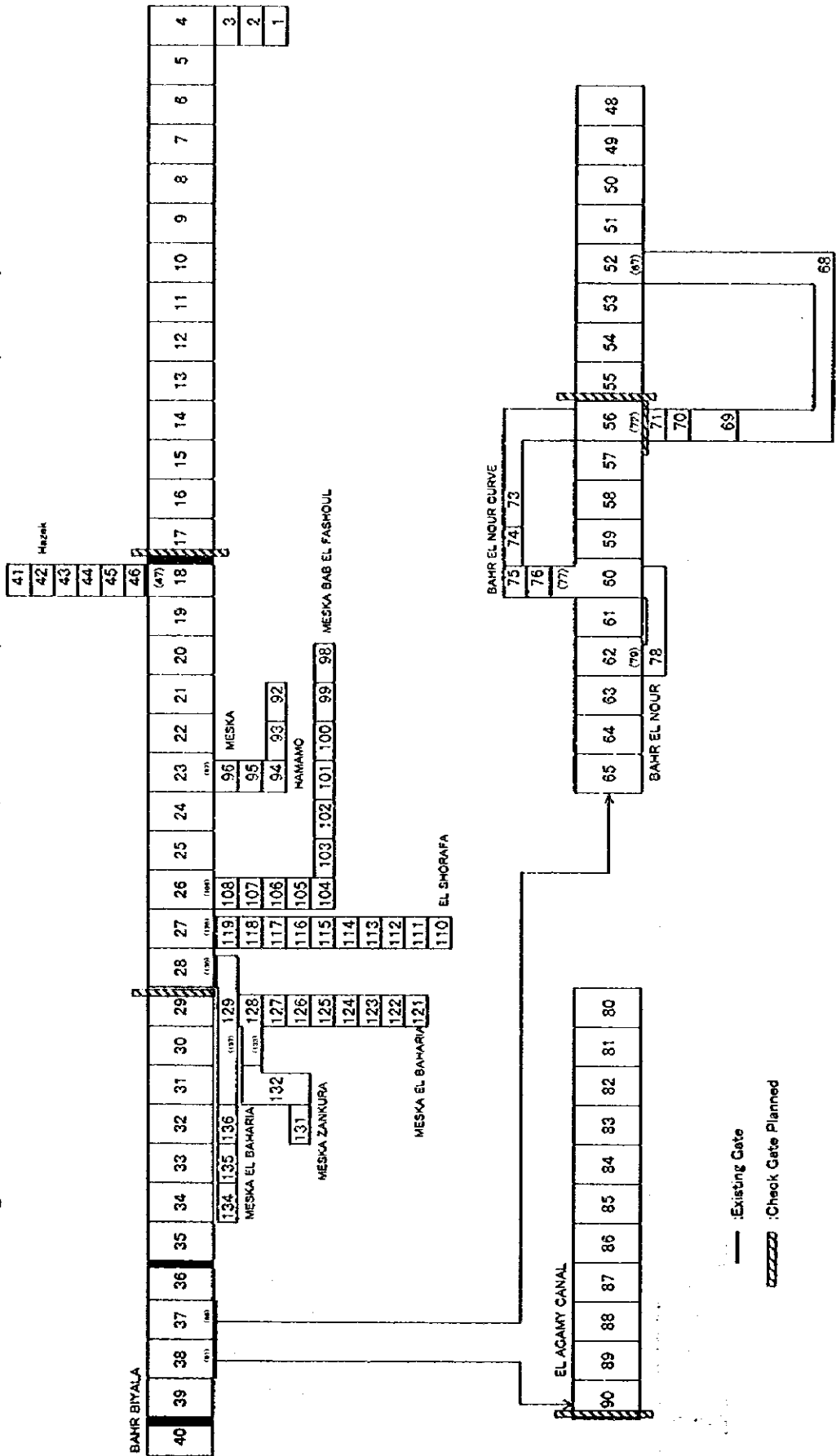


Figure F.20.4 Simulation Model for the Plan (Meskas Omitted) with Automatic Check Gate (Case 2B)

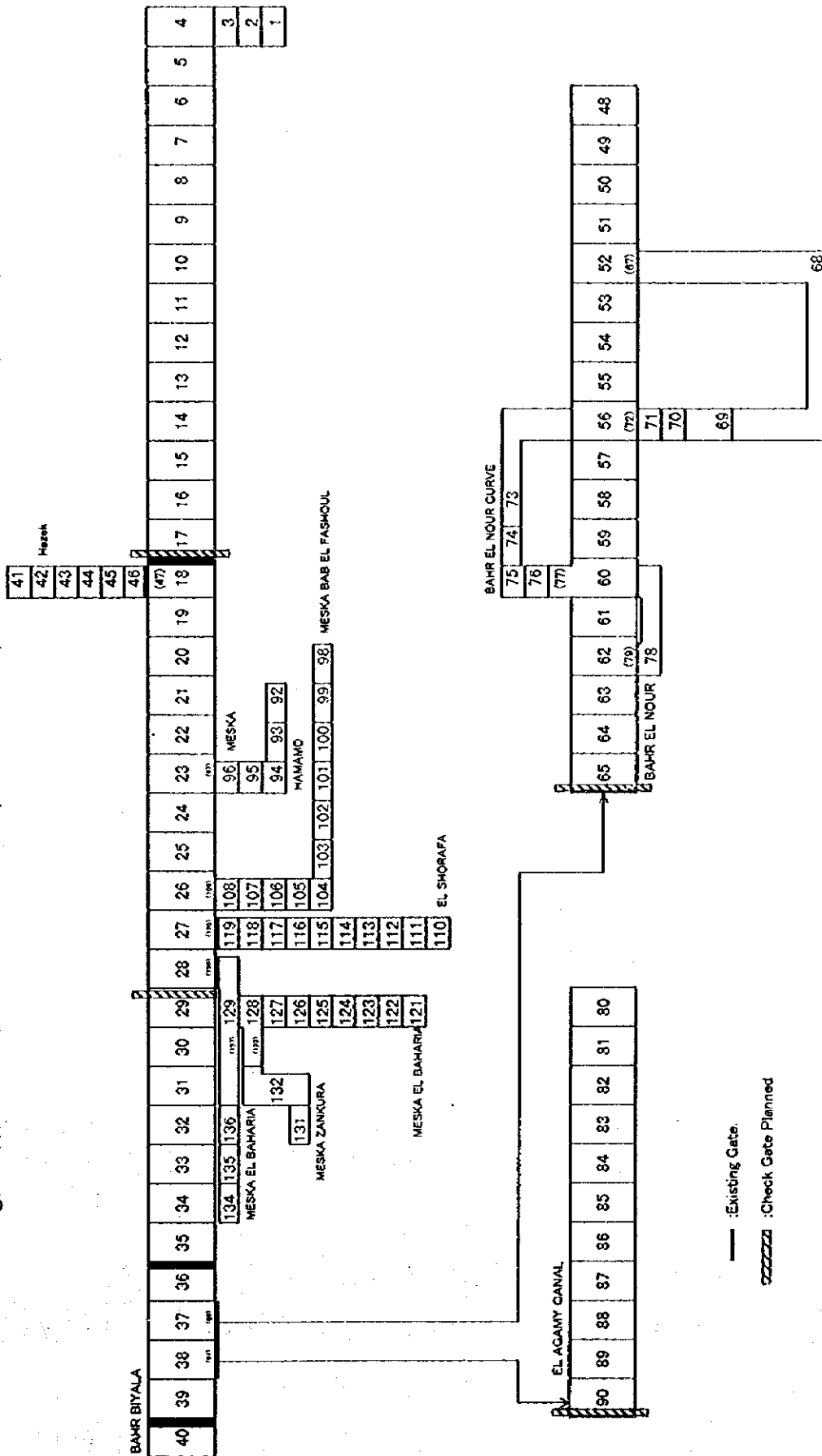


Table F. 20.1 Mesh Modeling Base Data (Present Condition for Bahr Biyala)

No	Canal	Section	Topo Map		Remarks	Canal Section Distance											Elevation					Sec. Type	Z0 EL m	AR1 m	AR2 m	AR3 m	SH EL m	AR4	AR5	RNS1	RNS2	SA ha
			Lng.	Sec.		X1	X2	X3	X4	X5	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8	Y9	Y10	Y11											
51	BAHR EL HOUR	No. 117	29	168		-5.00	-2.71	0.00	2.71	5.00	3.02	1.11	0.45	1.26	2.79	1	0.45	0.00	0.00	0.74	2.79	3.73	1.35	0.03	0.03	0.03	18.06					
52	BAHR EL HOUR	No. 109	29	167		-6.80	-4.01	0.00	4.01	6.80	2.86	1.00	0.59	1.00	2.99	1	0.59	0.00	0.00	0.41	2.86	9.76	1.45	0.03	0.03	0.03	12.06					
53	BAHR EL HOUR	No. 101	29	167		-7.20	-4.11	0.00	4.11	7.20	3.27	1.21	0.69	1.15	3.20	1	0.69	0.00	0.00	0.49	3.20	8.42	1.50	0.03	0.03	0.03	21.16					
54	BAHR EL HOUR	No. 93	29	166		-7.20	-4.04	0.00	4.04	7.20	3.26	1.15	0.59	1.11	3.54	1	0.59	0.00	0.00	0.54	3.26	7.49	1.40	0.03	0.03	0.03	21.16					
55	BAHR EL HOUR	No. 85	29	165		-5.65	-1.96	0.00	1.96	5.65	3.35	0.89	0.64	0.97	3.18	1	0.64	0.00	0.00	0.29	3.18	6.89	1.58	0.03	0.03	0.03	21.16					
56	BAHR EL HOUR	No. 77	28	164		-8.40	-5.07	0.00	5.07	8.40	3.13	0.91	0.54	0.99	3.16	1	0.54	0.00	0.00	0.41	3.13	12.48	1.52	0.03	0.03	0.03	21.16					
57	BAHR EL HOUR	No. 69	28	163		-7.30	-4.06	0.00	4.06	7.30	3.31	1.15	0.87	1.15	3.24	1	0.87	0.00	0.00	0.28	3.24	14.50	1.53	0.03	0.03	0.03	44.10					
58	BAHR EL HOUR	No. 61	28	163		-7.30	-4.71	0.00	4.71	7.30	3.13	1.00	0.75	0.95	2.90	1	0.75	0.00	0.00	0.23	2.90	21.20	1.54	0.03	0.03	0.03	44.10					
59	BAHR EL HOUR	No. 53	28	162		-7.65	-3.51	0.00	3.51	7.65	3.71	1.00	0.73	1.10	3.32	1	0.73	0.00	0.00	0.50	3.32	11.24	1.70	0.03	0.03	0.03	44.10					
60	BAHR EL HOUR	No. 45	28	161		-6.55	-2.82	0.00	2.82	6.55	3.53	1.04	0.52	1.00	3.63	1	0.52	0.00	0.00	0.50	3.53	5.65	1.46	0.03	0.03	0.03	33.60					
61	BAHR EL HOUR	No. 37	27	160		-7.50	-4.43	0.00	4.43	7.50	3.42	1.37	0.87	1.32	3.51	1	0.87	0.00	0.00	0.48	3.42	9.35	1.45	0.03	0.03	0.03	44.10					
62	BAHR EL HOUR	No. 29	27	159		-7.50	-3.74	0.00	3.74	7.50	3.70	1.19	0.68	1.14	3.47	1	0.68	0.00	0.00	0.49	3.47	7.73	1.56	0.03	0.03	0.03	44.10					
63	BAHR EL HOUR	No. 21	27	159		-6.65	-3.13	0.00	3.13	6.65	3.56	1.21	0.72	1.32	4.02	1	0.72	0.00	0.00	0.55	3.56	5.80	1.40	0.03	0.03	0.03	44.10					
64	BAHR EL HOUR	No. 13	27	158		-8.50	-4.53	0.00	4.53	8.50	3.76	1.11	0.42	1.15	3.55	1	0.42	0.00	0.00	0.71	3.55	6.39	1.58	0.03	0.03	0.03	44.10					
65	BAHR EL HOUR	No. 5	27	157		-8.10	-3.89	0.00	3.89	8.10	4.00	1.19	0.39	1.32	3.95	1	0.39	0.00	0.00	0.87	3.95	4.52	1.55	0.03	0.03	0.03	44.10					
66	BAHR EL HOUR				37 Dummy														0.00	3.73	0.00	1.63	0.03	0.03	0.03	0.00						
67	BAHR EL HOUR 3 CURVE				52 Dummy														0.00	0.41	2.85	9.78	1.45	0.03	0.03	0.00						
68	BAHR EL HOUR 3 CURVE	No. 31	26	156		-4.30	-1.11	0.00	1.11	4.30	3.09	0.96	0.76	1.06	2.90	1	0.76	0.00	0.00	0.25	2.90	4.63	1.62	0.03	0.03	21.16						
69	BAHR EL HOUR 3 CURVE	No. 23	26	155		-4.85	-1.69	0.00	1.69	4.85	3.71	0.93	0.71	0.91	2.79	1	0.71	0.00	0.00	0.24	2.79	7.24	1.59	0.03	0.03	21.16						
70	BAHR EL HOUR 3 CURVE	No. 15	26	154		-4.40	-1.70	0.00	1.70	4.40	2.96	1.16	0.86	1.23	3.09	1	0.86	0.00	0.00	0.33	2.96	5.26	1.47	0.03	0.03	21.16						
71	BAHR EL HOUR 3 CURVE	No. 7	26	153		-4.30	-0.97	0.00	0.97	4.30	3.33	1.11	0.76	1.06	3.03	1	0.76	0.00	0.00	0.33	3.03	3.00	1.60	0.03	0.03	21.16						
72	BAHR EL HOUR 2 CURVE				56 Dummy														0.00	0.41	3.13	12.48	1.52	0.03	0.03	0.00						
73	BAHR EL HOUR 2 CURVE	No. 27	25	152		-4.30	-1.17	0.00	1.17	4.30	3.26	1.17	0.92	1.02	3.31	1	0.92	0.00	0.00	0.18	3.26	8.19	1.43	0.03	0.03	21.74						
74	BAHR EL HOUR 2 CURVE	No. 19	25	151		-5.00	-1.57	0.00	1.57	5.00	3.41	1.12	0.97	1.22	3.19	1	0.97	0.00	0.00	0.20	3.19	8.37	1.62	0.03	0.03	21.74						
75	BAHR EL HOUR 2 CURVE	No. 11	25	151		-3.85	-0.52	0.00	0.52	3.85	3.49	1.27	1.12	1.27	3.42	1	1.12	0.00	0.00	0.15	3.42	3.47	1.52	0.03	0.03	21.74						
76	BAHR EL HOUR 2 CURVE	No. 3	25	150		-4.75	-0.86	0.00	0.86	4.75	3.58	1.32	0.98	1.12	3.42	1	0.98	0.00	0.00	0.24	3.42	4.34	1.49	0.03	0.03	21.74						
77	BAHR EL HOUR 2 CURVE				60 Dummy														0.00	0.50	3.53	5.65	1.46	0.03	0.03	0.00						
78	BAHR EL HOUR 1 CURVE	No. 11	24	148		-2.25	-0.98	0.00	0.98	2.25	3.54	1.42	1.37	1.42	3.53	1	1.37	0.00	0.00	0.05	3.53	19.60	0.60	0.03	0.03	33.60						
79	BAHR EL HOUR 1 CURVE				62 Dummy														0.00	0.49	4.47	7.73	1.56	0.03	0.03	0.00						
80	EL AGAMY	No. 85	13	109		-4.00	-3.03	0.00	3.03	4.00	2.51	1.86	1.49	1.84	2.89	1	1.49	0.00	0.00	0.36	2.51	8.42	1.21	0.03	0.03	27.87						
81	EL AGAMY	No. 77	12	108		-4.00	-2.23	0.00	2.23	4.00	2.89	1.71	1.34	1.76	3.09	1	1.34	0.00	0.00	0.40	2.89	5.07	1.42	0.03	0.03	27.87						
82	EL AGAMY	No. 69	12	107		-5.00	-2.24	0.00	2.24	5.00	3.37	1.53	1.24	1.55	3.19	1	1.24	0.00	0.00	0.31	3.19	7.36	1.60	0.03	0.03	27.87						
83	EL AGAMY	No. 61	12	107		-4.75	-2.94	0.00	2.94	4.75	2.77	1.56	1.16	1.51	2.79	1	1.16	0.00	0.00	0.38	2.77	7.88	1.45	0.03	0.03	27.87						
84	EL AGAMY	No. 53	12	106		-4.50	-2.03	0.00	2.03	4.50	3.18	1.53	0.99	1.56	2.95	1	0.99	0.00	0.00	0.56	2.95	3.66	1.63	0.03	0.03	27.87						
85	EL AGAMY	No. 45	12	105		-4.30	-1.99	0.00	1.99	4.30	3.01	1.47	1.06	1.46	2.95	1	1.06	0.00	0.00	0.41	2.95	4.91	1.53	0.03	0.03	27.87						
86	EL AGAMY	No. 37	11	104		-3.70	-0.78	0.00	0.78	3.70	3.32	1.37	0.92	1.37	3.26	1	0.92	0.00	0.00	0.45	3.26	1.73	1.52	0.03	0.03	27.87						
87	EL AGAMY	No. 29	11	103		-4.00	-1.59	0.00	1.59	4.00	3.01	1.47	0.97	1.47	3.19	1	0.97	0.00	0.00	0.50	3.01	3.38	1.42	0.03	0.03	27.87						
88	EL AGAMY	No. 21	11	103		-4.40	-1.70	0.00	1.70	4.40	3.22	1.42	0.97	1.39	3.29	1	0.97	0.00	0.00	0.44	3.22	3.91	1.40	0.03	0.03	27.87						
89	EL AGAMY	No. 13	11	102		-5.00	-2.29	0.00	2.29	5.00	3.31	1.50	1.20	1.48	3.36	1	1.20	0.00	0.00	0.29	3.31	7.91	1.47	0.03	0.03	27.87						
90	EL AGAMY	No. 5	11	101		-4.45	-1.56	0.00	1.56	4.45	3.65	1.73	1.38	1.73	3.71	1	1.38	0.00	0.00	0.35	3.66	4.46	1.48	0.03	0.03	27.87						
91	EL AGAMY				38 Dummy														0.00	0.00	3.32	0.00	1.31	0.03	0.03	0.00						
92	BAHR BIYALA					-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	1	0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	31.08						
93						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	1	0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	31.08						
94						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	1	0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	31.08						
95						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	1	0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	31.08						
96						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	1	0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	31.08						
97						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	1	0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	31.08						
98					11 Dummy														0.00	0.00	0.13	2.49	13.25	1.45	0.03	0.03	0.00					
99						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	1	0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	31.08						
100						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	1	0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	31.08						

Table F.2D.1 Mesh Modeling Base Data (Present Condition for Bahr Biyala)

No	Canal	Section	Tooo Map		Remarks	Canal Section Distance										Elevation										Sec. Type	Z0 EL.m	AR1 m	AR2 m	AR3 m	SH EL.m	ARA	ARS	RMS1	RMS2	SA ha
			Lng.	Sec.		X1	X2	X3	X4	X5	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8	Y9	Y10	Y11	Y12	Y13	Y14	Y15											
101						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	31.08										
102						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	31.08										
103						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	31.08										
104					11 Dummy																															
105						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	29.40										
106						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	21.00										
107					12 Dummy																															
108						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	33.60										
109						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	42.00										
110						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	50.40										
111					12 Dummy																															
112						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	29.40										
113						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	21.00										
114					13 Dummy																															
115						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	50.40										
116						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	33.60										
117						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	21.00										
118					15 Dummy																															
119						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	12.60										
120						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	16.80										
121						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	12.60										
122					16 Dummy																															
123						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	23.10										
124						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	18.90										
125						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	15.54										
126					18 Dummy																															
127						-0.75	-0.51	0.00	0.51	0.75	2.44	2.20	2.10	2.22	2.54	2.10	0.00	0.00	0.00	0.11	2.44	4.68	0.88	0.03	0.03	17.64										
128						-2.00	-0.97	0.00	0.97	2.00	2.52	0.81	0.60	0.88	2.21	0.60	0.00	0.00	0.00	0.25	2.21	4.04	0.69	0.03	0.03	15.96										
129						-1.75	-0.62	0.00	0.62	1.75	2.74	0.85	0.72	0.93	2.70	0.72	0.00	0.00	0.00	0.17	2.70	3.86	0.62	0.03	0.03	12.60										
130						-2.50	-0.94	0.00	0.94	2.50	3.11	0.88	0.53	0.78	2.98	0.53	0.00	0.00	0.00	0.30	2.98	3.22	0.70	0.03	0.03	25.20										
131						-2.00	-0.96	0.00	0.96	2.00	3.06	0.98	0.73	1.08	3.49	0.73	0.00	0.00	0.00	0.30	3.06	3.29	0.47	0.03	0.03	25.20										
132					23 Dummy																															
133						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	44.10										
134						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61	0.69	0.00	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	37.80										
135					23 Dummy																															
136						-2.90	-1.17	0.00	1.17	2.90	2.39	0.66	0.36	0.51	2.84	0.36	0.00	0.00	0.00	0.23	2.39	5.85	0.87	0.03	0.03	22.15										
137						-2.80	-1.09	0.00	1.09	2.80	2.46	0.75	0.45	0.90	2.45	0.45	0.00	0.00	0.00	0.32	2.45	3.02	1.05	0.03	0.03	22.15										
138						-2.50	-1.00	0.00	1.00	2.50	2.22	0.55	0.38	0.68	2.22	0.38	0.00	0.00	0.00	0.24	2.22	4.61	0.94	0.03	0.03	22.15										
139						-2.45	-1.07	0.00	1.07	2.45	2.33	0.60	0.40	0.58	2.32	0.40	0.00	0.00	0.00	0.18	2.32	6.24	0.79	0.03	0.03	22.15										
140						-1.25	-0.81	0.00	0.81	1.25	2.36	1.92	1.81	1.94	2.65	1.81	0.00	0.00	0.00	0.12	2.36	6.80	0.81	0.03	0.03	22.15										
141						-2.15	-0.89	0.00	0.89	2.15	2.52	0.84	0.72	0.85	2.77	0.72	0.00	0.00	0.00	0.13	2.52	7.13	0.70	0.03	0.03	22.15										
142						-2.00	-0.92	0.00	0.92	2.00	2.42	0.87	0.52	0.82	2.78	0.52	0.00	0.00	0.00	0.33	2.42	2.85	0.62	0.03	0.03	22.15										
143						-2.30	-0.95	0.00	0.95	2.30	2.73	0.66	0.37	0.87	3.04	0.37	0.00	0.00	0.00	0.40	2.73	2.59	0.64	0.03	0.03	22.15										
144						-3.10	-1.35	0.00	1.35	3.10	2.82	1.07	0.52	0.67	3.29	1.07	0.00	0.00	0.00	0.35	2.82	5.73	0.83	0.03	0.03	22.15										
145						-2.80	-1.15	0.00	1.15	2.80	2.68	1.03	0.78	0.88	3.09	0.78	0.00	0.00	0.00	0.18	2.68	8.05	0.87	0.03	0.03	22.15										
146						-2.75	-1.15	0.00	1.15	2.75	2.71	0.83	0.58	0.73	2.71	0.58	0.00	0.00	0.00	0.20	2.71	6.13	0.83	0.03	0.03	22.15										
147					26 Dummy																															
148						-2.00	-0.94	0.00	0.94	2.00	2.71	1.39	1.22	1.39	2.82	1.22	0.00	0.00	0.00	0.17	2.71	5.53	0.77	0.03	0.03	8.40										
149						-2.00	-1.09	0.00	1.09	2.00	2.59	1.45	1.37	1.57	2.88	1.37	0.00	0.00	0.00	0.14	2.59	9.54	0.75	0.03	0.03	21.00										
150						-1.50	-0.76	0.00	0.76	1.50	2.78	0.92	0.72	0.87	2.81	0.72	0.00	0.00	0.00	0.18	2.78	4.43	0.39	0.03	0.03	23.10										

Table F.20.1 Mesh Modeling Base Data (Present Condition for Bahr Blyala)

No	Canal	Section No.	Topo Map		Canal Section Distance								Elevation								Sec. Type	20 EL.m	AKI m	AR2 m	AR3 m	SH EL.m	AR4	ARS	RMS1	RMS2	SA ha
			Log.	Sec.	X1	X2	X3	X4	X5	Y1	Y2	Y3	Y4	Y5	Remarks																
201	RABAA ABU ZEID	No. 16	47	221	-2.35	-0.89	0.00	0.89	2.35	2.74	0.91	0.71	0.86	2.42	1	0.71	0.00	0.00	0.18	2.42	5.19	0.87	0.03	0.03	31.74						
202	RABAA ABU ZEID	No. 8	47	220	-2.25	-0.91	0.00	0.91	2.25	2.97	1.06	1.15	2.93	1	0.96	0.00	0.00	0.15	2.93	6.94	0.73	0.03	0.03	31.74							
203	RABAA ABU ZEID													186 Dummy																	
204	MESKA EL BAHARIA (B)	No. 31	38	197	-2.35	-0.73	0.00	0.73	2.35	2.90	1.55	1.48	2.90	1	1.48	0.00	0.00	0.10	2.90	8.26	1.22	0.03	0.03	31.74							
205	MESKA EL BAHARIA (B)	No. 23	38	196	-3.50	-0.81	0.00	0.81	3.50	3.08	1.22	1.07	3.18	1	1.07	0.00	0.00	0.13	3.08	6.75	1.44	0.03	0.03	31.74							
206	MESKA EL BAHARIA (B)	No. 15	38	195	-4.05	-1.20	0.00	1.20	4.05	2.87	0.97	0.72	3.25	1	0.72	0.00	0.00	0.25	2.87	4.80	1.37	0.03	0.03	31.74							
207	MESKA EL BAHARIA (B)													186 Dummy																	
208					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.85	0.00	0.00	0.17	2.61	5.37	0.88	0.03	0.03	8.40							
209														27 Dummy																	
210					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.85	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	4.20							
211					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.85	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	10.50							
212														29 Dummy																	
213					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.85	0.00	0.00	0.17	2.61	5.37	0.88	0.03	0.03	18.90							
214					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.85	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	27.30							
215														149 Dummy																	
216					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	1.37	0.00	0.00	0.14	2.59	9.54	0.75	0.03	0.03	0.00							
217														31 Dummy																	
218					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.52	0.00	0.00	0.23	3.24	8.78	1.38	0.03	0.03	0.00							
219					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.59	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	8.40							
220														216 Dummy																	
221					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.94	0.00	0.00	0.25	2.53	4.40	0.67	0.03	0.03	0.00							
222					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.59	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	18.06							
223					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.59	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	15.96							
224														31 Dummy																	
225					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.59	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	19.74							
226														32 Dummy																	
227					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	1.03	0.00	0.00	0.36	3.34	18.40	1.36	0.03	0.03	0.00							
228					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.59	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	25.20							
229					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.59	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	23.52							
230					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.59	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	19.32							
231					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.59	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	16.80							
232														33 Dummy																	
233					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.73	7.78	0.00	0.00	0.00	3.33	0.00	1.46	0.03	0.03	0.00						
234					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.59	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	16.80							
235														37 Dummy																	
236	BAHR EL NOUR	No. 28	56	249	-2.50	-0.92	0.00	0.92	2.50	2.52	0.70	0.58	2.79	1	0.58	0.00	0.00	0.12	2.52	7.67	0.81	0.03	0.03	16.31							
237	ROAD 25	No. 20	56	248	-2.85	-1.30	0.00	1.30	2.85	2.04	0.49	0.37	2.24	1	0.37	0.00	0.00	0.13	2.04	10.42	0.95	0.03	0.03	16.31							
238	ROAD 25	No. 12	56	248	-3.00	-1.37	0.00	1.37	3.00	2.47	0.84	0.73	2.60	1	0.73	0.00	0.00	0.10	2.47	14.79	0.96	0.03	0.03	16.31							
239	ROAD 25	No. 4	56	247	-2.70	-1.00	0.00	1.00	2.70	2.45	0.75	0.58	2.90	1	0.58	0.00	0.00	0.15	2.45	6.79	0.89	0.03	0.03	16.31							
240	ROAD 25													48 Dummy																	
241	EL FALAMEIN	No. 36	54	242	-2.70	-1.25	0.00	1.25	2.70	2.31	0.85	0.75	2.80	1	0.75	0.00	0.00	0.08	2.13	18.18	1.05	0.03	0.03	8.40							
242	EL FALAMEIN	No. 28	54	241	-2.25	-0.94	0.00	0.94	2.25	2.21	0.90	0.80	2.23	1	0.80	0.00	0.00	0.13	2.21	7.83	1.01	0.03	0.03	8.40							
243	EL FALAMEIN	No. 20	54	240	-1.75	-0.85	0.00	0.85	1.75	2.27	0.88	0.68	2.43	1	0.68	0.00	0.00	0.13	2.27	10.63	0.59	0.03	0.03	8.40							
244	EL FALAMEIN	No. 12	54	240	-2.25	-0.98	0.00	0.98	2.25	2.63	0.81	0.71	2.54	1	0.61	0.00	0.00	0.15	2.54	7.35	0.70	0.03	0.03	8.40							
245	EL FALAMEIN	No. 4	54	239	-2.00	-0.92	0.00	0.92	2.00	2.74	1.19	1.15	2.82	1	1.15	0.00	0.00	0.04	2.74	20.70	0.58	0.03	0.03	8.40							
246	EL FALAMEIN													54 Dummy																	
247					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	15.96							
248					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	15.96							
249														48 Dummy																	
250					-2.60	-1.05	0.00	1.05	2.60	2.61	0.85	0.85	2.61	1	0.26	0.00	0.00	0.78	2.68	4.31	1.60	0.03	0.03	0.00							

Table F. 20.1 Mesh Modeling Base Data (Present Condition for Bahr Bijala)

No	Canal	Section	Toda Map		Remarks	Canal Section Distance										Sec. Type	Z0 EL. m	AR1 m	AR2 m	AR3 m	SH EL. m	AR4	AR5	RNS1	RNS2	SA ha
			Eng.	Sec.		X1	X2	X3	X4	X5	Y1	Y2	Y3	Y4	Y5											
301						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	16.33
302					295 Dummy												0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	0.00
303						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	16.33
304					296 Dummy												0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	0.00
305						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	16.33
306					297 Dummy												0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	0.00
307	ABO KORA	No. 31	31	175		-3.00	-1.28	0.00	1.28	3.00	2.44	0.73	0.73	0.73	2.19		0.73	2.56	0.00	0.00	2.19	0.00	1.09	0.03	0.03	15.75
308	ABO KORA	No. 23	31	174		-3.00	-0.91	0.00	0.91	3.00	2.68	0.60	0.60	0.60	2.53		0.60	1.82	0.00	0.00	2.53	0.00	1.04	0.03	0.03	15.75
309	ABO KORA	No. 15	31	173		-2.90	-0.91	0.00	0.91	2.90	2.68	0.70	0.70	0.70	2.86		0.70	1.82	0.00	0.00	2.86	0.00	0.95	0.03	0.03	15.75
310	ABO KORA	No. 7	31	172		-2.40	-0.55	0.00	0.55	2.40	3.09	1.20	1.20	1.20	2.79		1.20	1.10	0.00	0.00	2.79	0.00	1.07	0.03	0.03	15.75
311	ABO KORA				57 Dummy												0.87	0.00	0.00	0.28	3.24	14.50	1.53	0.03	0.03	0.00
312						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	2.73
313						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	2.73
314					60 Dummy												0.52	0.00	0.00	0.50	3.53	5.65	1.46	0.03	0.03	0.00
315						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	21.00
316						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	21.00
317					60 Dummy												0.52	0.00	0.00	0.50	3.53	5.65	1.46	0.03	0.03	0.00
318						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	7.00
319						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	7.00
320						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	7.00
321					65 Dummy												0.39	0.00	0.00	0.87	3.95	4.52	1.55	0.03	0.03	0.00
322						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	8.40
323					85 Dummy												1.16	0.00	0.00	0.38	2.77	7.88	1.45	0.03	0.03	0.00
324						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	42.00
325					87 Dummy												0.97	0.00	0.00	0.50	3.01	3.28	1.42	0.03	0.03	0.00
326						-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61		0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03	16.80
327					46 Dummy												0.83	0.00	0.00	0.15	2.95	19.76	1.48	0.03	0.03	0.00

TOTAL AREA 6039.65 ha

Table F. 20. 2 Meska Dimensions

No.	Sec.	Topo. No.		Section Distance					Elevation				
		Lng.	Sec	X1	X2	X3	X4	X5	Y1	Y2	Y3	Y4	Y5
127	No. 36	55	246	-0.75	-0.51	0.00	0.51	0.75	2.44	2.20	2.10	2.22	2.54
128	No. 28	55	245	-2.00	-0.97	0.00	0.97	2.00	2.52	0.81	0.60	0.88	2.21
129	No. 20	55	244	-1.75	-0.62	0.00	0.62	1.75	2.74	0.85	0.72	0.93	2.70
130	No. 12	55	244	-2.50	-0.94	0.00	0.94	2.50	3.11	0.88	0.53	0.78	2.98
131	No. 4	55	243	-2.00	-0.96	0.00	0.96	2.00	3.06	0.98	0.73	1.08	3.49
136	No. 88	59	258	-2.90	-1.17	0.00	1.17	2.90	2.39	0.66	0.36	0.51	2.84
137	No. 80	58	257	-2.80	-1.09	0.00	1.09	2.80	2.46	0.75	0.45	0.90	2.45
138	No. 72	58	257	-2.50	-1.00	0.00	1.00	2.50	2.22	0.55	0.38	0.68	2.22
139	No. 64	58	256	-2.45	-1.07	0.00	1.07	2.45	2.33	0.60	0.40	0.55	2.32
140	No. 56	58	255	-1.25	-0.81	0.00	0.81	1.25	2.36	1.92	1.81	1.94	2.65
141	No. 48	58	254	-2.15	-0.89	0.00	0.89	2.15	2.52	0.84	0.72	0.85	2.77
142	No. 40	57	253	-2.00	-0.92	0.00	0.92	2.00	2.42	0.87	0.52	0.82	2.78
143	No. 32	57	253	-2.30	-0.95	0.00	0.95	2.30	2.73	0.66	0.37	0.87	3.04
144	No. 24	57	252	-3.10	-1.35	0.00	1.35	3.10	2.82	1.07	0.52	0.67	3.29
145	No. 16	57	251	-2.80	-1.15	0.00	1.15	2.80	2.68	1.03	0.78	0.88	3.09
146	No. 8	57	250	-2.75	-1.15	0.00	1.15	2.75	2.71	0.83	0.58	0.73	2.71
148	No. 24	48	225	-2.00	-0.94	0.00	0.94	2.00	2.71	1.39	1.22	1.39	2.82
149	No. 16	48	224	-2.00	-1.09	0.00	1.09	2.00	2.59	1.45	1.37	1.57	2.88
150	No. 8	48	223	-1.50	-0.76	0.00	0.76	1.50	2.78	0.92	0.72	0.87	2.81
152	No. 80	40	205	-3.50	-1.65	0.00	1.65	3.50	2.54	0.62	0.31	0.71	2.61
153	No. 72	40	205	-4.60	-2.35	0.00	2.35	4.60	3.01	0.56	0.31	0.64	2.81
154	No. 64	40	204	-3.50	-2.17	0.00	2.17	3.50	3.23	0.84	0.61	0.77	3.10
155	No. 56	40	203	-5.60	-1.94	0.00	1.94	5.60	3.03	0.40	-0.11	0.25	2.69
156	No. 48	40	202	-4.90	-2.22	0.00	2.22	4.90	2.47	0.76	0.24	0.72	2.51
157	No. 40	39	201	-4.60	-1.84	0.00	1.84	4.60	2.86	0.76	0.37	0.73	2.57
158	No. 32	39	201	-4.75	-1.75	0.00	1.75	4.75	2.46	0.62	0.40	0.64	2.64
159	No. 24	39	200	-3.75	-1.46	0.00	1.46	3.75	3.29	0.68	0.48	0.70	2.89
160	No. 16	39	199	-4.65	-1.82	0.00	1.82	4.65	2.70	0.92	0.82	0.77	2.66
161	No. 8	39	198	-4.50	-2.22	0.00	2.22	4.50	2.81	0.70	0.69	0.81	3.00
170	No. 16	49	227	-1.90	-0.70	0.00	0.70	1.90	2.79	1.08	0.90	0.97	2.45
171	No. 8	49	226	-1.70	-0.77	0.00	0.77	1.70	2.60	1.27	0.77	0.89	2.41
178	No. 61	37	193	-2.15	-0.82	0.00	0.82	2.15	2.72	0.54	0.50	0.52	2.37
179	No. 53	37	192	-2.30	-1.04	0.00	1.04	2.30	2.04	0.59	0.54	0.62	2.33
180	No. 45	37	191	-3.00	-1.28	0.00	1.28	3.00	2.12	0.43	0.40	0.42	2.12
181	No. 37	36	190	-3.00	-1.08	0.00	1.08	3.00	2.27	0.35	0.35	0.35	1.92
182	No. 29	36	189	-2.00	-0.64	0.00	0.64	2.00	2.56	0.54	0.52	0.53	2.42
183	No. 21	36	189	-3.00	-0.66	0.00	0.66	3.00	2.85	0.53	0.51	0.52	2.54
184	No. 13	36	188	-2.45	-0.83	0.00	0.83	2.45	2.80	0.50	0.48	0.49	2.41
185	No. 5	36	187	-2.80	-0.70	0.00	0.70	2.80	3.04	0.96	0.94	0.95	2.55
186	No. 7	38	194	-3.80	-0.97	0.00	0.97	3.80	3.66	0.83	0.64	0.87	3.37
189	No. 8	50	229	-3.60	-2.04	0.00	2.04	3.60	2.63	1.07	0.51	0.84	2.73
191	No. 47	34	182	-1.65	-0.68	0.00	0.68	1.65	2.20	0.58	0.30	0.58	2.23
192	No. 39	34	181	-1.65	-0.62	0.00	0.62	1.65	2.07	0.48	0.43	0.53	2.20
193	No. 31	33	181	-2.05	-0.79	0.00	0.79	2.05	2.31	0.63	0.33	0.63	2.28
194	No. 23	33	180	-2.00	-0.93	0.00	0.93	2.00	2.11	0.68	0.43	0.73	2.38
195	No. 15	33	179	-2.10	-0.98	0.00	0.98	2.10	2.47	0.98	0.53	0.88	2.67
196	No. 7	33	178	-2.15	-1.10	0.00	1.10	2.15	2.53	1.13	0.88	1.13	2.90
203	No. 16	47	221	-2.35	-0.89	0.00	0.89	2.35	2.74	0.91	0.71	0.86	2.42
202	No. 8	47	220	-2.25	-0.91	0.00	0.91	2.25	2.97	1.06	0.96	1.15	2.93
204	No. 31	38	197	-2.35	-0.73	0.00	0.73	2.35	2.90	1.55	1.48	1.60	2.90
205	No. 23	38	196	-3.60	-0.81	0.00	0.81	3.60	3.08	1.22	1.07	1.17	3.18
206	No. 15	38	195	-4.05	-1.20	0.00	1.20	4.05	2.87	0.97	0.72	0.97	3.26
236	No. 28	56	249	-2.50	-0.92	0.00	0.92	2.50	2.52	0.70	0.58	0.70	2.79
237	No. 20	56	248	-2.85	-1.30	0.00	1.30	2.85	2.04	0.49	0.37	0.50	2.24
238	No. 12	56	248	-3.00	-1.37	0.00	1.37	3.00	2.47	0.84	0.73	0.81	2.60
239	No. 4	56	247	-2.70	-1.00	0.00	1.00	2.70	2.45	0.75	0.58	0.71	2.90

Table F. 20. 2 Moska Dimensions

No.	Sec.	Topo. No.		Section Distance					Elevation				
		Lng.	Sec	X1	X2	X3	X4	X5	Y1	Y2	Y3	Y4	Y5
241	No. 36	54	242	-2.70	-1.25	0.00	1.25	2.70	2.31	0.86	0.75	0.80	2.13
242	No. 28	54	241	-2.25	-0.94	0.00	0.94	2.25	2.21	0.99	0.80	0.95	2.23
243	No. 20	54	240	-1.75	-0.85	0.00	0.85	1.75	2.27	0.88	0.68	0.73	2.43
244	No. 12	54	240	-2.25	-0.98	0.00	0.98	2.25	2.63	0.81	0.61	0.71	2.54
245	No. 4	54	239	-2.00	-0.92	0.00	0.92	2.00	2.74	1.19	1.15	1.20	2.82
253	No. 17	35	185	-2.85	-1.02	0.00	1.02	2.85	2.75	0.38	0.08	0.37	2.67
254	No. 9	35	184	-3.50	-1.01	0.00	1.01	3.50	2.68	0.79	0.11	0.77	2.43
256	No. 20	51	232	-2.65	-1.03	0.00	1.03	2.65	2.72	0.40	0.25	0.60	2.28
257	No. 12	51	232	-2.60	-1.13	0.00	1.13	2.60	2.39	0.55	0.25	0.60	2.55
258	No. 4	51	231	-2.50	-1.03	0.00	1.03	2.50	2.56	0.60	0.45	0.75	2.35
260	No. 21	52	236	-1.40	-0.70	0.00	0.70	1.40	2.21	0.80	0.75	0.80	2.13
261	No. 13	52	235	-1.50	-0.59	0.00	0.59	1.50	2.29	0.78	0.75	0.76	2.06
262	No. 5	52	234	-1.50	-0.72	0.00	0.72	1.50	2.63	1.07	1.05	1.08	2.15
264	No. 24	45	218	-0.50	-0.22	0.00	0.22	0.50	2.23	1.84	1.83	1.85	2.43
265	No. 16	45	217	-2.25	-0.82	0.00	0.82	2.25	2.27	0.84	0.74	0.94	2.22
266	No. 8	45	216	-4.00	-1.50	0.00	1.50	4.00	2.56	0.89	0.74	0.89	3.83
268	No. 16	43	211	-2.90	-1.30	0.00	1.30	2.90	2.63	1.03	1.01	1.02	2.44
269	No. 8	43	210	-2.25	-0.80	0.00	0.80	2.25	2.50	1.05	1.03	1.07	2.54
281	No. 27	42	209	-2.75	-1.07	0.00	1.07	2.75	2.33	0.25	0.21	0.22	2.53
282	No. 19	42	208	-2.00	-0.56	0.00	0.56	2.00	2.47	0.54	0.51	0.52	1.95
283	No. 11	42	208	-1.75	-0.64	0.00	0.64	1.75	2.67	0.59	0.56	0.58	2.63
284	No. 3	42	207	-2.00	-0.80	0.00	0.80	2.00	2.81	1.01	0.81	1.01	2.40
286	No. 19	53	238	-1.65	-0.66	0.00	0.66	1.65	2.75	1.03	0.95	1.03	2.53
287	No. 16	53	238	-1.80	-0.78	0.00	0.78	1.80	2.56	1.28	1.20	1.30	2.57
288	No. 8	53	237	-2.30	-0.99	0.00	0.99	2.30	2.60	1.29	1.18	1.26	3.03
290	No. 6	32		-2.00	-0.93	0.00	0.93	2.00	3.06	1.28	1.09	1.19	2.92
307	No. 31	31	175	-3.00	-1.28	0.00	1.28	3.00	2.44	0.73	0.73	0.73	2.19
308	No. 23	31	174	-3.00	-0.91	0.00	0.91	3.00	2.68	0.60	0.60	0.60	2.53
309	No. 15	31	173	-2.90	-0.91	0.00	0.91	2.90	2.68	0.70	0.70	0.70	2.86
310	No. 7	31	172	-2.40	-0.55	0.00	0.55	2.40	3.09	1.20	1.20	1.20	2.79
Ave				-2.60	-1.05	0.00	1.05	2.60	2.61	0.86	0.69	0.85	2.61