# Appendix 12.4.2 Sewage Treatment Plant - Capacity Calculation CAPACITY CALCULATION OF FACILITIES Alternative 2 - Nuwara Eliya (Aerated Lagoon)

#### **1** BASIC CONDITIONS

#### 1-1 BASIC ITEMS

(1) Name : Nuwara Eliya Sewage Treatment Plant

(2) Land Area :	Approximately	2.00 ha
(3) Elevation :	1855.000	m
(4) Inlet Pipe Level :	1854.850	m
(5) Pipe Diameter :	400	m
(6) Land Use :	Tea Plantation	
(7) Collection System :	Seperate Type	
(8) Treatment Method :	-	ent : Aerated Lagoon Method nt : Pond Accumulation
(9) Effluent Point :	Nanu Oya	
(10) Effluent Point Water Le	evel :	1852.000 m
(11) Target Year :	Year 2000 (Pha	se 1)

(12) Lowest Monthly Average Temperature

15 °C (January)

#### 1-2 Design Population

Design Population : 1,830 Pe

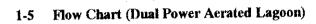
1,830 Persons (Total)

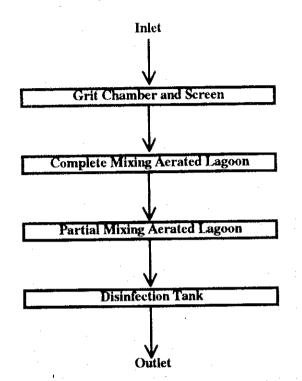
#### 1-3 Design Sewage Flow

ITEM	m3/day	m3/hr	m3/min	m3/sec
Daily Average	1,200	50.0	0.83	0.014
Daily Maximum	1,250	52.1	0.87	0.014
Hourly Maximum	2;400	100.0	1.67	0.028

#### 1-4 Design Sewage Quality

ITEM	INFLUENT	EFFLUENT	REMOVAL	REMARKS
	(mg/L)	(mg/L)	RATIO (%)	
BOD	240	30	88	
SS	250	50	80	





ITEMS	UNIT	Formula or Value	Application
1-6-1 Grit Chamber			
(1) Water Surface Load	m3/m2/day	> 1800	1,800
(2) Average Velocity	m/sec	> 0.3	0.3
1-6-2 Complete Mixing Aerated Lagoon			
(1) Retention Time	day	1.5 - 2.5	1.50
(2) Water Depth	m	3.0 - 4.0	3.0
(3) Power Requirement for Mixing	W/m3	> 6.0	6.0
1-6-3 Partial Mixing Aerated Lagoon			
(1) Retention Time	day	2.0	2.0
(2) Water Depth	m	2.0 - 4.0	3.0
(3) Power Requirement for Mixing	W/m3	> 1.0	1.0
(4) Number of Cell	Cell/Basin	1-3	3
1-6-4 Storm Water Settling Tank			
(1) Water Depth	m	1.5 - 3.0	1.5
(2) Retention Time (Hourly Max Rain)	hour	> 0.5	, 0.5
(3) Water Surface Load (Hourly Max Rain)	m3/m2/day	75 - 150	150.0
1-6-5 Disinfection Tank			
(1) Retention Time	min.	> 15	15.0
(2) Dosage	mg/l	2.0 - 4.0	3.0

#### 1-6 Design Criteria for Dual Power Aerated Lagoon

# 2 CAPACITY CALCULATION

# 2-1 Grit Chamber and Screen (Hourly Maximum)

ITEM	SIGN	UNIT	CALCULATION	RESULT
Туре	- -	-	Parallel Flow Type	
Design Flow	Q1	m3/day		2,400
	Q2	m3/sec		0.028
Water Surface Load	WSL	m3/m2/day	_	1,800
Required Surface Area	RSA	m2	Q1/WSL	1.333
Basin Number (Total)	BN	basin	-	
Basin Number (Stand-By)	BNS	basin	-	
Average Velocity	V	m/sec	-	0.30
Depth	Н	m	-	0.30
Width	W1	m	Q2/(V*H)	0.309
Therefore	W2	m	-	0.50
Length	L1	m	RSA/W2/(BN-BNS)	1.333
Therefore	L2	m	_	1.40
Dimension (W)	W	m	W2	0.50
(Ľ)	L	m	1.2	1.40
(Basin)		basin	BN	2
(Stand-By)	_	stand-by	BNS	1
Screen Type	14	- <u>/</u>	Fine Bar Screen	
Screen Set Number	SSN	set	BN	3
Check		UNIT	APPLICATION	RESULT
Water Surface Load	[	m3/m2/day	> 1800	1,714
Average Velocity		m/sec	> 0.3	0.09

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ITEM	SIGN	UNIT	CALCULATION	RESULT
Туре	-	-	Rectangular Type	
Design Flow	Q1	m3/day	-	1,250
	Q2	m3/hr	-	52.08
Retention Time	T1	day	-	1.50
Inlet BOD Quality	So	mg/L		240
Required Volume	<b>V</b> 1	m3/basin	Q1*T	1,875
Basin Number	BN	basin		4
Required Volume per Basin	VBN	m3/basin	Q1*T/BN	469
Water Depth	Н	m	-	3.00
Required Surface Area	А	m2	V/H	156
Width	W	m	-	14.00
Length	L1	m	A/W	11.161
Therefore	L2	m		12.00
Oxygen Demand Rate	PR1	kg/h	(4.16*10^-5)*r*Q1*So	19
-max. oxygen uptake	ĩ	W/m3	-	1.5
Aeration Unit Power Rate	PRO	kg/h	1000*PR1/(N*Q1*T1)	5.25
Therefore	PRO	W/m3	-	
-aeration performance	N	W/m3	-	1.9
Power Requirement	P1 .	kW	-	12.0
1) Oxygen Requirement	P10	kW	PR1/N	9.9
2) Mixing Power	P1M	kW	V1*P0*10^-3	11.3
Dimension (Width)	W	m	W	14.00
(Length)	: L	m	1.2	12.00
(Depth)	Н	m	H	3.00
(Basin)	-	basin	BN	4
Aerator Type	-	-	Slanting Shaft Screw Aerator	
Check		UNIT	APPLICATION	RESULT
Retention Time		day	1.5 - 2.5	1.61

# 2-2 Complete Mixing Aerated Lagoon (Daily Maximum)

ITEM	SIGN	UNIT	CALCULATION	RESULT
Туре	-	-	Rectangular Type	
Design Flow	Q1	m3/day		1,250
	Q2	m3/hr	PA	52.08
Retention Time	T2	day		2.00
Required Volume	V2	m3/basin	Q2*T	2,500
Basin Number	BN	basin		4
Cells Number	CN	cell/basin	-	3
Stand-by Cell Number	CNS	basin	-	1
Sludge Accumulation	SA	m3/year	365*Q1*Xi/(x*10^6)	627
-inert solid concentration	Xi	mg/l		
-weight fraction of solids	x	-	-	0.04
No. of Cells Cleaned per Year	CNC	basin	-	2
Total Sludge Accumulation	TSA	m3	_	941
Required Volume	v	m3/cell	(Q1*T+TSA)/(BN*CN-CNS)	313
Water Depth	D	m	-	4.00
Required Surface Area	Α	m2/cell	V/H	78
Width	Ŵ	m	-	12.00
Length	L1	m	A/W	6.517
Therefore	L1	m		15.00
Power Requirement	P2	kW	· · · · · · · · · · · · · · · · · · ·	3.0
1) Mixing Power	P2M	kW	Q1*T2*CN*10^-3	2.5
Dimension (Width)	W	m	W	12.00
(Length)	L	m	L1	15.00
(Depth)	H	m	H	4.00
(Basin)	-	basin	BN	4
(Cell)	-	cell/basin	CN	
(Stand-by Cell)	-	cell	-	1
Aerator Type	-	-	Slanting Shaft Screw Aerator	
Check		UNIT	APPLICATION	RESULT
Surface Area		m2	-	2,160
Retention Time		day	2.0	5.58

# 2-3 Partial Mixing Aerated Lagoon (Daily Maximum)

ITEM		SIGN	UNIT	CALCULATION	RESULT
Chemical Type				Chlorination Type	
Design Flow		Q1	m3/day	-	1,250
		Q2	m3/min	-	0.87
Retention Time		Т	min.	-	15.0
Basin Number		BN	basin	-	1
Required Volume		V	m3	Q2*T	13
Width		W	m ·		1.00
Water Depth		H	m	-	1.00
Length		L1	m	V/(W*H)	13.021
	therefore	L2	m	-	13:00
Dosage		D	mg/L	-	3.0
Required Chemical		RC1	kg/day	Q1*D*10^-3/C	3.75
	Therefore	RC2	kg/hr	RC1/24	0.16
Dimension	(Width)	W	m	W	1.00
	(Length)	L	m	1.2	13.00
	(Depth)	H	m	Н	1.00
	(Depth)	BN	basin	•	1
Chlorine Feeder			unit	including 1 for stand-by	2
Check			UNIT	APPLICATION	RESULT
Retention Time			min.	> 15	15.0

# 2-4 Disinfection Tank (Daily Maximum)

# Appendix 12.4.3 Sewage Treatment Plant - Capacity Calculation CAPACITY CALCULATION OF FACILITIES Alternative 2 - Hospital/Brewery (Aerated Lagoon)

#### 1 BASIC CONDITIONS

#### 1-1 BASIC ITEMS

(1) Name : Nuwara Eliya Sewage Treatment Plant

(2) Land Area :	Approximately	- ha
(3) Elevation :	1861.730	m
(4) Inlet Pipe Level :	1858.882	m
(5) Pipe Diameter :	225	m
(6) Land Use :	-	
(7) Collection System :	Seperate Type	
(8) Treatment Method :		ent : Aerated Lagoon Method nt : Pond Accumulation
(9) Effluent Point :	Stream to Barra	ick Plain

- (10) Effluent Point Water Level : 1860.000 m
- (11) Target Year : Year 2015 (Phase 2)
- (12) Lowest Monthly Average Temperature 15 °C (January)

#### 1-2 Design Population

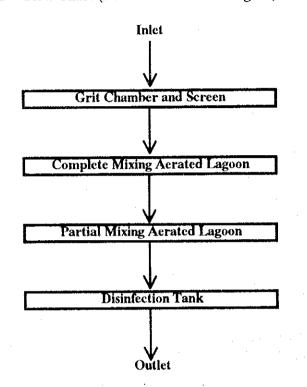
Design Population : 8,631 Persons (Total)

#### 1-3 Design Sewage Flow

ITEM	m3/day	m3/hr	m3/min	m3/sec
Daily Average	170	7.1	0.12	0.002
Daily Maximum	200	8.3	0.14	0,002
Hourly Maximum	330	13.8	0.23	0.004

#### 1-4 Design Sewage Quality

ITEM	INFLUENT	EFFLUENT	REMOVAL	REMARKS
	(mg/L)	(mg/L)	RATIO (%)	
BOD	240	30	88	
SS	250	50	80	



#### 1-5 Flow Chart (Dual Power Aerated Lagoon)

ITEMS	UNIT	Formula or Value	Application
1-6-1 Grit Chamber			
(1) Water Surface Load	m3/m2/day	> 1800	1,800
(2) Average Velocity	m/sec	> 0.3	0.3
1-6-2 Complete Mixing Aerated Lagoon		· · · · · · · · · · · · · · · · · · ·	
(1) Retention Time	day	1.5 - 2.5	1.50
(2) Water Depth	m	3.0 - 4.0	3.0
(3) Power Requirement for Mixing	W/m3	> 6.0	6.0
1-6-3 Partial Mixing Aerated Lagoon			
(1) Retention Time	day	2.0	2.0
(2) Water Depth	m	2.0 - 4.0	3.0
(3) Power Requirement for Mixing	W/m3	> 1.0	1.0
(4) Number of Cell	Cell/Basin	1 - 3	3
1-6-4 Storm Water Settling Tank			
(1) Water Depth	m	1.5 - 3.0	1.5
(2) Retention Time (Hourly Max Rain)	hour	> 0.5	0.5
(3) Water Surface Load (Hourly Max Rain)	m3/m2/day	75 - 150	150.0
1-6-5 Disinfection Tank			
(1) Retention Time	min.	> 15	15.0
(2) Dosage	mg/l	2.0 - 4.0	3.0

# 1-6 Design Criteria for Dual Power Aerated Lagoon

# 2 CAPACITY CALCULATION

# 2-1 Grit Chamber and Screen (Hourly Maximum)

ITEM	I	SIGN	UNIT	CALCULATION	RESULT
Туре			-	Parallel Flow Type	
Design Flow		Q1	m3/day	~	330
	t t	Q2	m3/sec	7	0.004
Water Surface Load		WSL	m3/m2/day		1,800
Required Surface Area	1	RSA	m2	Q1/WSL	0.183
Basin Number (Total)		BN	basin	-	2
Basin Number (Stand-		BNS	basin	-	1
Average Velocity		V	m/sec	· •	0.30
Depth		H	m	-	0.10
Width		W1	m	Q2/(V*H)	0.127
	Therefore	W2	m	-	0.30
Length		Ll	m	RSA/W2/(BN-BNS)	0.611
	Therefore	L2	m		2.20
Dimension	(W)	W	m	W2	0.30
, ,	(L)	L	m	1.2	2.20
	(Basin)	*	basin	BN	1
	(Stand-By)	-	stand-by	BNS	1
Screen Type		-		Fine Bar Screen	
Screen Set Number		SSN	set	BN	2
Check			UNIT	APPLICATION	RESULT
Water Surface Load			m3/m2/day	> 1800	500
Average Velocity			m/sec	> 0.3	0.13

ITEM	SIGN	UNIT	CALCULATION	RESULT
Туре			Rectangular Type	
Design Flow	Q1	m3/day	-	200
	Q2	m3/hr	-	8.33
Retention Time	T1	day	-	1.50
Inlet BOD Quality	So	mg/L	-	240
Required Volume	V1	m3/basin	Q1*T	300
Basin Number	BN	basin	-	1
Required Volume per Basin	VBN	m3/basin	Q1*T/BN	300
Water Depth	Н	m	-	3.00
Required Surface Area	Α	m2	V/H	100
Width	W	m		10.00
Length	L1	m	A/W	10.000
Therefore	L2	m	-	10.00
Oxygen Demand Rate	PR1	kg/h	(4.16*10^-5)*r*Q1*So	3
-max. oxygen uptake	r	W/m3	-	1.5
Aeration Unit Power Rate	PRO	kg/h	1000*PR1/(N*Q1*T1)	5.25
Therefore	PRO	W/m3	. <u> </u>	5.3
-aeration performance	N	W/m3	-	1.9
Power Requirement	P1	kW		2.0
1) Oxygen Requirement	P10	kW	PR1/N	1.6
2) Mixing Power	P1M	kW	V1*P0*10^-3	1.8
Dimension (Width)	W -	m	W	10.00
(Length)		m	1.2	10.00
(Depth)	H	m	Н	3.00
(Basin)	:	basin	BN	
Aerator Type	-	1	Slanting Shaft Screw Aerator	DD0111 C
Check		UNIT	APPLICATION	RESULT
Retention Time		day	1.5 - 2.5	1.50

# 2-2 Complete Mixing Aerated Lagoon (Daily Maximum)

ITEM	SIGN	UNIT	CALCULATION	RESULT
Туре	-	÷	Rectangular Type	
Design Flow	Q1	m3/day		200
	Q2	m3/hr	-	8.33
Retention Time	T2	day	-	2.00
Required Volume	V2	m3/basin	Q2*T	400
Basin Number	BN	basin	-	1
Cells Number	CN	cell/basin	-	3
Stand-by Cell Number	CNS	basin	-	1
Sludge Accumulation	SA	m3/year	365*Q1*Xi/(x*10^6)	100
-inert solid concentration	Xi	mg/l	-	
-weight fraction of solids	x	-	-	0.04
No. of Cells Cleaned per Year	CNC	basin	-	
Total Sludge Accumulation	TSA	m3	-	151
Required Volume	V	m3/cell	(Q1*T+TSA)/(BN*CN-CNS)	275
Water Depth	D	m	-	4.00
Required Surface Area	Α	m2/celi	V/H	69
Width	W	m		10.00
Length	L1	m	A/W	6.882
Therefore	L1	m		7.00
Power Requirement	P2	kW	and the second	1.
1) Mixing Power	P2M	kW	Q1*T2*CN*10^-3	0.4
Dimension (Width)	W	m	W	10.00
(Length)	L	m	L1	7.00
(Depth)	Н	m	H	4.00
(Basin)	••	basin	BN	
(Cell)		cell/basin	CN	
(Stand-by Cell)	-	cell	<u> </u>	<u> </u>
Aerator Type	-	. <b>.</b> .	Slanting Shaft Screw Aerator	
Check		UNIT	APPLICATION	RESULT
Surface Area		m2	-	210
Retention Time		day	2.0	2.05

# 2-3 Partial Mixing Aerated Lagoon (Daily Maximum)

ITEM		SIGN	UNIT	CALCULATION	RESULT
Chemical Type		-		Chlorination Type	
Design Flow		Q1	m3/day	_	200
U	1	Q2	m3/min		0.14
Retention Time		T	min.		15.0
Basin Number		BN	basin	-	1
Required Volume		· V	m3	Q2*T	2
Width		W	m	-	0:50
Water Depth		Н	m	-	0:50
Length		L1	m	V/(W*H)	8.333
	therefore	L2	m	-	9.00
Dosage		D	mg/L	-	3.0
Required Chemical		RC1	kg/day	Q1*D*10^-3/C	0.60
	Therefore	RC2	kg/hr	RC1/24	0.03
Dimension	(Width)	W	m	W	0.50
	(Length)	L	m	1.2	9.00
	(Depth)	H	m	Н	0.50
	(Depth)	BN	basin		. 1
Chlorine Feeder			unit	including 1 for stand-by	
Check			UNIT	APPLICATION	RESULT
Retention Time			min.	> 15	16.2

# 2-6 Disinfection Tank (Daily Maximum)

Appendix 12.5Summary of Construction CostNuwara EliyaExchange Rate = 1.

1.8 Yen/Rs

# **Construction Cost - Master Plan : Alternatives**

		Alternative 1	ve 1	,		Alternative 2	ve 2	
Facilities	Specifications	Civil	M&E	Total	Specifications	Civil	M&E	Total
. Sewer								
Sub-Total		236,022		236,022		225,720		225,720
. Pumping Station								
P/S 1	0.89*39*2	828	3,553		0.89*10*2	828	3,266	
P/S 2	2.82*24*2	1,634	4,602		1.93*24*2	1,442	4,294	
Sub-Total		2,462	8,155	10,617		2,270	7,561	9,831
2. Sewage Treatment Plant	ant							
Nuwara Eliva	2,700m3/day	73,321	78,957		2,500m3/day	72,228	74,477	
Hospital/Brewery					200m3/day	11,652	22,664	
Sub-Total		73,321	78,957	152,278		83,880	97,141	181,021
Total		311,805	87,112	398,917		311,870	104,702	416,572

# **Construction Cost - Feasibility Study**

L			M/P (Alternative 1	ative 1)			F/S (Phase 1)	e 1)			Phase 2	5	
	Facilities	Specifications	Civil	M&E	Total	Specifications	Civil	M&E	Total	Specifications	Civil	M&E	Total
<u>-</u>	Sewer												
	Sub-Total		236,022		236,022		145,085		145,085		90,937		90,937
н С	. Pumping Station												
	TP/S1	0.87*35*2	828	3,553		0.87*35*2	828	3,553			0	0	
	P/S 2	2.89*24*2	1,634	4,602		2.89*24*2	1,634	4,602			0	0	
	Sub-Total		2,462	8,155	10,617		2,462	8,155	10,617		0	0	0
5	. Sewage Treatment Plant	ant					-						
	Nuwara Eliya	2,700m3/day	73,321	78,957		1,400m3/day 41,910	41,910	40,116		1,400m3/day	31,411	38,841	
	Hospital/Brewery												
	Sub-Total		73,321	78,957	152,278		41,910		82,026		31,411	31,411 38,841	70,252
	Total		311,805	87,112	398,917		189,457	48,271	48,271 237,728		122,348	122,348 38,841	161,189

Appendix	12.6	Cost of Sewer
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Alternative 1 (A				<u></u>	Master Pla		Feasibility	
ITEM	DESCRIPTION	Depth	UNIT		QUANITTY		QUANTITY	COST
lay Pipe Laying	150 mm (Lateral)	1.5	m	5,498	5,200	28,589,600	4,000	21,992,000
	150 mm	1.5	៣	5,498	7,139	39,250,222	3,769	20,721,962
	225 mm	1.5	m	7,142	2,245	16,033,790	2,245	16,033,790
	225 mm	2.5	m	9,603	310	2,976,930	310	2,976,930
	300 mm	1.5	m	10,593	270	2,860,110	270	2,860,110
	300 mm	2.5	m	13,173	470	6,191,310	470	6,191,310
	300 mm	3.5	m	16,147	350	5,651,450	350	5,651,450
	400 mm	1.5	m	15,652	730	11,425,960	730	11,425,960
	400 mm	3.5	m	21,489	50	1,074,450	50	1,074,450
M Ding Laring	150 mm	1.5	m	7,358	1,400	10,301,200	1,400	10,301,200
DI Pipe Laying	200 mm	1.5	m	8,514	620	5,278,680	620	5,278,680
		1.5	Nr	67,379	335	22,571,965	244	16,440,470
Manhole	Type 1		Nr	79,205				
	Type 2		Nr	91,957			~	
	Type 3		Nr Nr	25,712	2,691	69,190,992	754	19,386,848
Connection Pipe	100mmPVC ,L=4m	·		5,098	2,691	13,718,718	754	3,843,892
Inspection Pit	RC,300×300	0.5	Nr			480,671	1	480,67
Siphon		3.5	Nr	480,671	40	480,071	40	425,64
Siphon Pipe	150mm×2	3.5	m	10,641	40	423,040	40	423,040
		1	1					
	L	<u>}</u>				AA ( 004 (00		
TOTAL	Sewer Main + Latera	<u> </u>		<u></u>	18,784	236,021,688	14,214	145,085,369
	Sewer Main + Latera Sewer Main			•	18,784 13,584	236,021,688	14,214 10,214	145,085,369
TOTAL	ł			•	13,584		10,214	
TOTAL Alternative 2	Sewer Main	(Ui	nit : Rs)	•	13,584 Master Pla	n	10,214 Feasibility	Study
TOTAL	ł	(Ui Depti	nit : Rs) 1 UNIT	A	13,584 Master Pla QUANTITY	n COST	10,214	
TOTAL Alternative 2	Sewer Main DESCRIPTION	(Ui	and the second s	5,498	13,584 Master Pla QUANTITY 5,200	n COST 28,589,600	10,214 Feasibility	Study
TOTAL Alternative 2 ITEM	Sewer Main DESCRIPTION	(Ui Depti	UNIT	5,498 5,498	13,584 Master Pla QUANTITY 5,200 7,139	en COST 28,589,600 39,250,222	10,214 Feasibility	Study
TOTAL Alternative 2 ITEM	Sewer Main DESCRIPTION 150 mm (Lateral)	(Ur Depti 1.5	n UNIT m	5,498	13,584 Master Pla QUANTITY 5,200 7,139 2,245	en COST 28,589,600 39,250,222 16,033,790	10,214 Feasibility	Study
TOTAL Alternative 2 ITEM	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm	(Ui Depti 1.5 1.5	n UNIT m m	5,498 5,498	13,584 Master Pla QUANTITY 5,200 7,139 2,245	en COST 28,589,600 39,250,222	10,214 Feasibility	Study
TOTAL Alternative 2 ITEM	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm	(Un Deptil 1.5 1.5 1.5	n UNIT m m m	5,498 5,498 7,142	13,584 Master Pl: QUANTITY 5,200 7,139 2,245 310	en COST 28,589,600 39,250,222 16,033,790	10,214 Feasibility	Study
TOTAL Alternative 2 ITEM	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm	(U) Dept 1.5 1.5 1.5 2.5 1.5	MUNIT m m m m	5,498 5,498 7,142 9,603	13,584 Master Pla QUANTITY 5,200 7,139 2,245 310 270	en COST 28,589,600 39,250,222 16,033,790 2,976,930	10,214 Feasibility	Study
TOTAL Alternative 2 ITEM	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm	(U) Dept1 1.5 1.5 2.5 1.5 2.5	m UNIT m m m m m m m	5,498 5,498 7,142 9,603 10,593 13,173	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470	EXAMPLE 128,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310	10,214 Feasibility	Study
TOTAL Alternative 2 ITEM	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm	(U) 1.5 1.5 1.5 2.5 1.5 2.5 3.5	m UNIT m m m m m m m	5,498 5,498 7,142 9,603 10,593 13,173 16,147	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350	en COST 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450	10,214 Feasibility QUANITTY	Study
TOTAL Alternative 2 ITEM	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm 300 mm	(Un Depti 1.5 1.5 2.5 1.5 2.5 3.5 1.5	MUNIT m m m m m m m m	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350           730	en COST 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450 11,425,960	10,214 Feasibility QUANITTY	Study
TOTAL Alternative 2 ITEM Clay Pipe Laying	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm 300 mm 400 mm	(Ui Depti 1.5 1.5 2.5 1.5 2.5 3.5 1.5 3.5 3.5	UNIT m m m m m m m m m	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652 21,489	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350           730           50	en COST 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450	10,214 Feasibility QUANITTY	Study
TOTAL Alternative 2 ITEM	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm 300 mm 400 mm 400 mm 150 mm	(U) Depti 1.5 1.5 2.5 1.5 2.5 3.5 1.5 3.5 1.5	UNIT m m m m m m m m m m	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652 21,489 7,358	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350           730           50	en 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450 11,425,960 1,074,450	10,214 Feasibility QUANITTY	Study
TOTAL Alternative 2 ITEM Clay Pipe Laying DI Pipe Laying	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm 300 mm 400 mm 400 mm 150 mm	(Ui Depti 1.5 1.5 2.5 1.5 2.5 3.5 1.5 3.5 3.5	MUNIT m m m m m m m m m m m m m	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652 21,489 7,358 8,514	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350           730           50           620	en 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450 11,425,960 1,074,450  5,278,680	10,214 Feasibility QUANITITY	Study
TOTAL Alternative 2 ITEM Clay Pipe Laying	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm 300 mm 400 mm 400 mm 150 mm 200 mm Type 1	(U) Depti 1.5 1.5 2.5 1.5 2.5 3.5 1.5 3.5 1.5	MUNIT m m m m m m m m m m Nr	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652 21,489 7,358 8,514 67,379	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350           730           50           620           335	en 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450 11,425,960 1,074,450	10,214 Feasibility QUANITITY	Study
TOTAL Alternative 2 ITEM Clay Pipe Laying DI Pipe Laying	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm 300 mm 400 mm 150 mm 150 mm 200 mm Type 1 Type 2	(U) Depti 1.5 1.5 2.5 1.5 2.5 3.5 1.5 3.5 1.5	MUNIT m m m m m m m m m m Nr Nr	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652 21,489 7,358 8,514 67,379 79,205	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350           730           620           335	en COST 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450 11,425,960 1,074,450  5,278,680 22,571,965 	10,214 Feasibility QUANITITY	Study
TOTAL Alternative 2 ITEM Clay Pipe Laying DI Pipe Laying Manhole	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm 300 mm 400 mm 150 mm 200 mm Type 1 Type 2 Type 3	(U) Depti 1.5 1.5 2.5 1.5 2.5 3.5 1.5 3.5 1.5	MUNIT m m m m m m m m m m Nr Nr Nr	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652 21,489 7,358 8,514 67,379 79,205 91,957	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350           730           50           620           335	en COST 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450 11,425,960 1,074,450  5,278,680 22,571,965 	10,214 Feasibility QUANTITY	Study
TOTAL Alternative 2 ITEM Clay Pipe Laying DI Pipe Laying Manhole Connection Pipe	Sewer Main           DESCRIPTION           150 mm (Lateral)           150 mm           225 mm           225 mm           300 mm           150 mm           200 mm           170 mm           100 mmPVC ,L=4m	(U) Depti 1.5 1.5 2.5 1.5 2.5 3.5 1.5 3.5 1.5	MUNIT m m m m m m m m m m Nr Nr Nr Nr	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652 21,489 7,358 8,514 67,379 79,205 91,957 25,712	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350           730           50           620           335	en COST 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450 11,425,960 1,074,450  5,278,680 22,571,965  69,190,992	10,214 Feasibility QUANTITY	Study
TOTAL Alternative 2 ITEM Clay Pipe Laying DI Pipe Laying Manhole Connection Pipe Inspection Pit	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm 300 mm 400 mm 150 mm 200 mm Type 1 Type 2 Type 3	(U) Dept1 1.5 1.5 2.5 1.5 2.5 3.5 1.5 1.5 1.5 1.5	MUNIT m m m m m m m m m m Nr Nr Nr Nr Nr	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652 21,489 7,358 8,514 67,379 79,205 91,957 25,712 5,098	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350           730           50	En COST 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450 11,425,960 10,074,450  5,278,680 22,571,965  69,190,992 13,718,718	10,214 Feasibility QUANTITY	Study
TOTAL Alternative 2 ITEM Clay Pipe Laying DI Pipe Laying Manhole Connection Pipe Inspection Pit Siphon	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm 300 mm 300 mm 150 mm 200 mm 150 mm 200 mm Type 1 Type 2 Type 3 100mmPVC ,L=4m RC,300×300	(U) Dept1 1.5 1.5 2.5 1.5 2.5 3.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1	MUNIT m m m m m m m m m m Nr Nr Nr Nr	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652 21,489 7,358 8,514 67,379 79,205 91,957 25,712 5,098 480,671	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350           730           50	En COST 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450 11,425,960 11,425,960 11,425,960 22,571,965  69,190,992 13,718,718 480,671	10,214 Feasibility QUANTITY	Study
TOTAL Alternative 2 ITEM Clay Pipe Laying DI Pipe Laying Manhole Connection Pipe Inspection Pit	Sewer Main           DESCRIPTION           150 mm (Lateral)           150 mm           225 mm           225 mm           300 mm           150 mm           200 mm           170 mm           100 mmPVC ,L=4m	(U) Dept1 1.5 1.5 2.5 1.5 2.5 3.5 1.5 1.5 1.5 1.5	MUNIT m m m m m m m m m m Nr Nr Nr Nr Nr	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652 21,489 7,358 8,514 67,379 79,205 91,957 25,712 5,098	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350           730           50	En COST 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450 11,425,960 10,074,450  5,278,680 22,571,965  69,190,992 13,718,718	10,214 Feasibility QUANTITY	Study
TOTAL Alternative 2 ITEM Clay Pipe Laying DI Pipe Laying Manhole Connection Pipe Inspection Pit Siphon Siphon Pipe	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm 300 mm 400 mm 400 mm 150 mm 200 mm Type 1 Type 2 Type 3 100mmPVC ,L=4m RC,300×300 150mm×2	(Un Depti 1.5 1.5 2.5 1.5 2.5 3.5 1.5 1.5 1.5 1.5 1.5 3.5 1.5 3.5 1.5 1.5 3.5 1.5	MUNIT m m m m m m m m m m m m Nr Nr Nr Nr Nr Nr	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652 21,489 7,358 8,514 67,379 79,205 91,957 25,712 5,098 480,671	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           2,70           470           350           730           50	en COST 28,589,600 39,250,222 16,033,790 2,976,930 2,976,930 2,860,110 6,191,310 5,651,450 11,425,960 1,074,450  5,278,680 22,571,965  69,190,992 13,718,718 480,671 425,640	10,214 Feasibility QUANTITY	Study
TOTAL Alternative 2 ITEM Clay Pipe Laying DI Pipe Laying Manhole Connection Pipe Inspection Pit Siphon	Sewer Main DESCRIPTION 150 mm (Lateral) 150 mm 225 mm 225 mm 300 mm 300 mm 300 mm 300 mm 150 mm 200 mm 150 mm 200 mm Type 1 Type 2 Type 3 100mmPVC ,L=4m RC,300×300	(Un Depti 1.5 1.5 2.5 1.5 2.5 3.5 1.5 1.5 1.5 1.5 1.5 3.5 1.5 3.5 1.5 1.5 3.5 1.5	MUNIT m m m m m m m m m m m m Nr Nr Nr Nr Nr Nr	5,498 5,498 7,142 9,603 10,593 13,173 16,147 15,652 21,489 7,358 8,514 67,379 79,205 91,957 25,712 5,098 480,671	13,584           Master Pla           QUANTITY           5,200           7,139           2,245           310           270           470           350           730           50	en COST 28,589,600 39,250,222 16,033,790 2,976,930 2,860,110 6,191,310 5,651,450 11,425,960 1,074,450  5,278,680 22,571,965  69,190,992 13,718,718 480,671 425,640 	10,214 Feasibility QUANTITY	Study

Manhole Span		50 m
Manhole Type	φ 150~600	Type 1
	φ 700~900	Type 2
	φ 900~1200	Type 3

# **Numbers of Service Connections**

	Nuwara Eliya	Reference
Size of Family (people/house)	4,84	
M/P Population (2015)	8,681	[
Domestic (No. of Houses)	1,794	
Total (No. of houses)	2,691	Domestic × 1.5
F/S Population (2005)	1,827	
Domestic (No. of Houses)	377	
Total (No. of Connections)	754	Domestic × 2

# Appendix 12.7 Unit Cost

Appendix 12.7.1	Unit Cost of Civil Works	
·		r

are used for cost estimate.

		•	1		are used for c	USE CSUITAIO.			وروبينا والمساد		
Item		NWSD	B Rate 97	Towns So	outh - Ground	Reservoir	Towns Se	outh - Pumpin	g Station	Applied	Adjusted
			Overhead 20%		Forign(Yen)	Total (Rs)	Local (Rs)	Forign(Yen)	Total (Rs)		
1. Excavation											
Bulldozer (incl. Backfilling	)	(Basement)	(Basement)								490.00
Backfoe (incl. Backfilling)		(Pit/Trench)	(Pil/french)	(150 mm)			(225 mm)				790.00
Rock excavation	m	1,469.00	1,763.00	69.00	544.38	371.43	1,716.00	195.27	1,824.48	1,808.99	1,990.00
2. Earth Filling					-						430.00
carth available at site	m <sup>3</sup>	141.00	169.00							169.00	190,00
earth to be borrowed	m²	324.00	389.00							389.00	430,00
3. Soil Disposal			i								310.00
On site	m <sup>3</sup>	68.00	82,00							68.00	80.00
Offsite		232.00	278.00							278.00	310.00
4. Piling											
On site 600 mm dia.	m			1,824.81	14,399.00	9,824.25				9,824.25	10,810.00
5. Concrete Work	1		Ī		[						
Grade 10											7,840.00
Foundations	m <sup>3</sup>	3,743.00	4,492.00	76.07	600.18	409.50	514.80	58.58	547.34	7,123.19	
Grade 20/30	1	(Grade 20)	1	(Grade 30)			(Grade 30)			8,658.97	9,530.00
Columns	m <sup>3</sup>	4,868.00	5,842.00	1,820.50	14,362.89	9,799.88	6,864.00	781.07	7,297.93	8,659.97	9,530.00
6. Form Work	1			T	[					960.43	1,060.00
7. Reinforcement	1		1	1					L	66,328.41	72,970.00
Tor steel		50,220.00	60,264.00	13,510.53	106,591.98	72,728.30	62,920.00	7,159.76	66,897.64	66,329,41	72,970.00
Mild steel	ton	46,920.00	56,304.00	11,312.83	89,253.07	60,897.87	62,920.00	7,159.76	66,897.64	66,329,41	72,970.00
8. Building							ļ				
Offices 2F, 126 m <sup>2</sup>	m <sup>2</sup>	9,600.00	11,520.00	13,494.97	1,535.61	14,348.09	ļ	ļ	·	14,226.22	15,700.00
Operating houses	m <sup>2</sup>	8,600,00	10,320.00	· ·			<u> </u>	ļ		ļ	20,000.00
Pumping Station BF, 181r	n²						31,855.72	3,624.91	33,869.56		37,000.00
Chlorine House 1F, 24m <sup>2</sup>	m²			17,014.23	1,973.50	18,110.62				17,953.99	19,800.00
Store houses 1F, 24m <sup>2</sup>	m	8,200.00	9,840.00	18,950.98	2,156.46	20,149.01				19,977.86	22,000.00
Quarters 1F, 100m <sup>2</sup>	I.	· · · · ·	1	17,496,47	1,971.32	18,591.64				18,435.19	20,300.00
9. Pavement	+	î	1	1	<u>+</u>	<u> </u>	T	T			
Reinstatement	m	t	· · · ·	206.58	1,629.82	1.112.04	Actual pay	ment to RDA	Rs. 2000.00)	2,000.00	2,000.00
10. Miscellaneous	1.		1		1		1	1	T T	Ī	
Miscellancous	╈	t		+			t	1			5 to 20 %
Intoctionous	1 ^		1			A	-				

A-12.7-1

Appendix 12.7.2	Unit Cost of	Piping	Materials
Appenaix 12.7.2	Unit Cost of	riping	Wateraals

are used for cost estimate.

							34 6 1 1			e		Applied	Adjusted
		Diameter (n	ոտ)	the second s	strends and strends an		Manufacturer	Level (De)	Towns Forign(Yen)		Total (Rs)	Applied	Adjusted
				Rs/m	Overhead 20%	Rs/m	Rs/m	Local (RS)	rongatienj	<u>C. D. (RS)</u>	Total (Rs)		
		Supply		000 0.00					<u></u>	·····	<u>├</u>		
	DIP			(CIF+C.D.)									3,500.00
-		200	mm	2,647.48	3,177.00			(5.50	6 467 50	661.72	3,807.10	3,807.10	4,190.00
		250	mm	2,981.44	3,578.00			65.58	6,467.59	the second second second	4,806.30	4,806.30	5,290.00
		300	nm	3,794.56	4,553.00	·		82.79	8,165.06	835.39		6,018.57	6,630.00
<b> </b>		350	mm	4,537.50	5,445.00			103.27	10,234.03	1,041.95	6,018.57 7,955.72	7,955.72	8,760.00
		400	nım	5,324.00	6,389.00			137.05	13,515.35	1,382.79		8,364.93	9,210,00
		450	mm	6,352.50	7,623.00			144.09	14,210.53	1,453.92	8,364.93 11,208.43	11,208,43	12,330.00
<b> </b>		500	mm	7,292.67	8,751.00			193.08	19,041.13		12,970.21	12,970.21	14,270.00
<u> </u>		600	mm	9,075.00	10,890.00			223.43	22,034.08	2,254.36	12,970.21	12,970.21	20,000.00
		700	mm	11,918.50	14,302.00			1/0 10	45 500 62	4,663.47	26,830.72	26,830.72	29,520.00
		800	ញា	14,762.00	17,714,00			462.19	45,580.63	4,003.47	20,030.72	20,030.72	35,000.00
L		900	mm	15,851.00	19,021.00					<b>_</b>	·		the second se
	PVC	C (type 600)	)		ļ					<b></b>	80.02	80.00	(type 600)
		.63	mm	50.00	60,00	L		55.95	55.18	<b> </b>	82.23	82.23	100.00
		75	mm	78.00	94.00	ļ			100.00		161.00	114.78	
$\square$		90	mm	118.00	142.00	ļ	ļ	109.75	108.23	<b></b>	161.29	161.29	180.00 270.00
		110	mm		208.00		·	161.15	158.93	ļ	236.83	236.83	
		160	mm		408.00	L	<b>.</b>	340.35	335.65	ł	500.18	500.18 980.45	560.00
		225	mm	655.00	786,00			667.15	657.94	Ļ	980.45	900,43	1,000.00
2. Se								<u> </u>		<u> </u>	Į		(1) (200)
	PV(	C (type 600	)				(type 400)	(type 600)	<u> </u>	<u> </u>			(type 600)
		110	ກາກ	2				161.15	158.93	<u> </u>	236.83	236.83	270.00
		160	mm	340.00			786.95	340.35	335.65	<u></u>	500.18	500.18	510,00
		225	mm	655.00	786.00		1,496.80	667.15	657.94	<u> </u>	980.45	980.45	990.00
		280	mm	1,013.00	1,216.00	<u>`</u>	2,294.65	<u> </u>		<u> </u>	1 · · · ·	2,294.65	2,300.00
	3	315	mm	<u>I</u>			2,888.02	:	· · · · · · · · · · · · · · · · · · ·	<u> </u>	<b></b>	2,888.02	2,890.00
	Hu	ne Pipe	<u></u>	`	<u></u>		L		- 1 <sup>2</sup>	· .			
		150	mm				198.39	<b></b>			<u></u>	· · · · · · · · · · · ·	
	L	225	mm	497.00	596.00		273.13		·	· · · · · · · · · · · · · · · · · · ·	<b>_</b>	ļ	
		· 250	BIM							ļ	<b>_</b>		
	L	300	mm				355.25				ļ	792.00	800.00
		375	mm	900.00	1,080.00		516.73	· · · · · · · · · · · · · · · · · · ·	ļ	. <b>.</b>		1,080.00	1,080.00
		400	imm				L	L	L	, <u> </u>		L	
	ļ	450	mm	995.00	1,194.00	Ļ	611.31	2,577.99	1,307.04		3,200.39	1,194.00	·1,200.00
		500	mm				<b>_</b>			ļ			<u> </u>
	ļ	544	mm			<b>_</b>	<b></b>	4,124.78	2,091.26		5,120.62	(with inner 1	
	1	600	มะก	<u> </u>	1,663.00		847.07	<b>_</b>				1,663.00	1,670.00
	<b> </b>	675	mm			5,960.00		<b></b>		<b></b>	+	5,960,00	5,960.00
	L	750	mu	1,868.00	) 2,242.00				<b></b>		<b>_</b>	6,790.00	6,790.00
		825	mit			7,630.00				<u> </u>	<b>_</b>	7,630.00	7,630.00
		900	nm				1,495.76		1		<u> </u>	3,660.00	3,660.00
L	L	1050	mm	3,300.00	3,960.00		3,820.13		_ <b>_</b>	<u> </u>	<u> </u>	4,752.00	4,760.00
	Cla	y Pipe						:		1 .	1.1.1		<u> </u>
	1		nın	410.00	492.00	730.8	8	1	1	1	1	730.88	740.00
	<u>t</u>	225				-	1	1	1		1	1,789.84	1,790.00
$\vdash$	⊢	223			110.00	1,107.0	·}	+		+	+		
H-	+	+				+	<u>_</u>	+	-+		+	in the second	4 4750 00
<b></b>	<b>_</b>	300	_		1,482.00			+		+		4,464.66	4,470.00
	4	400	-		- <b> </b>	8,578.3		<u> </u>	_ <u>_</u>	- <u> </u>	+	8,578.39	8,580.00
	1	450			<b></b>	9,959.2	· • · · · · · · · · · · · · · · · · · ·	+		_ <u></u>		9,959.28	9,960.00
	1	500	_		_ <b>_</b>	12,457.1	0 <u>1</u>	1			1	12,457.10	12,460.00
		600	) mn			24,476.3	~ <b>i</b>				<b>_</b>	24,476.30	24,480.00

Note : 1. For transmission mains of water supply, 20 % of the cost of pipes shall be add to compensate the cost of specials, valves etc. 2. For diatribution mains of water supply, 35 % of the cost of pipes shall be add to compensate the cost of specials, valves etc.

Appendix 12.7.3	Unit Cost of	Pipe	Laying
-----------------	--------------	------	--------

•							are used for c	ost estimate.				
		Diameter	r I	NWSDI	B Rate 97	and a local decision of the second	Towns South		Japan	Sri Lanka	Applied	Adjusted
		(man)		Rs/m	Overhead 20%	Local (Rs)	Foriga(Yen)	Total (Rs)	Man-Day	Rs/m		
لىمى ئىلى	ying										(only Pi	ie Laying)
	DIP	<u>'</u> T			(with 1 to 2m	excavation, bac	kfilling etc.)					
	T	200	nun	559.00	671.00		·		0.18	124.60	124.60	125.00
		250	nım	580.00	696.00	100.06	789.40	475.96	0.22	154.00	154.00	154.00
		300	mm	698.00	838,00	105.58	832.96	502.23	0.26	182,70	182.70	183.00
		350	mm	740.00	888.00	123.73	976.16	588.57	0.32	222.60	222.60	223.00
		400	mm	795.00	954.00	129.25	1,019.72	614.83	0.38	269,03	269.03	270.00
		450	<b>B</b> 101	852.00	1,022.00	149.53	1,180.10	711.48	0.45	316.87	316.87	317.00
		500	mm	942.00	1,130.00	258.50	2,039.45	1,229.67	0.52	365.40	365.40	366.00
		600	ntm	1,077.00	1,292.00				0.66	463.87	463.87	464.00
		700	nm	1,234.00	1,481.00				0.80	562.33	562.33	563.00
		800	ກາກ	1,395.00	1,674.00	385.00	3,037.48	1,831.42	0.96	672.00	672.00	672.00
		900	mm	1.578.00	1,894.00		1		1.09	765,10	765.10	766.00
	ΡVO				ipe Laving)	(with 1 to 2m	excavation, ba	ckfilling etc.	)		L	
	<u></u>	63	anm	11.76	14.00	29.04	229.11	138,14	0.04	30.10	30,10	31.00
		75	mm	11.76	14.00	29.04	229.11	138.14	0.04	30.10	30.10	31.00
		90	mm	13.94	17.00	29.04	229.11	138.14	0.06	39.90	39.90	40.00
		90 110	<u> </u>	15.00	18.00	34.98	275.98	166.40	0.06	39.90	39.90	40.00
		110	mm	15.00	18.00	38.94	307.22	185.24	0.07	51.80	51.80	52.00
~ <del>~ ~</del> ~~~			ศษา	13.00	22.00	40.04	315.90	190.47	0.10	72.80	72.80	73.00
		225	mm		22.00				0.14	98.00	98.00	98.00
	ļ	280	mm	18.74	22.00	<b>}</b>		[	0.17	119.00	119.00	119.00
		315	mm			<b></b>	·		+		<b>†</b>	<u>}</u>
						<u> </u>	ــــــــــــــــــــــــــــــــــــــ	+			+	<u> </u>
	Hu	me Pipe/Clay	y Pipe		ation, backfilling	depin is unk	nown)	<b>_</b>	0.32	224.00	112.00	112.00
		150	mm	134.00	the second s	<b></b>			0.32			139.00
		225	nım	164.00	197.00	<u> </u>			0.40			160.00
		250	mm			<u> </u>			0.40		_	185.00
		300	mm	227.00			_ <b>_</b>		0.55			210.00
		375	mm	270.00	324.00	<b>_</b>	_{-		0.60			215.00
		400	num					1 406 01			-	294.00
		450	mm	330.00	396.00	2,033.77	2,883.18	3,406.71	0.86			
		500	mm					0.100 01	-			
		544	mm			2,033.77	2,883.18	3,406.71	1.06			
	T	600	_	410.00	492.00	· <b> </b>	_ <b>_</b>		1.12			
	Ϊ.	675	mm									
	Γ	750	mm	500.00	600.00	· · · · · · · · · · · · · · · · · · ·			1.15		_	
C		825				<u> </u>			1.2			
	Γ	900	mm					<u>_</u>				
Γ	Ι	1050	mm	680.00	816.00				1.34	940,81	, 470,40	471.00
2.	Exca	vation	T									790.00
F	Ba	ckfoe	-							_	<b>.</b>	790.00
F		cl. Backfilli	ng)	1		[						
3.		Disposal	T	T								
F		ff site	m <sup>3</sup>	1		1						310.00
F					-+	+			1	-		
4.	_	cfilling with	2		_ <u>_</u>	1					1	1,000.00
_	_	ith sand supp	ly m <sup>3</sup>		_ <b>_</b>	- <b> </b>		+	+	+		
5.	Pave	ement	_					_ <u> </u>	-+			2,000.00
1	R	einstatement	m <sup>2</sup>	1		I						1 2,000.00

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# **Chapter 13**

Appendix 13.1	Sewer Network Hydraulic Analysis
Appendix 13.2	Trunk Sewer Profile
Appendix 13.3	Pumping Equipment

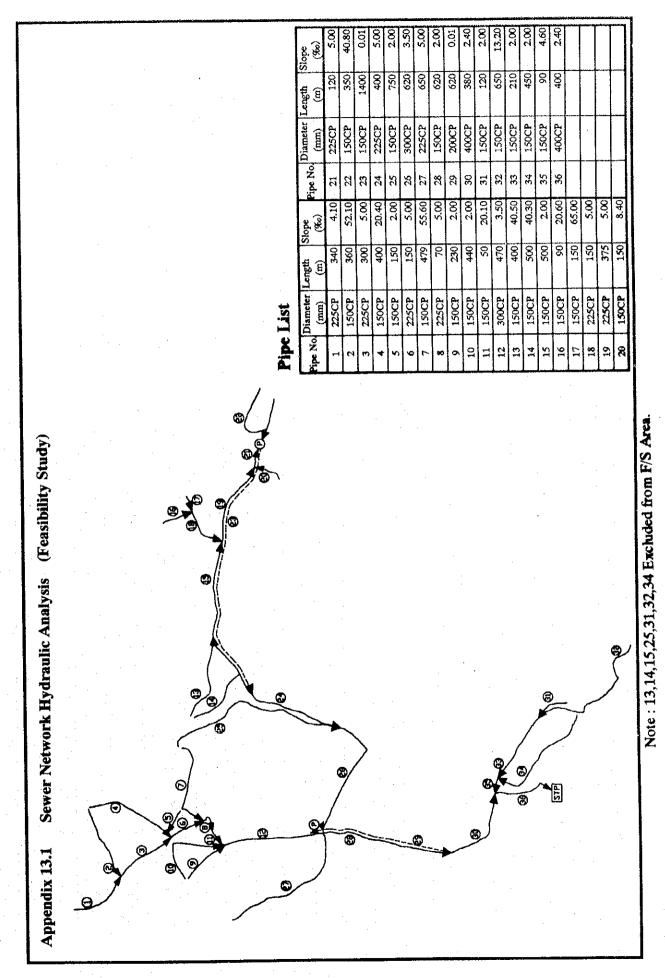
- Capacity Calculation Appendix 13.4 Sewage Treatment Plant

- Capacity Calculation

Appendix 13.5 Hydraulic Calculation

Appendix 13.6 Drawings

Appendix 13.7 Storage Capacity of Sewer



A-13.1-1

4

Sewage Flow Calculation Table (Nuwara Eliya)

WUnit Sewage Flow : 0.187m3/capita-day 00334+0.00066 0334+0.00254 Remarks <u>8,8</u> 2 2 518 គ្គុំខ្ល 298 82-55 <u>0</u> 0 5 8 50 A R - - - - -- j-190315 1901979 10 188071 1879539 10 188071 1879454 1 187916 1877912 1 187916 1904635 1 187916 1877989 1 187893 1875739 2 1875739 1875739 3 188203 1880859 1 187993 1878759 7 187916 1877902 1 1877805 1877802 1 00348 188438 1883209 188438 1881132 188071 1879462 188100 1879829 188071 1879629 1884538 1877802 Level **>**: ;; ł 188579 1 187893 G.L. ×: Design Sewer 00318 00068 ci0288 d0218 00318 00359 d0318 00136 00318 89000 m3/s Flow 0385 d723 0799 0799 2032 662.0 0385 a/s 1967 d799 1231 1111 1 ٨ 410 5210 Slope 2040 200 <u>8</u> <u>800</u> 200 5560 ខ្លួ <u>8</u> 200 % 150 150 150 150 225 225 225 225 150 225 150 Dia. Đ. 10 •0 •0 Ð 19 -0-0 ø 9 10 00018 00059 21100 00014 00134 00153 00153 00001 00018 C0153 00008 m3/s Acctum. 000184 000011 000588 001172 000144 001342 00150 001503 001503 000083 001503 Accum. m3/s Flow 000184 Other 000588 000400 000144 000011 000015 000150 000011 000083 **m**3/3 Sec. 00003 00003 00003 00003 Flow m3/s Population 148 148 Sewage Flow 148 148 Accum. ۵. Sec. 148 ۵. Pop/D P/ha n.3/s R. C. Service Area Accum. ۶q Storm Run-off Sec. 뼕 o Rainfall m3/s-ha per ha ain á. Ē 340 360 660 6 230 150 810 479 830 850 880 Accu Length 230 340 純 360 300 ŝ 150 150 479 ন্থ ន 8 Sec. Accum Service Area 120 5 . 양 : 33 8 -2 601 8 436 <del>1</del>9 **P**3 - - 2 104 ς. Sec. 122 --8 - g Å, - - 55 -8 1.1 ---6 109 8 - 8 Down stream Ш.  $i \sim$ e φ ç ŝ ្ឋ Pipe to. . LO \_\_\_\_\_\_ 6, 8-2 -4 5 ~ ŝ ശ ~ 5 Ξ.

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2	a-day		ks.																	
	0.187¤3/capita·day		Remarks						1											
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	WUnit Sewage Flow	Sewer		;	×							190255			186900		18772		186575	
	Unit:	Design Se	100	5	m3/s		00068	00216	00572	 doade		00306	00068		1	· · · ·	00388	00318	9 00318	
	*	De	с. Бе		a/s		200 0385	10 1222	350 0809	 50 1734		30 1730	200 0385		50 1237		00 2197	500 0799	500 0799	
			Slope		 >8		150 20	150 2010	300	 150 4050		150 4030	150 24		150 2050		150 6500	225	225	
	1			5	8		- 0	0	0	 e l		9	19.		6		Đ.	·ə	ø	
			Accum	H	s #3/s	·	74 00007	163 00016	565 00170	 90008			00027		93 00016		533 00059	526 00078	759 00127	
	-	Other Flow		. Accum	s m3/3		074 000074	000 000163	001665	 					E60000 E60		533 000533	000625	133 000759	
		3		Sec.	s m=3/s		000074	00006	+	 			27		07 cp0093		06 000533	15 15	51 000133	
Eliya)		Mo		1.10H	P m3/3				148 00003	 261 00006		433 00009	1252 00027		328 00007		258 00005	684 00015	2336 00051	
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(Nuwara				£.0.	a.3/5	·				 										
able			ice Area	Accus.	<b>k</b> d				<b> </b>	 •										
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tion		Stor		ມ ບ						 										
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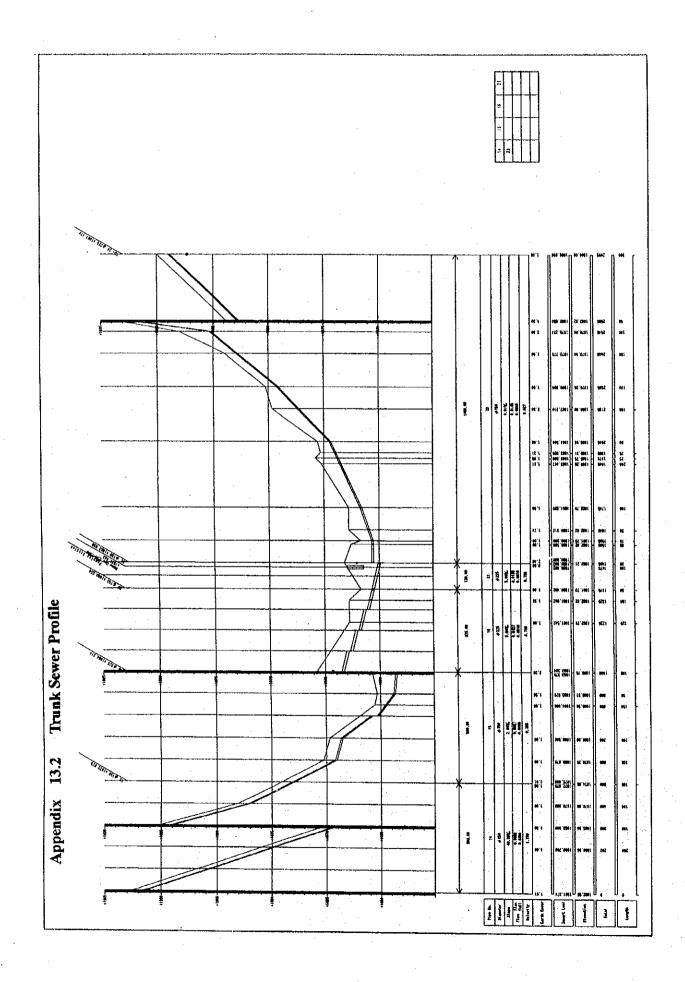
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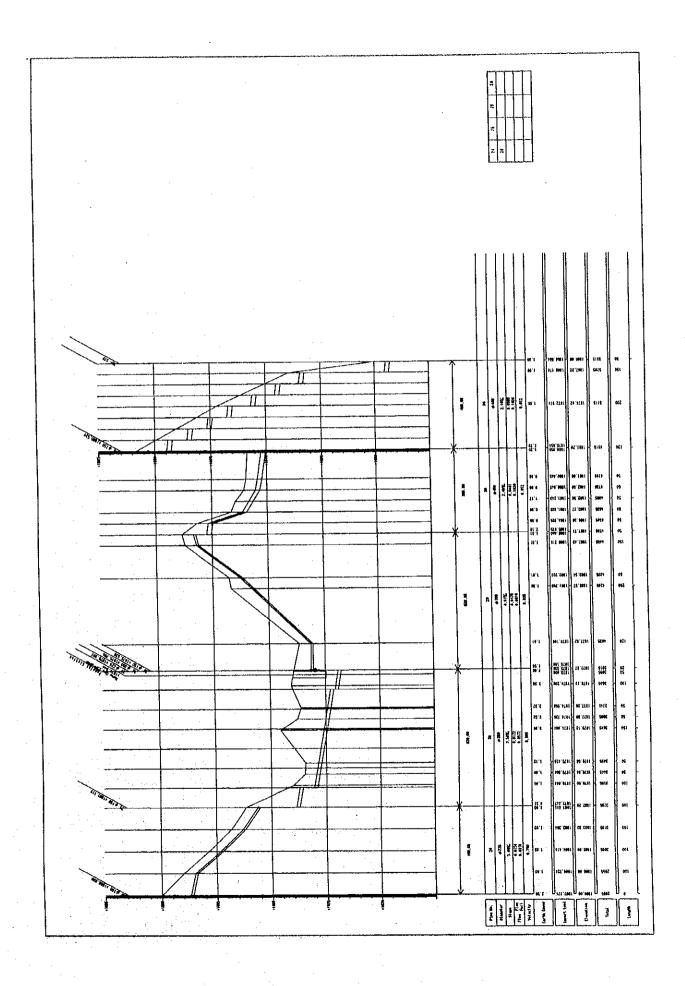
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		Flow	Accum		<b>a</b> .3/5	. <b></b>	000759			000759	000759	·	00038	000797		<b>c0</b> 1002	• • • • • •		003465	003465	
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š		Serv.	ۆ		ъц		021				85					256		53		507	
			Down	stream			53				26			29		ស្ត				36	·
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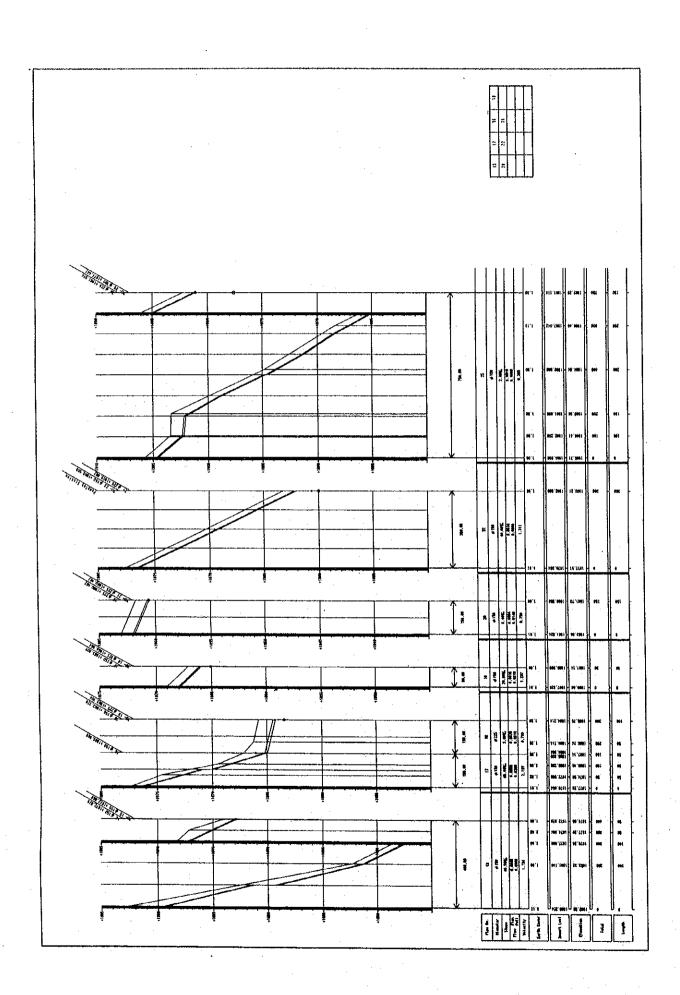
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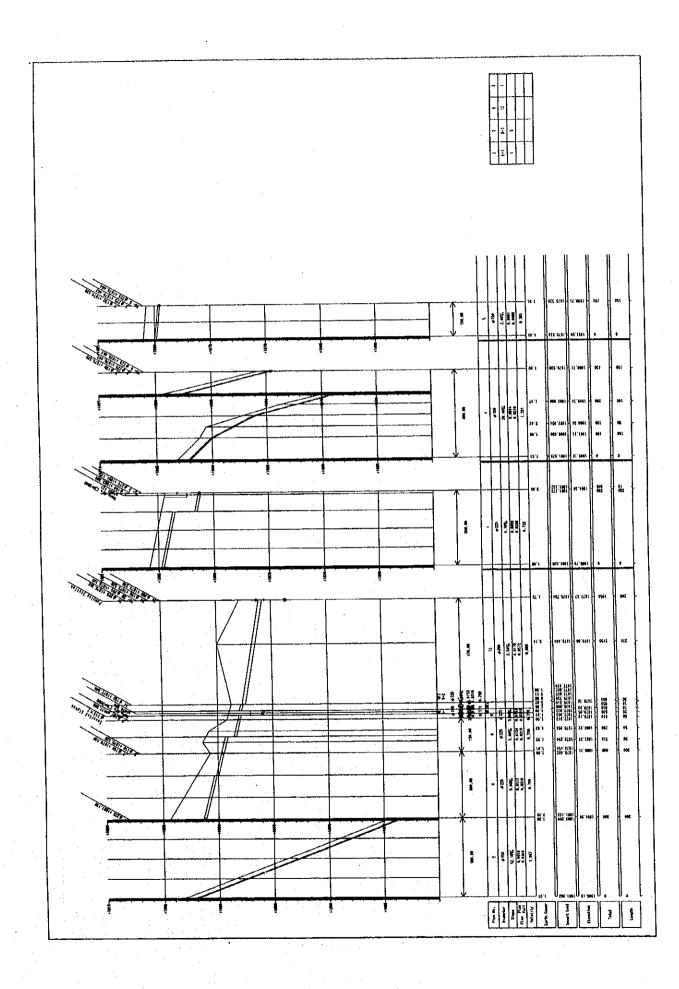
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. I :			Down S stream	<u> </u>	33			35							-					
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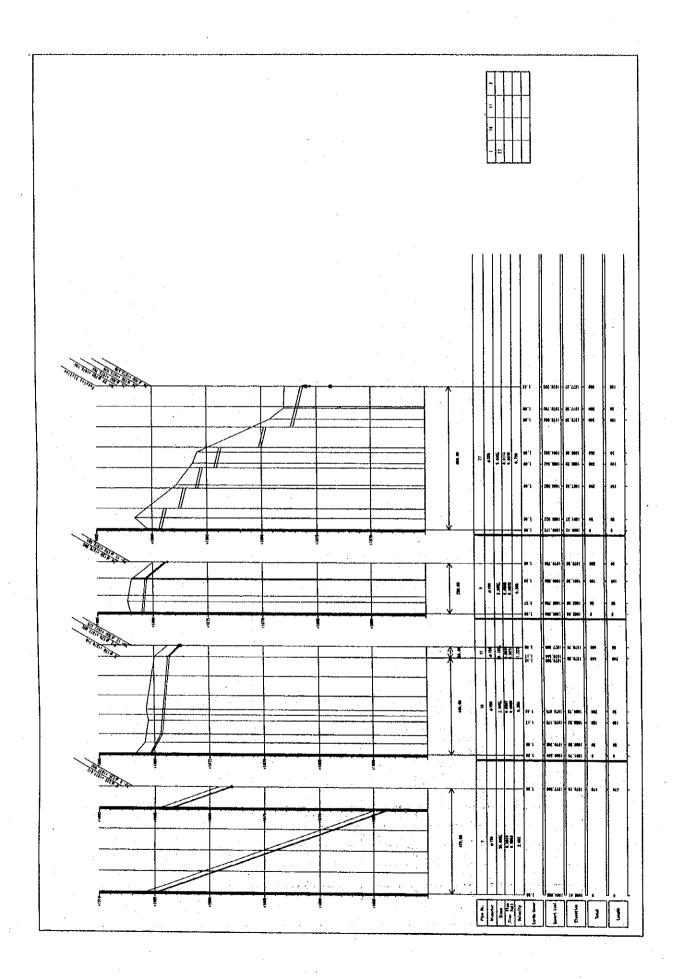
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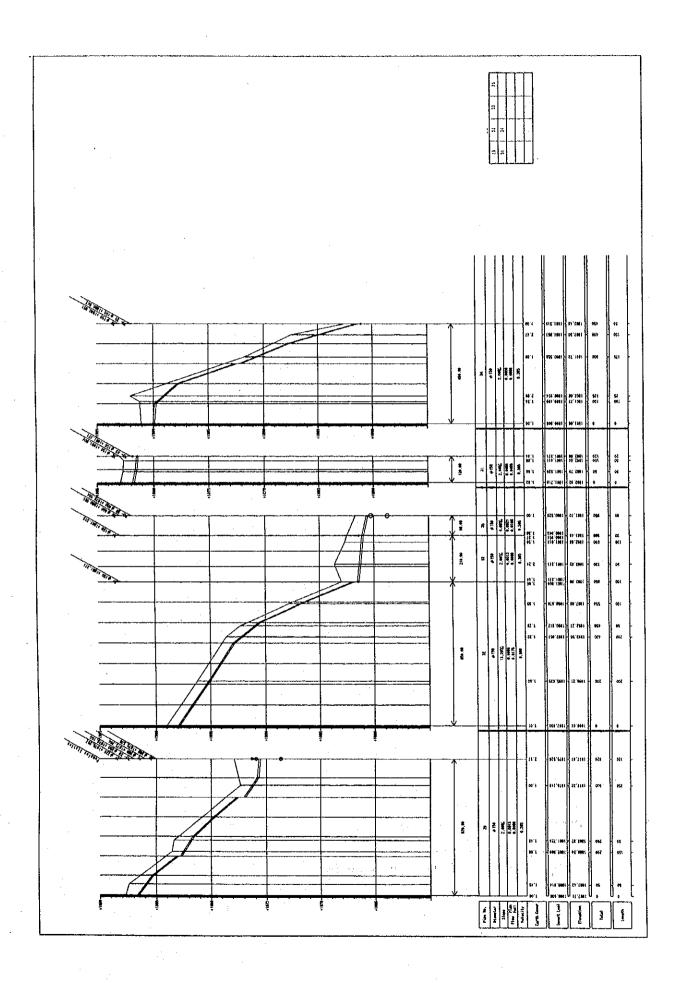












# Appendix 13.3 Pumping Equipment-Capacity Caluculation Nuiwara Eliya

# 1. Pumping Station No.1 (Hospital)

Fumping Station No.	r (mospital)					
Total Capacity		1,279	m3/da	ıy≔	0.89	m3/min
Quantity of pump		1	sets +	1 set for	r stand-by	×,
Pump Capacity		1,279				
	Q ==	0.888	m3/m	in		
	q =	0.0148	m3/se	c		
Diameter	Diameter = 14	46*(O/v)^(1	/2)			
Diamotor	= =		, <del></del> , mm	to	79	mm
	=		mm	10	12	
	where,v=	1.50		o	3.00	
Total Head	Total Head H	-61:67:62	_		38.3	
Total ficau	Total ficau fi			39.0 n		111
	antical band b			39.0 E		
	actual head h				29.42	m .
,		uction level			1,859.41	<b>m</b>
		lelivery leve			1,888.83	m
	friction loss (l					•
	h2 = 10.666*6			1^1.85*I		
	=	7.78	m			· · · ·
	where, c=	130				
100 A	D =	150	mm đ	ia /1000	н. <sup>н</sup>	
	L =	1,400				
	(v=	0.838		)		
	friction loss :			,		
	$h3 = f * (v^{*})$					
•	==	1.07	m			•
	where, v =		m/sec			
	where,	1.00		'ty	f/pc	f
· ·	check valve		Q	•	1.50	
				1		1.50
·	sluice valve			2	0.10	0.20
	increase			0	0.15	0.00
	90deg			5	0.18	0.90
	tee			2	1.15	2.30
	outlet			1	1.00	1.00
					total	5.90
Motor Output	Motor Output	= (0.163*r	*Q*H/	e)*(1+a)	)	
	-	10.8	kW			
		11.0	kW			
	where,r=	1.00				· .
	c=	0.60				•
	a=	0.15				
Quantificant and						
Specification	G.L. 9.1	л <b>п</b>				
Туре	Submersible 3	sewage Pun	ıp			
Diameter	100					÷ .
Capacity		m3/min				
Head	39.0					
Motor Output	11		-		: ·	
Quantity	1	sets + 1 set f	tor star	adby		

Pumping Station No.	2 (Victoria Pa					a 0a		
Total Capacity		4,061			0	2.82	m3/n	nin
Quantity of pump					for s	tand-by		
Pump Capacity	~	4,061						
	Q =	2.820						
	q =	0.0470	m3/s	ec				
Diameter	Diameter = 1							
	, = =		mm mm	tọ		142	mm	
	where,v=	1.50		to		3.00		
Total Head	Total Head H	(=h1+h2+h3	=			22.8	m	
				24.0	m			
	actual head h	1 = hd - hs	=			13.44		
		suction leve	l bs=			1,873.05		
		delivery lev				1,886.49	m	
	friction loss ( $h2 = 10.666^*$					pe		
	=	7.19		1				
	where, c=	130						
	D =			dia /1(	m			
	L=		) m					
	(v=	1.496		- (n				
	friction loss :		ш/м					
	$h3 = f * (v^{\prime})$							
		2/2 g) 2.13						
	=	2.66						
	where, v =	,2.00		Q'ty		f/pc		f
	where,			•	1	1.50		1.50
· · · ·	check valve				2	0.10		0.20
	sluice valve				0	0.10		0.20
	increase				5	0.13		0.90
	90deg				2	1.15		2.30
	tee				2 1	1.13		1.00
	outlet				1	total		5.90
Materia Onterest	Motor Outpu		-* <b>^</b> *i	1.1*/1	د،			
Motor Output		•	l kW					
			kŴ			1		
	= where,r=	1.00						
	-	0.60						
	e=							
	a=	0.15	• · · ·		•	an a		
Specification							н - н	
Туре	Submersible		mp					
Diameter		mm					· ·	
Capacity	2.82	m3/min						
Head	24.0							
Motor Outpu		kW						
Quantity	1	sets + 1 set	for st	landby		· · .		

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A-13.3-2

# Appendix 13.4 Sewage Treatment Plant - Capacity Calculation CAPACITY CALCULATION OF FACILITIES (Dual Power Aerated Lagoon)

#### **1** BASIC CONDITIONS

#### 1-1 BASIC ITEMS

- (1) Name : Nuwara Eliya Sewage Treatment Plant
- Approximately 2.3 ha (2) Land Area 1855.000 (3) Elevation m ٠ (4) Inlet Pipe Level : 1854.850 m 400 (5) Pipe Diameter : m Tea Plantation (6) Land Use ÷ (7) Collection System: Seperate Type Sewage Treatment : Aerated Lagoon Method (8) Treatment Method : Sludge Treatment : Pond Accumulation (9) Effluent Point : Nanu Oya (10) Effluent Point Water Level : 1852.000 m Year 2000 (Phase 1) (11) Target Year : 15 °C (January) (12) Lowest Monthly Average Temperature

#### 1-2 Design Population

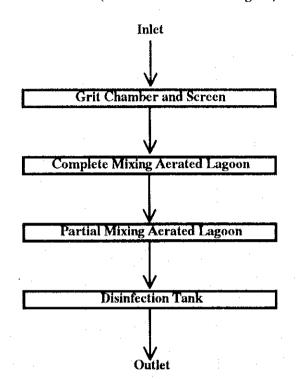
Design Population : 1,830 Persons (Total)

1-3 Design Sewage Flow

ITEM	m3/day	m3/hr	m3/min	m3/sec	
Daily Average	1,200	50.0	0.83	0.014	Ν.
Daily Maximum	1,400	58.3	0.97	0.016	3
Hourly Maximum	2,400	100.0	1.67	0.028	

#### 1-4 Design Sewage Quality

ITEM	INFLUENT (mg/L)	EFFLUENT (mg/L)	REMOVAL RATIO (%)	REMARKS
BOD	240	(mg/L) 30	88	
SS	250	50	80	



#### 1-5 Flow Chart (Dual Power Acrated Lagoon)

ITEMS	UNIT	Formula or Value	Application
I-6-1 Grit Chamber			
(1) Water Surface Load	m3/m2/day	> 1800	1,800
(2) Average Velocity	m/sec	> 0.3	0.3
1-6-2 Complete Mixing Aerated Lagoon			
(1) Retention Time	day	1.5 - 2.5	1.50
(2) Water Depth	m	3.0 - 4.0	3.0
(3) Power Requirement for Mixing	W/m3	> 6.0	6.0
1-6-3 Partial Mixing Aerated Lagoon			
(1) Retention Time	day	2.0	2.0
(2) Water Depth	m	2.0 - 4.0	3.0
(3) Power Requirement for Mixing	W/m3	> 1.0	1.0
(4) Number of Cell	Cell/Basin	1 - 3	3
1-6-4 Storm Water Settling Tank			
(1) Water Depth	m	1.5 - 3.0	1.5
<ul><li>(2) Retention Time (Hourly Max Rain)</li></ul>	hour	> 0.5	0.5
(3) Water Surface Load (Hourly Max Rain)	m3/m2/day	75 - 150	150.0
1-6-5 Disinfection Tank		<u></u>	
(1) Retention Time	min.	> 15	15.0
(2) Dosage	mg/l	2.0 - 4.0	3.0

### 1-6 Design Criteria for Dual Power Aerated Lagoon

## 2 CAPACITY CALCULATION

## 2-1 Grit Chamber and Screen (Hourly Maximum)

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ITEM	SIGN	UNIT	CALCULATION	RESULT
Туре	~		Parallel Flow Type	
Design Flow	Q1	m3/day		2,400
	Q2	m3/sec		0.028
Water Surface Load	WSL	m3/m2/day	-	1,800
Required Surface Area	RSA	m2	Q1/WSL	1.333
Basin Number (Total)	BN	basin	-	2
Basin Number (Stand-By)	BNS	basin	-	1
Average Velocity	v	m/sec	-	0.30
Depth	Н	m		0.30
Width	W1	m	Q2/(V*H)	0.309
Therefore	W2	m		0.50
Length	L1	m	RSA/W2/(BN-BNS)	2.667
Therefore	L2	m	-	2.70
Dimension (W)	W	m	W2	0.50
(L)	L	m	L2	2.70
(Basin)		basin	BN	1
(Stand-By)		stand-by	BNS	1
Screen Type			Fine Bar Screen	
Screen Set Number	SSN	set	BN	2
Check	·	UNIT	APPLICATION	RESULT
Water Surface Load	· · · ·	m3/m2/day	> 1800	1,778
Average Velocity		m/sec	> 0.3	0.19

ITEM	SIGN	UNIT	CALCULATION	RESULT
Гуре	-	-	Rectangular Type	
Design Flow	Q1	m3/day		1,400
	Q2	m3/hr		58.33
Retention Time	T1	day	-	1.50
Inlet BOD Quality	So	mg/L	<u> </u>	240
Required Volume	V1	m3/basin	Q1*T	2,100
Basin Number	BN	basin		2
Required Volume per Basin	VBN	m3/basin	Q1*T/BN	1,050
Water Depth	H	m	_	3.00
Required Surface Area	A	m2	V/H	350
Width	W	m	-	14.00
Length	L1	m	A/W	25.000
Therefore	L2	m	-	25.00
Oxygen Demand Rate	PR1	kg/h	(4.16*10^-5)*r*Q1*So	21
-max. oxygen uptake	ſ	W/m3	-	1.5
Aeration Unit Power Rate	PRO	kg/h	1000*PR1/(N*Q1*T1)	5.25
Therefore	PRO	W/m3	-	5,
-aeration performance	N	W/m3	-	1.9
Power Requirement	<b>P</b> 1	kW	<b>-</b>	13.0
1) Oxygen Requirement	P10	kW	PR1/N	11.0
2) Mixing Power	P1M	kW	V1*P0*10^-3	12.
Dimension (Width)	W	m	W	14.0
(Length)	L	m	1.2	25.0
(Depth)		m	Н	3.0
(Basin)		basin	BN	
Aerator Type	-	-	Slanting Shaft Screw Aerator	
Check		UNIT	APPLICATION	RESULT
Retention Time		day	1.5 - 2.5	1.5

## 2-2 Complete Mixing Aerated Lagoon (Daily Maximum)

ITEM	SIGN	UNIT	CALCULATION	RESULT
Туре	-		Rectangular Type	
Design Flow	Q1	m3/day	-	1,400
	Q2	m3/hr	-	58.33
Retention Time	T2	day	**	2.00
Required Volume	V2	m3/basin	Q2*T	2,800
Basin Number	BN	basin		2
Cells Number	CN	cell/basin		3
Stand-by Cell Number	CNS	basin	-	
Sludge Accumulation	SA	m3/year	365*Q1*Xi/(x*10^6)	703
-inert solid concentration	Xi	mg/l		55
-weight fraction of solids	x	-	-	0.04
No. of Cells Cleaned per Year	CNC	basin	<u> </u>	2
Total Sludge Accumulation	TSA	m3	-	1,054
Required Volume	V	m3/cell	(Q1*T+TSA)/(BN*CN-CNS)	
Water Depth	D	m	-	4.00
Required Surface Area	A	m2/cell	V/H	193
Width	W	m	-	12.00
Length	L1	m	A/W	16.058
Therefore	L1 -	m	-	16.00
Power Requirement	P2	kW	-	3.0
1) Mixing Power	P2M	kW	Q1*T2*CN*10^-3	2.8
Dimension (Width)	Ŵ	m	W	12.00
(Length)	L	m	L1	16.00
(Depth)	H	m	H	4.00
(Basin)	-	basin	BN	
(Cell)	-	cell/basin	CN	
(Stand-by Cell)	1	cell	-	]
Aerator Type	-	-	Slanting Shaft Screw Aerator	
Check		UNIT	APPLICATION	RESULT
Surface Area		m2	-	1,152
Retention Time		day	2.0	1.9

## 2-3 Partial Mixing Acrated Lagoon (Daily Maximum)

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ITEM		SIGN	UNIT	CALCULATION	RESULT
Chemical Type		÷		Chlorination Type	
Design Flow		Q1	m3/day		1,400
		Q2	m3/min	-	0.97
Retention Time		T	min.	-	15.0
Basin Number		BN	basin		
Required Volume		V	m3	Q2*T	15
Width		W	· m	_	1,00
Water Depth		H	m		1.00
Length		L1	m	V/(W*H)	14.583
	therefore	L2	m	-	15.00
Dosage		D	mg/L	-	3.0
Required Chemical		RC1	kg/day	Q1*D*10^-3/C	4.20
	Therefore	RC2	kg/hr	RC1/24	0.18
Dimension	(Width)	W	m	W	1.00
	(Length)	L	m	L2	15.00
	(Depth)	Н	m	H	1.00
	(Depth)	BN	basin	-	1
Chlorine Feeder		-	unit	including 1 for stand-by	
Check			UNIT	APPLICATION	RESULT
Retention Time	1		min.	> 15	15.4

## 2-6 Disinfection Tank (Daily Maximum)

# Appendix 13.5 Hydraulic Calculation

### 1. Design Condition

1.1 Design Wastewater Quantity

Flow	m <sup>3</sup> /day	m <sup>3</sup> /hour	m <sup>3</sup> /min	m <sup>3</sup> /sec	
Daily Average	Qd-ave	1,200	50.0	0.833	0.014
Daily Maxmum	Qd-max	1,400	58.3	0.972	0.016
Hourly Maximum	Qh-max	2,400	100.0	1.667	0.028

1.2 Unit and Capacity of Treatment Facilities

Facilities	Total	Duty	Stand-by	Capacity
Grit Chamber/Screen	2	1	1	Qh-max
Complete Mix Lagoon	1	1	0	Qd-max
Partial Mix Lagoon	3	3	0	Qd-max
Disinfection Tank	1	1	0	Qd-max

1.3 Discharge

Discharge Point	Nanu Oya
HWL	1852.00 m

#### 1.4 Formula for Hydraulic Calculation

a. Friction loss for streight Darcy-Weisbach	pipe			•
•	h = f * V	^2/(2*	g)	
				/(2000 * D)) * (L/D)
b. Friction loss for fittings				
	h = f * V	^2/(2*	g)	
	where,	f2 =	1.00	(Inlet)
		f3 =	0.50	(Outet)

#### 2. Hydraulic Calculation

2.1 Water Level of Disinfection Tank Effluent Chamber (WL1)

Qd-ave       Qd-max       Qh-max       (Unit)         Design Flow       Q       1,200       1,400       2,400 $m^3/day$ Q       0.014       0.016       0.028 $m^3/day$ Pipe Diameter       150       nm         Pipe Length       50.0 m         No. of Pipe       1 set         Velocity       V =       0.79       0.92       1.57       m/sec         Hydraulic Loss       h =       where,       f1 = $(0.02 + 1/(2000 * D)) * (L/L)$ $f2 = 1.00$ (Inlet) $f3 = 0.50$ (Outet)         Hydraulic Loss       h1 =       0.047       0.064       0.189       m         WL1 =       1852.00 +       h1 =       1852.07       1852.19 m       (Qd-max)       (Qd-max)         2.2 Water Level of Disinfection Tank (WL2)       weir Width       W =       1.0 m       no. of Weir       1 set         Weir Width       W =       1.0 m       no. of Weir       1 set       Weir level       hw =       1852.95 m         Overflow height       h =       (Q/(1.84 * W))^(2/3)       0.061       m	2.1 YY A	ter Level of Disting	COUDE LARK LA	nuoni Chai			
q       0.014       0.016       0.028 $m^3/sec$ Pipe Diameter       150 mm         Pipe Length       50.0 m         No. of Pipe       1 set         Velocity       V =       0.79       0.92       1.57       m/sec         Hydraulic Loss       h =       where,       f1 = (0.02 + 1 / (2000 * D)) * (L / D)       = 7.78E-06 (Straight Pipe)       f2 = 1.00       (Inlet)         f3 = 0.50       (Outet)       f3 = 0.50       (Outet)         Hydraulic Loss       h1 =       0.047       0.064       0.189       m         wL1 =       1852.00       + h1 =       1852.064       1852.189 m       say,       1852.19 m       (Qd-max) (Qh-max)         2.2 Water Level of Disinfection Tank (WL2)       Weir Width       W =       1.0 m       No. of Weir       1 set         Weir Width       W =       1.0 m       No. of Weir       1 set         Weir level       hw =       1852.95 m       Overflow height       h = (Q / (1.84 * W))^{(2/3)})         h2 =       0.038       0.043       0.061       m				Qd-ave	Qd-max	Qh-max	(Unit)
Pipe Diameter       150 mm         Pipe Length       50.0 m         No. of Pipe       1 set         Velocity       V =       0.79       0.92       1.57       m/sec         Hydraulic Loss       h =       where,       f1 = (0.02 + 1 / (2000 * D)) * (L / L)         =       7.78E-06 (Straight Pipe)       f2 = 1.00 (Inlet)         f3 = 0.50 (Outet)       f3 = 0.50 (Outet)         Hydraulic Loss       h1 =       0.047       0.064       0.189       m         WL1 =       1852.00 +       h1 =       1852.054       1852.189 m       say,       1852.19 m       (Qd-max) (Qh-max)         2.2 Water Level of Disinfection Tank (WL2)       Weir Width       W =       1.0 m       No. of Weir       1 set         Weir level       hw =       1852.95 m       Overflow height       h = (Q / (1.84 * W))^(2/3)       1.061       m		Design Flow	Q	1,200	1,400	2,400	m <sup>3</sup> /day
Pipe Length       50.0 m         No. of Pipe       1 set         Velocity       V =       0.79       0.92       1.57       m/sec         Hydraulic Loss       h =         m/sec       m/sec         Hydraulic Loss       h =         m/sec       m/sec         Hydraulic Loss       h =         m/sec       fl = (0.02 + 1 / (2000 * D)) * (L / D) $f2 = 1.00$ (Inlet)          m/sec       m/sec         Hydraulic Loss       h1 =       0.047       0.064       0.189       m         WL1 =       1852.00 +       h1 =       1852.054       1852.189 m       say,       1852.19 m         WL1 =       1852.00 +       h1 =       1852.071       1852.19 m       m       gas,       1852.19 m         Qd-max)       (Qh-max)       (Qh-max)       No. of Weir       1 set       set       m       sat         Weir level       hw =       1852.95 m       M       M       No.061 m       m         Overflow height       h =       (Q/(1.84 * W))^(2/3)       M       M       M       M       M       M       M			q	0.014	0.016	0.028	m <sup>3</sup> /sec
No. of Pipe       1 set         Velocity       V =       0.79       0.92       1.57       m/sec         Hydraulic Loss       h =       where,       f1 = (0.02 + 1 / (2000 * D)) * (L / D)       = 7.78E-06 (Straight Pipe)       = 7.78E-06 (Straight Pipe)       = 7.78E-06 (Straight Pipe)       = 7.78E-06 (Straight Pipe)       = 7.78E-06 (Outet)         Hydraulic Loss       h1 =       0.047       0.064       0.189       m         WL1 =       1852.00       + h1 =       1852.064       1852.189 m       say,       1852.19 m         WL1 =       1852.00       + h1 =       1852.071       1852.19 m       Qd-max)         Veir Width       W =       1.0 m       No. of Weir       1 set       Weir level       hw =       1852.95 m         Overflow height       h = (Q / (1.84 * W))^(2/3)       h.2 =       0.038       0.043       0.061       m		Pipe Diameter		150	mm		
Velocity       V = $0.79$ $0.92$ $1.57$ m/sec         Hydraulic Loss       h =       where, $f1 = (0.02 + 1/(2000 * D)) * (L/D)$ $= 7.78E-06$ (Straight Pipe) $f2 = 1.00$ (Inlet) $f2 = 1.00$ (Inlet) $f3 = 0.50$ (Outet)         Hydraulic Loss $h1 = 0.047$ $0.064$ $0.189$ m         WL1 = $1852.00$ + $h1$ = $1852.064$ $1852.189$ m         say, $1852.07$ $1852.19$ m         (Qd-max)       (Qh-max)         2.2 Water Level of Disinfection Tank (WL2)         Weir Width       W = $1.0$ m         No. of Weir       1 set         Weir level       hw = $1852.95$ m         Overflow height $h = (Q/(1.84 * W))^{(2/3)}$ h2 = $0.038$ $0.043$ $0.061$ m		Pipe Length		50.0	m		
Hydraulic Loss       h =         where, $f1 = (0.02 + 1/(2000 * D)) * (L/D)$ $= 7.78E-06$ (Straight Pipe). $f2 = 1.00$ (Inlet) $f3 = 0.50$ (Outet)         Hydraulic Loss $h1 = 0.047$ $WL1 = 1852.00 + h1 = 1852.064$ $WL1 = 1852.00 + h1 = 1852.064$ $WL1 = 1852.00 + h1 = 1852.07$ $RS2.19 m$ $(Qd-max)$ (Qh-max)         Weir Width $W = 1.0 m$ No. of Weir       1 set         Weir level $hw = 1852.95 m$ Overflow height $h = (Q/(1.84 * W))^{\circ}(2/3)$ $h2 = 0.038$ $0.043$ $0.061$		No. of Pipe		1	set		
where, $f1 = (0.02 + 1/(2000 * D)) * (L/D)$ = 7.78E-06 (Straight Pipe). f2 = 1.00 (Inlet) f3 = 0.50 (Outet) Hydraulic Loss $h1 = 0.047 0.064 0.189 m$ WL1 = 1852.00 + h1 = 1852.064 1852.189 m say, 1852.07 1852.19 m (Qd-max) (Qh-max) 2.2 Water Level of Disinfection Tank (WL2) Weir Width $W = 1.0 m$ No. of Weir 1 set Weir level $hw = 1852.95 m$ Overflow height $h = (Q/(1.84 * W))^{(2/3)}$ h2 = 0.038 0.043 0.061 m		Velocity	V =	0.79	0.92	1.57	m/sec
$= 7.78E-06 (Straight Pipe) .$ $f2 = 1.00 (Inlet) \\ f3 = 0.50 (Outet) \\ Hydraulic Loss h1 = 0.047 0.064 0.189 m \\ WL1 = 1852.00 + h1 = 1852.064 1852.189 m \\ say, 1852.07 1852.19 m \\ (Qd-max) (Qh-max) \\ (Qh-max) \\ Weir Width W = 1.0 m \\ No. of Weir 1 set \\ Weir level hw = 1852.95 m \\ Overflow height h = (Q/(1.84 * W))^{(2/3)} \\ h2 = 0.038 0.043 0.061 m \\ \end{bmatrix}$		Hydraulic Loss	h =				
$f2 = 1.00  (Inlet) \\ f3 = 0.50  (Outet) \\ \hline Hydraulic Loss \qquad h1 = 0.047  0.064  0.189  m \\ \hline WL1 = 1852.00  +  h1 = 1852.064  1852.189 \ m \\ say,  1852.07  1852.19 \ m \\ (Qd-max)  (Qh-max) \\ \hline Weir Width \qquad W = 1.0 \ m \\ No. of Weir \qquad 1 \ set \\ Weir level \qquad hw = 1852.95 \ m \\ Overflow height \qquad h = (Q/(1.84 * W))^{(2/3)} \\ \hline h2 = 0.038  0.043  0.061 \ m \\ \hline \end{array}$			where,	f1 =	(0.02 + 1)	' ( 2000 * D	))*(L/D
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				=	7.78E-06	(Straight Pi	pe).
Hydraulic Loss       h1 = $0.047$ $0.064$ $0.189$ m         WL1 =       1852.00       +       h1 =       1852.064       1852.189       m         say,       1852.07       1852.19       m       (Qd-max)       (Qh-max)         2.2 Water Level of Disinfection Tank (WL2)       Weir Width       W =       1.0       m         No. of Weir       1       set       Weir level       hw =       1852.95       m         Overflow height       h =       (Q/(1.84 * W))^(2/3)       h2 =       0.038       0.043       0.061       m				f2 =	1.00	(Inlet)	· · ·
WL1 = 1852.00 + h1 = 1852.064 1852.189 m say, 1852.07 1852.19 m (Qd-max) (Qh-max) $2.2 \text{ Water Level of Disinfection Tank (WL2)}$ Weir Width W = 1.0 m No. of Weir 1 set Weir level hw = 1852.95 m Overflow height h = (Q/(1.84 * W))^(2/3) $h2 = 0.038 0.043 0.061 m$		5		f3 =	0.50	(Outet)	
say, $1852.07$ 1852.19 m (Qd-max) (Qh-max) 2.2 Water Level of Disinfection Tank (WL2) Weir Width W = 1.0 m No. of Weir 1 set Weir level hw = 1852.95 m Overflow height h = (Q/(1.84 * W))^(2/3) h2 = 0.038 0.043 0.061 m		Hydraulic Loss	h1 =	0.047	0.064	0.189	m
(Qd-max)  (Qh-max) 2.2 Water Level of Disinfection Tank (WL2) Weir Width $W = 1.0 \text{ m}$ No. of Weir 1 set Weir level $hw = 1852.95 \text{ m}$ Overflow height $h = (Q/(1.84 * W))^{(2/3)}$ h2 = 0.038  0.043  0.061  m		WL1 =	1852.00	+ h1 =	1852.064	1852.189	m
2.2 Water Level of Disinfection Tank (WL2) Weir Width $W = 1.0 \text{ m}$ No. of Weir 1 set Weir level $hw = 1852.95 \text{ m}$ Overflow height $h = (Q/(1.84 * W))^{(2/3)}$ h2 = 0.038 0.043 0.061  m				say,	1852.07	1852.19	m
Weir Width       W =       1.0 m         No. of Weir       1 set         Weir level       hw =       1852.95 m         Overflow height       h = $(Q / (1.84 * W))^{(2/3)}$ h2 =       0.038       0.043       0.061 m				_		(Qh-max)	
Weir Width       W =       1.0 m         No. of Weir       1 set         Weir level       hw =       1852.95 m         Overflow height       h = $(Q / (1.84 * W))^{(2/3)}$ h2 =       0.038       0.043       0.061 m							
No. of Weir1 setWeir level $hw = 1852.95 \text{ m}$ Overflow height $h = (Q/(1.84 * W))^{(2/3)}$ $h2 = 0.038$ $0.043$ $0.061$ m	2.2 W		•	,			
Weir levelhw = $1852.95 \text{ m}$ Overflow heighth = $(Q/(1.84 * W))^{(2/3)}$ h2 = 0.0380.0430.061			W =				
Overflow height $h = (Q / (1.84 * W))^{(2/3)}$ $h2 = 0.038$ 0.0430.061m							
h2 = 0.038 0.043 0.061 m						· · ·	
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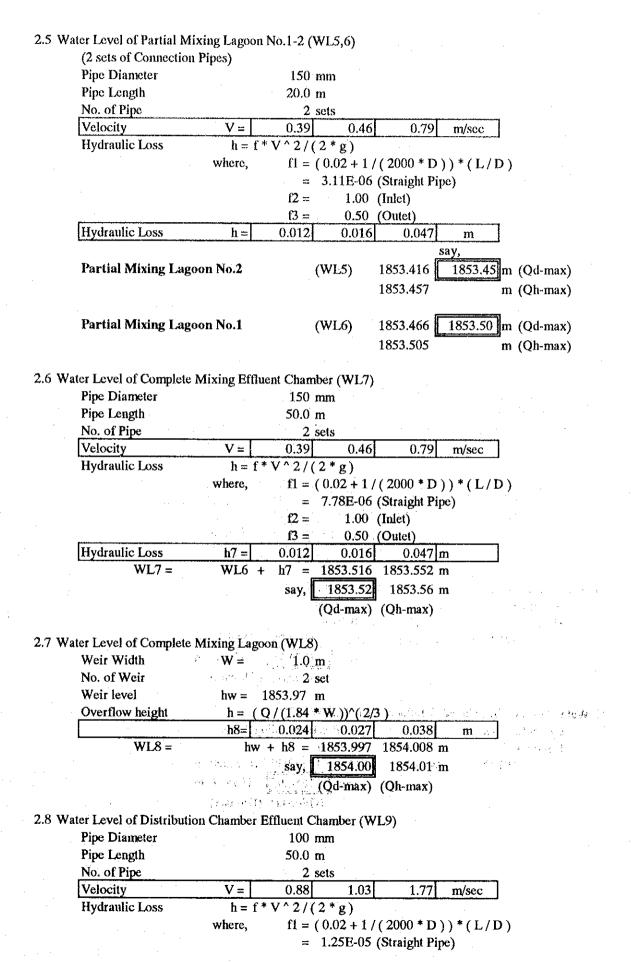
m	
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#### 2.3 Water Level of Partial Mixing No.3 Effluent Chamber (WL3)

	Pipe Diameter	150 mm						
	Pipe Length	50.0 m						
	No. of Pipe		1 se	1 sets				
•	Velocity	V =	0.79	0.92	1.57	m/sec		
	Hydraulic Loss	$h = f^*$	V^2/(2	*g)				
		where,	f1 = (0)	0.02 + 1 /	(2000 * D	))*(L/D)		
			= 7	.78E-06	(Straight Pi	ipe)		
			f2 =	1.00	(Inlet)			
			f3 =	0.50	(Outet)	1		
	Hydraulic Loss	h3 =	0.047	0.064	0.189	m		
	WL3 =	WL2 +	h3 = 1	853.064	1853.209	m		
			say,	1853.07	1853.21	m		
			(	Qd-max)	(Qh-max)			

2.4 Water Level of Partial Mixing Lagoon No.3 (WL4)

Weir Width	W = 1.0 m	
No. of Weir	2 set	
Weir level	hw = 1853.37 m	
Overflow height	$h = (Q / (1.84 * W))^{(2/3)}$	
· , · , ·	h4= 0.024 0.027 0.03	88 m
WL4 =	hw + h4 = 1853.397 1853.40	)8 m
	say, 1853.40 1853.4	11 m
	(Qd-max) (Qh-ma	x)
	À-13.5-2	



#### A-13.5-3

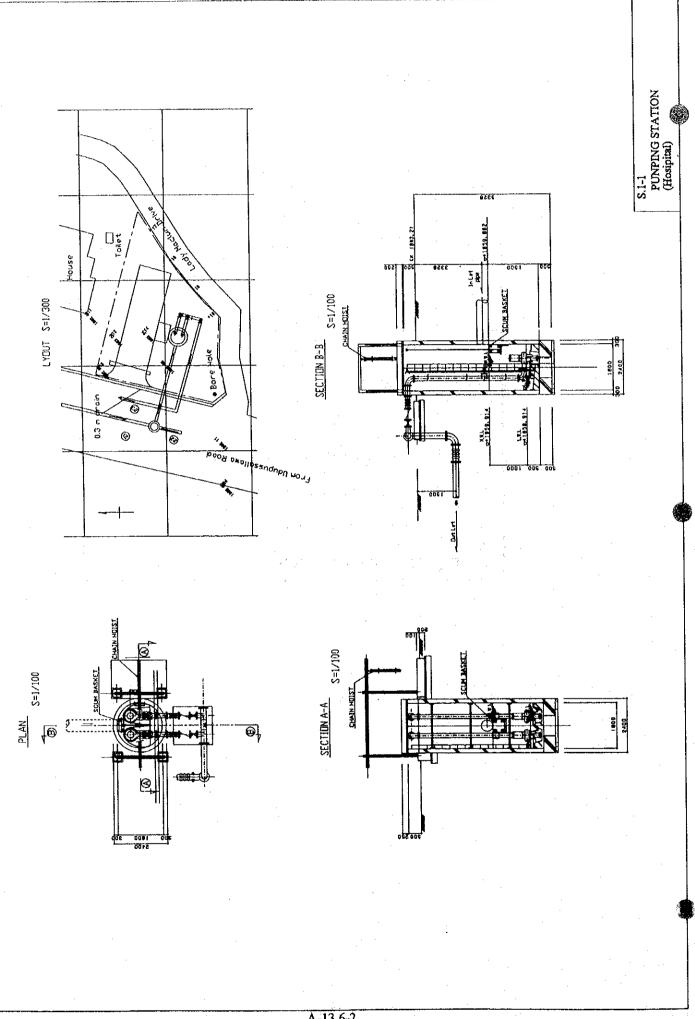
	f2 = 1.00 (Inlet)
	$f_{3} = 0.50$ (Outet)
Hydraulic Loss	h9 = 0.060 0.082 0.240 m
WL9 =	$WL8 + h9 = 1854.082 \ 1854.250 \ m$
WL) -	say, 1854.10 1854.25 m
	(Qd-max) (Qh-max)
2.9 Water Level of Distribution	n Chamber (WL10)
Weir Width	W = 0.5  m
No. of Weir	2 set
Weir level	hw = 1854.30 m
Overflow height	$h = (Q/(1.84 * W))^{(2/3)}$
[	h10 = 0.038  0.043  0.061  m
WL10 =	$hw + h10 = 1854.343 \ 1854.361 \ m$
	say, 1854.35 1854.37 m
	(Qd-max) (Qh-max)
2.10 Water Level of Parshall Flo	lum Effluent Chamber (WL11)
Pipe Diameter	150 mm
Pipe Length	50.0 m
No. of Pipe	1 sets
Velocity	V = 0.79  0.92  1.57  m/sec
Hydraulic Loss	$h = f * V^2/(2 * g)$
•	where, $f1 = (0.02 + 1 / (2000 * D)) * (L / D)$
	= 7.78E-06 (Straight Pipe)
	f2 = 1.00 (Inlet)
	f3 = 0.50 (Outet)
Hydraulic Loss	h11 = 0.047  0.064  0.189  m
WL11 =	WL10 + h11 = 1854.414 1854.559 m
	say, <u>1854.45</u> 1854.56 m
	(Qd-max) (Qh-max)
2.11 Water Level of Parshall F	Flum Influent Chamber (WL12)
No. of PF	1 set
Head loss	h12 = 0.30 m
WL12 =	WL11 + h12 = 1854.75 1854.86 m
	say, <u>1854.75</u> 1854.86 m
	(Qd-max) (Qh-max)
2.12 Water Level of Grit Chan	mber Influent Chamber (WL13)
No. of Screens	8 sets including 2 stes
Head loss	h13 = 0.20 m
WL13 =	$WL12 + h13 = 1854,950 \ 1855.060 \ m$
	say, 1854.95 1855.06 m
	(Qd-max) (Qh-max)

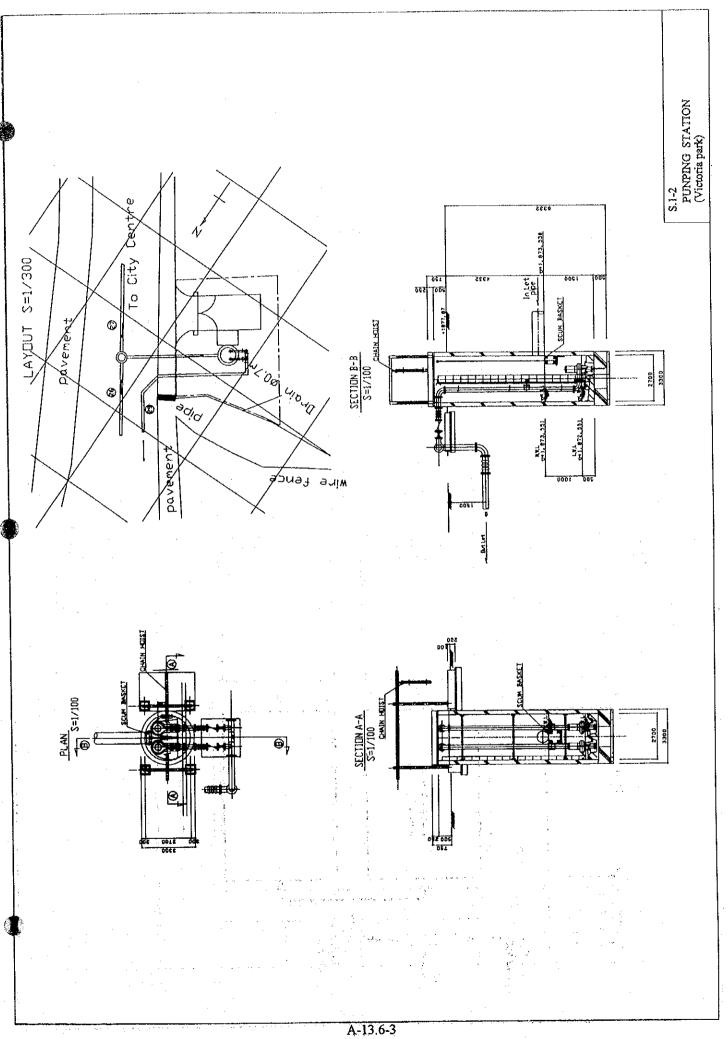
A-13.5-4

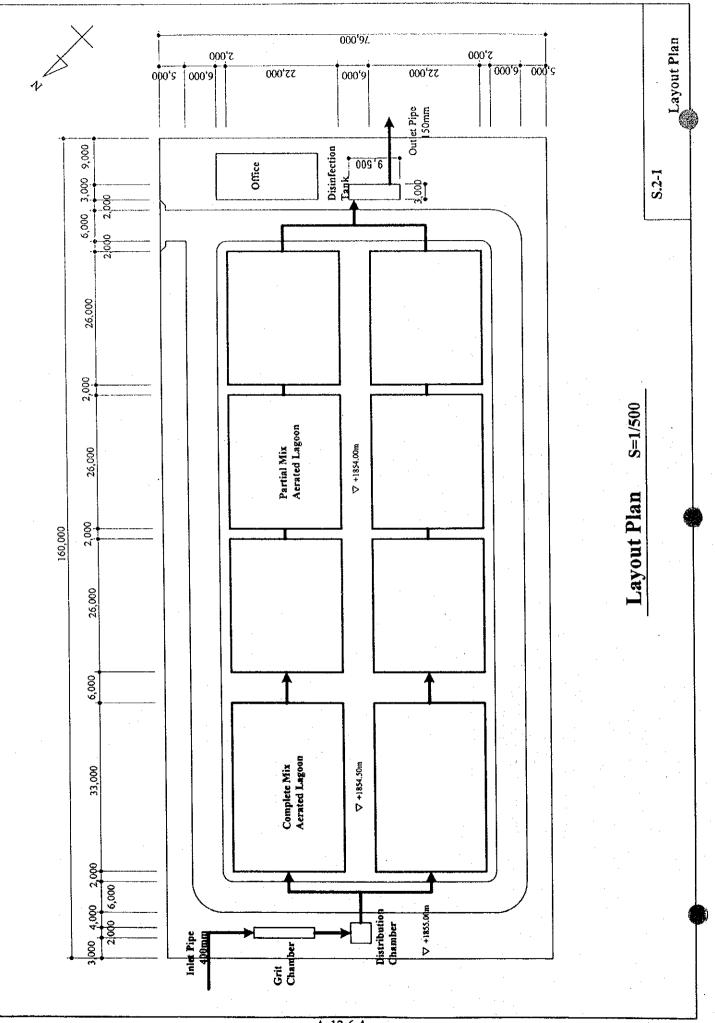
## Appendix 13.6 DRAWING

No.	DRAWING NAME
S.1-1	PUMP STATION (HOSPITAL)
S.1-2	PUMP STATION (VICTORIA PARK)
S.2-1	LAYOUT PLAN
S.2-2	HYDRAULIC PROFILE
S.2-3	FLOW DIAGRAM
S.2-4	GRID CHAMBER
S.2-5	COMPLETE MIXING AERATED LAGOON
<b>S.2-</b> 6	PARTIAL MIXING AERATED LAGOON
S.2-7	CHLORINATION TANK
S.2-8	ADMINISTRATION BUILDING

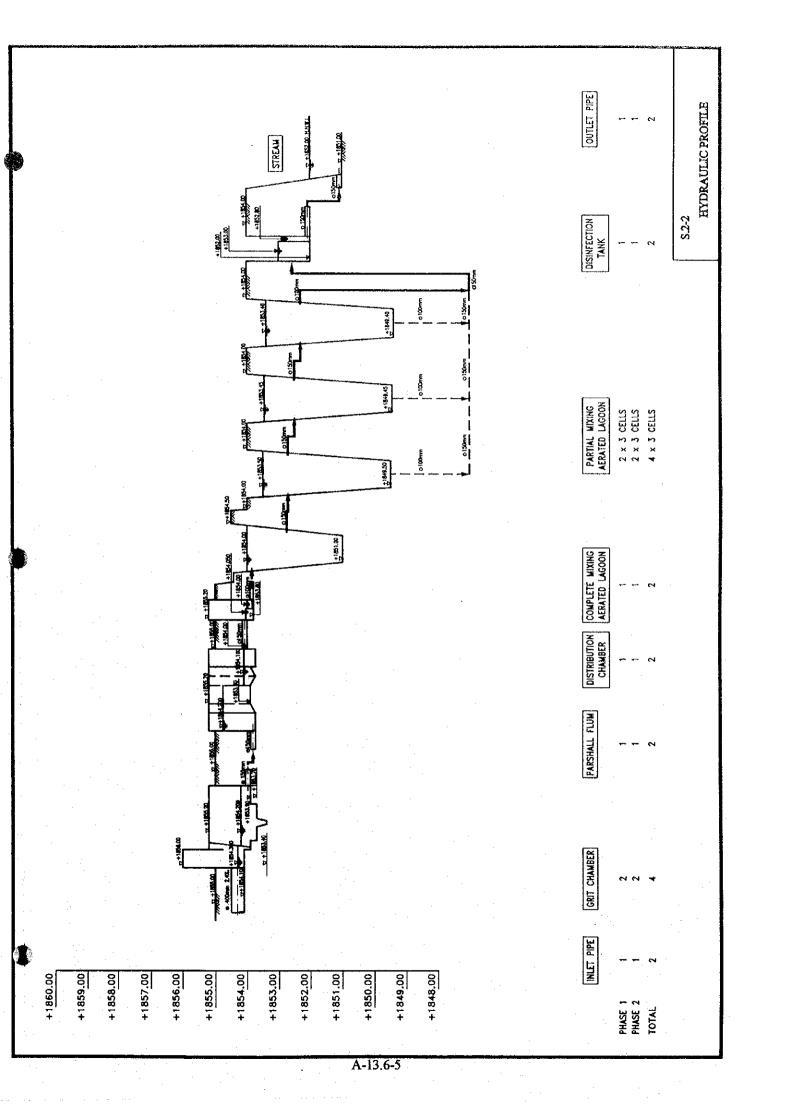
### DRAWING LIST

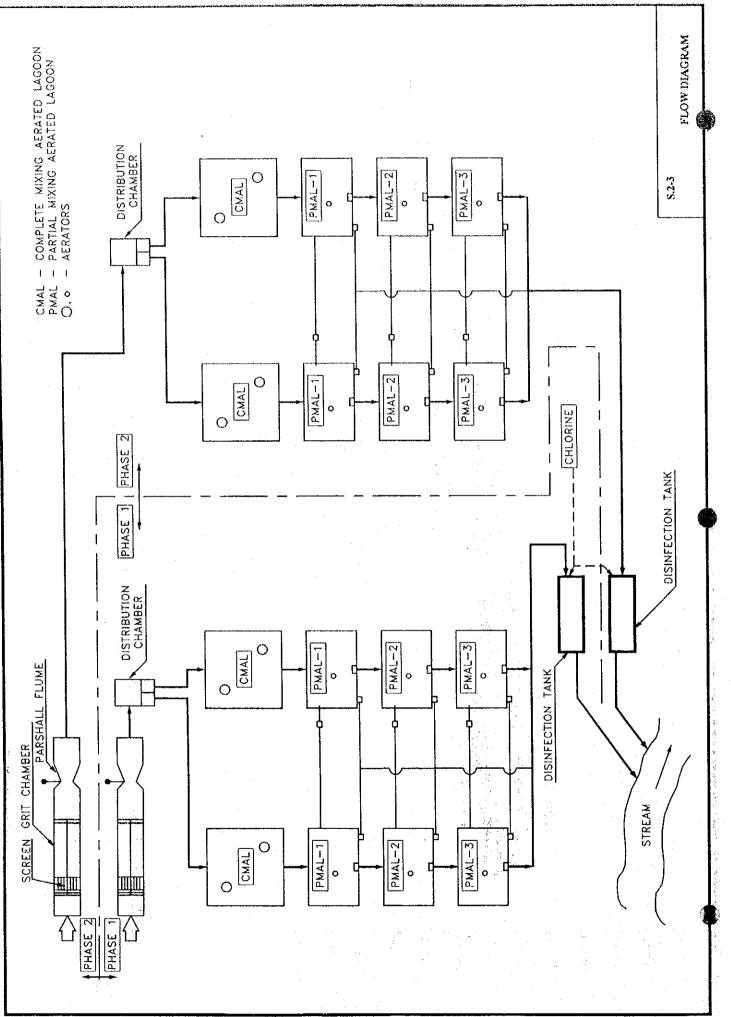


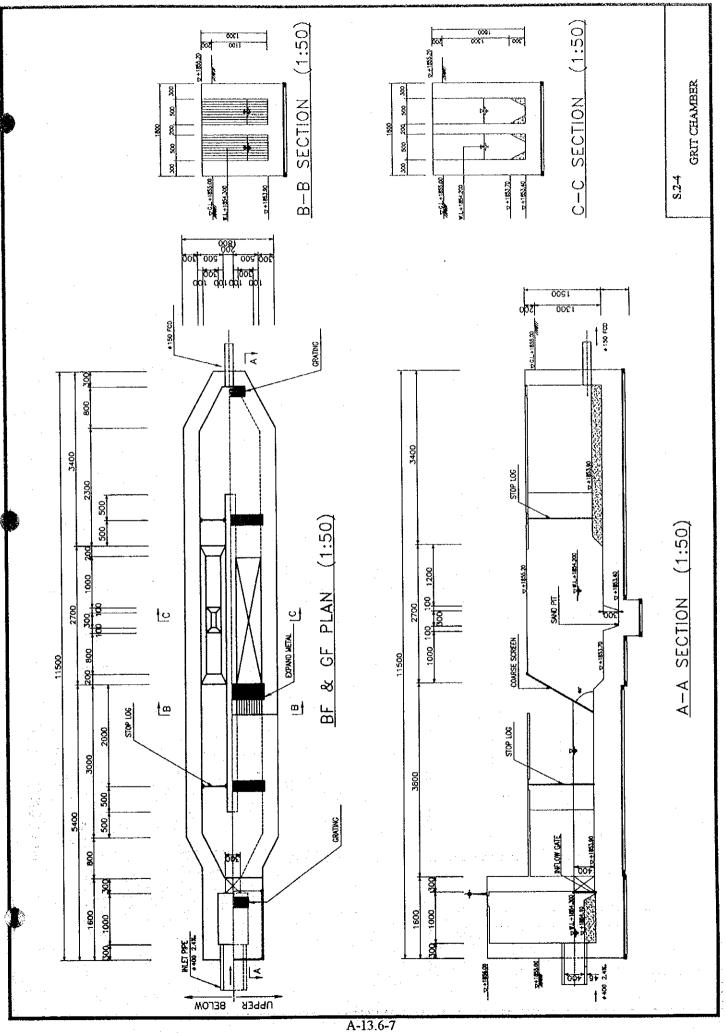


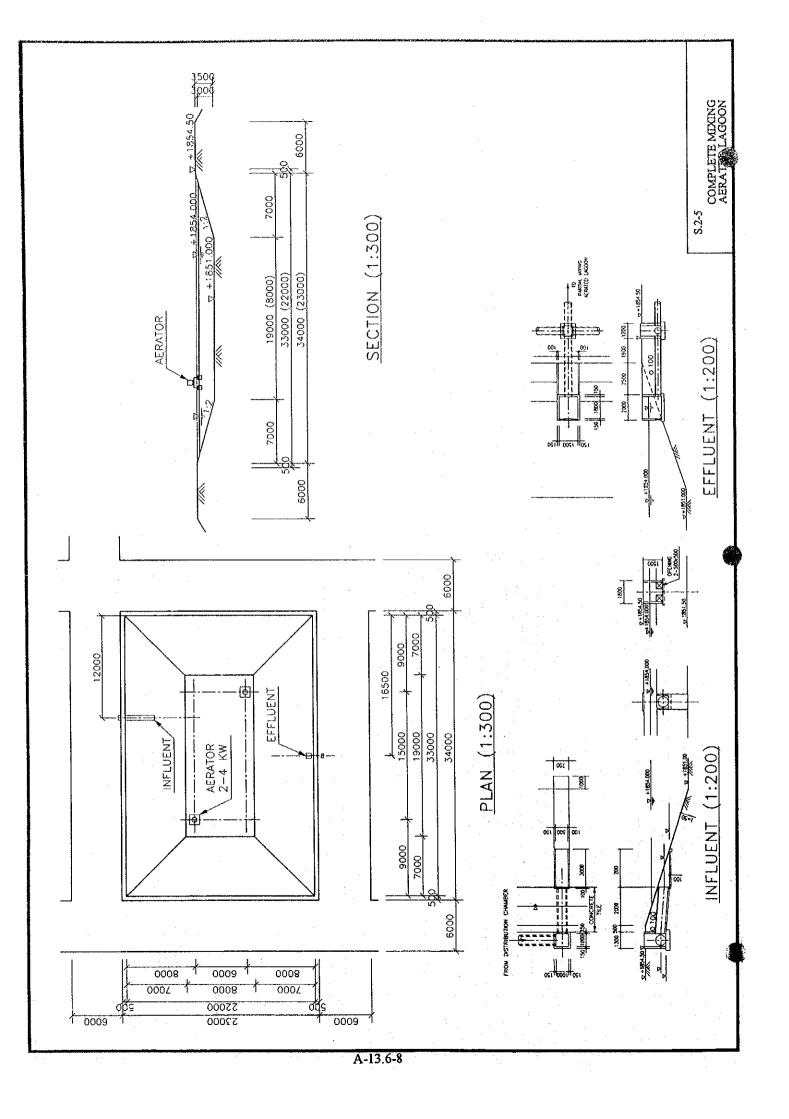


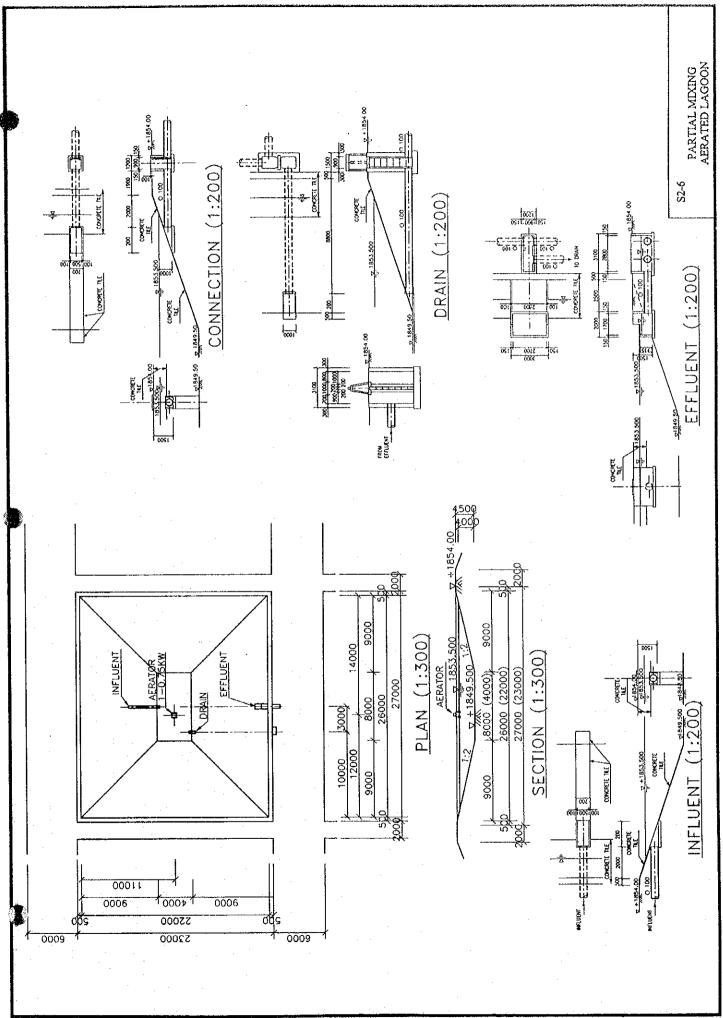
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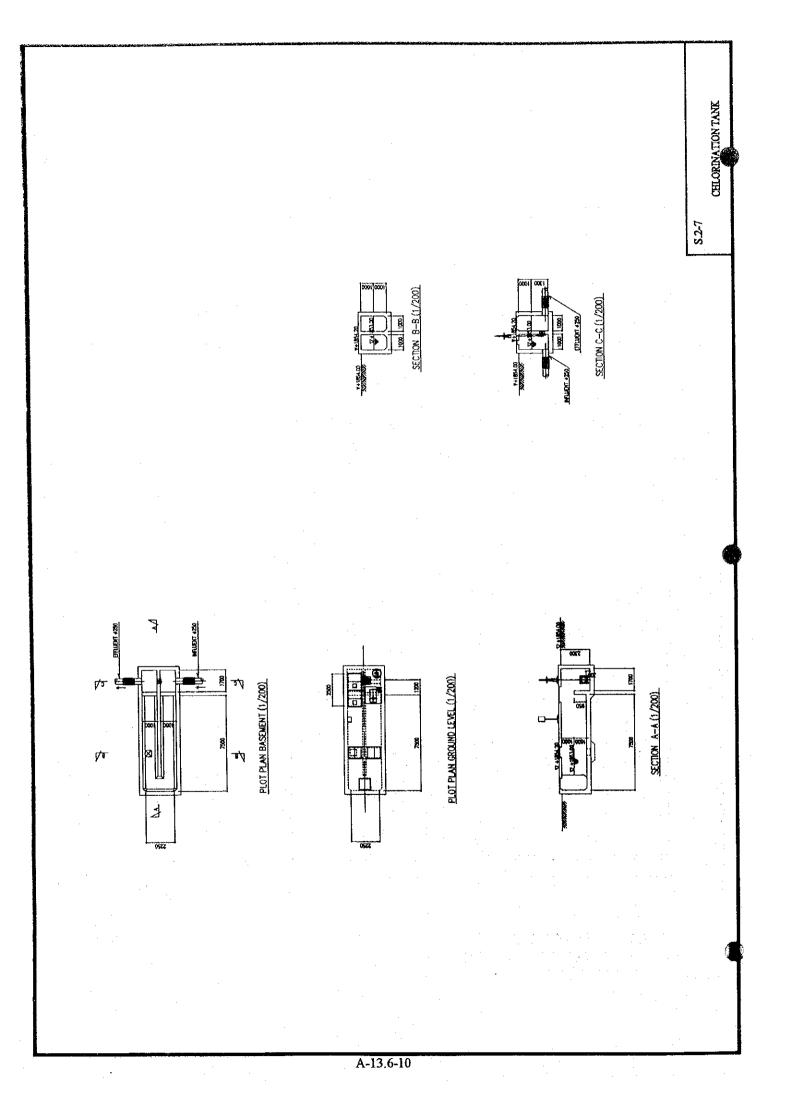


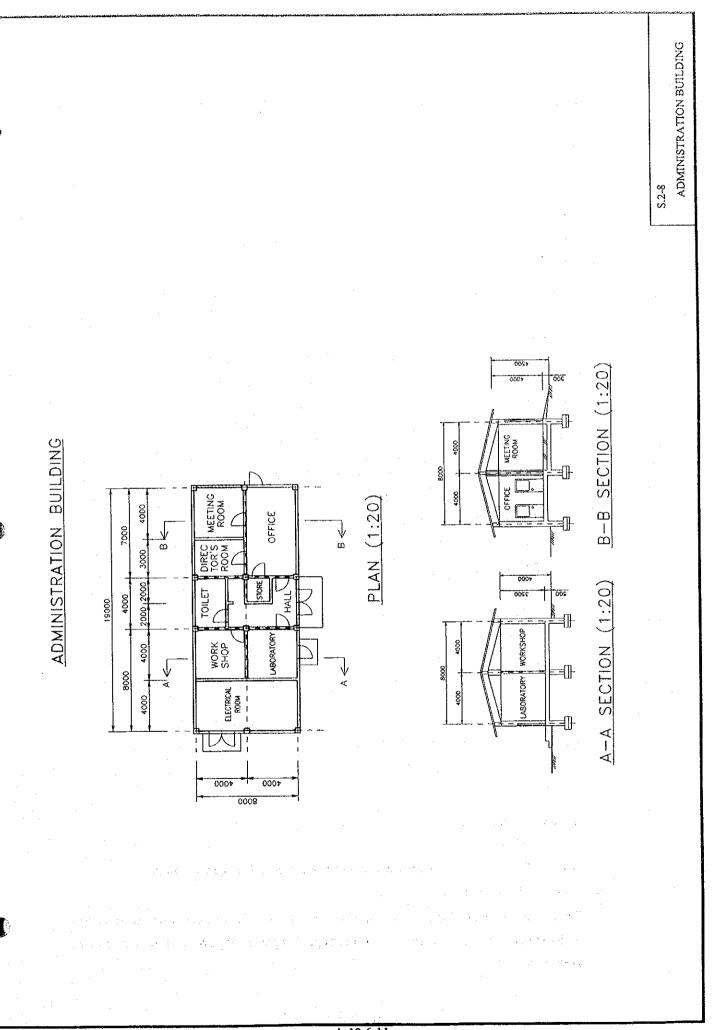






5-9





### Appendix 13.7 Storage Capacity of Sewer (Nuwara Eliya)

Phase 1 (2005)

#### 1. Hospital Pumping Station

(1) Sewage Flow

 $Q_{HM} = 0.89 \text{ m}3/\text{min} = 53.4 \text{ m}3/\text{hour}$  (Hourly Maximum Sewage Flow to Ps)

(2) Sewer to be used for Sewage

Since the lowest elevation near the pumping Station is +1,861.73m, sewers with invert level of +1,861.5m is considered to use for sewer storage. Length and Pipe Nos. of these sewers are as follows;

No. 19	Ø225	L = 150 m (Allowance 100%)
No. 21	Ø225	L = 120 m (Allowance 100%)

(3) Manhole

Nos. of Manhole $\frac{150 + 120}{50} \div 6$  (50m pitch)Manhole Depth1861.93 - 1860.482 = 1.25 m<br/>(No. 21)

- (4) Calculation of Storage Capacity
  - a) Sewer

$$\frac{0.225^2 \times 3.14}{4} \times (150 + 120) \times (1 - \frac{1}{2.0}) = 5.4 \text{ m}^3$$

b) Manhole

$$\frac{0.9^2 \times 3.14}{4} \times (1.25 - 0.225) \times 6 = \frac{3.9 \text{ m}^3}{70 \text{ tal}}$$

(5) Storage Time

 $\frac{9.3 \text{ m}^3}{53.4 \text{ m}^3/\text{day}} = 0.17 \text{ hour} = 10.4 \text{min}$ 

#### 2. Victoria Park Pumping Station

(1) Sewage Flow

 $Q_{HM} = 2.82 \text{ m}^3/\text{min} = 169.2 \text{ m}^3/\text{hour}$  (Hourly Maximum Sewage Flow to PS)

(2) Sewer to be used for Sewage

Since the lowest elevation near the pumping Station is +1,877m, sewers with invert level of +1,876.5m is considered to use for sewer storage. Length and Pipe Nos. of these sewers are as follows;

No.27	Ø225	L = 150 m	(Allo	wance 10	0%)
No.26	Ø300	L = 520 m	(	//	)
No.12	Ø300	L = 200 m	(	11	)
No.28	Ø150	L = 200 m	(	//	)

(3) Manhole

a)

Nos. Manhole  $\frac{150+520+200+200}{50} \doteq 22$  (50m pitch) Manhole Depth 1877.26-1874.556 = 2.70 m (No.26)

(4) Calculation of Storage Capacity

Sewre 
$$\left\{ \frac{0.225^2 \times 3.14}{4} \times 150 + \frac{0.300^2 \times 3.14}{4} \times (520 + 200) + \frac{0.1502 \times 3.14}{4} \times 200 \right\}$$

$$\times (1 - \frac{1}{2.0}) = 30.2 \text{ m}^3$$

b) Manhole

$$\frac{0.9^2 \times 3.14}{4} \times (2.7 - 0.30) \times 22 = 33.6 \,\mathrm{m}^3$$

Total 63.8 m<sup>3</sup>

(5) Pipe Storage Time

 $\frac{63.8 \text{ m}^3}{169.2 \text{ m}^3/\text{hour}} = 0.38 \text{ hour} = 22.6 \text{ min}$ 

# Chapter 14

# Appendix 14.1 Annual Operation and Maintenance Cost

## Appendix 14.1 Annual Operation and Maintenance Cost

#### Nuwara Eliya

## Master Plan Alternative 1 (Applied) -Operation Starting 2014

T4		Electricity					Man-Power			Spare Parts	
Item	m3/day	m3/hr	hrs	kW	kWh	Rs/month	No.	Rs/month	Rs/month	Cost	Rs/month
1. Sewer							3	6,000	18,000		
2. Pumping Station											
Nuwara Eliya											
P/S 1	985	53	18.4	11	203	34,599	0	6,000	0	3,553	2,961
P/S 2	2,506	169	14.8	22	326	51,559	0	6,000	0	4,602	3,835
3. Sewage Treatment Plant											
Nuwara Eliya	2,700	)m3/day	24	35	840	122,520	5	6,000	30,000	78,957	65,798
Hospital/Brewery											
4. Chlorine	2,338	2 mg/l				4,286					
5. Maintenance							2	10,000	20,000		
6. Manager/Engineer				1			2	15,000	30,000		
Sub-Total						212,964	12		98,000	87,112	72,593
Total		• • • •									
month 383,557					Chlorine	Electricity			Man-Power		Spare Parts
year 4,602,683					51,427	2,504,137			1,176,000		871,120
	•				L	• • • • • • • • • • • • • • • • • • • •				-	

#### Master Plan Alternative 2 (Not Applied)

<b>.</b>		Electricity					Man-Power			Spare Parts	
Item	m3/day	m3/hr	hrs	kW	kWh	Rs/month	No.	Rs/month	Rs/month	Cost	Rs/month
1. Sewer							3	6,000	18,000		
2. Lift Station											
Nuwara Eliya											
L/S 1	747	53	14.0	3.7	52	13,746	1	6,000	6,000	3,266	2,722
L/S 2	1,745	116	15.1	15	226	37,798	0	6,000	0	4,294	3,578
3. Sewage Treatment Plant											
Nuwara Eliya	2,500	m3/day	24	35	840	122,520	5	6,000	30,000	74,477	62,064
Hospital/Brewery	200	)m3/day	24	10	240	39,720	2		0	22,664	18,887
4. Chlorine	2,338	2 mg/l				4,286					
5. Maintenance							2	10,000	20,000		
6. Manager/Engineer							2	15,000	30,000		
Sub-Total					· ·	218,070	15		104,000	104,701	87,251
Total		······									
month 409,321					Chlorine	Electricity			Man-Power		Spare Parts
year 4,911,846					51,427	2,565,409			1,248,000		1,047,010

### Feasibility Study -Operation Starting 2004

8/

· .		Electricity					Man-Power			Spare Parts	
Item	m3/day	m3/hr	hrs	k₩	kWh	Rs/month	No.	Rs/month	Rs/month	Cost	Rs/month
1. Sewer							2	6,000	12,000		
2. Pumping Station								· .			
Nuwara Eliya											
P/S 1	985	53	18.4	11	203	34,599	0	6,000	0	3,553	2,961
P/S 2	2,506	169	14.8	22	326	51,559	0	6,000	0	4,602	3,835
3. Sewage Treatment Plant											
Nuwara Eliya	1,400	m3/day	24	21	504	76,152	3	6,000	18,000	40,116	33,430
Hospital/Brewery											
4. Chlorine	1,220	2 mg/l				2,236					
5. Maintenance							1	10,000	10,000		
6. Manager/Engineer							2	15,000	30,000		
Sub-Total						164,546	8		70,000	48,271	40,226
Total											
month 274,772					Chlorine	Electricity			Man-Power		Spare Parts
year 3,297,266					26,835	1,947,721	l		840,000		482,710

# Chapter 15

Appendix 15.1	<b>Initial Environmental Examination</b>
	Findings and Conclusions
Appendix 15.2	Water Quality Survey

(Wet Season)

Appendix 15.3 Water Quality Survey (Dry Season)

Appendix 15.4 Land Acquisition Procedures

Appendix 15.5 Wastewater Treatment Plants

Monitoring and Reporting Program

#### Appendix 15.1

Greater Kandy -- EIA -- Appendix 15/A -- IEE findings and conclusions

## INITIAL ENVIRONMENTAL EXAMINATION

### FINDINGS AND CONCLUSIONS

#### (EXECUTIVE SUMMARY)

#### 1. Purpose of the Initial Environmental examination

The Initial Environmental Examination (IEE) is conducted as an integral part of the Water Supply and Environmental Improvement Master Plan for the Greater Kandy and Nuwara Eliya areas.

The IEE has the following specific objects:

1) to achieve a sound knowledge of the actual condition of the environment within the project impact areas;

based on this, to preliminarily assess the possible and/or potential environmental impacts which may be realized through the implementation of the proposed Water Supply (WS) and Waste Water (WW) projects, and

 to assess the need of implementing a full Environmental Impact Assessment (EIA), which, if necessary, will be conducted as an integral part of the Feasibility Studies which will follow the Master Plan.

#### 2. Served population and water demand

#### 2.1 Kandy Municipal

- 1) Served population in 1998 is 554,310 persons;
- 2) Served population in 2015 will be 694,160 persons;
- 3) Present water demand is 117,200 m3/day (211 L/persons\*day)
- 4) Water demand in 2015 will be 195,900 m3/day (282 L/persons\*day)

#### 2.2 Nuwara Eliya

1) Served population in 1998 is 25,500 persons;

#### A-15.1-1

2) Served population in 2015 will be 51,400 persons;

- 3) Present water demand is 6,161 m3/day (241.6 L/person\*day)
- 4) Water demand in 2015 will be 16,320 m3/day (317.5 L/person\*day)

#### 3. Project description

#### 3.1 Water supply

#### 3.1.1 Kandy Municipal

- Extraction of additional 42,500 m3/day at existing Kandy Municipal Plant (actual capacity 33,400 m<sup>3</sup>/day);
- Up to 118,000 m<sup>3</sup>/day new treatment plant at Polgolla (actual capacity: 1440 m<sup>3</sup>/day)
- 3) Construction of 254 Km of transmission mains, ranging from 110 mm to 900 mm in diameter;
- 4) 61 reservoirs with a total storage capacity of 32,925 m<sup>3</sup>;
- 5) 45 pump stations, most of which will be located adjacent to reservoirs or treatment facilities.

#### 3.1.2 Nuwara Eliya

- 1) Expansion of groundwater water sources;
- Expansion of existing stream supply at Bambarakele by construction of a new dam;
- Expansion of existing Lovers Leap stream supply with construction of two new dams;
- 4) New supply from a stream near Jayalauka with a new dam and 10-12 Km transmission main.

Existing transmission and distribution system will require upgrade to handle additional supply.

#### 3.2 Wastewater treatment

#### 3.2.1 Greater Kandy

Three separate sub-areas are considered for priority interventions in the Greater Kandy Area: 1) Kandy Municipal, 2) Katugastota and 3) Akurana.

#### 1) Kandy Municipal

- New Treatment Plant, aerated lagoons, to be located in Getambe, with capacity of 90 L/s (about 8,000 m3/day). Required area is 2.7 ha.
- 2) Collection mains with diameter varying from 200 to 100m mm, for a total length of 20.13 km.
- 3) Two pump stations, with capacity of 8 L/sec and 100 L/sec, located at Lake side and Railroad.

#### 2) Katugastota

- New treatment plant, aerated lagoons, with capacity of 6.5 L/s. (561 m3/day).
   Total area required 0.5 ha.
- 2) 6.5 Km of collection mains, with diameter varying from 200 mm to 300 mm;
- 3) Two pump stations with capacity 3 L/s and 9 L/s, located at the bridge and at treatment plant site.

#### 3) Akurana

19400

- New treatment plant, aerated lagoons, with capacity of 6.0 L/s. (518 m3/day). Total area required: 0.5 ha.
- 2) 1.9 Km of collection mains, with diameter varying from 200 mm to 300 mm.

#### 3.2.2 Newara Eliya

The following WW treatment facilities are planned in Nuwara Eliya (FIG 2.2):

- 1) New treatment plant, aerated lagoons, with capacity of 20 L/sec (1728 m3/day), located in an area south of the Recreational Ground. Total required land is 0.5 ha;
- 2) 12.4 Km of collection mains, with diameter varying from 200 mm to 300 mm;
- 3) Two pump stations with capacity 9 L/s and 20 L/s, located at the brewery and at racetrack.

#### 4. Summary review of beneficial/adverse impacts

- The purpose of the present project is to prevent or alleviate the effect on the environment produced by the discharge of untreated or inadequately treated wastewater, and to improve the quality of life of resident people by increasing the amount of safe drinkable water supplied. When properly planned, designed, constructed and managed, the project will therefore have an overall beneficial impact on the environment.
- 2) The most important beneficial impacts will be:
- Reduction of public nuisance, because of increased safe water sources and reduction of open air sewers in urban areas;
- Improvement of public health, because of reduction of water vector diseases;
- Improvement of surface and underground water quality, because of reduction of untreated wastewater discharge.
- 3) The major permanent negative effect will be dislocation or resettlement of a few families actually living in the area selected for the new Polgolla water treatment plant. Resettlement, even if concerning a limited number of families, should be done in compliance with Sri Lankan Laws and regulations (see Par. 4.4). Compensation should be adequate in order to guarantee that dislocated/resettled families after the project will be "equal or better" than before.
- 4) Land acquisition for plant siting may also represent a problem, because almost all lands are private and chances of finding public lands where treatment plants or pumping stations may be sited are minimal.
- 5) Water quality in receiving surface and underground water bodies is likely to improve, because many raw sewage discharges will be replaced by a single treated waste water discharge, with strong reduction in the contaminants' content.
- 6) Major negative impact during construction will be on traffic and transportation, especially in densely populated urban areas, because of construction of mains. Kandy Municipal, Nuwara Eliya Municipal, and some of the minors town in Kandy District (Katugastota and Arakuna) will be affected.

- 7) A preliminary survey on traffic intensity in critical points of Kandy District has been carried out during the present study. Applicable mitigation measures (such as traffic diversion) will be studied in the EIA, but disturbances to population cannot be completely offset. A sound and thorough information campaign will also be helpful to mitigate the effects of public nuisance.
- 8) Noise and vibrations during construction are a routinely concern of EIA for projects which include deep trench excavation in urban areas, and may represent a critical issue in specific areas (high level residential areas, schools, hospitals). Mitigation measures will be provided in the EIA, but it is evident that negative impact cannot be completely offset. Again, an information campaign may help to overcame residents' complaints. Fortunately, this will be a temporary impact.
- 9) Offensive odors can be controlled at WS treatment plants, but are present at WW treatment plants, as a consequence of anaerobic decomposition. Impacts may be offset using adequate odor control techniques and with proper plant siting.
- 10) An important issue will be safety of workers and general public during construction, considering that all works will be conducted in densely populated areas. Suggestions on how to mitigate these effects will be given in the EIA. A specific Control and Monitoring Plan will be needed, establishing responsibilities as well as routinely and emergency procedures to be followed.
- 11) To make sure that the project will benefit the environment as expected, all domestic, public and commercial uses within the service areas should be required to connect to the system on a mandatory basis. The NWSDB, CEA and the Municipalities of Kandy and Nuwara Eliya, should be responsible for the enforcement of this measure.

#### 5. Intensity of Impacts

Intensity of impacts is evaluated according to criteria established by CEA and reported at Para. 2.3, page 9 of "Guidance for Implementing the Environmental Impact Assessment (EIA) Process. Intensity is referred to permanent impacts only. An overall evaluation will be given for each criteria, turning for details to the previous Environmental Impact Matrix and/or to the specific chapters.

#### A-15.1-5

Criteria for impacts' intensity evaluation	Degree of intensity		
Degree to which the proposed action will affect public health or safety	Highly positive		
Degree to which the proposed action will affect unique characteristics of a geographical area.	None		
Degree to which the impacts on the environment and related social conditions are likely to be highly controversial:	Minor controversies may arise related to resettlement of families in Kandy and land acquisition procedures;		
Degree to which the possible effects on environment are highly uncertain on involve unique or unknown risks	None		
Anticipated cumulative significant impacts which cannot be avoided / offset or mitigated:	None		
Degree to which the proposed action may affect the right of future generation to benefit from environmental and cultural resources:	None		

#### Intensity of impacts

## 6 Conclusions about EIA requirement

#### 6.1 General

According to present Sri Lankan regulations, the water extraction, WS treatment plants, WW treatment plants and appurtenant works which are part of the present project, are subject to the EIA process only as plant siting is concerned. The laying of pipeline in Kandy, Nuwara Eliya and minor town of Kandy District is not a prescribed project and therefore is not required to follow the EIA process. However, because of the potential social and environmental impacts arising out of this activity, it is recommended to formulate a sound management plan for this activity which will minimize the adverse impacts on the society and the natural environment.

EIA requirement for the different project components are summarized in Table 6.2.

#### 6.2 Recommendations of Central Environmental Authority

The following procedure is recommended by the Central Environmental Authority

- 1. NWSDB will officially submit the IEE to CEA;
- CEA will examine the report, and will assess if an EIA is needed or not, and to which extent. This step is necessary because the regulations expressed in Gazette 722/22 are to be considered as a general reference, and are subject to interpretation of the CEA;
- 3. CEA, on the base of IEE findings, will officially communicate to the NWSDB, within a two weeks period, if an EIA is definitely required or not.
- 4. If an EIA is required, the PP will also officially apply to the CEA, to know which will be the PAA entitled for revision and approval of the EIA;
- 5. The CEA will name a PAA and will officially communicate the name of the Agency to the PP.

#### 6.3 Consultant's recommendations and justification for an EIA

Considering the preliminary evaluation of anticipated environmental effects presented in Chapter 5, and the recommendations received by the CEA in Colombo, it's the Consultant's opinion that an EIA is fully justified and will be needed. The EIA must comply with both JICA and Sri Lankan CEA regulations. Terms of Reference are given in Chapter 7.

# **POSTGRADUATE INSTITUTE OF SCIENCE**

# UNIVERSITY OF PERADENIYA PERADENIYA SRI LANKA

# **Report on**

# WATER QUALITY EXAMINATION

# In the Kandy and Nuwara-Eliya Districts

# Second phase - Rainy Season

## Submitted to

## JICA study Team, NWSDB,Kandy

## By

Prof. O.A.lleperuma (Project co-ordinator) Department of Chemistry University of Peradeniya Peradeniya, Sri Lanka

September 8,98

#### **INTRODUCTION**

An agreement was signed between the JICA study team and the Postgraduate Institute of Science, University of Peradeniya in March 1998 for the chemical and biological analysis of water quality of springs, streams, ground water sources, raw sewage, water bodies (rivers and lakes) and sludge. This study was to take in two phases namely, the dry season and the rainy season. The report for the phase 1 of this project (dry season) has already been submitted and the present report is on the study carried out during the rainy season. This reason season from July to September was quite normal with intermittent dry days. The dry season in contrast was quite unusual in that it was an exceptionally warm dry season in the hill country. The study area covered the greater Kandy area and the Nuwara Eliya basin. The corresponding collection points are depicted in the attached maps.

#### Experimental

Samples were collected in cleaned acid washed bottles and sampling was carried out according to accepted methods. Sample preservation depending on the parameter to be analysed was carried out in situ. The general procedures employed for all analytical determinations are those given in "Standard Methods for the Examination of Water and Wastewater" 19<sup>th</sup> edition (1995) published by the American Public Health Association, Washington, D.C. The following table gives the analytical procedures followed.

Parameter	Method
BOD,COD	Standard titrimetric procedure
Chloride, Fluoride	Ion-selective electrodes
Total nitrogen	Kjeldhal method
Total phosphorus	Spectrophotometry (Vanadomolybdate method)
Sulphate	Turbidimetry
Nitrate, nitrite	Spectrophotometry (Azo dye method with cadmium reduction)
Cd,Fe,Pb,Mn,Co,Zn	Atomic absorption spectrophotometry
Cu	
As,Hg	Atomic absorption with hydride reduction
SS,TDS	Gravimetry

Microbiological examinations for *E.Coli* and coliforms were estimated according to the ISO 4831:1990 International standards using the most probable number counts. These gave far more accurate readings for sewege samples compared with the data reported in the first report.

#### **Results and Discussion**

#### (I) Raw water quality survey

Results of the raw water quality survey are given in tables 1-3 and the results of the pesticide analysis and their detection limits are given separately in annexure 1. There was total absence of any of the pesticides generally used in Sri Lanka in any of the water quality samples which were investigated (Annexure 1). In general these samples show increased turbidity and increased suspended solids compared to the values obtained during the dry season. The phosphate concentration also showed a significant increase in concentration during the rainy season specially in the Nuwara Eliya district. This is perhaps due to the washing of phosphate fertilisers which remain close to the ground during the dry season and gets leached into the streams and underground water resources during the rainy season. The total hardness of the water during the rainy season is about 50% of its values during the dry season.

The conductivity of ground water sources was high compared to those collected from springs from Nuwara-Eliya. This is probably due to high calcium and magnesium salts as indicated by total alkalinity and hardness. The sulphate contents of these samples were also high. Out of the bore hole wells, those at the Race course, Galway forest lodge, Interfashion, Hill club and Palladium had relatively high mineralisation as seen in higher conductivities. The nitrate and free ammonia contents of the Palladium bore hole was very high most probably due to faecal contamination. There was an unusual situation with respect of the analytical results of WQ/N/15.1 compared to analyses obtained later from the same bore hole. This is because this is a shallow bore hole and WO/N/15.1 was collected when the weather was dry and samples WQ/N/15.2 and WQ/N/15.3 during very high rain. As a result its iron content was very high, turbidity was also high and Cl was also high. In particular, this particular bore hole has high iron content also for the same reason. The water from this bore hole appeared brownish and this explains its high TDS values. There was no significant variation of the water composition for samples collected from springs over a 24 h period indicating little human activity. There is also no evidence of pesticide contamination for any of these samples (both spring water & bore holes at Nuwara Eliya). It is also clear that the sample at Lovers leap and Pedro intake had relatively high contamination by coliforms indicating human faecal contamination. The residual coliform counts from bore hole water samples probably arises due to contamination of the rubber hoses used to collect the sample and attached to the bore hole well.

It is also clear that the Palladium bore hole water is also highly contaminated as seen in its high bacterial contamination, high iron content, high chloride etc. This is a shallow bore hole present in a highly contaminated area and it is not surprising that its water is highly polluted. The high iron content may arise due to corroding metallic pipes since this bore hole is situated in the heart of the city. Also because of close proximity to septic tanks it exhibits a high level of ammonia. The Brewery bore hole was not in general use at the time samples were collected and the levels of heavy metals may be high for this reason.

The race course bore hole shows increased mineralisation (high conductivity) with higher concentrations of phosphate compared to other bore holes. This is due to it being close to an area which is intensively fertilised. Such fertiliser run-offs could explain its high phosphate level.

Samples from new bore holes WQ/N/18 and WQ/N/19 showed that the one near the golf course (WQ/N/19) has relatively high hardness and conductivity while that dug near Galway forest showed quite normal results.

Additional raw water quality samples were collected near the Gohagoda site where sample WQ/K/3 is the sample collected about 100 metres upstream of the sewage effluent flow. This sample clearly showed increased nitrate contamination but no big differences from other water quality samples.

#### Survey points and the keys to samples

Raw water quality

# KANDY

WQ/K/1	Intake point of Kandy water treatment plant.
WQ/K/2	Polgolla dam intake

Additional sample for raw water quality was selected near the proposed intake at Gohagoda (near Katugastota) just up river from the sewage dumping site.

WQ/K/3 Gohagoda -proposed intake point before sewage flow

## NUWARA ELIYA

Surface inta	ikes
WQ/N/ 1	Bambarakele
WQ/N/2	Shanthipura
WQ/N/3	Pedro intake
WQ/N/4	Water field (new)
WQ/N/5	Water field(old)
WQ/N/6	Piyatissapura
WQ/N/7	Brewery falls
WQ/N/8	Gemunupura
WQ/N/9	Lovers leap

Ground water resources

WQ/N/10	Hill club bore hole
WQ/N/11	Race course bore hole

Table 1. Raw water quality data (Kandy district) Units employed: Tempertaure <sup>o</sup>C,COD,BOD,SS,TDS,CI,SO<sub>4</sub><sup>2</sup>,As,Cd,Zn,Co ppm, Conductivity uscm<sup>-1</sup>, Coliform total at 35 C/100ml, *E.Coli*. At 44 C/100ml

TDS         Cf         alkalinity Free NH <sub>3</sub> NO <sub>3</sub> NO <sub>2</sub> F $PO_4^{-1}$ 28.5         4.2         7.8         ND         1.89         0.05         0.02         0.62           22.4         2.5         16.9         0.09         4.19         0.10         0.02         0.62           22.1         3.1         16.3         0.10         1.33         0.18         0.02         2.04           22.1         3.1         16.9         0.05         3.22         0.27         0.03         3.14           2         22.1         3.1         20.5         0.13         1.98         0.03         3.01           2         22.1         3.1         20.5         0.13         1.98         0.03         3.01           2         22.1         3.1         16.9         0.05         3.22         0.27         0.03         3.01           2         24.5         2.5         18.7         1.00         1.70         0.02         4.04           2         24.5         2.5         16.9         0.08         2.03         0.02         1.04           2         24.5         2.5         16.9						Total				I	6	Total
28.5         4.2         7.8         ND         1.89         0.05         0.02         0.64         3.01         3.0			onductivity	TDS	ö		ee NH <sub>3</sub>	NO <sup>3-</sup>	NO2	<b>LL</b> .	PO.	hardness
22.4         2.5         16.9         0.09         4.19         0.10         0.02         2.04           23.1         3.1         16.3         0.10         1.33         0.18         0.04         3.01           22.1         3.1         20.5         0.13         1.98         0.03         3.14           22.1         3.1         20.5         0.13         1.98         0.03         3.01           21.7         2.1         16.9         0.05         3.22         0.27         0.03         3.01           24.5         2.5         18.7         1.00         1.70         0.10         0.05         3.01           24.5         2.5         18.7         1.00         1.70         0.10         0.02         4.04           25.5         3.6         21.7         0.08         2.06         0.03         0.01           25.5         3.8         16.9         0.06         2.53         0.10         0.10         1.88           27.5         3.8         16.9         0.07         2.24         0.10         0.02         2.04           27.5         3.8         16.9         0.08         2.03         0.02         1.01	14.9	مر	57.1	28.5	4.2	7.8	QN	1.89	0.05	0.02	0.62	6.7
23.1       3.1       16.3       0.10       1.33       0.18       0.04       3.01         22.1       3.1       20.5       0.13       1.98       0.08       0.03       3.14         21.7       2.1       16.9       0.05       3.22       0.27       0.03       3.01         24.5       2.5       18.7       1.00       1.70       0.10       0.02       4.04         24.5       2.5       18.7       1.00       1.70       0.10       0.03       3.01         24.5       2.5       18.7       1.00       1.70       0.10       0.02       4.04         25.5       3.6       22.3       0.22       2.41       0.10       0.10       1.88         27.5       3.8       16.9       0.08       2.08       0.09       0.02       2.04         27.7       4.1       19.9       0.10       1.91       0.10       1.03       0.05       1.71         27.7       4.1       19.9       0.10       1.31       0.05       1.71         29.7       5.0       19.9       0.10       1.91       0.05       1.71         27.7       4.1       19.9       0.10 <t< td=""><th>22.3</th><th>۰ ص</th><th>43.6</th><td>22.4</td><td>2.5</td><td>16.9</td><td>0.09</td><td>4.19</td><td>0.10</td><td>0.02</td><td>2.04</td><td>4.8</td></t<>	22.3	۰ ص	43.6	22.4	2.5	16.9	0.09	4.19	0.10	0.02	2.04	4.8
22,1       3.1       20.5       0.13       1.98       0.08       0.03       3.14         21.7       2.1       16.9       0.05       3.22       0.27       0.03       3.01         24.5       2.5       18.7       1.00       1.70       0.10       0.02       4.04         24.8       3.6       21.7       0.08       2.06       0.03       0.06       0.91         25.5       3.6       22.3       0.22       2.41       0.10       0.02       4.04         27.5       3.8       16.9       0.06       2.53       0.10       0.10       1.88         27.5       3.8       16.9       0.08       2.08       0.09       0.02       2.04         27.7       4.1       19.9       0.10       1.91       0.10       0.02       1.81         27.7       4.1       19.9       0.10       1.91       0.07       0.03       3.85         27.7       4.1       19.9       0.10       1.91       0.05       1.71         27.5       3.4       1.93       0.07       0.03       3.85         27.7       4.1       19.9       0.101       1.91       0.13 <th></th> <th>ŝ</th> <th>46.4</th> <td>23.1</td> <td>3.1</td> <td>16.3</td> <td>0.10</td> <td>1.33</td> <td>0.18</td> <td>0.04</td> <td>3.01</td> <td>15.2</td>		ŝ	46.4	23.1	3.1	16.3	0.10	1.33	0.18	0.04	3.01	15.2
21.7       2.1       16.9       0.05       3.22       0.27       0.03       3.01         24.5       2.5       18.7       1.00       1.70       0.10       0.02       4.04         24.5       2.5       18.7       1.00       1.70       0.10       0.02       4.04         24.5       2.5       18.7       1.00       1.70       0.10       0.02       4.04         25.5       3.6       22.3       0.22       2.41       0.10       0.02       2.04         27.5       3.8       16.9       0.06       2.53       0.10       0.02       2.04         27.5       3.8       16.9       0.06       2.53       0.10       0.02       2.04         27.5       3.8       16.9       0.06       2.53       0.10       0.02       1.81         27.7       4.1       19.9       0.12       1.76       0.07       0.05       1.71         27.7       4.1       19.9       0.10       1.91       0.05       1.71         27.1       5.0       19.9       0.10       1.91       0.05       1.71         29.7       4.3       18.7       0.13       1.32 <t< td=""><th>14.7</th><th>~</th><th>44.2</th><td>22.1</td><td>3.1</td><td>20.5</td><td>0.13</td><td>1.98</td><td>0.08</td><td>0.03</td><td>3.14</td><td>15.2</td></t<>	14.7	~	44.2	22.1	3.1	20.5	0.13	1.98	0.08	0.03	3.14	15.2
24.5       2.5       18.7       1.00       1.70       0.10       0.02       4.04         24.8       3.6       21.7       0.08       2.06       0.08       0.06       0.91         25.5       3.6       22.3       0.22       2.41       0.10       0.10       1.88         27.5       3.8       16.9       0.06       2.53       0.10       0.02       2.04         27.5       3.8       16.9       0.06       2.53       0.10       0.10       1.81         27.5       3.8       16.9       0.06       2.53       0.10       0.02       2.04         27.7       4.1       19.9       0.08       2.08       0.09       0.02       1.81         27.7       4.1       19.9       0.12       1.76       0.07       0.05       1.71         27.7       4.1       19.9       0.10       1.91       0.13       1.32       0.07       1.63         29.7       5.0       19.9       0.10       1.91       0.05       1.71         29.7       5.0       1.91       1.31       0.03       3.85         25.3       2.15       0.19       0.07       0.03       <	25.1	~	43.3	21.7	2.1	16.9	0.05	3.22	0.27	0.03	3.01	17.0
24.8       3.6       21.7       0.08       2.06       0.08       0.06       0.91         25.5       3.6       22.3       0.22       2.41       0.10       0.10       1.88         27.5       3.8       16.9       0.06       2.53       0.10       0.02       2.04         25.9       2.7       16.9       0.08       2.08       0.09       0.02       2.04         27.7       4.1       19.9       0.12       1.76       0.07       0.05       1.71         27.7       4.1       19.9       0.12       1.76       0.07       0.05       1.71         27.7       4.1       19.9       0.12       1.76       0.07       0.05       1.71         27.7       4.1       19.9       0.10       1.91       0.13       1.56       1.71         29.7       5.0       19.9       0.10       1.91       0.05       6.85         25.3       4.3       18.7       0.13       1.32       0.07       0.03       3.85         26.4       3.9       23.6       0.10       1.40       0.08       0.07       3.58         26.0       4.1       3.52       0.29 <t< td=""><th>11.5</th><th>-</th><th>49.8</th><td>24.5</td><td>2.5</td><td>18.7</td><td>1.00</td><td>1.70</td><td>0.10</td><td>0.02</td><td>4,04</td><td>17.0</td></t<>	11.5	-	49.8	24.5	2.5	18.7	1.00	1.70	0.10	0.02	4,04	17.0
25.5       3.6       22.3       0.22       2.41       0.10       0.10       1.88         27.5       3.8       16.9       0.06       2.53       0.10       0.02       2.04         25.9       2.7       4.1       19.9       0.08       2.08       0.09       0.02       2.04         27.7       4.1       19.9       0.12       1.76       0.07       0.05       1.71         27.7       4.1       19.9       0.12       1.76       0.07       0.05       1.71         29.7       5.0       19.9       0.10       1.91       0.13       0.06       6.85         29.7       5.0       19.9       0.10       1.91       0.13       1.56       1.71         29.7       5.0       19.9       0.10       1.91       0.13       1.55       3.85         25.3       4.3       18.7       0.13       1.63       0.07       0.33       3.85         28.0       3.3       21.7       0.13       1.63       0.07       0.33       1.58         28.0       4.1       3.56       0.29       1.57       0.07       0.33       1.58         28.0       4.1 <td< td=""><th>26.1</th><th>, M</th><th>49.7</th><td>24.8</td><td>3.6</td><td>21.7</td><td>0.08</td><td>2.06</td><td>0.08</td><td>0.06</td><td>0.91</td><td>18.9</td></td<>	26.1	, M	49.7	24.8	3.6	21.7	0.08	2.06	0.08	0.06	0.91	18.9
27.5       3.8       16.9       0.06       2.53       0.10       0.02       2.04         25.9       2.7       16.9       0.08       2.08       0.09       0.02       1.81         27.7       4.1       19.9       0.12       1.76       0.07       0.05       1.71         29.7       5.0       19.9       0.10       1.91       0.13       0.06       6.85         29.7       5.0       19.9       0.10       1.91       0.13       0.05       1.71         29.7       5.0       19.9       0.10       1.91       0.13       1.55       1.71         29.7       5.0       19.9       0.10       1.91       0.13       1.55       1.71         29.8       3.3       21.7       0.13       1.53       0.07       0.03       3.85         28.0       3.18       0.13       1.63       0.07       0.33       1.58         28.0       4.1       3.56       0.29       1.57       0.07       0.33       1.58         28.0       4.1       3.56       0.29       1.57       0.07       0.33       1.58         31.2       2.5       0.46       4.78       <	25.1	<b>_</b>	51.1	25.5	3.6	22.3	0.22	2.41	0.10	0.10	1.88	18.9
25.9       2.7       16.9       0.08       2.08       0.09       0.02       1.81         27.7       4.1       19.9       0.12       1.76       0.07       0.05       1.71         29.7       5.0       19.9       0.12       1.76       0.07       0.05       1.71         29.7       5.0       19.9       0.10       1.91       0.13       0.05       6.85         25.3       4.3       18.7       0.13       1.32       0.08       0.03       3.85         28.0       3.3       21.7       0.13       1.63       0.07       0.33       1.58         28.0       3.3       21.7       0.10       1.40       0.08       0.07       3.35         28.0       4.1       35.6       0.29       1.57       0.08       0.07       3.58         58.0       4.1       35.6       0.29       1.57       0.08       0.07       3.58         31.2       2.5       20.5       0.46       4.78       0.19       0.15       2.15         26.0       1.99       21.1       ND       3.52       0.13       0.15       2.15	54.3	2	54.9	27.5	3.8	16.9	0.06	2.53	0.10	0.02	2.04	17.1
27.7       4.1       19.9       0.12       1.76       0.07       0.05       1.71         29.7       5.0       19.9       0.10       1.91       0.13       0.06       6.85         25.3       4.3       18.7       0.13       1.32       0.08       0.03       3.85         28.0       3.3       21.7       0.13       1.63       0.07       0.33       1.58         28.0       3.3       21.7       0.13       1.63       0.07       0.33       1.58         28.0       3.3       21.7       0.10       1.40       0.08       0.07       3.35         26.4       3.9       23.6       0.10       1.40       0.08       0.07       3.58         58.0       4.1       35.6       0.29       1.57       0.08       0.07       3.58         31.2       2.5       20.5       0.46       4.78       0.19       0.15       2.15         26.0       1.99       2.11       ND       3.52       0.13       0.16       1.51	23.3	~	51.7	25.9	2.7	16.9	0.08	2.08	0.09	0.02	1.81	4.8
29.7       5.0       19.9       0.10       1.91       0.13       0.06       6.85         25.3       4.3       18.7       0.13       1.32       0.08       0.03       3.85         28.0       3.3       21.7       0.13       1.63       0.07       0.33       1.58         28.0       3.3       21.7       0.13       1.63       0.07       0.33       1.58         26.4       3.9       23.6       0.10       1.40       0.08       0.07       3.58         58.0       4.1       35.6       0.29       1.57       0.08       0.07       3.58         31.2       2.5       20.5       0.46       4.78       0.19       0.15       2.15         26.0       1.99       21.1       ND       3.52       0.13       0.15       2.15	19.9	_	51.4	27.7	4.1	19.9	0.12	1.76	0.07	0.05	1.71	21.0
25.3       4.3       18.7       0.13       1.32       0.08       0.03       3.85         28.0       3.3       21.7       0.13       1.63       0.07       0.33       1.58         26.4       3.9       23.6       0.10       1.40       0.08       0.07       3.35         26.4       3.9       23.6       0.10       1.40       0.08       0.07       3.58         58.0       4.1       35.6       0.29       1.57       0.08       0.09       1.97         31.2       2.5       20.5       0.46       4.78       0.19       0.15       2.15         26.0       1.99       21.1       ND       3.52       0.13       0.15       2.15	16.4		59.2	29.7	5.0	19.9	0.10	1.91	0.13	0.06	6.85	21.0
28.0         3.3         21.7         0.13         1.63         0.07         0.33         1.58           26.4         3.9         23.6         0.10         1.40         0.08         0.07         3.58           58.0         4.1         35.6         0.29         1.57         0.08         0.09         1.97           58.0         4.1         35.6         0.29         1.57         0.08         0.09         1.97           31.2         2.5         20.5         0.46         4.78         0.19         0.15         2.15           26.0         1.99         21.1         ND         3.52         0.13         0.16         1.51	28.2	~	50.7	25.3	43	18.7	0.13	1.32	0.08	0.03	3.85	17.0
26.4         3.9         23.6         0.10         1.40         0.08         0.07         3.58           58.0         4.1         35.6         0.29         1.57         0.08         0.09         1.97           31.2         2.5         20.5         0.46         4.78         0.19         0.15         2.15           26.0         1.99         21.1         ND         3.52         0.13         0.16         1.51	11.7		56.0	28.0	3.3	21.7	0.13	1.63	0.07	0.33	1.58	17.0
58.0         4.1         35.6         0.29         1.57         0.08         0.09         1.97           31.2         2.5         20.5         0.46         4.78         0.19         0.15         2.15           26.0         1.99         21.1         ND         3.52         0.13         0.16         1.51	12.8	~	52.9	26.4	3.9	23.6	0.10	1.40	0.08	0.07	3.58	20.8
31.2 2.5 20.5 0.46 4.78 0.19 0.15 2.15 26.0 1.99 21.1 ND 3.52 0.13 0.16 1.51	27.5	~	55.8	58.0	4.1	35.6	0.29	1.57	0.08	0.09	1.97	28.3
26.0 1.99 21.1 ND 3.52 0.13 0.16 1.51	15.0	~	63.5	31.2	2.5	20.5	0.46	4.78	0.19	0.15	2.15	37.8
	23.3 10.0 6.8	~	52.1	26.0	1.99	21.1	Q	3.52	0.13	0.16	1.51	39.6

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Total iron		0 Z	Q	1.05	0.35	3 47		0.90	1.38	0.29	0.23	0 T C	0.0	0.54	0.35	0.54	0.00		1.94	0.6	QZ	2	Z	
á	2	g	Q	Q	QZ			2 Z	2	2	QN		Z	2	Q	Q		2	ON N	2	CZ	2	n	
•	۸ <b>۲</b>	0 Z	g	g	CZ		<u></u>	n	Q	D	CZ	2 4	n N	Q	Q	QN	ļ		Q	Q	Ç	<u></u>	Q	
- - -	бц	QZ	QN	QN		24	2 !	n Z	Q	Q	CZ	2	Q	Q	Q	CZ		Z	Q	Q		<u></u>	0 Z	
	uМ	۵z	QN	C Z			R	Q	Q	Q			ÖN	QZ	QN		2	n N	Q	Q	Ç	N N	g	
	ບັ	QN	CZ				n	Q	Q	QN		S	g	QZ	ç	2	2	Q	Q	Cz			Q	
	B	CZ					QZ	Q	QŅ.	C		אר	Q	QN			ב	Q	Q	CZ		nz	QN	
	D C					QN	Q	g	CZ		2 1	n	g	Cz			NC	Q	QN			Q	Q	
	E. coli			200	097	100	1600	190	ЕЛ		00	80	70	480		000	200	240	250		20	30	260	
Total	coliform	0001		001	1100	006	3400	2200	EAD.		800	300	200	2000	0000		2080	2600	COR.		000	100	1100	
	NO.	4	012 7	<10	101v	<104	<10 <sup>4</sup>	<10 <sup>4</sup>	4		₹10.	<10 <sup>4</sup>	4017		<u>,</u>		<10 <sup>1</sup>	<10 <sup>4</sup>	404	01. 4.0	-ni->	<10 <sup>1</sup>	<104	
	00 S	<b>V</b>	2. 2.	4.	2.1	1.8	2.2	R C	t e N v	, <mark>5</mark> , 1	1.9	3.3	Ť	t 1	, <b>1</b> , <b>1</b>	5.8	2.6	201		с Г	0.7	7.0	0.7	, , ,
		Sample	WO/K/1.1	WQ/K/1.2	WO/K/1.3	WQ/K/1.4	W0/K/1 5			WQ/K/1.7	WO/K/1.8	WO/K/2.1			WQ/K/2.3	WO/K/2.4	WO/K/2.5	AIDIN'S R		WQ/K/Z./	<b>WQ/K/2.8</b>	WOR(3.1	WO/K/3.2	

Table 1. Raw water quality data (Kandy district)continued

к 1

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	-	•												
								Total						Total
-		Turnter	Turbidity		onductivity	TDS	ö	alkalinity Fr	Free NH <sub>3</sub>	No.	NO2 <sup>-</sup>	ίι.,	PO *	hardness
Sample		I water				) ( ) (		i u	200	4 4 8	40 U	0.04	2.72	3.8
WQ/N1.1	23.0	15.5	0.89	4./	<b>C'</b> 01	2.0	1.10	0.0	0.0				Ċ	X X
MOM1 2	15.0	14.0	1.35	6.4	11.4	5.6	0.90	8.4	0.14	1.06	0.75	20.0	7.17	0 <b>f</b>
	20.2	15.0	0 79	7.0	15.3	7.2	1.10	5.4	0.02	0.41	0.45	0.20	1.79	5.7
	C - 0 4	) r ) <b>r</b>	0.70	6 9	15.4	7.0	0.90	6.0	0.13	4.47	0.62	0.02	0.81	8.G
MUNZ.Z	10.0	- C	1 20	4 C	414	<b>60</b> 10)	1.00	7.2	Q	0.20	0.30	0.02	1.96	7.6
			24. 72.	о « 1 с	110	4	0.85	9.1	0.01	1.94	0.56	0.02	1.82	<b>4</b> .8
WO/N/3.2	0.71			4 C		9.5	1.10	6.6	0.01	1.26	0.42	0.03	2.64	5.7
WQ/N/4.1	20.3		1.00	, α 1 α			1 00	7.2	0.27	0.93	0.75	0.02	3.21	4.8
WOW4.2			61-1 62-0	<b>7</b> 7 7	10.0		110	9.2	0.02	0.27	0.17	0.01	1.20	7.6
WQ/N5.1		0.0	0.10 4 75	- u	1 1 2		1 00	8.4	0.27	0.84	0.95	0.02	1.25	5.7
ZCNOM		- C 4 u	14.0	4 5 4		) () ()	1 07	7.8	Q	0.80	0.27	0.02	3.35	6.7
WQ/N/6.1	23.4	0.0	0.0 10			5 U		6 L		1.37	0.11	0.02	3.16	4.8
WO/N6.2	16.0	19.0	0.70	7 0	t	י ע ע		4 8	0.02	0.87	0.18	0.02	2.80	4.8
WONT.1	16.2	7.eL	00.1	1 F	- 0			5 <b>5</b>	019	0.52	0.88	0.02	1.69	<b>4</b> .8
WON7.2	10.1	9.9	1.40	 	0.4	n (				99.0	72 0	0.05	2.30	8.G
WQ/N/8.1	21:0	15.7	0.95	1.2	12.8	0 I	0.4	0 t 7 č	4 C 2 2 5	0.50	0.60	0.03	2.73	7.6
WQ/W8.2	17.3	14.2	0.82	6.8	2.11	0 I	0.90	0.1			0.00	0.05	2 82	5.7
WO/W9.1	20.9	15.1	1.84	6.5	11.1	5.5	1.10	α. 2	n.uz		+ 00 00			α • •
WQ/N9.2	18.4	14.8	1.20	6.0	10.8	5.0	1.00	7.2	0.38	2.02	0.02	0.02	20.0	ř

Table 2. Raw water quality data - Nuwara-Eliya district (Surface intakes)

	otal Iron	2	0.35	Q	0.35	Q	Q	0.11	9	2 2	Q	Q	Q	0.23	0.2	Q	0.18	Q	4 C C	0.30	
		Q Z	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	ð	Ð	Q	Q	Q	Q		R	
	As	Q	Q	Q	Q	QN	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	(	S	
	fł	Q	Q	Q	Q	QN	Q	Q	Q	QN	QN	QN	QN	Q	Q	Q	Q	Q	(	N.	
	Mn	Q	Q	Q	Q	QN	Q	Q	g	Q	QN	QN	Q	QN	QN	QN	g	QN		Q	
	ັວ	Q	Q	QN	QZ	Q	Q	QN	Q	QN	Q	Q	Q	QN	Q	QN	QN	QN		ON N	
	PO	QN	Q	Q	Q	QN	QN	QN	Q	QN	Q	Q	Q	Q	Q	Q	Q	Ę		ŝ	
	Сu	Q	Q	Q	0.2	Q	Q	QN	Q	Q	Ö	Q	2	Q	Q	QN	CZ	Ş	]	Q	
	E. coli	12	20	20	60	1000	120	16	20	10	4	40	100	N	9	32	05			80	
Total	coliform	36	200	140	160	2400	210	50	40	36	20	110	240	404	40	22	1.10	2100		140	
	CN.	<104	<104	<104	<104	<104	<104	<104	<104	<10 <sup>4</sup>	<104	404	40 7	- 10 - 10 - 10	<101	<104			27	<104	
	so, <sup>2-</sup>	1 20	1 10	1 70	1 20	1 30	1 20	1 60	1 40		1 50	2 C C						0.0	00.1	1.50	
	Sample	1 FINO MI			WOWD 2	WOWR 1						A SUCCESS							L'AN/OM	WQ/N/9.2	

Table 2. Raw water quality data - Nuwara-Eliya district (Surface intakes) continued

					conductivit		·	Total						Total
Sample	T air	T water	Turbidity		y	TDS		alkalinity Free NH <sub>3</sub>	free NH <sub>3</sub>	NO3	NO <sub>2</sub>	Ŀ	PO	hardness
WO/N/10.1	19.0	18.0	61.1	6.8	177.0	88.0	2.19	106.0	0.24	1.78	0.08	0.04	4.93	40.0
WO/10.2	20.0	18.8	36.5		186.0	93.0	1.62	109.0	0.09	2.47	0.12	0.04	9.02	81.0
WO/N/10.3	19.8	18.2	43.3		220.0	110.0	1.58	142.0	0.19	2.54	0.09	0.05	3.11	106.0
WQ/N/11.1	20.0	19.8	7.20		250.0	130.0	1.29	168.0	0.08	1.74	0.09	0.04	2.50	128.0
WO/N/11.2	16.0	18.5	22.40		250.0	125.0	1.62	165.0	0.04	1.48	0.08	0.02	9.45	123.0
W0/N/11.3	23.0	19.4	1.33		260.0	130.0	1.25	170.0	0.11	4.26	0.09	0.04	3.77	128.0
WQ/N/12.1	22.0	16.0	1.45		103.0	52.0	1.62	81.0	ON	2.72	0.18	0.03	2.73	55.0
WO/12.2	16.5	16.7	1.28		<b>99.</b> 0	49.0	1.81	54.0	0.07	4.26	0.09	0.02	6.21	43.0
WQ/N/12.3	24.0	16.5	0.96		<b>66</b> .0	49.0	1.58	57.0	0.10	3.06	0.12	0.07	2.08	40.0
WO/13.1	19.0	17.0	2.18		176.0	89.0	15.49	11.0	0.13	9.00	0.12	0.06	3.47	60.0
WO/N/13.2	17.5	17.1	1,15		176.0	89.0	26.91	12.0	0.07	7.41	0.10	0.04	5.77	53.0
WO/N/13.3	21.0	17.4	0.54		180.0	90.0	25.11	12.0	0.16	8.74	0.11	0.05	1.94	54.0
WO/N/14.1	20.0	19.0	2.34		260.0	130.0	2.04	171.0	0.07	2.78	0.09	0.04	44.	128.0
WQ/N/14.2	19.0	24.0	6.90		260.0	130.0	1.81	169.0	0.01	3.59	0.57	0.04	8.20	128.0
WQ/N/14.3	22.0	20.2	1.57		250.0	125.0	1.54	166.0	0.21	3.30	0.54	0.05	2.91	124.0
WO/N/15.1	19.0	17.9	775.0		1000.0	500.0	1.58	373.0	2.75	97.12	14.2	0.04	4.40	275.0
WQ/N/15.2	19.5	18.5	120.0		1020.0	490.01	124.00	391.0	0.16	32.17	2.06	0.02	3,45	294.0
WQ/N/15.3	19.0	18.9	800.0		1000.0	500.0	00.00	301.0	4.45	42.13	2.26	0.02	2.66	184.0
WQ/N/16.1	19.0	18.0	11.5	5.0	37.0	19.0	2.24	7.9	0.19	2.44	0.09	0.02	4.63	9.4
WQ/N/16.2	17.0	18.5	22.5		29.0	15.0	1.54	9.7	0.27	3,88	0.09	0.02	5.11	4.7
WQ/N/16.3	17.5	18.2	4.8		42.0	21.0	2.57	14.5	0.62	3.83	0.09	0.03	2.96	5.7
WQ/N/17.1	19.0	17.0	29.00		198.0	0.66	3.16	115.0	0.20	4.68	0.16	0.04	4.32	87.0
WQ/N/17.2	16.0	17.0	9.30		200.0	100.0	3.16	110.0	0.06	6.48	0.09	0.04	5.69	91.0
WQ/17.3	22.0	17.0	7.10		220.0	100.0	2.57	122.0	0.16	5.44	0.1	0.03	3.11	92.0
WQ/N/18	17.5	17.0	0.2		49.8	24.9	2.63	27.3	0.04	4.28	0.09	0.17	0.32	20.8
WQ/N/19	16.0	17.3	5.0		230.000	115.2	2.19	150.7	0.05	2.38	0.09	0.18	0.68	115.1

Table 3. Raw water quality data - Nuwara-Eliya district (Ground water sources)

.

		5.19	5.14	1.27	0.35	0.72	Q	Q	1.05	Q	1.65	0.50	0.24	0.29	0.44	Q	10.20	418.50	342.00	1.98	0.90	2.72	0.56	0.57	0.20	Q	Q	!
i	а а	Q	Q	2	0 Z	02	Q	0 Z	D	0 Z	0 Z	2 Z	Q	Q	D	Q	Q	Q	Q	Q	Ð	Ð	0 Z	2	Q	g	C Z	2
	As	Q	Q	Q	Q	g	Q	Q	Q	Q	QN	2	Q	9	Q	Ð	Q	Q	Q	Q	g	Q	Q	9	Ð	Q	CZ	2
	βĨ	Q	Q	Q	QN	Q	Q	Q	Q	Q	QN	Q	Q	Q	Q	QN	Q	Q	QN	Q	Q	Q	QN	Q	Q	QN		Š
	Mn	0,40	0.33	0.07	a	QN	QN	0.47	QN	g	QN	QN	0.15	a	QN	Q	1.62	9.33	7.93	0.07	0.13	0.07	QN	QN	0.05	QN		Ž
	ັວ	QN	Q	g	QN	Q	Q	Q	Q	Q	Q	g	Q	Q	Q	Q	QN	1.34	0.94	Q	Q	2	Q	g	Q	Q		Z
	8	Q	Q	QN	QN		2 Z	g	QN	Q N	Q	Q	Q	Q		Q	QN	Q	Q	0.03	QN	a Z	Q	Q		g		N N
	no	QN	Q	CN	S	2 Z		g	QN	QN	QN	QN		Q	2 Z		2	0.54	0.45	g	0.08	QN	QN			ŝ	2	Ŋ
	E. coli	10	32		8 2		2 <del>(</del>	: ¢	40	20	Z	ic	12	30	S US	8 6	0 <b>7</b>	2 2 2	908	E Z	p	0	ÎN.	60	40 40	P	Ē	Ē
Total	coliform	140	140	4		p c	8 4	6 6	1	205	Ż	Ē	Ē			e e	100	3 2	4 0	20° 20°	20	U V	909	110	13	4 0	27	20
	SON	<10 <sup>4</sup>	4 UF /				0 7 7	210 210 2	4 U F V	40F>	4 U F >	4012								<10 <sup>4</sup>	4 U ->	24042	2 1 0 7 1 0 7	2 T				<107
	so. <sup>2-</sup>	2 - C			7.17		1.00 1 0 1 0 1	0.10 1 AK		67.0 80.1	07.0 P0.2		1 5 0 0	0.0	N 0	0.0 000	0 H N N N	C / 7	0.00 11			2.4	4 7 B		7 - 17	3.UZ	2.18	1.97
	Samole	VALO ANI 40 4			WO/N/JU.S			W0/N11.5					WU/N13.2	WU/N/13.3		2.4LV/DM	WQ/N14.3	1.6L/N/DM		WU/N 15.5					ZULNOM	S. I LNIOM	WO/N/18	WQ/N/19

.

Table 3. Raw water quality data - Nuwara-Eliya district (Ground water sources)continued

Raw water qualitysurvey

Sample points :

1. Gatambe	o Doloolla	
Kandy		

3. Mahaweli river at Gohagoda Nuwara - Eliya

Surface intakes

1. Bambarakelle

Shanthipura
 Pedro intake

4. Water field - New

5. Water field - Old

6. Piyatissapura

7. Brewery intake

8. Gemunu Mawatha

9. Lovers slip

Ground water sources

10. Hill Club

11. Race Course bore hole

12. Upper Lake Road B.H.

13. Gaiway Forest Lodge

4. Interfashion

Palledium Hotel

16. Golf Club

17. Celon Brewery

19. New bore hole near golf ground 18. Galway new bore hole

WQ/N/12	Upper lake road bore hole
WQ/N/13	Galway forest bore hole
WQ/N/14	Interfashion bore hole
WQ/N/15	Palladium bore hole
WQ/N/16	Golf club bore hole
WQ/N/17	Brewery bore hole
WQ/N/18	Galway new bore hole
WQ/N/19	New bore hole near golf ground

The last two bore holes WQ/N/18 and WQ/N/19 are the newly dug wells and samples were collected once at the time they were dug and these data are also provided in the table for water quality (Nuwara-Eliya district)

## 2. Sewage quality survey

The location of sample collection and the key to sample numbers are given below:

Kandy K/1. High income house – Domestic sewage

K/2 Middle income house - Domestic sewage

K/3. Low income house - Domestic sewage

K/4. Hantana scheme - Before treatment

K/5. Office sewage - Education office, Kandy

K/6. High Income house- effluent from septic tank

K/7. Middle income house - Effluent from septic tank

K/8. Low income house - Effluent from septic tank

K/9 University office - Effluent from septic tank

K/10. Hantana scheme - After treatment

K/11. Hotel with treatment facility - Swiss Hotel Influent

K/12. Hotel with treatment facility - Swiss Hotel Effluent

K/13. Hotel (without treatment facility) Riverdale grey water

K/14. Industrial waste water - Chocolate company(before treatment

K/15. Industrial waste water - Chocolate company(after treatment)

K/16. Industrial waste water - Sun match company\*

K/17. Hospital sewage - Peradeniya teaching hospital - Before treatment

K/18. Hospital sewage - Peradeniya teaching hospital - After treatment

K/19. Sewage effluent from the Gohagoda garbage at the dumping site

K/20. Sewage effluent from Gohagoda at the stream which flows into river just before entry into river

\*Only one sample was collected from point 16 (Sun match company) since the effluent is discharged only at 3.00 p.m. from the factory.

*Nuwara-Eliya* N/1. Domestic sewage (middle income)

N/2. Domestic sewage (low income)

N/3 Domestic sewage (Ceybank hotel)

N/4. Municipality – Nuwara Eliya (office sewage)

N/5. Local eating house (domestic sewage)

N/6 Domestic sewage- hotel without treatment- Windsor hotel

N/7 Effluent from septic tank (middle income house)

N/8. Effluent from septic tank (Cey Bank Rest)

N/9 Effluent from septic tank (slum house)

N/10. Effluent from septic tank (municipality)

N/11.Hotel (with treatment facility) - before treatment (Grand Hotel)

N/12. Hotel (with treatment facility) - after treatment (Grand Hotel)

N/13. Industrial wastewater - drain (Ceylon Brewery)

N/14. Industrial wastewater - effluent after treatment (Ceylon Brewery)

N/15. Hospital sewage

N/16. Tea factory effluent

The analytical results are given in tables 4 & 5. The pH of the sewage samples were generally higher than 7.0 and hence within tolerance limits for disposal. Several had high sulphate contents (K/3,K/11,K/12,K/7,K/16). Contamination from chloride is very high in Suisse hotel influent (K/11), and those from K/16,K/19 and K/20. Phosphates may be high in sewege samples due to increased use of detergents for washing dishes etc. while the treatment appears to reduce this concentration. Among heavy metals, only zinc appears in almost all samples while cadmium is present in the sample K/11 (Riverdale grey water) and K/13 (Sun match company). Zinc probably originates in the galvanised tubing used in most sewage disposal systems.

The sewage effluent from the Gohagoda dumping site is quite dark in colour with a lot of dissolved solids (K/19 & K/20) and also had high Zinc. It also high chloride content. Sample SQ/N/8 (effluent from septic tank at Ceybank Rest) showed very high chloride & phosphate values while industrial waste water from the drain (Brewery) showed high sulphate content perhaps coming from the alum used for the treatment process.

The sample SQ/K/3.1 showing very high values for COD,SS and TDS and total nitrogen is owing to the fact that this particular sample when collected had a lot of suspended solids (taken early morning from the slums area housing scheme). This is the time that the cattle-sheds are washed and the water is highly turbid and contaminated with the excreta and cow-dung. The other two samples had less of all these parameters since only routine washing of dishes was involved at other times when the samples were collected.

#### 3. River water quality

The locations of sample collection and the keys to sample numbers is given below.

	បី		0 Z	Q	Q	0 Z	0 Z	0 Z	P	Q Z	9	g	Z	Ş				2 9	N	g	2	0 Z	Q	g	Q	Q	Q	Q	Q	Z		2
	Zu	0.08	0.12	¢.	0.22	0.24	0.16	0.64	0.22	0 13	0.05	0.05	200	0.04		0 0 0 0	0.05	0.0 40.0	0.12	0.08	0.04	0.04	0.04	0.02	0.03	0.02	1.22	0.8	1.06	049		N 1. 0
	g	g	Q	Q	Q	Q	CZ	Ż	2 Z		ź					2 !	D Z	Q	Q	Q	D Z	Z	0 Z	Q	Q	Q	g	Q	C	2 2	2	Ż
	As	Q	g	g	QZ	QN					ŝ					N	Q	2 Z	2	Q	QN	QN	0 Z	QZ	Q	DZ	0 Z					Z
	E coli	<10 <10	<10 <10	<10	<10	<10		18<10 <sup>5</sup>	10×10 10×10 <sup>5</sup>	0.402	18~10 <sup>4</sup>	10/10 15/10 <sup>4</sup>	10010	47.40 40.40 <sup>4</sup>		12×10	10×10 <sup>±</sup>	10×10	4×10 <sup>4</sup>	5x10 <sup>4</sup>	6x10 <sup>4</sup>	6x10 <sup>4</sup>	4x10 <sup>4</sup>	<10	<10	×10	4x10 <sup>5</sup>	4x10 <sup>5</sup>	2×10 <sup>5</sup>	22408	00.10	SUXIU
Total	coliform	17×10 <sup>5</sup>	18×10 <sup>5</sup>	17×10 <sup>5</sup>	24×10 <sup>5</sup>	20×10 <sup>5</sup>	100105	10210 20405	2000 10	32X10	20210	20X10	20X10	20 104	22X10	26×10"	20×10 <sup>4</sup>	22×10 <sup>°</sup>	18×10 <sup>4</sup>	24×10 <sup>4</sup>	20×10 <sup>4</sup>	22×10 <sup>4</sup>	16×10 <sup>4</sup>	13×10 <sup>4</sup>	10×10 <sup>4</sup>	12×10 <sup>4</sup>	4×10 <sup>5</sup>	4×10 <sup>5</sup>	2 4 U 2	2X 10	33X1U	30×10
	<del>с</del> +	1.78	1.36	2.20				1.00	42.90	US.12	0,04 0,04	0.34	co.01	13./4	10.10	10.40	11.20	9.80	12.80	11.20	10.50	8 60	9.20	9.46	7 80	7 92	7 26	2 4 C		0.00	22.8/	18.90
	N-L	213.0	186.0	0.000	220.0	0.002	2,0.0	330.0	105.2	1.1	0.45	n. :	15.4	29.0	54.5	50.5	48.6	60.8	54.6	60.6	58.2	54 60	60.80	26.2	15.4	ο	0. e	0.70	+ .DO	1.001	53.3	63.8
	SO₄ <sup>2.</sup>	8.2	7.6	8			7. F	9.9	43.8	22.5	C./	6.3	10.8	12.0	8.2	8.6	8.8	10.2	8.8	12.0		1.4		2 a a	10.0	100			רית ייי ה ייי	11.8	33.2	28.8
	<u>'</u>	35.2	25.8	28.0		4 2' C	35.U	40.4	269.0	50.1	7.9	20.0	25.1	37.2	25.2	20.8	26.2	25.8	25.8	28.6			207 207		7:07 7:07	1.01	3		0.00	62.6	794.3	524.0
	TDS	420	440			220	410	360	2680	490	650	260	190	362	212	260	320	280	276	212	4 6			0.002				213	320	310	220	210
	SS	1200	1150	610	700	760	180	222	940	100	270	140	250	250	160	230	240	250	230	018 018					010		007	2301	2020	2040	353	240
rict)	000	860	002		04/	626	548	602	40	380	49	57	300	231	180	210	226	208	280	2 4		707	R R		5 CCC		676	2866	2100	2200	613	524
ndy dist	BOD	210	220		230	240	210	180	203	92.7	123	70	90	135	120	118	06	108		20		27	124	130	230	0 0 0 0		110	120	142	15	80
, vey (Ka	Ţ		) v - r	- (	7.0	6.8 9	6.9	6.8	8.8	8.1	6.9	7.4	7.2	6.4	8.2	7.6	C -	4	- u		ים מים וימי	7 2	7.7	1.7	2 2 2 2	6.7	2.0	<b>4</b>	6.5	6.4	6.9	6.9
ality Sur	Tsewane	- 27 B		707	27.8	27.1	26.9	26.4	24.5	26.0	25.0	25.0	25.0	25.0	25.1	25.0	24.0	0.12		24.0	24.9	24.6	26.2	26.0	24.0	24.5	25.0	25.0	25.6	25.2	25.0	26.8
rege Qu	T eir T			21.0	27.2	27.2	27.4	26.8	25.0	27.5	27.0	27.5	28.0	27.0	27.0	0.10	2.14	20.0		26.4	26.3	26.1	26.0	25.8	26.0	28.0	27.0	28.5	28.8	28.4	27.0	27.3
Table 4. Sewege Quality Survey (Kandy district)	elames			Z.I.NIDS	SQ/K/1.3	SQ/K/2.1	SQ/K/2.2	SQ/K/2.3	SQ/K/3.1	SQ/K/3.2	SQ/K/3.3	SQ/K/4.1	SQ/K/4.2	SQ/K/4.3	SOIKI4 4	S NNOS			500 M4.1	SQ/K/4.8	SO/K/4.9	SQ/K/4.10	SQ/K/4.11	SO/K/4.12	SQ/K/5.1	SQ/K/5.2	SQ/K/5.3	SQ/K/6.1	SQ/K/6.2	SQ/K/6.3	SO/K/7.1	SQ/K/7.2

Bornage         H         BOrn         CCD         SS         TDS         CI         SQA*         T-N         T-P         coliform         E. coli         AS         Cd         Zn         Co           28.5         6.6         4.8         5.8         6.8         280         281         0.11         5.8         200         110         118         301         101         101         0.04         ND         0.17         ND           28.0         5.8         10         2.80         2.81         10.1         118         301         101         118         3010         ND         ND         0.17         ND           28.0         5.7         2.80         231         0.15         4.1         2.3         101         118         3010         101 <t< th=""><th>Ō</th><th>Table 4. Sewage Quality Survey (Kandy district) contd</th><th>ey (Ka</th><th>ndy dist</th><th>rrict) con</th><th>ltd</th><th></th><th></th><th>•</th><th></th><th></th><th>Total</th><th></th><th></th><th></th><th></th><th></th></t<>	Ō	Table 4. Sewage Quality Survey (Kandy district) contd	ey (Ka	ndy dist	rrict) con	ltd			•			Total					
86         580         280         220         610.0         30.2         60.8         20.5         20.8         10.7         10.8         10.0         0.46           41         65         190         240         3.8         10.2         16.5         7.08         10.0         10.0         0.46           33         57         250         290         2.14         2.9         26.8         8.31         28410 <sup>4</sup> 10.0         10.0         0.03           35         57         250         290         21.4         2.9         26.8         8.31         28410 <sup>4</sup> 10.0         10.0         0.01           8         8         280         2877         230         11.0         11.39         30x10 <sup>4</sup> 10.0         10.0         10.0           8         2271         100         190         56.1         31.3         13.0         13.0         13.0         13.0         10.0	Tsewage		H	BOD	COD	SS	TDS	Ū	\$04 <sup>2;</sup>	₽-T	۲- ۲-	coliform	ш Soli	As	р О	Zn	ů
20         1716         25931         330         199.5         6.1         85.5         7.08         16x10 <sup>5</sup> ND         ND         1.2           43         8         289         280         234         10.2         16.5         7.08         110         78         ND         ND         0.03           53         57         250         280         21.4         2.9         58.8         8.31         28x10 <sup>4</sup> 18x10 <sup>4</sup> ND         ND         0.03           215         462         130         200         214.0         46.2         30.1         190.6         76x10 <sup>4</sup> ND         ND         ND         0.02           215         462         130         13.2         13.0         190.5         76x10 <sup>4</sup> ND         ND         ND         0.02           216         490         30.6         10.55         30.71         200         24.10         10.71         ND         ND         ND         0.01           317         200         214.0         14.7         30.6         10.55         35x10 <sup>5</sup> ND         ND         ND         ND         ND         ND         ND         ND         <	26.3		6.8	86	580	280	220	610.0	30.2	60.8	20.50	28×10 <sup>5</sup>	28x10 <sup>5</sup>	QN	Q	0.46 .	Q
43         8         289         260         3.8         10.2         16.9         2.2.8         110         78         ND         ND         0.0         0.01           81         8         8         75         250         290         21.4         2.9         2.8.0         13.0         11.8         31.0         11.8         30.010         20.01         30.010         20.01         30.010         30.010         20.01         30.010         30.010         ND         ND         ND         ND         0.02           215         482         130         200         21.4         2.9         2.60         31.2         13.0         13.0         31.2         2.30         13.0         7.21         ND	24.5	-	6.2	20	1716	25931	330	199.5	6.1	85.5	7.08	16×10 <sup>3</sup>	16x10 <sup>3</sup>	QN	9	1.20	2
41         65         190         240         224         1,8         31.0         11,89         30x10 <sup>°</sup> 20x10 <sup>°</sup> ND         ND         0.03           25         57         256         290         21,4         2,9         26.8         8.31         28x10 <sup>°</sup> 18x10 <sup>°</sup> ND         ND         0.02           26         462         130         12.0         274.0         46.2         301         12.05         8.11         28x10 <sup>°</sup> ND         ND         ND         0.02           36         452         100         126.0         49.1         13.0         10.55         66x10 <sup>°</sup> 32x10 <sup>°</sup> ND         ND         ND         0.03           37         150         370         204         99.0         30.0         10.35         30x10 <sup>°</sup> 10x10 <sup>°</sup> ND         ND         0.01           377         200         370         13.5         4.8         20.7         14.1         17.1         18.75         30x10 <sup>°</sup> ND         ND         ND         0.01           30         777         200         37.7         18.75         30x10 <sup>°</sup> ND         ND         ND	26.0		6.6	43	80	289	260	ი თ. თ.	10.2	16.9	2.28	110	78	Q	Q	0.17	0 Z
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	26.0		7.5	<b>4</b> 1	65	190	240	22.4	1.8	31.0	11.89	30×10 <sup>4</sup>	20×10 <sup>+</sup>	Ω Z	Q	0.03	Q
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	27.7		7.6	53	57	250	290	21.4	2.9	26.8	8.31	28×10 <sup>4</sup>	18×10 <sup>4</sup>	Q	Q	0.02	2
6.7         215         462         130         201         19.05         75×10 <sup>2</sup> ND	25.5		7.5	<b>60</b>	ø	280	267	22.4	2.4	24.0	12.20	$24 \times 10^{4}$	16×10 <sup>4</sup>	0 N	Q	0.02	9
6.4         98         227         110         190         135.0         31.2         13.9         10.58         60x10 <sup>2</sup> 32x10 <sup>2</sup> ND         D	26.0	_	6.7	215	462	130	200	214.0	46.2	30.1	19.05	76×10 <sup>2</sup>	42x10 <sup>2</sup>	0 N	Q	Q	22
6.2         143         121         200         270         126.0         49.8         36.5         15.34         62x10 <sup>2</sup> ND         ND         ND         0.09           6.6         33         97         150         370         20.4         99.0         30.0         10.35         30x10 <sup>2</sup> ND         ND         ND         0.09           6.3         30         777         200         322         29.5         69.9         37.1         18.75         3x10 <sup>2</sup> ND         ND         ND         0.01           6.8         12.7         57         100         14.0         14.1         6.6         61.0         14.32         30x10 <sup>2</sup> ND         ND         ND         0.01           6.8         12.7         57         100         14.4         3.5         13.3         11.44         22x10 <sup>2</sup> ND         ND         ND         0.01           6.2         234         97         100         16.0         14.4         3.5         10.1         14.3         32x10 <sup>2</sup> ND         ND         ND         0.01           6.2         2345         97         14.7         33.0         12x10 <sup>2</sup>	26.5	•••	6.4	<u>98</u>	227	110	190	135.0	31.2	13.9	10.58	60×10 <sup>2</sup>	32×10 <sup>2</sup>	Q	Q	0.1	Q
6.6         33         97         150         370         20.4         99.0         30.0         10.35         30x10 <sup>2</sup> 10x10 <sup>2</sup> ND         ND         ND         ND         ND         ND         0.17           6.3         30         777         200         560         38.9         87.3         20.6         25.89         32x10 <sup>2</sup> 12x10 <sup>2</sup> ND         ND         ND         0.01           6.8         12.7         57         100         140         14.1         6.6         61.0         14.32         30x10 <sup>2</sup> 22x10 <sup>2</sup> ND         ND         0.01           6.6         107         33         90         180         13.5         4.8         20.7         11.44         28x10 <sup>2</sup> 20x10 <sup>2</sup> ND         ND         0.01           6.2         345         219         83.00         74.5         63.2         11.44         32x10 <sup>2</sup> 100         10	26.	G	6.2	143	121	200	270	126.0	49.8	36.6	15.34	62x10 <sup>2</sup>	30x10 <sup>2</sup>	0 N	Q	0.09	Q
6.3         81         32         100         560         38.9         87.3         20.6         25.89         32×10 <sup>2</sup> 12×10 <sup>2</sup> ND         ND         0.07           6.3         30         777         200         32.3         29.5         69.9         37.1         18.75         34×10 <sup>2</sup> 8×10 <sup>2</sup> ND         ND         0.07           6.8         12.7         57         100         140         14.1         6.6         61.0         14.32         33×10 <sup>3</sup> 22×10 <sup>2</sup> ND         ND         0.07           6.6         203         97         100         160         14.0         14.1         6.6         61.0         14.32         33×10 <sup>3</sup> 22×10 <sup>2</sup> ND         ND         D0.07           6.6         203         97         100         160         16.0         14.4         4.7         33.0         11.44         32×10 <sup>3</sup> 20×10 <sup>2</sup> ND         ND         D0.07           6.2         345         219         681         270         264         1.3         32×10 <sup>3</sup> 18×10 <sup>3</sup> 20×10 <sup>2</sup> ND         ND         D0.07           6.2         345         2	27.	0	6.6	33	97	150	370	20.4	0.66	30.0	10.35	30×10 <sup>2</sup>	10×10 <sup>2</sup>	Q	Q	Q	9
6.3         30         777         200         323         29.5         69.9         37.1         18.75         34x10 <sup>2</sup> ND         ND         0.17           6.8         12.7         57         100         14.0         14.1         6.6         61.0         14.32         30x10 <sup>3</sup> 22x10 <sup>2</sup> ND         ND         0.03           6.6         107         33         90         180         13.5         4.8         20.7         11.44         22x10 <sup>3</sup> ND         ND         0.03           6.6         203         97         100         160         14.4         4.7         33.0         11.44         22x10 <sup>3</sup> 18x10 <sup>3</sup> ND         ND         0.01           6.2         345         219         681         270         26.9         13.3         11.44         32x10 <sup>3</sup> 18x10 <sup>3</sup> ND         ND         0.01           6.2         345         213         23.1         5.40         122x10 <sup>3</sup> 28x10 <sup>3</sup> 18x10 <sup>3</sup> ND         ND         0.01           6.2         240         33.0         74.5         63.4         13.00         13.0         <11.11         48x10 <sup>6</sup> <t< td=""><td>27</td><td>o.</td><td>6.3</td><td>81</td><td>32</td><td>100</td><td>560</td><td>38.9</td><td>87.3</td><td>20.6</td><td>25.89</td><td>32×10<sup>2</sup></td><td>12×10<sup>2</sup></td><td>0 Z</td><td>Q</td><td>0.07</td><td>g</td></t<>	27	o.	6.3	81	32	100	560	38.9	87.3	20.6	25.89	32×10 <sup>2</sup>	12×10 <sup>2</sup>	0 Z	Q	0.07	g
6.8         12.7         57         100         14.1         6.6         61.0         14.3         20.7         11.44         22x10 <sup>2</sup> ND         ND         0.03           6.6         107         33         90         180         13.5         4.8         20.7         11.44         28x10 <sup>3</sup> 20x10 <sup>2</sup> ND         ND         0.03           6.6         203         97         100         160         14.4         4.7         33.0         11.44         28x10 <sup>3</sup> 20x10 <sup>2</sup> ND         ND         0.03           6.2         345         219         681         270         26.9         1.3         31.1         5.40         12x10 <sup>3</sup> 4.10         ND         ND         0.07           6.2         230         270         270         26.9         1.3         31.1         5.40         12x10 <sup>3</sup> 4.10         ND         ND         0.07           6.2         230         271         5.50         13.3         31.1         5.40         12x10 <sup>3</sup> 4.10         ND         ND         0.07           6.2         251         4.5         10.2         13.3         2.41.6         2.710	27	Ŋ	6.3	30	777	200	323	29.5	63.9	37.1	18.75	34x10 <sup>2</sup>	8×10 <sup>2</sup>	Q	Q	0.17	2
66         107         33         90         180         13.5         4.8         20.7         11.44         28x10 <sup>3</sup> 20x10 <sup>2</sup> ND         ND         0.07           6.6         203         97         100         160         14.4         4.7         33.0         11.44         28x10 <sup>3</sup> 20x10 <sup>2</sup> ND         ND         0.07           6.2         340         976         201         296         17.4         3.6         63.2         17.70         18x10 <sup>3</sup> <10         ND         ND         0.07           6.2         345         219         681         270         265         1.3         31.1         5.40         12x10 <sup>3</sup> <10         ND         ND         0.07           6.2         293         17.5         198         380.0         74.5         6.3.4         13.00         130         <10         ND         ND         0.07           6.2         193         380.0         74.5         6.3.4         13.00         130         <10         ND         ND         0.01           7.2         150         251         4.0         15.40         12.410 <sup>6</sup> 3.410 <sup>6</sup> ND	25	S	6.8	12.7	57	100	140	14.1	6.6	61.0	14.32	30×10 <sup>3</sup>	22×10 <sup>2</sup>	Q	Q	0.03	g
6.6         203         97         100         160         14.4         4.7         33.0         11.44         32x10 <sup>3</sup> 18x10 <sup>2</sup> ND         ND         0.07           6.2         340         976         201         296         17.4         3.6         63.2         17.70         18x10 <sup>3</sup> <10	25	Ŋ	6.6	107	33	60	180	13.5	4.8	20.7	11.44	28×10 <sup>3</sup>	20×10 <sup>2</sup>	Q	Q	0.07	2
6.2         340         976         201         296         17.4         3.6         63.2         17.70         18x10 <sup>3</sup> <10         ND         ND         ND         0.54           5.2         345         219         681         270         269         1.3         31.1         5.40         12x10 <sup>3</sup> <10	3	0.	6.6	203	97	100	160	14.4	4.7	33.0	11.44	32×10 <sup>3</sup>	18×10 <sup>2</sup>	g	g	0.07	2
5.2       345       219       681       270       26.9       1.3       31.1       5.40       12×10 <sup>3</sup> <10	30	ŝ	6.2	340	976	201.	296	17.4	3.6	63.2	17.70	18×10 <sup>3</sup>	<10	Q	2	0.54	D Z
6.2         290         202         175         198         380.0         74.5         6.3.4         13.00         130         <10         0.902         ND         0.13           7.2         150         251         450         240         30.9         12.9         44.3         6.13         40x10 <sup>6</sup> 3x10 <sup>6</sup> ND         ND         0.17           7.2         150         251         450         240         30.9         12.9         44.3         6.13         40x10 <sup>6</sup> 3x10 <sup>6</sup> ND         ND         0.14           6.8         52.7         48         650         191         17.0         10.8         15.4         8.66         42x10 <sup>6</sup> ND         ND         ND         0.14           10.8         20.2         57         560         280         17.0         13.4         19.5         4.74         16x10 <sup>6</sup> 3x10 <sup>6</sup> ND         ND         0.0           6.8         100         73         180         260         17.0         13.4         19.5         4.74         16x10 <sup>6</sup> 3x10 <sup>6</sup> ND         ND         0.0           6.9         3.2         130         15.52         <	Ň	9.5	5.2	345	219	681	270	26.9	1.3	31.1	5.40	12×10 <sup>3</sup>	v10 V	Q	Q	0.07	g
6.4         10.2         11.3         270         270         15.5         10.9         39.4         11.17         48x10 <sup>6</sup> ND         ND         ND         0.17           7.2         150         251         450         240         30.9         12.9         44.3         6.13         40x10 <sup>6</sup> 3x10 <sup>6</sup> ND         ND         0.14           6.8         52.7         48         650         191         17.0         10.8         15.4         8.66         42x10 <sup>6</sup> ND         ND         0.14           10.8         20.2         57         560         260         93.3         21.3         23.1         7.67         18x10 <sup>6</sup> ND         ND         ND         0.14           6.8         100         73         180         260         17.0         13.4         19.5         4.74         16x10 <sup>6</sup> 3x10 <sup>5</sup> ND         ND         0.16           5.9         75.2         130         160         351         17.0         15.52         14x10 <sup>6</sup> 2x10 <sup>5</sup> ND         ND         0.06           6.9         3.2         129         17.1         174.2         8.15         45x10 <sup>6</sup>	2	7.2	6.2	290	202	175	198	380.0	74.5	63.4	13.00	130	₹ 10	0.902	2	0.13	0 Z
7.2         150         251         450         240         30.9         12.9         44.3         6.13         40x10 <sup>6</sup> 3x10 <sup>6</sup> ND         ND         0.14           6.8         52.7         48         650         191         17.0         10.8         15.4         8.66         42x10 <sup>6</sup> ND         ND         ND         0.14           10.8         20.2         57         560         260         93.3         21.3         23.1         7.67         18x10 <sup>6</sup> X10 <sup>6</sup> ND         ND         0.14           6.8         100         73         180         260         17.0         13.4         19.5         4.74         16x10 <sup>6</sup> 3x10 <sup>6</sup> ND         ND         0.06           6.9         3.2         120         17.0         13.4         19.5         4.74         16x10 <sup>6</sup> 3x10 <sup>6</sup> ND         ND         0.06           6.9         3.2         1230         160         361         17.0         5.4         19.0         15.52         14x10 <sup>6</sup> 2x10 <sup>6</sup> ND         ND         0.06           7.9         3.1         1343         201         3100         676.1	Ň	4.0	6.4	10.2	113	270	270	15.5	10.9	39.4	11.17	48×10 <sup>6</sup>	3x10°	Q	Q	0,17	9 2
6.8         52.7         4.8         650         191         17.0         10.8         15.4         8.66         42×10 <sup>6</sup> ND         ND         ND         0.1           10.8         20.2         57         560         260         93.3         21.3         23.1         7.67         18×10 <sup>6</sup> 2×10 <sup>5</sup> ND         ND         0.0           6.8         100         73         180         260         17.0         13.4         19.5         4.74         16×10 <sup>6</sup> 2×10 <sup>5</sup> ND         ND         0.0           5.9         75.2         130         160         361         17.0         5.4         19.0         15.52         14×10 <sup>6</sup> 2×10 <sup>5</sup> ND         ND         0.0           6.9         3.2         1246         273         5280         794.3         7.8         223.1         8.15         45×10 <sup>4</sup> 2×10 <sup>5</sup> ND         ND         0.0           7.9         31         1343         201         3100         676.1         17.7         174.2         8.00         4500         1200         ND         ND         0.0           7.5         12.8         27         10.9 <t< td=""><td>2</td><td>6.0</td><td>7.2</td><td>150</td><td>251</td><td>450</td><td>240</td><td>30.9</td><td>12.9</td><td>44.3</td><td>6.13</td><td>40×10<sup>6</sup></td><td>3X10<sup>6</sup></td><td>Ð</td><td>Q</td><td>0.14</td><td>g</td></t<>	2	6.0	7.2	150	251	450	240	30.9	12.9	44.3	6.13	40×10 <sup>6</sup>	3X10 <sup>6</sup>	Ð	Q	0.14	g
10.8         20.2         57         560         26.0         93.3         21.3         23.1         7.67         18×10 <sup>6</sup> 2×10 <sup>5</sup> ND         ND         0.06           6.8         100         73         180         260         17.0         13.4         19.5         4.74         16×10 <sup>6</sup> 2×10 <sup>5</sup> ND         ND         0.06           5.9         75.2         130         160         361         17.0         5.4         19.0         15.52         14×10 <sup>6</sup> 2×10 <sup>5</sup> ND         ND         0.01           5.9         75.2         130         160         361         17.0         5.4         19.0         15.52         14×10 <sup>6</sup> 2×10 <sup>5</sup> ND         ND         0.05           7.9         3.1         1343         201         3100         676.1         17.7         174.2         8.00         4500         1200         ND         ND         0.05           7.5         12.8         2.4         70         25.7         10.9         29.9         7.46         3000         140         ND         0.05           7.5         7.7         2.4         6.0         43.1         5.75	2	5.0	6.8	52.7	48	650	191	17.0	10.8	15.4	8.66	42×10 <sup>6</sup>	4×10°	Q	92	0.1	g
6.8         100         73         180         260         17.0         13.4         19.5         4.74         16×10 <sup>6</sup> 3×10 <sup>5</sup> ND         ND         ND         0.1           5.9         75.2         130         160         361         17.0         5.4         19.0         15.52         14×10 <sup>6</sup> 3×10 <sup>5</sup> ND         ND         ND         0.1           6.9         3.2         1246         273         5280         794.3         7.8         223.1         8.15         45×10 <sup>6</sup> 2×10 <sup>5</sup> ND         ND         0.37           7.9         31         1343         201         3100         676.1         17.7         174.2         8.00         4500         1200         ND         ND         0.30           7.5         12.8         24         70         2770         25.7         10.9         29.9         7.46         3000         140         ND         0.03           7.5         7.7         24         660         250         74.1         14.4         10.3         7.46         2500         100         ND         0.05           7.0         220         97.1         5.75         2500 <td>N</td> <td>4.0</td> <td>10.8</td> <td>20.2</td> <td>57</td> <td>560</td> <td>260</td> <td>93.3</td> <td>21.3</td> <td>23.1</td> <td>7.67</td> <td>18×10<sup>5</sup></td> <td>2X10°</td> <td>Q</td> <td>Q</td> <td>0.06</td> <td>g</td>	N	4.0	10.8	20.2	57	560	260	93.3	21.3	23.1	7.67	18×10 <sup>5</sup>	2X10°	Q	Q	0.06	g
5.9       75.2       130       160       361       17.0       5.4       19.0       15.52       14×10 <sup>6</sup> 2×10 <sup>5</sup> ND       ND       0.37         6.9       3.2       1246       273       5280       794.3       7.8       223.1       8.15       45×10 <sup>4</sup> 2×105       ND       ND       0.30         7.9       31       1343       201       3100       676.1       17.7       174.2       8.00       4500       1200       ND       ND       0.30         7.5       12.8       24       70       270       25.7       10.9       29.9       7.46       3000       140       ND       0.057         7.5       7.7       24       660       25.0       74.1       14.4       10.3       7.46       2500       100       0.05         7.0       220       97       110       270       31.6       6.0       43.1       5.75       2500       100       ND       0.05         7.0       220       97       110       270       31.6       6.0       43.1       5.75       2500       100       ND       0.05         7.0       220       97       146	Ñ	5.0	6.8	100	73	180	260	17.0	13.4	19.5	4.74	16×10 <sup>6</sup>	3x10 <sup>5</sup>	Q	Q	0.1	2
6.9         3.2         1246         273         5280         794.3         7.8         223.1         8.15         45×10 <sup>4</sup> 2×105         ND         ND         0.30           7.9         31         1343         201         3100         676.1         17.7         174.2         8.00         4500         1200         ND         ND         0.30           7.5         12.8         24         70         2770         25.7         10.9         29.9         7.46         3000         140         ND         0.67           7.5         7.7         24         660         250         74.1         14.4         10.3         7.46         3000         140         ND         0.03           7.6         220         31.6         6.0         43.1         5.75         2500         100         ND         0.05           7.0         220         97         110         270         31.6         6.0         43.1         5.75         2500         100         ND         0.05           7.0         220         97         10.3         7.46         2500         100         ND         0.05           7.0         220         37.	Ň	5.0	5.9	75.2	130	160	361	17.0	5.4	19.0	15.52	14×10 <sup>6</sup>	2X10 <sup>5</sup>	Q	g	0.37	9
7.9     31     1343     201     3100     676.1     17.7     174.2     8.00     4500     1200     ND     ND     0.57       7.5     12.8     24     70     270     25.7     10.9     29.9     7.46     3000     140     ND     0.03       7.5     7.7     24     660     250     74.1     14.4     10.3     7.46     2500     100     ND     0.05       7.0     220     97     110     270     31.6     6.0     43.1     5.75     2500     100     ND     0.05	ň	5.0	6.9	3.2	1246	273	5280	794.3	7.8	223.1	8.15	45×10 <sup>4</sup>	2x105	Q	Q	0.30	0 Z
7.5     12.8     24     70     270     25.7     10.9     29.9     7.46     3000     140     ND     0.03       7.5     7.7     24     660     250     74.1     14.4     10.3     7.46     2500     100     ND     0.05       7.0     220     97     110     270     31.6     6.0     43.1     5.75     2500     100     ND     0.06	28	80	7.9	31	1343	201	3100	676.1	17.7	174.2	8.00	4500	1200	Q	Q	0.57	ß
7.5         7.7         24         660         250         74.1         14.4         10.3         7.46         2500         100         ND         0.05           7.0         220         97         110         270         31.6         6.0         43.1         5.75         2500         100         ND         0.06	25	У	7.5	12.8	24	20	270	25.7	10.9	29.9	7.46	3000	140	Q	Q	0.03	2
7.0 220 97 110 270 31.6 6.0 43.1 5.75 2500 100 ND ND 0.06	22	0	7.5	7.7	24	660	250	74.1	14.4	10.3	7.46	2500	100	Q	Q	0.05	g
	25	0	7.0	220	97	110	270	31.6	6.0	43.1	5.75	2500	100	g	g	0.06	P

Sampling points

High Income house - domestic sewege
 Middle income house - domestic sewege
 Low income house - domestic sewege

4. Hantana scheme- beforte treatment

5.Education office

6. High Income house- effluent from septic tank
 7. Middle income house -effluent from septic tank
 8. Low income house- effluent from septic tank

9. University office -effluent from septic tank

0. Hantana scheme- after treatment

1. Hotel with treatment facility -Suisse hotel influent

Hotel with treatment plant Suisse hotel -effluent
 Hotel without treatment facility - Riverdale grey water

Industrial waste water-Chocolate company before treatment
 Industrial waste water- Chocolate factory after treatment

 Industrial waste water -Sun match company
 Hospital sewege- Peradeniya hospital- before treatment
 Hospital sewege- Peradeniya hospital - after treatment
 Sewage effluent from Gohagoda at the dumping site
 Sewage effluent from Gohagoda at the stream which flows into river just before entry into river
 NWSDB

Table 5. Sewage Quality survey( Nuwara-Eliya district)	÷.	-Eliya dist	rict)			•			Total	:			t
TDS	COD SS TDS	TDS			ರ	SO₄ <sup>2-</sup>	N-T	q H	coliform	E. Coli	As	8 9	N Z
90.2 510.1 220	510.1 220		250		30.2	Q	31.6	7.47	23×10°		2	2 S	71.0
6.8 275.2 866.3 210	866.3 210		270		239.0	13.6	50.8	13.01	23×10 <sup>°</sup>	<b>0</b> 12		2	4
591 170	591 170		410		193.0	6.9	38.2	18.66	18×10°	، مان م		g g	0.0Z
10.4 143 251 82	251 82		240		7.9	52.8	78.5	5.58	11×10 <sup>°</sup>	2X10 <sup>°</sup>	2	n g	60'n
10.2 50 194 67	194 67		250		33.9	53.8	23.0	10.33	9x10č	5×10			0.06
10.4 188 81 50	81 50		350		37.2	55.3	44.7	7.49	11×10°	2X10 <sup>°</sup>		2 S	0.08
6.2 150 146 150	146 150		253	1	7.1	1.2	52.2	7.97	130×10°	<10 <10	Q Z	Q I	0.08
6.4 120 40 70	40 70		225		7.9	1.3	25.1	7.92	90×10'	<10	Q	Q	0.06
38 81 30	81 30		190		6.8	1.9	62.4	10.31	100×10 <sup>3</sup>	<10	0 Z	Q	0.06
6.6 115 16 80	16 80		160		50.1	2.8	15.3	5.80	300×10 <sup>2</sup>	200×10 <sup>2</sup>	0 Z	Q	0.05
90 437 70	437 70	•	180		10.9	4.6	72.4	10.98	250×10 <sup>2</sup>	180×10 <sup>2</sup>	Q	0 Z	0.04
8.0 5 65 60	65 60		240		53.7	10.6	28.6	12.50	320x10 <sup>2</sup>	200×10 <sup>4</sup>	Q	0 Z	0.44
6.4 325.2 1846 336	1846 336		350		166.0	17.5	74.5	7.54	13×10 <sup>6</sup>	49×10 <sup>5</sup>	QZ	Q	0.28
7.0 75.2 145.7 148	145.7 148		<b>6</b> 3		14.4	9.9	21.7	7.84	33×10°	26×10'	Q	Q Z	n Z
120 540 210	540 210		420		156.0	24.2	54.2	11.80	5x10°	5x10 <sup>°</sup>	OZ :	o i	0.22
6.8 140 526 180	526 180		430		128.0	20.2	50.8	10.20	5x10 <sup>°</sup>	5×10 <sup>°</sup>	Q I		0.10 0.10
6.8 136 488 200	488 200		520		148.2	23.8	62.0	12.80	4x10°	4×10°	Q I	<u>g</u>	0.15
6.9 180 809 350	809 350		510		299.0	21.8	69.9	21.54	11×10°	11×10°			0.22
6.9 153 518 350	518 350	•	470		162.0	30.6	44.2	20.05	10×10°	10×10°	Q	Q Z	0.14
6.9 73 243 320	243 320		430		229.0	30.9	33.1	21.39	8x10 <sup>°</sup>	8x10°	2	Q	0.07
6.7 132 320 220	320 220		310		120.0	16.2	61.8	18.60	14×10 <sup>3</sup>	14×10 <sup>3</sup>	Q	g	0.12
6.5 110 276 178	276 178		382		110.6	20.4	58.6	17.40	12×10 <sup>3</sup>	12X10°	0	0 Z	0.14
148 318 148	318 148		412		100.8	18.6	65.6	18.20	16×10 <sup>3</sup>	16×10'	Q	Q Z	0.12
6.8 230 710 82	710 82		190		100.6	10.2	80.4	6.80	17×10 <sup>6</sup>	11×10°	Q	g	0.22
6.8 216 652 104	652 104		160		120.4	11.5	86.8	7.20	13×10 <sup>6</sup>	10×10 <sup>6</sup>	g	۵ Z	0.2
6.8 208 720 120	720 120		182		110.5	10.8	75.8	5.80	18×10 <sup>6</sup>	10×10 <sup>6</sup>	Q	Q	0.14
<b>6.0</b> 118 178 10	178 10		197		79.4	6.2	83.5	14.29	94×10 <sup>2</sup>	94×10 <sup>2</sup>	0 Z	Q	0.07
6.9 75 219 10	219 10		230		44.7	4.2	31.1	12.43	82×10 <sup>2</sup>	80×10 <sup>2</sup>	Q	Q	0.08
7.1 153 146 50	146 50		220		33.9	10.5	83.5	16.11	86×10 <sup>2</sup>	86×10 <sup>2</sup>	Q	g	0.07

	ů	29		2 9					<u>ב</u>	2	2	2 S		Z	Q																
	uZ	0.04	0.04	0.05	10.0	0.27	0.34 4.0	0.09	0.19	0.19	0.U5	0.U6	0.09	0.82	0.19					finant	L Totoria	1/ Factory emulant - menasinon									
	b	2	2	o i	2	2 g	29		2	2	2		99	Q	Q					te Taa Daataa, affinant		uy enuen									
	As	Q Z	Q	O Z	o i	<b>2</b> 9	Q.	2	o Z	g g		Q I	2	D N	Q					10 100		17. 14.							·		
	ш 8 Ш	<10	~10 ^1	<10	v10	v10	<10	v10	×10	<10	ZX10	2×10°	2X10°	<10 10	18×10 <sup>2</sup>				•												
TotoT	coliform	6.8x10 <sup>2</sup>	6.4x10 <sup>2</sup>	5.2x10 <sup>4</sup>	23x10 <sup>4</sup>	18×10 <sup>+</sup>	26×10⁴	17×10°	12×10°	18×10č	79×10°	82×10°	86×10°	40	35x10 <sup>4</sup>							lei			÷					2	
	d-L	13.80	12.10	8.82	6.05	9.74	9.33	22.51	13.30	15.26	6.82	16.98	10.17	4.67	4.77							e - hotel without treatment facility- Windsor hotel	•	-			Before treatment	atment	1	water- effluent after treatment (Ceylon Brewery)	
	<b>N-1</b>	36.6	22.0	27.1	29.6	32.1	42.7	31.1	28.0	66.69	44.2	31.1	44.1	29.1	31.3							acility- V	(asr				Before ti	After trea	13. Industrial waste water- drain (Ceylon Brewery)	ent (Cey	
	SO4 <sup>2-</sup>	15.3	14.4	15.6	97.7	89.4	8.1	29.4	28.8	7.8	1.6	1.6	1.7	0.3	0.5							atment f	ome hot	est)	6) (i)	lity)	Hotel	I Hotei	In Brewe	r treatm	
	ū	25.1	32.4	15.8	6.3	3.1	5.0	16.2	16.2	7.4	14.1	53.7	4.4	5.0	19.9	(0400	(alling)	le)	iotel)		÷	out tre:	ddle inc	ybank r	m hous	unicipa	- Gran	- Grano	i (Ceylo	ent afte	
÷	TDS	80	180	60	1090	160	120	1322	896	1332	180	240	340	62	346	ant alter	(aunoui aiddiw) a	e (Low income)	e (ceybank hotel)	unicipality		otel with	Effluent from septic tank (Middle income house)	Effluent from septic tank (Ceybank rest)	<ol><li>Effluent from septic tank (slum house)</li></ol>	10. Effluent from septic tank (municipality)	ment facility - Grand Hotel	t facility	er- drair	er- effu	
ict) cont	SS	20	30	10	3300	370	196	2556	1186	2545	06	110	180	37	427		wage (M			e-Munic	house	wage - h	n septic t	septic t	n septic t	m septic	reatmen	reatmen	aste wat	aste wat	wage
iya distr		57	49	97	980.7	1174	57	820.1	712	777	49	49	24	372.4	170		1. Domestic sewage	Domestic sewage	3. Domestic sewage	4. Office sewege-Mi	<ol><li>Local eating house</li></ol>	Domestic sewag	ent from	ent from	ent from	uent fro	11. Hotel with treat	el with t	ustrial w	4. Industrial waste	5. Hospital sewag
wara-El		125	65	25	63	13	80	298	190	288	37	ŝ	ო	60.2	100.2	(	1. Dom	2. Dom	3. Dom	4.Office	5. Loca	6. Dom	7. Efflu	8. Efflu	9. Efflu	10. Eff	11. Hot	11. Hot	13. Indi	14. Indi	15. Hos
ey (Nur	, T	8.9	6.8	6.8	2.9	3.7	6.2	6.5	6.9	6.9	6.2	7.4	66	10	7.3		Eliya										•				
uality surv	Tsewade	21.0	215	20.5	21.5	18.0	20.0	25.0	25.0	24.0	17.0	17.5	17.5	24 5	23.2		Nuwara - Eliya				•	·									•
vede Q	, r ie	19.5	17.0	17.0	22.5	17.0	17:0	22.5	17.0	17.0	20:0	19.0	17.0	2.1	210	ts		•			•		•		•						1
Table 5. Sewege Quality survey (Nuwara-Eliya district) contd.	alumeS	SO/N/12 1	SO/N/12 2	SO/N/12 3	SON/13.1	SQ/N/13.2	SO/13.3	SO//14.1	SO/N/14.2	SO//14.3	SO/N/15-1	SOM/15.2	SOM/15.2		SQN/17	Sample points			: 		•	•							-		1 14 24 1

Kandy:	RWQ/K/I	Gangawata Korale- near University Gymnasium
	RWQ/K/2	Intake point of Kandy water treatment plant
	RWQ/K/3	Katugastota district (Pinga oya near meda-ela bridge)
	RWQ/K/4	Polgolla dam site intake
	RWQ/K/5	Stream near Polgolla University
	RWQ/K/6	Kundasale intake
	RWQ/K/7	Meda Ela
	RWQ/K/8	Down stream of the Gohagoda dumping site
Nuwara-Eliya	1 '	
	RWQ/N/1	Upstream of city's borders
	RWQ/N/2	Victoria park
	RWQ/N/3	Influent point to Gregory lake
	RWQ/N/4	Upstream of Hospital and Brewery
	RWQ/N/5	Influent point to Barrack's plain reservoir

The analytical data for samples are given in tables 6 & 7. The samples were most of the times brownish and muddy showing an increase in suspended solids and sometimes even high total dissolved solids during this season compared to the previous dry season data. The samples taken from Meda Ela which is a highly polluted canal show increased nitrate, sulphate, coliforms, suspended solids, etc. Dissolved oxygen was also very low for these samples.

Those samples collected from Nuwara Eliya were highly contaminated compared to Kandy samples. In particular, those samples collected at the influx point to Barracks Plain reservoir had very little dissolved oxygen with relatively high pH values. Also RWQ/N/4 and RWQ/N/5 showed high suspended and dissolved solids, high total nitrogen and high BOD values. These samples also had high COD values indicating increased contamination from organic wastes. This can be easily explained since sewage from the hospital, factories and even households are directly added to the stream feeding the Barracks Plain reservoir. There is also intensive agricultural activities and a lot of houses dumping septic tank wastes direct into this stream which explains the abnormal values for COD,SS, TDS and chloride for sample N/4.1. However apart from zinc which probably originate from rusting galvanized iron, heavy metal contamination is virtually non-existent.

It is also clear that the sample RWQ/N/3at the Victoria Park is highly contaminated due to coliforms and E. *coli* compared to RWQ/N/1 and RWQ/N/2. This is due to increased faecal contamination from human activity in the city.

Out of the Kandy samples RWQ/K/3 and RWQ/K/7 are those collected from Pinga-Oya and Meda-Ela and these are highly polluted streams which feed the Mahaweli river and this is the cause of their high level of contamination. The sample collected

	8	7.5	7.4	7.3	7.2	7.4	7.9	4 8	9.4 1	3.8 8	4.0	10		4	4.5	ы. 4	3.8	7.6	7.3	7.3	3.6	С «		0.3	7.6	
	800	3.7	4.2	3.2	1.7	1.2	1.7	4 7	4.7	4 2	4 7	~ ~	9 Q	4 2	6.4	4.2	3.2	4.2	3.7	3.2	7.7	α ٢	0.	8.2	N T	
	Condu	67.8	49.2	51.0	57.1	50.9	53.3	126.0	145.0	116.0	58.4		00.00	58.4	260.0	260.0	260.0	53.7	56.2	54.7	400.0		0.040	450.0	110.8	
	ပိ	2 Z	9	g	g	C Z	ź	ŝ	ŝ		2 5		<u>ב</u>	2 Z	Q	Q	0 Z	0 Z	g	g	C Z		Z	g	2 Z	
	ЧZ	0.02	Q	0.05	0.02	Z		200						Q	2 Z	0.01	0.02	0.13	Q	Z	Ś		17.0	0.21	Q	
	As	g	g	2	2 Z	ź					22	22	Z	g	Q	0 Z	0 Z	C Z	Z	Ê		2	Z	g	0 Z	
	S	Q	0 N	0 Z	Z								Z	Q	Q	Q	Q	Ż	Ż		ŝ			9	Q	
	ö	4.3	3.2	36	64			0 C	7 ( 7 (		່ວ່ວ	0 L 0 Q	13.5	3.2	17.9	7.1	7 9	8	i e	00	a i i t		44./	33.1	6.9	
	E. coli	600	1000	1200	1100			000			0071	800	200	1100	1200	1000	1000	1050	1350				1100	1000	1200	
	Total	2200	1700				2200	1300		0051	1450	2000	1300	1600	1900	0020	1750	1200				2000	1750	1400	2600	
	<del>д</del> -1	0.63		24.0			0.0 4 0	0.80	0.85	ی ج د د	0.50	0.85	0.65	0.80	1 07	78				0 00 7 0 0 7 0 0		0.92	0.4 1	0.95	140	2
	z- ⊢	0				0, 0 	4 9 9	5.1	9 0 7	6.Z	0. 7	- - -	າ ເບ	16.4	103	) (   -   -	- c		N I			12.0	10.7	5	8 27	
	SO₄ <sup>2-</sup>	ר ז	- <del>-</del>	0 <b>1</b> - c			9.	9	2.3	<del>ر</del> . دی	1.5	4.0	6.1	ີ ເດ ແຕ	44	t u	- 1 - 1	- (	21 C		4	6.6	13.0	A A	- 4 	<u>;</u>
	TDS	, ,		24.0 7 7 0	6.07 1	28.5	25.5	26.7	33.3	72.2	58.0	29.1	28,9.	00	120.0		2.00	0.821	20.02	28.2	21.3	200.0	270.0	0.000	0.011	2
district)	- SS	Ċ		20				110							- <b>T</b>			-			130	20 2(	30.2			2
(Kandy	COD		2°.	x x	8	8	16.2	32.4	32.4	24.3	4.0	<u>8</u> .1	8.1	- u	1 2 0		10.Z	32.4	8	œ	œ.	48.6	32 4		2 th 1	0.0
survey	F		5.4	5.4	5.7	5.5	5,4	5.0	6.2	5.2	5.2	5.1	5	4 C	) - 	י קי ני נ	4	<b>5.</b> 6	2.0	5.0	5.0	6.4	с Ч	) ( ) L	0	4.
Quality \$	water		23.6	23.7	24.3	22.9	23.7	23.9	25.4	27.3	26.2	25.0	141		23.0	26.3	26.5	26.1	26.6	26.0	24.0	25.1	26.4		20.2	24.2
r Water	Tair T	-	23.1	24.6	23.9	24.8	26.4	23.7	25.5	27.3	24.9	27.4	O YC		2 <b>4</b> .0	26.4	27.0	26.0	26.4	27.1	23.4	25.0		20.0	24.5	33.0
Table 6. River Water Quality Survey (Kandy district)	elomoo	odilibic	RWQ/K/1.1	RWQ/K/1.2	RWO/K/1.3	RWQ/K/2.1	RWO/K/2.2	RWQ/K/2.3	RWO/K/3.1	RWQ/K/3.2	RWO/K/3.3	RW0/K/4.1	C FINOWA		RWQ/K/4.3	RWQ/K/5.1	RWQ/K/5.2	RWO/K/5.3	RWQ/K/6.1	RWQ/K/6.2	RWO/K/6.3	RWO/K/7.1			RWO/K/7.3	RWQ/K/8.1

 2. Gatambe intake
 3. Pinga-Oya
 4. Doragamuwa junction
 5. Open University - Polgolla
 6. Kundasale
 7. Meda ela 1. Gymnasium

Kandy

River water quality Sample points

8. After Gohagoda intake

i

	8	7.9	8.4	7.7	5.5	5.1	3.5	5.1	5.1	4.8	5.4	5.3	3.7	2.2	1.9	4.7	
	BOD	0.6	0.5	0.5	6.8 9	3.7	25.7	0.7	3.2	21.7	25.2	18.7	25.2	28.2	28.5	21.7	
Condu	ctivity	15.3	12.3	12.7	53.0	62.0	76.0	66.0	70.0	84.0	126.0	144.6	116.0	58.4	58.0	58.4	
	ပိ	Q	Q	Ð	Ð	Q	0 Z	Q	Q	g	Ð	g	0 Z	Q	Q	g	
	Z	0.19	0.21	0.03	0.05	0.07	0.39	0.06	0.02	0.43	0.21	0.10	0.69	0.25	0.15	0.23	
	As	Q	Q	Q	Q	ĝ	0 Z	Q	Q	Q	Q	02	0Z	0 Z	g	Q	
	8	Q	Q	Q	0 Z	Q	D	g	Ð	Q	Q	Q	Q	Q	Q	Q	
	ច់	6.8	5.1	5,9	15.8	10.9	17.8	11.2	12.3	15.8	26.9	26.9	20	22.9	46.8	20.9	
	ію Ш	IIN	20	40	60	20	30	600	1180	760	70	30	10	10	1000	650	
	tal colifor	02	100	120	150	20	400	2400	3000	2000	340	210	110	120	4500	1000	
	а Н	3.91	4.73	7.16	6.98	2.73	10.56	3.40	6.26	10.86	8.61	6.46	7.03	7.41	6.46	4.60	
	z- L	1.27	5.30	13.36	13.36	3.30	8.66	0.59	1.30	20.08	5.97	3.60	2.61	20.08	1.90	1.94	
	so42-	0.95	1.60	1.10	1.13	1.18	1.12	4.75	4.00	6.10	3.60	5.15	6,00	8.13	8.25	16.30	
	TDS	4	28	44	53	~	63	<u>5</u>	83	60	21	121	133	290	141	310	
	SS	40	20	33	200	180	62	30	120	30	46	380	620	220	300	591	
	COD	48.6	218.6	12.1	36.4	16.2	291.4	8	40.5	680.0	81.0	307.6	202.4	60.7	153.8	121.4	
	На	99	9.9	6.8	94		99	63	929	) () () () ()	99	8.9	6.8	99	9.5	1.3	
	water	14.0	14.7	180	17.0	16.0	17.0	15.6	16.2	19 19 19	17.5	18.2	17.0	19.2	19.7	16.0 18.0	
	Tair	20.0												18.0	0.02	16.0	•
	Sample		C L/NOMA	EWON13		EWOND 2						RWO/N/4.2	BWO/N/4 3	EWO/N/51	PWON/5 2	RWON/53	

Nuwara - Eliya 1. Top Pass 2. Victoria Park 3. Gregory Lake 4. Hawa Eliya 5. Vajira Mawatha

Table 7. River Water Quality (Nuwara-Eliya district)

from a stream near Polgolla (RWQ/K/5) was also polluted which is reflected in the analytical data with high total nitrogen, chloride and BOD.

#### 4. Lake water quality

The location from where samples were collected and the key to samples is given below.

Kandy: LWQ/K/1, LWQ/K/2, LWQ/K/3, LWQ/K/4 Kandy Lake water samples along the length of the Lake on the Temple of the Tooth side (locations shown in the attached map)
 LWQ/K/5, LWQ/K/6, LWQ/K/7, LWQ/K/8 Kandy lake samples along the length of the Lake opposite the Temple of the Tooth side

LWQ/N/1	Gregory lake (near playground)
LWQ/N/2	Gregory lake (middle of the lake -southern end)
LWQ/N/3	Barrack Plains Reservoir (at the beginning)
LWQ/N/4	Barrack Plains Reservoir (end)
LWQ/N/5	Barrack Plains Reservoir (middle)
LWQ/N/6	Barracks Plains Reservoir (middle)
LWQ/N/7	Gregory lake(middle)
LWQ/N/8	Gregory lake(middle)

Note : More samples were collected from the lakes this season compared to the last season since it was felt that two samples collected in the first phase may not be enough to give a representative picture of the entire lake.

The analytical data are given in table 8 & 9.

The Kandy lake is relatively unpolluted compared to Nuwara Eliya lake system as seen in its higher DO values and lower COD values.

However, the total dissolved solids of the Kandy lake samples was relatively high due to more electrolytes dissolved in it and clearer water (less suspended solids). The barracks Plains reservoir which was virtually dry during the first phase was quite full of water at this time of collection.

Nuwara- Eliya lakes in general had high phosphate, high total nitrogen and high sulphate compared to Kandy lake. This is due to leaching of fertilizer residues sprayed on to vegetable plots during the dry season and which gets washed into lakes during the rainy season. The bacteria counts also show significant enhancement in spite of the dilution effects due to rain. This is because a lot of sewege and human waste get washed down with the rain and increase both coliform and E.Coli counts in the reservoirs.

	ថ	14.8	12.8	13.6	14°.		10.8	12.8	11.6	11.8	13.5	12.5	12.8	13.2	13.0	10.2	14.2	12.8	12.6	11.5 V	11.5	1.5	12.5	14.6	14.5	<b>?</b>	
Elec	Con	260.0	250.0	248.0	260.0	230.0	250.0	250.0	276.0	240,0	240.0	244.0	238.0	260.0	250.0	244.0	261.0	250.0	256.0	266.0	276.0	276.0	260	270	256	>	
	ပိ	ĨŻ	ΞŻ	ΞZ	ĒZ	ĨŻ	Z	Ī	ĪZ	EZ	ΞZ	IIN	EN	ĨŽ	ΞZ	Z	Ē	Nii	Ē	Z	ĨZ	ž	IZ	Z	EN.	111	
	Ч	Ē	ĨŻ	Z	Ī	ĪŻ	Ī,	Ē	IIN	ĒZ	ΪŻ	ĪŽ	Ē	0.96	0.78	0.83	1.96	1.96	1.86	ΪŻ	Ĩ	ī	ΪŻ	Ĩ	iiN	11	
	8	Ī	īz	Ē	īž	ΞŻ	ĒŻ	ΞŻ	ĨŻ	ËŻ	Ī	Ē	Ē	ΕŻ	EZ	Ē	ĪŽ	Ī	ĪŽ	Z	ΞŻ	ĒŻ	ĪZ	ĒŽ	EN		
Total	lon	0.06	0,1	0.08	0.23	0.2	0.26	0.64	0.52	0.68	0.32	0.36	0.3	0.25	0.26	0.3	1.25	1.25	1.28	4 12	1,2	1.2	2.38	1.78	4 A B	00.1	
	As	ĪŻ	, IIN	ΪÏ	ĨŻ	ΪŻ	ΞŻ	ΪŻ	ΪŅ	Ī	IIN	IIN.	ĩ	Nil	Nii	1!IZ	ΪŻ	ĨŻ	ΕŻ	ïŻ	ÎŻ	Ī	NIL	NIC		NIC	
	E.Coli	4500	2000	3000	1000	2200	2000	1200	1400	1200	800	1200	1000	1700	1200	1100	1700	1700	1700	14000	14000	14000	12000	12000		10000	
Total	coliform																										
	Ŭ	1.83													•										·		
		9.46			-				•																		
	so4 <sup>2-</sup> 1																										
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		63.0						·							•		•										
		റ																					-		-	•	
	_	3.2			•																						
		32.4	36.2	34.8	32.8	34.8	30.4	40.5	46.5	38.6	42.8	40 B	48.0	50 B	68.4	54.8	8.69	66. <b>4</b>	72.8	34.3	36.4	24.7		2007 2007		76.2	
	Ö	10.2	80	10.4	80	9.8	9.6	11 1	10.2	10.6	11.0			. 4	t e o u	) v ) v		- <b>6</b>	0.0	11 7	10.8		4 0	0 U	0.0	8.3	
	臣	2 00	99	0.8	6	8.4	6 8	4	0	4		r.α Σ.Γ			ວ່ຕ ວັດ	່		5			) <b>.</b>	ά			Ņ	80	
	Twater	28.0	0.05	28.7	27.8	0.66	28.2	28.0	100	0.02	28.4		1.02	787 0 80	0.04			0.02	28.5	28.0 0 8.0	100		707		7.87	28.6	
	Tair	27 K	28.5	28.0	27.5	28.5	0.80	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2. 2.	0.04	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 4		20°C			2.07 7.7 FC	2 4 6	0.80	2. 2. 7. 7.			20.0		C 07	28.0	
	SAMPLE																								LWUNV6.2	LWQ/K/8.3	

Table 8. Lake Water Quality survey- Kandy district

Sample points: Kandy : 8 points to cover the full area of lake points shown in the attached map

		ö	3.5	42	4.0	5.8	5 2	4.7	6.8	0 3	6.8 8	6.0	6.0	8,3 2,3	v- 00	- 0 - 1	0.	6.3	19.9	17.6	16.8	<b>4</b> .6	3.8 8	<b>4</b> .0	40	4.6	4, G		
	Elec	Con	87.5	96.7	96.5	130.9	117.7	101.6	138.0	136.1	135.6	133.4	133.5	135.8	1308		141.1	138.7	179.0	186.0	167.8	70.9	67.8	. 70.9	72.3	72.3	72.3		
		ပိ	Ī	Ī	IIZ	Ī	ĪZ	Z	Z	Z	Z	ĪZ	Ē	ĒZ	Π.		Ż	Z	ĪZ	Ĩ	Ē	Ī	ĒZ	Ē	IIZ	ĒZ	Ē		
		чZ	EZ.	IIX	IZ	0.24	ĪŽ	ž	z	ž	0.09	EZ	ΞŻ	ΞŻ	EN	2 :	Ē	Ż	Ē	ĒŽ	ĪŽ	ΞŻ	ĒŻ	ĒŽ	īž	Ē	ΪŻ		
		8	ĪŽ	ΪŇ	ĒZ	ΪN	ΪZ	ΪN	Z	ž	Ż	ĨZ	ΞZ	Z			Ē	Z	IIN	IIN	IIN	IIN	ĪZ	Ī	ĨZ	Z	IIN		
	Total	lron	0.62	0.25	IN	0.53	0.39	0.62	1 15	3.1	1.43	0.87	1.21	2.05	5 5	1.2.1	1.67	1.78	2.1	1.8	1.7	0.73	0.67	0.65	0.65	0.65	0.65		
		As	ÏZ	ĪZ	ΞZ	ĨZ	Z	z	Ī	Ż	Ī	ž	Ī	ž		Z	z	Ĩ	īž	ĨŽ	īž	Ī	īz	īz	IIN	ĪŽ	Ī		
		E.Coli	160	100	100	180	160	400	090	200	720	600	280	200	20000	2300	2300	2000	1.4×10 <sup>5</sup>	1.2×10 <sup>5</sup>	1.0×10 <sup>5</sup>	<100	<100	<100	<100	<100	<100		
	Total	colifarm	280	860	670	320	1100	1600	1960	2200	1850	2400	1700	2400	5	nixes	30×10	32×10 <sup>3</sup>	13×10 <sup>5</sup>	10×10 <sup>5</sup>	9×10 <sup>5</sup>	580	780	480	130	300	230	·	
		¢ ¢	3.32	3.54	4.32	5		0.83	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	100	3 65 2 65	1 09	2 32	120		3.84 42	3.7	3.64	2.59	2.7	2.67	3.81	3.56	3.24	1.88	5	1.94		middle
		Z-1-	11.06	11.59	2.02	6.28	13.10	- 0	C7.1		2 4 7 7 7 7 7 7	1010	7.87	10.1 1		0.42	0.8	0.65	15.85	14.7	13.8	5.74	5.68	80	13,19	12 83	13.56		Grenow Lake-
		so42-	8	44	4	. r-				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ς α α		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5 C	2.1	9.1	8.4	7.8	10.8	9.8	9.2	5.1	5.2	56	99	5	800		Greno
		TDS	48.6	48.5	10.04	2		6.00 00 00			- 00	0.10		) <del>,</del>		70.1	76	58.5	39.5	32.5	80.8	35.3	35.6	34.5	36.4	37.8	36.8	2	-
																					82					•			
		BOD																			38.5								
listrict)	1000000	000																			210.6 3								040
													<b>n</b>				1.0 9				14						ο ο ο ο α	·	
di mora	auwai a	Ţ																			69			5 0 5 4			ν α 1 ο		•
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		Twater	5 7 7		0, r - r	0, <u>7</u>	16.5	17.5	17.5	17,5	17.5	18.5	0.71	16.0	16.5	22.5	20.8	20.5		20.6	2007 000 000 000 000 000 000 000 000 000		0. U 0. U			0,0	7 0 7 0	0.1	Ē
to Motor	Le vval	Tair		0.01		0.0	.16.0	16.5	16.0	19.0	20.0	20.0	20.5	21.0	20.5	19.0	19.5					2 U	10.0	D. C.	0 U		2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	10.0	
T-U- 0 1 of Mater Ouelity (Numera-Elive district)	l adie 9. Lai					LWQ/N/1.3	LWQ/N2.1	LWQ/N2.2	LWQ/N/2.3	LWQ/N/3.1	LWO/N/3.2	LWQ/N3.3	LWO/N/4.1	LWQ/N/4.2	LWQ/N/4.3	LWQ/N/5.1	1 WO/N/5 2	LANDAUS 2										LWUN6.3	-

A-15.2-24

Samples: Nuwara - Eliya

Gregory Lake
 Gregory Lake - near the bridge
 Barrack plains - middle
 Barrack plains
 Barrack plains
 Barrack plains

7. Gregory Lake- middle 8. Gregory lake -middle

There was no significant variation in the Kandy lake samples collected at different locations except for bacterial counts and this is perhaps due to the close proximity to hotels which discharge raw effluent into this waterbody without any treatment.

## 5. Sludge quality survey

Samples were collected from both Kandy and Nuwara-Eliya. However there were problems collecting samples during the first survey for this analysis as planned in the schedule of work since septic pits are either permanently sealed or the sludge form septic tanks is regularly cleaned by the municipalities. We were however able to complete the leftover sludge samples from the first survey during this period.

The samples points and the key to samples is given below:

Kandy	SQ/K/1 SQ/K/2 SQ/K/3	Septic tank sludge-office complex (University) Hospital sludge Sludge from septic tank- middle income house
Nuwara Eliya	SQ/N/1 SQ/N/2	Sludge from septic tank- middle income house Public toilet

The analytical results are given in table 10. One notable feature is the presence of Zn as a heavy metal in all these samples. Perhaps this originates from the galvanised piping used in plumbing etc. The high phosphate content in domestic sewege may be a reflection of the increased use of phosphate based detergents.

Zn mg/kg 0.19 0.67 0.01 0.22 0.12
S Z Z Z Z Z
o e e e e e
¥ z z z z z
T-P mg/kg 6.00 13.00 7.5 8.5
7-N 8.3 8.3 8.7 8.7 8.7
tt VSSmg/kg SS mg/g 20.2 369.2 30.7 385.1 8.6 174.3 10.5 320.2 14.5 410.4
Water conter mg/9 462.1 172.2 547.3 547.7 476.2
Tsludge 28.3 28.3 28.3 28.3 20.3 20
Tair 28.7 28.6 29.1 21 21 20.8
SAMPLE SQ/K/1 SQ/K/2 SQ/K/3 SQ/N/1 SQ/N/2

Table 10.Sludge Quality survey (Kandy and Nuwara-Eliya districts)

Sludge quality survey

Sample points: Kandy

Senate
 Hospital
 Meewatura

Nuwara Eliya 1. Sludge from septic tank- middle income house 2. Public toilet

 $\begin{array}{c} \mathbf{b} \\ \mathbf{c} \\ \mathbf$  $\mathbb{R}$ Heptachlorepoxide Pirimiphos Methyl - HCH(Lindane) Parathion Methyl **Methamidaphos** Monocrotophos Chlorothaloni Chlorpyrifos Dimethoate <sup>=</sup>enitrothion Quinalphos Carbofuran Permethrin <sup>2</sup>rofenofos Darameter Endosulfar Darathion p'p, DDE p'p, DDD **Malathion** 000 Metalaxyl Diazinon β-HCH Pod <u>po</u> Fenthion Propanil a - HCH 8-HCH Dieldrin Vachlor Atrazine Captan Aldrin 0. D d d

Annexure 1- Pesticide analysis on water samples

	l imit	of De	term	etermination	no/)
raramere		2			)
a - HCH	2.0				
8 - HCH	4.0				
y - HCH(Lindane)	0.2				
8-HCH	0.2				
Aldrin	0.5				
Dieldrin	0.5				
Heptachlorepoxide	0.5				
Endosulfan	0.5				
p'p, DDE	0.5	·		·	
o'p, DDT	0.5			·	
p'p, DDT	0.5				
o'p, DDD	0.5				
p'p, DDD	0.5			•	
Chlorpyrifos	*				
Dimethoate	ŝ				
Diazinon	2				
Fenthion	2			ŗ	
Fenitrothion	2				
Malathion	2				
Monocrotophos	۰n	. ,		•	
Methamidaphos	ĥ				
Parathion	2				
Parathion Methyl	2			•	
<b>Pinmiphos Methyl</b>	N,	: .			
Profenotos	<b>N</b>				
Quinalphos	2				
Carbofuran	ĥ				
Chlorothalonil	'n				
Captan	<b>***</b>				:
Metalaxyl	Ņ		•		
Alachior	2				
Propanil	2				
Atrazine	n.	•••••			
Permethrin	2				

sp1 Wa/K/1.1	SP2 WQ/K/2.1	SP3 WQ/N/1.1	4	SP5 WQ/N/3.1	SP6 WQ/N/4.1	SP7 WQ/N/5.1		SP9 WQ/N/7.1	SP10 WQ/N/8.1	-	SP12 WQ/N/12	3	SP14 WQ/N/14	SP15 WQ/N/11.2	SP16 WQ/N/10.2	SP17 WQ/N/15.2	SP18 WQ/N/17.2	SP19 WQ/N/16.2	P20 Golf grou	SP21 galway - New	
S	S	S	တ	S	S	S	S	S	S	S	S	Ø	S	Ø	<sub>0</sub>	0	()	0	0)	0)	