Figure B-4 H-A Curve for Mereb3

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A all

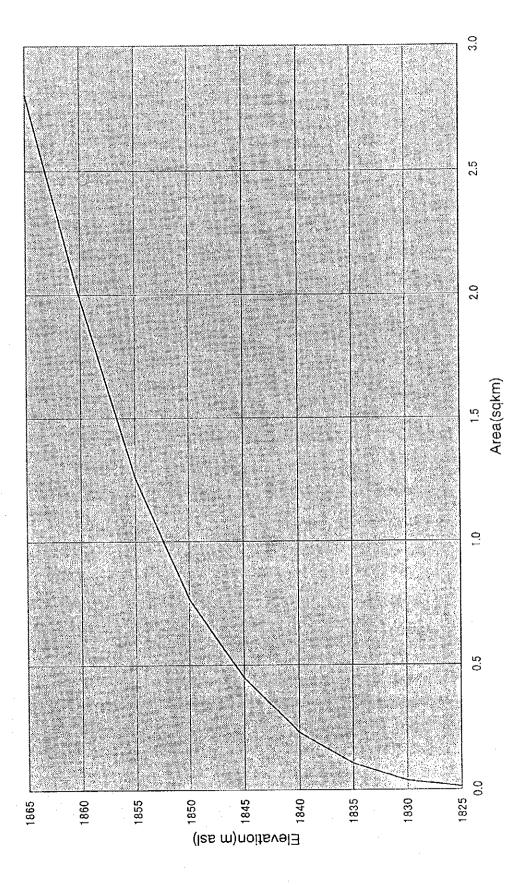


Figure B-5 H-V Curve for Mereb3

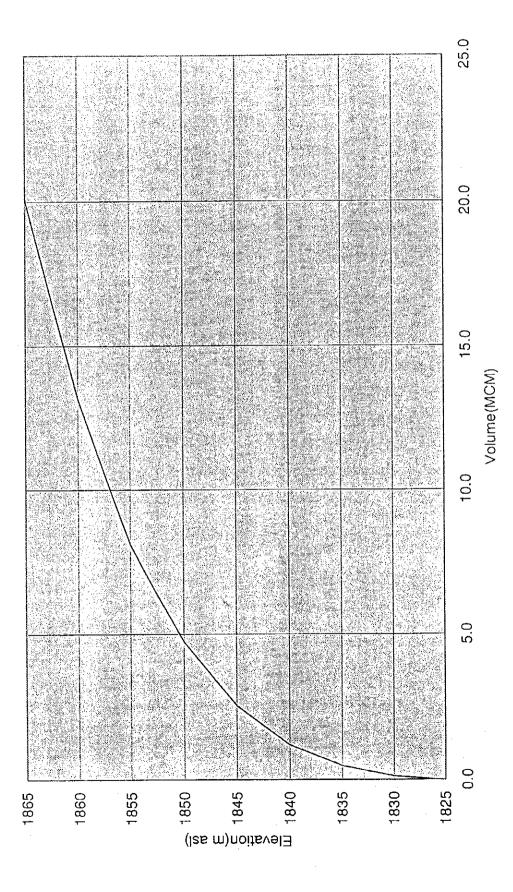
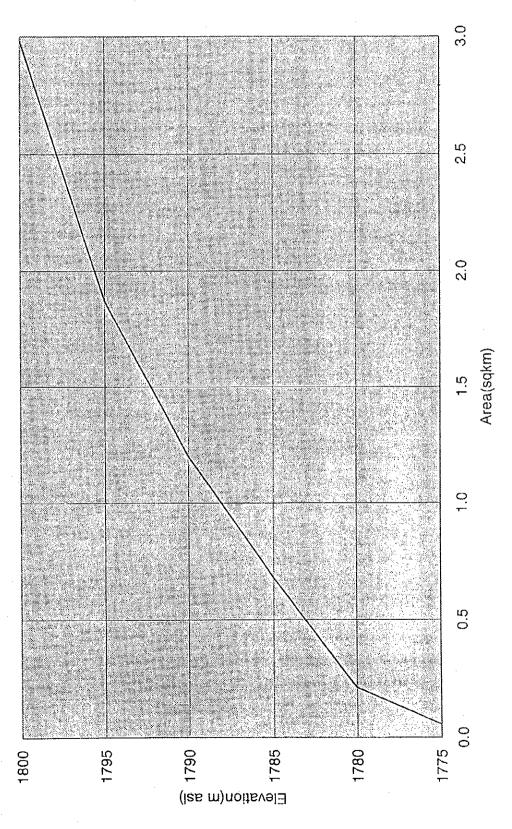


Figure B-6 H-A Curve for Mereb5

Sec. 1



(1) Reservoir Parametrs

In this connection, land-mark survey during the phase-1 field investigation was carried out and topographical map with 5m contour was prepared. Using this map, H-V and H-A curves for both dams were constructed. The reservoir parameters are tabulated below.

	Mereb 3			Mereb 5	
EL	Area	Volume	EL	Area	Volume
(m asl)	(sqkm)	(MCM)	(m asl)	(sqkm)	(MCM)
1825	0.013	0.000	1775	0.056	0.000
1830	0.037	0.125	1780	0.212	0.670
1835	0.106	0.483	1785	0.680	2.900
1840	0.230	1.198	1790	1.200	7.600
1845	0.451	2.543	1795	1.870	15.275
1850	0.768	4.750	1800	2.980	27.400
1855	1.258	8.113			
1860	1.980	13.160			
1865	2.804	20.055			

(2) Dam Height

Dam height will be selected using the following equation.

Dam height = $HWL + H_d + F_b$

where, HWL is high water level (m)

H_d is water depth in the spill-way (m)

F_b is free board (m)

(3) Spill-way

In deciding Spill-way size, maximum specific yield is calculated using Creager equation as follows.

$$q = CA^{(A^{-0.05}-1)}$$

where, q is maximum specific yield($m^3/sec/km^2$)

A is catchment area(km²)

C is a coefficient depending on regional characteristics

Considering C = 15, q may be calculated as $2.8755 \text{ m}^3/\text{sec/km}^2$

Now, Design flood discharge (Q) may be computed as

```
Q = q * A = 2.8755*492 = 1,415 = 1,450 \text{ m}^3/\text{sec}(\text{rounded})
```

Cont.

Next, calculation for various flow depths in Spill-way (H_d) with corresponding widths is performed using the following equation.

 $Q = CLH_d^{3/2}$

where, H_d is flow depth in the Spill-way (m)

Q is design flood discharge (m³/sec)

C is coefficient (2.1)

L is width of Spill-way (m)

Calculated depths with corresponding widths are as follows.

Flow depth(m)	Width(m)
1.0	690
2.0	245
2.5	175
3.0	133
3.5	106
4.0	87
5.0	62

From the amount of design flood discharge, flow depth(Hd) is selected as 3.5m with corresponding length(L) as 106m. It is noteworthy to mention that, from the topographical conditions, the location of the Spill-way should be on the right bank and a overflow type(without gate) structure is recommended.

(4) Sediment and Effective Capacity

A. Land

Assuming river bed width as 8m, flow depth as 2m and velocity as 2m/sec, inflow rate may be calculated as 32m3/sec. Using Bed Material Load Graph prepared by the Sector Study, calculation of sediment may be done as follows.

 $q_s = 1606.4 * Q^{0.5618}$ = 11300mg/l = 11.3kg/m³

Now, total volume may be found by multiplying inflow volume i.e. 25.0MCM and gives 282,500 tons/year. Dividing this value by density(1.8ton/m³) gives 156,944 m³/year, say 157,000 m³/year.

Considering dam life as 50 years, effective capacity may be calculated as follows.

Total amount of Sediment = $157,000*50 = 78,850,000m^3 = 8.0MCM$ (rounded)

Therefore, effective capacity = 25.0MCM - 8.0MCM = 17.0MCM. However, actual available amount for use has to be calculated subtracting the losses such as evaporation, percolation etc.

Cont.

(5) Low Water Level(LWL) and Flood Water Level(FWL)

From the H-V curve, for 8MCM of sediment, the elevation will be 1790.33m asl, which is the Low Water Level(LWL)

The Flood Water Level(FWL) may be computed as follows.

$$FWL = HWL + H_d = 1799m asl + 3.5 m = 1802.50m asl$$

(6) Crest Elevation and Width

The dam crest elevation may be calculated as follows.

 $HWL + H_d + F_b = 1799m asl + 3.5m + 1.5m = 1804m asl$

From the above dimensions, the total dam height would be

Crest level elevation – El at the foundation excavation i.e 1804m asl - 1770m asl = 34.0m

The Crest width is determined according to the formula recommended by International Association for Large Dams, which is as follows.

Crest width(B) = $3.6H^{1/3} - 3.0 = 3.6*34.0^{1/3} - 3.0 = 8.66m = 9.0m$ (rounded)

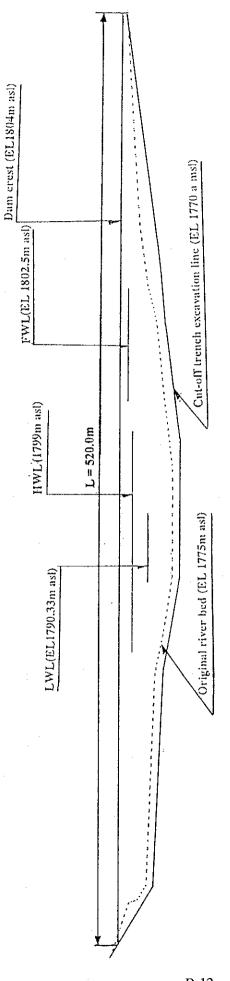
(7) Salient Features

i)	Name	: Mereb 5
ii)	Dam Type	: Rock-fill
iii)	Purpose	: Multi-purpose
iv)	Catchment Area	: 492.0 sqkm
v)	Reservoir Capacity	: 25.0 MCM
vi)	Surface Area	$: 2.8 \text{ km}^2$
vii)	Effective Storage	: 17.0 MCM
viii)	Dead Storage	: 8.0 MCM
ix)	Low Water Level(LWL)	: 1790.33m asl
x)	High Water Level(HWL)): 1799.0m asl
xi)	Flood Water Level(FWL): 1802.5m asl
xii)	Free Board	: 1.50m
xiii)	Dam Crest Level	: 1804.0m asl
xiv)	Crest Width	: 9.0m
xv)	Crest Length	: 520.0m
xvi)	Basement Width	: 135.0m
xvii)	Spill-way Length	: 106.0m
xviii)	Embankment Volume	: 665,000m ³
xix)	Approximate Cost	: Embankment Vol./Unit cost = 21.0million
		(32.0 US\$ per cubic meter)

Figure B-7 Longitudinal Section Along Mereb5 Dam Axis

A Start

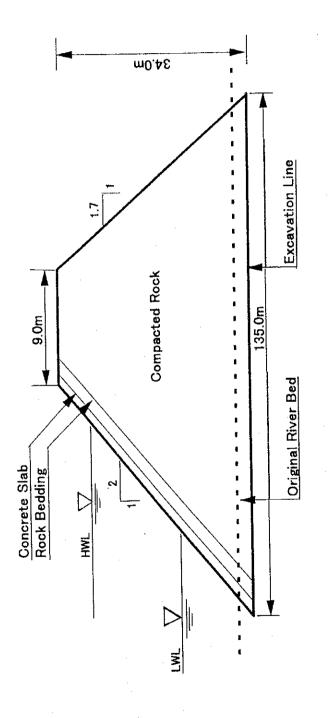
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Scale: 1:2000

Longitudinal Section Along Dam Axis

Figure B-8 Cross-section of Mereb5 Dam

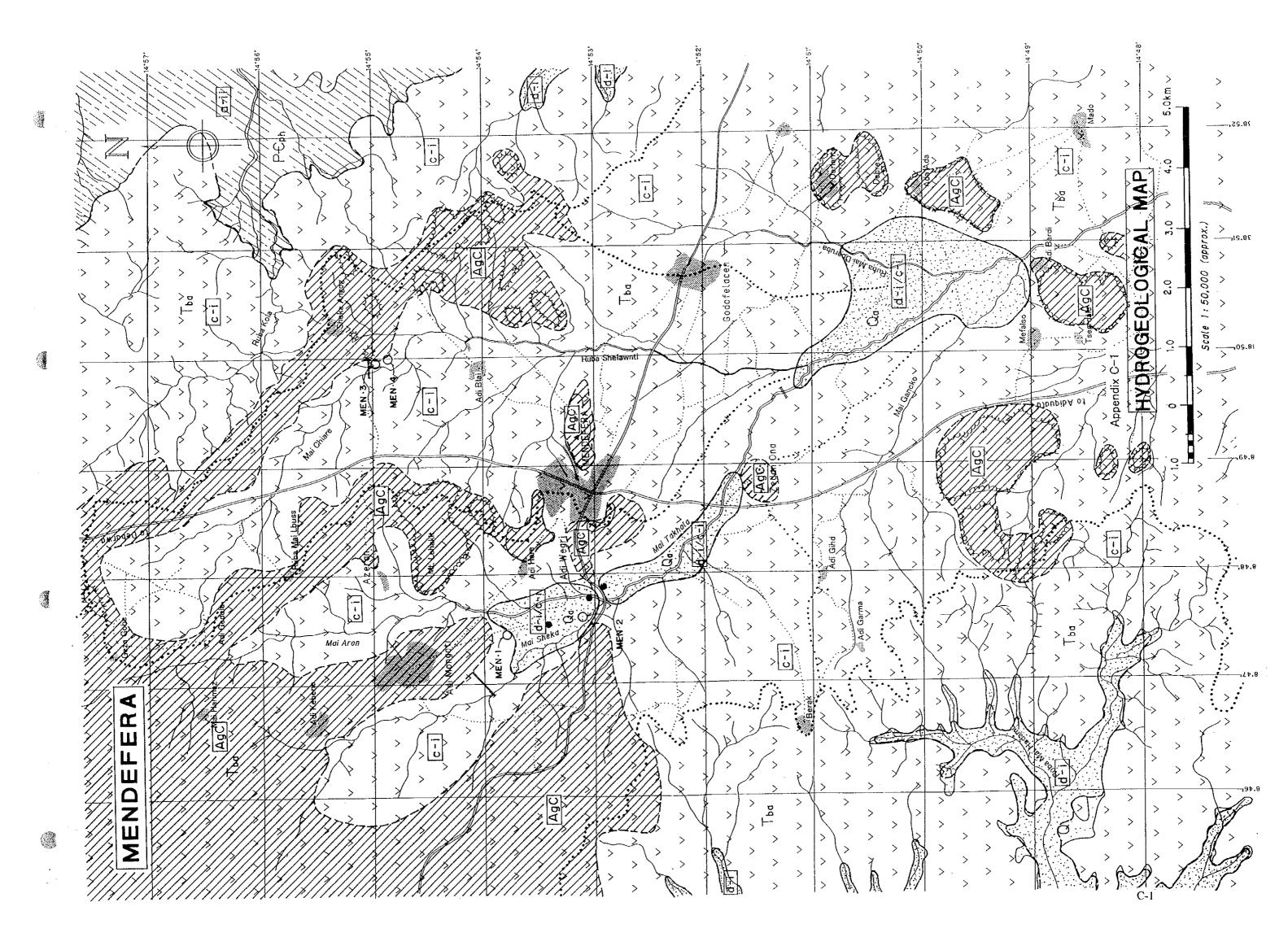


APPENDIX C

HYDROGEOLOGY

CHAPTER 3 THE DEBUB REGION

3.1 N	atural C	onditions	
C	2-1 HY	DROGEOLOGICAL MAP	C-1
C	2 Leg	gend on HYDROGEOLOGICAL MAP	C-2
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: Trachytics, Alkaline intrusives, Hornfels, Chart, and a part of basaltic volcanics. (b) Fissured aquifer of Sedimentary rocks : Paleozoic sandstone : Adigrat Sandstone : Colluvial deposits : Basaltic volcanics (d) Intergranular aquifer of Sediments : Alluvial deposits : Meta-volcanics : Test/Observation Well : Metamorphics Hydrogeological Legend (a) Fissured aquifer of Basements (c) Fissured aquifer of volcanics : Existing borehole : Basin boundary Gramite Aquitard and Aquiclude AgO [<u>-</u>] لما لما لما 8 1 1 1 1 1 1 1 Legend on HYDROGEOLOGICAL MASP 0 Precambrian Precambrian Precambrian Precambrian Precambrian Precambrian Precambrian Quaternary Quaternary Paleozoic Paleozoic Mesozoic Tertiary Tertiary Tertiary Granite (marginal phase) 0-2 0-2 : Alkaline Intrusives : Trachytic volcanics : Adigrat Sandstone : Basaltic volcanics : Alluvial deposits : Laterite covers Schist, Gneiss Geological Legend : Phyllite, Slate Metavolcanic : Sandstone : Dolomite : Hornfels : Gramite : Chart

*

6 Seally

C-2

Appendix C-3 Geophysical Prospecting Works

C-3.1, Works Volume

(1) Methodology and Equipment

In this Study, three kinds of geophysical prospecting were introduced; those were Very Low Frequency Electromagnetic wave sounding (VLF-EM), Horizontal electric Sounding (HS) and Vertical Electric Sounding (VES).

Equipment used in this work were as follows:

- for VES and HS

- for VLF

SYSCAL R-2 (Team) Terrameter SAS 300B (Dept. of Mines) ABEM WADI

(2) Works volume

Table C-3.1 G	eophysical Prospecting	Works	(Original plan)
---------------	------------------------	-------	-----------------

Township	Site	VLF	HS	VES
Debarwa	Near Adi Logo	-	2	8
:	The Mereb		(2)	(5)
Mendefera	Upstream of power plant		-	15
	Downstream of power plant		-	10
Dekemhare	East of old run-way	8	-	30
	Valley at 3.5km SE	.4	. 1	4
Segeneiti	Near the Municipality	4	1 .	4
0	Valley at 4.5km W	-	2	-
· · · · · · · · · · · · · · · · · · ·	Downstream of eastern valley	4	2	6
Adi Keyih	Upstream of eastern valley	4	2	6
	Valley at 4.0km NW	-	2	-
Senafe	Afoma area	-	2	7
	Small valley at SE	4	2	-
Total		28 ^{lines}	16 ^{lines}	90 ^{points}
			(2^{lines})	(5^{lines})

Note: () means small-scale survey.

Table C-3.2	Geophysical	Prospecting Works	(The final)

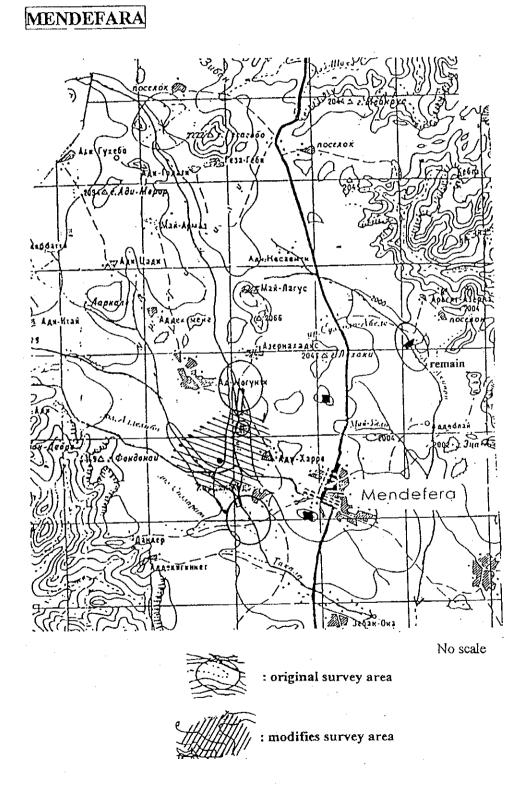
Township	Site	VLF	HS	VES	Remark
Debarwa	Near Adi Logo	-	2	9	Shift the
	The Mereb		(4)	(5)	site
Mendefera	Near the power plant	-	-	28	Unified
Dekemhare	East of old run-way	10	-	29	No change
	Valley at 3.5km SE	4	2	-	Shift the
Segeneiti	Near the Municipality	3	1	6	sites
	Valley at 4.5km W	- 5	2	8+(2)	
Adi Keyih	Upstream of eastern valley	-	4	6	Shift the
-	Valley beneath the town	3	-	-	sites
	Valley at 4.0km NW	6	2	13	
Senafe	Afoma area	-	3	8+(8)	No change
	Small valley at SE	6	2	-	
Total		37 ^{lines}	18 ^{lines}	107 points	
	· ·		(4^{lines})	(15 points)	

Note: () means small-scale survey.

C-3.2. Location Map of Geophysical Works

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C-3.3. Summarized Results of Geophysical Prospecting Works

The survey site is very flat plain covered by thin alluvial deposits, and the both sides (west and east) are bounded by gentle hills. These hills are consisted of rather fresh and hard basalt showing more than 1,000 ohm-m, however, the alluvial plain is underlain by weathered or fissured basalt showing several 10s to 150 ohm-m. The depth of weathered rock zone varies irregularly, from only 2,3m to nearly 80m. As a tendency, it is deep along the current streams route, but in between them there is a mound of fresh rock. Near the village of Adi Mongoti, it means the northern end of the survey area, bedrock is exposed out again. Further, the report of Department of Mines pointed out a fault passing through the upstream side of the Power Station.

Those situation suggest the major part of survey area forms an individual groundwater basin in between the two streams, separated from the wide Mai Takhala basin, further downstream of the survey area, by low hills and the fault. And two of the drilling points were proposed inside of the groundwater basin, just avoiding the fresh rock mound in the center of basin.

C-5

Test/Observation Well Drilling Works Appendix C-4

C-4.1. Work volume

(1) Type of Wells

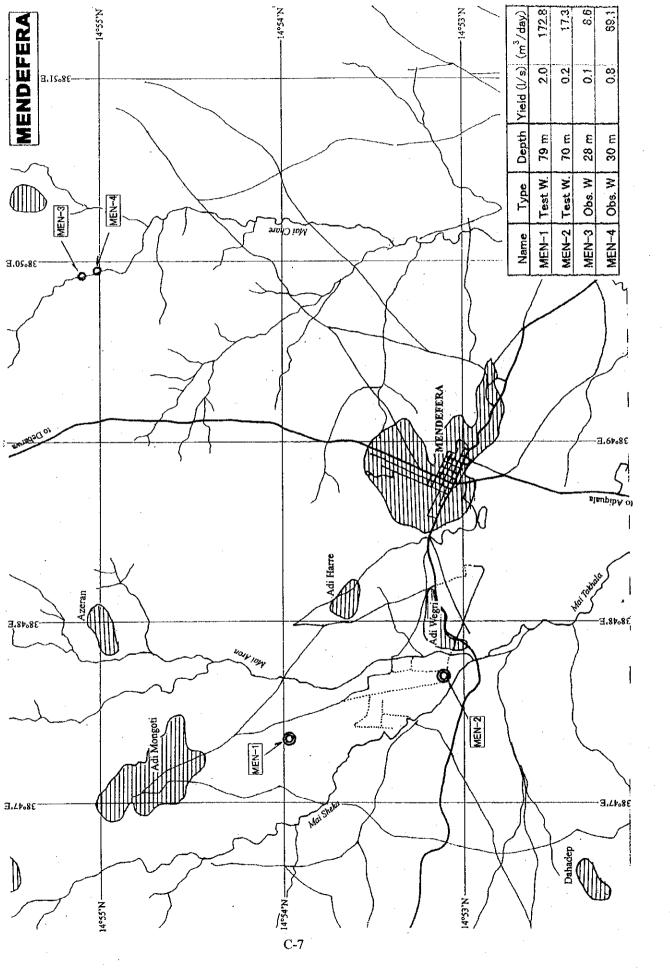
In this Study, two types of well are set; "Test Wells" and "Observation Wells". The main purpose of the Test Well is to know its exact hydrogeological condition and to evaluate the aquifer potential of the site. The purpose of the Observation Well is to estimate the recharging function of an existing dam to the groundwater system downstream. Two dams, namely Kilowlie Dam in Mendefera and Afoma Dam in Senafe, were selected for this study.

(2) Work volume

Table C.4.1 shows the final drilling plan. Those sites and the number of wells in each town were fixed but the depth of each drilling should be revised in accordance with the hydrogeological situation of the site.

Township	Site	Test Well	Obs.Well	Recorder*
Debarwa	West of the town	1 x 80m		1
Mendefera	Near the power plant	2 x 80m		1
· ·	Downstream of Kilowlie Dam		2 x 30m	2
Dekemhare	East of old run-way	2 x 80m		2
	Valley at 3.5km SE	1 x 60m		1
Segeneiti	Near the Municipality	1 x 60m		
0	Valley at 4.5km W	1 x 60m	<u> </u>	ļ
	Upstream of eastern valley	1 x 60m		
Adi Keyih	Valley at 4.0km NW	1 x 60m		1
Senafe	Afoma Dam downstream		1 x 60m	1
Total		10 ^{wells}	3 ^{wells}	9 ^{wells}
		(700m)	(120m)	

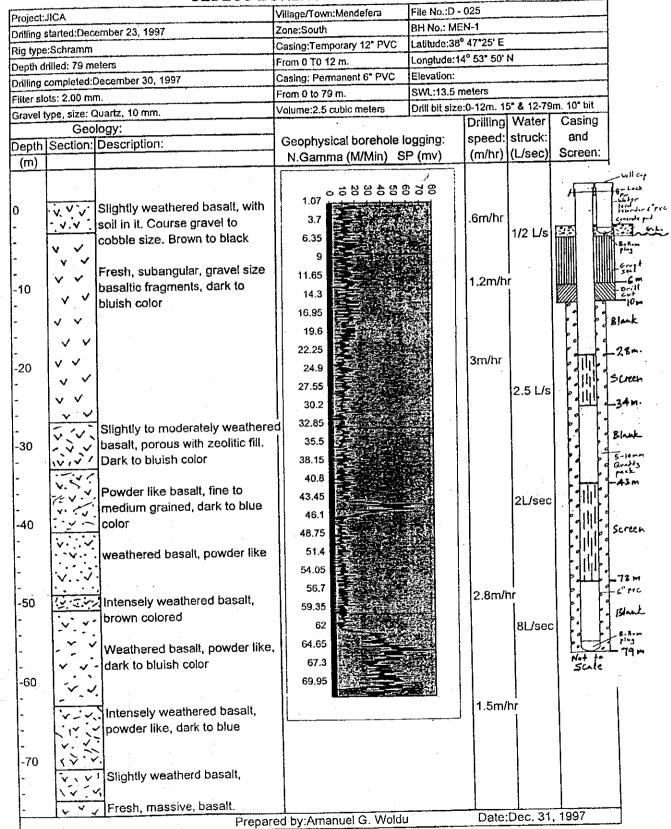
: Automatic water level recorder installatio



C-4.3 Lithological Logs

MEN-1

GEDECC BOREHOLE DRILLING DATA:



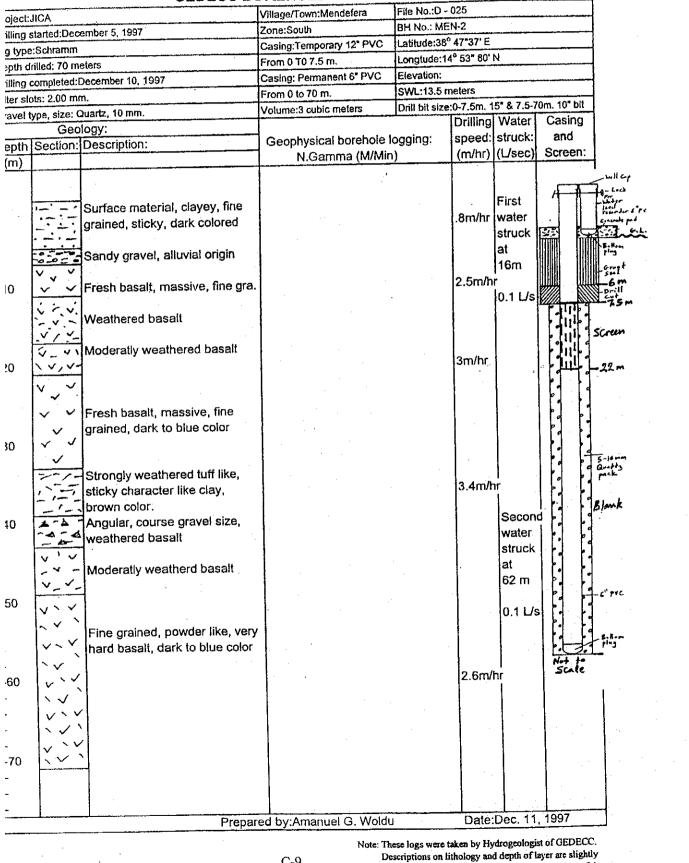
1. 3

Note: These logs were taken by Hydrogeologist of GEDECC. Descriptions on lithology and depth of layer are slightly different with the one taken by Drilling Supervisor of the Team which are explained in the main text.

C-8

MEN-2

GEDECC BOREHOLE DRILLING DATA:



C-9

Descriptions on lithology and depth of layer are slightly different with the one taken by Drilling Supervisor of the Team which are explained in the main text.

MEN-3

à.

(m)

0

-10

-20

-30

-40

-50

-60

-70

GEDECC BOREHOLE DRILLING DATA: File No.:D - 025 Village/Town:Mendefera Project:JICA BH No .: MEN-3 Drilling started:December 14, 1997 Zone:South Casing:Temporary 12" PVC Latitude:35° 50*00' E Rig type:Schramm Longlude:14° 54" 58' N From 0 T0 9 m. Depth drilled: 28 meters Casing: Permanent 6" PVC Elevation: Drilling completed:December 16, 1997 SWL:2.4 meters From 0 to 28 m. Filter slots: 2.00 mm. Drill bit size:0-9m. 15" & 9-28m. 10" bit Volume:2 cubic meters Gravel type, size: Quartz, 10 mm. Drilling Water Casing Geology: speed: struck: and Geophysical borehole logging: Depth Section: Description: (m/hr) (L/sec) Screen: N.Gamma (M/Min) Top soil, sticky character, clay 1.9m/hr to silt, volcanic ash origin Fresh basalt, massive, course gravel size, dark to bluish color 10.5 L/s Weathered basalt, course gravel 1.9m/hr 15 Δ 4 Angular, course basalt 4 Rounded, course basalt Angular, course basalt A

Note: These logs were taken by Hydrogeologist of GEDECC. Descriptions on lithology and depth of layer are slightly different with the one taken by Drilling Supervisor of the Team which are explained in the main text.

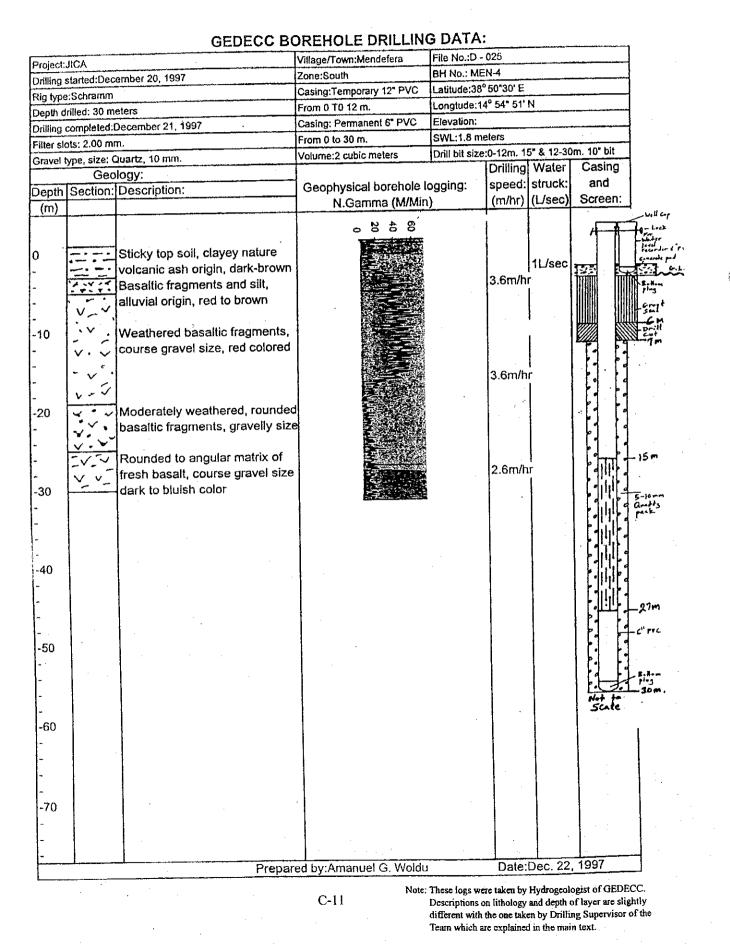
Date:Dec. 17, 1997

Blenk

scale

Prepared by:Amanuel G. Woldu

MEN-4



	Pump	ing Test	
ell ident Men-1	Description		
os. Well Distance [m]	Average Pump. Rate [m3/day]		Initial Sat. Thickness [m]
0.08	175.3900	4440.000	
			Resu
ansmissivity [m2/day] 2.537744	Storage Coefficient	Leakance [1/day]	Estimation Error [m] 1.61
t Method			Theis Method
2 4 9 10 10 12 12 14			
		100 ime [min]	10000

%

T

Appendix C-5Water QualityC-5.1Water qualities of Current water supply system

Report

On

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WATER QUALITY ANALYSIS

For

SEVEN TOWNS IN DEBUB REGION

Fikremariam Kahsai Department of water resources Asmara, Eritrea Oct.24,1997

Introduction

As per request of Japan international co-operation agency (JICA) study team, the laboratory of WRD has conducted water quality analysis for seven target towns in the southern region of the country. These towns are, Debarwa, Mendefera, Adi-Quala, Dekemhare, Segeneiti, Adi-Keyih, and Senafe. The study encompasses chemical, bacteriological and physical assessment of water samples. To accomplish the task, ten sampling points were chosen from each town.

Water source intended for drinking should fulfil requirements which are essential for the well being of the consumer. It should be safe, as well aesthetically acceptable. The basic aspect of water quality which should be examined are:

- 1. Chemical quality: Chemically, water for public supply should hold optimum concentration of ions and trace metals.
- 2. Bacteriological quality: It should be free from pathogenic micro-organisms.
- 3. Physical quality: Aesthetically it should be acceptable to consumers. Meaning, its taste should be palatable, its color and odor acceptable.

The bacteriological and physical examination of water points was carried out in the field, and the technique used for the enumeration of coliforms was membrane filtration. Concerning chemical analysis, water samples were brought to the WRD water laboratory in Asmara and analysed

The analytical results and location of of the sampling points (in UTM coordinates) are annexed within this report.

Evaluation of analytical data

Water for public water supply should be free from any pathogens, chemically safe for human consumption and aesthetically acceptable.

To meet the intended purpose some countries set their own drinking water standards which comply with their own specific conditions. Most countries in the world follow WHO guidelines. Inspite of this, there are no measure differences between standards of some developed countries and that of WHO.

For practical purposes of this report, all references and evaluations of analytical data are given on WHO guidelines.

1. Physio-Chemical characteristics:

A. Electrical conductivity (EC)

EC is a measure of the ability of salts in solution to carry an electric current. The EC value rises with the rise in the degree of mineralisation or salinity.

Potable water should consist optimum concentration of dissolved substances, to serve as feasible source. Consideration of EC value as water quality is mainly due to its effect on taste. WHO has not set a standard for EC value, but the guideline value for TDS(total dissolved solids) which is directly related to EC (TDS = kEC, Where k ranges 0.55 to 0.7 for natural waters) is 1000ppm.

Among the seventy samples analysed from the seven towns, a borehole in Adiquala (AD-06), a well in (SG-09), borehole and a well in Dekemhare (DK-04), (DK-10), have electrical conductivity value greater than $1200 \,\mu$ s/cm to impart disagreeable taste.

B. pH Value

The pH value which is a measure of the concentration of the hydrogen ion is used as indicator of either acidic or basic pollution. The pH value of all the waters in the towns lie within the range of 6.5-8.5 units, which is a recommended limit for drinking.

C. Turbidity

Clarity is an important water quality parameter of water supply. Turbidity in water is caused by suspended matter, such as clay, silt, finely divided organic and inorganic matter, and plankton and other microscopic organisms. If the turbidity exceeds 5NTU, then it is clearly visible in a glass of water and usually rejected by consumer on aesthetic grounds.

Turbidity higher than the recommended value was registered in Segeneyti, Kilowlie(Mendefera), Sememo(Adiquala), and Adi-Keyih dams. This is mainly caused by silt and clay materials transported with the flowing water during raining.

The other sources which are mainly ground water, have value less than 5NTU which meets the standard of WHO.

D. Total Hardness

Total hardness is the sum of calcium and magnesium concentrations, both expressed as calcium carbonate, in milligrams per litre. The hardness or softness of water varies from place to place and reflects the nature of the geology of the area with which the water has been in contact. In general, surface waters are softer than ground waters. Hard waters are associated with chalk and limestone catchment areas, whereas soft waters are associated with impermeable rocks such as grinite.

Very hard water, greater than 350 mg/l as CaCO3, causes scale deposition in pipelines and scum formation in boilers. Soft Waters, less than 75 mg/l as CaCO3 causes leaching of metals and corrosion.

The dams in Adi-Keyih(AK-09), Adi-Quala(AD-01), and Mendefera (Kilowlie)(MN-01) has 62, 54, and 48 mg/l total hardness as Calcium Carbonate, hence classified as soft water. Whereas, nine sampling points which are coded as SN-02, SN-08, AD-06, MN-06, MN-08, DB-06, SG-09, DK-04 and DK-10 has registered hardness value ranging 350 to 743 mg/l as Calcium Carbonate. Therefore, classified as very hard waters.

E. Nitrogenous Compounds

The chemical compounds nitrate, nitrite, and ammonia play a major role in evaluation of water quality. Three of them are interconnected by nitrogen cycle, hence one is a precursor of the other. oxidation of ammonia gives rise to nitrite and further to nitrate. The main concern of nitrate presence in excess is that it is linked to a condition known as blue baby syndrome or infant methaemoglobinemia. Due to its toxicity effect on human body, an upper limit value of 45mg/l has been set.

As the analytical results show, boreholes in Adi-Keyih (AK-10), Adi-Quala (AD-06), and Dubarwa (DB-05), a borehole(DK-04) and a well (DK-10) in Dekembare, registered 45.2, 89.5, 64.2, 97.4, and 51.8 mg/l nitrate respectively.

Besides, in Senafe at consumer's tap (SN-06), the levels of nitrite was 5.16mg/l. This is exceedingly high in relation to WHO guideline value, which is 3mg/l as nitrite. This could be due to old pipeline system which permits intrusion of contaminants.

The possible source of nitrate contamination is organic matter broken down by bacteria in the soil.

F. Chloride

Chloride is widely distributed in nature in the form of varied salts. Its presence in natural waters can be attributed to dissolution of salt deposits, sewage discharges and sea water intrusion in coastal areas.

The taste threshold for chloride in drinking water is dependent upon the associated cation, but is usually within the range 200-300mg/l. WHO recommends a guideline value of 250mg/l.

Among the seventy samples analysed, with the exception of a bore hole in Dekemhare (DK-04) which was found 260mg/l, all were found to contain less than 250mg/l, hence in the desired limit.

G. Sulphate

High sulphate concentrations in water may contribute to the corrosion of metals in the distribution system. Due to the cathartic effect of sulphate, a guideline value of 400mg/l is set.

The sulphate content of all the analysed samples is far less than the recommended guideline value, therefore there will not be any sulphate related problem with the water supplies.

H. Sodium

The recommended guideline value is 200mg/l which is based on taste thresholds. With the exception of a borehole in Dekemhare (DK-04) which is found to be 215mg/l, all the analysed samples showed a sodium level in the range of acceptable quantity.

I. Iron and Manganese

Both chemical elements are related with staining of laundry and sanitary ware. For this reason a guideline value of 0.3mg/l and 0.1mg/l is set for iron and manganese respectively. For health related reasons a 0.5mg/l guideline value is set for manganese.

Among the analysed samples, a borehole in Senafe (SN-10), a dam in Mendefera (MN-01), and a well in Segeneyti (SG-07) were found to contain 0.39mg/l, 0.41mg/l and 0.61mg/l of iron. The rest samples are free from iron which can cause staining.

Furthermore, four water sources are found to consist 0.2mg/l of manganese. These are, a spring and a hand dug well in Dubarwa (DB-09, DB-10), a well in Segeneyti (SG-07) and a borehole in Dekemhare (DK-05). The rest are found to be free from manganese induced staining problems.

J. Fluoride

Fluoride levels in excess of 1.5mg/l lead to an increase in the occurrence and severity of dental fluorosis (teeth become mottled and brittle). Normally, 1 to 2mg/l fluoride is mentained in public drinking water supplies for the prevention of dental carries in children. All the analysed samples of water showed that the sources contain optimum concentration of fluoride.

K. Copper

As Debarwa was a copper mining site, analysis of water points for copper was done to evaluate the water chemistry of the town.

The guidelines value for copper for health related considerations is 2mg/l.

All the samples analysed contain copper in the limits of the recommended value.

Conclusion Concerning Pysio-Chemical Characteristics

Generally the physio-chemical characteristics of water sources in the seven towns is evaluated as good. The few exceptions being a borehole in Adiquala (AD-06), a well in Segeneyti (SG-09), borehole and a well in Dekemhare (DK-04), (DK-10), which have electrical conductivity value greater than 1200 μ s/cm to impart disagreeable taste.

In addition, boreholes in Adi-Keyih (AK-10), Adi-Quala (AD-06), and Dubarwa (DB-05), a borehole(DK-04) and a well (DK-10) in Dekemhare, were found to contain 45.2, 89.5, 64.2, 97.4, and 51.8 mg/l nitrate respectively, which could be potentially health hazard to consumers.

2. Bacteriological Characteristics

The basic requirement for any water source to be considered as an acceptable source for drinking is that it should be freed from bacteria, virus and protozoan.

In evaluation of bacteriological safety of water, routinely testes are done to identify for organisms indicators of pollution. The coliform group of bacteria which are found in sewage, animal and human excrement are the accepted indicators of pathogenic micro-organisms.

WHO standard recommends drinking water must not contain faecal coliform bacteria. Otherwise, it is unsafe for human consumption.

Out of seventy samples analysed from the seven towns, 29 were found to be contaminated with bacteria which are faecal in origin. This shows that the sanitary conditions of the water sources and reservoirs is not well mentained. The most probable source of contamination is human and animal waste which adds up to dams, ground water sources and pipeline systems with run off, percolation and infiltration respectively.

Total coliform bacteria should not occur repeatedly in water samples in regular water quality monitoring programme. Thier presence in a single analysis, as in the case of this study, does not necessarly imply the water sources are unsafe.

Conclusion Concerning Bacteriological Characteristics

As twenty nine of the seventy sampling points were found to be bacteriologically contaminated, it can be concluded that some of the people in these towns is getting unsafe water. However, it is noteworthy to mention that high rate of contamination may be due to unusual rainfall in the area before sampling which may helped to carry/percolate human and animal waste to the sources.

To improve the situation:

- The sanitary condition of the surroundings of the water points should be improved.
- Open wells should be covered with slab and a pump installed.
- Supplies from surface water should be treated before distribution.
- Regular water quality monitoring programme should be introduced.
- Public awareness on hygiene and sanitation should be increased.

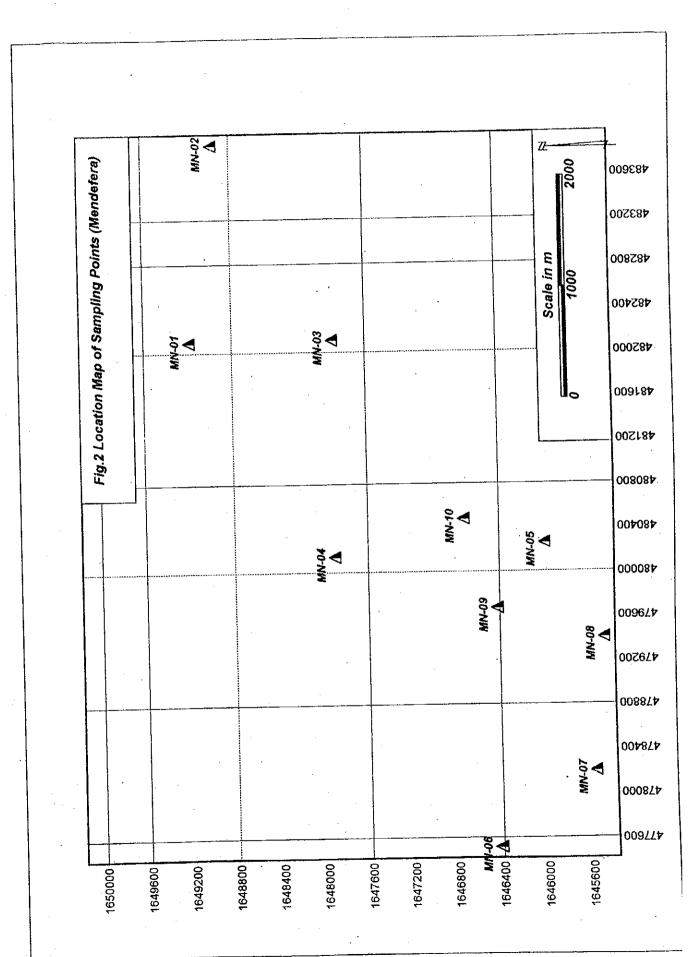
Table-2 Water Quality In Mendefera

Date Sampled 30/09/97								II. Bacteriological Quality	ical Q	<u>ality</u>			
								T.C.B = Total Coliform Bacteria	rm Bacte	eria teria			
Date Analysed 01/10/97	╞		Ŀ		1					E C B	-	Remarks	
Description	2	H Temp	0 Q Q Q	1aste	a'nı	Color	_	1.4.0		NOT A FO	+-		
us/cm	E	ي. ان			2			count/100ml, 35°c	count	countround, 44, 9 c	-	Cafe	
MN-01 Dam. Kitowite	152 7	7.5 23.	23.0 agreeable	e disagree	<u>5</u>	150 muddy		4			+		
HDW Kitowlia, not concrete	577 6	6.9 27.	27.9 agreeable	agreeable		<5 clear		0	_+	8		contarturated	5
eil	84	7.2 23	23.0 agreeable	agreeable		<5 clear		B	-	0		Safe	
		1	28.1 agreeable			<5 clear		2		56	<u>ہ</u>	contaminated	G
	1		22.5 agreeable		 	<5 clear		2		ន	-	contaminated	g
	1		6 arreable	25.6 arreable arreable	-	<5 clear		0		0		Safe	
			ideorar 3	AU.O agrocubic agreed		<5 clear	 	3		0		Safe	
ervoir at Konel				interview of	-	15 close		2		0		Safe	
MN-08 Reservoir at Forto		1	U agreeabl	23.0 agreeable agreedue	-					Manv		contaminated	ed
MN-08 Consumer's Tap	£88	7.3 26	7 agreeabl	26.7 agreeable agreeable		<5 clear	1	5	+		<u>}</u>	Safe	
III Chemical Quality						•			·				
Date Sampled 01/10/97					Ŭ,	z							
Date Analysed 14/10/97			•			<u> </u>							
Description	BW	g Na	K	۶e	Шn	HC03	204	10	Sol 1	N-NH3	NO2		_
l/oul		mg/i mg/i	l/Bm	l/bui	mg/l	mg/i) Bui	mg/l mg/l	1/6m	mg/l		-1-	2
MANLOA Dam Kilowilie	1	-	0	3.0	0.41 0.0		23	0			- 1		
MN-02 HDW, Kilowlia, not concrete	2	5	30	2.2 0.	0.01 0.0			0	<u>۳</u>		- 1	0.05 0.27	211.2
MN-C3 Underground reservoir, Kilowite	8	10	21	2.2 0.	0.09 0.0			0			- 1	1	
AM DA Main Reservolt 500 ctm		1	2	1.8	0.02 0.1	212	2	-	12				
	1	17		22	0.03	1 256	ģ	1	40	6.2			
					0.01 0.0	464		80	26 11.5	5	0.51	0.03 0.10	
					0.21 0.0	393		8	30 42.5	Ŀ.	0.43	0.01 0.21	13.0
MN-07 Underground Reservoir at Konet					Ŀ				40 20.8	8	0.54	0.01 0.22	20.9
									56 18.2	2	0.71	0.07 0.24	4 19.3
MN-09 Consumer's Tap					ŀ					19.5	0.16	0.04 0.27	7 11.8

* Note: HDW = Hand dug well BH = Borehole

J

C-19



C-20

Sec. 2

Auro

Report

on

WATER QUALITY ANALYSIS

JICA TESTING BOREHOLES IN DEBUB REGION

Fikremariam Kahsai Water Resources Department Asmara, Eritrea Feb. 19, 1998

Water Quality Evaluation of testing boreholes drilled in Debub region of JICA project

1. Mendefera :

Borehole No1 of Adimongoti is of acceptable with respect to chemical and bacteriological quality. Though manganese is present in significant concentration, it has not exceeded the WHO guidelines to cause any staining problems and, as the water is very soft it will be corrosive to pipelines. Besides, the pH is high (8.66) to make the water tastes alkaline.

2. Dubarwa :

This borehole has chemically and bacteriologically acceptable water quality although slightly hard due to calciumbicarbonate.

3. Segeneyti (SEG-01):

The water quality of this borehole is bacteriologically safe and based on the amount of total dissolved solids it is chemically acceptable for drinking. But, the concentration of manganese which is 0.4mg/l exceeds the WHO guidelines of 0.1 mg/l, therefore it will cause staining problem. The amount of ammonia though in the limits of WHO guidelines is considerable to show that there is domestic organic contamination. Furthermore it is slightly hard water which will consume considerable amount of soap for lathering.

4. Segeneyti (SEG-03) :

100

The source is bacteriologically safe for domestic water supply. Chemically the water quality is fairly good. The electrical conductivity value indicates that the dissolved solids are within the limits of WHO guidelines. Hence good quality with respect to dissolved solids. But, the source is slightly hard water and with manganese concentration exceeding the WHO guideline value to cause staining problem.

5. Adikeyih/ Tekondae (ADK-01):

The source is bacteriologically acceptable for drinking. The amount of dissolved solids indicated by the electrical conductivity value is considerable though in the limits of WHO guidelines.

The amount of ammonia is high showing sewage or organic pollution. Furthermore, the concentration of manganese is higher than WHO guideline value. The degree of clarity of the water is not satisfactory which is measured 5 NTU. Besides, it is very hard water due to calciumbicarbonate.

The source can be used as source of water supply only if no better alternative source is available.

6. Adi-Keyih/ Adiwegera (ADK-02):

The source is bacteriologically acceptable for drinking. Chemically the water quality is fairly good. The dissolved minerals is considerable though in the range of WHO guidelines and the concentration of manganese is high to cause staining in laundry and utensils. The amount of calcium is high to make the source hard water. The amount of ammonia though not exceeding WHO guidelines it indicates occurrence of organic contamination.

7. Senafe (SEN-02):

The borehole is found to contain bacteria indicators of faecal pollution. Therefore the source is bacteriologically unsafe for human consumption. Chemically, the source has good composition except for manganese (0.3 mg/l) which is exceeding the WHO guidelines of 0.1 mg/l for reasons of aesthetic.

8. Dekemhare : DEK-01 and DEK-02

These sources are found to be free from bacteriological contamination. Therefore bacteriologically safe for drinking. Chemically, though safe from health point of view, there are high concentration of calcium and magnesium to make the sources very hard water.

Table 1. Water Quality of JICA testing wells in Zoba Debub

. Physical Quality	~ 1			·				II. Bacteri	<u>II. Bacteriological Quality</u> T C B = Total Coliform Bacteria	~
e Sample	Date Sampled 05.01.98 = 30.01.98	98 - 30.0 290 - 80	1.98 29,08					F.C.B = Faec	F.C.B = Faecal Coliform Bacteria	
t Taba		14	Tamp	Odor	Taste	Turb	Turb Color	T.C.B	F.C.B	Remarks
Meli Iau Sub-Luna						NTU		count/100ml,35°c	count/100ml,44.6°c	
	us/cm	9	4	22.4 aureeahle	acreeable	0	0 clear	0	0	safe
Menderera	8			1	- deces	Ċ	O clear	0	0	safe
Dubarwa	762	₹. 1		22.2 agreeable	allecante					cafe
Segenevti	832	98.9		24.0 agreeable	agreeable	0	0 clear			2000
annadi	101	£ 74		22.5 agreeable	agreeable	0	clear	0	0	sale
oedenedin			1			ľ	5 middu	0	0	safe
Adi-Keyih	90	6.85		21.4 agreeable	agrecable	2	(mnnii)			
Adi-Kevih	948	6.77		20.7 agreeable	agreeable	0	0 clear	D		sale
Canala	PEL	ļ		21.5 agreeable	agreeable	0	0 clear	many	8	contaminated
EI GI C	5	1						C		safe
Dekemhare	1247	7.10		22.7 agreeable	agreeable	2	clear			0.00
Pelombaro	1181	E01	_	22 6 anreathe	acreeable		0 clear	5		2916

III. Chemical Quality Date Sampled 05.01.98 - 12.02.98

Sub-Zoba Ca Mg Na K Fe Mn HCO3 S04 Cl NO3 N·NH3 NO2 T Induitedent mg/l read h Mendetera 2.9 0.7 92.4 0.7 0.02 0.1 122.0 34.0 60.0 4.9 0.01 0.06 0.26 Dubarwa 86.0 37.7 42.9 7.6 0.05 0.4 42.0 85.0 45.0 1.3 0.54 0.16 0.26 Segenetyli 96.0 37.7 42.9 7.6 0.05 0.4 42.0 85.0 1.3 0.54 0.06 0.16 0.26 0.04 0.16 0.05 0.16 0.05 0.4 0.0 1.1 0.54 0.01 0.54 0.05 0.16 0.05 0.16 0.05 0.13 0.55 0.1 1	Ca Mg Na K Fe Mn HCO3 SO4 Cl NO3 N-M13 NO2 T Trationastic mg/l read h 2.9 0.7 92.4 0.7 0.02 0.1 122.0 34.0 60.0 4.9 0.01 0.05 0.4 86.0 37.7 42.9 7.6 0.05 0.4 420.0 35.0 10.6 0.02 0.34.0 66.0 4.9 0.01 0.26 7 96.0 37.7 42.9 7.6 0.05 0.4 420.0 32.0 30.0 10.6 0.02 0.16 0.02 124.0 10.26 0.049 0.42 122 124.0 10.26 0.049 0.42 122 110.0 30.54 0.000 1.22 124.0 10.56 0.049 0.42 124 124 122<	Ca Mg Na K Fe Mn HCO3 SO4 CI NO3 N-NH3 NU2 T Induinasion mg/i ref Induinasion C4 0 V 0.26 V		Date Analysed 13.01.96 - 18.02.90	ed 13.01.	98 - 18.	08.20		}					ſ		1			and the state
mg/l mg/l <t< th=""><th>mg/l mg/l <t< th=""><th>mg/l mg/l <th< th=""><th>Wall Idat</th><th>Sub-Zoha</th><th>S</th><th>Ma</th><th>Na</th><th>×</th><th>ů,</th><th></th><th>Мл</th><th></th><th>S04</th><th>5</th><th>NO3</th><th>- 1</th><th>NUZ</th><th></th><th>Laruness</th></th<></th></t<></th></t<>	mg/l mg/l <t< th=""><th>mg/l mg/l <th< th=""><th>Wall Idat</th><th>Sub-Zoha</th><th>S</th><th>Ma</th><th>Na</th><th>×</th><th>ů,</th><th></th><th>Мл</th><th></th><th>S04</th><th>5</th><th>NO3</th><th>- 1</th><th>NUZ</th><th></th><th>Laruness</th></th<></th></t<>	mg/l mg/l <th< th=""><th>Wall Idat</th><th>Sub-Zoha</th><th>S</th><th>Ma</th><th>Na</th><th>×</th><th>ů,</th><th></th><th>Мл</th><th></th><th>S04</th><th>5</th><th>NO3</th><th>- 1</th><th>NUZ</th><th></th><th>Laruness</th></th<>	Wall Idat	Sub-Zoha	S	Ma	Na	×	ů,		Мл		S04	5	NO3	- 1	NUZ		Laruness
mg/r 0.7 92.4 0.7 90.07 90.4 50.0 31.0 10.6 0.02 0.340 0.18 0.24 0.26 0.048 0.12 23.40 0.18 0.07 0.16 0.07 0.14 25.0 30.0 10.6 0.07 0.26 0.049 0.42 0.22 Segenetyi 102.0 32.8 35.2 0.6 0.07 0.4 55.0 34.0 71 0.54 0.000 1.22 Adi-Keylh 124.0 47.4 51.2 0.6 0.02 0.34 35.0 35.0 10.6 0.07 0.38 55.1 34.0 71 0.26 0.049 0.42	mg/r mg/r <th< th=""><th>mg/r mg/r <th< th=""><th></th><th>DAULT-VIDE</th><th>5</th><th></th><th></th><th>1/200</th><th></th><th></th><th>-</th><th>ma/l</th><th>ma/l</th><th> </th><th>l/bu</th><th></th><th></th><th>-</th><th>*G.d.h</th></th<></th></th<>	mg/r mg/r <th< th=""><th></th><th>DAULT-VIDE</th><th>5</th><th></th><th></th><th>1/200</th><th></th><th></th><th>-</th><th>ma/l</th><th>ma/l</th><th> </th><th>l/bu</th><th></th><th></th><th>-</th><th>*G.d.h</th></th<>		DAULT-VIDE	5			1/200			-	ma/l	ma/l		l/bu			-	*G.d.h
Mendetera 2.9 0.7 92.4 0.7 0.02 0.1 122.0 34.0 0.01 0.01 0.02 0.18 Dubarwa 86.0 32.8 30.8 0.5 0.04 0.0 427.0 32.0 30.0 0.6 0.02 0.340 0.18 Segeneyti 96.0 37.7 42.9 7.6 0.05 0.4 420.9 88.0 45.0 1.3 0.54 0.00 1.22 Segeneyti 102.0 32.8 35.2 0.6 0.07 0.4 555.1 34.0 40.0 7.1 0.26 0.42 Adi-Keylh 124.0 47.4 51.2 0.6 0.02 0.4 48.0 75.0 32.5 2.7 1.11 0.009 0.62 0.64 0.65 0.64 0.65 0.64 0.65 0.64 0.66 0.62 0.64 0.66 0.64 0.65 0.64 0.66 0.64 0.65 0.64 0.65 0.64	Mendetera 2.9 0.7 92.4 0.7 0.02 0.1 122.0 34.0 0.01 0.01 0.02 0.16 0.02 0.16 0.01 0.02 0.18 0.01 0.02 0.18 0.01 0.02 0.340 0.16 0.02 0.340 0.16 0.02 0.340 0.16 0.02 0.340 0.16 0.02 0.340 0.16 0.02 0.340 0.16 0.02 0.340 0.16 0.02 0.340 0.16 0.02 0.340 0.16 0.02 0.340 0.16 0.02 0.340 0.16 0.02 0.340 0.122 Segeneyti 102.0 32.8 35.2 0.06 0.07 0.4 55.0 32.5 2.7 1.11 0.00 0.05 0.4 20.7 50.0 1.65 0.007 0.36 0.62 0.62 0.62 0.62 0.62 0.62 0.62 0.62 0.62 0.62 0.62 0.62 0.62 0.62<	Mendetera 2.9 0.7 92.4 0.7 0.02 0.1 122.0 34.0 0.01 0.01 0.02 0.18 Dubarwa 86.0 32.8 30.8 0.5 0.04 0.0 427.0 32.0 30.0 10.6 0.02 0.340 0.18 Segeneyti 96.0 37.7 42.9 7.6 0.05 0.4 420.9 88.0 45.0 1.3 0.54 0.00 1.22 Segeneyti 102.0 32.8 35.2 0.6 0.07 0.4 556.1 34.0 40.0 7.1 0.26 0.42 Adi-Keylih 110.0 30.4 56.1 0.6 0.02 0.3 0.71 0.07 0.36 Senate 82.0 7.3 40.7 4.5 0.02 0.18 0.60 0.67 0.36 0.67 0.52 0.54 0.55 1.11 0.000 0.57 0.54 0.56 0.56 0.56 0.56 0.56			ingui	uñu	1/huu	1/Ruu	1	1			[2	ž	0.05	050
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Appendix C~6

Groundwater Monitoring Data

Groundwater monitoring data

	ater monitori	-					MENDEFERA(NO.4) a	+ 6-00 am	
planet and sold and s	ERA(NO.2) a			MENDEFER(NO.3) a		from G.L.	Date	Reading	from G.L
	ate	Reading	from G.L	Date (10:23)3/7	Reading 2m65.0	-2.650	(14:30)3/7	2m78.0	-2.780
(1	6:08)3/7	8m48.8	-8.488		2m63.0 2m63.2	-2.632	1998/3/8	2m79.0	-2.790
	1998/3/8	8m48.8	-8.488 -8.491	1998/3/8 1998/3/9	2m62.0	-2.620	1998/3/9	2m80.2	-2.802
	1998/3/9 1998/3/10	8m49.1 8m49.3	-8.497	1998/3/10	2m62.2	-2.622	1998/3/10	2m81.0	-2.810
		8m49.9	-8.493	1998/3/11	2m62.7	-2.627	1998/3/11	2m82.0	2.820
	1998/3/11	8m50.0	-8.499	1998/3/12	2m62.1	-2.261	1998/3/12	2m83.0	-2.830
	1998/3/12 1998/3/13	8m49.9	-8.499	1998/3/13	2m61.5	-2.615	1998/3/13	2m84.0	2.840
	1998/3/14	8m49.8	-8,498	1998/3/14	2m61.2	-2.612	1998/3/14	2m84.8	2.848
	1998/3/15	8m49.5	-8.495	1998/3/15	2m60.0	-2.600	1998/3/15	2m85.1	~2.851
	1998/3/16	8m49.0	-8.490	1998/3/16	2m62.2	-2,622	19 9 8/3/16	2m79.0	-2.790
	1998/3/17	8m48.6	-8.486	1998/3/17	2m63.2	-2.632	1998/3/17	2m79.0	-2.790
	1998/3/18	8m47.9	-8.479	1998/3/18	2m62.1	-2.621	1998/3/18	2m79.0	-2.7 9 0
	1998/3/19	8m47.6	-8.476	1998/3/19	2m61.0	-2.610	1998/3/19	2m79.1	-2.7 9 1
	1998/3/20	8m47.2	-8.472	1998/3/20	2m60.0	-2.600	1998/3/20	2m79.1	-2.791
	1998/3/21	8m46.8	-8.468	1998/3/21	2m60.4	-2.604	1998/3/21	2m80.0	-2.800
	1998/3/22	8m46.1	-8.461	1998/3/22	2m60.0	-2.600	1998/3/22	2m80.0	-2.800
	1998/3/23	8m45.8	-8.458	1998/3/23	2m58.6	-2.586	1998/3/23	2m80.0	-2.800
	1998/3/24	8m45.4	-8.454	1998/3/24	2m59.2	-2.592	1998/3/24	2m80.0	-2.800
	1998/3/25	8m45.1	-8.451	1998/3/25	2m60.1	-2.601	1998/3/25	2m80.1	-2.801
	1998/3/26	8m44.9	~8.449	1998/3/26	2m60.4	-2.604	1998/3/26	2m80.1	-2.801
	1998/3/27	8m44.4	-8.444	1998/3/27	2m59.2	-2.592	1998/3/27	2m80.1	-2.801
	1998/3/28	8m44.0	-8.440	1998/3/28	2m62.2	-2.622	1998/3/28	2m80.2	-2.802
j	1998/3/29	8m43.8	-8.438	1998/3/29	2m64.5	-2.645	1998/3/29	2m80.2	-2.802
	1998/3/30	8m42.9	-8.429	1998/3/30	2m65.3	-2.653	1998/3/30	2rn80.2	-2.802
	1998/3/31	8m42,5	-8.425	1998/3/31	2m67.9	-2.679	1998/3/31	2m80.3 2m80.3	-2.803 -2.803
	1998/4/1	8m42.0	-8.420	1998/4/1	2m69.2	-2.692	1998/4/1	2m80.3	-2.803
	1998/4/2	8m42.0	-8.420	1998/4/2	2m70.7	-2.707	1998/4/2 1998/4/3	2m80.3	-2.803
	1998/4/3	8m42.0	-8.420	1998/4/3	2m71.2 2m71.8	-2.712 -2.718	1998/4/4	2m80.3	-2.803
	1998/4/4	8m42.0	-8.420	1998/4/4	2m71.8 2m71.0	-2.710	1998/4/5	2m80.4	-2.804
	1998/4/5	8m42.0	-8.420	1998/4/5 1998/4/6	2m71.0 2m69.6	~2.696	1998/4/6	2m80.4	-2.804
	1998/4/6	8m39.8	-8.398 -8.396	1998/4/7	2m70.7	-2.707	1998/4/7	2m99.0	-2.990
	1998/4/7 1998/4/8	8m39.6 8m39.2	-8.390	1998/4/8	2m71.3	-2.713	1998/4/8	2m98.9	-2,989
	1998/4/9	8m38.9	-8.389	1998/4/9	2m71.6	-2.716	1998/4/9	2m98.9	-2,989
	1998/4/10	8m38.8	-8.388	1998/4/10	2m71.6	-2.716	1998/4/10	2m98.9	-2,989
	1998/4/11	8m38.0	-8.380	1998/4/11	2m71.2	-2.712	1998/4/11	2m98.9	-2.989
	1998/4/12	8m37.9	-8.379	1998/4/12	2m71.0	-2.710	1998/4/12	2m98.9	-2,989
	1998/4/13	8m37.3	-8.373	1998/4/13	2m69.8	-2.698	1998/4/13	2m99.0	-2.990
	1998/4/14	8m37.0	-8.370	1998/4/14	2m70.5	-2.705	1998/4/14	2m99.0	-2.990
	1998/4/15	8m36.8	-8.368	1998/4/15	2m71.1	-2.711	1998/4/15	2m99.0	-2.990
	1998/4/16	8m36.0	-8.360	1998/4/16	2m71.1	-2.711	1998/4/16	2m99.0	
	1998/4/17	8m35.7	-8.357	1998/4/17	2m71.3	-2.713	1998/4/17	2m 9 9.0	-2.990
	1998/4/18	8m35.4	8.354	1998/4/18	2m69.1	-2.691	1998/4/18	2m99.0	-2.990
	1998/4/19	8m35.5	~8,355	1998/4/19	2m67.5	-2.675	1998/4/19		
	1998/4/20	8m34.7	8.347	1998/4/20	2m66.1	-2.661	1998/4/20		
	1998/4/21	8m34.2	-8.342	1998/4/21	2m68.7	-2.687	1998/4/21	2m99.0	
	1998/4/22	8m33.7	-8.337	1998/4/22	2m69.1	-2.691	1998/4/22		
	1998/4/23		-8.333	1998/4/23	2m69.2	-2.692	1998/4/23		5
	1998/4/24		-8.330	1998/4/24	2m69.0	-2.690	1998/4/24		
	1998/4/25		-8.328	1998/4/25	2m69.2	-2.692	1998/4/25		· · · · · ·
	1998/4/26		-8.322	1998/4/26	2m66.6	-2,666	1998/4/20	·	
ļ	1998/4/27		-8.319	1998/4/27	2m66.9	-2.669	1998/4/28		
	1998/4/28		-8.313		2m68.6	~2.686 2.700	1998/4/29		
	1998/4/29		-8,310		2m70.0 2m69.6	-2.700	1998/4/30		
	1998/4/30				2m69.6	-2.696	1998/5/1		
	1998/5/1		-8.303	- F		-2.096	1998/5/2		
	1998/5/2					-2.721	1998/5/3		
	1998/5/3 1998/5/4						1998/5/4		
	1998/5/4				1 A A A A A A A A A A A A A A A A A A A		1998/5/5		
	1998/5/6						1998/5/6		
	1998/5/7						1998/5/7		
1	1998/5/8						1998/5/8		
1	1998/5/9						1998/5/9		
1	1998/5/10						1998/5/10		
i	1998/5/11						1998/5/11	2m98.0	-2.980
ſ				•					

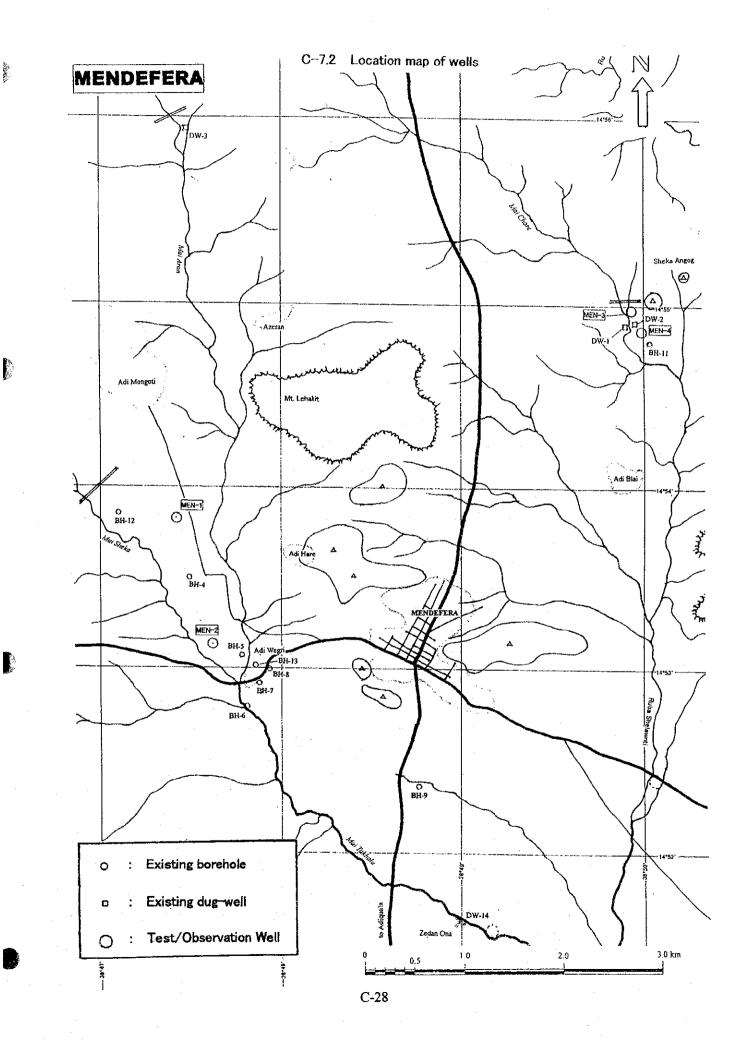
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1	1998/5/12	8m26.3	-8,263	1998/5/12	3m17.2	-3.172	1998/5/12	2m98.0	2.980	
	1998/5/13	8m26.0	-8.260	1998/5/13	3m17.2	-3.172	1998/5/13	3m00.1	-3,001	
	1998/5/14	8m25.6	-8,256	1998/5/14	3m17.2	~3.172	1998/5/14	3m00.1	-3.001	
	1998/5/15	8m25.4	-8.254	1998/5/15	3m17.2	-3.172	1998/5/15	3m00.1	3.001	
	1998/5/16	8m25.0	-8,250	1998/5/16	3m30.3	-3.303	1998/5/16	3m68.9	-3.689	
	1998/5/17	8m24.7	-8,247	1 99 8/5/17	3m31.3	-3.313	1998/5/17	3m69.0	-3.690	
	1998/5/18	8m24.2	-8.242	1998/5/18	3m33.0	-3.330	1998/5/18	3m70.8	-3.708	
	1998/5/19	8m23.9	-8.239	1998/5/19	3m35.7	-3.357	1998/5/19	3m70.8	-3.708	
	1998/5/20	8m23.5	-8,235	1998/5/20	3m30.2	-3.302	1998/5/20	3m73.7	-3.737	
	1998/5/21	8m23.0	-8.230	1998/5/21	3m37.5	-3.375	1998/5/21	3m73.0	-3.730	
	1998/5/22	8m22.7	-8.227	1998/5/22	3m38.7	-3.387	1998/5/22	3m73.0	-3.730	
1	1998/5/23	8m22.3	-8.223	1998/5/23	3m40.8	-3.408	1998/5/23			
	1998/5/24	8m22.0	-8.220	1998/5/24	3т40.8	-3.408	1998/5/24			
	1998/5/25	8m21.8	-8.218	1998/5/25	3т39.0	-3.390	1998/5/25			
	1998/5/26	8m21.5	-8.215	1998/5/26	3m38.4	-3.384	1998/5/26		ł	
1	1998/5/27	8m21.0	-8.210	1998/5/27	3m38.4	-3.384	1998/5/27	2m76.8	-2.768	
	1998/5/28	8m20.8	-8.208	1998/5/28	3m38.0	-3.380	1998/5/28	2m76.0	-2.760	
	1998/5/29	8m20.2	-8.202	1 9 98/5/29	3m37.9	-3.379	1998/5/29	2m75.6	-2.756	
	1998/5/30	8m20.0	-8.200	1998/5/30	3m37.7	-3.377	1998/5/30	2m75.1	-2.751	
	1998/5/31	8m19.8	-8.198	1998/5/31	3m37.0	3.370	1998/5/31	2m74.6	-2.746	
	1998/6/1	8m19.3	-8.193	1998/6/1	3m36.9	-3.369	1998/6/1	2m74.2	-2.742	
	1998/6/2	8m19,1	-8.191	1998/6/2	3m36.5	-3.365	1998/6/2	2m74.5	-2.745	
	1998/6/3	8m19.0	-8.190	1998/6/3	3m36.7	-3.367	1998/6/3	<u>2</u> m74.8	-2.748	
	1998/6/4	8m18.8	-8.188	1998/6/4	3m36.3	-3.363	1998/6/4	2m75.0	-2.750	
	1998/6/5	8m18.3	-8.183	1998/6/5	3m36.4	-3.364	1998/6/5	2m75.0	-2.750	
	1998/6/6	8m18.0	~8.180	1 998/ 6/6	3m36.4	-3364	1998/6/6	2m74.9	-2.749	
·	1998/6/7	8m17.5	-8.175	1998/6/7	3m36.4	-3.364	1998/6/7	2m74.8	-2.748	
	1998/6/8	8m17.1	-8.171	1998/6/8	3m34.0	-3.340	1998/6/8	2m74.7	-2.747	
	1998/6/9	8m16.9	-8.169	1998/6/9	3m32.7	-3.327	1998/6/9	2m74.1	-2,741	
	1998/6/10	8m16.4	-8.164	1998/6/10	3m31.3	-3.313	1998/6/10	2m73.9	-2.739	
· · ·	1998/6/11	8m16.1	-8.161	1998/6/11	3m30.2	-3.302	1998/6/11	2m74.0	-2.740	
	(10:40)6/11	8m16.0	-8.160	(11:15)6/11	<u>3m30.0</u>	-3.300	(11:30)6/11	2 <u>m73.2</u>	-2.732	

Appendix C-7 Well Inventory Study C-7.1 Well Inventory

			c				MENDEEDA	V											
Table 2	Well Inventory	2	~			-									Γ	- mind	-Remarkey	<well ident.<="" td=""><td></td></well>	
<well ident=""></well>	<location></location>	<altitute> <latitude: (m) deg nin sec </latitude: </altitute>	<latitude: <longi.=""> deg nin sec deg nin sec</latitude:>	ade: sec de	<longt< td=""><td>Sec. 1</td><td>> <wateruse> <constr. <dcpth3<diameter3="" <water<br="">year> (m) (m) evel(m)></constr.></wateruse></td><td><constr. <<="" td=""><td>(Deptha (m)</td><td>Diameters (II)</td><td></td><td><yield> EC(micro (l/min) S/cm)</yield></td><td>EC(micro S/cm)</td><td>£</td><td><rump system></rump </td><td>status></td><td>-trentat Na-</td><td>of WRD></td><td></td></constr.></td></longt<>	Sec. 1	> <wateruse> <constr. <dcpth3<diameter3="" <water<br="">year> (m) (m) evel(m)></constr.></wateruse>	<constr. <<="" td=""><td>(Deptha (m)</td><td>Diameters (II)</td><td></td><td><yield> EC(micro (l/min) S/cm)</yield></td><td>EC(micro S/cm)</td><td>£</td><td><rump system></rump </td><td>status></td><td>-trentat Na-</td><td>of WRD></td><td></td></constr.>	(Deptha (m)	Diameters (II)		<yield> EC(micro (l/min) S/cm)</yield>	EC(micro S/cm)	£	<rump system></rump 	status>	-trentat Na-	of WRD>	
+ 1994	Downstream of	T .	14 54 53 38	53.3	8 49		Public W/S 49 54 Mendefera	1994	5.1	9.05	s		634	7.00	Motor (YANTMAL) Functional	Functional			
	Downstream of	0201	14 54	54 3		56 h	Public W/S 49 56 Mcndefera	Italian period	5.1	8	4.8		542	7.25	Motor(LAM BHRUDINI)	Functional			
	Downstream of Mai Aron dam	2050	14 55	56	+	1 29	47 29 Mendefera	1997	1.6	Ś	0		584	7.35	Motor(LAM Not yet BHRDINI) installe		Public W/S in dry season only		
	Adi Moneoti	2000	53	30,38	<u></u>	291		Ethiopia n period	60	0.2032			1085	7.14	Submersible (LESTER)	Functional			
	Near electric	1005	14 53	9 9 9		47		Ethiopia n period	30				972	7.59	Submersible (LESTER)	Functional			
	powel statuti Mai Tabhala	1985	14 52	47		64	[1997	62						Capped	Capped			
1.	1 10 M	, cou					47 53 Out of use	Italian ncriod	U9	0.15	6.67				Out of use	Out of use			
	Mai Takhala	0661 1001	0 25 41		20 47 29 47 74 47		47 56 Domestic	£661		0.15			638	9.23	Hand (India Mark II)	Functional			
BH-8	Mai Jakhaja Noor stadium	1994	14 52			4	46 Capped	1996	60	0.1905		•			Capped	Capped			
BH-10	Ziban Una	1920	14 50	5		-	Capped	1997	72 ¹⁾	-					Capped	Capped			
RH_11	Downstream of K ilowlie dam	1969	14 54	54 48 3	38 50		2 Capped	9661	3						Out of use	Out of use			
BH-12	Adi Mongoti	2003	14 53	14 53 51 38	8 47			Ethiopia 11 period	99	2602.0									
BU.13	Adi Weeni	1995	14 53	· +=	38 47	151	51 Capped	1996	68	0.2032									
Date surveye Well ident : Bracket of co	Date surveyed : mainly 10 Oct., 1997 Date surveyed : mainly 10 Oct., 1997 Well ident. : BH:Borehole, DW:Dug well, R:Reservoir Bracket of construction year : year of repair	, 1997 V:Dug well, ear of repair	R.Re	servoi	1	1	 Drilling data of the Sector Study Bracket of Wpt. Diameter : inside diameter 	data of the /pt. Diame	: Sector	- Study side diamete	ŀ		Bracket o	î pump sı	Bracket of pump system : pump type and capacity	type and cal	acity		

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Appendix C-8 Technical Specification of Production Well

1. SCOPE OF WORKS

1.1. OBJECTIVES OF WORKS

1.2. CONTENTS OF WORKS

The content of works under this Contract consists of as below:

- Mobilization and Demobilization to/from the survey area, inclusive of moving from the Site to Site, and Site preparation.
- (2) Production Well Drilling; Drilling works, inclusive of a drilling, borehole logging, casing installation, gravelpacking, grout-sealing, development, head works, etc.
- (3) Pumping Test, composed of Preliminary, Step-drawdown, Constant discharge, and Recovery tests, inclusive of water sampling and water quality analysis.
- (4) Reporting, inclusive of daily drilling records, borehole and lithological logs, pumping test records, photographs, sketches, and so forth.

1.3. MEASUREMENT AND PAYMENT

The measurement and payment for the works carried out by the Contractor shall be made in accordance with the quantity actually worked out by the Contractor and confirmed by the Engineer's (Consultant's supervisor) measurement; and the unit or lump sum price specified in the Bill of Quantities, APPENDIX-___ of the Contract.

The unit or lump sum price specified in the Bill of Quantities shall be deemed to involve every costs necessary for the appropriate item of work inclusive of personnel, machinery amortization, consumable and permanently installed materials, overhead, profit, tax, duties and so forth. No extra payment shall be made for the lump sum price in case the quantities of works specified in the Bill of Quantities may be increased or decreased.

2. LOCATION OF WORKS

The works under this Contract are to be carried out in and around the six (6) towns as shown in the Figure-A "Location Map of the Drilling Works" attached.

The exact well drilling sites are to be indicated in-situ to the Contractor by the Engineer prior to the mobilization of drilling equipment.

3. EQUIPMENT, TOOLS, DEVICES AND MATERIALS TO BE EMPLOYED

3.1. GENERAL

The equipment, sampler, tools, measuring devices, and materials to be employed to the works under this Contract shall be provided by the Contractor, excepting water sampler for water quality analysis, and water quality meters for in-situ water quality test which are to be provided by the Study Team.

The Contractor shall submit, prior to the mobilization to the area, a list of equipment, samplers, and major tools, describing the model, type, capacity, specification, quantities to the Engineer for his approval.

3.2. SCREEN AND BLANC CASING

Blank casing pipes for the wells shall be made of PVC with inner-diameter of 6 inches. Screen pipes to be installed in the wells shall also be made of PVC with 6 inches diameter and of open ratio of more than ten percent (10%).

3.3. CENTRALIZER AND BOTTOM PLUG

Centralizer and bottom plug shall be of the same material and diameter of above mentioned pipes.

4. WORKS

4.1. MOBILIZATION AND DEMOBILIZATION

The Contractor shall mobilize and demobilize the personnel, equipment, tools, devices, and materials necessary for the works under this Contract to/from the work area under the Project from/to the Contractor's base within Eritrea.

The Contractor shall prepare the drilling sites to suite for the erection of equipment, working space, and others.

Further, the Contractor shall make moving the drilling equipment and others from a site to another site.

4.2. DRILLING OF WELLS

4.2.1. DRILLING

(1) Drilling Site

The exact site of well to be drilled is indicated in-situ to the Contractor by the Engineer prior to the mobilization to the area.

Upon the Engineer's indication, the Contractor shall mark out the point by means of wooden

or stone stake with the Well Number.

(2) Type of Well

The standard type of well is shown as the Figure-___ "Standard Well Structure", and explained as follows:

The well shall consist of blank casing, slotted screen, and bottom plug of PVC pipes in 150 mm (6 inches) diameter.

The drilling diameters, the bit size, shall be good enough for the casing and gravel-packing, and be not less than 240 mm (9-5/8 inches) except surface casing portion which required to drill by 317 mm (12-1/2 inches) or more larger size bit.

The depth of the well shall be just covering the aquifer portion and as instructed by the Engineer.

(3) Quantities of Drilling Works

The work quantities in the initial plan are as shown in the Table-_____ "Summary of the Works" and Table-_____ "Drilling Site and Plan" attached. The depth of each well and the total quantities are to be modified on the course of works in accordance with the Engineer's instruction. The unit and lump sum prices in the related items of the Bill of Quantities (APPENDIX-_____ of the Contract) shall never be revised even if the said modification may take place.

(4) Drilling Works

The drilling of well shall be carried out by fluid-circulating direct rotary and/or the down-thehole method or other method approved by the Engineer. The circulating fluid shall be as thin as possible except under an artesian condition.

The surface casing pipe at the top six (6) meter portion of all wells shall be installed to control sloughing and to ensure good condition to make the grout-sealing.

(5) Sampling

The drill-cut sampling about a half (0.5) kg in weight shall be collected at an interval of every one (1) meter and every change of formation encountered. The sample collected shall be put into a plastic bag together with a tag marked the Well Number and the depth collected. The sample corrected shall be submitted to the Engineer for his inspection for casing program immediately after the completion of well drilling.

(6) Daily Drilling Record

The Contractor shall provide the daily drilling record in a form approved by the Engineer

describing water level before and after the daily drilling work, drilling rate, characteristics of drill-cut, loss or increase of drilling fluid, and so forth. The record shall be submitted to the Engineer upon the completion of drilling of any well.

4.2.2. BOREHOLE LOGGING

Immediately after the completion of well drilling to the designated depth, the Contractor shall make borehole logging.

The logging items shall be of 1) resistivity (long and short) and 2) Spontaneous Potential (SP). The borehole log thus measured shall be submitted to the Engineer, immediately after completion of the logging, for his examination and formulation of the casing program.

4.2.3. INSTALLATION OF CASING AND SCREEN PIPES

On the basis of the results obtained from lithological and borehole logs; and so forth, the casing program shall be finally decided by the Engineer. In accordance with the Engineer's instruction on casing program, the Contractor shall install, in the center of the borehole, bottom plug, screen and blank casing pipes into the drilled hole. The centralizer shall be attached to the said pipes at every twelve (12) meters interval from the bottom or as instructed by the Engineer.

4.2.4. GRAVEL-PCKING AND GROUT-SEALING

(1) Gravel-packing

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Immediately after the casing installation is over, gravel-packing shall be carried out into the annular space between the pipes installed and the hole.

The packing gravel shall be composed of siliceous materials and selected gradation, approved by the Engineer prior to the installation work.

The most care shall be paid dropping gravel at equal rate and shaking the pipes to avoid sticking and bridging of gravel at the annular apace and/or the centralizer.

Upon the Engineer's instruction, drill-cut or impervious materials may be packed at the blank casing portion.

(2) Grout-sealing

The Contractor shall seal by means of cement or mortar grouting the annular space between the hole and casing pipes at the upper-most six (6) meters portion of the borehole.

4.2.5. DEVELOPMENT

Immediately after the gravel-packing is over, the borehole shall be developed by means of

jetting, surging by water or air, and water lifting by air or other appropriate manners. Borehole development shall be lasted when the lifted water is judged to be free from mud, sand, and other suspensions, and otherwise instructed by the Engineer, but for at least 24 hours.

4.2.6. PUMPING TEST

(1) Equipment and devices

The Contractor shall provide a proper pump and its attachment to be utilized for the pumping test. The type, name, capacity, and its specification shall be noticed to the Engineer for his approval prior to carry it to the site.

For measurement of discharge, the Contractor shall provide a calibrated wear, orifice or venture meter and/or accurate associated piezometer.

Water level in the well shall be measured by electric detective devices.

The pumped water shall be led and released at the position enough far from the teat well, not to disturb the test by re-infiltration, by proper conduit or through other suitable means.

(2) Preliminary Test

After setting of all equipment and devices, the pumping equipment shall be calibrated at various pumping rates in order to ensure that all the equipment are properly functioning and to select the pumping rate for the subsequent step-drawdown test, the drawdown and yield shall be presumed through the test.

The pumping rate shall be modified according to the drawdown at the pumping well, and the preliminary pumping shall be continued at least four (4) hours.

The static water level of both pumping and observatory well (if exist) shall be measured carefully before any pumping, and the tests described below shall be started after the water level recovered to the original water level.

(3) Step-drawdown Test

The borehole shall be pumped continuously at least three (3) increasing and two (2) decreasing discharge rates, maintaining each rate at a water level to be stable, but at least more than 180 minutes.

The pumping rate of each step shall be instructed by the Engineer based on the result of preliminary test.

For each pumping discharge, the water level at the borehole shall be measured and recorded in the manner shown below;

<u>Period</u>	Interval of recording
0 – 5 min.	30 sec.
5 – 15 min.	l min.
15 – 30 min.	5 min.
30 – 90 min.	10 min.
after 360 min.	30 min.

(4) Constant Discharge Test and Recovery Test

Pumping shall be continued at least 48 hours without any interruption. The constant discharge rate shall be instructed by the Engineer.

Water level of the borehole shall be measured and recorded during full pumping and recovery period. The measurement of recovery can be stopped when the recovery attains to the static water level.

The water level shall be measured and recorded as following time interval;

<u>Period</u>	Interval of recording
0 – 5 min.	30 sec.
5 – 15 min.	1 min .
15 – 30 min.	5 min.
30 – 180 min.	15 min.
180 – 360 min.	30 min.
360 – 900 min.	60 min.
after 900 min.	120 min

(5) Test Record

The Contractor shall submit the pumping test records, in a proper forms of hard-printed and floppy-disk-base approved by the Engineer, within three (3) days after the completion of any pumping test to the Engineer.

(6) In-situ Water Quality Analysis

The Contractor shall make a series of in-situ water quality test of water temperature, pH, EC, and so forth, and take water sample for laboratory water quality analysis, during the constant discharge test.

(7) Laboratory Water Quality Analysis

The Contractor shall send water samples to the laboratory of WRD, immediately after the

sampling. The items to be analyzed are as follows, and the cost on the analysis shall be born by the Contractor.

Cations: Ca, Mg, Na, K, Fe

Anions: HCO₃, CO₃, SO₄, Cl, NO₃

Others: Mn, NO₂, PO₄, F, B, SiO₂, N-NH₃

Physical Properties: TDS, Hardness, Conductivity, pH

Bacteriologic properties: Total coliform bacteria, Faecal coliform bacteria

4.2.7. HEADWORK

Upon the completion of all the works specified above, the Contractor shall place the concrete pad and well-cap to the wells as the following manners;

(1) Concrete Pad

The dimension of concrete pad for the well shall be 1.00 m of wide, 1.00 m of long, both centered by the drilled well, and 0.50 m of deep, or otherwise instructed by the Engineer. The concrete mix of the Portland cement, fine and coarse aggregates, by volume ratio, shall be of 1.2:4 or as instructed by the Engineer.

(2) Well-cap

All the wells completed shall be covered by cap. The design, dimension, size and type of cap shall be approved by the Engineer prior to actual providing.

(3) Installation of Automatic water-level recorder

The Contractor shall install total _____ of automatic water-level recorders provided by WRD into _____ monitoring wells existing or drilled under this Contract. Details on hook, wire, method to set, etc., shall be proposed by the Contractor for Engineer's approval prior to the installation work.

4.2.8. SITE CLEARANCE

On the completion of all the works in the field, the Contractor shall remove all equipment and materials concerned, clean up the site as almost same as original states before the commencement of the works.

4.2.9. REPORTING

The Contractor shall provide the following reports and records, and on all occasions submit them to the Engineer,

(1) Daily Reports

- Daily drilling record
- Daily work record

(2) Results

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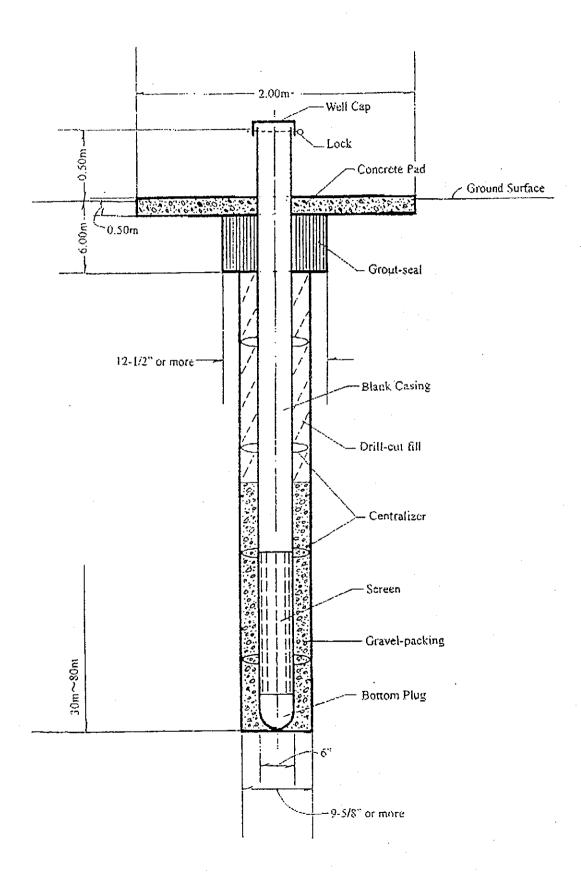
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- Drilling logs
- Lithological logs
- Borehole logs
- Pumping tests

(3) Color photograph (or sketch by the instruction)

- Typical work operation
- Site views
- Equipment, measuring devices and materials
- Other related to the execution of the works and indicated by the Engineer.

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Appendix C-9

Standard Design of Production Well

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