SUPPORTING REPORT F HYDRODYNAMIC SIMULATION

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SUPPORTING REPORT F HYDRODYNAMIC SIMULATION

1. Introduction

In "The Master Plan on Flood Control in the Northern Rural Region of Santa Cruz" in 1996, flood analyses were conducted in the Chane – Pailon Area and the San Juan – Antofagasta Area to simulate the flood area with and without the flood mitigation and drainage improvement measures. The flood in 1992 was used to calibrate the hydrodynamic model. The hydrodynamic model was then used to simulate the probable flood for design rainfalls with 2, 5, 10, 20 and 50 year return periods.

In this study, the hydrodynamic model used in the Master Plan Study in 1996 was updated by using the new cross sections from the newly constructed bridges and the topographic survey conducted during the Study. The purposes for these are:

- To verify the application of the formulated hydrodynamic model for the current floods,
- To clarify mainly:
 - the extent of the back water effect from downstream of the Rio Chane,
 - the effect of the overflow from the Rio Grande,
 - the effect of the natural retarding basins in both areas for flood mitigation,
 - the effect of the newly constructed bridges to the flow in the Study Area and
 - the effect of the confluence at the Arroyo Jochi and Tacuaral.
- To simulate the design floods at each return period years,
- To clarify the improvement of flood condition with the project implementation compared to the condition without the project implementation.

2. Hydrodynamic Model Structures

2.1 Model Formulation

The hydrodynamic model was formulated with the same basis as in the Master Plan Study in 1996. The model was set up for the river basins in the study area those were classified as the target areas for structural measures as follows:

The Chane – Pailon Area : The Rio Chane-Pailon basin and

The Okinawa Drainage basin

The San Juan – Antofagasta Area : The Arroyo Yapacanicito, Jochi and

Tacuaral basin

(1) Model Formulation in the Chane -- Pailon Area

The river system in the Rio Chane-Pailon basin and the Okinawa Drainage basin was composed of the main rivers, the Rio Chane and the Rio Pailon, 4 tributaries, the Quebrada Chacras, the Quebrada Toro, the Quebrada Maras and the Quebrada Meco and 1 drainage canal, the Okinawa Drainage. The basin was divided into 27 sub-basins in the main rivers, tributaries and drainage as follows:

River	Sub-basins	Total	Area (km²)
Rio Chane	A-1, A-2, A-3, A-4, A-5	10	1,368.80
	A-7, A-8, A-9, A-10, A-11		
Rio Pailon	Λ-6	1	211.87
QDA Chacras	B-1, B-2, B-3	3	224.25
QDA Chane	C-1, C-2, C-3, C-9	4	235.61
QDA Toro	C-4, C-5, C-6	3	171.29
QDA Maras	C-7, C-8	2	62.36
QDA Meco	D-1	1	244.82
Okinawa Drainage	E-1, E-2, E-3	3	381.50

The coordinates and chainages of the river system were shown in Table F.2.1. The area and the connecting points of the river system were shown in Table F.2.2, F.2.3 and F.2.4.

A total of 17 runoff points were set up in the river model with 15 points in the rivers and tributaries and 2 points in the drainage in for the calculation. The location of these points and the connection of sub-basins were shown in Figure F.2.1 and F.2.2.

(2) Model Formulation in the San Juan - Antofagasta Area

The river system in the Arroyo Yapacanicito, Jochi and Tacuaral basin was composed of the main rivers, the Arroyo Yapacanicito, the Arroyo Jochi and the Arroyo Tacuaral and some water flowing routes found during flood periods. These routes were set up as tributaries in the model namely the Jochi-Tacu, the R/W Embank and the TMP-R/W. The drainage basin was divided into 14 subbasins as follows:

River/Arroyo	Sub-basins	Total	Area (km²)
Arroyo Jochi	J-1, J-2, J-3, J-4	4	148.0
Arroyo Tacuaral	T-1, T-2, T-3, T-4	4	252.8
Arroyo Yapacanicito	YI-1, YI-2, YI-3, YI-4,	6	370.7
	Y2-1, Y2-2		

The coordinates and chainages of the river system were shown in Table F.2.5. The area and the connecting points of the river system were shown in Table F.2.6.

A total of 13 runoff points were set up in the river model with 5 points in the Arroyo Yapacanicito, 4 points in the Arroyo Jochi and 4 points in the Arroyo Tacuaral. The location of these points and the connection of sub-basins were shown in Figure F.2.3 and F.2.4.

2.2 Boundary Condition

The time series of flow rate in each sub-basin from the rainfall-runoff analysis were used as the inflows to the river system in the models.

Manning roughness coefficients of the rivers without the river improvement were set as follows:

Without the river improvement:

With the river improvement

Both areas = 0.003

The other necessary parameters in the simulation were set same as in the Master Plan Study in 1996.

Water levels at the downstream end of the rivers during the current floods in 1997 and 1998 were obtained from the questionnaire surveys conducted during the study in both river basins.

2.3 Hydrodynamic Simulation Program

A hydrodynamic simulation program so called MIKE11 developed by the Dennis Hydraulic Institute (DHI) used in the Master Plan Study in 1996 was adopted in this study to analyze the current floods with the unsteady flow condition. The calibration

results and necessary parameters in the model set up in the Master Plan Study in 1996 were also used in this simulation.

3. Hydrodynamic Simulation for the Current Floods

3.1 Purposes

The flood analysis was conducted using the current floods in 1997 - 1998 those were reported to create flood damages in the study area in order to clarify the following points:

- The application of the flood model for the current floods,
- The effect of the back water from the Rio Pirai to the Rio Chane.
- The effect of the overflow from the Rio Grande,
- The effect of the retarding basin at the upstream of the Rio Pailon and QDA Chane,
- The effect of the construction of seven bridges along the Route number 9,
- The effect of the inundation from the Rio Yapacani,
- The effect of the retarding at the confluence of the Arroyo Jochi and Tacuaral,
- The effect of the inflow from the Arroyo Jochi to the San Juan area and
- The effect of the contraction in the Arroyo Yapacanicito, Jochi, Tacuaral and others.

3.2 Simulation Set-up

The simulation was done for the floods in 1997 and 1998 in order to compare with the actual inundation depths and areas obtained from the flood damage survey conducted in this study.

(1) Simulation Set-up in the Chane – Pailon Area

The simulation periods were as follows:

The Rio Chane- Pailon basin : November - December 1997

The Okinawa drainage basin : November - December 1997

and February - March 1998

The changes of river condition and flow due to the construction of 7 bridges after 1995, the overflow from the Rio Grande basin and the back water from the Rio Piray basin were to be clarified in the simulation. These points were taken into consideration in the hydrodynamic model as follows:

The effects to be clarified	The condition set up in the simulation
1). The effect of the contraction and the meandering in the Rio Chane and the Rio Pailon	The cross-sections were set up at the contraction and meandering to obtain the changes of hydraulic characteristics
2). The effect of the overflow from the Rio Grande to the Okinawa drainage	The calculation was done using the rainfalls during the period that was reported to have the overflow
3). The back water effect from the Rio Piray to the Rio Chane	The water level at the downstream end was set up by considering the back water from the Rio Piray
4). The effect of retarding at the upstream of the Rio Pailon and QDA Chane	The retarding was set up in terms of the storage volume in the cross sections at the confluence
5). The effect from the construction of seven bridges along the national highway number 9	The cross sections at the bridges were used in the simulation to obtain the changes of hydraulic characteristics

(2) Simulation Set-up in the San Juan - Antofagasta Area

The simulation period was as follows:

The Arroyo Yapacanicito, Jochi and Tacuaral Basin : January – February 1997

The changes of river condition and flow during the flood period were to be clarified. The main causes of these changes were the overflow from the Rio Yapacani, the contraction in the Arroyo Yapacanicito, Jochi, Tacuaral and others, the effect of retarding at the confluence of the Arroyo Jochi and Tacuaral and the inflow from the Arroyo Jochi to the San Juan area. These points were taken into consideration in the hydrodynamic model as follows:

The effects to be clarified	The condition set up in the simulation
1). The effect of the inundation from the Rio Yapacani	From the questionnaire surveys, there was reportedly no inundation from the Rio Yapacani after 1995. Therefore, no condition set up for this effect
2). The effect of the contraction in the Arroyo Yapacanicito, Jochi, Tacuaral and others	The cross-sections were set up at the contraction to obtain the changes of hydraulic characteristics
The effect of retarding at the confluence of the Arroyo Jochi and Tacuaral	The retarding was set up in terms of the storage volume in the cross sections at the confluence
4). The effect of an inflow from the Arroyo Jochi to the San Juan area	From the questionnaire surveys, there was reportedly no inflow from the Arroyo Jochi to the San Juan area after 1995. Therefore, the river network was changed according to this condition

3.3 Simulation Results

(1) In the Chane - Pailon Area

The simulation was done for the floods during November – December 1997 for the Rio Chane – Pailon basin and during November – December 1997 and February – March 1998 for the Okinawa drainage basin.

The Rio Chane - Pailon basin

The effect of the back water from the Rio Piray and the contraction of the rivers were examined by varying the water level at the downstream end of the Rio Chane for 2 cases, those are

Case I: Water level set up from the questionnaire survey

Case II : Very high water level set up for the comparison

The simulation results revealed that

 In Case I, it was found that the water level profile from the simulation as shown in Figure F.3.1 was not much different from the flood damage survey conducted in this Study. The inundation depth varied 1.0 - 2.0 m. for the whole area. The maximum water levels and discharges were shown in Table F.3.1 and F.3.2.

The model was therefore considered applicable for these floods.

2) In Case II, it was apparent that the effect of back water was terminated at the chainage 63.60 km which was the location of a bridge across the river at the junction of the Rio Chane and Pailon (or the cross section No. R310 in the Master Plan Study in 1996) as shown in Figure F.3.2.

The hydraulic characteristics at the chainage 63.60 km and nearby were calculated as shown in Table F.3.3. The bank elevation at the chainage 63.60 km was sufficiently high to confine the peak water level during flood period in the river course while the other sections could not. Therefore, the Froude Number (Fr) at this section was comparatively high and the flow condition changed from the sub-critical flow in the upstream to almost the critical flow at this section and to the sub-critical flow again in the downstream. A summary of the Froude Number was as follows:

Chainage	Bank	Max WL	Cross section	Depth	Froude
	El. (m)	(m)	(m²)	(m)	Number
62.10	239.44	239.77	219,95	6.60	0.44
63.50	237.96	238.28	620.37	6.63	0.32
63.60	240.00	237.97	103:37	6.36	0.96
63.70	237,90	238.18	385.53	6.60	0.42
67.50	235.62	236.96	379.96	7.94	0.27

Note

Froude No. $Fr = Q/A\sqrt{gD}$

Where Q = Discharge m³/s,

A = Cross section m²

D = Hydraulic radius m, $g = 9.81 \text{ m/s}^2$

Therefore, it was summarized that the effect of the back water from the Rio Piray was terminated at the Chainage 63.60 km due to the contraction at that section and the flow condition at that section was almost a critical flow.

The retarding basin at the upstream of the Rio Pailon was located between the chainage 2.00 km and 6.00 km and that of the QDA Chane was located between the chainage 13.60 km and 16.30 km. The peak discharges were as follows:

Chainage	Maximum discharge		Remarks
	(m ³ /s)	Time	
RIO PAILON 2.500	125.35	1997/12/04 15:26	
RIO PAILON 3.500	121.52	1997/12/04 17:22	
RIO PAILON 4.500	118.92	1997/12/04 19:00	` [
RIO PAILON 5.500	116.36	1997/12/04 20:05	Effect of
RIO PAILON 6.500	75.51	1997/12/05 16:51	the retarding
RIO PAILON 7.500	75.01	1997/12/05 19:41	basin
RIO PAILON 8.500	74.70	1997/12/05 23:18	
RIO PAILON 9.500	74.58	1997/12/06 01:52	
QDA CHANE 14.017	191.43	1997/12/01 13:12	
QDA CHANE 14.850	191.28	1997/12/01 13:48	-
QDA CHANE 15.683	189.67	1997/12/01 14:30	
QDA CHANE 16.150	188.05	1997/12/01 14:40	Effect of
QDA CHANE 16.250	50.65	1997/12/01 22:42	the retarding
QDA CHANE 16.717	50.60	1997/12/01 22:53	basin
QDA CHANE 17.550	48.35	1997/12/01 23:14	
QDA CHANE 18,383	46.60	1997/12/01 23:53	
QDA CHANE 19.150	46.61	1997/12/01 23:56	

The peak discharge at the upstream of the Rio Pailon was reduced for about 35 % after passing through the retarding basin. But the delayed time of the peak and the decrease of water level between the upstream and downstream of the retarding basin could not be found clearly.

The peak discharge at the upstream of the QDA Chane was reduced remarkably for about 73 % after passing through the retarding basin. But the delayed time of the peak and the decrease of the water level between the upstream and downstream of the retarding basin could not be found clearly either.

4) The cross sections at the newly constructed bridges along the National Road No. 9 were used in the simulation. The results showed no any sudden change in the water level at these cross sections, therefore, it was summarized that there was no effect from the construction of these bridges to the flow.

The Okinawa Drainage

The effect of the overflow from the Rio Grande was verified. The simulation was done during the period with and without the overflow as reported in the flood damage survey as follows:

Case I: The flood during November - December 1997,

(Without overflow from Rio Grande)

Case II: The flood during February – March 1998,

(With overflow from Rio Grande)

The simulation results revealed that

1) In Case I, the inundation depth as shown in Figure F.3.3 was found to be about 1.0 m for the whole drainage basin from the simulation. This showed a good agreement with the flood damage survey that the inundation covered all the drainage basin. However, the inundation depth from the simulation was slightly higher than the questionnaire survey in the upstream. The maximum water levels and discharges were shown in Table F.3.4.

The model was therefore considered applicable for this flood.

2) In Case II, the simulation result as shown in Figure F.3.4 clarified that there was almost no inundation during that period because the rainfalls in the basin at that time were not extensive. The water level was about same as the bank elevation. However the questionnaire survey revealed that at that period the whole area was inundated by the discharges from the Rio Grande.

Therefore, it was summarized that the causes of inundation in the Okinawa Drainage were from the heavy rainfalls in the basin and the overflow from the Rio Grande.

(2) In the San Juan – Autofagasta Area

The simulation was done for the floods during January – February 1997. However, from the flood damage survey, it was found that during that period

- There was no inundation from the Rio Yapacani
- There was no inflow from the Arroyo Jochi to the San Juan area Therefore, these effects could not be verified from these floods.

The simulation results revealed that

 The simulation as shown in Figure F.3.5 was applicable for the floods in 1997 in comparison with the questionnaire survey on the flood damages.
 The water level in the Rio Yapacanicito was slightly lower than the flood damage survey but still in an acceptable range.

The model was therefore considered applicable for this flood.

2) The retarding basin at the confluence of the Arroyo Jochi and Tacuaral apparently delayed the peak period of the water level in the Arroyo Jochi's downstream of the retarding basin. The peak period in the upstream and downstream of the retarding basin were as follows:

Chainage	Maximum water level		Max. discharge	Remarks
	(m)	Time	(m^3/s)	
JOCHI 21.000	256.46	1997/02/06 06:40	55.68	
JOCHI 22,700	254.56	1997/02/06 22:51	55.68	
JOCHI 25.600	251.61	1997/02/07 11:48	55.68	
JOCHI 29.700	246.64	1997/02/04 04:28	66.32	Effect of
JOCHI 29.700	246.64	1997/02/04 04:28	66.32	the retarding
JOCHI 29,800	246.56	1997/02/04 09:18	66.32	basin
JOCHE 35,800	244.40	1997/02/08 15:27	35.18	[····· ·
JOCHI 39.600	244.10	1997/02/08 17:03	36.69	1

The retarding basin was located between the chainage 25.60 km and 35.80 km. The delayed time was in a range between 12-24 hours. The peak discharge in the Arroyo Jochi also decreased remarkably about 47% after the retarding basin.

However, the Arroyo Tacuaral also passed through this retarding basin but the delayed time at the downstream of the retarding basin could not be found. This was due to the topography of these rivers that the Arroyo Tacuaral has a lower elevation than the Arroyo Jochi. The flow direction in the retarding basin was mainly from the Arroyo Jochi towards the Arroyo Tacuaral. Therefore, the discharge at the downstream of the Arroyo Tacuaral after the retarding basin remarkably increased as follows:

Chainage	Maxin	Maximum discharge				
	(m^3/s)	Time				
TACUARAL 21.750	111.43	1997/02/05 19:14				
TACUARAL 25.050	111.06	1997/02/05 21:15				
TACUARAL 27.550	139.18	1997/02/05 04:01	Retarding			
TACUARAL 29.850	254.52	1997/02/04 05:37	Basin			
TACUARAL 35.000	173.99	1997/02/08 10:55	1			

Maximum water levels and discharges in the Arroyo Yapacanicito, Jochi and Tacuaral basin were shown in Table F.3.5.

3) The water level fluctuation in the longitudinal profile was not so high and no any sudden water level change was found along all the rivers. Therefore, the effect of the contraction and meandering was considered negligibly small.

4. Improvement of the Hydrodynamic Simulation

Although the flood analysis for the current floods showed satisfactory results, the model was improved for the hydraulic design by using a new topographic survey conducted by the JICA Study Team in 1998. The range of new cross-sections of the rivers and drainage set up in the model were as follows:

River	Chainage of new cros	s-section (km)	
	From	То	
The Chane-Pailor	n Area		
Chane	24.00	59.60	
Pailon	60.00	88.10	
Okinawa	0.00	26.80	
The San Juan - A	ntofagasta Arca	***	
Yapacanicito	14.30	31.70	
Jochi	13.80	25.60	
Tacuarai	16.80	22.60	
San Juan km 11	0.00	2.41	
San Juan km 13	0.00	3.82	
San Juan km 15	0.00	8.93	
San Juan km 17	0.00	4.27	
San Juan km 24	0.00	5.58	
San Juan km 28	0.00	10.55	
Antofagasta	0.00	8.80	
Road-cum-emb.	0.00	9.00	

The model structure was in principle exactly same as in the Master Plan Study in 1996 and the progress stage of this study, except the number and shapes of the new cross sections.

The flood simulation was also done again with the new cross sections in order to compare with the result from the flood simulation in the Master Plan Study in 1996 and the progress stage of this study. It is found that the results using the new cross section were almost exactly same as before with no significant difference.

The new cross sections are shown in the Data Book.

4.1 Condition Set-up in the Simulation

In order to obtain sufficient information for the river design, preparation of flood hazard maps and economic analysis, a total of 10 cases each in the Chane - Pailon Area and the San Juan - Antofagasta Area was set up in the simulation. These cases, as shown below, were considered as sufficient to reveal all the necessary hydrodynamic information including water level, flow rate, etc. for the further analysis. The simulation cases are as follows:

1	در بروی پروی کی در کار در در	Calculation cases					
Design Flow	Rio Char	ne-Pailon	ion A. Yapacanicito and others		on A. Yapacanicito and others		Remarks
(return period	Cross	section	Cross	ection	1		
year)	Existing	Design	Existing	Design	1		
2	· 1	1	1	1	Flow rate in the		
5	1	1	1	1	calulation was		
10	1	1	1	1	design flow		
20	t	1	1	1	with different		
50	1	1	1		return period		
Total cases	5	5	5	5	year		

All design discharge hydrograph had the same shape but different magnitude as explained in the following section.

4.2 Simulation Results for Design Discharge

Simulation for the design discharge was done in the study area for 2 cases, those are:

Case I:

Existing cross section with design discharge (without project)

Case II:

Design cross section with design discharge (with project)

Case I and II were considered as the cases without and with the implementation of the project respectively.

(1) In the Chane - Pailon Area

The simulation was done for the design discharge with the return period 2, 5, 10, 20 and 50 years with the same shape but different magnitude. Peak runoff at each return period of the sub-basins is summarized as follows:

River	Sub-basin	Peak runoff at each sub-basin (m³/s)						
	No.	2 years	5 years	10 years	20 years	50 years		
Chane - Pailon	A-1	126.8	178.1	212.1	244.6	286.7		
	A-2	173,5	248.4	298.5	347.0	410.2		
	Λ-3	196.9	279.6	334.6	387.5	456.3		
	A-4	218.2	311.1	371.9	430.4	503.4		
	A-5	55.2	77.2	91.8	106.4	124.4		
	A-6	323.3	464.9	558.2	648.9	761.9		
	Λ-7	169.6	242.9	291.2	338.1	396.7		
	Λ-8	321.3	490.3	603.3	709.0	849.0		
	A-9	210.7	318.7	390.6	457.8	546.6		
	B-1	33.8	47.1	55.8	64.1	74.8		
	B-2	181.3	257.5	308.3	357.1	420.6		
	B-3	149.1	208.8	248.2	285.8	334.5		
	C-1	14.7	20,5	24.4	28.0	32.7		
	C-2	76.1	106.2	126.0	145.0	169.5		
	C-3	188.5	265.7	317.0	365.8	429.0		
	C-4	96.6	134.4	159.3	183.6	215.0		
	C-5	47.8	65.9	77.7	88.9	103.5		
	C-6	194.8	275.0	328.3	379.3	445.4		
	C-7	87.1	122.0	144.9	166.7	194.9		
	C-8	76.4	107.1	127.5	147,0	172.2		
	D-I	314.3	449.4	538.6	625.2	733.3		
	A-10	104.1	148.4	177.6	206.1	241.7		
	A-11	307.8	444.5	535.0	622.9	732.9		
	C-9	231.5	326.3	389.1	449.0	526.4		
Okinawa	E-1	107.8	154.2	184.7	214.2	251.9		
	E-2	133.4	190.8	228.6	265.0	311.6		
	E-3	292.7	423.7	510.1	593.8	701.0		

Note: The sub-basin number is shown in the figure of flow model

The time series of the runoff or the design hydrograph used in the calculation for return period 2, 5, 10, 20 and 50 years were shown in the Supporting Report -- B.

For Case I (without the project), the cross sections were updated in the priority area by the new topographic survey as shown in the Data Book.

For Case II (with the project), the cross sections were the design sections as proposed in the Master Plan Study in 1996 which were considered as sufficiently large and suitable to accommodate the flood at the design return period. The dimension of the design sections are summarized as follows:

-			Pro				
River	Chaina	ge (km)	Тор		Side	Bed	River
	From	to	Width	Depth	Slope	Width	Slope
			(m)	(m)	(1/**)	(m)	(1/***)
Chane	60,00	81.90	75.0	6.0	2.0	51.0	1,212
	81.90	88.00	100.0	6.0	2.0	76.0	1,500
Pailon	36.50	51.40	65.0	5.0	2.0	45.0	995
	51.40	59.60	70.0	5.0	2.0	50.0	908
Okinawa	0.00	7.00	25.0	4.0	2.0	9.0	3,600
	7.00	25.60	28.0	4.0	2.0	12.0	3,300

Results of the calculation are shown in Table F.4.1, F.4.2, F.4.3 and F.4.4 and Figure F.4.1.

It is found that the water level decreased significantly in the design sections (with the project) from the existing sections (without the project). A summary of the water depth difference is shown below

Rio	Chainage	Water level difference (m) (WL without - WL with)					
****	(km)	2 year	5 year	10 year	20 year	50 year	
Chane	88.000	-0.44	-0.78	-0.85	-1.02	-0.74	
	86 400	-0.16	-0.48	-0.49	-0.20	-0.40	
	84,800	0.09	-0.18	-0.20	-0.20	-0.20	
	83.800	0.34	0.01	-0.09	0.16	-0.09	
	82.800	0.40	-0.02	-0.15	0.22	-0.08	
	81.900	0.38	-0.06	-0.20	-0.01	-0.13	
	81.000	0.52	0.14	0.05	0.14	0.29	
	80.000	1.29	0.53	0.43	0.47	0.42	
	78.800	1.36	0.64		0.81	0.51	
	77.700	0.87	0.17	0.03	0.22	0.08	
	76.500	0.68	-0.01	-0.15	0.03	-0.08	
	75.200	0.42	-0.08	-0.13	0.17	-0.0	
	74.300	0.29	-0.25	-0.38	0.53	-0.28	
	73,400	0.22	-0.44	-0.55	0.09	-0.47	
	72.500	0.18	-0.40	-0.52			
	71.500	0.12	-0.34	-0.42	-0.27		
	70.500	0.07	-0.41	-0.39			
	69.500	-0.05	-0.50	-0.45	-0.43	0.3	
	68.500	0.10	-0.38	-0.39	-0.24	-0.29	
	67.500	0.04	-0.41	-0.46	0.21		
	66.500	0.00	-0.48	-0.52			
	65.500	-0.05	-0.47	-0.56	0.12	-0.4	
	64.500	-0.15	-0.54	-0.53	0.20	-0.2	
	63.600	-0.27	-0.63	-0.65	-0.21	-0.4	
	62.600	-0.28	-0.60	-0.61	-0.43		
	61.600	0.13	-0.26	-0.47			
	60.800	0.27	-0.06	-0.26	0.17	-0.3	
	60.000	2.68	1.89	1.89	1.92	1.9	
A	erage	0.32	-0.16	-0.23	0.10	-0.1	

Rio	Chairman			evel differe		
K10	Chainage			thout • WI		
5.3	(km)	2 year	5 year	10 year	20 year	50 year
Pailon	59.600	2.61	1.80	1,77	1.92	1.82
	58.900	3.26	2.64	2.65	3.28	2.88
	58.200	2.85	2.53	2.45	3.11	2.62
	\$7.500	2.97	2.78	2.64	2.96	2.73
	56.800	4.52	4.28	4.16	4.63	4.19
	55.650	4.25	4.11	3.93	4.25	3.96
	54.500	3.66	3.58	3.36	3.67	3.38
į.	53.900	3.33	3.28	3.02	3.39	2.99
	53.200	3.10	2.95		3.08	2.92
į	52.500	3.15	2.96	2.83	3.30	2.85
1	51.400	2.94	2.77	2.67	2.95	2.67
1	50.300	2.90	2.71	2.63	2.85	2.59
1	49.200	2.94	2.77	2.70	2.76	2.68
1	47.800	2.00	1.85	1.72	2.19	1.69
-	46.500	2.04	1.80	1.72	2.06	1.73
	45.300	2.01	1.82	1,69	2.03	1.68
	44.200	1.64	1.44	1.39	1.63	1.49
	42.800	1.27	1.20	1.20	1.53	1.39
	41.500	1.39	1.34	1.34	1.60	1.45
	40.500	1.52	1.46	1.46	2.09	1.63
	39,500	1.38	1.36	1.45	2.04	1.74
	38.500	0.92	1.04	1.20	1.31	1.23
	37.800	1.24	1.35	1.47	1.63	0.82
l	37.100	1.61	1.69	1.80	2.19	1.44
! .	36.500	1.67	1.65	1.67	1.98	1.43
Ĺ	36.500	1.60	1.58	1.57	1.62	1.35
1	35.500	1.19	1.12	1.09	1.76	0.95
1	34.600	0.90	0.79	0.80	1.17	0.77
i	33.700	0.81	0.78	0.84	0.90	0.73
· ·	32.300	0.87	0.85	0.88	1.23	0.90
	31.300	0.71	0.72	0.79	1.34	0.92
!	30.600	0.72	0.72	0.79	1.09	0.98
	29.900	1.07	1.05	1.08	1.30	1.13
I	24.000	0.95	0.88	0.95	-17.37	1.13
l						
Aver	age	2.06	1.93	1.90	1.69	1.91

ſ	I	Water level difference (m)						
River/	Chainage		(WL without - WL with)					
Drainage	(km)	2 year	5 year	10 year		50 year		
Okinawa	26.800	0.00	0.00			0.00		
	25.600	0.09	0.05	0.06		0.02		
	24.100	0.24	0.14					
İ	23.600	0.26	0.17	0.21	0.15	0.07		
ŀ	22.400	0.85	0.88	0.89	0.90			
	20.600	0.56	0.57	0.61	0.64	0.67		
	19.100	0.90	0.83	0.83	0.85	0.88		
	18.300	1.12	1.02	1.02	1.03	1.05		
	16.600	1.11	1.00	1.00	1.00	1.00		
	15.900	1.01	0.89	0.88	0.89	0.91		
	14.000	0.82	0.73	0.73	0.75	0.79		
	13.200	0.87	0.69	0.68	0.69	0.70		
	12.000	0.93	0.64	0.68	0.65	0.66		
	10.100	1.15	0.83	0.88	0.84	0.82		
	9.300	1.14	0.82	0.87	0.82	0.81		
	8.400	1.03	0.72	0.79	0.75	0.73		
}	7.000	0.62	0.40	0.50	0.50	0.51		
	6.300	0.46	0.38	0.40	0.38	0.37		
	5.200	0.49	0.39	0.40	0.37	0.35		
	0.000	0.54	0.59	0.44	0.41	0.38		
Aver	age	0.70	0.58	0.60	0.59	0.58		

It should be noted the water level of the design cross sections (with the project) were higher than the existing sections (without the project) in some part because the design sections were set up in order to avoid the irregular flow. However, the effectiveness of the improvement with the project compared to the case without the project was considered from the decrease of the inundation depth as explained in the latter section.

(2) In the San Juan – Antofagasta Area

The Arroyo Yapacanicito, Jochi, Tacuaral, Tejeria and Antofagasta

The simulation was done for the design discharge with the return period 2, 5, 10, 20 and 50 years with the same shape but different magnitude as explained in the hydrological part. Peak runoff at each return period of the sub-basins is summarized as follows:

River	Sub-basin	Pe	eak runoff	at each sub	-basin (m³/	s)
	No.	2 years	5 years	10 years	20 years	50 years
Yapacanicito	Y1-L	143.0	194.5	228.0	260.8	302.3
	Y1-2	232.2	319.0	376.2	431.7	502.5
	Y1-3	176.8	246.4	292.4	337.2	394.7
	Y1-4	184.5	255.6	302.1	347.8	405.7
	Y2-1	120.7	166.5	196.8	226.2	263.9
	Y2-2	55.1	74.7	87.3	99.9	115.6
Jochi	J-1	109.2	151.0	178.4	205.1	239,2
	J-2	87.7	120.3	142.5	163.5	190.7
	1-3	151.3	209.1	247.2	284.3	331.7
	J-4	103.8	142.0	166.5	190.8	221.3
Tacuaral	T-1	111.9	154.2	181.8	209.0	243.5
	T-2	166.5	231.7	274.9	316.9	370.7
	Т-3	157.0	218.3	258.7	298.1	348.5
	T-4	183.5	251.8	296.1	339.7	394.9
Tejeria	-	67.2	88.1	101.5	114.4	131.1
Antofagasta	T-2	166.5	231.7	274.9	316.9	370.7

Note: 1) The sub-basin number is shown in the figure of flow model

2) Tejeria and Antofagasta have only one drainage basin each

3) Antofagasta basin is included in Tacuaral (T-2)

The time series of the runoff or the design hydrograph used in the calculation for return period 2, 5, 10, 20 and 50 years were shown in the Supporting Report B.

For Case I (without the project), the cross sections used were the existing cross section from the topographic survey conducted in this study as shown in the Data Book.

For Case II (with the project), the cross sections were the design sections as proposed in the Master Plan Study in 1996 which were considered as sufficiently large and suitable to accommodate the flood at the design return period. The dimension of the design sections are summarized as follows:

			Pro	posed c	ross sec	tion	
River	Chainag	e (km)	Тор		Side	Bed	River
	From	to .	Width	Depth	Slope	Width	Slope
.			(m)	(m)	(1/)	(m)	(1/***)
Yapacanicito	14.30	28.10	30.0	3.0	2.0	18.0	1,280
	28.10	31.70	35.0	3.0	2.0	23.0	1,280
Jochi	13.80	16.00	22.0	- 3.5	2,0	8.0	900
	16.00	25.60	30.0	3.5	2.0	16.0	900
Tacuaral	16.80	22.60	26.0	4.0	2.0	10.0	900
Tejeria	0.00	2.98	20.0	4.0	2.0	4.0	900
	2.98	8.16	22.0	4.0	2.0	6.0	900
Antofagasta	0.00	8.79	28.0	4.0	2.0	12.0	900

Results of the calculation are shown in Table F.4.5, F.4.6, F.4.7 and F.4.8 and Figure F.4.2.

It is found that the water level decreased significantly from the condition of "without the project" to "with the project" as shown below:

		Water level difference (m)					
Arroyo	Chainage		(WL wi	thout - W	/L with)	, 	
	(km)	2 year	5 year	10 year	20 year	50 year	
Yapacanicito	14.300	0.30	0.33	0.34	0.35	0.36	
	14.320	0.33	0.33	0.28	0.27	0.27	
	15.400	1.19	1.18	1.16	1.15	1.14	
	16.400	0.81	0.76	0.75	0.79	0.89	
	17.100	0.16	0.14	0.09	0.07	0.04	
·	19.000	-0.05	-0.07	-0.21	-0.40	-0.45	
	20.000	-0.04	-0.07	-0.19	-0.33	-0.41	
	20.400	-0.17	-0.23	-0.25	-0.26	-0.27	
	22.200	0.67	0.60	0.51	0.50	0.36	
	23,100	0.19	0.13	0.13	0.12	0.06	
	24.100	0.14	0.13	0.09	0.10	0.08	
	25.300	0.19	0.14	0.11	0.10	0.09	
	26.200	0.18	0.15	0.12	0.12	0.10	
	27,000	0.19	0.16	0.14	0.13	0.12	
	28.100	0.18	0.15	0.13	0.12	0.11	
	29.100	0.18	0.14	0.12	0.11	0.10	
	30.100	0.19	0.15	0.12	0.12	0.11	
1	31.100	0.19	0.15	0.13			
	31.700	0.19	0.15	0.13	0.12	0.11	
	Average	0.26	0.23	0.19	0.17		

It should be noted herein that some cross sections in the middle part of the Rio Yapacanicito had water level in the design sections higher than the existing sections because those existing sections were pretty low and therefore were designed to have higher elevation to avoid irregular flow. As a result, the water level in design section was higher than the existing section.

		Water level difference (m)						
Arroyo	Chainage		(WL wi	thout - W	L with)			
=	(km)	2 year	5 year	10 year	20 year	50 year		
Jochi	13.800	1.28	1.24	1.22	1.19	1.15		
	15.000	0.40	0.35	0.33	0.29	1.39		
	15.010	0.39	0.60	0.52	0.46	0.27		
	15.020	0.42	0.37	0.34	0.31	0.68		
	16.000	1.16	1.17	1.16	1.15	1.11		
	17.200	1.56	1.61	1.61	1.61	1.59		
	18.300	1.53	1.57	1.59	1.60	1.57		
	19.000	1.51	1.55	1.57	1.57	1.55		
·	20.000	1.28	1.33	1.36	1.37	1.34		
	20.900	1.32	1.38	1.41	1.42	1.40		
	21.900	1.34	1.37	1.39	1.40	1.37		
	22.700	1.55	1.57	1.58	1.58	1.56		
	22.710	1.48	1.60	1.67	1.91	1.86		
	22.720	1.51	1.54	1.55	1.56	1.54		
	23.700	1.67	1.72	1.75	1.77	1.77		
	24.900	1.90	1.54	1.43	1.41	1.40		
1	25.600	0.29	0.43	0.31	0.27	0.16		
	Average	1.21	1.23	1.22	1.23	1.28		

Arroyo	Chainage	Water level difference (m) (WL without - WL with)					
	(km)	2 year	5 year	10 year		50 year	
Tacuaral	16.800	0.65	0.38	0.33	0.34	0.18	
	16.810	0.65	0.37	0.33	0.34	0.18	
	16.820	0.65	0.38	0.33	0.34	0.18	
	17.600	0.65	0.37	0.33	0.34	0.18	
	18.500	0.65	0.38	0.33	0.34	0.18	
	19.100	0.65	0.36	0.32	0.34	0.18	
	19.110	0.66	0.40	0.35	0.34	0.18	
	19.120	0.65	0.33	0.29	0.34	0.18	
	20.000	0.67	0.46	0.41	0.34	0.18	
	21.200	0.62	0.20	0.17	0.34	0.19	
	22.100	0.71	0.73	0.65	0.35	0.17	
	22.600	0.54	0.61	0.59	0.33	0.20	
	Average	0.65	0.41	0.37	0.34	0.18	

Arroyo	Chainage	Water level difference (m) (WL without - WL with)				
	(km)	2 year	5 year	10 year	20 year	50 year
Tejeria	0.000	1.68	1.52	1.38	1.31	1.23
	1.010	0.95	0.82	0.60	0.47	0.47
	2.225	0.68	0.72	0.46	0.37	0,40
	2.975	0.54	0.52	0.44	0.41	0.37
ł	3.677	1.21	1.05	0.86	0.82	0.69
	4.860	1.10	0.97	0.85	0.86	0.59
	5.706	1.04	1.01	1.05	1.12	0.83
	6.879	0.92	0.83	0.73	0.65	0.60
	7.579	1,06	1.10	0.93	0.74	0.60
	8.160	1.60	1.60	1.60	1.60	1.60
	Average	1.08	1.01	0.89	0.83	0.74

Аггоуо	Chainage	Water level difference (m) (WL without - WL with)					
	(km)	2 year	5 year	10 year	20 year	50 year	
Antofagasta	0.000	1.26	1.04	0.99	0.99	1.04	
	1.040	1.10	0.90	0.85	0.83	0.87	
	1.920	1.17	0.96	0.91	0.89	0.93	
	2.550	1.19	1.00	0.96	0.95	0.96	
	3.490	0.67	0.56	0.58	0.62	0.68	
	4.300	1.07	0.93	0.92	0.93	0.96	
	5.240	0.80	0.78	0.81	0.84	0.89	
	6.560	0.46	0.35	0.38	0.42	0.49	
	7.640	1.21	0.93	0.91	0.94	0.99	
	8.250	1.70	1.35	1.30	1.32	1.36	
	8.800	0.85	0.56	0.49	0.50	0.53	
	10.600	0.00	0.00	0.00	0.00	0.00	
	Average	0.96	0.78	0.76	0.77	0.81	

The inundation depth was explained in the latter section. These results were also used afterwards for the flood mitigation measures.

The San Juan Drainage

The San Juan Drainage was not included in the hydrodynamic simulation due to its small size and low discharge. The flow condition during flood period was also considered as uniform rather than unsteady. Therefore, design discharge for the return period 2, 5, 10, 20 and 50 years were calculated from the Rational Formula and the flood condition was calculated from the uniform flow equation or Manning's Equation. Peak discharges at each return period in the drainage from the Rational Formula are as follow:

Drainage	Section	Peak discharge (m³/s)					
	No.	2 years	5 years	10 years	20 years	50 years	
San Juan	km 09.00	14.92	19.94	23.18	26.27	30.26	
	km 11.00	24.86	33.24	38.63	43.78	50.44	
	km 13.00	41.97	55.65	64.45	72.90	83.78	
	km 15.00	37.76	49.74	57.46	64.86	74.43	
	km 17.00	31.80	41.89	48.39	54.62	62.68	
	km 24.00	13.28	18.20	21.37	24.40	28.32	
	km 28.00	48.77	63.92	73.67	83.04	95.14	

The design cross sections were same as proposed in the Master Plan Study in 1996. The dimension of the design sections are summarized as follows:

	Pro	Proposed cross section				
San Juan	Top		Side	Bed	River	
Drainage	Width	Depth	Slope	Width	Slope	
	(m)	(m)	(1/**)	_(m)_	(1/***)	
km 09.00	11.0	3.0	1.0	11.0	1,500	
km 11.00	11.0	3.0	1.0	11.0	1,500	
km 13.00	11.0	3.0	1.0	11.0	1,500	
km 15.00	11.0	3.0	1.0	11.0	1,500	
km 17.00	11.0	3.0	1.0	11.0	1,500	
km 24.00	11.0	3.0	1.0	11.0	1,500	
km 28.00	11.0	3.0	1.0	11.0	1,500	

This design section was used for the whole San Juan Drainage as shown in the Data Book.

TABLES

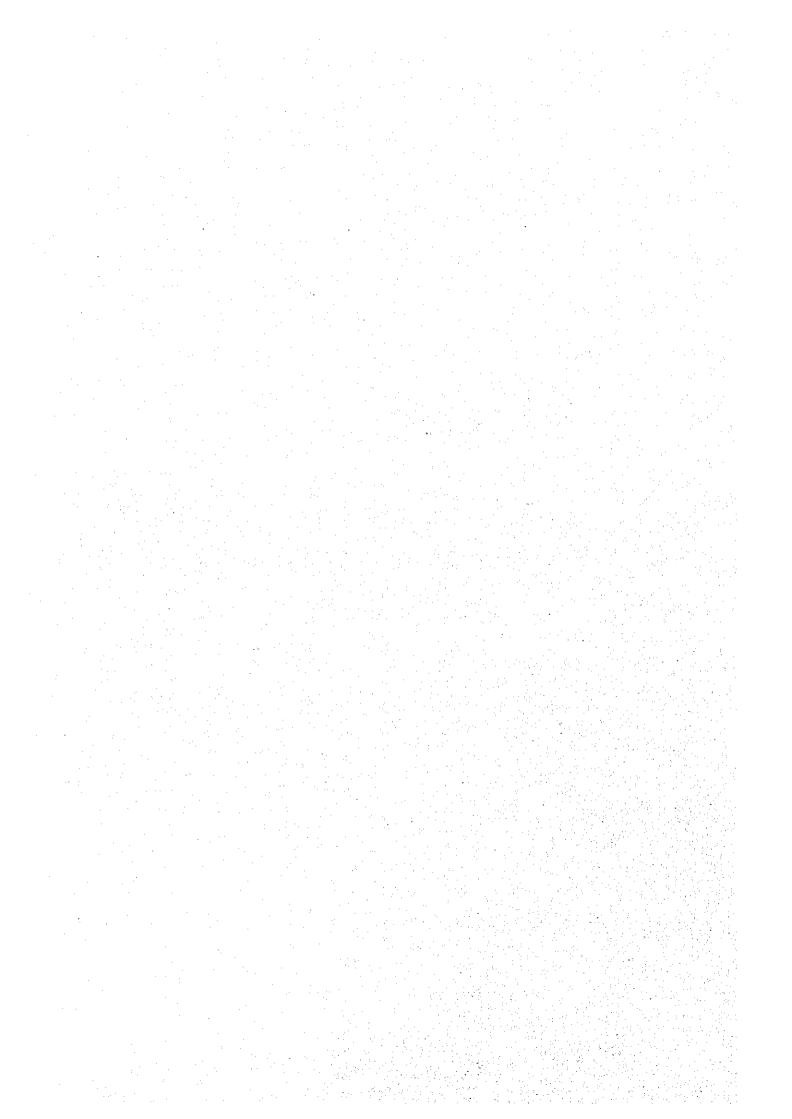


TABLE F.2.1 COORDINATES AND CHAINAGES IN THE HD MODEL IN THE RIO CHANE BASIN

River	Coordinate		Chainage
	X	Y	(m)
Rio	100,600	65,500	0
Chane	102,700	68,300	4,000
	105,200	71,000	8,000
	106,200	72,500	10,500
	107,500	75,400	14,000
	108,400	79,600	18,000
	109,700	82,800	22,000
	109,800	85,800	25,000
	109,700	89,500	28,500
	107,600	91,600	31,800
	107,600	93,300	33,700
	107,100	95,100	36,400
	107,000	95,200	36,500
	106,900	95,300	36,600
	105,200	97,000	38,500
٠	103,200	98,800	41,500
	102,500	101,000	44,200
	102,500	103,500	46,500
	100,300	104,500	49,200
	97,900	106,600	52,500
	97,600	108,700	54,500
	95,800	109,100	56,800
	93,700	108,900	59,600
	93,500	109,200	60,000
	92,300	110,900	62,100
	92,000	112,000	63,500
	92,000	112,200	63,600
	91,900	112,250	63,700
	88,800	113,700	67,500
	87,500	115,000	69,400
		117,500	
		118,800	
	83,000	119,000	77,700
	\$	120,500	·
	1	120,600	
	81,400	120,700	
		122,300	
		124,300	
	l	124,500	
		124,500	
	1	124,000	S
ŀ		125,500	
<u> </u>	69,000	126,000	95,000

River		linate	Chainage
	X	Y	(m)
QDA	90,500	77,500	0
Chane	89,800	81,500	4,500
	92,000	84,000	8,200
	93,300	86,500	11,000
, i	93,700	87,400	12,000
	93,600	89,300	13,600
	93,800	91,700	16,100
	93,800	91,800	16,200
	93,800	91,900	16,300
	93,800	94,400	18,800
	94,000	96,500	20,900
	94,300	98,000	23,300
	94,200	101,300	25,800
	93,400	103,800	28,200
	93,200	106,200	30,800
	93,500	109,100	34,000
Rio	121,000	68,000	0
Pailon	119,700	70,200	2,000
	118,000	74,000	6,000
	116,200	77,200	10,000
	115,400	79,900	12,600
	115,400	80,000	12,700
	115,400	80,100	12,800
	115,000	81,800	14,500
	114,200	83,400	16,400
	114,100	83,500	16,500
	114,000	83,600	16,600
	112,900	86,400	19,400
	111,400	86,400	21,200
	111,300	86,500	21,300
	111,200	86,600	21,400
	109,800	89,000	24,000
QDA	119,000	67,000	0
Meco	121,000	68,000	2,000
	121,000	67,300	2,200
Rio	107,700		
Chico	106,400		
п	106,300	95,200	2,000
	106,300		*
l	106,500	<u> </u>	

River	Coord	linate	Chainage
	X	Y	(m)
QDA	90,300	90,300	0
Toro	90,200	90,700	400
	90,200	90,900	500
	90,300	91,000	600
	90,500	94,300	3,400
	91,000	95,000	4,600
	91,200	96,800	6,200
	92,200	99,400	9,200
	92,400	101,400	11,200
	92,700	105,500	16,000
QDA	86,500	89,500	0
Maras	86,500	89,800	400
	86,600	90,000	500
	86,500	90,000	700
	88,500	93,300	3,800
	89,000	93,800	5,000
	89,800	94,300	6,000
	91,000	95,100	7,300
QDA	84,400	89,300	0
Chacras	84,500	89,500	400
	84,700	90,000	500
	84,800	90,000	700
	83,000	92,300	3,500
	79,800	97,000	10,000
	80,200	99,400	12,500
	78,500	102,500	16,000
	78,800	105,500	19,000
	79,200	107,900	21,500
	80,000	110,000	23,700
	80,200	113,500	27,500
	81,500	116,000	30,500
	79,800	117,500	33,000
	79,800	121,300	36,500

TABLE F.2.2 SUB-BASINS IN THE RIO CHANE BASIN

River	Basin	Area	Chainage (km)	
	No.	(km²)	Upstream	Downstream
Rio Chane	A-1	63.35	82.5	95.0
Rio Chane	A-2	198.68	60.0	82.5
Rio Chane	A-3	164.70	37.0	60.0
Rio Chane	A-4	60.10	32.0	37.0
Rio Chane	A-5	15.80	28.0	32.0
Rio Pailon	A-6	211.87	0.0	24.0
Rio Chane	A-7	112.68	0.0	28.0
Rio Chane	A-8	270.00	0.0	0.0
Rio Chane	A-9	141.89	0.0	0.0
Rio Chane	A-10	66.14	24.0	28.0
Rio Chane	A-11	275.46	28.0	31.8
QDA Chacras	B-1	6.72	34.5	36.5
QDA Chacras	B-2	153.49	0.5	34.5
QDA Chacras	B-3	64.04	0.0	
QDA Chane	C-1	3.18	18.0	22.0
QDA Chane	C-2	35.03	4.2	18.0
QDA Chane	C-3	88.83	0.0	16.2
QDA Toro	C-4	38.77	4.0	16.0
QDA Toro	C-5	11.36	0.5	4.0
QDA Toro	C-6	121.16	0.0	0.0
QDA Maras	C-7	23.93	0.5	7.3
QDA Maras	C-8	38.43	0.0	0.0
QDA Meco	D-1	244.82	0.0	2.1
QDA Chane	C-9	108.57	0.0	0.0
Total		2,519.00		

TABLE F.2.3 CONNECTING POINTS OF SUB-BASINS TO THE RIO CHANE NETWORK

			Chainage of river
Sub-basin		Connected	at Connecting Points
1		River	(m) [*]
	A-8	Rio Chane	0
2	A-9	Rio Chane	0
3	A-7	Rio Chane	28,000
4	A-10	Rio Chane	28,000
5	A-11	Rio Chane	31,800
6	A-5	Rio Chane	32,000
7	A-4	Rio Chane	37,000
8	A-3	Rio Chane	60,000
9	A-2	Rio Chane	82,500
10	A-1	Rio Chane	95,000
[11]	C-9	QDA Chane	Ō
12	C-3	QDA Chane	16,200
13	C-2	QDA Chane	18,000
14	C-1	QDA Chane	22,000
15	A-6	Rio Pailon	24,000
16	D-1	QDA Meco	21,000
17	C-6	QDA Toro	0
18	C-5	QDA Toro	4,000
19	C-4	QDA Toro	16,000
20	C-8	QDA Maras	0
21	C-7	QDA Maras	7,306
22	B-3	QDA Chacras	400
23	B-2	QDA Chacras	34,500
24	B-1	QDA Chacras	36,500

TABLE F.2.4 COORDINATES, CHAINAGES, SUB-BASINS AND CONNECTING POINTS IN THE HD MODEL IN THE OKINAWA DRAINAGE BASIN

River	Coord	Chainage	
	X	Y	(m)
Okinawa	0.0	0.0	0
Drainage	0.0	7.0	7,000
1 1	0.0	25.0	25,000
	0.0	28.0	28,000

River	Basin	Area	Chaina	ge (km)	
	No.	(km²)	Upstream	Downstream	
Okinawa	E-1	70.0	7.0	25.0	
Drainage	E-2	75.9	1.0	7.0	
	E-3	235.6	0,0	1.0	
Total		381.5			

Sub-basin	Connected River	Chainage of river at Connecting Points (m)
E-1	Okinawa	25,000
E-2	Drainage	7,000
E-3		1,000

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TABLE E2.5 COORDINATES AND CHAINAGES IN THE HD MODEL IN THE RIO YAPACANI BASIN

River	Coord	Chainage	
	XY		(m)
Arroyo	113.0	87.0	0
Jochi	113.0	90.0	3,000
	112.0	92.5	6,000
	109.5	94.0	9,520
	108.5	97.0	12,800
	109.0	100.0	15,360
	112.0	102.0	18,600
	112.5	104.0	21,000
	112.5	105.9	22,700
	112.5	106.0	22,800
	112.5	106.1	22,900
	113.5	108.0	25,600
	115.5	311.4	29,700
	115.5	111.4	29,800
	115.5	116.5	35,800
	113.0	121.0	43,400
Arroyo	116.0	88.0	0
Tacuaral	114.0	91.0	3,000
	113.0	94.0	6,000
	113.0	96.0	9,000
	115.0	99.0	12,000
	115.0	102.0	16,400
	115.0	104.0	18,240
	115.0	104.1	18,340
	115.0	104.2	18,440
	115.0	104.0	20,700
	115.0	105.1	20,800
	115.0	105.2	20,900
	114.2	106.0	22,600
	116.5	110.9	27,500
	116.5	111.0	27,600
]	118.5	114.0	32,100
	120.5	118,0	37,900
Апоуо	115.5	111.4	0
Jochi-Tacu	116.5	111.4	1,000

River	Coorc	Chainage	
	X	Y	(m)
Arroyo	110.5	86.0	0
Yapacanicito	110.0	87.2	1,500
	109.2	89.0	3,600
	108.0	91.2	6,100
	106.5	93.0	8,600
	107.0	96.3	12,200
	107.5	98.5	14,300
	108.0	100.5	16,800
	107.3	102.0	18,000
	107.5	105.0	21,000
	108.2	107.0	23,500
	104.5	108.5	27,100
	106.5	110.0	29,900
	105.0	115.0	34,900
	101.5	116.0	39,900
	99.0	119.0	44,900
	95.0	120.0	49,900
	94.0	118.5	51,300
	92.0	121.5	56,300
	88.0	125.0	62,300
San Juan	106.5	93.0	0
- DM1	103.0	93.0	2,400
	104.0	93.0	2,500
R/W	115.5	111.4	0
Embank	115.6	111.4	100
	102.1	117.0	10,900
	102.0	117.0	11,000
TMP-R/W	115.0	110.0	0
	115.4	111.4	100

TABLE F.2.6 SUB-BASINS IN THE RIO YAPACANI BASIN

River/Arroyo	Basin	Area	Chainage (m)		Chainage of River (m)
	No.	(km²)	Upstream	Downstream	at Connecting Points
Jochi	J-1	41.60	29,800	34,200	29,800
Jochi	J-2	11.80	25,600	29,800	25,600
Jochi	J-3	76.30	0	25,600	0
Jochi	J-4	18.30	0	Ö	0
Tacuaral	T-1	38.20	27,600	37,900	27,600
Tacuaral	T-2	88.20	27,600	27,600	27,600
Tacuaral	T-3	77.00	0	27,500	. 0
Tacuaral	T-4	49.40	0	0	0
Yapacanicito	Y1-1	66.80	51,300	62,300	51,300
Yapacanicito	Y1-2	98.40	29,900	51,300	29,900
Yapacanicito	Y1-3	95.90	8,600	29,900	8,600
Yapacanicito	Y1-4	34.90	0	8,600	0
Yapacanicito	Y2-1	62.80	51,300	51,300	51,300
Yapacanicito	Y2-2	11.90	51,300	51,300	51,300
Total		759.60			

TABLE F.3.1(1) MAXIMUM WATER LEVELS IN THE RIO CHANE-PAILON BASIN

River/Chainage	Maximum Water Level		
	(m)	Time	
RIO CHANE 0.000	314.39	1997/12/04 10:28	
RIO CHANE 1,000	313.66	1997/12/04 09:52	
RIO CHANE 2.000	312.83	1997/12/04 10:09	
RIO CHANE 3.000	312.00	1997/12/04 10:20	
RIO CHANE 4.000	310.82	1997/12/04 10:18	
RIO CHANE 5.000	309.06	1997/12/04 10:20	
RIO CHANE 6,000	307.34	1997/12/04 10:24	
RIO CHANE 7.000	305.51	1997/12/04 10:24	
RIO CHANE 8.000	304.01	1997/12/04 10:28	
RIO CHANE 8.833	302.99	1997/12/04 10:31	
RIO CHANE 9.667	302.04	1997/12/04 10:35	
RIO CHANE 10.500	300.66	1997/12/04 08:54	
RIO CHANE 11.375	298.26	1997/12/04 08:26	
RIO CHANE 12.250	295.88	1997/12/04 07:48	
RIO CHANE 13.125	293.45	1997/12/04 07:39	
RIO CHANE 14.000	291.04	1997/12/04 07:33	
RIO CHANE 15,000	288.50	1997/12/04 07:26	
RIO CHANE 16.000	285.97	1997/12/04 06:58	
RIO CHANE 17.000	283.45	1997/12/04 07:01	
RIO CHANE 18,000	280.94	1997/12/04 07:05	
RIO CHANE 19.000	278.43	1997/12/04 07:07	
RIO CHANE 20.000	275.93	1997/12/04 07:11	
RIO CHANE 21.000	273.42	1997/12/01 02:09	
RIO CHANE 22.000	270.96	1997/12/04 05:41	
RIO CHANE 23,000	268.43	1997/12/04 11:18	
RIO CHANE 24.000	266.36	1997/12/04 10:39	
RIO CHANE 25.000	263.89	1997/12/04 18:46	
RIO CHANE 25.875	262.46	1997/12/04 18:11	
RIO CHANE 26.750	261.08	1997/12/04 19:20	
RIO CHANE 27.625	259.72	1997/12/04 17:26	
RIO CHANE 28.500	258.34	1997/12/04 22:41	
RIO CHANE 28.500	258.34	1997/12/04 22:41	
RIO CHANE 29.325	257.50		
RIO CHANE 30.150	256.88		
RIO CHANE 30.975	256.24	1997/12/05 01:20	
RIO CHANE 31.800	255.15	1997/12/05 01:37	
RIO CHANE 32.750	254.59	1997/12/05 02:54	
RIO CHANE 33.700	253.97	1997/12/05 03:07	
RIO CHANE 33.700	253.97	1997/12/05 03:07	
RIO CHANE 34.600	253.91	1997/12/05 03:03	
RIO CHANE 35.500	253.83	1997/12/05 02:52	
RIO CHANE 36.400	253.67	1997/12/04 10:41	
RIO CHANE 36.500	253.72	1997/12/04 10:37	
RIO CHANE 36.600	253.77	1997/12/04 10:35	
RIO CHANE 37.550	252.14	1997/12/04 12:35	

River/Chainage	Maximum Water Level			
terron on annago	(m)	Time		
RIO CHANE 38.500	251.83	1997/12/05 05:03		
RIO CHANE 38.500	251.83	1997/12/05 05:03		
RIO CHANE 39.500	251.38			
RIO CHANE 40.500	250.91			
RIO CHANE 41,500	250.38			
RIO CHANE 42.400	250.15			
RIO CHANE 43,300				
RIO CHANE 44.200	249.96			
RIO CHANE 44.200	249.68			
	249.36			
RIO CHANE 45.733	249.16			
RIO CHANE 46.500	248.93			
RIO CHANE 47.400	248.41	1997/12/06 06:06		
RIO CHANE 48.300	247.92	1997/12/06 06:59		
RIO CHANE 49.200	247.45	1997/12/06 08:03		
RIO CHANE 50.025	247.05	1997/12/06 09:00		
RIO CHANE 50.850	246.70	1997/12/06 10:07		
RIO CHANE 51.675	246.36	1997/12/06 12:08		
RIO CHANE 52.500	245.97	1997/12/06 17:49		
RIO CHANE 53.500	245.46	1997/12/06 19:06		
RIO CHANE 54.500	244.75	1997/12/07 00:00		
RIO CHANE 55.267	243.88	1997/12/07 00:00		
RIO CHANB 56.033	242.98	1997/12/07 00:00		
RIO CHANE 56.800	242.52	1997/12/07 00:00		
RIO CHANE 57.733	242.14	1997/12/07 00:00		
RIO CHANE 58.667	241.80	1997/12/07. 00:00		
RIO CHANE 59.600	241.47	1997/12/01 17:17		
RIO CHANE 60.000	241.46	1997/12/01 17:11		
RIO CHANE 60.000	241.46	1997/12/01 17:11		
RIO CHANE 60.700	241.02	1997/12/01 18:06		
RIO CHANE 61.400	240.54	1997/12/01 18:49		
RIO CHANE 62,100	239.75	1997/12/01 19:31		
RIO CHANE 62.800	239.13	1997/12/01 20:13		
RIO CHANE 63,500	238.68	1997/12/01 20:48		
RIO CHANE 63,600	238.42	1997/12/01 20:58		
RIO CHANE 63.700	238.59	1997/12/01 20:56		
RIO CHANE 64.650	237.88	1997/12/01 22:45		
RIO CHANE 65.600	237.46	1997/12/01 23:58		
RIO CHANE 66.550	237.18	1997/12/02 01:00		
RIO CHANE 67.500	236.94	1997/12/02 01:53		
RIO CHANE 68.450	236.67	1997/12/02 02:35		
RIO CHANE 69.400	236.19	1997/12/02 03:36		
RIO CHANE 70.267	235.48	1997/12/02 04:20		
RIO CHANE 71.133	234.92	1997/12/02 05:01		
RIO CHANE 72.000	234.42	1997/12/02 05:36		
RIO CHANE 72.800	233.97	1997/12/02 06:15		

TABLE E3.1(2) MAXIMUM WATER LEVELS IN THE RIO CHANE-PAILON BASIN

River/Chainage	Maximum Water Level				
	(m)	Time			
RIO CHANE 73.600	233.53	1997/12/02 06:54			
RIO CHANE 74,400	233.09	1997/12/02 07:40			
RIO CHANE 75.200		1997/12/02 08:31			
RIO CHANE 76.033	232.24	1997/12/02 09:26			
RIO CHANE 76.867	231.88	1997/12/02 10:16			
RIO CHANE 77.700	231.60	1997/12/02 10:50			
RIO CHANE 78.433	231.36	1997/12/02 11:14			
RIO CHANE 79.167	231.09	1997/12/02 11:35			
RIO CHANE 79.900	230.71				
RIO CHANE 80.000	230.56	1997/12/02 12:13			
RIO CHANE 80.100	230.51				
RIO CHANE 81.040	229.77	1997/12/02 13:04			
RIO CHANE 81.980	229.15	agents a contract of the company of the contract of the contra			
RIO CHANE 82.920	228.70				
RIO CHANE 83.860	228.42				
RIO CHANE 84,800	228.37	1997/12/01 20:35			
RIO CHANB 84.800		1997/12/01 20:35			
RIO CHANE 85.575	228.26				
RIO CHANE 86.350		1997/12/01 21:11			
RIO CHANE 87.125		1997/12/01 21:45			
RIO CHANE 87.900		1997/12/01 22:24			
RIO CHANE 88.000	227.80	1997/12/01 22:33			
RIO CHANE 88.100	227.84				
RIO CHANE 88.900	227.37				
RIO CHANE 89,700		1997/12/01 23:21			
RIO CHANE 90.500	227.13				
RIO CHANE 91.333	227.11				
RIO CHANE 92,167	227.09				
RIO CHANE 93.000	227.07	· — · · · · · · · · · · · · · · · · · ·			
RIO CHANE 94,000	227.04				
RIO CHANE 95.000	227.00				
QDA CHANE 0.000	290.48				
QDA CHANE 0.900	289.48				
QDA CHANE 1.800	288.47				
QDA CHANE 2.700	287.46	·			
QDA CHANE 3.600	286.38				
QDA CHANE 4.500	285.57				
QDA CHANE 5.425	284.30				
QDA CHANE 6.350	283.02				
QDA CHANE 7.275	281.82				
QDA CHANE 8.200	280.41				
QDA CHANE 9.133	278.73	}			
QDA CHANE 10.067	277.12				
QDA CHANS 11.000	275.27				
QDA CHANE 12.000	272.48				
QDA CHANE 12.800	270.55				
QDA CHANE 13.600	268.82				
QDA CHANE 14.433	267.57	[
QDA CHANE 15.267 QDA CHANE 16.100	266.42 264.95	I			
QDA CHANE 16.200	264.69				
ZD11 CHINTO 10.000	1 204.09	1 22 m x 201 23.10			

River/Chainage	Maximum Water Level			
	(m) Time			
QDA CHANB 16.300	264.58	1997/12/01 22:47		
QDA CHANE 17.133	262.95	1997/12/01 23:14		
QDA CHANB 17.967	261.30	1997/12/01 23:57		
QDA CHANE 18.800	259.67	1997/12/01 23:50		
QDA CHANB 19.500	258.66	1997/12/01 23:59		
QDA CHANE 20.200	257.39	1997/12/01 23:58		
QDA CHANE 20.900	256.60	1997/12/02 00:30		
QDA CHANE 21.700	255.67	1997/12/02 02:20		
QDA CHANE 22.500	254.61	1997/12/02 03:44		
QDA CHANE 23.300	253.17	1997/12/02 03:45		
QDA CHANE 24.133	251.72	1997/12/02 05:15		
QDA CHANE 24.967	250.54	1997/12/02 06:39		
QDA CHANE 25.800	249.98	1997/12/02 06:48		
QDA CHANE 26.600	248.42	1997/12/02 07:49		
QDA CHANE 27.400	247.15			
QDA CHANE 28.200	245.76			
QDA CHANE 29.067	243.74	1997/12/02 07:54		
QDA CHANE 29.933	243.59	1997/12/01 13:30		
QDA CHANE 30.800	243.59	1997/12/01 13:25		
QDA CHANE 30.800	243.59	1997/12/01 13:25		
QDA CHANE 31,600	242.85	1997/12/01 14:40		
QDA CHANE 32.400	242.17	1997/12/01 15:09		
QDA CHANE 33.200	241.68	1997/12/01 15:48		
QDA CHANE 34.000	241.46	1997/12/01 17:11		
RIO PAILON 0.000	276.41	1997/12/04 16:28		
RIO PAILON 1.000	276.32	1997/12/04 17:31		
RIO PAILON 2.000 RIO PAILON 3.000	276.21	1997/12/04 18:48		
RIO PAILON 4.000	276.10 275.97	1997/12/04 20:07 1997/12/04 21:58		
RIO PAILON 5.000	275.81	1997/12/05 07:11		
RIO PAILON 6.000	275.68	1997/12/05 21:49		
RIO PAILON 7,000	275.56	1997/12/05 23:18		
RIO PAILON 8.000	275.42	1997/12/06 00:45		
RIO PAILON 9.000	275.24	1997/12/06 02:42		
RIO PAILON 10.000	274.81	1997/12/06 06:33		
RIO PAILON 10.867	273.59			
RIO PAILON 11.733	272.21			
RIO PAILON 12.600	271.00			
RIO PAILON 12.700	270.88			
RIO PAILON 12.800	270.70			
RIO PAILON 13.650	268.96			
RIO PAILON 14.500	267.43	·		
RIO PAILON 15.450	267.01			
RIO PAILON 16.400	266.54	1997/12/06 17:18		
RIO PAILON 16.500	266.45	1997/12/06 17:03		
RIO PAILON 16.600	266.28	1997/12/06 17:07		
RIO PAILON 17.533	264.09	1997/12/06 18:04		
RIO PAILON 18.467	262.73			
RIO PAILON 19.400	262.07	1997/12/06 21:56		
RIO PAILON 20.300	261.33	1997/12/06 23:48		
RIO PAILON 21.200	260.49	1997/12/07 00:00		

TABLE F.3.1(3) MAXIMUM WATER LEVELS IN THE RIO CHANE-PAILON BASIN

River/Chainage	Maximum Water Level				
	(m)	Time			
RIO PAILON 21.300	260.36	1997/12/07 00:00			
RIO PAILON 21.400	260.11	1997/12/07 00:00			
RIO PAILON 22:267	258,44	1997/12/04 23:39			
RIO PAILON 23.133	258.37	1997/12/04 23:00			
RIO PAILON 24.000	258.34	1997/12/04 22:41			
QDA MECO 0.000	276.62	1997/12/06 03:34			
QDA MEÇO 1.000	276.42	1997/12/04 16:22			
QDA MECO 2.000	276.41	1997/12/04 16:28			
QDA MECO 2.000	276.41	1997/12/04 16:28			
QDA MECO 2.200	277.00	1997/11/30 00:01			
R. CHICO II 0.000	253.97	1997/12/05 03:07			
R. CHICO II 0.950	252.84	1997/12/05 04:52			
R. CHICO II 1.900	252.82	1997/12/05 04:56			
R. CHICO II 2.000	252.82	1997/12/05 04:52			
R. CHICO II 2.200	252.00	1997/12/05 05:18			
R. CHICO II 3.000	251.83	1997/12/05 05:03			
QDA TORO 0.000	267.44	1997/12/01 04:00			
QDA TORO 0.400	267.13	1997/12/01 04:06			
QDA TORO 0.500	266.87	1997/12/01 04:07			
QDA TORO 0.600	266.36	1997/12/01 03:52			
QDA TORO 1.533	264.50	1997/12/01 04:28			
QDA TORO 2.467	263.19	1997/12/01 04:54			
QDA TORO 3.400	261.05	1997/12/01 05:17			
QDA TORO 4.000	258.89	1997/12/01 01:31			
QDA TORO 4.600	257.04	1997/12/01 00:09			
QDA TORO 4.600	257.04	1997/12/01 00:09			
QDA TORO 5.400	253.83	1997/12/01 00:30			
QDA TORO 6.200	251.14	1997/12/01 01:22			
QDA TORO 7.200	249.53	1997/12/01 02:27			
QDA TORO 8.200	249.00				
QDA TORO 9.200	248.69				
QDA TORO 10.200	248.50				
QDA TORO 11.200	248.34	1997/12/01 09:57			
QDA TORO 12.160	247.50	l			
QDA TORO 13.120	246.67				
QDA TORO 14.080	245.83				
QDA TORO 15.040	244.77	1997/12/01 12:51			
QDA TORO 16.000	243.59	1997/12/01 13:25			
QDA MARAS 0.000	272.85	1997/12/01 00:05			
QDA MARAS 0.500	272.54	1997/11/30 23:17			
QDA MARAS 0.700	272.09	1997/11/30 23:37			
QDA MARAS 1.475	270.38	1997/11/30 23:45			
QDA MARAS 2.250	268.92	1997/11/30 23:37			
QDA MARAS 3.025	267.60	1997/12/01 00:05			
QDA MARAS 3.800	266.19	1997/12/01 00:00			
QDA MARAS 4.400	264.57	1997/12/01 00:19			
QDA MARAS 5,000	263.04	1997/11/30 22:58			
QDA MARAS 6.000	259.77	1997/11/30 22:57			
QDA MARAS 6.650	257.40	1997/12/01 00:15			
QDA MARAS 7.300	257.04	1997/12/01 00:09			

River/Chainage	Maximum Water Leve				
	(m)	Time			
QDA CHACRAS 0.000	276.78	1997/12/01 01:27			
QDA CHACRAS 0.400	276.31	1997/12/01 04:25			
QDA CHACRAS 0.500	276.26	1997/12/01 04:37			
QDA CHACRAS 0.700	275.73	1997/12/01 04:37			
QDA CHACRAS 1.633	273.47	1997/12/01 04:50			
QDA CHACRAS 2.567	272.09	1997/12/01 05:00			
QDA CHACRAS 3.500	270.90	1997/12/01 05:35			
QDA CHACRAS 4.429	269.72	1997/12/01 05:50			
QDA CHACRAS 5.357	268.53	1997/12/01 06:13			
QDA CHACRAS 6.286	267.33	1997/12/01 06:32			
QDA CHACRAS 7.214	266.14	1997/12/01 06:58			
QDA CHACRAS 8.143	264.98	1997/12/01 07:24			
QDA CHACRAS 9.071	263.85	1997/12/01 07:52			
QDA CHACRAS 10.000	262.77	1997/12/01 08:12			
QDA CHACRAS 10.833	261.79	1997/12/01 08:39			
QDA CHACRAS 11.667	261.26	1997/12/01 08:47			
QDA CHACRAS 12.500	260.91	1997/12/01 08:47			
QDA CHACRAS 13.375	259.74	1997/12/01 08:59			
QDA CHACRAS 14.250	258.58	1997/12/01 09:17			
QDA CHACRAS 15.125	257.45	1997/12/01 09:43			
QDA CHACRAS 16.000	256.17	1997/12/01 10:13			
QDA CHACRAS 17.000	254.34	1997/12/01 10:40			
QDA CHACRAS 18.000	252,64	1997/12/01 10:55			
QDA CHACRAS 19,000	250.52	1997/12/01 10:54			
QDA CHACRAS 19.833	248,46	1997/12/01 11:05			
QDA CHACRAS 20.667	247.40	1997/12/01 11:30			
QDA CHACRAS 21.500	245.91	1997/12/01 11:44			
QDA CHACRAS 22.233	243.66	1997/12/01 12:00			
QDA CHACRAS 22.967	241.88	1997/12/01 12:15			
QDA CHACRAS 23,700	241.15	1997/12/01 12:16			
QDA CHACRAS 24.650	240.40	1997/12/01 12:21			
QDA CHACRAS 25.600	239.65	1997/12/01 12:26			
QDA CHACRAS 26.550	238.88	1997/12/01 12:30			
QDA CHACRAS 27.500	237.56	1997/12/01 12:30			
QDA CHACRAS 28.500	235.54	1997/12/01 12:46			
QDA CHACRAS 29.500	234.49	1997/12/01 13:27			
QDA CHACRAS 30,500	233.22	1997/12/01 13:57			
QDA CHACRAS 31.333	232.09	1997/12/01 14:35			
QDA CHACRAS 32.167	231.49	1997/12/01 14:44			
QDA CHACRAS 33.000	230.89				
QDA CHACRAS 33.875	229.59				
QDA CHACRAS 34.750	228.63				
QDA CHACRAS 35.625	228.41				
QDA CHACRAS 36.500	228.37	1997/12/01 20:35			

TABLE E3.2(1) MAXIMUM DISCHARGES IN THE RIO CHANE-PAILON BASIN

RIO CHANE 0.500	(m^3/s)			Maximum Discharge		
RIO CHANE 0.500	1 100	Time		(m ³ /s)	Time	
, and the second of the second	581.62	1997/12/04 09:18	RIO CHANE 46.117	370.67	1997/12/05 18:59	
RIO CHANE 1.500	579.26	1997/12/04 09:46	RIO CHANE 46.950	347,31	1997/12/06 05:02	
RIO CHANE 2.500	578.25	1997/12/04 10:07	RIO CHANE 47.850	347.13	1997/12/06 05:57	
RIO CHANE 3.500	577.89	1997/12/04 10:18	RIO CHANE 48,750	346.97	1997/12/06 06:47	
RIO CHANE 4.500	577.89	1997/12/04 10:20	RIO CHANE 49.612	346.71	1997/12/06 07:41	
RIO CHANE 5.500	577.90	1997/12/04 10:22	RIO CHANE 50.438	346,46	1997/12/06 08:30	
RIO CHANE 6.500	577.88	1997/12/04 10:24	RIO CHANE 51.263	346.18	1997/12/06 09:17	
RIO CHANE 7.500	577.91	1997/12/04 10:28	RIO CHANE 52.087	345.61	1997/12/06 10:07	
RIO CHANE 8.417	577.94	1997/12/04 10:30	RIO CHANE \$3,000	338.21	1997/12/06 17:07	
RIO CHANE 9.250	578.34	1997/12/04 10:33	RIO CHANE 54,000	337.89	1997/12/06 18:11	
RIO CHANE 10.083	581.88	1997/12/04 10:28	RIO CHANE 54,883	328.46	1997/12/07 00:00	
RIO CHANB 10.938	607.36	1997/12/04 09:16	RIO CHANE 55,650	327.89	1997/12/07 00:00	
RIO CHANE 11.813	669.23	1997/12/04 07:56	RIO CHANE 56,417	326.10	1997/12/07 00:00	
RIO CHANE 12.688	736.24	1997/12/04 07:00	RIO CHANE 57.267	323.02	1997/12/07 00:00	
RIO CHANE 13.563	795.08	1997/12/04 07:41	RIO CHANE 58.200	320.23	1997/12/07 00:00	
RIO CHANE 14.500	768.74	1997/12/04 07:15	RIO CHANB 59.133	318.26	1997/12/07 00:00	
RIO CHANE 15.500	731.96	1997/12/04 06:58	RIO CHANE 59.800	316.65	1997/12/07 00:00	
RIO CHANE 16.500	706.89	1997/12/04 06:01	RIO CHANE 60.350	496.22	1997/12/01 16:02	
RIO CHANE 17.500	711.56	1997/12/04 05:03	RIO CHANE 61.050	491.76	1997/12/01 17:32	
RIO CHANE 18.500	723.00	1997/12/04 05:05	RIO CHANE 61.750	488.54	1997/12/01 18:46	
RIO CHANE 19.500	727.67	1997/12/04 05:07	RIO CHANE 62.450	487.07	1997/12/01 19:15	
RIO CHANE 20.500	726.40	1997/12/04 05:09	RIO CHANE 63.150	485.19	1997/12/01 19:45	
RIO CHANE 21.500	728.49	1997/12/01 05:11	RIO CHANE 63.550	484.26	1997/12/01 20:00	
RIO CHANE 22.500	662.91	1997/12/04 05:41	RIO CHANE 63.650	484.25	1997/12/01 20:00	
RIO CHANE 23.500	578.20	1997/12/04 11:07	RIO CHANE 64.175	483.28	1997/12/01 20:24	
RIO CHANE 24.500	580.33	1997/12/04 11:20	RIO CHANE 65.125	480.30	1997/12/01 21:04	
RIO CHANE 25.438	402.42	1997/12/04 17:58	RIO CHANB 66.075	477.25	1997/12/01 21:48	
RIO CHANE 26.313	402.43	1997/12/04 18:30	RIO CHANE 67.025	473.01	1997/12/01 23:09	
RIO CHANE 27.188	401.44	1997/12/04 19:07	RIO CHANE 67.975	467.89	1997/12/02 00:27	
RIO CHANE 28.063	406.71	1997/12/04 19:48	RIO CHANE 68.925	463.84	1997/12/02 01:56	
RIO CHANE 28.913	431.75	1997/12/04 21:54	RIO CHANE 69.833	459.77	1997/12/02 03:02	
RIO CHANE 29.738	427.71	1997/12/04 23:31	RIO CHANE 70.700	457.27	1997/12/02 03:46	
RIO CHANE 30.563	425.87	1997/12/05 00:33	RIO CHANE 71 567	455.04	1997/12/02 04:26	
RIO CHANE 31.387	425.35	1997/12/05 01:03	RIO CHANB 72.400	452.98	1997/12/02 05:01	
RIO CHANE 32.275	430.46	1997/12/05 00:46	RIO CHANB 73.200	451.04	1997/12/02 05:36	
RIO CHANE 33.225	427.25	1997/12/05 02:07	RIO CHANE 74.000	449.09	1997/12/02 06:13	
RIO CHANE 34.150	60.84	1997/12/05 03:24	RIO CHANE 74.800	447.03	1997/12/02 06:48	
RIO CHANE 35.050	60.88	1997/12/05 03:35	RIO CHANE 75.617	444.59		
RIO CHANE 35.950	61.83	1997/12/05 04:45	RIO CHANE 76.450	441.48	1997/12/02 08:12	
RIO CHANE 36.450	61.95	1997/12/05 04:46	RIO CHANE 77.283	438.06	1997/12/02 08:59	
RIO CHANE 36.550	61.96	1997/12/05 04:46	RIO CHANE 78.067	435.16	1997/12/02 09:43	
RIO CHANE 37.075	154.90		RIO CHANE 78.800	432.97	1997/12/02 10:21	
RIO CHANE 38.025	151.53		RIO CHANE 79.533	431.58	1997/12/02 11:03	
RIO CHANE 39.000	472.59		RIO CHANE 79.950	430.68	1997/12/02 11:26	
RIO CHANE 40.000	471.37		RIO CHANE 80.050	430.49	1997/12/02 11:30	

TABLE F.3.2(2) MAXIMUM DISCHARGES IN THE RIO CHANE-PAILON BASIN

RIVER/Chainage (m ² /s) Time (m ² /s) (m ² /s) Time (m ² /s) (m ² /s) Time (m ² /s)				
RIO CHANE 80.570	River/Chainage	Maxi	mum Discharge	River/Chainag
RIO CHANE 81.510				\
RIO CHANE 81.510	RIO CHANE 80 570			ODA CHAND 20 SC
RIO CHANE 82.450 427.33 1997/12/02 13.26 RIO CHANE 83.390 430.38 1997/12/02 14.00 QDA CHANE 32.80 RIO CHANE 84.390 431.12 1997/12/01 22:13 QDA CHANE 32.80 RIO CHANE 87.950 539.72 1997/12/01 22:14 RIO PAILON 0.500 RIO CHANE 88.500 539.72 1997/12/01 22:14 RIO PAILON 0.500 RIO CHANE 88.500 539.57 1997/12/01 22:16 RIO PAILON 0.500 RIO CHANE 89.300 539.02 1997/12/01 22:26 RIO PAILON 3.500 RIO CHANE 90.100 538.62 1997/12/01 23:05 RIO PAILON 3.500 RIO CHANE 90.100 538.62 1997/12/01 23:08 RIO PAILON 3.500 RIO CHANE 90.17 538.38 1997/12/01 23:38 RIO PAILON 3.500 RIO CHANE 90.500 538.16 1997/12/01 23:38 RIO PAILON 4.500 RIO CHANE 90.500 538.16 1997/12/01 23:38 RIO PAILON 6.500 RIO CHANE 94.500 538.17 1997/12/01 23:49 RIO PAILON 7.500 RIO CHANE 94.500 538.17 1997/12/01 23:49 RIO PAILON 7.500 RIO CHANE 0.450 174.76 1997/12/01 02:40 RIO PAILON 8.500 QDA CHANE 1.350 172.25 1997/12/01 03:49 RIO PAILON 8.500 QDA CHANE 1.350 172.25 1997/12/01 03:49 RIO PAILON 10.43 QDA CHANE 4.650 150.65 1997/12/01 03:49 RIO PAILON 10.43 QDA CHANE 4.650 150.65 1997/12/01 03:49 RIO PAILON 10.43 QDA CHANE 4.650 150.65 1997/12/01 03:07 RIO PAILON 10.43 QDA CHANE 4.663 221.43 1997/12/01 03:07 RIO PAILON 12.65 QDA CHANE 6.813 216.40 1997/12/01 05:06 RIO PAILON 12.25 QDA CHANE 6.813 216.40 1997/12/01 05:45 RIO PAILON 12.25 QDA CHANE 6.813 216.40 1997/12/01 06:45 RIO PAILON 12.05 QDA CHANE 17.37 215.70 1997/12/01 06:45 RIO PAILON 12.05 QDA CHANE 11.500 199.39 1997/12/01 08:16 RIO PAILON 16.55 QDA CHANE 14.60 199.39 1997/12/01 03:45 RIO PAILON 16.55 QDA CHANE 15.683 189.67 1997/12/01 10:10 RIO PAILON 16.55 QDA CHANE 15.683 189.67 1997/12/01 10:10 RIO PAILON 12.05 QDA CHANE 15.683 189.67 1997/12/01 13:13 RIO PAILON 12.05 QDA CHANE 15.683 189.67 1997/12/01 13:48 RIO PAILON 22.70 QDA CHANE 15.500 48.83 1997/12/01 13:48 RIO PAILON 22.70 QDA CHANE 15.500 48.83 1997/12/01 23:34 RIO PAILON 22.70 QDA CHANE 15.500 48.83 1997/12/01 23:34 RIO PAILON 22.70 QDA CHANE 15.500 48.83 1997/12/01 23:34 RIO PAILON 22.70 QDA CHANE 25.300 44.43 1997/12/02 03:45 RIO PAILON 2				· · · · · · · · · · · · · · · · · · ·
RIO CHANE 83,390				
RIO CHANE 84.330	and the state of t			
RIO CHANE 87.950				
RIO CHANE 88.050				to the second of
RIO CHANE 88.500				
RIO CHANE 89.300 539.02 1997/12/01 22:49 RIO PAILON 2.500 RIO CHANE 90.100 538.62 1997/12/01 23:05 RIO PAILON 3.500 RIO CHANE 90.1750 538.38 1997/12/01 23:38 RIO PAILON 4.500 RIO CHANE 91.750 538.24 1997/12/01 23:38 RIO PAILON 5.500 RIO CHANE 92.583 538.18 1997/12/01 23:345 RIO PAILON 6.500 RIO CHANE 93.500 538.16 1997/12/01 23:45 RIO PAILON 6.500 RIO CHANE 94.500 538.17 1997/12/01 23:49 RIO PAILON 6.500 QDA CHANE 0.450 174.76 1997/12/01 03:49 RIO PAILON 9.500 QDA CHANE 1.350 172.25 1997/12/01 03:40 RIO PAILON 10.400 QDA CHANE 1.350 172.25 1997/12/01 03:53 RIO PAILON 10.400 QDA CHANE 4.050 150.65 1997/12/01 05:07 RIO PAILON 12.65 QDA CHANE 4.050 150.65 1997/12/01 05:07 RIO PAILON 12.65 QDA CHANE 4.063 221.43 1997/12/01 05:04 RIO PAILON 12.65 QDA CHANE 4.063 221.43 1997/12/01 05:05 RIO PAILON 12.65 QDA CHANE 6.813 216.40 1997/12/01 05:05 RIO PAILON 14.07 QDA CHANE 9.600 198.98 1997/12/01 06:46 RIO PAILON 14.07 QDA CHANE 10.533 195.35 1997/12/01 06:46 RIO PAILON 14.07 QDA CHANE 10.533 195.35 1997/12/01 08:16 RIO PAILON 16.55 QDA CHANE 11.500 193.35 1997/12/01 11:30 RIO PAILON 16.55 QDA CHANE 15.683 189.67 1997/12/01 13:12 RIO PAILON 16.55 QDA CHANE 15.683 189.67 1997/12/01 13:12 RIO PAILON 12.25 QDA CHANE 15.683 189.67 1997/12/01 13:48 RIO PAILON 21.25 QDA CHANE 15.683 189.67 1997/12/01 13:48 RIO PAILON 21.25 QDA CHANE 15.830 46.61 1997/12/01 23:53 QDA CHANE 15.830 46.61 1997/12/01 23:54 RIO PAILON 21.25 QDA CHANE 22.500 48.17 1997/12/02 23:54 RIO PAILON 21.25 QDA CHANE 22.500 44.43 1997/12/02 23:54 RIO PAILON 21.25 QDA CHANE 23.500 46.61 1997/12/02 23:54 RIO PAILON 21.25 QDA CHANE 23.500 46.61 1997/12/02 23:54 RIO PAILON 21.25 QDA CHANE 22.500 44.43 1997/12/02 23:54 RIO PAILON 21.25 QDA CHANE 25.383 40.41 1997/12/02				
RIO CHANE 90.100	RIO CHANE 89,300			
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	Kov chure 50.000	37./0	133711404 00.03	QUATORO 2.933

River/Chainage	Maximum Discharge			
	(m ³ /s) Time			
QDA CHANE 29.500	39.79			
QDA CHANE 30.367	40.15			
QDA CHANE 31.200	290.39	1997/12/01 12:49		
QDA CHANE 32.000	286.92	1997/12/01 14:02		
QDA CHANE 32.800	285.76	1997/12/01 14:39		
QDA CHANB 33.600	285.31	1997/12/01 14:48		
RIO PAILON 0.500	137.68	1997/12/04 12:22		
RIO PAILON 1.500	130.92			
RIO PAILON 2.500	125,35			
RIO PAILON 3.500	121.52	1997/12/04 17:22		
RIO PAILON 4.500	118.92	1997/12/04 19:00		
RIO PAILON 5.500	116.36	1997/12/04 20:05		
RIO PAILON 6.500	75.51	1997/12/05 16:51		
RIO PAILON 7.500	75.01	1997/12/05 19:41		
RIO PAILON 8.500	74.70			
RIO PAILON 9.500	74.58			
RIO PAILON 10.433	74.44			
RIO PAILON 11.300	74.29			
RIO PAILON 12.167	74.28	1997/12/06 15:37		
RIO PAILON 12.650	74.28	1997/12/06 15:41		
RIO PAILON 12.750	74.28	1997/12/06 15:42		
RIO PAILON 13.225	74.28	1997/12/06 15:42		
RIO PAILON 14.075	74.28	1997/12/06 15:47		
RIO PAILON 14.975	74.28	1997/12/06 15:56		
RIO PAILON 15.925	74.28	1997/12/06 17:15		
RIO PAILON 16.450 RIO PAILON 16.550	74.28	1997/12/06 17:18		
RIO PAILON 17.067	74.28 74.28	1997/12/06 17:18 1997/12/06 17:26		
RIO PAILON 18.000	74.28	1997/12/06 17:26 1997/12/06 17:30		
RIO PAILON 18.933	74.27	1997/12/06 17:19		
RIO PAILON 19.850	74.26	1997/12/06 17:11		
RIO PAILON 20,750	74.26	1997/12/06 17:02		
RIO PAILON 21.250	74.25			
RIO PAILON 21.350	74.25	1997/12/06 16:56		
RIO PAILON 21.833	74.25	1997/12/06 16:55		
RIO PAILON 22.700	74,40	1997/12/06 17:11		
RIO PAILON 23.567	76.81	1997/12/06 17:07		
QDA MECO 0.500	92.47	1997/12/06 03:30		
QDA MECO 1.500	91.67	1997/12/06 03:53		
QDA MECO 2.100	7.77	1997/11/30 00:01		
R. CHICO II 0.475	371.89	1997/12/04 22:26		
R. CHICO II 1.425	362.85			
R. CHICO II 1.950	555.25	1997/12/04 23:20		
R. CHICO II 2.100	516.63	1997/12/04 19:56		
R. CHICO II 2 600	361.06	1997/12/05 05:33		
QDA TORO 0.200	380.75	1997/11/30 22:19		
QDA TORO 0.450	223.29	1997/12/01 04:07		
QDA TORO 0.550	232.03	1997/12/01 03:59		
QDA TORO 1.067	232.67	1997/12/01 04:09		
QDA TORO 2.000	231.92	1997/12/01 04:31		
QDA TORO 2.933	230.86	1997/12/01 05:00		

TABLE F.3.2(3) MAXIMUM DISCHARGES IN THE RIO CHANE-PAILON BASIN

River/Chainage	Maxir	num Discharge
	(m³/s)	Time
QDA TORO 3.700	230.22	1997/12/01 05:12
QDA TORO 4.300	336.87	1997/12/01 01:27
QDA TORO 5,000	504.36	1997/12/01 01:08
QDA TORO 5.800	504.34	1997/12/01 01:13
QDA TORO 6.700	504.04	1997/12/01 01:31
QDA TORO 7.700	499.92	1997/12/01 01:49
QDA TORO 8.700	487.52	1997/12/01 02:25
QDA TORO 9.700	472.74	
QDA TORO 10.700	460.99	1997/12/01 03:14
QDA TORO 11.680	287.47	1997/12/01 08:34
QDA TORO 12.640	286.05	1997/12/01 09:15
QDA TORO 13.600	285.97	1997/12/01 09:50
QDA TORO 14,560	280.21	1997/12/01 11:28
QDA TORO 15.520	277.64	1997/12/01 12:11
QDA MARAS 0.250 ODA MARAS 0.600	93.52 171.27	1997/12/01 01:06 1997/11/30 23:00
ODA MARAS 1.087	169,23	1997/11/30 23:00 1997/11/30 23:37
QDA MARAS 1.863	169.14	1997/11/30 23:44
QDA MARAS 1.803	169.22	1997/11/30 23:51
QDA MARAS 3.413	169.00	1997/12/01 00:01
QDA MARAS 4.100	169.07	1997/12/01 00:10
QDA MARAS 4.700	179.60	1997/11/30 22:55
QDA MARAS 5.500	311.73	1997/11/30 22:55
QDA MARAS 6.325	201.29	1997/11/30 22:57
QDA MARAS 6.975	169.62	1997/12/01 00:22
QDA CHACRAS 0.200	212.85	1997/12/01 00:39
QDA CHACRAS 0,450	168.01	·
QDA CHACRAS 0.600	412.93	
QDA CHACRAS 1.167	412.61	1997/12/01 04:40
QDA CHACRAS 2.100	412.50	
QDA CHACRAS 3.033	412.45	
QDA CHACRAS 3.964	411.73	
QDA CHACRAS 4.893	411.52	
QDA CHACRAS 5.821	411.23	
QDA CHACRAS 6.750	410.76	
QDA CHACRAS 7.679	410.09	1997/12/01 06:59
QDA CHACRAS 8.607	409.21	1997/12/01 07:23
QDA CHACRAS 9.536	408.22	<u> </u>
QDA CHACRAS 10.417	407.65	1997/12/01 08:13
QDA CHACRAS 11.250	406.73	1997/12/01 08:36
QDA CHACRAS 12.083	406.57	1997/12/01 08:47
QDA CHACRAS 12.938	406.57	1997/12/01 08:50
QDA CHACRAS 13.813	406.47	1997/12/01 09:00
QDA CHACRAS 14.688	406.07	1997/12/01 09:18
QDA CHACRAS 15.563	405.26	1997/12/01 09:45
QDA CHACRAS 16.500	404.33	1997/12/01 10:18
QDA CHACRAS 17.500	403.70	1997/12/01 10:43
QDA CHACRAS 18.500	403.50	1997/12/01 10:56
QDA CHACRAS 19.417	403.51	#· -
QDA CHACRAS 20.250	403.38	
QDA CHACRAS 21.083	402.77	

River/Chainage	Maximum Discharge		
	(m³/s)	Time	
QDA CHACRAS 21.867	402.50	1997/12/01 11:48	
QDA CHACRAS 22.600	402.28	1997/12/01 12:03	
QDA CHACRAS 23.333	402.14	1997/12/01 12:14	
QDA CHACRAS 24.175	402.11	1997/12/01 12:17	
QDA CHACRAS 25.125	402.08	1997/12/01 12:23	
QDA CHACRAS 26.075	402.06	1997/12/01 12:28	
QDA CHACRAS 27.025	402.04	1997/12/01 12:31	
QDA CHACRAS 28.000	402.05	1997/12/01 12:33	
QDA CHACRAS 29.000	401.83	1997/12/01 12:46	
QDA CHACRAS 30,000	400.16	1997/12/01 13:23	
QDA CHACRAS 30.917	398.76	1997/12/01 14:00	
QDA CHACRAS 31.750	397.33	1997/12/01 14:30	
QDA CHACRAS 32.583	397.08	1997/12/01 14:44	
QDA CHACRAS 33.438	397.06	1997/12/01 14:46	
QDA CHACRAS 34.313	397.12	1997/12/01 14:48	
QDA CHACRAS 35.188	396.76	1997/12/01 14:55	
QDA CHACRAS 36.063	392.73	1997/12/01 15:06	

TABLE F.3.3 CALCULATION OF HYDRAULIC CHARACTERISTICS AT THE CHAINAGE 63.61 KM

Chainage	Elevation	on (m)	Max Q	Max WL	Depth	Cross section	Hydraulic	Froude
	Bed	Bank	(m³/s)	(m)	(m)	(m²)	Radius (m)	Number
62.10	233.17	239,44	494.0	239.77	6.60	219.95	2.71	0,44
63.50	231.65	237.96	494.0	238.28	6,63	620.37	0.62	0.32
63.60	231.61	240.00	494.0	237.97	6.36	103.37	2.50	0,96
63.70	231.58	237.90	494.0	238.18	6.60	385.53	0.97	0.42
67.50	229.02	235,62	494.0	236.96	7.94	379.96	2.44	0.27

TABLE F.3.4 MAXIMUM WATER LEVELS AND DISCHARGES IN THE OKINAWA DRAINAGE BASIN

River/Chainage	Maximum Water Level			
	(m)	Time		
OKI-DR 0.000	250.53	1997/12/05 01:09		
OKI-DR 7.000	248.24	1997/12/04 16:00		
OKI-DR 16.000	241.13	1997/12/05 00:39		
OKI-DR 25,000	234.94	1997/12/04 19:50		
OKI-DR 28,000	230.00	1997/11/30 00:10		

River/Chainage	Maximum Discharge		
. :	(m³/s)	Time	
OKI-DR 1.000	17.47	1997/12/05 01:20	
OKI-DR 11.500	117.25	1997/11/30 00:10	
OKI-DR 20.500	240.36	1997/11/30 00:10	
OKI-DR 26.500	426.91	1997/11/30 00:10	

TABLE E3.5 MAXIMUM WATER LEVELS AND DISCHARGES IN THE ARROYO YAPACANICITO, JOCHI AND TACUARAL BASIN

River/Chainage	Maxim	um Water Level	Remarks
	(m)	Time	
JOCHE 0.000	288.85	1997/02/04 04:35	
JOCHI 3.000	284.66	1997/02/04 03:43	
JOCHI 6.000	281.50	1997/02/05 01:46	
JOCHI 9.520	277.01	1997/02/05 15:19	1
JOCHI 12:800	268.96	1997/02/06 01:17	
JOCHI 15.360	264.50	1997/02/06 20:42	
JOCHI 18.600	259.61	1997/02/06 21:55	
JOCHI 21.000	256.46	1997/02/06 06:40	
JOCHI 22.700	254.56	1997/02/06 22:51	
JOCHI 25.600	251.61	1997/02/07 11:43	
JOCHI 29.700		1997/02/04 04:28	
JOCHI 29.700	246.64	1997/02/04 04:28	the retarding
JOCHI 29.800	246.56	1997/02/04 09:18	basin
JOCHI 35.800	244.40	1997/02/08 15:27	
JOCHI 39.600	244.10	1997/02/08 17:03	
JOCHI 43,400	244.00	1997/01/31 00:01	Effect of D/S water level
TACUARAL 0.000	279.65	1997/02/04 03:41	
TACUARAL 3.000	276.38	1997/02/04 02:33	
TACUARAL 6.000		1997/02/04 14:24	
TACUARAL 9.000	269.28	1997/02/04 12:31	
TACUARAL 12.000	265.48	1997/02/04 22:18	
TACUARAL 16.400	261.19	1997/02/05 09:21	
TACUARAL 18.240	260.38	1997/02/05 09:04	
TACUARAL 18:340	260.10	1997/02/05 09:00	
TACUARAL 18.440	259.90	1997/02/05 09:06	
TACUARAL 20.700	256.69	1997/02/05 18:42	
TACUARAL 20.800	256.41	1997/02/05 18:23	·
TACUARAL 20.900	256.38	1997/02/05 18:37	
TACUARAL 22.600		1997/02/05 21:15	
TACUARAL 27.500		1997/02/04 07:50	Effect of
TACUARAL 27.600		1997/02/04 04:39	the retarding
TACUARAL 27.600	246.63	~	basin
TACUARAL 32.100	· — · — · -	1997/02/08 11:44	·
TACUARAL 37.900	243.50		Effect of D/S water level
JOCHI-TACU 0.000		1997/02/04 04:28	
JOCHI-TACU 1.000	246.63		
YAPACANICITO 0.000	282.94	1997/02/03 16:05	
YAPACANICITO 1.500	281.38		
YAPACANICITO 3.600		1997/02/03 19:39	ļ i
YAPACANICITO 6.100	276.48		
YAPACANICITO 8.600 YAPACANICITO 8.600	274.63		
	274.63		ļ
YAPACANICITO 12.200 YAPACANICITO 14.300	270.60 266.20		{
YAPACANICITO 16.800	263.41		ļ i
YAPACANICITO 18.000			ł
YAPACANICITO 21.000		1997/02/06 04:59	Į.
YAPACANICITO 23.500	257.62 255.75		
YAPACANICITO 27.100	252.94		
YAPACANICITO 39,900	245.34		
YAPACANICITO 44.900	241.98		}
YAPACANICITO 49.900			Effort of DVS
YAPACANICITO 56.300			Effect of D/S water level
YAPACANICITO 59.300	234.30		
YAPACANICITO 62:300	234.00		
SANJUAN DMI 0.000	-		
SANJUAN-DMI 0.800	274.63 274.56		
SANJUAN-DMI 1.600	274.50		
SANJUAN-DMI 2.400	274.50		
SANJUAN-DMI 2500			Effect of D'S water level
SANDUAN-DMI 2.300	271.00	וניוטי/יגינו וויטי/יגינו	Enect of D.2 Mater level

River/Chainage	Maxin	num Discharge
	(m³/s)	Time
JOCHI, 6.920		1997/02/05 01:48
JOCHT 9.620	55.95	1997/02/05 15:22
JOCHT 14:080	55.85	1997/02/06 20:00
JOCHI 15.460	55.74	
JOCHI 19.800	55.69	1997/02/06 22:04
JOCHE 21.850	55.68	1997/02/06 22:27
JOCHI 22.750	55.68	
JOCHE 22.850	55.68	1997/02/06 23:06
JOCHI 24.250	\$5.68	1997/02/06 23:14
JOCHI 27.650	66.32	
JOCHI 29.750	35.18	
JOCHI 32.800	61.30	
JOCHI 37.700	36.69	
JOCHI 41.500	36.68	
TACUARAL 1.500 TACUARAL 4.500	189.95	
TACUARAL 7.500	167.51	
	167.95	
TACUARAL 10.500 TACUARAL 14.200	164.33	
TACUARAL 17.320	132.52	*
TACUARAL 18 290	132.48	
TACUARAL 18.390	132.48	
TACUARAL 19.570	132.66	
TACUARAL 20.750	111.42	
TACUARAL 20.850	111.42	
TACUARAL 21.750	111.43	
TACUARAL 25.050	111.06	1997/02/05 21:15
TACUARAL 27.550	139.18	1997/02/05 04:01
TACUARAL 29.850	254.52	1997/02/04 05:37
TACUARAL 35.000	173.99	1997/02/08 10:55
JOCHI-TACU 0.050	121.88	1997/02/09 18:26
YAPACANICITO 0.750	139.96	1997/02/03 16:07
YAPACANICITO 2.550	134.96	
YAPACANICITO 4.850	125.76	
YAPACANICITO 7.350	116.73	
YAPACANICITO 8.610	75.83	
YAPACANICITO 12.210	63.12	
YAPACANICITO 14.310	63.12	
YAPACANICITO 17.400	63.69	
YAPACANICITO 18.010	29.43	
YAPACANICITO 22.250	29.20	
YAPACANICITO 25:300 YAPACANICITO 28:500	29.56 30.24	1997/02/06 06:18
YAPACANICITO 32.400		1997/02/04 11:54
YAPACANICITO 37.400		1997/02/05 12:12
YAPACANICITO 42.400		1997/02/06 03:32
YAPACANICITO 47.400	111.14	
YAPACANICITO 50.600	126.05	
YAPACANICITO 53.800		1997/02/04 00:13
YAPACANICITO 57.800	228.19	
YAPACANICITO 60.800	228.03	
SANJUAN-DMI 0.400	84.02	
SANJUAN-DM1 1,200	76.36	1997/02/07 11:14
SANJUAN-DMI 2.000	67.59	**
SANJUAN-DMI 2.490	57.62	1997/02/04 06:41
		·

TABLE F.4.1(1) WATER LEVEL FROM HD CALCULATION IN THE

	(m)		50 vear	241.51	21.17	240.66	240.01	239.91	239.55	238.92	238.26	237.80	237.19	237.00	236.69	236.03	235.80	235.50	234.93	233.94	233.44	233.13	232.48	231.73	230.48	230.45	230.23	229.86	229.56	229.16	228.18
	Maximum water level from probable flood (m)	tion		241 37	240.48	239.82	239.72	239.37	238.73	238.04	237.58	236.93	236.79	236.76	235.73	235.54	235.20	234.60	233.70	233.41	232.99	232.66	231.85	231.37	230.22	230.02	228.62	229.36	229.36	228.72	228.16
	vel from pr	Design cross section	10 year	241.25	240.83	240.26	239,60	239.51	239.17	238.52	237.81	237.34	236.67	236.52	236.17	235.40	235.24	234.89	234.26	233.47	232.90	232.59	231.89	231 18	230.01	229.98	229.80	229.44	229.17	228.79	227.76
	m water le	Desig	5 vear	241.10	240.55	239.78	239.22	239.12	238.79	238.15	237.43	236.95	236.23	236.09	235.65	234.96	234.74	234.38	233.75	233.13	232.48	232.18	231.49	230 73	229.66	230.62	229.46	229.14	228.89	228.52	227.47
	Maxumu		2 vear	240.03	239.42	238.82	238.16	238.06	237.71	237.07	236.40	235.93	235.14	234.98	234.51	234.00	233.66	233.16	232.65	232.14	231.37	231.06	230.37	229.53	228.76	228.69	228.54	228.28	228.06	227.73	226.82
	(tt) poo		50 year	243.47	240.82	240.32	239.63	239.50	239.27	238.46	237.84	237.45	236.90	236.67	236.43	235.71	235.41	235.08	234.65	233.90	233.36	233.21	232.99	232.15	230.77	230.32	230.15	229.77	229.36	228.76	227.44
٠	robable fic	ction	20 year	243 29	240.65	240.00	239.29	239.16	238.93	238.16	237.52	237.14	236.55	236.33	236.07	235.27	235.04	234.69	234.23	233.58	233.02	232.88	232.66	231.84	230.36	230.01	229.86	229.52	229.16	228.52	227 14
BASIN	vel from p	Existing cross section	10 year	243.14	240.57	239.79	238.99	238.86	238.64	237.96	237.29	236.88	236.28	236.07	235.78	234.98	234.72	234.34	233.88	233.34	232.75	232.62	232.40	231.61	230.06	229.78	229.65	229.35	228.97	228.30	226.91
NILON	Maximum water level from probable flood (m)	Existin	5 year	242.99	240 49	239.52	238.62	238.49	238.25	237.68	236.95	236.54	235.85	235.59	235.24	234.62	234 34	233.94	233.50	233.05	232.47	232.35	232.13	231.26	229.80	229.56	229.44	229.15	228.71	228.04	226.69
ANE-PA	Maximu		2 year	242.71	239.69	238.95	237.88	237.79	237.56	237.02	236.40	235.97	235.24	234.93	234.58	234.12	233.84	233.38	232.94	232.56	232.05	231.93	231.73	230.82	229.28	229.07	228.94	228.62	228.15	227.57	226.38
RIO CHANE-PAILON BASIN	Prop.	Riverbed Er (m)	(m)	234.629	234.121	233.680	232.893	232.625	232.108	231.550			229.969	229.405	228.841	228.222	227.679	227.084	226.671	226.293	225.650	225.150	224.585	224.072	223.345	222.822	222.473	222.072	221.746	221.410	221 000
.			Right Bank	244.437	240.125	238.979	238.830	237.782	239.548	238.267	236.859	235.248	236.790	234.151	235.409	236.064	234.238	234.664	234.948	233.855	230.865	227.820	232.776	230.278	231,812	231.683	230.171	229.708	228.670	228.151	226.155
		Existing	Riverbed	238.242	233.709	232.972	231.949	231.799	230.725	231.065	229.245	228.568	228.911	228.623	227.598	226.602	227.436	226.925	226.330	225.706	226.328	224 950	224.770	225.922	223.990	223.542	222.832	222.236	221.616	221 955	221.794
			Left Bank	244.286	240.088	239.532		238 378	239 143		237.127	235.705		233.925			231.806			233.970	233.608	232 315	231.822	234.050	230,591	226.672	226.451	228.598	227.788	227.185	227.463
	Acc.	Topo Topo	Survey (m)	26,354	25.441	24,646	23,229	22,748	21,817	20,812	19,745	18,876	17,966	16,951	15.936	14,821	13,844	12,773	12,030	11,349	10.192	9,292	8,275	7,351	6.04	5,103	4,124	3,002	2,089	1,149	0
	Chainage	Model	(km)	000.09	60,800	61.600	62.600	63.600	64.500	65.500	66.500	67.500	68.500	69.500	70.500	71.500	72,500	73.400	74.300	75.200	76.500	77.700	78.800	80.000	81.000	81,900	82.800	83.800	84,800	86.400	88.000
		Section		No. 28	No. 27	No. 26	No. 25	No 24	No. 23	No. 22	No. 21	No. 20	No. 19	No. 18	No. 17	No. 16	No. 15	No. 14	No. 13	No. 12	No. 11	No. 10	0 oN	% 92. 22.	No. 7	No. 6	No. 5	No. 4	No. 3	No. 2	No. 1
		River		Chane																				_			_				

TABLE F.4.1(2) WATER LEVEL FROM HD CALCULATION IN THE

RIO CHANE-PAILON BASIN

		Į į	Acc.				Prop.	Maximus	Maximum water level from probable flood (m)	el from or	obabic flo	(m) po	Maximu	m water le	Maximum water level from probable flood (m)	obable flo	(ii)
River	Section		Distance in		Existing		Riverbed										
		Model	2001				EL (m)		Existin	Existing cross section	tion			Desig	Design cross section	tion	
		(Jung)	Survey (m)	Left Bank		Right Bank		2 year	\vdash		_	50 year	2 year	5 year	10 year	20 year	50 year
Pailon	No. 33	24.000	58,032		253.692	7	252.724	259.34	259.67	259.91	200.12	260.39	258.39	258.79	258.96	277.49	259.29
	No. 32	29.900	57,429	258.332	252.300		252.624	258.91	259.22	259.45	259.65	259.91	257.84	258.17	258.37	258.35	258.78
	No. 31	30,600	26,630	257.532	252.805	┝	252.491	258.42	258.79	259.04	259.25	259.52	257.70	258.04	258.21	258.16	258.54
	No. 30	31 300	55,181	256 591	251.823	<u></u>	252.249	258.18	258.56	258.81	259.01	259.27	257 47	257.84	258.02	257.67	258.35
	No. 29	32.300	54,048	256.273	251.902	256.255	252.060	257.79	258.16	258.39	258.58	258.81	256.92	257.31	257.51	257.35	257.91
	No. 28	33.700	53,048	256.163	251.573	-	251.894	257.35	257.69	257.89	258.06	258.27	256.54	256.91	257.05	257.16	257.54
	No. 27	34.600	52,167		252.195	-	251.747	257.17	257.46	257.62	257.75	257.92	256.27	256.67	256.82	256.58	257.15
•	No. 26	35.500	51,006	257.104		1	251.553	257.03	257.34	257.51	257.64	257.81	255.84	256.22	256.42	255.88	256.86
	No. 25	36.500	49.986	255.548		_	251.383	256.50	256.80	256.97	257.10	257.28	254.90	255.22	255.40	255.48	255.93
	No. 25	36.500	49,986	255.548	<u> </u>	├-	251.383	256.50	256.80	256.97	257.10	257.28	254 83	255.15	255.30	255.12	255.85
	No. 24	37.100	48,688	255.343		 -	250.518	256.10	256.49	256.74	256.94	257.18	254.49	254.80	254.94	254.75	255.74
	No. 23	37.800	47,686	254.669		! -	249.850	255.39	255.78	256.06	256.28	256.56	254.15	254.43	254.59	254.65	255.74
	No. 22	38.500	46,768		250.632		249.238	254.98	255.42	255.72	255.96	256.25	254.06	254.38	254.52	254.65	255.02
	No. 21	39.500	45,942		249.798		248.687	254.77	255.18	255.46	255.68	255.96	253.39	253.82	25401	253.64	254.22
	No. 20	40.500	44,756	252.351	248.077		247.897	254.30	254.67	254.91	255.10	255.35	252.78	253.21	253.45	253.01	253.72
	No. 19	41.500	43,217		248.613	252.968	246.871	253.63	253.94	254,14	254.33	254.57	252.24	252.60	252.80	252.73	253.12
	No. 18	42.800	42.781		247.857		246.580	252.90	253.23	253.46	253.65	253.91	251.63	252.03	252.26	252 12	252.52
	No. 17	4 200		251.052	248 427	├	245.814	252.43	252.76	252.98	253.17	253.41	250.79	251.32	251.59	251.54	251 92
	No. 16	45.300	40,697	•	248.296	┡	245.191	252.17	252.46	252.65	252.82	253.05	250.16	250.64	250.96	250.79	251.37
	No. 15	46.500	39,675	251.131	246.781	251.346	244.509	251.56	251.78	251.94	252.08	252.28	249.52	249.98	250.22	250.02	250.55
	No. 14	47.800	38,936	249.271	245.241	 	244.016	250.69	250.99	251.18	251.36	251.58	248.69	249.14	249.46	249.17	249.89
	No. 13	49.200	37,958	249.836	247.392	 	243.365	250.47	250.74	250.93	251.09	251.30	247.53	247.97	248.23	248.33	248.62
	No. 12	20.300	36,414.	248.898	247.532		242.335	249.76	250.03	250.21	250.36	250.58	246.86	247.32	247.58	247.51	247.99
	No. 11	\$1.400	35,150		246.367	_	241.493	249.02	249.31	249.50	249.67	249.89	246.08	246 54	246.83	246.72	247.22
	Sö	52 500	33,888		244.481	Н	240.651	248.49	248.76	248.95	249.11	249.33	245.34	245.80	246.12	245.81	246.48
	80	53.200	33,505	247.235	243.985		240.396	247.91	248.22	248.43	248.61	248.85	244.81	245.27	245.61	245.53	245.93
	% 0.8	53.900	32,447		243.073	-	239.691	247.59	247.99	248.23	248.42	248.68	244.26	24.71	245.21	245.03	245.69
	No. 7	54.500	31,742		-	ا	239.221	247.52	247.90	248.13	248.32	248.56	243.86	244.32	24.77	244.65	245.18
	9 0N	55.650	30,668	245.989		Η.	238.505	247.32	247.71	247.94	248.12	248.35	243.07	243.60	244.01	243.87	244.39
	No. 5	26.800	29,673				237.842	246.79	247.18	247.42	247.57	247.78	242.27	242.90	243.26	242.94	243.59
	No 4	57.500	28,754	244.455	239.598		237.229	244.73	245.25	245.42	245.58	245.79	241.76	242.47	242.78	242.62	243.06
		58.200					236.733	244.02	244.57	244.87	245.13	245.40	241.17	242.04	242.42	242.02	242.78
	No 2	28.90	27,331				236.280	243.73	244.22	244.49	244.78	245.06	240.47	241.58	241.82	241.50	242.18
	No. 1	29.600	26.354	244.286	238.242	244,437	235.629	242.71	242.99	243.14	243.29	243.47	240.10	241.19	241.37	241.37	241.65

TABLE F.4.1(3) WATER LEVEL FROM HD CALCULATION IN THE RIO CHANE-PAILON BASIN

River	1	PLACIFICATION WATER SEVEL INVITED PRESSURE LINCOL (1975)	2		2000			•				Rver	Model		Fyre	Forther (Toes textion	Set son	Farshay James dellan		Design	Design cross section	non	
_	Model		FXISTIN	Existing cross section	Ì			SS	Design cross section	Ctrom			{	ļ			100	\$		A 1100 A	10000	20.450	200
_	(Jun)	2 year	5 year			50 year	2 year	٠į	-	20,00	۶ ا		200	1	1	75.45	27.7	3	68.92.4	+.	-+-	577.5	77.76
L	. 5	90.05	35.	ਰ ਨ	2 2	2	800	8	_	0.00	200	<u> </u>	3 5	20.012	30 966	17. 17.	277.30	27.48	244	2096	277.13	276.62	7.4
_	900		280.02	2000	25.29	2037	289.67	280 92	70.067	794.67	2000	300	3 8		1		276 02	3.00	276.21	276.52	2767	6967	Ĭ.
ľ	1,800 288.69	- 1	20,03	60.68	787.77	35.55	60.88.9	20.50	V. 20.	3.007	Į	_	800	2762	276.52	77672		277.16	276.21	276.52	276.72	275.50	277
1	(0.107 M/			71.00	_÷	100	10,100	10 ya	2 0	×1,9%	1		2 200	25.50	275.55	275.50	75.50	7.75	275.50	275.50	275.50	257.16	35.55
1	3 3		2.00	-{	2 2 2	35.7%	785.65	06 SXC	1	4.5	ļ	Check	0000	257.17	257.46	257.62	257.75	257.92	7.95	256.91	257.05	256.54	257.1
	1	0:00		_	30.00	21.30	14.44	1	1	2.5.7.2	2×5.13		0,750	1256.55	256.83	257.02	257.17	257.37	255.99	15,83	256.44	255.92	366
1	1	7	2/2	•	Į.	10 506	¥ 1,00	283.40	27.7.50	0,000	283.01		200	286.13	256.46	256.66	256.85	1_	25551	255.76	255.86	8	1. 1. 1.
1			1000	+	ç	27.40	-	10.00	30,000	7.000	>> 0.00	-	2	Ļ	256.43	256.63	256.83	257.04	255,01	255.37	25550	35.33	35.55
-		201.70	400.40	000000		20.00	- 1	40.40	220.68	770 OK	2 OX		2400	256.08	256.37	256.57	256.74	26.96	254.88	25525	255.37	35.13	255.9
_[100,007	ㅗ	00000	200	10.00	10.70	30.05	2000	2 22	ľ		057 2		256.51	Į.,	18.8	57.73	254.76	255.10	255.14	34.65	255.7
Î	31.			•	30,7,00	61.7.15	- [4 (0)4	3.6	***	٠	_	ξ	L		25.74	256 64	!	Ľ	25.38	254.52	267.45	255.7
i			3 5	7 7	7 1	20,72		100	300		3/6	1		1	L	267 39	267 45	L	L	267.34	267,39	266.76	7.73
T	00011		77.46		7.5 7.5	000	ŧ	17.11	17.00	3000	1000	ŝ	0.40	7.4.5	39995	266 72	266 80	Ļ	266.60	266.60	267.88	266.57	267.0
ij	3		0.7		000	0,000	- 1	10000	2,07,0	1,6870	270.41		ç	⊥	266.46	266.50	266.56		266.58	20057	267.34	266.53	266.6
- [4	10.077	_	_1		20.20	•	07.074	210.77	267.730	1000		9	Ļ	76.33	766.41	266.53	26669	266.30	266.37	267.34	265.20	266.6
-	. 1	200.50	_	- 1	6	ý.		200.40	70007	20,00	10.000		3	\perp		1	265.30	L	l.,	26651	26551	263.49	38
l		8 / ?		- 5	9	6.15	- 1	3	3	2000	100		1	1	1	1 KR 47	9. 19.	7.5	1755	0.196	26.62	261.2X	5.92
-¦	15.267	-1585. -1	500.66	266.75	200.82	5.0	26.82	3	3 5	3	2 S		۽ ا	1		Į.	06.136	1	L	91.196	3K 13K	55×91	26.
	16.100	265.19	F	265.68	265.85	S .	263 02	9	_	Š.	7		}	4	30.034	90 030	1	1	⊥	358.85	25× 04	257.04	0 9 0
	16.200	565.06			365.69	SS .	262 62	262.98	263.19	262.96	203.02		3.5	1	1	ľ	┸	1	L.	25.75	10.00	1 S	110
_;	16300		265.00		265.17	265.28	62.24	202.57	202.75	201.	703.17		3	1	-		į	L	L.	167.4	25.701		į.
_			263.51		59:69	263.82	261.17	261.47	261.60	200.80	ï		3	4			}	Ί	1	0.00	1	157.434	
_					2628	262.43	260.14	26048	260.04	3	10.19	-	3	4	1	- 1	1	1	⅃.	2000	1000	20.00	į
					260.72	760,81	259.02	259.36	259.56	258.74	259.93		3	_	1	ľ	_1		1		0 2	200	
Γ	i	1	258.89		26.85	258.95		ñ	Ì	257.47	2882		8	1	1	Š.	_1		0707	00'097	7.00 L	200	240
ľ	20,200	257,51	257.63			257.82	57.19	257.29		\$ 9	257.55		×		4	(d)	, K	⅃.	5			20.00	
٢	20,000		_	257.02	257.12	257.25	! !	× 28	25641	255.61	7.95.7		9.500	4		┙	200	-1	_L	3	÷	007/47	ř.
7	21.700				256.20	256.34	255.24	25.52	255.57	254.75	255.85	_	200		_1		48.		Ϊ	0	1	Š.	
Сį	_	234.95	255.14	_	25.35	55.55 Se 55	254.18	Ż.	254.67	253.60	8	_	8	4	1	_	-1	1	Ι	1000	1000	100	3
(7)	T	_	254.05		254.27	28.38	253.05	23.3	253.46	252.34	23.79		8	4	_	8 / 8	1	<u>``ſ</u>	_i		0 2	00.20	900
C	24,133			252.43	252.55	252.67	251.76	252 02	22,19	251.25	252.56		2	4	_	3	90.00	_	. 1		000	CO CO	1
<u>'`</u>	1_			ž.	231.65	251.83	250.56	250 89	251.09	2.00	25 34.		2. 86	ž	1	245.95	46.04			8	3.	Ç.	6.0
۲,					251.00	251.16	249.40	249.73	249.93	249:00	250.36		3	_	1	6.45,43	V-0		- [1	3		
ri	1					250.06	248.30	28.82	248.84	247,88	249.25		16.000	3	10.4	4	4	4	1000	3	3		X
ď	27.400	248.08	08.85	25.35	245.89	249,05	247.19	247.52	247.72	246.60	248.12	Š Š	000		272.81	8	3	2/2.3/	212.14	70.77	90777	(7)	7
ľ	2x 200	246.56	27.72	27.50	27.75	247.93	25.5	246.26	246.45	245.05	246.83	Maras	0 400	_	27.73	272 39	272 49	272.60	271.94	272.25	272.40	272.51	27.6
ľ		244.50	245.33	245.71	24607	246 46	244 40	17.34	26.49	244.39	24529		0.00	271.83	272.07	272.18	272.27	272.35	271.84	272.0x	272.18	272.27	272.3
,	1		244.06		244 66	244 93	243 99	243.76	244.17	2, 2,	24.64		0 700	271.48	271.70	271.78	271.86	271.96	571.49	271.73	271.7%	271.86	27.9
٦	Ł	. A	244.01		*	244 73	242.97	243.65	244.08	244,29	24.54		1.475	269.98	270.17	270.24	57.07.29	270.34	270.02	270.21	27027	270,22	270.3
-	1	243.55	244.0	241.34	24.54	24.73	242.97	243.65	244.08	243.06	24.54		প্র	268.57	268.73	268.81	268.86	268.90	268.63	268.79	268.84	26.83	98
-		243.12		243.59	243.77	243.97	241.75	242.52	242.85	242.16	243.48		302	267.39	567.49	26/32	267.55	267.59	267.44	267.50	267.55	267.58	9.9
		242 X I		•	243.37	243.54	1	241.73	241.9X	241.59	242.44		3.80	8.58	265.98	38	266.16	2650	265.90	265,86	36.04	366 34	36
ľ		CL CPC	243.00	1	243.70	243.47	1	241.30	24147	241.37	21.78		94	264.16	264 46	764 53	264.56	264.58	262.88	262.91	26.35	26.798	36.0
ï	, (0.3)	3.27.1	3,00	f	241 29	243.47	240 63	241 10	241.25	276.92	241.51		\$ 000	262.75	263.01	263.02	263.03	263.05	259.66	259.74	259.78	259.84	χ. 3.
1													6.650	257.07	257.31	257.38	257.45	257.50	257.07	257.47	257.72	25/87	25.0

TABLE F.4.1(4) WATER LEVEL FROM HD CALCULATION IN THE

RIO CHANE-PAILON BASIN

	1-1		•	•	4	0	,	벙	v	4	-		œ	es	m	.	110	_		·~ '			200	<u>ب</u>
(m) poor		50 year				247.60	L	243.84	1	24 A			ı		١.		:		232 01	231.27	1 1			230.56
robable f	tion	20 year	252.63	S S	24×.49	247.44	245.95	243.71	8. 3	241.26	240.52	236.79	236.02	237.68	235.73	17.25	33.46	232.36	231.77	231.09	30.00	₹ ₹	229.39	38
from p	Design cross section	10 year	252.52	250.45	248.36	247.31	245.83	243.59	241.82	2.1.2	240.37	39.65	238.8X	237.57	235.58	27.75	23.28	232.18	231.59	230.96	229.83	8.62	229.20	22,17
vater lew	Design	5 year		•	24.23		1									1		_	ŧ			l i		22% 89
Maximum water level from probable flood (m)	:	2 year 5			_	:	245.48				239.96 2			237.31	235.16 2				1	230.60	į.		i. I	228.06
	_	ļ.,							•				Į.	1				<u>L</u>	L.	L	L	i	į l	ŀ
flood (n		50 year	i	3 250.63	248.64			243,84			3 240.71		3 239.19	3 237.82				232.62			230.11	i		22,022
probable	ection	20 year				247.45							239.03	237.68	235.74		•	232.38	231.78			ı	t I	138.19
el from ;	Existing cross section	10 year	252.53	250.45	248.37	247.32	245.83	243.60	241.83	241.12	38	239.65	238.89	237.58	235.59	24.55	233.30	232.19	231.60	28.97	229.72	229.08	28.5	228.97
water les	EXISTO	5 year	252.42	5	248		245.70	243.46	241.68 241.83			239.49	238.76	237.48	235.44	234.38 234.55	233.12	232.01	231.42	23.82	•	28.78	228.72	23
Maximum water level from probable flood (m)		2 year	32.21	11.057	248.03	!	245.49	243.21	241.43	ı	Į.		238.52	237.32	235.17	Į	•			230.61	•	ļ	!	22.15
0	Model	<u> </u>		9000	19,833	,		L_					26.550	_	Ł.	3,500		L_	Į.		•	L	F	36,500
		_		<u>.</u>	Ĺ		۲,		<u> </u>) [64	Ľ	ři L	ñ	2	a	į [~]	Ľ		ř	Ë	Ë	, Y		Ľ
	?		OD.	Chacras																				
																_								_
(w.) po		50 vear	277.13	276.45	276.32	275.53	273.24	271.94	270.79	269.60	268.40	267.20	266.02	264.87	263.78	262.72	261.79	261.27	260.93	259.78	258.64	257.53	256.26	254.45
obable flood (m)	LOD	⊢		1			1	!	1	1			ı	1		Ĺ.,								<u> </u>
from probable flood (m)	ross section	20 year	277.04	27633	276.19	275.44	273.12	271.85	270.71	269.50	268.28	267.06	265.87	264.70	263.59	262.56	261.64	261.13	260.80	259.65	258.50	257.39	256.13	254.31
ater level from probable flood (m)	Design cross section	10 year 20 year	276.94 277.04	276.24 276.33	276.08 276.19	275.36 275.44	273.01 273.12	271.78 271.85	270.65 270.71	269.41 269.50	268.17 268.28	266.94 267.06	265.73 265.87	264.56 264.70	263.43 263.59	262.40 262.56	261.50 261.64	261.01 261.13	260.70 260.80	259.54 259.65	258.39 258.50	257.2.7 257.39	256.02 256.13	254.20 254.31
unsum water level from probable flood (m)	Design cross section	5 year 10 year 20 year	276.81 276.94 277.04	276.11 276.24 276.33	275.94 276.08 276.19	275.28 275.36 275.44	272.90 273.01 273.12	271.70 271.78 271.85	270.58 270.65 270.71	269.32 269.41 269.50	268.06 268.17 268.28	266.82 266.94 267.06	265.60 265.73 265.87	264.41 264.56 264.70	263.26 263.43 263.59	262.23 262.40 262.56	261.35 261.50 261.64	260.89 261.01 261.13	260.59 260.70 260.80	259,43 259,54 259,65	258.26 258.39 258.50	257.15 257.27 257.39	255.91 256.02 256.13	254.09 254.20 254.31
Maximum water level from probable flood (m)	Design cross section	2 year 5 year 10 year 20 year	276.59 276.81 276.94 277.04	275.89 276.11 276.24 276.33	275.74 275.94 276.08 276.19	275.17 275.28 275.36 275.44	272.74 272.90 273.01 273.12	271.58 271.70 271.78 271.85	270.47 270.58 270.65 270.71	269.19 269.32 269.41 269.50	267.91 268.06 268.17 268.28	266.64 266.82 266.94 267.06	265.39 265.60 265.73 265.87	264.17 264.41 264.56 264.70	262.99 263.26 263.43 263.59	261.95 262.23 262.40 262.56	261.10 261.35 261.50 261.64	260,69 260,89 261,01 261,13	260.43 260.59 260.70 260.80	259.25 259.43 259.54 259.65	258.07 258.26 258.39 258.50	256.95 257.15 257.27 257.39	255.72 255.91 256.02 256.13	253.90 254.09 254.20 254.31
	Design cross section	5 year 10 year 20 year	277.02 276.59 276.81 276.94 277.04	276.45 275.89 276.11 276.24 276.33	276.33 275.74 275.94 276.08 276.19	275.53 275.17 275.28 275.36 275.44	273.24 272.74 272.90 273.01 273.12	271.58 271.70 271.78 271.85	270.47 270.58 270.65 270.71	269.60 269.19 269.32 269.41 269.50	268.39 267.91 268.06 268.17 268.28	267.20 266.64 266.82 266.94 267.06	266.02 265.39 265.60 265.73 265.87	264.87 264.17 264.41 264.56 264.70	263.78 262.99 263.26 263.43 263.59	262.72 261.95 262.23 262.40 262.56	261.79 261.10 261.35 261.50 261.64	261.28 260.69 260.89 261.01 261.13	260.93 260.43 260.59 260.70 260.80	259.78 259.25 259.43 259.54 259.65	258.64 258.07 258.26 258.39 258.50	257.53 256.98 257.15 257.27 257.39	255.72 255.91 256.02 256.13	90 254.09 254.20 254.31
		2 year 5 year 10 year 20 year	276.59 276.81 276.94 277.04	275.89 276.11 276.24 276.33	275.74 275.94 276.08 276.19	275.53 275.17 275.28 275.36 275.44	272.74 272.90 273.01 273.12	271.58 271.70 271.78 271.85	270.47 270.58 270.65 270.71	269.60 269.19 269.32 269.41 269.50	268.39 267.91 268.06 268.17 268.28	267.20 266.64 266.82 266.94 267.06	265.39 265.60 265.73 265.87	264.87 264.17 264.41 264.56 264.70	263.78 262.99 263.26 263.43 263.59	262.72 261.95 262.23 262.40 262.56	261.79 261.10 261.35 261.50 261.64	261.28 260.69 260.89 261.01 261.13	260.93 260.43 260.59 260.70 260.80	259.78 259.25 259.43 259.54 259.65	258.64 258.07 258.26 258.39 258.50	257.53 256.95 257.15 257.27 257.39	256.26 255.72 255.91 256.02 256.13	253.90 254.09 254.20 254.31
		20 year 50 year 2 year 5 year 10 year 20 year	276,93 277.02 276,59 276,81 276,94 277,04	276.30 276.45 275.89 276.11 276.24 276.33	276.33 275.74 275.94 276.08 276.19	275.44 275.53 275.17 275.28 275.36 275.44	273.24 272.74 272.90 273.01 273.12	271.58 271.70 271.78 271.85	270.71 270.78 270.47 270.58 270.65 270.71	269.51 269.60 269.19 269.32 269.41 269.50	268.28 268.39 267.91 268.06 268.17 268.28	267.20 266.64 266.82 266.94 267.06	265.87 266.02 265.39 265.60 265.73 265.87	264.71 264.87 264.17 264.41 264.56 264.70	263.59 263.78 262.99 263.26 263.43 263.59	262.56 262.72 261.95 262.23 262.40 262.56	261.64 261.79 261.10 261.35 261.50 261.64	261.13 261.28 260.69 260.89 261.01 261.13	260.93 260.43 260.59 260.70 260.80	259.78 259.25 259.43 259.54 259.65	258.51 258.64 258.07 258.26 258.39 258.50	257.39 257.53 256.95 257.15 257.27 257.39	256.13 256.26 255.72 255.91 256.02 256.13	254.45 253.90 254.09 254.20 254.31
	Existing cross section	10 year 20 year 50 year 2 year 5 year 10 year 20 year	276,84 276,93 277.02 276,59 276,81 276,94 277,04	276.18 276.30 276.45 275.89 276.11 276.24 276.33	276.00 276.15 276.33 275.74 275.94 276.08 276.19	275.36 275.44 275.53 275.17 275.28 275.36 275.44	273.01 273.12 273.24 272.74 272.90 273.01 273.12	271.78 271.86 271.94 271.58 271.70 271.78 271.85	270.65 270.71 270.78 270.47 270.58 270.65 270.71	269.42 269.51 269.60 269.19 269.32 269.41 269.50	268.17 268.28 268.39 267.91 268.06 268.17 268.28	266.94 267.06 267.20 266.64 266.82 266.94 267.06	265.74 265.87 266.02 265.39 265.60 265.73 265.87	264.71 264.87 264.17 264.41 264.56 264.70	263.43 263.59 263.78 262.99 263.26 263.43 263.59	262,41 262,56 262,72 261,95 262,23 262,40 262,56	261.51 261.64 261.79 261.10 261.35 261.50 261.64	261.02 261.13 261.28 260.69 260.89 261.01 261.13	260.71 260.81 260.93 260.43 260.59 260.70 260.80	259.54 259.65 259.78 259.25 259.43 259.54 259.65	258.39 258.51 258.64 258.07 258.26 258.39 258.50	257.28 257.39 257.33 256.95 257.15 257.27 257.39	256.03 256.13 256.26 255.72 255.91 256.02 256.13	254.21 254.32 254.45 253.90 254.09 254.20 254.31
		5 year 10 year 20 year 50 year 2 year 5 year 10 year 20 year	276.73 276.84 276.93 277.02 276.59 276.81 276.94 277.04	276.06 276.18 276.30 276.45 275.89 276.11 276.24 276.33	275.86 276.00 276.15 276.33 275.74 275.94 276.08 276.19	275.29 275.36 275.44 275.53 275.17 275.28 275.36 275.44	272.911 273.01 273.12 273.24 272.74 272.90 273.01 273.12	271,71 271,78 271,86 271,94 271,58 271,70 271,78 271,85	270.59 270.65 270.71 270.78 270.47 270.58 270.65 270.71	269.33 269.42 269.51 269.60 269.19 269.32 269.41 269.50	268.08 268.17 268.28 268.39 267.91 268.06 268.17 268.28	266.83 266.94 267.06 267.20 266.64 266.82 266.94 267.06	265.61 265.74 265.87 266.02 265.39 265.60 265.73 265.87	264.42 264.36 264.71 264.87 264.17 264.41 264.36 264.70	263.28 263.43 263.59 263.78 262.99 263.26 263.43 263.59	262.25 262.41 262.56 262.72 261.95 262.23 262.40 262.56	261.36 261.51 261.64 261.79 261.10 261.35 261.50 261.64	260.90 261.02 261.13 261.28 260.69 260.89 261.01 261.13	260.60 260.71 260.81 260.93 260.43 260.59 260.70 260.80	259.44 259.54 259.65 259.78 259.25 259.43 259.54 259.65	258.27 258.39 258.51 258.64 258.07 258.26 258.39 258.50	257.16 257.28 257.39 257.53 256.95 257.15 257.27 257.39	255,92 256,03 256,13 256,26 255,72 255,91 256,02 256,13	254.10 254.21 254.32 254.45 253.90 254.09 254.20 254.31
Maximum water level from probable flood (m)	Existing cross section	2 year 5 year 10 year 20 year 50 year 2 year 5 year 10 year 20 year	276.54 276.73 276.84 276.93 277.02 276.59 276.81 276.94 277.04	275.85 276.06 276.18 276.30 275.45 275.89 276.11 276.24 276.33	275.66 275.86 276.00 276.15 276.33 275.74 275.94 276.08 276.19	275.18 275.29 275.36 275.44 275.53 275.17 275.28 275.36 275.44	272.75 272.91 273.01 273.12 273.24 272.74 272.90 273.01 273.12	271,59 271,71 271,78 271,86 271,94 271,58 271,70 271,78 271,85	270.48 270.59 270.65 270.71 270.78 270.47 270.58 270.65 270.71	269.20 269.33 269.42 269.51 269.60 269.19 269.32 269.41 269.50	267.92 268.08 268.17 268.28 268.39 267.91 268.06 268.17 268.28	266.65 266.83 266.94 267.06 267.20 266.64 266.82 266.94 267.06	265.40 265.61 265.74 265.87 266.02 265.39 265.60 265.73 265.87	264.19 264.42 264.56 264.71 264.87 264.17 264.41 264.56 264.70	263.01 263.28 263.43 263.59 263.78 262.99 263.26 263.43 263.59	261.96 262.25 262.41 262.56 262.72 261.95 262.23 262.40 262.56	261.11 261.36 261.51 261.64 261.79 261.10 261.35 261.50 261.64	260,70 260,90 261,02 261,13 261,28 260,69 260,89 261,01 261,13	260.43 260.60 260.71 260.81 260.93 260.43 260.59 260.70 260.80	259.26 259.44 259.54 259.65 259.78 259.25 259.43 259.54 259.65	258.08 258.27 258.39 258.51 258.64 258.07 258.26 258.39 258.50	256.96 257.16 257.28 257.39 257.33 236.95 257.15 257.27 257.39	255.73 255.92 256.03 256.13 256.26 255.72 255.91 256.02 256.13	253.92 254.10 254.21 254.32 254.45 253.90 254.09 254.20 254.31
Maximum water level from probable flood (m)	Existing cross section	5 year 10 year 20 year 50 year 2 year 5 year 10 year 20 year	276.54 276.73 276.84 276.93 277.02 276.59 276.81 276.94 277.04	276.06 276.18 276.30 276.45 275.89 276.11 276.24 276.33	275.66 275.86 276.00 276.15 276.33 275.74 275.94 276.08 276.19	275.18 275.29 275.36 275.44 275.53 275.17 275.28 275.36 275.44	272.911 273.01 273.12 273.24 272.74 272.90 273.01 273.12	271,59 271,71 271,78 271,86 271,94 271,58 271,70 271,78 271,85	270.48 270.59 270.65 270.71 270.78 270.47 270.58 270.65 270.71	269.20 269.33 269.42 269.51 269.60 269.19 269.32 269.41 269.50	267.92 268.08 268.17 268.28 268.39 267.91 268.06 268.17 268.28	266.65 266.83 266.94 267.06 267.20 266.64 266.82 266.94 267.06	265.61 265.74 265.87 266.02 265.39 265.60 265.73 265.87	264.19 264.42 264.56 264.71 264.87 264.17 264.41 264.56 264.70	263.01 263.28 263.43 263.59 263.78 262.99 263.26 263.43 263.59	261.96 262.25 262.41 262.56 262.72 261.95 262.23 262.40 262.56	261.11 261.36 261.51 261.64 261.79 261.10 261.35 261.50 261.64	260,70 260,90 261,02 261,13 261,28 260,69 260,89 261,01 261,13	260.60 260.71 260.81 260.93 260.43 260.59 260.70 260.80	259.26 259.44 259.54 259.65 259.78 259.25 259.43 259.54 259.65	258.08 258.27 258.39 258.51 258.64 258.07 258.26 258.39 258.50	256.96 257.16 257.28 257.39 257.33 236.95 257.15 257.27 257.39	255.73 255.92 256.03 256.13 256.26 255.72 255.91 256.02 256.13	254.10 254.21 254.32 254.45 253.90 254.09 254.20 254.31

TABLE F.4.2(1) FLOW RATE FROM HD CALCULATION IN THE RIO CHANE-PAILON BASIN

-	5	the second consolidation is the second contract the second contract to the second contract									_											
	Model		Existu	Existing cross section	xtion			ğ	Design cross section	etion		Model		Existin	Existing cross section	ton			Design	Design cross section	uo	
	(Eg	2 vear	5 year	10 year	20 year	50 vear	-	5 year	10 year	20 year	50 year	<u> </u>	2 year	5 year	10 wear	20 year	50 year	2 vear	S wear	10 year	20 year	50 vea
Chane	0.500	521.45	787.41	964.32	1,129.48		L.	5443	3 807.81	954.97	1,153.70	38.150	493.16	783.37	,008.77	,216.72 1	472.84	461.44	536.34	585.96	80.440	1.018.
1	500	519.13	784.32	960.89	1,125.79	1,343.61	1 435.21	6259	3 805.98	952.89	1,151.01	39.000	485.56	747.45	961.67	.152.34	,409.72	674.00	799.16	888.28	981.30	1,017.
	2.500	518.19	783.26	959.74	1,124,61	1,342.36	5 434.88	652.4	805.44	952.30	1,150,25	40.000	480.25	732.55	935.32	.116.53 1	36.39	674.00	792.78	882.63	975.53	1,015.
	3.58	518.25	783.39	959.94	1,124,86	1,342.64	435.04	652.7	1 805.71	952.65	1,150.58	41.000	478.68	727.86	927.60	,102.77	χ. 8	668.60	790.71	877.46	88	1.01
1	4.500		783.80	960.59	1,125.68	1,125.68 1,343.52	2 435.33	653.1	0 806.23	953.27	1,151.23	41.825	414.34	602.00	745.22		.076.54	668.78	790.79	876.37	948.32	8
<u>!</u>	500		784.35	961.17	1,126.40	1344.37		653.5	3 806.7	953.92	1,151.99	42.475	413.75	601.30	744.12		86.740	08.89	788.18	872.32	\$44 98	ž
<u></u>	9	519.15	784 79	561.75	1.127.11	1,345,14	4 435,89	623.9	507.23	9.48	1.152.70	43.150	413.03	600.45	743.08	878.54	.073.08	665.80	786.57	870.15	942.07	985
1_	105	\$7015	785 30	38, 690	962 38 1 127 87		ı		807/8	955.21	1.153.32	43.850	412.25	580.50	742.04	877.14	(071.09	22.53	784.74	98.998	938.79	8
1	1 ×	7,015	785 60	80.89	962 81 1 128 38	1,5 9 15	ı	L	2 808 2	57 52 9	151.94	44.475	411.71	598.93	741.20	876.13	1,069.47	564.7	783.19	861.21	935.70	8,6
1	1000	×10.00	0 28	55.25	00 00 1 00 090		i	_	9808	2.956	1 154.42	45.025	41146	598.50	740.73	875.51	,068,43	98.799	782.23	858.85	933.53	ç
1.	1 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	6,000	100 XX	00.50	25 061 1 00 590		1	1	100%	27.720	1 155 00	45,600	411 21	61 X65	740.18	874.76	1.067.40	50.599	782.36	857.21	932.56	976
1	0.00	7777	100 701	10,430	120 20	12000	ļ		75.008	04779	1,9 551	46.200	411 12	0.03	739.71		0.66 31	665 23	782.51	857 30	43.2 6X	976
1	2	2000	200	2 2	60.00	6,000	-	L	1000	067.99	36.35	3C8 3A	410.83	06 30	75.75	0.8%	0,46.60	C4.542	125 67	X57.40	00.00	920
	Ş	e - - - -	V6 /8/	0	X00.00	7.000	1		0.00	1	20 73	7.7.47	A10.25	(2) XOX	73.5.64	867 A1	A 230	69 595	S C 52	857.44	62.67	Š
_1	7 200	27.00	2/ /8/	0	0.10		1	ļ	0000	0.000	1.130.0	051.07	17.004	207 80	734.84	77 77	85 450	13 559	78101	07 75 X	27 000	S
	2	371.4	/100/	8	900.00 1.133		. 1	- 1	0.00	2000	2000	03004	3,50	20, 40	06.764	Ľ	10 630	27.527	100.00	λ 20 23 0	96.00	6
لَــُ	14.719	521.63	3	80.00	1.133.02	0.1331.70	1	_ [811.3		1,156.13	40.03	70.00	1	3 4	1	10.000	2000	70.07	3	07.7	,
_	15.656	\$21.90	789.09			1,352.61			811.92		1,158.85	47.4/5	409.15	17.4.61	- 3.		JC.55.3	000.00	/0170/	\$ ¥	63,13	, ,
Ľ	16.594	522.13	789.52	69 /96		1,134,46 1,353,40	Ш		8 812.43	80.8	1,159.48	50.025	409.05	28.08	733.79	_	.052.83	\$	/8 	852.91	8.49 8.48	973.
Ľ	17.531	522.43	789.92	968.29	1,135,16				7 812.9	961.49	1.160.17	50.575	\$ \$.8	593.83	733.4×	% .5%	,052.17	\$ 5. 2.	781.40	853.03	%; %;	973
匚	18.500	522.76	790.40	968.88	1,135.82	1,354.93	3 438.81	658.8	7 813.4K	962.09	1,160.89	51.125	408.72	593.44	732.92	863.80	,051.09	00,39	781.35	852.73	928.39	973
]_	19.500	523.06	ı	969.43	1,136.56	1,355.80	L		9 813.94	962.67	1,161.56	51.675	408.28	592.74	731.97	862.55	14.610	62,19	781.52	852.85	928.51	973
<u>j'`</u>	20.500	523.35	791.36	10.076	1.137.33		8 440.26	659.7	2 814.46	83.2	1,162,19	\$2.22	407.70	591.84	730.74	860.92	27.72	\$6.39	781.68	852.96	38.6	973
` ``	21.500	523.63	701.80		1.138.05	1,357,33	L	099	814.9	963.95	1,162.88	52,850	395.10	571.43	704.62	828.46	10.800	664.61	781.88	853.09	928.71	27.
1	22.500	523 93	792.25	971.23	1.138.68	1.358.19	1	L	4 815.46	964.59	1,163.61	53.550	38.88	565.79	702.16	825.57	20.62	88.83	782.10	16.958	936.42	278
i.	23 500	524.07	792.63	971.76	1.139.37	971.76 1.139.37 1.358.89	439.94		11 815.48	25.25	1,163.76	54.200	391.16	267.08	65869	821.83	55.000	90.599	782.29	860.37	21.27	985
Ţ	24 500	45.523	703.15	971.80	1 139 20	971.80 1.139.20 1.357.88	<u>1</u>	١	8 819.32	968.49	1.167.76	54.787	370.45	\$49.85	675.60	800.28	976.02	665.25	782.46	808.01	968.78	8
ľ	25.438	347.76	476.37	569.35	662.79	793.09	ţ	i.	8 676.15	768.75	878.71	55.362	369.69	549.51	675.12	16.662	975.52	665.36	782.59	875.23	986 12	8
ľ	26 313	348.80	477.68	570.32	1	1	ŀ	1	0 674.97	770.63	883.43	55 938	368.20	\$49.38	674.81	799.74	975.24	665.57	782.77	882.72	863.56	8
15	27 188	348.74	479.02	273.44	667.44		ı	L	2 673.39	7,88	890.01	56.513	367.92	549.45	674.77	799.76	975.17	865.78	782.96	89021	971.07	1,017.
1	28 063	346.97	474 87	571.62	665.28	ı	L	557.70	0 673.28	769.76	893.33	\$7.150	368.06	549.61	674.93	799.92	975.29	666.01	783.18	898.50	979.51	1.026
12	28 850	425.77	594 57	728.65	ı	1,045.63	1_	3	9 677.46	749.61	823.99	\$7.850	368.21	549.57	674.84	09'662	20.576	666.27	783.42	907.66	988.88	1,037.
Ľ	29.550	472.63	665.71	818.19	ı		ŀ	681.3	5 743.59	80938	889.74	58.550	368.24	549.57	674.87	799.18	974.88	666.55	785.25	915.87	. 05.786	8.7
Ľ	30,250	518.92	736.10	10:/06	1,070.91	1,294.99		757.6	8 829.45	901.79	984.50	59.250	368.40	549.73	675.02	10.667	974.93	666.84	793.59	924.92 1	. 77.900	8
<u>i</u> "	30.950	561.01	803.82	79.566	1,173,55	1,417.35	-		1 917.90	1,000.92	1,107.15	29.800	368.48	549.81	675.11	788.20	975.27	60.799	800.14	932.09	014.15	.865
<u> </u>	31.800	576.13	832.27		1,219.15	1,472,19	690.75	ı	4 954.85	1.94	1,159,55	60.400	430.40	622.91	753.85	892.09 1.	10.960	910.92	367.78	581.75	35.83	88
<u> </u>	32.650	571.46	826.18	826.18 1,026.75	1,214,13	1,467.08		l	1 951.38	1,040,18	1,153.35	61.200	430.59	16.229	75.17	892.20	.096.12	914.58 1.	367.35	580.99	730.12	8
<u>.</u>	33.350	563.73	818.38	1,021.35	1,209.29	1,461.88	688.29	855.64	8 946.32	1,035.32	1.,146.65	62.100	430.77	622.83	2.0.2	891.65	1,095.25	918.21 1,	357.42	576.10	733.16	Ŕ
Ľ.	34.150	549.34	801.99	1,007.01	1,195.19	1,445.12	1_	ŧ.	3 627.90	687.08	1,124.57	63.050	430.25	621.89	753.36	890.93	.093.98	907.19	353.95 1.	577.15	735.71	č.
<u> </u>	35.050	435.06	614.38	735.59	853.36	1,008.77	<u> </u>	539.4	590.32	65036	786.02	87.138	429.63	620.32	752.32	889.69	092.72	891.76	342.39	576.25	25.57 27.	918
	35,950	434.49	613.43	737.58	1	855.33 1.016.35			\$ 586.95	646.55	752.61	65.000	431.94	620.34	752.31	889.63 1.	92.63	897.77 1.	3,39	582.24	748.49	32
	36.450	435.79	617.76	741.98	864.8	864.81 1,028.77			587.25	646.82	752.83	8.00	659	06 619 06 619	752.48	889.58	87.82	903 49	8	583.85	752.18	33
		436.08	617.83	742.06	865.29	865.29 1.029.72	460.69	1	2 587.32	889	752.89	67.000	123	619.69	752.02	880.08	800	200	337.70	280.60	752.13	98
	36.850	437.56	630.47	779.31	922 05	5		× 25.	5,155	7	753.03		77	300		20.00	2000		250 022		~ ×	
ĺ							┛	1			***	3	+	000	3	00	1000					

TABLE F.4.2(2) FLOW RATE FROM HD CALCULATION IN THE RIO CHANE-PAILON BASIN

2	Chainage in HD		n flow rate	Maximum flow rate from probable flood (m ³ /s)	vable floor	d (m ³ /s)	Maximum flow		rate from probable flood (m ³ /s)	ble flood	(m ³ /s)	Chainage in HD		Maximum flow rate from probable flood (m^3/s)	from pro	able flood	(s/¿w)	Maximum	flow rate	Maximum flow rate from probable flood (\mathfrak{m}^3/s)	ble flood ((s/, a
2	Model		Existin	Existing cross section	tion			Design	esign cross section	g g		Model		Existin	Existing cross section	non	-		Design	Design cross section	υo	
	E	2 year	5 year	10 year	à	SO year	2 year	5 year	10 year		50 year	(yan)	2 year	5 year	10 year	10 year 20 year 50 year		2 vear	2 wear	10 year 2	20 year 5	50 year
Chane	69.450	448.29	617.70	748.28	886.73	886.73 1,088.54	908.13	1,329.54	908.13 1,329.54 1,578.06 1,758.77	,758.77	1,938.44	83.300	478.53	643.62	746.50	880.86 1.082.85		928.38	378.77	1,378.77 1,634.14 1,823.24 2,013.8;	823.24 2	.013.87
	69,550	48.42	617.61	748.05	886.62 1,088.41	1,088.41	\$7.75	1,329,42	1.578.24	.759.16	1,939.05	84.300		646.31	747.59	880.66 1,082.51	.082.51	928.35	374.92	928.35 1,374.92 1,634.52 1,825.79 2,016.92	8.5.79	0.6.92
	70.050	449.61	617.38	747.18	886.21	886.21 1,088.01	806.88	1,329,01	906.88 1,329.01 1,579.57 1,761.19 1,942.46	761.19	92.46	85.200	573.62	797.49	950.97	101.94	269.91	,172.91	690.38	950.97 [1,101.94] 1,269.91 [1,172.91] 1,690.38 [1,972.46] 2,178.29 [2,405.27	178.29 2	20,27
	71.000	453.30	617.59	745.99	885.17	1,087.03	913.20	1,324.49	913.20 1,324.49 1,576.95 1,758.65 1,943.54	.758.65	,943.54	86.000	571.77	793.57	944.59	.092.00	264.53	. 161 16	682.78	944.59 [1,092.00] 1,264.53 [1,161.16 [1,682.78 1,967.13 2,173.23 2,398.46	173.23	398.86
	72,000	457.21	617.80	746.20	885.39	885.39 1,086.52	919.79 1,334.	1334.66	66 1,586.21 1,761.46 1,942.79	761.46	942.79	86.775	570.60	791.05	2.2	086.32	261.63	15204	678.71	941.24 1,086.32 1,261.63 1,152.04 1,678.71 1,963.96 2,168.83 2,392.52	168.83 2	397.53
	72,950	458.69	617.39	745.50	884 12	884.12 1.085.67	917.35 1,335		39 1,580.42 1,758.51	_	1,942,32	87.525	570.72	790 83	940.27	.084.65	260.60	,151,12	678.00	940.27 1,084.65 1,260.60 1,151.12 1,678.00 1,963.17 2,166.21 2,387.90	166.2]	387.90
	73.850	460.28	!	617.12 745.31	83.83	883.81 1.085.42	919.67 1,337	1,337,97	97 1,583.82 1,758.57 1,943.92	758.57	93.92	87.950	570.90	L. i	940.55	085.05	261.13 1	151 34 I	678.28	940.55 1,085.05 1,261.13 1,151.34 1,678.28 1,963.39 2,153.14 2,351.85	153.14 2	351.85
	74.750	L	617.30	4	883.58	883.58 1,085.23	925.85	925.85 1,347.03	1,587.74 1,764.98	764.98	952.20	88.050		791.07	940.63	085.16	261.28 1	. 151 43 1	678.38	940.63 [1,085,16] 1,261.28 [1,151.43 [1,678.38] 1,963.49 [2,153.23 [2,351.94	153 23 2	35.94
	75.525	L	618.52	745.66	883.74	883.74 1,085.29	931.05	1,354,72	931.05 1,354.72 1,596.39 1,774.39 1,962.70	774.39	962 70	88.500		571.13 791.25	940.90	195.280	261.86	,151.67	678.73	940.90 [1,085.56 [1,261.86]1,151.67 [1,678.73]1,963,66 [2,153.43]2,352.08	153,43 2	352.0k
	76.175	468.03	620.53	745.39	883.42	883.42 1,085.01	933.39	1,358.48	933.39 1,358.48 1,600.06 1,778.77	778.77	1,967.94	89.300			940.59	.085.20	261.92	15151	676.22	940.59 [1,085.20] 1,261.92 [1,151.51] 1,676.22 [1,961.33] 2,152.15 2,351.02	152.15 2	351.02
•••	76.800	468.09	622.23	745.17	883.07	883.07 1,084.72	930.08	1,359.08	930.08 1,359.08 1,601.80 1,782.00 1,972.45	782.00	.972.45	% 100	570.87	390.40	939.74	60.780	261.20 1	,148.94	,670.46	939.74 1,084.09 1,261.20 1,148.94 1,670.46 1,956.60 2,149.52 2,348.97	149.52 2	348.97
	77.400	468.30	623.89	744.98	882.78	882.78 1,084.44	928.73	1,359.47	928.73 1,359.47 1,602.40 1,783.65 1,974.00	.783.65	.974.00	90.917	570.43	789.48	938.68	.082.72	260.09	,144.52	62.28	938.68 1,082.72 1,260.09 1,144.52 1,664.20 1,951.93 2,147.06 2,347.14	147.06	X7.12
	77.975	468.81	625.53	744.82	882.52	882,52 1,084.21	928.41	1,361.62	928.41 1,361.62 1,603.82 1,784.14 1,975.05	784.14	375.05	91.750	570.12	788.89	938,14	.082.10 1	259.56 1	141.24	85.659.	938.14 [1,082.10] 1,259.56 [1,141.24 [1,659.58 [1,948.50] 2,145.32 [2,345.86	145.32 2	345.86
	78,525	469.32	656.99	744.63	882,22	882.22 1,083.94	927.90	927.90 1,362.91 1,605.41		1,786.44	1,976.57	92.583	570.14	788.69	938.03	.081.95	259.59 1	139.30	,656.77	938.03 [1,081.95 [1,259.59] 1,139.30 1,656.77 [1,946.38] 2,144.33 2,345.15	144.33 2	5.15
	79.075	470.29	628.63	744.49	881.92	881.92 1,083.69	931.80	1,367.12	931.80 1,367.12 1,608.32 1,790.53		1,978.08	93.500	570.34	788.77	938.21	,082.21	260.00	.138.47	.655.43	938.21 1,082.21 1,260.00 1,138.47 1,655.43 1,945.48 2,143.95 2,344.92	143.95	9.4
	79.625	471.50	630.30	02.4	881.89	831.89 1.083.68	935.20	935.20 1,370.48 1,612.47	1.612.47	1,795.33	1,983.42	94.500	570.66	789.09	19:886	.082.74	260.73 1	.138.60	655.39	938.61 [1,082,74] 1,260,73 [1,138.60] 1,655,39] 1,945,53 [2,144,21] 2,345,21	144.21 2	345.21
	79.950	472.18	644.63	891.25	881.88	881.88 1.083.67	937.49	937.49 1,370.81	1,614.32 1,797.95	797.95	1,986,44											
	80.050	472.45	631.66	744.53	881.88	881.88 1,083.67	938.19	938.19 1,370.97	1,614.94 1,798.75	. 798.75	1,987.37											
	80.550	473.49	633.28	744.53	881.86	881.86 1,083.67	941.68	1,372.85	941.68 1,372.85 1,618,12 1,802.97 1,992.11	.802.97	,992.11	-										
	81,450	475.86	636.41	744.73	881.86	881.86 1.083.43	947.60 1,381.	1,381.16	16 1,627.33 1,812.72 2,001.42	.812.72	,001.42											
	82,350	477,43	640.44	744.58	₹ 8.188	881.04 1.082.91	939.58	1,380.83	939.58 1,380.83 1,631,12 1,818,19 2,008,26	818.19	92.800											

TABLE F.4.2(3) FLOW RATE FROM HD CALCULATION IN THE RIO CHANE-PAILON BASIN

	Owinage.		n flow rate	Maximum flow rate from probable flood (m)	able flood	(w/w)	Макіти	m flow rat	Maximum flow rate from probable flood (m ³ /s)	bable floor	(m)(s)		Owner on HO	L	n flow rate	Maximum flow rate from probable flood (m ³ /s)	uble flood	(m ³ /s)	Maximun	n flow rate	Maximum flow rate from probable flood (π^3/s)	the flood	(9/,Ш
Kiwer	1 P		N. Carlotte	Note that order controls	acat.			Design	Design cross section	SOD:	Ī	× ×	.Wode!		Existin	Existing cross section	THOM			Design	Devien cross section	u)	
	(J.)		s year	Syear 10 mar 20 year	20 year	A year	2	S veak	30 year	20 year	50 year		§	2 vear	y year	10 wer	30 Value	10 year	2 wear	203.53	23 40	256 02	7 (O W
Parion	005.0			10 891	202.61	250.91	S S	135.51	0.80	207.0	300	3 6		2000	02.5	3 29	197.65	8		35.5K	30.52	15.65	07.70
	00°			\$.	8	25.72	8 8	01.0	109.13	30.00	3		26200	83.80	18.47	65.84	197.52	8	1.8.05	202.83	230.85	255.36	293.00
	2.00	\$ \$ \$	9	3 5	70.80	250.26	02.60	137.30	171.60	30,70	25.02		27.000	81.44	07.96.1	165.26	197.35	43.37	0.96.10	201.0	229.58	23.52	
_	3 8		3,0	× 7.	3,00	7. 19.	92.72	17774	172.45	209 75	261.34		27300	60.6	135.23	8.80 8.80	196.78	25.15	55.86	3	28 28	8	[0.5]
_	2 200	1	137.18		210.05	261.85	91.87	137.17	172.29	\$10.05	261.85		28.633	202	2. 8	15. 15.	18.08	8	-	9 5	e e	8 8	2
	9		503	111.40	133.77	167.08	8.73	8	11.40	133.7	96.79		8		28.82	8	200	9 8 8 8	55.63	200	89 01.4	8	5
	7.500	1	90,36	111.13	133.2X	×.	9	8		ñ.	3		70.00	26,60	22.7	8 5	1 4	2 5	A77.X3	} } }	6,259	1.4	827.46
	90 ×		90.33	11	01381	47.991	63.27	90.35	11004	0.55	8	-	000	1	330.60	77.00V	× × ×	\$30.67	26,22	3	652.85	714.19	22.72
	90° •	63.31	Ş. Ş.	_	133.20	86.93	6.31	8 2	100.V	2.5	8 (800	Ι.	100	176.0	2.4	99.40	4333	\$62.07	KC 259	714 12	825.37
	10.433	65.33	8 8		133.65	25.73	2 S	3 8	2010	11.1.4.V	1		13,600	2.057	327.33	74.04	432.57	508 12	428.33	86199	95.26	714.00	E24.03
	8	3	3 / S	2 2	9 3	10.47) 3 V	8,00	5	1		Vgo	935.0	82.15	115.75	137.75	159.07	185.66	82.15	115.75	137.75	154.07	145,000
	12.167	8	3 3	20.0	3	77.42.	8 S	3,00	110.42	17.16	179 (9	New Y	98	23.26	335.87	401.57	465.09	8	5.5	335.87	40.57	60.09	4
	200	63.48	ş ;	10.42	2 2	OF / 91	\$ S	8	110.4	33.68	67.69		218	4.27	\$ 12	\$60	603	639	1.5	5.32	9	603	9
	2,72	2 6	9	10	13381	9/9	63.62	0.00	110.55	133.81	16763	Chico D	0.375	3	18547	271.0	343.05	6 54	3.0	276.83	ξi ξ	335 651	30,00
	4.075	168	93.60	114.07	134.02	187.K7	21.69	09'66	1 4.0	174.02	67.87		21.1	08.80 20.80	15.75 36.75	70.74	\$	4	1970	107	20,40	, F	2,7
	14.975	20	11227	132.16	153,60	18.981	X2.33	113.77	132.16	153.60	18.6.51		8	2	8 ,F	3	700	37.37	2	0.7	3 5	130	001
	15.925	93.39	127.19	150.61	1,4.56	210.08	337	127.18	150.65		210.15		200	5 2	05/04/4	17 E V	1000	6	200	1.00	314.9	47.	31.40
	16.4.10			16.9 19.9	98.46	1 2 2 2	25.65	9 5	6 \ 6 \ 8	\$ 16. 20. 20.	3,4		2.725	163.21	\$633	02.597	19.48	088.35	130.01	271.03	314.94	36.14	331.71
	2 \{ 2 \{ 2 \}	1		10.0	2000	770 47	3 8	145.65	17.5	200.66	239.63	VQQ	0.200	65.33	279.41	332.39	382.86	446.34	.00.K7	279.43	332.44	383.03	6,46
	2 2	8 .	14.00 P	\$ 50 E	321.00	267.01	2 2	0×.09	191.25	65,122	263.47	Tore	0.450	214.66	279.47	32.1	34.364	5.75	ž		š	S S	476.08
	2 2	1	12.61	200.76	8,72	246.95	127.59	175.72	20 × 02	242 58	287.78		0.00	\$ 82	33.5	22	2	3	236.85	279.60	7,010	382.98	3
	0580	Ł	8	328.05	263.25	3.18	138.02	180	525.80	261.79	312 07		1.067	8.3	239.81	4	36X.7k	477.65	28.72	2.79.K.	٠ بر	3.	7
	3,00	ŀ	205.19	1	284.31	335.44	148.39	205.44	244.70	285.12	38.8	•	2000	201-52	\$	8	6 C	8 2	4 s	100	3 5	97.03	2 <u>4</u>
	21.250		71		2,86.20	349.2	3	213.80	24.8	207.15	8		2,33	3 5	1,5	1 2	٠ ۲ ۲	9 9 9,5	10.00		418.72	X9 6X	25.96.7
	31.380	155.32	1		3 3.	81.8	55.37	215.48	7.0.87		77.77		300	\perp	8	33631	363.48	432.42	203.67	285.13	416.81	961.39	A. 13
	2133	_!		- 1		20.00	0 1	100	77 176	77 8	8		2000	4	413.60	£ 4.97	5.8.4.1	601.40	308,89	413.05	486.42	534.12	616.01
	22.78	100		282 3	9 1	205.33	1X0 58	252.40	\$ 00.	15.73	412.26		2.800	312.16	418.16	489.08	535.49	606.53	311.88	416.14	490.36	\$39.93	13
100	0.450	-1	0.70	10.00	10.63	\$2.85	36.16	33	397.60	16/54	536.23		90,9	316.18	42.47	90 T67	0 0 0 0	80 89	38	22	\$ 5	£	63.0
2 4 2 5 2 5	9	1	I A	0	18.49	27.77	24.88	341.14	406.27	467.K7	57.72		28	320.25	425 7K	494.07	243,62	; ;	8	Ş.	200	9. 19.	3
	2.40	1	XXX.	414.83	478.14	560.10	36.00	348.79	414.83	478.34	01 095		8,5	318.41	6	2	14.00	Q (9.5	0	¥ \$	2 2	5 5
	3.150		354.89	422.57	4. CS	571.37	22.76	3	225	7	\$21.37		3 8	100		2 /2	3.00 KI	58X 74	2 2	4.58.73	Ş	\$ 7.	Š
	4.050		360.0	- 1	8	9 S	255.39	0000	20,00	100	3 5		9.9	2252	8	323.75	38.88	503	335.21	432.09	\$05.88	\$60.60	648.77
	4	3 5		\$ \frac{1}{2}	2 S	2,17	06.0%	01.961	4.037	15:53	613.73		200	226.38	286.14	324.35	359.16	405.27	338.90	435.82	\$10.4K	567.33	651.23
) () () () () () () () () () (97	389.7	45046	533.38	629.43	Z.	382.71	459.47	\$33.39	629.43		009'01	223.07	3. 3.	8 7,	350 21	11 50		4.19.5	212.03	27.5	654.12
	7.738	40.45	386.83	466.37	\$42.49	15	264.43	3	\$66.35	(T	₹ 8:		\$ \$	122	283.91	7	70 S	8 8	000	43.12	27.50	3 77.7	200
	X.667		277.04	15.43	900	306.40	2.5	2,65	315.05	350.70	\$		02.5.61	277	20.02	2 5	C# 151	0 0	21.44	10.01	1	17.12	76.87
	8	3.7	23.78	3 2	357.671	404	213.65	200.55	2.5	36.65	412.63	Maras	0.450	¥ (%	1000	8	1	17.16	17 18	110.01	25.023	SE ##	1.23
	300	- 1	- 1	ţ	370.33	420.76	23022	287.93	335.78	378.67	421.57	_	0090	12.1	10:74	114.85	50.	3	 8 	102.03	115.26	8	\$
	12,400	1	1 1		1,76.00	427.98	22.5	30.46	3.15.8	377.14	£		1.087	83.08	103.63	17.01	20.50	. y	25.00	103.50	12 24	1 5	0
	8	33	28.00	339.73		7	5,52	8	ž.	38,380	430.19		7000	190	30.5	74.71	146.39	9	8	100	12.4	67.14	0.7
	14.017	226.28	288.70		385.4×	24.5	33.00	20,50		380 53	1 2		37.	ES	116.18	8	6.41	165.37	92.47	115.52	130.82	146.27	167.92
	200		. [S	3		36 15	8	352.16	397.07	3		4,700	58.86	13321	13.0	164.86	188 21	8,5	124.98	139,43	160.10	98.
	9	100	1	13/2/	18 S	36.50	23, 13	444.03	354.71	396.07	452.34		5.500	102.89	75.05	59.93	180.33	35.73	8 4	5. 1.0	151.37	74.75	20065
	6.250		19091	190.98	241.26	313,19	163.34	745.42	278.32	289.56	35.		5.325	77.11	5.38	12	25.5	3	35.7	145.43	16.347	187.38	2
	16,717	1	П	ន	207.14	28.27	06.65	01.80	237.38	265.99	200				*	1	8	90.00			1 1 1 1 1		
	2.5	100		15.84 15.84	7 S	255.23	3	203.95	231.76	25×91	26.50												
	5	8	Т	167.9K	202.84	8,53	15.33	203.96	231.93	259.07	296.23												
	0.X.61	1	138,66	(0.80	202.93	35.46	158.39	203.88	212.05	259.15	296.38												
	20,550	1	138.65	168.05	202 MK	23	158.48	203.82	272.22	229.26	\$												
	8	1	<u>چ</u>	167.80	202.61	32.83	S. 3	20.47	33.80	257.97	90.56												
	8 8	- 1	17.78.1	\$ 5 \$	202.14	35.15	58.48	20402	317	28697	24.62												
	23,717	67.53	36.86	- -	197.01	877.8	158.44	204.08	271.94	256.92	294 62												
ļ		ł																					

TABLE F.4.2(4) FLOW RATE FROM HD CALCULATION IN THE RIO CHANE-PAILON BASIN

n³/s)		7. Year	477.90	486.45	£.	8	.05.83	212.90	21.50	531 38	<u>4</u>	1505	Ç	0. 0.	577.16	579.95	383.74	8 8 8	3	603.19	597.73	5K3.79			
Maximum flow rate from probable flood (m^2/ϵ)	e.	20 year 5	406.25	413.38	41 S. S.	424.50	429.87	435.75	8	451.25	450.37	467.52	476.00	4X3.60	488.05	435.44	492.67	498.23	\$ 400	50K.35	307.76	487.60			
norm probal	Design cross section	10 year		357.0	X.75	366.77	370.94	375.91	382.07		395.84	402.76		4 6.46	420.50	L			436.41		433.36	418.82			
flow rate fi	Designo		_			ı	312.39		321.59		1	į '		L_	1	356.37		li		Ļ	363.37	369.05			
Maximum			L.						230.48		238.34	242.24		L		253.61		نيا	58.47		259.16	253.86			
	-	40 year 2	478.86					514.22			L	Ш				1					59.60	504.52			
Maximum flow rate from probable flood (m^3/s)	uo	30 year 1.50	403.64	_ `	421.62	Ш		4.38.75		L		471.01	479.62		492.10	\$ 30		Ц.	66.50	515.65	516.01	510.0K			
om probat	Existing cross section	10 year 20	54.34	_:	\$6.38		Ļ				L_			23.23	425.43	42X.00		Щ.	2 2	146 SE		70 1			
flow rate fi	Existing	5 year	300.23		309.32	١.	Ц	321.71	ł I		<u>_</u>		ш		359.43	¥6.31			372.89	377.42	37K.S7	32			
Maximum		2 year	217.34	L	221.55		227.57	2,30,31	!	L.	241.91			3	14.7	2:6.72	, i	258.37	261.14	264.14	265.10	262.59			
9.	Mode	<u>``</u>	11461		<u>. </u>			23,333	24.175		L.			_	0000	L			3,438	7		36.063			
<u>0</u> -				_				L	L		1				L							<u>!</u>			
	: 	_	Vac	Chemic	-			_			_					<u>-</u>						_			
đ (m³/s)		Allow Oc.	331.71					L	L	≅ 3	!_			375.55		30) 19					33.22		448 8.I		05-194
bable floo	coon	Jest OC		257.55	258.43	_	١.			,	L	306.74	31.89	336.7	327.10	333.68	3,19.09	346.73	355.38	361.56	370.70	376.59	382.10	389.1	357.5K
	8	10 year	2.6.34	220.15	220.91	223.87	230.57	2.668	243.49	250.20	256.86	263.35	269.71	27.580	281.20	247.04	292.91	200.57	307.04	4.15	3	=	2,1	9	343.50
o from pro	o eros	10	ř.	7	ន	۶	Ė	74		!	•	ì					1	۲.	ľ,	ñ	3.040	325.51	3.0	n	
im flow rate from pro-	Design cross section	5 year 10	200.67 2.9	L.				_		!	•	221.64		Ļ	237 51	241.95			Ĺ			274.41 325	27x 33 3.10	283.31	289.27
Maximum flow rate from probable flood (m³/s)	Design cros	┝	200.67	_		87.95	99.56	198.78	204.52	210.22	215.94	221.04		232.57	237.51	241.95	247.15	252.69	Ĺ	264.87	270.16	274.41		204.97 283.31 3	209.10 289.27
(s/,	Design cross	2 year	14H,54 200.67	137.45 184.71	137.88 185.74	139.55 187.95	99.56	147.09 198.78	331.40 151.05 204.52	340,36 154.98 210.22	158.87 215.94	162.77 221.64	366.70 166.62 227.19	374.96 170.43 232.57	17,3 44 23,7 51	241.95	179.92 247.15	183,70 252.69	188.09 258.92	192,37 264.87	196.06 270.16	198.64 274.41			
(s/,		year 2 year 5 year	14H,54 200.67	300.83 137.45 184.71	137.88 185.74	139.55 187.95	143.32 193.66	147.09 198.78	331.40 151.05 204.52	154.98 210.22	158.87 215.94	162.77 221.64	366.70 166.62 227.19	374.96 170.43 232.57	173 84 237 51	176.46 241.95	398.39 [79.92] 247.15	407.34 183.70 252.69	188.09 258.92	192,37 264.87	435.73 196.06 270.16	198.64 274.41	201.46		209.10
(s/,		year 2 year 5 year	14H,54 200.67	300.83 137.45 184.71	301.83 137.84 185.34	225.54 262.91 305.95 139.35 187.95	232.07 270.46 314.84 143.32 193.66	238.08 277.53 323.14 147.09 198.78	331.40 151.05 204.52	251.45 292.34 340.36 154.98 210.22	349,33 158.87 215.94	264.71 307.44 358.16 162.77 221.64	271.22 314.70 366.70 166.62 227.19	277.54 321.69 374.96 170.43 232.57	383.00 173.84 237.51	334,98 391,39 176,46 241,95	340.60 398.19 (79.92 247.15	348,31 407,34 183,70 252,69	417.5% 188.09 258.92	365.20 477.26 192.37 264.87	435.73 196.06 270.16	442.88 198.64 274.41	384,0K 449,67 201,46	391.31 458.22	7 468.44 209.10
(s/,	Existing cross section Design orox	20 year 50 year 2 year 5 year	14H,54 200.67	300.83 137.45 184.71	191.20 222.57 259.45 301.83 137.88 185.34	193,65 225.54 262,91 305.95 139.55 187.95	199.15] 232.07 270.46 314.84 143.32 193.66	204.07 238.08 277.53 323.14 147.09 198.78	209.61 244.76 284.68 331.40 151.05 204.52	215.18 251.45 292.34 340.36 154.98 210.22	299,91 349,33 158,87 215,94	226.31 264.71 307.44 358.16 162.77 221.64	231.79 271.22 314.70 366.70 166.62 227.19	237.12 277.54 321.69 374.96 170.43 232.57	241.97 283.42 328.23 383.00 173.84 237.51	334,98 391,39 176,46 241,95	251.57 295.26 340.60 398.19 (79.92 247.15	257.11 301.95 348.31 407.34 183.70 252.69	263.36 309.44 356.97 417.58 188.09 258.92	316.60 365.20 427.26 192.37 264.87	274.70 322.97 372.43 435.73 196.06 270.16	278.97 328.24 378.38 442.88 198.64 274.41	333,20 384,0K 449,67 201,46	2K7 92 339.39 391.31 45K.22	293.99 346.75 399.87 468.44 209.10
		10 year 20 year 50 year 2 year 5 year	240.01 281.54 332.6K 148.54 200.67	142.22 190.61 221.84 258.60 300.83 137.45 184.71	142.62 191.20 222.57 259.48 301.83 137.88 185.34	193,65 225.54 262,91 305.95 139.55 187.95	232.07 270.46 314.84 143.32 193.66	204.07 238.08 277.53 323.14 147.09 198.78	244.76 284.68 331.40 151.05 204.52	215.18 251.45 292.34 340.36 154.98 210.22	258.10 299.91 349.33 158.87 215.94	226.31 264.71 307.44 358.16 162.77 221.64	231.79 271.22 314.70 366.70 166.62 227.19	237.12 277.54 321.69 374.96 170.43 232.57	177.28 241.97 283.42 328.23 383.00 173.84 237.51	179.65 246.33 289.30 334.98 391.39 176.46 241.95	183.05 251.57 295.26 340.60 398.19 179.92 247.15	186.88 257.11 301.95 348.31 407.34 183.70 252.69	191,30 263,36 309,44 356,97 417,58 188,09 258,92	195.65 269.36 316.60 365.20 427.26 192.37 264.87	274.70 322.97 372.43 435.73 196.06 270.16	278.97 328.24 378.38 442.88 198.64 274.41	282.92 333.20 384,0K 449,67 201,46	2K7 92 339.39 391.31 45K.22	346.75 399.87 468.44 209.10
Maximum flow rate from probable flood (m ² /s)	Existing cross section	Syear 10 year 20 year 50 year 2 year 5 year	150,39 204,96 240,01 281,54 332,68 148,54 200,67	142.22 190.61 221.84 258.60 300.83 137.45 184.71	142.62 191.20 222.57 259.48 301.83 137.88 185.34	144,20 193,65 225,54 262,91 305,95 139,55 187,95	147.81 199.15 232.07 270.46 314.84 143.32 193.66	151.41 204.07 238.08 277.53 323.14 147.09 198.78	155.20 209.61 244.76 284.68 331.40 151.05 204.52	158.97 215.18 251.45 292.34 340.36 154.98 210.22	162.69 220.77 258.10 299.91 349.33 158.87 215.94	166.48 226.31 264.71 307.44 358.16 162.77 221.64	170.28 231.79 271.22 314.70 346.70 166.62 227.19	174.00 237.12 277.54 321.69 374.96 170.43 232.57	177.28 241.97 283.42 328.23 383.00 173.84 237.51	179.65 246.33 289.30 334.98 391.39 176.46 241.95	183.05 251.57 295.26 340.60 398.19 179.92 247.15	186.88 257.11 301.95 348.31 407.34 183.70 252.69	191,30 263,36 309,44 356,97 417,58 188,09 258,92	195.65 269.36 316.60 365.20 427.26 192.37 264.87	199.17 274.70 322.97 372.43 435.73 196.06 270.16	278.97 328.24 378.38 442.88 198.64 274.41	205.41 282.92 333.23 384.0K 449.67 201.46	208.78 287.92 339.39 391.31 458.22	293.99 346.75 399.87 468.44 209.10

TABLE F.4.3 WATER LEVEL FROM HD CALCULATION IN THE OKINAWA DRAINAGE

		Channage	Act.		Existing		Maximu	Maximum water level from probable flood (m)	wel from p	robable fle	(m) po	Maximu	Maximum water level from probable flood (m)	vel from p	robabic f	000 (m)
C. C. C. C.	Carrion	H	Ω		3			Existn	Existing cross section	ction			Desig	Design cross section	COOU	
3				Left Bank	Riverbed	Riverbed Right Bank	2 year	5 vear	10 year 20 year	20 year	50 year	2 year	5 vear	-	20 vear	50 year
Owen	No 24	T-	Variation Variat	252,000		252,000	252.470	252,000 252,470 252,810 252,840 252,990 253,190 251,930 252,220 252,400	252.840	252.990	253.190	251.930	252.230	252.400	252.580	252.810
	No. 23	5.200	21.652	251.590	247.540	251.555	252,110	21.682 251.580 247.540 251.555 252.110 252.240 252.390 252.480 252.610 251.620 251.850 251.890 252.110 252.260	252 390	252.480	252 610	251.620	251.850	251.990	252.110	252.260
	No. 22	6.300	20,550	250.970	50 250.970 249.410	251.212	251.890	251.212 251.890 252.000 252.130	252.130	252.210 252.320 251.430 251.620 251.730 251.830 251.950	252 320	251 430	251.620	251.730	251.830	251.950
	No. 21	000.7	19,839	250.972	249,472	251.072	251.730	39 250.972 249.472 251.072 251.730 251.740 251.880 251.940 252.020 251.110 251.300 251.380 251.440	251.880	251.940	252 020	251.110	251.300	251.580		01010
	No. 20	8.400	18 429	250.316	129 250,316 249,161	250.381	251.570	250,381 251,570 251,530 251,720 251,770 251,850 250,540 250,810 250,930 251,020	251.720	251.770	251.850	250,540	220,810	250.950	221.020	37.10
	No. 19	9.300		70 250.744	249.214	249.214 250.744 25	251.470	1,470 251,430 251,610 251,660 251,740 250,330 250,610 250,740	251.610	231.680	251.740	250 330	250.610	250.740	20.00	20.53
	No. 18	10.100	16.711	250.348	249.762	250.468	251.300	249,762 250,468 251,300 251,270 251,450 251,510 251,580	251.450	251.510	251.580	250.150	250.150 250.440 250.570 250.670 250.760	250,570	220.670	200
	No. 17	11.100	15,740	740 250.595	248.775	251.155	251.010	248.775 251.155 251.010 250.590 251.160 251.220 251.230 249.920 250.210 250.330 250.430 25.530	21.18	251.220	251.290	249.920	250.210	30.33	36.65	250.05
	No. 16	12.000	14,807	807 250.425	248.483	251.281	250.650	248,483 251,281 250,650 250,640 250,800 250,860 250,970 249,720 250,000	250.800	250.860	250.970	243.720	30.00	3	2000	01000
	No. 15	13,200	13,639	339 249.579	248.524	250.679	250,300	248.524 250.679 250.300 250.400 250.520 250.620 250.740 249.430	250.520	250.620	250.740	249.430	259.710 259.850 269.930	3 3 3	26.647	30.00
	No. 14	14,000	12,846	249.609	248.219	250.149	250,050	26 249.609 248.219 250.149 250.050 250.220 250.350 250.460 250.600 249.230 249.490 249.620 249.251 249.710 249.810	250.350	250.480	250.600	249.230	3,45	749.670	747./10	218 818
	No. 13	15.300	11.538	538 248.720	247.015	248.810	249.810	747.015 248.810 249.810 250.020 250.170 250.290 250.430 248.820 249.230 249.400 249.400	250.170	250.29	250.430	248.920	249.230	35.35	3	5,0,5
	No. 12	15.900	10.968	248,711	247.081	248.916	249.760	247.081 248.916 249.760 249.970 250.110 250.230 250.370	250.110	250.230	250.3/0	248.75	248.750 249.080 249.230	V47.447	3.	20.74
	c Z	16 600	10 229	248.858	246.661	249.228	249.660	29 248.858 246.661 249.228 249.660 249.860 250.010 250.130 250.260 248.550 248.860 249.010	250.010	250.130	250.260	248.550	248.860	249.010	749.130	74.70
		18 300		248 719	245.914	248.789	249.170	248.719 245.914 248.789 249.170 249.350 249.470 249.580 249.700 248.050 248.330 248.450 248.550	249.470	249.580	249.700	248.050	248.330	248.450	248.550	248.650
		10.100	7,714	248,008	14 248 008 245 758	248 198	248.690	248.198 248.690 248.870 248.990 249.100 249.230 247.790 248.040 248.160 248.250	248.990	249.100	249.230	247.790	248.040	248.160	248.250	248.350
	No. S	20,600	6267	267 247,001	245.201	247 289	247,830	245,201 247,289 247,830 248,070 248,220 248,340 248,480 247,270 247,500	248.220	248.340	248.480	247.270	247.500	247.610	247.700	247.810
	No. 7	21,400	5,415	246.597	244.667	246 797	247.580	115 246.597 244.667 246.797 247.580 247.810 247.950 248.070 248.200	247.950	248.070	248 200	246,960	246.960 247.180 247.300 247.400 .447.510	247.300	34.48	010/47
	No. 6	22,400	4,433	246.567	245.247	246.807	247.260	133 246.567 245.247 246.807 247.260 247.460 247.460 247.770 246.410 246.580 246.680 246.000	247.570	247.670	247.770	246.410	240.580	340.680	0/20/	V. C. V. C.
	No. S	23.600		245.379	22 245.379 244.069	245.559	246.130	245.559 246.130 246.140 246.270 246.340 246.440 245.870 245.970 246.060 246.190	246.270	246.340	246.440	245.870	245.970	240.000	3	2/500
	No. 4	24.100	2,728	728 245.250	243.930	245.430	246.000	245.430 246.000 246.010 246.130 246.210 246.330 245.760 245.870 245.970	246.130	246.210	246.330	25.760	245.870	245.970	240.110	30.00
	No. 3	25.600	1,280	245.097	244.917	245.077	245,500	380 245.097 244.917 245.077 245.500 245.629 245.799	245.799	245.954 246.124	246.124	243.410	25.576 245.759	257.55	242.910 240.109	5000
	No. 2	26.500	302	244.929	243.077	244.869	245.290	002 244-929 243 077 244 869 245 250 245 450 245 640 245 830 246,020 245 249 249 620 245 820 245 820	245.640	245.830	246.020	245.250	2002	020.047	0.000	270.05
	No. I	26.800	0	244.414	242.944	244.704	245.200	0 244,414 242,944 244,704 245,200 245,400 245,600 245,800 246,000 245,200 245,200 245,400 245,000	245.600	245.800	246.000	245.200	245.400	30.047	245.800	240.082

TABLE F.4.4 FLOW RATE FROM HD CALCULATION IN THE OKINAWA DRAINAGE BASIN

	Chainage	Maximu	Maximum flow rate from probable flood (m^3/s)	e from pro	bable floc	(s/ _c m) po	Maxim	ım flow ra	Maximum flow rate from probable flood (m^3/s)	bable floc	d (m ³ /s)
Drainage			Existi	Existing cross section	sction			Desig	Design cross section	ction	
	(km)	2 year	5 year	10 year	20 year	50 year	2 year	5 year	10 year	20 year	50 year
Okinawa	1.000	32.830	41.586	75.128	79.205	84.509	14.995	22.601	28.128	33.782	41.554
	5.750	86.411	120.018	142.273	157.012	179.223	73.016	866.96	116.933	137.309	164.512
	6.650	97.692	137.304	163.922	181.646	208.703	86.237	114.875	138.528	162.822	195.120
	7.700	42.335	50.796	63.899	68.999	75.929	89.761	100.427	109.233	116.103	124.601
	8.850	43.161	51.970	63.918	600.69	76.087	95.472	108.325	116.174	123.302	132.527
	9.700	44.148	54.228	47.14	71.842	82.341	99.467	112.459	121.547	128.775	138.969
	10.600	36.800	44.675	59.544	64.654	71.774	103.936	118.544	128.237	135.747	144.214
	11.550	36.958	44.834	59.700	64.808	71.924	108.893	124.447	133.513	140.569	148.647
	12.600	37.133	45.010	59.875	64.984	72.099	114.543	131.765	140.726	147.466	154.936
	13.600	37.537	48.660	60.03	66.126	75.288	119.881	138.356	148.318	155.873	164.113
	14.650	41.743	54.236	65.248	74.385	85.388	125.657	146.045	156.713	165.131	174.722
	15.600	44.421	59.236	71.406	81.886	94.636	129.874	150.781	162.721	172.239	183,400
	16.250	46.556	62.787	75.821	87.208	101.114	133.280	154.790	167.108	177.244	189.385
	17.450	50.850	69.691	84.406	97.494	113.551	139.487	162.579	175.887	187.026	200.701
	18.700	55.385	77.095	93.567	108.465	126.844	146.126	170.895	185.500	198.066	213.809
	19.850	59.368	83.413	101.219	117.578	137.889	152.343	178.826	194.153	207.274	224.517
-	21.000	61.410	88.152	107.600	125.503	147.823	156.995	184.956	201.431	215.803	235.035
	21.900	63.135	91.950	112.657	131.765	155.645	160.433	190.053	207.197	222.462	243.256
	23.000	65.611	96.839	119.013	139.568	165.301	165.787	197.116	214.868	230.805	253.169
	23.850	36.891	44.635	56.643	62.231	69.931	107.945	117.026	119.561	125.492	141.090
	25.300	36.889	44.634	56.639	62.229	69.930	107.646	117.031	119.613	125.581	141.187
	26.650	36.888	44.634	56.639	62.239	69.930	107.645	117.031	119.614	125.582	141.188

TABLE F.4.5(1) WATER LEVEL FROM HD CALCULATION IN THE ARROYO YAPACANICITO, JOCHI AND TACUARAL

			Existin	Existing Elevation (m)	(w) uc	Σ		Maximum water level from probable floods (m) for existing and design cross sections	3	anic Iron	A 557 /447				
Arrovo	Section	Chainage in		•		2 Year	183	5	5 Year	10 Year	'car	20 Year	(car	50 Year	ង
		F/S (km)	Total	Bed	Right	Existing	Design	Existing	Design	Existing	Design	Existing	Design	Existing	Design
Yapacanicito		0000	283.02	278.61	2,82,36	282.95	282.95	283.37	283.37	283.60	283.60	283.79	283.79	28.02	22.02
	<u>, </u>	1.500	281.52	277.11	281.06	281,23	281.28	281.72	281.72	281.96	23. 28. 28.		282.16		282.40
		3,600	279.42	275.01	278.36	278.97	278.97	279.39	١.	279.63	279.63		279.85	١	80 80 80 80 80 80 80 80 80 80 80 80 80 8
		6,100	276.92	272.51	276.46	276.18	276.18	276.57	276.57	276.82	276.82	277.05	277.05	277.33	277.33
	-	009.8	274.42	270.01	273.96	274.37	274.37	274.48	274.48	274.54	274.24	274.61	274.61		274.69
		12200	270.82	266.41	270.36	270.05	270.05	270.26	270.26	270.37	270.37		270.48	270.62	270.62
	S	14,300	268.22	262.21	268.26	267.56	267.26	267.75	267.42	267.84	267.50		267.58	268.04	267.6
	Zo 2	14.320	268.22	262.21	268.26	267.44	267.11	267.61	267.28	267.70	267.42	267.78	267.51	267.87	267.6
	200	15.400	265.11	261.94		266.35	265.16	266.47	265.30	266.53	265.37	266.58	265.43	266.65	265.51
<u></u>	4 0	97,700	265.08	261.69		264.86	264.05	265.00	264.24	265.09	264.34	265.19	264.40	265.38	4,4
	20.5	17.100	262.85	260.39		262.67	262.51	262.71	26257	262.74	262.65	262.80	262.73	262.84	262.8
<u>-</u>	900	19,000	259.72	256.00	259.85	259.56	259.61	259.60	259.67	259.63	259.84	259.67	260.07	259.70	280.1
8	No. 7	20,000	257.77	255.32	259.68	257.60	257.62	257.65	257.72	257.68	257.87	257.72	258.05		258.1
· c	× OZ	20,400	254.71	252.78	256.60	255.79	25.96	255.89	256.11	255.94	256.19	255.93	25625		26.3
	S O	22,200	257.80	354.88	256.35	256.30	255.63	256.38	255.78	256.45	255.94	256.51	256.01		28
•	No. 10	23.100		254.24 257.95	257.95	255.52	255.33	255.58	255.45	255.74	255.61	255.81	255.69	255.83	25.7
· > :	Z o	24.100			255.07	255.59	255.44	255.69	255.56	255.75	255.66	255.81	255.71	255.88	255.80
	No. 12	25.300	Q.	253.39		255.50	255.31	255.60	255.46	255.65	255.54	255.81	255.71	256.02	255.9
	No. 13	26.200	253.98	252.91	256.31	254.40	254.22	27.73	254.58	254.95	254.83	255.16	255.04	255.40	25.3
	No. 14	27,000	253.70	252.04	255.56	254.40	254.20	33.25	2.27	255.04	254.90			255.52	25.4
	No. 15	28.100	255.88	252.31	253.64	253.51	253.32	253.93	253.77	254.17	254.04				2 2 3
· -	No. 16	29.100	255.18	251.65	253.17	253.29	23.12	253.72	253.57	253.97	253.85		254.08	``	X E
•	Zo. 17	30.100	254.60	251.36	252.38	252.56	252.37	252.97	252.82	253.22	253.09	253.44	253.32	253.69	S. S.
<u>'</u>	81 . 87	31.100	253.05	250.49	254.33	252.73	252.54	253.04	,	253.22	253.09	253.38	253.26	253.57	25. 26.
-	Se. 19	31.700	251.56	250.62	253.98	252.14	251.95	252.29	252.14	252.39	252.26	252.47	252.35	252.58	252.4
<u></u>		36.700	248.30	25.51	249.60	246.04	247.61	246.25	248.07	24635	248.34	246.43	248.59	246.55	248.8
	٠.	41.700	245.06	242.27	246.36	243.67	245.20	243.89	245.64	244.00	245.90	244.09	2,6,14	24 21	246.4
	٠	46.700	241.82	239.03	243.12	239.62	240.94	239.82	241.35	239.92	241.59	240.02	241.82	240.13	, 77 77 77
-		\$1.700	238.58	235.79	239.88	239.98	240.13	240.41	240.59	240.67	240.88	240.92	241.14	241.21	4 22
•	-	53.100	237.67	234.88	238.97	238.90	239.08	239.34	239.53	239.60	239.81	239.84	240.05	260.12	240.3
	1	58.100	234.43	231.64	235.73	239.35	239.67	239.82	240.16	240.09	240.42	240.32	240.62	240.56	240.8
	J	62.300	230.30	227.75	231.42	232.30	232.30	232.30	232.30	232.30	232.30	232.30	232.30	232.30	232.3

TABLE F.4.5(2) WATER LEVEL FROM HD CALCULATION IN THE ARROYO YAPACANICITO, JOCHI AND TACUARAL

Arroyo	Section	Chainage in			_	X			T.		5	20 Year	53	X Y	S.
		F/S (km)	ite (25	Richt	Existing	Design	Existing Design	Design	Existing	Sign	Existing Design	Design	Existing	Design
Jochi		0000	288 23	283.88	288 13		288.82	289.10	289 10		1	289.43	289.43	289.62	289.6
		3.000	284.23	279.88	284.39	284.69	284 69	285.16	285 16	285.43	285.43	285.65	285.65	285.90	285.9
		Γ	280.23	1	280.39	281.05	281.05	281.24	281.24	281.36	281 36	281.47	281.47	281.62	281.6
		9.520	275.49	271.88	275.11	276.47	276.47	276.68	276.68	276.81	276.81	276.92	276.92	277.06	277.0
		12,800	268.75	265.91	268.88	269.01	268.86	20.692	26892	269.07	268.96	269.08	269.00	269.10	269.0
	No. 1	13.800	29.997	264.83	266.32	267.63	266.35	267.69	26645	267.72	26651	267.75	266.56	267.78	266.6
	No. 2	15.000	265.08	262.11	265.08	265.11	264.7:	265.20	264.85	265.26	264.93	265.28	26.99	266.47	265.0
		15.010	265.08	261.03	265.08	265.27	22 22 38	265.43	264.83	265.42	8.8	265.42	8.88	888	265.8
_		15.020	265.08	262.11	265.08	265.08	264.66	265.17	264.83	265.22	26.88	265.25	26.2	265.71	265.0
E	No. 3	16.000	264.07	261.03	264.83	264.89	263.74	264.99	263.83	265.03	263.87	265.07	263.92	265.09	263.9
۵	No. 4	17.200	262.92	260.08	263.44	263.35	261 79	263.48	261.87	263.53	261.92	263.57	261.95	263,60	262.0
	No. 5	18.300	262.62	258 66	262.34	261.86	260.33	261.98	260.42	262.05	260.46	262.10	260.50	262.13	260.5
•	No. 6	19,000	261.55	257.75	261.02	260.95	259 44	261.08	259.53	261.14	259.58	261.19	259.62	26: 23	259.6
>	No.		260.78	256.80	260.60	260.70	259.42	260.84	259.51	260.92	259.56	260.97	259.60	8.18	259.6
•	No.	20 900	260.06		260.80	259.96	258.63	260.11	258.73	260.19	258.78	260.24	258.82	260.28	258.8
- E	No. 9	21.900	258.95	253.66	259.34	259.07	257.73	259.19	257.82	259.25	257.86		257.90	259.33	257.9
	No. 10	22.700	258.43	253.73	259.09	258.31	256.76	258.41	256.84	258.47	256.89		256.92	258.54	28
		22,710	258.91	253.73	259.09	258.44	256.96	258.76	257.16	259.08	257.42		257.24	259.42	257.5
-		22.720	258.91	253.73	259.09	258.20	256.68	258.31	256 77	258.36	256.81	258,41	256.85	258.44	256.9
_	Z	23.700	256.00	252.22	255.93	256.80	255.14	256.93	255.21	257.00	255.25	257.05	255.28	257.10	2553
	No. 12	24 900	2,4.19	250.38	254.33	254.59	252.69	254.66	253.13	254.71	253.28	ľ` '	253.34	χ. 8:	253.4
	No. 13	25.600	253.61	248.89	253.62	252.81	252.51	252.92	252.50	252.97	252.66	253.00	252.73	352.96	252.8
		29.700	251.36	24.03	251.88	246.75	245.98	246.07	246.22	246.27	246.40	246.47	246.57	246.69	28
		29.800	246.46	243.46	246.46	245.71	245.92	246.02	246.17	246.20	246.35	246.38	246.50	246.60	2,76.7
		35.800	245.50	242.34	243.55	243.72	243.74	243.82	243.85	243.88	243.92	243.93	8,4% 8,	23.8	24
		43.400	242.93	241.05	242.68	243.00	243.00	243.00	243.00	243.00	243.00	243.00	243.00	243.00	2430
Tacuarai		0.000		275.44	279.05	279.48	279.48	279.60	279.60	279.66	279.66	27.6.72	279.72	279.79	279.7
		3.000	275.73	271.8	275.57	276.14	276.14	276.31	276.31	276.41	276.41	276.49	276.49	276.59	2765
		0009	272.26	268.49	272.10	272.47	272,47	272.56	272.55	272.68	272.60	272.64	272.82	2728	272.6
		80.6	268.78	265.01	268.62	269.06	269.08	269.16	269.18	26921	269.23	269.25	3693	269.32	2693
		12.000		261.54	265.15		265.45	265.55	265.51	265.60	265.55	265.63	265.59	265.66	265.6
-	No. 1	16.800	260.35	255.88	260.49	260.58	259.92	260.72	260.34	260.74	260.41	260.76	260.42	280.7	2002
· E		16.810	260.35	255.88	260.49	260.63	259.98	24.18	263.80	260.79	260.46	- 1	265.55	267.63	267.4
	j	16.820	260,35	255.88	260.49	260.69	26.05 26.05	% % %	150.67	260.83	26.50	١	28 28	88	200
3. 1	No. 2	17.600	259.88	256.32	260.92	260.00	259.35	260.14	259.77	260.16	259.83	280.18	259.83	82.5	9
	No. 3	18.500	259.00	255.13	259.06 25	28.87	258.21	259.03	258.65	259.06	258.72	25.10	258.76	259.12	25.5
•	2. 4.	19.100	258.31	253.62	258.12	258.27	257.62	253.46	258.10	258.51	258.19	258.55	25821	258.59	258.4
>		19.110	23,752	253.62	258.12	258.51	257.85	258.45	258.05	258.77	258.42	288.95	258.61	259.32	25
ပ	1 	19.120	257.62	253.62	258.12	258.24	257.59	258.43	258.10	258.48	258,19	28852	258.18	258.56	258.3
8	No. 5	20.000	237.28	254.23	257.33	257.50	256.84	257.69	257.23	27.72	257.33	257.77	257.43	22/20	257.6
0	8	57.500 57.500	256.12	252.98	255.86	256.14	255.52	256.31	256.11	25635	256.18	28638	2569	256.41	138
c	No. 7	22.100	254.58	252.43	25.58	254.49	253.78	87.68	253.87	24.63	253.98	25,65	2 2 2 3 3	254.6	25
	No. 8	22.600	254.36	249.03	15.33	252.36	251.82	252.50	251.89	252.54	251.94	252.56	252.24	252.58	252.3
		27.500	245.41	240.19	245 22	245.77	246.00	246.08	246.25	246.26 246.26	2.6.43	246.43	246.58	246.61	246.8
		27.600	245.41	240.19	245.22	245.74	245.98	2,606	246.22	246.26	246.40	246.47	246.56	246.69	2.5
		32.100	243.30	239.30	243.50	04.445	244 24	27.4.64	24.69	744.76	24 84	2777	24.95	V3 776	245.0
			1		7		*	1			1	 	1	, ,	,

TABLE F.4.6(1) FLOW RATE FROM HD CALCULATION IN THE ARROYO YAPACANICITO, JOCHI AND TACUARAL

Arrovo	Chainnee in	2 Year		5 Year	Į.	10 Year	ar	20 Year	5 Year 10 Year 20 Year	50 Year	car
	F/S (km)	Existing	E C	Existing	Design	Existing	Design	Existing	Design	Existing	E SSI
Vapacanicito	0.750	138 59	138.59	191.55	191.55	225.63	225.63	258.77!	258.77	299.75	25.75 25.75
	0.5%	3.8.5	118.15	165,30	165.30	198.72	198.72	231.63	231.63	273.67	273.67
	4.850	101.18	101	138.92	138.92	167.74	167.74	197.73	197.73	236.37	2.6.5
	7.350	93.27	93.27	122.53	122.53	4,40	04.4	167.52		200.75	200.75
	8,610	52 63	52.63	60.02	60.02	65.10	65.10	72.95	72.95	83.13	85.13
	01.5.61	48.00	48.00	53.67	53.67	18.95	56.81	59.88	88.65	63.74	63.74
	14 110	48,00	47.50	53.67	53.68	26.80	\$6.80	59.88	59.88	63.73	63.73
	14 865	00 87	47.90	53.67	53.66	\$6.80	\$6.80	59.88		63.73	63.73
	14 900	48.00	47.98	53.67	53.66	26.80	56.80	88.65	59.87	63.72	63.7
	16.76	874	47.97	53.67	\$3.66	\$6.80	62.95	29.87	26.86	63.69	63.70
	80.0	47.80	47.96	53.67	53.65	26.80	56.75	\$9.87	19:65	63.64	63.4
_	9>*	8,4	47.96	53.66	53 65	\$6.79	56.75	59.87	i !	63.64	63,42
٠ (0	47 08	47.96	53.66	53.65	56.79	56.75	59.87	•	63.64	63.42
	20,200	27.92	47.96	53,60	53.66	\$6.74	56.74	59.82		63.59	63.4
_	21.300	47.26	47.97	53.05	53.67	56.23	56.73	56.33		63.15	63.39
_	22.640	39.58	48.02	4.3	53.70	47.08	\$6.74	49.83		53.30	63.3
•	23.600	39.48	48.25	12.27	53.74	47.02	8.7	49.78		53.26	63.39
>	24.700	39.37	48.93	44.20	\$4.01	16.93	56.85	49.73	59.62	53.19	63.39
	25.750	39.28	50.54	\$4.15	\$4.83	46.92	57.16	49.69		\$3.10	63.4
Ε	000.90	39.23	\$4.04	44.10	57.20	\$6.89	\$9.04	49,66		53.02	\$
.	27.550	39.23	57.40	4	61.63	46.85	63.54	49.63		52.91	70.01
-	28.600	39.33	61.22	45.89	3.8	49.57	68.78	52.83		15 65	77,04
	29.600	42.00	63,68	51.27	69,31	\$7.29	72.88			71.59	3
<u>.</u>	20 400	44 44	201.74	255.36	281.89	304.06	333.05			4:0.40	441.30
	31.400	181 97	201.74	254.75	281.38	303.36	332.19	350.80		409.55	440.3
	34,200	181.80	201.57	254.38	281.01	303.22	332.05	Í	379.57	408.81	439
	19.200	174 69	194.46	241,68	268.31	289.19	318.02		365.47	393.86	424.63
	44 200	56.98	186.72	227.55	254.17	273.22	302.05	319.80	348.36	375.55	406.3
	49 200	156.66	176.43	212.96	239.59	256.26	285.09		330.48	358.09	388.85
	52,400	264.65	296.83	364.26	405.33	428.81	476.94	86.067	\$45.35	570.69	\$50.59
	\$5,600	246.55	290.70	343.32	400 22	408.58	474,17			552.60	639 14
	204.00		10.00			37 33	77 8 VV	14.4.1	24.42	700 40	%0 VC V

TABLE F.4.6(2) FLOW RATE FROM HD CALCULATION IN THE ARROYO YAPACANICITO, JOCHI AND TACUARAL

Arroyo	Chainage in	2 Year	car	5 Year	ar	10 Year	çar	20	20 Year	50 Year	car
	F/S (km)	Existing	Design	Existing	Design	Existing	Design	Existing	Design	Existing	Design
ochi.	300	146.35	146.35	202.33	202.33	237,14	237.14	269.22	L	309.12	306
	4.500	143,41	143.41	199,10	02.00	233.90	233.90	266.17		306.41	306.4
	6.920	50.22	\$0.22	53.43	53.43	\$5.35	\$5.35	57.21		59.77	59.7
	9,620	46,51	46.51	50.24	50.24	52.39	\$2.39	\$2.2		56.71	56.7
	13.300	46.05	46.23	50.14	49.90	52.28	\$2.00	53.89			\$
	14.400	51,50	46.23	53.15	80.8	57.61	\$2.00	58.46	53.78		2. 4.
	15,003	54.65	4623	57.90	49.80	59.55	\$2.00	3.			56.43
	15.015	56.22	46.23	59.28	80.65	60.51	\$2.00	61.43	53.78	61.45	\$6.43
-	15,460	57.79	46.23	99.09	49.90	61.48	\$2.00	62.42	53.78		56.43
£	16.600	46.33	46.23	50.45	45.8	\$2.70	22.8	X 28	53.78		56.43
	17,750	46.02	46,23	49.89	8.64	52.13	25.00	53.67	53.78	\$2.89	56.43
	18.650	45.93	46.23	49.88	49 8	\$2.08	52.00	53.63	!	2	\$6.43
- (19,500	45.92	46.23	49.87	49.80	52.07	\$2.00	53.62		£ 83	56,43
-	20.450	45.90	46.23	49.87	49.90	\$2.05	\$2.00	53.61	53.78	83	\$6.4
>	21.400	45.88	46.23	49.86	49.80	\$2.04	\$2.00	53.61	53.78	\$ 1	56.43
v	22,300	45.88	46.23	49.86	8.64	52.03	52.00	53.61	53.78	\$ 3	56.43
E	22,705	45.87	46.23	49.86	49.90	52.03	\$2.00	53.61	53.78	4.2	56.43
٠	22,715	45.87	46.23	49.86	8.8	52.03	52.8 	\$3.60	53.78	25.23	56.43
c	23.210	45.87	46.23	49.86	86.64	52.03	\$2.8	53.60	•	X,72	56.43
-	24,300	45.86	46.23	49.85	68.67	\$2.02	8.12	\$3.60		54.68	56.44
	25.250	45.86	46.25	49.85	49.93	52.02	52.01	53.61	53.70	89.4%	:¥.
	27.650	48.64	104.59	\$8.04	141.30	62.31	153.26	84.93	175.46	62.62	200.33
	29,750	23.49	2.4	23.92	26.74	23.58	76.84	23.67		75.75	37.61
	32.800	19.70	20.48	25.91	26.79	30.11	31.13	3.6		27	87.11
	37.700	12.07	12.70	15.45	2	7.79	4.2	20.02		13. 12	31.20
	41.500	11.37	12.07	14.59	15.95	16.77	18.75	18.85		19.40	30.75
acuara	305.1	159.76	159.78	181,24	181.25	163.69	193.69	204.95		218.39	218.37
	4.500	158.70	158.75	180.28	180.27	192.66	192.63	203.73		216.89	216.87
	7.588	144.78	144.47	157.93	58.84	165.27	166.34	171.46		179.03	179.94
	10.500	<u>4</u>	143.78	158.05	158.86	165,49	166.73	171.84		179,53	180.53
	14.400	137.71	139.97	153.21	148.80	159.96	S	163.38	1	168.24	165.47
	16.80\$	168.07	153.32	183.51	198.74	198.46	217.94	207.07	- 1	229.20	242.69
€	16.815	168.35	177.72	173.51	<u>z</u>	8	201 16	203.05	1	217.50	Z3X Z
٩	17.210	146.01	140.12	4.8	80'68	184.51	180.67	3		178.89	222.32
_	808	27.10	140.12	151.02	148,82	8	167.50	157.85		3, 5	213.20
•	18.800	127.26	140.10	149.20	148 81	152.59	157.10	156.7	ı	158 30	205.97
>	19.105	155.37	140.16	161.65	162.64	166.41	172.59	197.48		203.37	225.36
•	19.115	169.62	158,74	169.88	75.77	183.09	95'681	3. 2.	١	205.28	209.32
E	19.560	112.02	140.16	135.07	148.83	141.09	177.77	145.83.		150.21	233.29
v	20.600	111.86	140.10	134.94	148.80	141.03	154.32	145.81		150.06	201.52
<u> </u>	21.650	111.54	140.10	134.74	148.80	140.92	154.32	145.78		149.71	180.31
<u>-</u>	22.350	111.77	140,11	134.81	148.80	140.95	154.32	145,80	171.58	149.53	189.90
	25.050	110.64	140.11	12.12	148.80	140.58	154.31	145.66		148.66	189.47
	27.550	103.63	128.86	127.83	151.16	138.11	165.15	148.32		159.88	198.78
	29.850	141.45	167.37	17.71	8.8	195.53	221.21	22.32	240.32	253.91	270.95
		-			1			The second second	-		

TABLE F.4.7 WATER LEVEL FROM HD CALCULATION IN THE ARROYO TACUARAL AND ANTOFAGASTA

t. Chainage in F/S (km) 10 0.000 290.93 289.03 289.03 290.90 9 1.010 290.93 288.89 292.46 8 2.225 290.60 286.05 290.87 7 2.975 290.28 283.89 290.94 4 5.706 283.38 280.13 284.24 4 5.706 283.38 280.13 284.24 4 5.706 283.05 277.15 287.32 2 7.579 280.87 277.15 287.32 2 7.579 280.87 260.40 260.90 26				Existin	Existing Elevation	(m) u	Maximur	n water le	Maximum water level from probable flood (m)	robable fic	(m) po	Maximui	n water le	vel from p	Maximum water level from probable flood (m)	od (m)
No. F/S (cm) Left Bed Right 2 year 5 year 10 year 292.05 No. 10 0.000 290.93 289.03 290.90 291.28 291.77 292.05 No. 9 1.010 293.33 288.89 292.46 291.00 291.47 292.05 No. 8 2.225 290.60 286.05 290.87 288.46 288.90 289.26 No. 7 2.975 284.79 281.85 280.94 286.41 286.78 289.26 No. 6 3.677 284.79 281.85 280.94 286.41 286.78 289.29 No. 5 4.860 283.05 278.16 283.45 282.35 282.35 No. 6 3.677 283.05 278.16 283.45 282.35 282.36 No. 7 4.860 283.05 278.16 283.45 282.35 282.56 No. 7 4.800 283.05 276.34 281.47 281.30 281.30 No. 12 </td <td>Arrovo</td> <td>Sect</td> <td>Chainage in</td> <td></td> <td>o o</td> <td></td> <td></td> <td>Existir</td> <td>ng cross se</td> <td>ction</td> <td></td> <td></td> <td>Desig</td> <td>Design cross section</td> <td>ction</td> <td></td>	Arrovo	Sect	Chainage in		o o			Existir	ng cross se	ction			Desig	Design cross section	ction	
No. 10 0,000 290.93 289.03 290.90 291.28 291.77 292.05 No. 9 1,010 293.33 288.89 292.46 291.00 291.45 291.70 No. 8 2,225 290.60 286.05 290.87 288.46 288.90 289.26 No. 7 2,975 290.28 286.05 286.05 284.96 286.73 287.08 No. 6 3,677 284.79 281.85 286.41 286.78 287.92 No. 5 4,860 283.38 280.13 284.96 285.39 282.36 No. 6 2,706 283.05 278.16 283.45 282.35 282.36 No. 1 8,706 283.05 278.16 287.32 281.80 281.90 No. 1 8,160 279.48 276.67 285.22 281.30 281.30 No. 1 1,042 260.40 260.10 263.00 263.00 263.00 No. 1 1,916 261.00 258.00)	ç	F/S (km)	Left	Bed	Right	2 year	5 year	10 year	20 year	50 year	2 year	5 year	10 year	20 year	50 year
No. 9 1 010 293.33 288.89 292.46 291.00 291.45 291.70 No. 8 2 225 290.60 286.05 290.87 288.46 288.90 289.26 No. 7 2 2975 290.60 286.05 290.94 286.41 286.78 287.08 No. 6 3 677 284.79 281.85 283.33 283.33 283.35 282.54 No. 5 4 860 283.38 280.13 284.96 282.37 285.59 No. 6 2 879 281.85 287.35 284.96 282.36 282.39 No. 7 4 860 283.38 280.13 284.34 282.35 282.39 No. 12 0.000 262.30 260.90 263.00 263.05 261.89 281.30 No. 11 1.042 260.40 260.12 262.20 261.99 263.45 263.63 No. 10 1.916 261.00 258.00 261.00 258.00 258.00 258.00 258.00	Teiens	S S	0000	290.93	289.03	290.90	291.28	291.77	292.05	292.25	292.42	289.61	290.25	290.67	290.95	291.19
No. 8 2.225 290.60 286.05 290.87 288.46 288.90 289.26 No. 7 2.975 290.28 283.89 290.94 286.41 286.78 287.08 No. 5 4.860 283.38 280.13 284.24 285.27 285.59 No. 4 5.706 283.38 280.13 284.24 283.35 282.35 No. 3 6.879 281.18 277.15 287.32 281.82 281.89 No. 1 8.160 279.48 276.67 285.22 281.83 281.30 281.30 No. 1 8.160 279.48 276.67 285.22 281.30 281.30 281.30 No. 1 8.160 279.48 276.67 285.22 281.30 281.30 281.30 No. 1 1.042 260.40 260.10 263.00 263.18 263.45 263.45 263.63 No. 1 1.944 269.40 257.00 259.00 250.03 250.04 259.00		3 0	1 010	203 33	288 89	292.46	291.00	291.45	291.70	291.88	292.12	290.06	290.62	291.10	291.40	291.65
No. 7 2 975 290.28 283.89 290.94 286.41 236.78 287.08 No. 6 3.677 284.79 281.85 285.62 284.96 285.27 285.59 No. 5 4.860 283.38 280.13 284.79 281.85 283.35 283.54 283.89 No. 4 5.706 283.08 277.15 287.32 281.82 282.94 No. 2 7.579 280.87 276.34 281.47 281.82 281.89 281.80 No. 1 8.160 279.48 276.67 285.22 281.83 281.83 281.83 No. 12 0.000 262.30 260.90 263.00 263.00 263.03 260.51 No. 11 1.042 260.40 260.12 262.20 261.99 263.45 263.63 No. 10 1.916 261.00 258.01 261.20 261.99 263.45 263.63 No. 2 2.549 2.549 2.55.00 2.50.00 250.00		× × ×	2000	09 060	286.05	290.87	288.46	288.90	289.26	289.47	289.76	287.78	288.19	288.80	289.10	289.35
No. 6 3.677 284.79 281.85 285.62 284.96 285.27 285.59 No. 5 4.860 283.38 280.13 284.24 283.33 283.54 283.89 No. 4 5.706 283.05 278.16 283.45 282.35 282.56 282.94 No. 2 7.579 280.87 276.54 281.32 281.82 281.90 282.15 No. 1 8.160 279.48 276.67 285.22 281.30 281.30 282.15 No. 12 0.000 262.30 260.90 263.00 263.18 263.45 263.63 No. 11 1.042 260.40 260.12 262.20 261.99 263.45 263.63 No. 10 1.916 261.00 258.01 261.20 261.03 260.30 260.03 260.30 260.03 260.33 260.33 260.33 260.33 260.33 260.33 260.33 260.33 260.33 260.33 260.33 260.33 260.33 260.33<		o co	2 975	290.28	283.89	290.94	286.41	286.78	287.08	287.38	287.66	285.88	286.26	286.64	286.97	287.29
No. 5 4.860 283.38 280.13 284.24 283.35 283.54 283.89 No. 4 5.706 283.05 278.16 283.45 282.35 282.56 282.94 No. 3 6.879 281.18 277.15 287.32 281.82 281.90 282.15 No. 1 8.160 279.48 276.67 285.22 281.30 281.30 282.15 No. 12 0.000 262.30 260.90 263.00 263.18 263.45 281.30 No. 11 1.042 260.40 260.10 262.20 261.99 262.31 263.65 No. 10 1.916 261.00 258.01 261.20 261.03 261.54 No. 10 1.916 261.00 259.90 260.03 260.37 263.63 No. 2 2.549 269.40 257.00 259.90 260.03 260.37 260.55 No. 3 3.492 257.40 258.30 258.60 258.60 258.03 258.67		No. 6	3.677	284.79	281.85	285.62	284.96	285.27	285.59	285.85	286.08	283.75	284.23	284.73	285.03	285.39
No. 4 5.706 283.05 278.16 283.45 282.35 282.56 282.94 No. 3 6.879 281.18 277.15 287.32 281.82 281.90 282.15 No. 1 7.579 280.87 276.34 281.47 281.73 281.85 281.97 No. 12 0.000 262.30 260.90 263.00 263.18 281.30 281.30 No. 11 1.042 260.40 260.12 262.20 261.99 262.33 263.65 No. 10 1.916 261.00 258.01 261.20 261.03 261.37 261.54 No. 9 2.549 269.40 257.00 259.90 260.03 260.37 269.55 No. 8 3.492 257.40 258.90 258.01 258.67 258.67 259.04 259.04 No. 9 2.542 258.30 258.30 258.23 258.67 258.91 No. 7 4.304 258.30 258.30 258.23 258.23 <		No. 5	4.860	283.38	280.13	284.24	283.33	283.54	283.89	284.10	284.34	282.22	282.57	283.04	283.24	283.75
No. 3 6.879 281.18 277.15 287.32 281.82 281.90 282.15 No. 1 7.579 280.87 276.34 281.47 281.73 281.85 281.97 No. 12 0.000 262.30 260.90 263.00 263.18 263.45 263.63 No. 11 1.042 260.40 260.90 263.00 261.99 263.45 263.63 No. 10 1.916 261.00 258.01 261.20 261.99 263.45 263.53 No. 9 2.549 269.40 257.00 259.90 260.03 260.55 No. 8 3.492 257.40 258.90 260.08 256.23 258.61 No. 7 4.304 258.80 254.96 258.40 258.67 258.91 No. 6 5.242 258.30 258.30 258.23 258.67 258.91 No. 7 4.304 258.30 258.30 258.23 258.67 258.91 No. 5 6.559 255.		No. 4	5.706	283.05	278.16	283.45	282.35	282.56	282.94	283.27	283.46	281.31	281.56	281.89	282.16	282.62
No. 2 7579 280.87 276.34 281.47 281.73 281.85 281.97 No. 12 8.160 279.48 276.67 285.22 281.30 281.30 281.30 No. 12 0.000 262.30 260.90 263.18 263.45 263.63 No. 11 1.042 260.40 260.12 261.20 261.99 262.33 263.61 No. 10 1.916 261.00 258.01 261.20 261.99 261.37 261.54 No. 9 2.549 269.40 257.00 259.90 260.08 260.37 260.55 No. 8 3.492 257.40 259.90 260.08 260.37 259.29 No. 7 4.304 258.80 254.05 258.20 258.67 258.91 No. 5 6.559 255.30 258.30 258.23 257.42 257.68 No. 6 5.242 255.30 253.30 253.30 255.31 255.31 No. 7 4.304 253.		No. 3	6.879	281.18		287.32	281.82	281.90	282.15	282.40	282.49	280.90	281.07	281.41	281.74	281.89
No. 1 8.160 279.48 276.67 285.22 281.30 281.30 281.30 No. 12 0.000 262.30 260.90 263.00 263.18 263.45 263.63 No. 11 1.042 260.40 260.12 262.20 261.99 263.45 263.51 No. 10 1.916 261.00 258.01 261.20 261.99 262.33 262.51 No. 9 2.549 269.40 257.00 259.90 260.08 260.37 260.55 No. 8 3.492 257.40 254.96 259.00 258.01 258.60 259.29 No. 7 4.304 258.80 254.96 258.30 258.67 258.91 No. 6 5.242 258.30 258.30 258.23 257.42 257.68 No. 5 6.559 255.30 253.30 255.33 255.34 255.31 No. 4 7.638 255.00 250.30 253.80 254.65 254.91 255.30 No		No 2	7.579	280.87	1	281.47	281.73	281.85	281.97	282.19	282.24	280.67	280.75	8 1.8 8.	281.45	281.64
No. 12 0.000 262.30 260.90 263.18 263.45 263.63 No. 12 0.000 262.30 260.90 263.00 261.99 262.33 262.51 No. 10 1.916 261.00 258.01 261.20 261.99 262.33 262.51 No. 9 2.549 269.40 257.00 259.90 260.08 260.37 260.55 No. 8 3.492 257.40 258.90 258.03 258.62 259.40 258.62 259.04 258.29 No. 7 4.304 258.80 254.05 258.30 258.67 258.91 No. 6 5.242 258.30 258.30 258.69 257.42 257.68 No. 5 6.559 255.50 250.34 255.30 255.33 255.31 No. 4 7.638 255.00 253.80 254.83 255.12 255.31 No. 2 8.797 253.00 253.80 253.80 254.91 255.20 No. 2 8.7		2	8 160	279.48	1	285.22	281.30	281.30	281.30	281.30	281.30	279.70	279.70	279.70	279.70	279.70
No. 11 1.042 260.40 260.12 262.20 261.99 262.33 262.51 No. 10 1.916 261.00 258.01 261.03 261.37 261.54 No. 9 2.549 269.40 257.00 259.90 260.08 260.37 261.54 No. 8 3.492 257.40 254.96 259.40 258.62 259.04 259.29 No. 7 4.304 258.80 254.05 258.30 258.67 258.91 No. 6 5.242 258.30 258.00 257.42 257.68 No. 5 6.559 255.07 258.00 257.42 257.68 No. 4 7.638 255.50 250.34 253.30 255.33 255.34 No. 3 8.253 255.00 257.09 257.65 257.99 255.31 No. 2 8.797 253.00 253.80 253.00 253.30 253.30 No. 2 8.797 253.10 251.50 253.00 253.20 253.5	Antofagasta	┸	0000	262.30	260 90	263.00	263.18	263.45	263.63	263.78	263.98	261.92	262.41	262.64	262.79	262.94
1.916 261.00 258.01 261.20 261.03 261.37 261.37 261.54 2.549 269.40 257.00 259.90 260.08 260.37 260.55 3.492 257.40 254.96 259.40 258.62 259.04 259.29 4.304 258.80 254.05 258.30 258.67 258.91 5.242 258.30 253.07 258.00 257.42 257.68 6.559 255.50 250.34 255.70 254.99 255.33 255.54 7.638 255.50 250.34 255.70 254.99 255.33 255.54 8.253 255.00 251.16 255.00 254.95 255.31 255.08 8.797 253.00 251.10 251.00 251.20 253.51 253.51	, money		1 042	260.40	-	262.20	261.99	262.33	262.51	262.67	262.88	260.89	261.43	261.66	261.84	262.01
2.549 269.40 257.00 259.90 260.08 260.37 269.55 3.492 2.57.40 2.54.96 2.59.40 258.62 259.04 259.29 4.304 2.58.80 2.54.05 2.58.30 2.58.23 2.58.67 2.58.91 5.242 2.58.30 2.58.70 2.56.99 2.57.42 2.57.68 6.559 2.55.50 2.50.34 2.55.70 2.54.99 2.55.33 2.55.54 7.638 2.55.60 2.50.30 2.53.80 2.54.83 2.55.12 2.55.31 8 253 2.55.00 2.51.16 2.55.00 2.54.65 2.55.31 2.55.08 8 797 2.53.00 2.46.65 2.53.00 2.53.30 2.53.31 2.55.08 8 797 2.53.00 2.46.65 2.53.00 2.53.00 2.53.32 2.53.51		1000	1 916	261.00		261 20	261.03	261.37	261.54	261.69	261.89	259.86	260.41	260.63	260.80	260.96
3.492 257.40 258.60 258.62 259.04 259.29 4.304 258.80 254.05 258.30 258.23 258.67 258.91 5.242 258.30 258.30 256.90 257.42 257.68 6.559 255.50 250.34 255.70 254.99 255.53 255.54 7.638 255.60 250.30 253.80 254.83 255.12 255.31 8.253 255.00 251.16 255.00 254.65 255.91 255.08 8.797 253.00 249.65 252.80 253.00 253.51 253.51 8.767 251.10 251.10 250.16 250.87 251.20		O CN	2 549	269.40	257.00	259.90	260.08	260.37	260.55	260.70	260.88	258.89	259.37	259.59	259.75	259.92
4.304 258.80 254.05 258.30 258.31 258.67 258.91 5.242 258.30 253.07 258.00 256.90 257.42 257.68 6.559 255.50 250.34 255.70 254.99 255.33 255.54 7.638 253.60 250.30 253.80 254.83 255.12 255.31 8.253 255.00 251.16 255.00 254.65 254.91 255.08 8.797 253.00 249.65 252.80 253.00 253.32 253.51 9.767 251.10 256.10 256.87 253.51		N S	3 492	257.40	254.96	259.40	258.62	259.04	259.29	259.50	259.73	257.95	258.48	258.71	258.88	259.05
5.242 258.30 253.07 258.00 256.90 257.42 257.68 6.559 255.50 250.34 255.70 254.99 255.33 255.54 7.638 253.60 250.30 253.80 254.83 255.12 255.31 8.253 255.00 251.16 255.00 254.65 254.91 255.08 8.797 253.00 249.65 252.80 253.00 253.32 253.51 9.767 251.10 250.10 250.16 250.87 251.20		No. 7	4 304	258.80		258.30	258.23	258.67	258.91	259.11	259.33	257.16	257.74	257.99	258.18	258.37
6.559 255.50 250.34 255.70 254.99 255.33 255.54 7.638 253.60 250.30 253.80 254.83 255.12 255.31 8.253 255.00 251.16 255.00 254.65 255.91 255.08 8.797 253.00 249.65 252.80 253.00 253.32 253.51 8.767 251.10 240.65 251.10 250.16 250.87 251.20		No 6	5.242	258.30		258.00	256.90	257.42	257.68	257.89	258.12	256.10	256.64	256.87	257.05	257.23
7.638 253.60 250.30 253.80 254.83 255.12 255.31 8.253 255.00 251.16 255.00 254.65 254.91 255.08 8.797 253.00 249.65 252.80 253.00 253.32 253.51 9.767 253.00 249.65 252.80 253.00 253.32 253.51		No. 5	6.559	255.50	1	255.70	254.99	255.33	255.54	255.72	255.93	254.53	254.98	255.16	255.30	255.44
8.253 255.00 251.16 255.00 254.65 254.91 255.08 8.797 253.00 249.65 252.80 253.00 253.32 253.51 9.707 251.10 249.65 251.10 250.16 250.87 251.20		No. 4	7.638	253.60	i	253.80	254.83	255.12	255.31	255.47	255.66	253.62	254.19	254.40	254.53	254.67
8.797 253.00 249.65 252.80 253.00 253.32 253.51		No. 3	8 253	255.00	251.16	255.00	254.65	254.91	255.08	255.22	255.38	252.95	253.56	253.78	253.90	254.02
6 767 351 10 340 KS 351 101 350 16 350 87 351 20		No. 2	8.797	253.00	249.65	252.80	253.00	253.32	253.51	253.65	253.83	252.15	252.76	253.02	253.15	253.30
1 0.797 01.002 01.102 01.103 01.103		No. 1	8.797	251.10	249.65	251.10	250.16	250.87	251.20	251.50	251.87	250.16	250.87	251.20	251.50	251.87

TABLE F.4.8 FLOW RATE FROM HD CALCULATION IN THE ARROYO TACUARAL AND ANTOFAGASTA

		Maximu	Maximum flow rate from probable flood (m ³ /s)	e from pro	bable floo	d (m ³ /s)	Maximu	m flow rat	Maximum flow rate from probable flood (m^3/s)	bable floo	d (m ³ /s)
Arroyo	Chainage in		Existin	Existing cross section	ction			Desig	Design cross section	ction	
	F/S (km)	2 year	5 year	10 year	20 year	50 year	2 year	5 year	10 year	20 year	50 year
Tejeria	0.505	6.40	7.62	9.65	10.69	11.76	6.61	7.86	66.6	11.20	12.88
	1.617	12.82	15.24	19.27	20.89	22.74	13.22	15.72	19.88	22.37	25.71
	2.600	19.23	22.92	29.07	32.03	35.38	19.82	23.58	29.84	33.56	38.57
	3.326	25.69	30.66	38.95	43.25	48.23	26.42	31.45	39.82	44.83	51.48
	4.268	32.01	38.38	49.00	54.86	61.39	32.69	39.00	49.51	55.77	64.11
	5.283	37.39	43.92	54.80	61.83	69.92	38.31	45.39	57.20	64.30	72.82
	6.292	49.29	57.59	71.42	80.31	98.06	49.72	59.22	75.05	84.16	99.15
	7.229	55.42	64.70	80.17	89.77	101.62	50.18	61.41	80.14	129.94	138.33
	7.869	67.50	82.10	97.54	108.74	123.27	60.52	88.59	96.70	109.44	127.78
Antofagasta	0.520	94.95	128.91	153.08	177.52	209.95	166.19	223.08	250.97	273.33	297.01
	1.480	94.87	128.80	152.91	177.34	209.74	165.95	222.94	250.88	273.23	296.95
	2.235	94.80	128.64	152.73	177.17	209.57	165.92	222.91	250.86	273.19	296.89
	3.020	94.73	128.52	152.58	177.01	209.39	165.89	222.88	250.79	273.12	296.74
	3.895	94.52	128.22	152.31	176.63	209.01	165.57	222.69	250.63	272.97	296.59
	4.770	94.48	128.13	152.19	176.45	208.84	165.54	222.65	250.59	272.92	296.54
	5.900	94.48	128.11	152.16	176.44	208.80	165.52	222.65	250.58	272.92	296.54
	7.100	94.41	127.99	151.91	176.18	208.57	165.49	222.60	250.54	272.87	296.48
	7.945	94.32	127.83	151.77	175.99	208.40	165.34	222.36	250.38	272.65	296.23
	8.525	94.33	127.83	151.77	175.97	208.39	165.34	222.36	250.37	272.63	296.19
	9.700	94.30	127.68	151.65	175.85	208.25	165.32	222.33	249.87	270.38	291.40