JAPAN INTERNATIONAL COOPERATION AGENCY
MINISTRY OF HOUSING AND URBAN DEVELOPMENT
DEMOCRATIC SOCIALIST REPUBLIC OF SRI LANKA

THE STUDY
ON
GREATER KANDY AND NUWARA ELIYA
WATER SUPPLY
AND
ENVIRONMENTAL IMPROVEMENT PLAN
IN
THE DEMOCRATIC SOCIALIST REPUBLIC
OF
SRI LANKA

VOLUME V

NUWARA ELIYA (SUPPORTING REPORT AND DATA)

FEBRUARY 1999



NIPPON JOGESUIDO SEKKEI CO., LTD.

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VOLUME V (SUPPORTING REPORT AND DATA, NUWARA ELIYA)

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Chapter 5

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APPENDIX 5.1 Alternative Water Sources in Nuwara Eliya

1. Alternative Water Sources

Three sources have been identified that could potentially be developed to provide additional water for Nuwara Eliya.

- · A stream near Jayalanka
- · The existing Bambarakele source
- · Groundwater

Although only very limited of flow measurement data are available for the surface water sources, sufficient information on rainfall, rainfall-runoff coefficients and evaporation rates are available for nearby catchment areas to allow an approximate estimate of yield from the proposed sources to be made. It is important to note that such an approximation is not as reliable as an analysis based on actual stream flow data and is not considered to be an adequate basis for design and construction of an impoundment facility.

Development of each of the surface water sources will require construction of impoundment, treatment, pumping and transmission facilities. Figure 1 illustrates the general arrangement of these facilities for the Jayalanka and Bambarakele sources. The locations of the proposed Bambarakele and Jayalanka dam sites are shown in Figure 2 and Figure 3, respectively. The Bambarakele and Jayalanka catchment areas are delineated in Figure 4 and Figure 5, respectively.

Three potential sites for construction of wells have been identified in the study area. The locations of these sites and the alignment of the transmission mains from the wells to service reservoirs in the Nuwara Eliya distribution system are shown in Figure 1.

A summary of the characteristics of the two potential surface water impoundments is presented in Table 1.

Table 1 Characteristics of Potential Surface Water Impoundments in Nuwara Eliya

Item	Jayalanka	Bambarakele
Surface Area (ha)	20.0	6.2
Catchment Area (ha)	568	220
Storage volume (m³)	2,100,000	550,000
Usable Storage volume (m³)	1,575,000	412,500
Dam Length (m)	270	220
Water Elevation (msl)		·
Low water	1,920	1,940
High Water	1,940	1,960
Approximate Yield (m³/d)	5,950	4,200

As can be seen from inspection of Table 2, the surface water source with the largest potential yield is at Jayalanka. A serious problem with this source is the presence of extensive vegetable plots in the catchment area where heavy use of fertilizers and agrochemicals to control pests pose a pollution threat. A considerable portion of the catchment area is used for growing tea, and it is estimated that up to 2,000 tea estate workers are housed there.

Acquisition of land used for vegetable cultivation is expected to cost about Rs.5,000,000 per hectare. Land costs for the area to be flooded by the impoundment, the dam site itself and a reasonable safety zone around the reservoir could cost in the neighborhood of Rs.150,000,000. A suitable level of protection against pollution would require as a minimum provision of adequate sanitation facilities for the resident catchment area population. Depending upon the extent of pollution by agrochemical compounds, it may be necessary to provide some form of advanced treatment or purchase and retire additional agricultural land. Some of the resident population may have to be resettled, with the attendant financial and social costs that are associated with any resettlement activity.

Although the yield from the Bambarakele source is estimated at 4,200 m³/d (see discussion above), a portion of this yield is already being used and cannot be counted as a new source. The lowest flow measurement available for Bambarakele, from an admittedly very limited amount of flow data, is 1,650 m³/d, which occurred in 1997. It is unlikely that this figure represents the low flow for a twenty year period of record that is commonly accepted as being required to establish a safe yield for a municipal water supply system. In the ten years of rainfall record currently available for the area, total rainfall during the dry months were up to 17 percent lower than the 1997 figure on two occasions. This suggests that the safe yield of the Bambarakele source without an impoundment is less than 1,650 m³/d, possibly as low as 1,400 m³/d. Given the above, it would appear that augmentation of the Bambarakele source

by construction of an impoundment reservoir could increase the safe yield available to the community by about 2,800 m³/d.

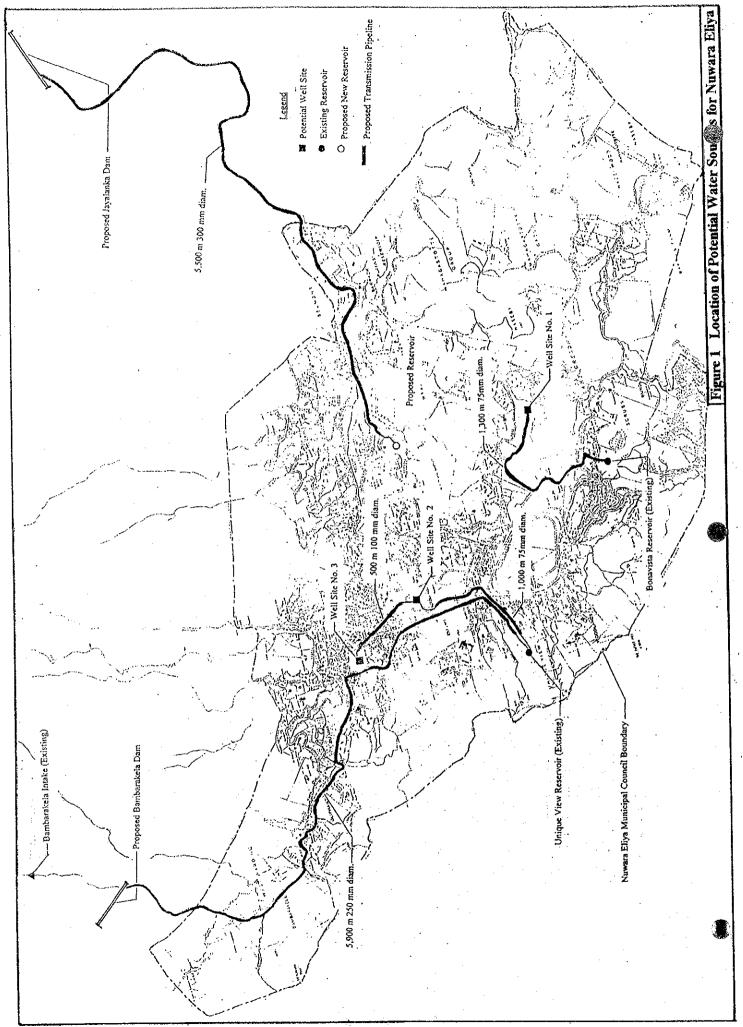
The Bambarakele source has some bacterial contamination due to human activities in the catchment area. Plans are under way to deal with this problem by installing pressure filters on the delivery main. Although filtration should be adequate for a stream source, additional treatment will be required after an impoundment reservoir has been built. Open storage reservoirs tend to accumulate nutrients from the catchment area and are subject to algae growth problems that will cause excessive clogging of filters. A conventional treatment facility, with sedimentation, coagulation and filtration, would be required for this source.

Hydrogeologic data in the Nuwara Eliya area is somewhat limited at the present time and it is difficult to accurately estimate the total yield that can be expected from groundwater. It is, however, the consensus among hydrogeologists working in the area that extraction of enough water to meet all of Nuwara Eliya's future needs (approximately 6,450 m³/d) is unlikely. Electrical resistivity surveys and test well drilling are being carried out under the current investigation that should allow a better estimate of local groundwater potential to be made.

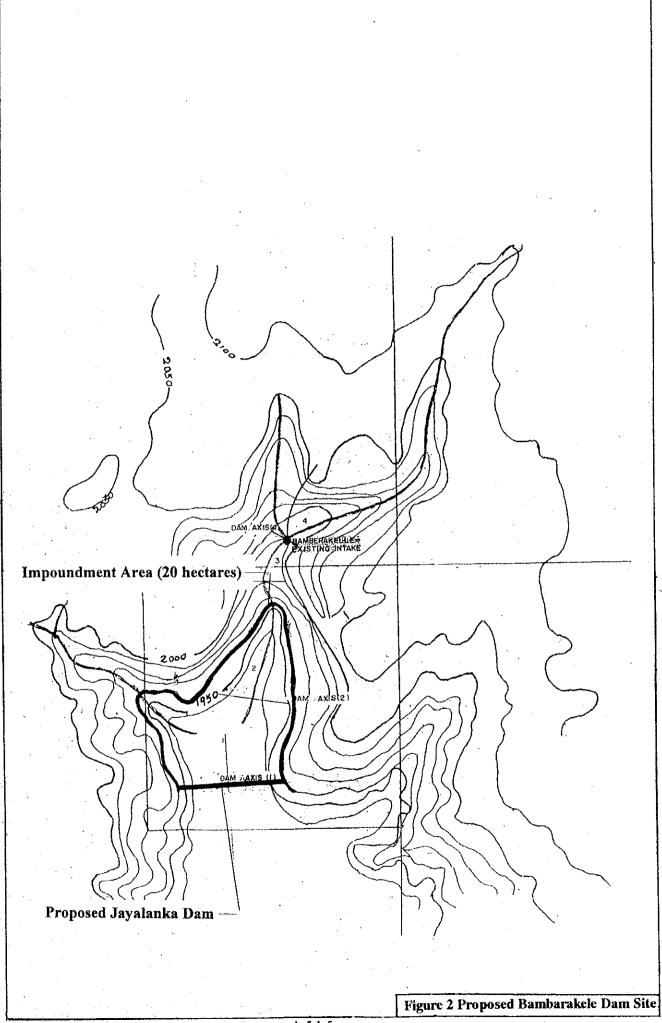
Production from existing wells in the area varies from less than 100 m³/d to 600 m³/d. For the purposes of this investigation, individual well production has been assumed to be 300 m³/d. For the purposes of comparing groundwater to alternative sources of water for Nuwara Eliya, it has been assumed that 900 m³/d can be obtained from this source.

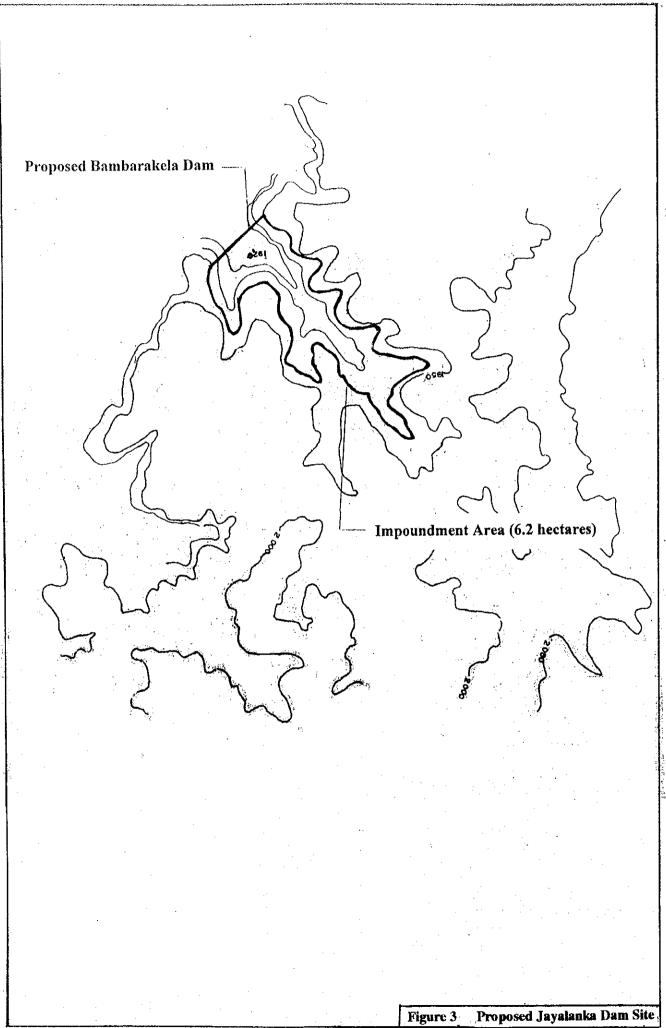
2. Alternative Water Source Costs

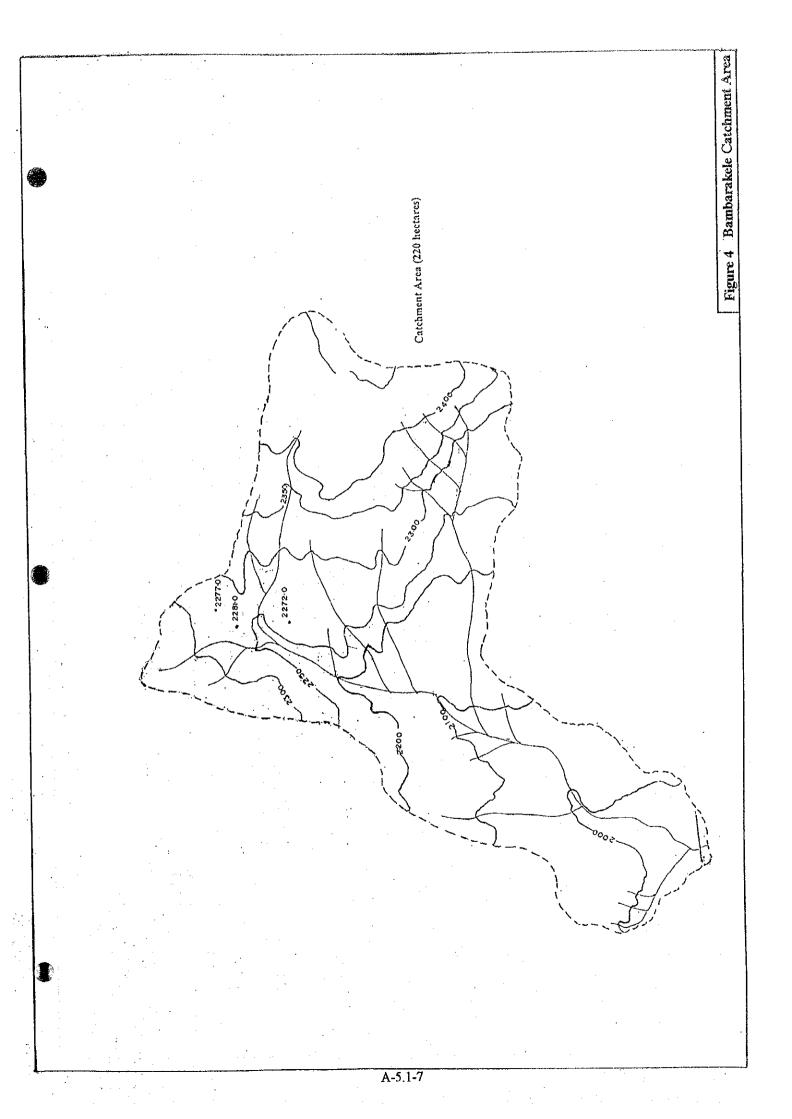
Estimated costs associated with development of the three alternative water sources are presented in Table 2. Pipelines were amortized over 30 years, treatment facilities over 20 years, and pump stations and wells over 15 years, at 12 percent interest. Pipeline O & M costs were estimated at one percent of capital cost and pump station and well O & M were estimated at 5 percent of capital cost. Treatment plant O & M costs were derived from a 1997 Degremont report on a facility of similar capacity. Power costs were calculated based on a power rate of Rs. 5.0/kWh. Unit costs were based on the service population in 2015.



A-5.1-4







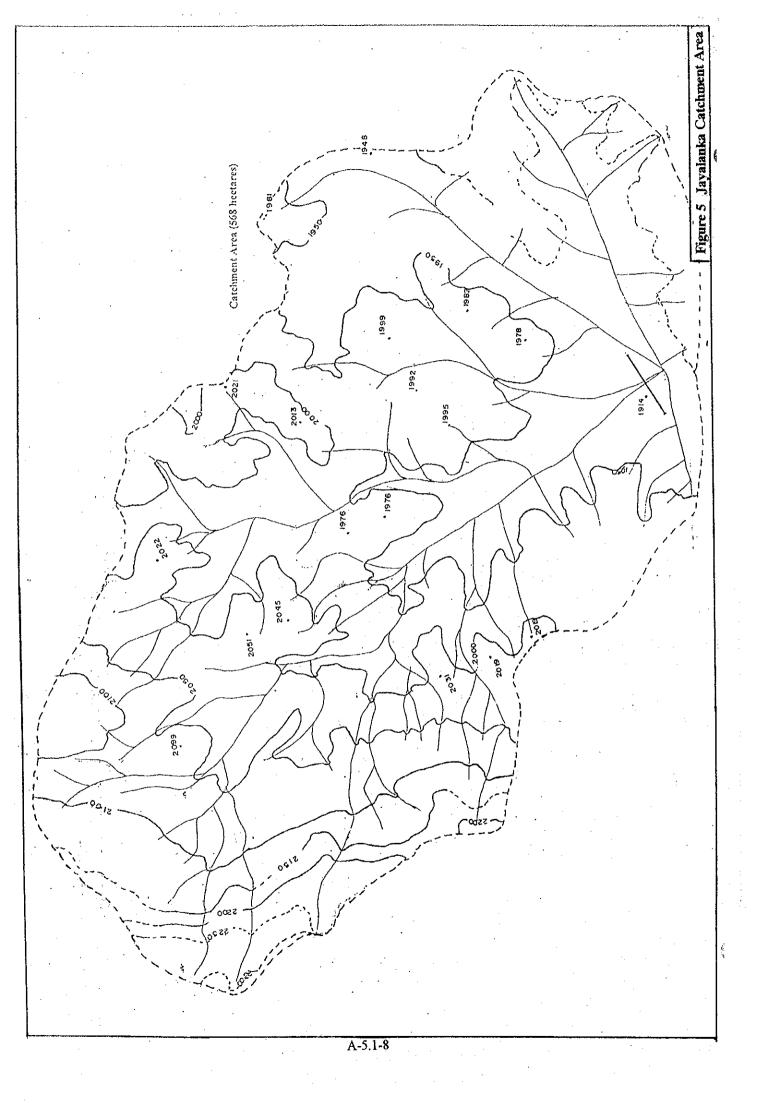


Table 2 Estimated Costs for Alternative Nuwara Eliya Water Sources

Item	Jayalanka	Bambarakele	Groundwater
Capital Cost (Rs.)			
Impoundment reservoir			
145,000 m ³		270,000,000	-
178,000 m ³	332,000,000	•	-
Subtotal-Impoundment	332,000,000	270,000,000	e .
Treatment Plant			
4,250 m³/d	-	106,300,000	
5,950 m³/d	148,800,000	-	
Subtotal-Treatment Plant	148,800,000	106,300,000	-
Pumping facilities	2,100,000	6,000,000	7,000,000
Transmission Main			
5,900 m 250mm diam.	_	45,200,000	
5,500 m 300mm diam.	55,200,000	-	-
2,300 m 75mm diam.	H	-	4,400,000
500 m 100mm diam.		-	1,100,000
Subtotal-Transmission Mains	55,200,000	45,200,000	5,500,000
Wells			16,000,000
Land Acquisition	150,000,000	46,000,000	2,100,000
Resettlement	20,000,000	5,000,000	\$4
Totals	708,100,000	478,500,000	30,600,000
Amountined Control Cont (Do /vm)			
Amortized Capital Cost (Rs./yr) Impoundment reservoir (50 year life)	39,840,000	32,400,000	
	18,451,200	13,181,200	
Treatment Plant (30 year life)	281,400	804,000	938,000
Pump Facilities (20 year life)	6,844,800	5,604,800	682,000
Transmission Main (30 year life)	0,044,000	3,004,600	2,144,000
Well (20 year life) Land Acquisition (50 years)	18,000,000	5,520,000	252,000
	2,400,000	600,000	232,000
Resettlement (50 years)	85,817,400	58,110,000	4,016,000
Total Amortized Cost (Rs./yr) O&M cost	03,017,400	30,110,000	4,010,000
Power	424,000	9,821,000	1,200,000
Maintenance	10,547,000	9,152,000	630,000
Total O&M Cost (Rs./yr)	10,971,000	18,973,000	1,830,000
Average Annual Cost (Rs./yr)	96,788,400	77,083,000	5,846,000
Available Yield (m³/day)	5,950	2,800	900
Unit Cost (Rs./m³)	44.57	75.42	17.80

3. Water Source Development Strategy

A comparison of estimated unit costs for the alternative water sources discussed above is presented in Table 2. As indicated in Table 2, the least expensive new water source is groundwater, with both of the surface water sources costing four to five times as much as groundwater. It is interesting to note that the average cost of water to Nuwara Eliya water utility

customers in 1997 was Rs 2.15 per m³. When compared to the cost of any of the potential new sources, it is obvious that water rates can be expected to escalate dramatically as new sources are developed.

The unit costs shown in Table 2 include only the cost of new sources and are for illustrative purposes only. At this stage of the Study, only preliminary estimates have been developed for the cost shown in Table 2. Although these costs will be substantially modified when the inexpensive existing water sources and the cost of modifications to the distribution system that will be required to accommodate the new sources are taken into account, they are still expected to be far higher than present day billing rates. Should current plans to implement a sewerage system be carried out, the perceived increase in costs to the average family will be higher still. The bulk of the existing sources are surface sources that can be fed by gravity to the distribution system. The low operating costs of this type of source, together with the fact that that most of the capital costs associated with these systems were retired long ago, has resulted in the exceptionally low costs enjoyed by the existing water utility customers

NRW is exceptionally high in the Nuwara Eliya system at 56 percent of production. Given the high cost of new sources relative to existing sources, it is obvious that any reduction in NRW that can be effected will result in a substantial lowering of future water rates. A high priority should therefore be given to NRW reduction and made an integral part of any future water supply augmentation plans.

Given the above, the recommended strategy for meeting future Nuwara Eliya water supply needs is to pursue a two stage development procedure, as illustrated in Figure 6. The first stage would concentrate on development of the least expensive alternative for augmenting supplies, namely groundwater. Stage one would also include investigations to establish the maximum potential yield from groundwater, a high priority NRW reduction program and a hydrological data collection program (stream flow, rainfall, topographic surveys and geotechnical information) aimed at providing sufficient data for a reliable technical evaluation of the potential surface sources. Stage two would involve evaluation of alternative water sources based on information gained during stage one, and implementation of the most cost effective mix of sources.

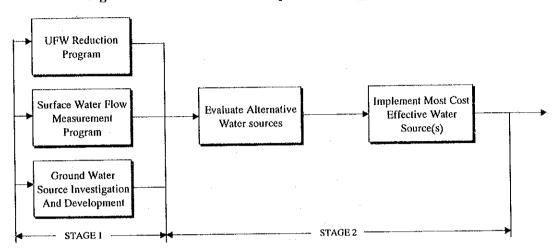


Figure 6 Water Source Development Strategy for Nuwara Eliya

Appendix 5.2 Specification for Potable Water, SLS 614 (1983)

Part 1 - Physical and Chemical Requirements

Part 1 - Physical and Chemical Require Characteristics		Max. Permissible Leve
PH	7.0-8.5 units	6.5-9.0 units
Colour	5 units	30 units
Odour	Unobjectionable	Unobjectionable
Taste	"	66
Turbidity	2-JTU	8-JTU
Elect. Conductivity	750 μS/cm	3,500 μS/cm
Chloride (Cl)	200 mg/l	1,200 mg/l
Chlorine - Free Residual (Cl)	-	0.2 "
Alkalinity (as CaCO ₃)	200 mg/l	400 "
Ammonia-Free	-	0.06 "
Ammonia-Albuminoid		0.15 "
Nitrate (as N)		10
Nitrite (as N)		0.01 "
Fluoride (as F)	0.6 mg/l	1.5 "
Phosphates - Total (PO)	_	2.0 "
Total Solids	500 mg/l	2,000 "
Hardness Total (as CaCO ₃)	250 "	600 "
Iron-Total (as Fe)	0.3 "	1.0 "
Sulphate	200 "	400 "
Calcium	100 "	240 "
Magnesium	30 to 150 *	150 "
Соррст	0.05 mg/l	1.5 "
Manganese	0.05 "	0.5 "
Zinc	5.0 "	15.0 "
Aluminium	-	0.2 "
Arsenic	-	0.05 "
Cadmium	-	0.005 "
Cyanide	-	0.05 "
Lead	-	0.05 "
Mercury	-	0.001 "
Selenium	-	0.01 "
Chromium	-	0.05 "
Anionic Detergents (as MBAS-LAS)	0.2 "	1.0 "
Phenolic Compounds (as Phenolic OH)	0.001 "	0.002 "
Oil & Grease	-	1.0 "
Pesticide Residue	(Refer to WHO &	FAO requirements)
Chemical Oxygen Demand (COD)		10 mg/l

^{*} Depending on Sulphate content, i.e. for 205 mg/l Sulphate, max. Mg is 30 mg/l; for less sulphate, more Mg is allowed.

Appendix 5.2 Specification for Potable Water, SLS 614 (1983)

Part 2 - Bacteriological Requirements

Requirements

- 1. Pipe born water supplies:
- Throughout any year, 95 percent of the samples shall not contain any coliform organisms in 100 ml.
- None of the samples examined shall contain more than 10 coliform organisms per 100 mt
- Coliform organisms shall not detectable in 100 ml of any two consecutive samples.
- None of the samples examined shall contain E. Coli. in 100 mg/l I (Fecal coliform)
- 2. Individual and small community supplies
- None of the samples examined shall contain more than 20 coliform organisms per 100 mg/l on repeated examination.
- No sample shall contain E. Coliform in 100 mg/l (Fecal coliform)

Note: Individual or small community supplies include wells, bores and springs

Appendix5.3 Recommended Peak Factor

1.1 Establishment of Load Factor to Estimate Daily Maximum Water Demand

Capacity of transmission line and distribution reservoir shall be determined based on the daily maximum water demand. In this study, the daily maximum water demand was estimated due to absence of past performance record/data.

In setting up of load factor (= daily average water demand/daily maximum water demand), actual performance data by size of water supply system in Japan was referred to. However, if UFW occupies considerable part of supply amount, the Japanese data may not be applied directly, while the effective supply amount basis (excluding UFW) of Japanese data may be applied similarly this study, since tendency of water consumption is deemed to be mostly similar in every country.

In this section, load factor was studied based on the following formula in application of some modification taking into account difference of UFW ratio.

Supply amount may be categorized as shown in the following figure and various coefficients are given by following formula. In the figure, most of non effective supply amount is deemed to be leakage and is assumed to be equal in both daily average supply amount and daily maximum supply amount.

Load factor R1 = A/B (Load factor is generally defined by this formula)	(1)
Effective ratio R2 = C/A	(2)
Non effective ratio $R3 = D/A = (1 - C/A) \dots \dots$	(3)
Daily average supply amount $A = C + D = C + A*R3 \dots \dots \dots \dots$	(4)
Daily maximum supply amount $B = E + F = E + A*R3 \dots \dots \dots \dots \dots \dots \dots$	(5)
Daily average effective supply amount $C = A - D = A - A*R3 = (1 - R3)*A$	(6)

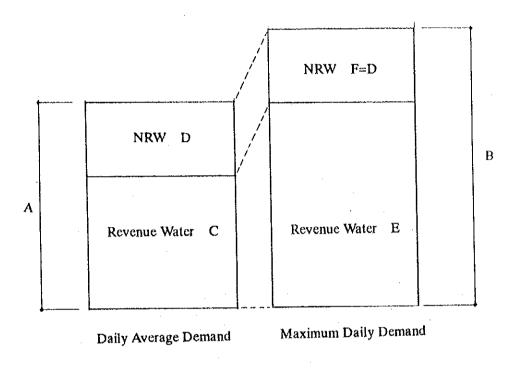


Figure 5.3.1 Supply Amount of RevenueWater and Non Revenue Water

Based on the above, modified load factor (R) can be expressed with R1 and R3 as follows:

Modified load factor
$$R = C/(C + A*R3/R1 - A*R2 = R1*(1 - R3)/(1 - R1*R3)$$
 (8)

Load factor (R1) can be expressed with R and R3 as follows:

Load factor R1 = A/B =
$$(C + A*R3)/(C/R + A*R3) = R/(1-(1-R)*R3) \dots (9)$$

Now, load factors R1 and effective ratio R1 (or non effective ratio) are known figures by size of water supply system based on the Water Supply Statistics of Japan, the modified load factor (R) can be estimated as follows.

Table 5.3.1 Past Performance Data of Load Factor and Effective Ratio in Japan

Served Population	Load Factor	Effective Ratio
(person)	(%)	(%)
500,000~1,000,000	82.5	94.0
50,000~100,000	79.6	90.3
30,000~50,000	78.1	87.5

Note: Water Supply Statistics of Japan, 1993

Load factor in Nuwara Eliya is estimated referring to the above table as follows:

Modified load factor
$$R = (0.796 \times (1 - 0.097)/(1 - 0.796 \times 0.097) = 0.779$$

Load factor $R1 = 0.779/(1 - (1 - 0.779) \times 0.25) = 0.825$

Coefficient to estimate the daily maximum supply amount is given as a reciprocal number of the load factor:

$$1/R1 = 1.21$$
 say 1.2

When load factor of Greater Kandy is estimated in the same manner:

Modified load factor
$$R = (0.825 \times (1 - 0.060)/(1 - 0.825 \times 0.060) = 0.816$$

Load factor $R1 = 0.816/(1 - (1 - 0.816) \times 0.25) = 0.855$

Coefficient of the daily maximum supply amount is:

$$1/R1 = 1.17$$
 say 1.2

1.2 Peak Factor

Capacity of distribution lines is to be determined based on the hourly maximum water demand or peak factor. However, the hourly maximum water demand or peak factor shall be estimated due to absence of past performance record/data in Nuwara Eliya as described in the previous section, Load Factor.

Peak factor (= hourly maximum supply amount/daily maximum supply amount) is likewise determined referring to the Japanese past performance data. It shall be noted that hourly fluctuation coefficient in Japan and peak factor in the study area are given different definitions, as follows:

Hourly fluctuation coefficient in Japan:

K = (hourly maximum supply amount)/(daily maximum supply amount)

Peak factor in the study area:

Peak factor = (hourly maximum supply amount)/(daily average supply amount)

Based on the above-mentioned difference of definition, peak factor in the study area shall be determined in application of load factor of daily maximum supply amount to the hourly fluctuation coefficient as follows:

Peak factor in the study area

= (Hourly fluctuation coefficient in Japan; K) x (Load factor of daily maximum supply amount)

The hourly fluctuation coefficient in Japan is shown in the following figure. Since Nuwara Eliya has daily maximum supply amount of about 10,000 cu.m/day, the hourly fluctuation coefficient (K) in Japan is considered to be 1.78, while load factor of daily maximum supply amount is estimated at 1.2. Thus, peak factor in the study area is estimated as follows:

Peak factor in study area = $1.78 \times 1.2 = 2.1$ say 2.0

In ADB D/R/D page 7 (Feb. 1998), peak factor is defined at 2.0.

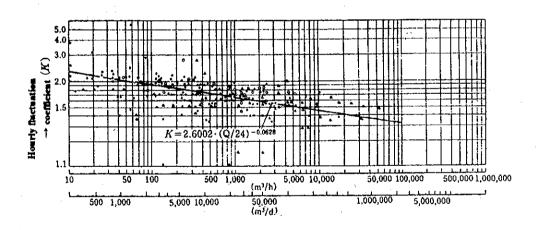


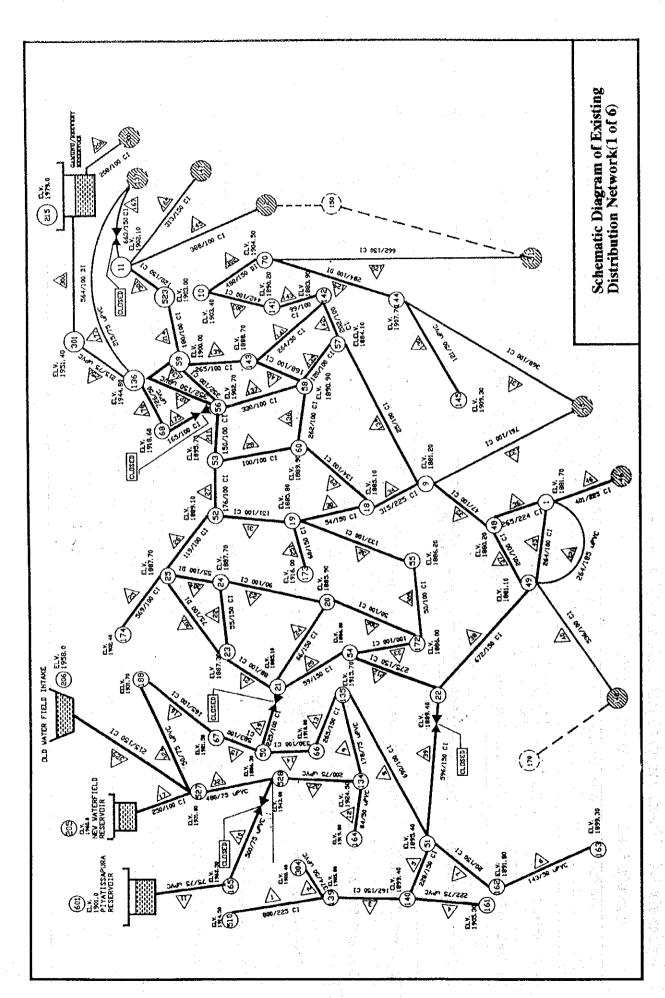
Figure 5.3.2 Relationship between Distributed Volume and Hourly Fluctuation Coefficient

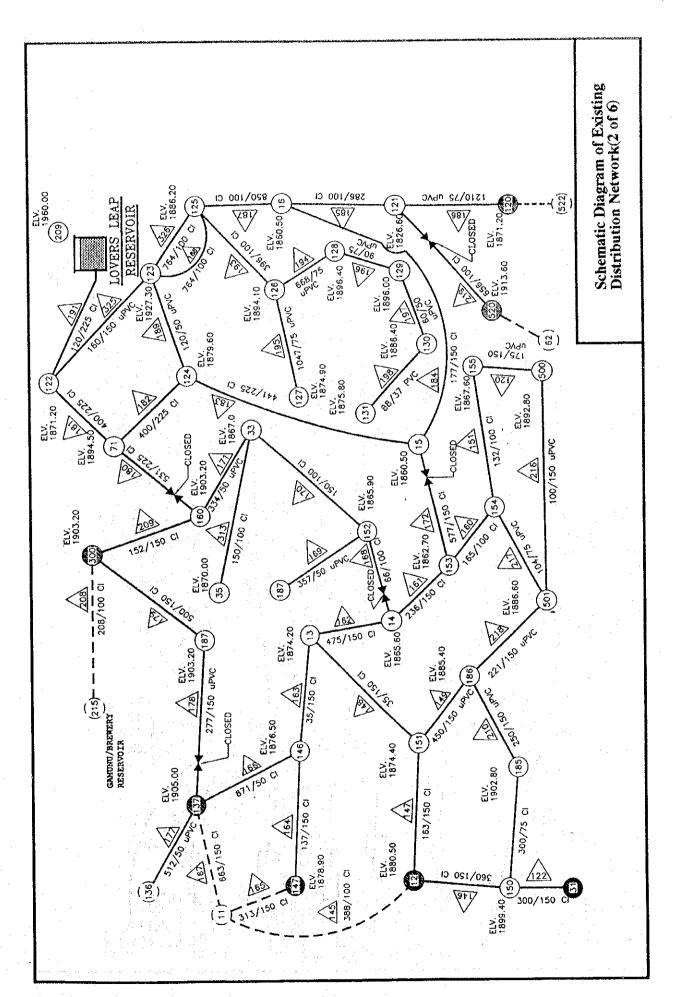
Appendix 5.4 Water Supply System Hydraulic Analysis

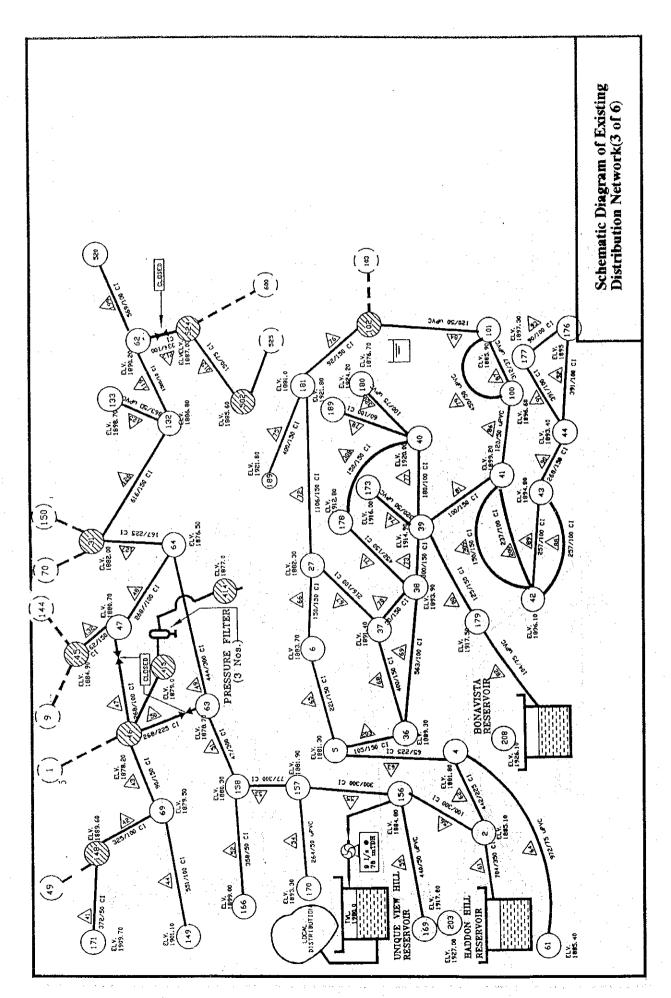
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Appendix 5.4.2	Node Demand List for Network Analysis (Year 2015)
Appendix 5.4.3	Node Demand List for Network Analysis (Year 2005)
Appendix 5.4.4	Magnification of Node Demand for Network Analysis
Appendix 5.4.5	Calculation of Node Demand for Vijithapura and Unique View Hill Reservoir
Appendix 5.4.6	Calculation of Node Demand for High Area 1 Reservoir

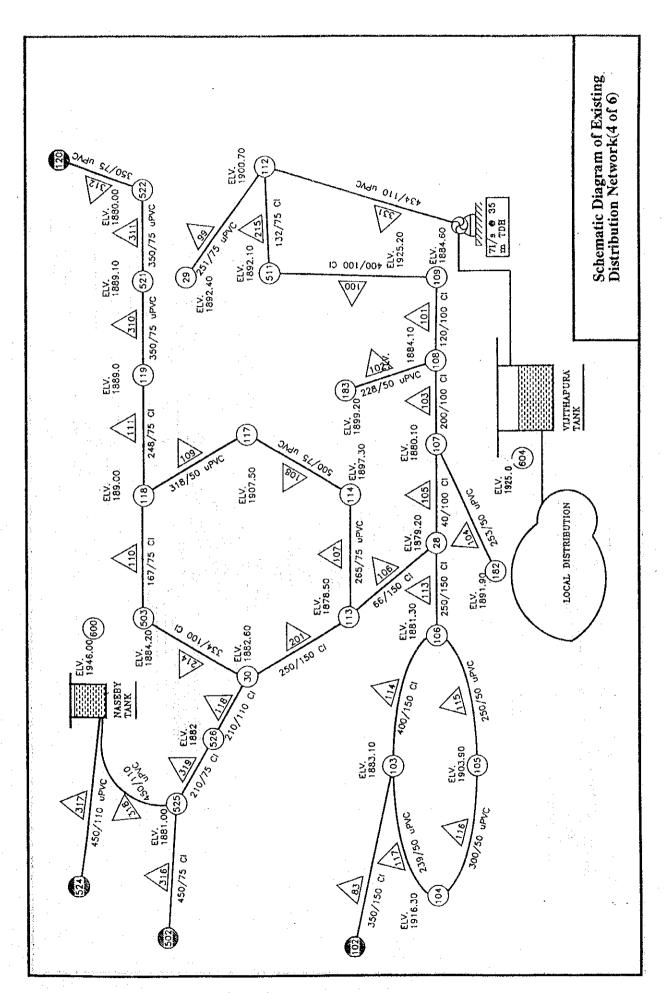
Appendix 5.4 Water Supply System Hydraulic Analysis
Appendix 5.4.1 NetWork Analysis

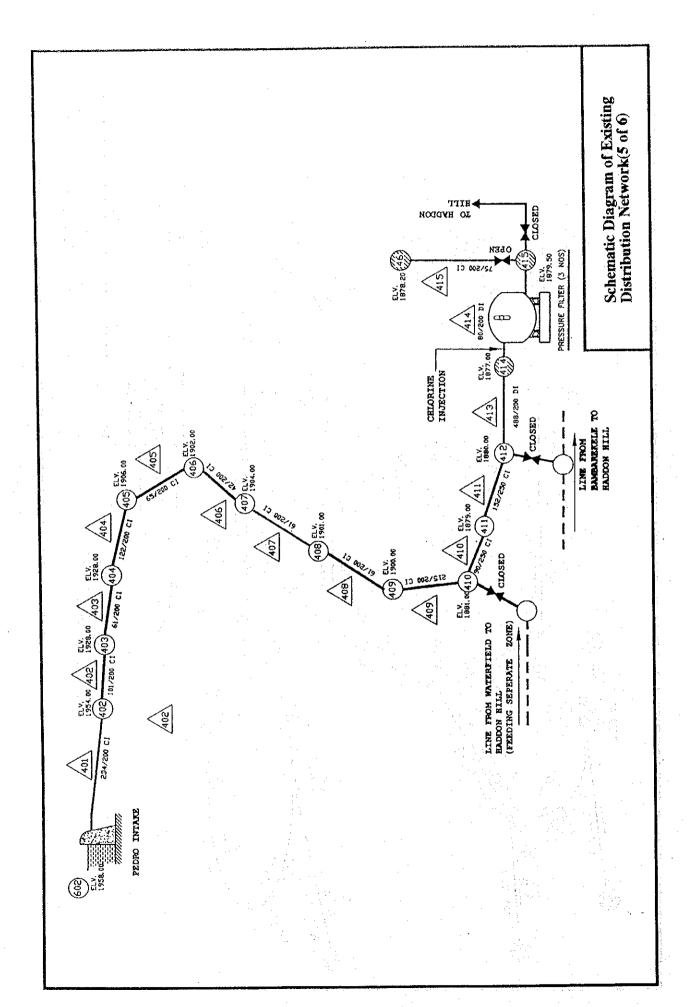
File Name	Main	Season	Purpose	NetWork	Augmentation of				Condition of Keservoir	reservoir
				Type	NetWork	Year	Type	Magnifcation		
NuwaExistO1	Dist	A 11	Culculatin for Cefficient of Leakage	Existing	None	1,995	Daily Mean	0.739	All Reservoir is Free Discharge	
NuwaExistYear2015	Dist	All		Existing	None	2,015	Hourly Max	1.622	All Reservoir is Free Discharge	
Nuwara201Year1995(2)	Dist	Dry	Effectiveness of Leakage Reduction for Proposed NetWork	Proposed	Augmentation For Year 2015	1,995	Daily Mean	0.739	Node of Demand No.205,206,215,209	The Others are Free Discharge
Nuwara011Year2015(2)	Dist	Dry	Pressure	Proposed	Augmentation For Year 2015	2,015	Hourly Max	1.622	Node of Demand No.205,206,215,209	The Others are Free Discharge
Nuwara012Year2015Mean(2)	Dist	Dry	Leakage	Proposed	Augmentation For Year 2015	2,015	Daily Mean	0.811	Node of Demand No.205,206,215,209	The Others are Free Discharge
Nuwara012Year1995Mean(3)	Dist	Rainy	Effectiveness of Leakage Reduction for Proposed NetWork	Proposed	Augmentation For Year 2015	1,995	Daily Mean	0.739	All Reservoir is Free Discharge	Excluding Pedro
G Nuwara011Year2015(3)	Dist	Rainy	Pressure	Proposed	Augmentation For Year 2015	2,015	Hourly Max	1.622	All Reservoir is Free Discharge	Excluding Pedro
H Nuwara011Year2015(4)	Dist	Rainy	Leakage	Proposed	Augmentation For Year 2015	2,015	Daily Mean	0.811	All Reservoir is Free Discharge	Excluding Pedro
Nuwara103Year2005FSDry	Dist	Dry	Pressure	Proposed	Augmentation For Year 2005	2,005	Hourly Max	1.547	Node of Demand No.205,206,215,209	The Others are Free Discharge
7 Ntm01	Trans	Rainy	Pressure	Proposed	Augmentation For Year 2015	2,015	Daily Max	1.000	All Reservoir is Free Discharge	
K Ntm02	Trans		Rainy Pressure	Proposed	Augmentation For Year 2005	2,005	Daily Max	1.000	All Reservoir is Free Discharge	

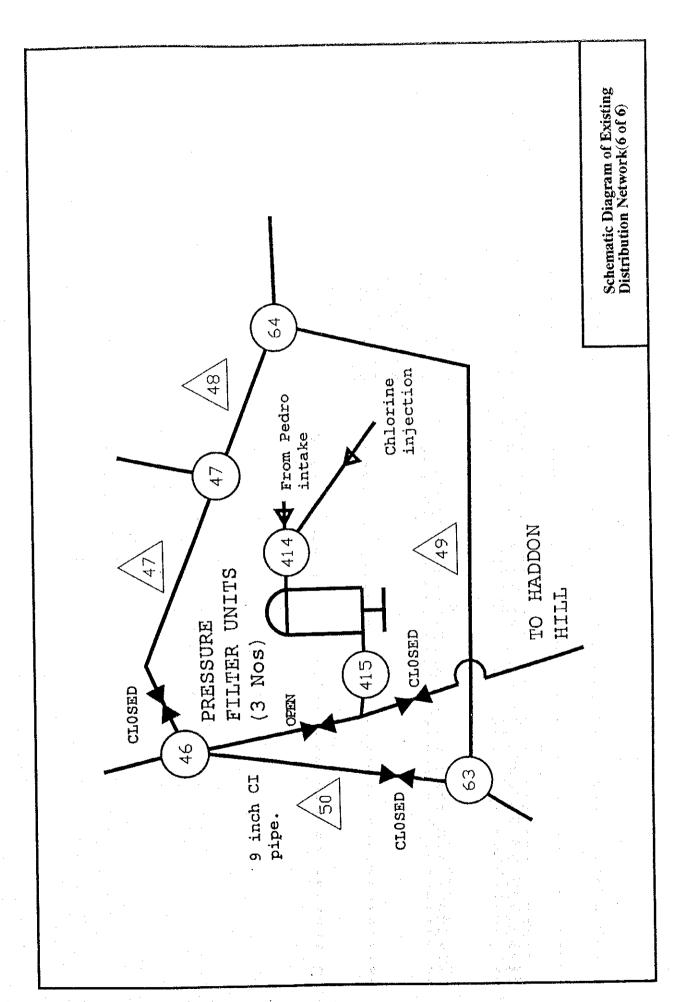












Net	Work	Analysi	S	Distribution Main
File Name Season Network Type	All	raExist01 ting		A
Demand		1995		
Reserver		lean r Level Fix harge Fix	í	All None
Magnificatio	on of D	emand	0.739	
Reservoir Da Node	ata	HWL	LWL	Reservoir
		(MSL)	(MSL)	
203		1,927.0	1,927.0	Haddon Hill
205		1,960.0		New Water Field
206		1,958.0	1,958.0	Old Water Field
208		1,930.0	1,930.0	Bonavista
209		1,960.0	1,960.0	Lovers Leap
215		1,979.0	1,979.0	Gamunu/Brewery
600		1,946.0	1,946.0	
601	1	1,991.0 1,958.0	1,991.0 1,958.0	Piyatissapura
602	1	1,990.0	1,000.0	Pedro Intake
Node Data				
Node Data	Grot	and Elev	Demand	•
node		(MSF)	(cu∎/d)	
1	1	1,881.7	122.0	0 0
ż	î	1,885.1	70.0	0 0
4	î	1,881.8	76.0	0 0
5	1	1.881.3	40.0	0 0
6	1	1.883.7	76.0	0 0
9	i	1,881.2	133.0	0 0
10	1	1,903.4	25.0	0 0
11	1	1,902.1	86.0	0 0
12	i	1,880.5	66.0	0 0
13	1	1,874.2	51.0	0 0:
14	1 .	1,865.6	66.0	0 0,
15	1 .	1,860.5	61.0	0 0
16	. 1	1,860.5	85.0	0 0
18		1,885.1	107.0	0 0
19	1	1,885.8	85.0	0 0
22		1,889.4	79.0	0 0
23	1	1,887.3	82.0	0 0
24	1	1,887.7	117.0	0 0
25	1	1,887.0	51.0	0 0
27	1	1,882.3	75.0	0 0
28 29	1 1	1,879.2 1,892.4	26.0 13.0	0 0
30	1	1,882.6	80.0	0 0
31	ì	1,882.0	93.0	0 0
36	ì	1,889.3	51.0	0 0
37	1	1,891.4	47.0	0 0
38	1	1,893.9	42.0	0 0
39	i	1,914.9	50.0	0 0
41	1	1,899.2	44.0	0 0
42	1	1,896.1	38.0	
43	1	1,894.8	40.0	
44	1	1,893.4	54.0	0 0
45	1	1,884.9	67.0	
46	1	1,878.2	127.0	0 0
47	1	1,880.7	36.0	
48	1	1,880.2	101.0	
49	1	1,881.1	160.0	
50	1	1,886.3	144.0	
51 52	1	1,895.4	47.0	
52 66	1	1,889.1	97.0	
55 56	i	1,886.2	89.0	0 0
56 57	1	1,902.7	49.0	
57 58	1	1,884.1 1,890.9	93.0 119.0	
60	1	1,889.9	100.0	
• • • • • • • • • • • • • • • • • • • •	•	.,	.0010	

61	1	1,885.4	50.0	0	0
			76.0	Ŏ	Ô
62	1	1,890.2			
63	i	1,878.7	38.0	0	0
64	i	1,876.5	44.0	0	0
66	1	1,910.0	40.0	0	0
67	1	1,921.5	38.0	Ô	0
		1,361.0			ŏ
68	1	1,918.6	42.0	0	
69	i	1,879.5	50.0	0	0
70	1	1,904.5	132.0	0	0
71	1	1,894.5	87.0	0	0
				ő	Ö
100	1	1,896.6	33.0		
101	i	1,885.9	25.0	0	0
102	1	1,876.7	37.0	0	0
103	1	1,883.1	50.0	0	0
104	i	1,916.3	19.0	0	0
			17.0	Õ	Ö
105	1	1,903.9			
106	1	1,881.3	43.0	0	0
107	i	1,880.1	32.0	0	0
108	1	1,884.1	30.0	0	0
109	i	1,884.6	20.0	0	0
				Ö	0
112	1	1,900.7	0.0		
113	1	1,878.5	29.0	0	0
114	1	1,897.3	57.0	0	- 0
117	Ī	1,907.5	59.0	0	0
		1,889.0	37.0	Ô	0
118	1				0
119	1	1,889.1	64.0	0	
120	1	1,871.2	113.0	. 0	0
121	1	1,862.6	109.0	0	0
122	î	1,950.0	89.0	0	0
			65.0	Ŏ	0
123	1	1,927.3			
124	1	1,879.6	68.0	0	. 0
125	1	1,886.2	108.0	0	0
126	1	1,894.1	107.0	0	· 0
127	ì	1,874.9	54.0	Ō	. 0
			38.0	Ō	0
128	1 .	1,896.4			
129	1	1,896.0	8.0	0	. 0
130	1	1,886.4	7.0	0	. 0
131	1	1,875.8	4.0	0	0
132	i	1,886.8	51.0	0	0
				Ŏ	0
133	1	1,898.7	18.0		
134	1	1,924.5	54.0	0	0
135	1	1,915.7	58.0	0	0
136	1	1,944.8	71.0	0	0
137	i	1,905.0	118.0	0	. 0
		1,000,0	165.0	Ö	0
139	1	1,905.8			
140	. 1	1,899.4	31.0	0	. 0
141	1	1,890.2	99.0	0	0
142	1	1,883.9	103.0	0	0
143	ĺ	1,888.7	110.0	0	. 0
		1,907.4	39.0	Ō	. 0
144	1	1,001.4			
145	1	1,909.3	6.0	0	. 0
146	i	1,876.5	54.0	0	. 0
147	1	1,878.9	98.0	0	0
148	1	1,889.6	63.0	0	. 0
149	ī	1,901.1	28.0	. 0	0
			118.0	0	0
150	1	1,899.4			
151	1.	1,874.4	76.0	0	0
152	1	1,865.9	66.0	0	0
153.	1	1,862.7	71.0	. 0	, 0
154	1	1,864.7	66.0	0	0
					0
155	1	1,867.6	22.0	0	
156	ı	1,884.8	40.0	0	0
157	1	1,881.9	24.0	. 0	0
158	Ì	1,880.3	24.0	. 0	0
			19.0	ŏ	. 0
160	1	1,903.2			
161	1	1,905.3	11.0	0	0
162	i	1,891.8	38.0	0	0
163	Ī	1,899.3	7.0	0	0
	1	1,919.8	4.0	Ō	. 0
164				ŏ	Ŏ
165	i	1,962.5	101.0		0
166	1	1,899.0	18.0	0	0
169	1	1,917.8	22.0	. 0	0
170	1	1,893.3	13.0	0	. 0
			19.0	· ŏ	Ŏ
171	1	1,909.7			0
21	- 1	1,885.1	97.0	0	U

20	1	1,885.9	83.0	0		0
174	1	1,902.4	104.0	0		0
53	1	1,895.7	97.0	0		0
176	1	1,895.0	23.0	0		0
177	1	1,897.3	23.0	0		0
178	1	1,912.8	55.0	0		0
179	1	1,917.5	25.0	0		0
181	i	1,881.0	80.0	0		0
182	1	1,891.9	13.0	0		0
183	1	1,899.2	12.0	0		0
185	1	1,902.8	66.0	0		0
186	i	1,885.4	66.0	0		0
187	1	1,903.2	76.0	0		0
188	1	1,931.7	8.0	0		0
189	İ	1,921.8	29.0	0		0
300	i	1,903.6	47.0	0		0
301	1	1,951.4	76.0	0		0
402	1	1,955.5	0.0	0		0
403	1	1,954.4	0.0	0 0		0 0
404	1	1,953.8	0.0	0		0
405	1	1,952.5	$\begin{array}{c} \textbf{0.0} \\ \textbf{0.0} \end{array}$	0		0
406 407	1 1	1,951.8 1,951.3	0.0	0		0
408	1	1,950.7	0.0	0		Õ
409	1	1,950.0	0.0	Ö	•	0
410	1	1,947.8	0.0	Ŏ	•	Ö
411	i	1,947.4	0.0	Õ		ŏ
412	1	1,946.9	0.0	ő		Ŏ
414	i	1,941.7	0.0	ŏ		Ō
415	1	1,940.8	0.0	Õ		0
59	î	1,900.0	122.0	0		0
500	ī	1,892.8	25.0	0		0
501	1	1,886.6	76.0	. 0		0
502	1	1,885.6	80.0	0		0
503	í	1,884.2	76.0	0		0
510	1	1,914.5	51.0	0		0
511	1	1,892.1	20.0	0		0
520	1	1,913.6	63.0	0		0
304	1	1,900.4	70.0	0		0
172	1	1,886.0	51.0	0	1	0
173	1	1,916.0	51.0	0		0
521	1	1,886.0	51.0	0		0
522	i	1,880.0	51.0	0		0
523	1	1,903.0	51.0	0	1.	0
524	1	1,887.0	51.0	0		0
525	1	1,881.0	51.0	0		0 0
526	1	1,882.0	51.0 30.0	0		0
527 528	1 1	1,931.0 1,943.0	30.0	0		Ö
33	1	1,867.0	51.0	0		Ö
35	1	1,870.0	61.0	Õ		Ö
40	i	1,920.0	40.0	Ö		ŏ
54	i	1,886.0	51.0	. 0	:	Ö
540	i	1,930.0	406.0	Õ		Ö
541	i	1,980.0	558.0	Õ		Ŏ
	-				•	
Booster	Pump Da	ta				
No.	Type	Node A	Node B	Pipe No.	Pres	
					(1	ı)

Booster No.	Pu∎p Type	A	Node	В	Pipe No.	Pressure
1 E		156 112		541 540	330 331	(m) 71.0 26.0

Turking Turkin Turkin Turking Turking Turking

1.43 + 1.1 + 3.1

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Pipe	Nota					
Pipe	No.	Node A N	lode B D		Length	C Value
		139	510	(mm) 225.0	(m) 800.0	120.0
	1 2	139	304	44.0	374.0	130.0
	3	139	140	150.0	162.0	120.0
	4	140	161	65.0	222.0	120.0
	5	51	140	150.0	228.0	120.0
	6	162	163	44.0	143.0	130.0
	7	51	162	150.0	20.0 690.0	120.0 120.0
	8 9	51 134	135 135	100.0 65.0	178.0	130.0
	12	134	164	44.0	84.0	130.0
	13	66	135	150.0	265.0	120.0
	14	50	66	100.0	530.0	120.0
	15	50	67	100.0	583.0	120.0
	16	67	188 . 54	100.0 150.0	165.0 59.0	120.0 120.0
	20 21	21 21	23	100.0	88.0	120.0
	22	23	24	150.0	55.0	120.0
	23	20	24	100.0	90.0	120.0
	24	20	21	150.0	66.0	120.0
	25	25	174	100.0	569.0	120.0 120.0
	26	25 52	52 53	100.0 100.0	110.0 176.0	120.0
	27 28	53	60	100.0	100.0	120.0
	29	18	60	100.0	134.0	120.0
	30	18	19	150.0	54.0	120.0
	31	19	52	100.0	151.0	120.0
	32	19	55 172	100.0 100.0	133.0 100.0	120.0 120.0
	33 34	54 9	18	225.0	315.0	120.0
	35	9	48	100.0	47.0	120.0
	36	1	48	225.0	265.0	120.0
	37		49	100.0	201.0	120.0
	38		49	150.0	672.0	120.0
	40 41	49 148	148 171	100.0 50.0	536.0 372.0	120.0 120.0
	42		148	100.0	325.0	120.0
	43		69	150.0	90.0	120.0
	44		149	100.0	551.0	120.0
	45		49	100.0	264.0	120.0
	46		46 64	225.0 100.0	401.0 268.0	120.0 120.0
	48 49		64	300.0	444.0	120.0
	51		158	300.0	47.0	120.0
	52		- 166	50.0	358.0	120.0
	53		158	300.0	77.0	120.0
	54 cc		170 157	$\frac{44.0}{300.0}$	264.0 300.0	130.0 120.0
	55 56		156	300.0	100.0	120.0
	59		169	44.0	440.0	130.0
	61	2	203	350.0	704.0	120.0
	62		4	225.0	442.0	120.0
	63 64		5 61	225.0 65.0	65.0 972.0	120.0 130.0
	65	5 5	6	150.0	221.0	120.0
	66		27	150.0	150.0	120.0
	67	7 27	37	100.0	216.0	120.0
	68		37	150.0	400.0	120.0
	69 70		38 38	100.0 150.0	563.0 30.0	120.0 120.0
	7		178	150.0	452.0	120.0
	72		181	150.0	1,106.0	120.0
	73		. 39	150.0	300.0	120.0
	74		173	44.0	320.0	130.0 120.0
	7: 7:		189 181	150.0 150.0	400.0 92.0	120.0
	8		179	150.0	125.0	
	8		41	150.0	100.0	120.0
	8	2 179	208	65.0	104.0	
	8		103	150.0	350.0 120.0	
	8 8		102 100	44.0 44.0	120.0	
	8			37.0	312.0	
	•					

88	42	43	100.0	257.0	120.0
89	42	43	100.0	257.0	120.0
	43	44	150.0	268.0	120.0
90	43 44	177	100.0	391.0	120.0
91	44	176	100.0	391.0	120.0
92	176	177	100.0	90.0	120.0
93			65.0	251.0	130.0
99	29	112		400.0	120.0
100	109	511	100.0		
101	108	109	100.0	120.0	120.0
102	108	183	44.0	228.0	130.0
103	107	108	100.0	200.0	120.0
104	107	182	44.0	253.0	130.0
105	28	107	100.0	40.0	120.0
106	28	113	150.0	66.0	120.0
107	113	114	65.0	265.0	130.0
108	114	117	65.0	500.0	130.0
109	117	118	44.0	318.0	130.0
111	118	119	75.0	248.0	120.0
113	28	106	150.0	250.0	120.0
114	103	106	150.0	400.0	120.0
115	105	106	44.0	250.0	130.0
116	104	105	44.0	300.0	130.0
117	103	104	44.0	239.0	130.0
118	30	526	100.0	210.0	120.0
120	155	500	140.0	175.0	130.0
121	150	185	75.0	300.0	120.0
122	31	150	150.0	300.0	120.0
125	132	133	44.0	363.0	130.0
126	31	132	150.0	616.0	120.0
127	31	64	225.0	167.0	120.0
128	31	70	150.0	862.0	120.0
129	. 70	144	100.0	284.0	120.0
130	144	145	44.0	121.0	130.0
131	45	144	100.0	368.0	120.0
132	45	47	150.0	162.0	120.0
134	9	57	100.0	25.0	120.0
135	57	58	100.0	120.0	120.0
136	58	60	100.0	262.0	120.0
137	56	58	100.0	330.0	120.0
140	58	143	100.0	168.0	120.0
141	142	143	50.0	264.0	120.0
142	57	142	100.0	202.0	120.0
143	141	142	100.0	99.0	120.0
145	11	12	100.0	388.0	120.0
146	12	150	150.0	360.0	120.0
147	12	151	150.0	163.0	120.0
148	13	151	150.0	35.0	120.0
149	151	186	140.0	450.0	130.0
151	154	155	100.0	132.0	120.0
160	153	154	100.0	165.0	120.0
161	14	153	150.0	236.0	120.0
162	13	14	150.0	475.0 35.0	120.0 120.0
163	13	146	150.0		120.0
164	146	147 147	150.0 150.0	137.0	120.0
165 168	11 14	152	100.0	313.0 66.0	120.0
170	33	152	100.0	150.0	120.0
		136	44.0	726.0	130.0
176	68	137		512.0	130.0
177	136 137	187	44.0 140.0	277.0	130.0
178	71				120.0
181	71	122	225.0 225.0	400.0 400.0	120.0
182		124 124	225.0	441.0	120.0
183	15				
184	15 16	16 121	150.0 100.0	177.0 286.0	120.0 120.0
185					
186	120	121	75.0 100.0	1,210.0 850.0	120.0 120.0
187	16 123	125		764.0	120.0
188	123	125	100.0		
189	123	124	44.0	120.0	130.0
190	122	123	140.0	160.0 120.0	130.0 120.0
191	122	209	225.0 100.0	396.0	120.0
193	125 126	126 128	65.0	668.0	130.0
194 195	126	127	65.0	1,047.0	130.0
196	128	129	65.0	90.0	130.0
Tan	120	143	00.0	30.0	100.0

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197	129	130	44.0		60.0	130.0
198	130	131	37.0		88.0	130.0
199	62	520	100.0		569.0	120.0
200	41	42	100.0		237.0	120.0
203	5	36	150.0	-	105.0	120.0
179	187	300	150.0		500.0	120.0
250	136	301	65.0	:	215.0	130.0
209	160	300	150.0		152.0	120.0
210	185	186	140.0		250.0	130.0
211	53	56 524	$100.0 \\ 97.0$		150.0 334.0	120.0 130.0
213 214	62 30	503	100.0		334.0	120.0
215	112	511	75.0		132.0	120.0
216	500	501	140.0		100.0	130.0
217	154	501	65.0		104.0	130.0
218	186	501	140.0		221.0	130.0
219	121	520	100.0		656.0	120.0
110	118	503	75.0		167.0	120.0
300	215	301	100.0		554.0	120.0
208	215	300	100.0		250.0	120.0
17	205	527	100.0		250.0	120.0
303	10	141	100.0		442.0	120.0
304	24	25	100.0		55.0	120.0
305	55	172 172	100.0		50.0 50.0	120.0 120.0
306	20 23	0.5	100.0		75.0	120.0
307 308	دم 40	178	150.0		150.0	120.0
77	39	40	100.0		180.0	120.0
78	40	189	100.0		60.0	120.0
79	100	101	44.0		450.0	130.0
309	41	42	150.0		150.0	120.0
310	119	521	65.0		350.0	130.0
311	521	522	65.0		350.0	130.0
312	120	522	65.0		350.0	130.0
313	33	35	100.0		150.0	120.0
301	11	523	150.0		120.0	120.0
314	59 502	523	100.0	÷	180.0 150.0	120.0 120.0
315 316	502 525	524 600	75.0 75.0		450.0	120.0
317	524	600	97.0		450.0	
318	525	600	97.0	 	450.0	130.0
319	525	526	75.0	i.	210.0	
321	527	528	65.0	: .	480.0	130.0
322	134	528	65.0		200.0	130.0
11	165	601	65.0		75.0	130.0
324	188	527	65.0	*	50.0	130.0
325	122	123	140.0		160.0	130.0
326	123	125	97.0	+ 1	764.0	130.0
327	56	59	140.0		352.0 264.0	130.0 130.0
328 329	1 206	49 527	158.0 150.0		215.0	120.0
330	156	541	100.0	1.7	931.0	
331	112		97.0		434.0	130.0
212	22			1.5	275.0	
401	402	602	200.0		234.0	
402	402	403	200.0	100	101.0	120.0
403	403	404			61.0	120.0
404	404	405	200.0		122.0	
405	405	406	200.0		65.0	
406	406	407	200.0		42.0	120.0
407	407	408	200.0	$e_{i,j} \cdot \cdot$	61.0	
408	408	409	200.0	1.3	61.0 215.0	
409 410	409 410	410	250.0		90.0	
411	411	412		7 Å.	152.0	
413	412		200.0		488.0	
414	414	415		4.	80.0	
415	46	415		5.0	75.0	
				1.12	1.5	4.0

Node	Net Work	Analysis	Dynamic	Distribut: Dynamic	ion Main Static	٨	
No.	of Pipe	Demand	Pressure	Pressure	Pressure		Leakage .
	(MSL)	(cua/d)	(MSL)	(m)	(m)		(cum/d)
1		90.3	1,943.1	61.4	109.3	0.0 0.0	0.0 37.1 0.0 24.2
2		51,8 56.2	1,926.8 1,926.5	41.7 44.7	105.9 109.2	0.0	0.0 26.2
,		29.6	1,926.5	45.2	109.7	0.0	0.0 26.5
(56.2	1,926.3	42.6	107.3	0.0	0.0 24.8
		98.4	1,939.2	58.0	109.8	0.0	0.0 34.9 0.0 20.0
10 11		18.5 63.6	1,938.4 1,927.7	35.0 25.6	87.6 88.9	0.0	0.0 20.0
12		48.8	1.926.9	46.4	110.5	0.0	0.0 27.2
13	3 1,874.2	37.7	1,926.9	52.7	116.8	0.0	0.0 31.3
1		48.8	1,926.7	61.1 98.9	125.4 130.5	0.0	0.0 36.9 0.0 62.6
1; 1;		45.1 62.9	1,959.4 1,959.0	98.5	130.5	0.0	0.0 62.4
1		79.2	1,939.1	54.0	105.9	0.0	0.0 32.2
1	9 1,885.8	62.9	1,939.1	53.3	105.2	0.0	0.0 31.7 0.0 30.1
2: 2		58.5 60.7	1,940.3 1,939.1	50.9 51.8	101.6 103.7	0.0 0.0	0.0 30.1 0.0 30.7
2		86.6	1,939.1	51.4	103.3	0.0	0.0 30.5
2	5 1,887.0	37.7	1,939.0	52.0	104.0	0.0	0.0 30.9
2			1,926.2	43.9	108.7	0.0	0.0 25.6 0.0 26.0
2	8 1,879.2 9 1,892.4		1,923.7 1,912.6	44.5 20.2	111.8 98.6	0.0	0.0 26.0 0.0 10.9
	0 1,882.6		1,941.7	59.1	108.4	0.0	0.0 35.5
3	1 1,882.0	68.8	1,926.8	44.8	109.0	0.0	0.0 26.2
	6 1,889.3		1,926.4	37.1 34.8	101.7 99.6	0.0 0.0	0.0 21.3 0.0 19.8
	7 1,891.4 $8 1,893.9$		1,926.2 1,926.1	32.2	97.i	0.0	0.0 18.3
	9 1,914.9		1,926.1	11.2	76.1	0.0	0.0 5.7
	1 1,899.2		1,926.1	26.9	91.8	0.0	0.0 15.0
	2 1,896.1		1,926.1 1,926.1	30.0 31.3	94.9 96.2	0.0	0.0 16.9 0.0 17.6
	13 1,894.8 14 1,893.4		1,926.1	32.7	97.6	0.0	0.0 18.5
	5 1,884.9		1,926.7	41.8	106.1	0.0	0.0 24.3
	6 1,878.2		1,944.5	66.3	112.8	0.0	0.0 40.3 0.0 27.0
	17 1,880.7 18 1,880.2		1,926.7 1,942.7	48.0 62.5	110.3 110.8	0.0	0.0 37.8
	1,881.1		1,942.7	61.6	109.9	0.0	0.0 37.2
5	io 1,886.:	106.6	1,952.6	66.3	104.7	0.0	0.0 40.4
	51 1,895.4		1,949.0 1,938.8	53.6 49.6	95.6 101.9	0.0 0.0	0.0 31.9 0.0 29.4
	52 1,889.3 55 1,886.3		1,939.2	53.0	104.8	0.0	0.0 31.5
	56 1,902.	7 36.3	1,935.6	32.9	88.3	0.0	0.0 18.7
	57 1,884.		1,938.8	54.7	106.9	0.0 0.0	0.0 32.6 0.0 27.6
	58 1,890,9 60 1,889.9		1,937.9 1,938.0	47.0 48.1	100.1 101.1	0.0	0.0 28.4
	61 1,885.		1,926.1	40.7	105.6	0.0	0.0 23.6
	62 1,890.		1,947.9	57.7	100.8	0.0	0.0 34.6
	63 1,878. 64 1,876.		1,926.8 1,926.8	48.1 50.3	112.3 114.5	0.0	0.0 28.3 0.0 29.8
	66 1,910.		1,951.4		81.0	0.0	0.0 24.0
	67 1,921.	5 28.1	1,955.3	33.8	69.5	0.0	0.0 19.2
	68 1,918.		1,976.7		72.4 111.5	0.0 0.0	0.0 34.9 0.0 39.4
	69 1,879. 70 1,904.		1,944.4 1,926.7		86.5	0.0	0.0 12.1
	71 1,894.		1,959.7	65.2	96.5	0.0	
	00 1,896.		1,925.5		94.4		0.0 9 9 16.2 6
	01 1,885. 02 1,876.	9 18.5 7 27.4	1,925.3 1,925.2				0.0 22.7 0.0 28.6
	03 1,883.		1,924.6			0.0	0.0 24.1
1	04 1,916.		1,924.2		74.7	0.0	0.0 3.9
	.05 1,903. .06 1,881.		1,924.0 1,924.0			0.0	0.0 10.9 0.0 24.9
	07 1,880.					0.0	0.0 25.1
1	08 1,884.	1 22.2	1,921.	37.2		0.0	0.0 21.3
	09 1,884.						0.0 20.4 0.0 6.1
	112 1,900. 113 1,878.					0.0	0.0 26.4
	113 1,870				93.7	0.0 🗹	0.0 14.9
1	1,907	5 43.7	1,926.	0 18.5			0.0 9.9
	1,889.					0.0 0.0	0.0 30.5 0.0 30.5
	[19 1,889] [20 1,871]					0.0	0.0 45.1
:	121 1,862	.6 80.7	1,954.	3 91.7	128.4	0.0	0.0 57.7
	122 1,950					0.0	0.0 5.0 0.0 18.4
	123 1,927 124 1,879					0.0	0.0 49.6
	125 1,886					0.0	0.0 44.8

Node	Net Work Elevation	Analysis Demand	Dynamic	Distributi Dynamic	Static	A		Leakage
No.	of Pipe		Pressure	Pressure (m)	Pressure (m)			(cum/d)
100	(MSL) 1,894.1	(cum/d) 79.2	(MSL) 1,958.8	(M) 64.7	96.9	0,0	0.0	39.3
126 127	1,874.9	40.0	1,958.2	83.3	116.1	0,0	0.0	51.9
128		28.1	1,958.4	62.0	94.6	0.0	0.0	37.5
129		5.9	1,958.4	62.4	95.0	0.0	0.0	37.7
130		5.2	1,958.4	72.0	104.6	0.0	0.0	44.1
131		3.0	1,958.4	82.6	115.2	0.0	$0.0 \\ 0.0$	51.4 23.1
132		37.7 13.3	1,926.8 1,926.6	$\begin{array}{c} 40.0 \\ 27.9 \end{array}$	$104.2 \\ 92.3$	0.0	0.0	15,6
133 134		40.0	1,952.1	27.6	66.5	0.0	0.0	15.4
135		42.9	1,951.3	35.6	75.3	0.0	0.0	20.4
136		52.5	1,978.3	33.5	46.2	0.0	0.0	19.1
137		87.3	1,978.5	73.5	86.0	0.0	0.0	$\frac{45.2}{25.1}$
139		122.1	1,948.9 1,948.9	43.1 49.5	85.2 91.6	0.0 0.0	0.0	29.3
140 141		22.9 73.3	1,938.5	48.3	100.8	0.0	0.0	28.4
142		76.2	1,938.5	54.6	107.1	0.0	0.0	32.6
143		81.4	1,937.9	49.2	102.3	0.0	0.0	29.1
144		28.9	1,926.7	19.3	83.6	0.0	0.0	10.4 9.3
145		4.4	1,926.7	17.4	81.7 114.5	0.0 0.0	0.0	29.9
146 147		40.0 72.5	1,926.9 1,927.1	50.4 48.2	112.1	0.0	0.0	28.4
148		46.6	1,943.6	54.0	101.4	0.0	0.0	32.2
149		20.7	1,944.4	43.3	89.9	0.0	0.0	25.3
150		87.3	1,926.8	27.4	91.6	0.0	0.0	15.3
15:		56.2	1,926.9	52.5	116.6 125.1	0.0	0.0	31.2 36.7
152		48.8 52.5	1,926.7 1,926.7	60.8 64.0	123.1	0.0	0.0	38.8
15: 15:		48.8	1.926.7	62.0	400.0	0.0	0.0	37.5
15		16.3	1,926.7	59 1	123.4	0.0	0.0	35.6
15		29.6	1,926.8	42.0	106.2	0.0	0.0	24.4
15		17.8	1,926.8	44.9	109.1	0.0 0.0	$0.0 \\ 0.0$	$\frac{26.3}{27.3}$
15		17.8 14.1	1,926.8 1,978.6	46.5 75.4	110.7 87.8	0.0	0.0	46.5
16 16		8.1	1,948.9	43.6	85.7	0.0.	0.0	25.5
16.		28.1	1,949.0	57.2	99.2	0.0	0.0	34.3
16		5.2	1,949.0	49.7	91.7	0.0	0.0	29.4
16		3.0	1,952.1	32.3	71.2	$0.0 \\ 0.0$	$0.0 \\ 0.0$	18.3 15.9
16		74.7 13.3	1,990.9 1,926.7	28.4 27.7	28.5 92.0	0.0	0.0	15.4
16 1 6		16.3	1,926.5		73.2	0.0	0.0	4.3
17	0 1,893.3	9.6	1,926.7	33.4	97.7	0.0	0.0	19.0
17		14.1	1,943.5		81.3	0.0	0.0	19.2 32,3
2		71.8	1,939.3		105.9 105.1	0.0	$0.0 \\ 0.0$	32.3 31.8
17	0 1,885.9 4 1,902.4	61.4 77.0	1,939.2 1,938.8		88.6	0.0	0.0	20.9
	3 1,895.7	71.8	1,937.7		95.3	0.0	0.0	24.4
17	6 1,895.0	17.0	1,926,1		96.0	0.0	0.0	17.5
17	7 1,897.3	17.0	1,926.1		93.7	0.0	$0.0 \\ 0.0$	16.1 6.8
17		40.7 18.5	1,926.0 1,926.2		78.2 73.5	0.0	0.0	4,3
17 18		59,2	1,925.4		110.0	0.0	0.0	26.0
18		9.6	1,923.2		99.1	0.0	0.0	17.6
18		8.9	1,921.2		91.8	0.0	0.0	12.0 13.2
18	35 1,902.8	48.8	1,926.8		88.2 105.6	$0.0 \\ 0.0$	0.0	24.0
18	36 1,885.4 37 1,903.2		1,926.8 1,978.6		87.8	0.0	0.0	46.4
- 18		5,9			59.3	0.0	0.0	13.4
18		21.5	1,925.7	3.9	69.2	0.0	0.0	1.8
	00 1,903.6		1,978.6		87.4	0.0	0.0	46.2 15.2
	1,951.4		1,978.7		39.6 35.5	0.0	$0.0 \\ 0.0$	0.2
	02 1,955.5 03 1,954.4		1,956.1 1,955.3		36,6	0.0	0.0	0.4
	04 1,953.8		1,954.8		37.2	0.0	0.0	0.4
	05 -1,952.5	0.0	1,953.8		38.5	0.0	0.0	0.6
	06 1,951.8		1,953.3			0.0	0.0	0.6 0.7
	07 1,951.3		1,953.0 1,952.3		39.7 40.3	0.0	0.0	0.8
	08 1,950.7 09 1,950.0		1,952.6			0.0	0.0	0.9
	10 1,947.8		1,950.		43.2	0.0	0.0	1.1
4	11 1,947.4	0.0	1,950.	2.6		0.0	0.0	1.2
	12 1,946.9		1,949.			0.0	0.0	1.2 1.8
	14 1,941.7					0.0	0.0	. 2.0
	15 1,940.8 59 1,900.0			-		0.0	0.0	19.1
	00 1,892.8		1,926.	7 33.9	98.2	0.0	0.0	19.3
	01 1,886.6					0.0	0.0	23.2 36.9
. 5	02 1,885.6	59.2	1,946.	7 61.1	100.4		0.0	50,0

	Net Work	Analysis	3	Distribut	ion Main	A		
Node	Elevation	Demand	Dynamic	Dynamic	Static			Leakage
No.	of Pipe	vewanu	Pressure	Pressure	Pressure			Learage
	(MSL)	(cum/d)	(MSL)	(n)	(m)			(cum/d)
503	1,884.2	56.2	1,941.1	56.9	106.8	0.0	0.0	34.1
510	1,914.5	37.7	1,948.9	34.4	76.5	0.0	0.0	19.6
511	1,892.1	14.8	1,916.9	24,8	98.9	0.0	0.0	13.7
520	1,913.6	46.6	1,950.6	37.0	77.4	0.0	0.0	21.2
304	1,900.4	51.8	1,946.8	46.4	90.6	0.0	0.0	27.2
172	1,886.0	37.7	1,939.2	53.2	105.0	0.0	0.0	31.7
173	1,916.0	37.7	1,925.1	9.1	75.0	0.0	0.0	4.5
521	1,886.0	37.7	1,941.1	55,1	105.0	0.0	0.0	32.9
522	1,880.0	37.7	1,942.4	62.4	111.0	0.0	0.0	37.7
523	1,903.0	37.7	1,928.2	25.2	88.0	0.0	0.0	13.9
524	1,887.0	37.7	1,946.8	59.8	104,0	0.0	0.0	36.0
525	1,881.0	37.7	1,945.1	64.1	110.0	0.0	0.0	38.9
526	1,882.0	37.7	1,942.2	60.2	109.0	0.0	0.0	36.3
527	1,931.0	22.2	1,958.0	27.0	60.0	0.0	0.0	15,0
528	1,943.0	22.2	1,953.5	10.5	48.0	0.0	0.0	5.3
33	1,867.0	37.7	1,926.7	59,6	124.0	0.0	0.0	35.9
35	1,870.0	45.1	1,926.6	56.6	121.0	0.0	0.0	33.9
40	1,920.0	29.6	1,925.9	5.9	71.0	0.0	0.0	2,8
54	1,886.0	37.7	1,939.4	53.4	105.0	0.0	0.0	31.8
540	1,930.0	486.9	1,935.3	5.3	61.0	0.0	0.0	2.5
541	1 980 0	669 7	1 985 0	5.0	11.0	0.0	0.0	2.3

Pipe No.		Net.	Work	Analy	sis	1	Distribut	tion Main			
1 1 139 510 800,00 225,00 120,00 37,00 .000 .000 .000 .000 .000 .000 .000				-					Velocity		loss
1	NO.				(m) ·					(0/00)	
1										0.00 5.70	
4 140 181 222.00 65.00 120.00 8.00 0.00 0.00 0.00 0.00 1.00 6 162 181 140 222.00 150.00 120.00 120.00 15.00 0.00 0.00 0.00 0.00 1.00 0.00 181 140 222.00 150.00 120.00 120.00 5.00 0.00 0.00 0.00 0.00 1.00 0.00 120.00 120.00 120.00 120.00 0.30 0.00 0.00 0.00 0.00 1.00 120.00 120.00 120.00 120.00 120.00 120.00 0.30 0.00 0.00 0.00 0.00 120.		2									
5 51 140 228.00 150.00 120.00 221.00 0.00 0.00 0.00 0.00 0		3 4						8.00	0.00	0.00	
Total 182		5	51								
8 51 135 890,00 100,00 120,00 -310,00 -0.50 -3.30 -2.30 121 134 144 84,00 44,00 130,00 130,00 130,00 0.00 0.00 0.00 0.00 0.00 133 66 155 255,00 150,00 120,00 250,00 0.40 0.24 0.13 0.11 14 50 66 530,00 100,00 120,00 250,00 0.40 0.24 0.13 0.15 15 50 67 883,00 100,00 120,00 -394,00 -0.50 -4.55 -2.60 0.60 0.20											
9	:	/ ጸ								-3.30	-2.30
13		9	134	135							
14											
15										2,40	1.30
20	1	5	50	67	583.00						
21											
222 23										2.50	0.20
24				24		150.00	120.00	39.00			
285											
26											0.10
27 52 53 176,00 100,00 120,00 429,00 0,80 5.00 1.110 28 53 60 100,00 100,00 120,00 -318,00 -0.50 -3.50 -0.30 29 18 60 134,00 100,00 120,00 530,00 0,70 8.10 1.10 30 18 19 54,00 155,00 120,00 211,00 0,10 0,20 0,00 31 19 55 151,00 100,00 120,00 210,00 -0.60 0,40 2.40 0.40 32 19 55 133,00 100,00 120,00 120,00 -110 0 -0.20 -0.50 -0.10 33 5 172 100,00 100,00 120,00 120,00 195,00 0,30 1,40 0,10 34 9 18 315,00 225,00 120,00 794,00 0,20 0.40 0,40 0,10 35 9 48 47,00 100,00 120,00 1,682,00 -2.40 -73,50 -3.50 36 1 48 265,00 225,00 120,00 1,683,00 -0.16 -0.10 0,00 37 43 49 201,00 100,00 120,00 -1,683,00 -0.16 -0.10 0,00 38 22 49 672,00 150,00 120,00 -446,00 -0.60 -3.60 -2.40 40 49 148 536,00 100,00 120,00 -246,00 -0.60 -3.60 -2.40 41 148 171 372,00 50,00 120,00 -946,00 -0.60 -3.60 -2.40 42 69 148 325,00 100,00 120,00 210,00 -0.30 -1.60 -0.90 41 148 325,00 100,00 120,00 -210,00 -0.30 -1.60 -0.90 44 69 149 551,00 100,00 120,00 271,00 0,10 0,30 -1.60 44 69 49 264,00 100,00 120,00 271,00 0,40 -2.60 0,80 45 1 49 264,00 100,00 120,00 -279,00 0,00 0,00 0,00 0,00 51 63 158 47,00 300,00 120,00 -279,00 0,10 0,00 0,00 0,00 52 158 166 356,00 50,00 120,00 120,00 130,00 0,00 0,00 0,00 0,00 54 157 170 264,00 44,00 130,00 120,00 280,00 0,10 0,30 0,10 55 158 156 169 344,00 340,00 120,00 270,00 0,00 0,00 0,00 0,00 55 158 169 170 264,00 44,00 130,00 120,00 288,00 0,10 0,00 0,00 0,00 56 2 158 169 440,00 44,00 130,00 120,00 288,00 0,10 0,00 0,00 0,00 56 2 158 169 440,00 44,00 130,00 120,00 288,00 0,10 0,00 0,00 0,00 56 2 158 169 440,00 44,00 130,00 130,00 130,00 0,00 0,00 0,00								240.00			0.20
29 18 60 134.00 100.00 120.00 503.00 0.70 8.10 1.10	2	7	52	53							
18											
ST									0.10	0.20	0.00
100 100	9	31	19	52	151.00			St. 1			
34 9 18 315.00 225.00 120.00 794.00 0.20 0.40 0.10 35 9 48 47.00 100.00 120.00 1,652.00 -2.40 -73.50 0.3.50 36 1 48 265.00 225.00 120.00 1,683.00 0.50 1.50 0.40 37 48 49 201.00 100.00 120.00 1,683.00 0.50 1.50 0.40 37 48 49 201.00 100.00 120.00 1.683.00 0.50 1.50 0.40 38 22 49 672.00 150.00 120.00 1.20.00 -946.00 -0.60 -360 -2.40 40 49 148 536.00 100.00 120.00 120.00 -210.00 -0.30 -1.60 -0.90 41 148 171 372.00 50.00 120.00 120.00 1.40 0.00 1.00 0.00 120.00 1.00 0.00 120.00 1.00 0.00 120.00 1.00 0.00 120.00 1.00 0.00 120.00 1.00 0.00 120.00 1.00 0.00 120.00 1.00 0.00 0											
S									0.20	0.40	0.10
37			9	48	47.00	100.00					
38											
40											-2.40
41 69 148 325.00 100.00 120.00 271.00 0.40 2.80 0.80 43 46 69 90.00 150.00 120.00 328.00 0.20 0.50 0.10 44 69 149 551.00 100.00 120.00 220.00 0.90 0.00 <t< td=""><td></td><td></td><td>49</td><td>148</td><td>536.00</td><td>100.00</td><td></td><td></td><td></td><td></td><td></td></t<>			49	148	536.00	100.00					
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83 102 103 350,00 150,00 120,00 652,00 0,40 1.80 0.60 84 101 102 120,00 44,00 130,00 6,00 0,10 0.10 0,00 86 41 100 120,00 44,00 130,00 49,00 0,40 5,20 0,60 87 100 101 312,00 37,00 180,00 10,00 0,10 0,10 0,70 0,20 88 42 43 257,00 100,00 120,00 51,00 0,10 0,10 0,00 89 42 43 257,00 100,00 120,00 51,00 0,10 0,10 0,00 90 43 44 268,00 150,00 120,00 74,00 0,10 0,00 0,00 91 44 177 391,00 100,00 120,00 17,00 0,00 0,00 0,00		81	39	41	100.00	150.00	120.00				
84 101 102 120.00 44.00 130.00 6.00 0.10 0.10 0.00 86 41 100 120.00 44.00 130.00 49.00 0.40 5.20 0.60 87 100 101 312.00 37.00 130.00 10.00 0.10 0.70 0.20 88 42 43 257.00 100.00 120.00 51.00 0.10 0.10 0.00 89 42 43 257.00 100.00 120.00 51.00 0.10 0.10 0.00 90 43 44 268.00 150.00 120.00 74.00 0.10 0.10 0.00 91 44 177 391.00 100.00 120.00 17.00 0.00 0.00 0.00 0.00											
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88 42 43 257.00 100.00 120.00 51.00 0.10 0.10 0.00 89 42 43 257.00 100.00 120.00 51.00 0.10 0.10 0.00 90 43 44 268.00 150.00 120.00 74.00 0.10 0.00 0.00 91 44 177 391.00 100.00 120.00 17.00 0.00 0.00 0.00		86	41	100	120.00	44.00	130.00				
89 42 43 257.00 100.00 120.00 51.00 0.10 0.10 0.00 90 43 44 268.00 150.00 120.00 74.00 0.10 0.00 0.00 91 44 177 391.00 100.00 120.00 17.00 0.00 0.00 0.00				101							
90 43 44 268.00 150.00 120.00 74.00 0.10 0.00 0.00 91 44 177 391.00 100.00 120.00 171.00 0.00 0.00 0.00	٠.			43				51.00	0.10	0.10	0.00
91 44 111 391.00 100.00 120.00		90	43	44	268.00	150.00	120.00				
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	Net Wo	rk Anal	ysis		Distribu	tion Main			
Pipe No.	Node A			Diameter	C	Flow	Velocity	Pressure Gradient	loss
			(m)	(mm)		(cup/d)	(m/s)	(0/00)	(m)
93 9 9		177 112	90.00 251.00	100.00 65.00	120.00 130.00	0.00 -9.00	0.00	0.00	0.00
100		511	400.00	100.00	120.00	511.00	0.80	8.40	3,40
101	108	109	120.00	100.00	120.00		0.80	8.80	1.10
102		183	228.00	44.00	130.00	8.00	0.10	0.20	0.10
103 104		108 182	200.00 253.00	100.00 44.00	120.00 130.00	557.00 9.00	0.80 0.10	9.80 0.30	$\frac{2.00}{0.10}$
105		107	40,00	100.00	120.00	590.00	0.90	10.90	0.40
106		113	66.00	150.00	120.00	-52.00	0.00	0.00	0.00
107 108		114 117	265,00 500,00	65.00 65.00	130.00 130.00	-73.00 -116.00	-0.30 -0.40	-1.60 -3.80	~0.40 ~1.90
109		118	318,00	44.00	130.00		-1.20	-45.60	-14.50
111	118	119	248,00	75.00	120.00	-28,00	-0.10	-0.20	0,00
113 114		106 106	250.00 400.00	150.00 150.00	120.00 120.00	-557.00 587.00	-0.40	-1.40 1.50	$-0.30 \\ 0.60$
115		106	250.00	44.00	130.00	1.00	0.00	0.00	0.00
116	104	105	300.00	44.00	130.00	14,00	0.10	0.50	0.20
117		104	239.00	44.00 100.00	130.00 120.00	28.00 -273.00	0.20 -0.40	1.90 -2.60	0.40 -0.60
118 120		526 500	210.00 175.00	140.00	130.00		0.00	7	
121		185	300.00	75.00	120.00	22.00	0.10	0.10	0.00
122		150	300.00	150.00	120.00		-0.10	-0.10	0.00
125 126		133 132	363.00 616.00	44.00 150.00	130.00 120.00	13.00 51.00	0.10	0.50 0.00	0.20 0.00
127		64	167.00	225.00	120.00	-148.00	0.00		0,00
128	31	70	662.00	150.00	120.00	127.00	0.10	0.10	0.10
129		144	284.00	100.00	120.00		0.00	0.00 0.10	0.00 0.00
130 131			121.00 368.00	44.00 100.00	130,00 120,00		0.00	0.00	0.00
132		47	162.00	150.00		-52.00	0.00	0.00	0.00
134			25.00	100.00	120.00	759.00	1.10	17.40	0.40
135 136			120.00 262.00	100,00 100,00	120,00 120,00	482.00 -111.00		7.50 -0.50	0.90 -0.10
137			330.00	100.00	120.00	-465.00	-0.70	-7.00	-2.30
140) 58	143	168.00	100.00	120,00	40.00 40.00	0.10	0.10	0.00
141			264.00	50.00 100.00	120.00 120.00	40.00 208.00	0.20 0.30	2,20 1,60	$0.60 \\ 0.30$
142 143			202.00 99.00	100.00	120 00	-91 00			0.00
149	5 11	12	388.00	100.00	120,00	248.00	0.40	2.20	0.90
140 147			360.00 163.00	150,00 150,00	120.00 120.00	209.00 -9.00	0.10	$0.20 \\ 0.00$	0.10
148			35.00	150.00	120.00	265.00	0.00		0.00
149	9 151	186	450.00	140,00	130.00	199.00	0.10	0.30	0.10
151			132.00	100.00	130.00	-20.00	0.00		0.00
160 161		154 153	165.00 236.00	100.00 150.00	120.00 120.00	14.00 67.00	0.00	0.00 0.00	0.00 0.00
162	2 13	14	475.00	150,00	120.00	247.00	0.20	0.30	0.10
163			35.00	150.00					-0.10
164 161			137.00 313.00	150.00 150.00	120.00 120.00		-0.40 0.40	-1.50 1.90	-0.20 0.60
168			66.00	100.00		131.00		0.70	0.00
170		152	150.00	100.00	120.00				0.00
176 171			726.00 512.00	44.00 44.00	130.00 130.00	-31,00 -12,00			-1.60 -0.20
178			277.00	140.00	130.00	-99.00	-0.10		0.00
18	1 71	122	400.00	225.00	120.00	-860,00	-0.30	-0.40	-0.20
18			400.00	225.00	120.00		0.20 -0.20	0.40 -0.30	0.10 -0.10
18: 18:			441,00 177,00	225,00 150.00	120.00 120.00				0.40
18		121	286.00	100.00	120.00	734.00	1.10	16.40	4.70
18			1,210.00		120.00			-8.10	-9.80
18' 18			850.00 764.00	100.00	120.00 120.00	-64.00 152.00		-0.20 0,90	-0.10 0.70
18			120.00	44.00	130.00	32,00	0.20	2.30	0.30
19			160.00	140.00	130,00	192.00	0.10	0.20	0.00
19 19			120.00 396.00	225.00 100.00	120.00	-1,312.00 161.00		-0.90 1.00	-0.10 0.40
19			668.00	65.00	130.00		0.10	0.60	0.40
19	5 126	127	1,047.00	65.00	130.00	40.00	0.10	0.50	0.80
19 19			90.00 60.00	65.00	130.00			0.10 0.20	0.00 0.00
19			88.00	37.00	130.00		0.10		0.00
19	9 62	520	569.00	100.00	120,00	-371.00	-0.60	-4.60	-2.60
20			237.00	100,00	120,00		0.00		0.00
20 17			105.00 500.00	150,00 150,00	120,00 120,00		0.30 -0.10	-0.10	0.10 -0.10
25			215.00	65.00	130.00	-71.00	-0.30	-1.50	-0.30
				* .					

	Net Wo	rk Anal	lysis		Distrib	ution Main			
Pipe No.	Node A	Node B	Length	Diameter	C	Flow	Velocity	Pressure Gradient	Loss
,,,,			(m)	(mm)		(cum/d)	(m/s)	(0/00)	(m)
209	160	300	152.00	150,00	120.00	-14.00	0.00	0.00	0.00
210		186	250.00	140.00	130.00	-26.00	0,00	0.00	0.00
211		56	150.00	100,00	120.00	675.00	1.00	14.00	2,10
213		524	334.00	97,00	130,00	315.00	0.50	3.40	1.10
214		503	334,00	100.00	120,00	214.00	0.30	1.70	0.60
215		511	132,00	75.00	120.00	-496.00	-1.30	-32.20	-4.30
216	500	501	100,00	140.00	130.00	-55.00	0.00	0.00	0.00
217	154	501	104.00	65,00	130.00	-13.00	-0.10	~0.10	0,00
218	186	501	221,00	140,00	130.00	125.00	0.10	0.10	0.00
219	121	520	656,00	100,00	120.00	418.00	0.60	5.80	3.80
110	118	503	167.00	75.00	120.00	-158.00	-0.40	-3.90	-0.70
300	215	301	554,00	100,00	120.00	127.00	0.20	0.60	0.30
208	215	300	250.00	100,00	120.00	205.00	0.30	1.50	0.40
17	205	527	250.00	100,00	120.00	501.00	0.70	8.10	2.00
303	10	141	442.00	100.00	120,00	-18.00	0.00	0.00	0.00
304	24	25	55.00	100.00	120.00	192.00	0.30	1.40	0.10
305	55	172	50.00	100.00	120.00	-177.00	-0.30	-1.20	-0.10
306	20	172	50.00	100.00	120.00	19.00	0.00	0.00	0.00
307	23	25	75,00	100.00	120.00	163.00	0.20	1.00	0.10
308	40	178	150.00	150.00	120.00	-235.00	-0.10	-0.30	0.00
77	39	40	180.00	100.00	120.00	170,00	0.30	1.10	0.20
78	40	189	60.00	100.00	120.00	375.00	0.60	4,70	0.30

Net Work Analysis

Distribution Main

NuvaExistYear2015 File Name Season All Network Type Existing Year 2015 Demand Hourly Max Water Level Fix All Reserver Discharge Fix None Magnification of Demand 1.622 Reservoir Data HWL LWL Reservoir Node (MSL) (MSL) 1,927.0 Haddon Hill 203 1,927.0 1,960.0 1,960.0 New Water Field 205 1,958.0 1,958.0 Old Water Field 206 1,930.0 208 1,930.0 Bonavista 209 1,960.0 1,960.0 Lovers Leap 1,979.0 1,979.0 Gamunu/Brewery 215 1,946.0 Naseby 600 1,946.0 601 1,991.0 1,991.0 Piyatissapura 1,958.0 Pedro Intake 602 1,958.0 Node Data **Ground Elev** Demand Node (cum/d) (MSL) 1,881.7 122.0 0 70.0 0 1,885.1 0 1,881.8 76.0 0 1,881.3 40.0 0 0 76.0 1,883.7 0 0 1,881.2 133.0 10 1,903.4 25.0 0 0 1,902.1 86.0 11 0 1,880.5 66.00 12 13 1,874.2 51.0 0 O 14 1,865.6 66.0 1,860.5 0 0 61.0 15 16 1,860.5 85.0 0 n 1,885.1 107.0 0 18 1,885.8 0 0 19 85.0 79.0 0 22 1,889.4 n 23 1,887.3 82.0 1,887.7 24 0 0 117.0 25 0 Ð 1,887.0 51.0 27 1,882.3 75.0 0 1,879.2 26.0 0 28 0 29 13.0 0 n 1,892.4 30 1,882.6 80.0 0 0 0 31 1,882.0 93.0 0 0 36 1,889.3 51.0 37 1,891.4 47.0 0 0 0 0 38 1,893.9 42.0 0 0 39 1,914.9 50.0 0 0 41 1,899.2 44.0 38.0 0 0 42 1,896.1 0 0 40.0 43 1,894.8 0 0 44 1,893.4 54.0 1,884.9 67.0 0 0 45 0 0 127.0 1,878.2 46 Õ 0 47 1,880.7 36.0 48 1,880.2 101.0 0 0 160.0 Û 0 491,881.1 Û 0 1,886.3 144.0 1,895.4 47.0 0 0 51 52 0 0 97.0 1,889.1 0 0 1,886.2 55 89.0 56 1,902.7 49.0 0 0 93.0 0 0 57 1,884.1

1,890.9

1,889.9

58

119.0

100.0

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0

0

61	1	1,885.4	50.0	0	0	
62	i	1,890.2	76.0	0	0	
	_		38.0	Ŏ	ŏ	
63	1	1,878.7				
64	. 1	1,876.5	44.0	0	0	
66	1	1,910.0	40.0	0	0	
67	1	1,921.5	38.0	0	0	
68	1	1,918.6	42.0	0	0	
69	i	1,879.5	50.0	0	0	
70	i	1,904.5	132.0	Ŏ	Ō,	
	-	1,004.0		ŏ	ŏ .	
71	1	1,894.5	87.0			
100	1	1,896.6	33.0	0	. 0 .	
101	ĺ	1,885.9	25.0	0	0	
102	1	1,876.7	37.0	0	0	
103	1	1,883.1	50.0	0	0	
104	ī	1,916.3	19.0	0	0	
105	i	1,903.9	17.0	Ŏ ·	Ö	
				ő	ŏ	
106	1	1,881.3	43.0			
107	1	1,880.1	32.0	0	0	
108	1	1,884.1	30.0	0	0	
109	1	1,884.6	20.0	0 .	0	
112	1	1,900.7	0.0	0	0	
113	1	1,878.5	29.0	0	0	
114	1	1,897.3	57.0	0 -	0	
117	1	1,907.5	59.0	0	0	
118	1	1,889.0	37.0	0	0	
119	1	1,889.1	64.0	0	0	
120	1	1,871.2	113.0	0	0	
121	1	1,862.6	109.0	0	0	
122	ī	1,950.0	89.0	0	0	
123	î	1,927.3	65.0	0	0	
		1,021.0		. 0	Ö	
124	. 1	1,879.6	68.0			
125	1	1,886.2	108.0	0	0	-
126	1	1,894.1	107.0	0	0 .	
127	1	1,874.9	54.0	0 :	0	
128	i	1,896.4	38.0	0 :	0	
129	i	1,896.0	8.0	0	0	
	- 1		7.0	ŏ÷	Ŏ	
130	-	1,886.4				. *
131	. 1 .	1,875.8	4.0	0 ·	0:.	
132	i	1,886.8	51.0	0 -	0:	
133	i	1,898.7	18.0	0	- 0⊹	
134	1	1,924.5	54.0	0 -	0	
135	Ī	1,915.7	58.0	0 .	0.	
136	i	1,944.8	71.0	Ō	Ŏ	44
				ŏ	Ö	
137	i	1,905.0	.118.0			
139	1	1,905.8	, 165.0	0.	0	10.00
140	1	1,899.4	31.0	0	0	100
141	1	1 000 0	99.0	0 ·	0	
142		1,890.2	00.0	Δ.		2.5
143	1			U	U	2 + 3 2 - 3
	i 1	1,883.9	103.0	0		
	1	1,883.9 1,888.7	103.0 110.0	0	0	
144	1	1,883.9 1,888.7 1,907.4	103.0 110.0 39.0	0	0	
144 145	1 1 1	1,883.9 1,888.7 1,907.4 1,909.3	103.0 110.0 39.0 6.0	0 0	0 0 0	
144 145 146	1 1 1 1	1,883.9 1,888.7 1,907.4 1,909.3 1,876.5	103.0 110.0 39.0 6.0 54.0	0 0 0	0 0 0 0	
144 145 146 147	1 1 1 1	1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9	103.0 110.0 39.0 6.0 54.0 98.0	0 0 0 0 0	0 0 0 0	
144 145 146 147 148	1 1 1 1 1	1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6	103.0 110.0 39.0 6.0 54.0 98.0 63.0	0 0 0 0 0 0	0 0 0 0 0 0	
144 145 146 147	1 1 1 1	1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0	0 0 0 0 0 0	0 0 0 0 0 0 0	
144 145 146 147 148 149	1 1 1 1	1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0	0 0 0 0 0 0	0 0 0 0 0 0	
144 145 146 147 148 149 150	1 1 1 1 1	1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0	0 0 0 0 0 0	0 0 0 0 0 0: 0:	
144 145 146 147 148 149 150	1 1 1 1 1 1	1,883.9 1,888.7 1,907.4 1,909.3 1,876.9 1,889.6 1,901.1 1,899.4 1,874.4	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0	0 0 0 0 0 0 0	0 0 0 0 0 0	
144 145 146 147 148 149 150 151	1 1 1 1 1 1 1	1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	
144 145 146 147 148 149 150 151 152	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 149 150 151 152 153	1 1 1 1 1 1 1	1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 149 150 151 152 153 154	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,867.6	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 149 150 151 152 153	1 1 1 1 1 1 1	1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 149 150 151 152 153 154 155		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 149 150 151 152 163 154 155 156		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,864.7 1,867.6 1,884.8 1,881.9	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0 66.0 22.0 40.0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 149 150 151 152 153 154 155 156 157		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8 1,881.9 1,880.3	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0 66.0 22.0 40.0 24.0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 149 150 151 152 153 154 155 156 157		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8 1,881.9 1,880.3 1,903.2	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0 66.0 22.0 40.0 24.0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 149 150 151 152 153 154 155 156 157 158		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,864.7 1,864.8 1,881.9 1,880.3 1,903.2 1,905.3	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0 66.0 22.0 40.0 24.0 24.0 19.0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 150 151 152 153 154 155 156 157 158		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8 1,881.9 1,880.3 1,903.2 1,905.3 1,891.8	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0 66.0 22.0 40.0 24.0 24.0 19.0 11.0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 150 151 152 153 154 155 156 157 158 160 161		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8 1,881.9 1,880.3 1,905.3 1,905.3 1,891.8 1,899.3	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0 66.0 22.0 40.9 24.0 24.0 19.0 11.0 38.0 7.0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 150 151 152 153 154 155 156 157 158 160 161		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8 1,881.9 1,880.3 1,903.2 1,905.3 1,891.8 1,899.3 1,919.8	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0 66.0 22.0 40.0 24.0 24.0 19.0 11.0 38.0 7.0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 150 151 152 153 154 155 156 157 158 160 161		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8 1,881.9 1,880.3 1,903.2 1,905.3 1,891.8 1,899.3 1,919.8	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0 66.0 22.0 40.9 24.0 24.0 19.0 11.0 38.0 7.0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 150 151 152 153 154 155 156 167 161 162 163 164		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8 1,881.9 1,880.3 1,903.2 1,905.3 1,891.8 1,899.3 1,919.8 1,962.5	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0 66.0 22.0 40.0 24.0 24.0 19.0 11.0 38.0 7.0 4.0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 150 151 152 153 154 155 166 161 162 163 164 165		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8 1,881.9 1,880.3 1,903.2 1,905.3 1,899.3 1,919.8 1,962.5 1,899.0	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 22.0 40.0 24.0 11.0 38.0 7.0 4.0 101.0 18.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 150 151 152 153 154 155 156 161 162 163 164 165 166		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8 1,881.9 1,880.3 1,903.2 1,905.3 1,891.8 1,899.3 1,919.8 1,962.5 1,899.0 1,917.8	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 22.0 40.0 24.0 11.0 38.0 7.0 4.0 101.0 18.0 22.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 150 151 152 153 154 155 156 161 162 163 164 165 166 169 170		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8 1,881.9 1,880.3 1,903.2 1,905.3 1,891.8 1,899.3 1,919.8 1,899.3 1,917.8 1,893.3	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 22.0 40.0 24.0 11.0 38.0 7.0 4.0 101.0 18.0 22.0 13.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 150 151 152 153 154 155 160 161 162 163 164 165 166 170 171		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,874.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8 1,881.9 1,880.3 1,903.2 1,905.3 1,891.8 1,899.3 1,919.8 1,962.5 1,899.0 1,917.8 1,893.3 1,909.7	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 71.0 66.0 22.0 40.0 24.0 19.0 11.0 38.0 7.0 4.0 101.0 18.0 22.0 13.0 19.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
144 145 146 147 148 150 151 152 153 154 155 156 161 162 163 164 165 166 169 170		1,883.9 1,888.7 1,907.4 1,909.3 1,876.5 1,878.9 1,889.6 1,901.1 1,899.4 1,865.9 1,862.7 1,864.7 1,867.6 1,884.8 1,881.9 1,880.3 1,903.2 1,905.3 1,891.8 1,899.3 1,919.8 1,899.3 1,917.8 1,893.3	103.0 110.0 39.0 6.0 54.0 98.0 63.0 28.0 118.0 76.0 66.0 22.0 40.0 24.0 11.0 38.0 7.0 4.0 101.0 18.0 22.0 13.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	

20	1	1,885.9	83.0	0	0
174	1	1,902.4	104.0	Ö	0
53	í	1,895.7	97.0	0	0
176	i	1,895.0	23.0	0	0
177	1	1,897.3	23.0	0	0
178	1	1,912.8	55.0	0	0
	i	1,917.5	25.0	Õ	0
179			80.0	Ŏ	Ŏ
181	1	1,881.0 1,891.9	13.0	ŏ	ō
182	1	1,899.2	12.0	Ŏ	Ŏ
183	1		66.0	ŏ	ŏ
185	1	1,902.8	66.0	. 0	0
186	1	1,885.4	76.0	Ŏ	Ŏ.
187	i	1,903.2		0	ő
188	į	1,931.7	8.0	0	Ö
189	i	1,921.8	29.0	0	0
300	1	1,903.6	47.0	0	0
301	į	1,951.4	76.0		0
402	1	1,955.5	0.0	0	
403	1	1,954.4	0.0	0	0 0
404	1	1,953.8	0.0	0	
405	1	1,952.5	0.0	0	0
406	1	1,951.8	0.0	0 :	0
407	1	1,951.3	0.0	0	0
408	1	1,950.7	0.0	0	0
409	i	1,950.0	0.0	0	0 -
410	1	1,947.8	0.0	0	0 :
411	1	1,947.4	0.0	0	0
412	1	1,946.9	0.0	0.	0
414	1	1,941.7	0.0	0	0
415	i	1,940.8	0.0	0	0
59	1	1,900.0	122.0	Û :	0
500	1	1,892.8	25.0	0	0.
501	1	1,886.6	76.0	0	0
502	1	1,885.6	80.0	0	0:
503	1	1,884.2	76.0	0.	0::
510	1	1,914.5	51.0	0 -	0
511	i	1,892.1	20.0	0 -	0
520	1	1,913.6	63.0	0	0
304	1	1,900.4	70.0	0::	0
172	1	1,886.0	51.0	0	0:
173	i	1,916.0	51.0	0:.	0
521	1	1,886.0	51.0	0	0
522	1	1,880.0	51.0	0	0
523	1	1,903.0	51.0	0	0
524	i	1,887.0	51.0	0	0
525	- 1	1,881.0	51.0	0 -	0
526	1	1,882.0	51.0	0	0
527	1	1,931.0	30.0	0	0
528	1	1,943.0	30.0	0	0
33	i	1,867.0	51.0	0 :	0
35	1	1,870.0	61.0	0 ,	0
40	i	1,920.0	40.0	0 :	0
54	1	1,886.0	51.0	0	0
540	1	1,930.0	406.0	0	0
541	1	1,980.0	558.0	. 0	0
				•	;

Booster Pump Da No. Type	ta Node A	Node B	Pipe No.	Pressure (m)
1 B	156	541	330 331	82.0
2 B	112	540		47.0

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* 656.1 1 min 1

0.71

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	Data No.	Node A No	de B D	iameter	Length	C Value
t The	,,,,,			(mm)	(1)	
	1	139	510	225.0	800.0	120.0
	2	139	304 140	44.0 150.0	374.0 162.0	130.0 120.0
	3 4	139 140	161	65.0	222.0	120.0
	5	51	140	150.0	228.0	120.0
	6	162	163	44.0	143.0	130.0
	7	51	162	150.0	20.0	120.0
	8	51 134	135 135	100.0 65.0	690.0 178.0	120.0 130.0
	9 12	134	164	44.0	84.0	130.0
	13	66	135	150.0	265.0	120.0
	14	50	66	100.0	530.0	120.0
	15	50	67	100.0	583.0	120.0 120.0
	16 20	67 21	188 54	100.0 150.0	165.0 59.0	120.0
	21	21	23	100.0	88.0	120.0
	22	23	24	150.0	55.0	120.0
	23	20	24	100.0	90.0	120.0
	24	20 25	21 174	150.0 100.0	66.0 569.0	120.0 120.0
	25 26	25 25	52	100.0	110.0	120.0
	27	52	53	100.0	176.0	120.0
	28	53	60	100.0	100.0	120.0
	29	18	60	100.0	134.0	120.0 120.0
	30 31	18 19	19 52	150.0 100.0	54.0 151.0	120.0
	32	19	55	100.0	133.0	120.0
	33	54	172	100.0	100.0	120.0
	34	9	18	225.0	315.0	120.0
	35	9	48	100.0	47.0 265.0	120.0 120.0
	36 37	1 48	48 49	225.0 100.0	201.0	120.0
	38	22	49	150.0	672.0	120.0
	40	49	148	100.0	536.0	120.0
	41	148	171	50.0	372.0	120.0
	42	69 46	148 69	100.0 150.0	325.0 90.0	120.0 120.0
	43 44	46 69	149	100.0	551.0	120.0
	45	1	49	100.0	264.0	120.0
	46	1	46	225.0	401.0	120.0
	. 48		64	100.0	268.0	120.0
	49 51	63 63	64 158	300.0 300.0	444.0 47.0	120.0 120.0
	52	158	166	50.0	358.0	120.0
	53	157	158	300.0	77.0	120.0
•	54		170	44.0	264.0	130.0
	55		157	300.0	300.0 100.0	120.0 120.0
	56 59		156 169	300.0 44.0	440.0	130.0
	61	2	203	350.0	704.0	120.0
	62	. 2	4	225.0	442.0	120.0
	63		· 5	225.0	65.0	120.0 130.0
-	64 65		61 6	65.0 150.0	972.0 221.0	120.0
	66		. 27	150.0	150.0	120.0
	67		37	100.0	216.0	120.0
	68		37	150.0	400.0	120.0
	69		38 38	100.0 150.0	563.0 30.0	120.0 120.0
	70 71		178	150.0	452.0	120.0
	72		181	150.0	1,106.0	120.0
	73		39	150.0	300.0	120.0
	74		173	44.0	320.0	130.0 120.0
	75 76		189 181	150.0 150.0	400.0 92.0	120.0
	80		179	150.0	125.0	120.0
	81	. 39	41	150.0	100.0	120.0
	82		208	65.0	104.0	
	83 84		103 102	150.0 44.0	350.0 120.0	
	86 86		102	44.0	120.0	
	87		101	37.0	312.0	130.0
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13.5 \$1.5 \$1.7 \$1.6 \$1.6

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88	42	43	100.0	257.0	120.0
89	42	43	100.0	257.0	120.0
90	43	44	150.0	268.0	120.0
91	44	177	100.0	391.0	120.0
92	44	176	100.0	391.0	120.0
93	176	177	100.0	90.0	120.0
99	29	112	65.0	251.0	130.0
100	109	511	100.0	400.0	120.0
101	108	109	100.0	120.0	120.0
102	108	183	44.0	228.0	130.0
103	107	108	100.0	200.0	120.0
104	107	182	44.0	253.0	130.0
105	28	107	100.0	40.0	120.0
106	28	113	150.0	66.0	120.0
107	113	114	65.0	265.0	130.0
108	114	117	65.0	500.0	130.0
109	117	118	44.0	318.0	130.0
111	118	119	75.0	248.0	120.0
113	28	106	150.0	250.0	120.0
			150.0	400.0	
114	103	106	150.0	400.0	120.0
115	105	106	44.0	250.0	130.0
116	104	105	44.0	300.0	130.0
117	103	104	44.0	239.0	130.0
118	30	526	100.0	210.0	120.0
120	155	500	140.0	175.0	130.0
121	150	185	75.0	300.0	120.0
122	31	150	150.0	300.0	120.0
125	132	133	44.0	363.0	130.0
126	31	132	150.0	616.0	120.0
127	31	64	225.0	167.0	120.0
128	31	70	150.0	662.0	120.0
129	70	144	100.0	284.0	120.0
130	144	145	44.0	121.0	130.0
131	45	144	100.0	368.0	120.0
132	45	47	150.0	162.0	120.0
134	9	57	100.0	25.0	120.0
135	57	58	100.0	120.0	120.0
136	58	60	100.0	262.0	120.0
137	56	58	100.0	330.0	120.0
140	58	143	100.0	168.0	120.0
141	142	143	50.0	264.0	120.0
142	57	142	100.0	202.0	120.0
143	141	142	100.0	99.0	120.0
145	11	12	100.0	388.0	120.0
146	12	150	150.0	360.0	120.0
147	12	151	150.0	163.0	120.0
148	13	151	150.0	35.0	120.0
		186			
149	151		140.0	450.0	130.0
151	154	155	100.0	132.0	120.0
160	153	154	100.0	165.0	120.0
161	14	153	150.0	236.0	120.0
162	13	14	150.0	475.0	120.0
163	13	146	150.0	35.0	120.0
164	146	147	150.0	137.0	
			_		120.0
165	11	147	150.0	313.0	120.0
168	14	152	100.0	66.0	120.0
170	33	152	100.0	150.0	120.0
176	68	136	44.0	726.0	130.0
177	136	137	44.0	512.0	130.0
178	137	187	140.0	277.0	130.0
181	71	122	225.0	400.0	120.0
182	71	124	225.0	400.0	120.0
183	15	124	225.0	441.0	120.0
184	15	16	150.0	177.0	120.0
185	16	121	100.0	286.0	120.0
186	120	121			
			75.0	1,210.0	120.0
187	16	125	100.0	850.0	120.0
188	123	125	100.0	764.0	120.0
189	123	124	44.0	120.0	130.0
190	122	123	140.0	160.0	130.0
191	122	209	225.0	120.0	120.0
193	125	126	100.0	396.0	120.0
194	126	128	65.0	668.0	130.0
195	126	127	65.0	1,047.0	130.0
196	128	129	65.0	90.0	130.0

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197	129	130	44.0	60.0	130.0
198	130	131	37.0	88.0	130.0
199	62	520	100.0	569.0	120.0
200	41	42	100.0	237.0	120.0
203	5	36	150.0	105.0	120.0
179	187	300	150.0	500.0	120.0
250	136	301	65.0	215.0	130.0
209	160	300	150.0	152.0 250.0	120.0 130.0
210 211	185 53	186 56	140.0 100.0	250.0 150.0	120.0
213	62	524	97.0	334.0	130.0
214	30	503	100.0	334.0	120.0
215	112	511	75.0	132.0	120.0
216	500	501	140.0	100.0	130.0
217	154	501	65.0	104.0	130.0
218	186	501	140.0	221.0	130.0
219	121	520	100.0	656.0	120.0
110	118	503	75.0	167.0	120.0
300	215	301	100.0	554.0	120.0
208	215	300	100.0	250.0	120.0
17	205	527	100.0	250.0	120.0
303	10	141	100.0	442.0	120.0
304	24	25	100.0 100.0	55.0 50.0	120.0 120.0
305 306	55 20	172 172	100.0	50.0 50.0	120.0
307	23	25	100.0	75.0	120.0
308	40	178	150.0	150.0	120.0
77	39	40	100.0	180.0	120.0
78.	40	189	100.0	60.0	120.0
79	100	101	44.0	450.0	130.0
309	41	42	150.0	150.0	120.0
310	119	521	65.0	350.0	130.0
311	521	522	65.0	350.0	130.0
312	120	522	65.0	350.0	130.0
313	33	35	100.0	150.0	120.0
301	11	523	150.0	120.0	120.0
314	59 500	523	100.0	180.0	120.0 120.0
315	502 525	524 600	75.0 75.0	150.0 450.0	120.0
316 317	523 524	600	97.0	450.0	130.0
318	525	600	97.0	450.0	130.0
319	525	526	75.0	210.0	120.0
321	527	528	65.0	480.0	130.0
322	134	528	65.0	200.0	130.0
11	165	601	65.0	75.0	130.0
324	188	527	65.0	50.0	130.0
325	122	123	140.0	160.0	130.0
326	123	125	97.0	764.0	130.0
327	56	59	140.0	352.0	130.0
328	1	49	158.0	264.0	130.0
329	206	527	150.0	215.0	120.0 120.0
330	156 112	541 540	100.0 97.0	931.0 434.0	130.0
331 212	22	54	150.0	275.0	120.0
401	402	602	200.0	234.0	120.0
402	402	403	200.0	101.0	120.0
403	403	404	200.0	61.0	120.0
404	404	405	200.0	122.0	120.0
405	405	406	200.0	65.0	120.0
406	406	407	200.0	42.0	
407	407	408	200.0	61.0	120.0
408	408	409	200.0	3.561.0	
409	409	410	200.0	215.0	
410	410	411	250.0	90.0	120.0
411	411	412	250.0	152.0 488.0	120.0 120.0
413	412	414 415	200.0 200.0	80.0	120.0
414	414 46	415	200.0	75.0	120.0
415	40	ゴブハ	200.0	1010	

	Net Work	Analysis		Distribut		В	
Node	Elevation	Demand	Dynamic	Dynamic Pressure	Static Pressure		Leakage
No.	of Pipe (MSL)	(cum/d)	Pressure (MSL)	rressure (m)	(n)		(cum/d)
1		197.6	1,925.9	44.2	109.3	0.0 0.0	(04) 4.)
2		113.4	1,925.6	40.5	105.9	0.0 0.0	
4		123.1	1,924.3	42.5	109.2	0.0 0.0	
5		64.8	1,924.1	42.8	109.7 107.3	0.0 0.0	
6		$123.1 \\ 215.5$	1,923.1 1,918.9	39.4 37.7	107.3	0.0 0.0	
10		40.5	1,917.2	13,8	87.6	0.0 0.0	
11		139.3	1,917.0	14.9	88.9	0.0 0.0	* .
12	1,880.5	106.9	1,917.7	37.2	110.5	0.0 0.0	
13		82.6	1,917.0	42.8	116.8	0.0 0.0	
14		106.9 98.8	1,916.5 1,958.7	50.9 98.2	125.4 130.5	0.0 0.0	
16 16		137.7	1,957.9	97.4	130.5	0.0 0.0	
18		173.3	1,918.7	33.6	105.9	0.0 0.0	
19		137.7	1,918.6	32.8	105.2	0.0	
22		128.0	1,920.4	31.0	101.6	0.0 0.0	4.00
2; 2		132.8 189.5	1,918.3 1,918.3	31.0 30.6	103.7 103.3	0.0 0.0 0.0 0.0	
25		82.6	1,918.2	31.2	104.0	0.0 0.0	* *.
2		121.5	1,922.6	40.3	108.7	0.0 0.0	
28	3 1,879.2	42.1	1,914.4	35.2	111.8	0.0 0.0	
29		21.1	1,893.8	1.4	98.6	0.0 0.0	1.1
3: 3		129.6 150.7	1,930,1 1,924,2	47.5 42.2	108,4 109,0	0.0 0.0 0.0 0.0	: .
3		82.6	1,923.6	34.3	101.7	0.0 0.0	4 4 4
3'		76.1	1,922.6	31.2	99.6	0.0 0.0	, *# · c
3		68.0	1,922.5	28.6	97.1		100
3		81.0	1,922.3	7.4	76.1	0.0	4. 1
4		71.3 61.6	1,922.2 1,922.1	23.0 26.0	91.8 94.9	0.0 0.0	
4		64.8	1,922.0	27.2	96.2	0.0 0.0	
	4 1,893.4	87.5	1,922.0	28.6	97.6	0.0 0.0	
	5 1,884.9	108.5	1,924.1	39.2	106.1	0.0 0.0	10 mm
	6 1,878.2 7 1,880.7	205.7 58.3	1,928.7 1,924.1	50.5 43.4	112.8 110.3	0.0 0.0 0.0 0.0	
	8 1,880.2	163.6	1,925.1	44.9	110.8	0.0 0.0	1 1
	9 1,881.1	259.2	1,925.1	44.0	109.9	0.0	1.7
	0 1,886.3	233.3	1,934.6	48.3	104.7	0.0	1.00
	1 1,895.4	76.1	1,919.2	23.8 29.0	95.6 101.9		F1.
	2 1,889.1 5 1,886.2	157.1 144.2	1,918.1 1,918.6	32.4	104.8		
	6 1,902.7	79.4	1,917.4	14.7		0.0 0.0	
	7 1,884.1	150.7	1,918.3	34.2	106.9	0.0	the same
	8 1,890.9	192.8 162.0	1,917.7	26.8 27.9	100.1 101.1	0.0 0.0	1. 11
	60 1,889.9 61 1,885.4	81.0	1,917.8 1,922.4	37.0	105.6	0.0 0.0	100
	2 1,890.2	123.1	1,946.2		100.8	0.0 0.0	65 (5)
	3 1,878.7	61.6	1,925.0	46.3	112.3	0.0 0.0	
	1,876.5	71.3	1,924.6		114.5		
	6 1,910.0 7 1,921.5	64.8 61.6	1,929.2 1,945.8		81.0 69.5	0.0 0.0	
	8 1,918.6	68.0	1,969.3		72.4		4.1
	i,879.5	81.0	1,928.6	49.1	111.5	0.0	
	0 1,904.5	213.8	1,924.0		86.5		
	71 1,894.5 00 1,896.6	140.9 53.5	1,959.3 1,920.0		96.5 94.4		1, 2, 3, 3, 4, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5,
	1,885.9		1,919.4		105.1		
	1,876.7		1,919.4		114.3	0.0 0.0	
	1,883.1	81.0	1,917.3		107.9	0.0 0.0	200
	1,916.3		1,915.8		74.7 87.1	0.0 0.0 0.0 0.0	The second second
	05 1,903.9 06 1,881.3		1,915.4 1,915.5		109.7	0.0 0.0 0.0 0.0	1.50
	07 1,880.1		1,913.5		110.9	0.0	1.50
10	08 1,884.1	48.6	1,909.6	25.4	106.9	0.0	
	09 1,884.6		1,907.5			0.0	
	12 1,900.7 13 1,878.5		1,893.8			0.0 0.0	
	13 1,876.3 14 1,897.3		1,914.2		93.7	0.0 0.0	
	17 1,907.5	95.6	1,914.6	7.1	83.5	0.0	
	18 1,889.0				102.0	0.0 0.0	
	19 1,889.1		1,925.8			0.0 0.0	
	20 1,871.2 21 1,862.6		1,929.5 1,950.9			0.0 0.0	
	22 1,950.0		1,959.7	9.7	41.0	0.0 0.0	
	23 1,927.3					0.0 0.0	
	24 1,879.6 25 1,886.2		1,959.0 1,957.8			$0.0 0.0 \\ 0.0 0.0$	
1.	ao 1,000,2	. 110,0	. 1,00(.0	, (1.1	0,101	0.0	

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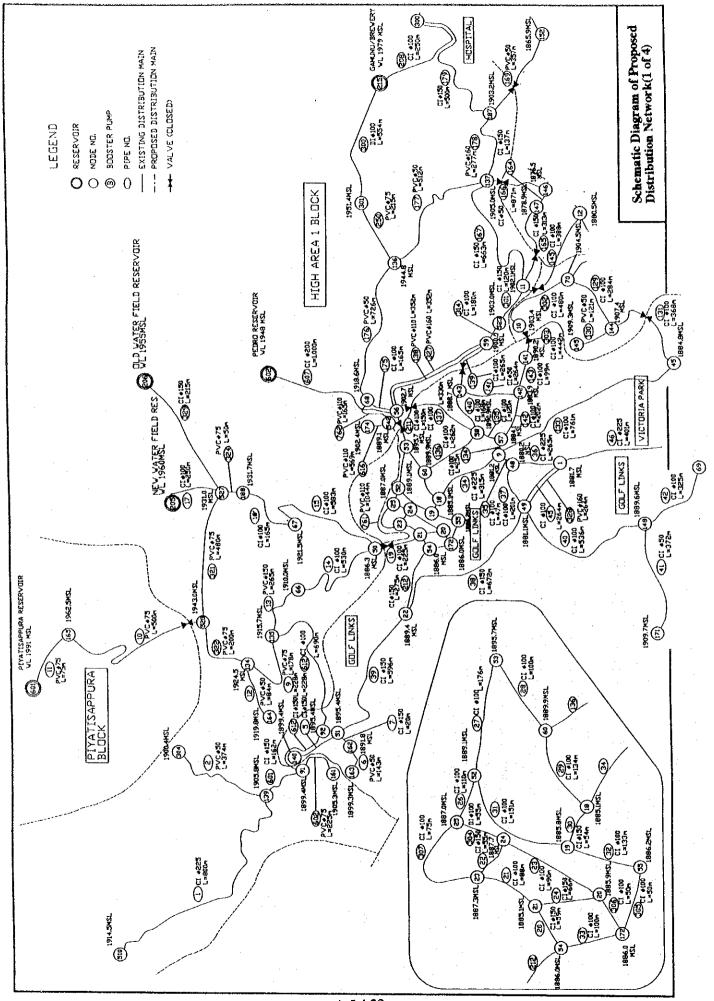
	Net Work	Analysis		Distributi	ion Main	В		
Node	Elevation	Demand	Dynamic	Dynamic	Static			Leakage
No.	of Pipe	(cun/d)	Pressure (MSL)	Pressure (m)	Pressure (m)			(cum/d)
126	(MSL) 1.894.1	(Cum/a) 173.3	1,956.2	62.1	96.9	0.0	0.0	(
127		87.5	1,953.8	78.9	116.1	0.0.	0.0	
128		61.6	1,954.5	58.1 58.5	94.6 95.0	0.0 0.0	$0.0 \\ 0.0$	
129 130		13,0 11.3	1,954.5 1,954.5	68.0	104.6	0.0	0.0	
131		6.5	1,954.4	78.6	115.2	0.0	0.0	
132	1,886.8	82.6	1,924.2	37.4	104.2	0.0 0.0	$0.0 \\ 0.0$	
133 134		29.2 87.5	1,923,4 1,932.2	24.7 7.7	$92.3 \\ 66.5$	0.0	0.0	
135		94.0	1,928.9	13.2	75.3	0.0	0.0	
136	1,944.8	115.0	1,976.1	31.3	46.2	0.0	$0.0 \\ 0.0$	
137		191.2 267.3	1,977.0 1,918.7	72.0 12.9	86.0 85.2	$0.0 \\ 0.0$	0.0	
139 140		50.2	1,918.9	19.5	91.6	0.0	0.0	
14		160.4	1,917.3	27.1	100.8	0.0	0.0	
142		166.9	1,917.4 1,917.4	33.5 28.7	107.1 102.3	0,0 0.0	$0.0 \\ 0.0$	
14: 14:		$\begin{array}{c} 178.2 \\ 63.2 \end{array}$	1,924.0	16.6	83.6	0.0	0.0	
149		9.7	1,924.0	14.7	81.7	0.0	0.0	
14		87.5	1,917.0	40.5 38.1	114.5 112.1	0.0 0.0	$0.0 \\ 0.0$	
14 ⁴ 14		158.8 102.1	1,917.0 1,926.7	37.1	101.4	0.0	0.0	
14		45,4	1,928.5	27.4	89.9	0.0	0.0	
15		191.2	1,920.4	21.0	91.6 116.6	0.0 0.0	$0.0 \\ 0.0$	
15 15		123.1 106.9	1,917.0 1,916.3	42.6 50.4	125.1	0.0	0.0	
15		115.0	1,916.5	53.8	128.3	0.0	0.0	
15	4 1,864.7	106.9	1,916.5	51.8	126.3	0.0 0.0	0.0	
15			1,916.6 1,925.4	49.0 40.6	123.4 106.2	0.0	0.0	
15 15			1,925.1	43.2	109.1	0.0	0.0	
15	8 1,880.3	38.9	1,925.1	44.8	110.7	0.0	$0.0 \\ 0.0$	÷
16			1,977.4 1,918.8	74.2 13.5	87.8 85.7	$0.0 \\ 0.0$	0.0	
16 16			1,919.1	27.3	99.2	0.0 .	0.0	
16		11.3	1,919.1	19.8	91.7	0.0	0.0	
16			1,932.2 1,990.5	12.4 28.0	71.2 28.5	0.0	$0.0 \\ 0.0$	
16 16			1,924.6	25.6	92.0	0.0	0.0	
î		35,6	1,924.2		73.2	0.0	0.0	
1			1,924.8 1,926.2		97.7 81.3	$0.0 \\ 0.0$	$0.0 \\ 0.0$	
17	71 1,909.7 21 1,885.1		1,918.7		105.9	0.0	0.0	
	20 1,885.9	134.5	1,918.6	32.7	105.1	0.0	0.0	
	74 1,902.4		1,917.6 1,917.7		88.6 95.3	0.0	$0.0 \\ 0.0$	
	53 1,895.7 76 1,895.0		1,921.9		96.0	0.0	0.0	
	77 1,897.3	37.3	1,921.9	24.6	93.7	0.0	0.0	
	78 1,912.8		1,921.8		78.2 73.5	0.0 0.0	0.0	
	79 1,917.8 81 1,881.0		1,922.4 1,920.0		110.0	0.0	0.0	
	82 1,891.9	21.1	1,913.2	21.3		0.0	0.0	
	83 1,899.2		1,909.3 1,916.8		91.8 88.2	0.0 0.0	$0.0 \\ 0.0$	
	85 1,902.8 86 1,885.4		1,916.8		105.6	0.0	0.0	
1	87 1,903.	2 123.1	1,977.1			0.0	0.0 0.0	
	88 1,931.° 89 1,921.°		1,949.5 1,920.8			0.0	0.0	
	89 1,921.8 80 1,903.8		1,977.4			0.0	0.0	
	01 1,951.	4 123.1	1,977.5			0.0	0.0 0.0	
	02 1,955.					0.0 0.0	0.0	
	03 1,954. 04 1,953.					0.0	0.0	
	05 1,952.	5 0.0	1,949.0		38.5	0.0	0.0	
	1,951.					0.0 0.0	0.0 0.0	
	107 1,951. 108 1,950.					0.0	0.0	
4	1,950.	0.0	1,945.0	~5.0	41.0	0.0	0.0	
	110 1,947.					0.0 0.0	0.0 0.0	
	111 1,947. 112 1,946.					0.0	0.0	
	114 1,941.	7 0.0	1,931.4	4 -10.3	49.3	0.0	0.0	
	115 1,940.					0.0 0.0	0.0 0.0	4
	59 1,900. 500 1,892.					0.0	0.0	
	501 1,886.		1,916.	6 30.0	104.4	0.0	0.0	
	502 1,885.		1,945.	5 59.1	105.4	0.0	0.0	

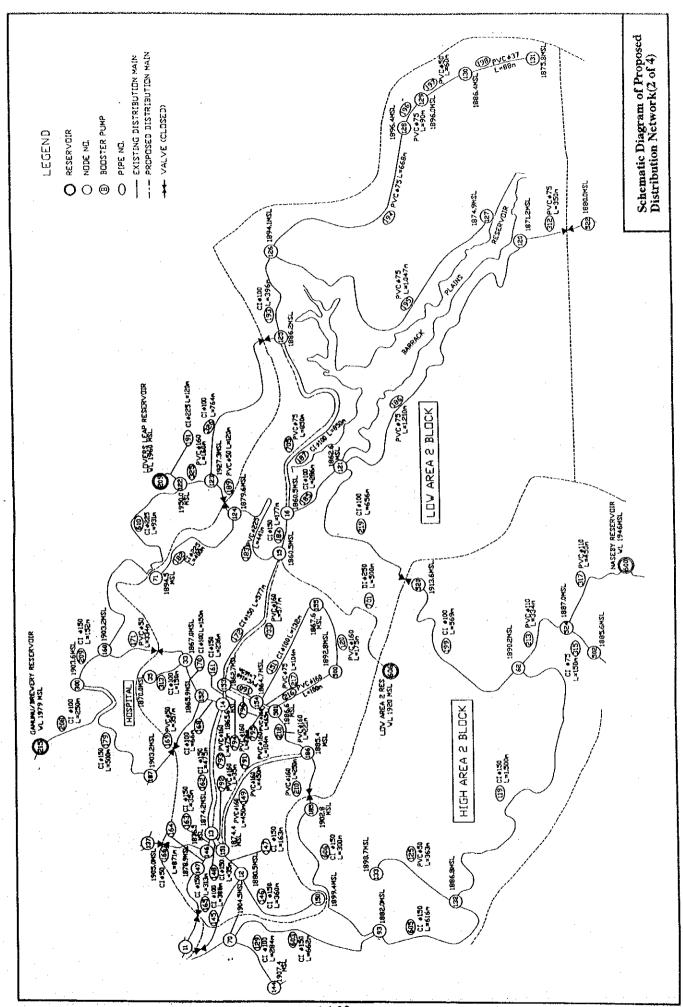
	Net Work	Analysis		Distribut	ion Main	В		•
Node	Elevation	Domand	Dynamic	Dynamic	Static			Leakage
No.	of Pipe	Demand	Pressure	Pressure	Pressure			istanage
	(MSL)	(cum/d)	(MSL)	(m)	(m)			(cum/d)
503	1,884.2	123.1	1,928,2	44.0	106.8	0.0	0.0	
510	1,914.5	82,6	1,918.7	4,2	76.5	0.0	0.0	
511	1,892.1	32.4	1,901,4	9.3	98.9	0.0	0.0	
520	1,913.6	102.1	1,947.7	34.1	77.4	0.0	0.0	
304	1,900.4	113.4	1,909.7	9.3	90,6	0.0	0.0	
172	1,886.0	82.6	1,918.6	32.6	105.0	0.0	0.0	
173	1,916.0	82.6	1,918.0	2,0	75.0	0.0	0.0	
521	1,886.0	82.6	1,925.8	39.8	105.0	0.0	0.0	
522	1,880.0	82.6	1,926.7	46.7	111.0	0.0	0.0	
523	1,903.0	82,6	1,917.0	14.0	88.0	0.0	0.0	
524	1,887.0	82,6	1,945.9	58.9	104.0	0.0	0.0	
525	1,881.0	82,6	1,942.6	61.6	110.0	0.0	0.0	•
526	1,882.0	82.6	1,932.1	50.1	109.0	0.0	0.0	
527	1,931.0	48,6	1,957.5	26.5	60.0	0.0	0.0	
528	1,943.0	48.6	1,938.5	-4.5	48.0	0.0	0.0	
33	1,867.0	82.6	1,916.1	49.1	124.0	0.0	0.0	
35	1,870.0	98.8	1,916.1	46.1	121.0	0.0	0.0	
40	1,920.0	64.8	1,921.7	1.7	71.0	0.0	0.0	
54	1,886.0	82.6	1,918.8	32.8	105.0	0.0	0.0	
540	1,930.0	657.7	1,935.0	5.0	61.0	0.0	0.0	
541	1,980.0	904.0	1,985.0	5.0	11.0	0.0	0.0	

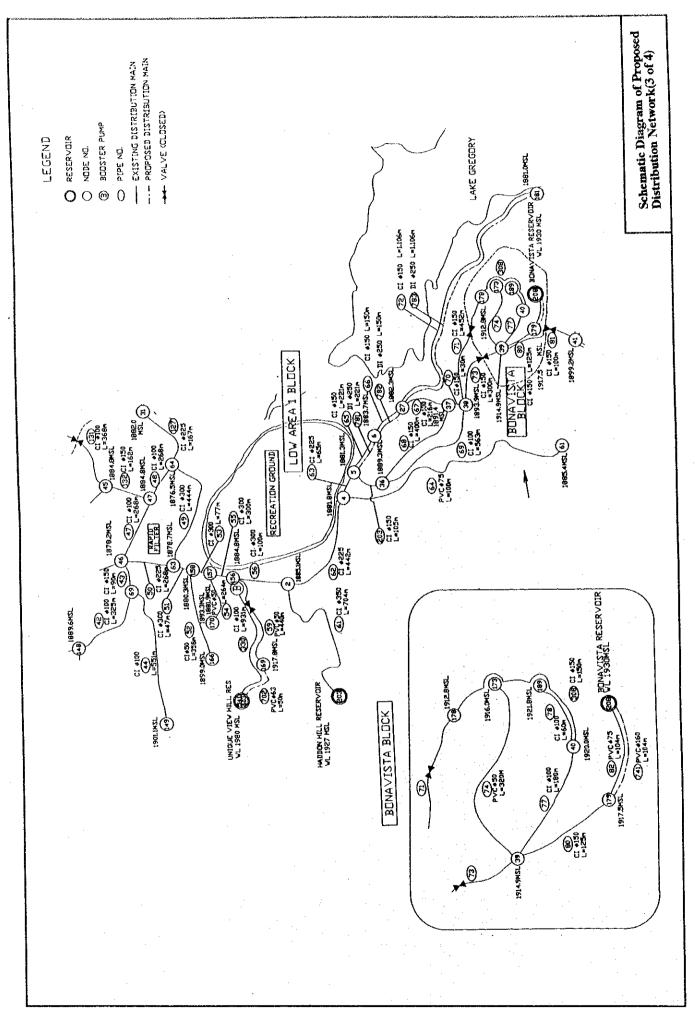
	Net	Work	Anal	vsis		Distrib	ution Main			
Pipe No.	Node		•		Diameter	C	Flow	Velocity	Pressure Gradient	loss
				(n)	(mm)		(cum/d)	(m/s)	(0/00)	(m)
1		139	510	800.00	225.00	120.00	82.00	0.00	0.00	0.00
2		139	304	374.00	44.00	130.00	113.00	0.90	24.20	9.00
3		139	140	162.00	150.00	120,00	-463.00	-0.30	-1.00	-0.20
4 5		140 51	161 140	222.00 228.00	65.00 150.00	120,00 120,00	17.00 531.00	0.10 0.30	$\substack{\textbf{0.10}\\\textbf{1.30}}$	$0.00 \\ 0.30$
6		162	163	143.00	44.00	130.00	11.00	0.10	0.30	0.10
7		51	162	20.00	150.00	120.00	72.00	0.10	0.00	0.00
ė	,	51	135	690.00	100.00	120.00	-680.00	-1.00	-14.20	-9,80
9		134	135	178.00	65.00	130.00	270.00	0.90	18.10	3.20
12		134	164	84.00	44.00	130.00	6.00	0.10	0.10	0.00
13		66	135	265.00	150.00	120.00	503.00	0.30	1.10	0.30
14		50	66	530.00	100.00	120.00	568.00	0.80	10,20	5.40
15		50	67	583.00	100.00	120.00	-801.00	-1.20	-19.20	-11.20
16 20		67 21	188 54	165,00 59,00	100.00 150.00	120,00 120,00	-863,00 -887,00	-1.30 -0.60	-22.10 -3.20	-3.60 -0.20
21		21	23	88.00	100.00	120.00	354.00	0.50	4.30	0.40
22		23	24	55.00	150.00	120.00	55.00	0.00	0.00	0,00
23		20	24	90.00	100.00	120.00	328.00	0.50	3.70	0.30
24		20	21	66.00	150,00	120.00	-375.00	-0.30	-0.70	0.00
25		25	174	569.00	100.00	120.00	168.00	0.30	1.10	0.60
26		25	52	110.00	100.00	120.00	110.00	0.20	0.50	0.10
27		52	53	176.00	100.00	120,00	260.00	0.40	2.40	0.40
28 29		53 18	60 60	100.00 134.00	100.00 100.00	120.00 120.00	-159.00 448.00	$-0.20 \\ 0.70$	-1.00 6.60	-0.10 0.90
30		18	19	54.00	150.00	120.00	512.00	0.30	1.20	0.10
31		19	52	151.00	100.00	120.00	307.00	0.50	3.30	0.50
32		19	55	133,00	100.00	120.00	67.00	0.10	0.20	0.00
33		54	172	100,00	100.00	120,00	247.00	0.40	2.20	0.20
34		9	18	315.00	225,00	120,00	1,133.00	0.30	0.70	0.20
35		9	48	47.00	100.00	120,00	-2,265.00	-3.30	-131.70	-6,20
36		1	48	265.00	225.00	120.00	2,420.00	$0.70 \\ 0.00$	2.90 0.00	$0.80 \\ 0.00$
37 38		48 22	49 49	201.00 672.00	100.00 150.00	120.00 120.00	-8.00 -1,345.00	-0.90	-7.00	-4.70
4(49	148	536.00	100.00	120.00	-289.00	-0.40	-2,90	-1.60
43		148	171	372.00	50,00	120.00	30.00	0.20	1,30	0,50
42		69	148	325,00	100.00	120,00	422.00	0.60	5,90	1,90
4.		46	69	90,00	150,00	120.00	549,00	0.40	1.30	0.10
44		69	149	551.00	100.00	120.00	45.00	0.10	0.10	0.10
48 48		1 1	49 46	264.00 401.00	100.00 225.00	120.00 120.00	287.00 -3,941.00	0.40 -1.10	2.90 -7.10	0,80 -2,80
48		47	64	268.00	100.00	120.00	-232.00	-0.30	-1.90	-0.50
49		63	64	444.00	300.00	120.00		0.40	0.80	0.40
51		63	158	47.00	300.00	120.00	-2,712.00	-0.40	-0.90	0.00
52		158	166	358.00	50,00	120.00	29.00	0.20	1.20	0.40
5		157	158	77.00	300.00	120.00	2,780.00	0.50	0.90	0.10
54		157	170	264.00	44.00	130.00	21.00	0.20	1.10	0.30
58 56		156 2	157 156	300.00 100.00	300.00 300.00	120.00 120.00	2,840.00 3,844.00	0.50 0.60	$\frac{0.90}{1.70}$	$0.30 \\ 0.20$
59		156	169	440.00	44.00	130.00	35.00	0.30	2.80	1.30
6		2	203	704.00	350.00	120,00	-6,401.00	-0.80	-2,00	-1.40
62		2	4	442.00	225.00	120.00	2,443.00	0.70	2,90	1.30
6	}	4	5	65.00	225,00	120.00	2,239.00	0.70	2.50	0.20
6		4	61	972.00	65.00	130.00	81.00	0,30	1.90	1.90
6		5	6	221.00	150.00	120.00	1,060.00	0.70	4.50	1.00
61 61		6 27	27 37	150,00 216.00	150.00 100.00	120.00 120.00	937.00 67.00	0.60 0.10	3.60 0.20	0.50 0.00
- 61		36	37	400.00	150.00	120.00	795.00	0.50	2.60	1.10
6		36	38	563.00	100.00	120.00	236,00	0.30	2.00	1.10
70		37	38	30.00	150.00	120.00	786,00	0.50	2.60	0.10
7.		38	178	452,00	150.00	120.00	565.00	0.40	1.40	0.60
7		27	181	1,106.00	150.00	120.00	748.00	0.50	2.40	2.60
. 7		38	39	300.00	150.00	120.00	389.00	0.30	0.70	0.20
7.		39	173	320.00	44.00	130.00	82.00	0.60	13.40 -1.90	4.30
7: 7:		181 102	189 181	400.00 92.00	150.00 150.00	120.00 120.00	-667.00 -1,286.00	-0.40 -0.80	-6.40	-0.80 -0.60
8		39	179	125.00	150.00	120.00	-533.00	-0.30	-1.30	-0.20
8		39	41	100.00	150.00	120.00	455.00	0.30	0.90	0.10
8.	2	179	208	104.00	65.00	130.00	-573.00	-2.00	-72.80	-7.60
. 8	3	102	103	350,00	150,00	120.00	1,229.00	0.80	5.90	2.10
8		101	102	120.00	44.00	130.00	2.00	0.00	0.00	0.00
. 8		41	100	120.00	44.00	130.00	96.00	0.70	17.90	2.10
. 8 8		100 42	101 43	312.00 257.00	37,00 100,00	130,00 120,00	18.00 113.00	0.20 0.20	2.00 0.50	$\begin{array}{c} 0.60 \\ 0.10 \end{array}$
8		42 42	43 43	257.00	100.00	120.00		0.20	0.50	0.10
9		43	44	268.00	150.00	120.00	162.00	0.10	0.10	0.00
9	i	44	177	391,00	100.00	120.00	37,00	0.10	0.10	0.00
9	Z .	44	176	391.00	100.00	120.00	37.00	0.10	0.10	0.00

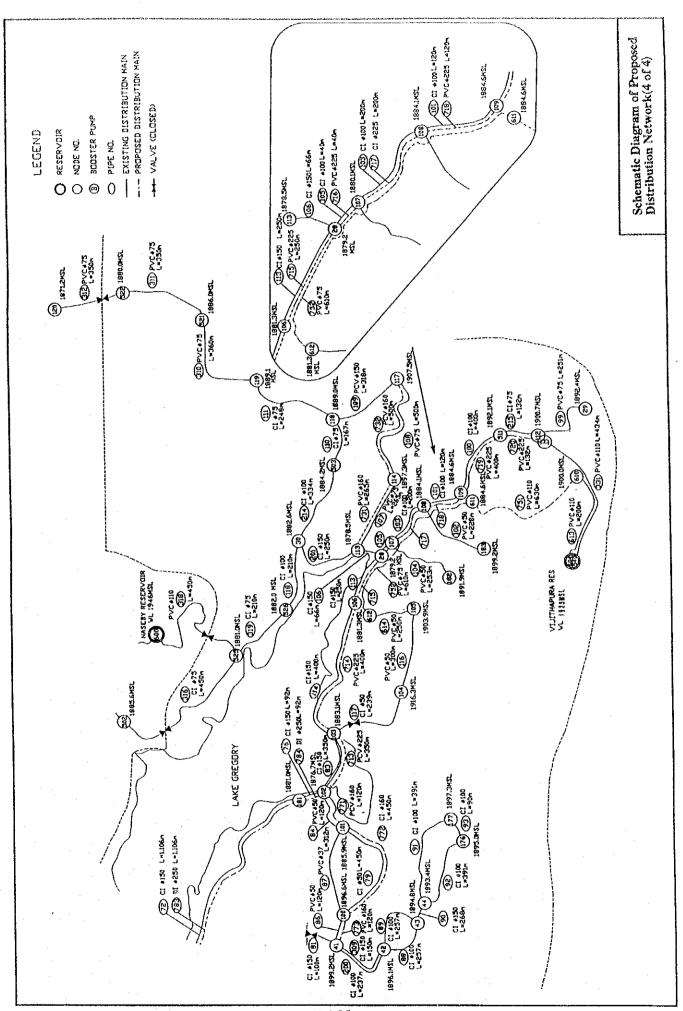
	Net.	Work	Analy	sis	[)istribu	tion Main			
Pipe	Node				Diameter	C		Velocity	Pressure Gradient	loss
No.				(m)	(mm)		(cum/d)	(m/s)	(0/00)	(m)
93		176	177	90.00		120.00	0.00 -21.00	0.00 -0.10	0,00 -0.20	0.00 0.00
99 1 0 0		29 109	112 511	251,00 400,00	65.00 100.00	130.00 120.00	711.00	1.10	15.40	6.20
101		108	109	120.00	100.00	120.00	743.00	1.10	16.70	2.00
102	2	108	183	228.00	44.00 100.00	130.00 120.00	19.00 811.00	0.10 1.20	0.90 19.70	0.20 3.90
100 104		107 107	108 182	200,00 253,00	44.00	130.00	21.00	0,20	1.10	0.30
10	5	28	107	40.00	100.00	120.00	884.00	1.30	23.10 0.10	0.90 0.00
100		28	113 114	66.00 265.00	150.00 65.00	120.00 130.00	93,00 46,00	0.10 0.20	0.70	0.20
10° 108		113 114	117	500.00	65.00	130.00	-45.00	-0.20	-0.70	-0.30
10	9	117	118	318.00	44.00	130.00	-141.00 93.00	-1.10 0.20	-36.40 1.50	-11.60 0.40
11 11		118 28	119 106	248.00 250.00	75.00 150.00	120.00 120.00	-1,020.00	-0.70	-4.20	-1.00
11		103	106	400.00	150.00	120.00	1,093.00	0,70	4.70	1.90
11	5	105	106	250.00	44.00 44.00	130.00 130.00	-3.00 24.00	0.00 0.20	0.00 1.40	$0.00 \\ 0.40$
11 11		104 103	105 104	300.00 239.00	44.00	130.00	54.00	0.40	6.30	1.50
11	8	30	526	210.00	100.00	120.00	-547.00	-0.80	-9.50 -0.10	-2.00 0.00
12		155	500 185	175.00 300.00	140.00 75.00	130.00 120.00	-142.00 288.00	-0.10 0.80	11.70	3,50
12 12		150 31	150	300.00	150,00	120.00	1,863.00	1.20	12.70	3.80
12	25	132	133	363.00	44.00	130.00	29.00 111.00	0.20 0.10	2.00° 0.10	0.70
12 12		31 31	132 64	616.00 167.00	150.00 225.00	120.00 120.00	-2,346.00	-0.70	-2.70	-0.50
12		31	70	662.00	150.00	120.00	221,00	0.10	0.30	0.20
12	29	70	144	284.00	100.00 44.00	120.00 130.00	7.00 9.00	0.00 0.10	0.00 0.30	0.00 0.00
13 13	30 31	144 45	145 144	121,00 368.09	100.00	120.00	65.00	0.10	0.20	0.10
13	32	45	47	162,00	150.00	120.00	-174.00	-0.10	-0.20 24.60	0.00 0.60
	34 25	9 57	57 58	25,00 120.00	100.00 100.00	120.00 120.00	916.00 404.00	1.40 0.60	5.40	0.70
	35 36	58	60	262.00	100.00	120.00	-126.00	-0.20	-0.60	-0.20
1	37	56	58	330.00	100.00	120.00	-153.00	-0.20 0.30	-0.90 1.30	$-0.30 \\ 0.20$
	40 41	58 142	143 143	168.00 264.00	100.00 50.00	120.00 120.00	185.00 -6.00	0.00	-0.10	0.00
	42	57	142	202.00	100.00	120.00	360.00	0.50	4.40	0.90
	43	141	142	99.00	100.00 100.00	120.00 120.00	~200.00 -230.00	-0.30 -0.30	-1.50 -1. 9 0	-0.10 -0.70
	45 46	11 12	12 150	388.00 360.00	150.00	120.00	-1,384.00	-0.90	-7.30	~2.60
1	47	12	151	163.00	150.00	120,00	1,046.00	0.70	4.40 -1.70	0.70 -0.10
	48	13 151	151 186	35,00 450,00	150.00 140.00	120.00 130.00	-635.00 288.00		0.50	0.20
	49 51	154	155	132.00	100.00	120.00	-106.00	-0.20	-0.50	-0.10
1	60	153	154	165.00	100.00	120.00	~56.00 58.00		-0.10 0.00	0.00 0.00
	161 162	14 13	153 14	236.00 475.00	150.00 150.00	120,00 120.00	454.00			0.40
1	163	13	146	35.00	150.00	120.00	99.00		0.10	$0.00 \\ 0.00$
	164	146	147 147	137.00 313.00	150.00 150.00		11.00 147.00			0.00
	165 168	11 14	152	66.00	100.00		288.00	0.40	2.90	0.20
	170	33	152	150.00	100.00		-181.00 -68.00			-0.20 -6.80
	176 177	68 136	136 137	726.00 512.00	44.00 44.00		-27.00			-0.90
	178	137	187	277.00	140.00	130.00	-218.00			-0.10 -0.40
	181	71 71	122 124	400.00 400.00	225.00 225.00		-1,368.00 1,227.00			0.30
	182 183	15	124	441.00	225.00		-1,166.00	-0.30	-0.70	-0.30
	184	15	16	177.00						0.80 7.00
	185 186	16 120	121 121	286.00 1,210.00					-17.60	-21.30
	187	16	125	850.00	100.00	120.00	17.0			0.00 1.80
	188	123	125 124	764.00 120.00						0.60
	189 190	123 122	123	160.00	and the second second		332.0	0 0.30	0,60	0.10
	191	122	209	120.00						-0.30 1.70
	193 194	125 126	126 128	396.00 668.00					2.50	1.60
	195	126	127	1,047.00	65.0	0 130.00	87.0	0 0.3	2.20	2.30
	196	128	129	90.00						0.00 0.10
	197 198	129 130	130 131	60,00 88,00		0 130.00	6.0	0 0.1	0.30	0.00
	199	62	520	569.00	100.0	0 120,00				-1,50 0.00
	200 203	41 5	42 36	237.00 105.00						0.50
	179	187	300	500.00	150.0	0 120.00	-341.0	0 -0.2	0 -0.60	-0.30
	250	136		215.00	65.0	0 130.00) -155.0	0 -0.5	0 -6.50	-1.40

•		Net Wo	rk Anal	ysis		Distribu	tion Main		_	
	Pipe No.	Node A		Length		C		Velocity	Pressure Gradient	Loss
				(n)	(mm)		(cum/d)	(m/s)	(0/00)	(m)
	209	160	300	152,00	150.00	120.00	-30.00	0.00	0.00 0.20	0.00 0.10
	210	185	186	250.00	140.00	130.00	181.00 262.00	0.10 0.40	2.40	0.40
	211	53	56	150.00 334.00	100.00 97.00	120.00 130.00	152.00	0.20	0.90	0.30
	213 214	62 30	524 503	334.00	100.00	120.00	417.00	0.60	5.80	1.90
	214	112	511	132.00	75.00	120.00	-678.00	-1,80	-57.40	-7.60
	216	500	501	100,00	140.00	130.00	-182.00	-0.10	-0.20	0.00
	217	154		104.00	65.00	130.00	-56.00	-0.20	-1.00	-0.10
	218	186		221.00	140.00	130.00	362.00	0.30	0.70	0.20
	219	121		656.00	100.00	120.00	377,00	0.60	4.80	3.10
	110	118		167.00	75.00	120.00	-294.00	-0.80 0.40	-12.20 2.70	-2.00 1.50
	300	215		554.00	100.00	120.00	278.00 448.00	0.70	6,60	1.60
	208			250,00 250,00	100,00 100,00	120.00	567.00	0.80	10.10	2.50
	17 303			442.00	100.00	120.00	-40,00	-0.10	-0.10	0.00
	303 304			55,00	100.00	120,00	195.00	0.30	1.40	0.10
	305			50,00	100,00	120.00	-77.00	-0.10	-0.30	0.00
	306			50.00	100.00	120.00	-87.00	-0.10	-0.30	0.00
	307			75.00	100,00	120,00	166.00	0.20	1.00	0.10
	308			150.00	150.00	120.00	-476.00	-0.30	-1.00	-0.10
	77			180.00	100,00	120.00	303.00	0.50	3.20	$0.60 \\ 0.90$
	- 78			60.00	100.00	120.00	714.00 24.00	1.10 0.20	15.60 1.40	0.60
	79			450.00	44.00 150.00	130.00 120.00	227.00	0.10	0.30	0.00
	309			150.00 350.00	65,00	130.00	-10.00	0.00	0.00	0.00
	310 311			350.00	65.00	130.00	-93.00	~0,30	-2.50	-0.90
	312				65.00	130.00	175.00	0.60	8.10	2.90
	313			150.00		120.00	98.00	0.10	0.40	0.10
	301			120.00	150.00	120.00	-56.00	0.00	0.00	0.00
	314			180.00	100.00	120.00	139,00	0.20	0.80	0.10
	318	502		150.00	75.00	120.00	-129.00	-0.30	-2.70	-0.40
	316			450.00	75.00	120.00	-227.00	-0.60 -0.10	-7.60 -0.20	-3.40 -0.10
	317				97.00	130.00 130.00	-60.00 -484.00	-0.10	-7.60	-3.40
	318				75.00	120.00	629.00	1.60		10.50
	319 321				65.00	130.00	413,00	1.40	39.60	19.00
	322				65.00	130.00	-364.00	-1 30	-31 40	-6.30
	1				65,00	130.00	-163.00	-0.60		-0.50
	324				65.00	130.00	-876.00	-3.10	-159.40	-8.00
	328	5 12:	2 123	160.00	140.00		332.00	0.30	0.60	0.10
	320	6 12			97.00		255.00		2,30 0.70	1.80 0.20
	32'	7 5	6 59		140.00		336.00	0.30	2.90	0.80
	32	8			158.00 150.00		1,036.00 770.00	0.50	2.50	0.50
	329				100.00		004.00	1.30	24.00	22.40
	33 33				97.00		657.00	1.00	13,30	5.80
	21				150.00	120.00	1,217.00	0.80	5.80	1.60
	40				200,00	120.00	-4,696.00	-1.70		-4.10
	40.				200.00	120,00	4,696.00	1.70	17.40	1.80
	40	3 40			200.00		4,696.00	1.70	17.40	1.10 2.10
	40				200.00		4,696.00	1.70	17.40 17.40	1.10
	40				200.00		4,696.00 4,696.00	1.70 1.70		0.70
	. 40				200,00 200,00		4,696.00	1.70	17.40	1.10
	40			61.00	200.00		4,696.00	1.70	17.40	1.10
	40 40				200.00		4,696.00	1.70	17.40	3.70
	41						4,696.00	1.10		0.50
	41				250.00	120.00	4,696.00	1.10		0.90
	41	3 41	.2 414				4,696.00			8.50
	41						4,696.00	1.70 -1.70		1.40 -1.30
	41	.5 4	6 418	5 75.00	200.00	120.00	-4,696.00	~1,10		1,00









A-5,4.35

Net Work Analysis

Distribution Main

File Name

Nuwara201Year1995(2)

Dry

Season Network Type

Proposed

Demand

Reserver

Year 1995 Day Mean Water Level Fix Discharge Fix

Except for Follows No.205,206,215,209

Magnification of Demand

0.739

Re	servoi	r Data			
N-	ode		HWL	LWL	Reservoir
			(MSL)	(MSL)	
	203	1	1,927.0	1,927.0	Haddon Hill
,	208	1	1,930.0	1,930.0	Bonavista
	600	1	1,946.0	1,946.0	Naseby
	601	1	1,991.0	1,991.0	Piyatisappura
	602	1	1,948.0	1,948.0	New Pedro Reserver
	603	1	1,980.0	1,980.0	Unique View
	604	1	1,925.0	1,925.0	Vijithapura
	606	i	1,920.0	1,920.0	New Loc Area 2

600	1	1,920.0	1,920.0	New	roe	Area	4		
Made Dete									
Node Data Node		Ground Elev	Demand						
ноце		(MSL)	(cum/d)						
1	1	1,881.7	122.0			0			0
2	1	1,885.1	70.0			Ŏ			0
. 4	1	1,881.8	76.0			ŏ			Ö
5	i	1,881.3	40.0			Ö			Ö
. 6	i	1,883.7	76.0			Ö			Õ
9	i	1,881.2	133.0			Ö			ŏ
10	î	1,903.4	25.0			Ŏ			Ö
11	1	1,902.1	86.0	•		Ö			0
12	1	1,880.5	66.0			Ŏ			Ö
13	ī	1,874.2	51.0			Ō.			0
14	i	1,865.6	66.0			0			0
15	1	1,860.5	61.0			0			0
16	1	1,860.5	85.0			0 -			0
18	ï	1,885.1	107.0			0			0
19	1	1,885.8	85.0			0			0
22	i	1,889.4	79.0			0			0
23	1	1,887.3	82.0			0			0
24	1	1,887.7	117.0			0			0
25	1	1,887.0	51.0			0 .			0
27	1	1,882.3	75.0			0 .			0
28	1	1,879.2	26.0			0			0
29	1	1,892.4	13.0			0			0
30	1	1,882.6	80.0			0			0
31	1	1,882.0	93.0			0			0
36	1	1,889.3	51.0			0			0
37	1	1,891.4	47.0			0			0
38	1	1,893.9	42.0			0			0
39	i	1,914.9	50.0			0			0
41	1	1,899.2	44.0			0			0
42	1	1,896.1	38.0			0			0
43	1	1,894.8	40.0			0			0
44	1	1,893.4	54.0			0			0
45	1	1,884.9	67.0			0			0
46	1	1,878.2	127.0			0			0
47	1	1,880.7	36.0			0			0
48	1	1,880.2	101.0			0			0
49	1	1,881.1	160.0			0			0
50	1	1,886.3	144.0			0			0
51	1	1,895.4	47.0			0			0
52	1	1,889.1	97.0			. 0			.0
55 56	1	1,886.2	89.0			0	-	٠.	0
56	1	1,902.7	49.0			0			0
57	1	1,884.1	93.0			0			0
58	1	1,890.9	119.0			0		1	0
60	1	1,889.9	100.0			0 0			0
61	1	1,885.4	50.0			· U			v

62	1	1,890.2	76.0	0	0
63	1	1,878.7	38.0	Ö	0
64	1	1,876.5	44.0	0	0
66	i	1,910.0	40.0	0	0
67	í	1,921.5	38.0	0	0
	i		42.0	Õ	0
68		1,918.6			
69	1	1,879.5	50.0	0	0
70	1	1,904.5	132.0	0	0
71	i	1,894.5	87.0	0	0
					ŏ
100	1	1,896.6	33.0	0	
101	i	1,885.9	25.0	0	0
102	1	1,876.7	37.0	0	0
103	Ī	1,883.1	50.0	0	0
					Ö
104	1	1,916.3	19.0	0	
105	1	1,903.9	17.0	0	0
106	i	1,881.3	43.0	0	0
107	i	1,880.1	32.0	0	0
			20.0	Ŏ	ŏ
108	· 1	1,884.1	30.0		
109	1	1,884.6	20.0	0	0
112	1	1,900.7	0.0	0	0
113	i	1,878.5	29.0	0	0
114	1	1,897.3	57.0	0	0
117	1	1,907.5	59.0	0	0
118	1	1,889.0	37.0	0	0
119	i	1,889.1	64.0	0	0
120	i	1,871.2	113.0	0	0
121	1	1,862.6	109.0	0	0
122	1	1,950.0	89.0	0	0
			65.0	0	0
123	1	1,927.3			
124	1	1,879.6	68.0	0	0
125	1	1,886.2	108.0	0	0
126	1	1,894.1	107.0	. 0	0
		1,874.9		0	Õ
127	1		54.0		
128	1	1,896.4	38.0	0	0
129	1	1,896.0	8.0	0	0
130	1	1,886.4	7.0	0	0
				Ö	0
131	1	1,875.8	4.0		
132	1	1,886.8	51.0	0	0
133	1	1,898.7	18.0	0	0
134	i	1,924.5	54.0	0	0
135	1	1,915.7	58.0	0	0
136	1	1,944.8	71.0	0	. 0
137	1	1,905.0	118.0	0	0
139	i	1,905.8	165.0	0	0
140	i	1,899.4	31.0	0	0
141	1	1,890.2	99.0	0	0
142	· 1	1,883.9	103.0	0	0
143	î	1,888.7	110.0	Ò	0
		1,000.1			
144	1	1,907.4	39.0	0	.0
145	1	1,909.3	6.0	0	0
146	1	1,876.5	54.0	0	0
147	ī	1,878.9	98.0	0	. 0
				ŏ	0
148	1	1,889.6	63.0		
149	1	1,901.1	28.0	0	0
150	1	1,899.4	118.0	0	0
151	ĩ	1,874.4	76.0	0	0
152	1	1,865.9	66.0	0	0
153	1	1,862.7	71.0	0	0
154	i	1,864.7	66.0	0	0
155	î	1,867.6	22.0	0	0
				Ö	Õ
156	1	1,884.8	40.0		
157	i	1,881.9	24.0	0	0
158	1	1,880.3	24.0	0	0
160	1	1,903.2	19.0	0	0
					ő
161	. 1	1,905.3	11.0	0	
162	1	1,891.8	38.0	0	0
163	1	1,899.3	7.0	0	0
	1	1,919.8	4.0	Ö	0
164					
165	1	1,962.5	101.0	0	0
166	1	1,899.0	18.0	0	0
169	ĺ	1,917.8	22.0	0	0
170	i	1,893.3	13.0	0	0
				_	Ö
171	1	1,909.7	19.0	0	
21	1	1,885.1	97.0	0	0
20	1	1,885.9	83.0	0	0
		•			

174	1	1,902.4	104.0	0	0
53	1	1,895.7	97.0	0	0
176	1	1,895.0	23.0	0	0
177	1	1,897.3	23.0	0	0
178	i	1,912.8	55.0	0	0
179	i	1,917.5	25.0	0	0
181	î	1,881.0	80.0	0	0
182	ĺ	1,891.9	13.0	Ö	0
183	i	1,899.2	12.0	Ö	Ó
185	i	1,902.8	66.0	Ŏ	Ó
186	1	1,885.4	66.0	Ŏ	Ŏ
	1	1,903.2	76.0	ŏ	ŏ
187	1	1,931.7	8.0	Ŏ.	ŏ
188	1		29.0	Ŏ	ŏ
189		1,921.8	47.0	0	0
300	1	1,903.6		0	Ö
301	1	1,951.4	76.0	0	. 0
59	1	1,900.0	122.0		0
500	1	1,892.8	25.0	0	0
501	1	1,886.6	76.0	0	
502	1	1,885.6	80.0	0	0
503	1	1,884.2	76.0	0	0
510	1	1,914.5	51.0	0	0
511	1	1,892.1	20.0	0	0
520	1	1,913.6	63.0	0	0
304	1	1,900.4	70.0	0	0
172	i	1,886.0	51.0	0	0
173	1	1,916.0	51.0	0	0
521	ĺ	1,886.0	51.0	0	0
522	1	1,880.0	51.0	0	0
523	1	1,903.0	51.0	0	0
524	1	1,887.0	51.0	0	0
525	1	1,881.0	51.0	0	0
526	1	1,882.0	51.0	0	0
527	1	1,931.0	30.0	0	0
528	1	1,943.0	30.0	0	0
33	ĺ	1,867.0	51.0	0	0
35	i	1,870.0	61.0	0	0
40	i	1,920.0	40.0	0	0
54	i	1,886.0	51.0	0	0
91	i	1,899.4	0.0	0	0
92	î	1,895.4	0.0	0	0
93	Î	1,882.0	0.0	0	. 0
540	î	1,930.0	694.0	Ō	. 0
541	i	1,980.0	928.0	Ŏ	0
542	·i	1,889.1	0.0	Ō	0
610	1	1,900.0	0.0	Ö	Ō
611	i	1,884.6	0.0	Õ	Ō
612	1	1,881.3	0.0	Ö	ŏ
205	1	1,947.0	-51.0	ŏ	ŏ
206	1	1,947.0	-291.0	0	ŏ
215	1	1,947.0	-197.0	0	ŏ
	1	1,947.0	-82.0	0	Ö
209	ı	1,041.0	04.0	Ū	

Booster No.	Pump Type	Data Node A	Node B	Pipe No.	Pressure
1	-	156	541	330	72.4
2		112	540	331	14.7

Pina	Data					
Pipe	No.	Node A	Node B	Diameter	Length	C Value
		190	510	(mm) 225.0	(m) 800.0	120.0
	1 2	139 139	304	44.0	374.0	130.0
	รี	51	140	150.0	228.0	120.0
	6	162	163	44.0	143.0	130.0
	7	51	162	150.0	20.0	120.0
	9 12	134 134	135 164	65.0 44.0	178.0 84.0	130.0 130.0
	13	66	135	150.0	265.0	120.0
	14	50	66	100.0	530.0	120.0
	15	50	67	100.0	583.0	120.0
	16	67	188	100.0 150.0	165.0 59.0	120.0 120.0
	20 21	21 21	54 23	100.0	88.0	120.0
	22	23	24	150.0	55.0	120.0
	23	20	24		90.0	120.0
	24	20	21	150.0	66.0	120.0
	26 27	25 52	52 53		110.0 176.0	120.0 120.0
	28	53	60		100.0	120.0
	29	18	60	100.0	134.0	120.0
	30	18	19		54.0	120.0
	31 32	19 19	52 55		151.0 133.0	120.0 120.0
	33	19 54	172		100.0	120.0
	34	9	18		315.0	120.0
	35	9	48		47.0	120.0
	36	1	48		265.0 201.0	120.0 120.0
	37 38	48 22	49 49		672.0	120.0
	39	22	51		596.0	120.0
	40	49			536.0	120.0
	41	148			372.0	120.0 120.0
	42 43	69 46	148 69		325.0 90.0	120.0
	44				551.0	120.0
	45	1	49	100.0	264.0	120.0
	46		46		401.0	120.0
	47 48				268.0 268.0	120.0 120.0
	49				444.0	120.0
	50	46	63	3 225.0	268.0	120.0
	51				47.0	120.0
	52 53				358.0 77.0	120.0 120.0
	54				264.0	130.0
	55	156	15'	7 300.0	300.0	120.0
	56		150		100.0	120.0
	61 62		203	3 350.0 4 225.0	704.0 442.0	120.0 120.0
	63			5 225.0	65.0	120.0
	64	4	6	1 65.0	972.0	130.0
	65			6 150.0	221.0	
	66 67				150.0 216.0	
	67 68				400.0	
	69				563.0	120.0
	70					
	72 74					
	76					
	80	39	9 . 17	9 150.0	125.0	120.0
	82	2 179				
	83					
	84 86					
	87			1 37.0	312.0	130.0
	88	3 4	2 4	3 100.0	257.0	120.0
	89					
	90 - 91			$\frac{4}{7}$ 150.0		
	92					
	9;					

99	29	112	65.0	251.0	130.0
100	109	511	100.0	400.0	120.0
101	108	109	100.0	120.0	120.0
		183	44.0	228.0	130.0
102	108			200.0	120.0
103	107	108	100.0	253.0	
104	107	182	44.0		130.0
105	28	107	100.0	40.0	120.0
106	28	113	150.0	66.0	120.0
107	113	114	65.0	265.0	130.0
108	114	117	65.0	500.0	130.0
109	117	118	44.0	318.0	130.0
111	118	119	75.0	248.0	120.0
113	28	106	150.0	250.0	120.0
114	103	106	150.0	400.0	120.0
116	104	105	44.0	300.0	130.0
118	30	526	100.0	210.0	120.0
119	62	132	150.0	1,500.0	120.0
120	155	500	140.0	175.0	130.0
125	132	133	44.0	363.0	130.0
127	31	64	225.0	167.0	120.0
129	70	144	100.0	284.0	120.0
130	144	145	44.0	121.0	130.0
132	45	47	150.0	162.0	120.0
133	9	45	100.0	761.0	120.0
134	9	57	100.0	25.0	120.0
135	57	58	100.0	120.0	120.0
136	58	60	100.0	262.0	120.0
138	56	59	97.0	352.0	130.0
140	58	143	100.0	168.0	120.0
141	142	143	50.0	264.0	120.0
142	57	142	100.0	202.0	120.0
143	141	142	100.0	99.0	120.0
146	12	150	150.0	360.0	120.0
	12	151	150.0	163.0	120.0
147		151		35.0	120.0
148	13		150.0		
149	151	186	140.0	450.0	130.0
151	154	155	100.0	132.0	120.0
160	153	154	100.0	165.0	120.0
161	14	153	150.0	236.0	120.0
162	13	14	150.0	475.0	120.0
163	13	146	150.0	35.0	120.0
164	146	147	150.0	137.0	120.0
167	11	137	150.0	663.0	120.0
168	14	152	100.0	66.0	120.0
170	33	152	100.0	150.0	120.0
175	56	68	100.0	165.0	120.0
176	68	136	44.0	726.0	130.0
177	136	137	44.0	512.0	130.0
178	137	187	140.0	277.0	130.0
182	71	124	225.0	400.0	120.0
183	15	124	225.0	441.0	120.0
184	15	16	150.0	177.0	120.0
185	16	121	100.0	286.0	120.0
186	120	121	75.0	1,210.0	120.0
187	16	125	100.0	850.0	120.0
	122	209	225.0	120.0	
191					120.0
193	125	126	100.0	396.0	120.0
194	126	128	65.0	668.0	130.0
195	126	127	65.0	1,047.0	130.0
196	128	129	65.0	90.0	130.0
197	129	130	44.0	60.0	130,0
198	130	131	37.0	88.0	130.0
199	62	520	100.0	569.0	120.0
200	41	42	100.0	237.0	120.0
201	30	113	150.0	250.0	120.0
203	5	36	150.0	105.0	120.0
179	187	300	150.0	500.0	120.0
250	136	301	65.0	215.0	130.0
209	160	300	150.0	152.0	120.0
213	62	524	97.0	334.0	130.0
214	30	503	100.0	334.0	120.0
215	112	511	75.0	132.0	120.0
216	500	501	140.0	100.0	130.0
217	154	501	65.0	104.0	130.0
218	186	501	140.0	221.0	130.0
710	100	301	140.0	771 · A	190.0

110	118	503	75.0	167.0	120.0
300	215	301	100.0	554.0	120.0
208	215	300	100.0	250.0	120.0
17	205	527	100.0	250.0	120.0
172	15	153	150.0	577.0	120.0
302	10	70	150.0	480.0	120.0
304	24	25	100.0	55.0	120.0
305	55	172	100.0	50.0	120.0
306	20	172	100.0	50.0	120.0
307	23	25	100.0	75.0	120.0
308	40	178	150.0	150.0	120.0
				180.0	120.0
77	39	40	100.0		
78	40	189	100.0	60.0	120.0
79	100	101	44.0	450.0	130.0
309	41	42	150.0	150.0	120.0
			100.0		
310	119	521	65.0	350.0	130.0
311	521	522	65.0	350.0	130.0
313	33	35	100.0	150.0	120.0
301	11	523	150.0	120.0	120.0
314	59	523	100.0	180.0	120.0
315	502	524	75.0	150.0	120.0
317	524	600	97.0	450.0	130.0
319	525	526	75.0	210.0	120.0
321	527	528	65.0	480.0	130.0
322	134	528	65.0	200.0	130.0
11	165	601	65.0	75.0	130.0
				70.0	
324	188	527	65.0	50.0	130.0
325	122	123	140.0	160.0	130.0
327	56	59	140.0	352.0	130.0
328	1	49	158.0	264.0	130.0
329	206	527	150.0	215.0	120.0
330	156	541	100.0	931.0	120.0
331	112	540	97.0	434.0	130.0
601	91	139	150.0	162.0	120.0
602	- 91	161	65.0	225.0	130.0
603	70	93	150.0	662.0	120.0
605	93	132	150.0	616.0	120.0
606	93	185	150.0	300.0	120.0
607	56	602	200.0	1,000.0	120.0
212	22	54	150.0	275.0	120.0
610	122	160	225.0	931.0	120.0
611	91	92	150.0	228.0	120.0
612	92	135	100.0	690.0	120.0
613	604	610	97.0	200.0	130.0
	-		91.0		
614	105	612	44.0	250.0	130.0
616	174	542	97.0	569.0	130.0
701	15	606	250.0	500.0	120.0
				50.0	
702	169	603	55.0		130.0
703	15	153	140.0	577.0	130.0
705	16	125	65.0	850.0	130.0
713	102	103	198.0	350.0	130.0
					130.0
714	103	106	198.0	400.0	
715	28	106	198.0	250.0	130.0
716	28	107	198.0	40.0	130.0
717	107	108	198.0	200.0	130.0
718	108	109	198.0	120.0	130.0
719	109	511	198.0	400.0	130.0
720	112	511	198.0	132.0	130.0
731	113	114	140.0	265.0	130.0
732	114	117	140.0	500.0	130.0
741	179	208	140.0	104.0	130.0
751	610	611	97.0	630.0	130.0
752	611	612	65.0	610.0	130.0
761	50	542	97.0	1,044.0	130.0
762	68	542	97.0	165.0	130.0
771	101	102	140.0	120.0	130.0
772		101	140.0	450.0	130.0
	100				
773	41	100	140.0	120.0	130.0
. 781	5	6	250.0	221.0	120.0
782	6	27	250.0	150.0	120.0
783	27	181	250.0	1,106.0	120.0
784	102	181	250.0	92.0	120.0
791	151	186	140.0	450.0	130.0
792	13	151	140.0	35.0	130.0
793	13	14	140.0	475.0	130.0

794	14	153	140.0	236.0	130.0
795	154	501	140.0	104.0	130.0
796	153	154	140.0	165.0	130.0

	Not	Work	Analysis		Distribut	ion Main	c		
Node	Ele	vation	Demand	Dynamic	Dynamic	Static	, ,		Leakage
No.		Pipe	(cum/d)	Pressure (MSL)	Pressure (m)	Pressure (m)			(cum/d)
		MSL) ,881.7	90.3	1,924.9	43.2	109.3	0.0	0.0	25.2
:	2 1	,885.1	51.8	1,926.2	41.1	105.9	0.0	$0.0 \\ 0.0$	23.8 25.5
		,881.8 ,881.3	$\begin{array}{c} 56.2 \\ 29.6 \end{array}$	1,925.5 1,925.4	43.6 44.1	109.2 109.7	0.0 0.0	0.0	25.7
		,883.7	56.2	1,925.3	41.6	. 107.3	0.0	0.0	24.1
		,881.2	98.4	1,924.0 1,941.0	42.8 37.6	109.8 87.6	0.0 0.0	$0.0 \\ 0.0$	24.9 21.6
1 ¹ 1		,903.4 ,902.1	18.5 63.6	1,946.6	44.5	88.9	0.0	0.0	26.0
1	2 1	,880.5	48.8	1,919.2	38,6	110.5	0.0	0.0	22.3 26.3
1		.,874.2 .,865.6	37.7 48.8	1,919.2 1,919.2	45.0 53.6	116.8 125.4	0.0 0.0	$0.0 \\ 0.0$	20.3 31.9
		,860.5	45.1	1,919.7	59.2	130.5	0.0	0.0	35.6
		,860.5	62.9 79.2	1,919.5 1,924.0	59.0 38.9	130.5 105.9	0.0 0.0	$0.0 \\ 0.0$	35.5 22.4
		1,885.1 1,885.8	62.9	1,924.0	38.2	105.2	0.0	0.0	22.0
2	2 1	,889.4	58.5	1,924.1	34.7	101.6	0.0	$0.0 \\ 0.0$	19.8 21.0
		1,887.3 1,887.7	60.7 86.6	1,923.9 1,923.9	36.6 36.2	$103.7 \\ 103.3$	0.0 0.0	0.0	20.7
		1,887.0	37.7	1,923.9	36.9	104.0	0.0	0.0	21.2
		1,882.3	55.5 19.2	1,925.2	42.9 44.9	108.7 111.8	0.0 0.0	0.0	$25.0 \\ 26.3$
		1,879.2 1,892.4	9.6	1,923.9	31.5	98.6	0.0	0.0	17.8
3	30	1,882,6	59.2	1,924.0	41.4	108.4	0.0	0.0	$\begin{array}{c} 24.0 \\ 25.6 \end{array}$
		1,882.0 1,889.3	68.8 37.7	1,925.8 1,925.3	43.8 36.0	109.0 101.7	0.0 0.0	$0.0 \\ 0.0$	20.6
		1,891.4	34.8	1,925.3	33.9	99.6	0.0	0.0	19.3
		1,893.9	31.1	1,925.3	31.4 15.1	97.1 76.1	0.0	$0.0 \\ 0.0$	17.7 7.9
		1,914.9 1,899.2	37.0 32.6	1,930.0 1,924.6	25.4	91.8	0.0	0.0	14.0
4	12	1,896.1	28.1	1,924.6	28.4	94.9	0.0	0.0	
		1,894.8 1,893.4	29.6 40.0	1,924.5 1,924.5	29.7 31.1	96.2 97.6	$0.0 \\ 0.0$	$0.0 \\ 0.0$	16.7 17.6
		1,884.9	49.6	1,925.3	40,4	106.1	0.0	0.0	23.4
	46	1,878.2	94,0	1,925,4		112.8 110.3	$0.0 \\ 0.0$	$0.0 \\ 0.0$	27.7 26.1
		1,880.7 1,880.2	26.6 74.7	1,925.3 1,924.8		110.3	0.0	0.0	26.1
	49	1,881.1	118.4	1,924.8	43,7	109.9	0.0	0.0	25.5
		1,886.3 1,895.4	106.6 34.8	1,943.2 1,924.1		104.7 95.6	0.0	$0.0 \\ 0.0$	34.1 16.0
		1,889.1	71.8	1,923.9		101.9	0.0	0.0	19.8
	55	1,886.2	65.9	1,923.9	37.7	104.8 88.3	0.0 0.0	0.0	21.7 26.1
		1,902.7 1,884.1	36.3 68.8	1,947.3 1,923.9		106.9	0.0	0.0	23.0
	58	1,890.9	88.1	1,923.9	33.0	100.1	0.0	0.0	18.7
	60 61	1,889.9 1,885.4	74.0 37.0	1,923.9 1,925.0		101.1 105.6	0.0 0.0	0.0	19.3 22.9
	61 62	1,890.2		1,941.6	51.4	100.8	0.0	0.0	30.5
	63	1,878.7	28.1	1,925.8		112.3 114.5	$0.0 \\ 0.0$	0.0 0.0	$27.7 \\ 29.1$
	64 66	1,876.5 1,910.0	32.6 29.6	1,925.8 1,942.0			0.0	0.0	18.1
	67	1,921.5	28.1	1,943.4	21.9	69.5	0.0	0.0	11.9 15.6
	68 69	1,918.6 1,879.5		1,946.8 1,925.4			0.0 0.0	$0.0 \\ 0.0$	26.9
	70	1,904.5		1,941.0	36.5	86.5	0.0	0.0	20.9 13.9
	71	1,894.5		1,919.7 1,924.6			0.0	$0.0 \\ 0.0$	15.6
	100 101	1,896.6 1,885.9		1,924.7			0.0	0.0	22.4
1	102	1,876.7	27.4	1,924.7	7 48.0		0.0 0.0	$0.0 \\ 0.0$	28.3 24.0
	03 104	1,883.1 1,916.3		1,924.9 1,929.3			0.0	0.0	6.7
	105	1,903.9	12.6	1,929.4	4 25.5	87.1	0.0	0.0	14.1
	106	1,881.3		1,924.3 1,924.3			0.0 0.0	$0.0 \\ 0.0$	25.0 25.7
	107 . 108	1,880.1 1,884.1					0.0	0.0	23.1
	109	1,884.6	14.8	1,924.			0.0	0.0	22.8 12.7
	112 113	1,900.7 1,878.5					0.0 0.0	0.0	26.7
	114	1,897.3	42.2	1,924.	1 26.8	93.7	0.0	0.0	14.9
	117	1,907.8					0.0 0.0	0.0 0.0	8.8 19.5
	118 119	1,889.0 1,889.1		1,922.	6 33.5		0.0	0.0	19.1
	120	1,871.2	2 83.6	1,917.	8 46.0	119.8	0.0	0.0	27.4 33.9
	121 122	1,862.0 1,950.0					0.0	0.0	0.0
	123	1,927.	3 48.1	1,946.	4 19.1	63.7	0.0	0.0	10.3
	124	1,879.					0.0	0.0 0.0	23.2 18.3
	125	1,886.	្ ខេរម	1,810,	. 06.0	10210		,,,,	

	Net Work	Analysis	.	Distribut	ion Main	C		
Node	Elevation	Demand	Dynamic	Dynamic Pressure	Static Pressure			Leakage
No.	of Pipe (MSL)	(cum/d)	Pressure (MSL)	(m)	(m)			(cum/d)
126	1,894.1	79.2	1,918.1	24.0	96.9	0.0	0.0	13.2
127	1,874,9	40.0 28.1	1,917.6 1,917.7	42.7 21.3	116.1 94.6	0.0 0.0	$0.0 \\ 0.0$	24.8 11.6
128 129	1,896.4 1,896.0	5.9	1,917.7	21.7	95.0	0.0	0.0	11.8
130	1,886.4	5.2	1,917.7	31.3	104.6	0.0	0.0	17.7
131	1,875.8	3.0	1,917.7	41.9	115.2	0.0 0.0	$0.0 \\ 0.0$	24.4 32.4
132 133	1,886.8 1,898.7	$37.7 \\ 13.3$	1,941.2 1,941.0	54.4 42.3	104.2 92.3	0.0	0.0	24,6
134	1,924.5	40.0	1,942.0	17.5	66.5	0.0	0.0	9.3
135		42.9	1,941.9	26.2	75.3	0.0	0.0	14.5
136 137		52.5 87.3	1,946.2 1,946.4	1.4 41.4	46.2 86.0	0.0 0.0	$0.0 \\ 0.0$	$\substack{0.6\\24.1}$
139		122.1	1,940.6	34,8	85.2	0.0	0.0	19.9
140	1,899.4	22.9	1,924.1	24.7	91.6	0.0	0.0	13.6
141 142		73,3 76.2	1,923.8 1,923.8	33.6 39.9	100.8 107.1	$0.0 \\ 0.0$	$0.0 \\ 0.0$	19.1 23.1
143		81.4	1,923.8	35.1	102.3	0.0	0.0	20.0
144	1,907.4	28.9	1,941.0	33.6	83.6	0.0	0.0	19.1
145 146		4.4 40.0	1,941.0 1,919.2	31.6 42.7	81.7 114.5	0.0 0.0	$0.0 \\ 0.0$	$\frac{17.9}{24.8}$
147		72.5	1,919.2	40.3	112.1	0.0	0.0	23.3
148	1,889.6	46.6	1,925.0	35.4	101.4	0.0	0.0	20.3
149		20.7	1,925.3	24.2 19.7	89.9 91.6	0.0 0.0	$0.0 \\ 0.0$	$\begin{array}{c} 13.3 \\ 10.6 \end{array}$
150 151		87.3 56.2	1,919.1 1,919.2	44.8	116.6	0.0	0.0	26.2
152	1,865.9	48.8	1,919.2	53.3	125,1	0.0	0.0	31.7
153		52.5	1,919.3	56.6	128.3	0.0	0.0	33.9
154 155		48.8 16.3	1,919.2 1,919.2	54.5 51.6	126.3 123.4	0.0 0.0	$0.0 \\ 0.0$	$\begin{array}{c} 32.5 \\ 30.6 \end{array}$
156		29.6	1,926.1	41.3	106.2	0.0	0.0	23.9
157		17.8	1,925.9	44.0	109.1	0.0	0.0	25.7
158 160		17.8 14.1	1,925.8 1,946.4	45.5 43.2	$\frac{110.7}{87.8}$	0.0	$0.0 \\ 0.0$	26.7 25.2
161		8.1	1,940.6	35.3	85.7	0.0	0.0	20.2
162	1,891.8	28.1	1,924.1	32.3	99.2	0.0	0.0	18.3
163 164		5.2 3.0	1,924.1 1,942.0	24.8	$\frac{91.7}{71.2}$	0.0 0.0	$0.0 \\ 0.0$	13.6 12.1
165		74.7	1,990.9	28.4	28.5	0.0	0.0	15,9
168	1,899.0	13.3	1,925.8	26.8	92.0	0.0	0.0	14.9
169 170		16.3 9.6	1,980.0 1,925.8	62.2 32.5	73.2 97.7	0.0 0.0	$0.0 \\ 0.0$	37.6 18.4
171		14.1	1,924.9	15.2	81.3	0.0	0.0	8.0
21	1,885.1	71.8	1,923.9		105.9	0.0	0.0	22.4
20 174		61.4 77.0	1,923.9 1,945.7	38.0 43.3	105.1 88.6	0.0 0.0	0.0	21.9 25.2
5		71.8	1,923.9	28.2	95.3	0.0	0.0	
170	6 1,895.0	17.0	1,924.5	29.5	96.0	0.0	0.0	16.6
17'		17.0	1,924.5		93.7 78.2	0.0	0.0	15.1 9.1
178 179		40.7 18.5	1,929.9 1,930.0		73.5	0.0	0.0	6.4
18	1 1,881.0	59.2	1,924.7	43.7	110.0	0.0	0.0	25.5
18		9.6 8.9	1,924.1 1,924.0	32.1 24.8	99.1 91.8	0.0 0.0	$0.0 \\ 0.0$	18.2 13.7
18i 18i			1,941.1		88.2	0.0	0.0	22,0
18	6 1,885.4	48.8	1,919.2	33.8	105.6	0.0	0.0.	19.2
18			1,946.4		87.8 59.3	0.0 0.0	0.0 0.0	25.2 6.1
18 18	9 1,921.8	21.5	1,943.5 1,929.9		69.2	0.0	0.0	4.0
30	0 1,903.6	34.8	1,946.4	42.8	87.4	0,0	0.0	24.9
30			1,946.3 1,947.2		39.6 91.0	0.0 0.0	0.0	0.0 27.7
5 50			1,919.2			0.0	0.0	14.7
50	1 1,886.6	56,2	1,919.2	32.6	104.4	0.0	0.0	18.5
50 50			1,942.9			0.0	0.0	34.4 22.7
50 51			1,923.6 1,940.6		106.8 76.5	$0.0 \\ 0.0$	0.0	14.5
51	1 1,892.1	14.8	1,924,	31.9	98.9	0.0	0.0	18.0
52			1,941.0			0.0	0.0	15,6
30 17			1,938. 1,923.	5 38.1 9 37.9		0.0	0.0 0.0	21.9 21.8
17	3 1,916.0	37.7	1,929.	13.0	75.0	0.0	0.0	6.7
52 50			1,922,			0.0	0.0	20.6 24.3
52 52			1,921,4 1,946.			0.0	0.0	25.4
52	4 1,887.0	37.7	1,943.	56.0	104.0	0.0	0.0	33.5
52						0.0	0.0	24.9 24.4
52	26 1,882.0	37.7	1,923.	9 41.9	109.0	0.0	0.0	24,4

	Net Work	Analysis	3	Distribut	ion Main	c		
Node	Elevation	Demand	Dynamic	Dynamic	Static			Leakage
No.	of Pipe		Pressure	Pressure	Pressure			_
	(MSL)	(cum/d)	(MSL)	(E)	(M)			(cum/d)
527	1,931.0	22.2	1,943.8	12.8	60.0	0.0	0.0	6.6
528	1,943.0	22.2	1,942.4	-0,6	48.0	0.0	0.0	0.0
33	1,867.0	37.7	1,919.1	52,1	124.0	0.0	0.0	31.0
35	1,870.0	45.1	1,919.1	49.1	121.0	0.0	0.0	29.0
40	1,920,0	29.6	1,929.9	9.9	71.0	0.0	0.0	5.0
54	1,886.0	37.7	1,923,9	37.9	105.0	0.0	0.0	21.8
91	1,899.4	0.0	1,940.7	41.3	91.6	0.0	0.0	23.9
92	1,895.4	0.0	1,940.7	45.3	95,6	0.0	0,0	26.5
93	1.882.0	0.0	1,941.1	59.0	109.0	0.0	0.0	35.5
540	1,930.0	513.6	1,935.0	5.0	61.0	0.0	0.0	2.3
541	1,980.0	686.7	1,985.0	5.0	11.0	0.0	0.0	2.4
542	1,889,1	0.0	1,945.8	56.7	101.9	0.0	0.0	34.0
610	1,900.0	0.0	1,930.0	30.0	91.0	0.0	0.0	16.9
611	1.884.6	0.0	1,930,0	45,4	106.4	0.0	0.0	26.6
612	1,881.3	0.0	1,929.8	48.5	109.7	0.0	0.0	28,6
205	1,947.0	-37.7	1,943.8	-3.2	44.0	0.0	0.0	0.0
206		-215.3	1,943.8	-3.2	44.0	0.0	0.0	0.0
215		-145.8	1,946.5	-0.5	44.0	0.0	0.0	0.0
209		-60.7	1,946.4	-0.6	44.0	0.0	0.0	0.0