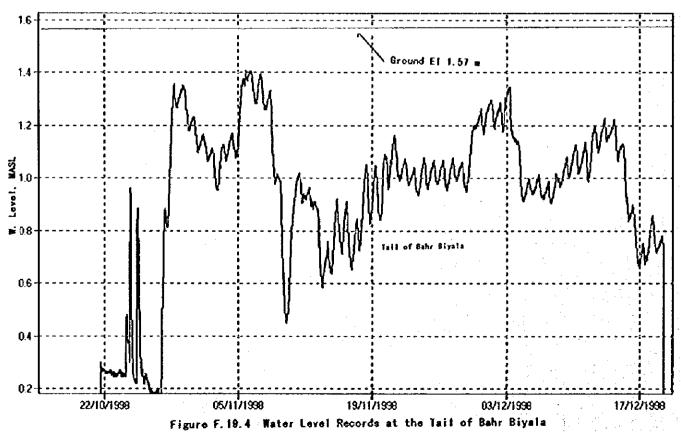


Figure F. 19.3 Water Level Records for Bahr Biyala Related Canals



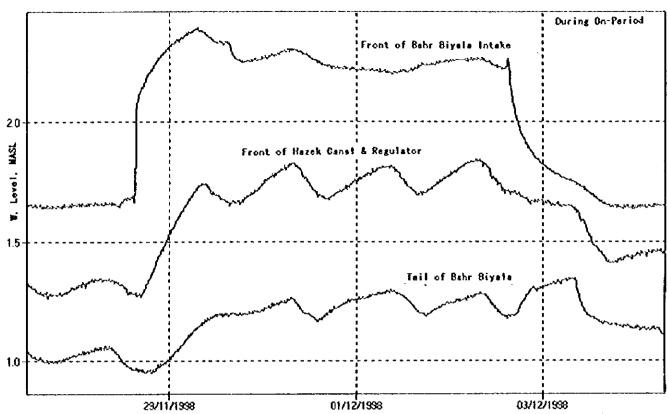


Figure F. 19.5 Water Level Records for Bahr Biyal Canal during an On-period Only

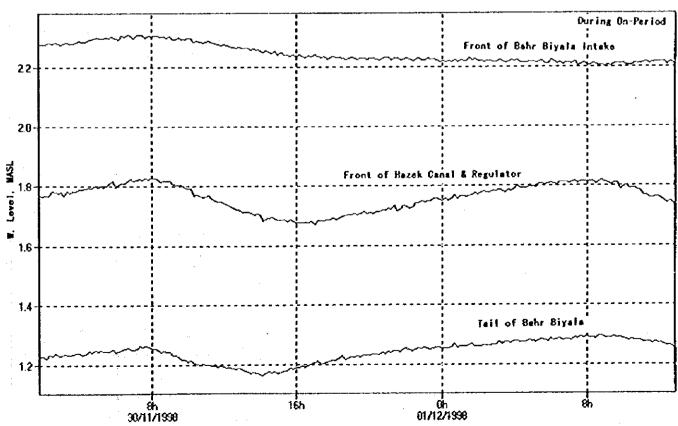
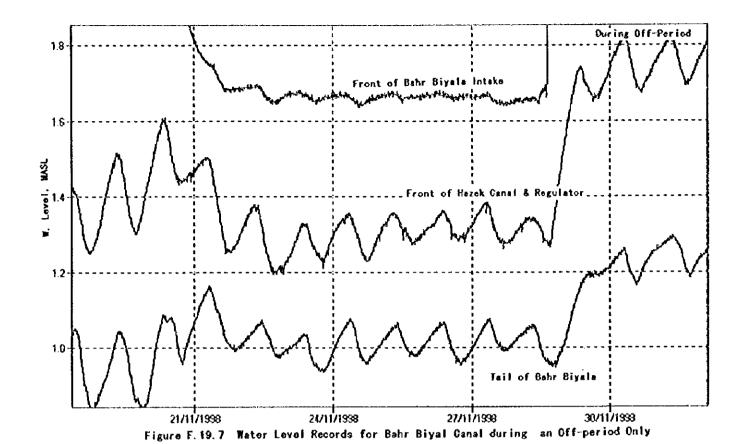
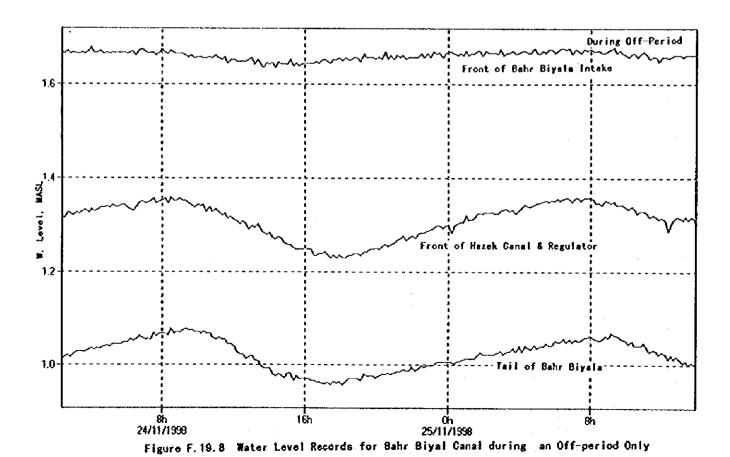
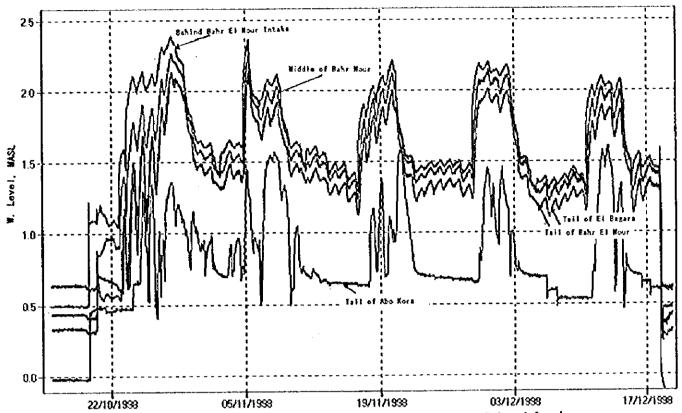
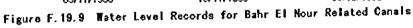


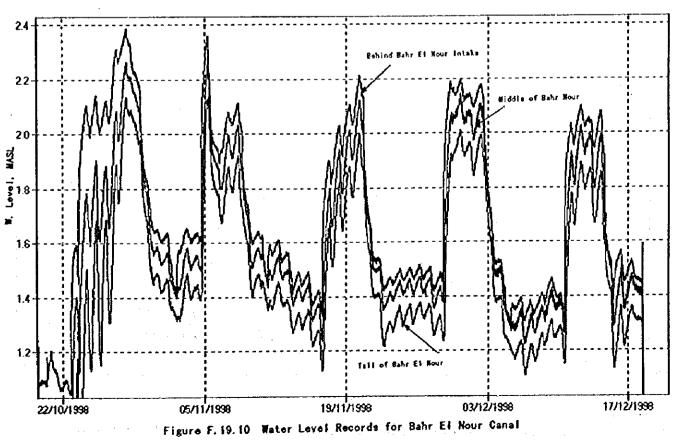
Figure F. 19.8 Water Level Records for Bahr Biyal Canal during an On-period Only











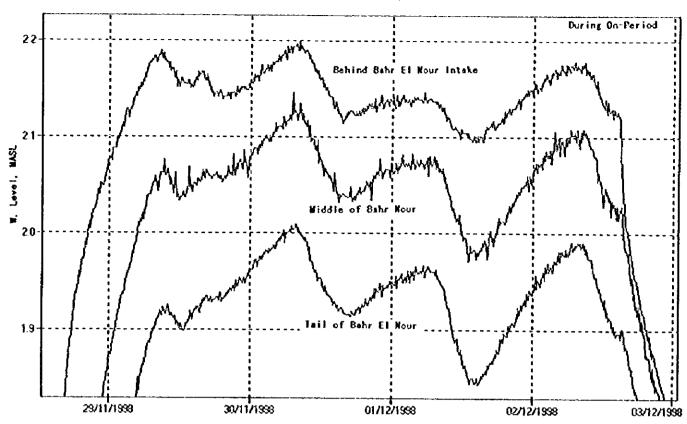


Figure F. 19.11 Water Level Records for Bahe El Nour Canal during an On-period Only

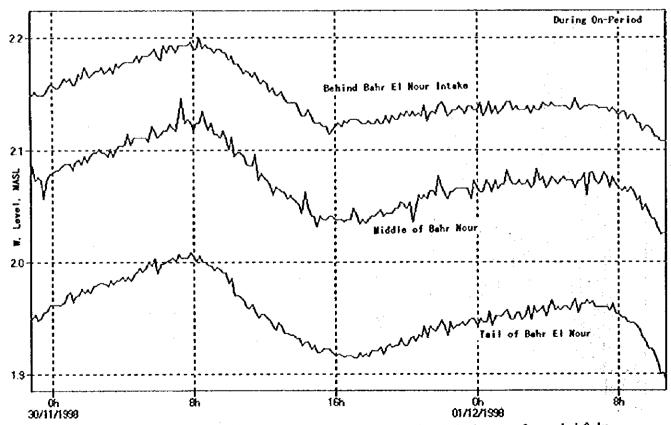
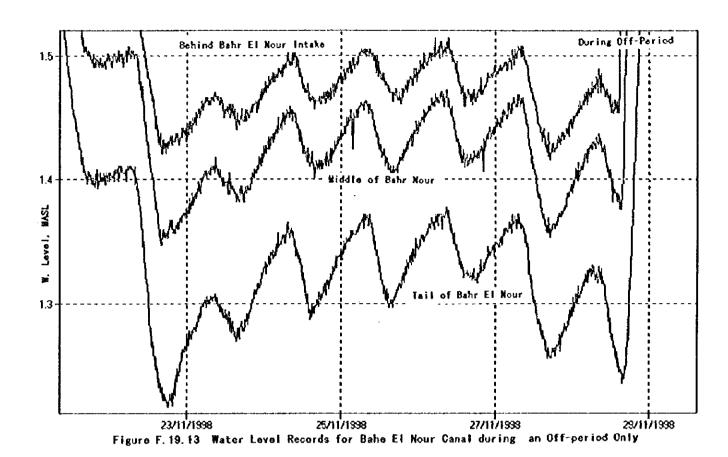


Figure F. 19.12 Water Level Records for Sahe El Nour Canal during an On-period Only



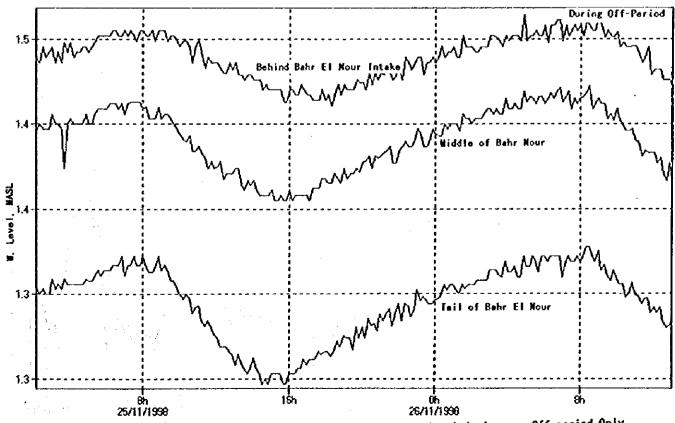


Figure F. 19. 14 Water Level Records for Bahe El Nour Canal during an Off-period Only

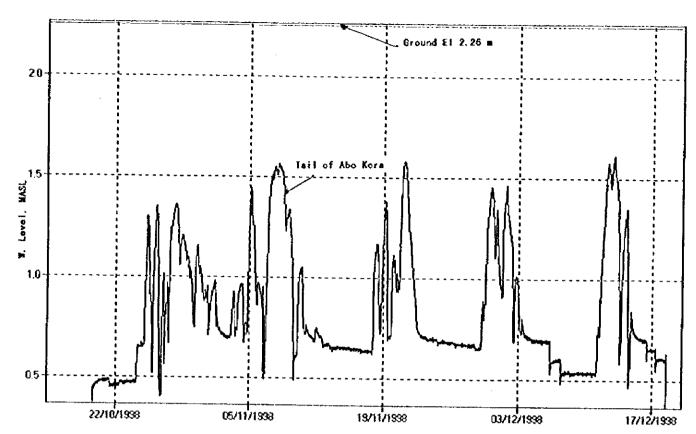


Figure F. 19. 15 Water Level Records at the Tail of Meska Abo Kora

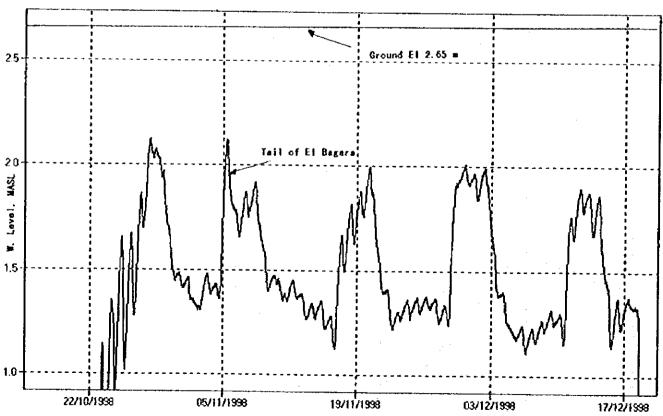


Figure F. 19. 16 Water Level Records at the Tail of Meska El Bagara

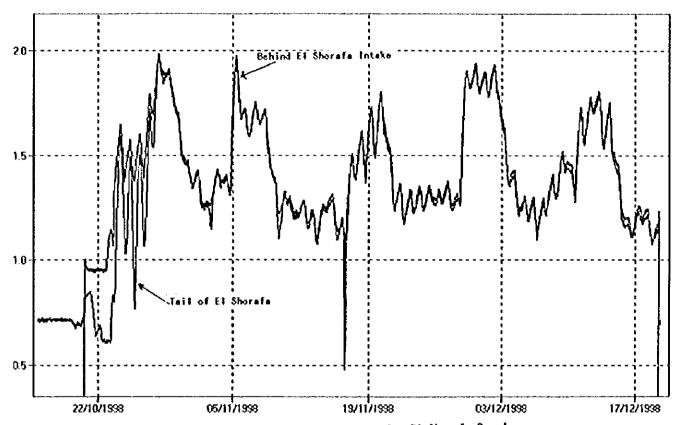
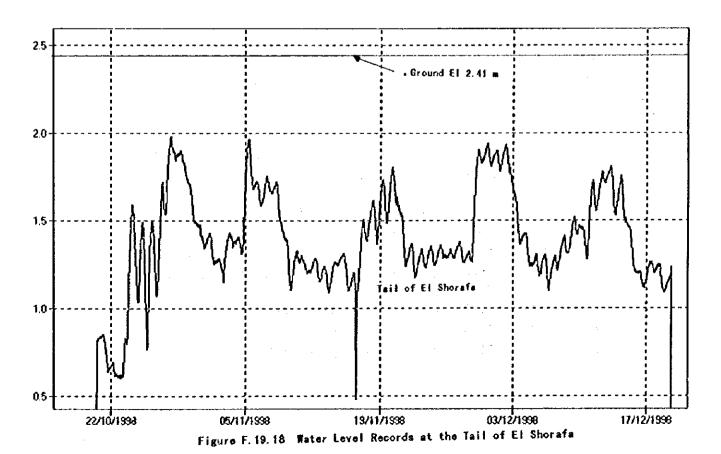


Figure F. 19. 17 Water Level Records for El Shorafa Canal

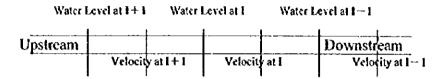


F.20 Unsteady Flow Simulation for Bahr Biyala Command Area

An unsteady flow simulation is carried out for Bahr Biyala command area. The objectives are; 1) to simulate the present conditions under rotational irrigation and to identify the problem incurred, and 2) to simulate the continuous flow to be introduced in future in line with one point lifting pump instead of current individual liftings and to verify the merit or otherwise identify the demerit accompanied if any.

F.20.1 Hydraulic Modeling of the Bahr Biyala Command Area

With reference to the topographic survey that had been carried out during Phase II survey, the Bahr Biyala command area is modeled. The model is composed of 327 meshes, including dummy nodes, each of which has both water level and velocity nodes as shown below;



There are 7 gates presently in the command area that had been undertaken in this simulation, and the dimensions are as below;

No.; From To	Name	Kind	Base El.m	Width	Number
38 -→ 90	El Agamy	Intake	1.035	2.0	1
37 → 65	Bahr El Nour	-do-	0.785	3.0	1
36 → 35	Bahr Biyala	-do-	1.100	2.0	2
28 → 187	Tahweelah B. Biyala	-do-	1.105	1.2	1
27 → 161	El Shorafa	-do-	-0.065	1.5	1
18 → 46	Hazek	-do-	-0.130	1.5	1
18 → 17	Biyala extension	Regulator	-0.135	1.5	<u> </u>

With the introduction of the one-point lifting pump, the present Meskas will be buried (big ones will remain even in future), and the modeling is done by excluding the meshes that correspond to the Meskas. The modeling information is shown in the following tables and figures:

Figure F.20.1	Simulation Model for the Present Condition (Case 1)
Figure F.20.2	Simulation Model for the Plan (Meska Omitted) (Case 2)
Figure F.20.3	Simulation Model for the Plan with Automatic Gate (Case 2A)
Figure F.20.4	Simulation Model for the Plan with Automatic Gate (Case 2B4) Automatic gate location is different from case 2A.
Table F.20.1	Mesh Modeling Base Data (Present Condition) (7 sheets)
Table F.20.2	Meska Dimensions (2 sheets)
Table F.20.3	Mesh Modeling Base Data (the Plan) (3 sheets)

F.20.2 Simulation Case

Simulation study is carried out for the cases of; 1) present condition, 2) planned condition without automatic check gate (downstream water level constant gate), and 3) planned condition with the automatic check gate. The simulation period is to be 10 days in June that requires the maximum irrigation water. Also, minimum requirement is checked with the irrigation water of 1.02 cu.m/s at October. The water requirement and the case are as below;

Present; 8.69 cu.m/s (Max. only)

(See Table F.18.3)

Planned; 6.16 cu.m/s (Max.)

1.02 cu.m/s (Min.)

(See Table F.18.3)

Case	Irrigation	Meska	Check Gate	Q, cu.m/s	C'dition	Sim. Period
Casel	Rotation	As the present	No	8.69	present	10 days in July
Case2	Continuous	Abolished'	No	6.16	Planed	10 days in July
Case2'	Continuous	-do-	No	1.02	Planned	10 days in October
Case2A&2B	Continuous	-do-	Yes	6.16	planned	10 days in July

Note; * Large Meskas are to remain.

(1) Flow Input to the Model

There is a small mixing pumping station at the tail of Bahr Biyala. The pump lifts the drainage water from Drain No.4 into Bahr Biyala, and works 10 hours per day during peak period with a discharge of 1.0 cu.m/s (0.417cu.m/s per 24 hours). Therefore, in order to know the discharge from the intake of Bahr Biyala, this 1.0 cu.m/s (0.417 per day) discharge has to be subtracted from the discharges of 8.69 and 6.16 cu.m/s shown in above table;

Present (Case1);

from Bahr Biyala intake $(8.69-0.417) \times 2 = 16.546$ eu.m/s (first 5 days only) from Bahr Biyala tail $1.0 \times 10/24 = 0.417$ cu.m/s (converted into 24 operation for the simplification)

Plan(in July, Case2);

from Bahr Biyala intake 6.16 - 0.417 = 5.743 cu.m/s (continuous) from Bahr Biyala tail $1.0 \times 10/24 = 0.417$ cu.m/s (converted into 24 operation for the simplification)

Plan(in October, Case2');

from Bahr Biyala intake 1.02 cu.m/s (continuous) from Bahr Biyala tail 0.0 (no supply)

(2) Outflow from the Model

Outflow from the model is the pumping from Meskas and canals onto the fields by the farmers, and the pumping is modeled on basis of sine curve as shown below;

```
Present (Upstream, Case1);

First 5 days; Q = (1.0 + SIN((T-6) π/12)) x 1.7 x 8.69 x a / A

Last 5 days; Q = (1.0 + SIN((T-6) π/12)) x 0.5 x 8.69 x a / A

Present (Downstream, Case1);

First 5 days; Q = (1.0 + SIN((T-10) π/12)) x 1.7 x 8.69 x a / A

Last 5 days; Q = (1.0 + SIN((T-10) π/12)) x 0.5 x 8.69 x a / A

Where;

6 & 10; 4 (10-6) hours difference between up and downstream areas

1.7 / 0.5; adjustment factor

8.69; design outflow, cu.m/s

a; command area by the node concerned, feddan

A; total irrigation area of Bahr Biyala; 14,380 feddan
```

Whole command area for Bahr Biyala is divided into 2 areas as upstream ad downstream, and the peak of the pumping is assumed, with reference to the field condition, to have 4 hours difference between the upstream and downstream. Adjustment factors 1.7 and 0.5 were decided in such way of; 1) With the factor of 1.7, high water levels in the canals within Bahr Biyala are to be almost equal at the last day of the first 5 days, and 2) With the factor of 0.5, canals within Bahr Biyala are to have almost 0 storage.

```
Plan (Upstream & Downstream, Case2, 2', 2A&2B);
          In July: Q = (1.0 + \alpha \times SIN((T-6)\pi/12)) \times 6.16 \times a/A
                   Q = (1.0 \pm \alpha \times SIN((T-6)\pi/12)) \times 1.02 \times a/A
          Where;
                              the peak is to show up at noon with this 6
                    6;
                              maximum sine factor, 0.5 applied
                     α;
                              design outflow in July, cu.m/s
                    6.16;
                               design outflow in October, cu.m/s
                    1.02;
                               command area by the node concerned, feddan
                    a;
                               total irrigation area of Bahr Biyala; 14,380 feddan
                    A:
```

Pumping pattern is assumed to be same between upstream and downstream areas, therefore only one pumping pattern is employed over the Bahr Biyala command area. Factor α is to be 0.5 in this study, which means maximum pumping shown at noon is 150% of the average and minimum pumping is 50% of the average.

(3) Roughness Coefficient

Roughness coefficient is estimated by using current measurement results done on Bahr Tera. The coefficient on Bahr Tera ranges between 0.024 and 0.028 (refer to Table F.17.4). With reference to the value, this simulation undertakes 0.03 taking into consideration poor maintenance condition than that of Bahr Tera.

(4) Automatic Gate Modeling

An automatic gate, downstream water level constant type, is modeled as; 1) there is a buffer of 0.05 m each at upstream and downstream of the gate, 2) when the downstream water level at the gate goes down 0.05 m, the gate starts opening with a speed of 1 cm/min, and 3) when the downstream water level goes up 0.05 m, the gate starts closing with a speed of 1 cm/min.

F.20.3 Simulation Results

(1) Casel (Present Condition)

- Under present condition (rotational irrigation), it takes about 6 hours that the water discharged fills canals at upstream area of Bahr Biyala, while takes 24 hours or more to have the canals at downstream area of Bahr Biyala filled (see Figure F.20.5).
- Under present condition, water levels at downstream of Bahr Biyala fluctuates widely since
 discharge coming from upstream area cannot keep pace with the pumping done by farmers
 due to the time lag to reach. The low water level shown at the downstream area of Bahr
 Biyala makes it difficult to supply water into Meskas and canals branching from Bahr Biyala
 (refer to Figure F.20.5).
- Under present condition, water levels at tails of representative canals and Meskas fluctuate
 more widely than those shown in Figure F.20.5. Meska Rab El Fashool (No. 137) often dries
 up since enough water cannot be delivered into the Meska because of the fluctuation in Bahr
 Biyala canal (see Figure F.20.6).
- Present condition's hydrograph reveals that the water in Bahr El Nour canal starts reverseflowing after the discharge from Bahr Biyala intake stopped. This is because that the Nour's
 capacity is relatively large comparing to other canals, therefore the reserved volume is easily
 withdrawn by Bahr Biyala (refer to Figure F.20.7).
- Present condition's hydrographs reveal that the water at around tail of Meskas and canals is
 flowing very unstable running forward and backward. Water management under this situation
 is very difficult, and the farmers would face difficulty to lift enough and stable water from the
 Meska (refer to Figure F.20.8).
- Present condition's hydraulic profile along Bahr Biyala fluctuates widely, giving difficulty to water management and making difficult to supply enough water to Meska and canals downward. While, Bahr Nour's hydraulic profile does not fluctuate so much because of the large capacity of the canal. After the discharge is stopped, the water level in Bahr Nour goes down quickly, and this can be explained by backward flow from Bahr El Nour into Bahr Biyala (Figures F.20.9 & F.20.10).
- Reservation in canals are at maximum such as; 230,000 cu.m in Bahr Biyala, 130,000 cu.m in Bahr El Nour, 35,000 cu.m in El Agamy, 230,000 cu.m in Meskas and canals other than aforementioned at upstream of Bahr Biyala, 140,000 cu.m in Meskas and canals other than aforementioned at downstream of Bahr Biyala, and as much as 270,000 cu.m will be lost by

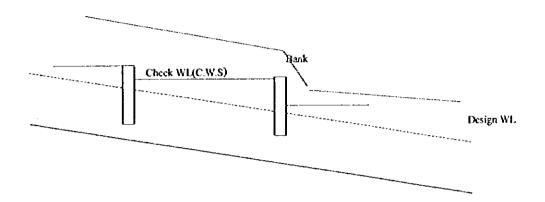
burying Meskas accompanied with one-point lifting pump (see Figure F.20.11)

- (2) Case2 (Continuous flow of max. 6.16 cu.m/s, Existing gates fully opened, Meska abolished)
 - With the continuous flow of maximum of 6.16 cu.m/s, the water level fluctuates with a range of 0.4 m only, and this does not seem to create any noticeable problem. However, when looking into the water level at the tail of Bahr Biyala (No.3), the water level is gradually raising up. This is because that some Meskas from Bahr Biyala cannot in-taken enough water, maybe because of the high bed level elevation, so that excess water goes to the downstream of Bahr Biyala (see Figures F.20.12, F.20.13, F.20.14, F.20.15).
 - Though the hydrograpfs do not give any problem, the hydrograpf at the intake of Bahr Nour
 performs very uniquely, showing reverse sine curve to the others. This shows unstable flow
 at around the intake of Bahr El Nour, incurred by unevenness of the bed level there (Figure
 F.20.13).
- (3) Case2' (Continuous flow of min. 1.02 cu.m/s, Existing gates fully opened & Operated, Meska abolished)
 - First, a simulation was made with the continuous flow of 1.02 cu.m/s and existing gates fully opened. This case revealed that the water level at the downstream of Bahr Biyala were raising up as observed in Figure F.20.12 but very sharply. This was caused by the fact that Meskas and canals from Bahr Biyala could not take enough water since the water level in the Bahr Biyala remained low. This suggests that check gates be required.
 - Secondary, with trial operations of the existing gates, several simulations were conducted. A simulation with the following gate operation revealed that the water level at the downstream of Bahr Biyala still did not stop raising up. This is because Meskas and canals from Bahr Biyala could not take enough water from Bahr Biyala because of the low water level in the Bahr Biyala. Also, since existing gate behaves as a gate keeping upstream water level constantly, the water level downstream of the gate often goes down quickly, making difficult that the farmers around take enough water (see Figures F.20.16, F.20.17, F.20.18, F.20.19).

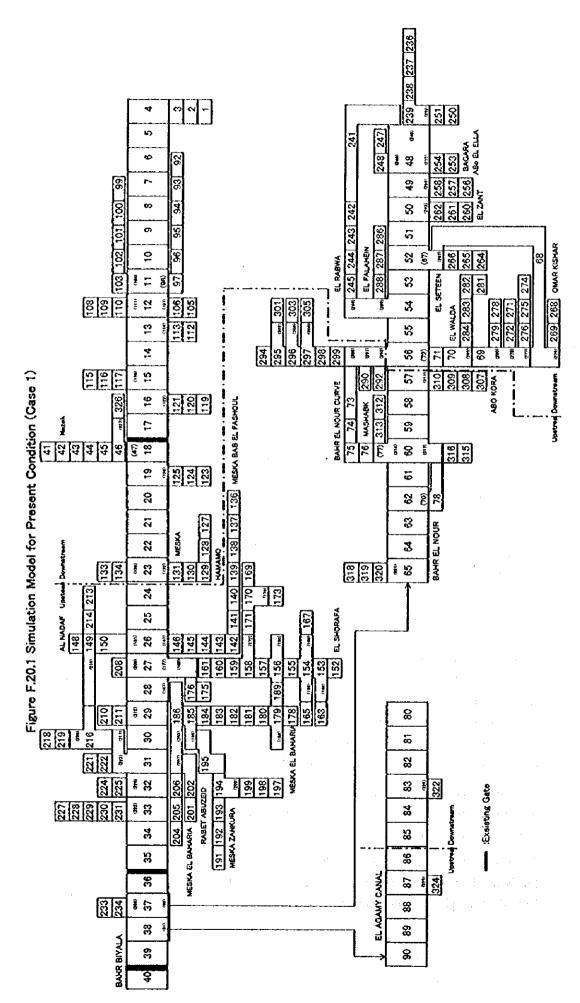
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No.: Fr to	Name	Opening, m
38 → 90	El Agamy	0.100
37 → 65	Bahr El Nour	0.060
36 → 35	Bahr Biyal	0.150
28 → 129	Tahweelah Bahr Biyala	Full open
27 → 119	El Shorafa	Full open
18 → 46	Hazek	0.060
18 → 17	Extension of Bhar Biyala	0.060

 Above results suggests that a automatic gate be required in order to raise water level in the Bahr Biyala during low water period of winter, so that Meskas and canals branching from Bahr Biyala can easily take enough water, and also to give enough water to downstream. This can be done with an automatic downstream water level control gate like Avio-Avis Gate.

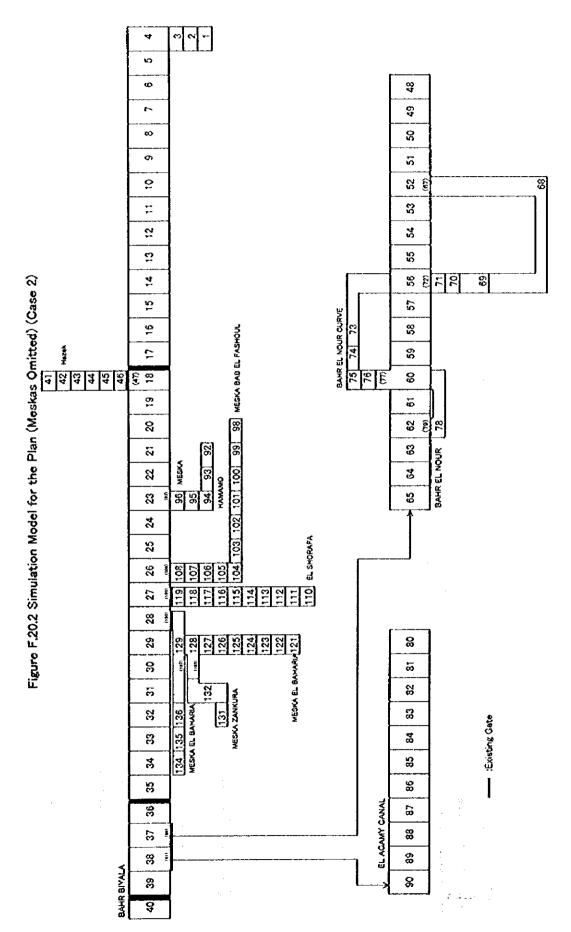
- (4) Case2A&2B (Continuous flow of max. 6.16 cu.m/s, With automatic checkgates, Meska abolished)
 - Location of check gate is decided in considering; 1) the canal bank elevation and the profile, 2) flow variation, 3) boundary of maintenance, and so on.



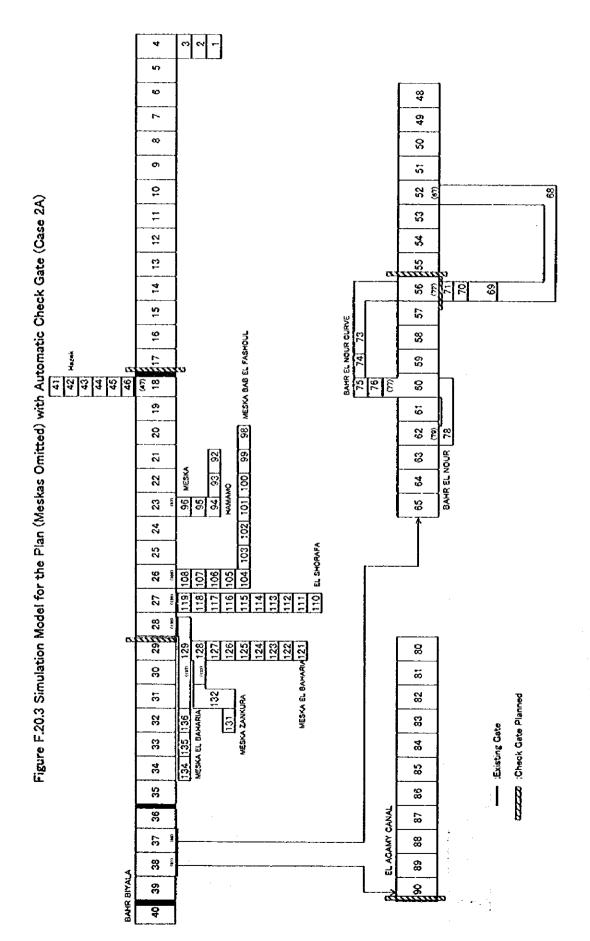
- Two check gates are planned on Bahr Biyala and the locations are to be in between; mesh No.17 & No.18 and mesh No.28 & No.29, check WLs of which are El. 1.5 m and El. 1.9 m respectively (See Figures F.20.20, F.20.21).
- Check gate on Bahr El Nour could be installed ether in between mesh No.55 and No.56 or the upstream of Bahr El Nour (in between mesh No.71 and No.56). The check WL is to be 2.0m. The former case is named Case2A and the latter Case2B (Figure F.20.22 and F.20.23).
- With the introduction of the gate keeping downstream water level constantly, the effect of pumping (outflow from the model) move to upstream area of the Bahr Biyala irrigation system. The water levels in the upstream of Bahr Biyala fluctuate within a rainge; 1.85 to 2.45 m at mesh No.29 to No.39, No.56 to No.65, and No.73 to No.78 for Case2A, and 1.85 to 2.60 m at mesh No.29 and No.39 for Case2B. The difference between the cases of Case 2A and 2B is not big with a mere 0.15 m only. Therefore, both cases are acceptable in terms of the simulation results but Case2A (check gate on Bahr El Nour is in the middle and not at the upstream) is preferred since the upstream is to have sluice gate (existing one) in order to measure the flow by using gate formula (see Figures F.20.24 to F.20.31).
- The hydrogaphs fluctuate periodically, and the flow at the intake of Bahr El Nour often goes backward. This would make difficult to measure the inflow volume into Bahr El Nour (Figure F.20.25 and F.20.29).
- The water level profile along Bahr Biyala does not give any problem, having enough water levels thanks to the downstream water level constant gate. The water level along Bahr El Nour does not give any problem either (see Figures F.20.26, F.20.27, F.20.30 and F.20.31).



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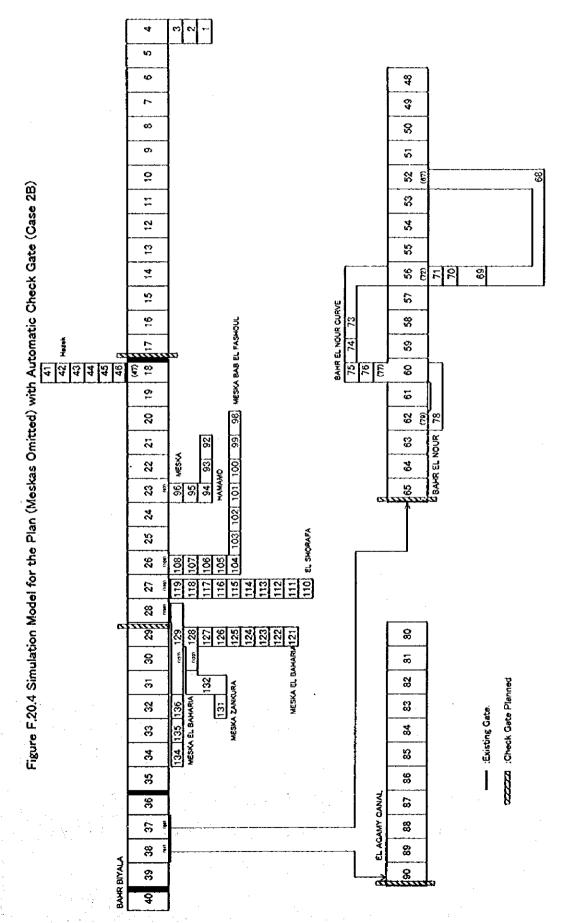


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		BAHR BIYALA			-15		-7. 70	_	다 당 (8	46 7.7		12 12 13 13 14			2	9		힉'		- 1	4		히		왕
1	7 5	SAHR BIYALA	No. 25	i 4	133		00 6	-5.48	9 6	48 6 6	9 6	8 52 	8 8	8 2	3 5	3 -4 -	<u> </u>	ة اد		71 3 60	35 29	388	3 2	0 03 36	3 5
37	£	BAHR BIYALA			112		-9. 50	L	8	9	3. 73	0. 53	0. 74	38	. 04		36	ď	18		0	-4	9	ខ	28
**		BAHR BIYALA	No. 9	14	111		-9.50 -			6 9.5	÷;	0.91	0.65	0.61	3.84	O.	12	o	8		l	1, 31	0.03	0. 03) 51	24
	25	BAHR BIYALA	No.	7		-+	-8.68	1, 72 0.		2 8.68	3 3.59	0, 95	90	7.08	1. 15	o	8	00	ខ	ı	Ö		0.03		24
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Table F. 20. 1 Mesh	ih Modeling Base	Data	7050n	(Present Condition	ion for	Bahr	Biyels)	ار							ł	ł		ŀ	ŀ			ŀ	Ì	
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55	BAHR EL MOUR		23	165	1	5, 65	6 8	~	٠٠ <u></u>	**	0.83	3	- 1		<u>"</u>	9			٠٠٠			8 8	3 6	91 . 2
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25 25	BANK EL MUR 2 CURVE	No. 11	52			-3.85 -0		L_	m	3.	L.		22	, 42	- -	12 0.	8	8	"	2			0.03	21, 74
Ш	BAMR EL MUR 2 CURVE	No. 3	52	150		-4. 25 -0.	ö		4	'n		86 .0		3. 42	-	O	8	00	**	7			3	21.74
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78	BAHR EL MUR 1 CURVE	¥o. 11	24	148		-2.25 -0	-0. 98 0.	00 00	98 2, 25	3.54	1. 42	1.37	1.42	3. 53	-	27	8	8	*3	-	1			23, 60
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81	CARD EL AGAMY		12		1	-4.00	0	8 3	٠	٠,	-		- 1			3	8	8	` ``	<u>.</u>	- 1		3	27. 87
28	CARD EL ACAMY		275	20.		5. 00 -2	5 6	2 S	24 5.00	3 37	5 3	72.	26	5 6	- -	2 4	8 8	8 8	7	21.	- 1		3 6	27.87
78	CARD EL ACANY	2	15			20 -	-2 03	3 8	ĕ ¬	Ĭ ~	-		1		<u>-</u>	2 8	3 8	3 8	1	1			8	27. 87
85	CARD EL ACAIT	No. 45	2	L	T	4.30	o	8	4	7	Ŀ	1, 06	٩		-	9	8	8	18	ŀs	L.		8	27.87
98	CARD EL ACAMY		Ξ	104		-3. 70 -0	o	8	-3	•	۲		ı			0	 8	8	۳,	چا	ı		8	27.87
87	CARD EL ACAMP	1 1	11	103		-4. 00 -1	ø	8 -	4	"			14			0	8	8	"				8	27. 87
88	CARD EL ACAIM	No. 21	Ξ	103		-4, 40 -1, 70	히	8	÷	••	-		1 1		-	97	8	8	"	7	1 1		9	27. 87.
88	CARD EL ACANT	- 1	Ξ	102		-5.00 -2	ø	رب اح	١	**	۲	1. 20	ı			Ö.	8	8	**	ᆵ	- 1			27.87
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91	GARD EL AGANY			ñ	38 Dummy	-	1	_					-	1		1.	82	8	"	2	- 1		9	0.
92 BAHR BIYALA				_		-2. 60 -1	o	8	۲,	~	98		2	61		53	8	8	٦	긁	- 1			31.08
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Tabi	F. 20. 1	Mesh Modeling Base Data		(Present Condition	t Cond	lition f	for Bahr	₿	yala)														l		[
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116							-2. 60	-1, 05		7		0.36	63	85 2.	61	0, 6				2. 61			93	, 63 33.	9
117							-2. 60	-1.05	8	05 2. 6	0 2.61	98 0	0, 69 0.	85 2.	-	0.6	ij	- 1		2. 61		0.88	8	03 2	8
118						15 Dummy			_				-	+	=	0.6	ı			2. 60	12. 24		8	ខ	8
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122						16 Dummy							\dashv		=	0.				3 8	10 67		8	8	8
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<u>8</u> 2		WESKA HARANO		25	- [-2.00	Ç5 P		_	~	0 81	8	~; 88	- 	9	I	- 1	ŀ	2, 21	4.0		8		ह्र
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132		MESKA HAKANO			1	23 Drummy		-	-	Ľ	ĿĽ		+	-	= - - - - -	0. 47	\perp			2.89	9		3	8	8
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137		BAS EL FASHOOL		l	257		-2.80	<u> </u>	0, 00	~		0, 75	55	2	45	0.45			0.38	2.45			8		15
138		BAB EL FASHOOL		28	257		-2. 50	-1 00	2	2. 5	2		38	63 2.	. 22	Ö		1	l	2 22	4 61	300	8	8	15
139		BAB EL FASHOOL			256		-2. 45	-1. 07	00	2.	2	09 '0		55 2.	32 :	0.4			i	2. 32			ខ		1.5
140		BAB. EL FASHOOL	No. S6		552		-1. 25	-0.81	00		٠,	1. 92	1.87	94 2.	1 59	1.8				2.36				8	25
141	,	BAB EL FASHOOL	No. 48		752		-2, 15	-0.89	00	7.	5 2.52	0. 84	0. 72	85 2.	1 22					2. 52	7. 13		0. 03	ខ	15
- 22		BAB EL FASHOOL			253		-2 8	92	9	~	~	0.87	25	82 2.	78						2.85	0, 62			2
5		BAB EL FASHOOL			253		-2.30	-0.95	00	7	2	0.66	37	3,	3				o				0.03	8	5
Ĭ		BAB EL FASHOOL	No. 24		252		9	-	8	*	- 1	20	- 1	نه ق	20	9.			0.35		5. 73	0.83	8	0. 03 22.	5
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2		BAB EL FASHOOL	ğ		52		22	5		15 2, 7	5 2.71	93		~	<u>-</u>		٥		- [2, 71		0.83	8	8	2
Š		BAB EL FASHOOL			- 1	26 Dummy						1		ŀ	=	9	1		히	3. 20	- 6	- 1	ខ	ខ	8
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5		EL NADAF	Se.	\$ P	224		-2. 00 -1. 09				2	1. 45	2	57. 2.	- 88		o		0.14	2. 59	9. 54	0.75	ខ	0, 03 21.	श
ž		EL MADAF	MO. 8				-1. 50		8 6	76 1. 5	0 2.78	0.92	0. 72 0.	87 2.	-	0, 73	Ö		이		4, 43	0, 39			의

Tabie F. 2	20. 1 Mesh	th Modeling Sase Data	- 1	0.20	t S	(Present Condition fo	for Bahr Bi	-	(8 8)						ŀ			}	}	╌	ŀ				
		•		100	Topo Mao			ះ្រ	ction Dis	2	3	E S	Elevatio	;	т	Sec.	- 78.	<u> </u>	2 - AR3	ξ <u>.</u>	AR4	ARU	2 6	2000	5 2
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35		EL SHRFA	No. 64	\$	1		25	L	0,00	=	•	o	o	0.77	3. 10			8	ģ	1	11		Ö	93	22. 02
155		EL SMRFA		3	İ		-5, 60	_		Z	ri	1	ģ			-	1	õ	e.	H	4	60 1.45	6	8	22. 02
156		EL SYRFA		4	202		-4, 90		8	22	2	o	0			_	li	8	0	: 1	4	-	9	8	22. 02
157		EL SHRFA		85 65	IJ		-4, 60		링	z l	2	이	٥			_		9	9	- 1	4		이	0.03	22. 02
158		EL, SHRFA	No. 32	33			-4. 75 -1. 75	- 1	힑	넔	~	이	이			_	- 1		힑	- 1	~	-	انه	8	22. 02
159		EL SHRFA	No. 24	39	200		-3.75		힑	힣	"i	힉	이			_	- 1	힑		- 1	اك		이	8	30.38
160		EL SHRFA	No. 16	39			-4. 65		힝	2	~	히	이			=	- 1	<u> </u>	힑	- 1	9	-	힉	g	30.38
191		EL SHRFA	No. 8	39	198		-4, 50	-2. 22	0. 00 2.	22	٧,	81 0.70	٥	0.81		-		9	9	- 1	120	-	히	헔	30, 38
162		EL SHRFA		ĺ		27 Dummy	0.00	0.00	0. 00	_						==		ĕ	2	- 1	-	_	힉		9
32		EL SHRFA					-2. 60	-1. 05	0.00	05 2.	50) 2.	61 0.85	0, 69	0.85	2. 61	_		g	닞		ပ	0	ಠ	8	
79		EL SMRFA	- -			153 Dummy		ŀ	8		_	_				II		8	9		ΒŞ	9	ਾ	3	9
165		EL SMRFA		1			-2. 60	-1.05	0. 00	32	2, 60 2, 61	51 0.85	3.68	0.85	2. 61	 		8	D.	ŀ	é	0	o	3	12. 60
166		EL SHRFA	-			1 SA Dummy	1	0.00	o. 60	L_	1	L	L		┝	 =	1	8	<u> </u>		=	0	ø	8	8
167		EL SHRFA					-2. 60	┺.	0, 00	05 2	60 2.6	61 0.86	0.69	0.85	2, 51	_	1	8	8		ف	o	Ö	3	12.60
168		EL SHRFA				154 Dummy	00 0	L.	0, 00			L		-		=		8	8		-	0	Ö	0. 03	0.00
169		EL SHRFA						١.	0, 00	2 20	60 2.	ď	ö	0.85	2.61	╁		8	8		ف	Ö	Ö	0.03	17.64
170		ABOU ABO EL NABE	Mo. 16	49	227			1	8	707	20 2	79 1.08		0.97	2, 45		i	8	Š	i I	Ġ	0	0,	0.03	17.64
171		AROU ABD EL MABE	1 _	49	L			L_	0, 00 0	177	70 2		ö	0.89		-	1	8	몽		٠i	0	Ö	0, 03	17, 64
172		ABOU ABD EL NABE			L	158 Dummy		Ł	8	\vdash	-	l	L			=		8	8	1	~	_	o	0, 03	0.00
<u> </u>									0.00	0.5	60 2.	61 0.86	0, 69	0.85	2.61	-	1	8	8	l	Ġ	0	o	03	16, 80
72: F.						170 Dummy		-	-		-				-	=		90	00		45	0	ø	0.03	0.00
Ļ							-2.50		0.00	SO	60 2.	61 0.86				-		90	90		6.	0	O,	8	16.80
<u> </u>							-2.60 -1.05	1	<u>L</u> .	. 05 2.	60 2.	0	ರ	0.85	2.61	_		8	2		ō	0	0	8	16, 80
122						27 Dummy								_		-	il	8	8	i	1.7	-	ರ	8	8 8
178		MESKA EL BAHARIA (A)		F	193		-2.15		9	82	15 2	5	o,		2, 37			8	90	ı	30	0	ø	ខ	9: 61
179		MESKA EL BAHARIA (A)		37			-2, 30 -1, 04			2	30 2	ರ	ŏ	0. 62	2, 33	-	i	8	8		16,	0	Ö	8	19, 16
180		MESKA EL SAHARIA (A)		37	181		[-3, 00] -1, 28		90	28 3.	00 2.	oj.	Ö		2. 12	1		ဗ္ဂ	9		53.		Ö	8	19, 16
181		MESKA EL BAHARIA (A)	No. 37	36	190		-3 00	-1. 08	ន	80	00	6	9		1. 92	=		91) 임		Ö	1.	ರ	8	9 10
182		MESKA EL BAHARIA (A)	ž	ا پر	l		-2.00	6	8	₹ ~:	00 2.	ဗ	Þ		2, 42	 -	ı	8	8		4.5	0	ø	8	19, 16
183			<u> </u>	36			-3.00	-0. 66	8	39	2.	ರ	ö		2. 54		l I	8	8	1 3	4.9	·.	٥	0.03	19, 16
134			-	ا چ			-2, 45 -0, 83	-O. 83	0.00	83 2.	45 2.	80 0.50	0. 48	0.49	2. 41	 	ı	8	8	i	29	0	Ö	0.03	19, 16
185		MESKA EL BAHARIA (A)	No. 5	36	187		-4. 95	-1.80	90	80 4.	95 3.	Ö	Ö		2, 55	-		00	00	l	135.	•	ø	0.03	31.74
186		WESKA EL BAHARIA (B)	No. 7	38	194		-3.80	-0.97	0.00 0.		80 3.	Ö	Ö	0.87	3. 37	_		8	8		*		Ö	0.03	31.74
187		MESKA EL BAHARIA (A)				28 Dummy										==		20	용	- 1	9		ਂ	8	8
138		UGNES ABOU RAKHA				179 Очяту											- 1	8	ខ្ល	1	2	oi =	ರ	8	8
189		UONES ABOU RAKHA	No. 8	20	229	1	-3, 60	-2.04	0.00	3.	60 2.	53 1. 07	0.51	0.84	2. 73	_	- 1	g	8	1	4	ö	ď	8	19. 16
190		UONES ABOU RAKHA				156 Dummy		-										00	90	4	4		٥	3	0
191		MESKA ZANKURA	No. 47	ĕ	182		-1.65		80	68	65 2	Ö	0	o			1	é	8	- 1	نہ	3	9	0.03	22. 37
192		MESKA ZANKURA	No. 39	ž			-1.65		8	2	65 2.	o	0	G			١	8	g	J	٠	9	Ö		22, 37
193		WESKA ZANKURA	No. 31	33	181		-2. 05		00	7.9	05. 2.	o	0	Ö				8	8		د	Ö	9		22. 37
7		MESKA ZAMKURA	No. 23	33			-2 00		8	5	2 00	ö	Ö	9		_		8	8	1	-1	٥	9	0 03	22, 37
195		MESKA ZAMKURA	No. 15	3			-2		8	98	10 2.	ď	٥	이			- 1	8	8	- 1	~	9	ੰ		24. 47
186		MESKA ZAMKURA	%. 7	22	178	185 Dummy	-2, 15 -1, 10		8		15 2	۲	0	-		_	- 1	8	8	- 1	4	-	0	0	0.00
197		MESKA ZAMKURA					-2.60		90	5	60 2.	=	٥	ď		_	· i	8	8	ŀ	ف	-			20, 27
198		MESKA ZAHKURA					-2 60		0.00	2 50	2	61 0.86	0, 69		2, 61		0.69	0.00	8	0, 17 2,	2, 61 6, 37	37 0, 88		0	22, 37
19.9		MESKA ZAMKURA					-2. 60	-1. 0S	8	0.5	60 2.	9	히	히		_	89	90	8		9	Ö	ø		22, 37
200		MESKA ZANKURA				194 Dummy						_			 	 _=	5	8	밁	ŀ	~	-	ات	0,03	0.00
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2 8	200	Canal page 1000 1000	00	7	Kemarks				֡֟֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֟֟֓֓֓֓֓֟֟֓֓֓֓֓֟֓֓֓֓֟	•	1	†	1	_1_	E (E 6	E 6	E .	┇	\perp		3 6	
<u> </u>	5 !	KARAA ABOU ZETO	اءً				ı	ار 3 ا	٠ [٠	ij	= :	; ;	از				3	3	 - -	2	ن اد	١	
~	202	RASAA ASOU ZEID	No. 8	47 220		-2. 25	0 21	8	91 2. 25	2. 97	- 9e	 95	15, 2, 93	-	9,	o	9		8		o 2	၀	~
∾	203	RABAA ABOU ZEID	4		186 Dummy		ı	1			L	- 1	ı	=	0.64	ı	90	0. 21	<u></u>	7. 66	0 / 0	03 0 03	8
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ř	205	MESKA EL BAHARIA (B)	23	38 196	91	-3, 60 -0, 81	0.81	8	- 1	1	22	- '-	· i	-	1. 07	- 1	9 8		4	6, 75	o l	<u>ا</u> ت	
N	90	MESKA EL BAHARIA (B)			_ !_	5	ŀ	8	201 4. 05	~	H	<u>ت</u>	25		0.77		9		2	6. 80	oj ,	٠.	"1
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~	215				149 Dummy		1							=	1. 37		o. 00	0, 14	5.8		9	Ö	0.00
7	216					-2.60	-1, 05, 0,	90	05 2. 60	2. 61	0.86 0.	69 0.	85 2 61	-	0, 69		0 0		119		ø	33 0. 03	37, 80
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į	218			_		-2 60	1	8	ام		9	69	~		0.69	ı	0,00	0.17	15	ļ	ø	9	ì
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2	22			_		-2. 60	-1, 05, 0.	8	05 2, 60	ı	0.86 0.	63	85 2.	-	0. 69	ŧ	9, 9	ر ان	!	1	ت	0	
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	92				32 Dummy		1			-		_	-	=	1. 03	ŧ	0.00	0.36	34		o,	٥	0.00
2	22					-2. 60 -		1.	7	2.	0.86 0	69 0.	2.	-	0, 69		0.00	0.17	22		o	3 0.03	25. 20
22	82					-2. 60 -	1. 0S G.	1.		2. 61	86	69 0.			0. 69		0.00	0.17	15		.0	o	23. 52
2	62			-		-2.60 -		1.	2.	7	0.86 0.	69 0.	2,		0. 69	1	0, 00	0.17	19	1	88 0.	o	19. 32
z.	30					-2.60		2	5 2. 60	2, 61	0.86 0	69 0.	85 2.61		0. 69		0,00	0. 17	L_	5. 37 0.	88	5	16.80
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S	23				33 Dummy		(B							=	0.73		0.00	0.00			46 0.	O	0.00
8	33					-2 60 -	-1.05 0.	8 -	۲,	2.61	98	63	2		69 0		0.00	0.17	19		83; 0.	3 0 03	16.80
<u>ال</u> م	2			_		-2 60	-1.05	1 05	5 2. 60	2.61	0.86	69	85 2. 61	-	0.69	- 1	g. 00	0 .7	23	5, 37 0.	88	0	10. 50
X	35				37 Dummy			4	1		+	_		=	0.86	- 1	0.00		2	1	0	9	
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3	n:	HOAD 25	-		43 Dummy		+	4		1	- 1	$\frac{1}{1}$		=	0.26	- 1	9	0.78	22		6 0	ت	- 1
	= (EL FALAMEIN	No. 36	542	2	-2. 70	-1. 25 -1.	8	2,70	5.3	0.86	ا د	80 2.13	-	0.75	- 1			2	18, 18	اه		- 1
	ا ج	EL FALAPEIN	83	1		2. 23	-	5 8		7,7	- 1	92 02	N	-	0.80	- 1		<u>0</u>	2		o O	_ [_
\$ i	2	EL FALAPETH	20		0	1.75	_1	8 9	[2, 27	- 1	6 8	_1		0.68	- 1	o. 00	0. 13	27	10. 63 0.	S3 0	ات	L
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	2	EL FALAHEIR	₩6. 4 4			-2.00	0 32 0	9 8	- 1	2. 74	1. 19		20 2.82		1. 15	0.00				0, 70	68 0.	ð	8.40
	9	EL FALANEIN		\downarrow	S& Dummy		- 1	-	ŀ	+	- 1	-		=	0.59	o. 00		0.54			ð	0	0.00
77.	7.1			_	 	-2, 60 -1, 05	0.0	1 05	2 2 60	_	0.86 0.	59	85 2.61		0. 69	0.00	9.00	0, 17	1.9	37	88	03 0, 03	
48	8		+	1		-2. 60 -	•	8	نا		- 1	ات 29				0.00			19		98 0	e)	-1
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Table F. 20. 1 Mesh	sh Modeling Base Data	- 1	resen	(Present Condition	tion for	r Bahr	<u>=</u>	3															
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252				ш	239 Dummy		Щ.	L					ŧ I	=	0.58	0.00	8	ŀ	1	o	89 0.03	0.03	0.00
253	BACARA	-1	35	185		-2.85 -	-1.02 0. (00 1.02	2.85	2.75	0.38 0.	08	37 2.67	-	0.08	0.00	8	li	. I	ರ	ø	0.03	11
356	BACARA	9	2	184		-3. 50 -	0		eri	22	2	6 =	ن2		= :	8	8 3				1	o ·	
256	ABOU EL ELLA	No. 20	5	232	+-	-2.65			~	- 12	9	25 0.	2	-	0 20	8 8	9 0	0,78	2.58 4.	4. 31 1. 6	83 0 03		22 87
257	ABOU EL ELLA	No. 12	51	232		-2. 60 -1. 13	o	00 1.13	2. 60	5	SS	25 0.	نہ ن	-	0.25	90	8	1		, 0	i ci	ته اد	22. 82
253	אשפח בר בררא	No. 4	51	231		-2. 50	Ö	00 1.03	ج:	1 .	0. 60	45 0.	75 2,35	-	0.45	0.00	8			Ö		1	22. 82
259	יאפסח בר בררץ			\mathbb{L}_{-1}	49 Dummy					Н				==	0.26	0.00	8	1	i i	=	6	0	0, 00
260	EL ZANT	No. 21	25	236		-1.40 -(ပ	ø	-	1.2	8	75 0.	2	-	0.75	0.00	90	!]	f I	9	6	o	21.00
192	EL ZANT		25	235		- 20 - 1	-0. 59 0.	00 0.59	!I	2, 29 0	0. 78 0.	75 0.	76 2.05	-	0.75	0.00	8	ll		히	9	6	21.00
262	EL ZANT	.ge	क्ष	1		-1.50	0	이		8	5	 'S	~		1. 05	0.00	8	ĺí		0	0	٥	21, 00
263	EL ZANT		1	- 1.	SO Dummy			١						=	0.35	8	8		1	-[٥	٥	000
265	EL SETESN	No. 24	5	218		20 20	9	0.5	200	2. 23 1	3	- i	85 2 43	1		8	8	ı	•	٠ ا	60 0.03	6	14, 00
266	GL SETEEN	9 2		717		2 2		이.	Ľ	,	2 G	٥ ا تا تا	Ni.	1	2	8	8 :	- 1	- 1	-	oj,	03	7.00
267	EL SETEEN		1	1	S2 Dummy	3	5	1	1	-	2	ું દ	اة-	-	9 0	3 8	3 8	- 1		_	17 0 03	3 5	2 0
268	EL HAGAR (KISHAR)	№ 16	3	L	1	-2 30		<u> </u> -	~	13	1, 03	=	1		0	3 8	3 8	1		-	9 0	10	3 8
269	EL HACAR (KISHAR)	%e. 8	4	210			9	00 0 80	2.25	2.50	S	3	07 2. 54		1 03	9	8	1		٦	d	9	2.00
270	EL MACAR (KISHAR)			j	68 Dummy		o		1_	\vdash	-	-		=	0.76	90.0	8			-	9	٥	0. 00
1772						-2.60 -	ø	00 1.05	Li	1.9	86	69	~	-	0.69	0, 00	8	1	1	g	o	6	7.35
222					-	-2.60 -			2.	2.61 0	0.86 0.	69 0.	85 2.61	-	0.69	0 00	8			9	o	ø	7, 35
233					69 Dummy							_		=	0.71	0, 00	00			نہ	O.	Ö	0.00
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27.0			1	-	1	- 09 -	Ö	00 1.05		L	0,86	69	85 2 61	-	0.69	0 00	8	. 1		3	Ö	9	11. 20
6/10		1	1	+	7	-2. 60 -1. 05	0		۲,	9	98	63	~		0.69	0.00	8	- 1	- 1	9	6	9	11. 20
117			1	+	69 Dummy		ŀ	1	'	-	+	-	-	=	0.71	8	8	•	1	-	9	익	9.0
27.0			T	+		00 7	2 2	200	2 5	2 2	98 6	62	85 2, 61	1	0.69	00	8	- 1	i	٠ <u> </u>	ci]	이	86 6
280				1	69 Dummy	7. 00	3		انا	╁	8	5	×]	- =	2 6	9 6	8 8	1	i i	이-	Ł	ပြုံ	2 S
182	EL WALDA		4.2	_	т	-2.75	9	-	~	12	35	210	١٠	-	1	3 8	3 8	1	£	1	ile	' c	3 3
282	EL WARDA	No. 19	45	208		-2.00 -([c]	00 0. 56	2.00	2.47 0	0.54	Si	52 1.95	F	0.51	90	8 8	1		9	9	9	13.65
283	EL WARDA		27	208		-1.75	9	0	-	2.9	29	95	2	-	95	8	8	[•	9	g	0 03	13, 65
282	EL WARDA	ž	2	202	7	2.00	히	히	<u>ن</u> ہ	20	. 01	81	~		0.81	a, 00	8	i I	: 1	ᅙ	ø	0.03	13. 65
282	EL WARDA		1	L	70 Dummy			_	ı	+	+			=	0.86	90.0	8	1			e,	0.03	0.00
787	C. Deput	20.	3 2	655		29 1	9 6	00 0 00	- 1	2. 75	. 03	0. 95 1. 03	2. 53		0.95	8	8	- 1	•	히	0	0 03	12. 38
288	EL RABWA		3 5	200	T	3 2	3 6	<u>ء</u> د	- 6	8 5	9		٠į.	- -	2	9	8 8	- 1	- 1	۰ انت	١	6	17. 88
522	EL RABWA			1	SA Dummy		از	1	i				3	- =	0 0	3 6	3 5		- 1	٠ د	s) c	ء اد	00.7
280	AL MASHABIT	No, 6	32	<u> </u>	+	-2. 00 -	-0.93 0.0	00 0 93	2.00	3.06	. 28 1.	09 1.19	9 2 92	<u>-</u>	1 03	3 6	3 8				, c	3 8	
291	AL MASHABK				56 Dummy			L				1_		=	0.54		2 2	i	•	i	Ö	6	00
282						-2.60 -1	-1, 05 0, 0	00 1, 05	2. 60	2.61 0	0.86 0.	69 0.	85 2.63	_	0.69		8	1		Ö	Ö	0.03	16. 80
282					S6 Dummy					_	-		_	=	0.54		g	ļ	ę.	-	0	0 03	0.00
762			†	+		-2. 60 -1. 05	o	-	۲,	. 9		69 0.	2		0.69		90	I		ᅙ	Ö	0 03	16. 33
262			1	+	1	-2. 60	0	-1	۲	5	띪	69	~		0. 69		9	ı		ᇹ	ဝ	이	16. 33
296			†		1	-2. 60 -1. 05	۰	-	~	ᇹ	댦	69	~;		69 0			1		ø	ان	0	16. 33
298			†	+		2 60 -1 05	۰ ا ۰	00 5	2 60	2.61	0 86	نا ق	85 2.61	-	0 63		8	1		행	oj.	8	15. 33
200		<u> </u>	1	+		2 60.	٥	- -	~i r	<u>.</u>	2 8	0 0	~i c	<u></u>	0.69		ا واع	- !		٠ ٠	히	٥¦٠	16.33
300			T	+	S6 Dummy	£. 000	5	-	V	-		اخ 2	ŀ	 =	200	8 8	 g g	2 2		이.	38 0.03	3	5 C
					-	1	-		1	-	-	-		1	5		1	1	ŧ	-	- 1		3

				,	Topo Map	_	_	Canal Se	ection	Distanc	Ç		Ē	evatio	Ę		Sec.	2	AR:	ARZ	AR3	K	ARG	ARS	SHS 1	RNS2
2	Canal	Canal	Section	ت	z. Sec.	c. Remarks	×	X2	X3	X	xe	۲۱	42	۲3	7.4	Y5	Type	EL. m	ŧ	E	E	EL.			0.03	0.03
301					_		-2. 6	-2, 60 -1, 05	5 0. 30	1.05	2.60	19'7	0.86	0.69	0.85	2.61	-	0.69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0.03
302			_			295 Dummy											=	0.69	00.00	0.00	0, 17	2.61	6.37	0.88	0	0.03
303				_	_		-2.5	-2. 50 -1. 05	5 0.00	1.05	2, 60	2.61	0, 86	69 0	0.85	2.61	_	0.69	0.00	0.00	0, 17	2.61	6.37	0.88	0.03	0 03
304					_	296 DUMMY	,	-									==	0. 69	0.00	o. 00	0.17		6, 37	0.88	0.03	0
305							-2. 60	0 -1 05	5 0. 00	1.05	2, 60	2. 61	0.86	0. 69	0.85	2.61	_	0. 69	0.00	0.00	0.17	2.61	6.37	0.88	0.03	0 03
306						297 Dummy			_								11	0.69	0.00	0, 00	0.17	2.61	6, 37	0.88	0.03	0 03
307		ABO KORA		31	31	175	1-3.00	0 -1.28	3 0.00	1.28	3.00	2. 44	0.73	0.73	0.73	2, 19	==	0. 73	2. 56	0.00	0.00	5. 19	0.00	1 09		0
308		ABO KORA	No. 2	23	31	174	-3.0	16 0-0	0 00	0.91	3, 00	2.68	09.0	0.60	0. 60	2. 53	==	0, 60	1.82	0.00	0.00	2. 53	L.,	1 04	0. 0.	8
308		ABO KORA		. 5	31	173	-2, 90	16 0- 0	C.	0	2.	89 2	0.70	0.70	0.70	2.	=		1, 82	0.00		2, 68	0.00	0.96	o	0
310		ABO KORA	No.	7	31	172	-2. 40	0 -0.55	0.00	0.55	2.40	3.09	1. 20	1. 20	1. 20	2, 79	1	1. 20	1, 10	0.00	0, 00	2, 79	တ	-	0.03	8
311		ABO KORA			_	57 Dummy											=	0.87	0.00	0.00	0, 28	3.24	14, 50	1.53	0.03	8
312				Ц			-2.60	0 -1, 05	5 0.00	1, 05	2.60	19 2	98 '0	0, 69	0.85	19 2		0.69	0, 00	9. O	ø	2,61	6.37	0.88	0, 03	8
313				L	_		-2. 60	0 -1.05	0.00	1, 05	2. 60	19.2	98.0	0.69	0.85	19 2	_	0.69	00.00	0.00	Ö	2, 61	6.37	0.88	0.03	0.03
314				_	_	60 Dummy	_										==	0. 52	0.00	C. 00	0, 50	3, 53	5,65	1.46	o	0.02
315					_	_	-2.6	-2. 60 -1. 05	i a. oa	1,05	2. 60	2.61	0.86	0.69	0.85	2.61	_	0. 69	0.00	0. 0.00	71.0	2.61	6.37	0.88	0, 03	0.03
316				L	_		-2. 60	0 -1.05	5 0.00	1.05	2. 60	19 '2	0.85	0.69	0.85	2.61	_	•	0.00	0.00	0.17	2.61	6.37	0.88	L_	0.03
317					_	SO Dummy											11	0. 52	0, 00	0.00	0.50	L				
318					_		-2. 60	0 +1.05	0.00	1.05	2.60	2.61	0.85	0.69	0.85	2.61	-	0. 69	0.00	0, 00	0, 17	2.61	6.37	0.88	0.03	0.63
319							-2. 60	3 -1, 05	0,00	1.05	2, 60	2.61	0, 86	0, 69	0.85	2, 61		0.69	0, 00	0.00	21 0	2.51		0.88		0.03
320						-	-2. 60	0 -1.05	a. 00	1.05	2. 60	2. 61	0.85	0.69	0.85	2.61	-	0.69	0, 00		21.0	2.6:	6.37	0.88	0.03	0.03
321				Ц		65 Dummy	_							-			=	0.39	0, 00	0.00	0.87	3, 95	4 52	-	0.03	0.03
322							-2.60	1 -1.05	0.00	1.05	2. 60	2 61	0.86	0.69	0.85	2, 61		0.69	0.00	0, 00	21.0	2.61	6.37	0.88	0, 03	0.03
323						83 Dummy	_										=	1, 16	0, 00	0.00	0.38	2.77		1.45	0.03	0.03
324					_		-2, 60	1 -1. 05	0.00	1.05	2, 60	2 61	0. 86	0.69	0.85	2, 61		0.69	0.00		ø	2.61	6 37	0,88	0.03	0.03
325						87 Dummy											1	0.97	0.00	0.00	0, 50	3.0	3, 28	1. 42		0.03
326							-2. 60	1 -1.05	0.00	1.05	2. 50	2. 61	0.86	0.69	0.85	2.61	-	0, 69	0, 00	o. 3 0	0, 17	٠.:	ض		0.03	
327						46 Dummy	_		_								==	0.83	000	8	0.15	2, 95	19, 76	1.48	0 03	0 03

Table F. 20. 2 Meska Dimensions

	ar source/edition/orthers	Es per marint	STREET SANTS	Q81	10 F. 2		OSKA	ni Maus	10115	. Yere a block to the			and the second
234 344	, , , , , , , , , , , , , , , , , , , ,	Topo.	No.		Sect	ion Dist	ance				levatio	n	
No.	Sec.	Lng.	Sec	χı	X2	Х3	X4	X5	Υı	ΥZ	Y3	Y4	Y 5
127	No. 36	55	246	-0.75	-0.51	0.00	0.51	0. 75	2. 44	2. 20	2. 10	2. 22	2. 54
128	No. 28	55	245	-2.00	-0. 97	0.00	0. 97	2. 00	2. 52	0. 81	0. 60	0.88	2. 21
129	No. 20	55	244	-1. 75	-0. 62	0.00	0. 62	1. 75	2. 74	0. 85	0. 72	0. 93	2. 70
130	No. 12	55	244	-2. 50	-0. 94	0.00	0.94	2. 50	3.11	0. 88	0.53	0.78	2. 98
		55	243	-2. 00	-0.96	0.00	0. 96	2. 00	3. 06	0. 98	0.73	1. 08	3. 49
131				-2. 90	-1. 17		1. 17	2. 90	2. 39	0. 66	0. 36	0. 51	2. 84
136	No. 88	59	258		-1. 09	0. 00 0. 00			2. 46	0. 85	0. 30	0. 90	
137	No. 80	58	257	-2. 80			1. 09	2. 80	2. 22				2. 45
138	No. 72	58	257	-2. 50	-1.00	0.00	1.00	2. 50		0. 55	0. 38	0.68	2. 22
139	No. 84	58	258	-2. 45	-1. 07	0.00	1. 07	2. 45	2. 33	0. 60	0.40	0. 55	2. 32
140	No. 56	58	255	-1. 25	-0. 81	0.00	0. 81	1. 25	2. 36	1. 92	1.81	1. 94	2. 65
141	No. 48	58	254	-2. 15	-0.89	0.00	0. 89	2. 15	2. 52	0. 84	0. 72	0. 85	2.71
142	No. 40	57	253	-2. 00	-0. 92	0.00	0. 92	2. 00	2. 42	0. 87	0. 52	0. 82	2. 78
143	No. 32	57	253	-2. 30	-0. 95	0.00	0. 95	2. 30	2. 73	0. 66	0. 37	0. 87	3. 04
144	No. 24	57	252	-3. 10	-1. 35	0.00	1. 35	3. 10	2. 82	1. 07	0. 52	0. 67	3. 29
145	No. 16	57	251	-2. 80	-1. 15	0. 00	1. 15	2. 80	2. 68	1. 03	0. 78	0. 88	3. 09
146	No. 8	57	250	-2. 75	-1. 15	0.00	1. 15	2. 75	2.71	0. 83	0. 58	0.73	2. 71
148	No. 24	48	225	-2. 00	-0. 94	0.00	0. 94	2.00	2. 71	1. 39	1. 22	1. 39	2. 82
149	No. 16	48	224	-2. 00	-1.09	0.0 0	1. 09	2. 00	2. 59	1. 45	1. 37	1. 57	2. 88
150	No. 8	48	223	-1. 50	-0.76		0.76	1. 50	2. 78	0. 92	0. 72	0. 87	2. 81
152	No. 80	40	205	-3. 50	-1.65	0.00	1. 65	3. 50	2. 54	0. 62	0. 31	0.71	2. 61
153	No. 72	40	205	-4. 60	-2. 35	0.00	2. 35	4. 60	3. 01	0. 56	0. 31	0. 64	2. 81
154	No. 64	40	204	-3. 50	-2. 17	0.00	2. 17	3. 50	3. 23	0. 84	0.61	0.77	3, 10
155	No. 56	40	203	-5.60	-1. 94	0. 00	1. 94	5. 60	3.03	0. 40	-0. 11	0. 25	2. 69
156	No. 48	40	202	-4. 90	-2. 22	0.00	2. 22	4. 90	2. 47	0. 76	0. 24	0. 72	2. 51
157	No. 40	39	201	-4. 60	-1. 84	0.00	1. 84	4. 60	2. 86	0. 76	0. 37	0. 73	2. 57
158	No. 32	39	201	-4. 75	-1.75	0.00	1. 75	4. 75	2. 46	0. 62	0.40	0. 64	2. 64
159	No. 24	39	200	-3. 75	-1. 46	0.00	1. 46	3. 75	3. 29	0. 68	0. 48	0.70	2. 89
160	No. 16	39	. 199	-4. 65	-1. 82	0.00	1. 82	4. 65	2. 70	0. 92	0. 82	0.77	2. 66
161	No. 8	39	198	-4. 50	-2. 22	0.00	2. 22	4. 50	2. 81	0. 70	0.69	0. 81	3. 00
170	No. 16	49	227	-1. 90	-0.70	0.00	0.70	1. 90	2. 79	1. 08	0. 90	0. 97	2. 45
171	No. 8	49	226	-1. 70	-0.77	0.00	0. 77	1. 70	2. 60	1. 27	0. 77	0. 89	2. 41
178	No. 61	37	193	-2. 15	-0. 82		0. 82	2. 15	2. 72	0. 54	0. 50	0. 52	2. 37
179	No. 53	37	192	-2. 30	-1. 04	0.00	1.04	2. 30	2. 04	0. 59	0. 54	0. 62	2. 33
180	No. 45	37		-3. 00	-1. 28	0.00	1. 28	3. 00	2. 12	0. 43	0. 40	0. 42	2. 12
181	No. 37									0. 35	0. 35	0.35	1. 92
182	No. 29	36					0. 64	2. 00	2. 56	0. 54	0. 52	0. 53	2. 42
183			-		-0. 66	0.00		3. 00	2. 85	0. 53	0. 51	0. 52	2. 54
184	No. 13		1		-0. 83	0. 00	0. 83	2. 45	2. 80	0. 50	0. 48	0.49	2. 41
185	No. 5			-2. 80	-0. 70	0.00	0. 70	2. 80	3. 04	0. 96	0. 94	0. 95	2. 55
186	No. 7				-0. 97	0.00	0. 97	3. 80	3. 66	0. 83	0. 64	0. 87	3. 37
189	No. 8	*		-3. 60	-2. 04	0.00	2. 04	3. 60	2. 63	1. 07	0. 51	0. 84	2. 73
191	No. 47			-1. 65	-0. 68	0.00	0.68	1. 65	2. 20	0. 58	0. 30	0. 58	2. 23
192				-1. 65	-0. 62	1	0. 62	1. 65	2. 07	0. 48	0. 43	0. 53	2. 20
193				-2. 05	-0.79	0.00	0. 79	2. 05	2. 31	0. 63	0. 33	0. 63	2. 28
194				· · · · · ·	-0. 93		0. 93	2. 00	2, 11	0. 58	0. 43	0. 73	2. 38
195				-2. 10	-0. 98		0. 98	2. 10	2. 47	0. 98	0. 53	0. 88	2. 67
196				-2. 15	-1. 10		1. 10	2. 15	2. 53	1. 13	0. 88	1. 13	2. 90
201	No. 16			-2. 35	-0. 89	0.00	0.89	2. 35	2.74	0. 91	0.71	0. 86	2. 42
202		47			-0. 91	0.00	0. 91	2. 25	2. 97	1.06	0. 96	1. 15	2. 93
204		38		-2. 35	-0.73	0.00	0. 73	2. 35	2. 90	1. 55	1. 48	1. 60	2. 90
205			·	-3. 60	-0.81	0.00	0. 81	3. 60	3. 08	1. 22	1, 07	1. 17	3. 18
205		•		-4. 0S	-1. 20	0.00	1. 20	4. 05	2. 87	0. 97	0. 72	0. 97	3. 26
				-4. U3 -2. 50	-0. 92	0.00	0. 92	2. 50	2. 52	0. 70	0. 58	0. 70	2. 79
236 237				-2. 50 -2. 85	-1. 30	0.00	1. 30	2. 85	2. 04	0. 10	0. 37	0. 10	2. 24
				-2. 83 -3. 00	-1. 37	0.00	1. 37		2. 47	0. 84	0. 73	0. 81	2. 60
238									2. 45	0. 75		0. 71	2. 90
239	No. 4	56	247	-2. 70	-1. 00	<u> 0. 00</u>	י שען	2. 10	£. 43]	V. 13	U. 20	0.11	2. 30

Table F. 20. 2 Meska Dimensions

-	********	Topo. No. Section Distance							Elevation				
		Topo.		Xi T		X3	X4	X5	YI	Y2 1	Y3	Y4	Y5
No.	Sec.	Lng.	Sec		X2								
241	No. 36	54	242	-2. 70	-1. 25	0.00	1. 25	2. 10	2. 31	0. 86	0. 75	0. 80	2. 13
242	No. 28	5.4	241	-2. 25	-0. 94	0.00	0. 94	2. 25	2. 21	0. 90	0.80	0. 95	2. 23
243	No. 20	54	240	-1. 75	~0. 85	0. 00	0. 85	1. 75	2. 27	0. 88	0. 68	0. 73	2. 43
244	No. 12	54	240	-2. 25	-0. 98	0. 00	0. 98	2. 25	2.63	0. 81	0.61	0. 71	2. 54
245	No. 4	54	239	-2.00	-0. 92	0.00	0. 92	2. 00	2, 74	1. 19	1. 15	1. 20	2. 82
253	No. 17	35	185	~2. 85	-1. 02	0.00	1. 02	2. 85	2. 75	0. 38	0. 08	0. 37	2. 67
254	No. 9	35	184	-3, 50	-1. 01	0.00	1. 01	3, 50	2. 68	0, 79	0.11	0. 77	2. 43
256	No. 20	51	232	-2. 65	-1. 03	0.00	1. 03	2. 65	2. 72	0. 40	0. 25	0. 60	2. 28
257	No. 12	51	232	-2. 60	-1. 13	0.00	1. 13	2. 60	2. 39	0. 55	0. 25	0. 60	2, 55
258	No. 4	51	231	-2. 50	-1. 03	0. 00	1. 03	2. 50	2. 56	0. 60	0. 45	0. 75	2. 35
260	No. 21	52	236	-1. 40	-0.70	0.00	0. 70	1. 40	2. 21	0. 80	0. 75	0. 80	2. 13
261	No. 13	52	235	-1. 50	-0.59	0. 00	0. 59	1.50	2. 29	0. 78	0. 75	0. 76	2. 06
262	No. 5	52	234	-1. 50	-0.72	0.00	0.72	1. 50	2. 63	1. 07	1. 05	1. 08	2. 15
264	No. 24	45	218	-0.50	-0. 22	0.00	0. 22	0. 50	2. 23	1. 84	1. 83	1. 85	2. 43
265	No. 16	45	217	-2. 25	-0. 82	0.00	0. 82	2. 25	2, 27	0. 84	0. 74	0. 94	2. 22
266	No. 8	45	216	-4.00	-1.50	0. 00	1. 50	4. 00	2. 56	0. 89	0. 74	0. 89	3. 83
268	No. 16	43	211	-2. 90	-1. 30	0.00	1. 30	2. 90	2. 63	1. 03	1, 01	1. 02	2. 44
269	No. 8	43	210	-2. 25	-0. 80	0.00	0.80	2. 25	2. 50	1. 05	₹. 0 3	1. 07	2. 54
281	No. 27	42	209	-2. 75	-1. 07	0. 00	1. 07	2. 75	2. 33	0. 25	0. 21	0. 22	2. 53
282	No. 19	42	208	-2. 00	-0.56	0.00	0. 56	2. 00	2.47	0, 54	0. 51	0. 52	1. 95
283	No. 11	42	208	-1. 75	-0.64	0. 00	0.64	1. 75	2. 67	0. 59	0. 56	0. 58	2. 63
284	No. 3	42	207	-2. 00	-0. 80	0. 00	0. 80	2. 00	2. 81	1. 01	0. 81	1. 01	2. 40
286	No. 19	53	238	-1.65	-0. 66	0.00	0. 66	1. 65	2. 75	1. 03	0. 95	1. 03	2. 53
287	No. 16	1	238	-1. 80	-0.78	0.00	0.78	1. 80	2. 56	1. 28	1. 20	1. 30	2. 57
288	No. 8		237	-2. 30	-0. 99	0.00	0. 99	2, 30	2, 60	1. 29	1. 18	1. 26	3. 03
290	No. 6	t — —		-2.00	-0.93	0.00	0. 93	2.00	3. 06	1. 28	1. 09	1. 19	2. 92
307	No. 31	31	175	-3.00	-1. 28	0.00	1. 28	3. 00	2.44	0. 73	0. 73	0.73	2. 19
308	No. 23	31	174	-3. 00	-0. 91	0. 00	0. 91	3. 00	2. 68	0. 60	0. 60	0. 60	2. 53
309	No. 15	31	173	-2. 9 0	-0. 91	0. 00	0. 91	2. 90	2. 68	0. 70	0.70	0. 70	2. 86
310	No. 7	31	172	-2. 40	-0. 55	0. 00	0. 55	2. 40	3. 09	1. 20	1. 20	1. 20	2. 79
Ave				-2. 60	-1. 05	0.00	1. 05	2. 60	2. 61	0. 86	0. 69	0. 85	2. 61