## 4.3.3 Vehicle fuel in MOT

## (1) Fuel property

The National Iranian Oil Company (NIOC) has specified standards of each fuel consumed in Iran, which must be met. According to them, the maximum permissible amount of metallic lead and sulfur in normal gasoline is 0.56/lit and 0.1w% respectively, and specific gravity must be 0.73, while the maximum permissible amount of sulfur in gas oil is 1.0w%, and specific gravity must be 0.83 to 0.86.

The JICA study team analyzed the components of normal gasoline and gas oil, and found that the metallic lead content was 0.22 g/lit and the sulfur content was 86 wtppm in normal gasoline, and that the sulfur content in gas oil was 0.8 wt%, which met the NIOC standards.

Table 4.3.3-1 shows the standards of European countries, the USA and Asian countries relating to the sulfur content in gas oil, and the actual values obtained from their analysis. The maximum permissible amount of sulfur in gas oil in all the developed countries is equal to or less than 0.2 w%, and among those countries the USA and Japan (effective from October, 1997) have a stricter standard of 0.05 w%. Also there are a few countries whose sulfur content amounts exceed 0.8 w%, which indicates that the amount of sulfur content in Iran's gas oil is one of the highest in the world.

## (2) Fuel consumption

Table 4.3.3-2 indicates the amount of fuel consumed by automobiles in the GTA. Amounts of sulfur contained in gas oil and gasoline is 1.0wt% (NIOC GAS OIL 606) and 0.1wt% (NIOC MOGAS 220) respectively.

Oxygenated gasoline has been used as vehicle fuel in Tehran since August 1990. Fig. 4.3.3-1 shows the percentage of oxygenated gasoline in the total gasoline consumption in Tehran from 1991 to 1995 on a yearly basis. Use of oxygenated gasoline has grown 0.28 % to 0.3 % a year, and extrapolation from the growth rate leads to the estimation that use of oxygenated gasoline will be about 4 % in 2001.

Table 4.3.3-3 indicates an amount of gas oil consumed by railways in Iran. The total amount of SOx emissions was calculated from this amount of total consumption, and their results are outlined in Table 4.3.3-4. In comparison with automobiles, an amount of SOx emitted by railways is very small and could therefore be ignored.

Table 4.3.3-1 Comparison of sulfur content of diesel oil standareds

turone IIS As of 1995

Europe, U.S.			AS 01 1000
Countrie	Standard (Upper limits) wt %	Actual values	Enforcement dates
EU Nations	0.2	0.04 - 0.3	Effective Oct. '94
	0.05		From Oct. '96
Belgium	0.2	0.11 - 0.7	Effective Oct. '89
Denmark	0.2	0.04 - 0.05	Effective Oct. '89
Irish Republic	0.3		
Italy	0.2	0.12 - 0.2	From Jan.'93(north) Oct. '93(south)
France	0.3	0.1 - 0.3	
Germany	0.2	0.05 - 0.19	
Greece	0.3	ř.	
Luxemburg	0.2	0.11 - 0.17	Effective Oct. '89
Netherlands	0.2	0.11 - 0.17	Effective Oct. '89
Portugal	0.3	0.23	
Spain	0.3	0.21 - 0.3	
United Kubgd	0.2	0.08 - 0.26	By BS EN 590 1993
U.S.	0.05		From Oct. '93

Asia

	Standard		en e
	(Upper limits		Sulfur reduction plan
Countrie	wt%	wt %	
Chaina	0.5		
Hong Kong	0.2	0.1 - 0.47	Euro 1 in '95
			Euro 2 in'96
			0.05% in '96
India	1	0.24 - 0.88	Effective Oct. '89
Indonesia	0.5	0.33 - 0.36	
Korea	0.2	0.13 - 0.17	0.1% in '96 Predicted 0.05% in '98
Malaysia	0.5	0.1	0.3% in '97
Pakistan	1	0.76 - 0.87	
Philippines	0.8		0.5% in '96
Singapore	0.5	0.26 - 0.47	Predicted 0.3% in '96
Taiwan	0.3		0.05% in '97
Thailand	0.5	0.32	0.5% in Jan.'96 Predicted 0.05% in 2000
Japan	0.2	0.24 - 0.88	From Oct. '92
	0.05		From Oct. '97

Surce: The 3rd meeting of experts on motorization and the environmental issue, part 2
Contents of countermeasures to prevent air pollution caused by motor vehicle,
Japan automobile standard internationalization center, December 6, 1995

Table 4.3.3-2 Fuel consumption by vehicles in GTA

	<del>,</del>	·		<del></del>	· · · · · · · · · · · · · · · · · · ·		<del> –</del> .	,		UNIT: 1	0 <sup>1</sup> liter
Year Type of Fuel	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995
Gas Oil	363,104	333,895	335,755	359,808	358,174	336,157	352,791	365,000	375,007	366,585	347,755
Normal Gasoline	1,698,628	1,649,713	1,736,912	1,752,064	1,935,085	2,067,530	2,188,519	2,320,360	2,434,406	2,467,244	2,599,646
Super Gasoline	148,457	20,469	1,421	8,584	6,298	6,362	13,023	41,609	76,206	99,252	124,473
Un-leaded Gasolin		······				3,499	24,364	11,686	38,235	58,060	68,224

Source: Air Quality Control Company (Quantity of gas oil consumption was amended in accordance with The URBAN AGE)

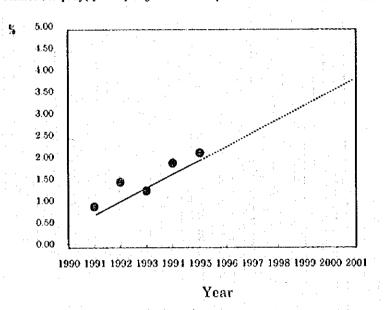


Fig. 4.3.3-1 Percentage of oxygenated gasoline in the total gasoline consumption in GTA

Table 4.3.3-3 Gas oil consumption in railway in IRAN

		Unit : liter
	1994	1995
Electric diesel	144,397,090	165,399,967
Cranes	368,562	276,011
Tehran station	18,211,778	23,180,331
Total	162,977,430	188,856,309

Source: Iranian Islamic Republic Railway

Table 4.3.3-4 Sox emission from raiway in IRAN

	Unit: ton/ye					
	1994	1995				
Electric diesel	2,484	2,845				
Cranes	6:	5				
Tehran station	313	399				
Total	2,803	3,249				

### 4.3.4 Traffic volume survey

MOT has established an area in the central part of the City in which unauthorized vehicles entry is restricted. In addition, controls have also been placed on the entry of large trucks into the city, as well as on the flow of traffic by establishing a large number of one-way streets.

In order to analyze the present status of pollution and evaluate impacts of these measures, it is necessary to understand the current status, such as the traffic volume within Tehran and their daily fluctuation patterns. Such variables are characterized by places, time and land usage in each area of the City, such as, commercial, industrial and residential areas and are affected by traffic regulations or restrictions.

The objectives of this survey are to understand the characteristics inherent with the volume of traffic and their daily fluctuation patterns within Tehran, and to correlate these findings for preparation of an effective countermeasure.

The survey was implemented at the 20 major intersections in Tehran as indicated in Fig.4.3.4-1. In selecting these locations, (1) past traffic volume survey results, (2) road types, (3) present status of traffic control, and (4) land usage have been taken into consideration. The names of the survey points and their numbers shown in Fig.4.3.4-1 are as follows:

- 1 BOZORG-RAH-E-RESALAT
- 2 MEDAN-E-FATEMI

- 3 MEDAN-E-ENQELAB
- 4 MEYDAN-E-GOMROK
- 5 INTERSECTION, SHAHID MOSTAFA KHOMEYNI and MOLAVI
- 6 INTERSECTION, JOMHURI-YE-ESLAMI and FERDOWSI
- 7 BOZORG-RAH-E-SHAHID DOKTOR CHAMRAN
- 8 BOZORG-RAH-E-SHEYKH FAZL-OL-LAH-NURI
- 9 MEYDAN-E-RESALAT
- 10 MEYDAN-E-KHORASAN
- 11 MEYDAN-E-AZADI
- 12 MEYDAN-E-VALI-YE-ASR
- 13 MEYDAN-E-SHUSH

- 14 INTERSECTION, VALI-YE-ASR and ENQELAB
- 15 INTERSECTION, SOHRVARDI and SHAHID AYATOLI A BEHESHITI
- 16 INTERSECTION, SABALAN and DAMAVAND
- 17 JADDEH-YE-KHORASAN
- 18 INTERSECTION, FADATYAN-E-ESLAM and JADDEH-YE-VARAMIN
- 19 INTERSECTION, QUAZVIN and AZARI
- 20 BOZORG RAH-E-AYATOLLAH-E-SADR



Fig. 4.3.4-1 Survey Sites of traffic volume survey and survey routes of field driving test

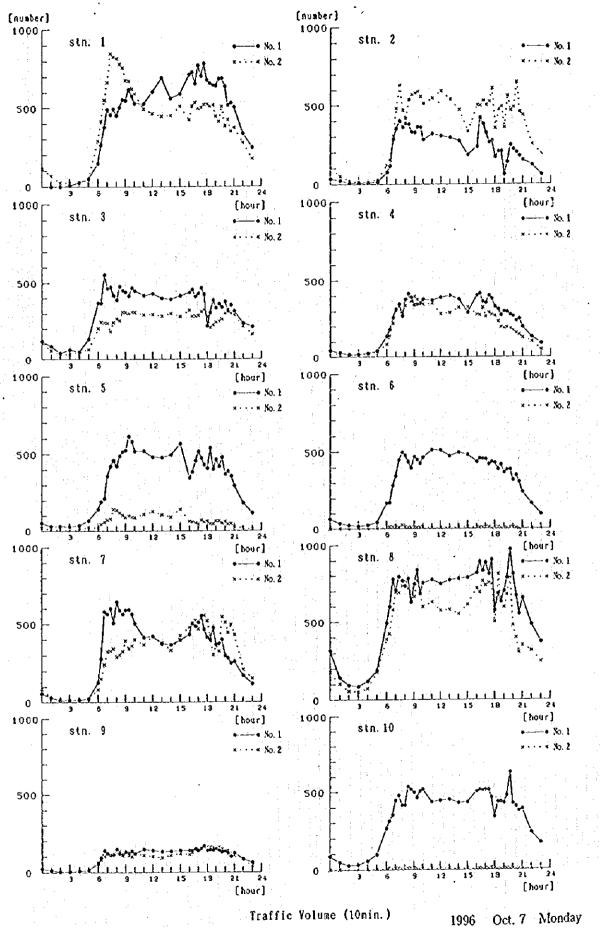


Fig.4.3.4-2(1) Fluctuation of daily traffic Volume

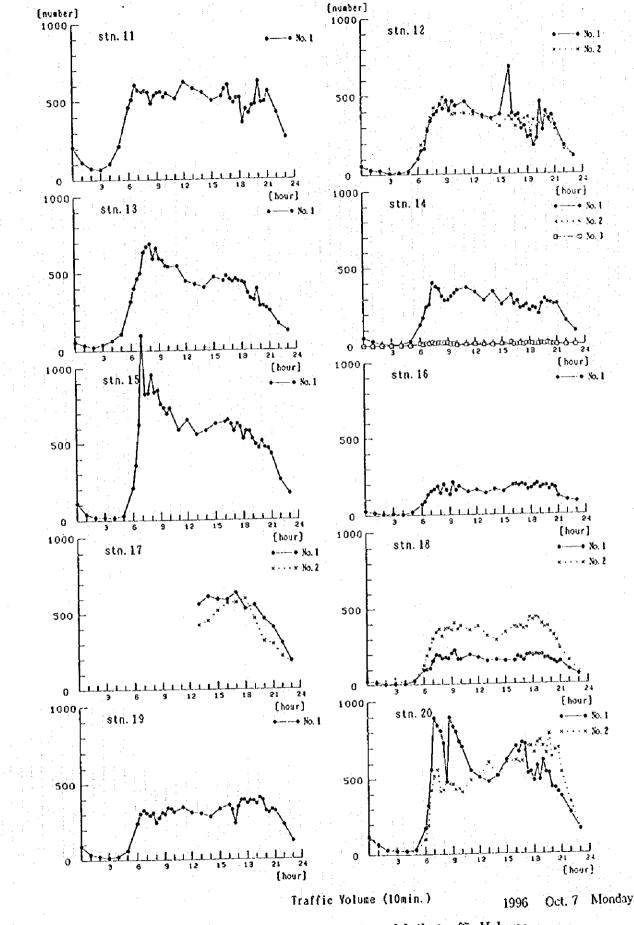


Fig.4.3.4-2(2) Fluctuation of daily traffic Volume

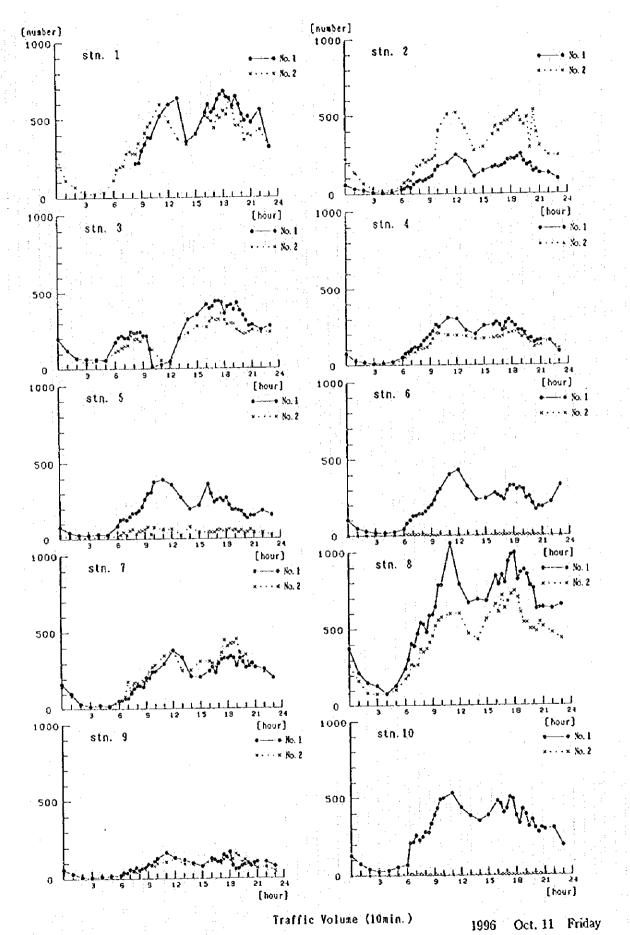


Fig.4.3.4-2(3) Fluctuation of daily traffic Volume

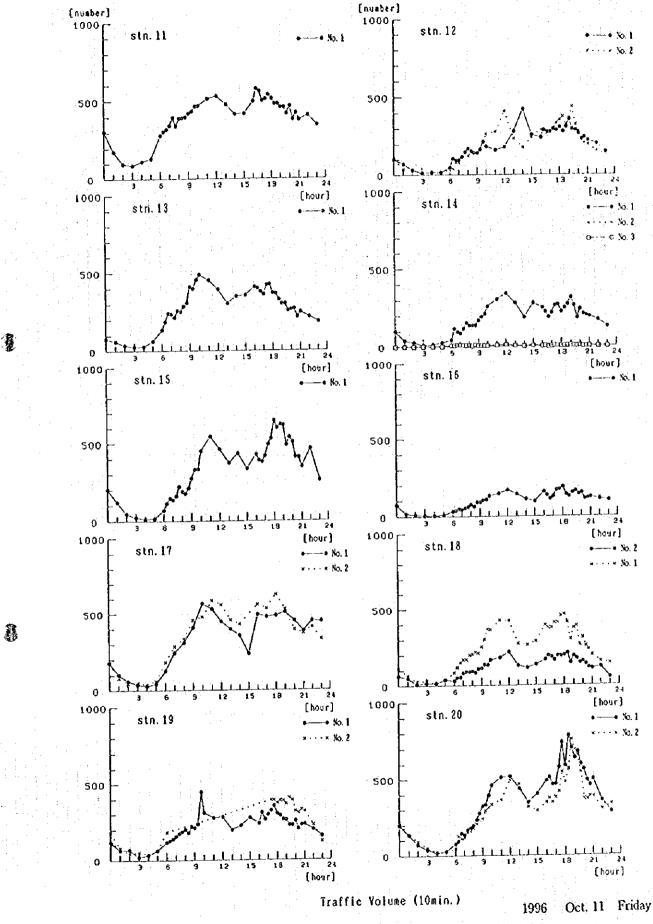


Fig.4.3.4-2(4) Fluctuation of daily traffic Volume

At each surveying point, a video camera with a recorder unit was installed to count traffics and classified by vehicle types and driving pictures were later played back. The types of vehicle were classified into seven categories, i.e. passenger cars, pick-ups, mini-buses, buses, mini trucks, trucks and motor cycles. Although recordings were made continuously over a 24hour period from midnight, measurements and counting were selectively carried out so as to meet the study objectives. The measurements were based on 10 minute periods from the beginning of every hour during the off-peak time, i.e. total of 10 minutes every hour, and additionally 10 minutes at a frequency of every 20 minutes during the peak hours totaling 30 minutes every hour.

-Measurement/Counting time in off-peak times;

12:00 midnight to 05:00, 10:00 to 15:00, 21:00 to 23:00

-Measurement/Counting time in peak times;

06:00 to 09:00, 16:00 to 20:00

The survey was carried out on two separate days; a normal working day and a holiday. As Thursday is a half-day and Friday is a holiday in Iran, Friday was selected as the holiday for the survey, and Monday was selected as the normal working day.

1st survey (working day): October 7, 1996 (Monday)

2nd survey (holiday) : October 11, 1996 (Friday)

### (1) Daily traffic volume fluctuations

The daily fluctuation patterns at each survey point are outlined in Fig.4.3.4-2(1) to 4.3.4-2(4). These daily fluctuations will be classified into the following three categories:

## 1) Restricted area pattern

This pattern may be applicable to the roads located in the restricted area and/or its vicinities. The survey sites numbered 6, 12, 14 corresponding to the restricted area, as well as 2, 3, 4 and 5 corresponding to the borders are included in this pattern.

The volume of traffic begins to increase from around 05:00, peaks between 07:00 and 09:00 and decreases after this hours until around 18:00. The rates of reduction are clearly similar at all survey points.

No remarkable peaks in traffic volume were observed in the mornings or evenings, while the main feature of this pattern is indicated by the daily fluctuation chart. The ratio of traffic volume among three periods in a day, i.e. prior to 05:00, between 05:00 and 06:00, and after 06:00, is approximately 1:10:5.

### 2) Main commuter road pattern

This pattern may be applicable to the main roads and highways linking the central part of Tehran with the suburbs. The survey sites numbered 1, 7, 10, 13 and 15 are governed by this pattern.

The traffic into the center of the city from the suburbs begins to increase around 05:00 and peaks between 06:00 and 09:00 in the same way as the above 1). The volume of traffic during the peak period is 1.5 to 2.0 times bigger than that observed in 1).

After the morning peak period, traffic volume is reduced until midday, and levels off during the hours of 12:00 and 15:00. The volume of traffic during this period was approximately a half or two-thirds of the morning peak period.

There were many locations where increases in traffic volume were recorded from about 15:00 until the peak reached at approximately 18:00. However, the evening peak was not so remarkable as the morning peak, with volumes remaining at around two thirds to three-quarters of those recorded in the morning.

On the other hand, the above-mentioned phenomena were reversed for the traffic heading from the center of the city to the suburbs. In other words, a peak was recorded in the evening, reflecting commutation from the suburbs into the city center.

Observing both of these types indicates that traffic volume peaks were apparent in the morning and the evening, and the main feature of this pattern is in the indication of

fluctuations in both types.

The ratio of traffic volume among five periods in a day -- prior to 05:00, between 05:00 and 12:00, between 12:00 and 15:00, between 15:00 and 21:00 and after 21:00 - was approximately 1:15:10:15:5.

## 3) By-pass pattern

This pattern may be applicable to the area surrounding Azadi Square in the western part of Tehran. The survey site numbered 8 and 11 are covered by this pattern.

Drastic increases in traffic volume was observed between 03:00 and 04:00, slightly earlier than the peaks described under 1), 2), which continued until about 06:00, leveled off between 06:00 and 09:00, and then began to decrease slightly. In other words, this pattern closely resembles that explained in 1), but the night-time traffic was 2.5 to 3 times greater than that of pattern described in 1).

It is thought that the reasons for the increased volume of night-time traffic at these survey sites is the effect of linking the western part of Tehran with the by-pass to the city of Karaj including a connection to the airport.

# (2) Traffic volume features of each vehicle type

The followings are the results of the traffic volume survey corresponding to vehicle types:

1) Passenger cars

Patterns similar tendencies to the fluctuation of overall traffic volume explained in (1) were observed, because passenger cars accounted for a large percentage of all vehicle types.

#### 2) Buses, mini-buses

The traffic volume in this sector was drastically smaller, but the fluctuation patterns were similar to those explained in (1)2). In other words, the fluctuations revealed the morning peak at around 07:00 and the evening peak at around 17:00, because companies and schools run buses in the city for business and student commuters during this period.

Traffic volume for this sector was not significant in early morning or at night because public buses transport tourists, company employees and students who do not ride them during the night and early morning.

## 3) Trucks, mini-trucks

There were many survey sites that recorded increased traffic volume before 05:00 and

after 21:00 in comparison with daytime traffic, because the entry of trucks into the city of Tehran during the daytime is restricted, and these restrictions are released at night.

At survey locations numbered 7 and 18, more traffic volume was observed on the trunk roads linking the suburbs with the center of Tehran, and less traffic in the restricted area.

## 4) Pick-ups

There was no remarkable peak in the morning or evening, and the fluctuation pattern was similar to that described under (1)1). In other words: namely, traffic volume began to increase after 05:00, leveled off between 09:00 and 18:00, and then dramatically decreased after that, indicating the fluctuation pattern of this vehicle type. As pick-ups are mostly used for transporting small-scale cargo, the traffic volume at survey points 4, 5 and 13, located near bazaars, was greater, but almost non-existent during the night and early morning when commercial activities are halted.

## 5) Motor cycles

A

The fluctuation pattern was similar to that of passenger cars. The highest level of traffic volume was recorded at survey points 4, 5, 10 and 13 near bazaars.

This report concentrates on the traffic volume on normal working days. It was thought that these data would be more important from the viewpoint of the effects on atmospheric pollution, because there are more working days than holidays. Simulations will be carried out with the use of the traffic characteristics observed on working days during the current phase of the study, but examinations will be carried out on the characteristics of holidays' traffic volume in the near future to incorporate the outcome in simulations if necessary.

# 4.3.5 Field driving test

As the pollutants contained in automobile exhaust gas differ according to the vehicular driving conditions, it is necessary to clearly understand the driving conditions in the relevant areas in order to verify and forecast the amount of pollutants to be emitted into the atmosphere. In order to examine the driving conditions within the city of Tehran, an automobile was mounted with speedometers and other measurement instrument and driven through pre-determined roadways at different times. A driving cycle, i.e. a test mode reflecting actual conditions within the city of Tehran, was determined on the basis of average

speed, idling, acceleration, deceleration, and a comparison of stable-speed ratio obtained from the results of the driving tests. The concentration, volume and temperature of the exhaust gas emitted during two of the driving tests were also measured, emission coefficients were calculated at ten second intervals, and a survey was carried out to verify a relationship between driving conditions and the emission coefficients.

The survey routes of the test drives are outlined in Fig.4.3.4-1. These routes were selected in consideration of the following points.

- -Roads, which have much traffic volume and are thought to contribute to atmospheric pollution.
- -Roads which have comparatively large intersections.
- The inclusion of several different types of roads (highways, trunk roads, etc.)

The names of the survey routes are as follows:

- A BOZORG RAH-E-SHAHID DOKTOR CHAMRAN
- B TEHRAN KARAJ FREE WAY
- C BEHESHT- E -ZAHRA, KARAJ RING ROAD
- D BESAT HIGHWAY
- E MEYDAN-E-GOMROK → MOLAVI → VALI-YE-ASR → INTERSECTION

DOCTOR HOSEYN-E-FATEMI

VALI-YE-ASR

F MOFATEH → SADI → EKBATAN → EMAMKHOMAYNI → BABHOMAYUN
DAVAR → BANZAM—E—KHORDAD → INTERSECTION

SHAHID MOSTAFA KHOMEYNI

BANZAM-E-KHORDAD

- G MEYDAN-E-EMAMHOSEYN → ENQELAB → AZADI → MEYDAN-E-AZADI
- H INTERSECTION → BOLVAR-E-KESHAVARZ → KARIM KHAN-E-ZAND

KARGAR

BOLVAR-E-KESHAVARZ

SHAHID HOJJAT-OL-ESLAM DOKTOR MOFATTEH → BAHAR-E-SHIRZ

### SHORVARDI → INTERSECTION

SHORVARDI

#### OSTAD MOTAHHAR

I INTERSECTION → DOKTOR ALI—YE—SHARIATI → MEYDAN—E—QODS

DOKTOR ALI-YE-SHARIATI

BOZORG RAH-E-RESALAT

J MEYDAN-E-TAJIRISH → VALI-YE-ASR → INTERSECTION

VALI-YE-ASR

DOKTOR HOSEYN-E-FATEMI

J1 MEYDAN-E-FATEMI → INTERSECTION

KARGAR

KESHAVARZ

K MEYDAN—E—QAZVIN  $\rightarrow$  QUAZVIN  $\rightarrow$  AZARI

SHAHID RAJA'I

SHUSH

N MEYDAN AVVEL → SAD-O-CHEHEL-O-DOVVOM-E-GHARBI → GOLBARG

→ SHAHID AYATOLLAH MADANI → SABALAN

N1 DOKTOR BEHESHITI

Nº MOTAHHARI

- S BOZORG RAH-E-SHEYKH FAZL-OL-LAH-E-NURI
- X MEYDAN-E-ENQELAB → KHOMEYNI → MEYDAN-E-MOHAMMADIYEH
- Y AMIRKABIR→MEYDAN-E-EMAMKHOMEYNI → MEYDAN-E-FERDOWSI
- Z MEYDAN-E-KHORASAN → MEYDAN-E-EMAMHOSEYN

The measurement items and methods of measurement for the field driving tests are outlined in Table 4.3.5-1, and the measurement systems are outlined in Fig. 4.3.5-1.

Table.4.3.5-1 Testing items and method

ITEM	TESTING METHOD or EQUIPMENT					
Car speed	Spatial filter type speed detector					
Engine rpm.	Ignition puls detector for secondary high voltage code					
Negative pressure	Digital pressure meter(Intake manifold)					
Temperature of exhaust gas	Thermo couple					
Dynamic pressure of exhaust gas	Pitot tube					
Concentration of CO,CO2,HC	NDIR gas filter correlation method					

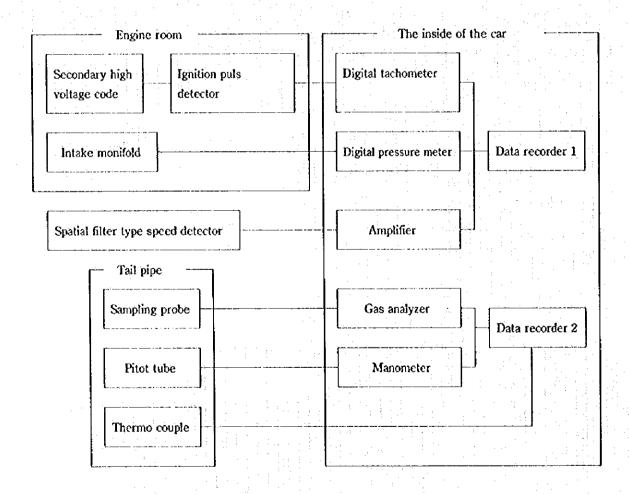


Fig. 4.3.5-1 Measurement system

The sampling interval was 0.5 seconds for the data recorder 1, and 10 seconds for the data recorder 2.

The survey was suspended if reasons other than normal congestion, such as road works and accidents, were delaying traffics on the selected roads. Also, abrupt overtaking was avoided and the vehicle was driven at the average speed dictated by the flow of traffic.

The test drives were implemented on normal working days and on holidays between September 29, 1996, and October 18, 1996. The surveys were conducted during the normal daytime including morning and evening peaks, but were not implemented at night.

A list of the field driving test results are provided in Table 4.3.5-2(1). Fig. 4.3.5-2 shows the emergence frequency of average vehicle speed ('average vehicle speed' will hereinafter be known as speed (2)), and Fig. 4.3.5-3 through Fig. 4.3.5-6 indicate the emergence frequency of idling, acceleration, deceleration and stable conditions.

The number of valid survey routes reached 70. Definitions of the terminology used hereinafter are as follows:

Speed (1) : Average vehicle speed excluding idling time.

Speed (2) : Average vehicle speed including idling time.

Idle : Ratio of the amount of time that the vehicle speed was 1.5km or less during running time.

Acceleration: Ratio of the amount of time that the acceleration speed was 1.5km/h/s or larger during running time.

Deceleration: Ratio of the amount of time that the deceleration speed was 1.5km/h/s or less during running time.

Stable : Ratio of the amount of time that the acceleration speed was -1.5km/h/s or larger,

1.5km/h/s or less during running time.

Table 4.3.5-2(1) Results of field driving tests

Run No.	Route	Date	Time	Running Time	Distance	Speed(1)	Speed(2)		Ratio	(%)	
				min.	km	km/h	km/h	Idle	Acceleration	Deceleration	Stable
2	Н	1996/9/26	15:21:00	12.38	5. 04	24.44	29. 51	16.69	22.88	22.41	38, 02
3	F	1996/9/29	15:54:00	30.80	8. 75	17. 05	21.71	20. 73	18.45	19. 29	41.53
4	Е	1996/9/29	16:49:00	26.03	6. 13	14.12	20.66	30.76	17. 16	17. 73	34.35
5	I	1996/9/29	17:32:00	19.69	7. 12	21.69	24. 82	12. 36	24.55	24.50	38.60
6	G	1996/9/30	15:55:00	31.83	9. 84	18.54	24.04	22. 07	20. 18	20.31	37.43
7	К	1996/9/30	16:50:00	15.11	3. 91	15. 54	18. 67	16, 55	20.96	20. 30	42, 20
8	И	1996/9/30	17:25:00	11.98	6. 38	31. 96	33. 28	3.98	21.00	20.21	54.87
9	N	1996/10/1	9:53:00	21. 47	8.61	24. 07	27, 50	12.07	18. 56	19.33	50,04
10	N1	1996/10/1	10:17:00	9.16	2. 83	18.56	23.65	21.02	18. 02	17.56	43,40
11	N2	1996/10/1	10:28:00	8. 79	2.77	18. 93	27.35	29. 76	18. 10	17.06	35.07
12	N1	1996/10/13	18:59:00	15. 73	2. 67	10. 20	15.31	31.73	13.82	15.36	39.09
13	N2	1996/10/13	19:17:00	9. 78	2. 83	17. 37	21.92	20. 12	18.76	21.48	39.64
14	1.	1996/10/13	14:13:00	16.69	7. 22	26.95	28. 53	8. 99	24.96	23. 17	<del> </del>
15	J	1996/10/13	14:35:00	26. 50	10.11	22. 90	27. 17	15. 38	16.89	17. 92	49. 81
16	Н	1996/10/13	15:10	9. 77	3.80	23. 32	28.77	18.52	24.32	21.67	35.49
17	F	1996/10/2	15:28:00	20. 14	6.83	20.34	23. 57	13.57	19. 40	18.08	48.94
18	E	1996/10/2	18:40:00	43.06	5.46	7. 61	15. 01	46. 12	14.34	15.68	23.86
19	I	1996/10/4	9:18:00	12.44	7. 11	34.31	35. 50	3.28	16.01	16.34	64.37
20	J	1996/10/4	9:33:00	18. 18	10. 49	<b>34.</b> 63	35. 15	1.47	16. 28		<del>}</del>
21	F	1996/10/4	10:06:00	12.50	6. 69	32.08	33. 59	4.31	<u> </u>	<b></b>	<del></del>
22	E	1996/10/4	10:30:00	20. 11	6. 13	18.30	23. 69	22.38	<del> </del>	<b></b>	{
23	N2	1996/10/4	10:53:00	5. \$5	2. 92	31.60	36.30	12.76	<del> </del>	<b> </b>	<del></del>
24	N1	1996/10/4	11:00:00	7.36	2.89	23.57	29. 97	<b></b>			<del> </del>
25	Y	1996/10/5	15:05:00	5.41	1.92	<del></del>	<del></del>				<del> </del> -
26	El	1996/10/5	15:43:00	13. 24	3.84	}	<del></del>	<b> </b>		<del> </del>	<del> </del> -
27	Z	1996/10/5	16:28:00	20.67	8. 11	23. 55	<del></del>	<del> </del>			<del> </del> -
28	N1	1996/10/5	16:28:00	11. 37	2. 78	14.68	23.92	37.76			<b></b>
25	N2	1996/10/5	<del> </del>			<del> </del>		17. 10			<b> </b>
32		1996/10/8	<b></b>	<del></del>	·	····	<del> </del>	<b></b>	<del> </del>	<del> </del>	<del> </del>
34	<del> </del>	1996/10/8	<del> </del>	<del> </del>				10. 45	<del></del>	<b>!</b>	<del></del>
38	+	1996/10/9		<b></b>					ļ	<del> </del>	<del> </del>
3(		1996/10/9	·	<u> </u>			<b> </b>	<del></del>			<b> </b>
37	<del> </del>	1996/10/9	<del> </del>	<del> </del>	<del></del>	<b></b>	<del></del>	26.80	<u> </u>		<del> </del>
38		1996/10/9	<del></del>	<u> </u>		<del> </del>	<del> </del>	13. 24	<u> </u>		·
39		1996/10/9	<del></del>	<del></del>	<del> </del>	<del> </del>	<del> </del>	27. 04	<del></del>	<del></del>	<del> </del>
4(	-	1996/10/9	-{	ļ	<del> </del>		<del> </del>	19. 84	<del> </del>	<del> </del>	<del> </del>
41	<del> </del>	1996/10/9	·	<del>{</del>		+	·	12.84	<del></del>	1	<del> </del> -
47	-	1996/10/10	·	<del></del>			·	19.43	<del> </del>	<del> </del>	<del> </del> -
4:		1996/10/10	<del> </del>	·	<del></del>			<b>+</b> -	· · · · · · · · · · · · · · · · · · ·	<del> </del>	<del> </del>
40	2	1996/10/11	10:38:00	24. 78	8.40	20.33	23. 43	12.98	21. 19	19.78	46.05

Table 4.3.5-2(2) Results of field driving tests

Run N	<u>.</u> ],	Route	Date	Time	Running Time	Distance	Speed(1)	Speed(2)		Ratio	(X)	
	-		<del> </del>		min.	km	km/h	km/h	Idle	Acceleration	Deceleration	Stable
}	47	G	1996/10/11	11:03:00	40. 42	<b>9.9</b> 8	14.82	21.15	29. 17	18. 76	18. 28	33. 79
<b></b>	48	ĸ	1996/10/11		11.51	3. 92	20.44	22.45	8.83	17.96	18. 03	55.18
}	49	Υ.	1996/10/11	12:56:00	11. 46	1.89	9.86	16.02	35.56	16. 87	19.71	27.85
}	50	1	1996/10/11	18:18:00	26. 01	6. 93	15.98	19.94	<b>19.0</b> 6	20.06	21.88	38. 99
	51	J	1996/10/11	18:50:00	34.56	10.23	17.76	20.69	13, 84	15.51	17. 22	<b>5</b> 3. <b>4</b> 4
	52	N2	1996/10/11	19:20:00	7.38	2.91	23. 65	<b>26.3</b> 9	10.27	19.30	19. 86	50.56
<u> </u>	<b>5</b> 3	G	1996/10/12		32.97	9, 83	17.90	22.40	19.84	19. 11	18.30	42.75
	54	X	1996/10/12	9:36:00	20, 43	4.56	13.39	19.05	28.71	14. 07	14.64	42.58
	55	Εl	1996/10/12	10:04:00	15. 61	3. 87	14.86	18, 49	19.27	15. 80	16. 60	48. 32
	56	Z	1996/10/12	10:27:00	20.72	8.34	24. 17	<b>26.3</b> 3	8.00	22.81	23.01	46. 18
-	57		1996/10/12	11:00:00	12.51	1.98	9.49	17.26	43.97	14.52	15.79	25. 72
<u> </u>	58	н	1996/10/14	8:50:00	13. 19	5.06	23.02	27.40	15.60	22.74	21.60	40.05
	59	Gi	1996/10/14	9:23:00	20.58	5. 17	15. 07	21.04	27.87	18. 63	19. 16	34. 35
	60	G2	1996/10/14	9:43:00	10.74	4. 60	25.70	28.58	9.78	25. 99	23. 35	40.88
	61	A	1996/10/14	10:08:00	12. 19	7. 18	<b>3</b> 5.35	48.90	27.41	9.02	10.05	53. 52
	62	В	1996/10/14	10:30:00	10.68	12.79	71.91	73. 23	1.80	10.93	12, 02	75. 25
	63	C.	1996/10/14	11:01:00	10.63	12.67	71.48	72.51	1.41	9, 72	12.30	76.57
	64	Jl	1996/10/17	16:56:00	6.54	2.74	25. 16	31.17	18.85	21,78	18.34	41.02
	<b>6</b> 5	El	1996/10/17	17:23:00	44.30	5.54	7.51	15.18	47.74	11.87	12, 45	27. 93
	66	N2	1996/10/17	18:08:00	6.14	2.82	27. 50	29. 85	7. 60	22.25	24. 83	45.32
	67	N1	1996/10/18	8:26:00	5, 59	2.90	31, 13	33.06	5.81	16.39	16, 54	61.25
	68	N2	1996/10/18	8:33:00	4. 62	2.88	37.37	38.28	2.34	22.70	18. 02	56.94
	69	X	1996/10/18	8:44:00	9. 13	5.04	33.12	36.51	9. 22	12.77	11, 68	66.33
	70	El	1996/10/18	8:58:00	8.08	3. 84	28. 52	28.80	0. 93	24.54	22,78	
;	71	Y	1996/10/18	9:28:00	13. 42	6.07	27. 14	29.72	8.51	20.31		
	72	EI	1996/10/18	9:45:00	14. 37	9. 90	41.35	<del></del>	11. 14	<del> </del>	<del></del>	
	73	S	1996/10/18	10:06:00	14. 38	9.78	40.83	Į	11.48	<del></del>	· · · · · · · · · · · · · · · · · · ·	<del>-}</del>
	75	G2	1996/10/18	10:28:00	10.75	4. 32	24.10		18.68			-{·
	76	F	1996/10/18	10:52:00	13.31	6.77	30.51		12.34	<del></del>		
	77	Z	1996/10/18	11:28:00	32.72	8. 15	14.95	23.65	35. 61	15. 79	15. 77	<del></del>
AY	3.				15.88	5.93	25.33	29.67	16. 51	18.38	18. 13	46. 99
MA	ζ,				44.30	17.91	74.01	75.97	47.74	25. 99	24.8	76.5
MI		<del></del> -			4. 62	1.89	7.51	15.01	0. 93	7.77	8. 90	23.80

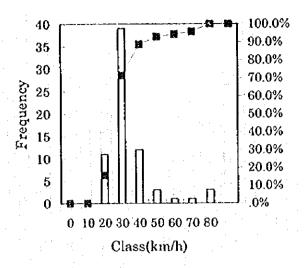


Fig. 4.3.5-2 Emergence frequency of car velocity

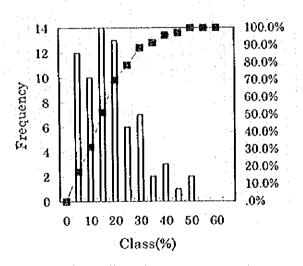


Fig. 4.3.5-3 Emergence frequency of idling

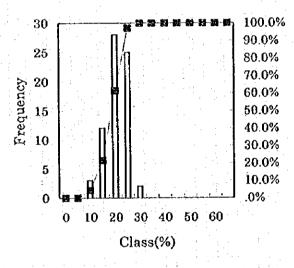


Fig.4.3.5-4 Emergency frequency of accelerating

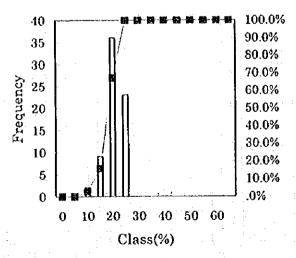


Fig.4.3.5-5 Emergence frequency of decelerating

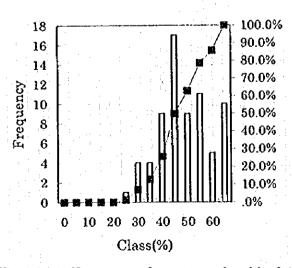


Fig.4.3.5-6 Emergence frequency of stable driving

All valid data including collected on highways show that the average vehicle speed during the daytime in the city of Tehran is 25.3km/h, the average idling ratio is 16.5%, the average acceleration ratio is 18.4%, the average deceleration ratio is 18.1% and the average stable speed is 47.0%. The figures excluding highways are 21.9km/h, 17.1%, 19.2%. 18.9% and 44.9% respectively. On trunk roads in Tehran during the peak rush hours, the idling ratio is large exceeding 40%. In the areas surrounding bazaars the ratio also exceeds 40% during the offpeak hours, which is a reflects commercial activities during the daytime and indicates congestion throughout the whole day. However, as the corresponding ratio of idling on the major trunk roads during the off-peak period is low, the final average idling ratio is also relatively low.

On the other hand, according to surveys in Tokyo, the average vehicle speed during daytime is 18.9km/h, and the idling ratio is 41.6% during peak hours and 31.2% during offpeak hours. If these figures are compared with the survey in Tehran, the traffic congestion within the city of Tehran is not so bad.

The concentration of exhaust gas, CO, CO<sub>2</sub>, HC, the amounts and temperature during driving were measured with a passenger car most commonly seen in Tehran (Paykan, 20-years old, 1600cc). Emission factors were calculated based on these measurement results, and relationship of vehicle speed, engine rotation and other factors were examined against each driving condition. Condition of maintenance for engine of the test car was in a state of deterioration.

The method of calculation of emission coefficients is as follows:

1) A pitot tube attached inside of vehicle's tail pipe measured total pressure and static pressure, and these measurements were recorded in a date logger. A thermos couple was also attached to the tail pipe and temperature was recorded in a data logger.

2) Mass of exhaust gas is obtained with the following equation:

$$\gamma = \gamma 0$$
. (Pa+Ps)
$$273 + \theta s$$
760

 $\gamma$  : Mass of moist exhaust gas unit (kg/m³), 1.3kg/m³ in case of air

- $\gamma_0$ : Mass of moist exhaust gas unit (kg/m³) calculated at temperature of zero degrees. Celsius and an atmospheric pressure of 760mmHg.
- Pa : Atmospheric pressure (mmHg), approximately 660mmHg in case of Tehran.
- Ps: Static pressure (mmHg) within tail pipe, 0mmHg in case of the survey.
- $\theta$  s. Temperature within tail pipe (degrees Celsius).
- 3) Equation to obtain flow speed of exhaust gas:

- V: Flow speed (m/s)
- C: Pitot tube coefficient (0.76)
- h. Dynamic pressure (total pressure static pressure)
- g: Gravitational acceleration speed (9.8m/s²)
- 4) Equation to obtain the flow rate of exhaust gas

$$Q=V \cdot 60 \cdot A$$

- Q: Flow rate (m³/min)
- V: Flow speed (m/s)
- A: Cross-sectional area of tail pipe (m²)
- 5) Conversion of flow rate of exhaust gas obtained with equation 4) into flow rate in a standard condition

QN=Q · 
$$\frac{273}{273+\theta}$$
 s  $\frac{(Pa+Ps)}{760}$ 

- QN: Flow rate of moist gas (m³/min)
- Q: Flow rate of exhaust gas (m³/min)
- Pa: Atmospheric pressure (mmHg), approximately 660mmHg in case of Tehran.
- Ps: Static pressure (mmHg) within tail pipe, OmmHg in case of this survey.
- $\theta$ s: Temperature within tail pipe (degrees Celsius).

QN': Flow rate of dry gas (m³/min)

QN: Flow rate of moist gas (m³/min)

Xw: Water content in exhaust gas (%)

The water content in exhaust gas measured before the start of the field-driving test was 7%.

6) By multiplying the flow rate of dry exhaust gas obtained in equation 5) with the measured values of each property, volume of exhaust for each unit of time (g/mi.) was calculated. For example, if concentration is 5%, Em (g/min) volume of exhaust for each unit of time is as follows:

 $Em = QN' \times 5 \times 10^{-2} / 22.4 \times 28$ 

22.4 is cubic content (liter) of the vapor 1 mol in a standard condition, and 28 is the molecular weight of CO. Emission factor, Ef (g/km) is calculated with the following equation if speed of vehicle during sampling is Sp (km/h).

 $Ef = Em \times 60/Sp$ 

B

The data obtained when driving along the route mentioned below on October 20th, 1996, are outlined in Fig.4.3.5-7 to Fig.4.3.5-9, which indicate the relationship between the emission factor of each pollutant calculated in accordance with the procedures 1) to 6) above and vehicle speed, engine rotation, and negative pressure of intake manifold.

AQCC --> DOKTOR ALI-YE-SHARI'ATI --> VOLVAR-E-MIR DAMAD --> VALI-YE-ASR OSTAD MOTAHHARI --> AQCC

Driving was carried out for 33 minutes and 40 seconds from 14:04:00 to 14:37:40. The emission factor, vehicle speed, engine rotation and load pressure were plotted at 10 second intervals. A driver and technical staff assigned to the measurements were in the car during the test drive. Because the measurement equipment weighed approximately 65kg, the total weight on board was as much as three adults.

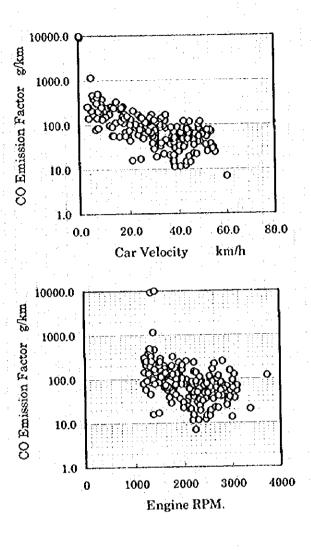
The average speed of the vehicle during driving was 28.0km/h, and the average exhaust coefficients for each pollutant was 210.9g/km for CO, 682.5g/km for CO<sub>2</sub> and 5.0g/km for HC. The relationship between the vehicle speed (V:km/h) and exhaust coefficients (EF:g/km) can be

obtained with the following equations:

CO: EF = 
$$1943.0 \cdot \text{V}^{-1.0}$$
 (R=0.85)

CO 2: EF = 
$$8761.6 \cdot V^{-0.1}$$
 (R=0.96)

$$HC: EF = 35.4 \cdot V^{-0.9}$$
 (R=0.72)



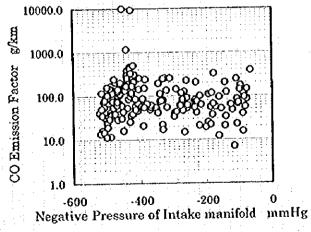
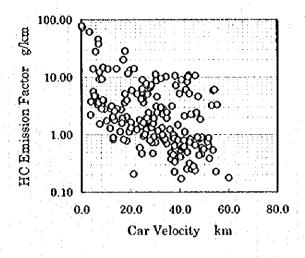
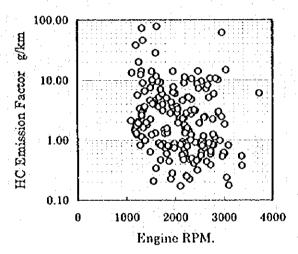


Fig.4.3.5-7 Relationship between CO emission factor and each parameter





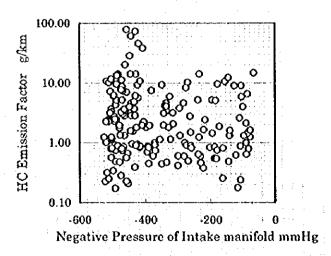
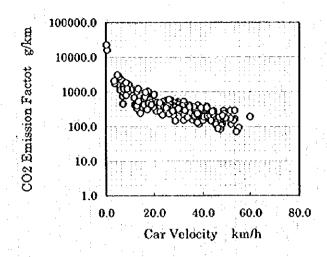
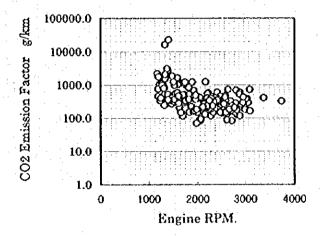


Fig. 4.3.5-8 Relationship between HC emission factor and each parameter





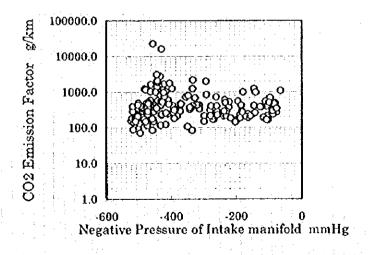


Fig. 4.3.5-9 Relationship between CO2 emission factor and each parameter

Prior to determination of the driving mode that is the representative driving pattern in the city of Tehran, major elements were analyzed such as variables for average vehicle speed, idling, acceleration, deceleration and ratio of stable driving obtained during the field driving test. The correlation matrix of each parameter is indicated in Table 4.3.5-3, and the position of eigen vectors is indicated in Fig. 4.3.5-10. The correlation matrix reveals that each of the average vehicle speed and ratio of stable speed is positively correlated with each of the ratio of acceleration and that of deceleration. On the other hand, each of the average vehicle speed and ratio of idling is negatively correlated with each of the ratio of idling and that of stable speed.

Table 4.3.4-3 Correlation matrix of each parameter

	Traveling Speed	Idling	Acceleration	Deceleration	Stable
Traveling Speed	1.00	-0.61	-0.30	-0.35	0.80
Idling	-0.61	1.00	-0.31	-0.26	-0.76
Acceleration	0.30	-0.31	1.00	0.94	-0.37
Deceleration	0.35	-0.26	0.94	1.00	-0.41
Stable	0.80	0.76	-0.37	0.41	1.00

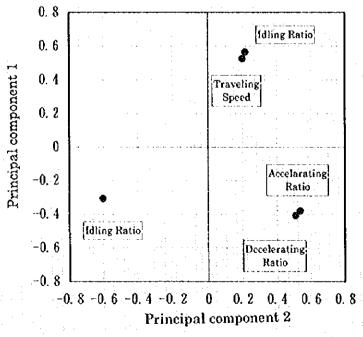


Fig. 4.3.5-10 Positioning of each parameter

It is found that each of the following driving conditions can be categorized into the standards from the positioning results of variables:

- Driving speedily and stably (highways)

,

- The average vehicle speed is comparatively low when acceleration and deceleration are repeated. (trunk roads during off-peak hours on a normal working day)
- The average vehicle speed is comparatively low and much idling is done. (during peak hours on a normal working day in the vicinity of bazaars)

The positioning was plotted in Fig.4.3.5.11 reflecting the result of each driving test, with principal component 1 on the horizontal axis and principal component 2 on the vertical axis. For comparison purposes, the main elements for standard ECE mode, 10 mode, 10/15 mode and 11 mode are also calculated and plotted.

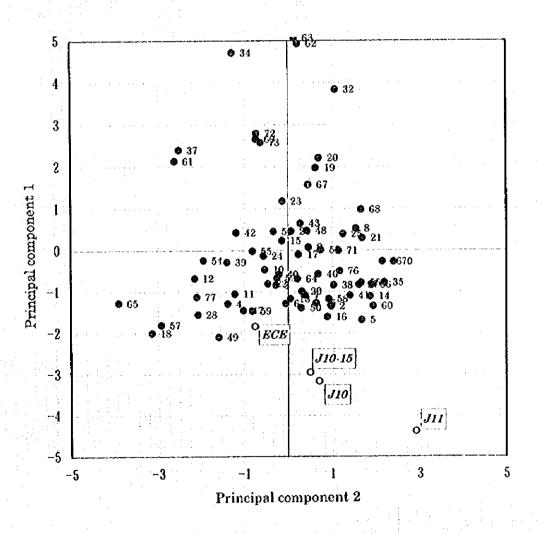


Fig4.3.5-11 Positioning of each test

Then, major elements obtained were analyzed in clusters as variables. The results are indicated in dendrogram on Fig.4.3.5-12. The driving results obtained from highways were excluded in the cluster analysis. The results of the driving survey based upon this dendrogram were categorized into four units, and the results obtained from the average survey results covering each cluster, were outlined in Table4.3.5-4. The driving results closest to these average values were chosen and determined as the Tehran mode. In addition, two examples were extracted from the results of driving on highways, and driving conditions for these six categories were determined as the representative driving mode in Tehran. These driving modes are indicated in Table4.3.5-5 and Fig.4.3.5-13.

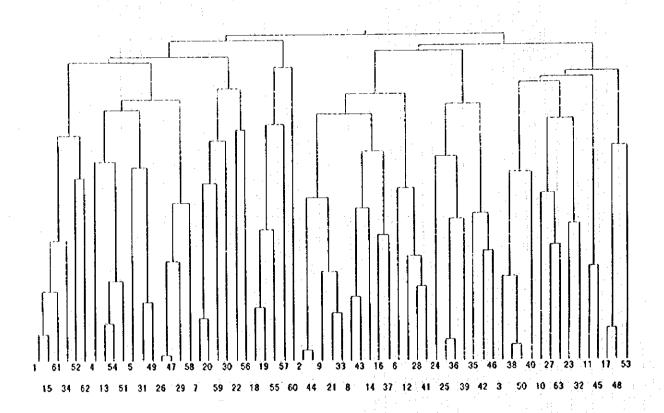


Fig.4.3.5-12 Dendrogram

Table 4.3.5-4 Average value of each parameter included in each cluster

Cluster	Running Time	Running Distance	Speed(1)	Speed(2)	Ratio(%)					
	min.	km	km/h	km/h	Idling	Accelerating	Decelerating	Stable		
Cluster 3	21.66	4.49	13.88	20.96	33.78	16.01	16.47	33.71		
Cluster 2	17.58	5.45	18.82	22.33	15.46	18,49	18.60	47.44		
Cluster 1	12.98	5.51	26.74	29.93	10.67	22.80	21.50	45.05		
Cluster 4	11.94	7.09	34.91	37.36	6.18	14.77	14.47	61.57		
Highway	11.53	10.80	56.28	62.74	11.70	10.77	11.55	65,99		

Table 4.3.5-5 Tehran mode

MODE	Run No.	Running Time	Running Distance	Speed(1)	Speed(2)		Ratio	(%)	
		min.	km	km/h	km/h	Idling	Accelerating	Decelerating	Stable
Tehran 1	28	11.37	2.78	14.68	23.92	37,76	17.01	16.28	28.96
Tehran 2	29	0.00	2.82	17.12	20.76	17.10	21.40	19.46	42.04
Tehran 3	41	11.17	5.06	27.19	31.29	12.84	24.40	22.01	40.75
Tehran 4	69	9.13	5.01	33.12	36.51	9.22	12.77	11.68	66.33
Highway(1)	<del>                                     </del>		6.23	40.32	55.26	26.80	10.16	8.90	54.14
Highway(2)		14.52	17.19	74.01	75.97	2.53	14.52	15.96	66.99

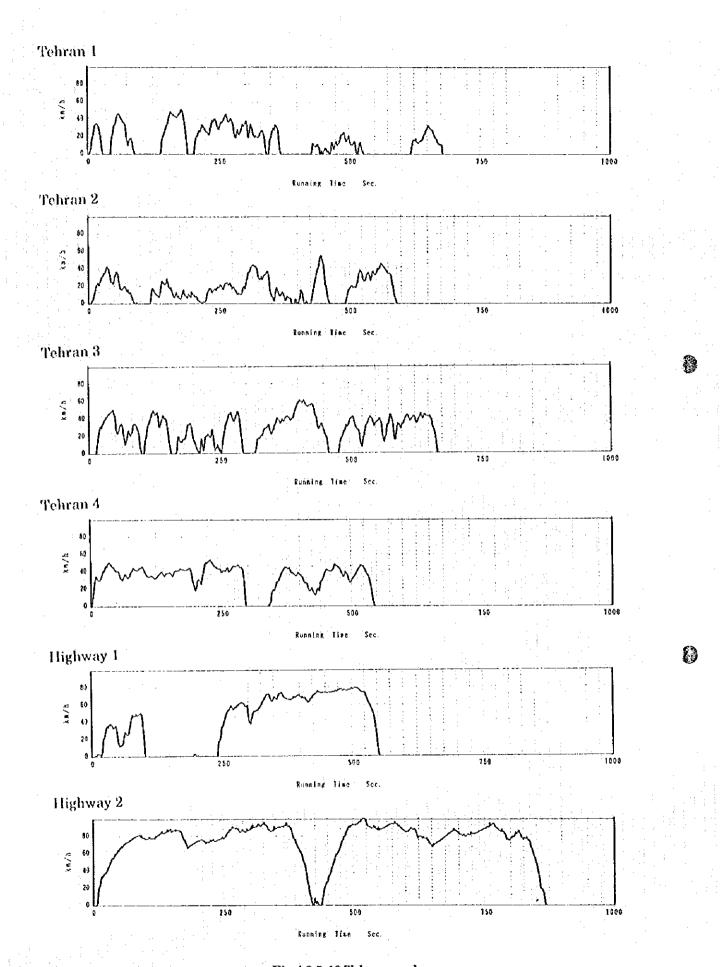


Fig.4.3.5-13 Tehran mode

### 4.3.6 Chassis dynamo test

8

8

Chassis dynamo tests are being continued in order to estimate an emission coefficient for CO, HC and NOx for selected vehicles. On the basis of the driving modes typical to Tehran determined in 4.3.5 and existing standard modes (ECE mode, EUDC, J10/15 mode, J11 mode), tests are being implemented on vehicle types outlined in Table 4.3.6-1 and the age of vehicles, taking into consideration the number of automobiles registered in Tehran, import conditions, structural conditions and other factors.

Results of chassis dynamo tests conducted according to the plan mentioned above are shown in Table 4.3.6-2.

Table 4.3.6-3 shows the results of chassis dynamo tests conducted by AQCC on the basis of the ECE mode in 1992. Test vehicles were selected in consideration of the number of automobiles registered in Tchran, so that vehicles with average levels of engine maintenance would be chosen.

Emission factors for CO and HC are 62.4g/km and 5.12g/km respectively when a simple average is taken from emission factors of these 48 vehicles.

Fig.4.3.6-1 indicates a reliance on speed for the average emission factors of Japanese vehicles before and after emission control of CO and HC imposed in 1973 and 1975. Subsequently because the vehicle emission control, the emission coefficients fell as shown in the Figure.

For comparison, related example of emission factors are plotted, namely, the above mentioned emission factors calculated from existing data, regulation values of emission factors in Japan, and the past experience of chassis dynamo tests implemented in Mexico City in view of its similarities to Tehran in topography and high-aged vehicle characteristics.

Table 4.3.6.4 shows the results obtained from the second chassis dynamo test using the ECE mode after replacing the air filters and carbureters of each test vehicle indicated in Table 4.3.-9 with new ones.

The mean emission factors are 31.96 g/km for CO, 2.66 g/km for IIC and 0.95 g/km for NOx, and the rate of emission is 51 %, 120 % and 101 % respectively compared with the results obtained from the first chassis dynamo test. While the emission of HC and NOx increased in the second test, the amount CO was reduced about 50 %, which indicates that

replacement of the two parts is an effective way of reducing CO emissions.

In comparison with these results of chassis dynamo tests shown in Fig.4.3.6-1, emission factors reflecting actual situation of Tehran are determined.

Table 4.3.6-1 Chassis dynamo test plan

CAR No	CAR TYPE	MANUFACTURED YEAR		TEST		Total Number	
			1	2	3	4	of Test
1	PAYKAN	1996	ECE	110-15	H1		3
2	PRIDE	1996	ECE	J10·15	н		6
3	PATROL	1996	ECE	J10-15	#11		9
4	REANULT 5	1996	ECE	J10·15	R1		12
5	PEUGEOT405	1996	ECE	J10-15	H.I.		15
6-1	PAYKAN	1971~1975	ECE	J10·15	111	ECE+EUDC	19
6-2	PAYKAN	1971~1975	TI	T4	HI	112	23
7	PAYKAN	1971~1975	TI	T2	T3	T4	27
8.	PAYKAN	1971~1975	T1.	T4	HI	H2	31
9	PAYKAN	1971~1975	110	J10·15	111		34
10	PAYKAN	1976~1980	ECE	J10·15	JH	ECE+EUDC	38
11	REANULT 5	1976~1980	ECE	J10·15	Т3		41
12	PAYKAN	1976~1980	Ti	T 2	13	T4	45
13	PAYKAN	1981~1985	ECE	110-15	311		48
14	PAYKAN	1981~1985	TI ·	Т3	Н1	112	52
15	REANULT 5	1981~1985	ECE	110-15			54
16	PAYKAN	1966~1970	110	J10·15	J11		57
17	PAYKAN	1986~1990	13	T4	112		60
18-1	PAYKAN	1976~1980	ECE	J10 • 15	311		63
18-2	PAYKAN	1976~1980	ECE	J10 · 15	J11		66
19	REANULT 5	1976~1980	T1	T4	112		69

NOTE (1) TI:TEHRANI . T2:TEHRAN2 , T3:TEHRAN3 , T4:TEHRAN4 , H1:HIGHWAYI , H2:HIGHWAY2 110:JAPANESEIONODE , 110-15:JAPANESEIO-ISNODE LA-4:US LA-4MODE

<sup>(2)</sup> Car No. 1~No. 5 : Brand New Car

<sup>(3) 18-1:</sup>Leaded Gasoline . 18-2:Unleaded Gasoline

Table 4.3.6-2(1) Results of chassis dynamo tests

Car No.	Model	REG. No.	Manufactured	Test	Average	HC	NOX	co	CO2
		1	year	Mode	speed(km/h)	g/km	g/km	g/km	g/km
1	PAYKAN	New PAKAN	Brand new	ECE	18.70	3.03	0.85	91.42	318.33
		:		J1015	22.70	4.37	0.45	127.98	197.97
			:	H1	40.32	2.29	0.64	80.29	172.83
2	PRIDE	New PRIDE	Brand new	ECE	18.70	1.84	i.71	27.40	188.87
			· · ·	J1015	22.70	1.38	1.03	28.74	135.14
* * 1				Н1	40.32	0.97	1.24	22.16	113.01
3	PATROL	New PATROL	Brand new	ECE	18.70	4.41	3.70	60.18	378.75
				J1015	22.70	2.97	2.65	56.27	268.24
				H1	40.32	1.73	3.89	41.30	249.14
4	REANULT5	New RENAULT5	Brand new	ECE.	18.70	2.05	1.54	23.07	207.69
				J1015	22.70	1.49	1.00	26.89	144.34
				H1	40.32	0.98	1.06	16.47	107.59
5	PEUGEOT	New PEUGEOT	Brand new	ECE	18.70	2.68	1.24	40.06	229.17
				J1015	22.70	1.90	1.02	40.74	180.56
				H1	40.32	1.40	1.31	31.00	148.03
6-1	PAYKAN	35833-THR-S	1973	ECE	18.70	5.21	0.41	158.61	271.17
	:	:		J1015	22.70	5.50	0.21	151.90	163.98
				J11	30.60	7.06	0.41	135.97	226.41
				ECEEUDC	1.11	3.03	0.93	100.26	223.91
6-2	PAYKAN	35833-THR-S	1973	T1	14.68	5.80	0.27	170.26	225.74
				T4	17.12	4.64	0.18	149.43	123.21
				H1	40.32	3.27	0.24	119.15	140.96
				H2	74.01	1.56	0.62	77.10	175.86
7	PAYKAN	21723	1975	Т1	14.68	12.20	0.30	150.83	155.49
		ļ		Т2	17.12	10.68	0.29	143.08	135.64
				Т3	27.19	6.00	0.24	104.74	115.54
				T4	33.12	4.47	0.19	88.87	100.67
8	PAYKAN	2187-THR-S	1972	T1	14.68	4.60	0.79	97.61	212.31
				T4	33.12	1.97	0.49	48.88	135.55
ŀ				H1	40.32	1.94	0.78	44.79	129.02
			<u> </u>	H2	74.01	1.28	1.44	38.69	173.54
9	PAYKAN	51727	1975	J10	17.70	3.86	0.50	1 1	181.64
				J1015	22.70	3.83	0.89	1	173.94
				J11	30.60	3.57	2.77		216.82
10	PAYKAN	63653-THR-25	1979	ECE	18.70	4.06	0.92		220.63
				J1015	<b>1</b> .	3.40	0.38		149.42
				J11	30.60	5.42	1.01		169.77
			<u> </u>	ECEEUDC	1	3.24	0.69	78.06	169.78

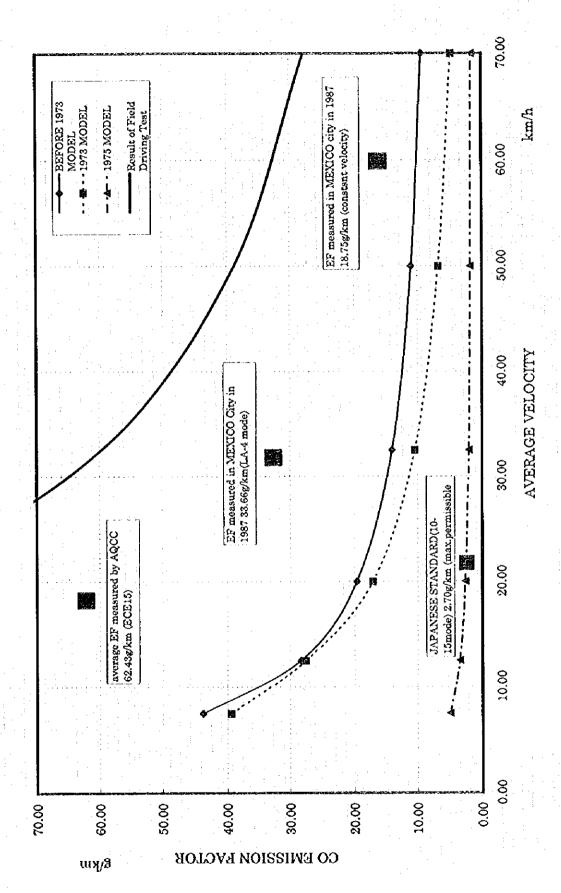
Table 4.3.6-2(2) Results of chassis dynamo tests

Car No.	Model	REG. No.	Manufactured	Test	Average	HC	NOX	CO	CO2
			year	Mode	speed(km/h	g/km	g/km	g/km	g/km
11	REANULT	79492	1988	ECE	18.70	2.72	1.28	33.35	206.94
		:		J1015	22.70	2.34	0.86	38.62	128.28
			1 1	Т3	27.19	2.42	0.86	32.82	118.41
12	PAYKAN	67446	1977	T1	14.68	3.17	1.16	81.51	212.27
<b>1</b>				Т2	17.12	3.09	0.57	85.74	175.17
				Т3	27.19	2.16	0.71	57.03	152.00
				T4	33.12	1.42	0.56	42.99	128.66
13	PAYKAN	67322-Mashad-11	1981	ECE	18.70	3.85	1.08	85.41	220.82
1		: .	•	J1015	22.70	3.49	0.56	88.26	147.13
				J11	30.60	4.86	2.18	54.23	197.86
14	PAYKAN	94356	1983	T1	14.68	12.62	0.46	162.51	165.01
				Т2	17.12	7.47	0.31	105.67	126.46
				H1 -	40.32	4.84	0.42	83.63	126.69
				H2	74.01	2.09	0.71	62.54	144.43
15	REANULT5	4259-THR-27	1982	ECE :	18.70	3.59	2.75	35.75	200.65
				J1015	22.70	2.97	1.08	42.94	127.48
16	PAYKAN	85642-Thr-B	1969	J10	17.70	4.26	0.85	86.65	194.66
			:	J1015	22.70	5.93	0.83	101.37	157.32
	REANULT			J11	30,60	4.36	2.21	54.64	189.47
17	PAYKAN	85638-Thr-29	1989	T1	14.68	15.64	0.53	179.61	183.28
		•		T4	33.12	5.22	0.29	90.26	116.12
			·	H2	74.01	2.39	1.64	42.65	168.16
18-1	PAYKAN	42523-THR-27	1980	ECE	18.70	3.06	1.12	39.30	282.71
				J1015	22.70	2.01	0.77	54.59	191.49
			(Unleaded)	J11	30.60	3.88	1.82	24.31	239.27
18-2	PAYKAN	42523 THR-27	1980	ECE	18.70	2.47	1.16	40.64	279.83
				J1015	22.70	2.02	0.64	55.59	176.10
			(Leaded)	J11	30.60	2.75	1.76	26.38	220.82
19	REANULT	31948-Abandon-1	1979	Т1	14.68	4.17	1.37	37.89	132.78
				T4	33.12	1.90	1.16	15.36	85.19
				112	74.01	1.08	1.77	17.01	98.04

Table 4.3.6-3 Results of chassis dynamo test conducted by AQCC(Befor tuning up)

No.	ТҮРЕ	REG No	AGE	cc	HC	co	NOX	CO2	HC+	Liter/	KM	Liter/
	-								NOX	100KM	Liter	100KM(MES
1	PAYKAN	12548	15	1725	14.64	125.80	0.58	131.49	15.22	16.37	6.11	19.1
2	PAYKAN	12877	11	1725	7.85	190.28	0.17	190.82	8.02	22.43	4.46	23.5
3	ТОҮОТА	14364	15	1600	4.54	65.19	0.32	158.60	4.86	12.00	8.33	12,4
4	PAYKAN	18789	9	1600	2 12	4.76	1.84	219.01	3.95	10.16	9.84	9.8
5	PAYKAN	21628	17	1725	3.88	83.15	0.49	178.22	4.36	13.99	7.15	12.7
6	PAYKAN	21878	6	1600	13.61	123.29	0.14	120.49	13.75	15.57	6.42	15.2
7	RENAULT	22119	1	1100	1.94	27.39	1.26	149.17	3.20	8.64	11.57	9.2
	PAYKAN	23646		1600	2.80	27.09	1.48	206.95	4.28	11.26	8.88	10.1
	PAYKAN	23673	ł .	1600	4.50	68.90	0.74		5.23	13.61	7.35	13.3
	PAYKAN	24178	}	1600	4.77	75.06	0.37	139.50	5.14	11.88	8.42	13.2
	PEUGECT	27573	!	1800	4.20	7.12		208.41	4.94	10.15	9.85	11.7
	RENAULT	28954	4.4	950	2.53	21.57	1.19	130.02	3.72	7.49	13.35	7.6
	CHEVROLET	29188	! .	2500	7.49	82.30	0.61	285.99	8.09	19.13	5.23	16.8
	CHEVROLET	29633		2500	3.33	37.99	1.17	217.65	4.51	12.55	7.97	12.7
	RENAULT	31418	1	1100	2.04	23.94	0.96	149.70	3.00	8.44	11.84	4.7
	NISSAN VANET			2000	4.28	81.90	2.03	384.38	6.31	22.95	4.36	17.
	NISSAN-VANET		11	2000	4.43	100.98	0.94	298.21	5.37	20.52	4.87	17.5
	RENAULT	33743		1100	2.92	19.02	1.28	163.73	4.20	8.84	11.31	8.
	BMW2002	33812	1	2000	1.92	14.30	1.42	185.01	3.35	9.31	10.74	9.2
	RENAULT	34971	10		3.43	28.87	0.89		4.31	7.28	13.74	9.5
	MAZDA VANET	39951		1600	8.18	102.97	0.03	1 4 24	9.09	16.88	5.92	17.8
	PAYKAN	44976	1	1725	3.60	63.84	0.72		4.33	13.40	7.46	12.7
	PAYKAN	46926	1	1725	6.76	95.21	0.12	1 1 1	7.41	15.40	6.45	15.8
	PAYKAN	46947		1725	2.05	18.76	1.02		3.08	14.91	6.71	14.9
		40347		2000	l i	55.90			5.86	13.58	7.36	14.5
	BMW2002		1		4.93	2.4			1. 1.			17
	CHEVROLET	49526		2800	10.91	109.94	0.3		11.21	16.85	5.93	
	TOYOTA	49887	,	1600	! (	28.78		l · I	4.32	8.93	11.20	
	PEUGECT	53462		1800	!!!	60.18			5.82	11.57	8.64	13.0
	NISSAN-VANET	<b>(</b>	i	2000		33.08	2.49		6.63	14.44	6.92	
	TOYOTA	55475	1	2000	3.24	73.40	0.82		4.06	15.96	6.27	14.9
	ТОУОТА	55575	L .	1587	6.59	100.98	0.27		6.86	15.04	6.65	13
	PAYKAN	56551		1725		95.39		184.69			6.09	
	PAYKAN	57735	1	1800	;	38.70	ļ	199.77	2.70		8.57	
	PAYKAN	59961	1	1725		42.62			4.47	<b>.</b>	7.39	1
	PAYKAN	63284	1	1800	L I	49.54	0.84		3.59		7.80	1. 1. 1.
	JEEP-SIMORGI		1	4229	1	23.39	1.18		5.31	19.76	5.06	
	JEEP SIMORGI		1	4229	1 :	30.58	3.32	7. 1	6.32	- 1	5.29	and the second second
	PAYKAN	72475	i	1725	ì . !	61.50	1	1	4.02			
	PEUGECT	73639		1800	<b>(</b>	25.10			3.51	1	8.98	
	MAZDA	75859	1	1600	<b>t</b>		}	<b>f</b>	7.16	1	9 9	1 to
	PAYKAN	81585	1	1725	i		1	235.72	3.62	1	8.35	
	RENAULT	82716	1	950			1 1 .	130.72	5.80	13.57	7.37	1
	PAYKAN	86369	1 .	1725	. 1	ı		186.19	7.82		5.99	
	PAYKAN	89337	1 .	1725		1		130.83	8.60	1	6.62	
45	PAYKAN	93861	9	1600	5.52	53.36	0.64	158.54	6.17	11.33	8.83	11.1
46	PAYKAN	91231	1 .	1600	1	40.71	1.54	179.24	5.01	11.08	9.03	13.0
47	RENAULT	94525	2	1100	15.50	114.47	0.44	162.97	15.98	17.09	5.85	15.4
48	RENAULT	91527	2	1100	1.66	11.50	0.99	158.75	2.65	7.93	12.60	8.0
	AVERAGE		11.9		5.12	62.42	0.9375	201.30	6.06	13.76	7.87	13.6

SOURCE: Air Quality Control Company



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Fig. 4.3.6-1 Reliance on speed for CO emission factors

Table 4.3.6-4 Results of chassis dynamo test conducted by AQCC(After tuning up)

No.	түре	REG.No.	AGE	СС	нс	co	NOX	CO2	HC+	Liter/	KMV	Liter/
110.		itiso.ito	non					002	NOX	100KM	Liter	100KM(MES.)
	PAYKAN	12548	15	1725	3.36	40.86	0.49	150.32	3.85	9.81	10.19	11.47
		12877		1725	3.84	110.01	0.43	164.61	3.92	15.24	6.56	19.75
	PAYKAN			1600	3.02	42.67	0.45	178.29	3.47	11.11	9.00	10.51
	TOYOTA	14364	13	1600	2.06	4.77	1.31	189.94	3.37	8.89	11.25	8.92
	PAYKAN	18789	-	1725	1.24	9.37	1.36	284.56	2.60	13.21	7,57	10.51
	PAYKAN	21628	. 1				0.79	178.39	5.04	12.10	8.26	11.47
	PAYKAN	21878		1600	4.25	54.66			3.22	7.51	13.31	8.92
	RENAULT	22119	100	1100		23.82	1.41	129.19		,		
1	PAYKAN	23646		1600	1.65	14.30	0.93	223.20	2.57	11.15		10.33
	PAYKAN	23673		1600	1.98	14.49	1.25	210.88	3.23	10.45	9.57	11.79
	PAYKAN	24178	6		2.59	35.65	0.69	178.32	3.28	10.57	9.46	1
	PEUGECT	27573	15	[ i	1.64	7.19	0.82	250.87	2.46	11.65	8.58	
	RENAULT	28954	14	1	2.17	11.91	1.03	178.76		8.90	11.23	7.33
	CHEVROLET	29188		2500	3.15	18.88	1.19	256.26	4.34	12.89	7.76	1
1	CHEVROLET	29633		25 <b>0</b> 0	2.79	29.70	1.46	247.30	4.25	13.20	7.58	
	RENAULT	31418		1100	1.98	23.98	0.61	130.33	2.59	7.60	13.17	1
1	NISSAN-VANET	ŀ	•	2000	2.91	42.85	0.67	217.67	3.57	12.82	7.80	1
	NISSAN-VANET			2000	2.49	78.04	0.82	286.15	3.30	18.16	5.51	1
	RENAULT	33743	i	1100	2.26	16.70	0.66	188.76	2.92	9.68	10.33	i .
19	BMW2002	33812	ł .	2000	1.98	7.13	1.32	198.18	3.30	9.40	10.54	the second second
20	RENAULT	34971	10		2.27	14.21	1.05	148.43	3.32	7.75	12.90	
21	MAZDA VANET	39951	7	1600	3.67	64.49	1.03		4.71	13.63		1
22	PAYKAN	44976	15	1725	1.03	4.68	0.68	359.33	1.72	16.12	6.20	I a second
23	PAYKAN	46926	15	1725	2.08	23.31	0.95	262.14	3.03	13.31	7.52	
24	PAYKAN	46947	15	1725	1.31	9.36	1.18	324.77	2.49	14.97	6.68	1
25	BMW2002	47864	17	2000	3.23	22.50	1.02	187.81	4.26	10.17	9.84	1 : -
26	CHEVROLET	49526	17	2800	4.16	63.49	0.49	209.19	4.59	14.04	7.12	1
27	ТОҮОТА	49887	15	1600	2.12	13.18	1.05	189.58	3.16	9.46	10,58	
28	PEUGECT	53462	15	1800	3.21	53.28	0.66	188.18	3.87	12.29	8.14	
29	NISSAN-VANET	53654	8	2000	2.83	•		267.19	4.57	13.35	7.49	1
30	TOYOTA	55475	9	2000	2.69	58.56	0.93	265.89	1	15.97	6.26	1
31	ТОҮОТА	55575	ļ	1587	•	69.95	0.33	160.63	3.78	12.27	8.15	
32	PAYKAN	56551	22	1725	1.81	9.41	1.48	287.47	3.29	13.42	7.45	12.11
33	PAYKAN	57735	1	1800	3.08	21,26	0.45	187.51	3.53	10.05	9.95	10.04
34	PAYKAN	59961	22	1725	2.78	32.95	0.93	246.58	3.71	13.39	7.47	11,47
35	PAYKAN	63284		1800		37.90	0.61	257.47	i i	14.08	7.10	11.95
36	JEEP-SIMORGI	63493	8	4229	3.53	20.80	1.54	531.23	5.06	25.06	3.99	17.2
37	JEEP-SIMORGE	63494	8	4229	2.05	16.26	2.04	421.80	4.10	19.78	5.06	15.93
38	B PAYKAN	72475	17	1725	2.41	27.98	0.99	332.95	3.40	16.76	5.97	12.74
39	PEUGECT	73639	15	1800	2.30	21.25	1.09	267.43	3.39	13.43	7.45	10.19
40	MAZDA	75859	-7	1600	4.35	70.81	0.59	261.82	4.91	16.86	5.93	14.97
42	PAYKAN	81585	22	1725	2.05	4.75	1.38	228.67	3.43	10.57	9.46	10.83
4:	RENAULT	82716	14	950	4.38	69.54	0.32	130.31	4.70	11.05	9.05	11.15
	PAYKAN	86369	22	1725	4.53	50.33	1.01	219.15	5.54	13.62	7.34	12.74
	PAYKAN	89337	1	1725	1	61.88	0.27	168.56	2.71	11.92	8.39	13.06
	PAYKAN	93861	1	1600	1	1	1 .	198.97			1 / /	
	PAYKAN	94234	1 .	1600		1		180.13	1	1	1	1
	RENAULT	94525	1	1100		1	1.	1	, .	ž .		1
1	RENAULT	94527	1	1100	1	1		184.69		1	ł .	1
	AVERAGE		11.9		6.10	<del></del>	<del> </del>	227.22	<del></del>	<del></del>	<del> </del>	+

SOURCE: Air Quality Control Company

## 4.4 Analysis of emission from mobile sources

# 4.4.1 Projection of characteristics of transportation and traffic in GTA

### (1)Traffic volume

The database mentioned in 4.3.1 includes traffic volume in 1994 and 2001 classified by the car type and link. In this report, the traffic volume given by the database is used to calculate an amount of emission of CO, SOx, and NOx.

### (2) Car velocity

The database mentioned above includes the average speed of each link estimated by TCTIS.

In this report, the traffic speed given by the database is used to calculate amount of emission of CO, SOx and NOx.

### (3) Emission factor

The emission of CO, SOx and NOx is specified according to each vehicle type as shown in Table 4.4.1-1, on the basis of the results of chassis dynamo tests, field driving tests and analysis of existing data.

#### CO emission factors

It is known that as amount of CO emissions from diesel automobiles is negligible compared with that of gasoline automobiles. Accordingly, it was assumed in this report that CO was not emitted from diesel automobiles but only from gasoline automobiles. We made regression analysis of the results of the chassis dynamo test conducted by the study team, and then specified the CO emission factor as a function of vehicle speed on the basis of the vehicle's age and by taking the existing data into account. For example, when a five year old passenger car is running 30.0 km/h, the emission factor (EF) is estimated at 26.4 g/km by applying 1242.0 for "a", -15.0 for "b" and 30.0 for "V" in the following equation:

$$EF = \mathbf{a} \cdot \mathbf{V}^{1} + \mathbf{b}$$

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The results are shown in Table 4.4.1-1. In the case where a passenger car is aged 15 years, "a" is 1242.0, "b" is 18.1, and EF is therefore 59.5 g/km.

As for motor cycles, since the age of all motor cycles is not known, it is assumed that all motor cycles are 10 years of age. Furthermore, an emission factor for high altitudes (23.6 g/km) specified by the U.S. Environmental Protection Agency (EPA) was used.

Table 4.4.1-1(2) Emission factor for each type of vehicle in Tehran

Car type	Pollutant	Car age	Component ratio	Equation : EF = a+b·v+cv <sup>2</sup> (g/km)
Motor cycle	со	Fix	- 1	23.6g/km
(Gasoline)	NOx	Fix		0.4g/km
	SOx	Fix		
Bus · truck (Gas oil) (Direct injection)	Pollutant	Car age	Component ratio	Equation : EF = a+b·v+cv* (g/ton km)
(Direct injection)	со		Bus Truck	a b c
1				8.723E-01 2.080E-02 2.130E-05
Bus • truck (Gas oil) (Direct injection)	Pollutant	Car age	Component ratio	Equation : EF = a+b·v+cv <sup>1</sup> (g/ton km)
(Direct injection)	NOx		Bus Truck	a b
		0 ~ 10	38 % 50 %	1,583E+00 -4.001E-02 4.108E-04
· · · · · · · · · · · · · · · · · · ·		$10 \sim 20$	31 % 26 %	1.107E+00 -3.190E-02 3.238E-04
		20~	31 % 24 %	1.030E+00 -3.001E-02 2.835E-04
Bus · Truck (Gas oil)	Pollutant	Car age	Component ratio	Equation : EF = a+b·v+cv² (litre/ton km)
(Direct injection)	SOx	•	Bus Truck	a b
		0~10	38 % 50 %	7.891E-02 -2.047E-03 1.924E-05
		10 ~	62 % 50 %	1.008E-01 -2.895E-03 2.703E-08
Bus · Truck (Gas oil) (Direct injection)	Pollutant	Car age	Component ratio	Equation : EF = a · V <sup>b</sup> (gton /km)
(Direct injection)	нс	•	Bus Truck	a b c
		Fix	•	1.441 -0.555 -
Taxi (LPG) (4-stroke)	Pollutant	Car age	Component ratio	Equation ; EF = a+b·v+cv <sup>2</sup> (g/km)
/4*SHOVC)	СО	•		a b c
		Fix		28.0 1.2

Tble4.4.1-1(1)Emission factor for each type of vehicle in Tehran

Car type	Pollutant	Car age	Component ratio	Equation:	$\mathbf{E}\mathbf{F} = \mathbf{a} \cdot \mathbf{v}^{1} + \mathbf{b}$	(g/km)
Passenger car	СО	-	_	а	b	c
(Gasoline) (4-stroke)		0 ~ 10	44 %	1242	-15.0	
		$10\sim 20$	36 %	1242	18.1	
		20 ~	20 %	1242	70.0	
Passenger car (Gasoline)	Pollutant	Car age	Component ratio	Equation :	EF = a+b·v+c	ev² (g/km)
(4-stroke)	NOx	_	-	a	ь	<b>c</b>
		0~10	44 %	2.300E+00	-1.410E-02	7.337E-04
		10 ~ 20	36 %	1.374E+00	-1.275E-02	3.499E-04
		20 ~	20 %	5.045E-01	-1.367E-02	3.211E-04
Passenger car (Gasoline)	Pollutant	Car age	Component ratio	Equation :	EF = a+b·v+	cv² (litre/km)
(4-stroke)	SOx	•	-	a	b	c
		0~10	44 %	1.759E-01	-4.264E-03	3.710E-05
		10~	56 %	2.564E-01	-7.639E-03	7.250E-05
Passenger car (Gasoline)	Pollutant	Car age	Component ratio	Equation :	EF = a · V	(g/km)
(4-stroke)	нс	•		a	ь	c
		0 ~ 10	44 %	12.950	-0.556	
		10 ~ 20	36 %	36.303	0.556	Y
		20 ~	20 %	70.300	-0.556	

SOx emission factors

The amount of SOx emissions does not depend on the state of fuel combustion, while that of

CO and NOx does. It can be obtained from the amount of fuel consumption and that of sulfur

content. The value of emission to be obtained from the amount of fuel consumption is given by

the following equation:

 $Q=W\times S_{D}\times S_{i}\times 10^{2}\times 64/32$ 

Q: The amount of SOx emissions (g)

W: The amount of fuel consumption (litter)

Sp: Specific gravity

Si: The amount of sulfur content (wt%)

Accordingly, the amount of fuel consumption by passenger cars, buses and trucks are shown

in Table 4.4.1-1 as a function of vehicle speed on the basis of a vehicle's age. The expression of

fuel consumption shown in the Table is in terms of consumption per ton of gross vehicle weight.

Consequently, in calculating the amount of fuel consumption, the results calculated according to

the expressions in the table must be multiplied by the gross vehicle weight of each type of vehicle.

In this report, we defined the gross vehicle weight as the average vehicle weight plus one-half of

the maximum load capacity. The gross vehicle weight of each type of vehicle is as follows:

Bus: 10 ton

Mini bus: 3.0 ton

Truck : 8.0 ton

Pick up : 1.2 ton

When a 20 year old truck is running at 30.0 km/h, the amount of fuel consumption is

calculated at 0.72 lit/km by applying 1.008E-01 for "a", 2.895E-03 for "b", 2.703E-05 for "c" and

30.0 for "V", and multiplying the obtained value, 0.12 lit /ton. km, with the gross vehicle weight,

6.0 ton.

El-a+b · V+c · V2

NOx emission factors

We specified NOx emissions from gasoline automobiles as shown in Table 4.4.1-2, using the

same procedure used to determine CO emissions: we made regression analysis, taking the

existing data into account. Since chassis dynamo tests cannot be carried out on diesel

automobiles in Tehran, it is impossible to specify NOx emissions comparing with the results obtained from the tests carried out on the spot. Accordingly, in calculating NOx emissions from buses and trucks, we used the equation introduced in the Japanese NOx manual.

As for motor cycles, on account of difficulty in knowing the ages of all motor cycles, as in the case of CO emissions, it is assumed that all motor cycles are 10 years of age, and the emission factors for high altitudes (0.4 g/km) specified by the U.S. Environmental Protection Agency (EPA) were used.

### 4.4.2 Analysis of emission amount from automobiles

The emission estimates of CO, SOx and NOx in GTA under the conditions specified in 4.4.1 are shown in Table 4.4.2-1.

Fig. 4.4.2-1 Amount of CO, SOx, NOx and HC emission from automobiles

***		The contract was not been a second of the contract of the cont			Polluta	nts	
Year	No	Car type	Unit	CO	HC	S0x	NOx
1994	1	Mobile source(total)	ton/year	826, 804	81, 691	8, 340	39, 610
	(1)	Motor Cycle	ton/year	64, 085	16, 293	179	1,086
:	(2)	Passenger Car	ton/year	478, 017	41, 296	1, 177	21, 865
t .	(3)	Taxi	ton/year	158, 572	13, 336	331	5, 381
:	(4)	Pick Up	ton/year	105, 660	9, 099	262	5, 030
:	(5)	Mini Bus	ton/year	4, 164	360	1, 325	1, 245
	(6)	Bus	ton/year	8, 492	756	2, 995	2, 784
	(7)	Truck	ton/year	7, 814	551	2, 071	2, 219

### 4.5 Analysis of emission from stationary source

#### 4.5.1 Measured results of target emission source

The results of measurement of exhaust gas emissions from stationary source described in section 3.4.2(4) are evaluated below.

#### (1) Brick manufacturing company (Sofal Jadid)

CO emission is very high although natural gas is used and an excess air ratio is very high, supposedly due to improper combustion of fuels in a furnace. It is believed that combustion can be improved by exchange of burner tips and that much energy can be saved by cutting an excess air ratio.

#### (2) Thermal power plant (Besat)

Measurement was conducted when natural gas was fueled. Further NOx can be reduced by cutting an excess air ratio since it is higher than in the case of usual operation of a thermal power plant.

#### (3) Tehran Refinery

Outlet temperatures of exhaust gas are higher than 430 C, meaning that energy conservation is possible through waste heat recovery with concurrent reduction of pollutants. As SOx emission is very high due to burning of high sulfur residues, countermeasures for total SOx reduction are to be considered.

**\$** 

### (4) Tehran Cement

The SPM concentrations have been high in No.4 and No.6 facilities during the time of first and second field surveys although electrostatic precipitators are installed. NOx emission is high in all factories while CO emission is abnormally high in the No.4 factory. SOx are practically not emitted because SOx can be absorbed in the process by chemical reaction with CaCO3 except flue gas from utilities units.

## (5) Combustion appliances for household use

Extremely high CO emission is observed in a hot water heater located on the closed ground floor supposedly due to imperfect combustion in the shortage of air supply. In general, CO emitted from the room heater is rather high compared with the projected emission factors, supposedly due to a lack of fresh air exchange in the closed room.

Table 4.5.1-1 shows the measured emission factors in comparison with the projected factors. Except some cases of CO, NOx and SOx mentioned above, the observed factors are almost the same with the projected ones within the allowable limit as shown in Fig 4.5.1-1.

Table 4.5.1-2 compares the measured concentration of SOx, NOx and SPM with the emission standards in Japan, the outcome of which are described below.

SOx: The K value of emissions from Tehran Refinery is larger than the expected value of 3.0, while the K values of the other emission sources are within the allowable limit.

(Note) Q=K \*10^-3\*He^2

where, Q: Allowable limit of emission value of SOx (Nm3/h)

K: Constant defined by areas

- 1) General emission standard (3.0-17.5)
- 2) Special emission standard(1.17-2.34)

He: Effective height of stack(m)

- NOx: NOx emissions of all the factories other than the brick and power plants are 40% higher on an average than the emission standard in Japan.
- SPM: In Tehran Cement, 5 out of 7 measurements are higher than the standard in Japan.

As a whole, a great deal of emission of pollutants can be reduced by means of strict combustion control and waste heat recovery procedures, since so many cases of imperfect combustion are observed for the room heaters as an example due to a design philosophy which have not fully taken thermal efficiency into account as well as improper operation and maintenance of these equipment.

Table 4.5.1-1: Comparison of emission factors between measurement & projected values

ttem	Ċ	Sofal Jadid	pipe	Besat				'n	ahran F	Tehran Refinery						Ţ	Tohran Cement	ment		
		(Brick)	S	(power plant)	Î	24-101	_	2H-151	15	2H-181		Boiler	36	No.4	4	No.5		No.6	No.7	
Chate		96 09 22	22	96.09.24		96.09.28		96.09.29	29	96 10 01	7.	96 10 02	2	96.10.05	30.	96.10.06	 9	96.10.08	96:10:09	8
Te Su	ľ	Natural Gas	ş	Natural Gas		Gas & Oil	₹	Gas & Oil	ō	Gas & Oil	- 8	Heavy Oil	ō	Natural Gas	Gas	Natural Gas	-	Natural Gas	Natural Gas	Sas
(Measured vs Projected)		Meas'd Proid		Meas d Proid		Meas'd Proj'd		Meas'd Proid		Meas'd Proid		Meas'd Proj'd		Meas'd Proj'd	Proje	Meas'd Proid	-Si	Meas'd Proj'd	Meas'd Pro'd	9
Outlet Temp	O	97				429	8	<u> </u>	180	446	88	426	180	148	 	188		128	115	
Excess Air Ratio		12.8		2.32	-	1.52	-	1.32		1.55		1.24		2.19		1.97		2.03	3.25	
Emission Factor					-		-			1							~**	:		
8	ğ	0.	K	0	<b>1</b>	12	16			69	16	0	9	E E	7	0	~	7	£	
šos	g/Gj	8.8		2.5		17.47	1637			285	1637		1637	3.6	-	0		0	0	-
χÖχ	O/C	839	ĸ	60 2	234	297	325	•	434	205	325	88	325	ş	£	760	t,	73	88	3
MGS.	Öζ	٥	ď	-	ـــــــــــــــــــــــــــــــــــــ	28	2			28	٤	5.3	2	122	ø	5.3	يي. ق	377	23	9

(2) Second field survey			•						}									İ		ŀ		l	
#em	Ş		:	ď	Room Heater	sater		:		8	Cooking Burner	umer	-	Boiler			Tehran Cemen	ment			Tehn	Tehran Refinery	ğ
	1	Ses Q	ō	Kerosene		Fire Place		Heater(NG)	<u>်</u>	S N		2	Wa	Water heater	ter No.4	7.	No.6	; ;	No.7	-	2H-101		Boiler
Date	Ŀ	97.02.18	18	97.02.18	-	97.02.19	<u>6</u>	97.02.19	_ "	97.02.22	7	97 02.22		97.02.20	L	97.02.25	97.02.26	92	97.03.06	×	97.03.01	6	97.03.02
Fuel	١.	Gas	Gas Qil	Kerosene		Natural Ga	5	Natural Gas		Natural Gas	500	A S	Na	Natural Gas	ss Natural Gas	s Gas	NG + HO		Natural Gas	335	FG + FO		Fuel Oil
(Measured vs Projected)	ł	Meas'd	D O	Meas'd Proid Meas'd Proid Meas'd Pro	<u>×</u>	eas'd Pr	<b>1</b> 2,60	'd Meas'd Proj'd		Meas'd Profd	_	Meas'd Proi'd		Meas'd Proi'd	'd Meas'd Proi'd		Meas'd Proid		Meas'd Pro'd		Meas'd Prold		Meas'd Profd
Outlet Temp	-	·	Γ	-	-	,	-	-			-		•		145		158		126	-	429 180	₹ 8	8
Excess Air Ratio	_		2												2.17		2.31		2.19	-	5.	1.14	Ţ
Emission Factor												-		_				-		~		_	_
8	Š	\$G: 308	15	385	15	234	8	32.2	8	0	83	0	8 1000	8	1800	1~	0	~	200	_	0 12	38	7
×OS	o/G	316	447	) W.	25	13.1		0		2:2	1	50	,			-	0	-	0	·-	4670 1404	2100	1404
ŎN	9/6	24.2	7	17.6	23	46.5	8	45	8	23.3	S	212	50 12.5		85	Б	Ş	2	ŝ	2 2	745 175	380	175
Mes	Ś	•	55		22		7.		7	•	7	•	7		212	9	Ą	9	7 98	9	ST 8 67	_	67
	l																						

Table 4.5.1-1. Comparison of emission factors between measurement & projected values

Vevine Survey														
llem	Š	Unit Sofat Jac	 ن	Betat			Tehrar	Tehran Refinery				Tehr	Tehran Coment	
		(Brick)	"	(power plant)		2H-101	L 2H-151	2H-181	8	Borter	No 4	No.5	No.5	No.7
Date		36095	£;	56 09 24		95 09 28	96 09 29	961001	£	96 10 02	36 10 05	96 10 06	96 10 08	96 10 09
ieo n		Natural G	5	Natural Gas		Gas & Oil	Gas & Oil	Gas & Oil		Неому О	Natural Gas	s Natural Gas	S Natural Gas	Natural Gas
(Measured vs Projected)		Mess'd Pro	Ď,	as di Pro	ž	asid Projid	Meas'd Pro'd	Meas'd Pro	o Meas	di Proj d	Meas C Pro	d Meas'd Proj	rold Meas giproid Meas of Proid	Weas'd Pro'd
Outlet Temp	O	76			Ľ	429 180	180	446 180	0 425	180	148	188	62.	115
Excess Air Ratio		12.8	2	2.32	-	1.52	1.32	1,55	1.24		219	1.97	2.03	3.25
Emission Factor										_				
3	j S	113	7	0		91 22	1	16	0	16	2570 7	0	2 2.1	33
Š	9/6	8.8	+	2.5	113	1747 1637	,	2150 1637		1637	9.4	0	0	0
ŏN	Ö/Ö	- 89	£	60 234		297 325		302 325	5 98	325	368 73	140 73	57.7.	536 73
WdS	g/G	0	· ·	9	ļ	28 70		28 70	53	70	327	53 6	372 6	23   6

(2) Second field survey	ļ							ļ					ŀ						l	
tem	Unit			Room	Room Heater				Cookin	Cooking Burner	~	Soiler			Tehran Cement	ent		.ehra	Jehran Refinery	,
		Gas Oil	} 	Kerosene	Fire Plac		Heater(NG)		NG	SQ1	(5	Water heater	ater	No.4	9.0N	No 7	<u>-</u>	2H-101	Δ)	Boiler
Oate	<u> </u>	97.02.18		97.02.18	97.02.1	9.	97.02.19		97.02.22	97 02 22	.22	97.02.20	20	97 02 25	97,02,26	97.03.05	ક	97.03.01	97.	97.03.02
flue)		Gas Oil		Kerosene	Natural Gas	Gas	Natural Gos	ļ	Natural Gas	LPG		Natural Gas		Natural Gas	NG + HO	Natural Gas	SeS	FG + FO	7	Fuel Oil
(Measured vs Projected)		Meas'd Proid Meas'd Proid Meas'd Proid Meas'd Proid	η We	s'd Proi'd	Meas'd P	N: p,lo,	leas'd Proi		Meas'd Proj'd		pioie	Meas'd Proj'd Meas'd Proj'd	voľd ľw	Meas'd'Pro'd	Meas'd Proj'd	d Meas'd F	P.O.	Weas'd Proid Meas'd Proid		Meas'd Proi'd
Outlet Temp	υ	_	ļ	-	   			· 				,		145	158	126		429 180	450 650	180
Excess Air Ratio		_												2.17	231	2 19		1.73	114	
Emission Factor		-	-					-									-			
8	ίς δ	106 15	585	<b>3</b> 5	87.	80	32.2 8	0	బ	0	ο <b>2</b>	10200	8	1850 7	0 7	36.3	P-	0 12	\$8.	12
ŠÓŠ	ίζ ά	316 447		39	:0	•	0	212	2 1	3.5	-	•		7,7	0	0	#*************************************	4670 1404	\$ 1.	402
Ň	ğ	242 71		17.6 62	597	 ও	45 50	233	3 50	81.8	20	12.5	S	625 73	73	188°	2	705 :75	8	175
SPM	Ş	55	, s	. 22	,	1.		<u>'</u>	7	,	7		7	2:2 6	284 6	36.4	(Q)	516 67		67
	Ì					ĺ							l							

Table 4.5.1-2 : Comparison table between measured emission concentration and emission standard in Jar

(1) First field survey	•																		ı
HAM	i i	Init Sofal Jadid		Result	100		Teh	Tehran Refinery	nerv					)-	<b>Tehran Cement</b>	ement			
		(Brick)	╆┈	(power plant)	2H-101	<b> </b>	2H-151		7. 181 181		Boiler	Z	No.4	No.5	5	No.6	"	No.7	
Oate	Ŀ	96.09.22	╁╴	96.09.24	96 09 28	<b></b> -	96.09.29		96,10.01		96.10.02	8	96.10.05	96.10.06	8	96.10.08	8	96,10.09	8
Puel	ŀ	Natural Gas	že Ze	Natural Gas	Gas & Oil		Gas & Oil	, ,	Gas & Oil		Heavy Oil	nteN	Natural Gas	Natural Gas Natural Gas	Çaş	Natural	SS	Natural Gas	Sas
(Measured vs stadard)	ļ	Meas'd Stan	VG Meas	distand	d Stand Meas distand	ew Pine	195 C Sta	n'd Me	as'd Star	rd Meas	d Stand	Meas	Stant	Wees'd	Pues.	Apas'd	p.ug	P.Seel	puris
SOX	×	K 0.27 3.00	2	8 8	3.00 3.22 3.00	8	9	8	3.0	8.3	38	0.11	3.00	3.00 4.10 3.00 4.80 3.00 0.11 3.00 0.03 3.00 0.02 3.00 0.02	3.00	0.02	8	8	8
ŏ	Wdd.	ppm 69 25	250   132	150	150 154 100 155 100 168 100 272 150 311 250	<u>.</u> 8	7.	8	-0		ន្ទ	ř.	32	8	S	350 418 250 516	82	9.5	Š
SPM	g/m3	0/m3 >0.005 0.1	ecome.	0.15	0.15 0.023 0.1	5.1	٥	1 0	324 0.	1 0.02	3 0,15	88	0	0.1   0.024   0.1   0.023   0.15   0.56   0.1   0.009   0.1   0.57   0.1   0.045   0.1	5	B	2	0.00	5

ttem	5			Tehran Cement	Sement				ehran	Tehran Refinery	
	:	No.4	4	No.6	9	No.7	7	2H-101	õ	Boiler	je.
Date	•	97.0	97.02.25	97.02.26	2,26	97.03.06	3.06	97.03.01	3.01	97.03.02	302
Fuel		Natura	Natural Gas	NG + HO	유	Natural Gas	Gas	FC+FO	ပ်	Puel O	ō
(Measured vs stadard)		Meas'd	Stan'd	Meas'd Stan'd Meas'd Stan'd	Stan'd	Meas'd	Stan'd	Meas'd Stan'd Meas'd Stan'd	Stan'd	Meas'd Stan'd	Stan'd
ŏ	¥	0.0	3.30	0.02	3,00	0.01	3.00	300	38	9	8
ŏ	wda	SSS   wdd	250	200	250	742	250	15.	5	ţ	Š
MdS	o/m3	O/m3 034 01	0.1	9	0.1	21.0	.0	ors 0.1 0.036	9		0.15

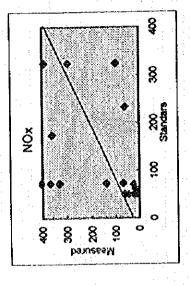
Table 4.5.1-2. Comparison table between measured emission concentration and emission standard in Jaban (1) First field survey

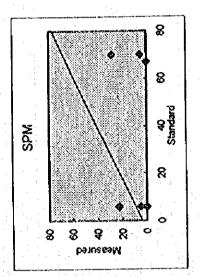
( ; ) FIRST HAID SOLVEY													ŀ							
mot	1,00	Intel Sofal lac		S. S. S. S.				ē	Tehran Ratinery	ofinery						Tehran	Tehran Cement			
2			<b>†</b>	(newer plant)	lant)	2H-101	5	2H-151		2H-181		Borler	ļ	No.4	۲.	No.5	No.6	S.	No.7	7
Core		26 09 5	1	96 09 24	22	96 09 28	88	96 09 29	9	10.01.96		96.10.02		96 10.05		96.10.06	96 10 08	80	96.10.09	8
Fuel	,	Natural G		Natural	Ş	Natural Gas Gas & Oit	ō	Gas & Oil		Gas & Oil		Heavy Oil	-	Natural Gas Natural Gas Natural Gas Natural Gas	s Natu	ral Gas	Natura	Gas	Natura	Gas
(Moseus or beautiful)		Mose of Sta	2 2	1025 C	D Let	Meas'd'S	p,ug	Stand Mass of Stand Mess of Stand Mess of Stand	an'd l	4035'C.S.	Mi Suc	easid Sta	Š og	eas'd Stan	SeeW. P.	d Stan'd	Measid	Stan'd	Meas'd	Stanta
XOX	¥	0.27	8 8		8	3.00 3.22 3.00	88	-	8	610	8	9	8	3.00 4.10 3.00 4.81 3.00 0.11 3.00 0.03 3.00 0.02 3.00 0.02 3.00	0 0.03	38	0.02	8	0 02	38
χον	600	g.	82	132	35	33.	8	132 150 154 100 155 100 168 100 212 150 311 250 199 350 418 250 516	8	168	<u>\$</u>	772	2	311 25	7 199	350	4:38	250	518	250
MdS	E/a	×0.005	0.1	-	0.15	0.15 0.023 0.1	0		-	0.024	0.1 0	023 0.	15	0.1 0.024 0.1 0.023 0.15 0.55 0: 0.009 0: 0.657 0.1 0.045 0.1	000	0	190	5	0.045	0.0
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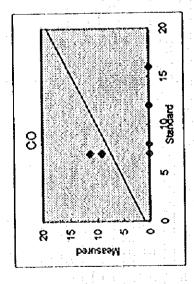
Fea	Š		-	enran Cement	Сетел			,	ohran	Tehran Refinery	
		No 4	4	N.	No.6	Ñ	No.7	2H-101	101	Boiler	ā
Date		97.02.25	2.25	97.0	97.02.26	97.0	97.03.06	97,03.01	3.01	97.03.02	8
ieo ii	·	Natural Gas	l Gas	NG	NG + HO	Natur	Natural Gas	FG + FO	ပ္ပ	Fuel O	ã
(Measured vs stadard)		Meas'd	p.ueiS	Meas'd	Stanid	Meas'd	Stan'd	Meas'd	Stan'd	Meas'd Stan'd Meas'd Stan'd Meas'd Stan'd Meas'd Stan'd Meas'd Stan'd	) ues
SOX	¥	0.0	3.80	0 02	3.00	X 0:0 3:00 0:02 3:00 0:01	ა 8	320	8	300 552	8
Ŝ	ωda	STE   mdd	250	302	250	272 250	250	144	Ş.	5	35
Mes	a/m3	0/m3 0.34 0.1	0.1	C; O	0	0.43 0.1 0.15 0.1 0.036	0.1	0.036	0		0 15

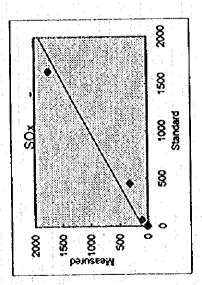
4-251

Fig. 4.5.1-1; Comparison of emission factors between measurement and projected values









## 4.5.2 Estimation of emission quantities in GTA

### (1) Summary of emission quantities

#### 1) Total GTA

As shown in Table 4.5.2-1, contributions of stationary emission sources and mobile emission sources to total emission of air pollution in GTA are projected in the case of 1994 at 29% and 71% respectively, demonstrating the dominance of mobile sources.

Concerning the contribution of each pollutant, stationary sources share 97% and 71% in SOx and NOx while mobile sources share 94%, 70% and 88% in CO, HC and SPM respectively.

The year of 1994 is selected for estimation of emission quantities, since publicized statistic data for energy consumption in Iran are available in the most abundance in this year among the several latest years.

Table 4.5.2-1: Emission quantity of air pollutants in GTA (1994)

(ton/year,%)

Source	SOx	NOx	CO	HC	SPM	(Total)
Stationary	253,981	95,571	51,421	34,701	25,113	460,786
Mobile	8,340	39,610	826,806	81,690	182,717	1,139,163
(Sub-total)	262,321	135,181	878,227	116,391	207,830	1,599,949
Stationary	96.8	70.7	5.9	29.8	12.1	<b>28</b> .8
Mobile	3.2	29.3	94.1	70.2	87.9	71.2
(Sub-total)	100.0	100.0	100.0	100.0	100.0	100.0

The emissions from stationary sources in total Iran are projected in the same procedure with the case of CTA, which is shown in Table 4.5.2-2 for reference.

Table 4.5.2-2: Stationary emission quantity of air pollutants in total Iran (1994)

(ton/year)

Source	SOx	NOx	CO	HC	SPM	(Total)
Stationary	1,186,885	470,315	140,181	168,212	95,486	2,061,079

(Note) Emissions from flaring associated gas are not included in this projection

#### 2) Sector-wise emission

As shown in Table 4.5.2-3 and Fig. 4.5.2-1, the following features are revealed.

- (a) SOx emissions from the manufacturing sector shares 64% of the total, followed by energy conversion of 19%, general service & household of 14% and the transport sector of 3%. In the manufacturing sector, nonmetal products have the biggest share of 32%, and Tehran Refinery alone 13%, while the transport sector shares only 3% in contrast to other kinds of emissions, since this sector uses low sulfur gasoline and diesel oil. The thermal power plants in GTA share only 6% since most of the fuels have already been substituted by natural gas except in winter when supply of natural gas is sometimes short.
- (b) NOx emission has tendency similar to SOx although the share of the transport sector reaches 29% of total emission. Nonmetal products and Tehran Refinery have 11% and 9.0% shares respectively, followed by power plants of 8.7%. The general service and household sector has 11% share, though this sector has numerous consuming units.
- (c) Most HC emission comes from the transport sector accounting for 70%, Tehran Refinery 14% and commercial & general 12%; the combined share of these 3 sectors totals 96%. HC emission sources of the commercial sector are represented by petrol stations, printing shops, dry cleaning shops and petroleum depots and not by shops of electric metal plating and painting, since information of these sources is not available despite their possible substantial volume. It is estimated that leakage of natural gas from rubber hose connections is substantial due to a lack of proper maintenance, especially in the commercial/household sector although their volume is not estimated at this stage.

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- (d) CO and SPM emissions are negligible in the case of stationary emission sources, since the transport sector has a dominant share of 94% and 88% respectively.
- (e) Respecting the emission of stationary sources on the whole, nonmetal products, refinery, and iron & steel are ranked high as illustrated in Fig. 4.5.2-2, but as far as the average emission per company is concerned, iron & steel is the first, which implies that pollution control can be most effectively put into practice in this sector as shown in Fig. 4.5.2-3.

(10tal) 16,721 2,439 7,427 30,161 100.01 1,599,949 22,047 24,106 74,301 34,750 87.9[1:136,163 39,551 (ton/year) 4 0 0 0 8 6 4.0 7 SPN 2.294 2.838 1,188 702 18277 100.0 207,830 1,535 1.648 888 13.2 6.0 12.2 ሂ 16,401 95.13 21.690 15.679 15.347 14,256 34,701 116,391 Emission volume Table 4.5.2-3: Sectorwise emission quantity of air pollutants in GTA (combustion+evaporation) 100.001 5.9 રાષ્ટ્ર 0.5 ၀ 29.3 826,836 7,262 6,688 7,145 10,984 4,549 2,863 953 445 98 3,577 51,421 100.0 878,227 2,387 9.0 8.7 70.7 Š 23,900 11,736 12,487 2,563 29,610 6,148 15,430 3,223 5,367 12,164 100.01 135,181 \$6.541 3.0 8 (Stationary source) ပ္တိ 50,289 16,069 8 340 35,720 21,242 979 3,627 12,379 83,425 19,252 6,348 12,553 34,220 15,029 167,923 20,691 253,981 2 General Service and Household 33 Wood Products
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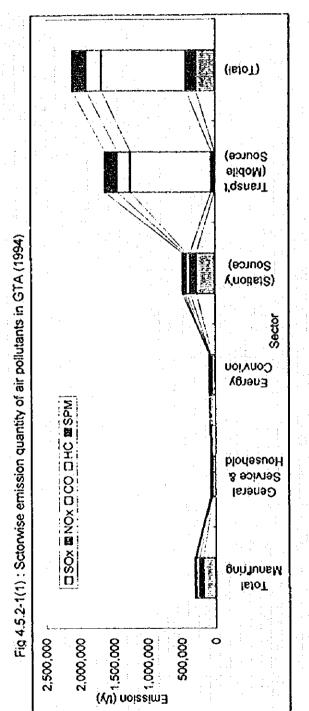
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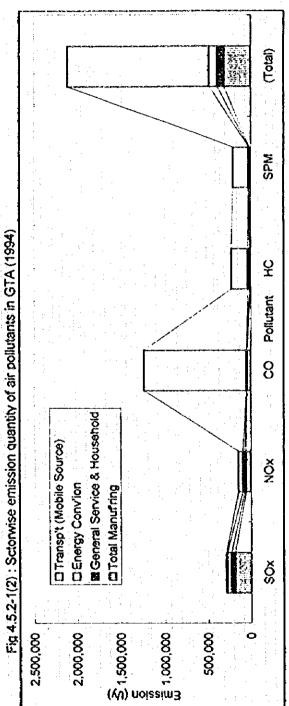
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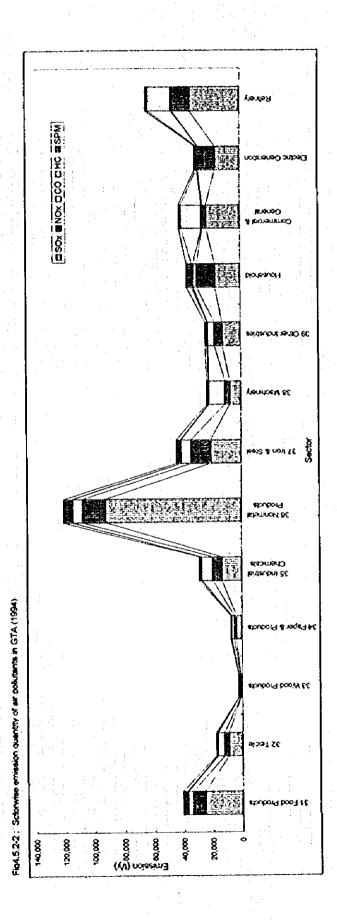
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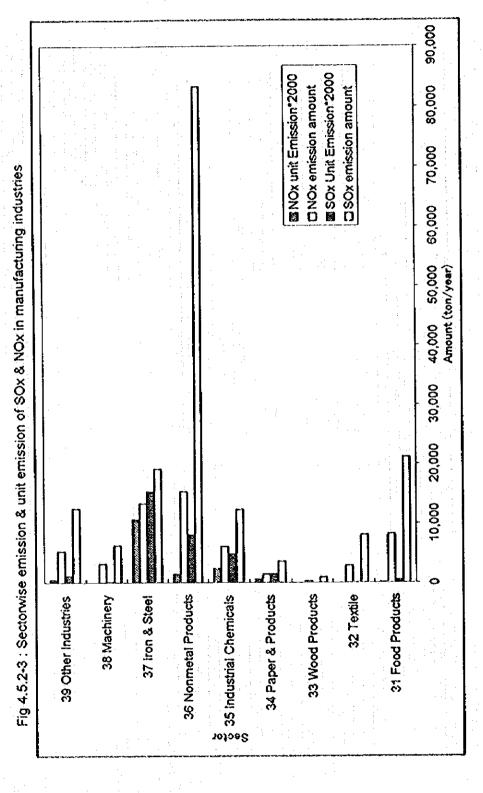
262,321

(Total)









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## 3) District-wise emission

In order to project dispersion of pollutants in GTA by means of the simulation model developed by the project team, district-wise emission quantities of air pollutants in GTA are projected as shown in Table 4.5.2-4 and Fig. 4.5.2-4, showing that the districts 20, 18, 16, 4, 9, 5 and 19 have higher ranks, among which district 20 spearheads since there are Tehran Refinery and Ray thermal power plant in this district. As shown in Table 4.5.2-5, Tehran Refinery and thermal power plants (Besat, Firouz, Ray) in the energy conversion sector have big shares of emission: 19% and 18% for SOx and NOx, 12% for HC only by Tehran Refinery when compared to the total emission amount of each pollutant in GTA.

Table 4.5.2-5: Emission quantities of pollutants by companies of energy conversion sector in GTA (1994)(combustion+evaporation)

					Emi	ssion quar	ntity		
	Sector	Capacity	District	SOx	NOx	co	HC	TSP	(Total)
				(Uy)	(t/y)	(t/y)	(Uy)	(Ưy)	(Vy)
1	Tehran refinery	220,000b/d	20DB	34,243	12,058	497	14,184	1,649	62,631
2	Thermal power plants	1,709Mw		16,106	11,748	451	723	1,191	30,219
2	- Besat	391Mw	16	14,172	5,022	207	288	684	20,372
2	- Firouz	75Mw	2	6	713	21	49	19	808
2	- Ray	1,243Mw	20DB	1,928	6,013	223	386	488	9,038
	(Total)		7. 11. 11. 11. 11. 11. 11. 11. 11. 11. 1	50,349	23,806	948	14,907	2,840	92,850
	GTA			262,321	135,181	878,227	116,391	207,830	1,599,950
	Ratio to GTA (%)			19.2	17.6	0.1	12.8	1.4	5.8

## (2) Major procedures for projection of energy consumption

Fundamental procedures for projecting emission quantities of pollutants are shown in Fig. 4.5.2-5. Detailed projection procedures for the following items are described in APPENDIX 4.5.2 of this report.

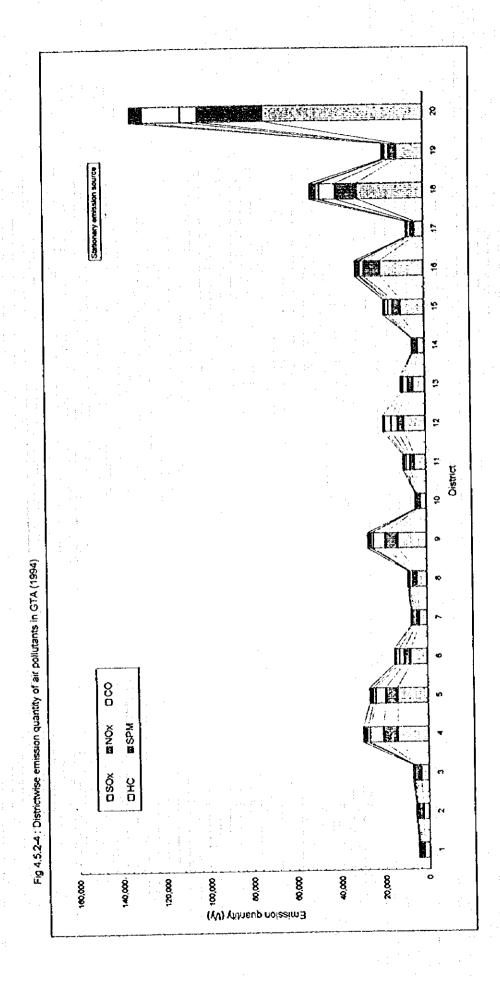
- **OFuel consumption in GTA**
- **②Emission factors of fuels**
- ③Emission quantity of pollutants in GTA

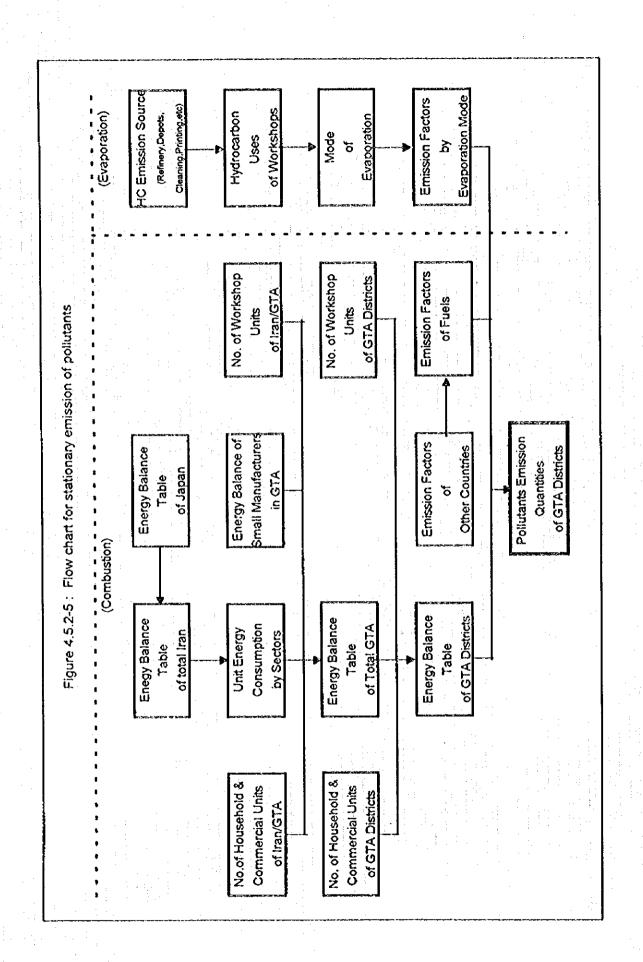
Table 4.52.-4(1): Districtwise stationary emission quantity of poliutants in GTA (1994)

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Fig.   Control	8		472.0	534.2	-	6,062.7	4,584,0	2,280,9	0.000,1	1,232,6		8	١.	2			· j		1,150.3	8	1,900,2	2,005,0	
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Table 4,5.2-4(2): Total stationary & nobile emission in GTA (1994)

١	(A mains) and an in			(IOMANAGE)				
Ц	Emission Pollytant	xos	NOX	8	) HC	Meds	(Total)	8
	Stationary	8 086 ESZ	95,571.0	51,421.2	34,700,5	25,112.9	460,786.4	28.8
2	Mobile	8,340 0	39,610 0	0.906,928		182,717.0	-	71.2
Ш	(Total)	262,320.8	135,161 0	878,227,2	116,390.5	207,829.9	1,599,949.4	1000





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In order to supplement the above projection, questionnaires for data collection shown in APPENDIX 4.5.2 were delivered to 550 workshops belonging to the following 4 categories with respect to the number of employee, of which 190 responses were returned. About 40 critical units among them were interviewed by AQCC engineers for further verification.

1≦Small≦10

51≦Medium large≦100

11≦Medium≦50

101≦Large

The full compilation of responses and summary sheets for the companies having more than 100 employee are tabulated in APPENDIX 4.5.2. The data in these tables are incorporated in the projection of district wise energy consumption.

Brief description of the categories for projecting pollutants are shown below.

39	Sector	Category	Emission Type
1	Manufacturing Industry	Food, Textile, Wood, Paper, Chemicals, Nonmetal, Iron/Steel, Machinery, Other	Point (>100) & Area (≦100)
2	Commercial/Household	Restaurant, Hotel, Office, House, etc.	Area
3	Energy Conversion	Refinery, Power Plant	Point

## 1) Projection of the energy balance of total Iran (1994)

In order to estimate sector-wise energy demand of GTA, the sector-wise energy balance of total Iran in 1994 was firstly projected in the form of Table 4.5.2-6 for determination of an umbrella and/or ceiling of sector-wise energy consumption of GTA. The data in the dark cells in Table 4.5.2-6 are either collected or calculated mostly based on the energy balance tables of total Iran (1994) prepared by MOE. The energy table format follows the portfolio of IEA/OECD, which is the prevalent pattern in the world.

## 2) Projection of the energy demand in GTA (1994)

Based on the energy balance of total Iran, energy demand in GTA was projected as shown in Table 4.5.2-7 by means of proportional allocation of energy by the number of workshops or commercial/household units between GTA and total Iran in the case where individual figures could not be collected. The data in the dark cells in Table 4.5.2-7 are also

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collected mostly from the energy balance tables of MOE. Fig. 4.5.2-6 shows the energy balance of total Iran vs. GTA, which visually indicates the energy position of GTA in Iran in terms of primary energy production, energy conversion capacity and final energy consumption.

3) Projection of the energy demand in GTA districts (1994)

Energy demand in each GTA district in Table 4.5.2-9 is projected by proportional allocation of energy demand in GTA by the number of workshops or commercial/ household units in each district in Table 4.5.2-8.

### (3) Emission factors of fuels

The emission factors by fuel combustion in Table 4.5.2-10 are evaluated on the basis of a variety of data sources in the world, some of which are verified through the field measurement, while the emission factors for HC evaporation are mostly collected in reflection of the factors of Japan shown in Table 4.5.2-11. SOx emission factors are calculated based on the sulfur content of fuels shown in Table 4.5.2-12.

# (4) Emission quantities of pollutants in GTA

Consequently, emission quantities of pollutants are calculated as a result of multiplying energy consumption with corresponding emission factors except HC evaporation which is estimated as a result of case-by-case studies. Table 4.5.2-13 illustrates sector-wise SOx emission quantities in GTA, while Table 4.5.2-14 illustrates district-wise SOx emission quantities in GTA, for which data sheets are provided for all pollutants as shown in APPENDIX 4.5.2. The emission quantities from the energy conversion sector in GTA are separately evaluated as shown in Table 4.5.2-15, since the scale of facilities in this sector is very large. Evaporation amounts of HC in GTA are also estimated apart from emission through combustion as shown in Table 4.5.2-16.

(Note): Heat values used in the projection are shown in Table 4.5.2-17.

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Table 4.5.2.-10: Emission factors by combustion

				* .				
e cua	Sector	Fuel	Unit	SOx	NOx [	CO	HC	SPM
e territo	1 Industry	Gasoline	g/Gj	37	165	7,744	298	41
		Kerosene	g/Gj	86	165	15	9	64
		Gas Oil	g/Gj	336	164	13	9	65
	+ 1 1 7	Heavy Oil	g/Gj	1,268	175	12	9	67
		LPG	g/Gj	61	52	7	2	8
•		Natural Gas	g/Gj	1	73	7	1	6
		Solid Fuel	g/Gj	590	250	170	0	74
•			, and the state of				1.	
			***************************************		, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			
256.00	2 Household &	Kerosene	g/Gj	86	62	15	11	22
	Commercial	Gas Oil	g/Gj	336	71	15	4	55
. :		Heavy Oil	g/Gj	1,268	70	15	4	71
		LPG	g/Gj	61	36	9	3	8
		Natural Gas	g/Gj	1	50	8	3	7
		Solid Fuel	g/Gj	590	215	800	1	74
	į							
22 (52)	3 Transport	Gasoline	g/Gj	37	301	8,845	800	575
		Jet Fuel	g/Gj	129	224	120	63	23
	:	Gas Oil	g/Gj	345	831	765	559	9,190
		LPG	g/Gj	61	132	15	3	112
ļ				CONTRACTOR OF CHESTORS	e and a Chandler for construction	1014 14 704 3474899214409911	,-, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,,	
937-50C	4 Power Plant	Gas Oil	g/Gj	336	284	15	15	66
	& Refinery	Heavy Oil	g/Gj	1,637	325	16	16	70
,		Natural Gas	g/Gj	1	234	7	16	6

(Note) Solid Fuel: Coal, Cokes, Oil Cokes

Table 4.5.2-11: Data base for hydrocarbon emission

The following figures show the average statistical figures compiled by National and Local Governmental Organizations in Japan.

# (1) Evaporating loss in refinery in Japan (1994)

(kl-crude/year)

- Crude oil input (100%)

270,857,000

- Refining loss (1.3%)

A 3,521,000

- Oil cokes

0.86%

- Flare

0.34%

- Evaporation

0.10%

## - Fuel consumption for refining (4.2%)

Heavy oil	2,675,386
Other petroleum fuel	123,326
LPG	14,050
Polinani das	8.569.924

(Source) G/p59

## (2) Yield of petroleum products (1994)

	(w%)		(w%)
- Gasoline	20.36	- Lube oil	1.09
- Naphtha	7.04	- Paraffine	0.07
- Jet oil	2.64	- Asphalt	2.64
- Kerosene	11.44	- LPG	3.81
- Gas oil	17.54		
- Heavy oil	32.27	×	
A type	12.09	1	
B type	0.07		
C type	20.11		(Source) G/p65

# (3) Emission of petroleum products in Tokyo (1994)

(Source) H/pl	5		er jandensist skist, deter Delenkis skist skist skist skist skist skist skist skist skist skist skist skist sk	(ton/year)
Emission	Sources		Gasoline	Kero/Gasoil/Heavyoil
Storage	Storage Tank	Breathing Loss	730	18.2
Failities		Receiving Loss	1,353	42.4
Delivering Fcilities	Tank Lorry	Delivering Loss	1,276	5.2
Petrol Station	Receiving	Receiving Loss	2,166	13.1
	Delivering	Delivering Loss	5,250	17.5
		(Total)	10,775	96.4

# (4) Emission factors for fuel oil handling facilities

Emissio	Sources		Petroleum Products	Emission Factors
Storage	Cone Roof	Breathing Loss	Gasoline	210kg/day
Failities	(5,000kl)	per tank	Crude Oil	90kg/day
:			Kerosene	0.83kg/day
			Gas Oil	0.70kg/day
		*	Heavy Oil	0.15kg/day
		Receiving Loss	Gasoline	1.00kg/kl
;			Crude Oil	0.52kg/ki
			Kerosene	0.0024kg/kl
·		1.	Gas Oil	0.0021kg/kl
			Heavy Oil	0.00045kg/ki
	Floating Roof	Delivering Loss	Gasoline	0.0016kg/kl
	(10,000kl)	(wet wall) per lot	Crude Oil	0.00048kg/kl
Loading	Ship	Receiving Loss	Gasoline	0.19kg/kl
Facilities			Crude Oil	0.12kg/kl
	Tank Lorry	Receiving Loss	Gasoline	0.89kg/kl
Filling Station	Unloading	Receiving Loss	Gasoline	1.08kg/kl
	Filling	Delivering Loss		1.44kg/kl

(Source) H/p62

## (5) Other hydrocarbon emission sources

Workshop	No. of workshop	Emission Volume(t/y)	Emission per Shop(t/y)	Share ratio (%)
Printing	12,000	33,000	2.75	41
Metal surface treatment	5,300	12,000	2.26	15
Painting	20,000	10,000	0.50	13
Petrol Station	2,660	10,775	2.52kg/kl	13
Cleaning	7,100	6,700	0.94	8
Others	12,600	8,000	0.63	10
(Total)	59,660	80,475		100

(Source) K/p6

0

# (6) Storage tank capacity of depots

(1,000 kl) (Total) Nazi Kan Ghoochak Ray 0 158 79 40 39 Gasoline 230 15 35 58 Kerosene 122 298 30 76 41 Gas Oil 151 240 Heavy Oil 240 0 926 115 (Total) 592 174

## (7) Fuel handling amount of depots

				(1,0	)00 kl)
	Ray	Kan	Ghoochak	Nazi	(Total)
Gasoline	1,662	578	534	0	2,774
Kerosene	1,092	170	268	134	1,663
Gas Oil	1,581	766	634	315	3,296
Heavy Oil	2,372	0	0	0	2,372
(Total)	6,707	1,514	1,436	449	10,105

(Note) Handling amount are projected based on the data supplied by Depots as well as Table 4.5.2.2-1.

								The second of
œ	v	<b> -</b>	ב	>	W		(Emission factor : දු/යJ)	
	Fuel	Specific	Heat	Sulfur	Emission	Calculation	Remark	
;		Gravity	Value	Content	Factor	Formula		
	Gasoline	0.75	1.75 8,400kcal/liter	0.086w%j		3710.75*0.86/(8400*4.187*10^-6)*2=37		
2	Jet Fuel	0.78	.78 8,700kcal/liter	0.30w%	129(	29 0.78*3/(8700*4.187*10^-6)*2=128.5	***************************************	-
	Kerosene	08.0	.80 8,900kcal/liter	0.20w%	)98	86 0.8*2.0/(8900*4,187*10^-6)*2=86		
7	Gas Oil	0.86	0.86 9.200kcal/liter	0.80w%		336~345 8.6*0.8/(9200*4.187*10^-6)*2=336~345	111.1 hadder vers in address versten i sten med de skrifte med des septem og de beste semt de beste dette 1891	,
4	5 Heaw Oil	0.95	5.95 9,700kcal/liter	2.71w%	1,268	268 9.5-2,71/(9700-4.187-10^-6)-2=1268	For general use	
:				3.50w%	1,637	.637 9.5*3.5/(9700*4.187*10^-6)*2=1637	For power plant and refinery use	***************************************
4	Sq.	0.55	0.5512.000kcal/kg   10g/100ft3	10g/100ft3		61 1.52/(12000*4.187*10^-6)*2=60.5 <sup>(1)</sup>	0.43Nm3/kg, C3=0.49Nm3/kg, C4=0.37Nm3/kg	7Nm3/kg
_	Natural Gas		9.800kcal/m3 (	0.001		0.00783/(9800*4.187*10^-6)*2=0.38	NG=0.783kg/m3	***************************************
	8 Solid Fuel		8,090kca//kg	1.00~%		590[10/(8090*4.187*10^-6)*2=590.4		

9 8 Electric Š 305 1 8 1,205 2 8 26,685 20,00 5,040 OH COKES 3 Refinery ŧ Products ŧ 8 18.560 47,875 13.97 74 166 90 5,328 43,298 170,853 1,005 24,271 104,400 2,005 3,130 2,391 1,736 1007 \$60,4 24,271 8 10211 192 1000 \* 277 Kerbusha Gas Oil 3.86 1,005 8 6 3 e 3,585 3 427 9800 7 \$ 9 200 3 8 50.23 16.00 S 20.578 8 77,162 300 2012 223,084 129,003 15 P. 3 250,944 35.562 20,073 16,036 986 4.139 50,237 156,805 3477 12442 Products Ĉ, 6.196 3,120 8,196 90 3,120 3.627 15,029 0340 4.139 08, 28 08, 28 262,624 81118 X 73 12,379 5 5 5 S 20.601 198.774 27.242 Total 35 Incuental Chemicals 36 Mechany 39 Other Industries 32 Teathe 33 Wood Products 'M Paper & Products 31 Food Products 37 km 6 See Commercial & General General Service and Household Total Menufactumo Emeeton Votome (Tehran) Agn, Egreeny Cometruction Rathery Horaehold Enteach Volume (man) Energy Convention 8 Same?

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Table 4.52-14: Districtwise SOx emission quantity in GTA (1994)

Continue								:				=							Acres (	(	
Communication   Communicatio		Ţ,	۲,		4	- 5	Č	4	8	0	10	11	12		*	15	10	1	18.	9	Ŕ
Control Cont	Casoline	-															,			-	1
Commission   Com	THAT DISTRIBUTION	1,0	5,1		18.6		2.5		2.4		1	4	C.e		•	5.6	42	3.2	82	97	10.5
Communicational 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	industrial Big Unit	00	0.0		0.0		0,0		00	ļ	0.0		0.0		00	0.0	0.0	00	00	00	8
Controlled   Con	Commercial/Household	0.0	00		0.0	į	00	ĺ	00	į	00		0.0	1	8	00	00	8	00	8	0
Companies   Comp	Energy Convention	0.0	00		00		0.0		0.0	.:	00		00		3	8	00	0	00	S	3
Communications   Column   Co	(Sub-total)	1 4	121		¥8.4 18.4		7.5		34		11		. 9		-	-65	4.2	3.2	20	8	á
Communications   Column   Co	3	_				-							-		_	1	+		+	+	1
Communicaciones   Control   Communicaciones   Control   Control   Communicaciones   Control   Communicaciones   Control   Control   Communicaciones   Control   Cont	_	262	9.0		63.7	3	8.00	13.2	28.2		6.7		*0*		13.8	8	Š	17.0	156.4	X	1
Communicacionesis (17.) (2.) (2.) (2.) (2.) (2.) (2.) (2.) (2	Production Bio Line	00	00	-	8		00		00		00		00		0.0	8	00	00	00	00	_
Control Cont		174 A	0.5%	=	4.55		0001		248.2		211.7	ľ	227.6	-	702	762.4	201.0	*90	187.6	0.1	1
Company Section   Control   Contro		c			000		00	İ.	00		00		0.0		0	0.0	0.0	0.0	0.0	0.0	00
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Proposition   Proposition	Energy Conversion	00	00		0.0	00	00	1	0.0		00		50		00	00	00	00	00	-1	J
Participation   Participatio	Suprement	S Sand	804.2	Í	5,010.2		1,885.0		1 982 4	3.0	57.7	34.	1 849		\$7.0	1 402.5	1416.6	ONB 4	4,370.3	- 1	L
Communication   Column   Col	1	-		1_												-					1
Communication   Communicatio		٤	27.6	j.	2 600 5	i	20550	٦	1 342 9	Ĺ	502.3	Ľ	2,326.9		612.7	6,563	5,374,7	1	Į		
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Communication   Communicatio			1	4.4	0.455		1 600 4		900				3.910.4		8	1 418	8	7820	4.796	673	
Communication   1,10,   1,10	Consultantion					ļ		1				L		١.	6	1		-	6	۶	1
Communication   Communicatio	Charley Conversion		6	1	g		6	1	00			Л.				20.02			ı		_
	(Sub-total)	1 140 4	1 1757	ŀ	4 524 5	`[	1	┸	2021	1	12/20	1	0.70				2		i		-
Commentation   Comm								-					:	]	1						
Communication   Communicatio	POSTER NOTES OF	2.6	•	-	2.2		10.0	1	*		1,3		) <b>Q</b>		•	93	\$2	•	32.6	7.6	*
Communicative communicative	Industrial Big Unit	°	00	1	6		0.0		00		0	1	ŏ		8	8	8	8	9	00	5
Communication   Color   Colo	Commerciathtoyashold	7,70	52.0		76.6	-	42.4		53.0	1	46.2	1	8		2/2	25.5		2	2 :	8	2
Commitment   Com	Energy Conversion	0.0	00		00	-	00		8	١	0.0		ŏ		8	0	1	8	00	8	1
Productive control of the control	(Sub-total)	+0+	5.3		4001	71.4	53.7		\$		2,2		93.		200	52.5	Ş	ŝ	6/		_
Properties   Pro	_																	-		+	$\frac{1}{1}$
Communication which Big Low   Comm	Industrial Non-big Unit	00	6	ļ	14.7		6.7	1.3	10		İ		*		50	\$5	3,0	35	r.	2.0	S.
Communicative parameter   0	Industrial Big Livit	Ö	8	ĺ	5		00	ô	8	ļ		.	10		0.7	2.2	2	8		8	:
Communication   Color   Colo	Commercial/Counsitorid	60	8.8		128		7.3		° a		7.8	l	ã		0.0	127	*	22	7.0	20	2
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Second Purising State   1705   2302   272.0   2900   1004-2 3,500.2   234,1   1181,5   1,000.0   1,400.0   240.0   1,400.0   1,400.0   240.0   1,400.0   240.0   1,400.0   240.0   1,400.0   240.0	(Sub-tetal)	96	12.3	٠	777		Ç		40.0				5		107	Ŕ	Ř	7	ž	2 5	į
Productive   110 6   3303   4772   \$1000 5   3210 6   1,5014   3000 5   1,5014   3					_	1		-	2								1	+	1		1:
Communication   Column   Col	PACIFICATION CONTROL	1105	330.3		C 098'G	3.278.9	1,501.4		1004.2	ĵ	١	7	1,070,	7	٦	1475.1	S	1,021.5	1	3	
Communication   Column   Col	Industrial Big Unit	00	0		8				0.0				Y0		1	60		8	0%	66	00
Concession   Colored   Concession   Colored	Commencial/toyanhold	00	00		0.0	Ì		8	8	Į	1		10		1	00	-	8	90	00	00
Committee;   110 5   1200 2   1201 2	Energy Conversion	0.0	0.0		0.0		970	90	9.0				8	_[	١	링	١	3	0.0	8	J
Total   Market Name   1440,2   1774,7   2,566,6   11,501,6   12,577.5   5,886,2   1,871,1   2,986,9   1,932,2   1,932,2   4,933,6   1,371,2   2,564,0   2,564,0   2,564,2   2,547,1   1,026,4   1,027,2   1,024,4   1,027,2   1,024,4   1,027,2   1,024,4   1,027,2   1,024,4   1,027,2   1,024,4   1,027,2   1,024,4   1,027,2   1,024,4   1,027,2   1,024,2   1,	(Sup-inter)	15 01.1	130	i	5,969.3		1 501 4	0.80%	1 99. 2		'n	1,0	1,670	-		1 175 1	23	1001	\$ 005.1	_i	į
Conference   Con															1		1	-		- 1	£
00 18 00 00 305 18 00 00 00 00 00 00 00 00 00 00 00 00 00	Production function United	14503	77.		11.561.6		5,886.2		2,980.0	=		_1		1	ļ	\$	7 202 6		- 4	ł	· 2
1,016.6   1,427.6   1,500.4   2,514.1   1,502.6   1,500.1   1,502.6   1,502.6   1,500.4   1,503.7   1,500.6   1,502.6   1,503.6   1,50	industrial Bry Unit	0.0	1.8		30.5		0.0		2.0			184.2	10		0.7	352.3	Ŕ	00	Į	1	ᅶ
00 00 00 00 00 00 00 00 00 00 00 00 00	Commercial/Household	1.018.6	1.402.8		2.514.1	_ !	1,800.1	1,834.9	1.679.1	-	,	: 1		İ	1,903.7	2 703.3	8	0.020	- 1	- 1	
3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Energy Conversion	00	3.0	1 1:	0.0		00	ı	00	_1		ı	3		8		*	0	8	ᇻ	
	(Sub-total)	2 408 0	2 007 3		14 106 2		7,756.3	5	4.84.0	_1		ı	\$ 032	╝	3,020.5	- 1	۶į	4,77.1	8	ξĮ	2000

5 Table 4.5.2-16: Emission quantity of pollutants by combustion from energy conversion sector in GTA (1994) 7 1.Tehran Refinery Channe Emission Volume District Fuel Consumption Sector Height HC (Total) <u>co</u> SPM HFO NĢ Total Fuel SOx NOx Gas Oil 10 Code (10^10kca) (10^10kcal) (10^10kca)} (የላ W (M W W) ር/ኒ (0) (10^10kcal) (10^8 b/y) 1,639 49,129 497 692 34,243 12,058 792 12 Refinery 10 0 122 12 2 145 13 (Note) (Flare Stack) 14 15 (Note) Cimney dimensions of Refinery No 2 Refinery No 1 Refinery 16 Heater Height ID: 17 Heater Fegt above prade 18 above prade (Feet) (Feet) (Feet) (Fack) 19 211-101 20 H-101 5.9 211-102 118 100 H-102 21 173 2H-151 22 H-151 140 150 5-3 24-151 100 H-201 23 213-201 100 4.6 200 24 5 H-251 252 255 100 46 6 211-202 6 H-254 100 25 13-6 211-251,252,253 200 250 26 7 <u>H-301</u> 100 46 8 211-254 8 H-430 200 27 9 2H-301 250 9 H-801 28 5.9 100 10 214 401,402 29 10 Boiler 250 150-10 1/21 6-6 11 24 403 11 14 1101 108-9 30 12 2H-404 150-10 1/2" 6.6 118.6 4 11 1/2 31 12 H-1102 105 3-6 13 2H-405 151 11 13 H-1202 32 100 14 2H 601 120-8 4.2 33 14 H-1301 15 214-801 138 12 15 H-1302 44 34 16 2N-1001 250 16 H-1401 35 36 (Source) Interview 37 38 2 Thermal Power Plant Chimney Emission Volume District Prodction Fuel Consumption 40 Sector Capacity Height Total Fuel SOx NOx ço HC SPM (Total) HEO Gas Oil NG 41 M. (v) (m) (Vy) (10^10kcal) (CV) N) M (GAh) (10^10kca) (10^10kca) (10^10kca) 42 14,172 5,022 201 288 684 20,373 215 430 204 43 Besat 391MW 1,49 \_\_11 19 808 21 49 713 17 73 73 75N/V 44 Firouzi 9,038 385 488 449 1,928 6,013 223 1,329 45 1243144 200E 30,219 737 1,088 16,106 1325MV 45 (Source) AAC/PS 47 48 49 3 Total 50 Emission Volum-Fuel Consumption 51 sector Total Fuel SO<sub>3</sub> NOx CO HC SPM (Total) ROG ŊĢ HFO 52 Gas Oil M) (10410kca) (VV) \_0/1 10/10kca (10^10xcai) (10^10kcal) (10^10kcal) M W 0/1 53 49,129 1,033 34,243 12,05 497 692 1,639 517 54 Tehran Refinery 21 495 11,749 723 1,190 30,219 15,106

55

Thermal Power Plant

(Total)

168

1,088

23,807

2,829

1,415

38 C O E F G F

# 39 Table 4.5.2-16: Total evaporation of HC in GTA (1994)

40 (	(B38.H62)		(ton/year)		
41	District	Commercial Shops	Depots & Refinery	(Total)	
42	: 1	525		525	
: 43	2	361		361	
- 44	3	453		453	
45	4 4	249	480	729	
46	5	409	520	929	
47	6	1,071		1,071	
48	7	873		873	
49	8	323		323	
50	9	691		691	
51	10	466		466	
52	11	872		872	
53	12	2,806		2,806	
54	13	403		403	
55	14	471		471	
56	15	937		937	
57	16	188		188	
58	17.	218		218	
59	18	857	2	859	
60	19	177		177	
61	20	730	14,988	15,718	
62	(Total)	13,080	15,990	29,070	

Table 4.5.2-17 Heat values of materials

THE RESIDENCE OF THE PROPERTY			
Matenals	Unit	Heat value	
Crude oil	kcal/liter	9,250	
Gasoline	kcal/liter	8,400	
Naphtha	kcal/liter	8,000	
Jet fuel	kcal/liter	8,700	
Kerosene	kcal/liter	8,900	
Gas oil	kcal/liter	9,200	
Heavy oil	kcal/liter	9,700	
Lube oil	kcal∕liter	9,600	
LPG	kcal/kg	12,000	
Natural gas	kcal/m3	9,800	
Coal	kcal/kg	6,950	
Cokes	kcal/kg	7,200	
Oil cokes	kcal/kg	8,500	
Electricity	kcal/kwh	860	

Note; Regarding the materials relating this section, please refer to Supporting report of following sections.

### [Final report Supporting]

- 4.5.2 Estimation of emission quantities in GTA
  - 4.5.2-1 Energy supply/demand balance in total Iran
  - 4.5.2-2 Energy demand in GTA
  - 4.5.2-3 Energy demand in GTA districts
  - 4.5.2-4 Projection of emission factors for pollutants
  - 4.5.2-5 Emission quantities of pollutants in GTA