

JAPAN INTERNATIONAL COOPERATION AGENCY

MINISTRY OF PUBLIC WORKS, TOURISM AND

TERRESTRIAL TRANSPORT

REPUBLIC OF ALBANIA

THE STUDY
ON
THE SEWERAGE SYSTEM
IN
METROPOLITAN TIRANA
IN
THE REPUBLIC OF ALBANIA

FINAL REPORT

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JAPAN INTERNATIONAL COOPERATION AGENCY

MINISTRY OF PUBLIC WORKS, TOURISM AND

TERRITORY ADJUSTMENT

REPUBLIC OF ALBANIA

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SUPPORTING REPORT

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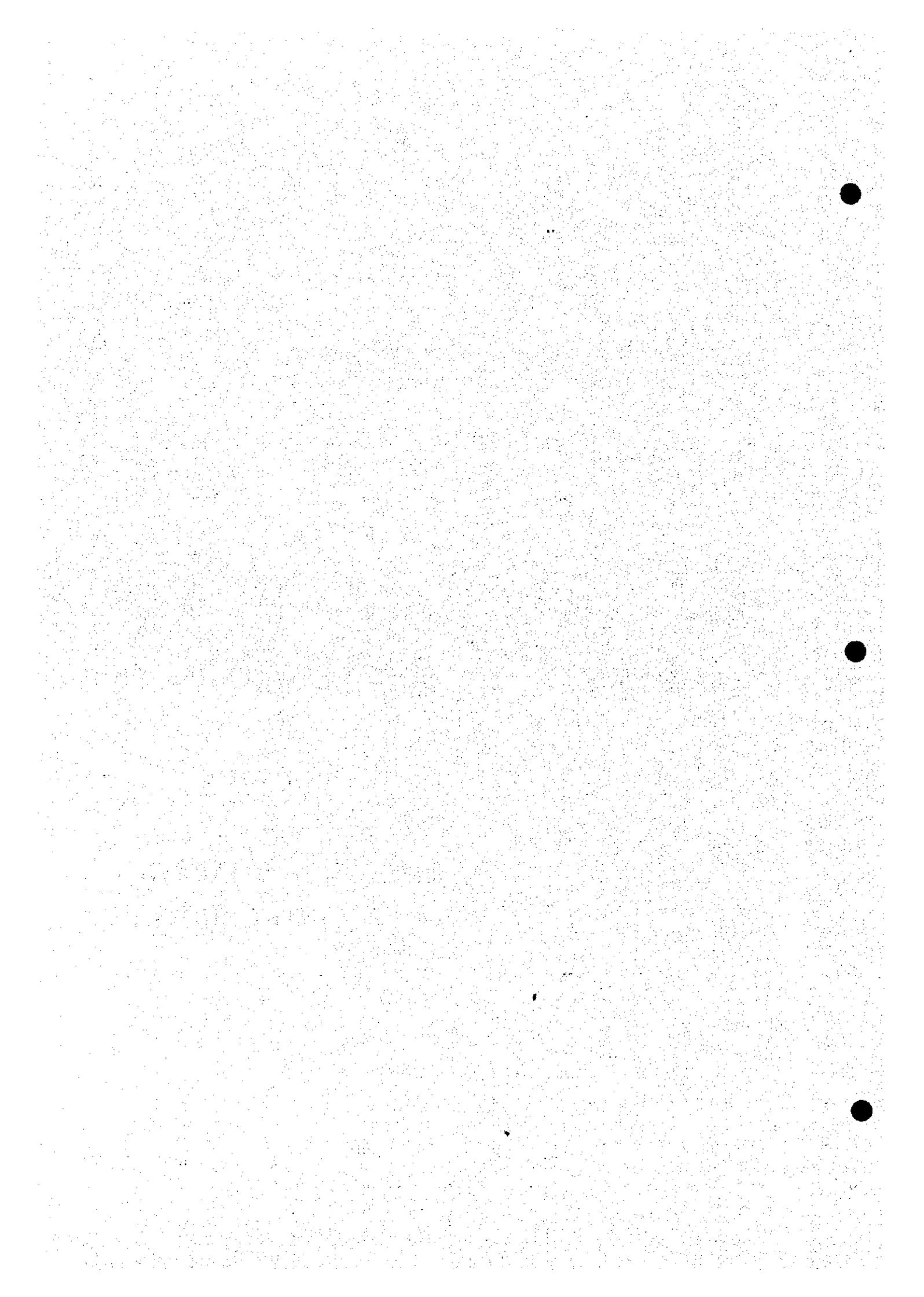
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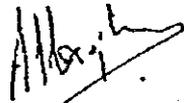
CHAPTER 1
INTRODUCTION



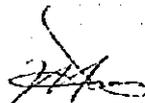
**Minutes of Discussion on the Inception Report for
the Study on the Sewerage System in Metropolitan Tirana
for
The Republic of Albania**

9 August 1996

Tirana, Albania

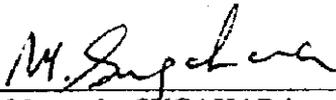


Albert BROJKA
Minister
Ministry of Public Works,
Tourism and Territorial Adjustment

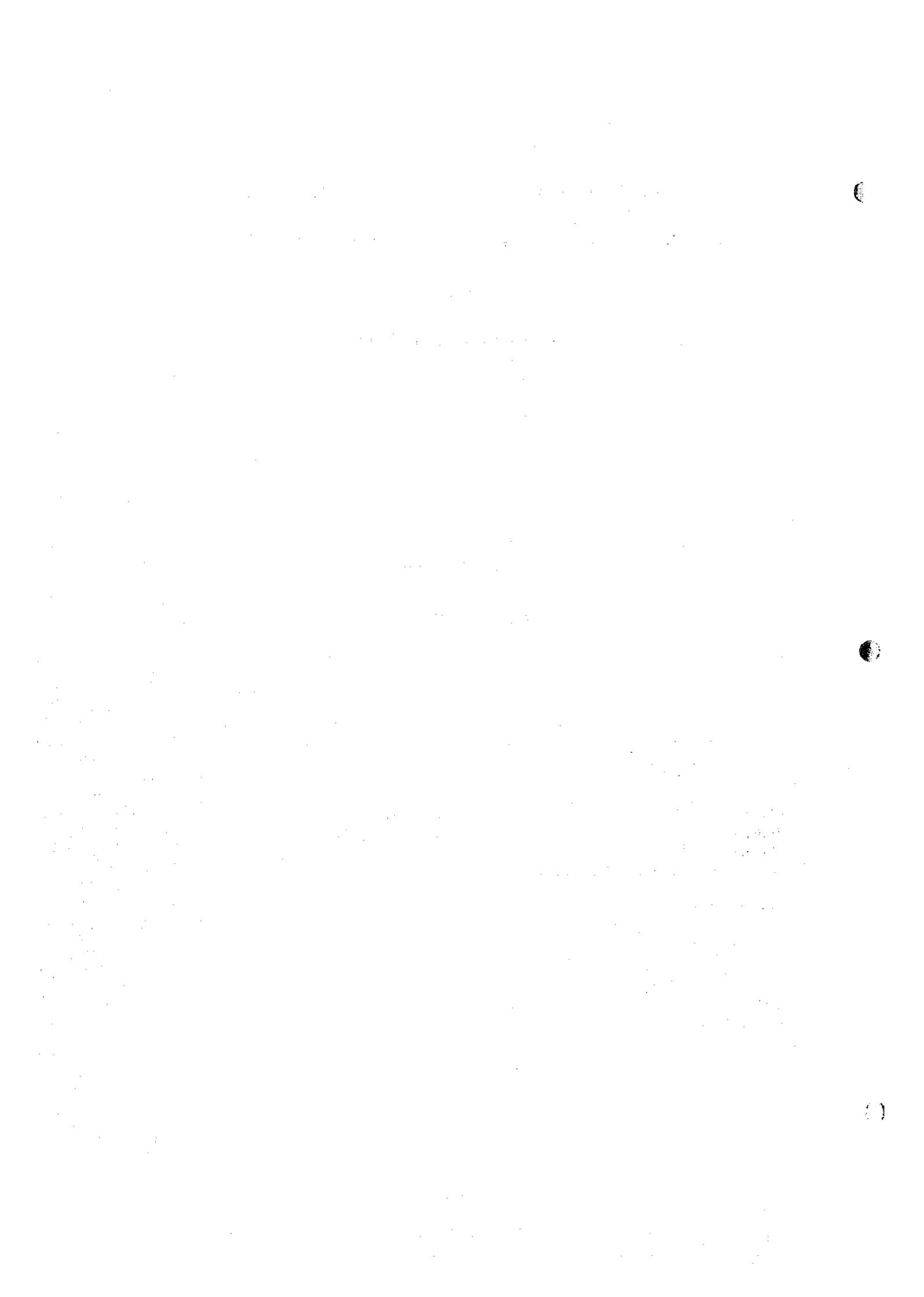


Kenji HORI
JICA Study Team Leader

WITNESSED by:



Prof. Masataka SUGAHARA
Chairman
JICA Advisory Committee



Based on the results of the Preparatory Study, the Japan International Cooperation Agency (JICA) decided to conduct the Study on the Sewerage System in Metropolitan Tirana in the Republic of Albania (hereinafter referred to as "the Study") and sent to Albania a Study Team, headed by Kenji HORI (hereinafter referred to as "the Study Team"), from August 4 to August 11, 1996 in order to explain the Inception Report and confirm Scope of Work of the Study.

During their stay in Albania, the Study Team held meetings with the Directorate of the Project Management Unit, the Ministry of Public Works, Tourism and Territorial Adjustment, and other authorities concerning the Government of Albania and conducted a field survey in the study area.

In the course of the meetings and the field survey, both parties have discussed and agreed on the outline shown below. The Study Team will proceed to continue its work and to prepare the Study Report.

The list of those who attended these meetings are shown in Appendix-1.

Outline of Minutes of Discussion

1. The Study Area

Both the Study Team and the Albanian side confirmed that the Study covers Metropolitan Tirana, which has an area of 2,700 ha and is shown in Appendix-2.

2. The Category of Wastewater

Both sides agreed to include the wastewater from farming activities (the livestock industry) in the scope of the Study if this type of wastewater complies with the suitable effluent standards to be recommended under the scope of the Study.

3. Counterpart Agency

Directorate of Water Supply and Sewerage (DWSS), Ministry of Public Works, Tourism and Territorial Adjustment shall act as the counterpart agency for the Study at its own expense, in order to give full support to the counterpart activities.

4. The Members of the Steering Committee

The Albanian side agreed the members of the Steering Committee will be decided by the end of August 1996.

The steering committee is to act advice and decision making at their own expense.

5. The Members of the Counterpart Team

The Study Team requested to the Albanian side to provide/nominate the members of the counterpart team for the Study so as to conduct the Study smoothly from the following sectors at their own expense.

(1) Full-time coordinator from MOPWT

(2) Planning engineer(s) for water supply and sewerage from MOPWT

(3) Mechanical/Electrical engineer

The Albanian side replied to provide to the Study Team by August 15, 1996.

6. JICA Counterpart Training

The Study Team informed the Albanian side that JICA is ready to invite a member of the counterpart team to Japan for training to help facilitate the smooth conduct of the Study.

7. Provision of an Office for the Study Team

The Study Team reminded the Albanian side to provide a suitable office with equipment, desks, chairs, and tables for planning and drawing work. The Albanian side promised to provide a suitable office space to the Study Team by August 12, 1996.

8. Land for the Sewage Treatment Plant

The Albanian side showed the Study Team a candidate site for sewage treatment plant. The Study Team, however, will prepare alternative plans taking into account of technical and economical aspects.

Albanian

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9. Non-interference with the Other Projects in the Field of Water Supply and Sewerage System

Both sides confirmed that the other projects do/will not interfere with the Study.

The Albanian side agreed to inform the Study Team about the contents and scope of the work of the new project(s) concerning to the water supply and sewerage/sanitation, when this kind of project commences.

10. Arrangement of the Planning Fundamentals

Both sides agreed to arrange the planning fundamentals such as water consumption per capita per day as much as possible with other concerned projects.

11. Systematic Tariff Collection

Both sides agreed that, regarding the tariff collection for the sewage works, the Study will aim to establish the most comprehensive system, which will be followed to the tariff of the water works.

12. Related Organization Chart

The Study Team requested to Albanian side to provide related organization chart concerning water works/sewerage works of Albanian government, Tirana district and Municipality of Tirana. Albanian side provided the chart to the Study Team.

Albanian

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Appendix-1 Attendance List

| Name | Position | Place of Employment |
|----------------|--|--|
| Albert BROJKA | Minister | Ministry of Public Works, Tourism and Territorial Adjustment |
| Stavri RISTANI | Director | Ministry of Public Works, Tourism and Territorial Adjustment Directorate of Water Supply and Sewerage |
| Juli SHLLAKU | Director | Ministry of Public Works, Tourism and Territorial Adjustment Territorial Planning Department |
| Valdet KODRA | Desk of Japan | Council of Ministers Department of Economic Development and Foreign Aid Coordination |
| Kujtim HOXHA | Chief of the Sector for Public Services | Municipality of TIRANA |
| Merita MULLAJ | Chief Engineer | Enterprize for the Maintenance of Roads and Sewerage of TIRANA |
| Fahri MAHO | Specialist for Sewerage | Ministry of Public Works, Tourism and Territorial Adjustment Directorate of Water Supply and Sewerage |
| Mirand CAUSHI | Chief of the Sewerage Sctor | Ministry of Public Works, Tourism and Territorial Adjustment Directorate of Water Supply and Sewerage |
| Arben ZAJMI | Director | Ministry of Public Works, Tourism and Territorial Adjustment Project Implementation Unit for the Bovilla Part of Water and Sewerage of TIRANA |
| Xhorxhi BUCKA | Specialist for Water Spplly | Ministry of Public Works, Tourism and Territorial Adjustment Directorate of Water Supply and Sewerage |
| Artan ZYLFI | Director | Water Work Company for the District of TIRANA |

Alb...

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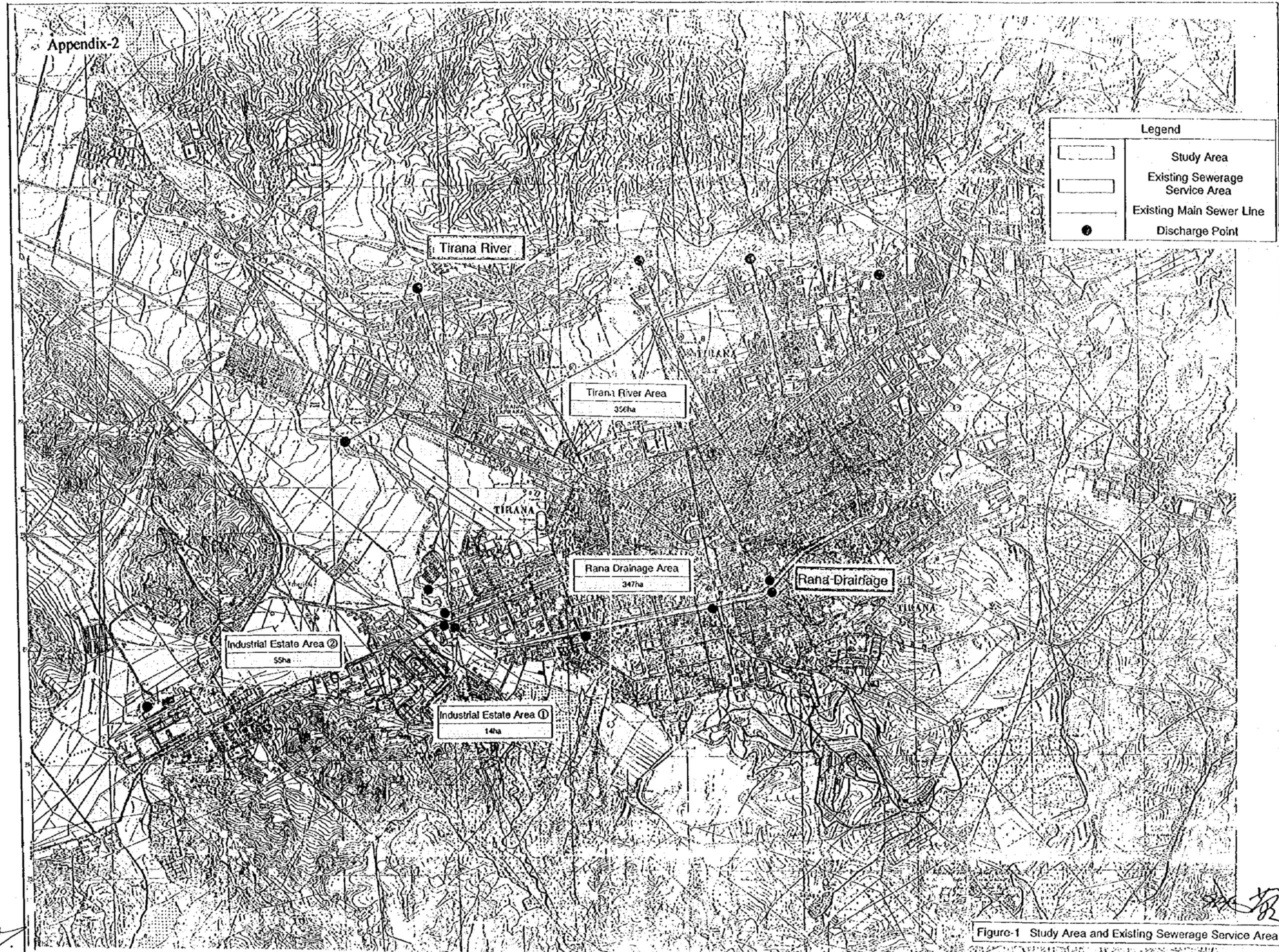


Figure-1 Study Area and Existing Sewerage Service Area

Albana

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**Minutes of Meeting on the Interim Report for
The Study on the Sewerage System in Metropolitan Tirana
in
The Republic of Albania**

**Agreed upon between
Ministry of Public Works, Territorial Adjustment and Tourism
and
Japan International Cooperation Agency**

18 December 1996

Tirana, Albania

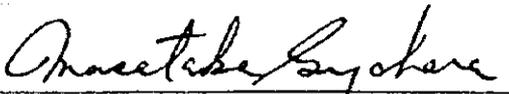


Ernest NOKA
Vice Minister
Ministry of Public Works,
Territorial Adjustment and Tourism



Kenji HORI
JICA Study Team Leader

WITNESSED by:



Prof. Masataka SUGAHARA
Chairman
JICA Advisory Committee



Based on the results of the Preparatory Study, the Japan International Cooperation Agency (JICA) decided to conduct the Study on the Sewerage System in Metropolitan Tirana in the Republic of Albania (hereinafter referred to as "the Study") and sent to Albania a Study Team, headed by Kenji HORI (hereinafter referred to as "the Study Team"), from 4 August to 27 September, 1996 as the 1st field work.

The Study Team had submitted the Progress Report (1) as the outcome of the field investigation and study on 23 September, 1996. On the basis of the discussion results on the Report, the Study Team had reviewed and developed it through a continuous home work in Japan and then submitted a report to the Government of Albania as the Interim Report on 13 December, 1996, and started the 2nd field work having a schedule for the work till 17 February, 1997 as to scrutinize the project conditions.

During their study in Albania, the Study Team held initial meetings with the Directorate of the Project Management Unit, the Ministry of Public Works, Territorial Adjustment and Tourism, and other authorities concerning the Government of Albania.

In the course of the meetings, both parties have discussed and agreed on the outline shown below. The list of those who attended these meetings are shown in Appendix.

The outline of minutes of the meeting are :

1. Fundamental Conditions for the Study

Both the Study Team and the Albanian side confirmed that the fundamental conditions for the Study mentioned in the Interim Report, such as planned sewerage area, planned population, demand for water in target year, planned target water quality and priority area to be improved urgently the current environmental situation are satisfactory.

2. Sewage Treatment Method

The Albanian side agreed that sewage treatment method, aerated lagoon system, recommended by the Study Team are acceptable to employ for the project.



The Albanian side requested to submit a comparison regarding construction cost including land, operation & maintenance cost and advantage/disadvantage taking into account of the operation and maintenance.

3. The Land (as a candidate land) for Construction of the Sewage Treatment Plant

The Albanian side informed that the land around Laknasi for construction of the treatment plant proposed by the Study Team will be possible to be obtained and no land problem affected by the coal mining is considered, because the mining is closed at present and mining area is not in the candidated place of the plant.

4. Improvement of the Storm Drainage

The Albanian side agreed that an improvement of the existing sewer on purpose to storm drainage should not be treated in the scope of the Study because of the reason mentioned in the Interim Report. An emergency inundation countermeasures in the urgent improvement areas, however, will be provided under this project. In connection to this matter, both parties agreed that only preliminary computer-aid calculation will be carried out to indicate the required size of sewers for improvement of the existing sewer network.

5. Regulation on the Water Pollution Control

The Albanian side informed that draft new regulation on the water pollution control is preparing and will be published in January 1997. The target BOD value for discharge of the wastewater to the river will be regulated as 25 mg/l.

6. Counterpart Training in Japan

Mr. Fahri Maho, Specialist for Sewerage, Directorate of Water Supply and Sewerage, MOPWT was nominated as a participant for the training, and an application document will be given to the JICA through general route in the Government of Albania as soon as possible.



Appendix Attendance List

| Name | Position | Place of Employment |
|----------------|---|---|
| Ernest NOKA | Vice Minister | Ministry of Public Works, Territorial Adjustment and Tourism |
| Stavri RISTANI | Director | Ministry of Public Works, Territorial Adjustment and Tourism Directorate of Water Supply and Sewerage |
| Mirand CAUSHI | Chief of the Sewerage Sector | Ministry of Public Works, Territorial Adjustment and Tourism Directorate of Water Supply and Sewerage |
| Mariana COKU | Chief of the Water Supply Sector | Ministry of Public Works, Territorial Adjustment and Tourism Directorate of Water Supply and Sewerage |
| Fahri MAHO | Specialist for Sewerage | Ministry of Public Works, Territorial Adjustment and Tourism Directorate of Water Supply and Sewerage |
| Arian JOVANI | Specialist for Water Supply | Ministry of Public Works, Territorial Adjustment and Tourism Directorate of Water Supply and Sewerage |
| Etleva MILKANI | Specialist for Sewerage | Ministry of Public Works, Territorial Adjustment and Tourism Directorate of Water Supply and Sewerage |
| Merieta KOCA | Specialist | Council of Ministers DEDAC |
| Bujar REME | Sanitary Engineer | Ministry of Health and Environment |
| Juli SHLLAKU | Director | Municipality of TIRANA Department of Urban Planning |
| Luljeta HOXHA | Specialist for Water Supply & Sewerage | Municipality of TIRANA Department of Urban Plannig |

Shkoll


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| Name | Position | Place of Employment |
|-----------------|----------------------------------|---|
| Lulezim QENAMI | Director | Municipality of TIRANA Department of Public Work |
| Xhemal CECO | Specialist | Municipality of TIRANA Department of Road and Sewerage |
| Merita MULLAJ | Chief Engineer | Enterprize for the Maintenance of Roads and Sewerage of TIRANA |
| Faruk TORO | Director | Water Works Enterprise of Tirana |
| Nazmi RUDI | Director | Hydraugeology Enterprise |
| Fatlinda MURTHI | Specialist for Urban Planning | Urban Planning Institute |
| Thoma KORINI | Director | University of Geology and Mining Department of Mining |

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Minutes of Discussions
on
the Progress Report 2
for
the Study on Sewerage System in Metropolitan Tirana
in
the Republic of Albania

The discussions on the captioned report was held at the Ministry of Public Works, Tourism and Territorial Adjustment from 11th to 12th February 1997 by the presence of officials from the Ministry of Public Works, Tourism and Territorial Adjustment, members of the project steering committee and the JICA Study Team.

The contents and each subject of the Progress Report 2 were explained by the Study Team to Albanian officials concerned and a series of discussions were held. Major subjects discussed and conclusions reached among others were given below.

1. What is the basis on revision of planned sewage quality from BOD 260 mg/l and SS 250 mg/l to 200 mg/l of both BOD and SS, respectively?

Two factors are considered in the adjustment:

- 1) Technical leakage of sewage from sewer pipes and groundwater infiltration into sewer pipes are considered at 35 % and 15 % of the planed daily average sewage flow.
 - 2) Water quality examination results conducted during the Stage 1 field work, especially domestic sewage and industrial wastewater.
2. What is the reason of decrease on area requirement and power consumption of the aerated lagoon from Progress Report-1 to Progress Report-2?

This reduction owes to the revision of the planned sewage quality and quantity as mentioned above in view of BOD loading. In addition, the influence of wastewater temperature in lagoon and atmospheric temperature was reflected to decrease retention time required for the lagoon and the depth of lagoon ^{we} and to decrease area requirement.



3. What is the source and basis of design criteria for aerated lagoon?

Several commonly known technical references, such as design manual issued by EPA (Environmental Protection Agency) of U.S.A, were referred. In the preliminary design, so-called "dual-power-level, multi-cellular aerated lagoon" is adopted as economical treatment process.

4. What was the outcome of water quality examination conducted during the Stage 2 field work?

The water sampling entailed to four consecutive weeks to obtain the required number of samples. The examination results will be submitted to the Study Team on February 13 from the Institute of Public Health, Ministry of Health and Environmental Protection, and will be incorporated in the Draft Final Report together with such results obtained during the Stage 1 field work.

5. Construction cost, operation and maintenance cost, and advantage/disadvantage in operation and maintenance are taken up in the comparison of aerated lagoon method and oxidation ditch method. More precise comparison of these two methods are desired to be incorporated in the Draft Final Report.

The method of comparison presented in the Progress Report 2 will be retained as it is. However, additional technical information on oxidation ditch method will be prepared and furnished separately. The counterpart training of JICA to be held in Japan is an another opportunity to learn more about the different engineering practices.

6. Application of PVC pipe to sewer system is desired to be considered. Quality of material and cost information can be furnished to the Study Team.

Applicability of PVC pipe will be studied and its result will be incorporated in the Draft Final Report.



7. Please recommend final treatment and disposal of excess sludge from the sewage treatment plant.

Not only for technical measures, but also relevant actions to be taken up for this specific subject will be contained in the Draft Final Report.

8. The JICA Study has projected the future population in the Study Area at approximately 730,000 in 2010, while other projects/studies show approximately one million.

The said figure (730,000 persons) by the target year 2010 had been confirmed with officials concerned during the Stage I field work. It was also mentioned in our report that the future population of Metropolitan Tirana would reach one million during 2020s. It shall be noted that future population shall be projected not only in view of future land use, but also comprehensively taking into account industrial and economic development, and these frame values are subject to review prior to commence the implementation of the project.

9. Please prepare disbursement schedule by classification of foreign and local fund.

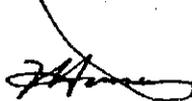
Any cost estimate presented in the Progress Report 2 is preliminary and detailed cost estimate with their foreign and local breakdown will be prepared during the Stage 2 domestic work to incorporate in the Draft Final Report.

The discussions on the Progress Report 2 was adjourned at 1:20 p.m. on 12 February 1997. It was agreed among attendees of discussions that the above mentioned results of discussions will be thoroughly taken into consideration during the Stage 2 domestic work and reflected on the Draft Final Report of the whole Study.

This minutes of discussions was noted and confirmed on 12 February 1997 by:



Mr. Ernest NOKA
Vice Minister
Ministry of Public Works, Tourism and
Territorial Adjustment



Mr. Kenji HORI
Team Leader
JICA Study Team

Attendants List

February. 11. 1997

10:00 AM

| Nr | Name | Organisation / Position |
|----|----------------|---|
| 1 | Fahri Maho | Chief of Steering Community of Study on Sewerage System in Tirana |
| 2 | | Technical Advision, Phare Water PMU |
| 3 | Ermira Tase | Specialist of future PMU |
| 4 | Nazmi Rudi | Director of Hydro-geology of Albania |
| 5 | Miranda Çaushi | Chief of the Sector of Sewerage |
| 6 | Eva Milkani | Specialist at the General Directory of Watersuuply and Sewerage |
| 7 | Shpresa Leka | Director at the Directory of Planning and Regulation of Territory |
| 8 | Xhemal Çeço | Municipality of Tirana (Directory of Sewerage and Roads) |
| 9 | Arjan Jovani | Specialist at the General Directory of Watersuuply and Sewerage |

Attendants List

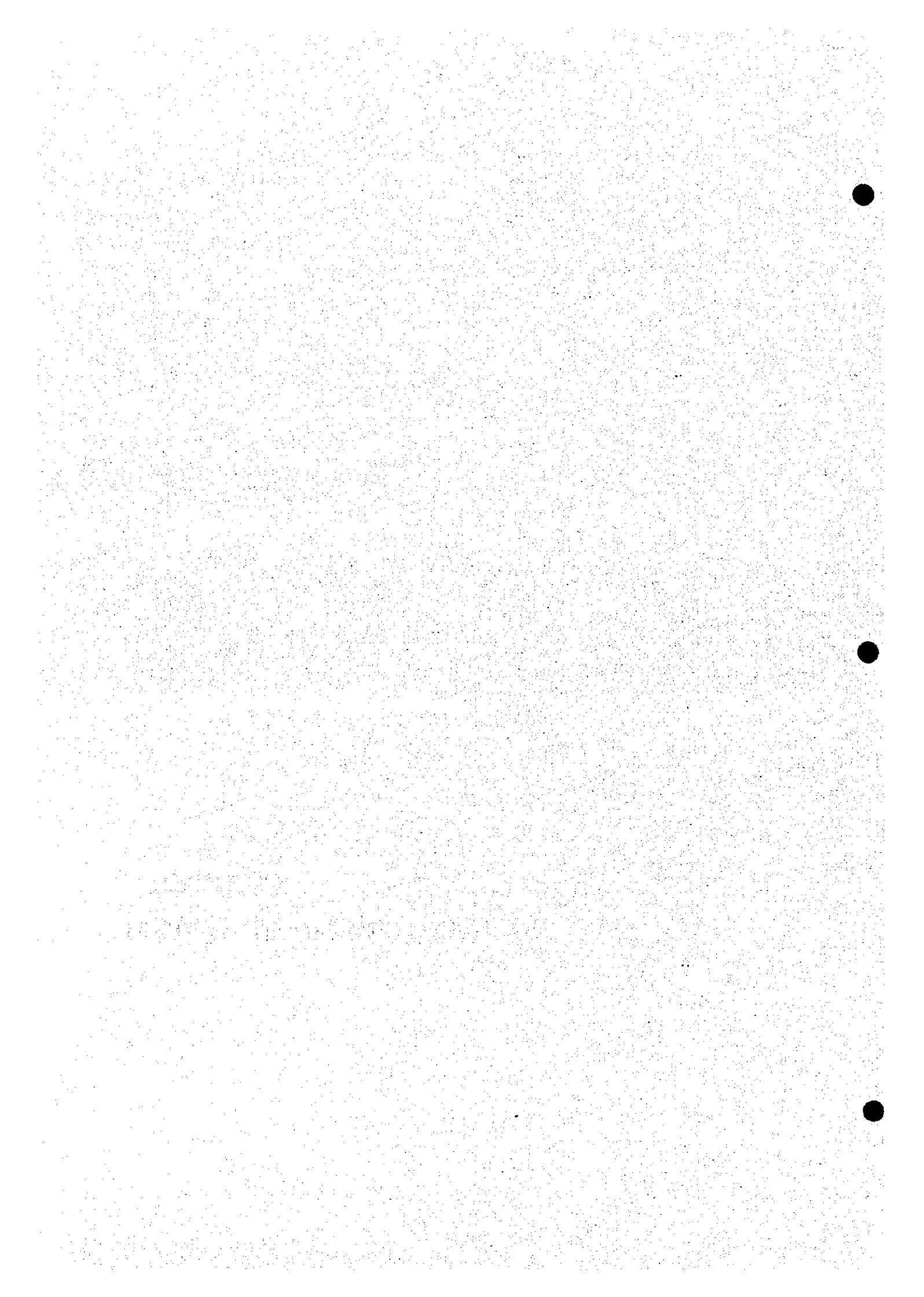
February. 12. 1997

10.00 AM

| NR | Name | Organisation / Position |
|----|-------------------|---|
| 1 | Fahri Maho | Chief of Steering Community of Study on Sewerage System in Tirana |
| 2 | Nazmi Rudi | Director of Hydro-geology of Albania |
| 3 | Lorena Kostallari | Specialist DEDAC |
| 4 | Mariana Çoku | Chief of the Sector of Watersupply |
| 5 | Arjan Jovani | Specialist at the General Directory of Watersupply and Sewerage |
| 6 | Bujar Reme | Sanitary Engineer, Ministry of Health and Environment |
| 7 | Ermira Tase | Specialist of future PMU |
| 8 | Eva Milkani | Specialist at the General Directory of Watersupply and Sewerage |
| 9 | Xhemal Çeço | Municipality of Tirana (Directory of Sewerage and Roads) |



CHAPTER 4
EXISTING SEWERAGE SYSTEM



4.1.1 Evaluation of Existing Sewage Collection System

Table 4.1.1 exhibits breakdown of sewer area served by sewer lines having pipe diameter of 400 mm or larger.

Table 4.1.1 Breakdown of Sewered Area by its Catchment Area

| Contents | Area (ha) | Tirana | Central | Lana North | Lana South | Kombinat | Total |
|----------------|-----------|--------|---------|------------|------------|----------|--------|
| Length (m) | A < 10 | 8,095 | 6,135 | 18,105 | 10,373 | 2,008 | 44,716 |
| | A < 20 | 2,128 | 2,256 | 5,043 | 6,280 | 580 | 16,287 |
| | A < 30 | 1,798 | 2,140 | 3,137 | 3,279 | 372 | 10,726 |
| | A < 50 | 1,576 | 827 | 1,866 | 605 | 961 | 5,835 |
| | A < 100 | 2,974 | 2,171 | 808 | 1,039 | | 6,992 |
| | A > 100 | 2,881 | 2,101 | 4,357 | 2,810 | | 12,149 |
| | Total | 19,452 | 15,630 | 33,316 | 24,386 | 3,921 | 96,705 |
| Percentage (%) | A < 10 | 42 | 39 | 54 | 43 | 51 | 46 |
| | A < 20 | 11 | 14 | 15 | 26 | 15 | 17 |
| | A < 30 | 9 | 14 | 9 | 13 | 9 | 11 |
| | A < 50 | 8 | 5 | 6 | 2 | 25 | 6 |
| | A < 100 | 15 | 14 | 2 | 4 | | 7 |
| | A > 100 | 15 | 13 | 13 | 12 | | 13 |
| | Total | 100 | 100 | 100 | 100 | 100 | 100 |

Note : $D \geq 400$

It is verified from the above tables that about half of existing sewer lines, even having diameter of 400 mm or larger, have their respective service area of less than 10 ha, owing to its principal design as the combined system.

Evaluation procedure is as follows:

- a. Flow capacity (safe ratio) is calculated as $F/C(\%)$:

$$F/C = (\text{planned sewage quantity}) / (\text{full flow capacity of sewer line}) \times 100\%$$
- b. Summation of total length and $F/C(\%)$ by pipe diameter as shown in each Table.

1) Flow capacity as combined system (C-1)

Sanitary Sewage Flow

Sanitary Sewage per Capita = 440 liter/day (Hourly Maximum)

Storm Water Flow

Rainfall Intensity Formula = $\frac{2750}{t + 17}$ (Return Period : 4 Year)

For Main Pipe ($D \geq 500$)

Rainfall Intensity Formula = $\frac{2520}{t + 17}$ (Return Period : 2.5 Year)

For Small Pipe ($D \leq 400$)

Runoff Coefficient = 0.5

Inlet Time = 5 min

Assumed Average Velocity = 1.5 m/sec

Table 4.1.2 Result of Existing Sewer Evaluation

| | Dia (mm) | F/C ≤ 100% | F/C ≤ 150% | F/C ≤ 200% | F/C > 200% | Total | |
|----------------------|----------------------|---------------|---------------|---------------|---------------|--------|--------|
| Length (m) | 400 | 3,423 | 2,990 | 3,226 | 20,056 | 29,695 | |
| | 500 | 2,877 | 1,419 | 1,236 | 9,837 | 15,369 | |
| | 600 | 5,027 | 2,505 | 2384 | 11,507 | 21,423 | |
| | 800 | 3,486 | 1,373 | 1,104 | 3,096 | 9,059 | |
| | 1000 | 1,042 | 227 | 868 | 3,702 | 5,839 | |
| | 700x500 | | 316 | | | 316 | |
| | 1000x500 | | | 199 | | 199 | |
| | 1500x700 | | 1,536 | 210 | 138 | 1,884 | |
| | Network Total | | 15,855 | 10,366 | 9,227 | 48,336 | 83,784 |
| | 600 | 2,170 | 1,204 | | | 3,374 | |
| | 800 | 452 | 179 | 242 | 4,364 | 5,237 | |
| | 1000 | | 20 | 421 | 2,739 | 3,180 | |
| | 1000x600 | | | | 1,130 | 1,130 | |
| | Interceptor Total | | 2,622 | 1,403 | 663 | 8,233 | 12,921 |
| | Total | | 18,477 | 11,769 | 9,890 | 56,569 | 96,705 |
| | Percentage (%) | 400 | 12 | 10 | 11 | 68 | 100 |
| 500 | | 19 | 9 | 8 | 64 | 100 | |
| 600 | | 23 | 12 | 11 | 54 | 100 | |
| 800 | | 38 | 15 | 12 | 34 | 100 | |
| 1000 | | 18 | 4 | 15 | 63 | 100 | |
| 700x500 | | | 100 | | | 100 | |
| 1000x500 | | | | 100 | | 100 | |
| 1500x700 | | | 82 | 11 | 7 | 100 | |
| Network Total | | | 19 | 12 | 11 | 58 | 100 |
| 600 | | 64 | 36 | | | 100 | |
| 800 | | 9 | 3 | 5 | 83 | 100 | |
| 1000 | | | 1 | 13 | 86 | 100 | |
| 1000x600 | | | | | 100 | 100 | |
| Interceptor Total | | | 20 | 11 | 5 | 64 | 100 |
| Total | | | 19 | 12 | 10 | 58 | 100 |

2) Flow capacity as combined system (C-2)

Design conditions is same as C-1.

Table 4.1.3 Result of Existing Sewer Evaluation (Combined : Case-2)

| | Dia (mm) | F/C ≤ 100% | F/C ≤ 150% | F/C ≤ 200% | F/C > 200% | Total | |
|----------------------|----------------------|------------|------------|------------|------------|--------|--------|
| Lenth (m) | 400 | 3,777 | 3,418 | 3,382 | 19,118 | 29,695 | |
| | 500 | 3,054 | 1,419 | 1,236 | 9,660 | 15,369 | |
| | 600 | 5,027 | 2,505 | 2,384 | 11,507 | 21,423 | |
| | 800 | 3,486 | 1,373 | 1,104 | 3,096 | 9,059 | |
| | 1000 | 1,042 | 227 | 868 | 3,702 | 5,839 | |
| | 700x500 | | 316 | | | 316 | |
| | 1000x500 | | | 199 | | 199 | |
| | 1500x700 | | 1,536 | 210 | 138 | 1,884 | |
| | Network Total | | 16,386 | 10,794 | 9,383 | 47,221 | 83,784 |
| | 600 | 2,170 | 1,204 | | | 3,374 | |
| | 800 | 3,132 | 823 | 1,272 | | 5,237 | |
| | 1000 | 2,118 | 1,062 | | | 3,180 | |
| | 1000x600 | 1,130 | | | | 1,130 | |
| | Interceptor Total | | 8,550 | 3,099 | 1,272 | | 12,921 |
| | Total | | 24,936 | 13,893 | 10,655 | 47,221 | 96,705 |
| | Percentage (%) | 400 | 13 | 12 | 11 | 64 | 100 |
| | | 500 | 20 | 9 | 8 | 63 | 100 |
| 600 | | 23 | 12 | 11 | 54 | 100 | |
| 800 | | 38 | 15 | 12 | 34 | 100 | |
| 1000 | | 18 | 4 | 15 | 63 | 100 | |
| 700x500 | | | 100 | | | 100 | |
| 1000x500 | | | | 100 | | 100 | |
| 1500x700 | | | 82 | 11 | 7 | 100 | |
| Network Total | | | 20 | 13 | 11 | 56 | 100 |
| 600 | | 64 | 36 | | | 100 | |
| 800 | | 60 | 16 | 24 | | 100 | |
| 1000 | | 67 | 33 | | | 100 | |
| 1000x600 | | 100 | | | | 100 | |
| Interceptor Total | | | 66 | 24 | 10 | 100 | |
| Total | | | 26 | 14 | 11 | 49 | 100 |

3) Flow capacity as combined system (C-3)

As reference information, the flow capacity of existing sewer for the current sanitary sewage and storm flow was evaluated.

Sanitary Sewage Flow

Population Density = Existing Density
Sanitary Sewage per Capita = 150 liter/day (Hourly Maximum)

Storm Water Flow

Rainfall Intensity Formula = $\frac{1970}{t + 18}$ (Return Period : 0.5 Year)
For Main Pipe ($D \geq 500$)
Rainfall Intensity Formula = $\frac{1970}{t + 18}$ (Return Period : 0.5 Year)
For Small Pipe ($D \leq 400$)
Runoff Coefficient = 0.4
Inlet Time = 10 min
Assumed Average Velocity = 1.5 m/sec

Table 4.1.4 Result of Existing Sewer Evaluation

| | Dia (mm) | F/C ≤ 100% | F/C ≤ 150% | F/C ≤ 200% | F/C > 200% | Total |
|----------------------|----------------------|---------------|---------------|---------------|---------------|--------|
| Length (m) | 400 | 9,639 | 3,788 | 4,105 | 12,163 | 29,695 |
| | 500 | 5,587 | 3,085 | 2,099 | 4,598 | 15,369 |
| | 600 | 9,916 | 713 | 3,420 | 7,374 | 21,423 |
| | 800 | 5,963 | 1,619 | 638 | 839 | 9,059 |
| | 1000 | 2,137 | 656 | 970 | 2,076 | 5,839 |
| | 700x500 | 316 | | | | 316 |
| | 1000x500 | 199 | | | | 199 |
| | 1500x700 | 1,746 | 138 | | | 1,884 |
| | Network Total | 35,503 | 9,999 | 11,232 | 27,050 | 83,784 |
| | 600 | 3,374 | | | | 3,374 |
| | 800 | 2,015 | 763 | 476 | 1,983 | 5,237 |
| | 1000 | 441 | 678 | 447 | 1,614 | 3,180 |
| | 1000x600 | | | 1,130 | | 1,130 |
| | Interceptor Total | 5,830 | 1,441 | 2,053 | 3,597 | 12,921 |
| | Total | 41,333 | 11,440 | 13,285 | 30,647 | 96,705 |
| | Percentage (%) | 400 | 32 | 13 | 14 | 41 |
| 500 | | 36 | 20 | 14 | 30 | 100 |
| 600 | | 46 | 3 | 16 | 34 | 100 |
| 800 | | 66 | 18 | 7 | 9 | 100 |
| 1000 | | 37 | 11 | 17 | 36 | 100 |
| 700x500 | | 100 | | | | 100 |
| 1000x500 | | 100 | | | | 100 |
| 1500x700 | | 93 | 7 | | | 100 |
| Network Total | | 42 | 12 | 13 | 32 | 100 |
| 600 | | 100 | | | | 100 |
| 800 | | 38 | 15 | 9 | 38 | 100 |
| 1000 | | 14 | 21 | 14 | 51 | 100 |
| 1000x600 | | | | 100 | | 100 |
| Interceptor Total | | 45 | 11 | 16 | 28 | 100 |
| Total | | 43 | 12 | 14 | 32 | 100 |

This evaluation indicated that about half of existing sewer has flow capacity against the present swage flow.

4) Flow capacity as storm sewer of separate system

Storm Water Flow

| | | | |
|---------------------------------|---|-----------------------|----------------------------|
| Rainfall Intensity Formula | = | $\frac{2750}{t + 17}$ | (Return Period : 4 Year) |
| For Main Pipe ($D \geq 500$) | | | |
| Rainfall Intensity Formula | = | $\frac{2520}{t + 17}$ | (Return Period : 2.5 Year) |
| For Small Pipe ($D \leq 400$) | | | |
| Runoff Coefficient | = | 0.5 | |
| Inlet Time | = | 5 min | |
| Assumed Average Velocity | = | 1.5 m/sec | |

Table 4.1.5 Result of Existing Sewer Evaluation

| | Dia (mm) | F/C \leq 100% | F/C \leq 150% | F/C \leq 200% | F/C > 200% | Total |
|-------------------|----------|--------------------|--------------------|--------------------|---------------|--------|
| Length (m) | 400 | 3,423 | 2,990 | 3,544 | 19,738 | 29,695 |
| | 500 | 2,877 | 1,419 | 1,291 | 9,782 | 15,369 |
| | 600 | 8,640 | 2,638 | 2,012 | 11,507 | 24,797 |
| | 800 | 5,156 | 1,718 | 1,104 | 6,318 | 14,296 |
| | 1000 | 1,062 | 648 | 868 | 6,441 | 9,019 |
| | 700x500 | | 316 | | | 316 |
| | 1000x500 | | | 199 | | 199 |
| | 1000x600 | | | | 1,130 | 1,130 |
| | 1500x700 | | 1,536 | 210 | 138 | 1,884 |
| | Total | | 21,158 | 11,265 | 9,228 | 55,054 |
| Percentage (%) | 400 | 12 | 10 | 12 | 66 | 100 |
| | 500 | 19 | 9 | 8 | 64 | 100 |
| | 600 | 35 | 11 | 8 | 46 | 100 |
| | 800 | 36 | 12 | 8 | 44 | 100 |
| | 1000 | 12 | 7 | 10 | 71 | 100 |
| | 700x500 | | 100 | | | 100 |
| | 1000x500 | | | 100 | | 100 |
| | 1000x600 | | | | 100 | 100 |
| | 1500x700 | | 82 | 11 | 7 | 100 |
| | Total | | 22 | 12 | 10 | 57 |

This evaluation revealed that only 22% of the existing sewer could accommodate the planned sewage flow with only for storm sewer of separate system in the year 2010.

5) Flow capacity as sanitary sewer of separate system

Sanitary Sewage Flow
 Sanitary Sewage per Capita = 440 liter/day (Hourly Maximum)

Table 4.1.6 Result of Existing Pipe Evaluation

| | Dia (mm) | F/C ≤ 50% | F/C ≤ 100% | F/C ≤ 150% | F/C > 150% | Total |
|-------------------|----------|-----------|------------|------------|------------|--------|
| Length (m) | 400 | 29,252 | 443 | | | 29,695 |
| | 500 | 15,369 | | | | 15,369 |
| | 600 | 24,797 | | | | 24,797 |
| | 800 | 12,370 | 1,926 | | | 14,296 |
| | 1000 | 8,785 | 234 | | | 9,019 |
| | 700x500 | 316 | | | | 316 |
| | 1000x500 | 199 | | | | 199 |
| | 1000x600 | 1,130 | | | | 1,130 |
| | 1500x700 | 1,884 | | | | 1,884 |
| | Total | 94,102 | 2,603 | | | 96,705 |
| Percentage (%) | 400 | 99 | 1 | | | 100 |
| | 500 | 100 | | | | 100 |
| | 600 | 100 | | | | 100 |
| | 800 | 87 | 13 | | | 100 |
| | 1000 | 97 | 3 | | | 100 |
| | 700x500 | 100 | | | | 100 |
| | 1000x500 | 100 | | | | 100 |
| | 1000x600 | 100 | | | | 100 |
| | 1500x700 | 100 | | | | 100 |
| | Total | 97 | 3 | | | 100 |

This evaluation revealed that almost all existing sewer could accommodate the planned sanitary sewage flow in the year 2010.

Table 4.1.7 Evaluation of Existing Sewer Capacity (For Combined Sewer : Case-1)

Sanitary Sewage Flow
 Sanitary Sewage per Capita = 440 liter/day (Hourly Maximum)

Storm Water Flow
 Rainfall Intensity Formula = 2750 (Return Period : 4 Year)
 For Main Pipe ($D \geq 500$) $t + 17$
 Rainfall Intensity Formula = 2520 (Return Period : 2.5 Year)
 For Small Pipe ($D \leq 400$) $t + 17$
 Runoff Coefficient = 0.5
 Inlet Time = 5 min
 Assumed Average Velocity = 1.5 m/sec

| No. | Down Stream | Length (m) | | Area (ha) | | Sewage Quantity | | | Existing Pipe Specification | | | | Capacity | |
|--------|-------------|------------|-----------|-----------|-----------------|-----------------|---------------|--------------|-----------------------------|-------|---------|--------------|-----------|-------|
| | | Increment | Increment | Total | Sanitary Sewage | Storm Water | Remain Sewage | $Q_1(m^3/s)$ | D (mm) | I (%) | V (m/s) | $Q_2(m^3/s)$ | Q_1/Q_2 | Judge |
| 1001 | 1004 | 826 | 9.80 | 9.80 | 0.013 | 1.200 | | 1.213 | 600 | 12.4 | 2.42 | 0.684 | 177% | NG |
| 1002 | 1003 | 94 | 4.10 | 4.10 | 0.006 | 0.624 | | 0.629 | 300 | 17.0 | 1.78 | 0.126 | 500% | NG |
| 1003 | 1004 | 295 | 6.60 | 10.70 | 0.014 | 1.424 | | 1.438 | 400 | 19.1 | 2.29 | 0.288 | 500% | NG |
| 1004 | 1009 | 355 | 5.47 | 25.97 | 0.035 | 2.826 | | 2.861 | 600 | 22.0 | 3.22 | 0.910 | 314% | NG |
| 1005 | 1006 | 450 | 7.60 | 7.60 | 0.010 | 1.075 | | 1.085 | 600 | 18.6 | 2.96 | 0.837 | 130% | NG |
| 1006 | 1008 | 249 | 8.30 | 15.90 | 0.021 | 2.038 | | 2.059 | 600 | 2.0 | 0.97 | 0.274 | 751% | NG |
| 1007 | 1008 | 205 | 2.88 | 2.88 | 0.004 | 0.415 | | 0.419 | 400 | 20.9 | 2.40 | 0.302 | 139% | NG |
| 1008 | 1009 | 252 | 3.03 | 21.81 | 0.029 | 2.555 | | 2.585 | 600 | 16.6 | 2.80 | 0.792 | 326% | NG |
| 1009 | 1011 | 360 | 6.37 | 54.15 | 0.073 | 5.290 | | 5.363 | 600 | 27.2 | 3.58 | 1.012 | 530% | NG |
| 1010 | 1011 | 564 | 4.03 | 4.03 | 0.005 | 0.544 | | 0.549 | 600 | 21.9 | 3.21 | 0.908 | 61% | OK |
| Out-11 | | | | | | | | -5.676 | | | | | | |
| 1011 | 1012 | 824 | 0.97 | 59.15 | 0.080 | 0.119 | 0.157 | 0.356 | 600 | 18.0 | 2.91 | 0.823 | 43% | OK |
| 1012 | 1021 | 491 | 0.00 | 59.15 | 0.080 | 0.101 | 0.157 | 0.338 | 600 | 6.3 | 1.72 | 0.486 | 70% | OK |
| 1013 | 1014 | 247 | 1.33 | 1.33 | 0.002 | 0.206 | | 0.207 | 600 | 17.2 | 2.85 | 0.806 | 26% | OK |
| 1014 | 1015 | 163 | 4.25 | 5.58 | 0.008 | 0.734 | | 0.742 | 400 | 2.0 | 0.74 | 0.093 | 798% | NG |
| 1015 | 1016 | 268 | 7.90 | 13.48 | 0.018 | 1.745 | | 1.763 | 500 | 2.0 | 0.86 | 0.169 | 1044% | NG |
| 1016 | 1017B | 708 | 7.90 | 21.38 | 0.029 | 2.001 | | 2.030 | 400 | 12.8 | 1.87 | 0.235 | 864% | NG |
| 1017A | 1017B | 186 | 1.20 | 1.20 | 0.002 | 0.190 | | 0.192 | 500 | 41.3 | 3.91 | 0.768 | 25% | OK |
| 1017B | 1020 | 122 | 1.30 | 23.88 | 0.032 | 2.351 | | 2.383 | 500 | 2.6 | 0.98 | 0.192 | 1238% | NG |
| 1018 | 1019 | 426 | 4.59 | 4.59 | 0.006 | 0.657 | | 0.663 | 600 | 2.0 | 0.97 | 0.274 | 242% | NG |
| 1019 | 1020 | 100 | 2.85 | 7.44 | 0.010 | 1.022 | | 1.032 | 800 | 1.9 | 1.15 | 0.578 | 179% | NG |
| 1020 | 1021 | 895 | 0.00 | 31.32 | 0.042 | 2.456 | | 2.499 | 800 | 5.6 | 1.97 | 0.990 | 252% | NG |
| Out-12 | | | | | | | | -2.470 | | | | | | |
| 1021 | 1060 | 855 | 0.00 | 90.47 | 0.122 | 0.000 | 0.244 | 0.366 | 600 | 5.2 | 1.57 | 0.444 | 83% | OK |
| 1022 | 1023 | 100 | 0.77 | 0.77 | 0.001 | 0.117 | | 0.118 | 400 | 5.9 | 1.27 | 0.160 | 74% | OK |
| 1023 | 1024 | 86 | 0.69 | 1.46 | 0.002 | 0.212 | | 0.214 | 400 | 14.0 | 1.96 | 0.246 | 87% | OK |
| 1024 | 1025 | 91 | 0.81 | 2.27 | 0.003 | 0.317 | | 0.320 | 400 | 9.8 | 1.64 | 0.206 | 155% | NG |
| 1025 | 1027 | 127 | 0.83 | 3.10 | 0.004 | 0.447 | | 0.451 | 500 | 20.4 | 2.75 | 0.540 | 84% | OK |
| 1026 | 1027 | 50 | 0.28 | 0.28 | 0.000 | 0.043 | | 0.044 | 400 | 1.9 | 0.72 | 0.090 | 48% | OK |
| 1027 | 1028 | 127 | 0.83 | 4.21 | 0.006 | 0.576 | | 0.582 | 500 | 11.8 | 2.09 | 0.410 | 142% | NG |
| 1028 | 1035 | 180 | 1.03 | 5.24 | 0.007 | 0.669 | | 0.676 | 600 | 6.1 | 1.70 | 0.481 | 141% | NG |
| 1029 | 1031 | 326 | 2.47 | 2.47 | 0.003 | 0.338 | | 0.341 | 400 | 8.2 | 1.50 | 0.188 | 181% | NG |
| 1030 | 1031 | 209 | 1.80 | 1.80 | 0.002 | 0.283 | | 0.285 | 600 | 15.3 | 2.69 | 0.761 | 38% | OK |
| 1031 | 1034 | 227 | 2.35 | 6.62 | 0.009 | 0.900 | | 0.909 | 500 | 7.6 | 1.68 | 0.330 | 275% | NG |
| 1032 | 1034 | 132 | 1.36 | 1.36 | 0.002 | 0.203 | | 0.204 | 400 | 2.0 | 0.74 | 0.093 | 220% | NG |
| 1033 | 1034 | 103 | 1.59 | 1.59 | 0.002 | 0.241 | | 0.243 | 400 | 2.0 | 0.74 | 0.093 | 261% | NG |
| 1034 | 1035 | 151 | 1.14 | 10.71 | 0.014 | 1.373 | | 1.387 | 500 | 12.5 | 2.15 | 0.422 | 329% | NG |
| 1035 | 1037 | 220 | 2.36 | 18.31 | 0.025 | 2.165 | | 2.190 | 500 | 13.6 | 2.24 | 0.440 | 498% | NG |
| 1036 | 1037 | 339 | 2.14 | 2.14 | 0.003 | 0.290 | | 0.293 | 400 | 9.4 | 1.61 | 0.202 | 145% | NG |
| 1037 | 1041 | 347 | 4.19 | 24.64 | 0.033 | 2.600 | | 2.633 | 500 | 2.0 | 0.86 | 0.169 | 1559% | NG |
| 1038 | 1039 | 110 | 1.70 | 1.70 | 0.002 | 0.256 | | 0.259 | 400 | 7.2 | 1.41 | 0.177 | 146% | NG |
| 1039 | 1040 | 140 | 1.15 | 2.85 | 0.004 | 0.439 | | 0.443 | 500 | 6.4 | 1.54 | 0.302 | 146% | NG |
| 1040 | 1041 | 124 | 1.15 | 4.00 | 0.005 | 0.583 | | 0.589 | 600 | 11.3 | 2.31 | 0.653 | 90% | OK |
| 1041 | 1044 | 136 | 0.85 | 29.49 | 0.040 | 2.988 | | 3.027 | 500 | 22.0 | 2.85 | 0.560 | 541% | NG |
| 1042 | 1044 | 73 | 2.17 | 2.17 | 0.003 | 0.364 | | 0.366 | 500 | 42.4 | 3.96 | 0.778 | 47% | OK |
| 1043 | 1044 | 78 | 0.49 | 0.49 | 0.001 | 0.082 | | 0.082 | 500 | 2.5 | 0.96 | 0.188 | 44% | OK |
| 1044 | 1049 | 286 | 2.08 | 34.23 | 0.046 | 3.197 | | 3.243 | 500 | 18.5 | 2.62 | 0.514 | 630% | NG |

| No. | Down Stream | Length (m) | | Area (ha) | | Sewage Quantity | | | Existing Pipe Specification | | | | Capacity | | |
|--------|-------------|------------|-----------|-----------|-----------------|-----------------|---------------|------------------------------------|-----------------------------|---------------------|---------|------------------------------------|--------------------------------|-------|--|
| | | Increment | Increment | Total | Sanitary Sewage | Storm Water | Remain Sewage | Q ₁ (m ³ /s) | D (mm) | I (% _s) | V (m/s) | Q ₂ (m ³ /s) | Q ₁ /Q ₂ | Judge | |
| 1045 | 1046 | 283 | 3.12 | 3.12 | 0.004 | 0.435 | | 0.439 | 400 | 12.7 | 1.87 | 0.235 | 187% | NG | |
| 1046 | 1048 | 125 | 1.70 | 4.82 | 0.007 | 0.695 | | 0.701 | 500 | 10.9 | 2.01 | 0.395 | 178% | NG | |
| 1047 | 1048 | 123 | 2.35 | 2.35 | 0.003 | 0.384 | | 0.387 | 500 | 16.2 | 2.45 | 0.481 | 80% | OK | |
| 1048 | 1049 | 156 | 1.80 | 8.97 | 0.012 | 1.211 | | 1.223 | 500 | 4.4 | 1.28 | 0.251 | 487% | NG | |
| 1049 | 1053 | 274 | 0.90 | 44.10 | 0.060 | 3.837 | | 3.896 | 800 | 2.0 | 1.18 | 0.593 | 657% | NG | |
| 1050 | 1051 | 56 | 0.80 | 0.80 | 0.001 | 0.135 | | 0.136 | 500 | 2.0 | 0.86 | 0.169 | 81% | OK | |
| 1051 | 1052 | 149 | 2.65 | 3.45 | 0.005 | 0.542 | | 0.547 | 600 | 2.0 | 0.97 | 0.274 | 199% | NG | |
| 1052 | 1053 | 157 | 0.85 | 4.30 | 0.006 | 0.632 | | 0.637 | 800 | 1.8 | 1.12 | 0.563 | 113% | NG | |
| 1053 | 1057 | 121 | 1.08 | 49.48 | 0.067 | 4.172 | | 4.239 | 800 | 2.0 | 1.18 | 0.593 | 715% | NG | |
| 1054 | 1056 | 325 | 2.64 | 2.64 | 0.004 | 0.394 | | 0.397 | 600 | 16.6 | 2.80 | 0.792 | 50% | OK | |
| 1055 | 1056 | 373 | 3.30 | 3.30 | 0.004 | 0.483 | | 0.487 | 600 | 12.0 | 2.38 | 0.673 | 72% | OK | |
| 1056 | 1057 | 296 | 1.30 | 7.24 | 0.010 | 0.941 | | 0.950 | 800 | 2.0 | 1.18 | 0.593 | 160% | NG | |
| 1057 | 1060 | 444 | 6.15 | 62.87 | 0.085 | 4.783 | | 4.868 | 1000 | 2.0 | 1.37 | 1.076 | 452% | NG | |
| 1058 | 1059 | 300 | 3.29 | 3.29 | 0.004 | 0.455 | | 0.460 | 400 | 17.6 | 2.20 | 0.276 | 166% | NG | |
| 1059 | 1060 | 945 | 7.30 | 10.59 | 0.014 | 1.130 | | 1.144 | 600 | 2.0 | 0.97 | 0.274 | 417% | NG | |
| Out-13 | | | | | | | | -5.715 | | | | 0.00 | 0.000 | | |
| 1060 | 1061 | 722 | 0.00 | 163.93 | 0.221 | 0.000 | 0.442 | 0.664 | 600 | 8.6 | 2.01 | 0.568 | 117% | NG | |
| 1061 | 1062 | 482 | 0.00 | 163.93 | 0.221 | 0.000 | 0.442 | 0.664 | 600 | 7.8 | 1.92 | 0.543 | 122% | NG | |
| 1062 | 1063 | 280 | 36.20 | 200.13 | 0.270 | 3.591 | 0.442 | 4.304 | 800 | 17.4 | 3.47 | 1.744 | 247% | NG | |
| 1063 | 1065 | 267 | 3.45 | 203.58 | 0.275 | 3.649 | 0.442 | 4.366 | 800 | 3.3 | 1.51 | 0.759 | 575% | NG | |
| 1064 | 1065 | 149 | 3.83 | 3.83 | 0.005 | 0.617 | | 0.622 | 1000 | 3.3 | 1.75 | 1.374 | 45% | OK | |
| 1065 | To STP | 1130 | 6.20 | 213.61 | 0.288 | 3.649 | 0.442 | 4.380 | 1000x600 | 3.8 | 1.93 | 1.042 | 420% | NG | |
| Out-14 | | | | | | | | -3.803 | | | | | | | |
| To STP | | | | | 0.288 | | 0.576 | 0.865 | | | | | | | |
| 2001 | 2002 | 480 | 14.95 | 14.95 | 0.023 | 1.917 | | 1.939 | 400 | 5.8 | 1.26 | 0.158 | 1225% | NG | |
| 2002 | 2003 | 193 | 4.38 | 19.33 | 0.030 | 2.503 | | 2.532 | 500 | 26.2 | 3.11 | 0.611 | 415% | NG | |
| 2003 | 2005 | 242 | 3.74 | 23.07 | 0.035 | 2.736 | | 2.772 | 600 | 18.5 | 2.95 | 0.834 | 332% | NG | |
| 2004 | 2005 | 348 | 6.90 | 6.90 | 0.011 | 1.018 | | 1.028 | 600 | 9.1 | 2.07 | 0.585 | 176% | NG | |
| 2005 | 2007 | 169 | 1.15 | 31.12 | 0.048 | 3.496 | | 3.543 | 600 | 8.2 | 1.97 | 0.557 | 636% | NG | |
| 2006 | 2007 | 300 | 1.60 | 1.60 | 0.002 | 0.221 | | 0.224 | 400 | 5.0 | 1.17 | 0.147 | 152% | NG | |
| 2007 | 2009 | 48 | 0.23 | 32.95 | 0.050 | 3.637 | | 3.688 | 600 | 12.5 | 2.43 | 0.687 | 537% | NG | |
| 2008 | 2009 | 273 | 2.10 | 2.10 | 0.003 | 0.294 | | 0.297 | 300 | 5.1 | 0.98 | 0.069 | 429% | NG | |
| 2009 | 2011 | 262 | 2.10 | 37.15 | 0.057 | 3.784 | | 3.841 | 1500x700 | 9.5 | 3.67 | 3.468 | 111% | NG | |
| 2010A | 2010B | 50 | 0.54 | 0.54 | 0.001 | 0.084 | | 0.084 | 300 | 11.9 | 1.49 | 0.105 | 80% | OK | |
| 2010B | 2011 | 175 | 1.67 | 2.21 | 0.003 | 0.316 | | 0.319 | 400 | 2.0 | 0.74 | 0.093 | 343% | NG | |
| 2011 | 2013 | 210 | 0.40 | 39.76 | 0.061 | 3.816 | | 3.876 | 1500x700 | 4.0 | 2.38 | 2.249 | 172% | NG | |
| 2012 | 2013 | 218 | 5.20 | 5.20 | 0.008 | 0.746 | | 0.754 | 400 | 14.2 | 1.97 | 0.248 | 305% | NG | |
| 2013 | 2015 | 138 | 0.80 | 45.76 | 0.070 | 4.222 | | 4.292 | 1500x700 | 2.0 | 1.68 | 1.588 | 270% | NG | |
| 2014 | 2015 | 102 | 1.35 | 1.35 | 0.002 | 0.205 | | 0.207 | 400 | 4.9 | 1.16 | 0.146 | 142% | NG | |
| 2015 | 2017 | 850 | 6.00 | 53.11 | 0.081 | 3.993 | | 4.074 | 1500x700 | 6.3 | 2.99 | 2.826 | 144% | NG | |
| 2016 | 2017 | 150 | 1.03 | 1.03 | 0.002 | 0.152 | | 0.154 | 400 | 4.0 | 1.05 | 0.132 | 116% | NG | |
| 2017 | 2019 | 280 | 1.35 | 55.49 | 0.085 | 3.932 | | 4.017 | 1500x700 | 8.3 | 3.43 | 3.241 | 124% | NG | |
| 2018 | 2019 | 206 | 1.60 | 1.60 | 0.002 | 0.251 | | 0.254 | 600 | 10.6 | 2.24 | 0.633 | 40% | OK | |
| 2019 | 2021 | 132 | 0.35 | 57.44 | 0.088 | 3.960 | | 4.048 | 1000 | 20.2 | 4.34 | 3.409 | 119% | NG | |
| 2020 | 2021 | 118 | 2.82 | 2.82 | 0.004 | 0.424 | | 0.428 | 400 | 24.5 | 2.59 | 0.325 | 131% | NG | |
| 2021 | 2025 | 250 | 1.14 | 61.40 | 0.094 | 4.029 | | 4.123 | 1000 | 2.0 | 1.37 | 1.076 | 383% | NG | |
| 2022 | 2024 | 269 | 5.75 | 5.75 | 0.009 | 0.878 | | 0.887 | 500 | 10.4 | 1.96 | 0.385 | 231% | NG | |
| 2023 | 2024 | 313 | 2.71 | 2.71 | 0.004 | 0.372 | | 0.376 | 400 | 6.3 | 1.32 | 0.166 | 227% | NG | |
| 2024 | 2025 | 150 | 1.10 | 9.56 | 0.015 | 1.347 | | 1.362 | 500 | 1.5 | 0.74 | 0.145 | 937% | NG | |
| 2025 | 2030 | 290 | 5.30 | 76.26 | 0.116 | 4.744 | | 4.860 | 1000 | 4.4 | 2.02 | 1.587 | 306% | NG | |
| 2026 | 2027 | 253 | 3.12 | 3.12 | 0.005 | 0.440 | | 0.445 | 300 | 11.8 | 1.49 | 0.105 | 423% | NG | |
| 2027 | 2029 | 193 | 1.85 | 4.97 | 0.008 | 0.644 | | 0.652 | 400 | 15.5 | 2.06 | 0.259 | 252% | NG | |
| 2028 | 2029 | 341 | 2.99 | 2.99 | 0.005 | 0.406 | | 0.410 | 400 | 13.3 | 1.91 | 0.240 | 171% | NG | |
| 2029 | 2030 | 175 | 0.54 | 8.50 | 0.013 | 1.123 | | 1.136 | 500 | 4.2 | 1.25 | 0.245 | 463% | NG | |
| 2030 | 2033 | 144 | 1.20 | 85.96 | 0.131 | 5.211 | | 5.343 | 1500x700 | 15.9 | 4.75 | 4.489 | 119% | NG | |
| 2031 | 2032 | 212 | 1.66 | 1.66 | 0.003 | 0.238 | | 0.241 | 400 | 10.8 | 1.72 | 0.216 | 111% | NG | |
| 2032 | 2033 | 316 | 2.82 | 4.48 | 0.007 | 0.613 | | 0.620 | 700x500 | 5.0 | 1.84 | 0.580 | 107% | NG | |
| 2033 | 2034 | 95 | 0.84 | 91.28 | 0.139 | 5.447 | | 5.587 | 1000 | 46.3 | 6.57 | 5.160 | 108% | NG | |
| 2034 | 2044 | 130 | 0.77 | 92.05 | 0.141 | 5.368 | | 5.508 | 800 | 2.0 | 1.18 | 0.593 | 929% | NG | |
| 2035 | 2037 | 130 | 0.90 | 0.90 | 0.001 | 0.147 | | 0.148 | 600 | 6.1 | 1.70 | 0.481 | 31% | OK | |
| 2036 | 2037 | 111 | 1.40 | 1.40 | 0.002 | 0.211 | | 0.213 | 400 | 7.2 | 1.41 | 0.177 | 120% | NG | |

| No. | Down Stream | Length (m) | Area (ha) | | Sewage Quantity | | | Existing Pipe Specification | | | | Capacity | | |
|--------|-------------|------------|-----------|--------|-----------------|-------------|---------------|------------------------------------|--------|-------|---------|------------------------------------|--------------------------------|-------|
| | | | Increment | Total | Sanitary Sewage | Storm Water | Remain Sewage | Q ₁ (m ³ /s) | D (mm) | I (%) | V (m/s) | Q ₂ (m ³ /s) | Q ₁ /Q ₂ | Judge |
| 2037 | 2040 | 438 | 3.80 | 6.10 | 0.009 | 0.823 | | 0.833 | 600 | 23.0 | 3.29 | 0.930 | 90% | OK |
| 2038 | 2040 | 187 | 3.08 | 3.08 | 0.005 | 0.447 | | 0.452 | 400 | 2.0 | 0.74 | 0.093 | 486% | NG |
| 2039 | 2040 | 145 | 0.80 | 0.80 | 0.001 | 0.129 | | 0.131 | 500 | 27.5 | 3.19 | 0.626 | 21% | OK |
| 2040 | 2042 | 538 | 9.90 | 19.88 | 0.030 | 2.214 | | 2.244 | 800 | 8.1 | 2.37 | 1.191 | 188% | NG |
| 2041 | 2042 | 451 | 2.14 | 2.14 | 0.003 | 0.277 | | 0.281 | 400 | 15.7 | 2.08 | 0.261 | 107% | NG |
| 2042 | 2044 | 47 | 0.08 | 22.10 | 0.034 | 2.426 | | 2.459 | 1000 | 2.0 | 1.37 | 1.076 | 229% | NG |
| 2043 | 2044 | 102 | 16.60 | 16.60 | 0.025 | 2.745 | | 2.770 | 800 | 16.6 | 3.39 | 1.704 | 163% | NG |
| 2044 | 2052 | 302 | 0.00 | 130.75 | 0.200 | 7.259 | | 7.458 | 1000 | 4.0 | 1.93 | 1.516 | 492% | NG |
| 2045 | 2046 | 269 | 2.27 | 2.27 | 0.003 | 0.318 | | 0.321 | 400 | 24.9 | 2.62 | 0.329 | 98% | OK |
| 2046 | 2049 | 272 | 4.30 | 6.57 | 0.010 | 0.896 | | 0.906 | 600 | 9.9 | 2.16 | 0.611 | 148% | NG |
| 2047 | 2048 | 196 | 5.50 | 5.50 | 0.008 | 0.795 | | 0.804 | 300 | 2.0 | 0.61 | 0.043 | 1864% | NG |
| 2048 | 2049 | 208 | 3.40 | 8.90 | 0.014 | 1.175 | | 1.189 | 400 | 2.0 | 0.74 | 0.093 | 1279% | NG |
| 2049 | 2051 | 618 | 8.20 | 23.67 | 0.036 | 2.590 | | 2.627 | 600 | 6.7 | 1.78 | 0.503 | 522% | NG |
| 2050 | 2051 | 130 | 1.10 | 1.10 | 0.002 | 0.165 | | 0.166 | 400 | 4.6 | 1.12 | 0.141 | 118% | NG |
| 2051 | 2052 | 365 | 0.30 | 25.07 | 0.038 | 2.462 | | 2.500 | 800 | 4.6 | 1.78 | 0.895 | 279% | NG |
| 2052 | 2053 | 469 | 0.00 | 155.82 | 0.238 | 8.043 | | 8.280 | 600 | 6.1 | 1.70 | 0.481 | 1723% | NG |
| 2053 | 2062 | 930 | 6.33 | 162.15 | 0.248 | 7.338 | | 7.585 | 1000 | 4.8 | 2.11 | 1.657 | 458% | NG |
| 2054 | 2055 | 48 | 0.80 | 0.80 | 0.001 | 0.124 | | 0.126 | 400 | 2.0 | 0.74 | 0.093 | 135% | NG |
| 2055 | 2056 | 151 | 2.47 | 3.27 | 0.005 | 0.516 | | 0.521 | 500 | 5.3 | 1.40 | 0.275 | 190% | NG |
| 2056 | 2057 | 67 | 0.24 | 3.51 | 0.005 | 0.536 | | 0.542 | 600 | 28.3 | 3.65 | 1.032 | 52% | OK |
| 2057 | 2058 | 115 | 14.50 | 18.01 | 0.027 | 2.626 | | 2.653 | 500 | 5.2 | 1.39 | 0.273 | 972% | NG |
| 2058 | 2059 | 152 | 0.00 | 18.01 | 0.027 | 2.466 | | 2.493 | 500 | 31.5 | 3.41 | 0.670 | 372% | NG |
| 2059 | 2061 | 676 | 0.00 | 18.01 | 0.027 | 1.943 | | 1.971 | 600 | 6.5 | 1.75 | 0.495 | 398% | NG |
| 2060 | 2061 | 117 | 3.00 | 3.00 | 0.005 | 0.492 | | 0.496 | 500 | 2.0 | 0.86 | 0.169 | 294% | NG |
| 2061 | 2062 | 868 | 0.00 | 21.01 | 0.032 | 1.779 | | 1.811 | 1000 | 2.0 | 1.37 | 1.076 | 168% | NG |
| 2062 | To STP | 400 | 0.00 | 183.16 | 0.280 | 7.878 | | 8.158 | 1000 | 2.0 | 1.37 | 1.076 | 758% | NG |
| Out-21 | | | | | | | | -7.319 | | | | | | |
| To STP | | | | | 0.280 | | 0.559 | 0.839 | | | | | | |
| 3001 | 3008 | 725 | 24.00 | 24.00 | 0.043 | 2.791 | | 2.833 | 400 | 18.2 | 2.24 | 0.281 | 1007% | NG |
| 3002 | 3004 | 275 | 5.80 | 5.80 | 0.010 | 0.809 | | 0.819 | 400 | 17.8 | 2.21 | 0.278 | 295% | NG |
| 3003 | 3004 | 108 | 0.35 | 0.35 | 0.001 | 0.053 | | 0.053 | 400 | 12.9 | 1.88 | 0.236 | 23% | OK |
| 3004 | 3007 | 42 | 0.10 | 6.25 | 0.011 | 0.858 | | 0.869 | 400 | 57.1 | 3.96 | 0.498 | 175% | NG |
| 3005 | 3006 | 203 | 1.43 | 1.43 | 0.003 | 0.206 | | 0.209 | 300 | 9.8 | 1.35 | 0.095 | 219% | NG |
| 3006 | 3007 | 130 | 0.45 | 1.88 | 0.003 | 0.256 | | 0.259 | 400 | 49.2 | 3.68 | 0.462 | 56% | OK |
| 3007 | 3008 | 25 | 0.03 | 8.16 | 0.015 | 1.098 | | 1.113 | 400 | 2.0 | 0.74 | 0.093 | 1197% | NG |
| 3008 | 3009 | 82 | 1.57 | 33.73 | 0.060 | 4.156 | | 4.216 | 500 | 6.7 | 1.57 | 0.308 | 1368% | NG |
| 3009 | 3011 | 215 | 8.12 | 41.85 | 0.075 | 4.786 | | 4.860 | 600 | 13.9 | 2.56 | 0.724 | 671% | NG |
| 3010 | 3011 | 152 | 1.14 | 1.14 | 0.002 | 0.168 | | 0.170 | 400 | 12.4 | 1.85 | 0.232 | 73% | OK |
| 3011 | 3013 | 66 | 0.20 | 43.19 | 0.077 | 4.838 | | 4.914 | 600 | 21.2 | 3.16 | 0.893 | 550% | NG |
| 3012 | 3013 | 149 | 0.90 | 0.90 | 0.002 | 0.133 | | 0.135 | 400 | 7.3 | 1.42 | 0.178 | 75% | OK |
| 3013 | 3017 | 58 | 1.48 | 45.57 | 0.081 | 5.016 | | 5.097 | 500 | 10.3 | 1.95 | 0.383 | 1331% | NG |
| 3014 | 3015 | 221 | 2.25 | 2.25 | 0.004 | 0.321 | | 0.325 | 300 | 20.3 | 1.95 | 0.138 | 236% | NG |
| 3015 | 3016 | 278 | 4.27 | 6.52 | 0.012 | 0.830 | | 0.841 | 400 | 3.4 | 0.97 | 0.122 | 690% | NG |
| 3016 | 3017 | 180 | 2.94 | 9.46 | 0.017 | 1.122 | | 1.139 | 400 | 2.7 | 0.86 | 0.108 | 1054% | NG |
| 3017 | 3021 | 352 | 7.25 | 62.28 | 0.111 | 6.163 | | 6.273 | 800 | 13.9 | 3.10 | 1.558 | 403% | NG |
| 3018 | 3019 | 227 | 2.42 | 2.42 | 0.004 | 0.377 | | 0.382 | 500 | 2.0 | 0.86 | 0.169 | 226% | NG |
| 3019 | 3020 | 558 | 15.68 | 18.10 | 0.032 | 2.252 | | 2.284 | 600 | 11.9 | 2.37 | 0.670 | 341% | NG |
| 3020 | 3021 | 308 | 2.50 | 20.60 | 0.037 | 2.307 | | 2.344 | 600 | 2.9 | 1.17 | 0.331 | 709% | NG |
| 3021 | 3025 | 132 | 0.60 | 83.48 | 0.149 | 7.951 | | 8.100 | 600 | 3.0 | 1.19 | 0.336 | 2407% | NG |
| 3022 | 3023 | 120 | 1.05 | 1.05 | 0.002 | 0.158 | | 0.160 | 400 | 12.5 | 1.85 | 0.232 | 69% | OK |
| 3023 | 3024 | 268 | 1.93 | 2.98 | 0.005 | 0.433 | | 0.438 | 500 | 19.0 | 2.65 | 0.520 | 84% | OK |
| 3024 | 3025 | 93 | 0.13 | 3.11 | 0.006 | 0.435 | | 0.441 | 600 | 20.4 | 3.10 | 0.877 | 50% | OK |
| 3025 | 3026 | 63 | 0.30 | 86.89 | 0.155 | 8.134 | | 8.289 | 600 | 7.9 | 1.93 | 0.546 | 1519% | NG |
| 3026 | 3027 | 190 | 2.50 | 89.39 | 0.159 | 7.959 | | 8.118 | 800 | 24.7 | 4.13 | 2.076 | 391% | NG |
| 3027 | 3029 | 71 | 0.20 | 89.59 | 0.160 | 7.830 | | 7.990 | 600 | 18.3 | 2.94 | 0.831 | 961% | NG |
| | 3028 | | 4.05 | 4.05 | 0.007 | | | 0.007 | | | | | | |
| 3028 | 3029 | 543 | 7.00 | 11.05 | 0.020 | 0.955 | | 0.975 | 800 | 14.7 | 3.19 | 1.603 | 61% | OK |
| Out-31 | | | | | | | | -9.502 | | | | | | |
| 3029 | 3032 | 256 | 3.20 | 103.84 | 0.185 | 0.493 | 0.358 | 1.036 | 800 | 15.2 | 3.24 | 1.629 | 64% | OK |
| 3030 | 3031 | 402 | 5.91 | 5.91 | 0.011 | 0.781 | | 0.791 | 400 | 11.4 | 1.77 | 0.222 | 356% | NG |
| 3031 | 3032 | 305 | 5.28 | 11.19 | 0.020 | 1.429 | | 1.449 | 600 | 19.0 | 2.99 | 0.845 | 171% | NG |

| No. | Down Stream | Length (m) | | Area (ha) | | Sewage Quantity | | | Existing Pipe Specification | | | | Capacity | |
|--------|-------------|------------|-----------|-----------|-----------------|-----------------|---------------|------------------------------------|-----------------------------|-------|---------|------------------------------------|--------------------------------|-------|
| | | Increment | Increment | Total | Sanitary Sewage | Storm Water | Remain Sewage | Q ₁ (m ³ /s) | D (mm) | I (%) | V (m/s) | Q ₂ (m ³ /s) | Q ₁ /Q ₂ | Judge |
| 3032 | 3039 | 370 | 3.85 | 118.88 | 0.212 | 2.402 | 0.358 | 2.972 | 800 | 7.2 | 2.23 | 1.121 | 265% | NG |
| 3033 | 3035 | 142 | 0.92 | 0.92 | 0.002 | 0.149 | | 0.151 | 500 | 2.0 | 0.86 | 0.169 | 89% | OK |
| 3034 | 3035 | 83 | 0.81 | 0.81 | 0.001 | 0.124 | | 0.125 | 400 | 2.0 | 0.74 | 0.093 | 135% | NG |
| 3035 | 3036 | 85 | 0.94 | 2.67 | 0.005 | 0.381 | | 0.386 | 400 | 10.7 | 1.71 | 0.215 | 180% | NG |
| 3036 | 3038 | 169 | 1.35 | 4.02 | 0.007 | 0.582 | | 0.589 | 500 | 8.2 | 1.74 | 0.342 | 172% | NG |
| 3037 | 3038 | 278 | 1.60 | 1.60 | 0.003 | 0.243 | | 0.246 | 500 | 10.4 | 1.96 | 0.385 | 64% | OK |
| 3038 | 3039 | 166 | 1.15 | 6.77 | 0.012 | 0.917 | | 0.929 | 600 | 28.9 | 3.69 | 1.043 | 89% | OK |
| 3039 | 3041 | 113 | 0.65 | 126.30 | 0.225 | 3.245 | 0.358 | 3.829 | 800 | 10.9 | 2.75 | 1.382 | 277% | NG |
| 3040 | 3041 | 155 | 1.46 | 1.46 | 0.003 | 0.216 | | 0.218 | 400 | 27.7 | 2.76 | 0.347 | 63% | OK |
| 3041 | 3062 | 365 | 2.30 | 130.06 | 0.232 | 3.276 | 0.358 | 3.866 | 800 | 2.8 | 1.39 | 0.699 | 553% | NG |
| 3042 | 3044 | 410 | 5.20 | 5.20 | 0.009 | 0.747 | | 0.756 | 600 | 13.4 | 2.51 | 0.710 | 107% | NG |
| 3043 | 3044 | 98 | 0.77 | 0.77 | 0.001 | 0.117 | | 0.118 | 400 | 2.0 | 0.74 | 0.093 | 127% | NG |
| 3044 | 3045 | 221 | 2.45 | 8.42 | 0.015 | 1.109 | | 1.124 | 500 | 9.9 | 1.91 | 0.375 | 300% | NG |
| 3045 | 3052 | 454 | 11.51 | 19.93 | 0.035 | 2.232 | | 2.268 | 600 | 12.3 | 2.41 | 0.681 | 333% | NG |
| 3046 | 3048 | 263 | 4.73 | 4.73 | 0.008 | 0.665 | | 0.673 | 400 | 2.0 | 0.74 | 0.093 | 724% | NG |
| 3047 | 3048 | 167 | 2.87 | 2.87 | 0.005 | 0.420 | | 0.425 | 400 | 4.7 | 1.14 | 0.143 | 297% | NG |
| 3048 | 3050 | 58 | 0.70 | 8.30 | 0.015 | 1.135 | | 1.150 | 400 | 2.0 | 0.74 | 0.093 | 1236% | NG |
| 3049 | 3050 | 272 | 1.83 | 1.83 | 0.003 | 0.256 | | 0.259 | 400 | 9.5 | 1.62 | 0.204 | 127% | NG |
| 3050 | 3051 | 173 | 1.42 | 11.55 | 0.021 | 1.470 | | 1.491 | 400 | 2.0 | 0.74 | 0.093 | 1603% | NG |
| 3051 | 3052 | 77 | 0.29 | 11.84 | 0.021 | 1.598 | | 1.619 | 600 | 2.0 | 0.97 | 0.274 | 590% | NG |
| 3052 | 3055 | 174 | 1.46 | 33.23 | 0.059 | 3.526 | | 3.585 | 600 | 2.0 | 0.97 | 0.274 | 1307% | NG |
| 3053 | 3054 | 118 | 0.43 | 0.43 | 0.001 | 0.065 | | 0.065 | 400 | 2.0 | 0.74 | 0.093 | 70% | OK |
| 3054 | 3055 | 98 | 0.35 | 0.78 | 0.001 | 0.122 | | 0.123 | 500 | 6.7 | 1.57 | 0.308 | 40% | OK |
| 3055 | 3060 | 12 | 0.01 | 34.02 | 0.061 | 3.599 | | 3.660 | 600 | 2.0 | 0.97 | 0.274 | 1334% | NG |
| 3056 | 3059 | 287 | 2.82 | 2.82 | 0.005 | 0.427 | | 0.432 | 500 | 13.2 | 2.21 | 0.434 | 100% | OK |
| 3057 | 3059 | 203 | 1.29 | 1.29 | 0.002 | 0.203 | | 0.205 | 500 | 17.2 | 2.52 | 0.495 | 41% | OK |
| 3058 | 3059 | 111 | 0.46 | 0.46 | 0.001 | 0.069 | | 0.070 | 400 | 2.0 | 0.74 | 0.093 | 76% | OK |
| 3059 | 3060 | 235 | 1.18 | 5.75 | 0.010 | 0.790 | | 0.800 | 600 | 8.8 | 2.04 | 0.577 | 139% | NG |
| 3060 | 3061 | 114 | 0.45 | 40.22 | 0.072 | 4.107 | | 4.179 | 600 | 2.0 | 0.97 | 0.274 | 1524% | NG |
| 3061 | 3062 | 348 | 8.47 | 48.69 | 0.087 | 4.503 | | 4.590 | 600 | 6.7 | 1.78 | 0.503 | 912% | NG |
| 3062 | 3075 | 514 | 9.30 | 188.05 | 0.335 | 8.346 | 0.358 | 9.040 | 800 | 3.6 | 1.58 | 0.794 | 1138% | NG |
| 3063 | 3065 | 256 | 1.33 | 1.33 | 0.002 | 0.205 | | 0.207 | 600 | 7.8 | 1.92 | 0.543 | 38% | OK |
| 3064 | 3065 | 216 | 1.32 | 1.32 | 0.002 | 0.207 | | 0.209 | 600 | 8.3 | 1.98 | 0.560 | 37% | OK |
| 3065 | 3067 | 86 | 0.75 | 3.40 | 0.006 | 0.503 | | 0.509 | 600 | 2.0 | 0.97 | 0.274 | 186% | NG |
| 3066 | 3067 | 232 | 2.02 | 2.02 | 0.004 | 0.314 | | 0.317 | 600 | 9.0 | 2.06 | 0.582 | 54% | OK |
| 3067 | 3075 | 372 | 2.20 | 7.62 | 0.014 | 0.973 | | 0.987 | 600 | 11.2 | 2.30 | 0.650 | 152% | NG |
| 3068 | 3070 | 416 | 4.63 | 4.63 | 0.008 | 0.665 | | 0.673 | 500 | 2.0 | 0.86 | 0.169 | 399% | NG |
| 3069 | 3070 | 285 | 3.24 | 3.24 | 0.006 | 0.450 | | 0.456 | 400 | 2.8 | 0.88 | 0.111 | 412% | NG |
| 3070 | 3072 | 176 | 1.12 | 8.99 | 0.016 | 1.201 | | 1.217 | 500 | 2.1 | 0.88 | 0.173 | 704% | NG |
| 3071 | 3072 | 114 | 0.68 | 0.68 | 0.001 | 0.102 | | 0.103 | 400 | 9.6 | 1.62 | 0.204 | 51% | OK |
| 3072 | 3074 | 100 | 0.41 | 10.08 | 0.018 | 1.296 | | 1.314 | 500 | 2.9 | 1.04 | 0.204 | 644% | NG |
| 3073 | 3074 | 127 | 0.86 | 0.86 | 0.002 | 0.129 | | 0.130 | 400 | 14.9 | 2.02 | 0.254 | 51% | OK |
| 3074 | 3075 | 574 | 3.36 | 14.30 | 0.025 | 1.513 | | 1.538 | 500 | 7.1 | 1.62 | 0.318 | 484% | NG |
| 3075 | 3077 | 415 | 0.15 | 210.12 | 0.374 | 9.376 | 0.358 | 10.108 | 800 | 2.0 | 1.18 | 0.593 | 1704% | NG |
| 3076 | 3077 | 220 | 1.93 | 1.93 | 0.003 | 0.302 | | 0.306 | 500 | 9.0 | 1.82 | 0.357 | 86% | OK |
| Out-32 | | | | | | | | -9.281 | | | | | | |
| 3077 | 3079 | 270 | 2.80 | 214.85 | 0.383 | 0.428 | 0.755 | 1.565 | 800 | 2.0 | 1.18 | 0.593 | 264% | NG |
| 3078 | 3079 | 533 | 5.32 | 5.32 | 0.009 | 0.667 | | 0.677 | 300 | 2.0 | 0.61 | 0.043 | 1570% | NG |
| 3079 | 3085 | 233 | 0.76 | 220.93 | 0.393 | 1.229 | 0.755 | 2.377 | 800 | 2.0 | 1.18 | 0.593 | 401% | NG |
| 3080 | 3082 | 134 | 0.47 | 0.47 | 0.001 | 0.070 | | 0.071 | 200 | 10.4 | 1.06 | 0.033 | 213% | NG |
| 3081 | 3082 | 70 | 1.43 | 1.43 | 0.003 | 0.220 | | 0.222 | 400 | 2.0 | 0.74 | 0.093 | 239% | NG |
| 3082 | 3084 | 47 | 0.21 | 2.11 | 0.004 | 0.308 | | 0.311 | 400 | 2.0 | 0.74 | 0.093 | 335% | NG |
| 3083 | 3084 | 212 | 1.68 | 1.68 | 0.003 | 0.263 | | 0.266 | 500 | 2.0 | 0.86 | 0.169 | 158% | NG |
| 3084 | 3085 | 70 | 0.21 | 4.00 | 0.007 | 0.609 | | 0.616 | 500 | 2.0 | 0.86 | 0.169 | 365% | NG |
| 3085 | 3104 | 421 | 3.12 | 228.05 | 0.406 | 1.892 | 0.755 | 3.053 | 1000 | 5.8 | 2.32 | 1.822 | 168% | NG |
| 3086 | 3087 | 290 | 2.72 | 2.72 | 0.005 | 0.378 | | 0.383 | 300 | 6.8 | 1.13 | 0.080 | 479% | NG |
| 3087 | 3092 | 95 | 0.30 | 3.02 | 0.005 | 0.402 | | 0.407 | 400 | 27.3 | 2.74 | 0.344 | 118% | NG |
| 3088 | 3089 | 52 | 0.36 | 0.36 | 0.001 | 0.056 | | 0.056 | 300 | 2.0 | 0.61 | 0.043 | 131% | NG |
| 3089 | 3092 | 220 | 1.25 | 1.61 | 0.003 | 0.225 | | 0.228 | 400 | 20.8 | 2.39 | 0.300 | 76% | OK |
| 3091 | 3092 | 199 | 5.17 | 5.17 | 0.009 | 0.748 | | 0.757 | 300 | 3.0 | 0.75 | 0.053 | 1428% | NG |
| 3092 | 3096 | 344 | 4.64 | 14.44 | 0.026 | 1.832 | | 1.858 | 500 | 4.9 | 1.35 | 0.265 | 701% | NG |

| No. | Down Stream | Length (m) | Area (ha) | | Sewage Quantity | | | Existing Pipe Specification | | | | Capacity | | |
|--------|-------------|------------|-----------|--------|-----------------|-------------|---------------|------------------------------------|----------|-------|---------|------------------------------------|--------------------------------|-------|
| | | | Increment | Total | Sanitary Sewage | Storm Water | Remain Sewage | Q ₁ (m ³ /s) | D (mm) | I (‰) | V (m/s) | Q ₂ (m ³ /s) | Q ₁ /Q ₂ | Judge |
| 3093 | 3095 | 327 | 1.95 | 1.95 | 0.003 | 0.267 | | 0.270 | 300 | 2.0 | 0.61 | 0.043 | 626% | NG |
| 3094 | 3095 | 290 | 2.15 | 2.15 | 0.004 | 0.299 | | 0.302 | 300 | 6.8 | 1.13 | 0.080 | 379% | NG |
| 3095 | 3096 | 267 | 0.30 | 4.40 | 0.008 | 0.538 | | 0.546 | 400 | 5.4 | 1.22 | 0.153 | 356% | NG |
| 3096 | 3097 | 191 | 0.38 | 19.22 | 0.034 | 2.280 | | 2.314 | 600 | 9.9 | 2.16 | 0.611 | 379% | NG |
| 3097 | 3100 | 30 | 0.02 | 19.24 | 0.034 | 2.254 | | 2.288 | 600 | 2.0 | 0.97 | 0.274 | 834% | NG |
| 3098 | 3099 | 91 | 0.34 | 0.34 | 0.001 | 0.052 | | 0.052 | 300 | 2.0 | 0.61 | 0.043 | 121% | NG |
| 3099 | 3100 | 251 | 1.24 | 1.58 | 0.003 | 0.234 | | 0.237 | 600 | 8.8 | 2.04 | 0.577 | 41% | OK |
| 3100 | 3103 | 93 | 0.78 | 21.60 | 0.038 | 2.455 | | 2.494 | 800 | 2.0 | 1.18 | 0.593 | 420% | NG |
| 3101 | 3102 | 230 | 1.92 | 1.92 | 0.003 | 0.273 | | 0.277 | 300 | 2.0 | 0.61 | 0.043 | 641% | NG |
| 3102 | 3103 | 239 | 2.20 | 4.12 | 0.007 | 0.579 | | 0.586 | 600 | 8.9 | 2.05 | 0.580 | 101% | NG |
| 3103 | 3104 | 101 | 0.82 | 26.54 | 0.047 | 2.921 | | 2.969 | 800 | 2.0 | 1.18 | 0.593 | 500% | NG |
| 3104 | 3107 | 257 | 2.41 | 257.00 | 0.458 | 4.891 | 0.755 | 6.104 | 1000 | 2.0 | 1.37 | 1.076 | 567% | NG |
| 3105 | 3106 | 187 | 1.49 | 1.49 | 0.003 | 0.236 | | 0.239 | 800 | 2.1 | 1.21 | 0.608 | 39% | OK |
| 3106 | 3107 | 210 | 1.82 | 3.31 | 0.006 | 0.479 | | 0.485 | 500 | 2.0 | 0.86 | 0.169 | 287% | NG |
| 3107 | 3109 | 667 | 11.60 | 271.91 | 0.484 | 5.380 | 0.755 | 6.619 | 1000 | 3.1 | 1.70 | 1.335 | 496% | NG |
| 3108 | 3109 | 193 | 2.23 | 2.23 | 0.004 | 0.353 | | 0.357 | 500 | 5.1 | 1.37 | 0.269 | 133% | NG |
| 3109 | 3113 | 456 | 4.93 | 279.07 | 0.497 | 5.378 | 0.755 | 6.630 | 1000 | 2.0 | 1.37 | 1.076 | 616% | NG |
| 3110 | 3112 | 491 | 2.69 | 2.69 | 0.005 | 0.374 | | 0.378 | 600 | 5.2 | 1.57 | 0.444 | 85% | OK |
| 3111 | 3112 | 181 | 4.18 | 4.18 | 0.007 | 0.610 | | 0.617 | 400 | 7.7 | 1.45 | 0.182 | 339% | NG |
| 3112 | 3113 | 489 | 4.41 | 11.28 | 0.020 | 1.310 | | 1.330 | 600 | 2.0 | 0.97 | 0.274 | 485% | NG |
| Out-33 | | | | | | | | -6.408 | | | | | | |
| 3113 | 3127 | 20 | 0.50 | 290.85 | 0.518 | | 1.034 | 1.552 | 1000 | 2.0 | 1.37 | 1.076 | 144% | NG |
| 3114 | 3116 | 579 | 3.68 | 3.68 | 0.007 | 0.495 | | 0.501 | 500 | 4.6 | 1.30 | 0.255 | 196% | NG |
| 3115 | 3116 | 67 | 0.44 | 0.44 | 0.001 | 0.068 | | 0.069 | 400 | 8.9 | 1.56 | 0.196 | 35% | OK |
| 3116 | 3118 | 68 | 0.32 | 4.44 | 0.008 | 0.581 | | 0.589 | 600 | 10.2 | 2.19 | 0.619 | 95% | OK |
| 3117 | 3118 | 70 | 1.40 | 1.40 | 0.002 | 0.215 | | 0.217 | 400 | 2.0 | 0.74 | 0.093 | 234% | NG |
| 3118 | 3121 | 199 | 2.38 | 8.22 | 0.015 | 1.000 | | 1.015 | 1000x500 | 2.0 | 1.32 | 0.594 | 171% | NG |
| 3119 | 3120 | 268 | 3.27 | 3.27 | 0.006 | 0.458 | | 0.464 | 400 | 6.3 | 1.32 | 0.166 | 279% | NG |
| 3120 | 3121 | 213 | 3.16 | 6.43 | 0.011 | 0.900 | | 0.911 | 500 | 7.9 | 1.71 | 0.336 | 271% | NG |
| 3121 | 3125 | 232 | 2.40 | 17.05 | 0.030 | 1.915 | | 1.946 | 500 | 9.7 | 1.89 | 0.371 | 524% | NG |
| 3122 | 3124 | 276 | 2.60 | 2.60 | 0.005 | 0.363 | | 0.367 | 400 | 9.4 | 1.61 | 0.202 | 181% | NG |
| 3123 | 3124 | 124 | 1.80 | 1.80 | 0.003 | 0.269 | | 0.272 | 400 | 3.2 | 0.94 | 0.118 | 231% | NG |
| 3124 | 3125 | 208 | 0.81 | 5.21 | 0.009 | 0.666 | | 0.675 | 400 | 2.0 | 0.74 | 0.093 | 726% | NG |
| 3125 | 3126 | 500 | 4.58 | 26.84 | 0.048 | 2.378 | | 2.426 | 400 | 10.3 | 1.68 | 0.211 | 1149% | NG |
| 3126 | 3127 | 1009 | 0.00 | 26.84 | 0.048 | 2.022 | | 2.070 | 600 | 3.2 | 1.23 | 0.348 | 595% | NG |
| Out-34 | | | | | | | | -1.925 | | | | | | |
| 3127 | 3152 | 97 | 0.05 | 317.74 | 0.566 | | 1.131 | 1.697 | | | | | | |
| 3128 | 3129 | 254 | 2.27 | 2.27 | 0.004 | 0.320 | | 0.324 | 300 | 8.2 | 1.24 | 0.088 | 370% | NG |
| 3129 | 3131 | 71 | 1.33 | 3.60 | 0.006 | 0.492 | | 0.499 | 400 | 2.0 | 0.74 | 0.093 | 536% | NG |
| 3130 | 3131 | 201 | 1.00 | 1.00 | 0.002 | 0.145 | | 0.146 | 400 | 8.9 | 1.56 | 0.196 | 75% | OK |
| 3131 | 3136 | 122 | 1.40 | 6.00 | 0.011 | 0.849 | | 0.859 | 500 | 2.0 | 0.86 | 0.169 | 509% | NG |
| 3132 | 3133 | 124 | 0.60 | 0.60 | 0.001 | 0.090 | | 0.091 | 300 | 9.6 | 1.34 | 0.095 | 96% | OK |
| 3133 | 3135 | 95 | 0.40 | 1.00 | 0.002 | 0.143 | | 0.145 | 400 | 9.4 | 1.61 | 0.202 | 72% | OK |
| 3134 | 3135 | 149 | 1.16 | 1.16 | 0.002 | 0.171 | | 0.173 | 400 | 2.6 | 0.85 | 0.107 | 162% | NG |
| 3135 | 3136 | 20 | 0.05 | 2.21 | 0.004 | 0.313 | | 0.317 | 400 | 2.0 | 0.74 | 0.093 | 341% | NG |
| 3136 | 3141 | 287 | 4.10 | 12.31 | 0.022 | 1.557 | | 1.579 | 600 | 9.4 | 2.11 | 0.597 | 265% | NG |
| 3137 | 3138 | 328 | 3.02 | 3.02 | 0.005 | 0.451 | | 0.456 | 500 | 8.5 | 1.77 | 0.348 | 131% | NG |
| 3138 | 3140 | 138 | 0.60 | 3.62 | 0.006 | 0.508 | | 0.515 | 600 | 2.0 | 0.97 | 0.274 | 188% | NG |
| 3139 | 3140 | 122 | 4.10 | 4.10 | 0.007 | 0.613 | | 0.621 | 400 | 7.3 | 1.42 | 0.178 | 348% | NG |
| 3140 | 3141 | 68 | 0.39 | 8.11 | 0.014 | 1.110 | | 1.125 | 800 | 2.0 | 1.18 | 0.593 | 190% | NG |
| 3141 | 3142 | 120 | 0.43 | 20.85 | 0.037 | 2.528 | | 2.565 | 800 | 2.0 | 1.18 | 0.593 | 432% | NG |
| 3142 | 3148 | 281 | 1.25 | 22.10 | 0.039 | 2.440 | | 2.479 | 800 | 6.9 | 2.19 | 1.101 | 225% | NG |
| 3143 | 3144 | 159 | 1.39 | 1.39 | 0.002 | 0.204 | | 0.207 | 300 | 16.9 | 1.78 | 0.126 | 164% | NG |
| 3144 | 3145 | 302 | 1.76 | 3.15 | 0.006 | 0.407 | | 0.412 | 400 | 8.9 | 1.56 | 0.196 | 210% | NG |
| 3145 | 3147 | 248 | 5.98 | 9.13 | 0.016 | 1.166 | | 1.183 | 500 | 6.5 | 1.55 | 0.304 | 389% | NG |
| 3146 | 3147 | 185 | 0.70 | 0.70 | 0.001 | 0.111 | | 0.112 | 600 | 4.3 | 1.42 | 0.401 | 28% | OK |
| 3147 | 3148 | 497 | 7.44 | 17.27 | 0.031 | 1.863 | | 1.894 | 600 | 4.6 | 1.47 | 0.416 | 456% | NG |
| 3148 | 3151 | 367 | 1.19 | 40.56 | 0.072 | 3.922 | | 3.994 | 1000 | 4.6 | 2.07 | 1.626 | 246% | NG |
| 3149 | 3150 | 218 | 0.70 | 0.70 | 0.001 | 0.100 | | 0.102 | 300 | 15.1 | 1.68 | 0.119 | 86% | OK |
| 3150 | 3151 | 404 | 3.47 | 4.17 | 0.007 | 0.505 | | 0.512 | 400 | 2.7 | 0.86 | 0.108 | 474% | NG |
| 3151 | 3152 | 430 | 2.30 | 47.03 | 0.084 | 4.055 | | 4.139 | 1000 | 2.0 | 1.37 | 1.076 | 385% | NG |

| No. | Down Stream | Length (m) Increment | Area (ha) | | Sewage Quantity | | | Existing Pipe Specification | | | | Capacity | | |
|--------|-------------|-------------------------|-----------|--------|-----------------|-------------|---------------|------------------------------------|--------|-------|---------|------------------------------------|--------------------------------|-------|
| | | | Increment | Total | Sanitary Sewage | Storm Water | Remain Sewage | Q ₁ (m ³ /s) | D (mm) | I (%) | V (m/s) | Q ₂ (m ³ /s) | Q ₁ /Q ₂ | Judge |
| Out-35 | | | | | | | | -3.887 | | | | | | |
| 3152 | 3154 | 43 | 0.06 | 364.83 | 0.650 | | 1.299 | 1.949 | | | | | | |
| 3153 | 3154 | 464 | 1.32 | 1.32 | 0.002 | 0.170 | | 0.172 | 400 | 2.0 | 0.74 | 0.093 | 185% | NG |
| 3154 | 3157 | 22 | 0.01 | 366.16 | 0.652 | 0.170 | 1.299 | 2.121 | | | | | | |
| 3155 | 3156 | 537 | 3.38 | 3.38 | 0.006 | 0.423 | | 0.429 | 300 | 8.3 | 1.25 | 0.088 | 485% | NG |
| 3156 | 3157 | 480 | 3.45 | 6.83 | 0.012 | 0.718 | | 0.730 | 400 | 2.0 | 0.74 | 0.093 | 785% | NG |
| 3157 | 3164 | 181 | 0.70 | 373.69 | 0.665 | 0.888 | 1.299 | 2.852 | | | | | | |
| 3158 | 3159 | 175 | 1.41 | 1.41 | 0.003 | 0.206 | | 0.209 | 300 | 2.8 | 0.72 | 0.051 | 411% | NG |
| 3159 | 3161 | 149 | 0.81 | 2.22 | 0.004 | 0.304 | | 0.307 | 400 | 3.3 | 0.95 | 0.119 | 258% | NG |
| 3160 | 3161 | 169 | 1.25 | 1.25 | 0.002 | 0.183 | | 0.185 | 400 | 2.0 | 0.74 | 0.093 | 199% | NG |
| 3161 | 3163 | 194 | 5.50 | 8.97 | 0.016 | 1.232 | | 1.248 | 600 | 2.0 | 0.97 | 0.274 | 455% | NG |
| 3162 | 3163 | 150 | 2.50 | 2.50 | 0.004 | 0.369 | | 0.374 | 400 | 2.0 | 0.74 | 0.093 | 402% | NG |
| 3163 | 3164 | 189 | 0.80 | 12.27 | 0.022 | 1.567 | | 1.589 | 600 | 4.2 | 1.41 | 0.399 | 399% | NG |
| Out-36 | | | | | | | | -2.380 | | | | | | |
| 3164 | 3170 | 439 | 3.70 | 389.66 | 0.694 | | 1.374 | 2.068 | | | | | | |
| 3165 | 3166 | 479 | 4.05 | 4.05 | 0.007 | 0.519 | | 0.526 | 300 | 9.1 | 1.31 | 0.093 | 569% | NG |
| 3166 | 3167 | 106 | 0.56 | 4.61 | 0.008 | 0.566 | | 0.574 | 300 | 2.0 | 0.61 | 0.043 | 1332% | NG |
| 3167 | 3168 | 144 | 1.18 | 5.79 | 0.010 | 0.735 | | 0.745 | 800 | 4.3 | 1.73 | 0.870 | 86% | OK |
| 3168 | 3169 | 137 | 0.97 | 6.76 | 0.012 | 0.817 | | 0.829 | 800 | 2.0 | 1.18 | 0.593 | 140% | NG |
| 3169 | 3170 | 392 | 0.00 | 6.76 | 0.012 | 0.717 | | 0.729 | 800 | 13.0 | 3.00 | 1.508 | 48% | OK |
| Out-37 | | | | | | | | -0.680 | | | | | | |
| 3170 | To STP | 930 | 0.00 | 396.42 | 0.706 | | 1.412 | 2.118 | | | | | | |
| 4001 | 4002 | 24 | 5.70 | 5.70 | 0.010 | 0.895 | | 0.904 | 200 | 41.6 | 2.13 | 0.067 | 1351% | NG |
| 4002 | 4003 | 64 | 2.90 | 8.60 | 0.015 | 1.309 | | 1.323 | 300 | 46.8 | 2.96 | 0.209 | 633% | NG |
| 4003 | 4004 | 837 | 13.00 | 21.60 | 0.037 | 2.341 | | 2.377 | 400 | 8.0 | 1.48 | 0.186 | 1278% | NG |
| 4004 | 4006 | 46 | 0.35 | 21.95 | 0.038 | 2.342 | | 2.380 | 300 | 73.1 | 3.70 | 0.262 | 910% | NG |
| | 4005 | | 10.78 | | 0.018 | | | 0.018 | | | | | | |
| 4005 | 4006 | 637 | 4.60 | 4.60 | 0.026 | 0.553 | | 0.580 | 300 | 17.5 | 1.81 | 0.128 | 453% | NG |
| 4006 | 4007 | 34 | 0.25 | 26.80 | 0.064 | 2.825 | | 2.890 | 300 | 11.7 | 1.48 | 0.105 | 2762% | NG |
| 4007 | 4011 | 295 | 2.42 | 29.22 | 0.068 | 2.810 | | 2.878 | 400 | 8.1 | 1.49 | 0.187 | 1537% | NG |
| 4009 | 4010 | 147 | 0.72 | 0.72 | 0.001 | 0.107 | | 0.108 | 300 | 10.2 | 1.38 | 0.098 | 111% | NG |
| 4010 | 4011 | 538 | 11.78 | 12.50 | 0.021 | 1.478 | | 1.499 | 400 | 15.7 | 2.08 | 0.261 | 574% | NG |
| 4011 | 4012 | 74 | 2.68 | 44.40 | 0.094 | 0.411 | | 0.506 | 400 | 7.6 | 1.44 | 0.181 | 279% | NG |
| Out-41 | | | | | | | | -0.317 | | | | | | |
| 4012 | 4013 | 162 | 2.25 | 46.65 | 0.098 | 0.331 | 0.189 | 0.618 | 400 | 9.2 | 1.59 | 0.200 | 309% | NG |
| Out-42 | | | | | | | | -0.421 | | | | | | |
| 4013 | 4015 | 156 | 1.56 | 48.21 | 0.101 | 0.230 | 0.196 | 0.527 | 400 | 5.1 | 1.18 | 0.148 | 356% | NG |
| 4014 | 4015 | 377 | 2.17 | 2.17 | 0.004 | 0.290 | | 0.294 | 400 | 15.6 | 2.07 | 0.260 | 113% | NG |
| 4015 | 4017 | 266 | 2.68 | 53.06 | 0.109 | 0.840 | 0.196 | 1.146 | 400 | 12.0 | 1.82 | 0.229 | 501% | NG |
| 4016 | 4017 | 913 | 12.80 | 12.80 | 0.022 | 1.523 | | 1.545 | 800 | 22.8 | 3.97 | 1.996 | 77% | OK |
| 4017 | 4024 | 154 | 0.88 | 66.74 | 0.132 | 2.702 | 0.196 | 3.031 | 800 | 20.1 | 3.73 | 1.875 | 162% | NG |
| 4018 | 4021 | 313 | 5.26 | 5.26 | 0.009 | 0.722 | | 0.731 | 300 | 17.2 | 1.79 | 0.127 | 578% | NG |
| 4019 | 4020 | 68 | 1.00 | 1.00 | 0.002 | 0.154 | | 0.155 | 300 | 2.0 | 0.61 | 0.043 | 360% | NG |
| 4020 | 4021 | 260 | 1.03 | 2.03 | 0.003 | 0.278 | | 0.281 | 300 | 19.8 | 1.92 | 0.136 | 207% | NG |
| 4021 | 4022 | 57 | 0.35 | 7.64 | 0.013 | 1.017 | | 1.030 | 400 | 24.8 | 2.61 | 0.328 | 314% | NG |
| 4022 | 4023 | 36 | 0.53 | 8.17 | 0.014 | 1.071 | | 1.085 | 400 | 55.5 | 3.90 | 0.490 | 221% | NG |
| | 4023 | | 4.01 | | 0.007 | | | 0.007 | | | | | | |
| 4023 | 4024 | 446 | 4.60 | 12.77 | 0.029 | 1.414 | | 1.443 | 400 | 9.1 | 1.58 | 0.199 | 727% | NG |
| 4024 | 4025 | 170 | 0.88 | 80.39 | 0.163 | 4.253 | 0.196 | 4.612 | 800 | 10.5 | 2.70 | 1.357 | 340% | NG |
| Out-43 | | | | | | | | -4.287 | | | | | | |
| | 4025 | | 7.30 | | 0.012 | | | 0.012 | | | | | | |
| 4025 | 4028 | 196 | 0.97 | 81.36 | 0.177 | 0.153 | 0.325 | 0.655 | 800 | 22.4 | 3.94 | 1.980 | 33% | OK |
| 4026 | 4027 | 976 | 12.24 | 12.24 | 0.021 | 1.306 | | 1.327 | 400 | 30.2 | 2.88 | 0.362 | 367% | NG |
| 4027 | 4028 | 305 | 1.50 | 13.74 | 0.023 | 1.450 | | 1.473 | 500 | 7.5 | 1.67 | 0.328 | 449% | NG |
| | 4028 | | 14.00 | | 0.024 | | | 0.024 | | | | | | |
| 4028 | 4054 | 183 | 0.85 | 95.95 | 0.226 | 2.268 | 0.325 | 2.819 | 800 | 2.0 | 1.18 | 0.593 | 475% | NG |
| 4029 | 4030 | 52 | 1.41 | 1.41 | 0.002 | 0.218 | | 0.221 | 300 | 57.6 | 3.28 | 0.232 | 95% | OK |
| 4030 | 4031 | 215 | 1.92 | 3.33 | 0.006 | 0.466 | | 0.472 | 400 | 6.9 | 1.38 | 0.173 | 272% | NG |
| 4031 | 4036 | 178 | 0.78 | 4.11 | 0.007 | 0.584 | | 0.591 | 500 | 2.0 | 0.86 | 0.169 | 350% | NG |
| 4032 | 4033 | 77 | 0.65 | 0.65 | 0.001 | 0.099 | | 0.100 | 200 | 87.0 | 3.08 | 0.097 | 104% | NG |
| 4033 | 4034 | 153 | 0.88 | 1.53 | 0.003 | 0.218 | | 0.220 | 300 | 23.5 | 2.10 | 0.148 | 148% | NG |

| No. | Down Stream | Length (m) | | Area (ha) | | Sewage Quantity | | | Existing Pipe Specification | | | | Capacity | |
|--------|-------------|------------|-----------|-----------|-----------------|-----------------|---------------|------------------------------------|-----------------------------|-------|---------|------------------------------------|--------------------------------|-------|
| | | Increment | Increment | Total | Sanitary Sewage | Storm Water | Remain Sewage | Q ₁ (m ³ /s) | D (mm) | I (%) | V (m/s) | Q ₂ (m ³ /s) | Q ₁ /Q ₂ | Judge |
| 4034 | 4035 | 169 | 4.18 | 5.71 | 0.010 | 0.757 | | 0.767 | 400 | 20.1 | 2.35 | 0.295 | 260% | NG |
| 4035 | 4036 | 55 | 0.27 | 5.98 | 0.010 | 0.846 | | 0.856 | 500 | 12.7 | 2.17 | 0.426 | 201% | NG |
| 4036 | 4045 | 343 | 2.64 | 12.73 | 0.022 | 1.574 | | 1.595 | 500 | 29.5 | 3.30 | 0.648 | 246% | NG |
| 4037 | 4038 | 175 | 2.49 | 2.49 | 0.004 | 0.365 | | 0.369 | 300 | 18.2 | 1.85 | 0.131 | 282% | NG |
| 4038 | 4041 | 89 | 0.67 | 3.16 | 0.005 | 0.444 | | 0.450 | 400 | 26.9 | 2.72 | 0.342 | 132% | NG |
| 4039 | 4040 | 119 | 0.88 | 0.88 | 0.002 | 0.132 | | 0.134 | 300 | 47.0 | 2.97 | 0.210 | 64% | OK |
| 4040 | 4041 | 50 | 0.10 | 0.98 | 0.002 | 0.144 | | 0.145 | 400 | 2.0 | 0.74 | 0.093 | 156% | NG |
| 4041 | 4042 | 210 | 0.76 | 4.90 | 0.008 | 0.628 | | 0.637 | 400 | 19.5 | 2.31 | 0.290 | 219% | NO |
| 4042 | 4045 | 10 | 0.01 | 4.91 | 0.008 | 0.684 | | 0.693 | 500 | 3.4 | 1.12 | 0.220 | 315% | NG |
| 4043 | 4044 | 119 | 0.55 | 0.55 | 0.001 | 0.083 | | 0.084 | 300 | 42.5 | 2.82 | 0.199 | 42% | OK |
| 4044 | 4045 | 259 | 0.81 | 1.36 | 0.002 | 0.182 | | 0.184 | 400 | 16.9 | 2.15 | 0.270 | 68% | OK |
| 4045 | 4053 | 231 | 1.43 | 20.43 | 0.035 | 2.141 | | 2.176 | 400 | 4.3 | 1.09 | 0.137 | 1588% | NG |
| 4046 | 4047 | 168 | 1.02 | 1.02 | 0.002 | 0.149 | | 0.151 | 300 | 2.3 | 0.66 | 0.047 | 324% | NG |
| 4047 | 4048 | 161 | 1.24 | 2.26 | 0.004 | 0.308 | | 0.312 | 400 | 2.0 | 0.74 | 0.093 | 335% | NG |
| 4048 | 4050 | 423 | 9.14 | 11.40 | 0.019 | 1.432 | | 1.452 | 500 | 30.2 | 3.34 | 0.656 | 221% | NG |
| 4049 | 4050 | 197 | 0.88 | 0.88 | 0.002 | 0.139 | | 0.140 | 500 | 31.4 | 3.41 | 0.670 | 21% | OK |
| 4050 | 4051 | 253 | 2.78 | 15.06 | 0.026 | 1.588 | | 1.613 | 400 | 7.1 | 1.40 | 0.176 | 917% | NG |
| Out-44 | | | | | | | | -1.562 | | | | | | |
| 4051 | 4052 | 354 | 6.88 | 21.94 | 0.037 | 0.930 | 0.051 | 3.019 | 400 | 2.8 | 0.88 | 0.111 | 921% | NG |
| | 4052 | | 21.39 | | 0.037 | | | 0.037 | | | | | | |
| 4052 | 4053 | 404 | 8.05 | 29.99 | 0.088 | 1.876 | | 1.964 | 600 | 9.9 | 2.16 | 0.611 | 322% | NG |
| 4053 | 4054 | 70 | 0.30 | 50.72 | 0.123 | 4.365 | | 4.489 | 600 | 4.2 | 1.41 | 0.399 | 1126% | NG |
| 4054 | 4056 | 115 | 0.31 | 146.98 | 0.349 | 7.157 | 0.377 | 7.883 | 800 | 2.0 | 1.18 | 0.593 | 1329% | NG |
| 4055 | 4056 | 265 | 2.53 | 2.53 | 0.004 | 0.388 | | 0.392 | 500 | 8.6 | 1.78 | 0.350 | 112% | NG |
| 4056 | 4060 | 99 | 0.34 | 149.85 | 0.354 | 7.265 | 0.377 | 7.996 | 800 | 2.0 | 1.18 | 0.593 | 1348% | NG |
| 4057 | 4059 | 62 | 0.50 | 0.50 | 0.001 | 0.077 | | 0.078 | 400 | 2.0 | 0.74 | 0.093 | 84% | OK |
| 4058 | 4059 | 58 | 1.22 | 1.22 | 0.002 | 0.189 | | 0.191 | 400 | 2.0 | 0.74 | 0.093 | 205% | NG |
| 4059 | 4060 | 279 | 7.64 | 9.36 | 0.016 | 1.386 | | 1.402 | 500 | 14.9 | 2.35 | 0.461 | 304% | NG |
| 4060 | 4062 | 25 | 0.03 | 159.24 | 0.370 | 8.431 | 0.377 | 9.178 | 800 | 2.0 | 1.18 | 0.593 | 1547% | NG |
| 4061 | 4062 | 712 | 4.94 | 4.94 | 0.008 | 0.578 | | 0.587 | 400 | 5.7 | 1.25 | 0.157 | 374% | NG |
| Out-45 | | | | | | | | -9.329 | | | | | | |
| 4062 | 4064 | 88 | 0.27 | 164.45 | 0.379 | 0.045 | 0.758 | 1.182 | 800 | 2.0 | 1.18 | 0.593 | 199% | NG |
| 4063 | 4064 | 258 | 2.07 | 2.07 | 0.004 | 0.318 | | 0.321 | 600 | 2.0 | 0.97 | 0.274 | 117% | NG |
| 4064 | 4068 | 93 | 0.31 | 166.83 | 0.383 | 0.422 | 0.758 | 1.563 | 800 | 2.0 | 1.18 | 0.593 | 263% | NG |
| 4065 | 4068 | 461 | 3.64 | 3.64 | 0.006 | 0.513 | | 0.519 | 600 | 3.6 | 1.30 | 0.368 | 141% | NG |
| Out-46 | | | | | | | | -1.303 | | | | | | |
| 4068 | 4070 | 168 | 0.80 | 171.27 | 0.391 | 0.128 | 0.779 | 1.298 | 800 | 2.0 | 1.18 | 0.593 | 219% | NG |
| 4069 | 4070 | 77 | 0.38 | 0.38 | 0.001 | 0.058 | | 0.059 | 400 | 5.1 | 1.18 | 0.148 | 40% | OK |
| 4070 | 4078 | 179 | 1.02 | 172.67 | 0.393 | 0.324 | 0.779 | 1.497 | 800 | 5.9 | 2.02 | 1.015 | 147% | NG |
| 4071 | 4073 | 155 | 1.15 | 1.15 | 0.002 | 0.185 | | 0.187 | 800 | 6.4 | 2.10 | 1.056 | 18% | OK |
| 4072 | 4073 | 58 | 0.28 | 0.28 | 0.000 | 0.043 | | 0.044 | 400 | 2.0 | 0.74 | 0.093 | 47% | OK |
| 4073 | 4075 | 176 | 1.21 | 2.64 | 0.005 | 0.392 | | 0.397 | 500 | 10.7 | 1.99 | 0.391 | 102% | NG |
| 4074 | 4075 | 94 | 0.45 | 0.45 | 0.001 | 0.068 | | 0.069 | 400 | 5.3 | 1.21 | 0.152 | 46% | OK |
| 4075 | 4077 | 74 | 0.40 | 3.49 | 0.006 | 0.503 | | 0.509 | 600 | 8.1 | 1.95 | 0.551 | 92% | OK |
| 4076 | 4077 | 334 | 1.20 | 1.20 | 0.002 | 0.178 | | 0.180 | 500 | 8.9 | 1.81 | 0.355 | 51% | OK |
| 4077 | 4078 | 94 | 0.58 | 5.27 | 0.009 | 0.732 | | 0.741 | 800 | 2.0 | 1.18 | 0.593 | 125% | NG |
| 4078 | 4102 | 191 | 1.83 | 179.77 | 0.405 | 1.269 | 0.779 | 2.453 | 800 | 7.9 | 2.34 | 1.176 | 209% | NG |
| 4079 | 4080 | 107 | 1.37 | 1.37 | 0.002 | 0.207 | | 0.209 | 400 | 2.0 | 0.74 | 0.093 | 225% | NG |
| 4080 | 4082 | 256 | 2.72 | 4.09 | 0.007 | 0.551 | | 0.558 | 400 | 7.7 | 1.45 | 0.182 | 306% | NG |
| 4081 | 4082 | 165 | 0.95 | 0.95 | 0.002 | 0.152 | | 0.154 | 800 | 13.9 | 3.10 | 1.558 | 10% | OK |
| 4082 | 4085 | 174 | 1.18 | 6.22 | 0.011 | 0.848 | | 0.859 | 800 | 10.3 | 2.67 | 1.342 | 64% | OK |
| 4083 | 4084 | 80 | 0.64 | 0.64 | 0.001 | 0.098 | | 0.099 | 400 | 32.5 | 2.99 | 0.376 | 26% | OK |
| 4084 | 4085 | 189 | 3.11 | 3.75 | 0.006 | 0.573 | | 0.579 | 500 | 2.0 | 0.86 | 0.169 | 343% | NG |
| 4085 | 4087 | 182 | 1.07 | 11.04 | 0.019 | 1.406 | | 1.424 | 600 | 2.0 | 0.97 | 0.274 | 519% | NG |
| 4086 | 4087 | 158 | 3.57 | 3.57 | 0.006 | 0.573 | | 0.579 | 800 | 10.1 | 2.64 | 1.327 | 44% | OK |
| 4087 | 4091 | 78 | 0.26 | 14.87 | 0.025 | 1.838 | | 1.863 | 800 | 2.0 | 1.18 | 0.593 | 314% | NG |
| 4090 | 4091 | 162 | 1.27 | 1.27 | 0.002 | 0.204 | | 0.206 | 800 | 2.0 | 1.18 | 0.593 | 35% | OK |
| 4091 | 4097 | 96 | 0.43 | 16.57 | 0.028 | 1.984 | | 2.012 | 800 | 2.0 | 1.18 | 0.593 | 339% | NG |
| 4092 | 4094 | 157 | 1.16 | 1.16 | 0.002 | 0.187 | | 0.189 | 800 | 9.5 | 2.56 | 1.287 | 15% | OK |
| 4093 | 4094 | 69 | 0.31 | 0.31 | 0.001 | 0.052 | | 0.052 | 600 | 37.6 | 4.21 | 1.190 | 4% | OK |
| 4094 | 4096 | 97 | 0.39 | 1.86 | 0.003 | 0.286 | | 0.290 | 800 | 2.0 | 1.18 | 0.593 | 49% | OK |

| No. | Down Stream | Length (m) Increment | Area (ha) | | Sewage Quantity | | | Existing Pipe Specification | | | | Capacity | | |
|---------|-------------|-------------------------|-----------|--------|-----------------|-------------|---------------|------------------------------------|--------|-------|---------|------------------------------------|--------------------------------|-------|
| | | | Increment | Total | Sanitary Sewage | Storm Water | Remain Sewage | Q ₁ (m ³ /s) | D (mm) | I (%) | V (m/s) | Q ₂ (m ³ /s) | Q ₁ /Q ₂ | Judge |
| 4095 | 4096 | 87 | 0.24 | 0.24 | 0.000 | 0.040 | | 0.040 | 800 | 2.0 | 1.18 | 0.593 | 7% | OK |
| 4096 | 4097 | 178 | 1.28 | 3.38 | 0.006 | 0.482 | | 0.487 | 500 | 2.0 | 0.86 | 0.169 | 289% | NG |
| 4097 | 4099 | 215 | 2.23 | 22.18 | 0.038 | 2.470 | | 2.508 | 600 | 5.9 | 1.67 | 0.472 | 531% | NG |
| 4098 | 4099 | 190 | 2.50 | 2.50 | 0.004 | 0.396 | | 0.400 | 500 | 7.3 | 1.64 | 0.322 | 124% | NG |
| 4099 | 4101 | 68 | 0.35 | 25.03 | 0.043 | 2.724 | | 2.766 | 1000 | 2.9 | 1.64 | 1.288 | 215% | NG |
| 4100 | 4101 | 177 | 1.10 | 1.10 | 0.002 | 0.160 | | 0.162 | 400 | 11.2 | 1.75 | 0.220 | 74% | OK |
| 4101 | 4102 | 174 | 1.27 | 27.40 | 0.047 | 2.828 | | 2.875 | 1000 | 2.0 | 1.37 | 1.076 | 267% | NG |
| 4102 | 4104 | 73 | 0.29 | 207.46 | 0.453 | 4.906 | 0.779 | 6.137 | 800 | 11.6 | 2.83 | 1.423 | 431% | NG |
| 4103 | 4104 | 361 | 2.90 | 2.90 | 0.005 | 0.390 | | 0.395 | 400 | 2.4 | 0.81 | 0.102 | 388% | NG |
| Out-47 | | | | | | | | -5.617 | | | | | | |
| 4104 | 4110 | 420 | 2.80 | 213.16 | 0.462 | 0.401 | 0.915 | 1.778 | 800 | 3.8 | 1.62 | 0.814 | 218% | NG |
| 4105 | 4106 | 62 | 0.54 | 0.54 | 0.001 | 0.091 | | 0.092 | 500 | 12.9 | 2.18 | 0.428 | 21% | OK |
| 4106 | 4107 | 243 | 4.91 | 5.45 | 0.009 | 0.820 | | 0.829 | 600 | 18.5 | 2.95 | 0.834 | 99% | OK |
| 4107 | 4110 | 627 | 4.81 | 10.26 | 0.018 | 1.209 | | 1.227 | 800 | 4.7 | 1.80 | 0.905 | 136% | NG |
| 4108 | 4109 | 384 | 5.70 | 5.70 | 0.010 | 0.828 | | 0.838 | 500 | 2.3 | 0.92 | 0.181 | 464% | NG |
| 4109 | 4110 | 99 | 0.67 | 6.37 | 0.011 | 0.875 | | 0.886 | 600 | 2.0 | 0.97 | 0.274 | 323% | NG |
| 4110 | 4118 | 95 | 0.35 | 230.14 | 0.492 | 2.518 | 0.915 | 3.925 | 1000 | 2.0 | 1.37 | 1.076 | 365% | NG |
| 4111 | 4112 | 152 | 1.46 | 1.46 | 0.002 | 0.235 | | 0.238 | 800 | 34.2 | 4.87 | 2.448 | 10% | OK |
| | 4112 | | 8.38 | | | | | 0.000 | | | | | | |
| 4112 | 4113 | 358 | 9.88 | 11.34 | 0.034 | 1.564 | | 1.597 | 800 | 13.9 | 3.10 | 1.558 | 103% | NG |
| Out-48 | | | | | | | | -1.530 | | | | | | |
| 4113 | 4114 | 177 | 3.39 | 14.73 | 0.039 | 0.539 | 0.067 | 0.646 | 500 | 2.2 | 0.90 | 0.177 | 366% | NG |
| 4114 | 4115 | 325 | 8.68 | 23.41 | 0.054 | 1.670 | | 1.725 | 500 | 11.9 | 2.10 | 0.412 | 418% | NG |
| 4115 | 4117 | 166 | 0.74 | 24.15 | 0.056 | 1.664 | | 1.720 | 500 | 2.0 | 0.86 | 0.169 | 1018% | NG |
| 4116 | 4117 | 289 | 1.68 | 1.68 | 0.003 | 0.233 | | 0.236 | 200 | 2.4 | 0.51 | 0.016 | 1474% | NG |
| 4117 | 4118 | 80 | 0.36 | 26.19 | 0.059 | 1.872 | | 1.931 | 500 | 5.1 | 1.37 | 0.269 | 718% | NG |
| 4118 | 4120 | 447 | 8.80 | 265.13 | 0.573 | 4.739 | 0.983 | 6.295 | 1000 | 4.2 | 1.98 | 1.555 | 405% | NG |
| 4119 | 4120 | 150 | 0.82 | 0.82 | 0.001 | 0.121 | | 0.122 | 400 | 6.6 | 1.35 | 0.170 | 72% | OK |
| 4120 | 4122 | 583 | 2.62 | 268.57 | 0.579 | 4.314 | 0.983 | 5.875 | 1000 | 6.6 | 2.48 | 1.948 | 302% | NG |
| 4121 | 4122 | 223 | 2.72 | 2.72 | 0.005 | 0.389 | | 0.393 | 300 | 14.7 | 1.66 | 0.117 | 335% | NG |
| 4122 | 4132 | 234 | 4.20 | 275.49 | 0.590 | 4.659 | 0.983 | 6.232 | 1000 | 2.0 | 1.37 | 1.076 | 579% | NG |
| 4123 | 4124 | 110 | 1.10 | 1.10 | 0.002 | 0.166 | | 0.168 | 300 | 2.7 | 0.71 | 0.050 | 334% | NG |
| 4124 | 4125 | 548 | 6.00 | 7.10 | 0.012 | 0.848 | | 0.860 | 400 | 6.9 | 1.38 | 0.173 | 496% | NG |
| 4125 | 4129 | 368 | 4.50 | 11.60 | 0.020 | 1.327 | | 1.346 | 500 | 18.4 | 2.61 | 0.512 | 263% | NG |
| 4126 | 4127 | 473 | 6.90 | 6.90 | 0.012 | 0.885 | | 0.896 | 400 | 9.0 | 1.57 | 0.197 | 454% | NG |
| 4127 | 4128 | 341 | 7.50 | 14.40 | 0.025 | 1.626 | | 1.650 | 300 | 7.6 | 1.19 | 0.084 | 1962% | NG |
| 4128 | 4129 | 197 | 1.50 | 15.90 | 0.027 | 1.676 | | 1.703 | 400 | 11.6 | 1.78 | 0.224 | 762% | NG |
| 4129 | 4131 | 130 | 0.80 | 28.30 | 0.048 | 2.846 | | 2.895 | 400 | 37.6 | 3.21 | 0.403 | 718% | NG |
| 4130 | 4131 | 435 | 5.90 | 5.90 | 0.010 | 0.771 | | 0.781 | 400 | 33.5 | 3.03 | 0.381 | 205% | NG |
| 4131 | 4132 | 213 | 0.90 | 35.10 | 0.060 | 3.302 | | 3.362 | 400 | 2.0 | 0.74 | 0.093 | 3616% | NG |
| Out-49 | | | | | | | | -8.294 | | | | | | |
| 4132 | To STP | 0 | 0.00 | 310.59 | 0.650 | | 1.301 | 1.951 | 1000 | 2.0 | 1.37 | 1.076 | 181% | NG |
| 5001 | 5002 | 94 | 0.50 | 0.50 | 0.001 | 0.076 | | 0.077 | 400 | 28.7 | 2.81 | 0.353 | 22% | OK |
| 5002 | 5006 | 519 | 5.35 | 5.85 | 0.009 | 0.776 | | 0.785 | 1000 | 7.3 | 2.61 | 2.050 | 38% | OK |
| 5003 | 5004 | 100 | 0.50 | 0.50 | 0.001 | 0.076 | | 0.077 | 300 | 7.9 | 1.22 | 0.086 | 89% | OK |
| 5004 | 5005 | 350 | 2.70 | 3.20 | 0.005 | 0.415 | | 0.420 | 400 | 11.1 | 1.75 | 0.220 | 191% | NG |
| 5005 | 5006 | 179 | 4.15 | 7.35 | 0.011 | 0.968 | | 0.979 | 1000 | 11.7 | 3.30 | 2.592 | 38% | OK |
| 5006 | To STP | 195 | 1.10 | 14.30 | 0.021 | 1.751 | | 1.772 | 1000 | 6.6 | 2.48 | 1.948 | 91% | OK |
| Outfall | | | | | | | | -1.729 | | | | | | |
| To STP | | | | | 0.021 | | 0.043 | 0.064 | | | | | | |
| 6001 | 6002 | 87 | 0.30 | 0.30 | 0.000 | 0.046 | | 0.046 | 200 | 14.9 | 1.27 | 0.040 | 116% | NG |
| 6002 | 6003 | 273 | 4.20 | 4.50 | 0.007 | 0.606 | | 0.612 | 300 | 13.1 | 1.57 | 0.111 | 552% | NG |
| 6003 | 6006 | 358 | 4.80 | 9.30 | 0.014 | 1.085 | | 1.099 | 300 | 8.3 | 1.25 | 0.088 | 1244% | NG |
| 6004 | 6005 | 216 | 2.40 | 2.40 | 0.004 | 0.344 | | 0.348 | 200 | 14.4 | 1.25 | 0.039 | 886% | NG |
| 6005 | 6006 | 396 | 4.60 | 7.00 | 0.010 | 0.851 | | 0.861 | 300 | 25.0 | 2.16 | 0.153 | 564% | NG |
| 6006 | 6009 | 225 | 2.30 | 18.60 | 0.028 | 2.003 | | 2.031 | 400 | 16.4 | 2.12 | 0.266 | 762% | NG |
| 6007 | 6008 | 117 | 1.10 | 1.10 | 0.002 | 0.165 | | 0.167 | 300 | 2.0 | 0.61 | 0.043 | 387% | NG |
| 6008 | 6009 | 290 | 2.40 | 3.50 | 0.005 | 0.462 | | 0.467 | 400 | 2.0 | 0.74 | 0.093 | 503% | NG |
| 6009 | 6013 | 48 | 0.20 | 22.30 | 0.033 | 2.365 | | 2.398 | 300 | 2.0 | 0.61 | 0.043 | 5562% | NG |
| 6010 | 6011 | 350 | 3.00 | 3.00 | 0.004 | 0.405 | | 0.410 | 200 | 19.1 | 1.44 | 0.045 | 906% | NG |
| 6011 | 6012 | 260 | 4.50 | 7.50 | 0.011 | 0.911 | | 0.923 | 300 | 13.0 | 1.56 | 0.110 | 837% | NG |

| No. | Down Stream | Length (m) | | Area (ha) | | Sewage Quantity | | | Existing Pipe Specification | | | | Capacity | |
|---------|-------------|------------|-----------|-----------|-----------------|-----------------|---------------|------------------------------------|-----------------------------|-------|---------|------------------------------------|--------------------------------|-------|
| | | Increment | Increment | Total | Sanitary Sewage | Storm Water | Remain Sewage | Q ₁ (m ³ /s) | D (mm) | I (%) | V (m/s) | Q ₂ (m ³ /s) | Q ₁ /Q ₂ | Judge |
| 6012 | 6013 | 215 | 1.30 | 8.80 | 0.013 | 0.987 | | 1.000 | 400 | 5.5 | 1.23 | 0.155 | 647% | NG |
| 6013 | To STP | 961 | 0.00 | 31.10 | 0.046 | 2.491 | | 2.537 | 400 | 2.0 | 0.74 | 0.093 | 2728% | NG |
| Outfall | | | | | | | | -2.444 | | | | | | |
| To STP | | | | | 0.046 | | 0.093 | 0.139 | | | | | | |
| 7001 | 7002 | 451 | 4.08 | 4.08 | 0.006 | 0.529 | | 0.535 | 200 | 23.9 | 1.61 | 0.051 | 1058% | NG |
| 7002 | 7003 | 100 | 3.50 | 7.58 | 0.011 | 0.944 | | 0.955 | 200 | 12.0 | 1.14 | 0.036 | 2668% | NG |
| 7003 | 7004 | 160 | 3.10 | 10.68 | 0.016 | 1.364 | | 1.380 | 600 | 21.8 | 3.21 | 0.908 | 152% | NG |
| 7004 | To STP | 250 | 14.90 | 25.58 | 0.038 | 2.988 | | 3.026 | 600 | 12.8 | 2.46 | 0.696 | 435% | NG |
| Outfall | | | | | | | | -2.950 | | | | | | |
| To STP | | | | | 0.038 | | 0.076 | 0.114 | | | | | | |