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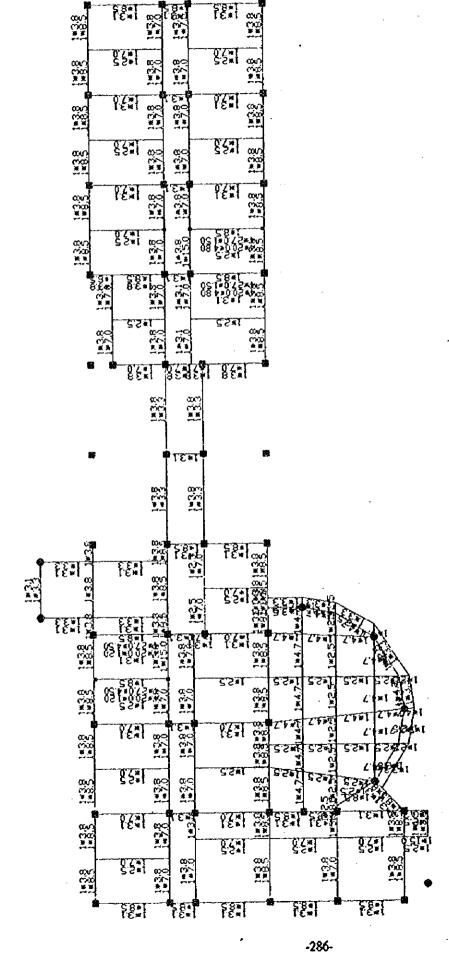
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3rd floor (floor load)

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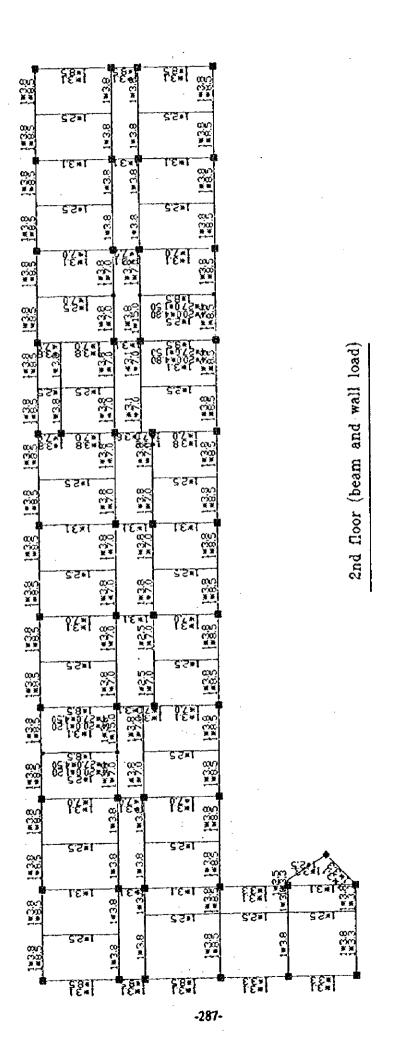
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Ist floor (beam and wall load)

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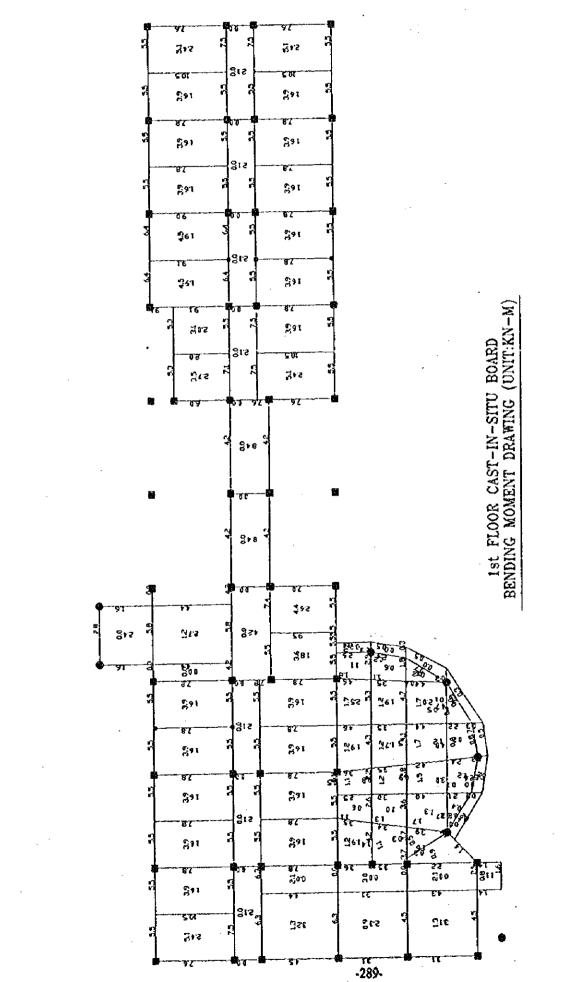
3rd floor (beam and wall load)

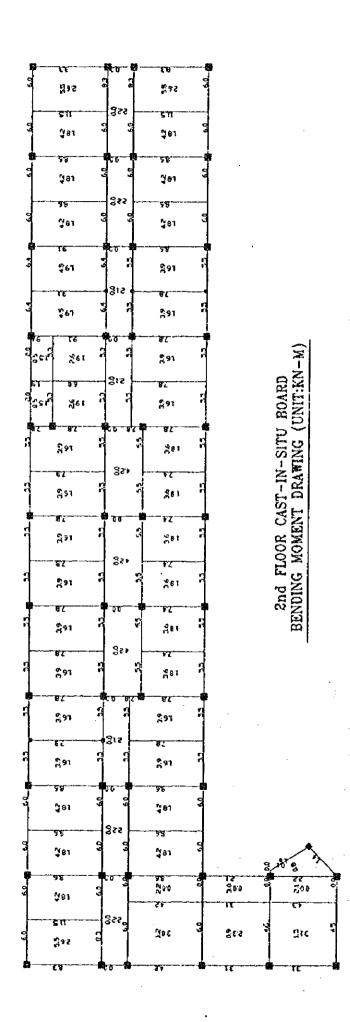
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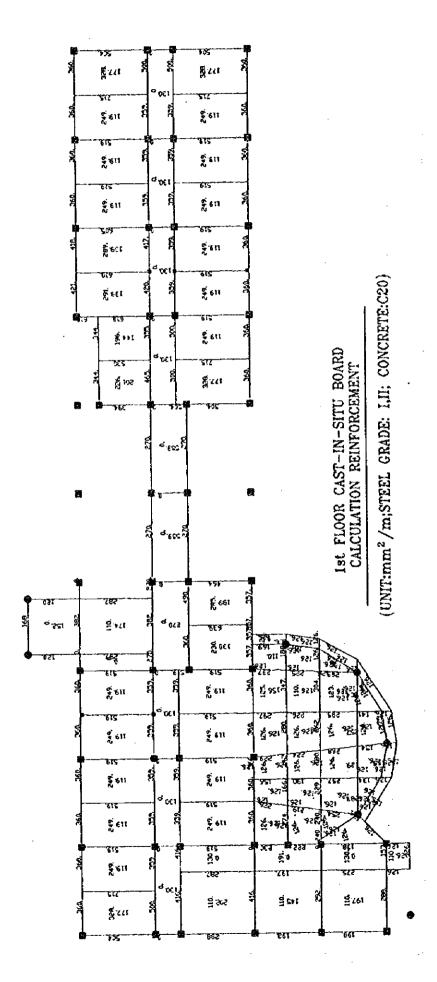
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3rd FLOOR CAST-IN-SITU BOARD BENDING MOMENT DRAWING (UNIT:KN-M)

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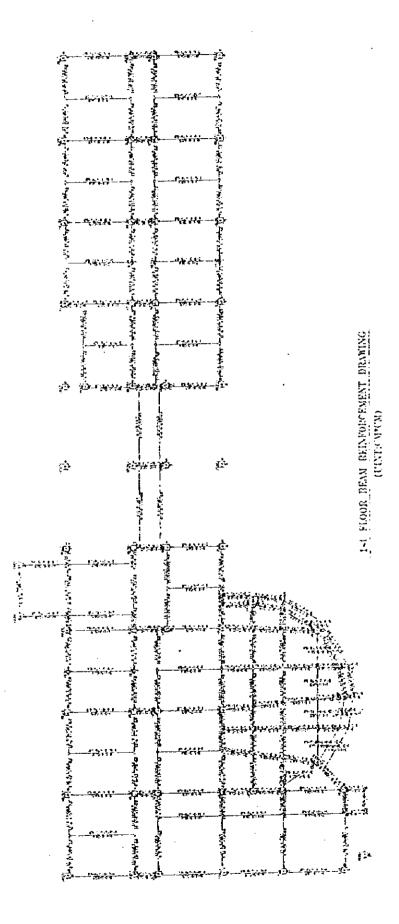
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3rd FLOOR CAST-IN-SITU BOARD CALCULATION REINFORCEMENT

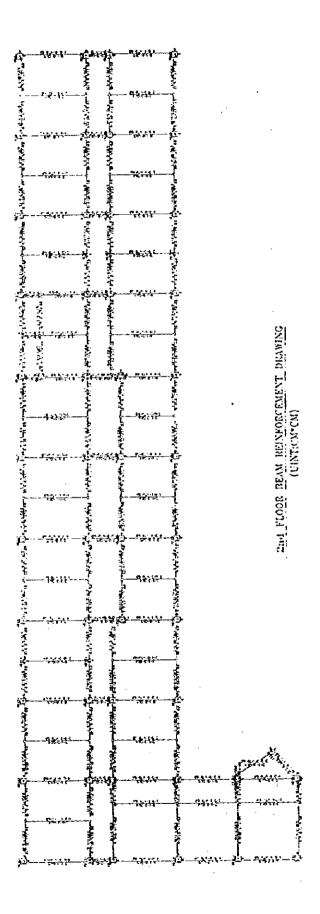
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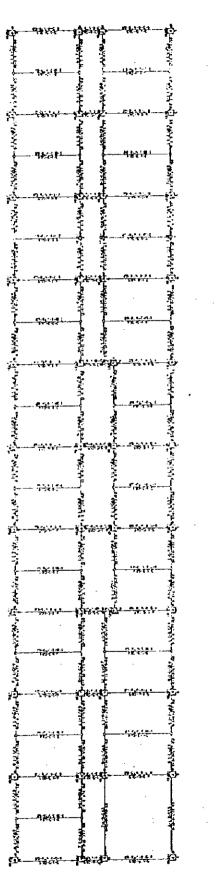


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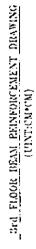
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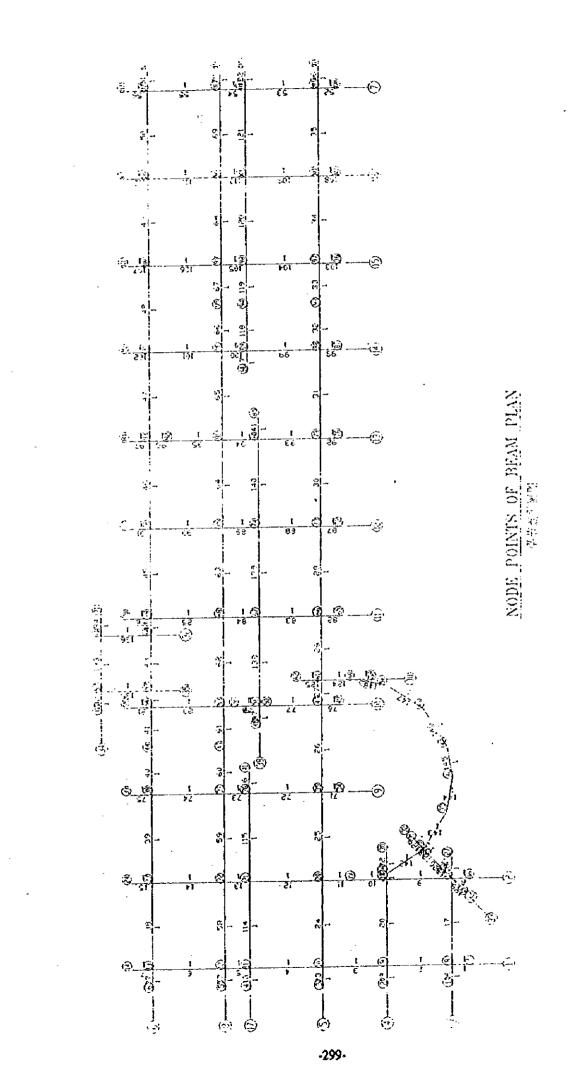
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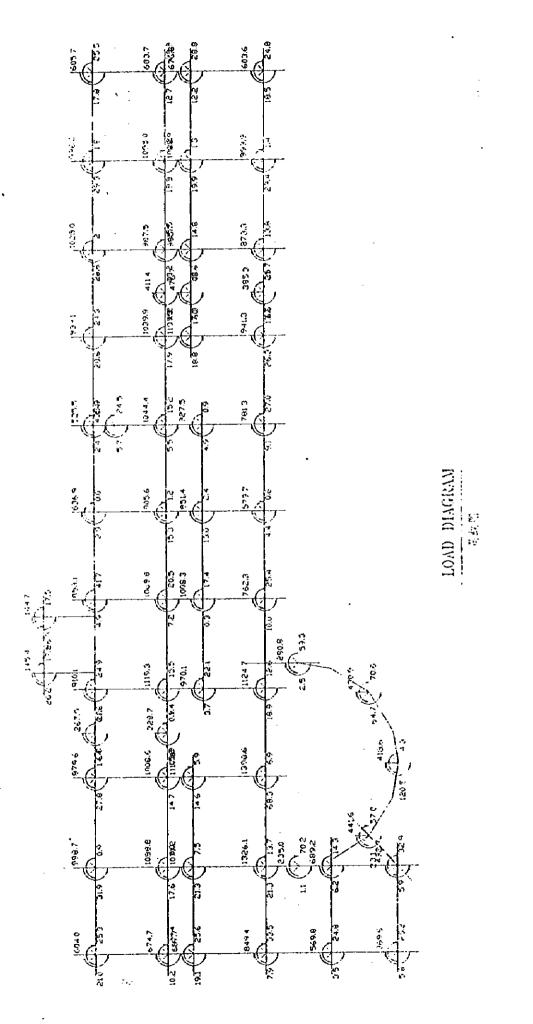
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1 •	Design Introduction	P2
2•	Output of Floors Mass and Center TAT - M.OUT	P4
3•	Output of Period and Earthquake Forces and Displacements of Floor Ta	AT-4.OUT
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4•	Output of Combined Force of Column, Wall and Brace on Each Floor	NZ - 1.0UT
		P8
5•	The Combined Force of Column, Brace and Wall Bottom on Ground F	loor DCNL.OUT
		P53
6•	Output of Reinforcements PJ-1.OUT	P88
7•	Figures 附图	

1 • Design Introduction

II. Frame seismic grade:					
III. Foundation Type :R	.C. independ	lent Foundation	·	÷.	÷ 1
IV.Seismic intensity: 7			•		· 1
V. Site soil type: IV					
VI.Structure importance		=1.0		•	
VII Soil endurance: R=90					
VIII. Materials: column	-C25	beam board -	- C25		
IX. Load:			·····		
1. Living load:					
	roof		0.7KN/m2		
2. Static load:					
	roof	ceilir	ng 0.30KN/m2		
	struc	ture layer (100r	nm) 2.50KN/m2		
	roof	(roof 1)	2.00KN/m2	-	
		total	4.80KN/m2		
X. Selection of main men					
1. column	400x400mm				
2. Main beam	. ,				
bxh=	250x600mm				
	(L=9000mm)			
bxh=	250x750mm				
Longitudinal	beam				
bxh=	240x450mm				
3. Board thickn	ess				
h=10	mm(

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2. Shanghai City's << Base Foundation Design Codes >> DBJ08--11--89;

3. Shanghai City's << Base Treatment Technical Codes >> DBJ08--40--94;

- 4. Shanghai City's << Building Anti-seismic Design Standards >> DBJ08--09--92;
- . 5. << Shanghai Pudong Airport Oil Depot Rock & Soil Investigation Immediate Report >> made by China Aviation Industry Investigation & Design Institute;

XII. Computer programs

China Building Science Research Institue CAD Engineering Department PMCAD CAD, structure plan CAD;August, 1996

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TAT Three-dimensional analysis program of high-riser building structure; August, 1996

JCCAD Independent foundation & strip foundation design; XIII. Conclusion:

It is concluded from calculation above, the integral strength and deformation of structure meet the design requirements, the geometric dimensions also meet the requirements of strength and deformation regulated by Codes. The primary data of structural model, major calculation results, combining results of main internal forces of each member, structural layout, internal force drawing, reinforcing results of major members refer the next page, based on which construction drawings are made.

2 • Output of Floors Mass and Center

1	•		Output	of Floors	s Mass and (Center		• •
1	•	-	·	ſ	AT-M.OU	r ·		*
. 1	•			*****				*
1	*	Sym	bols:					*
3	* No	Numbe	r of floor					*
1	* To	wer Nun	nber of tower	г				*
1	• we	eight Tot	al weight of	floor(kN)			*
;	*	(selfw	eight of stru	cture + s	ab loading	+ loading)		*
1	* Ma	iss Total	mass of eacl	h floor(kg	g)(Weight/1	0.)		+
ł	• x,	Y-Center	- Coordinate	of mass o	enter(m)			+
1	* Ve	r-Load 7	fotal load of	loading f	loor(kN)			*
:	*		cluding selfw	-		nn/wali)		*
;	* R-)	-	tal rotation n	-				+
:			Wind force i					*
	-		entricity betw				iter(m)	*
:			Shear of e	-				*
:			Moment of		•		nì	*
,		•	of each floor(oor og mine	10100(1011)	,	*
;	*****	*********	*********		*******	*********	*********	********
							• • • • • • • • • •	
ih T	ower	Weight	F-Weight	Mass	X-Center	Y-Center	Ver-Load	R-Mass
		(kN)	(kN)	(t)	(m)	(m)	(kN)	(t*m2)
1	3	21233.0	21233.	2123.3	40.6	10.8	15390.0	1647826.

Total Vertical Loads =	15390. (kN)
Total Structure Weight =	21233. (kN)
Total Mass =	2123.3 (t)

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*	Output of Period and Earthquake Forces and Displacements of Floor	*
	TAT-4.OUT	*
*		*
*	Symbols:	*
*	T(Nm) Natural vibration period of structure(sec)	*
*	Fir Number of floor	*
*	Nt Number of tower	*
*	Nm Number of modes	*
*	Mode(Nm) Natural vibration mode	1
*	Force(Nm) Earthquake force of modes(kN)	•
*	Qox,y Ground base shear of seismic force in X,Y direction(kN)	4.5.1
Ŧ	Mox,y Base moment of seismic force in X,Y direction	on(kN-r
*	Ge Total weight of structure(kN)	
*	X,Y,T-Direct Mode and Seismic force in torsional couple X,Y-DISP Horizontal displacement of mass center(mm)	
*	Angle Horizontal rotation angle(rad)	
*	dx,y Interfloor displacement in X,Y direction(mm)	
*	h Height of each floor(m)	
*	Tower Number of	tow
*	Hmax Maximum Height of	floor(n
+	Dmax Maximum displacement on top p	part(mn

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The Vibration Modes-X & Earthquake Forces-X

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Calculation book 6 Oil Car Storage No Nt Mode 1 Force 1 (kN) Force 1 Mode 2 Force 2 No Nt Mode 1 (kN) (kN) 1 1.0000 1698.64 1 Qox/Ge = Qox =1698.642 (kN) 8.00% 10191.850 (kN-m) Mox = The Vibration of Y-Direction Y-Direction Period (Second) T1 = 0.3905 (s) T1 = 0.3905 (s)T2 == ******** (s) The Vibration Modes-Y & Earthquake Forces-Y Mode 1 No Nt Force 1 (kN) No Nt Mode 1 Force 1 Mode 2 Force 2 (kN) (kN) 1 1 1.0000 1698.64 Qoy = 1698.642 (kN) Qoy/Ge = 8.00% Moy = 10191.850 (kN-m) ------ Displacements of Floor ------TYPE1 ==== The displacements of floor under X-Earthquake Force Flr Nt X-DISP **Y-DISP** Angle dx/h dx h (mm) (mm) (rad) (mm) (m) 1 0.36 0.27 1 0.00001 0.36 6.00 1/9999. Tower = 1 (Dmax/Hmax=1/9999.), Dmax= 0.4(mm) Hmax= 6.00(m) TYPE2 ----- The displacements of floor under Y-Earthquake Force

R

Fir	Nt	X-DISP	Y-DISP	Angle	dy/h	dy	h
		(mm)	(mm)	(rad)		(mm)	(m)
1	1	0.27	3.09	0.00008	1/1942.	3.09	6.00
To	wer =	1 (Dmax/Hmax=1	1/1942.), Dma	x= 3.1(m	m) Hmax	(= 6.0)0(m)

TYPE3 ==== The displacements of floor under Dead Vertical Force

Flr	Nt	X-DISP	Y-DISP	Angle
		(mm)	(mm)	(rad)
1	1	0.01	-0.01	0.00000

TYPE4 ==== The displacements of floor under Live Vertical Force

1. . .

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Fir	Nt	X-DISP	Y-DISP	Angle
		(mm)	(mm)	(rad)
1	1	0.00	0.00	0.00000

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Output of Combined Force of Column, Wall and Brace on Eac	h Floor
NZ-1.OUT	
Symbols:	
C,W,G Element number of column, shear wall and brace	
ND(TOP,BOT) Number of up and down node of column, w	vall, brace *
V-X,Y Shear in X,Y direction(kN)	*
N Axial force(kN)	
M-X,Y Moment in X,Y direction(kN-m)	
N(11-12) Number of branch of shear wall	*
11-12 Number of nodes in front and back of wall branch	*
M,N,V-T Moment, axial force and shear of branch	*
B-I,J Number of node on left and right of beam	*

| No. of Floor = 1 |

С(ТҮРЕ	9)	ND	V-X	V-'	Y =	N=	M-X	M-Y
1(1)	1	тор	-0.06	-15.5	50 -274	1.94	-62.18	0.30
	1	BOT	0.06	15.50) -2'	74.94	-30.81	0.07
1(2)	1	TOP	-0.05	-13.18	3 -23	32.78	-52.89	0.25
	1	BOT	0.05	13.18	-2	32.78	-26.21	0.06
1(3)	1	TOP	1.00	-14.77	-26	2.90	-59.00	-2.76
	ł	BOT	-1.00	14.77	-26	2.90	-29.59	-3.27
1(4)	1	TOP	-1.13	-14.41	-26 1	.87	-58.04	3.34
	1	BOT	1.13	14.41	-261.87	-28.40	3.42	
1(5)	1 '	ТОР	1.94	-12.39	-260.79	-52.63	-5.25	
	1	BOT	-1.94	12.39	-260.79	-21.69	-6.40	
1(6)	1 1	ГОР	-2.06	-16.79	-263.97	-64.41	5.83	
	1	BOT	2.06	16.79	-263.97	-36.31	6.56	
ł(7)	1 1	гор	1.01	-12.33	-219.17	-49.25	-2.80 ·	

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cul	lati	ion bo	onk one	Car Storage				
	1	BOT	-1.01	12.33	-219.17	-24.76	-3.28	
8)			-1.12					
			1.12					
			1.95					
			-1.95					
			-2.05					
-	1	BOT	2.05	14.35	-220.24	-31.47		
			0.05				-0.16	
			-0.05					
			0.04					
			-0.04					
3)	2	TOP	1.02	-15.34	-263.01	-61.17	-2.81	
	2	BOT	-1.02	15.34	-263.01	-30.90	-3.30	
(4)	2	TOP	-0.92	-14.76	-262.80	-59.59	2.52	
	2	BOT	0.92	14.76	-262.80	-28.94	3.02	
	2	TOP	2.07	-11.54	-260.60	-50.97	-5.76	
	2	BOT	-2.07	11.54	-260.60	-18.26	-6.65	
			-1.97					
			1.97					
			1.01					
			-1.01					
			-0.93					
			0.93					
(9)			2.05					
			-2.06					
(10)			-1.98					
			1.98					
(1)	3	тор	· 0.04	-16.01	-275.29	-64.24	-0.12	
			-0.04					
(2)							-0.11	
			-0.04					
(3)			1.03					
			-1.03					
(4)							2.61	
			0.95					
(5)			2.06					
			-2.06					
(6)			-1.98					
							6.39	
(7)			1.02					
	3	BOT	-1.02	12.97	-219.22	-20.32	-3.29	

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	3 BOT	0.95	12.15	-218.65	-23.61	3.09	
3(9)	3 TOP						
	3 BOT						
3(10)) 3 TOP						÷ .
• •	3 BOT						
• = • • • • • •						••••	
4(1)	4 TOP					0.03	-
	4 BOT	-0.01	16.01	-275.57	-31.83	-0.06	
4(2)	4 TOP	0.00	-13.62	-233.31	-54.63	0.02	
	4 BOT	0.00	13.62	-233.31	-27.07	-0.05	
	4 TOP						
	4 BOT						-
4(4)	4 TOP	-0.98	-14.54	-262.65	-59.05	2.75	
	4 BOT	0.98	14.54	-262.65	-28.22	3.13	
4(5)	4 TOP	2.02	-8.94	-258.94	-44.04	-5.58	
	4 BOT	-2.02	8.94	-258.94	-9.63	-6.56	
4(6)	4 TOP	-2.02	-21.19	-267.04	-76.86	5.64	
	4 BOT	2.02	21.19	-267.04	-50.28	6.46	
4(7)	4 TOP	0.99	-13.08	-219.50	-51.78	-2.70	
	4 BOT	-0.99	13.08	-219.50	-26.70	-3.23	
4(8)	4 TOP	-0.98	-12.03	-218.82	-48.97	2.75	· .
	4 BOT	0.98	12.03	-218.82	-23.23	3.14	
4(9)	4 TOP	2.02	-6.43	-215.11	-33.96	-5.58	
	4 BOT	-2.02	6.43	-215.11	-4.63	-6.55	
4(10)	4 TOP	-2.02	-18.68	-223.21	-66.79	5.63	:
	4 BOT	2.02	18.68	-223.21	-45.29	6.47	
					******	: •••	••.
						-0.9 6	:
	5 BOT	-0.25	16.02	-273.88	-31.84	-0.55	
5(2)	5 TOP	0.21	-13.62	-231.88	-54.65	-0.81	
	5 BOT	-0.21	13.62	-231.88	-27.08	-0.46	
5(3)	5 TOP	1.22	-15.71	-261.83	-62.18	-3.60	•
	5 BOT						
5(4)						1.80	: .
						2.66	
5(5)	5 TOP						
						-7.01	
5(6)	5 TOP	-1.77	-22.50	-266.23	-80.39	4.67	· : ·
	5 BOT	1.77	22.50	-266.23	-54.63	5.98	÷
5(7)	5 TOP						÷
				-218.27			
5(8)	5 TOP						
				-217.36			
5(9)	5 TOP	2.21	-5.13	-212.97	-30.48	-6.32	

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		вот	-2.21	5.13	-212.97	-0.31	-6.92
\$(10)			-1.81				
5(10)			1.81				
			-1.31				5,30
			: 1.31				
			-1.11				
			1.11				
6(3)	6	ТОР	-0.23	-15.64	-272.07	-61.76	2.20
	6	BOT	0.23	15.64	-272.07	-32.10	-0.81
			-2.26				
	6	BOT	2.26	14.14	-271.48	-27.11	5.67
6(5)	6	TOP	0.83	-6.16	-265.63	-36.33	-0.78
			-0.83				
6(6)	6	ТОР	-3.32	-23.62	-277.92	-83.14	10.86
	6	BOT	3.32	23.62	-277.92	-58.60	9.05
6(7)	6	TOP	-0.02	-13.16	-226.78	-51.80	1.36
	6	BOT	0.02	13.16	-226.78	-27.17	-1.22
6(8)	6	TOP	-2.05	-11.66	-225.19	-47.76	7.04
	6	BOT	2.05	11.66	-226.19	-22.17	5.27
• •			1.03				
	6	BOT	-1.03	3.67	-220.34	4.33	-4.59
			-3.11				
			3.11				8.64
			8.71				
			-8.71				
7(2)			7.38				
	7		-7.38				
7(3)			9.08				
			-9.08				
7(4)						-42.89	
			•7.48				
7(5)		TOP		-1.20		-18.19	
	•		-9.96				
7(6)		TOP		-21.33		-72.21	
			-6.60				
7(7)							
			-7.70		•		
7(8)			6.10				
		BOT			-135.74		
7(9)		TOP		0.68	-	-10.65	
			-8.58				
7(10)	7	TOP	5.22	-19.45	-142.24	•64.67	-23.42

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		DOT	6.00	10.45	142.24	62.05	7.01	
							-7.91	• •
							34.74	
	8	BOT	8.65	11.76	-170.25	-23.38	17.13	-
(2)	8	ТОР	-7.33	-9.94	-143.59	-39.87	29.45	
	8	BOT	7.33	9.94	-143.59	-19.77	14.52	
					-164.25			
	8	BOT	7.42	12.15	-164.25	-25.32	13.47	
							35.04	
• •					-164.51			
					-156.25			· .
•••							10.46	
					-172.51			
							22.12	
					-136.85			:
					-136.85			
							29.53	
							16.40	
							23.30	
							7.74	
							31.77	
,					-145.11			
					-177711			
9(1)	9	TOP	1.39	-15.82	-284.83	-63.45	-5.52	
	9	BOT	-1.39	15.82	-284.83	-31.44	-2.81	
9(2)	9	TOP	1.18	-13.45	-241.16	-53.96	-4.68	
	9	BOT	-1.18	13.45	-241.16	-26.74	-2.38	
9(3)	9	ТОР	2.33	-15.88	-272.65	-62.39	-8.08	
	9	BOT	-2.33	15.88	-272.65	-32.89	-5.91	
9(4)							-2.41	
	9				-270.94			
9(5)	9	TOP			-264.60			
	9	вот					-9.28	
		ТОР					0.57	-
	9	вот					3.96	
)(7)							-7.21	. •
							-5.46	
			0.08		-225.64			 ±1
、- <i>)</i>							1.03	
i o y					-219.30			
							-10.19 -8.84	
0(10)							-8.84 1.45	
ハコマト	7	IUF	•V.77	-23.00	-433.08	•0V.32 ·	1.45	

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		-16.02 -273.88		
		16.02 -273.88		
• •		-13.62 -231.87		
		13.62 -231.87		
		-16.18 -262.08		
		16.18 -262.08		
10(4)10 TOP	-1.15	-13.97 -260.68	-57.52	3.41
10 BOT	1.15	13.97 -260.68	-26.31	- 3.46
10(5) 10 TOP	1.84	-2.31 -252.89	-26.25	-4.86
10 BOT	-1.84	2.31 -252.89	12.42	-6.21
10(6)10 TOP	-2.18	-27.85 -269.87	-94.71	6.28
10 BOT	2.18	27.85 -269.87	-72.37	6.78
10(7)10 TOP	0.84	-13.67 -218.51	-53.36	-2.11
10 BOT	-0.84	13.67 -218.51	-28.64	-2.94
10(8)10 TOP	-1.12	-11.46 -217.12	-47.44	3.29
10 BOT	1.12	11.46 -217.12	-21.31	3.41
10(9)10 TOP	1.87	0.21 -209.33	-16.17	-4.98
10 BOT	-1.87	-0.21 -209.33	17.42	-6.26
10(10) 10 TOP	-2.15	-25.33 -226.31	-84.63	6.16
		25.33 -226.31		
		-16.01 -275.57		-0.24
		16.01 -275.57		
11(2)11 TOP	0.06	-13.62 -233.31	-54.64	-0.21
11 BOT	-0.06	13.62 -233.31	-27.08	-0.16
		-16.29 -263.80		
		16.29 -263.80		
		-13.85 -262.18		
		13.85 -262.18		
		-0.99 -253.70		
		0.99 -253.70		
		-29.15 -272.27		
		29.15 -272.27		
		-13.78 -219.97		
· · · · ·		13.78 -219.97		
		-11.34 -218.35		
		i 11.34 −218.35		
		1.52 -209.87		
		-1.52 -209.87		
		-26.63 -228.44		
		26.63 -228.44		
		20.03 -228.44		
10/ 1\ 12 TOP	-	-16.01 -275.31	-	
• •				
17 ROI	-0.03	16.01 -275.31	-51.84	-0.11

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		محاد المحجول المراجع المراجع محادثتها والمستحا المراجع المحادث محادث المحادث ومراجل والتراجعا ترما		
12(2)12 TOP	0.03	-13.62 -233.09 -	54.64	-0.07
		13.62 -233.09		
		-16.40 -263.62 -		
		16.40 -263.62		
		-13.74 -261.86 -:		
		13.74 -261.86		
		0.31 -252.58 -		
		-0.31 -252.58		
		-30.45 -272.90 -10		
• •		30.45 -272.90		
				-2.78 a to the two
=		13.89 -219.83		
				2.66
		11.23 -218.07		
				-5.67
12 BOT	-2.04	-2.82 -208.79	26.10	-6.60
				5.54
		27.94 -229.11		
13(1)13 TOP	0.04	-16.01 -275.31 -	64.25	-0.13
		16.01 -275.31		
		-13.62 -233.09 -		
		13.62 -233.09		
13(3)13 TOP	1.02	-16.52 -263.70 -	64.34	-2.84
13 BOT	-1.02	16.52 -263.70	-34.77	-3.31
13(4)13 TOP	-0.94	-13.62 -261.79 -:	56.58	2.60
13 BOT	0.94	13.62 -261.79	-25.16	3.06
13(5)13 TOP	2.06	1.62 -251.73	-15.73	-5.72
		-1.62 -251.73		
13(6)13 TOP	-1.98	-31.76 -273.76 -10	05.20	5.49
		31.76 -273.76		
13(7)13 TOP	1.02	-14.01 -219.91 -	54.27	-2.82
13 BOT	-1.02	14.01 -219.91	-29.78	-3.29
		-11.11 -218.00		
13 BOT	··· 0.95	11.11 -218.00	-20.17	3.08
13(9)13 TOP	2.05	4.13 -207.94	-5.65	-5.70
13 BOT	-2.05	-4.13 -207.94	30.43	-6.61
13(10) 13 TOP	-1.99	-29.25 -229.97 -	95.12	5.51
13 BOT	1.99	29.25 -229.97	-80.37	6.41
		- * * * * * * * * * * * * * * * * * * *		
				0.01
		16.01 -275.54		
14(2)14 TOP	0.01	-13.62 -233.29 -	54.64	0.01
		13.62 -233.29		
			-	

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14(3)14 TOP	0.99	-16.63	-263.99	-64.65	-2.71
14 BOT					
4(4)14 TOP					
14 BOT					
(5)14 TOP					
14 BOT					
(6)14 TOP					
14 BOT					
(7)14 TOP					
14 BOT					
4(8)14 TOP					
14 BOT					
4(9)14 TOP					
14 BOT					
4(10) 14 TOP					
14 BOT					
5(1)15 TOP					-0.86
15 BOT					
5(2)15 TOP					
15 BOT					
(3)15 TOP					
15 BOT					
(4)15 TOP					
15 BOT					
(5)15 TOP					
15 BOT					
(6)15 TOP					
15 BOT					
5(7)15 TOP					
15 BOT					
6(8)15 TOP					
15 BOT					
(9) 15 TOP					
15 BOT					
5(10) 15 TOP					
15 BOT					
12 801					0,11
(1)16 TOP					4.69
16 BOT					
6(2)16 TOP					
16 BOT					
(3) 16 TOP					
(3) 16 TOP 16 BOT					
10 801	0.08	10.79	• 4 1 4. 4 1	->>.70	-1.11

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		Construction of the second distribution of the s			
16(4) 16 TOP	-2.12	-13.20 -270.33	-55.36	7.30	· · ·
16 BOT	2.12	13.20 -270.33	-23.87	5.39	-
16(5) 16 TOP	0.95	5.61 -257.48	-4.93	-1.27	
16 BOT	-0.95	-5.61 -257.48	38.59	-4.43	
16(6) 16 TOP	-3.15	-35.60 -285.12	-115.39	10.19	•
		35.60 -285.12			
		-14.29 -227.05			-
		14.29 -227.05			
		-10.70 -225.11			· .
		10.70 -225.11			
		8.11 -212.26			· .
		-8.11 -212.26			
		-33.10 -239.91			
		33.10 -239.91			
17(1)17 TOP	7.84	-11.88 -171.67	-47.66	-31.41	: •
17 BOT	-7.84	11.88 -171.67	-23.63	-15.62	
17(2)17 TOP	6.65	-10.05 -144.79	-40.29	-26.64	
17 BOT	-6.65	10.05 -144.79	-19.98	-13.25	
17(3) 17 TOP	8.23	-13.29 -167.71	-50.76	-31.77	
17 BOT	-8.23	13.29 -167.71	-28.96	-17.63	
		-9.48 -163.75			. :
17 BOT	-6.65	9.48 -163.75	-16.33	-12.03	
17(5)17 TOP	9.26	10.55 -152.54	13.17	-34.63	-
17 BOT	-9.26	-10.55 -152.54	50.16	-20.94	
17(6)17 TOP	5.62	-33.33 -178.92	-104.51	-25.02	-
17 BOT	-5.62	33.33 -178.92	-95.44	-8.72	÷ .
17(7)17 TOP	6.99	-11.39 -140.09	-43.15	-26.80	· · ·
17 BOT	-6.99	11.39 -140.09	-25.19	-15,16	
17(8)17 TOP	5.41	-7.59 -136.13	-32.97	-22.91	• -
		7.59 -136.13			
17(9)17 TOP	8.02	12.45 -124.92	20.78	-29.66	
		-12.45 -124.92			· ·
17(10) 17 TOP	4.38	-31.43 -151.30	-96.90	-20.05	• • • • • • • • • • • • • • • • • • • •
17 BOT	-4.38	31.43 -151.30	-91.67	-6.25	. •
==**>=>*******			**		•
18(1)18 TOP	1.33	3.11 -409.63	12.51	-5.27	· .
		-3.11 -409.63			
18(2)18 TOP	1.13	2.65 -347.82	10.63	-4.49	
18 BOT	-1.13	-2.65 -347.82	5.24	-2.28	•
		2.72 -387.58			
18 BOT	-2.46	-2.72 -387.58	5.14	-6.37	•
18(4) 18 TOP	0.03	3.14 -387.38	12.39	-1.52	:
18 BOT	-0.03	-3.14 -387.38	6.46	1.34	

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18/ 5) 18 TOP	1.48	5.54 -388.91	19.32	-5.83
		-5.54 -388.91		
		0.32 -386.04		
		-0.32 -386.04		
		2.23 -323.00		
		-2.23 -323.00		
		2.65 -322.80		
		-2.65 -322.80		
		5.05 -324.33		
-		-5.05 -324.33		
		-0.17 -321.47		
-		0.17 -321.47		
19(1)19 TOP	-0.16	3.47 -399.81	13.94	0.69
19 BOT	0.16	-3.47 -399.81	6.87	0.27
		2.95 -339.46		
19 BOT	0.14	-2.95 -339.46	5.84	0.23
		2.92 -378.12		
19 BOT	-0.99	-2.92 -378.12	5.38	-3.46
19(4)19 TOP	-1.30	3.61 -378.40	14.13	3.81
19 BOT	1.30	-3.61 -378.40	7.55	3.98
19(5)19 TOP	-0.12	7.42 -379.02	25.12	0.61
19 BOT	0.12	-7.42 -379.02	19.40	0.14
19(6)19 TOP	-0.18	-0.89 -377.50	1.13	0.69
19 BOT	0.18	0.89 -377.50	-6.46	0.38
19(7)19 TOP	1.02	2.37 -315.07	9.93	-2.61
19 BOT	-1.02	-2.37 -315.07	4.31	-3.51
		3.07 -315.36		
19 BOT	1.27	-3.07 -315.36	6.47	3.93
• •		6.88 -315.97		
		-6.88 -315.97		
19(10) 19 TOP	-0.15	-1.43 -314.46	-1.05	0.58
19 BOT	0.15	1.43 -314.46	-7.54	0.34
		3.48 -401.39		
		-3.48 -401.39		
		2.96 -340.81		
		-2.96 -340.81		
20(3)20 TOP	1.23	2.79 -379.65	11.77	-3.43
		-2.79 -379.65		
		3.76 -379.85		
		-3.76 -379.85		
		8.97 -381.09		
20 BOT	-0.13	-8.97 -381.09	24.23	-0.36

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20(6)20 TOP	0.01	-2.43 -378.41	-3.29	-0.07	
		2.43 -378.41			
		2.25 -316.36			
		-2.25 -316.36			
		3.21 -316.56			
		-3.21 -316.56			
		8.43 -317.80			
-		-8.43 -317.80			
		-2.97 -315.12			
		2.97 -315.12			
		3.48 -401.37			
•••		-3.48 -401.37			
		2.96 -340.79			· ·
		-2.96 -340.79			
		2.66 -379.58			
		-2.66 -379.58			
		3.89 -379.88			
		-3.89 -379.88			
		10.52 -381.39			
		-10.52 -381.39			
		-3.97 -378.06			-
		3.97 -378.06			
		2.11 -316.29			
		-2.11 -316.29			
		3.35 -316.59			
		-3.35 -316.59			
		9.97 -318.11			
		-9.97 -318.11			
		-4.52 -314.77			
21 BOT	0.05	4.52 -314.77	-17.15	0.13	
		\$ * ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ 			
22(1)22 TOP	0.22	3.48 -400.01	13.98	-0.83	
22 BOT	-0.22	-3.48 -400.01	6.89	-0.48	-
		2.96 -339.63			
		-2.96 -339.63			
		2.52 -378.31			
		-2.52 -378.31			
		4.03 -378.58	-		
		-4.03 -378.58			
		12.06 -380.47			_ · ·
		-12.06 -380.47			
		-5.52 -376.42			
		5.52 -376.42			
	-0,12	5.56 -510.46	20.07	0.20	

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22(7)22 TOP	1.32	1.97	-315.23	8.79	-3.82
22 BOT	-1.32	-1.97	-315.23	3.06	-4.10
22(8)22 TOP	-0.98	3.48	-315.51	13.14	2.53
22 BOT	0.98	-3.48	-315.51	7.75	3.35
22(9)22 TOP	0.23	11.52	-317.40	36.34	-0.80
22 BOT	-0.23	-11.52	-317.40	32.77	-0.55
22(10) 22 TOP	0.12	-6.06	-313.34	-14.41	-0.50
22 BOT	-0.12	6.06	-313.34	-21.97	-0.20

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22 B	-0.23	-11.22	+317.40	22.11	-0.55	
22(10) 22 TO	P 0.12	-6.06	-313.34	-14.41	-0.50	
	OT -0.12					
23(1)23 TO	P -1.08	3.42	-408.83	13.73	4.38	
	OT 1.08					
	P -0.92					
	OT 0.92					·
23(3)23 TO	P 0.17	2.33	-386.32	10.37	0.79	
	OT -0.17					
	P -2.21					
23 B	OT 2.21	-4.11	-387.19	9.14	5.78	
23(5)23 TO	P -0.96	13.55	-389.13	42.77	3.97	
	ют 0.96					
23(6)23 TO	P -1.07	-7.12	-384.38	-16.90	4.28	
	BOT 1.07					
23(7)23 TO	P 0.34	1.79	-321.86	8.21	0.11	
23 B	BOT -0.34	-1.79	-321.86	2.54	-2.16	
23(8)23 TO	P -2.04	3.57	-322.73	13.34	6.77	
23 B	BOT 2.04	-3.57	-322.73	8.08	5.45	
23(9)23 TO	P -0.79	13.02	-324.67	40.62	3.29	
	BOT 0.79					
23(10) 23 TC	OP -0.90	-7.65	-319.92	-19.06	3.60	
	BOT 0.90				1.83	
	P 7.64					
24 B	BOT -7.64	-2.53	-273.54	5.00	-15.22	
24(2)24 TO	P 6.50	2.14	-230.99	8.60	-26.05	
24 B	BOT -6.50	-2.14	-230.99	4.23	-12.96	
24(3)24 TO	P 8.11	1.39	-263.69	6.77	-31.06	
24 B	BOT -8.11	-1.39	-263.69	1.59	-17.60	
24(4)24 TO	P 6.22	3.45	-262.52	··· 12.70	-26.35	
24 B	BOT -6.22	-3.45	-262.52	7.98	-10.95	
24(5)24 TO	P 7.21	14.30	-265.85	44.04	-28.82	
24 B	BOT -7.21	-14.30	-265.85	41.78	-14.43	. • •
	P 7.12					
	вот -7.12					-
24(7)24 TO	P 6.92	0 .99	-219.84	5.15	-26.27	
	BOT -6.92					:

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24(8)24 TOP	5.02	3.04	-218.67	11.08	-21.57	
24 BOT						
24(9)24 TOP						
24 BOT						
24(10) 24 TOP						
24 BOT						
25(1)25 TOP					30.44	
25 BOT						
25(2)25 TOP						
25 BOT						
25(3)25 TOP						
25 BOT						
25(4)25 TOP						
25 BOT						
25(5)25 TOP						
25 BOT						
25(6)25 TOP						
25 BOT						
25(7)25 TOP						
25 BOT						
25(8)25 TOP						
25 BOT						
25(9)25 TOP						· .
25 BOT						
25(10) 25 TOP	-5.97	-10.00	-216.44	-26.57	23.92	
25 BOT						
					\$	
26(1)26 TOP	1.16	3.41	-408.85	13.73	-4.60	
			-408.85	6.76	-2.35	
26(2)26 TOP	0.99	2.90	-347.15	11.67	-3.91	• . :
					-2.00	
26(3)26 TOP	2.28	2.05	-386.73	9,55	-7.67	
26 BOT	-2.28	-2.05	-386.73	2.72	-6.02	
26(4)26 TOP	-0.10	4.39	-386.81	16.32	-1.00	•
26 BOT	0.10	-4.39	-386.81	10.02	1.60	
26(5)26 TOP	1.15	16.78	-389.90	52.09	-4.49	1 - 1 - <b>1</b> - <b>1</b>
26 BOT	-1.15	-16.78	-389.90	48.60	-2.39	
26(6)26 TOP	1.04	-10.35	-383.63	-26.22	-4.18	· · ·
				-35.86		
26(7)26 TOP			-			
• -				1.66		
26(8)26 TOP						
• •			-	8.96		

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26(9)26 TOP	0.96	16.25	-325.44	49.93	-3.77
26 BOT					
26(10) 26 TOP	0.85	-10.88	-319.17	-28.38	-3.46
26 BOT					
27(1)27 TOP	-0.14	3.48	-400.00	13.97	0.61
27 BOT					
27(2)27 TOP	-0.12	2.96	-339.62	11.88	0.52
27 BOT					
27(3)27 TOP	1.02	1.97	-378.10	9.38	-2.59
27 BOT					
27(4)27 TOP					
27 BOT					
27(5)27 TOP					
27 BOT					
27(6)27 TOP					
27 BOT					
27(7)27 TOP					
27 BOT					
27(8)27 TOP					
27 BOT					
27(9)27 TOP					
27 BOT					
27(10) 27 TOP					
27 BOT					
28(1)28 TOP	0.07	3.48	-401.40	13.97	-0.22
28 BOT					
28(2)28 TOP					
28 BOT					
28(3)28 TOP					
				1.99	
28(4)28 TOP					
28 BOT					
28(5)28 TOP					
				58.33	
28(6)28 TOP					
28 BOT					
28(7)28 TOP					
				0.91	
28( 8) 28 TOP					
28 BOT	1.10	-4.17	-316.79	9.89	3.60
28(9) 28 TOP					
				57.25	

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28(10) 28 TOP	0.00	-13.93	-312.63	-37.12	-0.02	:
28 BOT						
29(1)29 TOP						
29 BOT						
29(2)29 TOP						
29 BOT						
29(3)29 TOP						
29 BOT						
29(4)29 TOP						
29 BOT						
29(5)29 TOP						
29 BOT						
29(6)29 TOP						
29 BOT						
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29 BOT						
29(8)29 TOP						
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29(9)29 TOP						
29 BOT						
29(10) 29 TOP		-				
29 BOT						
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30(1)30 TOP						
30 BOT 30(2)30 TOP						
• •						
30 BOT						
30(3)30 TOP						
				1.14		
30(4) 30 TOP				18.10		
			-			
30( 5) 30 TOP				70.16 67.95		· .
30(6)30 TOP						
				-43.85		
30(7) 30 TOP				6.02		
				0.06		
30(8)30 TOP			-316.69			
30 BOT					3.64	
30(9)30 TOP				67.96		
				66.87		
30(10) 30 TOP						
30 BOT	0.02	17.02	-311.75	-56.08	0.07	-

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31(1)31 TOP	0.02	3.47	-401.34	13.97	-0.03
31 BOT					
31(2)31 TOP					
31 BOT					
31(3)31 TOP	1.17	1.42	-379.27	7.82	-3.22
31 BOT	-1.17	-1.42	-379.27	0.72	-3.82
31(4)31 TOP	-1.14	5.12	-380.13	18.49	3.18
31 BOT	. 1.14	-5.12	-380.13	12.23	3.66
31(5)31 TOP	0.07	24.56	-384.61	74.62	-0.17
31 BOT	-0.07	-24.56	-384.61	72.76	-0.25
31(6)31 TOP	-0.04	-18.02	-374.80	-48.31	0.13
31 BOT					
31(7)31 TOP	1.17	0.88	-315.99	5.63	-3.22
31 BOT	-1.17	-0.88	-315.99	-0.36	-3.80
31(8)31 TOP	-1.14	4.57	-316.85	16.29	3.18
31 BOT					
31(9)31 TOP	0.07	24.02	-321.33	72.42	-0.17
31 BOT	-0.07	-24.02	-321.33	71.68	-0.24
31(10) 31 TOP					
31 BOT	0.04	18.57	-311.51	-60.89	
***************************************					
32(1)32 TOP	0.16	3.48	-400.37	13.97	-0.61
32 BOT	-0.16	-3.48	-400.37	6.88	-0.38
32(2)32 TOP	0.14	2.96	-339.93	11.88	-0.52
32 BOT	-0.14	-2.96	-339.93	5.85	-0.32
32(3)32 TOP	1.30	1.29	-378.37	7.43	-3.75
32 BOT					
32(4) 32 TOP	-1.00	5.25	-379.21	18.88	2.60
32 BOT	: 1.00	-5.25	-379.21	12.65	3.38
32( 5) 32 TOP	0.21	26.11	-384.06	79.08	-0.72
32 BOT	-0.21	-26.11	-384.06	77.57	-0.52
32(6)32 TOP	0.10	-19.57	-373.52	-52.77	-0.43
32 BOT					
32(7)32 TOP	1.28	0.74	-315.24	5.24	-3.65
32 BOT	-1.28	-0.74	-315.24	-0.78	-4.02
32(8)32 TOP	-1.02	4.71	-316.08	16.69	2.70
32 BOT					
32(9) 32 TOP					
32 BOT					
32(10) 32 TOP					
32 BOT					
*****					
33(1)33 TOP	-0.75	3.44	-407.97	13.82	3.06

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						-And for the Contractor of the Contractor
33 BOT	0.75	-3.44	-407.97	6.81	1.44	
33(2)33 TOP						
33 BOT	0.64	-2.92	-346.42	5.79	1.23	•
33(3)33 TOP						
33 BOT	-0.49	-1.12	-385.17	-0.19	-2.45	
33(4)33 TOP						
33 BOT	1.89	-5.36	-386.60	13.00	5.16	
33(5)33 TOP	-0.64	27.62	-391.45	83.41	2.68	-
33 BOT	0.64	-27.62	-391.45	82.32	1.16	
33(6)33 TOP	-0.76	-21.14	-380.33	-57.36	3.05	
33 BOT	0.76	21.14	-380.33	-69.50	1.54	
33(7)33 TOP	0.60	0.58	-320.86	4.74	-0.95	
33 BOT	-0.60	-0.58	-320.86	-1.25	-2.68	
33(8)33 TOP	-1.77	4.82	-322.29	16.97	5.72	
33 BOT	1.77	-4.82	-322.29	11.94	4.93	
33(9)33 TOP	-0.52	27.08	-327.13	81.24	2.20	
33 BOT	0.52	-27.08	-327.13	81.25	0.93	
33(10) 33 TOP	-0.65	-21.68	-316.01	-59.53	2.57	
33 BOT	0.65	21.68	-316.01	-70.57	1.32	z
						· · ·
34(1)34 TOP	5.63	2.53	-276.82	10.19	-22.55	-
34 BOT	-5.63	-2.53	-276.82	5.01	-11.23	
34(2)34 TOP	4.81	2.14	-233.78	8.62	-19.25	
34 BOT	-4.81	-2.14	<u>-233.78</u>	4.24	-9.59	
34(3)34 TOP	6.19	0.17	-266.53	3.24	-23.34	•
34 BOT	-6.19	-0.17	-266.53	-2.23	-13.77	
34(4)34 TOP	4.28	4.68	-265.93	16.27	-18.59	
34 BOT	-4.28	-4.68	-265.93	11.81	-7.11	. •
34( 5) 34 TOP	5.23	28.36	-272.25	84.64	-20.89	· :
34 BOT	-5.23	-28.36	-272.25	85.53	-10.51	
34(6)34 TOP	5.24	-23.51	-260.21	-65.13	-21.04	· · ·
34 BOT						
34(7)34 TOP	5.31	-0.24	-222.16	1.62	-19.84	•
34 BOT					-12.03	· •
34(8)34 TOP	3.41	4.28	-221.56	14.65	-15.10	•
34 BOT	-3.41	-4.28	-221.56	11.01	-5.37	
34(9)34 TOP	4.36	27.96	-227.88	83.02	-17.39	۰. -
34 BOT	-4.36	-27.96	-227.88	84.74	-8.77	
34(10) 34 TOP	4.36	-23.92	-215.84	-66.76	-17.55	:•
34 BOT						
4		****	**********	*********		· · · · ·
35(1)35 TOP	1.35	-3.08	-408.09	-12.34	-5.36	
35 BOT	-1.35	3.08	-408.09	-6.14	-2.73	
35(2)35 TOP	1.15	-2.62	-346.51	-10.49	-4.56	:
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35         BOT $\cdot 1.15$ $2.62$ $\cdot 3.11$ $\cdot 386.07$ $\cdot 12.23$ $\cdot 8.80$ 35         BOT $\cdot 2.62$ $\cdot 3.11$ $\cdot 386.07$ $\cdot 12.23$ $\cdot 8.80$ 35         BOT $\cdot 2.62$ $\cdot 3.11$ $\cdot 386.07$ $\cdot 12.23$ $\cdot 6.80$ 35         BOT $\cdot 0.09$ $\cdot 2.69$ $\cdot 386.00$ $\cdot 11.01$ $\cdot 1.25$ 35         BOT $\cdot 0.80$ $\cdot 0.29$ $\cdot 384.89$ $-4.07$ $\cdot 8.86$ 35         BOT $\cdot 3.32$ $\cdot 5.51$ $\cdot 387.18$ $\cdot 19.16$ $\cdot 10.91$ 35         BOT $\cdot 3.32$ $\cdot 5.51$ $\cdot 387.18$ $\cdot 10.29$ $\cdot 7.97$ 35         BOT $\cdot 2.01$ $\cdot 2.63$ $\cdot 321.73$ $\cdot 0.29$ $\cdot 7.41$ 35         BOT $\cdot 0.30$ $\cdot 2.20$ $\cdot 321.66$ $-4.16$ $2.22$ 35         BOT $\cdot 0.10$ $\cdot 0.20$ $\cdot 321.65$ $\cdot 7.13$ $t.007$ 35         BOT $\cdot 1.01$ $\cdot 0.20$ <	الى ئەتىيە بىيەت بىيەر بىرىغىن بىيەر بىيە بىيەر بى يىلى					
35(3) 35       TOP       2.62       -3.11       -386.07       -12.23       -8.80         35       BOT       -2.62       3.11       -386.07       -6.44       -6.90         35(4) 35       TOP       -0.09       -2.69       -386.00       -11.01       -1.25         35       BOT       0.80       -0.29       -384.89       -4.07       0.86         35       BOT       0.80       0.29       -384.89       -2.35       3.93         35(6) 35       TOP       3.32       -5.51       -387.18       -19.16       -10.91         35       BOT       -2.41       -2.63       -321.73       -10.29       -7.97         35       BOT       -2.41       -2.63       -321.66       -4.16       2.22         35(8) 35       TOP       -3.0       -2.20       -321.66       -4.16       2.22         35(9) 35       TOP       -1.01       0.20       -320.55       3.31       4.36         35(10) 35       TOP       3.11       -5.03       -322.85       -17.23       -10.07         36       BOT       0.16       -3.44       -398.15       -13.77       0.70         36       BOT	35 BOT	-1.15 °	2.62 -346.51	-5.22	-2.32	
35       BOT $-2.62$ $3.11$ $-386.07$ $-6.44$ $-6.90$ $35(4)$ $35$ TOP $-0.09$ $-2.69$ $-386.00$ $-11.01$ $-1.25$ $35$ BOT $0.09$ $2.69$ $-386.00$ $-5.12$ $1.79$ $35(5)$ $35$ TOP $0.80$ $0.29$ $-384.89$ $2.35$ $3.93$ $35(6)$ $35$ TOP $3.32$ $-5.51$ $-387.18$ $-19.16$ $-10.91$ $35$ BOT $-3.32$ $5.51$ $-387.18$ $-13.91$ $-9.04$ $35(7)$ $35$ TOP $2.41$ $2.63$ $-321.73$ $-5.48$ $-6.48$ $35(8)$ $35$ TOP $-0.30$ $-2.20$ $-321.66$ $-9.07$ $-0.41$ $35$ BOT $0.30$ $2.20$ $-321.55$ $3.31$ $4.36$ $35(9)$ $35$ TOP $1.01$ $-0.20$ $-322.85$ $-17.23$ $-10.07$ $35$ BOT $0.16$ $-3.44$ $-398.15$ $-13.77$ $0.70$ $36$ BOT $0.14$						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	35 BOT	-2.62	3.11 -386.07	-6.44	-6.90	
35         BOT         0.09 $2.69$ $-386.00$ $-5.12$ $1.79$ $35(5)$ $35$ TOP $-0.80$ $-0.29$ $-384.89$ $-4.07$ $0.86$ $35$ BOT $0.80$ $0.29$ $-384.89$ $2.35$ $3.93$ $35(6)$ $35$ TOP $3.32$ $-5.51$ $-387.18$ $-19.01$ $-9.04$ $35$ BOT $-3.32$ $5.51$ $-387.18$ $-19.01$ $-9.04$ $35$ BOT $-2.41$ $-2.63$ $-321.73$ $-5.48$ $-6.48$ $35(8)$ $35$ TOP $-0.30$ $-2.20$ $-321.66$ $-9.07$ $-0.41$ $35$ BOT $1.01$ $-0.20$ $-320.55$ $-2.13$ $1.69$ $35$ BOT $1.01$ $-0.20$ $-322.85$ $-17.23$ $+10.07$ $35$ BOT $0.16$ $-3.44$ $-398.15$ $-13.77$ $0.70$ $36$ BOT $0.14$ $2.92$ $-338.05$ $-11$	35(4)35 TOP	-0.09	-2.69 -386.00	-11.01	-1.25	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	35 BOT	0.09	2.69 -386.00	-5.12	1.79	
35         BOT         0.80         0.29 $-384.89$ 2.35 $3.93$ 35(6) 35         TOP $3.32$ $-5.51$ $-387.18$ $-19.16$ $-10.91$ 35         BOT $-3.32$ $5.51$ $-387.18$ $-13.91$ $-9.04$ 35(7) 35         TOP $2.41$ $-2.63$ $-321.73$ $-10.29$ $-7.97$ 35         BOT $-2.41$ $2.63$ $-321.73$ $-5.48$ $-6.48$ 35(8) 35         TOP $-0.30$ $-2.20$ $-321.66$ $-9.07$ $-0.41$ 35         BOT $-0.10$ $0.20$ $-320.55$ $-3.13$ $4.36$ 35(10) 35         TOP $3.11$ $-5.03$ $-322.85$ $-17.23$ $-10.07$ $36$ BOT $0.16$ $-3.44$ $-398.15$ $-13.77$ $0.70$ $36(2)$ 36         TOP $-0.16$ $-3.44$ $-398.15$ $-13.77$ $0.70$ $36$ AOT $-1.17$ $-3.58$ $-376.76$						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						
35       BOT $-3.32$ $5.51$ $-387.18$ $-13.91$ $-9.04$ $35(7)$ 35       TOP $2.41$ $-2.63$ $-321.73$ $-10.29$ $-7.97$ $35$ BOT $-2.41$ $2.63$ $-321.73$ $-5.48$ $-6.48$ $35(8)$ 35       TOP $-0.30$ $-2.20$ $-321.66$ $-9.07$ $-0.41$ $35$ BOT $0.30$ $-2.20$ $-321.66$ $-4.16$ $2.22$ $35(9)$ 35       TOP $-1.01$ $0.20$ $-320.55$ $-2.13$ $1.69$ $35$ BOT $1.01$ $-0.20$ $-320.55$ $-2.13$ $1.69$ $35$ BOT $3.11$ $-5.03$ $-322.85$ $-17.23$ $-10.07$ $36$ BOT $-3.11$ $5.03$ $-322.85$ $-12.99$ $-8.61$ $$	35(6)35 TOP	3.32	-5.51 -387.18	-19.16	-10.91	
35         BOT         -2.41         2.63         -321.73         -5.48         -6.48           35(8) 35         TOP         -0.30         -2.20         -321.66         -9.07         -0.41           35         BOT         0.30         2.20         -321.66         -4.16         2.22           35(9) 35         TOP         -1.01         0.20         -320.55         -2.13         1.69           35         BOT         1.01         -0.20         -322.85         -17.23         -10.07           35         BOT         -3.11         5.03         -322.85         -17.23         -10.07           35         BOT         -3.11         5.03         -322.85         -17.23         -10.07           36         BOT         0.16         -3.44         -398.15         -13.77         0.70           36         BOT         0.14         -2.92         -338.05         -11.71         0.60           36(3) 36         TOP         -1.17         -3.58         -376.76         -7.53         -4.03           36(4) 36         TOP         -1.48         -2.89         -376.65         -11.96         4.32           36         BOT         1.48						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	35(7)35 TOP	2.41	-2.63 -321.73	-10.29	-7.97	
35BOT $0.30$ $2.20$ $-321.66$ $-4.16$ $2.22$ $35(9)$ 35TOP $-1.01$ $0.20$ $-320.55$ $-2.13$ $1.69$ $35$ BOT $1.01$ $-0.20$ $-320.55$ $3.31$ $4.36$ $35(10)$ 35TOP $3.11$ $-5.03$ $-322.85$ $-17.23$ $-10.07$ $35$ BOT $-3.11$ $5.03$ $-322.85$ $-12.95$ $-8.61$ $$	35 BOT	-2.41	2.63 -321.73	-5.48	-6.48	-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
35BOT $1.01$ $-0.20$ $-320.55$ $3.31$ $4.36$ 35(10) 35TOP $3.11$ $-5.03$ $-322.85$ $-17.23$ $-10.07$ 35BOT $-3.11$ $5.03$ $-322.85$ $-12.95$ $-8.61$	35 BOT	0.30	2.20 -321.66	-4.16	2.22	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						
35BOT $-3.11$ $5.03$ $-322.85$ $-12.95$ $-8.61$ 36(1) 36TOP $0.16$ $-3.44$ $-398.15$ $-13.77$ $0.70$ 36BOT $0.16$ $3.44$ $-398.15$ $-6.85$ $0.27$ 36(2) 36TOP $-0.14$ $-2.92$ $-338.05$ $-11.71$ $0.60$ 36BOT $0.14$ $2.92$ $-338.05$ $-5.82$ $0.23$ 36(3) 36TOP $1.17$ $-3.58$ $-376.76$ $-13.97$ $-2.99$ 36BOT $-1.17$ $3.58$ $-376.65$ $-11.96$ $4.32$ 36BOT $-1.48$ $-2.89$ $-376.65$ $-5.37$ $4.55$ 36(5) 36TOP $-2.05$ $0.92$ $-375.91$ $-0.98$ $5.87$ 36BOT $2.05$ $-0.92$ $-375.91$ $-6.48$ $6.41$ 36(6) 36TOP $1.74$ $-7.39$ $-377.50$ $-24.96$ $-4.55$ 36BOT $-1.74$ $7.39$ $-377.50$ $-19.38$ $-5.89$ 36(7) 36TOP $1.20$ $3.04$ $-313.97$ $-11.81$ $-3.10$ 36BOT $1.45$ $2.35$ $-313.87$ $-9.80$ $4.21$ 36BOT $1.45$ $2.35$ $-313.87$ $-4.29$ $4.51$ 36(9) 36TOP $2.02$ $1.46$ $-313.12$ $1.18$ $5.76$ 36BOT $2.02$ $1.46$ $-313.12$ $7.56$ $6.37$ 36(10) 36TOP $1.77$ $-6.85$ $-314.72$ <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td></t<>						
36(1) 36 TOP $0.16$ $3.44$ $-398.15$ $-13.77$ $0.70$ $36$ BOT $0.16$ $3.44$ $-398.15$ $-6.85$ $0.27$ $36(2) 36$ TOP $-0.14$ $2.92$ $-338.05$ $-11.71$ $0.60$ $36$ BOT $0.14$ $2.92$ $-338.05$ $-5.82$ $0.23$ $36(3) 36$ TOP $1.17$ $-3.58$ $-376.76$ $-13.97$ $-2.99$ $36$ BOT $-1.17$ $3.58$ $-376.76$ $-7.53$ $-4.03$ $36(4) 36$ TOP $-1.17$ $3.58$ $-376.76$ $-7.53$ $-4.03$ $36(4) 36$ TOP $-1.48$ $2.89$ $-376.65$ $-5.37$ $4.55$ $36(5) 36$ TOP $-2.05$ $0.92$ $-375.91$ $-0.98$ $5.87$ $36$ BOT $2.05$ $-0.92$ $-375.91$ $-0.98$ $5.87$ $36$ BOT $2.05$ $-0.92$ $-377.50$ $-24.96$ $-4.55$ $36$ BOT $-1.74$ $7.39$ $-377.50$ $-19.38$ $-5.89$ $36(7) 36$ TOP $1.20$ $-3.04$ $-313.97$ $-11.81$ $-3.10$ $36$ BOT $-1.20$ $3.04$ $-313.97$ $-11.81$ $-3.10$ $36$ BOT $1.45$ $2.35$ $-313.87$ $-9.80$ $4.21$ $36$ BOT $2.02$ $1.46$ $-313.12$ $1.18$ $5.76$ $36$ BOT $2.02$ $1.46$ $-313.12$ $1.81$ $-5.94$ $36$ BOT $2.02$ $1.46$ $-313.12$ $-1.81$ $-5.94$ $36$ BOT $2.02$ $-1.46$ $-313.12$ $-18.3$						
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36(10) 36 TOP       1.77       -6.85       -314.72       -22.80       -4.66         36 BOT       -1.77       6.85       -314.72       -18.31       -5.94						
36         BOT         -1.77         6.85         -314.72         -18.31         -5.94           37(1) 37         TOP         0.07         -3.45         -399.76         -13.81         -0.25           37         BOT         -0.07         3.45         -399.76         -6.87         -0.20           37(2) 37         TOP         0.06         -2.93         -339.42         -11.74         -0.22           37         BOT         -0.06         2.93         -339.42         -5.84         -0.17						
37(1) 37 TOP       0.07       -3.45       -399.76       -13.81       -0.25         37 BOT       -0.07       3.45       -399.76       -6.87       -0.20         37(2) 37 TOP       0.06       -2.93       -339.42       -11.74       -0.22         37 BOT       -0.06       2.93       -339.42       -5.84       -0.17	-					
37(1) 37 TOP       0.07       -3.45       -399.76       -13.81       -0.25         37 BOT       -0.07       3.45       -399.76       -6.87       -0.20         37(2) 37 TOP       0.06       -2.93       -339.42       -11.74       -0.22         37 BOT       -0.06       2.93       -339.42       -5.84       -0.17					-3.94	
37         BOT         -0.07         3.45         -399.76         -6.87         -0.20           37(2) 37         TOP         0.06         -2.93         -339.42         -11.74         -0.22           37         BOT         -0.06         2.93         -339.42         -5.84         -0.17		· 0 07	2 45 200 76	12 81	-0.25	
37(2) 37       TOP       0.06       -2.93       -339.42       -11.74       -0.22         37       BOT       -0.06       2.93       -339.42       -5.84       -0.17						
37 BOT -0.06 2.93 -339.42 -5.84 -0.17						
27/2\27 TOD 1/0 .372 .7274 .1//0 .201						
37(3) 37 TOP 1.40 -3.73 -378.34 -14.40 -3.91	37(3)31 IUP	1.40	-3113 -370,34	-14.40	-3.71	

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37 BOT	-1.40	3.73 -378.34	-7.97	-4,48	
		-2.76 -378.10			
		2.76 -378.10			
		2.45 -376.88			
		-2.45 -376.88			
		-8.95 -379.56			
• •		8.95 -379.56			
		-3.19 -315.30			
		3.19 -315.30			
		-2.22 -315.07			
		2.22 -315.07			
37(9)37 TOP	-1.86	3.00 -313.84	5.62	· 5.11	
37 BOT	1.86	-3.00 -313.84	12.35	6.05	• •
		-8.40 -316.52			
37 BOT	-1.98	8.40 -316.52	-23.13	-6.35	<u>.</u>
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38(1)38 TOP	0.01	-3.45 -399.74	-13.81	0.03	
38 BOT	-0.01	3.45 -399.74	-6.87	-0.06	
		-2.93 -339.40			
38 BOT	-0.01	2.93 -339.40	-5.84	-0.05	
38(3)38 TOP	1.33	-3.86 -378.33	-14.79	-3.65	· · · . ·
38 BOT	-1.33	3.86 -378.33	-8.39	-4.35	
38(4)38 TOP	-1.32	-2.63 -378.06	-11.22	3.70	
		2.63 -378.06			
38(5)38 TOP	-1.91	4.00 -376.54	7.91	5.33	
38 BOT	1.91	-4.00 -376.54	16.09	6.14	
38(6)38 TOP	1,92	-10.49 -379.85	-33.92	-5.27	· · · · ·
		10.49 -379.85			
		-3.32 -315.30			
		3.32 -315.30			
		-2.09 -315.03			
		2.09 -315.03			
		4.54 -313.50			
		-4.54 -313.50			
		-9.95 -316.82			
		9.95 -316.82			
		·····			
		-3.45 -398.37			
		3.45 -398.37			
		-2.93 -338.24			
		2.93 -338.24			
		-4.00 -377.13			
		4.00 -377.13			-
39(4)39 TOP	-1.12	-2.49 -376.70	-10.83	2.87	

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41 BOT	-5.59	-9.45 -258.29	32,15	-8.77
-		-14.31 -266.40		
41 BOT	-8.73	14.31 -266.40	-41.83	-19.78
41(7)41 TOP	7.06	-3.04 -219.79	-11.05	-26.62
		3.04 -219.79		
41(8)41 TOP	4.88	-1.00 -217.45	-5.15	-21.21
41 BOT	-4.88	1.00 -217.45	-0.85	-8.08
41(9)41 TOP	4.40	9.86 -214.56	26.20	-20.01
41 BOT	-4.40	-9.86 -214.56	32.96	-6.39
41(10) 41 TOP	7.54	-13.90 -222.68	•42.39	-27.82
41 BOT	-7.54	· 13.90 ·222.68	-41.03	-17.40
		-2.53 -272.67		
		<b>2.53</b> -272.67		
		-2.14 -230.25		
		2.14 -230.25		
		-3.46 -261.59		
		3.46 -261.59		
		-1.39 -262.99		
		1.39 -262.99		
42( 5) 42 TOP	-8.67	9.59 -260.84	24.98	32.46
		-9.59 -260.84		
42(6)42 TOP	-5.53	-14.45 -263.74	-44.41	24.65
		14.45 -263.74		
42(7)42 TOP	-4.83	-3.06 -217.88	-11.09	21.09
42 BOT	4.83	3.06 -217.88	-7.26	7.90
		-0.98 -219.28		
42 BOT	7.01	0.98 -219.28	-0.81	15.54
42(9)42 TOP	-7.49	10.00 -217.13	26.60	27.70
		-10.00 -217.13		
42(10) 42 TOP	-4.35	-14.04 -220.03	-42.79	19.89
42 BOT	4.35	14.04 -220.03	-41.45	
		*		
•				-4.61
		3.39 -407.22		
				-3.92
				-2.00
				-8.17
				-6.59
		-2.02 -384.70		
				2.16
43( 5) 43 TOP	-0.88	10.37 -381.73	26.37	1.18
				4.09
43(6)43 TOP	3.06	-16.76 -388.74	-51.94	-9.86

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43 BOT	-3.06	16.76 -388.74	-48.59	-8.52
		-3.83 -321.56		
		3.83 -321.56		
		-1.49 -320.50		
		1.49 -320.50		
		10.90 -317.53		
		-10.90 -317.53		
		-16.22 -324.53		
		16.22 -324.53		
44(1)44 TOP	-0.14	-3.45 -398.37	-13.82	0.61
		3.45 -398.37		
44( 2) 44 TOP	-0.12	-2.93 -338.23	-11.75	0.52
44 BOT	0.12	2.93 -338.23	-5.85	0.19
		-4.55 -377.16		
		4.55 -377.16		
44(4)44 TOP	-1.46	-1.94 -376.65	-9.24	4.23
		1.94 -376.65		
		11.86 -373.48		
		-11.86 -373.48		
		-18.36 -380.33		
		18.36 -380.33		
		-4.01 -314.35		
		4.01 -314.35		
		-1.40 -313.83		
		1.40 -313.83		
		12.40 -310.66		
		-12.40 -310.66		
		-17.82 -317.51		
		17.82 -317.51		
	A 07	-3.45 -399.77	_13.87	-0.22
43(1)43 IOF	-0.07	3.45 -399.77	-15.02	-0.18
45 DOI	· 0.07	-2.93 -339.42	-11.75	-0.19
45(2)45 IOI 35 BOT	.0.06	2.93 •339.42	-5.85	-0.16
45(3)45 TOP	1 39	-4.69 -378.57	-17.17	-3.89
45 BOT	-1 39	4.69 -378.57	-10.97	-4.47
		-1.81 -377.89		
		1.81 -377.89		
		13.41 -374.38		
45 BOT	1.85	-13.41 -374.38	45.38	6.03
45(6)45 TOP	1.98	-19.90 -382.07	-61.09	-5.51
		19.90 -382.07		
		-4.15 -315.53		

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45 BOT -	-1.38	4.15 -315.53	-9.89	-4.44
45(8)45 TOP	-1.28	-1.26 -314.85	-6.68	3.50
		1.26 -314.85		
		13.95 -311.34		
		-13.95 -311.34		
45(10) 45 TOP	1.97	-19.36 -319.04	-58.92	-5.47
		19.36 -319.04		-6.34
		-3.45 -399.55		-0.09
		3.45 -399.55		
		-2.93 -339.24		
		2.93 -339.24		
		-4.83 -378.38		
		4,83 -378.38		
		-1.67 -377.66		
		1.67 -377.66		
46(5)46 TOP	-1.88	14.95 <b>-</b> 373.82	39.53	5.21
46 BOT	1.88	-14.95 -373.82	50.19	6.09
46(6)46 TOP	1.95	-21.45 -382.21	-65.56	-5.37
		21.45 -382.21		
		-4.28 -315.38		
46 BOT	-1.35	4.28 -315.38	-10.31	-4.39
46(8)46 TOP	-1.30	-1.13 -314.65	-6.29	3.61
46 BOT	1.30	1.13 -314.65	-0.49	4.21
46(9)46 TOP	-1.89	15.49 -310.82	41.70	5.23
46 BOT	1.89	-15.49 -310.82	51.27	6.11
46(10) 46 TOP	1.94	-20.91 -319.21	-63.39	-5.36
46 BOT	-1.94	20.91 -319.21	-62.06	-6.28
		-3.45 -399.56		0.13
		<b>3.45</b> - <b>399.56</b>		
		-2.93 -339.25		
		2.93 -339.25		
		-4.96 -378.42		
		4.96 -378.42		
				3.56
		1.54 -377.63		
47(5)47 TOP		16.50 -373.48		
• •		-16.50 -373.48		
47 ROT	4 ~ 7	10100 01010		
		-23.00 -382.58	-70.02	-5.41
47(6)47 TOP	1.95			-5.41 -6.32
47( 6) 47 TOP 47 BOT	1.95 -1.95	23.00 -382.58	-67.95	-6.32
47( 6) 47 TOP 47 BOT 47( 7) 47 TOP	1.95 -1.95 1.36	23.00 -382.58	-67.95 -15.79	-6.32 -3.77

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		ومحقوق الارتباع المنافعة والمتركب والارتباع والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمحاد	The second se	
47 BOT	1.30	0.99 -314.63	-0.07	4.19
		17.04 -310.47		
		-17.04 -310.47		
		-22.45 -319.58		
		22.45 -319.58		
			*********	
48(1)48 TOP	0.02	-3.45 -399.71	-13.82	-0.03
48 BOT	-0.02	3.45 -399.71	-6.88	-0.09
48(2)48 TOP	0.02	-2.93 -339.38	-11.75	-0.02
		2.93 -339.38		
		-5.10 -378.59		
48 BOT	-1.35	5.10 -378.59	-12.23	-4.38
48(4)48 TOP	-1.31	-1.40 -377.75	-7.68	3.65
48 BOT	1.31	1.40 -377.75	-0.73	4.22
48(5)48 TOP	-1.90	18.04 -373.27	48.45	5.28
48 BOT	1.90	-18.04 -373.27	59.81	6.12
48(6)48 TOP	1.93	-24.54 -383.07	-74.48	-5.32
48 BOT	-1.93	24.54 -383.07	-72.77	-6.28
48(7)48 TOP	1.34	-4.56 -315.56	-16.18	-3.70
48 BOT	-1.34	4.56 -315.56	-11.15	-4.36
48(8)48 TOP	-1.32	-0.86 -314.72	-5.51	3.66
48 BOT	1.32	0.86 -314.72	2. 0.35	4.23
48(9)48 TOP	1.90	18.58 -310.24	50.62	5.28
48 BOT	1.90	-18.58 -310.24	60.89	6.13
		-24.00 -320.04		
48 BOT	-1.93	24.00 -320.04	-71.69	-6.26
		***		
49(1)49 TOP	0.17	-3.45 -398.73	-13.82	-0.62
		3.45 -398.73		
		-2.93 -338.54		
		2.93 -338.54		
		-5.23 -377.76		
		5.23 -377.76		
		-1.27 -376.76		
		1.27 -376.76		
		19.59 -371.93		
		-19.59 -371.93		
		-26.09 -382.59		
•		:= 26.09 -382.59		
		-4.69 -314.88		
		4.69 -314.88		
		-0.73 -313.88		
		0.73 -313.88		
49(9)49 TOP	-1.78	20.13 -309.05	55.08	4.78

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a second and the second s					
49 BOT	1.78	-20.13 -3	09.05 65.70	5.88	-
49(10) 49 TOP					
			19.71 -76.50		
50(1)50 TOP				3.07	
50 BOT					
50(2)50 TOP	-0.64	-2.90 -345	.02 -11.63	2.61	
50 BOT					:
50(3)50 TOP					
50 BOT					
50(4)50 TOP	-2.07	-1.10 -384	.13 -6.77	6.70	:
			0.18		
50( 5) 50 TOP	-2.68	21.17 -379	.16 57.50	8.42	
50 BOT					
50( 6) 50 TOP					-
· · ·			89.54 -82.33		-
50( 7) 50 TOP					
50 BOT					
50(8)50 TOP					
50 BOT					
50(9)50 TOP					· .
50 BOT					
50(10) 50 TOP					
			25.48 -81.26		
			**************************************		
51(1)51 TOP					
51 BOT	-5.64	2.54 -2	-5.08	-11.25	
51(2)51 TOP	4.81	-2.15 -233	.07 -8.61	-19.27	· ·
51 BOT	-4.81	2.15 -2	-4.30	-9.60	•
51(3)51 TOP	6.32	-4.69 -266	.91 -16.26	-23.68	· . ·
51 BOT					
51(4)51 TOP	4.16	-0.18 -263	.98 -3.25	-18.30	•
51 BOT	-4.16	0.18 -2	63.98 2.15	-6.65	· ·
51(5)51 TOP	3.72	23.50 -25	8.11 65.13	-17.27	t i i
51 BOT	-3.72	-23.50 -2	58.11 75.87	-5.04	
51(6)51 TOP			-84.63		·
51 BOT	-6.76	28.37 -2	-85.60	-15.87	. •
51(7)51 TOP	5.45	-4.28 -222	.67 -14.63	-20.18	
51 BOT	-5.45	4.28 -2	22.67 -11.07	-12.52	:
51(8)51 TOP					
51 BOT					
51(9)51 TOP					
51 BOT					
51(10) 51 TOP					• .

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51 BOT			-228.55		
52(1) 52 TOP					
52 BOT					
52(2) 52 TOP					
52 BOT					
52(3) 52 TOP					
52 BOT					
52(4) 52 TOP					
			-263.69		
52( 5) 52 TOP	-3.83	16.90	-265.83	64.91	10.61
52 BOT					
52(6) 52 TOP	3.68	12.52	-261.34	53.20	-9.88
52 BOT					
52(7) 52 TOP					
52 BOT	-1.45	-12.08	-219.56	23.74	-4.78
52(8) 52 TOP	-1.58	12.44	-219.76	49.69	4.51
52 BOT	1.58	-12.44	-219.76	24.93	4.97
52(9) 52 TOP	-3.82	14.45	-221.90	55.07	10.55
52 BOT	3.82	-14.45	-221.90	31.63	12.38
52(10) 52 TOP	3.69	10.07	-217.41	43.35	-9.94
52 BOT					-12.19
53(1) 53 TOP	0.06		-276.89		-0.17
53 BOT	-0.06	-16.12	-276.89	32.01	-0.16
53(2)53 TOP	0.05	13.71	-234.43	55.05	-0.15
53 BOT	-0.05	-13.71	-234.43	27.22	-0.14
53(3)53 TOP	1.55	14.88	-264.02	60.12	-4.30
53 BOT	-1.55	-14.88	-264.02	29.15	-4.99
53(4) 53 TOP	-1.45	15.47	-264,44	61.70	3.98
53 BOT	1.45	-15.47	-264.44	31.10	4.70
53( 5) 53 TOP	-3.85	18.68	-266.41	70.33	10.66
53 BOT	3.85	-18.68	266.41	41.78	12.42
53(6)53 TOP	3.95	11.66	-262.05	51.50	-10.99
53 BOT	-3.95	-11.66	-262.05	18.47	-12.71
53(7)53 TOP	1.54	12.35	-219.98	49.97	-4.28
53 BOT	-1.54	-12.35	-219.98	24.13	•4.97
53(8)53 TOP	-1.45	12.94	-220.40	51.55	4.01
53 BOT	1.45	-12.94	-220.40	26.08	4.72
53(9)53 TOP					
53 BOT					
53(10) 53 TOP	3.94	9.13	-218.01	41.35	-10.96
			-218.01		-12.69
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		West Comparison of the local data and the local dat			
54(1)54 TOP	0.04	16.14 -276.6	7 64.81	-0.13	
54 BOT					
54(2)54 TOP					
54 BOT					
54(3)54 TOP					
54 BOT					
54(4)54 TOP					
		-15.60 -264			
54( 5) 54 TOP					
54 BOT					
54(6)54 TOP	3.92	10.37 -260.8	2 48.08	-10.85	
54 BOT	-3.92	-10.37 -260.	82 14.17	-12.65	:
54(7)54 TOP	1.53	12.25 -219.7	5 49.73	-4.25	
54 BOT	-1.53	-12.25 -219.	75 23.78	-4.96	2
54(8)54 TOP	-1.47	13.07 -220.2	51.92	4.06	•
54 BOT	1.47	-13.07 -220	.28 26.49	4.75	
54(9) 54 TOP	-3.84	17.48 -223.23	2 63.73	10.64	
54 BOT	3.84	-17.48 -223	.22 41.12	12.42	
54(10) 54 TOP					
54 BOT					
55(1)55 TOP					
55 BOT					
55(2)55 TOP					•
55 BOT					
55(3) 55 TOP					
55 BOT					_
55(4)55 TOP					
		-15.71 -264			
55( 5) 55 TOP					
		-21.31 -268			
55(6)55 TOP					· .
55 BOT					
55(7) 55 TOP					
55 BOT 55(8)55 TOP					
55 BOT					
55 BOT 55(9) 55 TOP					
55 BOT					
-55(10) 55 TOP					
		-6.53 -216.			
		-0.33 -210			
56(1) 56 TOP					
		-16.15 -275.2			
10 101	-0.23	-10.13 *473.	21 32.00	-0.33	

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A section was associated by the main sector in the sector of the sector in the sector of the sector	م¥ماليك. استظر من ا≣ك خديث والي			**************************************	
56(2)56 TOP	0.21	13.73	-233.06	55.14	-0.81
56 BOT	-0.21	-13.73	-233.06	27.27	-0.47
56(3)56 TOP					
56 BOT					
56(4)56 TOP					
_ 56 BOT	1.26	-15.83	-263.06	32.28	4.32
56( 5) 56 TOP					
56 BOT	3.63	-22.63	-267.47	· 54.83	11.98
56(6)56 TOP					
56 BOT					
56(7)56 TOP					
56 BOT	-1.69	-12.03	-218.53	23.02	-5.27
56(8) 56 TOP					
56 BOT					
56(9) 56 TOP					
56 BOT	3.66	-20.09	-223.69	49.81	12.06
56(10) 56 TOP	4,06	5.23	-214.12	30.92	-11.44
56 BOT					
57(1)57 TOP					
57 BOT					
57(2) 57 TOP					
57 BOT					
57(3)57 TOP					
57 BOT					
57(4)57 TOP					
57 BOT					
57( 5) 57 TOP					
57 BOT					
57(6)57 TOP					
57 BOT					
57(7) 57 TOP	0.51	11.76	-226.77	48.21	-0.13
57 BOT	-0.51	-11.76	-226.77	22.34	-2.92
57(8) 57 TOP					
					6.96
57(9)57 TOP					
-					14.77
57(10) 57 TOP					
					-10.72
					· ·
58(1)58 TOP	8.71	11.80	-170.99	47.40	-34.91
					-17.35
58(2)58 TOP					
					-14.71

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		and a second			and the second
58(3)58 TOP	9.51	10.44 -165.58	43.07	-36.26	
58 BOT	-9.51	-10.44 -165.58	19.56	-20.81	
58(4) 58 TOP	7.05	12.19 -164.56	47.78	-30.13	
		-12.19 -164.56			
		21.39 -168.94			
		-21.39 -168.94			
		1.24 -161.20			
		-1.24 -161.20			
		8.55 -138.07			
		-8.55 -138.07			
		10.30 -137.05			
		-10.30 -137.05			÷
		19.50 -141.43			
		-19.50 -141.43			-
		-0.65 -133.69			
		0.65 -133.69			
58 BU1	-10.10	0.03 -133.09	*14.09	-24.73	
20( 1) 60 TOD	0 2 1	1191 170 02	47.40	21 71	
		11.81 -170.93			
		-11.81 -170.93			
• •		9.98 -144.17			
		-9.98 -144.17			
		10.45 -163.36			
		-10.45 -163.36			
• •		12.18 -166.67			
		-12.18 -166.67			
		21.44 -174.49			
		-21.44 -174.49			
		1.19 -155.55			
59 BOT		-1.19 -155.55			
		8.56 -135.86			
		-8.56 -135.86			
		10.29 -139.17			
		-10.29 -139.17			
59( 9) 59 TOP	-10.05	19.55 -146.98	64.95	35.56	:
		-19.55 -146.98			
59(10) 59 TOP	-3.65	-0.70 -128.05	10.76	19.51	-
59 BOT	3.65	0.70 -128.05	-14.94	2.39	
		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			
60(1)60 TOP	1.39	15.94 -286.22	64.01	-5,52	
60 BOT	-1.39	-15.94 -286.22	31.65	-2.81	
60(2)60 TOP	1.18	13.56 -242.35	54.43	4.68	. ·
60 BOT	-1.18	-13.56 -242.35	26.92	-2.38	
60(3)60 TOP	2.86	14.02 -272.74	57.59	-9.57	:
		-14.02 -272.74			

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					0.02
60(4)60 TOP					
60 BOT	0.23	-16.00	-273.45	33.08	2.27
60(5)60 TOP					
60 BOT					
60( 6) 60 TOP					
60 BOT					
60(7)60 TOP					
60 BOT	-2.64	-11.51	-227.23	21.54	-7.16
60( 8) 60 TOP	-0.44	13.50	-227.93	52.87	-0.05
60 BOT	0.44	-13.50	-227.93	28.12	2.72
60(9)60 TOP	-2.89	23.98	-234.40	80.96	6.81
60 BOT					
60(10) 60 TOP					
60 BOT					
61(1)61 TOP					0.74
61 BOT					
61(2)61 TOP					
61 BOT					
61(3)61 TOP					
61 BOT					
61(4)61 TOP					
61 BOT					
61(5)61 TOP :					
61 BOT					
61(6)61 TOP					
				-12.23	
61(7)61 TOP					
61 BOT					
61(8)61 TOP					
61 BOT					
61(9)61 TOP					
61 BOT					
61(10) 61 TOP					
				-17.26	-12.20
					0.00
62(1)62 TOP					
62 BOT					
62(2)62 TOP		-			
62 BOT					
62(3)62 TOP				-	
62 BOT	-1.57	-13.97			-5.03
62(4)62 TOP					3.93 4.67

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an a		-	and which the last strength in the			
62( 5) 62 TOP	-3.81	29.26	-273.57	98.71	10.53	
62 BOT						
62(6)62 TOP						
62 BOT						
62(7)62 TOP						
62 BOT						
62(8)62 TOP						
62 BOT						
62(9)62 TOP						
62 BOT						
62(10) 62 TOP						
62 BOT						
				-21.00		. <u>.</u> .
63(1)63 TOP						·
63 BOT						
63(2)63 TOP						
63 BOT						-
63(3)63 TOP						-
63 BOT						
63(4)63 TOP						
63 BOT						
63(5)63 TOP						
63 BOT						
63(6)63 TOP						
63 BOT						
63(7)63 TOP	1 53	11 22	-233.00	-20.91	-12.03	
63 BOT	-1.53	-11.32	•219.1J	47.25	-4.21	
63(8)63 TOP						
63 BOT	1.47	12.99	-220.92	54.39 29.55	4.09	
63(9)63 TOP	.3.85	-13,99 20 04	-220.92	29.55	4.76	
63(9)63 TOP 63 BOT	-J.0J 2.95	20.04	-230.19	92.05	10.68	
63(10) 63 TOP 63 BOT	-2.90	-2.13	-209.85	9.59	-10.81	
63 BOT						
64(1)64 TOP	0.05	10.14	-276.70	64.80	-0.13	
64 BOT	-0.05	-10.14	-276.70	32.04	-0.14	
64(2)64 TOP	0.04	13.73	-234.27	55.12	-0.11	
64 BOT	• •0.04	-13.73	-234.27	27.25	-0.12	
64(3)64 TOP	1.54	13.74	-263.09	57.10	['] -4.27	
64 BOT	-1.54	-13.74	-263.09	25.35	-4.98	· .
64(4)64 TOP	-1.46	16.64	265.00	64.86	4.03	· · · · · · · · · · · · · · · · · · ·
64 BOT	1.46	-16.64	-265.00	34.96	4.72	
64( 5) 64 TOP						• • •
64 BOT	3.84	-31.88	-275.06	85.55	12.40	-

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and the second			and a subgroup of the subscription of the subs	فسيستحربه تناقيت بوتين مستوقع	
64(6)64 TOP	3.92	-1.50	-253.03	16.25	-10.87
64 BOT					
64(7)64 TOP					
64 BOT		-			
64(8)64 TOP					
64 BOT					
64(9)64 TOP					
64 BOT					
64(10) 64 TOP					
64 BOT					
			-209.02	-50,28	-12.04
65(1)65 TOP	0.01	16.14	-276.93	64.80	0.01
65 BOT	-0.01	-16.14	-276.93	32.04	-0.07
65(2)65 TOP	0.01	13.73	-234.47	55.11	0.01
65 BOT	-0.01	-13.73	-234.47	27.25	-0.06
65(3)65 TOP					
65 BOT	-1.51	-13.63	-263.23	24.96	-4.92
65(4)65 TOP					
65 BOT	1.49	-16.75	-265.30	35.33	4.79
65(5)65 TOP					
65 BOT					
65(6)65 TOP	3.89	-2.81	-252.37	12.74	-10.75
65 BOT					
65(7)65 TOP	- 1.51	11.09	-219.18	46.63	-4.15
65 BOT					
65(8)65 TOP	-1.49	14.22	-221.26	55.00	4.16
65 BOT					
65(9)65 TOP					
	3.87				
65(10) 65 TOP					
65 BOT					
66(1)66 TOP					-0.86
66 BOT					
66(2)66 TOP					
66 BOT					
66(3)66 TOP					
66 BOT					
66(4)66 TOP					
66 BOT					
66( 5) 66 TOP					
66 BOT					
66( 6) 66 TOP					
66 BOT		-	-		

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	66(7)66 TOP	1.67	10.99	-217.97	46.35	-4.80	
	66 BOT						
	66(8)66 TOP						
	66 BOT						
	66(9)66 TOP						
	66 BOT						
	66(10) 66 TOP						
	66 BOT						
	67(1)67 TOP	-1.15	16.05	-285.73	64.45	4.68	
	67 BOT	1.15	-16.05	-285.73	31.87	2.24	
	67(2)67 TOP						-
	67 BOT	0.98	-13.65	-241.93	27.10	1.90	
	67(3)67 TOP	0.44	13.32	-271.14	55.88	0.13	
	67 BOT						· .
	67(4)67 TOP	-2.64	16.90	-274.08	65.46	8.77	·:
	67 BOT	2.64	-16.90	-274.08	35.94	7.07	
	67(5)67 TOP	-5.06	35.72	-286.81	115.90	15.54	
	67 BOT					_	
	67(6)67 TOP						· .
	67 BOT	-2.87	5.49	-258.41	-38.41	-10.56	
	67(7)67 TOP						
	67 BOT						÷ .
	67(8)67 TOP						
	67 BOT						·
	67(9)67 TOP				•		
	67 BOT						
	67(10)67 TOP						
					-43.41		
			*			• .	
	68(1)68 TOP	7.83	11.93	-172.37	47.89	-31.39	
	68 BOT	-7.83	-11.93	-172.37	23.67	-15.61	-
	68(2)68 TOP	6.64	10.08	-145.39	40.50	-26.62	·. ·
	68 BOT	-6.64	-10.08	-145.39	20.01	-13.24	
	68(3)68 TOP	8.68	9.51	-166.20	40.74	-32.92	
	68 BOT	-8.68	-9.51	-166.20	16.34	-19.16	
	68(4)68 TOP	6.20	13.34	-166.58	51.03	-26.69	5 <b>1</b> 2
	68 BOT	-6.20	-13.34	-166.58	29.02	-10.48	: •
	68(5)68 TOP						
	68 BOT	-4.10	-33.38	-178.24	95.50		
	68(6)68 TOP						
	68 BOT						
	68(7)68 TOP						
	68 BOT						

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68( 8) 68	TOP	4.96	11.44	-138.8	5 43	3.38	-21.72	
• •	BOT							
	ТОР							
• •	BOT							•
68(10) 68	ТОР	9.54	-12.43	-126.8	l -20	).64	-33.43	
	вот					-	-23.81	
W(TYPE)	ND	V-X	v	-Y	=N=		м-х	М-Ү
1( 1) 69	тор	•9.10	13.61	-791.16	282	2.17	55.81	
69	BOT	9.10	-13.6	1 -791.	16 -2	00.49	-1.19	)
N(I1-I2)	M-T	N-T -	V-T ·	M-	B N	I-B	V-B	
1( 4- 2)	104.6	58 -48	7.70	13.34	-100	).55	-525.47	-13.34
2(1-3)	-15.0	<b>9 -20</b> 4	1.44	8.47	-0	.28	-170.80	-8.45
3(2-5)	3.9		9.01	-1.03	-0	.72	-94.88	1.05
1( 2) 69	тор		11.47	-662.94	239	9.27	47.35	
69	BOT	7.68	-11.4	7 -662.	94 -1	70.45	-1.26	5
N(I1-I2)	M-T -	N-T -	V-T ·	M-	B N	-B	V-B	
	87.8							
2(1-3)	-12.8	9 -171	.94	7.20	-0	.22	-143.39	-7.18
3(2-5)	3.2	2 -8	2.70	-0.81	-0	.67	-79.46	0.83
1( 3) 69	TOP 3	92.74	37.47	-371.0	3 28	0.95	-1037.15	
69	BOT	-392.74	-37.47	-371.0	08 -	56.14	-1319.30	
N(I1-I2)	M-T	N-T -	• V-T ·	M-	B N		V-B	
1(4-2)	206.9	3 -992	2.97	48.85	- 172	2.39	696.24	-48.85
2(1-3)	232.6	5 33	7.39 -2	260.93	306	5.62	-641.56	261.00
3(2-5)	-113.8	6 284	4.50	130.56	-135	5.22	•425.75	-130.43
• •	TOP -4							
	BOT							5
	M-T							~~ ~~
	-1.9							
	-260.6							
3(2-5)	121.8	-48	1.22 -1	32.91	134	.29	238.70	132.80
	TOP -7:							_
	• ВОТ М-Т							7
								648.07
1(4-2)	840.5	/ 30	4./9 -0	J TO.V /	-170			
1(4-2) 2(1-3)	840.3 -308.3							

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1(6) 69 TOP 740.57 652.71 -49.49 1645.82 -1952.97	
69 BOT -740.57 -652.71 -49.49 2270.41 -2490.43	÷ .
N(11-12) M-T N-T V-T M-B N-B V-B	
1(4-2) -641.43 -1527.32 673.92 9.76 1826.63 -673.92	
2(1-3) 280.31 472.34 -322.26 432.83 -702.11 322.87	
3(2-5) -358.76 1005.49 399.06 -388.21 -1174.00 -398.45	
1(7) 69 TOP 394.20 35.27 -241.30 236.29 -1045.97	
69 BOT -394.20 -35.27 -241.30 -24.66 -1319.26	
N(11-I2) M-T V-T M-B V-B	-
1(4-2) 189.85 -912.76 46.69 187.98 782.56 -46.69	
2(1-3) 234.99 370.56 -262.26 306.67 -613.70 262.39	
3(2-5) -114.52 300.90 130.76 -135.14 -410.17 -130.63	
	-
t(8) 69 TOP -408.82 -13.30 -1056.49 210.41 1134.15	
69 BOT 408.82 13.30 -1056.49 -290.21 1318.80	
N(II-I2) M-T N-T V-T M-B V-B	
1(4-2) -19.07 110.66 -25.16 -343.91 -1645.80 25.16	
2(1-3) -258.33 -702.32 275.55 -307.21 335.03 -275.66	·
3(2-5) 121.14 -464.83 -132.71 134.36 254.28 132.61	
•	
1(9)69 TOP -756.65 -628.54 -1378.08 -1154.46 2049.96	
1( 9) 69 TOP -756.65 -628.54 -1378.08 -1154.46 2049.96 69 BOT 756.65 628.54 -1378.08 -2616.76 2489.92	
69 BOT 756.65 628.54 -1378.08 -2616.76 2489.92	
69 BOT 756.65 628.54 -1378.08 -2616.76 2489.92 N(I1-I2) M-T V-T M-B N-B V-B	
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(11-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63	
69         BOT         756.65         628.54         -1378.08         -2616.76         2489.92           N(I1-I2)         M-T         N-T         V-T         M-B         N-B         V-B            1(4-2)         829.29         645.00         -650.23         -181.29         -2776.20         650.23           2(1-3)         -305.98         -837.27         336.88         -433.42         395.58         -337.47           3(2-5)         366.04         -1185.81         -401.21         387.36         1002.54         400.63	
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(11-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63         1(10) 69       TOP       742.03       650.51       80.29       1601.15       -1961.79	
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(11-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63         1(10)       69       TOP       742.03       650.51       80.29       1601.15       -1961.79         69       BOT       -742.03       -650.51       80.29       2301.89       -2490.38	
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(11-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63         1(10)       69       TOP       742.03       650.51       80.29       1601.15       -1961.79         69       BOT       -742.03       -650.51       80.29       2301.89       -2490.38         N(I1-12)       M-T       N-T       W-T       M-B       N-B       V-B	•
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(11-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63         1(10)       69       TOP       742.03       650.51       80.29       1601.15       -1961.79         69       BOT       -742.03       -650.51       80.29       2301.89       -2490.38         N(11-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       -658.51       -1447.11       671.76       25.36       1912.96       -671.76	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(11-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63         1(10)       69       TOP       742.03       650.51       80.29       1601.15       -1961.79         69       BOT       -742.03       -650.51       80.29       2301.89       -2490.38         N(11-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       -658.51       -1447.11       671.76       25.36       1912.96       -671.76	•
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(11-12)       M-T       N-T       W-T       M-B       N-B       V-B          1(4-2)       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63         1(10) 69       TOP       742.03       650.51       80.29       1601.15       -1961.79         69       BOT       -742.03       -650.51       80.29       2301.89       -2490.38         N(11-12)       M-T       N-T       V-T       M-B       V-B          1(4-2)       -658.51       -1447.11       671.76       25.36       1912.96       -671.76         2(1-3)       282.64       505.51       -323.59       432.89       -674.25       324.19         3(2-5)       -359.42       1021.88       399.26       -388.14       -1158.42       -398.65	•
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(11-12) M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63         I(10) 69       TOP       742.03       650.51       80.29       1601.15       -1961.79         69       BOT       -742.03       -650.51       80.29       2301.89       -2490.38         N(11-12)       M-T       N-T       V-T       M-B       V-B          1(4-2)       -658.51       -1447.11       671.76       25.36       1912.96       -671.76         2(1-3)       282.64       505.51       -323.59       432.89       -674.25       324.19         3(2-5)       -359.42       1021.88       399.26       -388.14       -1158.42       -398.65	•
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(I1-12)       M-T       N-T       V-T       M-B       N-B       V-B         1(4-2)       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63         I(10) 69       TOP       742.03       650.51       80.29       2301.89       -2490.38         N(I1-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(10) 69       TOP       742.03       650.51       80.29       2301.89       -2490.38         N(I1-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       -658.51       -1447.11       671.76       25.36       1912.96       -671.76         2(1-3)       282.64       505.51       -323.59       432.89       -674.25       324.19         3(2-5)       -359.42       1021.88       399.26       -388.14	•
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(I1-12)       M-T       N-T       W-T       M-B       N-B       V-B          1{4-2}       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63         1(10) 69       TOP       742.03       650.51       80.29       1601.15       -1961.79         69       BOT       -742.03       -650.51       80.29       2301.89       -2490.38         N(I1-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       -658.51       -1447.11       671.76       25.36       1912.96       -671.76         2(1-3)       282.64       505.51       -323.59       432.89       -674.25       324.19         3(2-5)       -359.42       1021.88       399.26       -388.14       -1158.42       -398.65	
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(11-12)       M-T       N-T       W-T       M-B       N-B       W-B          1(4-2)       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63         I(10) 69       TOP       742.03       650.51       80.29       1601.15       -1961.79         69       BOT       -742.03       -650.51       80.29       2301.89       -2490.38         N(11-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       -658.51       -1447.11       671.76       25.36       1912.96       -671.76         2(1-3)       282.64       505.51       -323.59       432.89       -674.25       324.19         3(2-5)       -359.42       1021.88       399.26       -388.14       -1158.42       -398.65	•
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(11-12)       M-T       N-T       W-T       M-B       N-B       V-B          1(4-2)       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63         1(10) 69       TOP       742.03       650.51       80.29       1601.15       -1961.79         69       BOT       -742.03       -650.51       80.29       2301.89       -2490.38         N(11-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       -658.51       -1447.11       671.76       25.36       1912.96       -671.76         2(1-3)       282.64       505.51       -323.59       432.89       -674.25       324.19         3(2-5)       -359.42       1021.88       399.26       -388.14       -1158.42       -398.65         70       BOT       -61.62       33.74       -1191	•
69       BOT       756.65       628.54       -1378.08       -2616.76       2489.92         N(11-12)       M-T       N-T       W-T       M-B       N-B       W-B          1(4-2)       829.29       645.00       -650.23       -181.29       -2776.20       650.23         2(1-3)       -305.98       -837.27       336.88       -433.42       395.58       -337.47         3(2-5)       366.04       -1185.81       -401.21       387.36       1002.54       400.63         I(10) 69       TOP       742.03       650.51       80.29       1601.15       -1961.79         69       BOT       -742.03       -650.51       80.29       2301.89       -2490.38         N(11-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(4-2)       -658.51       -1447.11       671.76       25.36       1912.96       -671.76         2(1-3)       282.64       505.51       -323.59       432.89       -674.25       324.19         3(2-5)       -359.42       1021.88       399.26       -388.14       -1158.42       -398.65	•

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				-401.94		
				40 229.12		8
				B N-B		
				-27.93		
				71.53		
3(2-5)	2.47	-232.92	14.74	-4.79	-150.87	-14.75
4( 7- 6)	-5.84	-92.48	-1.35	-1.86	-97.85	1.35
•.	• .					
2(3)70 T	OP 457.8	88 1012.	.80 -1428.34	4 178.90	-1165.83	
				34 5897.92		
				B N-B		
1(4-2)	-337.25	-256.00	-70.91	-244.56	-1515.77	70.85
2(1-3)	292.85	-404.66	-1021.16	1526.89	-226.05	1021.29
3(2-5)	-53.91	-522.93	88.78	-135.03	-197.40	-88.65
4( 7- 6)	7.15	-244.75	12.22	8.62	510.88	-12.16
	•	:				
				-1039.20		
70	BOT 34	2.61 10	75.55 -890	.99 -5414.10	) 1346.6	50
				·B N-B		
1( 4- 2)	140.10	-550.01	-56.34	183.16	670.36	56.40
2(1-3)	-351.41	-358.59	1070.15	-1374.14	-666.45	-1070.29
				124.75		
4( 7- 6)	-19.83	24.30	-15.15	-12.65	-742.83	15.09
	· · · · ·		10 1639 60	) <u>376 20</u>	020 02	
				) 376.39		)K
				.50 8606.2		
				·B N·B 626.85		
				1402.44		
				138.56		
4(7-6)	-170.65	-214.43	-44.24	-156.98	005.00	44.00
A( () <b>A</b> A T		<i>(</i> ) ( )	0 0 700 0	3 -1236.69	1204 79	
· ·						n
				.83 -8122.40		0
				·B N-B		1165 11
				-688.25		
27 1 21				-1249.68		
	100 14	-746.14	588.59			
3(2-5)			40		00000	
3(2-5)			41.30	152.95	-895.54	-41.07
3( 2- 5) 4( 7- 6)	157.97	-6.03			. • •	
3(2-5) 4(7-6) 2(7)70 T	157.97 OP 448.	-6.03 27 1018	.03 -1235.0	152.95 6 250.59 06 5857.60	-1127.76	

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Calculat	ion book	Oil Car St	orage	<u></u>			
1(4-2)	-320.82	-188.83	-60.31	-239.44	-1445.32	60.25	
	297.73						
• •	-54.33				-168.27		
	8.21				530.21	-12.40	-
	-			-			
	TOP -352.2						
	BOT 35					7 .	
	M-T						
	156.53						
	-346.53						
	58.47						
4(7-6)	-18.77	42.67	-14.91	-12.32	-723.50	14.04	
2(9)70	TOP -491.9	98 1502	.33 -1345.22	2 - 448.08	976.08		
	BOT 49					3	
N(11-12)	M-T	N-T V	/-T M-	B N-B	V-B		
	-8.20					-1048.46	
	5.21						
3(2-5)	204.70	260.65	-358.89	139.41	-1454.53	359.71	
4( 7- 6)	-169.59	-196.06	-44.00	-156.65	682.93	44.35	
70 N(11-12) 1( 4- 2) 2( 1- 3) 3( 2- 5)	TOP 588 BOT -58 M-T -156.09 -54.01 -200.56 159.02	8.04 15 N-T V -34.99 137.10 -702.00	54.62 -587 √-T M· -1154.14 1620.71 385.89	.55 -8162.72 ·B N-B -683.13 -1262.41	2 -2171.5 V-B 505.09 -1379.73 1163.31	1154.50 -1621.54 -386.72	
71 N(11-12) 1( 1- 2)	M-T -329.53 26.29	10.11 - N-T -681.44 -256.64	58.06 -1038 V-T M 58.50	.77 -271.8 -B N-B 60.93 6.00	8 1.0 V•B -657.37	-58.50 5.20	
3(2)71	TOP -8.	61 49	.64 .875.4	3 529.72	50.93		
71			49.64 -875				
	M-T						
	-281.24				-554.04		•
• •	22.42				-215.71		
3(2-4)			1.50				
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3(3)71 TOP 368.93 98.43 -1478.94 1042.80 -972.58
71 BOT -368.93 -98.43 -1478.94 -452.23 -1240.98
N(11·12) M-T N-T V-T M-B N-B V-B
1(1-2) -278.04 -217.97 79.15 443.02 -1810.47 -79.15
2(1-3) -219.64 -788.46 243.14 -298.72 109.36 -243.39
3(2-4) 120.92 -472.52 -130.39 138.19 222.17 130.14
3(.2-4) 120.72 -472.32 -130.39 130.19 222.11 130.07
3(4)71 TOP -387.86 9.02 -531.47 109.32 1083.58
71 BOT 387.86 -9.02 -531.47 -55.19 1243.60
N(I1-I2) M-T N-T V-T M-B N-B V-B
1(1-2) -335.49 -1099.29 29.14 -329.94 538.47 -29.14
2(1-3) 268.71 294.80 -253.30 310.16 -601.95 253.29
3(2-4) -114.67 273.01 133.57 -130.35 -467.99 -133.58
·
3(5)71 TOP -739.06 955.66 -146.55 870.69 2013.23
71 BOT 739.06 -955.66 -146.55 4863.29 2421.12
N(I1-I2) M-T N-T V-T M-B N-B V-B
l(1-2) 458.10 -1605.54 992.74 -1301.41 1598.68 -992.74
2(1-3) 310.62 497.73 -260.51 433.58 -292.77 260.98
3(2-4) -361.85 961.26 427.97 -384.50 -1452.45 -427.50
3(6)71 TOP 720.12 -848.21 -1863.87 281.42 -1902.23
71 BOT -720.12 848.21 -1863.87 -5370.71 -2418.50
N(I1-I2) M-T N-T V-T M-B N-B V-B
1(1-2) -1071.62 288.29 -884.45 1414.49 -2870.68 884.45
2(1-3) -261.55 -991.39 250.35 -422.14 -199.82 -251.08
3(2-4) 368.10 -1160.76 -424.79 392.35 1206.63 424.06
3(7)71 TOP 370.50 89.47 -1311.41 946.79 -981.83
71 BOT -370.50 -89.47 -1311.41 -409.95 -1241.20
N(11-12) M-T N-T V-T M-B N-B V-B
1(1-2) -226.91 -108.20 70.12 433.59 -1704.47 -70.12
2(1-3) -223.73 -747.32 243.99 -299.68 150.41 -244.21
3(2-4) 120.40 -455.89 -130.66 137.54 242.66 130.43
3(8)71 TOP -386.29 0.07 -363.94 13.31 1074.33
71 BOT 386.29 +0.07 -363.94 +12.90 1243.38
N(11-12) M-T N-T V-T M-B V-B
1(1-2) -284.36 -989.52 20.12 -339.36 644.47 -20.12
2(1-3) 264.62 335.94 -252.45 309.21 -560.90 252.46
3(2-4) -115.19 289.64 133.31 -131.00 -447.51 -133.30
2/ 0) 21 TOD 237 48 046 21 20 00 274 68 2002 08
3(9)71 TOP -737.48 946.71 20.99 774.68 2003.98
71 BOT 737.48 -946.71 20.99 4905.57 2420.90

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N(11-12)	M-T• Ì	<b>∤.</b> Ƴ <b>V-</b> T	M·B	N-B	V-B	
	509.22					
	306.53					
	-362.37					
5(2-1)						
3(10) 71 T	OP 721.	-857.17	-1696.33	185.41	-1911.48	
	BOT -721					
	M-T }					
	-1020.49					893.48
2(1-3)	-265.64	-950.25	251.19	-423.09	-158.77	-251.91
3(2-4)	367.58	-1144.14	425.06	391.69	1227.12	424.34
5(2-4)	501100	••••			: -	
wy						,
4(3)72 T	OP -0.7	4 1.01	-162.36	8.23	2.98	
	BOT					
	M•T ]					· .
	-6.16					
	1.39					
2(1-5)	1,55	01110				
4(2)72 T	OP -0.6	3 0.83	-135.37	6.91	2.53	
	BOT					
	M-T					
• •	-5.20					-1.00
•	. 1.18				-48.34	
2(1.5)						-
4(3)72 T	OP 5.:	35 -44.68	-3.22	-100.84	-15.86	
• •	BOT -					
	M-T					
• •	55.16					43.64
	-5.56					
2(1 2)						
4(4)72 T	OP -6.7	5 46.79	-321.04	116.95	21.48	
	вот					
	M-T					
	-67.01					
• •	8.16					
-(				· .		
4(5)72 T	OP 3.	89 -127.3	5 141.87	-342.84	-11.17	-
	BOT •					
	M-T					-
• •	145.34					
	4.90					
<u> </u>	7120	102.88				
.1( 6) 72 T	ЮР -5.2					
4(U) <i>14</i> I	-J.	.7 147.40	· -+vv.12	50.00	10,70	

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72 BOT 5.29 -129.46 -466.12	417.79 14.95
N(11-12) M-T N-T V-T M-B	
1(1-2) -157.19 -536.68 122.79	
2(1-3) -2.30 70.56 41.36	
4(7) 72 TOP 5.46 -44.85 23.80	-102.18 -16.33
72 BOT -5.46 44.85 23.80	
N(I1-I2) M-T N-T V-T M-B	
1(1-2) 56.15 75.04 -43.84	81.64 -91.98 43.84
2(1-3) -5.77 -51.23 -10.94	-3.74 115.78 10.94
4(8)72 TOP -6.63 46.61 -294.02	115.61 21.01
72 BOT 6.63 -46.61 -294.02	
N(11-12) M-T N-T V-T M-B	
1(1-2) -66.02 -249.70 45.90	-82.81 -80.94 -45.90
2(1-3) 7.94 -44.32 10.48	
-(,	
4(9) 72 TOP 4.00 -127.52 168.89	-344.18 -11.63
72 BOT -4.00 127.52 168.89	
N(II-I2) M-T N-T V-T M-B -	
1(1-2) 146.33 344.55 -120.52	
2(1-3) 4.68 -175.66 -41.87	
2(1.5)	
4(10) 72 TOP -5.17 129.28 -439.10	357.61 16.31
72 BOT 5.17 -129.28 -439.10	
N(I1-I2) M-T N-T V-T M-B -	
1(1-2) -156.21 -519.22 122.58	
2(1-3) -2.51 80.11 41.41	
5(1)73 TOP 1.54 -0.23 -306.44	-10.04 -5.71
73 BOT -1.54 0.23 -306.44	
N(I1-I2) M-T N-T V-T M-B -	
1(1-2) -3.67 -192.35 0.16	
2(4-3) -5.71 -114.10 -1.54	
5(2) 73 TOP 1.30 -0.22 -257.13	-8.74 -4.84
73 BOT -1.30 0.22 -257.13	
N(11-12) M-T N-T V-T M-B -	
1(1-2) -3.22 -161.57 0.17	
2(4-3) -4.84 -95.56 -1.31	
	2 · · · · · · · · ·
5(3)73 TOP 4.07 131.80 -73.63	304.57 -16.08
73 BOT -4.07 -131.80 -73.63	

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N(11-12) ----- M-T ----- N-T ----- V-T ------ M-B ----- N-B ----- V-B ----. 224.44 -294.05 131.85 1(1-2) 142.36 110.06 -131.85 -5.66 220.42 -1.73 2(4-3) -14.29 -183.68 1.73 5(4) 73 TOP -1.16 -132.04 -527.19 -322.03 5.26 73 BOT 1.16 132.04 -527.19 -470.19 1.72 N(I1-I2) ----- M-T ----- N-T ----- V-T ------ M-B ----- N-B ----- V-B -----79.17 -131.96 1(1-2) -148.60 -485.99 131.96 -215.99 2(4-3) 3.49 -41.20 -4.64 -0.82 -448.02 4.64 5(5)73 TOP 19.86 -25.57 -254.79 -187.26 -66.91 73 BOT -19.86 25.57 -254.79 33.84 -52.23 N(11-12) ----- M-T ----- N-T ----- V-T ------ M-B ----- N-B ----- V-B ----24.09 -166.53 -24.67 1(1-2) -74.94 -259.09 24.67 -67.27 4.30 -20.96 -51.54 -88.26 20.96 2(4-3) 5(6) 73 TOP -16.95 25.34 -346.02 169.80 56.09 73 BOT 16.95 -25.34 -346.02 -17.79 45.60 · . N(11-12) ----- M-T ----- N-T ----- V-T ----- M-B ----- N-B ----- V-B ----1(1-2) 68.70 -116.84 -24.57 -15.64 -206.69 24.57 45.06 -139.34 56.46 -229.18 18.04 -18.04 2(4-3) 5(7)73 TOP 3.83 131.82 -23.56 306.02 -15.18 73 BOT -3.83 -131.82 -23.56 484.90 -7.80 N(I1-J2) ----- M-T ----- V-T ----- M-B ----- V-B ----- V-B -----142.88 141.38 -131.86 223.74 -262.95 131.86 1(1-2) 2(4-3) -13.39 -164.94 1.97 -5.12 239.39 -1.97 ۰. 5(8)73 TOP -1.41 -132.02 -477.12 -320.57 6.16 73 BOT 1.41 132.02 -477.12 -471.53 2.27 ·; . N(11-12) ----- M-T ----- V-T ----- M-B ----- V-B ----- V-B ----1(1-2) -148.08 -454.66 131.95 -216.70 -48.07 -131.95 2(4-3) 4.39 •22.46 -4.40 -0.28 -429.05 4.40 5(9)73 TOP 19.61 -25.55 -204.72 -185.81 -66.01 73 BOT -19.61 25.55 -204.72 32.50 -51.68 N(11-12) ----- N-T ----- V-T ----- M-B ----- V-B ----- V-B ----23.39 -135.43 -74.42 -227.76 24.66 1(1-2) -24.66 2(4-3) -66.37 23.04 -20.72 -51.00 -69.29 20.72 5(10) 73 TOP -17.19 25.36 -295.96 171.26 56.99 17.19 -25.36 -295.96 -19.12 73 BOT 46.15 N(11-12) ----- M-T ----- N-T ----- V-T ----- M-B ----- N-B ----- V-B ----1(1-2) 69.22 -85.51 -24.58 -16.34 -175.58 24.58

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2( 4- 3)	57.3	36 -210	0.44	18.29	45.60	-120.37	-18.2
6(1)74	тор	0.00	-1.63	-174.18	-5.97	0.06	
74	BOT	0.00	1.63	3 -174.18	-3.79	-0.04	
				M-B -			
1( 3- 2)	-5.9	97 -174	1.18	-1.63	-3.79	-174.18	1.63
				-146.24			
74	BOT	0.00	1.3	8 -146.24	-3.22	-0.03	
· · ·				М-В -			
1(3-2)	-5.(	-140	5.24	-1.38	-3.22	-146.24	1.38
6(3)74	ТОР	0.77	-2.31	-100.72	-11.64	-1.70	
74	BOT	-0.77	2.31	-100.72	-2.22	-2.91	
N(11-12)	M-T ·	N-T ·	V-T -	M·B -	N-B	V-B	
1( 3- 2)	-11.0	54 -10(	).72	-2.31	-2.22	-100.72	2.31
6( 4) 74	тор	-0.77	-0.76	-240.18	0.35	1.80	
74	BOT	0.77	0.7	6 -240.18	-4.92	2 2.84	
N(11-12)	M-T ·	N-T -	V-T -	M-B -	N-B	V-B	
1(3-2)	0.	35 -24	0.18	-0.76	-4.92	-240.18	0.7
6( 5) 74	ТОР	-0.45	-27.07	-206.53	-89.68	1.28	
74	BOT	0.45	27.0	7 -206.53	-72.71	l 1.41	
				······ M·B ·			
l( 3- 2)	-89.0	58 -206	5.53 -7	27.06	-72.71	-206.53	27.00
6( 6) 74	ТОР	0.44	23.99	-134.37	78.39	-1.18	
74	BOT	-0.44	-23.99	-134.37	65.57	-1.48	
· ·				М.В.			
I( 3- 2)	78.	39 <b>-1</b> 3	4.37	23.99	65.57	-134.37	-23.9
6( 7) 74	тор	0.77	-2.05	-72.31	-10.70	-1.71	
74	BOT	-0.77	2.05	-72.31	-1.63	-2.91	
N(11-12)	M-T -	N-T -	V-T -	M-B -	N-B	V•B	•
1(3-2)	-10.1		2.31	-2.05	-1.63	-72.31	2.05
6( 8) 74	ТОР			-211.77	1.29	1.79	
74	BOT	0.77	0.5	-211.77	-4.32	2.85	
N(11-J2)	M-T -	N-T -	V-T -	····· M·B -	N-B	V-B	

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74	BOT	0.45	26.81	-178.12	-72.12	1.42	-
				M•B •			
						-178.12	26.81
				-105.96			
				-105.96			
				M-B			
1(3-2)	7	9.33 -10	15.96	24.25	66.17	-105.96	-24.25
 7(1)75 [/]	гор	-0.01	0.22	-142.55	1.38	0.08	
				-142.55			
N(I1-I2)	M-	Т N•Т	V-T	M-B -	N-B	V-B	
						-142.55	-0.22
-						0.07	-
				-119.73			
• •				M-B -			
1( 3- 2)		1.15 -11	9.73	0.18	-0.05	-119.73	-0.18
7(3)75	ТОР	0.70	1.74	-91.86	6.12	-1.63	
. ,				-91.86			
N(11-12)	M-	T N-T	V-T	M-B -	N-B	V-B	
1( 3- 2)		6.12 -9	91.86	1.74	4.34	-91.86	-1.74
7( 4) 75	тор	-0.73	-1.29	-186.86	-3.37	1.78	
						2.58	
				М.В -			
1( 3- 2)	-	3.37 -18	6.86	-1.29	-4.35	-186.86	1.29
		-		-250.08			• .
						2.70	
				М-В -			
1(3-2)	-4	2.68 -25	5 <b>0.08 -</b> 1	3.49	-38.25	-250.08	13.49
7( 6) 75	TOP	0.74	13.94	-28.64	45.43	-1.75	:
75	BOT	-0.74	-13.94	-28.64	38.24	-2.72	
N(11-12)				М-В -			
1( 3- 2)	4	15.43 -2	28.64	13.95	38.24	-28.64	
						110	
• •						-1.64	
75				-68.64 - M-B		-2.60	

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7(8) 75 TOP -0.72 -1.32 -163.64 -3.60 1.76	
75 BOT 0.72 1.32 -163.64 -4.35 2.58	
N(11-12) M-T N-T V-T M-B N-B V-B	
1(3-2) -3.60 -163.64 -1.32 -4.35 -163.64	1.32
7(9)75 TOP -0.76 -13.52 -226.86 -42.90 1.88	
75 BOT 0.76 13.52 -226.86 -38.24 2.70	
N(I1-I2) M-T N-T V-T M-B N-B V-B	
1(3-2) -42.91 -226.86 -13.53 -38.25 -226.86	13.53
· · ·	
7(10) 75 TOP 0.75 13.91 -5.42 45.20 -1.76	
75 BOT -0.75 -13.91 -5.42 38.24 -2.72	
N(I1-I2) M-T N-T V-T M-B N-B V-B	
1(3-2) 45.20 -5.42 13.91 38.24 -5.42	-13.91
8(1) 76 TOP 0.46 -1.50 -249.46 -9.21 -0.96	
76 BOT -0.46 1.50 -249.46 0.22 -1.83	
N(I1-I2) M-T N-T V-T M-B N-B V-B	
1(1-2) -1.45 -118.11 1.20 -1.14 -110.41	-1.20
2(1-3) -1.80 -131.36 1.01 1.52 -139.05	-1.01
8(2) 76 TOP 0.40 -1.30 -209.57 -8.00 -0.83	
76 BOT -0.40 1.30 -209.57 0.17 -1.57	
76 BOT -0.40 1.30 -209.57 0.17 -1.57	-1.04
76 BOT -0.40 1.30 -209.57 0.17 -1.57 N(I1-I2) M-T V-T M-B N-B V-B	
76         BOT         -0.40         1.30         -209.57         0.17         -1.57           N(I1-I2)         M-T         N-T         V-T         M-B         N-B         V-B            1(1-2)         -1.26         -99.42         1.04         -0.98         -92.73	
76         BOT         -0.40         1.30         -209.57         0.17         -1.57           N(I1-I2)         M-T         N-T         V-T         M-B         N-B         V-B            1(1-2)         -1.26         -99.42         1.04         -0.98         -92.73	
76         BOT         -0.40         1.30         -209.57         0.17         -1.57           N(I1-I2)         M-T         N-T         V-T         M-B         N-B         V-B            1(1-2)         -1.26         -99.42         1.04         -0.98         -92.73           2(1-3)         -1.56         -110.15         0.88         1.30         -116.84	
76       BOT       -0.40       1.30       -209.57       0.17       -1.57         N(I1-I2)       M-T       N-T       V-T       M-B       N-B       V-B          1(1-2)       -1.26       -99.42       1.04       -0.98       -92.73         2(1-3)       -1.56       -110.15       0.88       1.30       -116.84         8(3) 76       TOP       13.18       48.28       -408.74       109.16       -36.79	
76         BOT         -0.40         1.30         -209.57         0.17         -1.57           N(I1-I2)         M-T         N-T         V-T         M-B         N-B         V-B            1(1-2)         -1.26         -99.42         1.04         -0.98         -92.73           2(1-3)         -1.56         -110.15         0.88         1.30         -116.84           8(3) 76         TOP         13.18         48.28         -408.74         109.16         -36.79           76         BOT         -13.18         -48.28         -408.74         180.54         -42.26	-0.88
76       BOT       -0.40       1.30       -209.57       0.17       -1.57         N(I1-I2)       M-T       N-T       V-T       M-B       N-B       V-B          1(1-2)       -1.26       -99.42       1.04       -0.98       -92.73         2(1-3)       -1.56       -110.15       0.88       1.30       -116.84         8(3)       76       TOP       13.18       48.28       -408.74       109.16       -36.79         76       BOT       -13.18       -48.28       -408.74       180.54       -42.26         N(I1-12)        N-T        V-T        N-B	-0.88 15.08
76       BOT       -0.40       1.30       -209.57       0.17       -1.57         N(I1-I2)        M-T        V-T        M-B        V-B          1(1-2)       -1.26       -99.42       1.04       -0.98       -92.73         2(1-3)       -1.56       -110.15       0.88       1.30       -116.84         8(3)       76       TOP       13.18       48.28       -408.74       109.16       -36.79         76       BOT       -13.18       -48.28       -408.74       180.54       -42.26         N(I1-12)        M-T        V-T        M-B        V-B         1(1-2)       -13.33       -112.44       -15.08       -10.25       -302.52         2(1-3)       59.77       -296.30       -47.72       84.00       -106.22	-0.88 15.08
76       BOT       -0.40       1.30       -209.57       0.17       -1.57         N(I1-I2)        M-T        V-T        M-B        V-B          1(1-2)       -1.26       -99.42       1.04       -0.98       -92.73         2(1-3)       -1.56       -110.15       0.88       1.30       -116.84         8(3)       76       TOP       13.18       48.28       -408.74       109.16       -36.79         76       BOT       -13.18       -48.28       -408.74       180.54       -42.26         N(I1-12)        M-T        V-T        M-B        V-B         1(1-2)       -13.33       -112.44       -15.08       -10.25       -302.52	-0.88 15.08
76       BOT       -0.40       1.30       -209.57       0.17       -1.57         N(I1-I2)       M-T       N-T       V-T       M-B       N-B       V-B          1(1-2)       -1.26       -99.42       1.04       -0.98       -92.73         2(1-3)       -1.56       -110.15       0.88       1.30       -116.84         8(3)       76       TOP       13.18       48.28       -408.74       109.16       -36.79         76       BOT       -13.18       -48.28       -408.74       180.54       -42.26         N(I1-12)        M-T        V-T        M-B        V-B         1(1-2)       -13.33       -112.44       -15.08       -10.25       -302.52         2(1-3)       59.77       -296.30       -47.72       84.00       -106.22         8(4)       76       TOP       -12.34       -50.90       -78.66       -125.39       35.09         76       BOT       12.34       50.90       -78.66       -180.02       38.92	-0.88 15.08
76       BOT       -0.40       1.30       -209.57       0.17       -1.57         N(I1-I2)       M-T       N-T       V-T       M-B       N-B       V-B          1(1-2)       -1.26       -99.42       1.04       -0.98       -92.73         2(1-3)       -1.56       -110.15       0.88       1.30       -116.84         8(3)       76       TOP       13.18       48.28       -408.74       109.16       -36.79         76       BOT       -13.18       -48.28       -408.74       180.54       -42.26         N(I1-12)       M-T       N-T       V-T       M-B       N-B       V-B         1(1-2)       -13.33       -112.44       -15.08       -10.25       -302.52         2(1-3)       59.77       -296.30       -47.72       84.00       -106.22         8(4)       76       TOP       -12.34       -50.90       -78.66       -125.39       35.09         76       BOT       12.34       50.90       -78.66       -180.02       38.92         N(I1-12)       M-T       N-T       N-T       M-B       N-B       V-B	-0.88 15.08 47.72
76       BOT       -0.40       1.30       -209.57       0.17       -1.57         N(I1-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(1-2)       -1.26       -99.42       1.04       -0.98       -92.73         2(1-3)       -1.56       -110.15       0.88       1.30       -116.84         8(3)       76       TOP       13.18       48.28       -408.74       109.16       -36.79         76       BOT       -13.18       -48.28       -408.74       180.54       -42.26         N(I1-12)       M-T       N-T       V-T       M-B       N-B       V-B         1(1-2)       -13.33       -112.44       -15.08       -10.25       -302.52         2(1-3)       59.77       -296.30       -47.72       84.00       -106.22         8(4)       76       TOP       -12.34       -50.90       -78.66       -125.39       35.09         76       BOT       12.34       50.90       -78.66       -180.02       38.92         N(I1-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(1-2)       10.76       -	-0.88 15.08 47.72
76       BOT       -0.40       1.30       -209.57       0.17       -1.57         N(I1-I2)       M-T       N-T       V-T       M-B       N-B       V-B          1(1-2)       -1.26       -99.42       1.04       -0.98       -92.73         2(1-3)       -1.56       -110.15       0.88       1.30       -116.84         8(3)       76       TOP       13.18       48.28       -408.74       109.16       -36.79         76       BOT       -13.18       -48.28       -408.74       180.54       -42.26         N(I1-12)       M-T       N-T       V-T       M-B       N-B       V-B         1(1-2)       -13.33       -112.44       -15.08       -10.25       -302.52         2(1-3)       59.77       -296.30       -47.72       84.00       -106.22         8(4)       76       TOP       -12.34       -50.90       -78.66       -125.39       35.09         76       BOT       12.34       50.90       -78.66       -180.02       38.92         N(I1-12)       M-T       N-T       N-T       M-B       N-B       V-B	-0.88 15.08 47.72
76BOT $-0.40$ $1.30$ $-209.57$ $0.17$ $-1.57$ N(I1-I2) $$ M-T $$ V-T $$ M-B $$ V-B $$ 1(1-2) $-1.26$ $-99.42$ $1.04$ $-0.98$ $-92.73$ 2(1-3) $-1.56$ $-110.15$ $0.88$ $1.30$ $-116.84$ 8(3)76TOP $13.18$ $48.28$ $-408.74$ $109.16$ $-36.79$ 76BOT $-13.18$ $-48.28$ $-408.74$ $180.54$ $-42.26$ N(I1-I2) $$ M-T $$ V-T $$ M-B $$ 1(1-2) $-13.33$ $-112.44$ $-15.08$ $-10.25$ $-302.52$ 2(1-3) $59.77$ $-296.30$ $-47.72$ $84.00$ $-106.22$ 8(4)76TOP $-12.34$ $-50.90$ $-78.66$ $-125.39$ $35.09$ 76BOT $12.34$ $50.90$ $-78.66$ $-180.02$ $38.92$ N(I1-I2) $$ N-T $$ V-T $$ M-B $$ 1(1-2) $10.76$ $-116.93$ $17.20$ $8.18$ $86.66$ 2(1-3) $-62.93$ $38.27$ $49.47$ $-81.19$ $-165.32$	-0.88 15.08 47.72
76       BOT       -0.40       1.30       -209.57       0.17       -1.57         N(I1-I2)       M-T       N-T       V-T       M-B       N-B       V-B          1(1-2)       -1.26       -99.42       1.04       -0.98       -92.73         2(1-3)       -1.56       -110.15       0.88       1.30       -116.84         8(3)       76       TOP       13.18       48.28       -408.74       109.16       -36.79         76       BOT       -13.18       -48.28       -408.74       180.54       -42.26         N(I1-12)       M-T       N-T       V-T       M-B       N-B       V-B         1(1-2)       -13.33       -112.44       -15.08       -10.25       -302.52         2(1-3)       59.77       -296.30       -47.72       84.00       -106.22         8(4)       76       TOP       -12.34       -50.90       -78.66       -125.39       35.09         76       BOT       12.34       50.90       -78.66       -180.02       38.92         N(I1-12)       M-T       N-T       V-T       M-B       N-B       V-B          1(1-2)       10.76       -	-0.88 15.08 47.72
76BOT $-0.40$ $1.30$ $-209.57$ $0.17$ $-1.57$ N(I1-I2) $$ M-T $$ V-T $$ M-B $$ V-B $$ 1(1-2) $-1.26$ $-99.42$ $1.04$ $-0.98$ $-92.73$ 2(1-3) $-1.56$ $-110.15$ $0.88$ $1.30$ $-116.84$ 8(3)76TOP $13.18$ $48.28$ $-408.74$ $109.16$ $-36.79$ 76BOT $-13.18$ $-48.28$ $-408.74$ $180.54$ $-42.26$ N(I1-I2) $$ M-T $$ V-T $$ M-B $$ 1(1-2) $-13.33$ $-112.44$ $-15.08$ $-10.25$ $-302.52$ 2(1-3) $59.77$ $-296.30$ $-47.72$ $84.00$ $-106.22$ 8(4)76TOP $-12.34$ $-50.90$ $-78.66$ $-125.39$ $35.09$ 76BOT $12.34$ $50.90$ $-78.66$ $-180.02$ $38.92$ N(I1-I2) $$ N-T $$ V-T $$ M-B $$ 1(1-2) $10.76$ $-116.93$ $17.20$ $8.18$ $86.66$ 2(1-3) $-62.93$ $38.27$ $49.47$ $-81.19$ $-165.32$	-0.88 15.08 47.72

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Calculati	on book	Oil Car St	orage	:			
ł( 1- 2)	22.01	246.74	-84.20	34.02	-501.89	84.20	
2( 1- 3)	154.00	-445.11	-149.17	179.56	303.52	149.17	
8(6)76 1	OP -9.1	18 -173.6	2 -289.03	-477.58	30.35	:	
76	BOT	9.18 17	3.62 -289.	03 -564.14	24.7	3	
N(I1-I2) -	M-T	N-T V	-T M-I	з N-В	V-B		
1( 1- 2)	-24.58	-476.11	86.33	-36.09	286.02	-86.33	
2(1-3)	-157.15	187.08	150.92	-176.75	-575.05	-150.92	
8(7)76 1	TOP 13.	11 48.	50 -368.13	110.51	-36.65	-	•
76	BOT -1	3.11 -4	8.50 -368.1	180.49	-41.98		
N(I1-J2) -	M•T	N-T V	-T M-	B N-B	V-B		÷
1(1-2)	-13.12	-93.33	-15.25	-10.08	-284.54	15.25	
2(1-3)	60.03	-274.80	-47.87	83.77	-83.59	47.87	
8(8) <b>7</b> 6 1	OP -12.4	41 -50.0	58 -38.04	-124.03	35.23		
76	BOT	2.41	50.68 -38.	.04 -180.03	7 39.2	0	
N(11-12) -	М-Т	N-T V	-T M-	B N-B	V•B		
l(1-2)	10.98	-97.82	17.02	8.35	104.65	-17.02	
2(1-3)	-62.66	59.77	49.32	-81.43	-142.69	-49.32	
8(9)76	гор 9.	95 171	.22 -157.75	462.71	-31.91		
76	BOT -	9.95 -17	1.22 -157.3	75 564.62	-27.79	ł	
N(11-12) -	M-T	N-T V	-T M-I	B N-B	V-B		-
l( 1- 2)	22.22	265.85	-84.38	34.19	-483.90	84.38	
2(1-3)	154.26	-423.61	-149.32	179.33	326.14	149.32	
8(10) 76	тор -9	.25 -173.	40 -248.42	-476.23	30.50		
76	BOT	9.25 1	73.40 -248	.42 -564.19	25.0	1	
N(11-12) -	M-T	N-T V	-T M-	B N-B	V-B		
l(1-2)	-24.36	-457.00	86.15	-35.92	304.01	-86.15	
2(1-3)	-156.89	208 58	150.77	-176.98	-552 43	-150.77	

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5 • The Combined Force of Column, Brace and Wall Bottom on Ground Floor

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| The Combined Force of Column, Brace and Wall Bottom on Ground Floor |

Total-	Colun	nns = 68	Total-	Shear Walls =	- 8			
N-C(Nc)	N	V-X	<b>V-</b>	Y =1	<b>\</b> ≓	М•Х	M	I-Y NE
1(5)	1	-1.94	12.39	-260.79	-21.69	-6.40	1	Vxmax
1(1)	1	0.06	15.50	-274.94	-30.81	0.07	0	Vymax
1(10)	1	2.05	14.35	-220.24	-31.47	6.54	1	Nmin
1(1)	1	0.06	15.50	-274.94	-30.81	0.07	0	Nmax
1(1)	1	0.06	15.50	-274.94	-30.81	0.07	0	Mxmax
1(5)	1	-1.94	12.39	-260.79	-21.69	-6.40	1	Mymax
1(1)	1	0.06	15.50	-274.94	-30.81	0.07	0	V-V
1(0)	1	0.06	15.50	-274.94	-30.81	0.07	0	Wx+V
1(0)	1	0.06	15.50	-274.94	-30.81	0.07	0	-Wx+V
1(0)	1	0.06	15.50	-274.94	-30.81	0.07	.0	Wy+\
1(0)	1	0.06	15.50	-274.94	-30.81	0.07	0	-₩y+V
1(0)	1	-1.00	14.77	-262.90	-29.59	-3.27	1	Ex+V
1(0)	1	1.13	14.41	-261.87	-28.40	3.42	3	-Ex+V
1(0)	1	-1.94	12.39	-260.79	-21.69	-6.40	1	Ey+V
1(0)	1	2.06	16.79	-263.97	-36.31	6.56	1	-Ey+V
2(5)	2	-2.07	11.54	-260.60	-18.26	-6.65	1	Vxmax
2(1)	2	-0.05	15.99	-275.48	-31.79	-0.15	0	Vymax
2(10)	2	1.98	. 16.05	-221.39	-36.59	6.40	1	Nmin
2(1)	2	-0.05	15.99	-275.48	-31.79	-0.15	0	Nmax
2(6)	2	1.97	18.56	-265.21	-41.57	6.38	1	Mxmax
2(5)	2	-2.07	11.54	-260.60	-18.26	-6.65	1	Mymax
2(1)	2	-0.05	15.99	-275.48	-31.79	-0.15	0	V-V
2(0)	2	-0.05	15.99	-275.48	-31.79	-0.15	0	Wx+V
2(0)	2	-0.05	15.99	-275.48	-31.79	-0.15	0	•Wx+V
2( 0)	2	-0.05	15.99	-275.48	-31.79	-0.15	0	Wy+V
-	2	-0.05	15.99	-275.48	-31.79	-0.15	0	-Wy+V
2(0)	2	-1.02	15.34	-263.01	-30.90	-3.30	1	Ex+V
	2	0.92	14.76	-262.80	-28.94	3.02	1	-Ex+V

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فتحاد بعدانة الدائلا متتاعا	10. Dec. 10. Colds	All all the second s			والاعتباد والمراجب ويراج ورجاب ويراطوه بالمراجعة كالمنادكات		·	
2( 0)	2	-2.07	11.54	-260.60	-18.26	-6.65	1	Ey+V
2( 0)	2	1.97	18.56	-265.21	-41.57	6.38	1	-Ey+V
3(5)	3	-2.06	10.25	-259.54	-13.97	-6.63	1	Vxmax
3(1)	3	-0.04	16.01	-275.29	-31.83	-0.13	0	Vymax
3(10)	3	1.99	17.37	-222.11	-40.96	6.41	1	-
3(1)	3	-0.04	16.01	-275.29	-31.83	-0.13	0	Nmax
3(6)	3	1.98	19.89	-265.90	-45.95	6.39	1	Mxma
3(5)	3	-2.06	10.25	-259.54	-13.97	-6.63	1	Mymax
3(1)	3	-0.04	16.01	-275.29	-31.83	-0.13	0	V-V
3(0)	3	-0.04	16.01	-275.29	-31.83	-0.13	Ō	Wx+V
3(0)	3	-0.04	16.01	-275.29	-31.83	-0.13	Õ	-Wx+V
3(0)	3	-0.04	16.01	-275.29	-31.83	-0.13	Ŭ,	Wy+V
3(0)	3	-0.04	16.01	-275.29	-31.83	-0.13	0	-Wy+V
3(0)	3	-1.03	15.48	-263.01	-31.31	-3.31	1	Ex+V
3(0)	3	0.95	14.66	-262.44	-28.60	3.07		-Ex+V
3(0)	3	-2.06	10.25	-259.54	-13.97	-6.63	1	Ey+V
3(0)	3	1.98	19.89	-265.90	-45.95	6.39	1	-Ey+V
	-					0.57	•	
4( 5)	4	-2.02	8.94	-258.94	-9.63	-6.56	1	Vxmax
4( 6)	4	2.02	21.19	-267.04	-50.28	6.46	1	Vymax
4(10)	4	2.02	18.68	-223.21	-45.29	6.47	1	Nmin
4(1)	4	-0.01	16.01	-275.57	-31.83	-0.06	0	Nmax
4( 6)	4	2.02	21.19	-267.04	-50.28	6.46	1	Mxmax
4(5)	4	-2.02	8.94	-258.94	-9.63	-6.56	1	Mymax
4(1)	4	-0.01	16.01	-275.57	-31.83	-0.06	0	V-V
4( 0)	4	-0.01	16.01	-275.57	-31.83	-0.06	0	Wx+V
4( 0)	4	-0.01	16.01	-275.57	-31.83	-0.06	0	-Wx+V
4(0)	4	-0.01	16.01	-275.57	-31.83	-0.06	0	Wy+V
4(0)	4	-0.01	16.01	-275.57	-31.83	-0.06	0	-Wy+V
4(0)	4	+0. <del>99</del>	15.59	-263.33	-31.69	-3.24	1	Ex+V
4( 0)	4	0.98	14.54	-262.65	-28.22	3.13	ł	•Ex+V
4( 0)	4	-2.02	8.94	-258.94	-9.63	-6.56	1	Ey+V
4( 0)	4	2.02	21.19	-267.04	-50.28	6.46	1	-Ey+V
							-	_, .
• •	5	-2.25	7.64	-256.53	-5.30	-7.01	1	Vxmax
5(6)	5	1.77	22.50	-266.23	-54.63	5.98	1	Vymax
5(10)	5	1.81	19.99	-222.66	-49.64	6.07	1	Nmin
5(1)	5	-0.25	16.02	-273.88	-31.84	-0.55	0	Nmax
5(6)	5	1.77	22.50	-266.23	-54.63	5.98	1	Mxmax
5( 5)	5	-2.25	7.64	-256.53	-5.30	-7.01	1	Mymax
5(1)	5	-0.25	16.02	-273.88	-31.84	-0.55	Ð	V-V
5(0)	5	-0.25	16.02	-273.88	-31.84	-0.55	0	Wx+V
5(0)	5	-0.25	16.02	-273.88	-31.84	-0.55	0	-Wx+V

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alcula	ation	book	Oil Car Storage					
5(0)	5	-0.25	16.02	-273.88	-31.84	-0.55	0	Wy+V
5(0)	5	-0.25	16.02	-273.88	-31.84	-0.55	0	-Wy+V
5(0)	5	-1.22	15.71	-261.83	-32.08	-3.69	1	Ex+V
5(0)	5	0.74	14.44	-260.93	-27.85	2.66	1	-Ex+V
5(0)	5	-2.25	7.64	-256.53	-5.30	-7.01	1	Ey+V
5(0)	. 5 .	1.77	.22.50	-266.23	-54.63	5.98	1	•Ey+V
6( 6)	6	3.32	23.62	-277.92	-58.60	9.05	1	Vxma
6( 6)	6	3.32	23.62	-277.92	-58.60	9.05	1	Vyma
6(10)	6	3.11	21.14	-232.63	-53.66	8.64	1	Nmin
6(1)	6	1.31	15.82	-284.82	-31.44	2.55	0	Nmax
6(6)	6	3.32	23.62	-277.92	-58.60	9.05	ì	Mxma
6(6)	6	3.32	23.62	-277.92	-58.60	9.05	1	Myma
6(1)	6	1.31	15.82	-284.82	-31.44	2.55	0	V-V
6( 0)	6	1.31	15.82	-284.82	-31.44	2.55	0	Wx+
6(0)	6	1.31	15.82	-284.82	-31.44	2.55	0	-Wx+'
6(0)	6	1.31	15.82	-284.82	-31.44	2.55	0	Wy+
6(0)	6	1.31	15.82	-284.82	-31.44	2.55	0	•Wy+`
6(0)	6	0.23	15.64	-272.07	-32.10	-0.81	1	Ex+V
6(0)	6	2.26	14.14	-271.48	-27.11	5.67	l	-Ex+V
6(0)	6	-0.83	6.16	-265.63	-0.61	-4.19	1	Ey+V
6(0)	6	3.32	23.62	-277.92	-58.60	9.05	1	-Ey+\
7(1)	7	-8.71	11.76	-170.31	-23.38	-17.35	0	Vxmax
7(6)	7	-6.60	21.33	-169.64	-55.79	-10.66	1	Vymax
7(10)	. <b>7</b>	-5.22	19.45	-142.24	-52.05	-7.91	1	Nmin
7(1)	7	-8.71	11.76	-170.31	-23.38	-17.35	0	Nmax
7(6)	7	-6.60	21.33	-169.64	-55.79	-10.66	1	Mxma
7(5)	7	-9.96	1.20	-159.22	10.98	-22.33	1	Myma
7(1)	<b>7</b> .	-8.71	11.76	-170.31	-23.38	-17.35	0	V-V
7(0)	7.	-8.71	11.76	-170.31	-23.38	-17.35	0	Wx+V
7(0)	7	-8.71	11.76	-170.31	-23.38	-17.35	0	-Wx+V
7(0)	7	-8.71	11.76	-170.31	-23.38	-17.35	0	Wy+V
7(0)	7.	-8.71	11.76	-170.31	-23.38	-17.35	0	-Wy+\
7(0)	7	•9.08	12.13	-165.71	-25.27	-19.32	1	Ex+V
7(0)	7	-7.48	10.41	-163.15	-19.54	-13.67	t	-Ex+V
7(0)		-9.96	1.20	-159.22	10.98	-22.33	1	Ey+V
7(0)	7	-6.60	21.33	-169.64	-55.79	-10.66	1	-Ey+V
8(1)	8	8.65	11.76	-170.25	-23.38	17.13	0	Vxma
8(6)	8	. 9.90	21.40	-172.51	-56.08	22.12	1	Vyma
8(10)	8	8.53	19.52	-145.11	-52.35	. 19.41	1	Nmin
8(1)	8	8.65	11.76	-170.25	-23.38	17.13	0	Nmax
8(6)	8	9.90	21.40	-172.51	-56.08	22.12	1	Mxma

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alcul	ation	book	Oil Car Storag		╤╍╱╌╌╲┾╴═┶┲╴╋╸╼╘╸┱╲┾╶╧╸	<b></b>		:
8(6)	8	9.90	21.40	-172.51	-56.08	22.12	1	Mymax
8(1)	8	8.65	11.76	-170.25	-23.38	17.13	0	<b>V-V</b>
8(0)	8	8.65	11.76	-170.25	-23.38	17.13	0	Wx+V
8(0)	8	8.65	11.76	-170.25	-23.38	17.13	0	-Wx+V
8(0)	8	8.65	11.76	-170.25	-23.38	17.13	0	₩y+V
8(0)	8	8.65	11.76	-170.25	-23.38	17.13	0	-Wy+V
8(0)	8	7.42	12.15	-164.25	-25.32	13.47	1	Ex+V
8(0)	8	9.03	10.39	-164.51	-19.49	19.12	1	-Ex+V
8( 0)	8	6.54	1.13	-156.25	11.27	10.46	1	Ey+V
<b>8( 0)</b> .	8	9.90	21.40	-172.51	-56.08	22.12	1	-Ey+V
9( 5)	9	-3.39	3.42	-264.60	8.46	-9.28	i	Vxmax
9(6)	9	0.75	26.36	-278.98	-67.67	3.96	1	Vymax
9(10)	9	0.97	23.88	-233.68	-62.73	4.40	1	Nmin
9(1)	9	-1.39	15.82	-284.83	-31.44	-2.81	0	Nmax
9(6)	9	0.75	26.36	-278.98	-67.67	3.96	1	Mxmax
9( 5)	9	-3.39	3.42	-264.60	8.46	-9.28	1	Мутах
9(1)	9	-1.39	15.82	-284.83	-31.44	-2.81	0	V-V
9( 0)	9	-1.39	15.82	-284.83	-31.44	-2.81	0	Wx+V
9( 0)	9	-1.39	15.82	-284.83	-31.44	-2.81	0	-Wx+V
9( 0)	9	-1.39	15.82	-284.83	-31.44	-2.81	0	Wy+V
9( 0)	9	-1.39	15.82	-284.83	-31.44	-2.81	0	-Wy+V
9( 0)	9	-2.33	15.88	-272.65	-32.89	-5.91	1	Ex+V
9( 0)	9	-0.30	13.90	-270.94	-26.32	0.58	1	-Ex+V
9( 0)	9	-3.39	3.42	-264.60	8.46	-9.28	1	Ey+V
9( 0)	9	0.75	26.36	-278.98	-67.67	3.96	1	-Ey+V
10( 5)	10	-1.84	2.31	-252.89	12.42	-6.21	1	Vxmax
10( 6)	10	2.18	27.85	-269.87	-72.37	6.78	1	Vymax
10(10)	10	2.15	25.33	-226.31	-67.37	6.73	1	Nmin
10( <b>i</b> )	10	0.17	16.02	-273.88	-31.85	0.30	0	Nmax
10( 6)	10	2.18	27.85	-269.87	-72.37	6.78	1	Mxmax
10( 5)	10	-1.84	2.31	-252.89	12.42	-6.21	1	Mymax
• •	10	0.17	16.02	-273.88	-31.85	0.30	0	· V-V
10( 0)	10	0.17	16.02	-273.88	-31.85	0.30	0	Wx+V
	10	0.17	16.02	-273.88	-31.85	0.30	0	-Wx+V
10( 0)	10	0.17	16.02	-273.88	-31.85	0.30	0	Wy+V
10( 0)	10	0.17	16.02	-273.88	-31.85	0.30	0	-Wy+V
10( 0)	10	-0.81	16.18	-262.08	-33.64	-2.89	1	Ex+V
10( 0)	10	1.15	13.97	-260.68	-26.31	3.46	1	-Ex+V
10( 0)	10	-1.84	2.31	-252.89	12.42	-6.21	1	Ey+V
10( 0)	10		27.85			6.78	1	-Ey+V
+ 1 < 2		-2.09	0.99		16.77		1	Vxmax

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Calcula	ation	book o	il Car Storage					
11(6)	11	1.95	29.15	-272.27	-76.69	6.34	1	Vymax
11(10)	11	1.96	26.63	-228.44	-71.70	6.37	1	Nmin
	11	-0.07	16.01	-275.57	-31.83	-0.19	0	Nmax
11(6)	11	1.95	29.15	-272.27	-76.69	6.34	1	Mxmax
11(5)	11	-2.09	0.99	-253.70	16.77	-6.69	1	Mymax
11(1)	11	-0.07	16.01	-275.57	-31.83	-0.19	0	V-V
11(0)	11	-0.07	16.01	-275.57	-31.83	-0.19	0	Wx+V
11(0)	11	-0.07	16.01	-275.57	-31.83	-0.19	0	-Wx+V
11(0)	11 ·	-0.07	16.01	-275.57	-31.83	-0.19	0	Wy+V
11(0)	11	-0.07	16.01	-275.57	-31.83	-0.19	0	-Wy+V
11(0)	i1	-1.05	16.29	-263.80	-34.01	-3,36	1	Ex+V
11(0)	11	0.92	13.85	-262.18	-25.91	3.01	1	•Ex+V
11(0)	11	-2.09	0.99	-253.70	16.77	-6.69	1	Ey+V
11(0)	11	1.95	29.15	-272.27	-76.69	6.34	1	•Ey+V
12(5)	12	-2.05	-0.31	-252.58	21.10	-6.61	1	Vxmax
12(6)	12	1.99	30.45	<b>-27</b> 2.90	-81.03	6.41	1	Vymax
12(10)	12	1.99	27.94	-229.11	-76.04	6.42	1	Nmin
12(1)	12	-0.03	16.01	-275.31	-31.84	-0.11	0	Nmax
12(6)	12	1.99	30.45	-272.90	-81.03	6.41	1	Mxmax
12(5)	12	-2.05	-0.31	-252.58	21.10	-6.61	¥	Mymax
12(1)	12	-0.03	16.01	-275.31	-31.84	-0.11	Ð	<b>V-V</b>
12(0)	12	-0.03	16.01	-275.31	-31.84	-0.11	0	Wx+V
12(0)	12	-0.03	16.01	-275.31	-31.84	-0.11	0	-Wx+V
12(0)	12	-0.03	16.01	-275.31	-31.84	-0.11	0	Wy+V
12(0)	12 -	-0.03	16.01	-275.31	-31.84	-0.11	0	-Wy+V
12(0)		-1.01	16.40	-263.62	-34.39	-3.29	1	Ex+V
	12	0.95	13.74	-261.86	-25.54	3.08	1	•Ex+V
-	12	-2.05				-6.61	ì	Ey+V
	12	1.99	30.45	-272.90	-81.03		1	
13(5)			-1.62	-251.73	25.44	-6.63	1	Vxmax
• •	13	1.98	31.76	-273.76		6.39	1	Vymax
		1.99		-229.97	-80.37	6.41	1	Nmin
13(1)		-0.04	16.01	-275.31	-31.84	-0.14	0	Nmax
13(6)			31.76	-273.76	-85.37	6.39	1	Mxmax
13(5)	13 :		-1.62	-251.73	25.44	-6.63	1	Mymax
• •	13 :		16.01	-275.31	-31.84	-0.14	0	v-v
• •	13		16.01	-275.31	-31.84	-0.14	0	Wx+V
	13		16.01	-275.31	-31.84	-0.14	0	-Wx+V
13(0)			16.01	-275.31	-31.84	-0.14	0	Wy+V
13(0)	13 13	-0.04		-275.31		-0.14	0	-Wy+V
13(0)			16.52	-263.70		-3.31	ĩ	Ex+V
12(0)	13 -	-1.02	10.32	-702.10		4.54	•	

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Calculation	book	Oil Car Storage		<u> </u>	3 		<u></u>
13(0) 13	-2.06	-1.62	-251.73	25.44	-6.63	1	Ey+V
13(0) 13	1.98	31.76	-273.76	-85.37	6.39	1	-Ey+V
	-2.03	-2.93	-251.08	29.78	-6.57	1	Vxmax
14(6) 14	2.01	33.07	-274.85	-89.70	6.45	1	Vymax
14(10) 14	2.01	30.55	-231.02	-84.71	6.46	1	Nmin
14(1) 14	-0.01	16.01	-275.54	-31.84	-0.07	0	Nmax
14(6) 14	2.01	33.07	-274.85	-89.70	6.45	1	Mxmax
14(5) 14	-2.03	-2.93	-251.08	29.78	-6.57	1	Mymax
14(1) 14	-0.01	16.01	-275.54	-31.84	-0.07	0	. V•V -
14(0) 14	-0.01	16.01	-275.54	-31.84	-0.07	0	Wx+V
14(0) 14	-0.01	16.01	-275.54	-31.84	-0.07	0	-Wx+V
14(0) 14	-0.01	16.01	-275.54	-31.84	-0.07	0	Wy+V
14(0) 14	-0.01	16.01	-275.54	-31.84	-0.07	0	-Wy+V
14(0) 14	-0.99	16.63	-263.99	-35.15	-3.24	1	Ex+V
14(0) 14	0.98	13.51	-261.94	-24.78	3.13	1	•Ex+V
14(0) 14	-2.03	-2.93	-251.08	29.78	-6.57	1	Ey+V
14(0) 14	2.01	33.07	-274.85	-89.70	6.45	1	-Ey+V
15(5) 15	-2.23	-4.22	-248.83	34.09	-6.97	1	Vxmax
15(6) 15	1.80	34.38	-274.25	-94.06	6.04	1	Vymax
15(10) 15	1.84	31.87	-230.66	-89.06	6.11	1	Nmin
15(1) 15	-0.23	16.02	-274.04	-31.86	-0.50	0	Nmax
15(6) 15	1.80	34.38	-274.25	-94.06	6.04	1	Mxmax
15(5) 15	-2.23	-4.22	-248.83	34.09	-6.97	ŧ	Mymax
15(1) 15	-0.23	16.02	-274.04	-31.86	-0.50	0	V V
15(0) 15	-0.23	16.02	-274.94	-31.86	-0.50	0	Wx+V
15(0) 15	-0.23	16.02	-274.04	-31.86	-0.50	0	-₩x+V
15(0) 15	-0.23	16.02	-274.04	-31.86	-0.50	0	Wy+V
15(0) 15	-0.23	16.02	-274.04	-31.86	-0.50	0	-Wy+V
15(0) 15	-1.19	16.76	-262.68	-35.55	-3.64	1	Ex+V
15(0) 15	0.77	13.40	-260.40	-24.42	2.71	1	-Ex+V
15(0) 15	-2.23	-4.22	-248.83	34.09	-6.97	1	Ey+V
15(0) 15		34.38			6.04	1	•Ey+V
16(6) 16	3.15	35.60		•	8.71	1	Vxmax
16(6) 16	3.15	35.60	-285.12	-98.23	8.71	1	Vymax
16(10) 16	2.97		-239.91	-93.26	8.36	1	Nmin
16(1) 16	1.16	15.93	-284.33		2.25	0	Nmax
16(6) 16	3.15		-285.12		8.71	i	Mxmax
16(6) 16	3.15				8.71	1	Mymax
16(1) 16	1.16	15.93		-31.67	2.25	0	<b>v-v</b>
16(0) 16	1.16	15.93			2.25	0	Wx+V
16(0) 16	1.16	15.93			2.25	0	•Wx+V

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alcula	ation	book	Oil Car Storage	Č				
16( 0)	16	1.16	15.93	-284.33	-31.67	2.25	0	Wy+\
16(0)	16	1.16	15.93	-284.33	-31.67	2.25	0	•Wy+V
16(0)	16	0.08	16.79	-272.27	-35.76	-1.11	1	Ex+V
16(0)	16 ¹	2.12	13.20	-270.33	-23.87	5.39	1	-Ex+V
16(0)	16 -	-0.95	-5.61	-257.48	38.59	-4.43	ł	Ey+V
16( 0)	16	.3.15	. 35.60	-285.12	-98.23	8.71	1	-Ey+V
17(1)	17	-7.84	11.88	-171.67	-23.63	-15.62	0	Vxmax
17(6)	17	-5.62	33.33	-178.92	-95.44	-8.72	I	Vymax
17(10)	17	-4.38	31.43	-151.30	-91.67	-6.25	1	Nmin
17(1)	17	-7.84	11.88	-171.67	-23.63	-15.62	0	Nmax
17(6)	17	-5.62	33.33	-178.92	-95.44	-8.72	1	Mxmax
17(5)	17	-9.26	-10.55	-152.54	50.16	-20.94	1	Mymax
17(1)	17	-7.84	11.88	-171.67	-23.63	-15.62	0	٧.٧
17(0)	17 -	-7,84	11.88	-171.67	-23.63	-15.62	0	Wx+V
17(0)	17	-7.84	11.88	-171.67	-23.63	-15.62	0	-Wx+V
17(0)	17	-7.84	11.88	-171.67	-23.63	-15.62	0	₩y+\
17(0)	17	-7.84	11.88	-171.67	-23.63	-15.62	0	-Wy+∖
17(0)	17	-8.23	13.29	-167.71	-28.96	-17.63	1	Ex+V
17(0)	17	-6.65	9.48	-163.75	-16.33	-12.03	1	-Ex+V
17(0)	17	-9.26	-10.55	-152.54	50.16	-20.94	1	Ey+V
17( 0)	17 .	-5.62	33.33	-178.92	-95.44	-8.72	1	-Ey+V
18( 3)	18	-2.46	-2.72	-387.58	5.14	-6.37	1	Vxmax
18( 5)	18	-1.48	-5.54	-388.91	13.93	-3.06	1	Vymax
18(10)	18	•0.80	0.17	-321.47	-3.30	-1.56	1	Nmin
18(1)	18	-1.33	-3.11	-409.63	6.16	-2.68	0	Nmax
18( 5)	18 .	-1.48	-5.54	-388.91	13.93	-3.06	1	Mxma
18(3)	18 :	-2.46	-2.72	-387.58	5.14	-6.37	1	Myma
18(1)	18	-1.33	-3.11	-409.63	6.16	-2.68	0	V-V
18( 0)	18 .	-1.33	-3.11	-409.63	6.16	-2.68	0	Wx+V
18( 0)	18 ·	-1.33	-3.11	-409.63	6.16	-2.68	0	∙₩x+\
18(0)	18	-1.33	-3.11	-409.63	6.16	-2.68	0.	Wy+V
18(0)	18	-1.33	-3.11	-409.63	6.16	-2.68	0	-Wy+V
18( 0)	18	-2.46	-2.72	-387.58	5.14	-6.37	1	Ex+V
18(0)	18	-0.03	-3.14	-387.38	6.46	1.34	1	-Ex+¥
18(0)	18	-1.48	-5.54	-388.91	13.93	-3.06	1	Ey+V
18(0)	18	-1.01	-0.32	-386.04	-2.33	-1.97	1	-Ey+V
19(4)	19	1.30	-3.61	-378.40	7.55		1	Vxma
19( 5)	19	0.12	-7.42	-379.02	19,40	0.14	1	Vyma
19(10)	19	0.15	1.43	-314.46	-7.54	0.34	1	Nmin
19(1)		0.16	-3.47	-399.81	6.87	0.27	0	Nmax
19(5)			-7,42	-379.02	19.40	0.14	1	Mxma

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Calcul	ation	book	Oil Car Storag	sc		1	2-2-2-1-2-1-2-1-2-1-		6
19(3)	19	-0.99	-2.92	-378.12	5.38	-3.46	1	Mymax	
19(1)	19	0.16	-3.47	-399.81	6.87	0.27	0	<b>V-V</b>	
19( 0)	19	0.16	-3.47	-399.81	6.87	0.27	0	Wx+V	•
19( 0)	19	0.16	-3.47	-399.81	6.87	0.27	0	-Wx+V	
19( 0)	19	0.16	-3.47	-399.81	6.87	0.27	0	Wy+V	
19( 0)	19	0.16	-3.47	-399.81	6.87	0.27	0	-Wy+V	
19( 0)	19	-0.99	-2.92	-378.12	5.38	-3.46	1	Ex+V	
19( 0)	19	1.30	-3.61	-378.40	7.55	3.98	1	-Ex+V	
19( 0)	19	0.12	-7.42	-379.02	19.40	0.14	1	· Ey+V	
19( 0)	19	0.18	0.89	-377.50	-6.46	0.38	1	•Ey+V	
20(3)	20	-1.23	-2.79	-379,65	4.98	-3.92	1	Vxmax	
20( 5)	20	-0.13	-8.97	-381.09	24.23	-0.36	1	Vymax	
20(10)	20	0.00	2.97	-315.12	-12.34	0.03	1	Nmin	
20(1)	20	-0.07	-3.48	-401.39	6.89	-0.20	0	Nmax	
20( 5)	20	-0.13	-8.97	-381.09	24.23	-0.36	1	Mxmax	
20(3)	20	-1.23	-2.79	-379.65	4.98	-3.92	1	Mymax	
20(1)	20	-0.07	-3.48	-401.39	6.89	-0.20	0	٧٠V	
20( 0)	20	-0.07	-3.48	-401.39	6.89	-0.20	0	Wx+V	
20(0)	20	-0.07	-3.48	-401.39	6.89	-0.20	0	-Wx+V	
20(0)	20	-0.07	-3.48	-401.39	6.89	-0.20	0	Wy+V	
20(0)	20	-0.07	-3.48	-401.39	6.89	-0.20	0	-Wy+V	
20(0)	20	-1.23	-2.79	-379.65	4.98	-3.92	1	Ex+V	
20(0)	20	1.09	-3.76	-379.85	7.99	3.56	1	-Ex+V	
20(0)	20	-0.13	-8.97	-381.09	24.23	-0.36	1	Ey+V	
20( 0)	20	-0.01	2.43	-378.41	-11.26	0.00	1	-Ey+V	
21(3)			-2.66		4.56	-3.79	1	Vxmax	
21(5)		-0.06				-0.23	1	Vymax	
21(10)		0.05				0.13	1	Nmin	
21(1)		-0.01		-401.37	6.89	-0.06	0	Nmax	
21(5)		-0.06		-381.39	29.04	-0.23	1	Mxmax	
21(3)			-2.66		4.56	-3.79	1	Mymax	
21(1)		-0.01	-3.48	-401.37	6.89	-0.06		V-V	
	21	-0.01	-3.48	-401.37	6.89	-0.06		Wx+V	
21(0)		-0.01				-0.06	0	-Wx+V	
21(0)		-0.01		-401.37	6.89	-0.06	0		
• • •	21	-0.01	-3.48	-401.37	6.89	-0.06		-Wy+V	
21(0)		-1.16			4.56	-3.79		Ex+V	
21(0) 21(0)			-3.89		8.41	3.69	1		
21(0)		-0.06				-0.23		Ey+V	
21(0)	<i>2</i> 1	0.05	3.97	-378.06	-16.07	0.12	1 :	•Ey+V	
22( 3)	22	-1.36	-2.52	-378.31	4.14	-4.18	1	Vxmax	

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Calculation	book	Oil Car Stora	ş¢	98-10- 1-1-1-1-2-1-2-1-1-1-2-1-1-2-1-1-2-1-			
22(5) 22	-0.26	-12.06	-380.47	33.85	-0.63	1	Vymax
22(10) 22	-0.12	6.06	-313.34	-21.97	-0.20	1	Nmin
22(1) 22	-0.22	-3.48	-400.01	6.89	-0.48	0	Nmax
22(5) 22	-0.26	-12.06	-380.47	33.85	•0.63	1	Mxmax
22(3) 22	-1.36	-2.52	-378.31	4.14	-4.18	1	Mymax
22(1) 22	-0.22	-3.48	-400.01	6.89	-0.48	0	V-V
22(0) 22	-0.22	-3.48	-400.01	6.89	-0.48	0	Wx+V
22(0) 22	-0.22	-3.48	-400.01	6.89	-0.48	0	-Wx+V
22(0) 22	-0.22	-3.48	-400.01	6.89	-0.48	0	Wy+V
22(0) 22	-0.22	-3.48	-400.01	6.89	-0.48	0	•Wy+V
22(0) 22	-1.36	-2.52	-378.31	4.14	-4.18	ł	Ex+V
22(0) 22	0.95	-4.03	-378.58	8.83	3.28	1	-Ex+V
22(0) 22	-0.26	-12.06	-380.47	33.85	-0.63	1	Ey+V
22(0) 22	-0.15	5.52	-376.42	-20.89	-0.28	1	-Ey+V
23(4) 23	2.21	-4.11	-387.19	9.14	5.78	1	Vxmax
23(5) 23	0.96	-13.55	-389.13	38.55	1.80	1	Vymax
23(10) 23	0.90	7.65	-319.92	-26.87	1.83	1	Nmin
23(1) 23	1.08	-3.42	-408.83	6.76	2.09	0	Nmax
23(5) 23	0.96	-13.55	-389.13	38.55	1.80	1	Mxmax
23(4) 23	2.21	-4.11	-387.19	9.14	5.78	1	Mymax
23(1) 23	1.08	-3.42	-408.83	6.76	2.09	0	V-V
23(0) 23	1.08	-3.42	-408.83	6.76	2.09	0	Wx+V
23(0) 23	1.08	-3.42	-408.83	6.76	2.09	0	-Wx+V
23(0) 23	1.08	-3.42	-408.83	6.76	2.09	0	` ₩y+V
23(0) 23	1.08	-3.42	-408.83	6.76	2.09	0	-Wy+V
23(0) 23	-0.17	-2.33	-386.32	3.60	-1.83	l	Ex+V
23(0) 23	2.21	-4.11	-387.19	9.14	5.78	1	-Ex+V
23(0) 23	0.96	-13.55	-389.13	38.55	1.80	1	Ey+V
23(0) 23	•				2.16	1	-Ey+V
24(1) 24			-273.54		-15.22	0	Vxmax
24(5) 24	-7.21	-14.30	-265.85	41.78	-14.43	1	Vymax
24(10) 24	-5.92	9.87	-216.51	-33.01	-11.74	1	Nmin
24(1) 24	-7.64	-2.53	-273.54	5.00	-15.22	0	Nmax
24(5) 24	-7.21	-14.30	-265.85	41.78	-14.43	1	Mxmax
24(1) 24	-7.64	-2.53	-273.54	5.00	-15.22	0	Mymax
24(1) 24	-7.64	-2.53	-273.54	5.00	-15.22	0	V-V
24(0) 24	-7.64	-2.53	-273.54	5.00	-15.22	0	Wx+V
24(0) 24	-7.64	-2.53	-273.54	5.00	-15.22	0	-Wx+V
24(0) 24	-7.64	-2.53	-273.54	5.00	-15.22	0	Wy+V
24(0) 24	-7.64	-2.53	-273.54	5.00	-15.22	0	-Wy+V
24(0) 24	-8.11	-1.39	-263.69	1.59	-17.60	1	
24(0) 24	-6.22	-3.45	-262.52	7.98	-10.95	i	-Ex+V

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24( 0)	24	-7.21	-14.30	-265.85	41.78	-14.43	1	Ey+V
24( 0)	24	-7.12	9.46	-260.36	-32.21	-14.12	1	-Ey+V
25(1)	25	7.57	-2.53	-273.48	5.00	14.99	0	Vxmax
25(5)	25	7.06	-14.44	-265.82	42.20	13.91	1	Vymaz
25(10)	25	5.97	10.00	-216.44	-33.42	11.88	1	Nmin
25(1)	25	7.57	-2.53	-273.48	5.00	14.99	0	Nmax
25(5)	25	7.06	-14.44	-265.82	42.20	13.91	1	Mxma
25(1)	25	7.57	-2.53	-273.48	5.00	14.99	0	i Myma
25(1)	25	7.57	-2.53	-273.48	5.00	14.99	0	. <b>V-V</b>
25(0)	25	7.57	-2.53	-273.48	5.00	14.99	0	Wx+
25(0)	25	7.57	-2.53	-273.48	5.00	14.99	0	-Wx+'
25(0)	25	7.57	-2.53	-273.48	5.00	14.99	0	Wy+
25(0)	25	7.57	-2.53	-273.48	5.00	14.99	0	-Wy+
25(0)	25	6.16	-1.39	-261.99	1.56	10.75	1	Ex+
25(0)	25	8.05	-3.46	-264.12	8.01	17.39	1	-Ex+\
25(0)	25	7.06	-14.44	-265.82	42.20	13.91	1	Ey+
25(0)	25	7.15	9.60	-260.29	-32.63	14.23	1	-Ey+\
26(3)	26	-2.28	-2.05	-386.73	2.72	-6.02	1	Vxmax
26( 5)	26	-1.15	-16.78	-389.90	48.60	-2.39	1	Vymax
26(10)	26	-0.85	10.88	-319.17	-36.92	-1.66	1	Nmin
26(1)	26	-1.16	-3.41	-408.85	6.76	-2.35	0	Nmax
26(5)	26	-1.15	-16.78	-389.90	48.60	-2.39	1	Mxma
26(3)	26	-2.28	-2.05	-386.73	2.72	-6.02	1	Myma
26(1)	26	-1.16	-3.41	-408.85	6.76	-2.35	0	V-V
26( 0)	26	-1.16	-3.41	-408.85	6.76	-2.35	0	Wx+
26(0)	26	-1.16	-3.41	-408.85	6.76	-2.35	0	-Wx+V
26( 0)	26	-1.16	-3.41	-408.85	6.76	-2.35	0	Wy+
26( 0)	26	-1.16	-3.41	-408.85	6.76	-2.35	0	-Wy+V
26( 0)	26	-2.28	-2.05	-386.73	2.72	-6.02	1	Ex+V
26( 0)	26	. 0.10	-4.39	-386.81	10.02	1.60	1	-Ex+1
26( 0)	26	-1.15	-16.78	-389.90	48.60	-2.39	1	Ey+V
26( 0)	26	-1.04	10.35	-383.63	-35.86	-2.03	1	-Ey+V
27(4)	27	1.28	-4.58	•		3.95	1	Vxma
27(5)	27	0.08	-18.38	-381.92	53.52	0.05	1	Vyma
27(10)	27	0.17	12.38	-311.88	-41.64	0.36	1	Nmir
27(1)	27	0.14	-3.48	-400.00	6.88	0.23	0	Nmax
27(5)	27	0.08	-18.38	-381.92	53.52	0.05	ł	Mxma
27(3)	27	-1.02	-1.97	-378.10	2.41	-3.51	1	Myma
27(1)	27	0.14	-3.48	-400.00	6.88	0.23	0	٧-٧
27(0)	27	0.14	-3.48	-400.00	6.88	0.23	0	Wx+
27(0)	27	0.14	-3.48	-400.00	6.88	0.23	0	-Wx+

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alcul	ation	book	Oil Car Storage	;	10. 1711-1. (19. 19. 17 19. 19. 19. 19. 19. 19. 19. 19. 19. 19.	انگونگان او وی و هکرو هکرو		
27( 0)	27	0.14	-3.48	-400.00	6.88	0.23	0	Wy+V
27(0)	27	0.14	-3.48	-400.00	6.88	0.23	0	∙₩y+\
27(0)	27	-1.02	-1.97	-378.10	2.41	-3.51	1	Ex+V
27(0)	27	1.28	-4.58	-378.78	10.55	3.95	1	-Ex+V
27(0)	27	0.08	-18.38	-381.92	53.52	0.05	ł	Ey+V
27(0)	27	0.19	11.84	-374.96	-40.56	0.40	1	-Ey+V
28( 3)	28	-1.22	-1.83	-379.43	1.99	-3.91	1	Vxmax
28( 5)	28	-0.12	-19.93	-383.60	58.33	-0.35	1	Vymax
28(10)	28	0.00	13.93	-312.63	-46.45	0.04	1	Nmin
28(1)	28	-0.07	-3.48	-401.40	6.88	-0.18	0	Nmax
28( 5)	28	-0.12	-19.93	-383.60	58.33	-0.35	1	Mxmax
28(3)	28	-1.22	-1.83	-379.43	1.99	-3.91	1	Mymax
28(1)	28	-0.07	-3.48	-401.40	6.88	-0.18	0	V-V
28( 0)	28	-0.07	-3.48	-401.40	6.88	-0.18	0	Wx+V
28( 0)	28	-0.07	-3.48	-401.40	6.88	-0.18	0	-Wx+V
28( 0)	28	-0.07	-3.48	-401.40	6.88	-0.18	0	Wy+V
28( 0)	28	-0.07	-3.48	-401.40	6.88	-0.18	0	-Wy+V
28( 0)	28	-1.22	-1.83	-379.43	1.99	-3.91	1	Ex+V
28(0)	28	1.09	-4.71	-380.09	10.97	3.57	1	-Ex+V
28( 0)	28	-0.12	-19.93	-383.60	58.33	-0.35	1	Ey+V
28( 0)	28	-0.01	13.38	-375.92	-45.38	0.01	1	-Ey+V
29(3)	29	-1.19	-1.69	-379.19	1.57	-3.84	ł	Vxmax
29(5)	29	-0.09	-21.47	-383.75	63.14	-0.28	1	Vymax
29(10)	29	0.03	15.47	-312.10	-51.27	0.09	1	Nmin
29(1)	29	-0.03	-3.48	-401.18	6.88	-0.12	0	Nmax
29(5)	29	-0.09	-21.47	-383.75	63.14	-0.28	1	Mxmax
29(3)	29	: <b>-1.19</b>	-1.69	-379.19	1.57	-3.84	1	Mymax
29( I)	29	-0.03	-3.48	-401.18	6.88	-0.12	0	V-V
29( 0)	29	-0.03	-3.48	-401.18	6.88	-0.12	0	Wx+\
29( 0)	29	-0.03	-3.48	-401.18	6.88	-0.12	0	-Wx+V
29( 0)	29	-0.03	-3.48	-401.18	6.88	-0.12	0	Wy+V
29( 0)	29	-0.03	-3.48	-401.18	6.88	-0.12	0	-Wy+V
29( 0)	29	-1.19	-1.69	-379.19	1.57	-3.84	1	Ex+V
29( 0)	29	1.13	-4.85	-379.92	11.39	3.63	1	-Ex+V
29( 0)	29	-0.09	-21.47	-383.75	63.14	-0.28	1	Ey+V
29( 0)	29	0.02	14.93			0.07	1	-Ey+V
30( 3)	30		-1.56	-379.17	1.14	-3.86	1	
30( 5)	30	-0.09	-23.02	-384.11	67.95		1	•
30(10)	30	0.02	17.02	-311.75	-56.08	0.07		
30(1)	30	-0.04	-3.48	-401.19	6.88	-0.13	0	Nmax
30(5)	30	-0.09	-23.02	-384.11	67.95	-0.30	1	Mxmax

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Calcula	atio	n book	Oil Car Storag	e			· · · · · · · · · · · · · · · · · · ·		6
30(3)	30	-1.20	-1.56	-379.17	1.14	-3.86	1	Mymax	
30(1)	30	-0.04	-3.48	-401.19	6.88	-0.13	0	<b>V-V</b>	
30( 0)	30	-0.04	-3.48	-401.19	6.88	-0.13	0	Wx+V	
30(0)	30	-0.04	-3.48	-401.19	6.88	-0.13	0	-Wx+V	
30(0)	30	-0.04	-3.48	-401.19	6.88	-0.13	0	Wy+V	
30( 0)	30	-0.04	-3.48	-401.19	6.88	-0.13	0	-Wy+V	
30( 0)	30	-1.20	-1.56	-379.17	1.14	-3.86	1	Ex+V	
30( 0)	30	1.12	-4.98	-379.95	11.81	3.62	ł	-Ex+V	
30 <b>( 0)</b>	30	-0.09	-23.02	-384.11	67.95	-0.30	1	Ey+V	
30( 0)	30	0.01	16.47	-375.01	-55.00	0.05	1	-Ey+V	
31(3)	31	-1.17	-1.42	-379.27	0.72	-3.82	1	Vxmax	
31(5)	31	-0.07	-24.56	-384.61	72.76	-0.25	1	Vymax	
31(10)	31	0.04	18.57	-311.51	-60.89	0.11	1	Nmin	
31(1)	31	-0.02	-3.47	-401.34	6.88	-0.09	0	Nmax .	
31(5)	31	-0.07	-24.56	-384.61	72.76	-0.25	1	Mxmax	
31(3)	31	-1.17	-1.42	-379.27	0.72	-3.82	1	Mymax	
31(1)	31	-0.02	-3.47	-401.34	6.88	-0.09	0	V-V	
31(0)	31	-0.02	-3.47	-401.34	6.88	-0.09	0	Wx+V	
31(0)	31	-0.02	-3.47	-401.34	6.88	-0.09	0	-Wx+V	
31(0)	31	-0.02	-3.47	-401.34	6.88	-0.09	0	Wy+V	
31(0)	31	-0.02	-3.47	-401.34	6.88	-0.09	0	•Wy+V	
31(0)	31	-1.17	-1.42	-379.27	0.72	-3.82	1	Ex+V	
31(0)	31	1.14	-5.12	-380.13	12.23	3.66	1	-Ex+V	
31(0)	31	-0.07	-24.56	-384.61	72.76	-0.25	1	Ey+V	
31(0)	31	0.04	18.02	-374.80	-59.81	0.10	1	-Ey+V	
32(3)	32	-1.30	-1.29	-378.37	0.30	-4.08	i	Vxmax	
32(5)	32	-0.21	-26.11	-384.06	77.57	-0.52	1	Vymax	
32(10)	32	-0.07	20.11	-310.39	-65.70	-0.12	1	Nmin	
32(1)	32	-0.16	-3.48	-400.37	6.88	-0.38	0.	Nmax	
32(5)	32	-0.21	-26.11	-384.06	77.57	-0.52	1	Mxmax	
	32	-1.30	-1.29	-378.37	0.30	-4.08	1	Mymax	:
32(1)	32	-0.16	-3.48	-400.37	6.88	-0.38	0	V-V	
• •	32	-0.16	-3.48	-400.37	6.88	-0.38	0	Wx+V	
32(0)		-0.16	-3.48	-400.37	6.88	-0.38	0	-Wx+V	
• •	32	-0.16	-3.48	-400.37	6.88			Wy+V	
•••	32	-0.16	-3.48	-400.37	6.88	-0.38	0	-Wy+V	
• •	32	-1.30	-1.29	-378.37	0.30	-4.08	1	Ex+V	
	32	1.00		-379.21		3.38	1	•Ex+V	
• •	32	-0.21	-26.11		77.57	-0.52		Ey+V	
32(0)	32	-0.10	19.57	-373.52	-64.63	-0.18	1	•Ey+V	
33(4)	33	1.89	-5.36	-386.60	13.00	5.16	1	Vxmax	

						1	Versey
33(5) 33	0.64	-27,62	-391.45	82.32	1.16 1.32	1 1	Vymax Nmin
33(10) 33	0.65	21.68	-316.01	-70.57			Nmax
33(1) 33	0.75	-3.44	-407.97	6.81	1.44	0,	Mxmax
33(5) 33	0.64	-27.62	-391.45	82.32	1.16	1	
33(4) 33	1.89	-5.36	-386.60	13.00	5.16	1	Mymax V-V
33(1) 33	0.75	-3.44	-407.97	6.81	1.44	0	
33(0) 33	0.75	-3.44	-407.97	6.81	1.44	0	Wx+V
33(0) 33	0.75	-3.44	-407.97	6.81	1.44	0	-Wx+V
33(0) 33	0.75	-3,44	-407.97	6.81	1.44	0	₩y+\
33(0) 33	0.75	-3.44	-407.97	6.81	1.44	0	-Wy+V
33(0) 33 .	-0.49	-1.12	-385.17	-0.19	-2.45	1	Ex+V
33(0) 33	1.89	-5.36	-386.60	13.00	5.16	1	-Ex+V
33(0) 33	0.64	-27.62	-391.45	82.32	1.16	1	Ey+V
33(0) 33	0.76	21.14	-380.33	-69.50	1.54	1	-Ey+V
34(1) 34	-5.63	-2.53	-276.82	5.01	-11.23	0	Vxmax
34(5) 34	-5.23	-28.36	-272.25	85.53	-10.51	1	Vymax
34(10) 34	-4.36	23.92	-215.84	-76.75	-8.64	1	Nmin
34(1) 34	-5.63	-2.53	-276.82	5.01	-11.23	0	Nmax
34(5) 34	-5.23	-28.36	-272.25	85.53	-10.51	1	Mxmax
34(1) 34	-5.63	-2.53	-276.82	5.01	-11.23	0	Mymax
34(1) 34 .	-5.63	-2.53	·276.82	5.01	-11.23	0	V-V
34(0) 34	-5.63	-2.53	-276.82	5.01	-11.23	0	Wx+V
34(0) 34	-5.63	-2,53	-276.82	5,01	-11.23	0	-Wx+V
34(0) 34	-5.63	-2.53	-276.82	5.01	-11.23	0	Wy+V
34(0) 34	-5.63	-2.53	-276.82	5.01	-11.23	0	-₩y+V
34(0) 34	-6.19	-0.17	-266.53	-2.23	-13.77	1	Ex+V
34(0) 34	-4.28	-4.68	-265.93	11.81	-7.11	1	-Ex+V
34(0) 34	-5.23	-28.36	-272.25	85.53	-10.51	1	Ey+V
• •	-5.24	23.51	-260.21	-75.95	-10.38	1	-Ey+V
35(6) 35	-3.32	5.51	-387.18	-13.91	-9.04	ł	Vxmax
35(6) 35	-3.32	5.51			-9.04	3	Vymax
• •	-3.11	5.03	-322.85	-12.95	-8.61	1	Nmin
35(1) 35	-1.35	3.08	-408.09	•6.14	-2.73	0	Nmax
•	-3.32	5.51		-13.91	-9.04	1	Mxmax
35(6) 35	-3.32	5.51	-387.18	-13.91	-9.04	1	Mymax
35(1) 35	-1.35	3.08	-408.09	-6.14	-2.73	0	V-V
35(0) 35	-1.35	3.08	-408.09	-6.14	-2.73	0	Wx+V
35(0) 35 35(0) 35	-1.35	3.08	-408.09	-6.14	-2.73	0	-Wx+V
	-1.35	3.08	-408.09	-6.14	-2.73	0	Wy+\
35(0) 35 s	-1.35		-408.09		-2.73	0	-Wy+V
35(0) 35 35(0) 35	-1.55		-386.07		-6.90	1	•

Calcul	atio	on book	Oil Car Storage	- 43 - 2000 - 2010 - 2010				14-14-18-18-18 ⁻¹⁴ -12-	6
35( 0)	35	0.80	0.29	-384.89	· 2.35	3.93	1	Ey+V	
35( 0)	35	-3.32	5.51	-387.18	-13.91	-9.04	1	•Ey+V	
36( 5)	36	2.05	-0.92	-375.91	6.48	6.41	1	Vxmax	
36(6)	36	-1.74	7.39	-377.50	-19.38	-5.89	1	Vymax	
36(10)	36	-1.77	6.85	-314.72	-18.31	-5.94	1	Nmin	
36(1)	36	0.16	3.44	-398.15	-6.85	0.27	0	Nmax	
36(6)	36	-1.74	7.39	-377.50	-19.38	-5.89	1	Mxmax	
36(5)	36	2.05	-0.92	-375.91	6.48	6.41	1	Mymax	
36(1)	36	0.16	3.44	-398.15	-6.85	0.27	0	V-V	
36(0)	36	0.16	3.44	-398.15	-6.85	0.27	0	Wx+V	
36(0)	36	0.16	3.44	-398.15	-6.85	0.27	0	•₩x+V	
36(0)	36	0.16	3.44	-398.15	-6.85	0.27	0	Wy+V	
36(0)	36	0.16	3.44	-398.15	-6.85	0.27	0	•Wy+V	
36(0)	36	-1.17	3.58	-376.76	-7.53	-4.03	1	Ex+V	
36(0)	36	1.48	2.89	-376.65	-5.37	4.55	1	•Ex+V	
36(0)	36	2.05	-0.92	-375.91	6.48	6.41	1	Ey+V	
36( 0)	36	-1.74	7.39	-377.50	-19.38	-5.89	1	Ey+V	
37(5)	37	1.85	-2.45	-376.88	11.28	6.02	1	Vxmax	•
37(6)	37	-1.99	8.95	-379.56	-24.21	-6.38	1	Vymax	
37(10)	37	-1.98	8.40	-316.52	-23.13	-6.35	1	Nmin	
37(1)	37	-0.07	3.45	-399.76	-6.87	-0.20	0	Nmax	
37(6)	37	-1.99	8.95	-379.56	-24.21	-6.38	1	Mxmax	
37(5)	37	1.85	-2.45	-376.88	11.28	6.02	1	Мутах	
37(1)	37	-0.07	3.45	-399.76	-6.87	-0.20	0	<b>v-v</b>	
37(0)	.37	-0.07	3.45	-399.76	-6.87	-0.20	0	Wx+V	
37(0)	37	-0.07	3.45	-399.76		-0.20	0	-Wx+V	
37(0)	37	-0.07	3.45	-399.76	-6.87	-0.20	0	Wy+V	
37( 0)	37	-0.07	3.45	-399.76	-6.87	-0.20		-₩y+V	
37( 0)	37	-1.40	3.73	-378.34	-7.97	-4.48		Ex+V	
37( 0)	37	1.26	2.76	-378.10	-4.96			-Ex+V	
37(0)	37	1.85	-2.45	-376.88	11.28	6.02	1	Ey+V	
37( 0)	37	-1.99	8.95	-379.56				•Ey+V	
			, 			· · · _		• •	
38( 5)	38	1.91	-4.00	-376.54	16.09	6.14	1	Vxmax	
38( 6)	38	-1.92	10.49	-379.85	-29.03	-6.25	1	Vymax	
38(10)	38	-1.92	9.95	-316.82	-27.95			Nmin	
38(1)	38	-0.01	3.45	-399.74	-6.87	-0.06	0	Nmax	
38(-6)	38	-1.92	10.49	-379.85	-29.03	-6.25	1	Mxmax	
38(5)	38	1.91	-4.00	-376.54	16.09	6.14	1	Mymax	-
38(1)	38	-0.01	3.45	-399.74	-6.87	-0.06	0	v-v	
38( 0)	38	-0.01	3.45	-399.74	-6.87	-0.06	0	Wx+V	
38( 0)	38	-0.01	3.45	-399.74	-6.87	-0.06	0	-Wx+V	

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	38	-0.01	3.45	-399.74	-6.87 -6.87	-0.06 -0.06	0 0	Wy+V -Wy+V
38(0)	38	-0.01	3.45	-399.74	-8.39	-4.35	1	Ex+V
38(0)	38	-1.33	3.86	-378.33	-8.59 -4.54	4.24	1	-Ex+V
38(0)	38	1.32	2.63	-378.06	-4.54 16.09	4.24 6.14	1	Ey+V
38( 0) 38( 0)	38 38	1.91 -1.92	-4.00 10.49	-376.54 -379.85	-29.03	-6.25	1	-Ey+V
			10.04	270.00	-33.84	-6.63	1	Vxmax
39(6)	39	-2.11	12.04	-379.00	-33.84 -33.84	-6.63	1	Vymax
39(6)	39	-2.11	12.04	-379.00 -316.18	-32.76	-6.55	1	Nmin
39(10)	39 20	-2.08	11.50 3.45	-398.37	-6.87	-0.48	0	Nmax
39(1)	39 20	-0.22	3.43 12.04	-379.00	-33.84	-6.63	1	Mxmax
39(6)	39 · 39 ·	-2.11 -2.11	12.04	-379.00	-33.84	-6.63	1	Mymax
39(6) 39(1)	39 39	-0.22	3.45	-398.37	-6.87	-0.48	0	V-V
39(0)	39 39	-0.22	3,45	-398.37	-6.87	-0.48	0	Wx+V
39(0) 39(0)	39	-0.22	3.45	-398.37	-6.87	-0.48	0	-Wx+V
39(0)	39	-0.22	3.45	-398.37	-6.87	-0.48	0	Wy+V
39(0)	39	-0.22	3.45	-398.37	-6.87	-0.48	0	-Wy+V
39(0)	39	-1.53	4.00	-377.13	-8.82	-4.74	1	Ex+V
39(0)	39	1.12	2.49	-376.70	-4.12	3.83	I	-Ex+V
39(0)	39	1.70	-5.54	-374.82	<b>20.9</b> 0	5.72	1	Ey+V
39( 0)	39	-2.11	12.04	-379.00	-33.84	-6.63	1	-Ey+V
40( 5)	40	2.99	-7.15	-383.21	25.82	8.28	1	Vxma
40(6)	40	-0.95	13.53	-387.23	-38.54	-4.33	1	Vymax
40(10)	40	-1.12	13.00	-323.02	-37.48	-4.66	1	Nmin
40(1)	40	1.08	3.39	-407.20	-6.75	2.09	0	Nmax
40(6)	40	-0.95	13.53	-387.23	-38.54	-4.33	1	Mxmax
40(5)	40	2.99	-7.15	-383.21	25.82	8.28	1	Myma
40(1)	40	1.08	3.39	-407.20	-6.75	2.09	0	V-V
40( 0)	40	1.08	3.39	-407.20	-6.75	2.09	0	Wx+
40( 0)	40	1.08	3.39	-407.20	-6.75	2.09	0	-Wx+V
40( 0)	40	1.08	3.39	-407.20	-6.75	2.09	0	Wy+
40( 0)	40	·s 1.08	3.39	-407.20	-6.75	2.09	0	•Wy+\
40( 0)	40	-0.35	4.08	-385.16	-9.13	-2.40	1	Ex+V
40(0)	40		2.30	-385.28	-3.59	6.35	1	•Ex+V
40( 0)	40	2.99	-7.15	-383.21	25.82	8.28	1	Ey+V
40 <b>( 0)</b>	40	-0.95	13.53		-38.54	-4.33	1	-Ey+V
41(1)	41		2,53		-5.06		0	Vхлах
41(6)	41	-8.73	14.31	•			1	Vymax
41(10)	41	-7.54	13.90	-222.68			1	Nmin
41(1)	41	-7,63	2.53	. 272 73	-5.06	-15.22	0	Nmax

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41(6)	41	-8.73	14.31	-266.40	-41.83	-19.78	1	Mymax
. ,	41	-7.63	2.53	-272.73	-5.06	-15.22	Ð	<b>V-V</b>
	41	-7.63	2.53	-272.73	-5.06	-15.22	0	Wx+V
	41	-7.63	2.53	-272.73	-5.06	-15.22	0	-Wx+V
	41	-7.63	2.53	-272.73	-5.06	-15.22	0	Wy+V
• • •	41	-7.63	2.53	-272.73	-5.06	-15.22	0	•Wy+V
	41	-8.25	3.45	-263.52	-8.03	-18.09	1	Ex+V
41(0)	41	-6.08	1.40	-261.17	-1.66	-10.46	1	-Ex+V
41(0)	41	-5.59	-9.45	-258.29	32.15	-8.77	1	Ey+V
41(0)	41	-8.73	14.31	-266.40	-41.83	-19.78	1	-Ey+V
42(1)	42	7.57	2.53	-272.67	-5.06	14.99	0	Vxmax
42(6)	42	5.53	14.45	-263.74	-42.26	8.56	1	Vymax
42(10)	42	4.35	14.04	-220.03	-41.45	6.22	1	Nmin
42(1)	42	7.57	2.53	-272.67	-5.06	14.99	0	Nmax
42(6)	42	5.53	14.45	-263.74	-42.26	8.56	1	Mxmax
42(5)	42	8.67	-9.59	-260.84	32.58	19.57	ł	Mymax
42(1)	42	7.57	2.53	-272.67	-5.06	14.99	0	• <b>V-V</b>
42(0)	42	7.57	2.53	-272.67	-5.06	14.99	0	Wx+V
42(0)	42	7.57	2.53	-272.67	-5.06	14.99	0	-Wx+V
42(0)	42	7.57	2.53	-272.67	-5.06	14.99	0	` ₩y+V
42(0)	42	7.57	2.53	-272.67	-5.06	14.99	0	•Wy+V
42(0)	42	6.02	3.46	-261.59	-8.07	10.25	1	Ex+V
42(0)	42	8.19	1.39	-262.99	-1.61	17.89	1	-Ex+V
42(0)	42	8.67	-9.59	-260.84	32.58	19.57	1	Ey+V
42( 0)	42	5.53	14.45	-263.74	-42.26	8.56	1	-Ey+V
43(3)	43	-2.46	4.36	-385.77	-10.01	-6.59	ł	Vxmax
43(6)	43	-3.06	16.76	-388.74	-48.59	-8.52	1	Vymax
43(10)	43	-2.88	16.22	-324.53	-47.53	-8.15	1	Nmin
43(1)	43	-1.16	3.39	-407.22	-6.75	-2.35	0	Nmax
43(6)	43	-3.06	16.76	-388.74	-48.59	-8.52	1	Mxmax
43(6)	43	-3.06	16.76	-388.74	-48.59	-8.52	1	Mymax
43(1)	43	-1.16	3.39	-407.22	-6.75	-2.35	0	V-V
43(0)	43	-1.16	3.39	-407.22	-6.75	-2.35	0	Wx+V
43(0)	43	-1.16	3.39	-407.22	-6.75	-2.35	0	-Wx+V
43(0)	43	-1.16	3.39	-407.22	-6.75	-2.35	0	⁺ Wy+V
43(0)	43	-1.16	3.39	-407.22	-6.75	-2.35	Ð	-Wy+V
43(0)	43	-2.46	4.36	-385.77	-10.01	-6.59	1	Ex+V
43(0)	43	0.28	2.02	-384.70	-2.72	2.16	1	-Ex+V
43(0)	43	0.88	-10.37	-381.73	35.87	4.09	1	Ey+V
43(0)	43	-3.06	16.76	-388.74		-8.52	1	•Ey+V
44( 5)	44	2.04	-11.86	-373.48	40.57	6.40	1	Vxmax

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alculation	book o	Dil Car Storage	) 	والمستقدم والمراجع والمراجع والمراجع والمعارفين والمعارفين والمعارفين والمعارفين والمعارفين والمعارفين			ny manager manada yana an
44(6) 44	-1.77	18.36	-380.33	-53.51	-5.96	1	Vymax
44(10) 44	-1.79	17.82	-317.51	-52.44	-5.99	1	Nmin
44(1) 44	0.14	3.45	-398.37	-6.87	0.23	0	Nmax
44(6) 44	-1.77	18.36	-380.33	-53.51	-5.96	1	Mxmax
44(5) 44	2.04	-11.86	-373.48	40.57	6.40	1	Mymax
44(1) 44	0.14	3.45	-398.37	-6.87	0.23	0	V-V
44(0) 44	0.14	3.45	-398.37	-6.87	0.23	0	Wx+V
44(0) 44	0.14	3.45	-398.37	-6.87	0.23	0	-Wx+V
44(0) 44	0.14	3.45	-398.37	-6.87	0.23	0	₩y+\
44(0) 44	0.14	3.45	-398.37	-6.87	0.23	0	-₩y+V
44(0) 44	-1.19	4.55	-377.16	-10.54	-4.05	1	Ex+V
44(0) 44	1.46	1.94	-376.65	-2.41	4.50	1	-Ex+V
44(0) 44	2.04	-11.86	-373.48	40.57	6.40	1	Ey+V
44(0) 44	-1.77	18.36	-380.33	-53.51	-5.96	1	-Ey+V
45(5) 45	1.85	-13.41	-374.38	45.38	6.03	1	Vxmax
45(6) 45	-1.98	19.90	-382.07	-58.33	-6.37	1	Vymax
45(10) 45	-1.97	19.36	-319.04	-57.25	-6.34	1	Nmin
45(1) 45	-0.07	3.45	-399.77	-6.88	-0.18	0	Nmax
45(6) 45	-1.98	19.90	-382.07	-58.33	-6.37	1	Mxmax
45(5) 45	1.85	-13.41	-374.38	45.38	6.03	1	Mymax
45(1) 45	-0.07	3.45	-399.77	-6.88	-0.18	0	V-V
45(0) 45	-0.07	3.45	-399.77	-6.88	-0.18	0	Wx+V
45(0) 45	-0.07	3.45	-399.77	-6.88	-0.18	0	-Wx+V
45(0) 45	-0.07	3.45	-399.77	-6.88	-0.18	0	Wy+V
45(0) 45	-0.07	3.45	-399.77	-6.88	-0.18	0	-Wy+V
45(0) 45	-1.39	4.69	-378.57	-10.97	-4.47	1	Ex+V
45(0) 45	1.27	1.81	-377.89	-1.99	4.13	1	-Ex+V
45(0) 45	1.85	-13.41	-374.38	45.38	6.03	3	Ey+\
45(0) 45	-1.98	19.90			-6.37	1	-Ey+V
46(5) 46	1.88		-373.82		6.09	l	Vxma
46(6) 46	-1.95	21.45	-382.21	-63.14	-6.30	ł	Vymax
46(10) 46	-1.94	20.91	-319.21	-62.06	-6.28	1	Nmin
46(1) 46	-0.03	3.45	-399.55	-6.88	-0.12	0	Nmax
46(6) 46	-1.95	21.45	-382.21	-63.14	-6.30	1	Mxmax
	1.88	-14.95	-373.82	50.19	6.09	1	Myma
46(1) 46	-0.03	3.45	-399.55	-6.88	-0.12	0	V-V
• •	-0.03	3.45	-399,55	-6.88	-0.12	0	Wx+V
46(0) 46	-0.03	3.45	-399.55	-6.88	-0.12	0	-Wx+V
46(0) 46	•0.03	3.45	-399.55	-6.88	-0.12	0	Wy+V
. ,	-0.03	3.45	-399.55	•6.88	-0.12	0	-Wy+V
	-1.36	4.83	-378.38	-11.39	-4.40	1	Ex+V
46(0) 46	1.30	1.67	-377.66	-1.57	4.19	1	-Ex+V

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Ey+V	1	6.09	50.19	-373.82	-14.95	1.88	46	46( 0)
-Ey+V	ł	-6.30	-63.14	-382.21	21.45	-1.95	46	46( 0)
Vxmax	1	6.07	55.00	-373.48	-16.50	1.87	47	47( 5)
Vymax	1	-6.32	-67.95	-382.58	23.00	-1.95	47	47(6)
Nmin	1	-6.30	-66.87	-319.58	22.45	-1.95	47 ·	47(10)
Nmax	0	-0.14	-6.88	-399.56	3.45	-0.04	47	47(1)
Mxmax	1	6.07	55.00	-373.48	-16.50	1.87	47	47(5)
Mymax	1	6.07	55.00	-373.48	-16.50	1.87	47	47(5)
V-V	0	-0.14	-6.88	-399.56	3.45	-0.04	47	47(1)
Wx+V	0	-0.14	-6.88	-399.56	3.45	-0.04	47	47(0)
-Wx+V	0	-0.14	-6.88	-399.56	3.45	-0.04	47	47( 0)
₩y+V	0	-0.14	-6.88	-399.56	3.45	•0.04	47	47(0)
-Wy∻V	0	-0.14	-6.88	-399.56	3.45	-0.04	47	47(0)
Ex+V	1	-4.42	-11.81	-378.42	4.96	-1.37	47	47(0)
-Ex+V	1	4.17	-1.15	-377.63	1.54	1.29	47	47(0)
Ey+V	1	6.07	55.00	-373.48	-16.50	1.87	47	47(0)
-Ey+V	l	-6.32	-67.95	-382.58	23.00	-1.95	47	47( 0)
Vxmax	1	6.12	59.81	-373.27	-18.04	1.90	48	48( 5)
Vymax	1	-6.28	-72.77	-383.07	24.54	-1.93	48	48(6)
Nmin	1	-6.26	-71.69	-320.04	24.00	-1.93	48	48(10)
Nmax	0	-0.09	-6.88	-399.71	3.45	-0.02	48	48(1)
Mxmax	1	6.12	59.81	-373.27	-18.04	1.90	48	48(5)
Mymax	1	6.12	59.81	-373.27	-18.04	1.90	48	48( 5)
V-V	0	-0.09	-6.88	-399.71	3.45	-0.02	48	48(1)
Wx+V	0	-0.09	-6.88	-399.71	3.45	-0.02	48	48(0)
-Wx+V	0	-0.09	-6.88	-399.71	3.45	-0.02	48	48(0)
Wy+V	0	-0.09	-6.88	-399.71	3.45	-0.02	48	48(0)
-Wy+V	0	-0.09	-6.88	-399.71	3.45	-0.02	48	48(0)
Ex+V	1	-4.38	-12.23	-378.59	5.10	-1.35	48	48(0)
-Ex+V	ł	4.22	-0.73	-377.75	1.40	1.31	48	48(0)
Ey+V	1	6.12	59.81	-373.27	-18.04	1.90	48	48(0)
-Ey+V	1		-72.77	-383.07	24.54	-1.93	48	48( 0)
Vxmax	1	-6.53	-77.58	-382.59	26.09	-2.06	49	 49( 6)
Vymax		-6.53				-2.06	49	49(6)
Nmin			-76.50	-319.71	25.55	-2.03		49(10)
Nmax	0	-0.38	-6.88	-398.73	3.45	-0.17	49	49(1)
Mxmax			64.62	-371.93	-19.59	1.75		49(5)
Mymax			64.62	-371.93	-19.59	1.75		49(5)
V-V		-0.38	-6.88	-398.73	3.45	-0.17	49	49(1)
Wx+V		-0.38	-6.88	-398.73	3.45	-0.17	49	49(0)
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aicuid	111011		Oil Car Storage	-	<u></u>			
49( 0)	49	•0.17	3.45	-398.73	-6.88	-0.38	0	Wy+V
•••	49	-0.17	3.45	-398.73	<b>-6.88</b>	-0.38	0	•Wy+V
• •	49 ·	-1.48	5.23	-377.76	-12.66	-4.63	1	Ex+V
	49 ·	1.17	1.27	-376.76	-0.31	3.93	1	-Ex+V
	49	1.75	-19.59	-371.93	64.62	5.82	1	Ey+V
49( 0)	49	-2.06	26.09	-382.59	-77.58	-6.53	1	-Ey+V
50( 5)	50	2.68	-21.17	-379.16	69.50	7.67	1	Vxmax
50( 6)	50	-1.27	27.60	-389.54	-82.33	-4.97	1	Vymax
50(10)	50	-1.39	27.06	-325.48	-81.26	-5.19	1	Nmin
50(1)	50	0.75	3.41	-406.33	-6.81	1.44	0	Nmax
50( 5)	50	2.68	-21.17	-379.16	69.50	7.67	1	Mxma
50( 5)	50 ·	2.68	-21.17	-379.16	69.50	7.67	1	Myma
50(1)	50	0.75	3.41	-406.33	-6.81	1.44	0	٧-٧
50( 0)	50	0.75	3.41	-406.33	-6.81	1.44	0	Wx+'
50( 0)	50	0.75	3.41	-406.33	-6.81	1.44	0	-Wx+V
50(0)	50	0.75	3.41	-406.33	-6.81	1.44	0	Wy+'
50( 0)	50	0.75	3.41	-406.33	-6.81	1.44	0	-Wy+V
50(0)	50	-0.66	5.34	-384.57	-13.01	-3.02	1	Ex+V
50(0)	50	2.07	1.10	-384.13	0.18	5.73	1	-Ex+V
50(0)	50	2.68	-21.17	-379.16	69.50	7.67	1	Ey+V
50(0)	50	-1.27	27.60	-389.54	-82.33	-4.97	1	-Ey+V
51(1)	51	-5.64	2.54	-275.99	-5.08	-11.25	0	Vxmax
51(5)	51	-3.72	-23.50	-258.11	75.87	-5.04	1	Vymax
51(10)	51	-5.89	27.97	-228.55	-84.79	-14.13	1	Nmin
51(1)	51	-5.64	2.54	-275.99	-5.08	-11.25	0	Nmax
51(5)	51	-3.72	<b>-23</b> .50	-258.11	75.87	-5.04	1	Mxmax
51(3)	51	-6.32	4.69	-266.91	-11.88	-14.27	1	-
51(1)	51	-5.64	2.54	-275.99	-5.08	-11.25	0	<b>V-V</b>
51(0)	51	-5.64	2.54	-275.99	-5.08	-11.25	0	Wx+\
51(0)	51 -	-5.64	2.54	-275.99	-5.08	-11.25	0	-Wx+V
51(0)	51	-5.64	2.54	-275.99	-5.08	-	0	Wy+V
51(0)	51	-5.64	2.54	-275.99	-5.08		0	•
51(0)	51	-6.32	4.69	-266.91	-11.88	-14.27	1	Ex+V
51(0)	51	-4.16	0.18					•Ex+V
51(0)	51	-3.72	-23.50	-258.11	75.87	-5.04	1	Ey+V
51(0)	- 51	-6.76	28.37	-272.79	-85.60	-15.87	1	-Ey+V
			-16.90		36.49	12.39		Vxma
			-15.63	-		0.11		Vyma
52(10)	52	•3.69	-10.07	-217.41				Nmin
52(1)	52	0.08	-15.63	-276.22	31.03	0.11	0	Nmax
52(1)	52	0.08	-15.63	-276.22	31.03	0.11	0	Mxma

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52(5)	52	3.83	-16,90	-265.83	36.49	12.39	ł	Mymax
52(1)	52	0.08	-15.63	-276.22	31.03	0.11	0	V-V
52(0)	52	0.08	-15.63	-276.22	31.03	0.11	0	Wx+V
52( 0)	52	0.08	-15.63	-276.22	31.03	0.11	0	-Wx+V
52( 0)	52	0.08	-15.63	-276.22	31.03	0.11	0	Wy+V
52( 0)	52	0.08	-15.63	-276.22	31.03	0.11	0	-Wy+V
52( 0)	52	-1.43	-14.53	-263.49	28.61	-4.76	1	Ex+V
52( 0)	52	1.59	-14.89	-263.69	29.80	4.99	1	-Ex+V
52( 0)	52	3.83	-16.90	-265.83	36.49	12.39	1	Ey+V
52(0)	52	-3.68	-12.52	-261.34	21.91	-12.17	1	-Ey+V
53( 5)	53	3.85	-18.68	-266.41	41.78	12.42	1	Vxmax
53(1)	53	-0.06	-16.12	-276.89	32.01	-0.16	0	Vymax
53(10)	53	-3.94	-9.13	-218.01	13.45	-12.69	1	Nmin
53(1)	53	-0.06	-16.12	-276.89	32.01	-0.16	0	Nmax
53( 5)	53	3.85	-18.68	-266.41	41.78	12.42	1	Mxmax
53( 5)	53	3.85	-18.68	-266.41	41.78	12.42	1	Mymax
53(1)	53	-0.06	-16.12	-276.89	32.01	-0.16	0	V-V
53( 0)	53	-0.06	-16.12	-276.89	32.01	-0.16	0	Wx+V
53(0)	53	-0.06	-16.12	-276.89	32.01	-0.16	0	-Wx+V
53(0)	53	-0.06	-16.12	-276.89	32.01	-0.16	0	₩y+V
53(0)	53	-0.06	-16.12	-276.89	32.01	-0.16	0	-Wy+V
53(0)	53	-1.55	-14.88	-264.02	29.15	-4.99	1	Ex+V
53(0)	53	1.45	-15.47	-264.44	31.10	4.70	1	-Ex+V
53(0)	53	3.85	-18.68	-266.41	41.78	12.42	1	Ey+V
53(0)	53	-3.95	-11.66	-262.05	18.47	-12.71	1	-Ey+V
54( 5)	54	3.84	-20.01	-267.22	46.15	12.40	1	Vxmax
54(1)	54	-0.04	-16.14	-276.67	32.05	-0.14	0	Vymax
54(10)	54	-3.91	-7.84	-216.82	9.14	-12.63	1	Nmin
54(1)	54	-0.04	-16.14	-276.67	32.05	-0.14	0	Nmax
54( 5)	54	3.84	-20.01	-267.22	46.15	12.40	1	Mxmax
54( 5)	54	3.84	-20.01	-267.22	46.15	12.40	1	Mymax
54(1)	54	-0.04	-16.14	-276.67	32.05	-0.14	0	<b>V-V</b>
54( 0)	54	-0.04	-16.14	-276.67	32.05	-0.14	0	Wx+V
54( 0)	54	-0.04	-16.14	-276.67	32.05	-0.14	0	-Wx+V
54( 0)	54	-0.04	-16.14	-276.67	32.05	-0.14	0	Wy+V
54( 0)	54	-0.04	-16.14	-276.67	32.05	-0.14	0	-Wy+V
54( 0)	54	-1.54	-14.78	-263.76	28.80	-4.98	1	Ex+V
54( 0)	54	1.46	-15.60	-264.29	31.52	4.73	- 1	•Ex+V
54(0)	54	3.84	-20.01	-267.22	46.15	12.40	ł	Ey+V
54( 0)	54	-3.92	-10.37	-260.82	14.17	-12.65	1	•Ey+V
55( 5)	55	3.88	-21.31	-268.35	50.48	12.48	1	Vxmax

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55( 5) 55	3.88	-21.31	-268.35	50.48	12.48	1	Vymax
55(10) 55	-3.89	-6.53	-216.19	4.80	-12.58	1	Nmin
55(1) 55	-0.01	-16.14	-276.96	32.04	-0.06	0	Nmax
55( 5) 55	3.88	-21.31	-268.35	50.48	12.48	1	Mxmax
55( 5) 55	3.88	-21.31	-268.35	50.48	12.48	1	Mymax
55(1) 55	-0.01	-16.14	-276.96	32.04	-0.06	0	V-V
55(0) 55	-0.01	-16.14	-276.96	32.04	-0.06	0	₩x+V
55( 0) 55	-0.01	-16.14	-276.96	32.04	-0.06	Ð	-Wx+V
55(0) 55	-0.01	-16.14	-276.96	32.04	-0.06	0	Wy+V
55( 0) 55	-0.01	-16.14	-276.96	32.04	-0.06	0	-Wy+V
55(0) 55	-1.51	-14.67	-263.94	28.42	-4.91	1	Ex+V
55(0) 55	1.50	-15.71	-264.65	31.89	4.80	1	-Ex+V
55(0) 55	3.88	-21.31	-268.35	50.48	12.48	1	Ey+V
55(0) 55	-3.89	-9.07	-260.24	9.83	-12.59	1	-Ey+V
56(5) 56	3.63	-22.63	-267.47	54.83	11.98	1	Vxmax
56(5) 56	3.63	-22.63	-267.47	54.83	11.98	1	Vymax
56(10) 56	-4.06	-5.23	-214.12	0.47	-12.93	ł	Nmin
56(1) 56	-0.25	-16.15	-275.27	32.06	-0.55	0	Nmax
56(5) 56	3.63	-22.63	-267.47	54.83	11.98	1	Mxma
56(5) 56	3.63	-22.63	-267.47	54.83	11.98	1	Mymax
56(1) 56	-0.25	-16.15	-275.27	32.06	-0.55	0	V-V
56(0) 56	-0.25	-16.15	-275.27	32.06	-0.55	0	Wx+V
56(0) 56	-0.25	-16.15	-275.27	32.06	-0.55	0	-Wx+V
56(0) 56	-0.25	-16.15	-275.27	32.06	-0.55	0	`Wy+V
56(0) 56	-0.25	-16.15	-275.27	32.06	-0.55	0	-Wy+V
56(0) 56	-1.73	-14.56	-262.31	28.05	-5.35	1	Ex+V
56(0) 56	1.26	-15.83	-263.06	32.28	4.32	1	-Ex+V
56(0) 56		-22.63	-267.47	54.83	11.98	1	Ey+V
56(0) 56	-4.10	-7.77		5.50	-13.01	Į	∙Ey+V
57(5) 57			-279.60		15.17	1	Vxmax
57(5) 57			-279.60	58.79	15.17	1	Vymax
57(10) 57			-221.05	-4.16	-10.72	1	Nmin
57(1) 57	1.31	-15.94	-286.21	31.65	2.55	0	Nmax
57(5) 57			-279.60	58.79	15.17	1	Mxma
57(5) 57			-279.60	58.79	15.17	1	Myma
	1.31		-286.21	31.65	2.55	0	V-V
57(0) 57	1.31	-	-286.21	31.65	2.55	0	Wx+V
57(0) 57		-15.94	-286.21	31.65	2.55	0	-Wx+V
	1.31	-15.94		31.65	2.55	0	Wy+V
•	1.31			31.65	2.55	0	-Wy+∖
	-0.30	-		27.31	-2.51	1	Ex+V
57(0) 57	2.79	-15.76		32.29	7.36	1	-Ex+V

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(	Calcul	ation	book	Oil Car Storag	¢					7
	57(0)	57	5.23	-23.74	-279.60	58.79	15.17	1	Ey+V	
	57(0)	57	-2.74	-6.28	-266.56	0.80	-10.32	ł	-Ey+V	
					*****				· . ·	
	58( 6)	58	-11.48	-1.24	-161.20	-10,95	-27.68	1	Vxmax	
	58( 5)	58	-5.08	-21.39	-168.94	55.86	-5.32	1	Vymax	
	58(10)	<b>58</b> -	-10.10	0.65	-133.69	-14.69	-24.93	1	Nmin	
	58(1)	58	-8.71	-11.80	-170.99	23.43	-17.35	0	Nmax	
	58( 5)	58	-5.08	-21.39	-168.94	55.86	-5.32	1	Mxmax	
	58( 6)	58	-11.48	-1.24	-161.20	-10.95	-27.68	1	Mymax	
	58(1)	58	-8.71	-11.80	-170.99	23.43	-17.35	0	• <b>V-V</b>	
	58( 0)	58	-8.71	-11.80	-170.99	23.43	-17.35	0	Wx+V	
	58( 0)	58	-8.71	-11.80	-170.99	23.43	-17.35	0	-Wx+V	
	58( 0)	58	-8.71	-11.80	-170.99	23.43	-17.35	0	∵ Wy+V	
	58( 0)	58	-8.71	-11.80	-170.99	23.43	-17.35	0	-Wy+V	
	58( 0)	58	-9.51	-10.44	-165.58	19.56	-20.81	1	Ex+V	
	58( 0)	58	-7.05	-12.19	-164.56	25.34	-12.18	1	-Ex+V	
	58( 0)	58	-5.08	-21.39	-168.94	55.86	-5.32	1	Ey+V	
	58( 0)	58	-11.48	-1.24	-161.20	-10.95	-27.68	1	-Ey+V	
	59( 5)	59	11.42	-21.44	-174.49	56.11	27.47	1	Vxmax	
	59( 5)	59	11.42	-21.44	-174.49	56.11	27.47	1	Vymax	
	59(10)	59	3.65	0.70	-128.05	-14.94	2.39	ł	Nmin	·
	59(1)	59	8.64	-11.81	-170.93	23.43	17.12	0	Nmax	
	59( 5)	59	11.42	-21.44	-174.49	56.11	27.47	1	Mxmax	
	59( 5)	59	11.42	-21.44	-174.49	56.11	27.47	1	Mymax	
	59(1)	59	8.64	-11.81	-170.93	23.43	17.12	0	<b>V-V</b>	
	59( 0)	. 59	8.64	-11.81	-170.93	23.43	17.12	0	Wx+V	
	59( 0)	59	8.64	-11.81	-170.93	23.43	17.12	0	•Wx+V	
	59( 0)	59	8.64	-11.81	-170.93	23.43	17.12	0	Wy+V	
	59( 0)	59	8.64	-11.81	-170.93	23.43	17.12	0	•Wy+V	
	59( 0)	59	6.99	-10.45	-163.36	19.56	11.97	1	Ex+V	
	59( 0)	59	9.45	-12.18	-166.67	25.34	20.60	1	•Ex+V	·
	59( 0)	59	11.42	-21.44	-174.49	56.11	27.47	1	Ey+V	
	59( 0)	<b>59</b>	5.02	-1.19	-155.55	-11.20	5.11	1	-Ey+V	•
						**********			•	
	60( 6)		-5.31	-3.54	-266.28	-8.27	-15.41	1	Vxmax	
	60( 5)	60	2.67	-26.48	-279.91	67.86	10.08	1	Vymax	
	60(10)	60	-5.09	-1.04	-220.76	-13.24	-14.97	1	Nmin	·
	60(1)	60	-1.39	-15.94	-286.22	31.65	-2.81	0	Nmax	·
	60(-5)	60	2.67	-26.48	-279.91	67.86	10.08	1	Mxmax	
	60( 6)	60	-5.31	-3.54	-266.28	-8.27	-15.41	1	Mymax	
	60(1)	60	-1.39	-15.94	-286.22	31.65	-2.81	0	· V-V	·
	60( 0)	60	-1.39	-15.94	-286.22	31.65	-2.81	0	Wx+V	
	60( 0)	60	-1.39	-15.94	-286.22	31.65	-2.81	0	-Wx+V	1

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60( 0)	60	-1.39	-15.94	-286.22	31.65	-2.81	0	Wy+V
60( 0)	60 ⁻	-1.39	-15.94	-286.22	31.65	-2.81	0	-Wy+V
60( 0)	60	-2.86	-14.02	-272.74	26.50	-7.60	1	Ex+V
60( 0)	60 ⁻	0.23	-16.00	-273.45	33.08	2.27	1	-Ex+V
60(0)	60	2.67	-26.48	-279.91	67.86	10.08	1	Ey+V
60( 0)	60	-5,31	-3.54	-266.28	-8.27	-15.41	1	-Ey+V
61(5)	61	4.03	-27.96	-271.23	72.56	12.78	١	Vxmax
61( 5)	61	4.03	-27.96	-271.23	72.56	12.78	1	Vymax
61(10)	61	-3.73	0.11	-210.35	-17.26	-12.26	1	Nmin
61(1)	61	0.17	-16.15	-275.26	32.05	0.29	0	Nmax
61(5)	61	4.03	-27.96	-271.23	72.56	12.78	1	Mxma
61(5)	61 '	4.03	-27.96	-271.23	72.56	12.78	1	Myma
61(1)	61	0.17	-16.15	-275.26	32.05	0.29	0	<b>V-V</b> .
61(0)	61	0.17	-16.15	-275.26	32.05	0.29	0	Wx+V
61(0)	61	0.17	-16.15	-275.26	32.05	0.29	0	-Wx+\
61(0)	61	0.17	-16.15	-275.26	32.05	0.29	0	₩у+`
61(0)	61	0.17	-16.15	-275.26	32.05	0.29	0	-Wy+\
61(0)	61	-1.33	-14.09	-261.90	26.50	-4.55	ł	Ex+V
61(0)	61	1.66	-16.30	-263.46	33.83	5.12	1	•Ex+V
61(0)	61	4.03	-27.96	-271.23	72.56	12.78	1	Ey+V
61(0)	61	-3.70	-2.42	-254.13	-12.23	-12.21	1	-Ey+V
62( 5)	62	3.81	-29.26	-273.57	76.88	12.35	1	Vxma
62(5)	62	3.81	-29.26	-273.57	76.88	12.35	1	Vyma
62(10)	62	-3.94	1.42	-210.97	-21.60	-12.69	1	Nmin
62(1)	62	-0.07	-16.14	-276.96	32.04	-0.20	0	Nmax
62(5)	62	3.81	-29.26	-273.57	76.88	12.35	1	
62(5)	62	3.81	-29.26	-273.57	76.88	12.35		•
62(1)	<b>62</b>	-0.07	-16.14	-276.96		-0.20		V-V
62( 0)	62	-0.07	-16.14	-276.96		-0.20	0	Wx+\
62( 0)	62					-0.20	0	-Wx+V
62( 0)	62	-0.07	-16.14	-276.96		-0.20		Wy+\
62( 0)	62	-0.07	-16.14	-276.96		-0.20	0	-
62( 0)	62	-1.57	-13.97			-5.03	1	
62( 0)	62	1.43	-16.41	-265.09				-Ex+V
62( 0)	62	3.81	-29.26	-273.57	76.88			Ey+\
62(0)	62			-255.02		-12.72	1	∙Ey+V
	63	3.85	-30.57	-274.20	81.22	[.] 12.42		Vxma
			-30.57			12.42		•
63(10)	) 63	-3.90	2.73	-209.88		-		
63(1)	63	-0.03	-16.14					
63( 5)	63	3.85	-30.57	-274.20	81.22	12,42	1	Mxma

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