

Appendix 12.3 Pumping Station - Capacity Calculation

1. Pumping Facility

| Alternative | | Alternative 1 | | | | Alternative 2 | | |
|---------------------|---------------------|---------------|----------|----------|-------------|---------------|-------------|-------------|
| Area | | Kandy | | | | Kandy | | Katugastota |
| Pump Station | | P/S 1 | P/S 2-1 | P/S 2-2 | STP | P/S 1 | STP | P/S 1 |
| P/S Flow | m ³ /sec | 0.01220 | 0.02900 | 0.02900 | 0.30000 | 0.00700 | 0.27333 | 0.02900 |
| | m ³ /min | 0.732 | 1.740 | 1.740 | 18.000 | 0.420 | 16.400 | 1.740 |
| P/S Type | | Circular | Circular | Circular | Rectangular | Circular | Rectangular | Circular |
| Number (+1)-standby | | 1 (+1) | 1 (+1) | 1 (+1) | 2 (+1) | 1 (+1) | 2 (+1) | 1 (+1) |
| Capacity | m ³ /min | 0.74 | 1.74 | 1.74 | 9.00 | 0.42 | 8.20 | 1.74 |
| Head | m | 9 | 48 | 48 | 12 | 14 | 14 | 18 |
| h1 = | m | 7.00 | 40.00 | 40.00 | 10.00 | 7.00 | 10.00 | 15.00 |
| h2 = | m | 0.2 | 26.99 | 26.99 | 0.25 | 6.51 | 0.29 | 1.42 |
| D = | mm | 250 | 150 | 150 | 600 | 100 | 450 | 200 |
| L = | m | 630 | 1,400 | 1,400 | 150 | 650 | 50 | 300 |
| V = | m/sec | 0.249 | 1.641 | 1.641 | 1.061 | 0.891 | 1.719 | 0.923 |
| h3 = | m | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 |
| Diameter | mm | 79 | 122 | 122 | 392 | 60 | 374 | 122 |
| Diameter | mm | 150 | 125 | 125 | 400 | 150 | 400 | 125 |
| Motor Output | kW | 2.1 | 26.1 | 26.1 | 33.7 | 1.8 | 35.9 | 9.8 |
| Motor Output | kW | 2.2 | 30 | 30 | 37 | 2.2 | 37 | 11 |

2. Pump Pit (Circular)

| Alternative | | Alternative 1 | | | Alternative 2 | |
|------------------------------|---------------------|---------------|----------|----------|---------------|----------|
| Area | | Kandy | | | Katugastota | Kandy |
| Pump Station | | P/S 1-1 | P/S 1-2 | P/S 2 | P/S 1 | P/S 2 |
| P/S Flow | m ³ /sec | 0.02900 | 0.02900 | 0.01220 | 0.02900 | 0.01220 |
| | m ³ /min | 1.740 | 1.740 | 0.732 | 1.740 | 0.732 |
| P/S Type | | Circular | Circular | Circular | Circular | Circular |
| Number (+1)-standby | | 1 (+1) | 1 (+1) | 1 (+1) | 1 (+1) | 1 (+1) |
| Capacity | m ³ /min | 1.74 | 1.74 | 0.74 | 1.74 | 0.74 |
| Pump Minimum Starting Period | min | 15 | 15 | 8 | 8 | 8 |
| Pump Pit Capacity | cu.m | 6.53 | 6.53 | 1.48 | 3.48 | 1.48 |
| Therefore | cu.m | 7.00 | 7.00 | 2.00 | 4.00 | 2.00 |
| Ground Level | m | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Inlet Pipe Level | m | -4.00 | -4.00 | -4.00 | -4.00 | -4.00 |
| Effective Depth | m | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Top | m | 0.50 | 0.50 | 0.50 | 0.50 | 0.50 |
| Bottom | m | 0.50 | 0.50 | 0.50 | 0.50 | 0.50 |
| Required Area | sq.m | 7.00 | 7.00 | 2.00 | 4.00 | 2.00 |
| Diameter | m | 2.99 | 2.99 | 1.60 | 2.26 | 1.60 |
| Therefore | m | 3.00 | 3.00 | 1.60 | 2.50 | 1.60 |
| Dimension (DIA) | m | 3.00 | 3.00 | 1.60 | 2.50 | 1.60 |
| (D) | m | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 |
| Retention Time | min | 4.06 | 4.06 | 2.75 | 2.82 | 2.75 |

3. Pump Pit (Rectangular)

| Alternative | | Alter. - 1 | Alter. - 2 |
|------------------------------|---------------------|-------------|-------------|
| Area | | Kandy | Kandy |
| Pump Station | | STP | STP |
| P/S Flow | m ³ /sec | 0.29570 | 0.26670 |
| | m ³ /min | 17.742 | 16.002 |
| P/S Type | | Rectangular | Rectangular |
| Number (+1)-standby | | 3 (+1) | 3 (+1) |
| Capacity | m ³ /min | 5.92 | 5.34 |
| Pump Minimum Starting Period | min | 15 | 15 |
| Pump Pit Capacity | cu.m | 22.20 | 20.03 |
| Therefore | cu.m | 24.00 | 22.00 |
| Ground Level | m | 0.00 | 0.00 |
| Inlet Pipe Level | m | -4.00 | -4.00 |
| Effective Depth | m | 0.80 | 0.80 |
| Top | m | 0.50 | 0.50 |
| Bottom | m | 0.70 | 0.70 |
| Required Area | sq.m | 30.00 | 27.50 |
| Width | m | 7.00 | 7.00 |
| Length | m | 4.29 | 3.93 |
| Therefore | m | 4.90 | 4.90 |
| Dimension | (W) | 7.00 | 7.00 |
| | (L) | 4.90 | 4.90 |
| | (D) | 6.00 | 6.00 |
| Retention Time | min | 9.47 | 10.50 |

Appendix 12.4

Sewage Treatment Plant – Capacity Calculation

Appendix 12.4.1 Alternative 1 – Kandy (Oxidation Ditch)

Appendix 12.4.2 Alternative 2 – Kandy (Oxidation Ditch)

Appendix 12.4.3 Alternative 2 – Katugastota (Dual Power Aerated Lagoon)



Appendix 12.4.1 Sewage Treatment Plant - Capacity Calculation

CAPACITY CALCULATION OF FACILITIES Alternative 1 - Kandy (Oxidation Ditch)

1 BASIC CONDITIONS

1-1 BASIC ITEMS

- (1) Name : Kandy Sewage Treatment Plant
- (2) Land Area : Approximately 3.00 ha
- (3) Elevation : 474.000 m
- (4) Inlet Pipe Level : 465.883 m
- (5) Pipe Diameter : 600 m
- (6) Land Use :
- (7) Collection System : Seperate Type
- (8) Treatment Method : Sewage Treatment : Oxidation Ditch Method
Sludge Treatment : Sludge Thickener, Drying Bed
- (9) Effluent Point : Mada Ela River
- (10) Effluent Point Water Level : 470.640 m
- (11) Target Year : Year 2005 (Phase 1), Year 2015 (Phase 2)
- (12) Lowest Monthly Average Temperature 23.6 °C (January)

1-2 Design Population

Design Population : 55,000 Persons (Total)

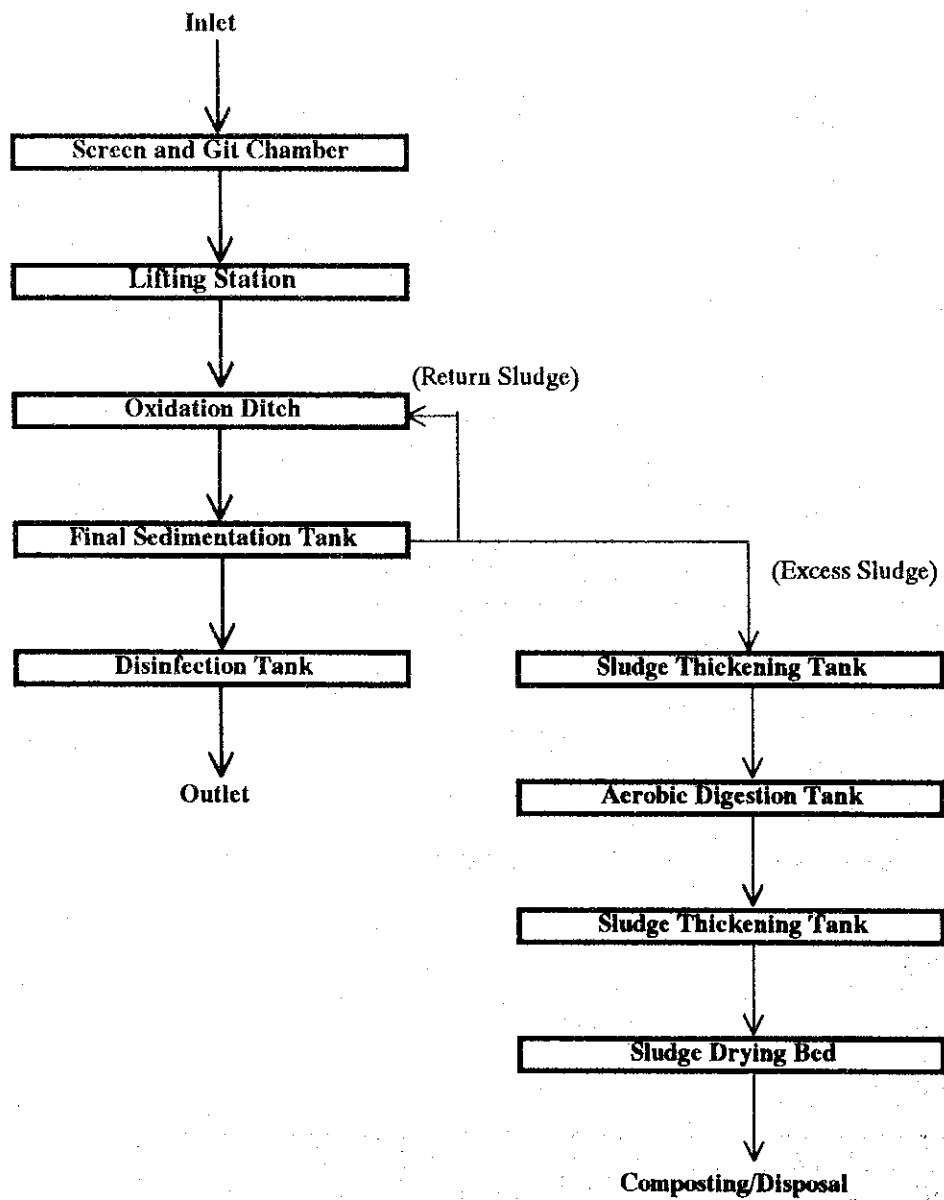
1-3 Design Sewage Flow

| ITEM | m3/day | m3/hr | m3/min | m3/sec |
|----------------|--------|--------|--------|--------|
| Daily Average | 15,220 | 634.2 | 10.57 | 0.176 |
| Daily Maximum | 18,000 | 750.0 | 12.50 | 0.208 |
| Hourly Maximum | 25,540 | 1064.2 | 17.74 | 0.296 |

1-4 Design Sewage Quality

| ITEM | INFLUENT (mg/L) | EFFLUENT (mg/L) | REMOVAL RATIO (%) | REMARKS |
|------|--------------------|--------------------|----------------------|---------|
| BOD | 240 | 30 | 88 | |
| SS | 250 | 50 | 80 | |

1-5 Flow Chart (Oxidation Ditch)



1-6 Design Criteria for Oxidation Ditch

| ITEMS | UNIT | Formula or Value | Application |
|---------------------------------------|-------------------------------------|-------------------|--------------|
| 1-6-1 Grit Chamber | | | |
| (1) Water Surface Load | m ³ /m ² /sec | < 1800 | 1,800 |
| (2) Average Velocity | m/sec | < 0.3 | 0.3 |
| 1-6-2 Oxidation Ditch | | | |
| (1) BOD-SS Load | kg/kg/day | 0.03 - 0.05 | 0.05 |
| (2) MLSS Concentration | mg/l | 3,000 - 4,000 | 4,000 |
| (3) Return Sludge Ratio | % | 100 - 200 | 150 |
| (4) Water Depth | m | 1.0 - 3.0 | Same as Left |
| (5) Width | m | 2.0 - 6.0 | Same as Left |
| (6) Retention Time | hour | 24 - 48 | Same as Left |
| (6) Oxygen Requirement | kgO ₂ /kgBOD | 1.4 - 2.2 | 2.0 |
| (7) Sludge Age | day | 8 - 50 | Same as Left |
| 1-6-3 Final Sedimentation Tank | | | |
| (1) Water Surface Load | m ³ /m ² /day | 8 - 12 | 8 - 12 |
| (2) Retention Time | hour | 6.0 - 12.0 | Same as Left |
| (3) Water Depth | m | 3.0 - 4.0 | 3.0 |
| 1-6-4 Disinfection Tank | | | |
| (1) Retention Time | min. | > 15 | 15 |
| (2) Dosage | mg/l | 2.0 - 4.0 | 3.0 |
| 1-6-5 Sludge Thickening Tank | | | |
| (1) Solid Matter Load | kg/m ² /day | 60 - 90 | 70 |
| (2) Water Depth | m | Approximately 4.0 | 4.0 |
| 1-6-6 Aerobic Digestion Tank | | | |
| (1) Retention Time | day | 10.0 - 15.0 | Same as Left |
| (2) Solid Matter Load | kg/m ² /day | 1.60 - 4.81 | Same as Left |
| 1-6-7 Sludge Drying Bed | | | |
| (1) Drying Period | day | 15 - 30 | 20 |
| (2) Depth of Bed | m | 0.3 - 1.0 | 0.3 |

2 CAPACITY CALCULATION

2-1 Grit Chamber and Screen (Hourly Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|-------------------------|------|-------------------------------------|--------------------|--------|
| Type | - | - | Parallel Flow Type | |
| Design Flow | Q1 | m ³ /day | - | 25,540 |
| | Q2 | m ³ /sec | - | 0.30 |
| Water Surface Load | WSL | m ³ /m ² /day | - | 1,800 |
| Required Surface Area | RSA | m ² | Q1/WSL | 14.189 |
| Basin Number (Total) | BN | basin | - | 6 |
| Basin Number (Stand-By) | BNS | basin | - | 2 |
| Average Velocity | V | m/sec | - | 0.30 |
| Depth | H | m | - | 0.80 |
| Width | W1 | m | Q2/(V*H) | 1.232 |
| Therefore | W2 | m | - | 1.20 |
| Length | L1 | m | RSA/W2/(BN-BNS) | 2.956 |
| Therefore | L2 | m | - | 2.70 |
| Dimension (W) | W | m | W2 | 1.20 |
| (L) | L | m | L2 | 2.70 |
| (Basin) | - | basin | BN | 4 |
| (Stand-By) | - | stand-by | BNS | 2 |
| Screen Type | - | - | Fine Bar Screen | |
| Screen Set Number | SSN | set | BN | 6 |
| Check | | UNIT | APPLICATION | RESULT |
| Water Surface Load | | m ³ /m ² /day | < 1800 | 1,971 |
| Average Velocity | | m/sec | < 0.3 | 0.08 |

2-2 Oxidation Ditch (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|-----------------------|--------|-----------------------|--------------------------------------|---------|
| Type | - | - | Re-circulation Flow Type | |
| Design Flow | Q1 | m ³ /day | - | 18,000 |
| | Q2 | m ³ /hr | - | 750.0 |
| Basin Number | BN | Basin | - | 6 |
| Inlet BOD Quality | C | mg/L | - | 240 |
| Inlet SS Quality | S | mg/L | - | 250 |
| Inlet BOD Matter | M | kg/day | $Q1 \cdot C \cdot 10^{-3}$ | 4,320 |
| BOD-SS Load | BS | kg/kg/day | - | 0.05 |
| MLSS Concentration | SS | mg/L | - | 4,000 |
| Required Volume | V1 | m ³ | $M/(SS \cdot BS \cdot 10^{-3})$ | 21,600 |
| Therefore | V2 | m ³ | - | 21,600 |
| Retention Time | T | hr | $(V2/Q1) \cdot 24$ | 28.8 |
| Return Sludge Ratio | R1 | % | - | 150 |
| | R2 | - | R1/100 | 1.5 |
| Return Sludge Quality | RS1 | mg/L | $(SS \cdot (1+R2) - C)/R2$ | 6,507 |
| Therefore | RS2 | mg/L | - | 6,510 |
| Sludge Age | SA | day | $SS \cdot V2 / (Q1 \cdot S)$ | 19.2 |
| Width | W | m | - | 6.0 |
| Water Depth | H | m | - | 3.0 |
| Length | L1 | m | $(V2/BN)/(W \cdot H)$ | 200.0 |
| Therefore | L2 | m | - | 200.0 |
| Dimension (Width) | W | m | W | 6.0 |
| (Depth) | H | m | H | 3.0 |
| (Length) | L | m | L2 | 200.0 |
| (Basin Number) | - | basin | BN | 6 |
| Required Oxygen | O2-day | kgO ₂ /day | $Q1 \cdot C \cdot 10^{-3} \cdot 2.0$ | 8,640.0 |
| | O2-hr | kgO ₂ /hr | $(O2\text{-day})/24$ | 360.0 |
| Aerator Motor Output | - | kW | $O2\text{-hr}/1.9$ | 189.5 |
| | - | kW | - | 180.0 |
| Aerator Type | - | - | Slanting Shaft Screw Aerator | |
| Check | | UNIT | APPLICATION | RESULT |
| Retention Time | | hour | 24 - 48 | 28.8 |
| Oxygen Supply | | kgO ₂ /kg | 1.4 - 2.2 | 2.0 |
| Sludge Age | | day | 8 - 50 | 19.2 |

2-3 Final Sedimentation Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|--|------|-----------|--|--------|
| Type | - | - | Radial Flow Circular Type | |
| Design Flow | Q1 | m3/day | - | 18,000 |
| | Q2 | m3/sec | - | 750.00 |
| Basin Number | BN | Basin | - | 6 |
| Water Surface Load Therefore | L | m3/m2/day | $4.14 \times 10^4 \times T^{0.95} \times SS^{-1.35}$ | 11.4 |
| | L | m3/m2/day | - | 12.0 |
| Required Surface Area | A1 | m2 | Q1/L | 1500.0 |
| | A2 | m2/Basin | A1/BN | 250.0 |
| Water Depth | H | m | - | 3.0 |
| Diameter Therefore | D1 | m | $(A2/3.14)^{0.5 \times 2}$ | 17.8 |
| | D2 | m | - | 18.0 |
| Dimension (Diam) (Depth) (Basin Number) | D | m | D2 | 18.0 |
| | H | m | H | 3.0 |
| | - | Basin | BN | 6 |
| Sludge Collector Type | - | - | Central Drive Type | |
| Check | | UNIT | APPLICATION | RESULT |
| Water Surface Load | | m3/m2/day | 8 - 12 | 11.8 |
| Retention Time | | hour | 6.0 - 12.0 | 5.1 |

2-4 Disinfection Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|--|------|--------|----------------------------------|--------|
| Chemical Type | - | - | Chlorination Type | |
| Design Flow | Q1 | m3/day | - | 18,000 |
| | Q2 | m3/min | - | 12.50 |
| Retention Time | T | min. | - | 15.0 |
| Basin Number | BN | basin | - | 2 |
| Required Volume | V | m3 | Q2*T | 94 |
| Width | W | m | - | 3.00 |
| Water Depth | H | m | - | 1.50 |
| Length therefore | L1 | m | $V/(W \times H)$ | 20.833 |
| | L2 | m | - | 21.00 |
| Dosage | D | mg/L | - | 3.0 |
| Required Chemical Therefore | RC1 | kg/day | $Q1 \times D \times 10^{-3} / C$ | 54.00 |
| | RC2 | kg/hr | RC1/24 | 2.25 |
| Dimension (W) (Length) (Depth) (Basin) | W | m | W | 3.0 |
| | L | m | L2 | 21.0 |
| | H | m | H | 1.5 |
| | BN | basin | - | 2 |
| Chlorine Feeder | - | unit | including 1 for stand-by | 3 |
| Check | | UNIT | APPLICATION | RESULT |
| Retention Time | | min. | 15 | 15.1 |

2-5 Sludge Thickening Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|--|-------|------------------------|---|--------|
| Type | - | - | Radial Flow Circular Type | |
| Design Flow | Q1 | m ³ /day | - | 18,000 |
| | Q2 | m ³ /hr | - | 634.2 |
| Basin Number | BN | Basin | - | 2 |
| Inlet SS Quality | C | mg/L | - | 250 |
| Removal Ratio | R1 | % | - | 80 |
| | R2 | - | R1/100 | 0.80 |
| Sludge Generation Ratio (Oxidation Ditch) | SG1 | % | - | 75 |
| | SG2 | - | SG1/100 | 0.75 |
| Inlet SS Matter | M | kg/day | $Q1 \cdot C \cdot R2 \cdot SG2 \cdot 10^{-3}$ | 2,700 |
| Solid Matter Load | L | kg/m ² /day | - | 70.0 |
| Required Surface Area | A1 | m ² | M/L | 38.6 |
| | A2 | m ² /Basin | A1/BN | 19.3 |
| Water Depth | H | m | - | 4.0 |
| Diameter | D1 | m | $(A2/3.14)^{0.5 \cdot 2}$ | 5.0 |
| Therefore | D2 | m | - | 5.0 |
| Dimension | D | m | D2 | 5.0 |
| (Depth) | H | m | H | 4.0 |
| (Basin) | Basin | Basin | BN | 2 |
| Check | | UNIT | APPLICATION | RESULT |
| Solid Matter Load | | kg/m ² /day | 70 | 68.8 |

2-6 Aerobic Sludge Digestion Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|------------------------------|-------|------------------------|---|---------|
| Type | - | - | Circular Type | |
| Basin Number | BN | Basin | - | 2 |
| Design Flow | Q1 | m ³ /day | - | 18,000 |
| Inlet SS Matter | M | kg/day | - | 2,700 |
| Moisture Content | G | % | - | 97.5 |
| Sludge Volume | V1 | m ³ /day | $M \cdot 100 / (100 - G)$ | 108.0 |
| Temperature - Summer | TS | °C | - | 26.5 |
| - Winter | TW | °C | - | 23.6 |
| Temperature - Sludge Age | TSA | day-°C | VolatileSolidReduction=40% | 470 |
| Sludge Age | SA | day | TSA/TS | 19.9 |
| Total Mass of VSS | VSS | kg/day | $0.8 \cdot M$ | 2,160 |
| VSS Reduction - Summer (41%) | VRS | kg/day | $VSS \cdot 0.4$ | 864.0 |
| - Winter (40%) | VRW | kg/day | $VSS \cdot 0.41$ | 885.6 |
| Required Volume | V | m ³ | $V1 / 0.7 / (0.125 \cdot 0.8 + 1 / SA)$ | 514 |
| Water Depth | H | m | - | 4.0 |
| Diameter | D1 | m | $(A2/3.14)^{0.5 \cdot 2}$ | 12.8 |
| Therefore | D2 | m | - | 13.0 |
| Dimension | D | m | D2 | 13.0 |
| (Depth) | H | m | H | 4.0 |
| (Basin) | Basin | Basin | BN | 2 |
| Required Oxygen | RO | kgO ₂ /day | $2.3 \cdot VRS$ | 1987.2 |
| Required Air | RA | kg-Air/hr | $RO / (0.1 \cdot 0.233 \cdot 1.293) / 1440$ | 2,748.4 |
| Check | | UNIT | APPLICATION | RESULT |
| Retention Time | | day | 10.0 - 15.0 | 4.9 |
| Solid Matter Load | | kg/m ³ /day | 1.60 - 4.81 | 10.2 |

2-7 Sludge Thickening Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|---------------------------------|-------|------------------------|-----------------------------|--------|
| Type | - | - | Radial Flow Circular Type | |
| Basin Number | BN | Basin | - | 2 |
| Inlet SS Matter to Digestion | M1 | kg/day | - | 2,700 |
| Removal Ratio at Digestion | R1 | % | - | 40% |
| Inlet SS Matter | M2 | kg/day | $M1 \cdot (1 - R1)$ | 1620 |
| Moisture Content | G | % | - | 99.0 |
| Sludge Volume | V1 | m ³ /day | $M2 \cdot 100 / (100 - G)$ | 162.0 |
| Solid Matter Load | L | kg/m ² /day | - | 70.0 |
| Required Surface Area | A1 | m ² | M/L | 23.1 |
| | A2 | m ² /Basin | A1/BN | 11.6 |
| Water Depth | H | m | - | 4.0 |
| Diameter | D1 | m | $(A2 / 3.14)^{0.5} \cdot 2$ | 3.8 |
| | D2 | m | - | 5.0 |
| Dimension (Depth) (Basin) | D | m | D2 | 5.0 |
| | H | m | H | 4.0 |
| | Basin | Basin | BN | 2 |
| Check | | UNIT | APPLICATION | RESULT |
| Solid Matter Load | | kg/m ² /day | 70 | 41.3 |

2-8 Sludge Drying Bed (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|--|-------|---------------------|-------------------------------------|--------|
| Design Flow | Q1 | m ³ /day | - | 18,000 |
| Inlet SS Matter | M1 | kg/day | $Q1 \cdot C \cdot R2 \cdot 10^{-3}$ | 1,620 |
| | M2 | t/day | $M1 / 1000$ | 1.62 |
| Moisture Content | G | % | - | 97.0 |
| Sludge Volume | V1 | m ³ /day | $M2 \cdot 100 / (100 - G)$ | 54.0 |
| Drying Period | P | day | - | 10 |
| Required Volume | V2 | m ³ /day | $V1 \cdot P$ | 540.0 |
| Depth of Bed | H | m | - | 0.3 |
| Required Area | A | m ² | $V2 / H$ | 1,800 |
| Unit Number | UN | Unit | - | 20 |
| Width per Unit | W | m | - | 6.0 |
| Length per Unit | L1 | m | $A / (UN \cdot W)$ | 15.0 |
| | L2 | m | - | 15.0 |
| Dimension (Width) (Length) (Depth) (Basin) | W | m | W | 6.0 |
| | L | m | L2 | 15.0 |
| | H | m | H | 0.3 |
| | Basin | Basin | BN | 20.0 |
| Check | | UNIT | APPLICATION | RESULT |
| Drying Period | | day | 20 | 10.0 |

Appendix 12.4.2 Sewage Treatment Plant - Capacity Calculation

CAPACITY CALCULATION OF FACILITIES Alternative 2 - Kandy (Oxidation Ditch)

1 BASIC CONDITIONS

1-1 BASIC ITEMS

- (1) Name : Kandy Sewage Treatment Plant
- (2) Land Area : Approximately 3.00 ha
- (3) Elevation : 474.000 m
- (4) Inlet Pipe Level : 465.883 m
- (5) Pipe Diameter : 600 m
- (6) Land Use :
- (7) Collection System : Seperate Type
- (8) Treatment Method : Sewage Treatment : Oxidation Ditch Method
Sludge Treatment : Sludge Thickener, Drying Bed
- (9) Effluent Point : Mada Ela River
- (10) Effluent Point Water Level : 470.640 m
- (11) Target Year : Year 2005 (Phase 1), Year 2015 (Phase 2)
- (12) Lowest Monthly Average Temperature 23.6 °C (January)

1-2 Design Population

Design Population : 49,700 Persons (Total)

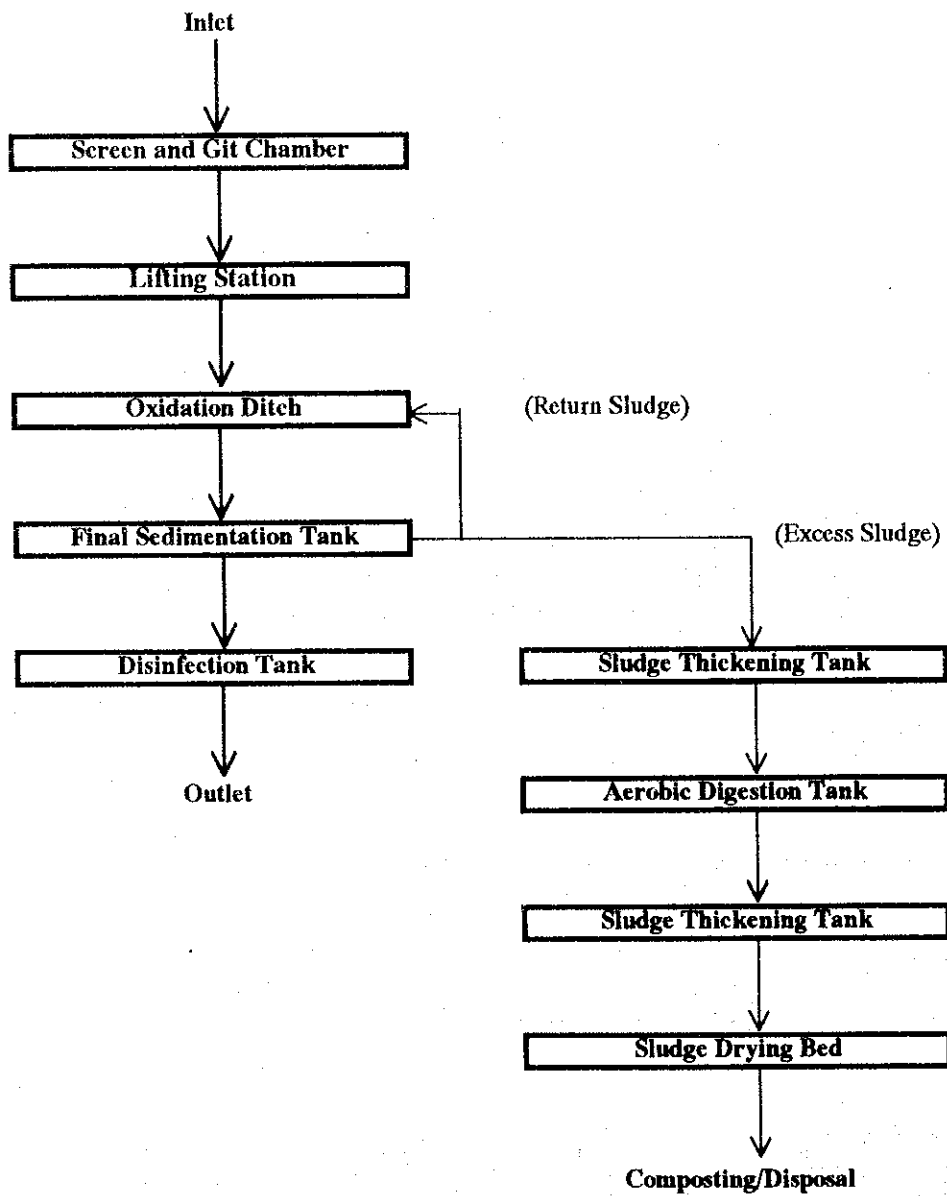
1-3 Design Sewage Flow

| ITEM | m3/day | m3/hr | m3/min | m3/sec |
|----------------|--------|-------|--------|--------|
| Daily Average | 13,700 | 570.8 | 9.51 | 0.159 |
| Daily Maximum | 17,000 | 708.3 | 11.81 | 0.197 |
| Hourly Maximum | 23,030 | 959.6 | 15.99 | 0.267 |

1-4 Design Sewage Quality

| ITEM | INFLUENT (mg/L) | EFFLUENT (mg/L) | REMOVAL RATIO (%) | REMARKS |
|------|--------------------|--------------------|----------------------|---------|
| BOD | 240 | 30 | 88 | |
| SS | 250 | 50 | 80 | |

1-5 Flow Chart (Oxidation Ditch)



1-6 Design Criteria for Oxidation Ditch

| ITEMS | UNIT | Formula or Value | Application |
|--------------------------------|-------------------------------------|-------------------|--------------|
| 1-6-1 Grit Chamber | | | |
| (1) Water Surface Load | m ³ /m ² /sec | < 1800 | 1,800 |
| (2) Average Velocity | m/sec | < 0.3 | 0.3 |
| 1-6-2 Oxidation Ditch | | | |
| (1) BOD-SS Load | kg/kg/day | 0.03 - 0.05 | 0.05 |
| (2) MLSS Concentration | mg/l | 3,000 - 4,000 | 4,000 |
| (3) Return Sludge Ratio | % | 100 - 200 | 150 |
| (4) Water Depth | m | 1.0 - 3.0 | Same as Left |
| (5) Width | m | 2.0 - 6.0 | Same as Left |
| (6) Retention Time | hour | 24 - 48 | Same as Left |
| (6) Oxygen Requirement | kgO ₂ /kgBOD | 1.4 - 2.2 | 2.0 |
| (7) Sludge Age | day | 8 - 50 | Same as Left |
| 1-6-3 Final Sedimentation Tank | | | |
| (1) Water Surface Load | m ³ /m ² /day | 8 - 12 | 8 - 12 |
| (2) Retention Time | hour | 6.0 - 12.0 | Same as Left |
| (3) Water Depth | m | 3.0 - 4.0 | 3.0 |
| 1-6-4 Disinfection Tank | | | |
| (1) Retention Time | min. | > 15 | 15 |
| (2) Dosage | mg/l | 2.0 - 4.0 | 3.0 |
| 1-6-5 Sludge Thickening Tank | | | |
| (1) Solid Matter Load | kg/m ² /day | 60 - 90 | 70 |
| (2) Water Depth | m | Approximately 4.0 | 4.0 |
| 1-6-6 Aerobic Digestion Tank | | | |
| (1) Retention Time | day | 10.0 - 15.0 | Same as Left |
| (2) Solid Matter Load | kg/m ² /day | 1.60 - 4.81 | Same as Left |
| 1-6-7 Sludge Drying Bed | | | |
| (1) Drying Period | day | 15 - 30 | 20 |
| (2) Depth of Bed | m | 0.3 - 1.0 | 0.3 |

2 CAPACITY CALCULATION

2-1 Grit Chamber and Screen (Hourly Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|--|------|-----------|--------------------|--------|
| Type | - | - | Parallel Flow Type | |
| Design Flow | Q1 | m3/day | - | 23,030 |
| | Q2 | m3/sec | - | 0.27 |
| Water Surface Load | WSL | m3/m2/day | - | 1,800 |
| Required Surface Area | RSA | m2 | Q1/WSL | 12.794 |
| Basin Number (Total) | BN | basin | - | 6 |
| Basin Number (Stand-By) | BNS | basin | - | 2 |
| Average Velocity | V | m/sec | - | 0.30 |
| Depth | H | m | - | 0.80 |
| Width Therefore | W1 | m | Q2/(V*H) | 1.111 |
| | W2 | m | - | 1.20 |
| Length Therefore | L1 | m | RSA/W2/(BN-BNS) | 2.666 |
| | L2 | m | - | 2.70 |
| Dimension (W) (L) (Basin) (Stand-By) | W | m | W2 | 1.20 |
| | L | m | L2 | 2.70 |
| | - | basin | BN | 4 |
| | - | stand-by | BNS | 2 |
| Screen Type | - | - | Fine Bar Screen | |
| Screen Set Number | SSN | set | BN | 6 |
| Check | | UNIT | APPLICATION | RESULT |
| Water Surface Load | | m3/m2/day | < 1800 | 1,777 |
| Average Velocity | | m/sec | < 0.3 | 0.07 |

2-2 Oxidation Ditch (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|-----------------------|--------|-----------------------|--------------------------------------|---------|
| Type | - | - | Re-circulation Flow Type | |
| Design Flow | Q1 | m ³ /day | - | 17,000 |
| | Q2 | m ³ /hr | - | 708.3 |
| Basin Number | BN | Basin | - | 6 |
| Inlet BOD Quality | C | mg/L | - | 240 |
| Inlet SS Quality | S | mg/L | - | 250 |
| Inlet BOD Matter | M | kg/day | $Q1 \cdot C \cdot 10^{-3}$ | 4,080 |
| BOD-SS Load | BS | kg/kg/day | - | 0.05 |
| MLSS Concentration | SS | mg/L | - | 4,000 |
| Required Volume | V1 | m ³ | $M / (SS \cdot BS \cdot 10^{-3})$ | 20,400 |
| Therefore | V2 | m ³ | - | 20,400 |
| Retention Time | T | hr | $(V2/Q1) \cdot 24$ | 28.8 |
| Return Sludge Ratio | R1 | % | - | 150 |
| | R2 | - | $R1/100$ | 1.5 |
| Return Sludge Quality | RS1 | mg/L | $(SS \cdot (1+R2) - C) / R2$ | 6,507 |
| Therefore | RS2 | mg/L | - | 6,510 |
| Sludge Age | SA | day | $SS \cdot V2 / (Q1 \cdot S)$ | 19.2 |
| Width | W | m | - | 6.0 |
| Water Depth | H | m | - | 3.0 |
| Length | L1 | m | $(V2/BN) / (W \cdot H)$ | 188.9 |
| Therefore | L2 | m | - | 190.0 |
| Dimension (Width) | W | m | W | 6.0 |
| (Depth) | H | m | H | 3.0 |
| (Length) | L | m | L2 | 190.0 |
| (Basin Number) | - | basin | BN | 6 |
| Required Oxygen | O2-day | kgO ₂ /day | $Q1 \cdot C \cdot 10^{-3} \cdot 2.0$ | 8,160.0 |
| | O2-hr | kgO ₂ /hr | $(O2-day) / 24$ | 340.0 |
| Aerator Motor Output | - | kW | $O2-hr / 1.9$ | 178.9 |
| | - | kW | - | 180.0 |
| Aerator Type | - | - | Slanting Shaft Screw Aerator | |
| Check | | UNIT | APPLICATION | RESULT |
| Retention Time | | hour | 24 - 48 | 29.0 |
| Oxygen Supply | | kgO ₂ /kg | 1.4 - 2.2 | 2.0 |
| Sludge Age | | day | 8 - 50 | 19.2 |

2-3 Final Sedimentation Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|--|------|-----------|--|--------|
| Type | - | - | Radial Flow Circular Type | |
| Design Flow | Q1 | m3/day | - | 17,000 |
| | Q2 | m3/sec | - | 708.33 |
| Basin Number | BN | Basin | - | 6 |
| Water Surface Load Therefore | L | m3/m2/day | $4.14 \times 10^4 \times 1^{0.95} \times SS^{-1.35}$ | 11.4 |
| | L | m3/m2/day | - | 12.0 |
| Required Surface Area | A1 | m2 | Q1/L | 1416.7 |
| | A2 | m2/Basin | A1/BN | 236.1 |
| Water Depth | H | m | - | 3.0 |
| Diameter Therefore | D1 | m | $(A2/3.14)^{0.5 \times 2}$ | 17.3 |
| | D2 | m | - | 16.0 |
| Dimension (Diameter) (Depth) (Basin Number) | D | m | D2 | 16.0 |
| | H | m | H | 3.0 |
| | - | Basin | BN | 6 |
| Sludge Collector Type | - | - | Central Drive Type | |
| Check | | UNIT | APPLICATION | RESULT |
| Water Surface Load | | m3/m2/day | 8 - 12 | 14.1 |
| Retention Time | | hour | 6.0 - 12.0 | 4.3 |

2-4 Disinfection Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|--|------|--------|----------------------------------|--------|
| Chemical Type | - | - | Chlorination Type | |
| Design Flow | Q1 | m3/day | - | 17,000 |
| | Q2 | m3/min | - | 11.81 |
| Retention Time | T | min. | - | 15.0 |
| Basin Number | BN | basin | - | 2 |
| Required Volume | V | m3 | Q2*T | 89 |
| Width | W | m | - | 3.00 |
| Water Depth | H | m | - | 1.50 |
| Length therefore | L1 | m | $V/(W \times H)$ | 19.676 |
| | L2 | m | - | 20.00 |
| Dosage | D | mg/L | - | 3.0 |
| Required Chemical Therefore | RC1 | kg/day | $Q1 \times D \times 10^{-3} / C$ | 51.00 |
| | RC2 | kg/hr | RC1/24 | 2.13 |
| Dimension (W) (Length) (Depth) (Basin) | W | m | W | 3.0 |
| | L | m | L2 | 20.0 |
| | H | m | H | 1.5 |
| | BN | basin | - | 2 |
| Chlorine Feeder | - | unit | including 1 for stand-by | 3 |
| Check | | UNIT | APPLICATION | RESULT |
| Retention Time | | min. | 15 | 15.2 |

2-5 Sludge Thickening Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|--|-------|-----------|---|--------|
| Type | - | - | Radial Flow Circular Type | |
| Design Flow | Q1 | m3/day | - | 17,000 |
| | Q2 | m3/hr | - | 570.8 |
| Basin Number | BN | Basin | - | 2 |
| Inlet SS Quality | C | mg/L | - | 250 |
| Removal Ratio | R1 | % | - | 80 |
| | R2 | - | R1/100 | 0.80 |
| Sludge Generation Ratio (Oxidation Ditch) | SG1 | % | - | 75 |
| | SG2 | - | SG1/100 | 0.75 |
| Inlet SS Matter | M | kg/day | $Q1 \cdot C \cdot R2 \cdot SG2 \cdot 10^{-3}$ | 2,550 |
| Solid Matter Load | L | kg/m2/day | - | 70.0 |
| Required Surface Area | A1 | m2 | M/L | 36.4 |
| | A2 | m2/Basin | A1/BN | 18.2 |
| Water Depth | H | m | - | 4.0 |
| Diameter | D1 | m | $(A2/3.14)^{0.5 \cdot 2}$ | 4.8 |
| Therefore | D2 | m | - | 5.0 |
| Dimension | D | m | D2 | 5.0 |
| (Depth) | H | m | H | 4.0 |
| (Basin) | Basin | Basin | BN | 2 |
| Check | | UNIT | APPLICATION | RESULT |
| Solid Matter Load | | kg/m2/day | 70 | 65.0 |

2-6 Aerobic Sludge Digestion Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|------------------------------|-------|-----------|---|---------|
| Type | - | - | Circular Type | |
| Basin Number | BN | Basin | - | 2 |
| Design Flow | Q1 | m3/day | - | 17,000 |
| Inlet SS Matter | M | kg/day | - | 2,550 |
| Moisture Content | G | % | - | 97.5 |
| Sludge Volume | V1 | m3/day | $M \cdot 100 / (100 - G)$ | 102.0 |
| Temperature - Summer | TS | °C | - | 26.5 |
| - Winter | TW | °C | - | 23.6 |
| Temperature - Sludge Age | TSA | day-°C | VolatileSolidReduction=40% | 470 |
| Sludge Age | SA | day | TSA/TS | 19.9 |
| Total Mass of VSS | VSS | kg/day | $0.8 \cdot M$ | 2,040 |
| VSS Reduction - Summer (41%) | VRS | kg/day | $VSS \cdot 0.4$ | 816.0 |
| - Winter (40%) | VRW | kg/day | $VSS \cdot 0.41$ | 836.4 |
| Required Volume | V | m3 | $V1 / 0.7 / (0.125 \cdot 0.8 + 1/SA)$ | 485 |
| Water Depth | H | m | - | 4.0 |
| Diameter | D1 | m | $(A2/3.14)^{0.5 \cdot 2}$ | 12.4 |
| Therefore | D2 | m | - | 13.0 |
| Dimension | D | m | D2 | 13.0 |
| (Depth) | H | m | H | 4.0 |
| (Basin) | Basin | Basin | BN | 2 |
| Required Oxygen | RO | kgO2/day | $2.3 \cdot VRS$ | 1876.8 |
| Required Air | RA | kg-Air/hr | $RO / (0.1 \cdot 0.233 \cdot 1.293) / 1440$ | 2,595.7 |
| Check | | UNIT | APPLICATION | RESULT |
| Retention Time | | day | 10.0 - 15.0 | 5.2 |
| Solid Matter Load | | kg/m3/day | 1.60 - 4.81 | 9.6 |

2-7 Sludge Thickening Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|------------------------------|---------------|-----------|----------------------------|--------|
| Type | - | - | Radial Flow Circular Type | |
| Basin Number | BN | Basin | - | 2 |
| Inlet SS Matter to Digestion | M1 | kg/day | - | 2,550 |
| Removal Ratio at Digestion | R1 | % | - | 40% |
| Inlet SS Matter | M2 | kg/day | $M1 \cdot (1 - R1)$ | 1530 |
| Moisture Content | G | % | - | 99.0 |
| Sludge Volume | V1 | m3/day | $M2 \cdot 100 / (100 - G)$ | 153.0 |
| Solid Matter Load | L | kg/m2/day | - | 70.0 |
| Required Surface Area | A1 | m2 | M/L | 21.9 |
| | A2 | m2/Basin | A1/BN | 10.9 |
| Water Depth | H | m | - | 4.0 |
| Diameter | D1 | m | $(A2/3.14)^{0.5} \cdot 2$ | 3.7 |
| | D2 | m | - | 5.0 |
| Dimension | D | m | D2 | 5.0 |
| | (Depth) H | m | H | 4.0 |
| | (Basin) Basin | Basin | BN | 2 |
| Check | | UNIT | APPLICATION | RESULT |
| Solid Matter Load | | kg/m2/day | 70 | 39.0 |

2-8 Sludge Drying Bed (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|------------------|---------------|--------|-------------------------------------|--------|
| Design Flow | Q1 | m3/day | - | 17,000 |
| Inlet SS Matter | M1 | kg/day | $Q1 \cdot C \cdot R2 \cdot 10^{-3}$ | 1,530 |
| | M2 | t/day | $M1/1000$ | 1.53 |
| Moisture Content | G | % | - | 99.0 |
| Sludge Volume | V1 | m3/day | $M2 \cdot 100 / (100 - G)$ | 51.0 |
| Drying Period | P | day | - | 10 |
| Required Volume | V2 | m3/day | $V1 \cdot P$ | 510.0 |
| Depth of Bed | H | m | - | 0.3 |
| Required Area | A | m2 | $V2/H$ | 1,700 |
| Unit Number | UN | Unit | - | 20 |
| Width per Unit | W | m | - | 6.0 |
| Length per Unit | L1 | m | $A/(UN \cdot W)$ | 14.2 |
| | L2 | m | - | 14.5 |
| Dimension | (Width) W | m | W | 6.0 |
| | (Length) L | m | L2 | 14.5 |
| | (Depth) H | m | H | 0.3 |
| | (Basin) Basin | Basin | BN | 20.0 |
| Check | | UNIT | APPLICATION | RESULT |
| Drying Period | | day | 20 | 10.2 |

Appendix 12.4.3 Sewage Treatment Plant - Capacity Calculation

CAPACITY CALCULATION OF FACILITIES Alternative 2 - Katugasutota (Dual Power Aerated Lagoon)

1 BASIC CONDITIONS

1-1 BASIC ITEMS

- (1) Name : Katugastota Sewage Treatment Plant
- (2) Land Area : Approximately 1.20 ha
- (3) Elevation : 475.950 m
- (4) Inlet Pipe Level : 472.447 m
- (5) Pipe Diameter : 300 m
- (6) Land Use :
- (7) Collection System : Seperate Type
- (8) Treatment Method : Sewage Treatment : Aerated Lagoon Method
Sludge Treatment : Pond Accumulation
- (9) Effluent Point : Mahaweli Ganga
- (10) Effluent Point Water Level : 446.4 m
- (11) Target Year : Year 2005 (Phase 1), Year 2015 (Phase 2)
- (12) Lowest Monthly Average Temperature 23.6 °C (January)

1-2 Design Population

Design Population : 5,260 Persons

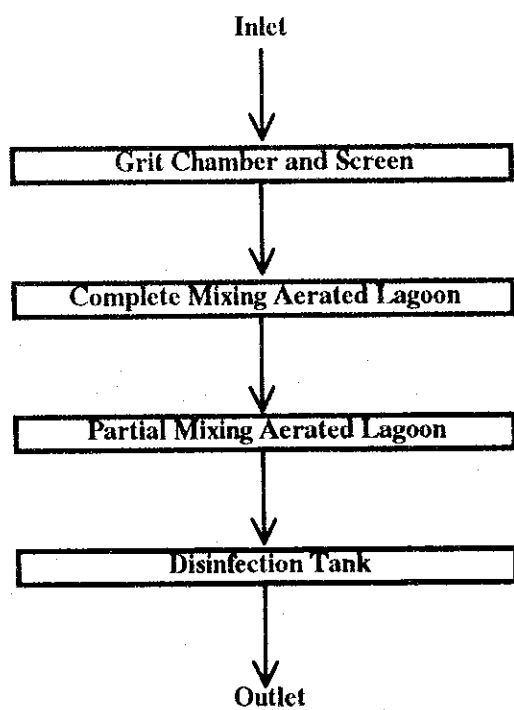
1-3 Design Sewage Flow

| ITEM | m3/day | m3/hr | m3/min | m3/sec |
|----------------|--------|-------|--------|--------|
| Daily Average | 1,500 | 62.5 | 1.04 | 0.017 |
| Daily Maximum | 1,700 | 70.8 | 1.18 | 0.020 |
| Hourly Maximum | 2,500 | 104.2 | 1.74 | 0.029 |

1-4 Design Sewage Quality

| ITEM | INFLUENT (mg/L) | EFFLUENT (mg/L) | REMOVAL RATIO (%) | REMARKS |
|------|--------------------|--------------------|----------------------|---------|
| BOD | 240 | 30 | 88 | |
| SS | 250 | 50 | 80 | |

1-5 Flow Chart (Dual Power Aerated Lagoon)



1-6 Design Criteria for Dual Power Aerated Lagoon

| ITEMS | UNIT | Formula or Value | Application |
|---|-------------------------------------|------------------|-------------|
| 1-6-1 Grit Chamber | | | |
| (1) Water Surface Load | m ³ /m ² /day | > 1800 | 1,800 |
| (2) Average Velocity | m/sec | > 0.3 | 0.3 |
| 1-6-2 Complete Mixing Aerated Lagoon | | | |
| (1) Retention Time | day | 1.5 - 2.5 | 1.50 |
| (2) Water Depth | m | 3.0 - 4.0 | 3.0 |
| (3) Power Requirement for Mixing | W/m ³ | > 6.0 | 6.0 |
| 1-6-3 Partial Mixing Aerated Lagoon | | | |
| (1) Retention Time | day | 2.0 | 2.0 |
| (2) Water Depth | m | 2.0 - 4.0 | 3.0 |
| (3) Power Requirement for Mixing | W/m ³ | > 1.0 | 1.0 |
| (4) Number of Cell | Cell/Basin | 1 - 3 | 3 |
| 1-6-4 Storm Water Settling Tank | | | |
| (1) Water Depth | m | 1.5 - 3.0 | 1.5 |
| (2) Retention Time (Hourly Max. - Rain) | hour | > 0.5 | 0.5 |
| (3) Water Surface Load (Hourly Max. - Rain) | m ³ /m ² /day | 75 - 150 | 150.0 |
| 1-6-5 Disinfection Tank | | | |
| (1) Retention Time | min. | > 15 | 15.0 |
| (2) Dosage | mg/l | 2.0 - 4.0 | 3.0 |

2 CAPACITY CALCULATION

2-1 Grit Chamber and Screen (Hourly Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|-------------------------|--------------|-----------|--------------------|--------|
| Type | - | - | Parallel Flow Type | |
| Design Flow | Q1 | m3/day | - | 2,500 |
| | Q2 | m3/sec | - | 0.029 |
| Water Surface Load | WSL | m3/m2/day | - | 1,800 |
| Required Surface Area | RSA | m2 | Q1/WSL | 1.389 |
| Basin Number (Total) | BN | basin | - | 2 |
| Basin Number (Stand-By) | BNS | basin | - | 1 |
| Average Velocity | V | m/sec | - | 0.30 |
| Depth | H | m | - | 0.20 |
| Width | W1 | m | Q2/(V*H) | 0.482 |
| | Therefore W2 | m | - | 0.50 |
| Length | L1 | m | RSA/W2/(BN-BNS) | 2.778 |
| | Therefore L2 | m | - | 3.00 |
| Dimension | (W) | W | W2 | 0.50 |
| | (L) | L | L2 | 3.00 |
| | (Basin) | - | basin | BN |
| | (Stand-By) | - | stand-by | BNS |
| Screen Type | - | - | Fine Bar Screen | |
| Screen Set Number | SSN | set | BN | 2 |
| Check | | UNIT | APPLICATION | RESULT |
| Water Surface Load | | m3/m2/day | > 1800 | 1,667 |
| Average Velocity | | m/sec | > 0.3 | 0.29 |

2-2 Complete Mixing Aerated Lagoon (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|---------------------------|------|-----------------------|--|--------|
| Type | - | - | Rectangular Type | |
| Design Flow | Q1 | m ³ /day | - | 1,700 |
| | Q2 | m ³ /hr | - | 70.83 |
| Retention Time | T1 | day | - | 1.50 |
| Inlet BOD Quality | So | mg/L | - | 240 |
| Required Volume | V1 | m ³ /basin | $Q1 \cdot T$ | 2,550 |
| Basin Number | BN | basin | - | 2 |
| Required Volume per Basin | VBN | m ³ /basin | $Q1 \cdot T / BN$ | 1,275 |
| Water Depth | H | m | - | 3.00 |
| Required Surface Area | A | m ² | V/H | 425 |
| Width | W | m | - | 30.00 |
| Length | L1 | m | A/W | 14.167 |
| Therefore | L2 | m | - | 15.00 |
| Oxygen Demand Rate | PR1 | kg/h | $(4.16 \cdot 10^{-5}) \cdot r \cdot Q1 \cdot So$ | 25 |
| -max. oxygen uptake | r | W/m ³ | - | 1.5 |
| Aeration Unit Power Rate | PRO | kg/h | $1000 \cdot PR1 / (N \cdot Q1 \cdot T1)$ | 5.25 |
| Therefore | PRO | W/m ³ | - | 5.6 |
| -aeration performance | N | W/m ³ | - | 1.9 |
| Power Requirement | P1 | kW | - | 16.0 |
| 1) Oxygen Requirement | P1O | kW | $PR1 / N$ | 13.4 |
| 2) Mixing Power | P1M | kW | $V1 \cdot P0 \cdot 10^{-3}$ | 15.3 |
| Dimension (Width) | W | m | W | 30.00 |
| (Length) | L | m | L2 | 15.00 |
| (Depth) | H | m | H | 3.00 |
| (Basin) | - | basin | BN | 2 |
| Aerator Type | - | - | Slanting Shaft Screw Aerator | |
| Check | | UNIT | APPLICATION | RESULT |
| Retention Time | | day | 1.5 - 2.5 | 1.59 |

2-3 Partial Mixing Aerated Lagoon (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|-------------------------------|------|------------|--|--------|
| Type | - | - | Rectangular Type | |
| Design Flow | Q1 | m3/day | - | 1,700 |
| | Q2 | m3/hr | - | 70.83 |
| Retention Time | T2 | day | - | 2.00 |
| Required Volume | V2 | m3/basin | $Q2 \cdot T$ | 3,400 |
| Basin Number | BN | basin | - | 2 |
| Cells Number | CN | cell/basin | - | 3 |
| Stand-by Cell Number | CNS | basin | - | 1 |
| Sludge Accumulation | SA | m3/year | $365 \cdot Q1 \cdot Xi / (x \cdot 10^6)$ | 853 |
| -inert solid concentration | Xi | mg/l | - | 55 |
| -weight fraction of solids | x | - | - | 0.04 |
| No. of Cells Cleaned per Year | CNC | basin | - | 3 |
| Total Sludge Accumulation | TSA | m3 | - | 1,280 |
| Required Volume | V | m3/cell | $(Q1 \cdot T + TSA) / (BN \cdot CN - CNS)$ | 936 |
| Water Depth | D | m | - | 4.00 |
| Required Surface Area | A | m2/cell | V/H | 234 |
| Width | W | m | - | 30.00 |
| Length | L1 | m | A/W | 7.800 |
| Therefore | L1 | m | - | 8.00 |
| Power Requirement | P2 | kW | - | 4.0 |
| 1) Mixing Power | P2M | kW | $Q1 \cdot T2 \cdot CN \cdot 10^{-3}$ | 3.4 |
| Dimension (Width) | W | m | W | 30.00 |
| (Length) | L | m | L1 | 8.00 |
| (Depth) | H | m | H | 4.00 |
| (Basin) | - | basin | BN | 2 |
| (Cell) | - | cell/basin | CN | 3 |
| (Stand-by Cell) | - | cell | - | 1 |
| Aerator Type | - | - | Slanting Shaft Screw Aerator | |
| Check | | UNIT | APPLICATION | RESULT |
| Surface Area | | m2 | - | 1,440 |
| Retention Time | | day | 2.0 | 2.07 |

2-6 Disinfection Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|-------------------|------|---------------------|--------------------------|--------|
| Chemical Type | - | - | Chlorination Type | |
| Design Flow | Q1 | m ³ /day | - | 1,700 |
| | Q2 | m ³ /min | - | 1.18 |
| Retention Time | T | min. | - | 15.0 |
| Basin Number | BN | basin | - | 1 |
| Required Volume | V | m ³ | Q2*T | 18 |
| Width | W | m | - | 1.00 |
| Water Depth | H | m | - | 1.00 |
| Length | L1 | m | V/(W*H) | 17.708 |
| therefore | L2 | m | - | 18.00 |
| Dosage | D | mg/L | - | 3.0 |
| Required Chemical | RC1 | kg/day | Q1*D*10 ⁻³ /C | 5.10 |
| Therefore | RC2 | kg/hr | RC1/24 | 0.21 |
| Dimension (Width) | W | m | W | 1.00 |
| (Length) | L | m | L2 | 18.00 |
| (Depth) | H | m | H | 1.00 |
| (Depth) | BN | basin | - | 1 |
| Chlorine Feeder | - | unit | including 1 for stand-by | 3 |
| Check | | UNIT | APPLICATION | RESULT |
| Retention Time | | min. | > 15 | 15.2 |

Appendix 12.5 Summary of Construction Cost

Kandy

Exchange Rate = 1.8 Yen/Rs

Construction Cost - Master Plan : Alternatives

| Facilities | Alternative 1 | | | Alternative 2 | | |
|---------------------------|----------------|-----------|---------|----------------|-----------|-----------|
| | Specifications | Civil | M & E | Specifications | Civil | M & E |
| 1. Sewer | | | | | | |
| Sub-Total | | 777,683 | | | 747,251 | |
| 2. Pumping Station | | | | | | |
| Kandy | | | | | | |
| P/S 1 | 0.74*27*2 | 918 | 2,185 | 0.74*27*2 | 918 | 2,185 |
| P/S 2-1 | 1.74*48*2 | 1,383 | 4,211 | | | |
| P/S 2-2 | 1.74*48*2 | 1,383 | 4,211 | | | |
| STP-1 | 9.0*14*4 | 7,211 | 12,050 | 8.2*14*4 | 7,211 | 11,275 |
| STP-2 | 4.5*14*4 | 0 | 3,661 | 4.1*14*4 | 0 | 3,454 |
| Katugastota | | | | | | |
| STP | | | | 1.74*24*2 | 1,210 | 2,438 |
| Sub-Total | | 10,895 | 26,317 | | 9,339 | 19,351 |
| 3. Sewage Treatment Plant | | | | | | |
| Kandy | 18,000m3/day | 358,896 | 666,558 | 17,000m3/day | 344,809 | 636,899 |
| Katugastota | | | | 1,700m3/day | 45,428 | 35,242 |
| Sub-Total | | 358,896 | 666,558 | | 390,237 | 672,141 |
| Total | | 1,147,474 | 692,875 | | 1,146,827 | 691,492 |
| | | | | | | 1,838,319 |

Construction Cost - Feasibility Study

| Facilities | M/P (Alternative 2) | | | F/S (Phase 1) | | | Phase 2 | | |
|---------------------------|---------------------|-----------|---------|----------------|---------|---------|----------------|---------|---------|
| | Specifications | Civil | M & E | Specifications | Civil | M & E | Specifications | Civil | M & E |
| 1. Sewer | | | | | | | | | |
| Sub-Total | | 747,251 | | | 463,191 | | | 284,060 | |
| 2. Pumping Station | | | | | | | | | |
| Kandy | | | | | | | | | |
| P/S 1 | 0.74*27*2 | 918 | 2,185 | 0.74*27*2 | 918 | 2,185 | | | |
| STP-1 | 8.2*14*2 | 7,211 | 11,275 | 8.2*14*2 | 7,211 | 8,137 | 8.2*14*2 | 0 | 3,137 |
| STP-2 | 4.1*14*2 | 0 | 3,454 | 4.1*14*2 | 0 | 1,727 | 4.1*14*2 | 0 | 1,727 |
| Katugastota | | | | | | | | | |
| STP | 1.74*24*2 | 1,210 | 2,438 | | 0 | 0 | 1.74*24*2 | 1,210 | 2,438 |
| Sub-Total | | 9,339 | 19,351 | | 8,129 | 12,049 | | 1,210 | 7,302 |
| 3. Sewage Treatment Plant | | | | | | | | | |
| Kandy | 17,000m3/day | 344,809 | 636,899 | | | | 8,500m3/day | 154,102 | 316,654 |
| Katugastota | 1,700m3/day | 45,428 | 35,242 | | 0 | 0 | 1,700m3/day | 45,428 | 35,242 |
| Sub-Total | | 390,237 | 672,141 | | 190,707 | 320,246 | | 199,530 | 351,896 |
| Total | | 1,146,827 | 691,492 | | 662,027 | 332,294 | | 484,800 | 359,197 |
| | | | | | | | | | 843,997 |

Appendix 12.6 Cost of Sewer

Alternative 2 (Applied)

(Unit : Rs)

Master Plan

Feasibility Study

| ITEM | DESCRIPTION | Depth | UNIT | RATE | QUANTITY | COST | QUANTITY | COST |
|------------------|----------------------|-------|------|-----------|----------|-------------|----------|-------------|
| Clay Pipe Laying | 150 mm (Lateral) | 1.5 | m | 5,498 | 9,300 | 51,131,400 | 4,500 | 24,741,000 |
| | 150 mm | 1.5 | m | 5,498 | 4,651 | 25,571,198 | 4,651 | 25,571,198 |
| | 150 mm | 2.5 | m | 7,871 | 793 | 6,241,703 | 793 | 6,241,703 |
| | 225 mm | 1.5 | m | 7,142 | 1,527 | 10,905,834 | 1,527 | 10,905,834 |
| | 225 mm | 2.5 | m | 9,603 | 1,859 | 17,851,977 | 1,509 | 14,490,927 |
| | 225 mm | 3.5 | m | 12,459 | 691 | 8,609,169 | 691 | 8,609,169 |
| | 225 mm | 7.5 | m | 27,832 | 100 | 2,783,200 | 0 | 0 |
| | 300 mm | 1.5 | m | 10,593 | 1,942 | 20,571,606 | 1,942 | 20,571,606 |
| | 300 mm | 2.5 | m | 13,173 | 680 | 8,957,640 | 680 | 8,957,640 |
| | 300 mm | 3.5 | m | 16,147 | 80 | 1,291,760 | 80 | 1,291,760 |
| | 300 mm | 7.5 | m | 31,994 | 80 | 2,559,520 | 80 | 2,559,520 |
| | 400 mm | 1.5 | m | 15,652 | 2,590 | 40,538,680 | 840 | 13,147,680 |
| | 400 mm | 2.5 | m | 18,373 | 548 | 10,068,404 | 348 | 6,393,804 |
| | 400 mm | 4.5 | m | 25,001 | 200 | 5,000,200 | 0 | 0 |
| | 450 mm | 1.5 | m | 17,475 | 75 | 1,310,625 | 75 | 1,310,625 |
| | 500 mm | 1.5 | m | 20,461 | 288 | 5,892,768 | 288 | 5,892,768 |
| | 500 mm | 2.5 | m | 23,318 | 70 | 1,632,260 | 70 | 1,632,260 |
| | 600 mm | 1.5 | m | 33,513 | 312 | 10,456,056 | 312 | 10,456,056 |
| | 600 mm | 2.5 | m | 36,508 | 55 | 2,007,940 | 55 | 2,007,940 |
| HP Pipe Laying | 675 mm | 1.5 | m | 16,046 | 500 | 8,023,000 | 500 | 8,023,000 |
| | 675 mm | 2.5 | m | 19,178 | 180 | 3,452,040 | 180 | 3,452,040 |
| | 675 mm | 3.5 | m | 22,704 | 120 | 2,724,480 | 120 | 2,724,480 |
| | 675 mm | 4.5 | m | 26,626 | 190 | 5,058,940 | 190 | 5,058,940 |
| | 675 mm | 5.5 | m | 30,942 | 100 | 3,094,200 | 100 | 3,094,200 |
| | 750 mm | 2.5 | m | 21,242 | 150 | 3,186,300 | 150 | 3,186,300 |
| | 825 mm | 1.5 | m | 20,005 | 400 | 8,002,000 | 400 | 8,002,000 |
| | 825 mm | 2.5 | m | 23,413 | 480 | 11,238,240 | 480 | 11,238,240 |
| | 825 mm | 4.5 | m | 31,416 | 700 | 21,991,200 | 700 | 21,991,200 |
| | 825 mm | 7.5 | m | 46,382 | 50 | 2,319,100 | 50 | 2,319,100 |
| DI Pipe Laying | 100 mm | 1.5 | m | 6,242 | 650 | 4,057,300 | 650 | 4,057,300 |
| | 150 mm | | m | 7,358 | - | - | - | - |
| Manhole | Type 1 | | Nr | 80,181 | 517 | 41,453,577 | 369 | 29,586,789 |
| | Type 2 | | Nr | 93,941 | 57 | 5,354,637 | 57 | 5,354,637 |
| | Type 3 | | Nr | 109,418 | - | - | - | - |
| Connection Pipe | 100mmPVC ,L=4m | | Nr | 25,712 | 12,402 | 318,880,224 | 5,794 | 148,975,328 |
| Inspection Pit | RC,300x300 | | Nr | 5,098 | 12,402 | 63,225,396 | 5,794 | 29,537,812 |
| Siphon | | 4.5 | Nr | 868,712 | 1 | 868,712 | 1 | 868,712 |
| Siphon Pipe | 450mmx2 | 4.5 | m | 27,024 | 40 | 1,080,960 | 40 | 1,080,960 |
| Siphon | | 7.5 | Nr | 1,053,558 | 1 | 1,053,558 | 1 | 1,053,558 |
| Siphon Pipe | 450mmx2 | 7.5 | m | 40,127 | 40 | 1,605,080 | 40 | 1,605,080 |
| Road Crossing | Jacking(675mm) | | m | 240,000 | 30 | 7,200,000 | 30 | 7,200,000 |
| TOTAL | Sewer Main + Lateral | | | | 29,361 | 747,250,884 | 21,961 | 463,191,166 |
| | Sewer Main | | | | 20,061 | | 17,461 | |

Alternative 1

(Unit : Rs) Master Plan

Feasibility Study

| ITEM | DESCRIPTION | Depth | UNIT | RATE | QUANTITY | COST | QUANTITY | COST |
|------------------|----------------------|-------|------|-----------|----------|-------------|----------|------|
| Clay Pipe Laying | 150 mm (Lateral) | 1.5 | m | 5,498 | 9,300 | 51,131,400 | | |
| | 150 mm | 1.5 | m | 5,498 | 4,651 | 25,571,198 | | |
| | 150 mm | 2.5 | m | 7,871 | 793 | 6,241,703 | | |
| | 225 mm | 1.5 | m | 7,142 | 1,527 | 10,905,834 | | |
| | 225 mm | 2.5 | m | 9,603 | 1,859 | 17,851,977 | | |
| | 225 mm | 3.5 | m | 12,459 | 691 | 8,609,169 | | |
| | 225 mm | 7.5 | m | 27,832 | 100 | 2,783,200 | | |
| | 300 mm | 1.5 | m | 10,593 | 1,268 | 13,431,924 | | |
| | 300 mm | 2.5 | m | 13,173 | 320 | 4,215,360 | | |
| | 300 mm | 7.5 | m | 31,994 | 80 | 2,559,520 | | |
| | 400 mm | 1.5 | m | 15,652 | 2,590 | 40,538,680 | | |
| | 400 mm | 2.5 | m | 18,373 | 548 | 10,068,404 | | |
| | 400 mm | 4.5 | m | 25,001 | 200 | 5,000,200 | | |
| | 450 mm | 1.5 | m | 17,475 | 674 | 11,778,150 | | |
| | 450 mm | 2.5 | m | 20,263 | 360 | 7,294,680 | | |
| | 450 mm | 3.5 | m | 23,446 | 80 | 1,875,680 | | |
| | 600 mm | 1.5 | m | 33,513 | 363 | 12,165,219 | | |
| | 600 mm | 2.5 | m | 36,508 | 70 | 2,555,560 | | |
| HP Pipe Laying | 675 mm | 1.5 | m | 16,046 | 632 | 10,141,072 | | |
| | 675 mm | 2.5 | m | 19,178 | 55 | 1,054,790 | | |
| | 675 mm | 3.5 | m | 22,704 | 120 | 2,724,480 | | |
| | 675 mm | 4.5 | m | 26,626 | 100 | 2,662,600 | | |
| | 675 mm | 5.5 | m | 30,942 | 100 | 3,094,200 | | |
| | 750 mm | 1.5 | m | 17,972 | 180 | 3,234,960 | | |
| | 750 mm | 2.5 | m | 21,242 | 330 | 7,009,860 | | |
| | 750 mm | 4.5 | m | 28,964 | 90 | 2,606,760 | | |
| | 825 mm | 1.5 | m | 20,005 | 400 | 8,002,000 | | |
| | 825 mm | 2.5 | m | 23,413 | 480 | 11,238,240 | | |
| | 825 mm | 4.5 | m | 31,416 | 700 | 21,991,200 | | |
| | 825 mm | 7.5 | m | 46,382 | 50 | 2,319,100 | | |
| DI Pipe Laying | 100 mm | 1.5 | m | 6,242 | 650 | 4,057,300 | | |
| | 200 mm | 1.5 | m | 8,514 | 2,600 | 22,136,400 | | |
| Manhole | Type 1 | | Nr | 80,181 | 509 | 40,812,129 | | |
| | Type 2 | | Nr | 93,941 | 65 | 6,106,165 | | |
| | Type 3 | | Nr | 109,418 | - | - | | |
| Connection Pipe | 100mmPVC ,L=4m | | Nr | 25,712 | 12,402 | 318,880,224 | | |
| Inspection Pit | RC,300x300 | | Nr | 5,098 | 12,402 | 63,225,396 | | |
| Siphon | | 4.5 | Nr | 868,712 | 1 | 868,712 | | |
| Siphon Pipe | 450mmx2 | 4.5 | m | 27,024 | 40 | 1,080,960 | | |
| Siphon | | 7.5 | Nr | 1,053,558 | 1 | 1,053,558 | | |
| Siphon Pipe | 450mmx2 | 7.5 | m | 40,127 | 40 | 1,605,080 | | |
| Road Crossing | Jacking(675mm) | | m | 240,000 | 30 | 7,200,000 | | |
| TOTAL | Sewer Main + Lateral | | | | 31,961 | 777,683,044 | | |
| | Sewer Main | | | | 22,661 | | | |

| | | |
|--------------|----------------|--------|
| Manhole Span | 50 | m |
| Manhole Type | 150 to 600 mm | Type 1 |
| | 700 to 900 mm | Type 2 |
| | 900 to 1200 mm | Type 3 |

Numbers of Service Connections

| | Kandy | Reference |
|-------------------------------|--------|----------------|
| Size of Family (people/house) | 6.65 | |
| M/P Population (2015) | 54,985 | |
| Domestic (No. of Houses) | 8,268 | |
| Total (No. of houses) | 12,402 | Domestic x 1.5 |
| F/S Population (2005) | 19,262 | |
| Domestic (No. of Houses) | 2,897 | |
| Total (No. of Connections) | 5,794 | Domestic x 2 |

Appendix 12.7 Unit Cost

Appendix 12.7.1 Unit Cost of Civil Works

are used for cost estimate.

| | | Item | | NWSDB Rate '97 | | Towns South - Ground Reservoir | | | Towns South - Pumping Station | | | Applied | Adjusted |
|-------------------|--|---------------------------------------|----------------|----------------|--------------|--------------------------------|---------------|------------|------------------------------------|---------------|------------|-----------|-----------|
| | | | | | Overhead 20% | Local (Rs) | Foreign (Yen) | Total (Rs) | Local (Rs) | Foreign (Yen) | Total (Rs) | | |
| 1. Excavation | | | | | | | | | | | | | |
| | | Bulldozer (incl. Backfilling) | | (Basement) | (Basement) | | | | | | | | 490.00 |
| | | Backhoe (incl. Backfilling) | | (Pit/Trench) | (Pit/Trench) | (150 mm) | | | (225 mm) | | | | 790.00 |
| | | Rock excavation | m ³ | 1,469.00 | 1,763.00 | 69.00 | 544.38 | 371.43 | 1,716.00 | 195.27 | 1,824.48 | 1,808.99 | 1,990.00 |
| 2. Earth Filling | | | | | | | | | | | | | |
| | | earth available at site | m ³ | 141.00 | 169.00 | | | | | | | 169.00 | 190.00 |
| | | earth to be borrowed | m ³ | 324.00 | 389.00 | | | | | | | 389.00 | 430.00 |
| 3. Soil Disposal | | | | | | | | | | | | | |
| | | On site | m ³ | 68.00 | 82.00 | | | | | | | 68.00 | 80.00 |
| | | Off site | m ³ | 232.00 | 278.00 | | | | | | | 278.00 | 310.00 |
| 4. Piling | | | | | | | | | | | | | |
| | | On site 600 mm dia. | m | | | 1,824.81 | 14,399.00 | 9,824.25 | | | | 9,824.25 | 10,810.00 |
| 5. Concrete Work | | | | | | | | | | | | | |
| | | Grade 10 | | | | | | | | | | | 7,840.00 |
| | | Foundations | m ³ | 3,743.00 | 4,492.00 | 76.07 | 600.18 | 409.50 | 514.80 | 58.58 | 547.34 | 7,123.19 | |
| | | Grade 20/30 | | (Grade 20) | | (Grade 30) | | | (Grade 30) | | | 8,658.97 | 9,530.00 |
| | | Columns | m ³ | 4,868.00 | 5,842.00 | 1,820.50 | 14,362.89 | 9,799.88 | 6,864.00 | 781.07 | 7,297.93 | 8,659.97 | 9,530.00 |
| 6. Form Work | | | | | | | | | | | | | |
| | | | | | | | | | | | | 960.43 | 1,060.00 |
| 7. Reinforcement | | | | | | | | | | | | | |
| | | Tor steel | | 50,220.00 | 60,264.00 | 13,510.53 | 106,591.98 | 72,728.30 | 62,920.00 | 7,159.76 | 66,897.64 | 66,329.41 | 72,970.00 |
| | | Mild steel | ton | 46,920.00 | 56,304.00 | 11,312.83 | 89,253.07 | 60,897.87 | 62,920.00 | 7,159.76 | 66,897.64 | 66,329.41 | 72,970.00 |
| 8. Building | | | | | | | | | | | | | |
| | | Offices 2F, 126 m ² | m ² | 9,600.00 | 11,520.00 | 13,494.97 | 1,535.61 | 14,348.09 | | | | 14,226.22 | 15,700.00 |
| | | Operating houses | m ² | 8,600.00 | 10,320.00 | | | | | | | | 20,000.00 |
| | | Pumping Station BF, 181m ² | | | | | | | 31,855.72 | 3,624.91 | 33,869.56 | 33,581.87 | 37,000.00 |
| | | Chlorine House 1F, 24m ² | m ² | | | 17,014.23 | 1,973.50 | 18,110.62 | | | | 17,953.99 | 19,800.00 |
| | | Store houses 1F, 24m ² | m ² | 8,200.00 | 9,840.00 | 18,950.98 | 2,156.46 | 20,149.01 | | | | 19,977.86 | 22,000.00 |
| | | Quarters 1F, 100m ² | m ² | | | 17,496.47 | 1,971.32 | 18,591.64 | | | | 18,435.19 | 20,300.00 |
| 9. Pavement | | | | | | | | | | | | | |
| | | Reinstatement | m ² | - | - | 206.58 | 1,629.82 | 1,112.04 | Actual payment to RDA Rs. 2000.00) | | | 2,000.00 | 2,000.00 |
| 10. Miscellaneous | | | | | | | | | | | | | |
| | | Miscellaneous | % | - | - | | | | | | | | 5 to 20 % |

Appendix 12.7.2 Unit Cost of Piping Materials

are used for cost estimate.

| | | Diameter (mm) | | NWSDB Rate 97 | | Beire Lake | Manufacturer | Towns South | | | | Applied | Adjusted |
|-----------------|----------------|---------------|----|---------------|--------------|------------|--------------|-------------|---------------|------------|------------|---------------------|------------|
| | | | | Rs/m | Overhead 20% | Rs/m | Rs/m | Local (Rs) | Foreign (Yen) | C. D. (Rs) | Total (Rs) | | |
| 1. Water Supply | | | | | | | | | | | | | |
| | DIP | | | (CIF+C.D.) | | | | | | | | | |
| | | 200 | mm | 2,647.48 | 3,177.00 | | | 65.58 | 6,467.59 | 661.72 | 3,807.10 | 3,807.10 | 3,500.00 |
| | | 250 | mm | 2,981.44 | 3,578.00 | | | | | | | | 4,190.00 |
| | | 300 | mm | 3,794.56 | 4,553.00 | | | 82.79 | 8,165.06 | 835.39 | 4,806.30 | 4,806.30 | 5,290.00 |
| | | 350 | mm | 4,537.50 | 5,445.00 | | | 103.27 | 10,234.03 | 1,041.95 | 6,018.57 | 6,018.57 | 6,630.00 |
| | | 400 | mm | 5,324.00 | 6,389.00 | | | 137.05 | 13,515.35 | 1,382.79 | 7,955.72 | 7,955.72 | 8,760.00 |
| | | 450 | mm | 6,352.50 | 7,623.00 | | | 144.09 | 14,210.53 | 1,453.92 | 8,364.93 | 8,364.93 | 9,210.00 |
| | | 500 | mm | 7,292.67 | 8,751.00 | | | 193.08 | 19,041.13 | 1,948.15 | 11,208.43 | 11,208.43 | 12,330.00 |
| | | 600 | mm | 9,075.00 | 10,890.00 | | | 223.43 | 22,034.08 | 2,254.36 | 12,970.21 | 12,970.21 | 14,270.00 |
| | | 700 | mm | 11,918.50 | 14,302.00 | | | | | | | | 20,000.00 |
| | | 800 | mm | 14,762.00 | 17,714.00 | | | 462.19 | 45,580.63 | 4,663.47 | 26,830.72 | 26,830.72 | 29,520.00 |
| | | 900 | mm | 15,851.00 | 19,021.00 | | | | | | | | 35,000.00 |
| | PVC (type 600) | | | | | | | | | | | | (type 600) |
| | | 63 | mm | 50.00 | 60.00 | | | 55.95 | 55.18 | | 82.23 | 82.23 | 100.00 |
| | | 75 | mm | 78.00 | 94.00 | | | | | | | 114.78 | 130.00 |
| | | 90 | mm | 118.00 | 142.00 | | | 109.75 | 108.23 | | 161.29 | 161.29 | 180.00 |
| | | 110 | mm | 173.00 | 208.00 | | | 161.15 | 158.93 | | 236.83 | 236.83 | 270.00 |
| | | 160 | mm | 340.00 | 408.00 | | | 340.35 | 335.65 | | 500.18 | 500.18 | 560.00 |
| | | 225 | mm | 655.00 | 786.00 | | | 667.15 | 657.94 | | 980.45 | 980.45 | 1,080.00 |
| 2. Sewerage | | | | | | | | | | | | | |
| | PVC (type 600) | | | | | | (type 400) | (type 600) | | | | | (type 600) |
| | | 110 | mm | 173.00 | 208.00 | | | 161.15 | 158.93 | | 236.83 | 236.83 | 270.00 |
| | | 160 | mm | 340.00 | 408.00 | | 786.95 | 340.35 | 335.65 | | 500.18 | 500.18 | 510.00 |
| | | 225 | mm | 655.00 | 786.00 | | 1,496.80 | 667.15 | 657.94 | | 980.45 | 980.45 | 990.00 |
| | | 280 | mm | 1,013.00 | 1,216.00 | | 2,294.65 | | | | | 2,294.65 | 2,300.00 |
| | | 315 | mm | | | | 2,888.02 | | | | | 2,888.02 | 2,890.00 |
| | Hume Pipe | | | | | | | | | | | | |
| | | 150 | mm | 352.00 | 422.00 | | 198.39 | | | | | | |
| | | 225 | mm | 497.00 | 596.00 | | 273.13 | | | | | | |
| | | 250 | mm | | | | | | | | | | |
| | | 300 | mm | 660.00 | 792.00 | | 355.25 | | | | | 792.00 | 800.00 |
| | | 375 | mm | 900.00 | 1,080.00 | | 516.73 | | | | | 1,080.00 | 1,080.00 |
| | | 400 | mm | | | | | | | | | | |
| | | 450 | mm | 995.00 | 1,194.00 | | 611.31 | 2,577.99 | 1,307.04 | | 3,200.39 | 1,194.00 | 1,200.00 |
| | | 500 | mm | | | | | | | | | | |
| | | 544 | mm | | | | | 4,124.78 | 2,091.26 | | 5,120.62 | (with inner lining) | |
| | | 600 | mm | 1,386.00 | 1,663.00 | | 847.07 | | | | | 1,663.00 | 1,670.00 |
| | | 675 | mm | | | 5,960.00 | | | | | | 5,960.00 | 5,960.00 |
| | | 750 | mm | 1,868.00 | 2,242.00 | 6,790.00 | 1,092.52 | | | | | 6,790.00 | 6,790.00 |
| | | 825 | mm | | | 7,630.00 | 1,093.52 | | | | | 7,630.00 | 7,630.00 |
| | | 900 | mm | 2,542.00 | 3,050.00 | | 1,495.76 | | | | | 3,660.00 | 3,660.00 |
| | | 1050 | mm | 3,300.00 | 3,960.00 | | 3,820.13 | | | | | 4,752.00 | 4,760.00 |
| | Clay Pipe | | | | | | | | | | | | |
| | | 150 | mm | 410.00 | 492.00 | 730.88 | | | | | | 730.88 | 740.00 |
| | | 225 | mm | 648.00 | 778.00 | 1,789.84 | | | | | | 1,789.84 | 1,790.00 |
| | | 250 | mm | | | | | | | | | | |
| | | 300 | mm | 1,235.00 | 1,482.00 | 4,464.66 | | | | | | 4,464.66 | 4,470.00 |
| | | 400 | mm | | | 8,578.39 | | | | | | 8,578.39 | 8,580.00 |
| | | 450 | mm | | | 9,959.28 | | | | | | 9,959.28 | 9,960.00 |
| | | 500 | mm | | | 12,457.10 | | | | | | 12,457.10 | 12,460.00 |
| | | 600 | mm | | | 24,476.30 | | | | | | 24,476.30 | 24,480.00 |

Note : 1. For transmission mains of water supply, 20 % of the cost of pipes shall be add to compensate the cost of specials, valves etc.

2. For distribution mains of water supply, 35 % of the cost of pipes shall be add to compensate the cost of specials, valves etc.

Appendix 12.7.3 Unit Cost of Pipe Laying

are used for cost estimate.

| Diameter | | | NWSDB Rate 97 | | Towns South | | | Japan | Sri Lanka | Applied | Adjusted |
|--------------------------|---------------------|----------------|---|--------------|---|--------------|------------|---------|-----------|--------------------|----------|
| (mm) | | | Rs/m | Overhead 20% | Local (Rs) | Foreign(Yen) | Total (Rs) | Man-Day | Rs/m | | |
| 1. Laying | | | | | | | | | | (only Pipe Laying) | |
| DIP | | | (with 1 to 2m excavation, backfilling etc.) | | | | | | | | |
| | | 200 mm | 559.00 | 671.00 | | | | 0.18 | 124.60 | 124.60 | 125.00 |
| | | 250 mm | 580.00 | 696.00 | 100.06 | 789.40 | 475.96 | 0.22 | 154.00 | 154.00 | 154.00 |
| | | 300 mm | 698.00 | 838.00 | 105.58 | 832.96 | 502.23 | 0.26 | 182.70 | 182.70 | 183.00 |
| | | 350 mm | 740.00 | 888.00 | 123.73 | 976.16 | 588.57 | 0.32 | 222.60 | 222.60 | 223.00 |
| | | 400 mm | 795.00 | 954.00 | 129.25 | 1,019.72 | 614.83 | 0.38 | 269.03 | 269.03 | 270.00 |
| | | 450 mm | 852.00 | 1,022.00 | 149.53 | 1,180.10 | 711.48 | 0.45 | 316.87 | 316.87 | 317.00 |
| | | 500 mm | 942.00 | 1,130.00 | 258.50 | 2,039.45 | 1,229.67 | 0.52 | 365.40 | 365.40 | 366.00 |
| | | 600 mm | 1,077.00 | 1,292.00 | | | | 0.66 | 463.87 | 463.87 | 464.00 |
| | | 700 mm | 1,234.00 | 1,481.00 | | | | 0.80 | 562.33 | 562.33 | 563.00 |
| | | 800 mm | 1,395.00 | 1,674.00 | 385.00 | 3,037.48 | 1,831.42 | 0.96 | 672.00 | 672.00 | 672.00 |
| | | 900 mm | 1,578.00 | 1,894.00 | | | | 1.09 | 765.10 | 765.10 | 766.00 |
| PVC | | | (only Pipe Laying) | | (with 1 to 2m excavation, backfilling etc.) | | | | | | |
| | | 63 mm | 11.76 | 14.00 | 29.04 | 229.11 | 138.14 | 0.04 | 30.10 | 30.10 | 31.00 |
| | | 75 mm | 11.76 | 14.00 | 29.04 | 229.11 | 138.14 | 0.04 | 30.10 | 30.10 | 31.00 |
| | | 90 mm | 13.94 | 17.00 | 29.04 | 229.11 | 138.14 | 0.06 | 39.90 | 39.90 | 40.00 |
| | | 110 mm | 15.00 | 18.00 | 34.98 | 275.98 | 166.40 | 0.06 | 39.90 | 39.90 | 40.00 |
| | | 160 mm | 15.00 | 18.00 | 38.94 | 307.22 | 185.24 | 0.07 | 51.80 | 51.80 | 52.00 |
| | | 225 mm | 18.15 | 22.00 | 40.04 | 315.90 | 190.47 | 0.10 | 72.80 | 72.80 | 73.00 |
| | | 280 mm | 18.74 | 22.00 | | | | 0.14 | 98.00 | 98.00 | 98.00 |
| | | 315 mm | | | | | | 0.17 | 119.00 | 119.00 | 119.00 |
| Hume Pipe/Clay Pipe | | | (with excavation, backfilling) | | (depth is unknown) | | | | | | |
| | | 150 mm | 134.00 | 161.00 | | | | 0.32 | 224.00 | 112.00 | 112.00 |
| | | 225 mm | 164.00 | 197.00 | | | | 0.40 | 277.20 | 138.60 | 139.00 |
| | | 250 mm | | | | | | 0.46 | 319.20 | 159.60 | 160.00 |
| | | 300 mm | 227.00 | 272.00 | | | | 0.53 | 369.60 | 184.80 | 185.00 |
| | | 375 mm | 270.00 | 324.00 | | | | 0.60 | 420.00 | 210.00 | 210.00 |
| | | 400 mm | | | | | | 0.61 | 428.40 | 214.20 | 215.00 |
| | | 450 mm | 330.00 | 396.00 | 2,033.77 | 2,883.18 | 3,406.71 | 0.84 | 588.00 | 294.00 | 294.00 |
| | | 500 mm | | | | | | 0.86 | 604.80 | 302.40 | 303.00 |
| | | 544 mm | | | 2,033.77 | 2,883.18 | 3,406.71 | 0.96 | 672.00 | 336.00 | 336.00 |
| | | 600 mm | 410.00 | 492.00 | | | | 1.06 | 744.80 | 372.40 | 373.00 |
| | | 675 mm | | | | | | 1.12 | 784.00 | 392.00 | 392.00 |
| | | 750 mm | 500.00 | 600.00 | | | | 1.15 | 803.60 | 401.80 | 402.00 |
| | | 825 mm | | | | | | 1.20 | 840.00 | 420.00 | 420.00 |
| | | 900 mm | 650.00 | 780.00 | | | | 1.23 | 862.40 | 431.20 | 432.00 |
| | | 1050 mm | 680.00 | 816.00 | | | | 1.34 | 940.80 | 470.40 | 471.00 |
| 2. Excavation | | | | | | | | | | | |
| | Backhoe | | | | | | | | | | 790.00 |
| | (incl. Backfilling) | | | | | | | | | | |
| 3. Soil Disposal | | | | | | | | | | | |
| | Off site | m ³ | | | | | | | | | 310.00 |
| 4. Backfilling with sand | | | | | | | | | | | |
| | with sand supply | m ³ | | | | | | | | | 1,000.00 |
| 5. Pavement | | | | | | | | | | | |
| | Reinstatement | m ² | | | | | | | | | 2,000.00 |

Chapter 13

**Appendix 13.1 Sewer Network Hydraulic Analysis
(F/S)**

Appendix 13.2 Trunk Sewer Profile

**Appendix 13.3 Pumping Equipment
- Capacity Calculation**

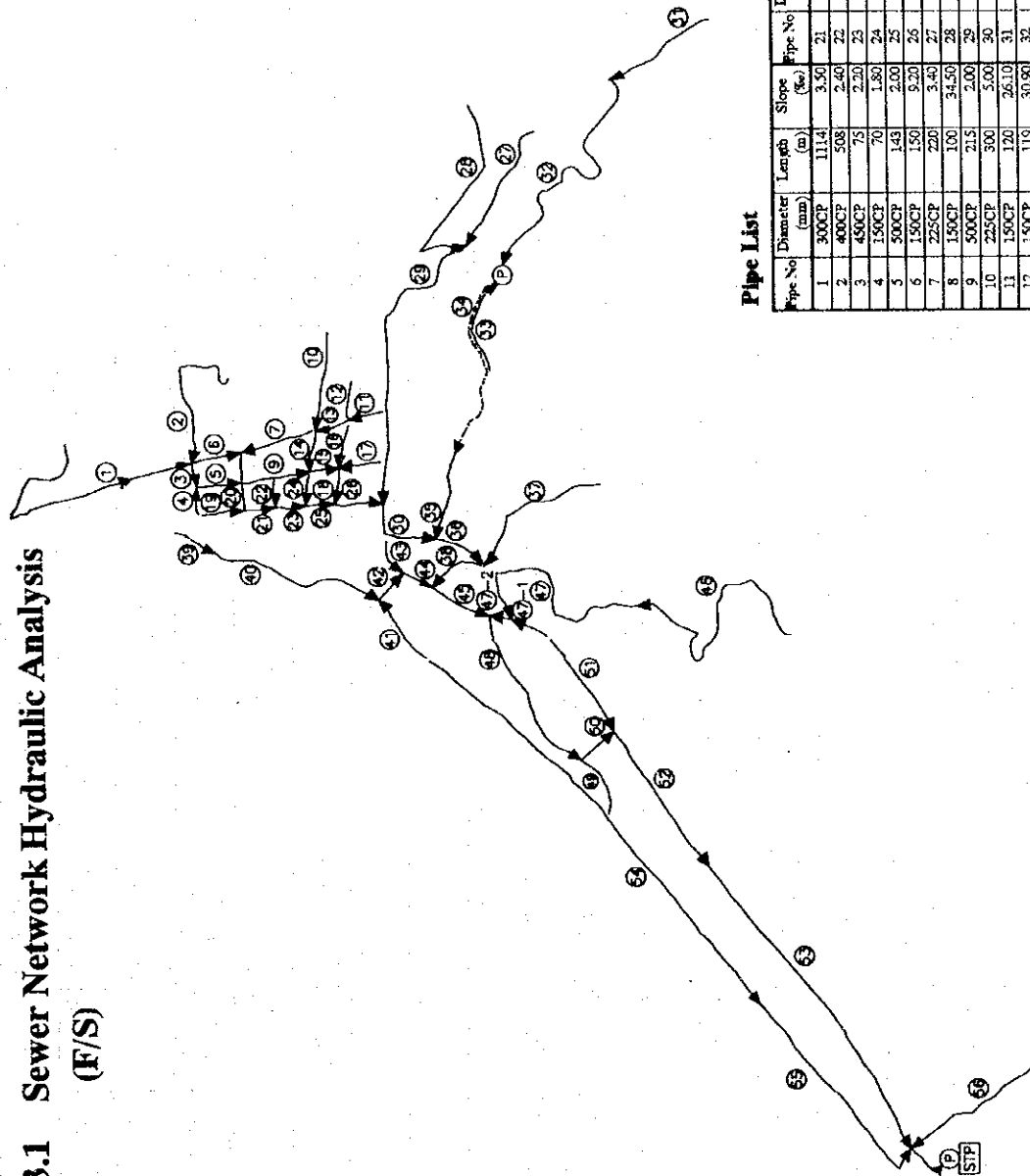
**Appendix 13.4 Sewage Treatment Plant
- Capacity Calculation**

Appendix 13.5 Hydraulic Calculation

Appendix 13.6 Drawings

Appendix 13.7 Storage Capacity of Sewer (Kandy)

Appendix 13.1 Sewer Network Hydraulic Analysis (F/S)



Pipe List

| Pipe No | Diameter (mm) | Length (m) | Slope (%) | Pipe No | Diameter (mm) | Length (m) | Slope (%) | Pipe No | Diameter (mm) | Length (m) | Slope (%) |
|---------|---------------|------------|-----------|---------|---------------|------------|-----------|---------|---------------|------------|-----------|
| 1 | 300CP | 111.4 | 3.50 | 21 | 225CP | 100 | 1.50 | 41 | 150CP | 250 | 21.20 |
| 2 | 400CP | 508 | 2.40 | 22 | 150CP | 90 | 15.80 | 42 | 300CP | 100 | 3.50 |
| 3 | 450CP | 75 | 2.20 | 23 | 225CP | 95 | 5.00 | 43 | 150CP | 250 | 13.50 |
| 4 | 150CP | 70 | 1.80 | 24 | 150CP | 100 | 11.20 | 44 | 300CP | 80 | 3.50 |
| 5 | 300CP | 143 | 2.00 | 25 | 225CP | 92 | 5.00 | 45 | 675CP | 200 | 1.40 |
| 6 | 150CP | 150 | 9.20 | 26 | 600CP | 152 | 1.60 | 46 | 225CP | 1022 | 5.00 |
| 7 | 225CP | 220 | 3.40 | 27 | 150CP | 500 | 1.50 | 47 | 300CP | 808 | 3.50 |
| 8 | 150CP | 100 | 34.50 | 28 | 150CP | 550 | 39.90 | 47-1 | 150CP | 130 | 41.80 |
| 9 | 500CP | 215 | 2.00 | 29 | 225CP | 1000 | 5.00 | 47-2 | 300CP | 70 | 3.50 |
| 10 | 225CP | 300 | 5.00 | 30 | 675CP | 270 | 1.40 | 48 | 675CP | 450 | 1.40 |
| 11 | 150CP | 120 | 26.10 | 31 | 150CP | 350 | 31.00 | 49 | 150CP | 254 | 28.50 |
| 12 | 150CP | 119 | 30.90 | 32 | 150CP | 900 | 3.40 | 50 | 750CP | 150 | 1.20 |
| 13 | 225CP | 100 | 1.50 | 33 | 225CP | 500 | 1.50 | 51 | 150CP | 350 | 25.60 |
| 14 | 300CP | 130 | 3.50 | 34 | 100CP | 650 | 0.01 | 52 | 825CP | 500 | 1.20 |
| 15 | 600CP | 95 | 1.60 | 35 | 150CP | 269 | 50.00 | 53 | 825CP | 1100 | 1.20 |
| 16 | 150CP | 143 | 44.70 | 36 | 675CP | 100 | 1.40 | 54 | 400CP | 1500 | 2.40 |
| 17 | 150CP | 140 | 40.60 | 37 | 150CP | 580 | 7.30 | 55 | 400CP | 650 | 2.40 |
| 18 | 600CP | 120 | 1.60 | 38 | 675CP | 70 | 1.40 | 56 | 225CP | 450 | 5.00 |
| 19 | 150CP | 126 | 31.90 | 39 | 225CP | 198 | 5.00 | 57 | 825CP | 50 | 1.20 |
| 20 | 150CP | 93 | 1.50 | 40 | 300CP | 550 | 3.50 | | | | |

Note : 54,55,56 Excluded from F/S Area.

Sewage Flow Calculation Table (Kandy)

P 1

※Unit Sewage Flow : 0.324m³/capita·day

| Pipe No. | Down stream | Service Area | | Length | | T min | Storm Run-off | | | | | Sewage Flow | | | Other Flow | | Design Sewer | | | | | Remarks | | | | | |
|----------|-------------|--------------|--------|--------|------|----------|-----------------------|--------------|----|------|-------|-------------|------|--------|------------|--------|--------------|-------|------|------|-------|---------|-------|--------|-----|----|----|
| | | Sec. | Accum. | ha | C | | Rainfall per ha | Service Area | | R.O. | Pop/D | Flow | Sec. | Accum. | Accum. | Dia. | Slope | V | Flow | G.L. | Level | | D | | | | |
| | | | | | | | | ha | ha | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | ha | ha | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | ha | ha |
| 1 | 3 | 499 | 499 | 1114 | 1114 | | | | | | | | 3742 | 3742 | 00140 | 001143 | 001143 | 00254 | 300 | 350 | 0809 | 00572 | 53550 | 533014 | 185 | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2 | | 123 | 123 | 508 | 508 | | | | | | | | 307 | 307 | 00012 | 003796 | 003796 | 00392 | 400 | 240 | 0812 | 01020 | 50814 | 506694 | 100 | | |
| 3 | 5 | | 522 | 75 | 1189 | | | | | | | | | 4049 | 00152 | 000086 | 005025 | 00655 | 450 | 220 | 0841 | 01337 | 50814 | 505890 | 175 | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4 | | | | 70 | 70 | | | | | | | | | | | 000086 | 000086 | 00009 | 150 | 180 | 0366 | 00065 | 50726 | 506389 | 100 | | |
| 5 | 9 | | 522 | 143 | 1332 | | | | | | | | | 4049 | 00152 | 000129 | 005240 | 00676 | 500 | 200 | 0860 | 01689 | 50726 | 502980 | 372 | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 7 | 8 | | | 220 | 220 | | | | | | | | | | | 000453 | 000453 | 00045 | 225 | 340 | 0658 | 00262 | 50675 | 505502 | 100 | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | | | | 150 | 150 | | | | | | | | | | | 000151 | 000151 | 00015 | 150 | 920 | 0827 | 00146 | 50814 | 506631 | 134 | | |
| 8 | | | | 100 | 320 | | | | | | | | | | | 000173 | 000777 | 00078 | 225 | 3450 | 2098 | 00834 | 50875 | 509172 | 133 | | |
| 9 | 15 | | 522 | 215 | 1547 | | | | | | | | | 4049 | 00152 | 000151 | 006168 | 00769 | 500 | 200 | 0860 | 01689 | 50297 | 501414 | 100 | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 10 | 14 | 227 | 227 | 300 | 300 | | | | | | | | 385 | 385 | 00014 | 001035 | 001035 | 00118 | 225 | 500 | 0799 | 00318 | 51100 | 503085 | 167 | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Sewage Flow Calculation Table (Kandy)

P 2

※Unit Sewage Flow : 0.324m³/capita·day

| Pipe No. | Down stream | Service Area | | Length | | T | Storm Run-off | | | | | Sewage Flow | | | Other Flow | | Accum. | Design Sewer | | | | Remarks | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | Sec. | Accum. | ha | m | | min | Rainfall per ha | C | Service Area | | R.O. | Pop/D | Population | | Flow | | Sec. | Accum. | Dia. | Slope % | | V m/s | Flow m3/s | G.L. | Level D | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Sewage Flow Calculation Table (Kandy)

P 3

※Unit Sewage Flow : 0.324m³/capita·day

| Pipe No. | Down stream | Service Area | | Length | | T | Storm Run-off | | | | | | Sewage Flow | | | | Other Flow | | Accum. | Design Sewer | | | | | Remarks | | | | | | | | | | | | |
|----------|-------------|--------------|--------|--------|------|-----|----------------------|-----------------|----|--------------|-------------------|------|-------------|------------|--------|-------------------|-------------------|-------------------|--------|--------------|-------|-------|--------|--------|---------|-------|---|---|---|-------------------|-------------------|----|---|-----|---|---|---|
| | | Sec. | Accum. | ha | m | | min | Rainfall per ha | C | Service Area | | R.O. | Pop/D | Population | | Flow | Sec. | Accum. | | Dia. | Slope | V | Flow | G.L. | | Level | D | | | | | | | | | | |
| | | | | | | | | | | ha | ha | | | P/ha | P | | | | | | | | | | | | | P | P | m ³ /s | m ³ /s | mm | % | m/s | M | M | m |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | ha | ha | m | m | min | m ³ /s-ha | | ha | ha | m ³ /s | P/ha | P | P | P | m ³ /s | m ³ /s | m ³ /s | mm | % | m/s | M | M | m | | | | | | | | | | | | | |
| 22 | | | | 90 | 90 | | | | | | | | | | | 000108 | 000108 | 00011 | 150 | 1580 | 1083 | 00191 | 50320 | 502021 | 101 | | | | | | | | | | | | |
| 23 | 25 | | | 95 | 321 | | | | | | | | | | | 000302 | 000305 | 00091 | 225 | 500 | 0799 | 00318 | 50072 | 498870 | 285 | | | | | | | | | | | | |
| 24 | | | | 100 | 100 | | | | | | | | | | | 000086 | 000086 | 00009 | 150 | 1120 | 0912 | 00161 | 50072 | 499423 | 113 | | | | | | | | | | | | |
| 25 | | | | 92 | 413 | | | | | | | | | | | 000324 | 001315 | 00132 | 225 | 500 | 0799 | 00318 | 50004 | 497735 | 206 | | | | | | | | | | | | |
| 26 | 30 | | 849 | 152 | 1914 | | | | | | | | 4434 | 00166 | 000302 | 009963 | 01162 | 600 | 150 | 0869 | 02456 | 50304 | 497360 | 201 | | | | | | | | | | | | | |
| 28 | 29 | 590 | 590 | 550 | 550 | | | | | | | 1173 | 1173 | 00044 | | | | 00044 | 150 | 3990 | 1721 | 00304 | 51248 | 511309 | 100 | | | | | | | | | | | | |
| 27 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 29 | | 101 | 101 | 500 | 500 | | | | | | | | 244 | 244 | 00009 | | | 00009 | 150 | 150 | 0334 | 00059 | 51248 | 510484 | 183 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 30 | 36 | 131 | 882 | 1000 | 1550 | | | | | | | | 365 | 1782 | 00067 | 000388 | 000388 | 00106 | 225 | 500 | 0799 | 00318 | 50185 | 500602 | 100 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 37 | 1748 | 270 | 2184 | | | | | | | | 43 | 6259 | 00235 | 000086 | 010437 | 01279 | 675 | 140 | 0879 | 03145 | 49979 | 498463 | 259 | | | | | | | | | | | | |
| 31 | | 113 | 113 | 350 | 350 | | | | | | | | 68 | 68 | 00003 | | | 00003 | 150 | 3100 | 1517 | 00268 | 51800 | 514829 | 100 | | | | | | | | | | | | |
| 32 | 34 | 352 | 445 | 900 | 1250 | | | | | | | | 760 | 828 | 00031 | | | 00031 | 150 | 340 | 0503 | 00089 | 51287 | 509161 | 354 | | | | | | | | | | | | |

Sewage Flow Calculation Table (Kandy)

P 4

*Unit Sewage Flow : 0.324m³/capita-day

| Pipe No. | Down stream | Service Area | | Length | | T | Storm Run-off | | | | Sewage Flow | | | | Other Flow | | Accum. | Design Sewer | | | | Remarks | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | Sec. | Accum. | ha | m | | m | m | C | Rainfall per ha | Service Area | | R.O. | Pop/D | Population | | | Flow | Sec. | Accum. | Accum. | | Dia. | Slope | V | Flow | G.L. | Level | D | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | ha | m | | | ha | m | | | | | | | | | | | | | | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P | P |

Sewage Flow Calculation Table (Kandy)

P 5

※Unit Sewage Flow : 0.324m³/capita·day

| Pipe No. | Down stream | Service Area | | Length | | T min | Storm Run-off | | | | Sewage Flow | | | Other Flow | | Design Sewer | | | | | | Remarks | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | Sec. | Accum. | C | Service Area | | R.O. | Pop/d | Population | | Flow | Sec. | Accum. | Accum. | Dia. | Slope % | V m/s | Flow m3/s | G.L. | Level | D m | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| 44 | | ha | ha | m | m | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

6

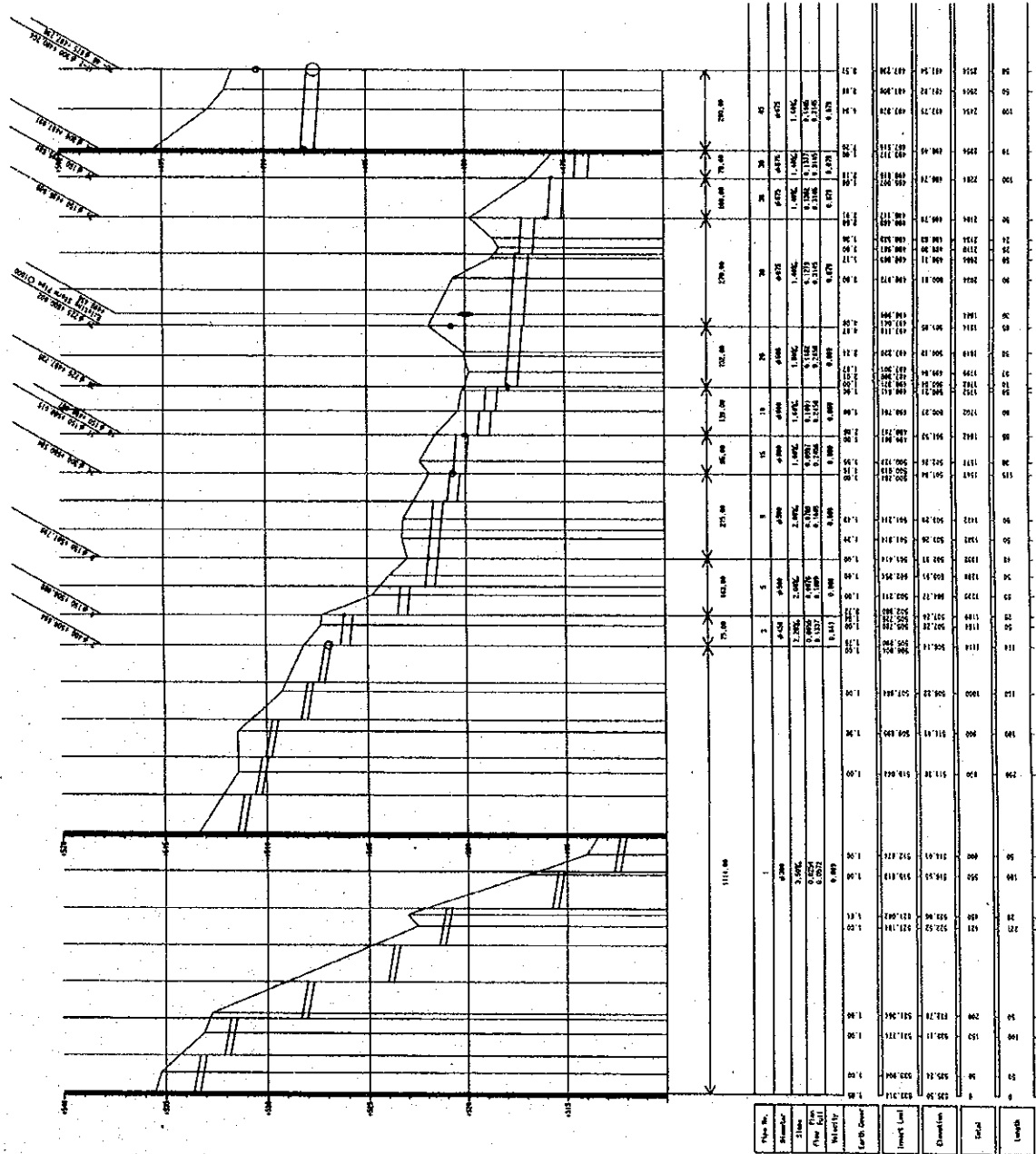
0.4

6

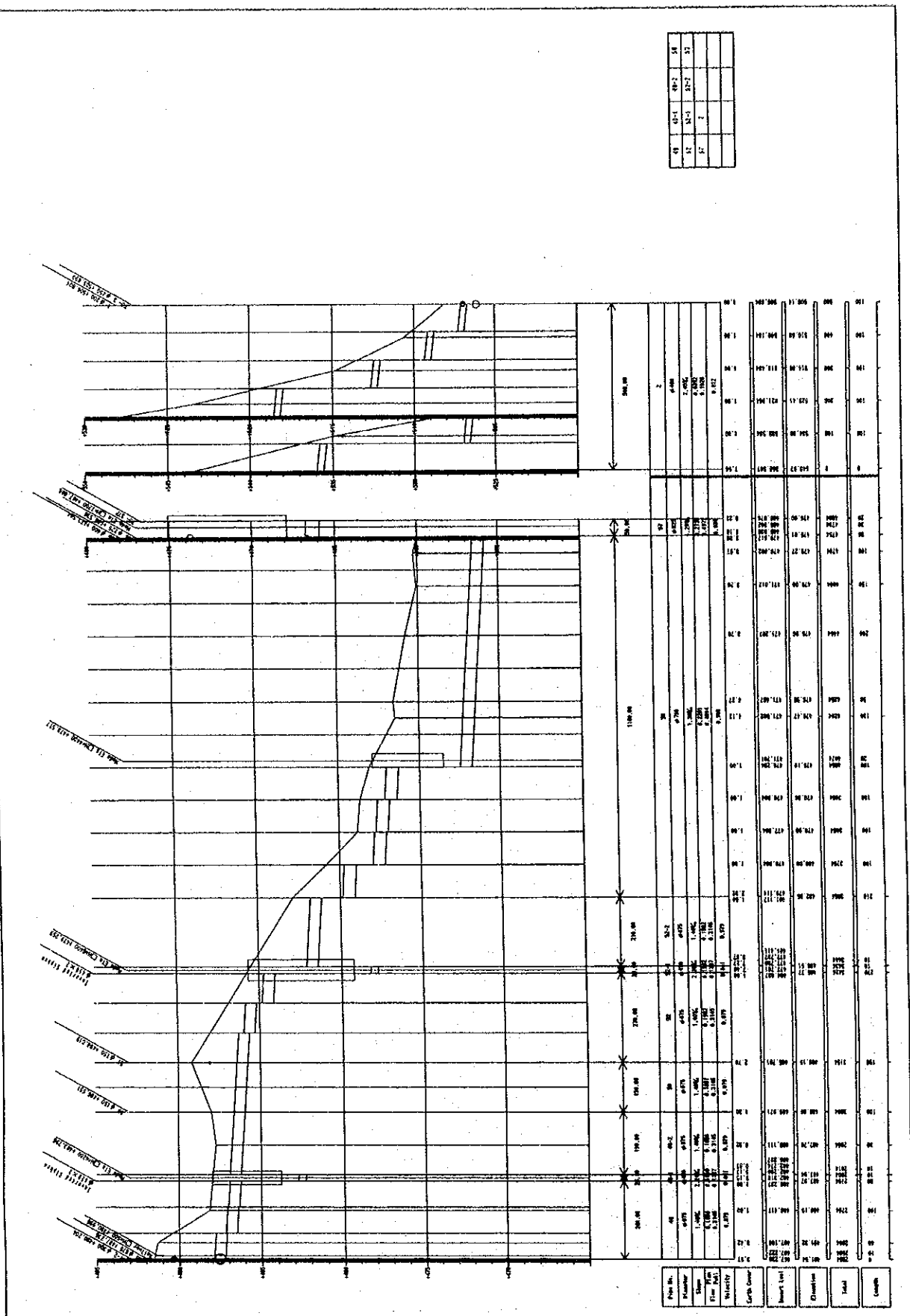
0.4

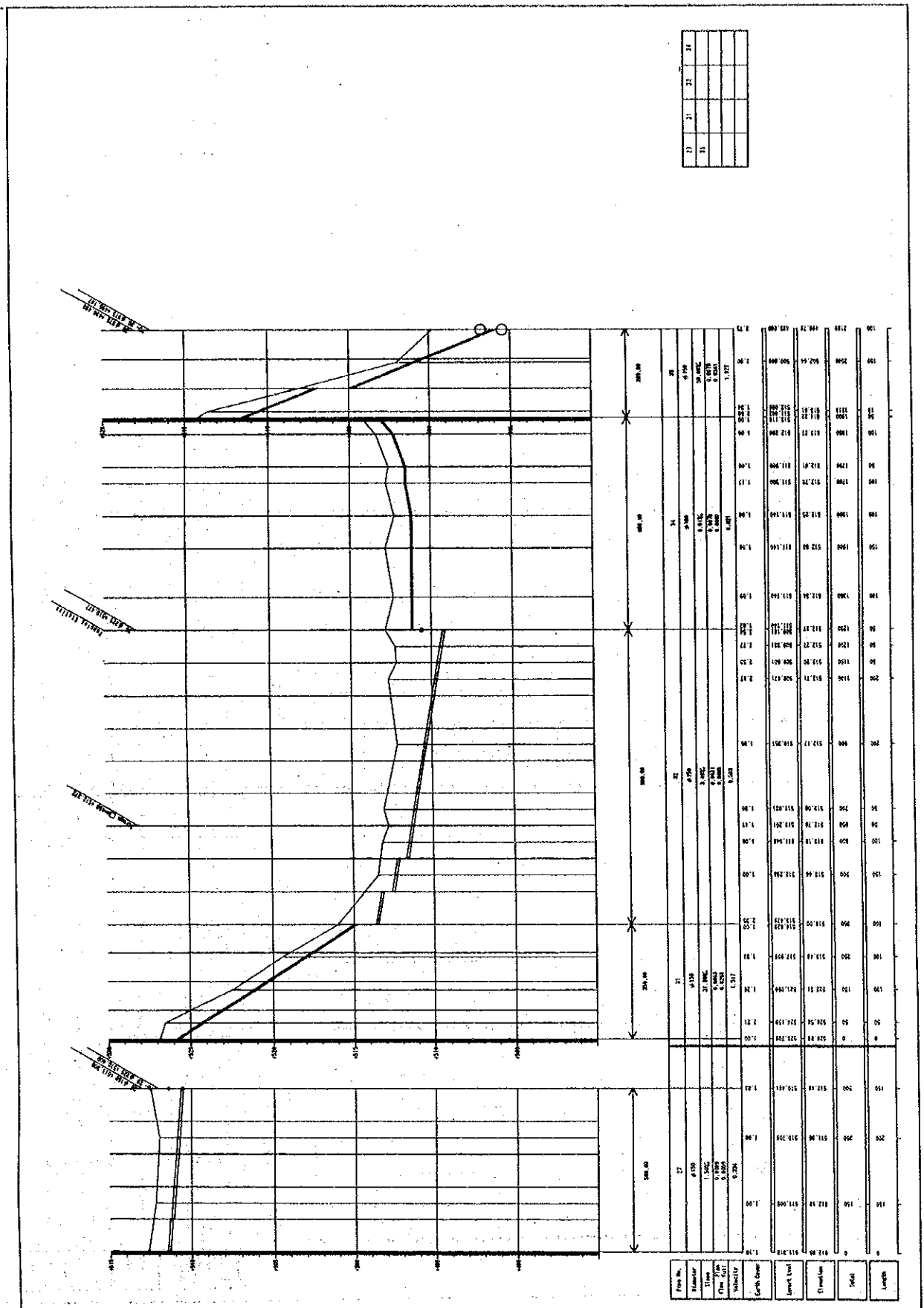
A-13.1-7

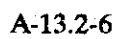
Appendix 13.2 Trunk Sewer Profile

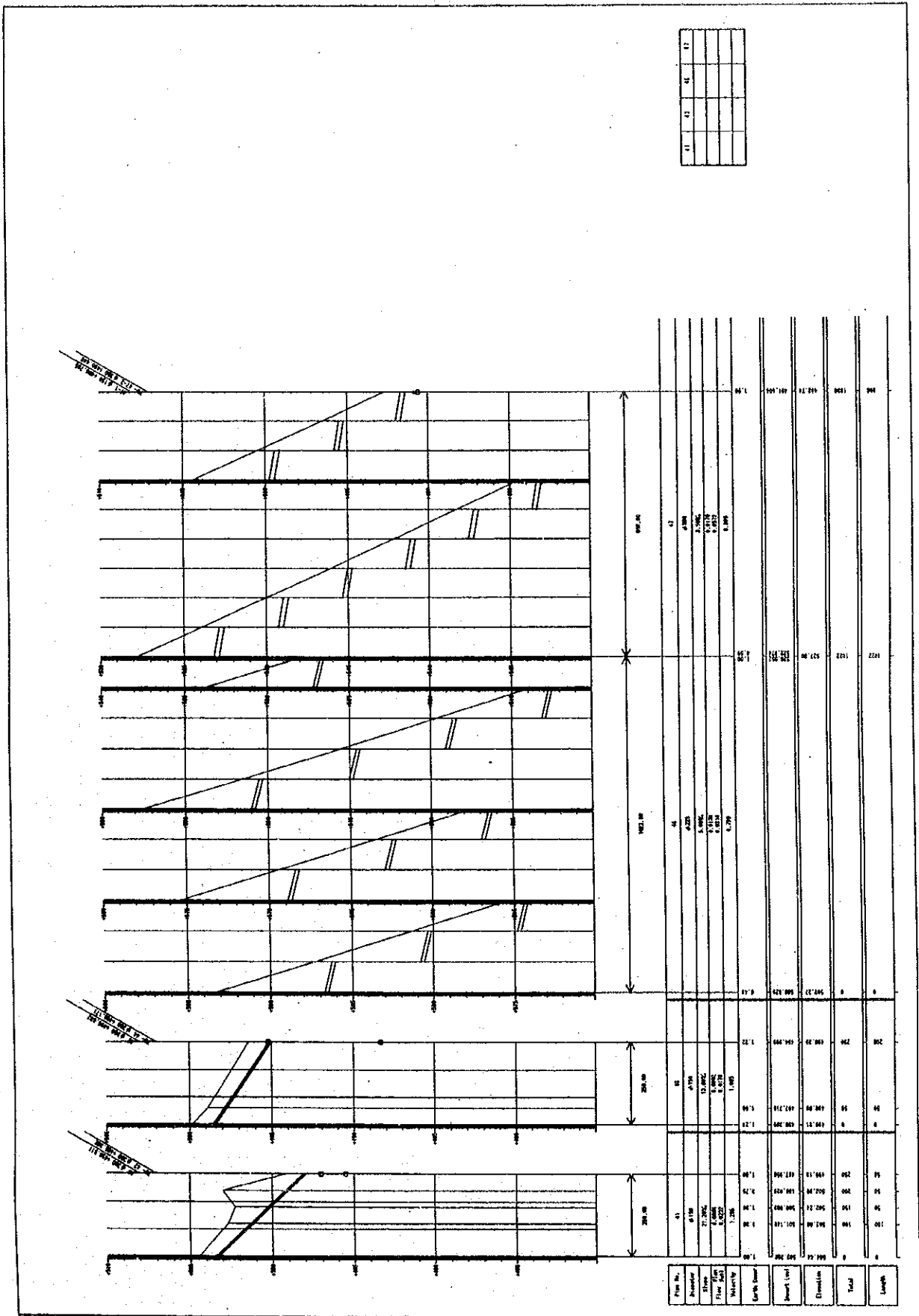


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|------|------|------|------|------|
| 1 | 2 | 3 | 4 | 5 |
| 15 | 16 | 17 | 18 | 19 |
| 20 | 21 | 22 | 23 | 24 |
| 25 | 26 | 27 | 28 | 29 |
| 30 | 31 | 32 | 33 | 34 |
| 35 | 36 | 37 | 38 | 39 |
| 40 | 41 | 42 | 43 | 44 |
| 45 | 46 | 47 | 48 | 49 |
| 50 | 51 | 52 | 53 | 54 |
| 55 | 56 | 57 | 58 | 59 |
| 60 | 61 | 62 | 63 | 64 |
| 65 | 66 | 67 | 68 | 69 |
| 70 | 71 | 72 | 73 | 74 |
| 75 | 76 | 77 | 78 | 79 |
| 80 | 81 | 82 | 83 | 84 |
| 85 | 86 | 87 | 88 | 89 |
| 90 | 91 | 92 | 93 | 94 |
| 95 | 96 | 97 | 98 | 99 |
| 100 | 101 | 102 | 103 | 104 |
| 105 | 106 | 107 | 108 | 109 |
| 110 | 111 | 112 | 113 | 114 |
| 115 | 116 | 117 | 118 | 119 |
| 120 | 121 | 122 | 123 | 124 |
| 125 | 126 | 127 | 128 | 129 |
| 130 | 131 | 132 | 133 | 134 |
| 135 | 136 | 137 | 138 | 139 |
| 140 | 141 | 142 | 143 | 144 |
| 145 | 146 | 147 | 148 | 149 |
| 150 | 151 | 152 | 153 | 154 |
| 155 | 156 | 157 | 158 | 159 |
| 160 | 161 | 162 | 163 | 164 |
| 165 | 166 | 167 | 168 | 169 |
| 170 | 171 | 172 | 173 | 174 |
| 175 | 176 | 177 | 178 | 179 |
| 180 | 181 | 182 | 183 | 184 |
| 185 | 186 | 187 | 188 | 189 |
| 190 | 191 | 192 | 193 | 194 |
| 195 | 196 | 197 | 198 | 199 |
| 200 | 201 | 202 | 203 | 204 |
| 205 | 206 | 207 | 208 | 209 |
| 210 | 211 | 212 | 213 | 214 |
| 215 | 216 | 217 | 218 | 219 |
| 220 | 221 | 222 | 223 | 224 |
| 225 | 226 | 227 | 228 | 229 |
| 230 | 231 | 232 | 233 | 234 |
| 235 | 236 | 237 | 238 | 239 |
| 240 | 241 | 242 | 243 | 244 |
| 245 | 246 | 247 | 248 | 249 |
| 250 | 251 | 252 | 253 | 254 |
| 255 | 256 | 257 | 258 | 259 |
| 260 | 261 | 262 | 263 | 264 |
| 265 | 266 | 267 | 268 | 269 |
| 270 | 271 | 272 | 273 | 274 |
| 275 | 276 | 277 | 278 | 279 |
| 280 | 281 | 282 | 283 | 284 |
| 285 | 286 | 287 | 288 | 289 |
| 290 | 291 | 292 | 293 | 294 |
| 295 | 296 | 297 | 298 | 299 |
| 300 | 301 | 302 | 303 | 304 |
| 305 | 306 | 307 | 308 | 309 |
| 310 | 311 | 312 | 313 | 314 |
| 315 | 316 | 317 | 318 | 319 |
| 320 | 321 | 322 | 323 | 324 |
| 325 | 326 | 327 | 328 | 329 |
| 330 | 331 | 332 | 333 | 334 |
| 335 | 336 | 337 | 338 | 339 |
| 340 | 341 | 342 | 343 | 344 |
| 345 | 346 | 347 | 348 | 349 |
| 350 | 351 | 352 | 353 | 354 |
| 355 | 356 | 357 | 358 | 359 |
| 360 | 361 | 362 | 363 | 364 |
| 365 | 366 | 367 | 368 | 369 |
| 370 | 371 | 372 | 373 | 374 |
| 375 | 376 | 377 | 378 | 379 |
| 380 | 381 | 382 | 383 | 384 |
| 385 | 386 | 387 | 388 | 389 |
| 390 | 391 | 392 | 393 | 394 |
| 395 | 396 | 397 | 398 | 399 |
| 400 | 401 | 402 | 403 | 404 |
| 405 | 406 | 407 | 408 | 409 |
| 410 | 411 | 412 | 413 | 414 |
| 415 | 416 | 417 | 418 | 419 |
| 420 | 421 | 422 | 423 | 424 |
| 425 | 426 | 427 | 428 | 429 |
| 430 | 431 | 432 | 433 | 434 |
| 435 | 436 | 437 | 438 | 439 |
| 440 | 441 | 442 | 443 | 444 |
| 445 | 446 | 447 | 448 | 449 |
| 450 | 451 | 452 | 453 | 454 |
| 455 | 456 | 457 | 458 | 459 |
| 460 | 461 | 462 | 463 | 464 |
| 465 | 466 | 467 | 468 | 469 |
| 470 | 471 | 472 | 473 | 474 |
| 475 | 476 | 477 | 478 | 479 |
| 480 | 481 | 482 | 483 | 484 |
| 485 | 486 | 487 | 488 | 489 |
| 490 | 491 | 492 | 493 | 494 |
| 495 | 496 | 497 | 498 | 499 |
| 500 | 501 | 502 | 503 | 504 |
| 505 | 506 | 507 | 508 | 509 |
| 510 | 511 | 512 | 513 | 514 |
| 515 | 516 | 517 | 518 | 519 |
| 520 | 521 | 522 | 523 | 524 |
| 525 | 526 | 527 | 528 | 529 |
| 530 | 531 | 532 | 533 | 534 |
| 535 | 536 | 537 | 538 | 539 |
| 540 | 541 | 542 | 543 | 544 |
| 545 | 546 | 547 | 548 | 549 |
| 550 | 551 | 552 | 553 | 554 |
| 555 | 556 | 557 | 558 | 559 |
| 560 | 561 | 562 | 563 | 564 |
| 565 | 566 | 567 | 568 | 569 |
| 570 | 571 | 572 | 573 | 574 |
| 575 | 576 | 577 | 578 | 579 |
| 580 | 581 | 582 | 583 | 584 |
| 585 | 586 | 587 | 588 | 589 |
| 590 | 591 | 592 | 593 | 594 |
| 595 | 596 | 597 | 598 | 599 |
| 600 | 601 | 602 | 603 | 604 |
| 605 | 606 | 607 | 608 | 609 |
| 610 | 611 | 612 | 613 | 614 |
| 615 | 616 | 617 | 618 | 619 |
| 620 | 621 | 622 | 623 | 624 |
| 625 | 626 | 627 | 628 | 629 |
| 630 | 631 | 632 | 633 | 634 |
| 635 | 636 | 637 | 638 | 639 |
| 640 | 641 | 642 | 643 | 644 |
| 645 | 646 | 647 | 648 | 649 |
| 650 | 651 | 652 | 653 | 654 |
| 655 | 656 | 657 | 658 | 659 |
| 660 | 661 | 662 | 663 | 664 |
| 665 | 666 | 667 | 668 | 669 |
| 670 | 671 | 672 | 673 | 674 |
| 675 | 676 | 677 | 678 | 679 |
| 680 | 681 | 682 | 683 | 684 |
| 685 | 686 | 687 | 688 | 689 |
| 690 | 691 | 692 | 693 | 694 |
| 695 | 696 | 697 | 698 | 699 |
| 700 | 701 | 702 | 703 | 704 |
| 705 | 706 | 707 | 708 | 709 |
| 710 | 711 | 712 | 713 | 714 |
| 715 | 716 | 717 | 718 | 719 |
| 720 | 721 | 722 | 723 | 724 |
| 725 | 726 | 727 | 728 | 729 |
| 730 | 731 | 732 | 733 | 734 |
| 735 | 736 | 737 | 738 | 739 |
| 740 | 741 | 742 | 743 | 744 |
| 745 | 746 | 747 | 748 | 749 |
| 750 | 751 | 752 | 753 | 754 |
| 755 | 756 | 757 | 758 | 759 |
| 760 | 761 | 762 | 763 | 764 |
| 765 | 766 | 767 | 768 | 769 |
| 770 | 771 | 772 | 773 | 774 |
| 775 | 776 | 777 | 778 | 779 |
| 780 | 781 | 782 | 783 | 784 |
| 785 | 786 | 787 | 788 | 789 |
| 790 | 791 | 792 | 793 | 794 |
| 795 | 796 | 797 | 798 | 799 |
| 800 | 801 | 802 | 803 | 804 |
| 805 | 806 | 807 | 808 | 809 |
| 810 | 811 | 812 | 813 | 814 |
| 815 | 816 | 817 | 818 | 819 |
| 820 | 821 | 822 | 823 | 824 |
| 825 | 826 | 827 | 828 | 829 |
| 830 | 831 | 832 | 833 | 834 |
| 835 | 836 | 837 | 838 | 839 |
| 840 | 841 | 842 | 843 | 844 |
| 845 | 846 | 847 | 848 | 849 |
| 850 | 851 | 852 | 853 | 854 |
| 855 | 856 | 857 | 858 | 859 |
| 860 | 861 | 862 | 863 | 864 |
| 865 | 866 | 867 | 868 | 869 |
| 870 | 871 | 872 | 873 | 874 |
| 875 | 876 | 877 | 878 | 879 |
| 880 | 881 | 882 | 883 | 884 |
| 885 | 886 | 887 | 888 | 889 |
| 890 | 891 | 892 | 893 | 894 |
| 895 | 896 | 897 | 898 | 899 |
| 900 | 901 | 902 | 903 | 904 |
| 905 | 906 | 907 | 908 | 909 |
| 910 | 911 | 912 | 913 | 914 |
| 915 | 916 | 917 | 918 | 919 |
| 920 | 921 | 922 | 923 | 924 |
| 925 | 926 | 927 | 928 | 929 |
| 930 | 931 | 932 | 933 | 934 |
| 935 | 936 | 937 | 938 | 939 |
| 940 | 941 | 942 | 943 | 944 |
| 945 | 946 | 947 | 948 | 949 |
| 950 | 951 | 952 | 953 | 954 |
| 955 | 956 | 957 | 958 | 959 |
| 960 | 961 | 962 | 963 | 964 |
| 965 | 966 | 967 | 968 | 969 |
| 970 | 971 | 972 | 973 | 974 |
| 975 | 976 | 977 | 978 | 979 |
| 980 | 981 | 982 | 983 | 984 |
| 985 | 986 | 987 | 988 | 989 |
| 990 | 991 | 992 | 993 | 994 |
| 995 | 996 | 997 | 998 | 999 |
| 1000 | 1001 | 1002 | 1003 | 1004 |
| 1005 | 1006 | 1007 | 1008 | 1009 |
| 1010 | 1011 | 1012 | 1013 | 1014 |
| 1015 | 1016 | 1017 | 1018 | 1019 |
| 1020 | 1021 | 1022 | 1023 | 1024 |
| 1025 | 1026 | 1027 | 1028 | 1029 |
| 1030 | 1031 | 1032 | 1033 | 1034 |
| 1035 | 1036 | 1037 | 1038 | 1039 |
| 1040 | 1041 | 1042 | 1043 | 1044 |
| 1045 | 1046 | 1047 | 1048 | 1049 |
| 1050 | 1051 | 1052 | 1053 | 1054 |
| 1055 | 1056 | 1057 | 1058 | 1059 |
| 1060 | 1061 | 1062 | 1063 | 1064 |
| 1065 | 1066 | 1067 | 1068 | 1069 |
| 1070 | 1071 | 1072 | 1073 | 1074 |
| 1075 | 1076 | 1077 | 1078 | 1079 |
| 1080 | 1081 | 1082 | 1083 | 1084 |
| 1085 | 1086 | 1087 | 1088 | 1089 |
| 1090 | 1091 | 1092 | 1093 | 1094 |
| 1095 | 1096 | 1097 | 1098 | 1099 |
| 1100 | 1101 | 1102 | 1103 | 1104 |
| 1105 | 1106 | 1107 | 1108 | 1109 |
| 1110 | 1111 | 1112 | 1113 | 1114 |
| 1115 | 1116 | 1117 | 1118 | 1119 |
| 1120 | 1121 | 1122 | 1123 | 1124 |
| 1125 | 1126 | 1127 | 1128 | 1129 |
| 1130 | 1131 | 1132 | 1133 | 1134 |
| 1135 | 1136 | 1137 | 1138 | 1139 |
| 1140 | 1141 | 1142 | 1143 | 1144 |
| 1145 | 1146 | 1147 | 1148 | 1149 |
| 1150 | 1151 | 1152 | 1153 | 1154 |
| 1155 | 1156 | 1157 | 1158 | 1159 |
| 1160 | 1161 | 1162 | 1163 | 1164 |
| 1165 | 1166 | 1167 | 1168 | 1169 |
| 1170 | 1171 | 1172 | 1173 | 1174 |
| 1175 | 1176 | 1177 | 1178 | 1179 |
| 1180 | 1181 | 1182 | 1183 | 1184 |
| 1185 | 1186 | 1187 | 1188 | 1189 |
| 1190 | 1191 | 1192 | 1193 | 1194 |
| 1195 | 1196 | 1197 | 1198 | 1199 |
| 1200 | 1201 | 1202 | 1203 | 1204 |
| 1205 | 1206 | 1207 | 1208 | 1209 |
| 1210 | 1211 | 1212 | 1213 | 1214 |
| 1215 | 1216 | 1217 | 1218 | 1219 |
| 1220 | 1221 | 1222 | 1223 | 1224 |
| 1225 | 1226 | 1227 | 1228 | 1229 |
| 1230 | 1231 | 1232 | 1233 | 1234 |
| 1235 | 1236 | 1237 | 1238 | 1239 |
| 1240 | 1241 | 1242 | 1243 | 1244 |
| 1245 | 1246 | 1247 | 1248 | 1249 |
| 1250 | 1251 | 1252 | 1253 | 1254 |
| 1255 | 1256 | 1257 | 1258 | 1259 |
| 1260 | 1261 | 1262 | 1263 | 1264 |
| 1265 | 1266 | 1267 | 1268 | 1269 |
| 1270 | 1271 | 1272 | 1273 | 1274 |
| 1275 | 1276 | 1277 | 1278 | 1279 |
| 1280 | 1281 | 1282 | 1283 | 1284 |
| 1285 | 1286 | 1287 | 1288 | 1289 |
| 1290 | 1291 | 1292 | 1293 | 129 |









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|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|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| 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 | 101 | 102 | 103 | 104 | 105 | 106 | 107 | 108 | 109 | 110 | 111 | 112 | 113 | 114 | 115 | 116 | 117 | 118 | 119 | 120 | 121 | 122 | 123 | 124 | 125 | 126 | 127 | 128 | 129 | 130 | 131 | 132 | 133 | 134 | 135 | 136 | 137 | 138 | 139 | 140 | 141 | 142 | 143 | 144 | 145 | 146 | 147 | 148 | 149 | 150 | 151 | 152 | 153 | 154 | 155 | 156 | 157 | 158 | 159 | 160 | 161 | 162 | 163 | 164 | 165 | 166 | 167 | 168 | 169 | 170 | 171 | 172 | 173 | 174 | 175 | 176 | 177 | 178 | 179 | 180 | 181 | 182 | 183 | 184 | 185 | 186 | 187 | 188 | 189 | 190 | 191 | 192 | 193 | 194 | 195 | 196 | 197 | 198 | 199 | 200 | 201 | 202 | 203 | 204 | 205 | 206 | 207 | 208 | 209 | 210 | 211 | 212 | 213 | 214 | 215 | 216 | 217 | 218 | 219 | 220 | 221 | 222 | 223 | 224 | 225 | 226 | 227 | 228 | 229 | 230 | 231 | 232 | 233 | 234 | 235 | 236 | 237 | 238 | 239 | 240 | 241 | 242 | 243 | 244 | 245 | 246 | 247 | 248 | 249 | 250 | 251 | 252 | 253 | 254 | 255 | 256 | 257 | 258 | 259 | 260 | 261 | 262 | 263 | 264 | 265 | 266 | 267 | 268 | 269 | 270 | 271 | 272 | 273 | 274 | 275 | 276 | 277 | 278 | 279 | 280 | 281 | 282 | 283 | 284 | 285 | 286 | 287 | 288 | 289 | 290 | 291 | 292 | 293 | 294 | 295 | 296 | 297 | 298 | 299 | 300 | 301 | 302 | 303 | 304 | 305 | 306 | 307 | 308 | 309 | 310 | 311 | 312 | 313 | 314 | 315 | 316 | 317 | 318 | 319 | 320 | 321 | 322 | 323 | 324 | 325 | 326 | 327 | 328 | 329 | 330 | 331 | 332 | 333 | 334 | 335 | 336 | 337 | 338 | 339 | 340 | 341 | 342 | 343 | 344 | 345 | 346 | 347 | 348 | 349 | 350 | 351 | 352 | 353 | 354 | 355 | 356 | 357 | 358 | 359 | 360 | 361 | 362 | 363 | 364 | 365 | 366 | 367 | 368 | 369 | 370 | 371 | 372 | 373 | 374 | 375 | 376 | 377 | 378 | 379 | 380 | 381 | 382 | 383 | 384 | 385 | 386 | 387 | 388 | 389 | 390 | 391 | 392 | 393 | 394 | 395 | 396 | 397 | 398 | 399 | 400 | 401 | 402 | 403 | 404 | 405 | 406 | 407 | 408 | 409 | 410 | 411 | 412 | 413 | 414 | 415 | 416 | 417 | 418 | 419 | 420 | 421 | 422 | 423 | 424 | 425 | 426 | 427 | 428 | 429 | 430 | 431 | 432 | 433 | 434 | 435 | 436 | 437 | 438 | 439 | 440 | 441 | 442 | 443 | 444 | 445 | 446 | 447 | 448 | 449 | 450 | 451 | 452 | 453 | 454 | 455 | 456 | 457 | 458 | 459 | 460 | 461 | 462 | 463 | 464 | 465 | 466 | 467 | 468 | 469 | 470 | 471 | 472 | 473 | 474 | 475 | 476 | 477 | 478 | 479 | 480 | 481 | 482 | 483 | 484 | 485 | 486 | 487 | 488 | 489 | 490 | 491 | 492 | 493 | 494 | 495 | 496 | 497 | 498 | 499 | 500 | 501 | 502 | 503 | 504 | 505 | 506 | 507 | 508 | 509 | 510 | 511 | 512 | 513 | 514 | 515 | 516 | 517 | 518 | 519 | 520 | 521 | 522 | 523 | 524 | 525 | 526 | 527 | 528 | 529 | 530 | 531 | 532 | 533 | 534 | 535 | 536 | 537 | 538 | 539 | 540 | 541 | 542 | 543 | 544 | 545 | 546 | 547 | 548 | 549 | 550 | 551 | 552 | 553 | 554 | 555 | 556 | 557 | 558 | 559 | 560 | 561 | 562 | 563 | 564 | 565 | 566 | 567 | 568 | 569 | 570 | 571 | 572 | 573 | 574 | 575 | 576 | 577 | 578 | 579 | 580 | 581 | 582 | 583 | 584 | 585 | 586 | 587 | 588 | 589 | 590 | 591 | 592 | 593 | 594 | 595 | 596 | 597 | 598 | 599 | 600 | 601 | 602 | 603 | 604 | 605 | 606 | 607 | 608 | 609 | 610 | 611 | 612 | 613 | 614 | 615 | 616 | 617 | 618 | 619 | 620 | 621 | 622 | 623 | 624 | 625 | 626 | 627 | 628 | 629 | 630 | 631 | 632 | 633 | 634 | 635 | 636 | 637 | 638 | 639 | 640 | 641 | 642 | 643 | 644 | 645 | 646 | 647 | 648 | 649 | 650 | 651 | 652 | 653 | 654 | 655 | 656 | 657 | 658 | 659 | 660 | 661 | 662 | 663 | 664 | 665 | 666 | 667 | 668 | 669 | 670 | 671 | 672 | 673 | 674 | 675 | 676 | 677 | 678 | 679 | 680 | 681 | 682 | 683 | 684 | 685 | 686 | 687 | 688 | 689 | 690 | 691 | 692 | 693 | 694 | 695 | 696 | 697 | 698 | 699 | 700 | 701 | 702 | 703 | 704 | 705 | 706 | 707 | 708 | 709 | 710 | 711 | 712 | 713 | 714 | 715 | 716 | 717 | 718 | 719 | 720 | 721 | 722 | 723 | 724 | 725 | 726 | 727 | 728 | 729 | 730 | 731 | 732 | 733 | 734 | 735 | 736 | 737 | 738 | 739 | 740 | 741 | 742 | 743 | 744 | 745 | 746 | 747 | 748 | 749 | 750 | 751 | 752 | 753 | 754 | 755 | 756 | 757 | 758 | 759 | 760 | 761 | 762 | 763 | 764 | 765 | 766 | 767 | 768 | 769 | 770 | 771 | 772 | 773 | 774 | 775 | 776 | 777 | 778 | 779 | 780 | 781 | 782 | 783 | 784 | 785 | 786 | 787 | 788 | 789 | 790 | 791 | 792 | 793 | 794 | 795 | 796 | 797 | 798 | 799 | 800 | 801 | 802 | 803 | 804 | 805 | 806 | 807 | 808 | 809 | 810 | 811 | 812 | 813 | 814 | 815 | 816 | 817 | 818 | 819 | 820 | 821 | 822 | 823 | 824 | 825 | 826 | 827 | 828 | 829 | 830 | 831 | 832 | 833 | 834 | 835 | 836 | 837 | 838 | 839 | 840 | 841 | 842 | 843 | 844 | 845 | 846 | 847 | 848 | 849 | 850 | 851 | 852 | 853 | 854 | 855 | 856 | 857 | 858 | 859 | 860 | 861 | 862 | 863 | 864 | 865 | 866 | 867 | 868 | 869 | 870 | 871 | 872 | 873 | 874 | 875 | 876 | 877 | 878 | 879 | 880 | 881 | 882 | 883 | 884 | 885 | 886 | 887 | 888 | 889 | 890 | 891 | 892 | 893 | 894 | 895 | 896 | 897 | 898 | 899 | 900 | 901 | 902 | 903 | 904 | 905 | 906 | 907 | 908 | 909 | 910 | 911 | 912 | 913 | 914 | 915 | 916 | 917 | 918 | 919 | 920 | 921 | 922 | 923 | 924 | 925 | 926 | 927 | 928 | 929 | 930 | 931 | 932 | 933 | 934 | 935 | 936 | 937 | 938 | 939 | 940 | 941 | 942 | 943 | 944 | 945 | 946 | 947 | 948 | 949 | 950 | 951 | 952 | 953 | 954 | 955 | 956 | 957 | 958 | 959 | 960 | 961 | 962 | 963 | 964 | 965 | 966 | 967 | 968 | 969 | 970 | 971 | 972 | 973 | 974 | 975 | 976 | 977 | 978 | 979 | 980 | 981 | 982 | 983 | 984 | 985 | 986 | 987 | 988 | 989 | 990 | 991 | 992 | 993 | 994 | 995 | 996 | 997 | 998 | 999 | 1000 | 1001 | 1002 | 1003 | 1004 | 1005 | 1006 | 1007 | 1008 | 1009 | 1010 | 1011 | 1012 | 1013 | 1014 | 1015 | 1016 | 1017 | 1018 | 1019 | 1020 | 1021 | 1022 | 1023 | 1024 | 1025 | 1026 | 1027 | 1028 | 1029 | 1030 | 1031 | 1032 | 1033 | 1034 | 1035 | 1036 | 1037 | 1038 | 1039 | 1040 | 1041 | 1042 | 1043 | 1044 | 1045 | 1046 | 1047 | 1048 | 1049 | 1050 | 1051 | 1052 | 1053 | 1054 | 1055 | 1056 | 1057 | 1058 | 1059 | 1060 | 1061 | 1062 | 1063 | 1064 | 1065 | 1066 | 1067 | 1068 | 1069 | 1070 | 1071 | 1072 | 1073 | 1074 | 1075 | 1076 | 1077 | 1078 | 1079 | 1080 | 1081 | 1082 | 1083 | 1084 | 1085 | 1086 | 1087 | 1088 | 1089 | 1090 | 1091 | 1092 | 1093 | 1094 | 1095 | 1096 | 1097 | 1098 | 1099 | 1100 | 1101 | 1102 | 1103 | 1104 | 1105 | 1106 | 1107 | 1108 | 1109 | 1110 | 1111 | 1112 | 1113 | 1114 | 1115 | 1116 | 1117 | 1118 | 1119 | 1120 | 1121 | 1122 | 1123 | 1124 | 1125 | 1126 | 1127 | 1128 | 1129 | 1130 | 1131 | 1132 | 1133 | 1134 | 1135 | 1136 | 1137 | 1138 | 1139 | 1140 | 1141 | 1142 | 1143 | 1144 | 1145 | 1146 | 1147 | 1148 | 1149 | 1150 | 1151 | 1152 | 1153 | 1154 | 1155 | 1156 | 1157 | 1158 | 1159 | 1160 | 1161 | 1162 | 1163 | 1164 | 1165 | 1166 | 1167 | 1168 | 1169 | 1170 | 1171 | 1172 | 1173 | 1174 | 1175 | 1176 | 1177 | 1178 | 1179 | 1180 | 1181 | 1182 | 1183 | 1184 | 1185 | 1186 | 1187 | 1188 | 1189 | 1190 | 1191 | 1192 | 1193 | 1194 | 1195 | 1196 | 1197 | 1198 | 1199 | 1200 | 1201 | 1202 | 1203 | 1204 | 1205 | 1206 | 1207 | 1208 | 1209 | 1210 | 1211 | 1212 | 1213 | 1214 | 1215 | 1216 | 1217 | 1218 | 1219 | 1220 | 1221 | 1222 | 1223 | 1224 | 1225 | 1226 | 1227 | 1228 | 1229 | 1230 | 1231 | 1232 | 1233 | 1234 | 1235 | 1236 | 1237 | 1238 | 1239 | 1240 | 1241 | 1242 | 1243 | 1244 | 1245 | 1246 | 1247 | 1248 | 1249 | 1250 | 1251 | 1252 | 1253 | 1254 | 1255 | 1256 | 1257 | 1258 | 1259 | 1260 | 1261 | 1262 | 1263 | 1264 | 1265 | 1266 | 1267 | 1268 | 1269 | 1270 | 1271 | 1272 | 1273 | 1274 | 1275 | 1276 | 1277 | 1278 | 1279 | 1280 | 1281 | 1282 | 1283 | 1284 | 1285 | 1286 | 1287 | 1288 | 1289 | 1290 | 1291 | 1292 | 1293 | 1294 | 1295 | 1296 | 1297 | 1298 | 1299 | 1300 | 1301 | 1302 | 1303 | 1304 | 1305 | 1306 | 1307 | 1308 | 1309 | 1310 | 1311 | 1312 | 1313 | 1314 | 1315 | 1316 | 1317 | 1318 | 1319 | 1320 | 1321 | 1322 | 1323 | 1324 | 1325 | 1326 | 1327 | 1328 | 1329 | 1330 | 1331 | 1332 | 1333 | 1334 | 1335 | 1336 | 1337 | 1338 | 1339 | 1340 | 1341 | 1342 | 1343 | 1344 | 1345 | 1346 | 1347 | 1348 | 1349 | 1350 | 1351 | 1352 | 1353 | 1354 | 1355 | 1356 | 1357 | 1358 | 1359 | 1360 | 1361 | 1362 | 1363 | 1364 | 1365 | 1366 | 1367 | 1368 | 1369 | 1370 | 1371 | 1372 | 1373 | 1374 | 1375 | 1376 | 1377 | 1378 | 1379 | 1380 | 1381 | 1382 | 1383 | 1384 | 1385 | 1386 | 1387 | 1388 | 1389 | 1390 | 1391 | 1392 | 1393 | 1394 | 1395 | 1396 | 1397 | 1398 | 1399 | 1400 | 1401 | 1402 | 1403 | 1404 | 1405 | 1406 | 1407 | 1408 | 1409 | 1410 | 1411 | 1412 | 1413 | 1414 | 1415 | 1416 | 1417 | 1418 | 1419 | 1420 | 1421 | 1422 | 1423 | 1424 | 1425 | 1426 | 1427 | 1428 | 1429 | 1430 | 1431 | 1432 | 1433 | 1434 | 1435 | 1436 | 1437 | 1438 | 1439 | 1440 | 1441 | 1442 | 1443 | 1444 | 1445 | 1446 | 1447 | 1448 | 1449 | 1450 | 1451 | 1452 | 1453 | 1454 | 1455 | 1456 | 1457 | 1458 | 1459 | 1460 | 1461 | 1462 | 1463 | 1464 | 1465 | 1466 | 1467 | 1468 | 1469 | 1470 | 1471 | 1472 | 1473 | 1474 | 1475 | 1476 | 1477 | 1478 | 1479 | 1480 | 1481 | 1482 | 1483 | 1484 | 1485 | 1486 | 1487 | 1488 | 1489 | 1490 | 1491 | 1492 | 1493 | 1494 | 1495 | 1496 | 1497 | 1498 | 1499 | 1500 | 1501 | 1502 |
|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|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Appendix 13.3 Pumping Equipment-Capacity Caluculation Kandy

1. Pumping Station No.2 (Kandy Lake)

Total Capacity 605 m³/day= 0.42 m³/min
 Quantity of pump 1 sets + 1 set for stand-by
 Pump Capacity 605 m³/day
 $Q = 0.420 \text{ m}^3/\text{min}$
 $q = 0.0070 \text{ m}^3/\text{sec}$

Diameter Diameter = $146 \cdot (Q/v)^{1/2}$
 = 77 mm to 55 mm
 = 65 mm
 where, $v = 1.50$ to 3.00

Total Head Total Head $H = h_1 + h_2 + h_3 = 12.3 \text{ m}$
 = 14.0 m
 actual head $h_1 = h_d - h_s = 4.45 \text{ m}$
 suction level $h_s = 508.66 \text{ m}$
 delivery level $h_d = 513.11 \text{ m}$
 friction loss (Hazen Williams): straight pipe
 $h_2 = 10.666 \cdot c^{-1.85} \cdot D^{-4.87} \cdot q^{1.85} \cdot L$
 = 6.51 m
 where, $c = 130$
 $D = 100 \text{ mm dia} / 1000$
 $L = 650 \text{ m}$
 $(v = 0.892 \text{ m/sec})$

friction loss : fittings

$$h_3 = f \cdot (v^2 / 2 \cdot g)$$

$$= 1.34 \text{ m}$$

where, $v = 2.11 \text{ m/sec}$

| where, | Q^{ty} | f/pc | f |
|--------------|-----------------|--------|------|
| check valve | 1 | 1.50 | 1.50 |
| sluice valve | 2 | 0.10 | 0.20 |
| increase | 0 | 0.15 | 0.00 |
| 90deg | 5 | 0.18 | 0.90 |
| tee | 2 | 1.15 | 2.30 |
| outlet | 1 | 1.00 | 1.00 |
| | total | | 5.90 |

Motor Output Motor Output = $(0.163 \cdot r \cdot Q \cdot H / e) \cdot (1 + a)$
 = 1.8 kW
 = 2.2 kW
 where, $r = 1.00$
 $e = 0.60$
 $a = 0.15$

Specification

| | |
|--------------|----------------------------|
| Type | Submersible Sewage Pump |
| Diameter | 65 mm |
| Capacity | 0.42 m ³ /min |
| Head | 14.0 m |
| Motor Output | 2.2 kW |
| Quantity | 1 sets + 1 set for standby |

2. Sewage Treatment Plant (Large)

Total Capacity 23,613 m³/day= 16.40 m³/min
 Quantity of pump 2 sets + 1 set for stand-by
 Pump Capacity 11,807 m³/day
 $Q = 8.199 \text{ m}^3/\text{min}$
 $q = 0.1366 \text{ m}^3/\text{sec}$

Diameter Diameter = $146 \cdot (Q/v)^{1/2}$
 $= 341 \text{ mm}$ to 241 mm
 $= 250 \text{ mm}$
 where, $v = 1.50$ to 3.00

Total Head Total Head $H = h_1 + h_2 + h_3 = 12.2 \text{ m}$
 $= 14.0 \text{ m}$

actual head $h_1 = h_d - h_s = 9.62 \text{ m}$

suction level $h_s = 465.38 \text{ m}$

delivery level $h_d = 475.00 \text{ m}$

friction loss (Hazen Williams): straight pipe

$h_2 = 10.666 \cdot c^{-1.85} \cdot D^{-4.87} \cdot q^{1.85} \cdot L$

$= 0.29 \text{ m}$

where, $c = 130$

$D = 450 \text{ mm dia} / 1000$

$L = 50 \text{ m}$

$(v = 1.718 \text{ m/sec})$

friction loss : fittings

$h_3 = f \cdot (v^2 / 2 \cdot g)$

$= 2.33 \text{ m}$

where, $v = 2.78 \text{ m/sec}$

where,

| | Qty | f/pc | f |
|--------------|-----|------|-------------|
| check valve | 1 | 1.50 | 1.50 |
| sluice valve | 2 | 0.10 | 0.20 |
| increase | 0 | 0.15 | 0.00 |
| 90deg | 5 | 0.18 | 0.90 |
| tee | 2 | 1.15 | 2.30 |
| outlet | 1 | 1.00 | 1.00 |
| total | | | 5.90 |

Motor Output Motor Output = $(0.163 \cdot r \cdot Q \cdot H / e) \cdot (1 + a)$

$= 35.9 \text{ kW}$

$= 37.0 \text{ kW}$

where, $r = 1.00$

$e = 0.60$

$a = 0.15$

Specification

| | |
|--------------|----------------------------|
| Type | Submersible Sewage Pump |
| Diameter | 250 mm |
| Capacity | 8.2 m ³ /min |
| Head | 14.0 m |
| Motor Output | 37 kW |
| Quantity | 2 sets + 1 set for standby |

3. Sewage Treatment Plant (Small)

Total Capacity 23,613 m³/day= 16.40 m³/min
 Quantity of pump 4 sets + 1 set for stand-by
 Pump Capacity 5,903 m³/day
 Q = 4.099 m³/min
 q = 0.0683 m³/sec

Diameter Diameter = $146 \cdot (Q/v)^{1/2}$
 = 241 mm to 171 mm
 = 200 mm
 where, v = 1.50 to 3.00

Total Head Total Head H = h₁ + h₂ + h₃ = 11.3 m
 = 14.0 m

actual head h₁ = h_d - h_s = 9.62 m
 suction level h_s = 465.38 m
 delivery level h_d = 475.00 m

friction loss (Hazen Williams) : straight pipe

$$h_2 = 10.666 \cdot c^{-1.85} \cdot D^{-4.87} \cdot q^{1.85} \cdot L$$

$$= 0.29 \text{ m}$$

where, c = 130

D = 450 mm dia / 1000

L = 50 m

(v = 1.718 m/sec)

friction loss : fittings

$$h_3 = f \cdot (v^2 / 2 \cdot g)$$

$$= 1.42 \text{ m}$$

where, v = 2.17 m/sec

where,

| | Q'ty | f/pc | f |
|--------------|------|------|-------------|
| check valve | 1 | 1.50 | 1.50 |
| sluice valve | 2 | 0.10 | 0.20 |
| increase | 0 | 0.15 | 0.00 |
| 90deg | 5 | 0.18 | 0.90 |
| tee | 2 | 1.15 | 2.30 |
| outlet | 1 | 1.00 | 1.00 |
| total | | | 5.90 |

Motor Output Motor Output = $(0.163 \cdot r \cdot Q \cdot H / e) \cdot (1 + a)$

$$= 17.9 \text{ kW}$$

$$= 18.5 \text{ kW}$$

where, r = 1.00

e = 0.60

a = 0.15

Specification

| | |
|--------------|----------------------------|
| Type | Submersible Sewage Pump |
| Diameter | 200 mm |
| Capacity | 4.1 m ³ /min |
| Head | 14.0 m |
| Motor Output | 18.5 kW |
| Quantity | 4 sets + 1 set for standby |

Appendix 13.4 Sewage Treatment Plant - Capacity Calculation

CAPACITY CALCULATION OF FACILITIES (Oxidation Ditch)

1 BASIC CONDITIONS

1-1 BASIC ITEMS

- (1) Name : Kandy Sewage Treatment Plant
- (2) Land Area : Approximately 1.00 ha
- (3) Elevation : 474.000 m
- (4) Inlet Pipe Level : 465.883 m
- (5) Pipe Diameter : 600 m
- (6) Land Use : Paddy Field
- (7) Collection System : Seperate Type
- (8) Treatment Method : Sewage Treatment : Oxidation Ditch Method
Sludge Treatment : Sludge Digestion and Drying Bed
- (9) Effluent Point : Mada Ela River
- (10) Effluent Point Water Level : 470.640 m
- (11) Target Year : Year 2005 (Phase 1)
- (12) Lowest Monthly Average Temperature : 23.6 °C (January)

1-2 Design Population

Design Population : 19,260 Persons (Total)

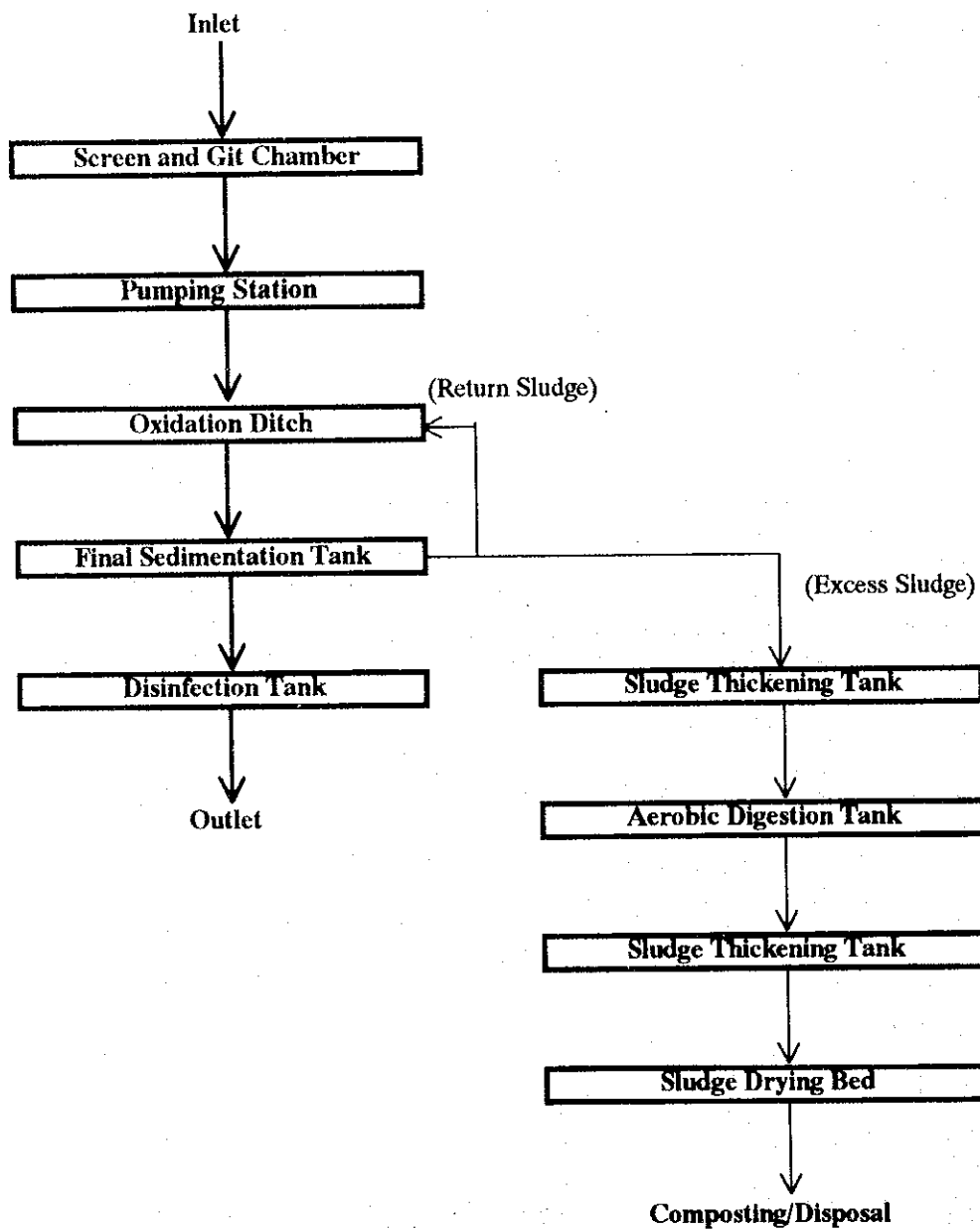
1-3 Design Sewage Flow

| ITEM | m ³ /day | m ³ /hr | m ³ /min | m ³ /sec |
|----------------|---------------------|--------------------|---------------------|---------------------|
| Daily Average | 6,950 | 289.6 | 4.83 | 0.080 |
| Daily Maximum | 8,500 | 354.2 | 5.90 | 0.098 |
| Hourly Maximum | 11,550 | 481.3 | 8.02 | 0.134 |

1-4 Design Sewage Quality

| ITEM | INFLUENT (mg/L) | EFFLUENT (mg/L) | REMOVAL RATIO (%) | REMARKS |
|------|--------------------|--------------------|----------------------|---------|
| BOD | 240 | 30 | 88 | |
| SS | 250 | 50 | 80 | |

1-5 Flow Chart (Oxidation Ditch)



1-6 Design Criteria for Oxidation Ditch

| ITEMS | UNIT | Formula or Value | Application |
|--------------------------------|-------------------------------------|-------------------|--------------|
| 1-6-1 Oxidation Ditch | | | |
| (1) BOD-SS Load | kg/kg/day | 0.03 - 0.05 | 0.05 |
| (2) MLSS Concentration | mg/l | 3,000 - 4,000 | 4,000 |
| (3) Return Sludge Ratio | % | 100 - 200 | 150 |
| (4) Water Depth | m | 1.0 - 3.0 | Same as Left |
| (5) Width | m | 2.0 - 6.0 | Same as Left |
| (6) Retention Time | hour | 24 - 48 | Same as Left |
| (6) Oxygen Requirement | kgO ₂ /kgBOD | 1.4 - 2.2 | 2.0 |
| (7) Sludge Age | day | 8 - 50 | Same as Left |
| 1-6-2 Final Sedimentation Tank | | | |
| (1) Water Surface Load | m ³ /m ² /day | 8 - 12 | 8 - 12 |
| (2) Retention Time | hour | 6.0 - 12.0 | Same as Left |
| (3) Water Depth | m | 3.0 - 4.0 | 3.0 |
| 1-6-3 Disinfection Tank | | | |
| (1) Retention Time | min. | > 15 | 15 |
| (2) Dosage | mg/l | 2.0 - 4.0 | 3.0 |
| 1-6-4 Sludge Thickening Tank | | | |
| (1) Solid Matter Load | kg/m ² /day | 60 - 90 | 70 |
| (2) Water Depth | m | Approximately 4.0 | 4.0 |
| 1-6-5 Aerobic Digestion Tank | | | |
| (1) Retention Time | day | 10.0 - 15.0 | Same as Left |
| (2) Solid Matter Load | kg/m ² /day | 1.60 - 4.81 | Same as Left |
| 1-6-6 Sludge Drying Bed | | | |
| (1) Drying Period | day | 15 - 30 | 20 |
| (2) Depth of Bed | m | 0.3 - 1.0 | 0.3 |

2 CAPACITY CALCULATION

2-1 Oxidation Ditch (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|---|--------|---------------------|------------------------------|---------|
| Type | - | - | Re-circulation Flow Type | |
| Design Flow | Q1 | m ³ /day | - | 8,500 |
| | Q2 | m ³ /hr | - | 354.2 |
| Basin Number | BN | Basin | - | 3 |
| Inlet BOD Quality | C | mg/L | - | 240 |
| Inlet SS Quality | S | mg/L | - | 250 |
| Inlet BOD Matter | M | kg/day | $Q1 * C * 10^{-3}$ | 2,040 |
| BOD-SS Load | BS | kg/kg/day | - | 0.05 |
| MLSS Concentration | SS | mg/L | - | 4,000 |
| Required Volume Therefore | V1 | m ³ | $M / (SS * BS * 10^{-3})$ | 10,200 |
| | V2 | m ³ | - | 10,200 |
| Retention Time | T | hr | $(V2 / Q1) * 24$ | 28.8 |
| Return Sludge Ratio | R1 | % | - | 150 |
| | R2 | - | $R1 / 100$ | 1.5 |
| Return Sludge Quality Therefore | RS1 | mg/L | $(SS * (1 + R2) - C) / R2$ | 6,507 |
| | RS2 | mg/L | - | 6,510 |
| Sludge Age | SA | day | $SS * V2 / (Q1 * S)$ | 19.2 |
| Width | W | m | - | 6.0 |
| Water Depth | H | m | - | 3.0 |
| Length Therefore | L1 | m | $(V2 / BN) / (W * H)$ | 188.9 |
| | L2 | m | - | 190.0 |
| Dimension (Width) (Depth) (Length) (Basin Number) | W | m | W | 6.0 |
| | H | m | H | 3.0 |
| | L | m | L2 | 190.0 |
| | - | basin | BN | 3 |
| Required Oxygen | O2-day | kgO2/day | $Q1 * C * 10^{-3} * 2.0$ | 4,080.0 |
| | O2-hr | kgO2/hr | $(O2\text{-day}) / 24$ | 170.0 |
| Aerator Motor Output | - | kW | $O2\text{-hr} / 1.9$ | 89.5 |
| | - | kW | - | 90.0 |
| Aerator Type | - | - | Slanting Shaft Screw Aerator | |
| Check | | UNIT | APPLICATION | RESULT |
| Retention Time | | hour | 24 - 48 | 29.0 |
| Oxygen Supply | | kgO2/kg | 1.4 - 2.2 | 2.0 |
| Sludge Age | | day | 8 - 50 | 19.2 |

2-2 Final Sedimentation Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|-----------------------|------|-------------------------------------|--|--------|
| Type | - | - | Radial Flow Circular Type | |
| Design Flow | Q1 | m ³ /day | - | 8,500 |
| | Q2 | m ³ /sec | - | 354.17 |
| Basin Number | BN | Basin | - | 3 |
| Water Surface Load | L | m ³ /m ² /day | $4.14 \times 10^4 \cdot T^{0.95} \cdot SS^{-1.35}$ | 11.4 |
| Therefore | L | m ³ /m ² /day | - | 12.0 |
| Required Surface Area | A1 | m ² | Q1/L | 708.3 |
| | A2 | m ² /Basin | A1/BN | 236.1 |
| Water Depth | H | m | - | 3.0 |
| Diameter | D1 | m | $(A2/3.14)^{0.5 \cdot 2}$ | 17.3 |
| Therefore | D2 | m | - | 16.0 |
| Dimension (Diam) | D | m | D2 | 16.0 |
| (Depth) | H | m | H | 3.0 |
| (Basin Number) | - | Basin | BN | 3 |
| Sludge Collector Type | - | - | Central Drive Type | |
| Check | | UNIT | APPLICATION | RESULT |
| Water Surface Load | | m ³ /m ² /day | 8 - 12 | 14.1 |
| Retention Time | | hour | 6.0 - 12.0 | 3.4 |

2-3 Disinfection Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|-------------------|------|---------------------|--------------------------------|--------|
| Chemical Type | - | - | Chlorination Type | |
| Design Flow | Q1 | m ³ /day | - | 8,500 |
| | Q2 | m ³ /min | - | 5.90 |
| Retention Time | T | min. | - | 15.0 |
| Basin Number | BN | basin | - | 1 |
| Required Volume | V | m ³ | Q2*T | 89 |
| Width | W | m | - | 3.00 |
| Water Depth | H | m | - | 1.50 |
| Length | L1 | m | $V/(W \cdot H)$ | 19.676 |
| therefore | L2 | m | - | 20.00 |
| Dosage | D | mg/L | - | 2.0 |
| Required Chemical | RC1 | kg/day | $Q1 \cdot D \cdot 10^{-3} / C$ | 17.00 |
| Therefore | RC2 | kg/hr | RC1/24 | 0.71 |
| Dimension (W) | W | m | W | 3.0 |
| (Length) | L | m | L2 | 20.0 |
| (Depth) | H | m | H | 1.5 |
| (Basin) | BN | basin | - | 1 |
| Chlorine Feeder | - | unit | including 1 for stand-by | 3 |
| Check | | UNIT | APPLICATION | RESULT |
| Retention Time | | min. | 15 | 15.2 |

2-4 Sludge Thickening Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|---|-------|------------------------|---|--------|
| Type | - | - | Radial Flow Circular Type | |
| Design Flow | Q1 | m ³ /day | - | 8,500 |
| | Q2 | m ³ /hr | - | 289.6 |
| Basin Number | BN | Basin | - | 1 |
| Inlet SS Quality | C | mg/L | - | 250 |
| Removal Ratio | R1 | % | - | 80 |
| | R2 | - | R1/100 | 0.80 |
| Sludge Generation Ratio (Oxidation Ditch) | SG1 | % | - | 75 |
| | SG2 | - | SG1/100 | 0.75 |
| Inlet SS Matter | M | kg/day | $Q1 \cdot C \cdot R2 \cdot SG2 \cdot 10^{-3}$ | 1,275 |
| Solid Matter Load | L | kg/m ² /day | - | 70.0 |
| Required Surface Area | A1 | m ² | M/L | 18.2 |
| | A2 | m ² /Basin | A1/BN | 18.2 |
| Water Depth | H | m | - | 4.0 |
| Diameter | D1 | m | $(A2/3.14)^{0.5 \cdot 2}$ | 4.8 |
| Therefore | D2 | m | - | 5.0 |
| Dimension (Depth) | D | m | D2 | 5.0 |
| (Basin) | H | m | H | 4.0 |
| | Basin | Basin | BN | 1 |
| Check | | UNIT | APPLICATION | RESULT |
| Solid Matter Load | | kg/m ² /day | 70 | 65.0 |

2-5 Aerobic Sludge Digestion Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|------------------------------|-------|------------------------|---|---------|
| Type | - | - | Circular Type | |
| Basin Number | BN | Basin | - | 1 |
| Design Flow | Q1 | m ³ /day | - | 8,500 |
| Inlet SS Matter | M | kg/day | - | 1,275 |
| Moisture Content | G | % | - | 97.5 |
| Sludge Volume | V1 | m ³ /day | $M \cdot 100 / (100 - G)$ | 51.0 |
| Temperature - Summer | TS | °C | - | 26.5 |
| - Winter | TW | °C | - | 23.6 |
| Temperature - Sludge Age | TSA | day-°C | VolatileSolidReduction=40% | 470 |
| Sludge Age | SA | day | TSA/TS | 19.9 |
| Total Mass of VSS | VSS | kg/day | 0.8 * M | 1,020 |
| VSS Reduction - Summer (41%) | VRS | kg/day | VSS * 0.4 | 408.0 |
| - Winter (40%) | VRW | kg/day | VSS * 0.41 | 418.2 |
| Required Volume | V | m ³ | $V1 / 0.7 / (0.125 \cdot 0.8 + 1/SA)$ | 485 |
| Water Depth | H | m | - | 4.0 |
| Diameter | D1 | m | $(A2/3.14)^{0.5 \cdot 2}$ | 12.4 |
| Therefore | D2 | m | - | 13.0 |
| Dimension (Depth) | D | m | D2 | 13.0 |
| (Basin) | H | m | H | 4.0 |
| | Basin | Basin | BN | 1 |
| Required Oxygen | RO | kgO ₂ /day | 2.3 * VRS | 938.4 |
| Required Air | RA | kg-Air/hr | $RO / (0.1 \cdot 0.233 \cdot 1.293) / 1440$ | 1,297.8 |
| Check | | UNIT | APPLICATION | RESULT |
| Retention Time | | day | 10.0 - 15.0 | 10.4 |
| Solid Matter Load | | kg/m ³ /day | 1.60 - 4.81 | 2.4 |

2-6 Sludge Thickening Tank (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|---------------------------------|-------|-----------|---------------------------|--------|
| Type | - | - | Radial-Flow Circular Type | |
| Basin Number | BN | Basin | - | 1 |
| Inlet SS Matter to Digestion | M1 | kg/day | - | 1,275 |
| Removal Ratio at Digestion | R1 | % | - | 40% |
| Inlet SS Matter | M2 | kg/day | $M1*(1-R1)$ | 765 |
| Moisture Content | G | % | - | 99.0 |
| Sludge Volume | V1 | m3/day | $M2*100/(100-G)$ | 76.5 |
| Solid Matter Load | L | kg/m2/day | - | 70.0 |
| Required Surface Area | A1 | m2 | M/L | 10.9 |
| | A2 | m2/Basin | A1/BN | 10.9 |
| Water Depth | H | m | - | 4.0 |
| Diameter | D1 | m | $(A2/3.14)^{0.5*2}$ | 3.7 |
| | D2 | m | - | 5.0 |
| Dimension (Depth) (Basin) | D | m | D2 | 5.0 |
| | H | m | H | 4.0 |
| | Basin | Basin | BN | 1 |
| | | | | |
| Check | | UNIT | APPLICATION | RESULT |
| Solid Matter Load | | kg/m2/day | 70 | 39.0 |

2-7 Sludge Drying Bed (Daily Maximum)

| ITEM | SIGN | UNIT | CALCULATION | RESULT |
|--|-------|--------|-------------------|--------|
| Design Flow | Q1 | m3/day | - | 8,500 |
| Inlet SS Matter | M1 | kg/day | $Q1*C*R2*10^{-3}$ | 765 |
| | M2 | t/day | $M1/1000$ | 0.765 |
| Moisture Content | G | % | - | 97.0 |
| Sludge Volume | V1 | m3/day | $M2*100/(100-G)$ | 25.5 |
| Drying Period | P | day | - | 10 |
| Required Volume | V2 | m3/day | $V1*P$ | 255.0 |
| Depth of Bed | H | m | - | 0.3 |
| Required Area | A | m2 | $V2/H$ | 850 |
| Unit Number | UN | Unit | - | 10 |
| Width per Unit | W | m | - | 6.0 |
| Length per Unit | L1 | m | $A/(UN*W)$ | 14.2 |
| | L2 | m | - | 14.5 |
| Dimension (Width) (Length) (Depth) (Basin) | W | m | W | 6.0 |
| | L | m | L2 | 14.5 |
| | H | m | H | 0.3 |
| | Basin | Basin | BN | 10.0 |
| Check | | UNIT | APPLICATION | RESULT |
| Drying Period | | day | 20 | 10.2 |

Appendix 13.5 Hydraulic Calculation

1. Design Condition

1.1 Design Wastewater Quantity

| Flow | | m ³ /day | m ³ /hour | m ³ /min | m ³ /sec |
|----------------|--------|---------------------|----------------------|---------------------|---------------------|
| Daily Average | Qd-ave | 6,950 | 289.6 | 4.826 | 0.080 |
| Daily Maximum | Qd-max | 8,500 | 354.2 | 5.903 | 0.098 |
| Hourly Maximum | Qh-max | 11,550 | 481.3 | 8.021 | 0.134 |

1.2 Unit and Capacity of Treatment Facilities

| Facilities | Total | Duty | Stand-by | Capacity |
|---------------------|-------|------|----------|----------|
| Grit Chamber/Screen | 2 | 2 | 1 | Qhw-max |
| Oxydation Ditch | 3 | 3 | 0 | Qd-ave |
| Sedimentation Tank | 3 | 3 | 0 | Qd-ave |
| Disinfection Tank | 1 | 1 | 0 | Qd-ave |

1.3 Discharge

Discharge Point Meda Ela
 HWL 470.64 m

1.4 Formula for Hydraulic Calculation

a. Friction loss for streight pipe

Darcy-Weisbach

$$\text{Head Loss} \quad h = f * V^2 / (2 * g)$$

$$\text{where,} \quad f1 = (0.02 + 1 / (2000 * D)) * (L / D)$$

b. Friction loss for fittings

$$\text{Head Loss} \quad h = f * V^2 / (2 * g)$$

$$\text{where,} \quad \begin{aligned} f2 &= 1.00 \text{ (Inlet)} \\ f3 &= 0.50 \text{ (Outlet)} \end{aligned}$$

2. Hydraulic Calculation

2.1 Water Level of Disinfection Tank Effluent Chamber (WL1)

| | | Qd-ave | Qd-max | Qh-max | (Unit) |
|-------------|---|--------|--------|--------|---------------------|
| Design Flow | Q | 6,950 | 8,500 | 11,550 | m ³ /day |
| | q | 0.080 | 0.098 | 0.134 | m ³ /sec |

Pipe Diameter 300 mm

Pipe Length 50.0 m

No. of Pipe 1 set

| | | | | | |
|----------|-----|------|------|------|-------|
| Velocity | V = | 1.14 | 1.39 | 1.89 | m/sec |
|----------|-----|------|------|------|-------|

Hydraulic Loss $h = f * V^2 / (2 * g)$

where, $f1 = (0.02 + 1 / (2000 * D)) * (L / D)$

= 3.6111E-06 (Straight Pipe)

f2 = 1.00 (Inlet)

f3 = 0.50 (Outlet)

| | | | | | |
|----------------|------|-------|-------|-------|---|
| Hydraulic Loss | h1 = | 0.099 | 0.148 | 0.274 | m |
|----------------|------|-------|-------|-------|---|

WL1 = 470.640 + h1 = 470.788 470.914 m

say, 470.79 470.92 m

(Qd-max) (Qh-max)

2.2 Water Level of Disinfection Tank (WL2)

Weir Width W = 1.0 m

No. of Weir 1 set

Weir level hw = 473.10 m

Overflow height $h = (Q / (1.84 * W))^{2/3}$

| | | | | | |
|--|------|-------|-------|-------|---|
| | h2 = | 0.124 | 0.142 | 0.174 | m |
|--|------|-------|-------|-------|---|

WL2 = hw + h2 = 473.242 473.274 m

say, 473.25 473.28 m

(Qd-max) (Qh-max)

2.3 Water Level of Settled Water Effluent Chamber (WL3)

Pipe Diameter 200 mm

Pipe Length 50.0 m

No. of Pipe 3 sets

| | | | | | |
|----------|-----|------|------|------|-------|
| Velocity | V = | 0.85 | 1.04 | 1.42 | m/sec |
|----------|-----|------|------|------|-------|

Hydraulic Loss $h = f * V^2 / (2 * g)$

where, $f1 = (0.02 + 1 / (2000 * D)) * (L / D)$

= 5.625E-06 (Straight Pipe)

f2 = 1.00 (Inlet)

f3 = 0.50 (Outlet)

| | | | | | |
|----------------|------|-------|-------|-------|---|
| Hydraulic Loss | h3 = | 0.056 | 0.083 | 0.154 | m |
|----------------|------|-------|-------|-------|---|

WL3 = WL2 + h3 = 473.333 473.434 m

say, 473.34 473.44 m

(Qd-max) (Qh-max)

2.4 Water Level of Sedimentation Tank Trough (WL4)

No. of Sedimentation Tank 3 tanks

Tank Diameter D = 16.0 m

Trough Length L = 25.1 m

Trough Width B = 0.3 m free fall

Trough Level hw = 473.50 m

Critical Water Level $h_{cl} = ((Q^2)/(g * B^2))^{(1/3)}$

| | | | | | |
|--|-------|-------|-------|-------|---|
| | hcl = | 0.093 | 0.107 | 0.131 | m |
|--|-------|-------|-------|-------|---|

Hydraulic Loss $h_4 = (3)^{(1/2)} * h_{cl}$

| | | | | | |
|--|-----|-------|-------|-------|---|
| | h = | 0.162 | 0.185 | 0.227 | m |
|--|-----|-------|-------|-------|---|

WL4 = hw + h4 = 473.685 473.727 m

say, 473.69 473.73 m

(Qd-max) (Qh-max)

2.5 Water Level of Sedimentation Tank (WL5)

No. of Sedimentation Tank 3 tanks

Tank Diameter 16.0 m

No. of Notches (8 nos/m) 402 nos

Weir level hw = 473.98 m

Hydraulic Loss $h_5 = ((Q/n)/1.42)^{(2/5)}$

| | | | | | |
|--|-----|-------|-------|-------|---|
| | h = | 0.019 | 0.020 | 0.023 | m |
|--|-----|-------|-------|-------|---|

WL5 = hw + h5 = 474.000 474.003 m

say, 474.00 474.01 m

(Qd-max) (Qh-max)

2.6 Water Level of Oxidation Ditch Effluent Chamber (WL6)

Pipe Diameter 200 mm

Pipe Length 50.0 m

No. of Pipe 3 sets

| | | | | | |
|----------|-----|------|------|------|-------|
| Velocity | V = | 0.85 | 1.04 | 1.42 | m/sec |
|----------|-----|------|------|------|-------|

Hydraulic Loss $h = f * V^2 / (2 * g)$

where, $f_1 = (0.02 + 1 / (2000 * D)) * (L / D)$

= 5.625E-06 (Straight Pipe)

f2 = 1.00 (Inlet)

f3 = 0.50 (Outlet)

| | | | | | |
|----------------|------|-------|-------|-------|---|
| Hydraulic Loss | h6 = | 0.056 | 0.083 | 0.154 | m |
|----------------|------|-------|-------|-------|---|

WL6 = WL5 + h6 = 474.083 474.164 m

say, 474.09 474.17 m

(Qd-max) (Qh-max)

2.7 Water Level of Oxidation Ditch (WL7)

No. of Sedimentation Tank 3 tanks

Weir Width $W = 1.0$ m

No. of Weir 1 set

Weir level $hw = 474.33$ m

Overflow height $h = (Q / (1.84 * W))^{(2/3)}$

| | | | | | |
|--|---------|-------|-------|-------|---|
| | $h_2 =$ | 0.060 | 0.068 | 0.084 | m |
|--|---------|-------|-------|-------|---|

WL7 = $hw + h_7 = 474.398$ 474.414 m

say, 474.40 474.42 m

(Qd-max) (Qh-max)

2.8 Water Level of Distribution Chamber - Effluent (WL8)

Pipe Diameter 200 mm

Pipe Length 50.0 m

No. of Pipe 3 sets

| | | | | | |
|----------|-------|------|------|------|-------|
| Velocity | $V =$ | 0.85 | 1.04 | 1.42 | m/sec |
|----------|-------|------|------|------|-------|

Hydraulic Loss $h = f * V^2 / (2 * g)$

where, $f_1 = (0.02 + 1 / (2000 * D)) * (L / D)$

= 5.625E-06 (Straight Pipe)

$f_2 = 1.00$ (Inlet)

$f_3 = 0.50$ (Outlet)

| | | | | | |
|----------------|---------|-------|-------|-------|---|
| Hydraulic Loss | $h_6 =$ | 0.056 | 0.083 | 0.154 | m |
|----------------|---------|-------|-------|-------|---|

WL8 = WL7 + + $h_8 = 474.483$ 474.574 m

say, 474.49 474.58 m

(Qd-max) (Qh-max)

2.9 Water Level of Distribution Influent (WL9)

No. of Sedimentation Tank 3 sets

Weir Width $W = 1.0$ m

No. of Weir 1 set

Weir level $hw = 474.70$ m

Overflow height $h = (Q / (1.84 * W))^{(2/3)}$

| | | | | | |
|--|---------|-------|-------|-------|---|
| | $h_2 =$ | 0.060 | 0.068 | 0.084 | m |
|--|---------|-------|-------|-------|---|

WL9 = $hw + h_9 = 474.768$ 474.784 m

say, 474.77 474.79 m

(Qd-max) (Qh-max)

2.10 Water Level of Grit Chamber Effluent Chamber (WL10)

Pipe Diameter 400 mm

Pipe Length 50.0 m

No. of Pipe 1 set

| | | | | | |
|----------|-------|------|------|------|-------|
| Velocity | $V =$ | 0.64 | 0.78 | 1.06 | m/sec |
|----------|-------|------|------|------|-------|

Hydraulic Loss $h = f * V^2 / (2 * g)$

where, $f1 = (0.02 + 1 / (2000 * D)) * (L / D)$
 $= 2.6563E-06$ (Straight Pipe)

$f2 = 1.00$ (Inlet)

$f3 = 0.50$ (Outlet)

| | | | | | |
|----------------|--------|-------|-------|-------|---|
| Hydraulic Loss | $h6 =$ | 0.031 | 0.047 | 0.087 | m |
|----------------|--------|-------|-------|-------|---|

$WL10 = WL9 + h10 = 474.817 \quad 474.877 \text{ m}$

say, $\boxed{474.82}$ 474.88 m
 (Qd-max) (Qh-max)

2.11 Water Level of Grit Chamber Influent Chamber (WL15)

No. of Screens 3 sets including 1 for standby

Head loss $h11 = 0.10 \text{ m}$

$WL11 = WL10 + h11 = 474.920 \quad 474.980 \text{ m}$

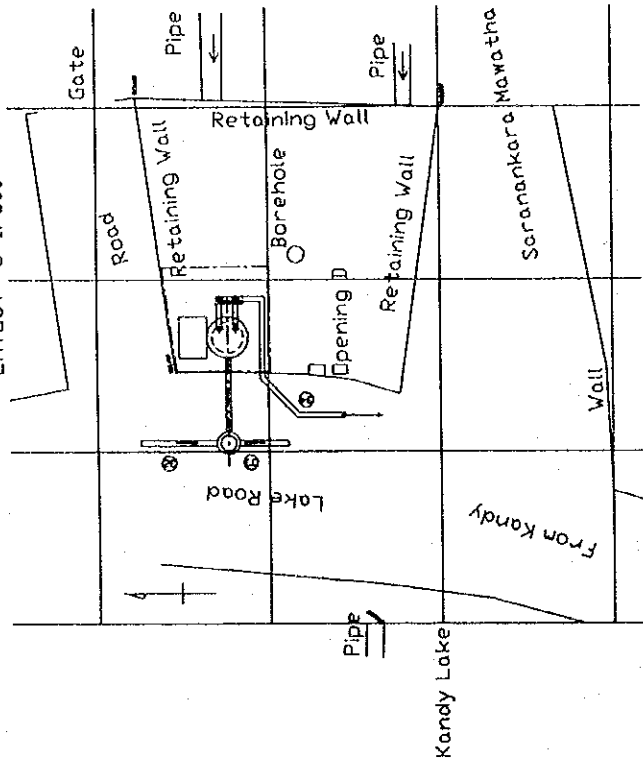
say, $\boxed{474.92}$ 474.98 m
 (Qd-max) (Qh-max)

Appendix 13.6 DRAWING

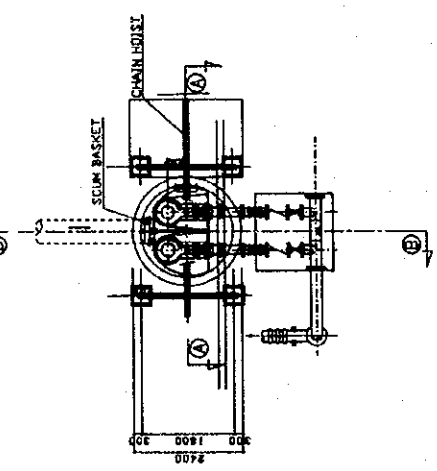
DRAWING LIST

| No. | DRAWING NAME |
|--------|-------------------------------|
| S.1-1 | PUMP STATION (LAKE) |
| S.2-1 | SEWAGE TREATMENT PLANT LAYOUT |
| S.2-2 | HYDRAULIC PROFILE |
| S.2-3 | FLOW DIAGRAM (1) |
| S.2-4 | FLOW DIAGRAM (2) |
| S.2-5 | PUMPING STATION (1) |
| S.2-6 | PUMPING STATION (2) |
| S.2-7 | OXIDATION DITCH |
| S.2-8 | SEDIMENTATION BASIN |
| S.2-9 | DISINFECTION TANK |
| S.2-10 | RETURN SLUDGE PUMP ROOM |
| S.2-11 | SLUDGE THICKENING TANK |
| S.2-12 | AEROBIC SLUDGE DIGESTION TANK |
| S.2-13 | SLUDGE DRYING BED LAYOUT |
| S.2-14 | SLUDGE DRYING BED |

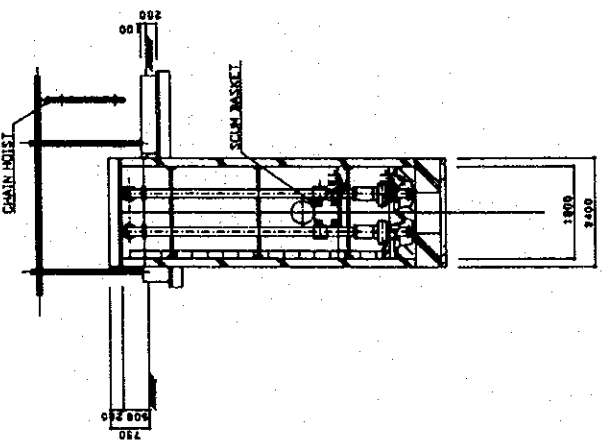
LAYOUT S=1/300



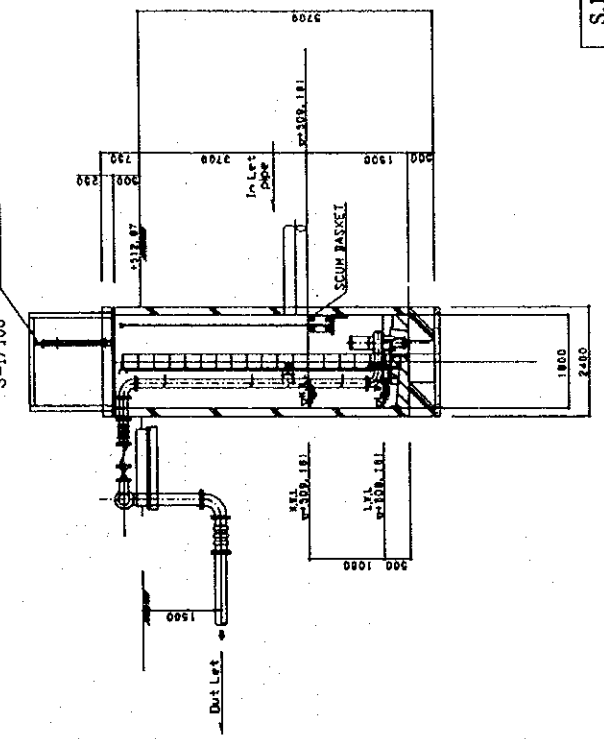
PLAN S=1/100



SECTION A-A S=1/100



SECTION B-B S=1/100

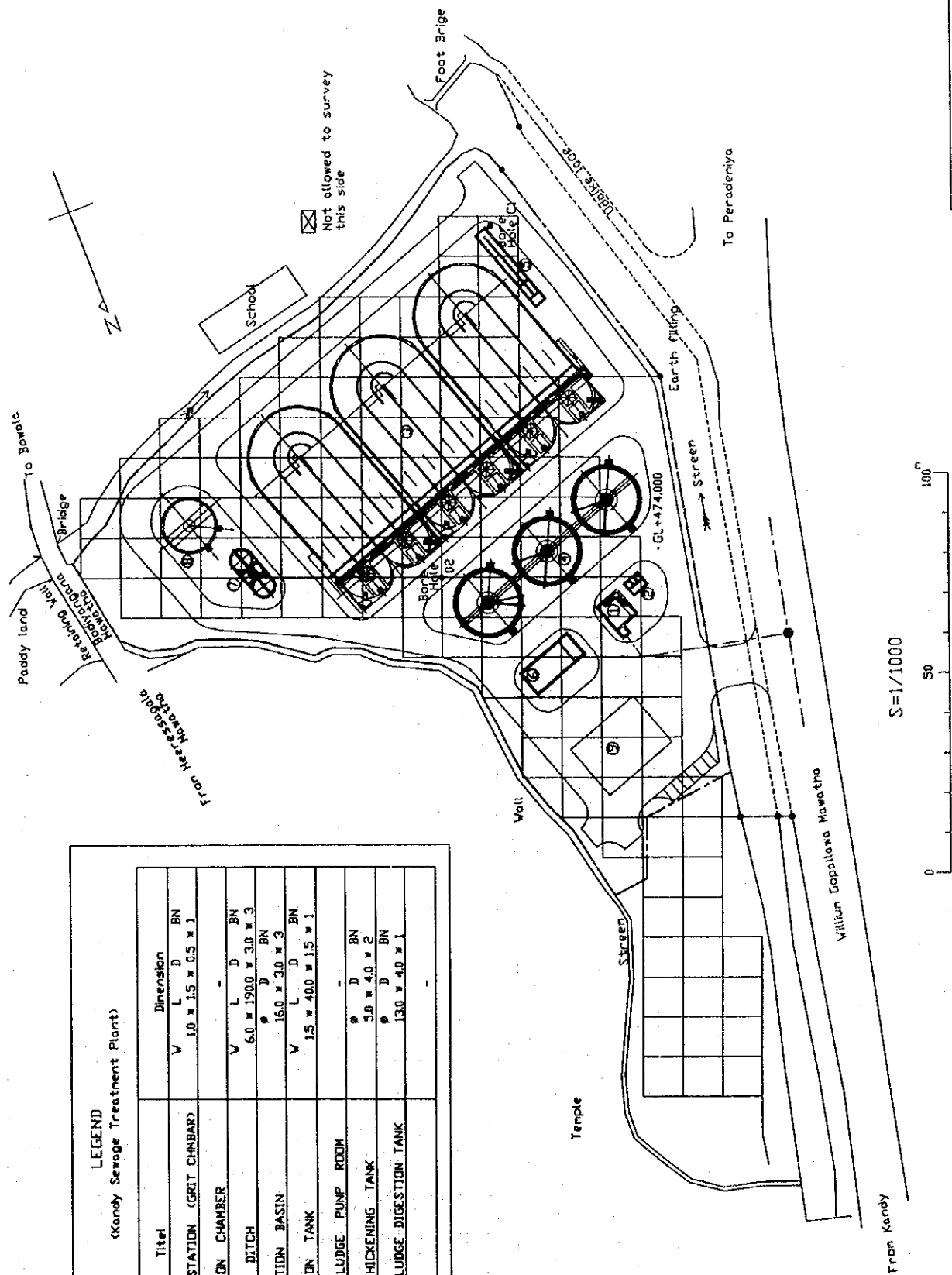


S.I-1
PUMPING STATION
(LAKE)

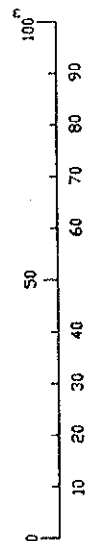
LAYOUT

LEGEND
(Kandy Sewage Treatment Plant)

| No. | Title | Dimension | | |
|-----|--------------------------------|--|-----|------|
| | | V | L | BN |
| ① | PUMPING STATION (GRIT CHAMBER) | $1.0 \times 1.5 \times 0.5 \times 1$ | | |
| ② | DISTRIBUTION CHAMBER | | | |
| ③ | OXIDATION DITCH | $6.0 \times 19.00 \times 3.0 \times 3$ | L | BN |
| ④ | SEDIMENTATION BASIN | $16.0 \times 3.0 \times 3$ | D | BN |
| ⑤ | DISINFECTION TANK | $1.5 \times 4.0 \times 1.5 \times 1$ | L | BN |
| ⑥ | RETURN SLUDGE PUMP ROOM | | | |
| ⑦ | SLUDGE THICKENING TANK | $5.0 \times 4.0 \times 2$ | D | BN |
| ⑧ | AEROBIC SLUDGE DIGESTION TANK | $13.0 \times 4.0 \times 1$ | D | BN |
| ⑨ | OFFICE | | | |



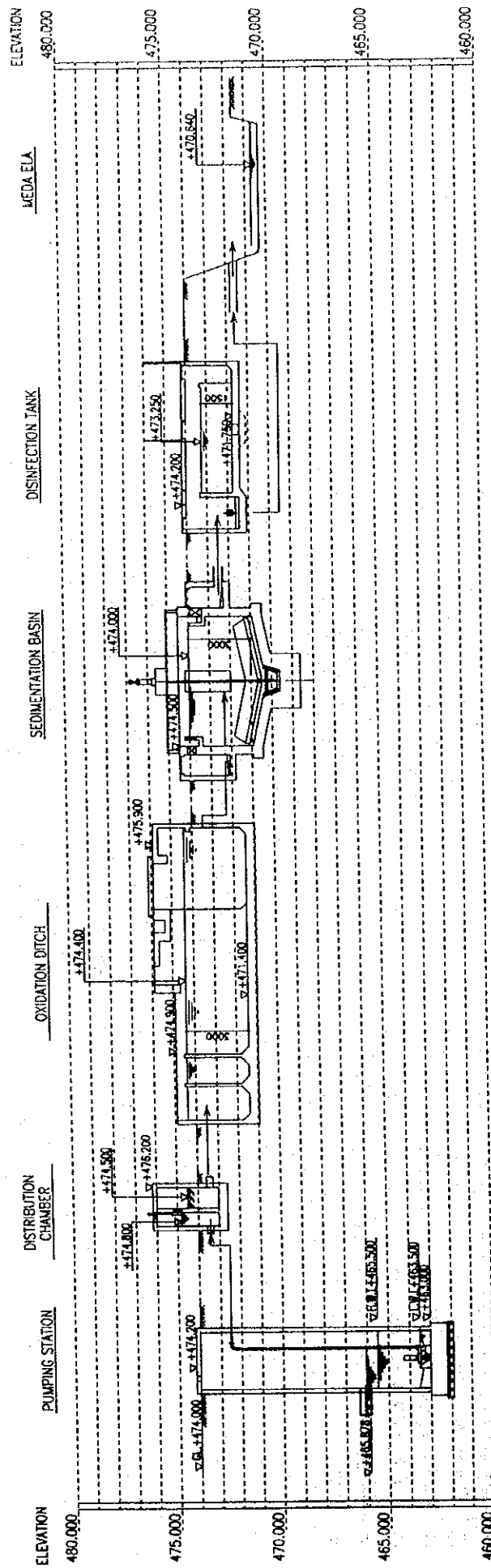
From Kandy

$$S=1/1000$$


S.2-1 SLUDGE DRYING BED LAYOUT

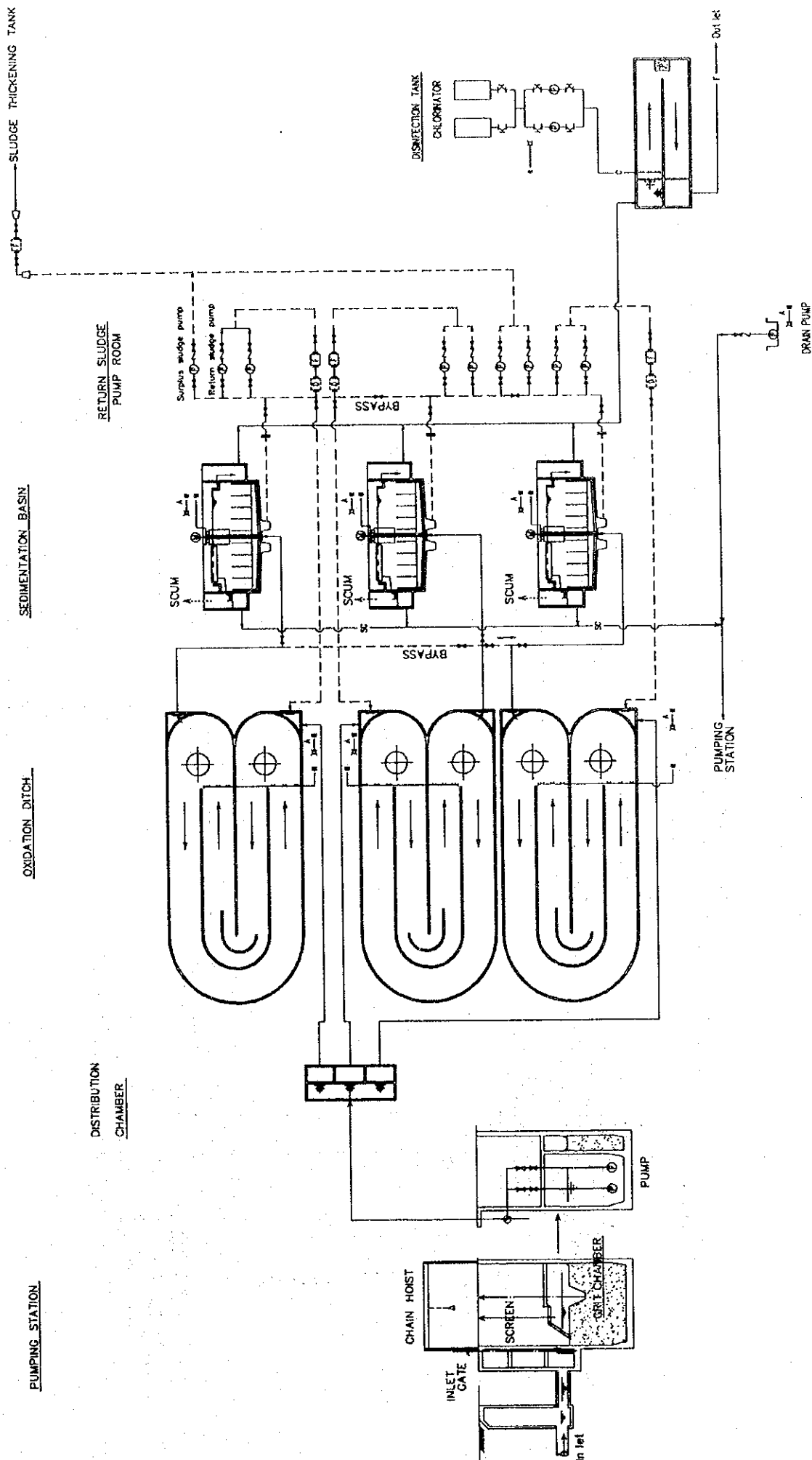
PROPOSED SEWERAGE TREATMENT PLANT
SITE SURVEY AT BOWALA

HYDRAULIC PROFILE



S2-2
HYDRAULIC PROFILE

FLOW DIAGRAM (1)



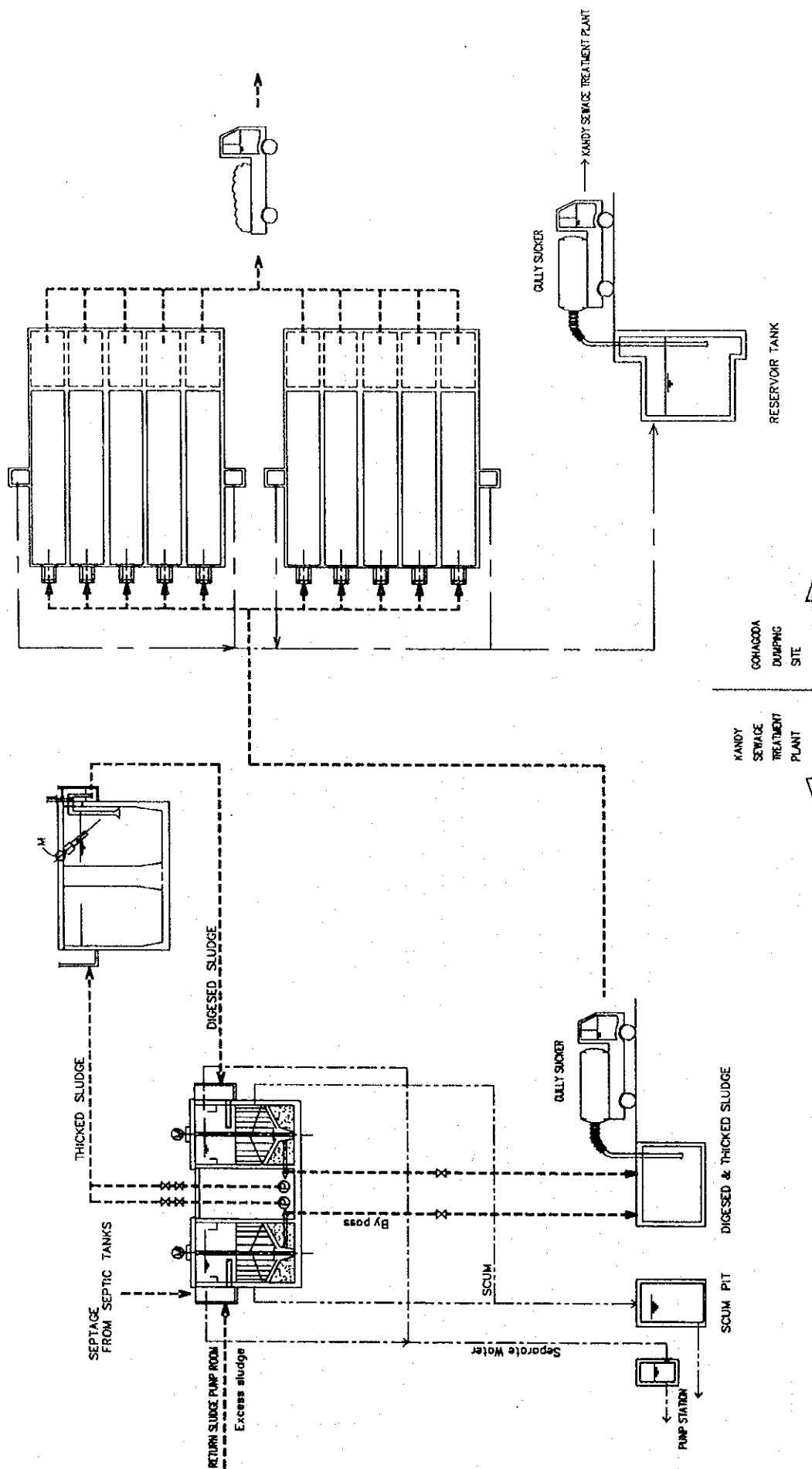
S.2-3
FLOW DIAGRAM (1)

FLOW DIAGRAM(2)

SLUDGE THICKENING TANK

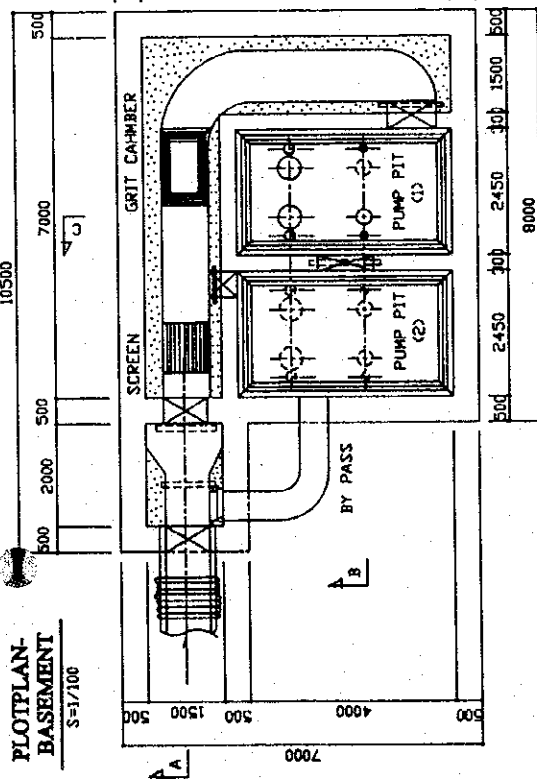
AEROBIC SLUDGE DIGESTION TANK

SLUDGE DRYING BED

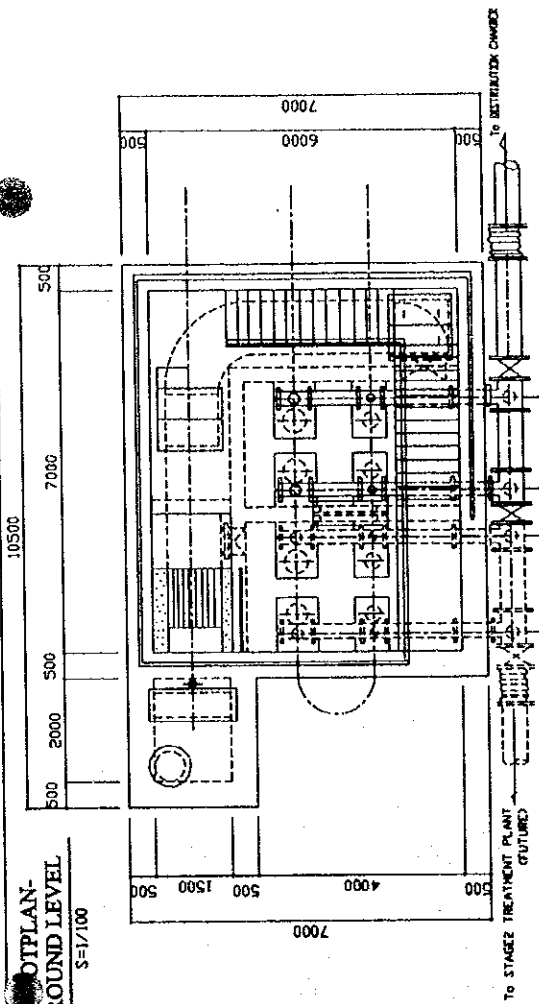


S.2-4
FLOW DIAGRAM (2)

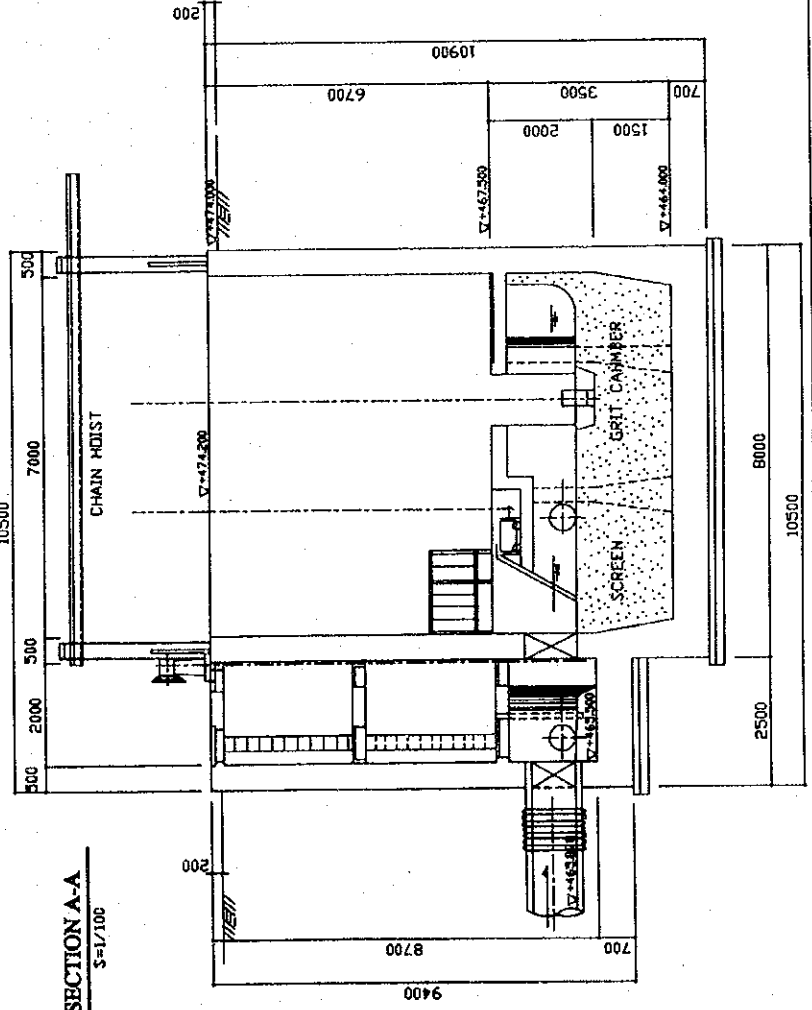
**PLOT PLAN -
BASEMENT**
S=1/100



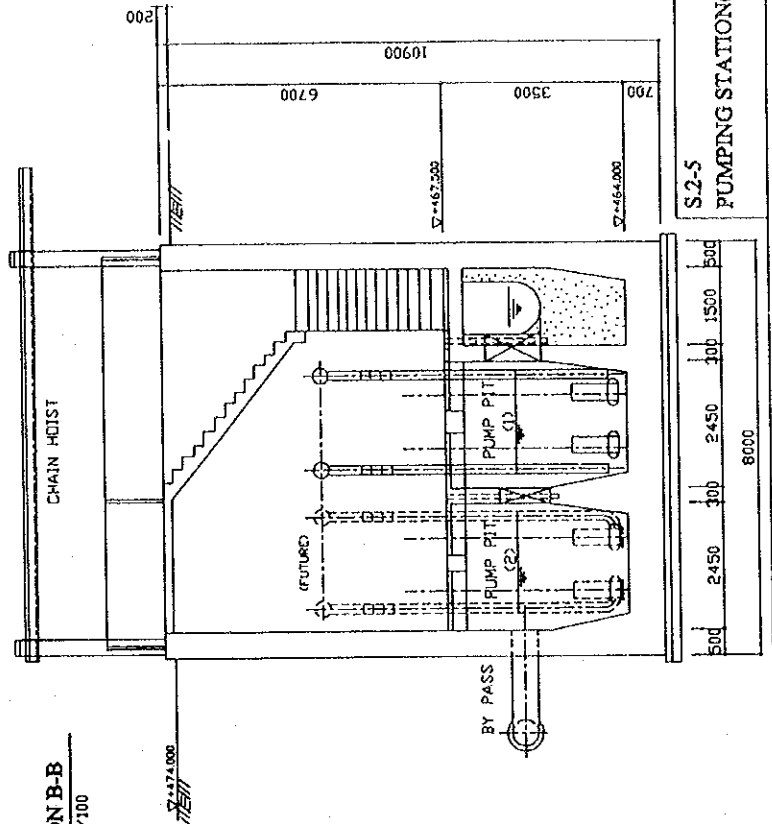
**PLOT PLAN -
GROUND LEVEL**
S=1/100



SECTION A-A
S=1/100



SECTION B-B
S=1/100

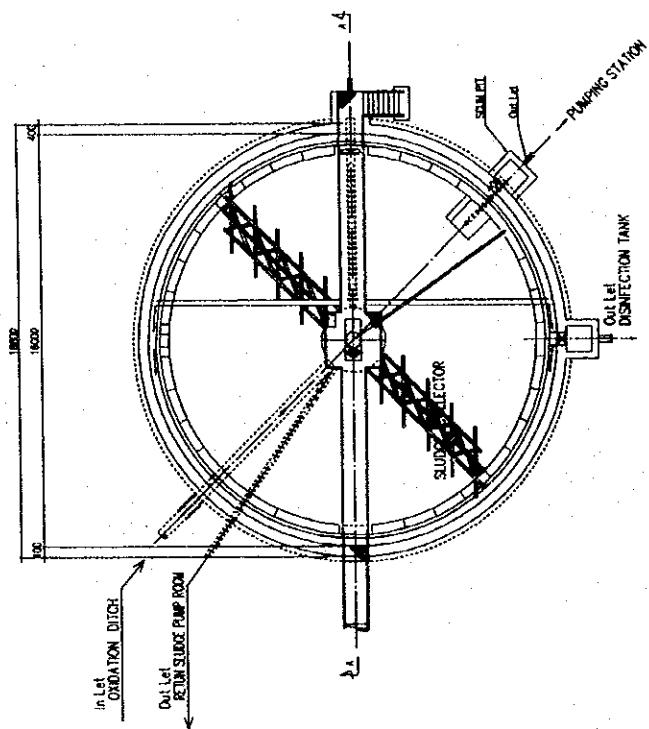


**S.2-5
PUMPING STATION(1)**

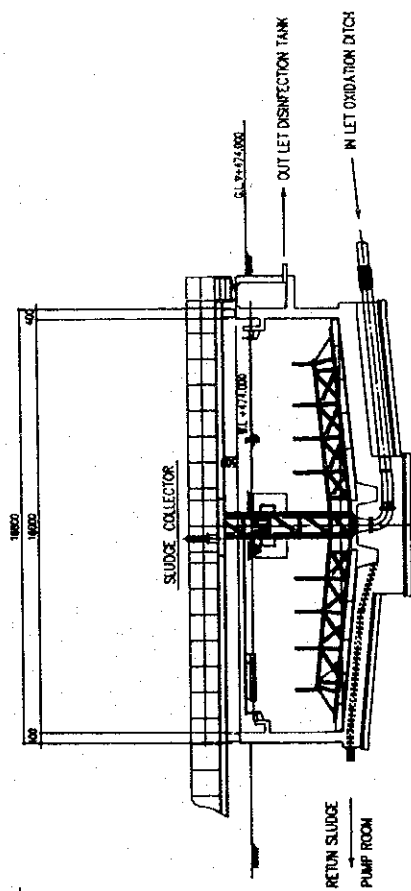


SEDIMENTATION BASIN

PLAN
S=1/200

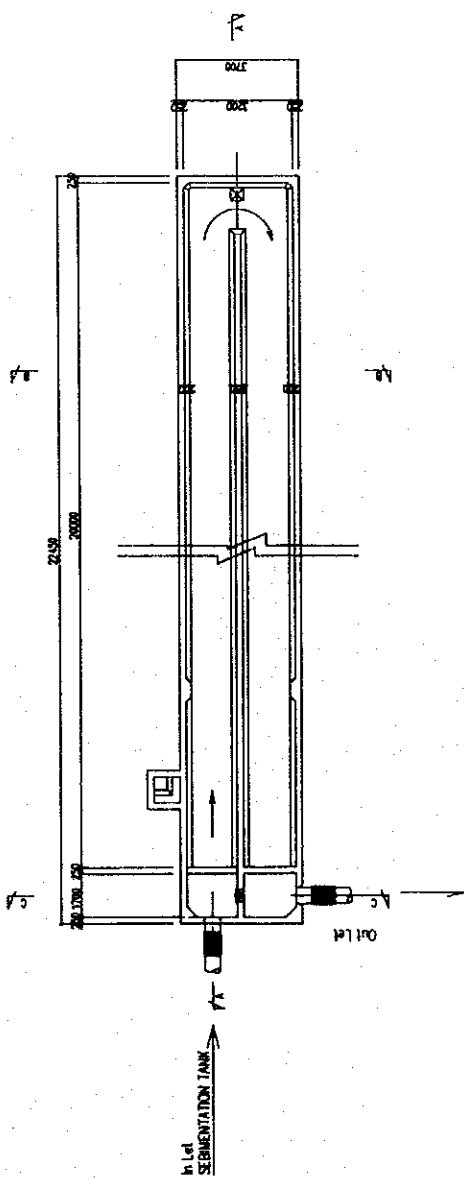


SECTION A-A
S=1/200

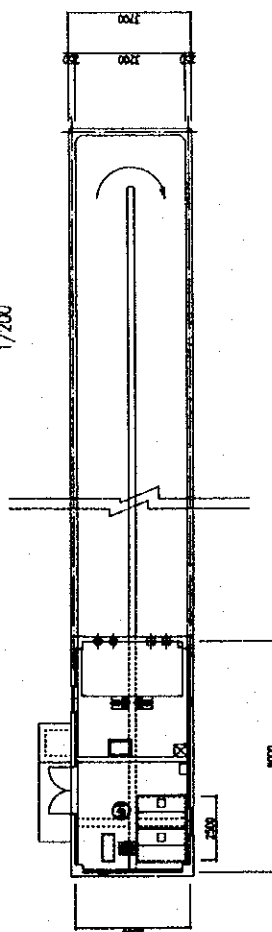


S2-8
SEDIMENTATION BASIN

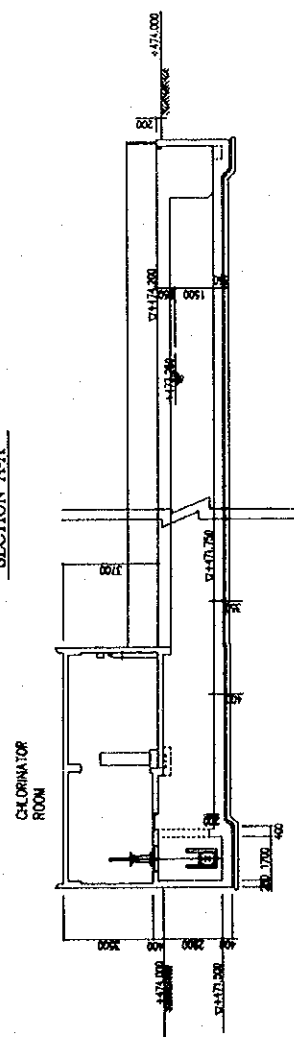
PLOT PLAN BASEMENT 1/200



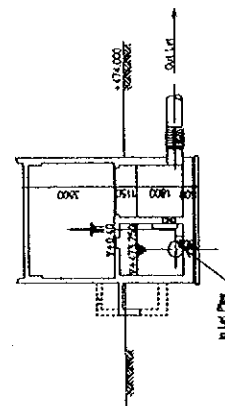
PLOT PLAN GROUND LEVEL 1/200



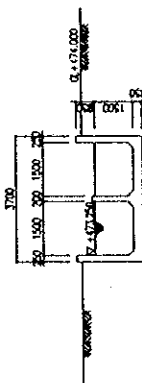
SECTION A-A



SECTION C-C

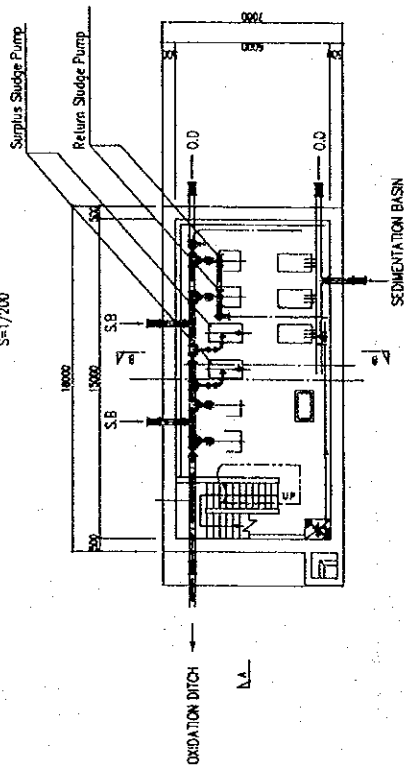


SECTION B-B

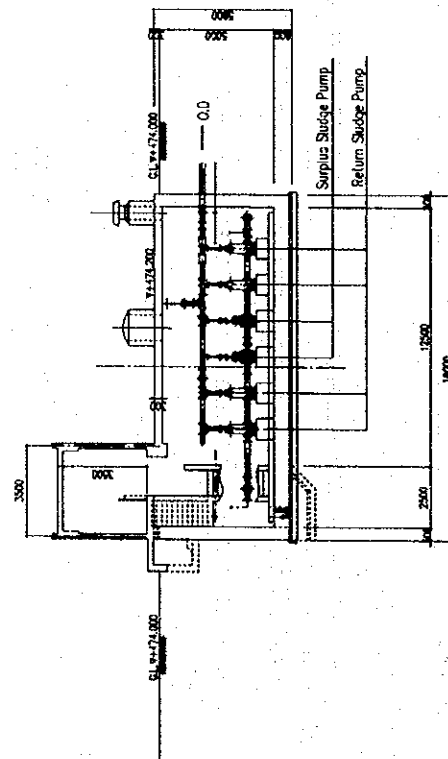


RETURN SLUDGE PUMP ROOM

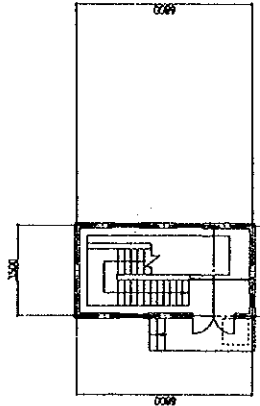
PLOT PLAN BASEMENT
S=1/200



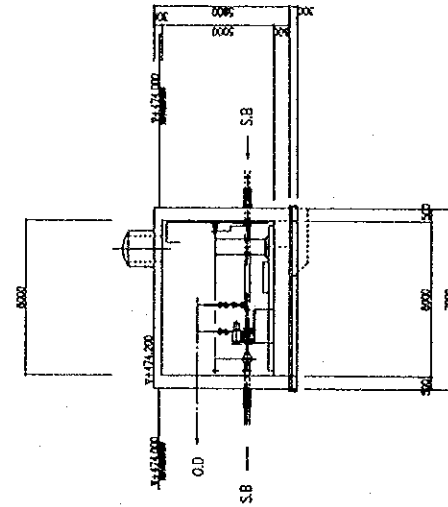
SECTION A-A
S=1/200



PLOT PLAN GROUND LEVEL
S=1/200



SECTION B-B
S=1/200



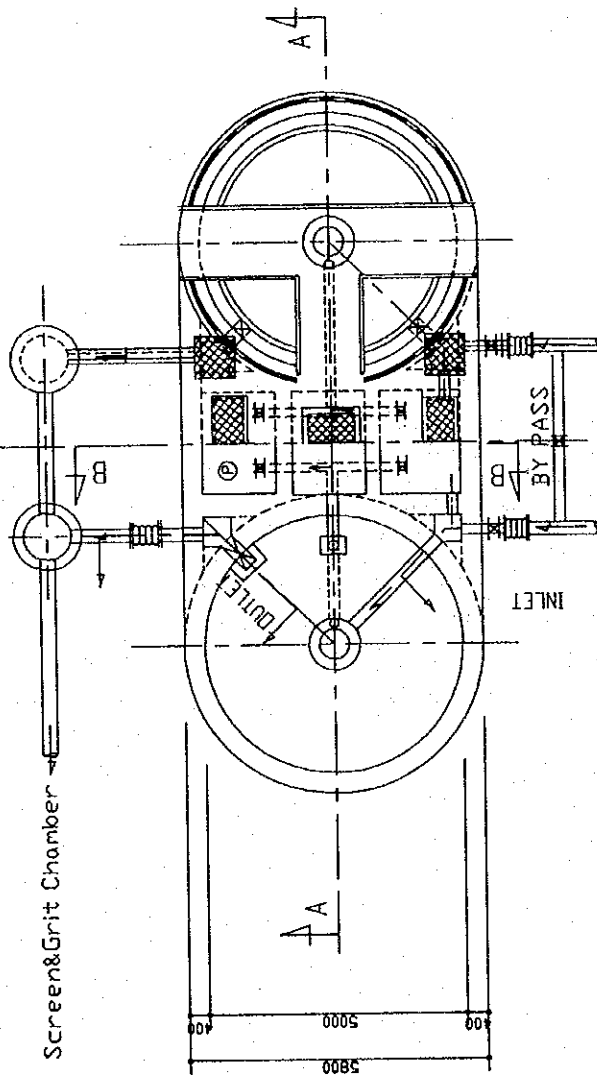
S.2-10
RETURN SLUDGE PUMP ROOM

PLOT PLAN

AEROBIC SLUDGE DIGESTION TANK

SLUDGE THICKENING TANK

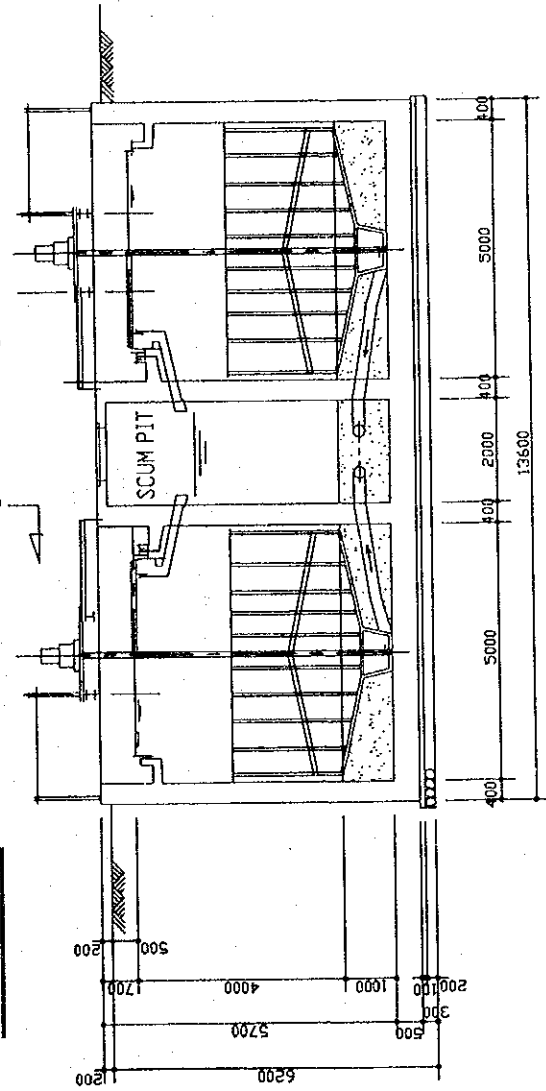
BASEMENT GROUND LEVEL



SECTION A-A

Excess Sludge

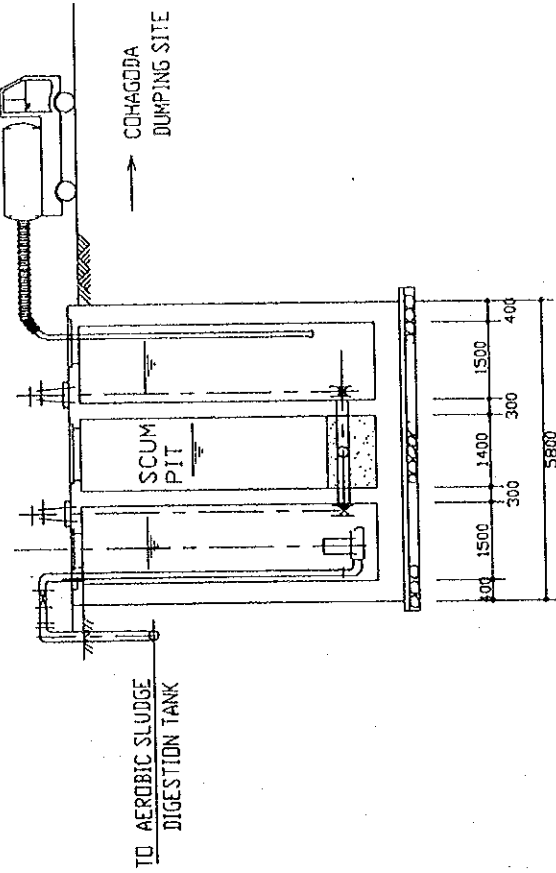
Digested Sludge



SECTION B-B

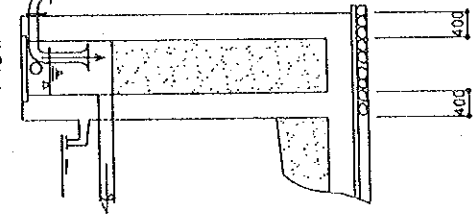
Excess Sludge

Digested Sludge

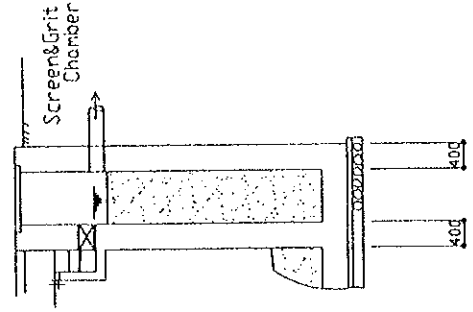


INLET

Over Flow



OUTLET

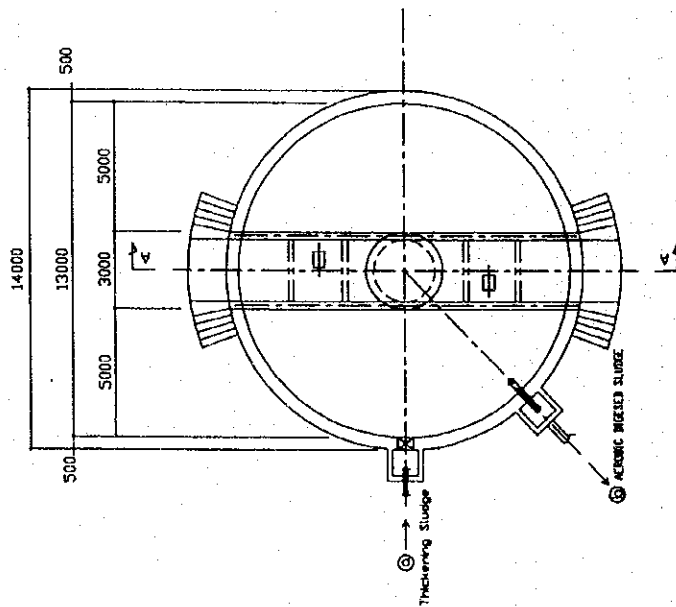


S.2-11

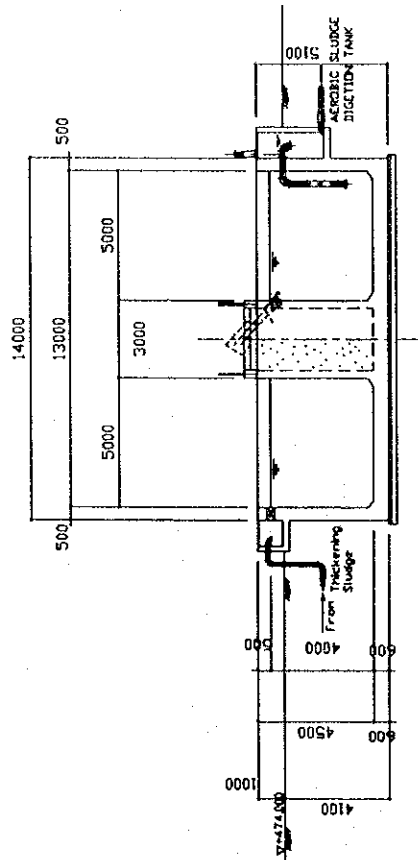
SLUDGE THICKENING TANK

AEROBIC SLUDGE DIGESTION TANK

PLOTPLAN S=1/200

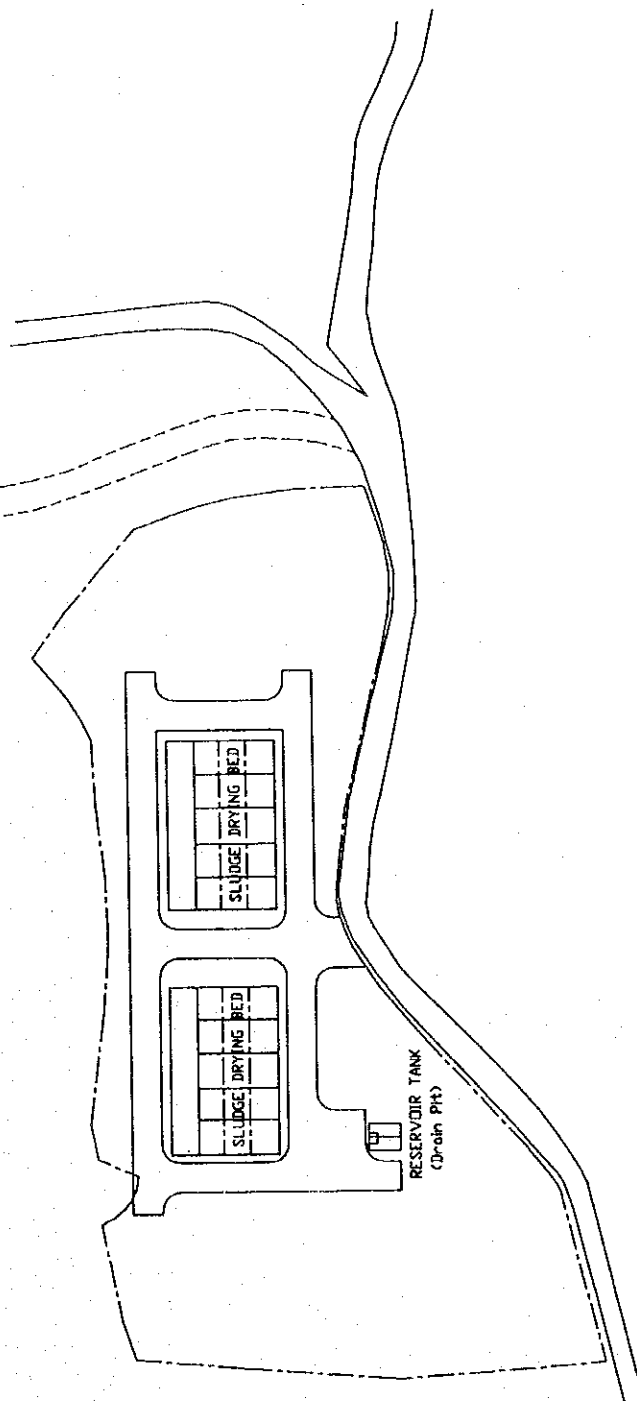


SECTION A-A S=1/200



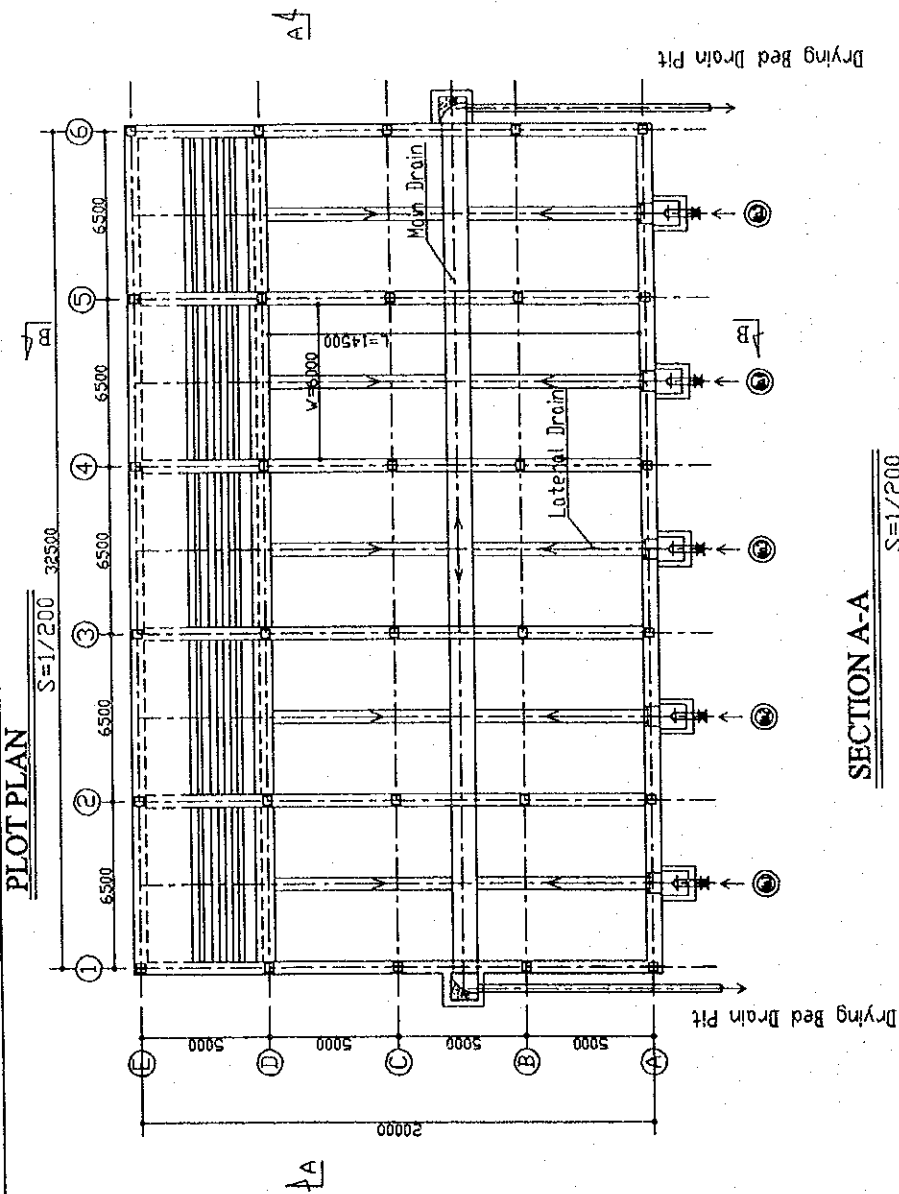
S.2-12
AEROBIC SLUDGE DIGESTION TANK

SLUDGE DRYING BED LAYOUT
(GOHAGODA DUMPING SITE)

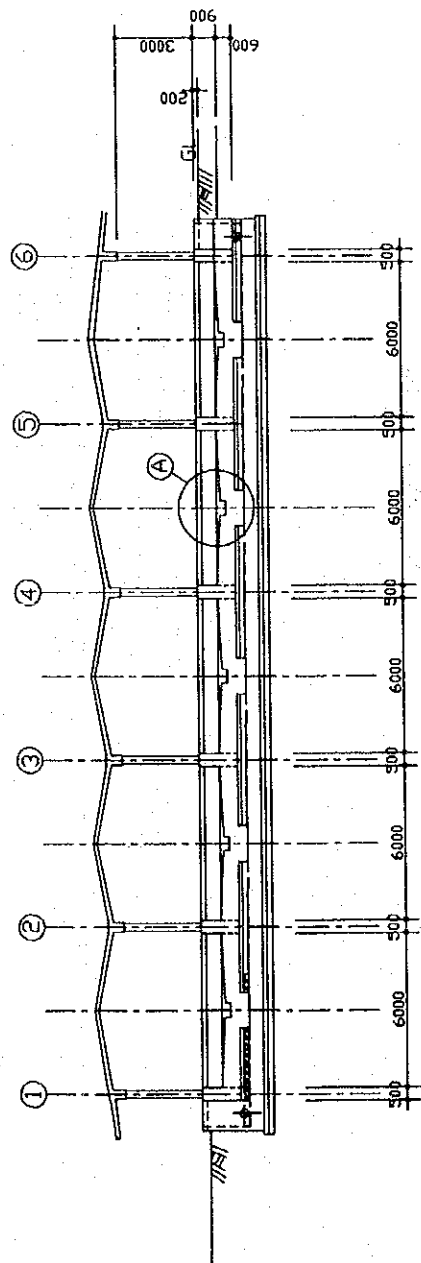


S=1/1000

PLOT PLAN

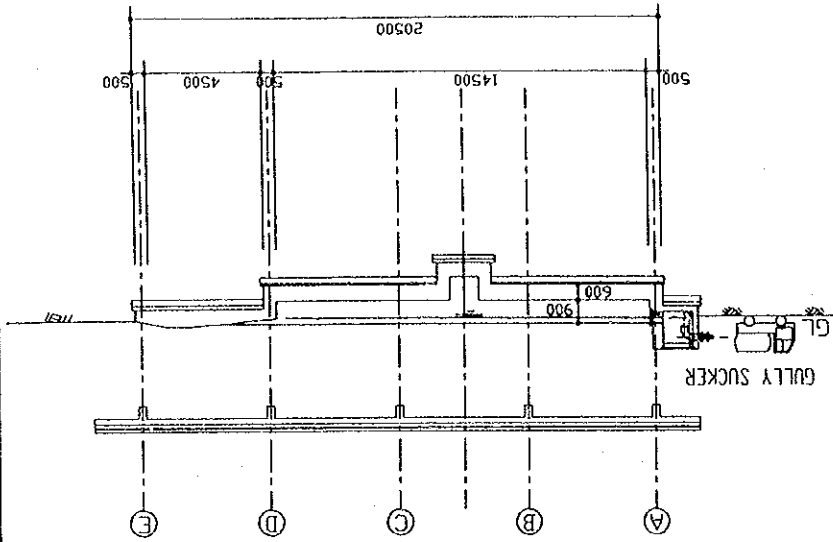


SECTION A-A

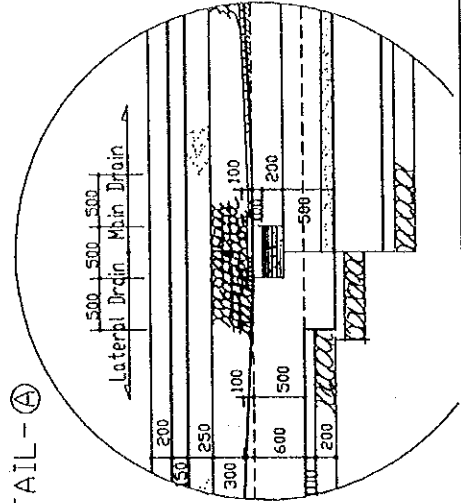


SECTION B-B

$S=1/200$



DETAIL - A



S2-14
SLUDGE DRYING BED

Appendix 13.7 Storage Capacity of Sewer (Kandy)

Phase 1 (2005)

1 Pumping Station in Kandy STP

(1) Sewage Flow

$$Q_{HM} = 12,200 \text{ m}^3/\text{day} = 508 \text{ m}^3/\text{hour} \text{ (Hourly Maximum Sewage Flow to STP)}$$

(2) Sewer to be used for Sewage

Since Pumping Station is located at GL+474m, sewers with invert level of +473m is considered to use for sewer storage. Length and Pipe Nos. of these sewers are as follows;

$$\text{No. 57 } \phi 825, L = 50\text{m} \quad (\text{Allowance } 50\%)$$

$$\text{No. 53 } \phi 750, L = 750\text{m} \quad (\text{Allowance } 50\%)$$

(3) Manhole

$$\text{Nos. of Manhole} \quad \frac{50+750}{50} = 16 \quad (50\text{m pitch})$$

$$\text{Manhole Depth} \quad 475.01 - 470.817 = 4.2\text{m} \\ (\text{up to No.53})$$

(4) Calculation of Storage Capacity

a) Sewer

$$\left[\frac{0.825^2 \times 3.14}{4} \times 50 + \frac{0.75^2 \times 3.14}{4} \times 750 \right] \times \left(1 - \frac{1}{1.5}\right) = 119.3 \text{ m}^3$$

b) Manhole

$$\frac{1.2^2 \times 3.14}{4} \times (4.2 - 0.825) \times 16 \quad = 61.0\text{m}^3$$

$$\text{Total} \quad 180.3\text{m}^3$$

(5) Storage Time

$$\frac{180.3\text{m}^3}{508\text{m}^3/\text{hour}} = 0.35 \text{ hour} = 20.9 \text{ min}$$

2. Kandy Lake Pumping Station

(1) Sewage Flow

$$Q_{HM} = 0.0031 \text{ m}^3/\text{sec} = 11.16 \text{ m}^3/\text{hour}$$

(Hourly Maximum Sewage Flow to Kandy Lake PS)

(2) Sewer to be used for Sewage

Since Pumping Station is located at GL+512.87m, sewers with invert level of +512.5m is considered to use for sewer storage. Length and Pipe Nos. of these sewers are as follows;

$$\text{No.32. } \phi 150 \quad L = 750\text{m} \text{ (Allowance } 50\%)$$

(3) Manhole

$$\text{Nos. of Manhole} \quad \frac{750}{50} = 15 \quad (50\text{m pitch})$$

$$\text{Manhole Depth} \quad 512.17 - 510.351 = 1.8$$

(Center of No. 32)

(4) Calculation of Storage Capacity

a) Sewer

$$\frac{0.15^2 \times 3.14}{4} \times 750 \times \left(1 - \frac{1}{2.0}\right) = 6.6\text{m}^3$$

b) Manhole

$$\frac{0.9^2 \times 3.14}{4} \times (1.8 \times 0.15) \times 15 = 15.7\text{m}^3$$

$$\text{Total} \quad 22.3\text{m}^3$$

(5) Storage Time

$$\frac{22.3 \text{ m}^3}{11.16 \text{ m}^3/\text{hour}} = 2.0 \text{ hour} = \underline{120.0 \text{ min}}$$