		DAILY	MATER RESERVOIR RESERVOIR	ATER MA VOIR AN	MANAGEMENT AND FOWER B	1 00 ²¹ 111	17AR OPE	IAT RATION LLA	RECORDS	က်
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PEAR : 1993 MONTH:GEPTEMBER FAIL D/S FAIL D/S FAIL D/S FAIL D/S FAIL DAY	MATER MANAGEMENT SECRETARIAT DAILY RESERVOIR SCHEME NAME : FOLGOLLA	DAILY	WATER MAI RESERVOIR ANI RESERVOIR SCI
DATE NO DIVER ENER AVIL D/S RAIN (GCM) (MCM) (GUH) (MM) (MCM) (GCM) (MCM) (GHN) (MM) (MCM) (GCM) (MCM) (GHN) (MM) (MCM) (A 2007 4.933 0.875 38.0 0.1 0.3 SAT 2 3 5.127 4.992 0.902 38.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	1993	i	199
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	YEAR	1993		MONTH: OCTO	ρq	EX		
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WATER MANAGEMENT SECRETARIAT DAILY RESERVOIR AND POWER PLANT OPERATION RECORDS RESERVOIR SCHEME NAME: "POLGOLLA YEAR : 1992	DAY DATE IN DIVER ENER AVIL D/S RAIN FLOW -SION -GY -ABLE RELE FALL CAPAASE (ACM) (MW) (MCM) (MM) (MM)	4,895 0.91 37.0 4.4 P 4,898 0.899 37.0 5.8 4,896 0.907 37.0 5.8	4 5.622 4.894 0.869 37.0 1.0 3 5.675 4.147 0.762 37.0 1.4 8 7.769 4.895 0.903 37.0 0.8 2	7 7.062 4.894 0.895 37.0 1.9 20. 8 18.14 4.895 0.902 37.0 13.0 9. 9 15.51 4.894 0.889 37.0 10.8 2.	10 16.08 4.895 0.891 37.0 11.0 11 15.14 4.607 0.848 37.0 11.7 12 18.33 3.371 0.654 37.0 15.0	14 21.38 4.253 0.773 37.0 17.1 0 15 14.06 4.894 0.902 37.0 9.4 0 16 11.08 4.894 0.891 37.0 6.3 0 17 9.394 4.895 0.905 37.0 4.5 0	8 8.88 4.894 0.887 37.0 3.9 0 0 7.724 4.764 0.87 37.0 3.1 0 0.5.748 4.894 0.892 37.0 1.1 0.1 0.1 5.812 4.546 0.837 37.0 1.1 0	23 5.876 4.894 0.904 37.0 1. 23 5.631 4.896 0.897 37.0 0. 24 4.91 4.8 0.9 37.0 0.	26 5.681 4.894 0.888 37.0 0.3 0 87.7 7.042 4.334 0.794 37.0 0.3 0 88 6.0694 37.0 1.8 0 88 6.004 37.0 1.8 0 88 6.004 37.0 1.0	30 5.707 4.896 0.885 37.0 0.8 2 31 5.121 4.219 0.888 37.0 0.6 1	Totals 303,3 144,8 26.75 155-0 140.
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YEAR : 1992 MÜNTH:DECEMBER DAY DATE IN DIVER ENER AVIL D/S RAIN (mcm) (mcm) - GNA - GNA - ABLE RELE FALL CREAT - GNA - GNA - GNA - GNA - GNA TUE		DAILY	WATE RESERVO RESERVO	# # # E	MANAGEMENT AND POWER P SCHEME NAME	NT SECRE	KETARIAT IT OPERAT POLGOLLA	ы "	an 'RÉCORDS	ro
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	YEAR	1991		MONTH	MONTH:DECEMBER	<u>а</u>		!
	D.≱.	DATE	IN FLOW	DIVER- SION	ENER -67	AVIL -ABLE	D/S RELE	RAIN FALL
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Appendix5.4 Recommended Peak Factor

1.1 Establishment of Load Factor to Estimate Daily Maximum Water Demand

Capacity of transmission line and distribution reservoir shall be determined based on the daily maximum water demand. In this study, the daily maximum water demand was estimated due to absence of past performance record/data.

In setting up of load factor (= daily average water demand/daily maximum water demand), actual performance data by size of water supply system in Japan was referred to. However, if UFW occupies considerable part of supply amount, the Japanese data may not be applied directly, while the effective supply amount basis (excluding UFW) of Japanese data may be applied similarly this study, since tendency of water consumption is deemed to be mostly similar in every country.

In this section, load factor was studied based on the following formula in application of some modification taking into account difference of UFW ratio.

Supply amount may be categorized as shown in the following figure and various coefficients are given by following formula. In the figure, most of non effective supply amount is deemed to be leakage and is assumed to be equal in both daily average supply amount and daily maximum supply amount.

Load factor R1 = A/B (Load factor is generally defined by this formula)	(1)
Effective ratio R2 = C/A	(2)
Non effective ratio $R3 = D/A = (1 - C/A) \dots \dots$	(3)
Daily average supply amount $A = C + D = C + A*R3 \dots \dots \dots \dots \dots \dots \dots \dots$	(4)
Daily maximum supply amount $B = E + F = E + A*R3 \dots \dots \dots \dots \dots \dots \dots$	(5)
Daily average effective supply amount $C = A - D = A - A*R3 = (1 - R3)*A \dots$	(6

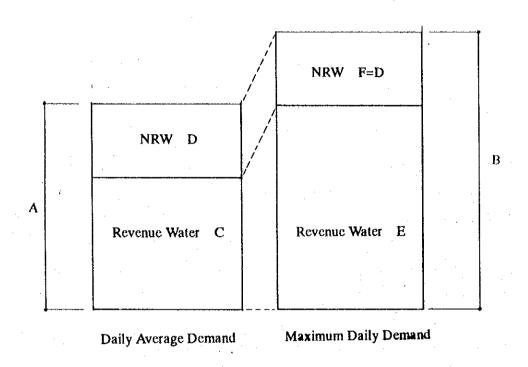


Figure 5.4.1 Supply Amount of Revenue Water and Non Revenue Water

Based on the above, modified load factor (R) can be expressed with R1 and R3 as follows:

Modified load factor
$$R = C/(C + A*R3/R1 - A*R2 = R1*(1 - R3)/(1 - R1*R3)$$
 (8)

Load factor (R1) can be expressed with R and R3 as follows:

Load factor R1 = A/B =
$$(C + A*R3)/(C/R + A*R3) = R/(1-(1-R)*R3)$$
 (9)

Now, load factors R1 and effective ratio R1 (or non effective ratio) are known figures by size of water supply system based on the Water Supply Statistics of Japan, the modified load factor (R) can be estimated as follows.

Table 5.4.1 Past Performance Data of Load Factor and Effective Ratio in Japan

Served Population	Load Factor	Effective Ratio
(person)	(%)	(%)
500,000~1,000,000	82.5	94.0
50,000~100,000	79.6	90.3
30,000~50,000	78.1	87.5

Note: Water Supply Statistics of Japan, 1993

Load factor in Nuwara Eliya is estimated referring to the above table as follows:

Modified load factor
$$R = (0.796 \times (1 - 0.097)/(1 - 0.796 \times 0.097) = 0.779$$

Load factor $R1 = 0.779/(1 - (1 - 0.779) \times 0.25) = 0.825$

Coefficient to estimate the daily maximum supply amount is given as a reciprocal number of the load factor:

$$1/R1 = 1.21$$
 say 1.2

When load factor of Greater Kandy is estimated in the same manner:

Modified load factor
$$R = (0.825 \times (1 - 0.060)/(1 - 0.825 \times 0.060) = 0.816$$

Load factor $R1 = 0.816/(1 - (1 - 0.816) \times 0.25) = 0.855$

Coefficient of the daily maximum supply amount is:

$$1/R1 = 1.17$$
 say 1.2

1.2 Peak Factor

Capacity of distribution lines is to be determined based on the hourly maximum water demand or peak factor. However, the hourly maximum water demand or peak factor shall be estimated due to absence of past performance record/data in Nuwara Eliya as described in the previous section, Load Factor.

Peak factor (= hourly maximum supply amount/daily maximum supply amount) is likewise determined referring to the Japanese past performance data. It shall be noted that hourly fluctuation coefficient in Japan and peak factor in the study area are given different definitions, as follows:

Hourly fluctuation coefficient in Japan:

K = (hourly maximum supply amount)/(daily maximum supply amount)

Peak factor in the study area:

Peak factor = (hourly maximum supply amount)/(daily average supply amount)

Based on the above-mentioned difference of definition, peak factor in the study area shall be determined in application of load factor of daily maximum supply amount to the hourly fluctuation coefficient as follows:

Peak factor in the study area

= (Hourly fluctuation coefficient in Japan; K) x (Load factor of daily maximum supply amount)

The hourly fluctuation coefficient in Japan is shown in the following figure.

Since Nuwara Eliya has daily maximum supply amount of about 10,000 cu.m/day, the hourly fluctuation coefficient (K) in Japan is considered to be 1.78, while load factor of daily maximum supply amount is estimated at 1.2. Thus, peak factor in the study area is estimated as follows:

Peak factor in study area = $1.78 \times 1.2 = 2.1$ say 2.0

In ADB D/R/D page 7 (Feb. 1998), peak factor is defined at 2.0.

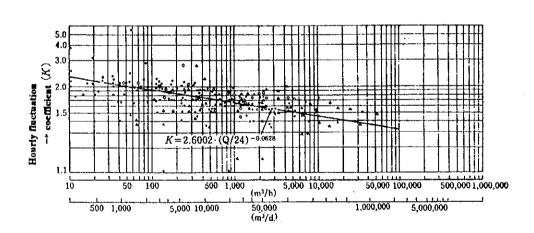


Figure 5.4.2 Relationship between Distributed Volume and Hourly Fluctuation Coefficient

Appendix 5.5 Specification for Potable Water, SLS 614 (1983)

art 1 - Physical and Chemical Requirer Characteristics	Max. Desirable Level	Max. Permissible Leve
PH	7.0-8.5 units	6.5-9.0 units
Colour	5 units	30 units
Odour	Unobjectionable	Unobjectionable
Taste	"	"
Turbidity	2-JTU	8-JTU
Elect. Conductivity	750 µS/cm	3,500 μS/cm
Chloride (Cl)	200 mg/l	1,200 mg/l
Chlorine - Free Residual (Cl)	••	0.2 "
Alkalinity (as CaCO ₃)	200 mg/l	400 "
Ammonia-Free	•	0.06 "
Ammonia-Albuminoid	_	0.15 "
Nitrate (as N)	-	10
Nitrite (as N)	-	0.01 "
Fluoride (as F)	0.6 mg/l	1.5 "
Phosphates - Total (PO)	_	2.0 "
Total Solids	500 mg/l	2,000 "
Hardness Total (as CaCO ₃)	250 "	600 "
Iron-Total (as Fe)	0.3 "	1.0 "
Sulphate	200 "	400 "
Calcium	100 "	240 "
Magnesium	30 to 150 *	150 "
Copper	0.05 mg/l	1.5 "
Manganese	0.05 "	0.5 "
Zinc	5.0 "	15.0 "
Aluminium	-	0.2 "
Arsenic		0.05 "
Cadmium	-	0.005 "
Cyanide	-	0.05 "
Lead	-	0.05 "
Mercury	-	0.001 "
Selenium	-	0.01 "
Chromium	-	0.05 "
Anionic Detergents (as MBAS-LAS)	0.2 "	1.0 "
Phenolic Compounds (as Phenolic OH)	0.001 "	0.002 "
Oil & Grease	-	1.0 "
Pesticide Residue	(Refer to WHO &	& FAO requirements)
Chemical Oxygen Demand (COD)		10 mg/l

^{*} Depending on Sulphate content, i.e. for 205 mg/l Sulphate, max. Mg is 30 mg/l; for less sulphate, more Mg is allowed.

Appendix 5.5 Specification for Potable Water, SLS 614 (1983)

Part 2 - Bacteriological Requirements

Requirements

- 1. Pipe born water supplies:
- Throughout any year, 95 percent of the samples shall not contain any coliform organisms in 100 ml.
- None of the samples examined shall contain more than 10 coliform organisms per 100 ml.
- Coliform organisms shall not detectable in 100 ml of any two consecutive samples.
- None of the samples examined shall contain E. Coli. in 100 mg/l I (Fecal coliform)
- 2. Individual and small community supplies
- None of the samples examined shall contain more than 20 coliform organisms per 100 mg/l on repeated examination.
- No sample shall contain E. Coliform in 100 mg/l (Fecal coliform)

Note: Individual or small community supplies include wells, bores and springs