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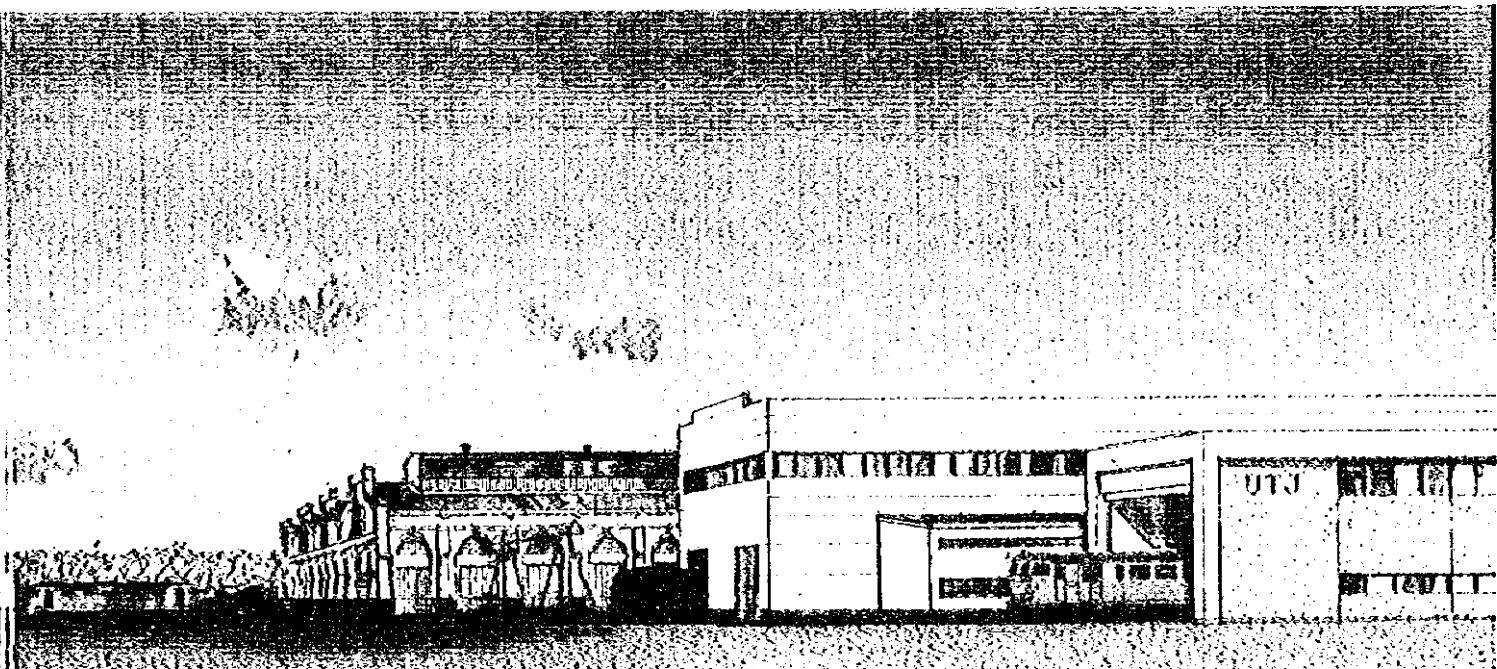
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REPUBLIC OF UZBEKISTAN

社会開発調査部報告書

THE FEASIBILITY STUDY
ON
THE CONSTRUCTION OF ELECTRIC LOCOMOTIVE REPAIR
WORKSHOP
IN
UZBEKISTAN

FINAL REPORT
APPENDIX



JULY 1997

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JAPAN RAILWAY TECHNICAL SERVICE
JAPAN TRANSPORTATION CONSULTANTS, INC.
PACIFIC CONSULTANTS INTERNATIONAL

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JICA
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WORKSHOP IN UZBEKISTAN
FINAL REPORT
JULY 1997
JAPAN INTERNATIONAL COOPERATION AGENCY
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APPENDIX**

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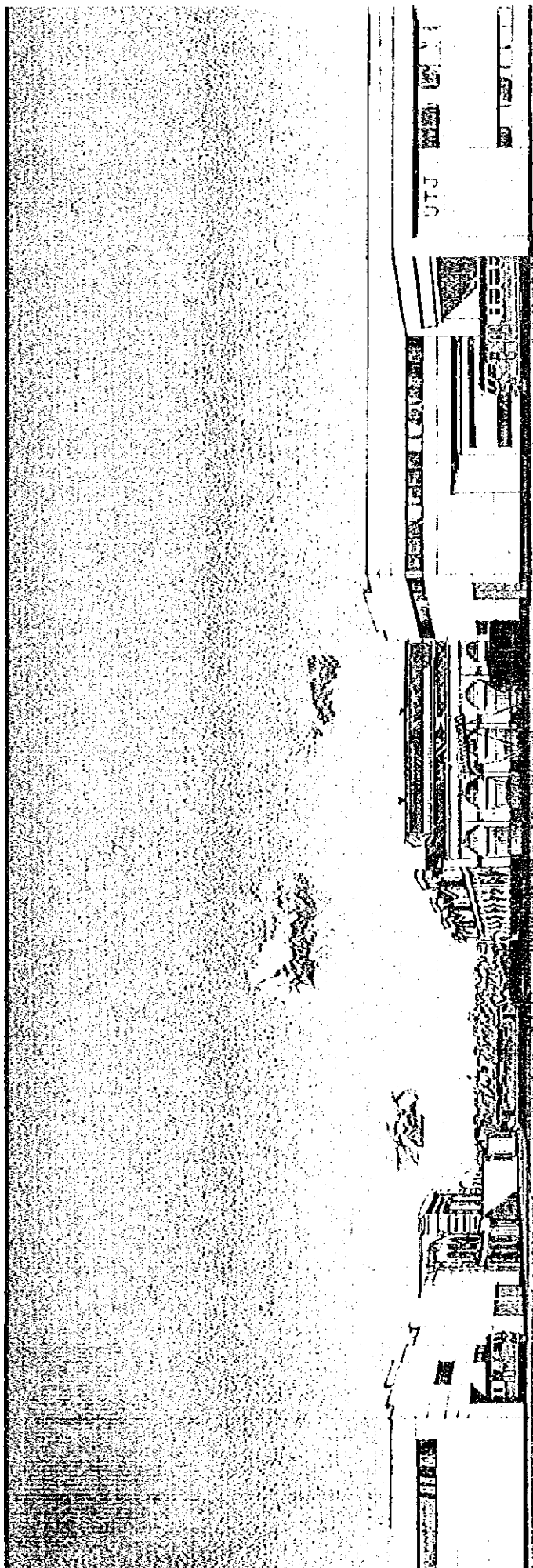
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Application date January , 1997



ELECTRIC LOCOMOTIVE REPAIR WORKSHOP

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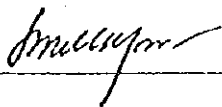
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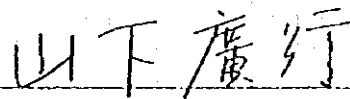
Appendix 1 Scope of Work for The Feasibility Study on the Construction of Electric Locomotive Repair Workshop in Uzbekistan Agreed Upon Between Uzbekistan Railways and Japan International Cooperation Agency

SCOPE OF WORK
FOR
THE FEASIBILITY STUDY
ON
THE CONSTRUCTION OF ELECTRIC LOCOMOTIVE REPAIR WORKSHOP
IN
UZBEKISTAN
AGREED UPON BETWEEN
UZBEKISTAN RAILWAYS
AND
JAPAN INTERNATIONAL COOPERATION AGENCY

Tashkent , July 18 , 1996



Mr. Mikhail Z. MARTYANOV
Vice Chairman
Uzbekistan Railways



Mr. Hiroyuki YAMASHITA
Leader
Preparatory Study Team
Japan International
Cooperation Agency

I. INTRODUCTION

In response to the request of the Government of Uzbekistan, the Government of Japan decided to conduct the Feasibility Study on the Construction of Electric Locomotive Repair Workshop in Uzbekistan (hereinafter referred to as "the Study") in accordance with the relevant laws and regulations in force in Japan.

Accordingly, the Japan International Cooperation Agency (hereinafter referred to as "JICA"), the official agency responsible for the implementation of the technical cooperation programs of the Government of Japan, will undertake the Study, in close cooperation with the authorities concerned of the Government of Uzbekistan.

The present document sets forth the Scope of Work with regard to the Study.

II. OBJECTIVES OF THE STUDY

The objectives of the study for the project are to organise the base for repair workshop, to conduct a feasibility study on the construction of electric locomotive repair workshop in Uzbekistan.

III. STUDY AREA

The study area to be covered is Uzbekistan depot and Tashkent Repair Workshop, Tashkent Region

IV. SCOPE OF THE STUDY

In order to achieve the objectives mentioned above, the Study shall cover the following items;

1. Evaluation of the present conditions

- (1) Collection, and analysis of relevant reports, data, and information
- (2) Survey of social and economic conditions
- (3) Examination of present condition on Uzbekistan Railways (hereinafter referred to as " UTJ ")
 - 1) railway facilities
 - 2) railway network and train operation conditions
 - 3) repair workshops
 - 4) repair and inspection system for electric locomotive and electric railcar
- (4) Review of the electrification plan

2. Demand forecast (Target year 2010)
 - (1) Projection of socio-economic framework
 - (2) Forecast of transportation demand (all mode)
 - (3) Estimation of the railway traffic volume by passenger and freight
3. Initial Environmental Examination (IEE)
4. Basic concept of the future plans for repair shops
5. Undertaking of a feasibility study
 - (1) Survey on natural conditions
 - (2) Survey on present environmental conditions
 - (3) Estimation of the number of electric locomotives and electric railcars in the future
 - (4) Formulation of repair and inspection systems for electric locomotives and electric railcars
 - (5) Preliminary engineering design
 - 1) optimum location of the repair workshop
 - 2) scale and layout of the repair workshop
 - 3) number and kind of the facilities and equipment
 - 4) principle technical specification of the facilities and equipment
 - (6) Preliminary cost estimation
 - (7) Evaluation of the site of the repair workshop
 - (8) Formulation of an operation and maintenance program
 - (9) Formulation of an implementation program
 - (10) Project evaluation
 - 1) economic evaluation
 - 2) financial evaluation
 - 3) environmental impact assessment (EIA)
6. Overall evaluation and recommendation

V. STUDY SCHEDULE

The Study shall be conducted in accordance with the attached tentative schedule.

MF

Incomplete

VI. REPORTS

JICA shall prepare and submit the following reports in English to the Government of Uzbekistan.

1. Inception Report

Twenty (20) copies
At the commencement of the Study

2. Progress Report

Twenty (20) copies
Within two (2) months after the commencement of the Study

3. Draft Final Report

Twenty (20) copies
Within six (6) months after the commencement of the Study
The written comments on the Draft Final Report from the Government of Uzbekistan shall be delivered to JICA within one (1) month after submission of the report.

4. Final Report

Forty (40) copies
Within two (2) months after the receipt of the written comments on the Draft Final Report from the Government of Uzbekistan.

VII. UNDERTAKING OF THE GOVERNMENT OF UZBEKISTAN

1. To facilitate smooth conduct of the Study, the Government of Uzbekistan shall take necessary measures ;
 - (1) To secure the safety of the Japanese study team (hereinafter referred to as " the Team ")
 - (2) To permit the members of the Team to enter, leave and sojourn in Uzbekistan for the duration of their assignment therein, and exempt them from foreign registration requirements and consular fees,
 - (3) To exempt the members of the Team from taxes, duties and other charges on equipment, machinery and other materials brought into and out of Uzbekistan for the conduct of the Study,
 - (4) To exempt the members of the Team from income tax and charges of any kind imposed on or in connection with any emoluments or allowances paid to the members of the Team for their services in connection with the implementation of the Study,
 - (5) To provide necessary facilities to the Team for remittance as well as utilization of the funds introduced into Uzbekistan from Japan in connection with the implementation of the Study,

UF



- (6) To secure permission for entry into private properties or restricted areas for the implementation of the Study,
 - (7) To secure permission for the Team to take all data and documents including maps and photographs related to the Study out of Uzbekistan to Japan,
 - (8) To provide medical services as needed. Its expenses will be chargeable on members of the Team.
2. The Government of Uzbekistan shall bear claims, if any arises, against the members of the Team resulting from, occurring in the course of, or otherwise connected with, the discharge of their duties in the implementation of the Study, except when such claims arise from gross negligence or willful misconduct on the part of the members of the Team.
 3. UTJ shall act as counterpart agency to the Team and also as coordinating body in relation with other governmental and non-governmental organizations concerned for the smooth implementation of the Study.
 4. UTJ shall, at its own expense, provide the Team with the following, in cooperation with other organizations concerned :
 - (1) Available data and information related to the Study,
 - (2) Counterpart personnel,
 - (3) Suitable office space with necessary office equipment in Tashkent and the study area, if necessary,
 - (4) Credentials of identification cards,
 - (5) Appropriate number of vehicles with drivers.

VIII. UNDERTAKING OF JICA

For the implementation of the Study, JICA shall take the following measures :

1. To dispatch, at its own expense, the Team to Uzbekistan,
2. To pursue technology transfer to the Uzbekistan counterpart personnel in the course of the Study.

IX. OTHERS

JICA and UTJ shall consult with each other in respect of any matter that may arise from or in connection with the Study.

UTJ



TENTATIVE SCHEDULE OF THE STUDY

	1	2	3	4	5	6	7	8	9	10
Work in Uzbekistan										
Work in Japan										
Reports	▲ IC/R	▲ P/R				▲ DF/R		▲ F/R		

IC/R : Inception Report

P/R : Progress Report

DF/R : Draft Final Report

F/R : Final Report

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Appendix 5-1 Data on Natural and Environmental Condition of Uzbekistan

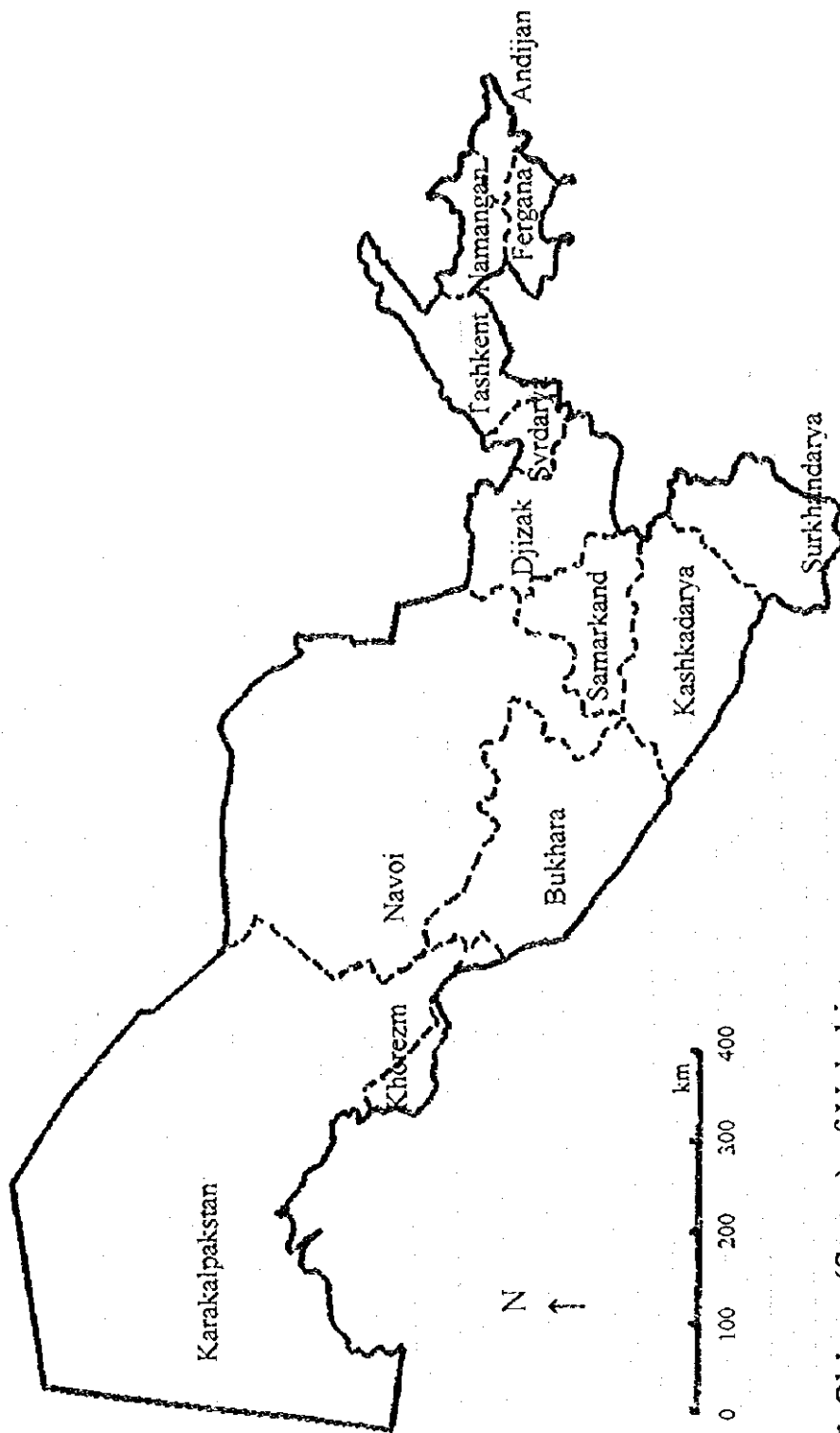


Fig.1 Oblasts (States) of Uzbekistan

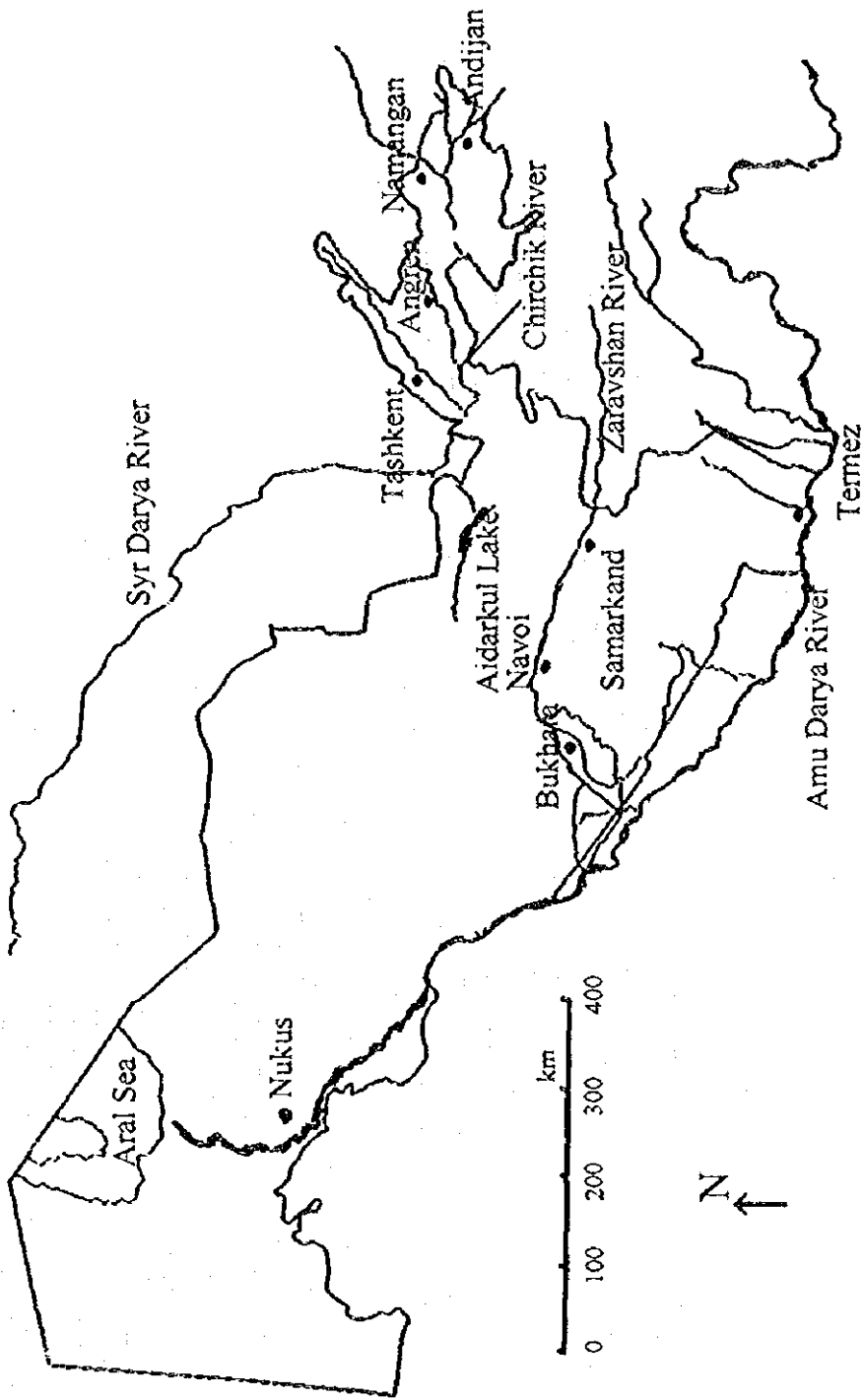


Fig.2 Major River and Lakes of Uzbekistan

Table 1 Groundwater Resources and Usage in Uzbekistan in 1994

Oblast	Approved reserves (thousands of m ³)	Groundwater use for				Irrigation water	Pastures	Total	Extraction as a percentage of approved reserves (%)
		Drinking water	Industrial supply						
Andijan	1,687	756	-	3	-	758	45		
Namangan	3,541	323	-	1,714	-	2,037	58		
Fergana	5,183	418	354	1,815	-	2,587	50		
	1,719	545	17	15	-	577	34		
Bukhara	374	54	-	2	13	69	18		
Navoi	1,050	27	15	215	50	307	29		
Tashkent	3,675	1,225	190	7	-	1,422	39		
Dizak	708	240	-	-	-	240	34		
Syrdarya	531	81	-	-	-	81	15		
Surkhandarya	602	146	-	-	-	146	24		
Kashkadarya	597	247	1	94	1	343	57		
Khorezm	337	11	-	-	-	11	3		
Karakalpakstan	526	33	-	2	77	112	21		
Total	20,530	4,106	577	3,867	141	8,690	42		

(Source: State Committee for Nature Protection (through DAI))

Table 2 Water Quality Standards in Uzbekistan

Items	Unit	Maximum Permissible Concentration	
		fisheries	drinking water supply
BOD ₅	mg O/l	3	6
COD	mg O/l	30	30
pH		6.5 to 8.5	6.5 to 8.5
Oil products	mg/l	0.05	0.3
Phenol	mg/l	0.001	0.001
Cadmium	mg/l	0.005	0.01
Iron	mg/l	0.5	0.5
Copper	mg/l	0.01	1
Nickel	mg/l	0.01	0.1
Tin	mg/l	0.03	0.1
Chromium	mg/l	0.001	0.1
Zinc	mg/l	0.01	1
Arsenic	mg/l	0.05	0.5
Mercury	mg/l	0.005	0.005
Cyanide	mg/l	0.05	0.1
Ammonium Nitrogen	mg N/l	0.39	2
Nitrite Nitrogen	mg N/l	0.08	0.08
Nitrate Nitrogen	mg N/l	0.1	10
Chlorine	mg/l	none	1.5
Detergents (Synthetic Surfactant)	mg/l	0.1	0.5

(Source: State Committee for Nature Protection (through DAI))

Table 3 Water Quality Standard for Discharge to Municipal Sewage Treatment System in Uzbekistan

Items	Unit	Maximum Permissible Concentration discharge to sewerage treatment
BOD ₅	mg O/l	500
COD	mg O/l	500
pH		6 to 9
Oil products	mg/l	5
Phenol	mg/l	5
Cadmium	mg/l	5
Iron	mg/l	5
Copper	mg/l	0.5
Nickel	mg/l	0.5
Tin	mg/l	0.5
Chromium	mg/l	0.1
Zinc	mg/l	1
Arsenic	mg/l	0.1
Mercury	mg/l	0.1
Cyanide	mg/l	-
Ammonium Nitrogen	mg N/l	100
Nitrite Nitrogen	mg N/l	100
Nitrate Nitrogen	mg N/l	100
Chlorine	mg/l	-
Detergents (Synthetic Surfactant)	mg/l	-

(Source: State Committee for Nature Protection (through DAI))

Table 4 Limited Permissible Concentration (LPC) on the Air Quality
in the Former USSR

Substance	Limited Permissible Concentration (LPC), mg/m ³	
	Onetime Maximum	Daily Average
Carbon monoxide	5	3
Nitrogen dioxide	0.085	0.04
Ozone	0.16	0.03
Particulate matter	0.5	0.15
Form aldehyde	0.035	0.003

(Source: Item of the USSR decree on the atmospheric air protection
(approved 22nd August, 1984))

Table 5 Potable Water Supply in Uzbekistan.

	Karakalpakstan	Tashkent City	Tashkent without Tashkent City	Uzbekistan total
Capacity 1000m ³				
-1975	70	1,341	355	2,643
-1980	80	1,841	433	3,781
-1985	135	2,041	570	5,034
-1990	202	2,240	819	6,797
Coverage % of population				
-1975	64	82	74	74
-1980	63	86	80	77
-1985	65	90	85	80
-1990	67	94	86	84
Consumption lit./day/person				
-1975	128	500	370	310
-1980	152	620	470	370
-1985	162	718	477	383
-1990	254	750	499	470

(Source: State Committee for Nature Protection (through DAI))

Table 6 Highly Polluted River in Tashkent Oblast

Water source/river	Pollution source	Pollutants
Chirchik River	Chirchikselmash Plant	oil products
	Chirchik electric motors plant	nitrogen compounds, oil products
	JV "Kaproaktam"	caprolactam
	Chirchik Vodokanal	nitrogen compounds, oil products, phosphates
	Tashvodocanal	nitrogen compounds, metals, BOD, phosphates
	Excavator plant	oil products
	Tashkent aircraft plant	chromium
	Kurganchyisky plant	nitrogen compounds, BOD
	Novomihaylovsky	nitrogen compounds, BOD, phosphates
	Sergly agro-industrial complex	nitrogen compounds, BOD, phosphates
	Uzbekistan poultry factory	nitrogen compounds, BOD, phosphates
	Chinaz fish fodder plant	nitrogen compounds, BOD
	Sergely reinforced concrete structured plant	oil products, iron, suspended solids
	collector drains from irrigated lands	salts, pesticides, metals
Karasu (right bank)	Tashkent tractor plant	oil products
Salar Canal and then the Chirchik River	Almazar car repair plant #5	oil products, chromium, nonmetals
	Aircraft factory	oil products
	Yangul biochemical plant	nitrogen compounds, BOD, phosphates
Bozsu Canal and then Syr Darya River	Tashkent electrical power generation station	thermal pollution, oil products
	Aircraft factory	chromium, copper, oil products
	Taxi park #7	oil products
	Bus park #4	oil products
	Tashkent Railways	oil products
	Yangul pig-breeding complex	nitrogen compounds, BOD, phosphates
	Yangul poultry factory	nitrogen compounds, BOD, phosphates
	Tashvodocanal	nitrogen compounds, metal, BOD, phosphates
	Ahangaran River	Yangiabad mine administration #2
Uaylipsky plant		nitrogen compounds, BOD, phosphates
Angren ceramic plant		oil products
Namangan Vodocanal		metal
Kokand Vodocanal		nitrogen compounds, BOD, phosphates
Fergana Vodocanal		nitrogen compounds, BOD, phosphates
Rishtan Vodocanal		nitrogen compounds, BOD, phosphates
Kokand superphosphate plant		oil products, phenols, nitrogen compounds
"Rustam" Kokand		nitrogen compounds, oil products
Fergana train park, Kokand		oil products
Kokand fat factory	fats	

(Source: State Committee for Nature Protection (through DAI))

Table 7 Locations of Highly polluted Groundwater in Tashkent Oblast

River basin/location	pollution source	pollutants
Chirchik Valley, and Kibray and other water intake	Electrohimprom railway poultry factory quarries of non-ore materials Interrayon sewage water collector	nitrogen compounds
Akhangran Valley	Akhangran mining and metallurgic plant waste dumps	mineral salts sulfates phosphates cadmium selenium
Aquifers between the Chirchik and Akhangran Rivers	livestock breeding poultry factories Jute-kenaf plants improper disposal of chemicals and fertilizers dumps of industrial and domestic waste	mineral salts sulfates phosphates cadmium selenium nitrogen compounds

(Source: State Committee for Nature Protection (through DAI))

Table 8 Number of Enterprises Generation More than 100,000 m³ of Wastewater per Year

oblast	number of enterprises, by type																Total
	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	
Fergana	1	2	3	0	2	4	5	0	5	4	3	7	1	0	0	0	37
Tashkent	1	17	13	10	12	11	21	13	2	4	1	0	4	3	3	9	124
Karakalpakstan	0	0	0	0	0	0	0	0	0	0	0	0	1	1	0	0	2
Uzbekistan total	11	37	24	11	19	49	46	18	11	11	8	9	8	4	4	11	281

type of enterprises	
A textile industry	I petroleum processing
B construction industry	J chemical industry
C transportation industry	K medical services industry
D nonferrous metals industry	L cotton processing
E mining	M energy production
F food processing industry	N fisheries
G municipal wastewater treatment plants	O furniture production
H machine building/metal working industry	P lubricant production

(Source: State Committee for Nature Protection (through DAI))

Table 9 Capacity and Coverage of Wastewater Treatment Facilities in Uzbekistan

	Capacity, 1,000 m ³ /day					Coverage, % of population served				
	1975	1980	1985	1990	1990	1975	1980	1985	1985	1990
Karakalpakstan	0	0	0	6	0	0	0	0	0	10
Tashkent City	902	1,170	1,370	1,670	65	70	80			
Tashkent without Tashkent City	210	330	450	495	29	42	46			
Fergana	160	210	210	319	17	23	37			
Uzbekistan total	1,516	2,110	2,690	3,494	26	29	33			

(Source: State Committee for Nature Protection)

Table 10 Fines for Discharge of
Pollutants in Uzbekistan

Wastewater Discharge	
pollutant	rate, sum/ton
ammonium nitrogen	1,024
nitrite nitrogen	20,000
nitrate nitrogen	44
acetone	8,000
benzene	800
cadmium	80,000
cobalt	40,000
arsenic	8,000
oil products	80,000
nickel	40,000
sulfates	4
lead	13,320
phenols	400,000
fluoride	8,000
chloride	1.2
zinc	40,000
cyanide	8,000

(Source: State Committee for Nature
Protection (through DAI))

Table 11 Fossil Fuel Reserves in Uzbekistan

Energy resource	Reserved quantity	Production levels
natural gas	2 trillion m ³	47 billion m ³ in 1994 almost 50 billion m ³ in 1995 (total production is forecast to rise to 60 billion m ³ per year by 2000)
coal	2 billion tons	3.8 million tons in 1993
petroleum	300 million tons	5.5 million tons in 1994 almost 8 million tons in 1995 (total production is forecast to rise to 9 million tons per year by 2010)

Sources: Economy of Uzbekistan (National Bank for Foreign Economic Activity of the Republic Uzbekistan, 1993) and Uzbekistan Profile (for presentation at the 1996 EBRD Annual Meeting) (through DAI)

Table 12 Aggregate Air Pollutant Emission in Uzbekistan

Place	Year	Emissions of air pollutants, thousands of tons							total
		Particulate	sulfur oxide	carbon monoxide	nitrogen oxide	hydrocarbons			
Tashkent City	1990	11.2	1.5	15.3	4.8	6.2		39.4	
	1991	9.2	1.3	13.8	4.8	5.2		34.6	
	1992	4.5	0.9	8.9	4.9	3.8		23.2	
	1993	3.3	0.8	9.3	4.7	3.2		21.4	
	1994	2.9	0.8	7.8	3.0	2.7		18.2	
Tashkent Oblast	1995	2.1	0.6	7.1	3.7	0.9		15.0	
	1990	83.7	272.4	38.8	43.2	4.4		447.2	
	1991	80.6	256.5	41.9	41.5	10.6		436.0	
	1992	75.3	234.1	41.5	36.9	6.6		396.9	
	1993	75.3	190.6	29.7	32.3	4.9		335.2	
Uzbekistan	1994	64.0	161.8	24.1	30.7	3.8		285.9	
	1995	65.9	167.7	18.2	27.3	4.5		286.6	
	1990	252.1	541.6	129.6	117.1	215.2		1,277.1	
	1991	224.9	499.9	143.9	111.7	213.2		1,214.8	
	1992	203.3	455.2	159.1	100.0	175.8		1,107.8	
	1993	178.1	442.2	136.3	92.9	163.2		1,020.8	
	1994	147.1	376.7	152.7	148.4	97.0		928.7	
	1995	127.0	399.9	147.5	78.3	141.8		901.7	

(Source: State Committee for Nature Protection (through DAI))

Table 13 Mean Annual Concentration of Air Pollutants for Tashkent City

Pollutant	mean annual concentration of air pollutants (concentration is given as a multiple of MPC)				
	1991	1992	1993	1994	1995
particulate	1.3	1	1	1.3	1.7
SO ₂	0.2	0.2	0.2	0.2	0.2
hydrocarbons	1	1.1	0.7	1	0.9
NO ₂	2	1.5	1.3	1.5	1.3
NO	1.2	0.5	0.5	0.5	0.5
ammonium	1.2	1	1	0.8	0.8
Pb	0.6	0.5	0.6	0	0

(Source: State Committee for Nature Protection (through DAI))

Appendix 5-2 Data on the Environmental Condition of Tashkent Workshop

Table 1 Water Consumption in Tashkent Workshop

	Allowed 100% Capacity		Actual	
	m ³ /day	1000 m ³ /year	m ³ /day	1000 m ³ /year
Water Intake total	5459	1247	3789	1031
surface water	0	0	0	0
groundwater	4892	1094	3553	945
city water supply system	567	153	236	86
Water Consumption	5459	1247	3789	1031
domestic	567	153	236	86
(from groundwater)	0	0	0	0
industrial	4892	1094	3553	945
(from groundwater)	4892	1094	3553	945

(Source: Tashkent Workshop)

Table 2. Water Consumption (allowed 100% capacity) by section in Tashkent Workshop

Section	units	number of units	operating period (h/day)	operating days/year	Recycling systems		Water Consumption	
					m ³ /day	1000 m ³ /year	average l/day	m ³ /day
Industrial Needs					5135	1386.2	4892	1094
1. power plant room (winter period)				151			1038	156.7
(summer period)				154			611	94.1
2. boilers			24	151			409.8	61.9
3. washing machines		5	15.6	266			579	154
			7.8	266			6.4	1.7
4. cooling machines			15.6	294			1020	299.6
5. cooling cupola		3	16	266	52	13.8	118.3	31.6
6. cooling compressors				266	1024	272.4	635.4	169.1
7. water-cooling tower					4059	1100	414	110
8. distillation apparatus			7.8	266			11.4	3
9. transport							42.9	11.4
10. watering (green area)	m ²	1250					3	3.8
(concrete)	m ²	9500					0.4	3.8
(sanitary zone)	m ²	10000					0.4	4
11. fire-fighting								0.7
Domestic Needs							1590	567
1. canteen	person	2000?		266			12	194.4
2. laundry	person	1000		266			75	75
3. administration	person	414	7.8	266			12	4.9
4. goods shop	place	2	7.8	266			12	0.024
5. food stuffs shop	place	1	7.8	266			250	0.25
6. club	place	1	7.8	266			8.6	0.009
7. gymnasium	person	40	15	365			50	2
8. pool	person	20	15	365			100	2.04
9. shower (I shift)	set	300	7.8	266			500	150
(II shift)	set	150	7.8	266			500	75
10. welfare center (I)	person	635	15.6	266			45	28.6
(II)	person	1403	15.6	266			25	36.1
Total							5453	1247

(Source: Tashkent Workshop)

Table 3 Wastewater discharge (allowed 100% capacity) by section in Tashkent Workshop

Section	units	number of units	operating period (h/day)	operating days/year	wastewater discharge		disposal place
					average l/day	1000 m ³ /year	
Industrial Needs							
1. power plant room (winter period)				151		3170	784.2
(summer period)				154			
2. boilers			24	151		409.8	61.9 municipal treatment plant
3. washing machines			15.6	266		579	154 treatment facility
		5	7.8	266		6.4	1.7 treatment facility
4. cooling machines			15.6	294		1020	299.6 municipal treatment plant
5. cooling cupola		3	16	266		118.3	31.6 municipal treatment plant
6. cooling compressors				266		635.4	169.1 municipal treatment plant
7. water-cooling tower							
8. distillation apparatus			7.8	266		11.4	3 municipal treatment plant
9. transport						42.4	11.3 municipal treatment plant
10. watering (green area) (concrete) (sanitary zone)	m ²	1250		180			
	m ²	9500		180			
	m ²	10000		180			
11. fire-fighting							
Domestic Needs							
1. canteen	person	2000?		266		1590	153
2. laundry	person	1000		266		12	194.4
3. administration	person	414	7.8	266		75	75
4. goods shop	place	2	7.8	266		12	4.9
5. food stuffs shop	place	1	7.8	266		12	0.024
6. club	place	1	7.8	266		250	0.07
7. gymnasium	person	40	15	365		8.6	0.009
8. pool	person	20	15	365		100	2
9. shower (I shift) (II shift)	set	300	7.8	266		500	150
10. welfare center (I) (II)	person	635	15.6	266		45	28.6
	person	1403	15.6	266		25	36.1
Total						3737	937.2

(Source: Tashkent Workshop)

Table 4 Emission into Air in Tashkent Workshop

Pollutant	1993(actual)		2000(prospect)		2005 (suggested allowable)	
	g/sec	tons/year	g/sec	tons/year	g/sec	tons/year
Total	244.025252	2728.30628	98.1352124	355.274702	78.7038526	214.104341
Solid (total)	28.910834	224.550442	6.1058724	31.8857376	6.8276646	41.904135
Aluminum oxide	0.013	0.036	0.0013	0.0039	0.0063	0.0179
Aerosol (paint)	0.033	0.21	0.0309	0.327	0.0443	0.334
Aerosol (welding)	0.152	1.312	0.038	0.215	0.0425	0.233
Suspended solids	24.723	214.368	5.267	28.384	4.336	22.47
Ferric oxide	0.152	1.312	0.0629	0.49	1.061	3.183
Manganese dioxide	0.0046	0.0229	0.00467	0.0227	0.0361	0.675
Magnesium oxide	-	-	-	-	0.0499	0.475
Cupric oxide	0.0132	0.0329	0.0065	0.0268	0.0225	0.0458
Tin sulfate	-	-	-	-	0.00028	0.0068
Tin chloride	-	-	0.0000033	0.0000125	0.0000066	0.000021
Wood dust	0.395	1.31	0.432	1.432	0.432	1.432
Ash (organic dust)	3.374	5.711	0.2119	0.7481	0.0832	0.104
Lead	0.000358	0.000141	0.0000283	0.0000122	0.00021	0.000034
Dust with SiO ₂ <70%	0.000195	0.0012	0.000178	0.001087	0.565	10.67
Badly dissolved fluoride	0.000165	0.00126	-	-	0.0001	0.0016
Chrome (VI)	0.000016	0.000041	0.0000148	0.0001459	0.0031	0.0384
Cotton glass dust	0.0503	0.233	0.0503	0.2339	0.0503	0.233
Dust with 20%< SiO ₂ <70%	-	-	0.000178	0.00108	0.000368	0.00158
Calcium oxide	-	-	-	-	0.0945	1.789
Liquid and gas (total)	215.114418	2503.75584	92.02934	323.388964	71.876188	172.200208
Nitrogen dioxide	30.02	99.94	2.338	6.975	2.338	0.975
Nitrogen oxide	1.505	8.173	1.511	8.216	1.439	8.368
Ammonia	0.0048	0.011	0.00568	0.0122	0.00612	0.0128
Sulfur anhydride	1.885	14.918	44.161	37.113	43.694	29.251
Acetone	0.8119	4.115	0.434	3.44	0.424	3.403
Benzopyrene	0.000316	0.00034	0.000014	0.0000042	0.00002	0.000006
Petrol	1.456	20.244	1.456	20.244	0.92	11.979
Benzene	0.00609	0.192	0.0877	1.41	0.0877	1.41
Butyl acetate	0.12	1.383	0.217	1.83	0.2038	1.777
HCl	0.00315	0.0094	0.000372	0.0017	0.0043	0.038
HNO ₃	-	-	0.00468	0.014	0.0047	0.014
H ₂ SO ₄	0.004252	0.0276	0.0078	0.0435	0.002	0.016
Kerosine	-	-	0.084	0.314	0.192	0.71
Acetic acid	-	-	0.0012	0.0022	0.00181	0.00516
Xylene	0.534	5.29	0.687	7.0297	0.678	7.175
Grease steam	-	-	0.000056	0.00016	0.075	0.429
Sodium carbonate	0.0089	0.041	0.0482	0.0928	0.0539	0.564
Nickel (dissolved salts)	-	-	0.0016	0.0008	0.00013	0.0016
Hydrogen sulfide	0.00131	0.0412	0.0013	0.0441	0.0013	0.044
Ethyl alcohol	0.229	1.289	-	-	0.00157	0.00224
Solvent	0.0976	1.268	0.263	2.87	1.211	10.74
Toluene	0.414	2.826	0.374	3.403	0.308	3.139
Sodium triphosphate	-	-	0.0191	0.0367	0.166	0.257
Carbon monoxide	175.0537	2308.86	37.892	211.036	17.721	70.413
Phenol	0.0017	0.0518	0.0017	0.0518	0.0017	0.0518
Hydrocarbon	1.487	20.077	0.0635	0.418	-	-
Formaldehyde	0.013	0.026	0.0134	0.0267	0.0134	0.026
HF	0.0005	0.0029	0.000448	0.0024	0.000448	0.0024
Cyanide	-	-	0.00059	0.0042	0.00059	0.0042
Ethyl acetate	0.0006	0.0698	0.0001	0.012	0.0001	0.012
Ethyl cellosolbe	0.259	3.975	0.2938	5.93	0.283	5.89
White spirit	0.936	9.102	1.642	10.612	1.639	11.443
Butanol	0.07	0.736	0.07	0.736	0.0565	0.683
Ethanol	0.183	1.047	0.183	1.047	0.163	0.968
Sodium hydroxide	0.0086	0.0398	0.0121	0.179	0.0311	2.155
Tetrachloroethylene	-	-	0.014	0.151	0.014	0.151
Vanadium pentoxide	-	-	0.14	0.09	0.14	0.09

(Source: Tashkent Workshop)

Table 5 (1.3) Pollutant emissions parameters for Diesel Locomotive Building in Tashkent Workshop in 1992

Section	Sources of Pollutants		Number of working hours in a year	Name of source	Source number	Height of source(m)	Emission of Pollutants			Name of pollutants	Emission g/s	ton/year	
	Name	Number					Diameter of Stack(m)	Emission speed (m/s)	Volume (m ³ /s)				Temperature (°C)
Washing	Washing machine	1	1570	Stack	266	15	0.6	0.8	0.58	41	Sodium hydroxide	0.000023	0.00013
	Engine washing unit	1	2777	Stack	291	15	0.4	4.43	0.56	41	Suspended materials Sodium hydroxide	0.0018 0.0000094	0.018 0.000077
Painting	Hooper	1	2018	Stack	292	8	0.8	3.6	1.02	150	Carbon monoxide Nitrogen oxides	0.355 0.592	2.58 0.43
	Medium	1	4148	Stack	299	15	0.5	5.5	4.3	24	Xylene White-spirit Solvent	0.0322 0.1162 0.0167	0.481 1.733 0.2496
											Toluene Paint aerosol	0.0024 0.0075	0.55814 0.106
	Medium	1	3876	Stack	300	15	0.5	5.5	4.3	24	Xylene White-spirit Solvent	0.0322 0.1162 0.0167	0.481 1.733 0.2496
											Toluene Paint aerosol Benzene Acetone	0.0024 0.0251 0.0054 0.0787	0.0364 0.375 0.8605 1.173
P K U	Medium	1	4148	Stack	301	15	0.5	5.5	4.3	24	Xylene White-spirit Solvent	0.0322 0.1162 0.0167	0.481 1.733 0.2496
											Toluene Benzene	0.0024 0.01	0.0364 0.1485
	Medium	1	4149	Stack	302	15	0.5	5.5	4.3	24	Xylene White-spirit Solvent	0.0322 0.1162 0.0167	0.481 1.733 0.2496
Diesel	Welding	1	1388	Stack	303	10	0.3	10.4	0.74	30	Oxide of iron	0.0024	0.012
	Bath	1	1887	Stack	322	15	0.8	2.9	0.82	30	Suspended materials	0.0001	0.00005
	Grinding	1	859	Stack	323	12	0.35	7.1	0.68	30	Suspended materials	0.007	0.038
	Painting-drying room	1	2177	Stack	324	15	0.9	1.4	2.8	29	Xylene White-spirit Acetone	0.00689 0.05208 0.00582	0.054 0.482 0.0456
											Benzene Paint aerosol	0.05 0.0035	0.254 0.02389
	Painting-drying room	1	2177	Stack	325	15	0.9	3.5	2.23	29	Xylene White-spirit Acetone	0.00689 0.05208 0.00582	0.054 0.482 0.0456
	Diesel testing-stand	1	2083	Stack	326	18	0.9	3.1	2.2	30	Soot Carbon monoxide Nitrogen oxides	0.0008 0.0284 0.006	0.006 0.159 0.035

(Source: Tashkent Workshop)

Table 5 (2.3) Pollutant emissions parameters for Diesel Locomotive Building in Tashkent Workshop in 1992

Section	Sources of Pollutants		Number of working hours in a year	Name of source	Source number	Height of source(m)	Diameter of Stack(m)	Emission of Pollutants		Temperature (°C)	Name of pollutants	Emission	
	Name	Number						speed (m/s)	volume (m ³ /s)			g/s	ton/year
Diesel	Diesel testing-stand	1	2083	Stack	327	18	0.9	3.1	2.2	30	Soot	0.0068	0.006
	Diesel testing-stand	1	2083	Stack	328	18	0.9	3.1	2.2	30	Carbon monoxide Nitrogen oxides	0.0264 0.009	0.139 0.035
	Diesel testing-stand	1	2083	Stack	329	18	0.9	3.1	2.2	30	Carbon monoxide Nitrogen oxides	0.0264 0.006	0.139 0.035
	Sprayer stand	1	1851	Stack	334	12	0.4	4.2	0.53	27	Suspended materials Benzene	0.0024 0.023	0.016 0.348
	Washing for parts	1	1873	Stack	336	15	0.4	3.3	0.41	21	Suspended materials Benzene	0.0086 0.011	0.0058 0.0039
	Argon welding	1	788	Stack	337	8	0.3	4.7	0.33	34	Oxide of iron Aluminum oxide	0.0032 0.013	0.0092 0.0039
	Preparing paint	1	1784	Stack	338	8	0.3	5.5	0.39	20	Xylene Acetone Toluene	0.0175 0.042 0.105	0.1124 0.281 0.953
	Examination stand	1	1405	Stack	339	11	0.4	2.3	0.29	30	Benzene	0.013	0.0058
	Welding post	1	1543	Stack	340	15	0.4	3.3	0.41	25	Oxide of iron Oxide of manganese	0.0018 0.00006	0.01 0.000029
	Medium	1	3388	Stack	341	15	0.9	0.9	4.1	29	Oxide of iron Oxide of manganese	0.021 0.0004	0.256 0.0005
P K U	Sectional	1	1099	Stack	304	6	0.45	11.9	1.89	24	Benzene Oxide of iron Oxide of manganese	0.0205 0.0096 0.0028	0.187 0.035 0.00068
	Sectional	1	1234	Stack	305	6	0.6	2.5	0.71	23	Nitrogen oxides Oxide of iron Oxide of manganese Carbon monoxide Nitrogen oxides	0.0027 0.0001 0.0001 0.008 0.0028	0.012 0.00004 0.00004 0.036 0.008
	Heater	1	2015	Stack	306	6	0.6	3.4	1.98	120	Carbon monoxide Nitrogen oxides	0.355 0.592	2.58 0.43
	Welding post	1	1694	Stack	307	12	0.5	17.2	3.37	28	Oxide of iron Oxide of manganese	0.01 0.0002	0.091 0.00013
	Grinding machine	1	185	Stack	308	12	0.35	2.1	0.2	28	Suspended materials Lead	0.000033 0.000023	0.000023 0.00009
	Welding	1	2165	Stack	309	18	0.55	3.8	0.91	34	Oxide of iron Oxide of manganese Dust (20%SiO ₂ 70%) Calcium fluoride Hydrofluoric acid Nitrogen oxides	0.0012 0.000034 0.00008 0.00017 0.00055 0.000079 0.000034	0.000265 0.000065 0.00013 0.00042 0.000079 0.000034
	Washing tank	1	995	Stack	310	10	0.3	11.2	0.8	34	Suspended materials Benzene	0.0012 0.01	0.0043 0.035
	Welding post	1	1315	Stack	311	10	0.4	4.3	0.56	25	Oxide of iron Oxide of manganese	0.0019 0.00005	0.009 0.000024
	Washing for parts	1	3406	Stack	312	12	0.6	8.8	2.32	40	Suspended materials Benzene	0.0033 0.0034	0.065 0.018

(Source: Tashkent Workshop)

Table 5 (3.3) Pollutant emissions parameters for Diesel Locomotive Building in Tashkent Workshops in 1992

Section	Sources of Pollutants		Number of working hours in a year	Name of source	Source number	Height of source(m)	Diameter of Stack(m)	Emission of Pollutants		Temperature (°C)	Name of pollutants	Emission	
	Name	Number						speed (m/s)	volume (m ³ /s)			k/s	ton/year
	Washing machine	1	347	Stack	313	8	0.55	1.8	0.43	49	Suspended materials	0.00005	0.00015
	Welding post	1	3444	Stack	314	18	0.63	0.25	0.75	32	Sodium hydroxide Benzine	0.00034 0.00025	0.00026 0.031
	Burning furnace	1	2814	Stack	315	5	0.3	4.1	0.20	110	Oxide of iron Oxide of manganese Suspended materials Carbon monoxide	0.00005 0.00468 0.0061 0.06157	0.00005 0.04742 0.0061 0.02272
	Washing machine	1	1597	Stack	317	10	0.3	6.9	0.48	40	Suspended materials Sodium hydroxide	0.00012 0.00005	0.0069 0.00028
Diesel	Washing bath	1	215	Stack	319	18	0.45	3.1	0.48	38	Sodium hydroxide Benzine	0.00008 0.00015	0.00006 0.0188
	Grinding Mechanic	1 1	808 1365	Stack Stack	342 343	18 15	0.6 0.5	5.9 1.83	1.5 0.36	23 27	Suspended materials Suspended materials Benzine	0.00648 0.0012 0.001	0.01882 0.0059 0.0049
	Electro-erosional Grinding	1 1	272 230	Stack Stack	344 345	6 13	0.2 0.35	6.7 9.4	0.21 0.31	38 28	Suspended materials Suspended materials	0.0005 0.0014	0.00049 0.0016

(Source: Tashkent Workshop)

Table 6 Pollutant emission parameters for new facilities of Diesel Locomotive Building in Tashkent Workshop in 2000

Section	Sources of Pollutants		Number of working hours in a year	Name of source	Source number	Height of source (m)	Diameter of Stack (m)	Emission of Pollutants			Temperature (°C)	Name of pollutants	Maximum purification system (%)	Emission in 2000
	Name	Number						speed (m/s)	volume (m³/s)	kg/s				
Turning car	Welding post	1088 Stack	420	1088 Stack	420	15	0.3	10	0.97	25	Carbon monoxide	99	0.0124	
													Suspended materials	0.0142
													Oxide of manganese	0.000081
	Welding post	1514 Stack	423	1514 Stack	423	15	0.35	10.8	0.38	25	Carbon monoxide	99	0.0000081	
													Nitrogen oxides	0.000006
													Oxide of iron	0.000132
													Chromium anhydride	0.000003
	Painting room	1388 Stack	431	1388 Stack	431	19	0.71	10.6	4.16	18	Paint aerosol	99	0.00000052	
													Carbon monoxide	0.000017
													Nitrogen oxides	0.000029
Drying room	2863 Stack	432	2863 Stack	432	15	0.25	11.4	0.55	60	Solvent	99	0.00000014		
												Oxide of manganese	0.015	
												Suspended materials	0.0000001	
												Chromium anhydride	0.000046	
Repair complex	Washing bath	1038 Stack	433	1038 Stack	19	0.225	10.5	0.42	40	Kerosene	99	0.00000068		
												Oxide of iron	0.000007	
												Chromium anhydride	0.0000026	
	Washing turning car	519 Stack	441	519 Stack	441	15	0.225	10.5	0.42	40	Sodium carbonate	99	0.046	
													Carbon monoxide	0.019
	Grinding machine	915 Stack	443	915 Stack	443	10	0.53	16.3	5.05	18	Woody dust	98	0.037	
													Suspended materials	0.0133
	Welding machine	1031 Stack	447	1031 Stack	447	15	0.25	10.5	0.97	25	Oxide of manganese	99	0.000013	
													Oxide of iron	0.000132
	Welding machine	538 Stack	448	538 Stack	448	15	0.25	10.2	0.98	25	Nitrogen oxides	99	0.000013	
Carbon monoxide													0.00081	
Suspended materials													0.00065	
Welding post	1102 Stack	449	1102 Stack	449	15	0.25	10.2	0.98	25	Oxide of manganese	99	0.000014		
												Oxide of iron	0.000013	

(Source: Tashkent Workshop)

Table 7 (1/2) Pollutant emissions parameters for foundry factory in Tashkent Workshop in 1992

Section	Sources of Pollutants		Number of working hours in a year	Name of source	Source number	Height of source (m)	Diameter of stack (m)	Emission of Pollutants		Temperature (°C)	Names of pollutants	Emission (1992)		Emission (2000)	
	Name	Number						Speed (m/s)	Volume (m³/s)			g/s	ton/year	g/s	ton/year
Compressor	1301	Stack	1	132	6	0.6	6.8	1.95	0.0296	0.145	0.0296	0.145	0.0296	0.145	
	1914	Stack	7	143	7	0.9	6.2	3.94	0.0238	0.154	0.0238	0.154	0.0238	0.154	
	1651	Stack	1	135	4	0.3	12.3	0.87	0.0037	0.022	0.0037	0.022	0.0037	0.022	
	1012	Stack	1	139	4	0.3	9	3.9	0.0247	0.099	0.0247	0.099	0.0247	0.099	
Heater	2018	Stack	1	138	5	0.6	3.2	0.9	0.355	2.38	0.355	2.38	0.355	2.38	
	3095	Stack	1	140	9	0.8	5.5	2.75	0.08	0.853	0.08	0.853	0.08	0.853	
Heater	112	Stack	1	144	12	0.45	10.3	1.65	0.177	0.177	0.177	0.177	0.177	0.177	
	819	Stack	1	145	6	0.45	3.2	0.51	0.038	0.172	0.038	0.172	0.038	0.172	
Warm (heater)	2018	Stack	1	146	6	0.5	5.1	1	0.355	2.58	0.355	2.58	0.355	2.58	
	2084	Stack	1	147	10	0.45	3.4	0.56	0.0965	0.0724	0.0965	0.0724	0.0965	0.0724	
Cutting metals	97	Stack	1	149	4	5.6	0.5	4.5	0.014	0.0049	0.014	0.0049	0.014	0.0049	
	1768	Stack	1	150	9	0.8	5.3	2.7	0.0039	0.01	0.0039	0.01	0.0039	0.01	
Furnace for melting	1704	Stack	1	153	10	0.7	5.9	2.27	0.0064	0.0023	0.0064	0.0023	0.0064	0.0023	
	1704	Stack	1	153	10	0.7	5.9	2.27	0.0335	0.217	0.0335	0.217	0.0335	0.217	
Open-hearth furnace	2170	Stack	1	194	14	0.7	6.8	2.6	0.0678	0.416	0.0678	0.416	0.0678	0.416	
	3714	Stack	1	155	25	1	3.4	2.67	0.0039	0.01	0.0039	0.01	0.0039	0.01	
Drum for drying	1656	Stack	1	157	14	0.63	6.2	1.91	0.00791	0.05488	0.00791	0.05488	0.00791	0.05488	
	1730	Stack	1	130	6	0.8	5	2.5	0.0272	1.727	0.0272	1.727	0.0272	1.727	
Room for blowing	410	Stack	1	128	14	0.5	10.1	1.98	0.0252	0.146	0.0252	0.146	0.0252	0.146	
	1831	Stack	1	127	29	1	2.7	2.12	0.03	0.03	0.03	0.03	0.03	0.03	
Furnace for burning	1675	Stack	1	126	25	1	2.9	2.28	0.0287	0.176	0.0287	0.176	0.0287	0.176	
	3388	Stack	1	124	8	0.6	8.4	2.37	0.0285	1.804	0.0285	1.804	0.0285	1.804	
Room for blowing	1751	Stack	1	123	14	0.9	1.2	0.77	0.0158	0.0996	0.0158	0.0996	0.0158	0.0996	
	1751	Stack	1	122	14	0.9	1.2	0.77	0.0158	0.0996	0.0158	0.0996	0.0158	0.0996	
Ventilation	1751	Stack	1	121	14	0.9	1.2	0.77	0.0158	0.0996	0.0158	0.0996	0.0158	0.0996	
	1751	Stack	1	120	14	0.9	1.2	0.77	0.0158	0.0996	0.0158	0.0996	0.0158	0.0996	
Ventilation	1751	Stack	1	119	14	0.9	1.2	0.77	0.0158	0.0996	0.0158	0.0996	0.0158	0.0996	
	1751	Stack	1	118	14	0.9	1.2	0.77	0.0158	0.0996	0.0158	0.0996	0.0158	0.0996	
Ventilation	1751	Stack	1	117	14	0.9	1.2	0.77	0.0158	0.0996	0.0158	0.0996	0.0158	0.0996	
	1751	Stack	1	116	14	0.9	1.2	0.77	0.0158	0.0996	0.0158	0.0996	0.0158	0.0996	
Pouring cast iron	3395	Stack	1	173	12	0.5	2	0.39	0.081	0.59	0.081	0.59	0.081	0.59	
	3114	Stack	1	172	12	0.5	2.1	0.41	0.066	0.14	0.066	0.14	0.066	0.14	

(Source: Tashkent Workshop)

Table 7 (2/2) Pollutant emissions parameters for foundry factory in Tashkent Workshop in 1992

Section	Sources of Pollutants		Number of working hours in a year	Name of source	Source number	Height of source(m)	Diameter of stack(m)	Emission of Pollutants		Temperature, °C	Name of pollutants	Emission(1992)		Emission(2000)	
	Name	Number						speed (m/s)	Volume (m ³ /s)			kg/s	ton/year	kg/s	ton/year
	Pouring cast iron		1	3114 Stack	171	12	0.5	2.1	0.41	27	Carbon monoxide	0.068	0.74	0	0
	Furnace for drying mold		1	1832 Stack	189	10	0.63	3.9	1.18	150	Suspended materials	0.033	0.21776	0.033	0.21776
	Welding		1	3215 Stack	168	8	0.8	5.9	3.69	27	Carbon monoxide	0.1096	0.6805	0.1096	0.6805
	Mining		1	3214 Stack	170	9	0.95	3.7	4.04	27	Suspended materials	0.0219	0.1315	0.0219	0.1315
	Drum for grinding metal		1	3298 Stack	177	9	0.95	3.6	2.33	25	Carbon monoxide	0.0092	0.0602	0.0092	0.0602
	Pouring cast iron		1	3296 Stack	175	12	0.5	2.1	0.41	25	Suspended materials	0.007	0.0081	0.007	0.0081
	Pouring cast iron		1	3395 Stack	174	12	0.5	2	0.39	24	Suspended materials	0.0007	0.0081	0.0007	0.0081
	Cupola		1	4789 Stack	179	18	3.5	1.4	13.46	700	Carbon monoxide	0.075	0.89	0.075	0.89
	Cupola		1	4789 Stack	180	18	3.5	1.4	13.46	700	Suspended materials	0.1159	1.327	0.1159	1.327
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.081	0.99	0.081	0.99
	Cupola		1	4789 Stack	180	18	3.5	1.4	13.46	700	Carbon monoxide	0.132	1.57	0.132	1.57
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Sulfur dioxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	180	18	3.5	1.4	13.46	700	Sulfur dioxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Sulfur dioxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Sulfur dioxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	6.04	41.49	6.04	41.49
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.15	2.58	0.15	2.58
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.1753	3.01	0.1753	3.01
	Cupola		1	4789 Stack	181	18	3.5	1.4	13.46	700	Carbon monoxide	0.216	3.709	0.216	3.709
	Cupola		1	4789 Stack	181										

Table 6 Pollutant emissions parameters for galvanic and electro-apparatus factory in Tashkent Workshop in 1992

Section	Sources of Pollutants		Number of working hours in a year	Name of source	Source number	Height of source(m)	Emission of Pollutants		Temperature (°C)	Name of pollutants	Emission(1992)		Emission(2000)	
	Name	Number					Diameter of Stack(m)	Speed (m/s)			m ³ /s	kg/s	ton/year	kg/s
Galvanic factory	Chromo bath	1	3282	Stack	207	8	0.5	7.5	5.4	23 chromium anhydride	0.000011	0.000014	0.000014	0.000013
	Etching bath	1	3282	Stack	208	8	0.5	7.5	5.4	Sodium hydroxide	0.001	0.121	0.001	0.121
	Etching bath	1	748	Stack	209	8	0.5	6.7	3.02	Sulfuric acid	0.0036	0.16	0.0036	0.16
	Etching bath	1	1592	Stack	211	10	0.2	10.2	0.31	Sodium hydroxide	0.00375	0.01011	0.00375	0.01011
	Accumulator charge	1	3273	Stack	215	9	0.7	4.9	1.89	Suspended materials	0.0008	0.0045	0.0008	0.0045
F C M	Nickel bath	1	138	Stack	467	13	0.28	11.2	0.99	Sodium hydroxide	0.00201	0.02369	0.00201	0.02369
	Coil rebar	1	1641	Stack	267	8	0.3	5.9	0.42	Sulfuric acid	0.0042	0.0275	0.0042	0.0275
Electro-apparatus factory	Distill. Bath	1	185	Stack	285	8	0.08	4.2	0.02	Suspended materials	0.0011	0.0065	0.0011	0.0065
	Bath	32 non-organized	269	4	5.6	0.5	4.5	0.0000076	0.0000076	0.0000076	0.0000076	0.0000076	0.0000076	
	Warehouse	1	1597	Stack	270	6	0.6	1.3	0.38	Benzene	0.0028	0.016	0.0028	0.016
	Warehouse	1	1597	Stack	271	6	0.6	1.3	0.39	Suspended materials	0.0028	0.016	0.0028	0.016
	Ventilation	1	1481	Stack	272	9	0.5	0.57	0.11	Suspended materials	0.00045	0.0024	0.00045	0.0024

(Source: Tashkent Workshop)

Table 9 Wastes produced from Tashkent Workshop

Type of Waste	Produced Waste		Recycle		Non-used Waste	
	Source of Waste	Quantity ton/year	Quantity ton/year	Way of Use	Quantity ton/year	Destination
glass	replacement from coach	80	80	reproducing plant		
linoleum	replacement from coach	42	20	to be sold to population	22	municipal disposal place
wall paper	replacement from coach	51			51	municipal disposal place
artificial leather	replacement from coach	59			59	municipal disposal place
isolation material (cotton glass)	some phases of technology process	61			61	municipal disposal place
rubber	some phases of technology process	26			26	municipal disposal place
hard paper	some phases of technology process	5	5	reproduction plant		
wood	some phases of technology process	580	580	to be sold to population		
cloth for cleaning	some phases of technology process	65			65	municipal disposal place
oil and grease	runoff of lubricants and waste of cleaning machines	369	100	regeneration	269	oil base
metal	rejected products (spare parts)	11845			11845	reproducing plant
burned earth	from casting shop and foundry shop	600			600	municipal disposal place
garbage (with leaves)	from all parts	1000			1000	municipal disposal place
construction wastes (20% combustible)	small construction wastes	500			500	municipal disposal place

(Source: Tashkent Workshop)

Appendix 5-3 Data on Environmental Condition of Uzbekistan Depot

Table 1 Water Consumption at Sections of Uzbekistan Depot (Industrial Need)

Name of item	Number of Units	Norm of water consumption (m ³)	Annual consumption	
			(day/year)	(m ³)
1. Main Depot (TP-1, TP-2 and other shops) Washing section Washing of parts and details	1,335 sections	1		1,335
2. Mechanic section Machine maintenance and its cooling	8 machines	0.035	365	102.2
3. Rheostat diesel loco tests	7 sections per year	11		77
4. Washing locomotives Outside (external) washing electric locomotives	1,212 sections	2		2424
5. Outside washing of electric sections	5,986 sections	2		11,972
6. Outside washing diesel locomotives	55 sections	2		110
7. Accumulator washing and charging	11,175.50	2		22,351
8. Compressor 6 hours/day *10 m ³ /min	600 minutes	0.0025	365	5,749
9. Compressor in TP-1, production of 18 m ³ /min	1,200 minutes	0.004	365	18,834
10. Compressor at the sand drying machine production of 5.3 m ³ /min	1,440	0.0025	365	7312.4
11. Forging section Hammer	1	0.04	307	12.28
12. Servicing personnel	0.5	5	307	767.5
13. O F M				
a) Preparation of cold mixture of concrete	10 m ³	0.275	307	844.25
b) Preparation of lime mixture solution	3 m ³	0.22	307	270.16
c) Watering of concrete in summer	20 m ³	0.4	153	1,224
d) Brickwork with a cold mixture solution	4,000 bricks	0.18		720
e) Preparation of cement	20 m ³	0.304	307	1842
f) Plastering works	400 m ³	0.004	307	491.2
g) Lime slake	25 tons	4		100
14. Vehicles				
a) Washing of freight vehicles (trucks)	5	0.8	365	1,460
b) Washing of sedan cars	6	0.5	365	1,095
c) Washing of bus	2	2.5	365	1,825
d) Washing of motor	2	0.025	365	18.25
e) Repair of freight cars 1 month per vehicle	5	0.7	30	105
f) Repair of sedan cars	6	0.5	30	90

(Source: Uzbekistan Depot)

Table 2 (1/2) Water Consumption at Sections of Uzbekistan Depot (Drinking and Domestic Need)

Name of item	Number of Units	Norm of water consumption (m ³)	Annual consumption	
			(day/year)	(m ³)
1. Canteen				
a) Preparation of lunch	300 dishes	0.036	365	3942
b) Washing of dishes	6	0.25	365	547.5
c) Drinking/ domestic need of personnel	5 people	0.025	365	45.63
2. Food-stuffs shop				
	1 people	0.02	307	6.1
3. Drinking/domestic needs of workers				
	230 people	0.025	365	2098.75
4. Hand-washing basin				
	4	0.06	365	876
5. Shower				
	2307 people	0.04	365	3958
6. Cleaning of rooms				
	28000 m ³	0.08	365	8176
7. Administrative building				
	100 people	0.1864		18.64
8. Administrative building				
	100	0.025	365	912.5
9. Equipping of diesel locomotives				
	7 section	0.18	365	460
b) Full cooling system at the equipping	7	0.1	183	128.1
10. Laboratory				
a) Filter preparation	5 filters	0.36	365	657
b) Distillate preparation for accumulator charging		0.18	365	65.7
11. Watering of territory				
	82000 m ²	0.004	212	69536
12. Watering of green plants				
	100	0.004	212	84.8
13. Buffet				
	2	0.25	307	153.3
14. Boiler room				
	3	150	130	58500
15. Domestic need of personnel				
	1 people	0.025	307	7.62
16. Chemical laundry				
	3	0.08x25	307	1842
17. Fire extinguisher charging section				
	1 charge/day	0.25	365	91.3
18. Acetylene charging welding section				
	1 charge/day	0.35	365	127.75
19. Toilet/running water per day				
	1	3.5	365	1310
20. Preparation of soda water tab in TP-1				
	1	0.3	365	1314

(Source: Uzbekistan Depot)

Table 2 (2/2) Water Consumption at Sections of Uzbekistan Depot
(Technical Maintenance of Railcars)

Name of item	Number of Units	Norm of water consumption (m ³)	Annual consumption	
			(day/year)	(m ³)
1. Drinking /domestic needs	3 people	0.035	365	38.325
2. Washing wagons	1504 sections	0.002	365	1097.9
3. Showers	3 people	0.04	200	24
4. Hand-wash basin	3 people	0.025	365	27.34

(Team rest house in Uzbekistan station)

1. Domestic needs	3 people	0.025	365	27.37
2. Watering of territory	1500 m ³	0.004	212	1272
3. Rest house of loco-motive teams	45 people	0.025	365	410.6
4. Watering of gardens	600 m ³	0.025	212	3180
5. Showers	45 people	0.06	365	985.5

(Source: Uzbekistan Depot)

Table 3 (1/2) Pollution Emissions Parameters (into atmosphere) for Uzbekistan Depot (Source: Uzbekistan Depot)

Section	Sources of Pollutants		Number of working hours in a year	Name of source	Height of source (m)	Diameter of Stack (m)	Emission of Pollutants		Name of treatment	Quality of treatment (%)	Name of pollutants	Emission	
	Name	Number					Speed (m/s)	Temperature (°C)				Emission (m³/a)	Volume (m³/a)
Fire extinguisher charge section	Tank	1	1178	Stack	3	0.2	10	0.314	35.7	-	Alkaline	0.00022	0.0014
	Engine rewinding bench	1	254	Stack	2	0.4	9	1.13	35.7	-	Xylene White spirit	2.6	0.01
	Accumulator	1	1270	Stack	3	0.15	9.5	0.168	35.7	-	Sulfuric acid	0.000006	0.0003
Charge section	Bath	2	127	Stack	4	0.3	11	0.777	35.7	-	Alkaline	0.00027	0.000005
	Accumulator	1	1178	Stack	5	0.35	2.6	0.237	35.7	95	Abrasive metal dust	0.0022	0.00289
	Grinding machine	1	365	Stack	5	0.35	2.6	0.237	35.7	3 m n-900	Oxides of iron	0.03548	0.23346
	Mechanical saw	1	365	Stack	5	0.35	2.6	0.237	35.7	3 m n-900	Oxides of manganese	0.010553	0.00709
	Planer	1	365	Stack	5	0.35	2.6	0.237	35.7	3 m n-900	Nitrogen oxides	0.0178	0.117
	Lathe	1	2190	Stack	5	0.35	2.6	0.237	35.7	3 m n-900	Carbon monoxide	0.0176	0.11571
	Welding unit	1	2555	Stack	5	0.35	2.6	0.237	35.7	3 m n-900	Emulsion	0.000037	0.00022
Pressing black-smith section	Gas welding	1	1825	Stack	7	0.25	9.5	0.0486	35.7	-	Solid substance	0.03367	1.0474
	Smith forge	1	3650	Stack	7	0.5	11	2.159	120	-	Carbon monoxide	0.00557	0.1655
											Nitrogen oxides	0.02247	0.0325
Mechanic Section	Milling machine	1	3650	Stack	5	0.35	2.6	0.237	35.7	-	Emulsion	0.000375	0.00142
	Planer	2	3650	Stack	5	0.15	9.5	0.168	35.7	-	Abrasive metal dust	0.0097	0.05206
	Lathe	3	3650	Stack	5	0.15	9.5	0.168	35.7	-	Abrasive metal dust	0.0022	0.00289
	Face grinding machine	1	1095	Stack	5	0.35	2.6	0.237	35.7	-	Kerosene	0.10825	0.57
	Cylindrical grinding machine	1	730	Stack	5	0.35	2.6	0.237	35.7	-	Hydrocarbon	0.1794	0.663
	Grinding machine	1	1825	Stack	5	0.35	2.6	0.237	35.7	-	Induction oil	0.0000013	0.000014
	Baths	2	1460	Stack	5	0.15	9.5	0.168	35.7	-	Oxides of iron	0.03548	0.23346
	Foot stand	1	2190	Stack	5	0.15	9.5	0.168	35.7	-	Oxides of manganese	0.010553	0.00539
	Organic materials washing section	2	3650	Stack	5	0.25	9.5	1.864	35.7	-	Nitrogen oxides	0.0178	0.117
	Welding section	1	1778	Stack	5	0.25	9.5	1.864	35.7	-	Carbon monoxide	0.0176	0.11571
Fuel equipment section	Gas welding	1	1270	Stack	12	0.15	10.5	0.186	35.7	-	Oxides of iron	0.0027	0.00437
											Oxides of manganese	0.00019	0.00051
											Abrasive metal dust	0.022	0.0302
											Abrasive metal dust	0.022	0.0302
											Abrasive metal dust	0.022	0.0302
											Abrasive metal dust	0.022	0.0302
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											Abrasive metal dust	0.022	0.0302
											Abrasive metal dust	0.022	0.0302
											Abrasive metal dust	0.022	0.0302
Washing section	Washing machine	1	730	Stack	16	0.25	10.5	1.01	35.7	-	Sodium carbonate	0.01	0.02628
	Turnst. lathe	1	1095	Stack	17	0.35	10.5	1.01	35.7	-	Emulsion	0.000018	0.01095
O.F.M.	Electric welding	1	3650	Stack	7	0.4	12	1.507	35.7	-	Oxides of iron	0.03548	0.14902
	Gas welding	1	1095	Stack	7	0.4	12	1.507	35.7	-	Oxides of manganese	0.010553	0.00539
Fuel	Lathe	1	730	Stack	16	0.25	10.5	1.01	35.7	-	Nitrogen oxides	0.0178	0.0702
											Carbon monoxide	0.0176	0.0694
Fuel	Grinding machine	1	365	Stack	5	0.35	2.6	0.237	35.7	95	Abrasive metal dust	0.000018	0.01095
	Tank	14	8760	Stack	5	0.35	2.6	0.237	35.7	3 m n-900	Diesel fuel	0.00022	0.0018
Garage	Gas station	2	1825	Stack	10	0.5	1.6	0.314	35.7	-	Benzine	0.005	0.15892
											Mineral oil	0.00002	0.0006
											Hydrocarbon	0.8235	0.0948
											Emulsion	0.000018	0.0005
											Abrasive metal dust	0.0176	0.19105

Table 4 (1/2) Pollutant emissions parameters in future perspective for Uzbekistan Depot

Section	Sources of Pollutants		Number of working hours in a year	Name of source	Source number	Height of source(m)	Diameter of Stack(m)	Emission of Pollutants		Name of treatment	Quality of treatment (%)	Name of pollutants	Emission	
	Name	Number						Speed (m/s)	Volume (m ³ /s)				Temperature (°C)	%
Fitter repair section	Washing and drying filter unit	1		Stack	42	8	0.5	7.8	1.53	35.7	-	Hydrocarbons	0.03	0.25
	Parts washing bath	1		Stack	42	8	0.5	7.8	1.53	35.7	-	Hydrocarbons	0.03	0.25
	Sedimentation tank	1		Stack	43	9	0.355	16	1.6	35.7	-	Nitrogen oxides	0.005	0.04
	Washing machine	1		Stack	44	9	0.315	6.9	0.53	35.7	-	Carbon monoxide	0.006	0.06
	Bath for impregnation	1		Stack	44	9	0.315	6.9	0.53	35.7	-	Oxides of manganese	0.002	0.02
Electric units repair section	Gas welding	1		Stack	45	8	0.5	1.27	0.25	35.7	-	Silicon	0.001	0.01
	Electric welding	1		Stack	45	8	0.5	1.27	0.25	35.7	-	Oxides of iron	0.0298	0.298
Refrigerator repair section	Parts heating and drying box	1		Stack	46	9	0.4	3.4	0.42	35.7	-	Lead aerosol	0.00005	0.00004
	Electric bath for welding nozzle	2		Stack	46	9	0.4	3.4	0.42	35.7	-	Hydrocarbon	0.001	0.01
Assembly-line operation of diesel locomotive repair	Stand	1		Stack	47	17	0.25	18	0.87	35.7	-	Lead aerosol	0.0000002	0.0000005
	Welding chamber	1		Stack	47	17	0.25	18	0.87	35.7	-	Alkaline	0.0026	0.0211
Transformer inspection section	Paint chamber	1		Stack	48	17	0.63	6.3	1.8	35.7	-	Sulfuric acid	0.013	0.1
	Drying chamber	1		Stack	49	17	0.25	10	0.5	100	-	Oxides of manganese	0.006	0.06
	Drying chamber	1		Stack	50	17	0.83	9	2.3	80	-	Silicon	0.002	0.02
	Washing machine	1		Stack	51	17	0.28	13.5	0.83	100	-	Fluorides	0.003	0.03
	Drying unit	1		Stack	51	17	0.28	13.5	0.83	100	-	Oxides of iron	0.018	0.03
Wheel lathe section	Wheel washing machine	2		Stack	52	17	0.315	8.4	0.6	95	-	Xylene	0.3	2.7
	Chamber for air cooling of engine and generator	1		Stack	53	17	0.56	10	2.5	35.7	-	Xylene	0.04	0.35
Boiling washing machine	Boiling washing machine	1		Stack	54	17	0.25	5.1	0.25	80	-	Alkaline	0.007	0.007
	Chamber for air cooling of parts of engines	1		Stack	55	17	0.56	10	2.5	35.7	-	Xylene	0.03	0.27
Collector soldering unit	Collector soldering unit	1		Stack	56	17	0.18	2.8	0.07	35.7	-	Alkaline	0.0002	0.002
	Drying furnace	3		Stack	57	8	0.63	4.8	1.3	100	-	inorganic dust	0.0002	0.2
Drying section	Drying chamber	1		Stack	58	17	0.9	10	6.23	35.7	-	Lead aerosol	0.000036	0.000054
	Impregnating furnace unit	1		Stack	59	8	0.7	1.7	0.65	35.7	-	Xylene	0.09	0.8
Roller section	Washing machine	1		Stack	60	17	0.9	10	6.23	35.7	-	Xylene	0.03	0.3
	Engine washing unit	1		Stack	61	17	0.2	17.4	0.55	80	-	Xylene	0.039	0.339
Polymer section	Polymerization chamber	1		Stack	62	8	0.4	13.2	1.65	35.7	-	Alkaline	0.0002	0.002
	Revolving stand	1		Stack	62	8	0.4	13.2	1.65	35.7	-	Alkaline	0.0002	0.002
Ventilator cabin	Ventilator cabin	1		Stack	63	8	0.35	8.8	0.43	35.7	-	Acetone	0.2	0.3
	Absorber box	1		Stack	63	8	0.35	8.8	0.43	35.7	-	Hydrocarbon	0.03	0.25

(Source: Uzbekistan Depot)

Table 4 (2/2) Pollutant emissions parameters in future perspective for Uzbekistan Depot

Section	Sources of Pollutants		Number of working hours in a year	Name of source	Source number	Height of source (m)	Diameter of Stack (m)	Emission of Pollutants			Name of treatment	Quality of treatment (%)	Name of pollutants	Emission g/s	ton/year
	Name	Number						Emission speed (m/s)	Volume (m ³ /s)	Temperature (°C)					
Babbit section	Furnace for babbit	1													
	Electric furnace	2													
	Induction bath	1		Stack	64	8	0.4	12.7	1.6	150	-	-	Lead aerosol	0.00001	
	Babbit machine	1		Stack	65	8	0.4	6.6	0.88	35.7	-	-	Hydrocarbon	0.05	
	Babbit bath	1													
Blachmith secto	Babbit machine	1		Stack	66	8	0.4	5.7	1.17	150	-	-	Carbon monoxide	0.02	
	Forge	1											Nitrogen oxides	0.001	
Thermal section	Induction unit	1													
	Electric furnace	1													
	Oil tank	1		Stack	67	8	0.315	15	1.16	150	-	-	Benzine	0.0008	
	Washing machine	1		Stack	68	3.5	0.15	7.4	0.18	50	-	-	Hydrocarbons	0.001	
		1											Alkaline	0.001	
Boiler room	Welding post	1		Stack	69	13.4	0.2	13.3	0.42	35.7	-	-	Hydrocarbons	0.009	
		1											Oxides of manganese	0.0002	
		1											Silicon	0.0005	
		1											Fluoride	0.0048	
	4		Stack	70	30	1.6	11.8	23.7	142	-	-	Oxides of iron	1.618		
												Nitrogen oxides	5.214		
												Carbon monoxide	0.009		
														85.56	

(Source: Uzbekistan Depot)

Table 5 Noise in the Working Place for Uzbekistan Depot

Place	Additional Information	Noise Characteristics				Levels of Noise pressure in dB and in octave lines in Hz												
		Spectra		Time characteristics				Maximum allowable level										
		Wide band width	Tense	Constant	Vibrated	Interrupted	Impulse	31.5	63	125	250	500	1000	2000	4000	8000	BA	
IP-1 shop	Babbit machine	+			+			107	95	87	82	78	75	73	71	69	60	
Ventilation fan (excess)		+						74	70	72	76	73	75	68	70	65	80	
Pneumatic press for rubber and plastics (excess)		+			+			92	89	83	79	80	82	75	72	69	82	
Hydro press (excess)		+						74	65	72	67	73	77	72	70	66	77	
Equipment test stand (excess)		+				+		98	92	88	83	85	87	83	80	78	98	
Sharpening machine (excess)		+			+			65	64	67	75	79	81	79	74	72	82	
Drilling machine		+						70	72	74	68	71	74	73	68	60	70	
Lathe		+						74	75	77	80	78	75	74	69	64	76	
Tool room (excess)		+			+			92	88	90	87	89	85	80	88	75	91	
Milling machine No 1886		+			+			80	76	74	77	75	73	70	69	61	74	
Test grinding machine No 9359 (excess)		+						75	77	74	77	80	75	74	72	70	83	
Machine shop milling machine No 5147		+			+			73	72	75	75	71	68	70	67	63	74	
Planing machine No 5582 (excess)		+			+			80	77	79	82	80	77	79	75	72	82	
Grinding machine No 3108 (excess)		+			+			84	78	73	77	75	76	70	72	70	78	
Tool grinding machine No 9382 (excess)		+			+			79	80	77	78	81	80	77	79	76	85	
Lathe No 808 (excess)		+			+			73	74	76	78	77	74	70	64	64	79	
Lathe No 1500 (excess)		+			+			72	74	77	79	76	74	77	72	66	76	
Mechanic scissors (excess)		+			+			75	79	77	78	82	83	76	72	70	85	
Drilling machine		+			+			66	64	70	75	71	66	64	62	60	73	
Compressor repair work		+			+			75	73	69	70	72	66	60	58	56	67	
Compressor test (excess)		+			+			80	82	90	96	88	84	82	73	70	87	
IP3 shop bogie repair section		+			+			76	74	74	77	75	73	73	71	65	77	
Lathe No 4254		+			+			72	71	76	79	77	75	72	72	63	78	
Bogie assembling section (excess)		+			+			77	74	76	78	80	79	76	74	67	82	
Shop for automatic coupling repair sets (excess)		+			+			79	77	69	74	78	80	84	78	80	85	
Welding		+			+			71	74	72	78	75	72	71	68	63	74	
Machine shop lathe No 1292		+			+			75	73	74	76	70	72	68	64	64	74	
Tool grinding machine (excess)		+			+			78	77	73	76	80	74	75	72	70	81	
Section for top equipment repair (excess)		+			+			72	70	75	71	74	77	78	70	66	76	
Pentograph test stand		+			+			69	67	68	71	73	65	67	64	51	62	
Regulation of resetting equipment stand		+			+			70	64	65	67	64	62	60	57	55	66	
Suppression test stand		+			+			76	75	77	70	72	71	74	68	60	72	
Electrical equipment shop		+			+			62	58	60	63	64	63	58	55	50	70	
Equipment regulation stand		+			+			65	62	66	70	65	67	61	60	57	73	
Relay regulation stand		+			+			60	63	62	57	59	51	47	45	42	60	
Tool grinding machine (excess)		+			+			70	69	70	74	79	80	78	77	70	86	
Electrical machine shop		+			+							1	5	5	6	1	6	
Winding section		+			+			68	62	64	66	65	68	65	62	57	70	
Welding section		+			+			69	70	67	70	72	71	67	63	60	72	
Hard facing under flux		+			+			70	73	75	74	77	72	70	67	62	73	
Planing machine (excess)		+			+			79	80	85	78	93	90	84	83	80	100	
Surface marking machine (excess)		+			+			80	79	88	92	90	89	85	80	77	94	
Circular Saw (excess)		+			+			76	83	81	85	85	90	92	94	86	102	
Rocking type Saw (excess)		+			+			81	78	90	87	89	88	86	90	85	94	
IP1 shop																		
Beginning along central line		+			+			70	74	72	70	71	72	63	67	61	74	
In the middle		+			+			73	78	75	74	76	73	71	70	65	78	
At the end, automatic coupling section (excess)		+			+			71	66	74	77	75	72	73	73	70	80	
During shunting locomotive working (excess)		+			+			77	79	76	78	80	78	76	74	72	87	
Overhead travelling crane (excess)		+			+			68	74	75	75	73	78	70	68	66	78	

(Source: Uzbekistan Depot)

Table 6 (1/2) Inside air measurements under 100% capacity of equipment for Uzbekistan Depot (1995)

Location for sampling (comments)	Temperature (°C)	Relative humidity (%)	Distance from the floor (m)	Distance from the source (m)	Aspiration speed (L/min)	Component	Determined Concentration (mg/m ³)	Maximum allowable concentration (mg/m ³)						
Section of automatic coupling repair Working place (ventilation fan (working))	23.5	71	1.5	0.5	20	Welding aerosol	26 22.8 28.1	4						
						10	Mn aerosol	0.04 0.03 0.04	0.2					
					10		Chromium anhydride	0.0231 0.0399 0.0378	0.01					
						300mL	Nitrogen oxides	7 8.5 7	2					
							Carbon monoxide	25 38 43.7	20					
						In the middle of room	23.5	71	1.5	0.5	20	Welding aerosol	15.4 13.3 9.5	4
10	Chromium anhydride	0.0126 0.0083 0.0083	0.01											
	300mL	Nitrogen oxides	2 3 2	2										
		Carbon monoxide	25 25 38	20										
	Grinding by manual grinding machine	26	42	1.5	0.5						20	Metal dust	12.9 10.2 15.8	6
Mechanic shop Tool grinding machine (No ventilation, windows and doors are open)												21	65	1.5
						Boring of lead plain bearings	21	65	1.5	0.5				
	Metal dust	8.9 17.9 13.2	6											
Boring of bronze parts (There is ventilation)	21	65	1.5	0.5	20	Bronze dust	3.9 3.8 2.6	8						
						Lead aerosol	0.0052 0.0052 0.004	0.01						
									Boring of balance rollers (No ventilation)	22	62	1.5	0.5	20
Tool shop Tool grinding machine (No ventilation)	22	65	1.5	0.5	20	Abrasive dust	13.7 12.1 11.1	6						
						Shaft turning (No ventilation)	22	65	1.5	0.5	20	Metal dust	3.2 1.8 2.6	6
												Polymer section Vulcanization of rubber (No ventilation, not working)	23	52
Sulfur anhydride	not detected not detected not detected	10												
			CO	15 15 20	20									

(Source: Uzbekistan Depot)

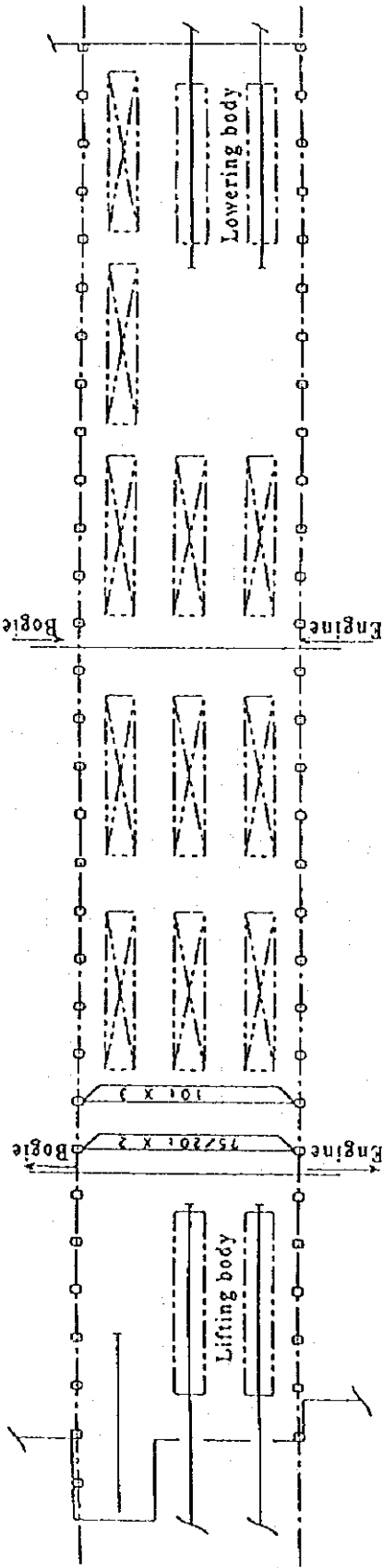
Table 6 (2:2) Inside air measurements under 100% capacity of equipment for Uzbekistan Depot (1995)

Location for sampling (Comments)	Temperature (°C)	Relative humidity (%)	Distance from the floor (m)	Distance from the source (m)	Aspiration speed (L/min)	Component	Determined Concentration (mg/m ³)	Maximum allowable concentration (mg/m ³)
Calcium casting section								
Melting furnace for babbit pigs			1.5	0.5	20	Lead aerosol	0.018 0.013 0.017	0.01
Bearing boring (local ventilation)			1.5	0.5	20	Lead aerosol	0.018 0.016 0.015	
					1	Hydrochloric acid	0.16 0.46 0.58	5
Calcination section								
Dust from						Lead	0.03 mg	none (should not be)
window							0.02 mg	
door							0.07 mg	
window-sill							0.03 mg	
wall							not detected	
table for in- struments							0.06 mg	
radiator							0.09 mg	
blower							0.12 mg	
samovar							not detected	
cup							not detected	
AOH								
Joining machine (no ventilation)	20	68	1.5	0.5	20	Wood dust	5.8 5.3 4.7	6
Lathe (no ventilation)						Wood dust	7.4 10 10.5	
Marking machine (no ventilation)						Wood dust	17.4 32.1 28.4	
Circular saw (no ventilation)						Wood dust	105.8 52.1 62.1	

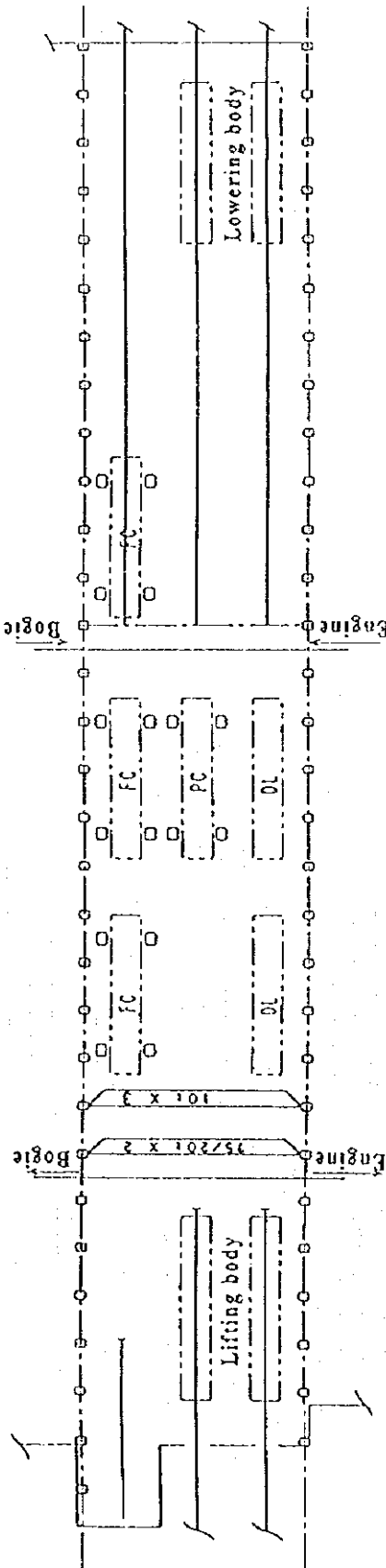
(Source: Uzbekistan Depot)

Appendix 11.2.1 Workshop Design

Bodyshop for locomotive (improvement)



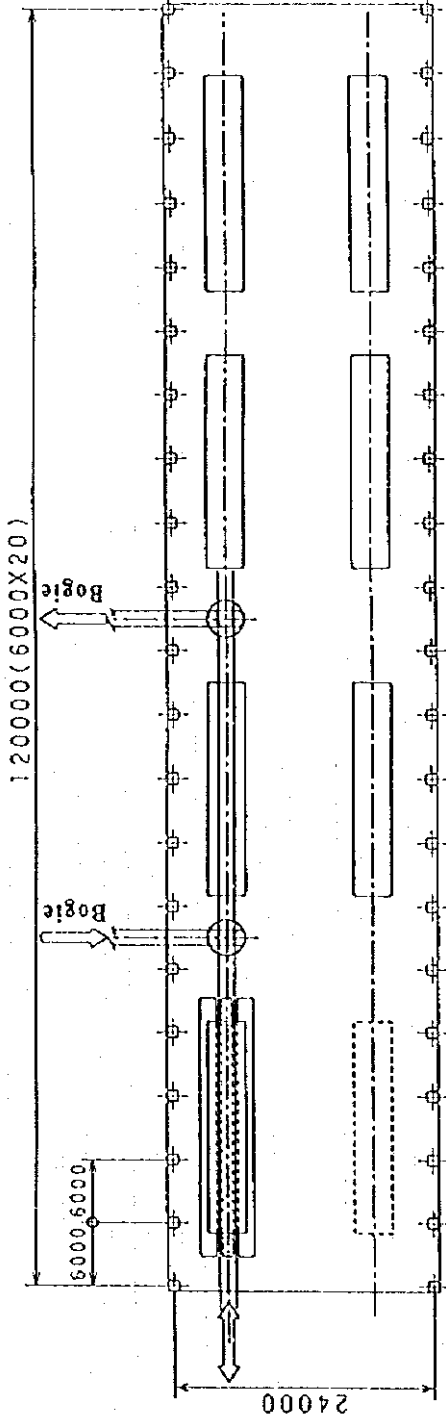
Bodyshop for locomotive (Present state)



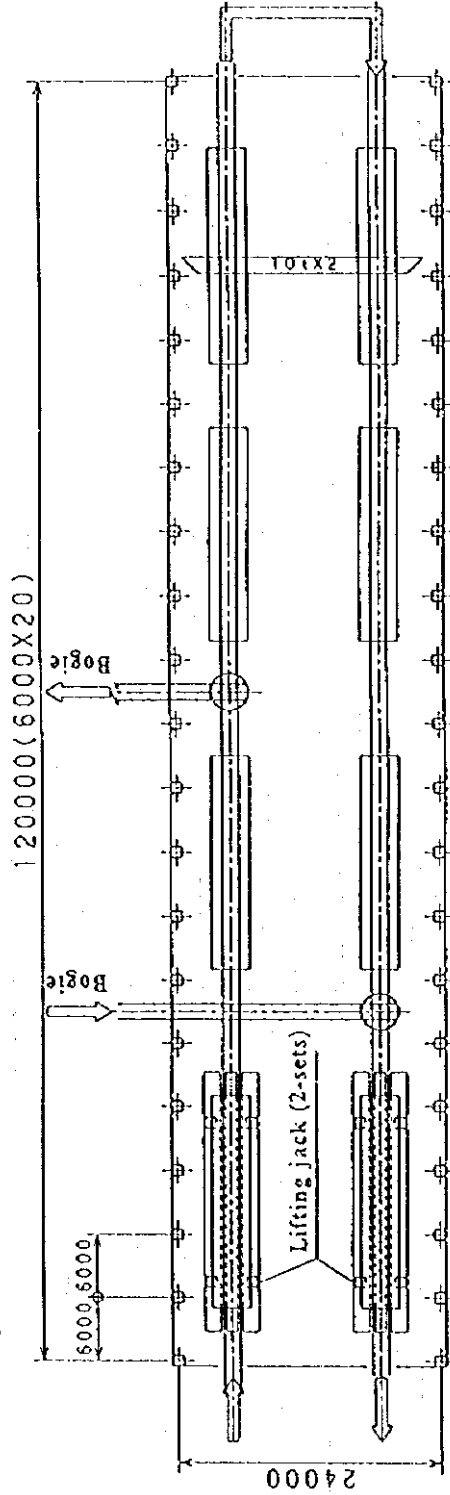
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30

Appendix 11.2.1 Fig 1 Arrangement Plan of Locomotives

Plan of inspection / repairing shed for EC (Overhead travelling crane) Body 20m (L) x 3.5m (W)

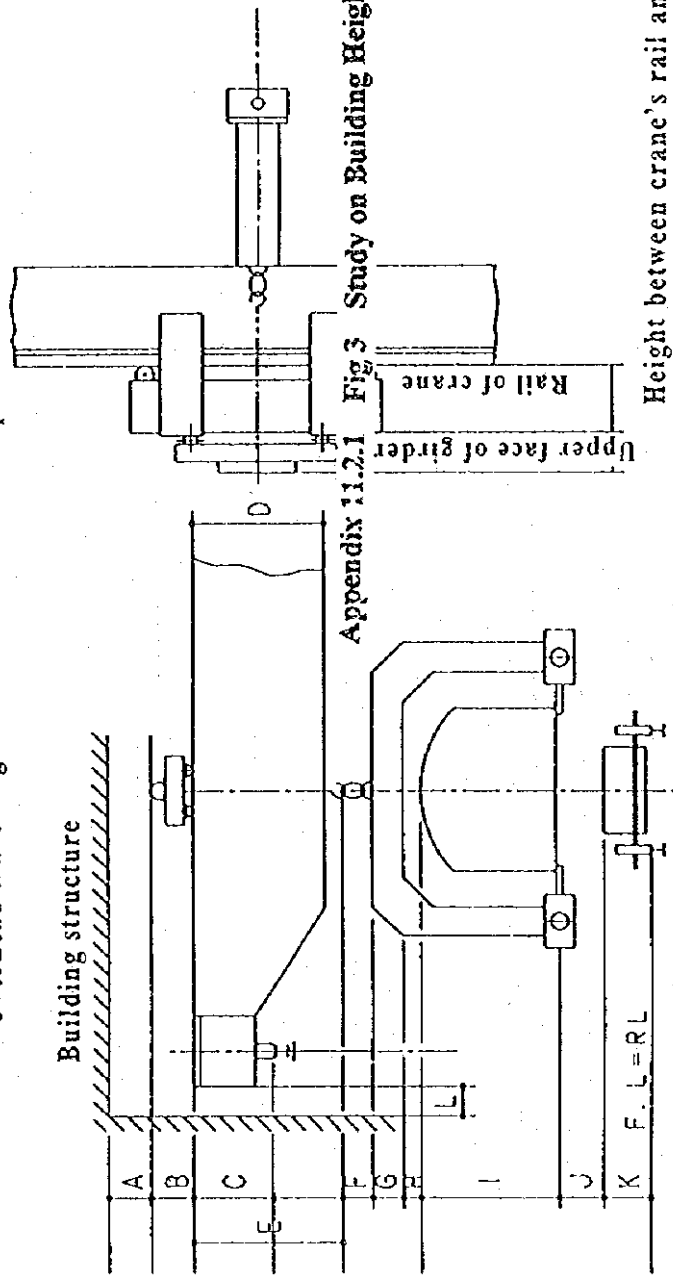


Plan of inspection / repairing shed for EC (Lifting jack)



Appendix 11.2.1 Fig 2 Arrangement Plan of car-body

Overhead travelling crane 20t x 22500mm span



Appendix 11.2.1 Fig 3 Study on Building Height of Car body Shop

Height between crane's rail and lower part of building

$$= A+B+C$$

$$= 400 + 1,500 + 550 = 2,450 \text{ mm or more}$$

Height between crane's rail and F.L.(R.L.)

$$= E-C+F+G+H+I+J+K$$

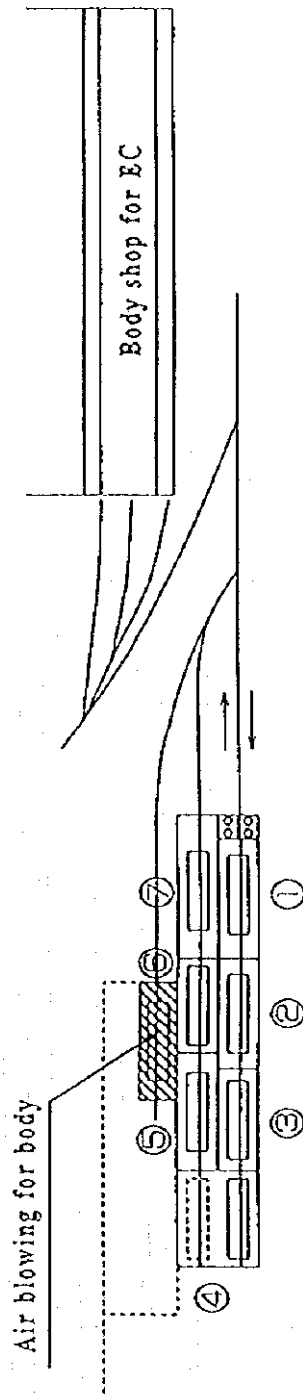
$$= 1,200 - 550 + 500 + 500 + 800$$

$$+ 4,200 + 1,000 + 1,500 = 9,150 \text{ mm}$$

$$\text{Height of building} = 2,450 + 9,150 = 11,600 \text{ mm}$$

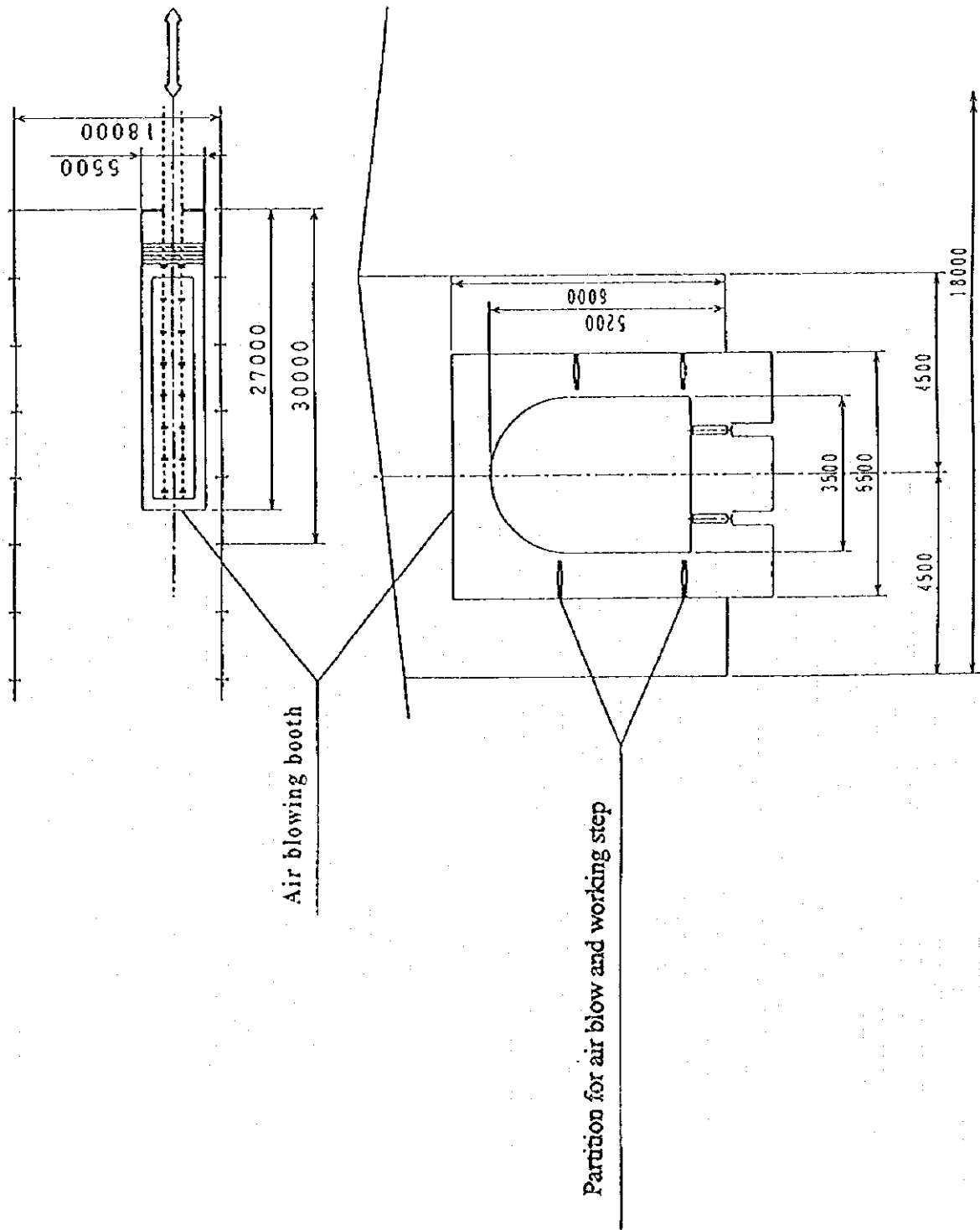
A:	400 or more	F:	500	K:	1,500
B:	1,500	G:	500	L:	400 or more
C:	550	H:	800		
D:	1,000	I:	4,200		
E:	1,200	J:	1,000		

Appendix 11.2.1 Fig 3 Study on Building Height of Car body Shop

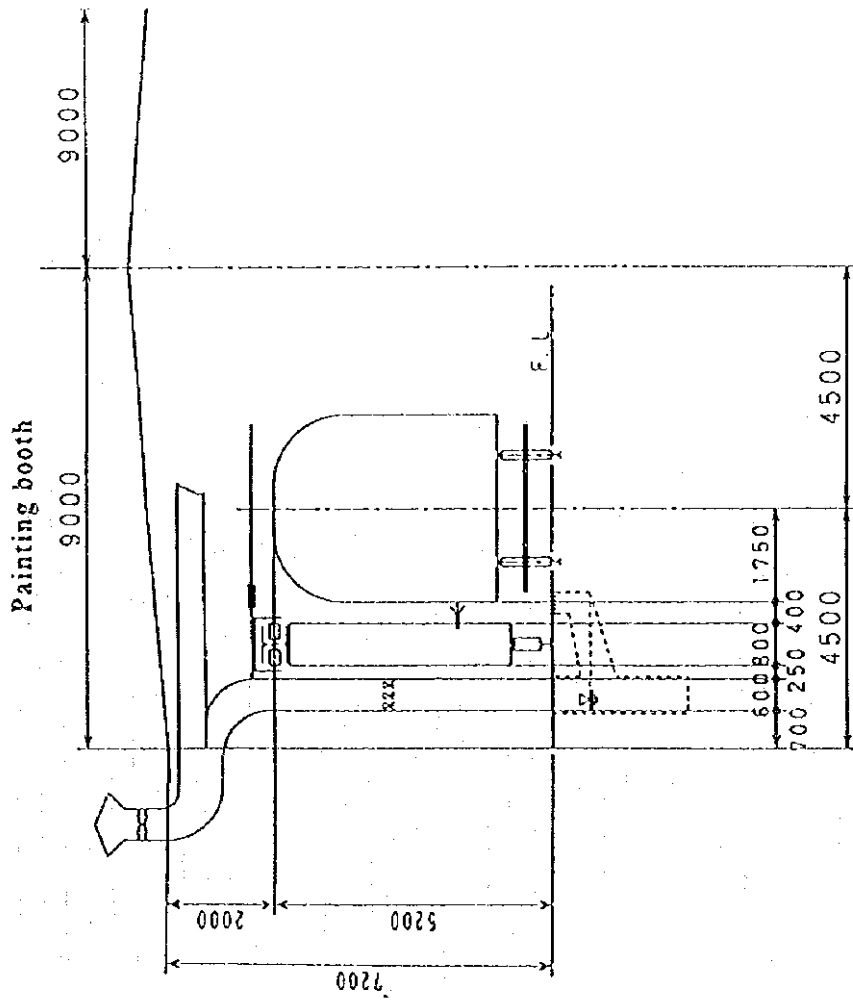


- First step of Tact system
 - ① Machine cleaning of body-side
 - Cleaning of front/ear of body by manual work
 - Preparation for painting
- Second step of Tact system
 - ② First painting
 - ③ Drying
- Third step of Tact system
 - ④ Preparation for painting
 - Traversing of body
 - ⑤ Second painting
- Fourth step of Tact system
 - ⑥ Drying
 - ⑦ Marking

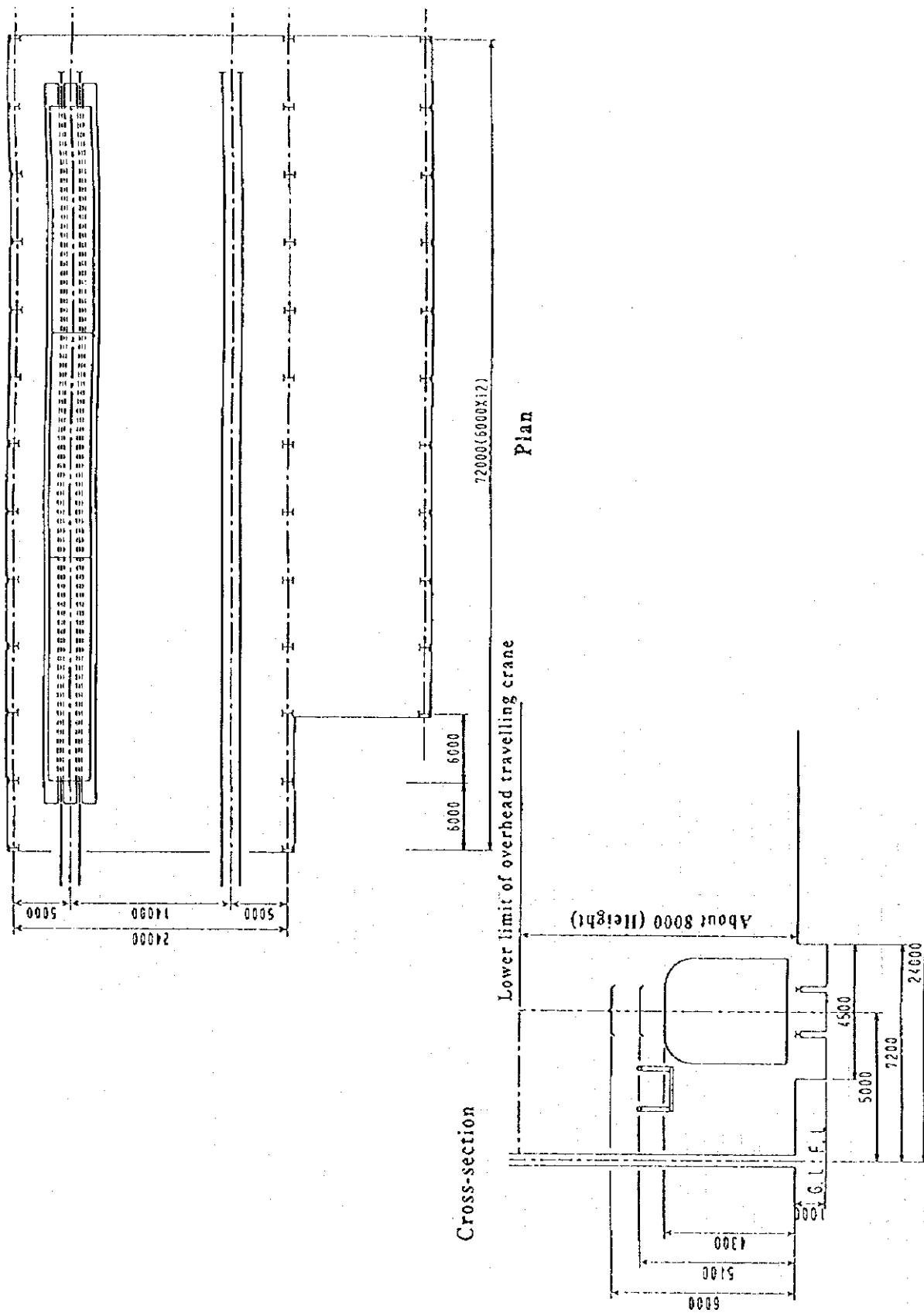
Appendix 11.2.1 Fig 4 Blowing / Painting Shed and Sequence of Painting Work



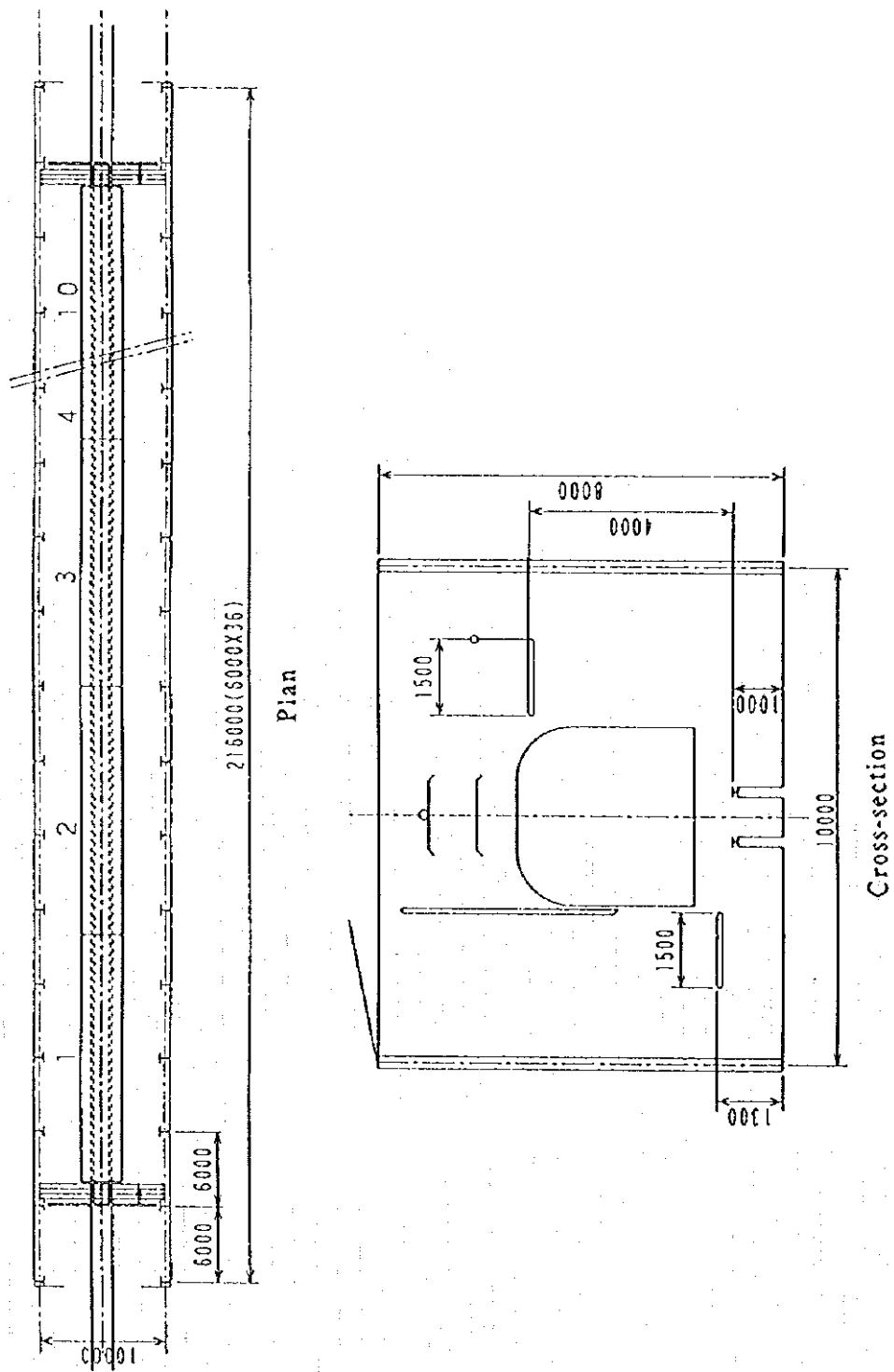
Appendix 11.2.1 Fig 5 Study on Air Blowing Shed for EC



Appendix 11.2.1 Fig 6 Study on Painting Facilities



Appendix 11.2.1 Fig 7 Study on Final Inspection Shed for EL



Appendix 11.2.1 Fig 8 Study on In-coming/Final Inspection Shed for EC

Appendix 11.2.3-1 Reduction Method of Wastewater in Plating shop

Appendix 11.2.3-1 Reduction Method of Waste and Wastewater in Plating Shop

Electroplating wastes predominantly include spent process baths and rinse water contaminated by drag-out. Most of the wastes contained in drag-out (e.g., heavy metals, organic compounds, cyanide) are toxic and must be converted to some less hazardous form (e.g., chemical/physical processes). A typical electroplating process is shown in Fig. 1 of Appendix 11.2.3-1. Plated workpieces are rinsed with water, water used in this rinse process is physico-chemically treated and this process produces sludge (including heavy metals) and wastewater, which is one of causes which deteriorate the environmental condition.

The problem of the reduction of pollution loads produced by the electroplating industry represents one of the most classical and also most studied cases concerning attempts to apply technique for the recovery of metals from wastes. Electroplating waste can be minimized by the following methods:

- perfecting various operating practices;
- optimizing rinse system (improving efficiency); and
- modifying process and equipment.

In general, when there is reduction in waste generation, reduction in wastewater quality is also observed. Changing operation practices and improving rinse efficiency tend to be less costly and should be implemented prior to considering modification of process and equipment. The following aspects should be considered:

- reducing loss of metals and chemicals;
- minimizing or reducing drag-out chemicals;
- conserving water;
- recirculation rinse water; and
- increasing recyclability of unavoidable waste.

Considering the reduction in waste generation, one example is shown in Fig. 2 of Appendix 11.2.3-1. Water which is used in the rinse process is separated two parts, a concentrated water and a diluted water with the reverse osmosis treatment. If the former is recyclable, this concentrated solution is reused in the electroplating process, but if not, metals are recovered with electrolysis. The latter is reused as a rinse water.

Another example is shown in Fig. 3 of Appendix 11.2.3-1. This electroplating process includes:

- increasing the number of rinse baths;
- removing contaminants from plating and rinse baths; and
- distilling rinse solution to separate into a concentrated solution and water

Increasing the number of rinse baths reduces the waste and wastewater to be treated, and contaminants produced in the processes are removed from plating and rinse baths, which make plating and rinse baths reusable. Furthermore, the distillation separates the used rinse solution into a concentrated solution and water. The former is reused in the electroplating bath, and the latter is reused as a rinse water.

In the process of alkali cleansing for workpieces, the same consideration is useful.

A summary is:

(1) Increasing the number of rinse baths reduces the consumption of water, and the production of wastewater and wastes.

(2) Removing contaminants from plating and rinse baths to make plating and rinse baths reusable.

1) Oil skimming: Oil and grease are removed.

2) Filtration: Contaminants removal from plating baths.

3) Microfiltration and Ultrafiltration: This is a dynamic mechanical filtering process performed by means of membranes which allow selective separation, purification and concentration of organic substance of high molecular weight. Small particles (of the order of a micron), such as those produced by metal surface working can be separated. Some of the fields of application of microfiltration and ultrafiltration in the purification of industrial outflows are:

- oily emulsion;
- outflow water from metal finishing treatments;
- outflow water containing high concentration of tensionactives; and
- outflow water from painting plants.

(3) Concentrating used rinse solution to make it reused in the electroplating process

1) Distillation: Distillation is a simple and reliable process which is widely applied. It is the best process for chrome-plating. In general, the evaporation gives rise to a condensate containing traces of metals, which, however, can be used for the final rinse while the concentrate may be recycled for the metal-finishing bath. Many types of evaporator are available on the market, generally intended for the recovery of chrome. Vacuum concentrators, powered by electricity which, by means of cooling circuit working as heat pump, can concentrate water solutions with various concentration ratios

depending on needs, are particularly suitable. The advantages of these concentrators are:

- extreme compactness;
- low energy consumption;
- no fumes, smells, noises and vibrations;
- low maintenance; and
- possibility of treating thermolabile substances, thanks to the low operating temperature.

2) Reverse osmosis: The reverse osmosis is the separation of a component of a solution from another component of the same solution by means of a pressure exerted on a semipermeable membrane. The porosity of the membranes used for reverse osmosis may vary from 5 to 250 Angstrom; up to 99% of salts may be removed. The reverse osmosis treatment can be applied in the following main sectors:

- treatment of outflows containing colorings with their possible recovery;
- treatment of outflows containing oily emulsions, latex and electrophoretic paints; and
- treatment of metal salts and reuse of the water in cleaning.

The concentrated solution can be reused in the electroplating process and the purified water can be also used in the rinse process.

3) Electrodialysis: This is a process in which electrically charged membranes are used to separate ions from water solutions by the effect of a difference of electric potential.

4) Electrolysis: Recovery of metal content.

5) Solvent Extraction: Solvent extraction has all the characteristics to allow efficient recovery of metals from sludge mixtures or solutions, also because it is possible to recover the single metals, although up to now the costs are higher than the value of the metals recovered. Its greatest possibilities of application are in the selective separation of metals, by the formation of metal compounds which can dissolve in an organic phase. Specific chelating agents are normally used to extract the metal (Cd, Cr, Cu, Ni and Zn) in the organic phase. Experience has shown that there are various metal-chelation compounds, many of which dissolve in organic solvent. As in general the chelating compounds are much more expensive than the metals to be recovered, it must be possible to recycle the chelating material.

6) Chelating resins: Chelating resins selectively adsorb heavy metal ions from aqueous solutions.

(4) Removing Neutral Salts: Used alkaline or acidic aqueous solution is neutralized under relatively

high concentration and the neutral salts are recovered from the neutralized aqueous solution with solar energy, because the salinization of the surface water system is one of the most important environmental problems in Uzbekistan.

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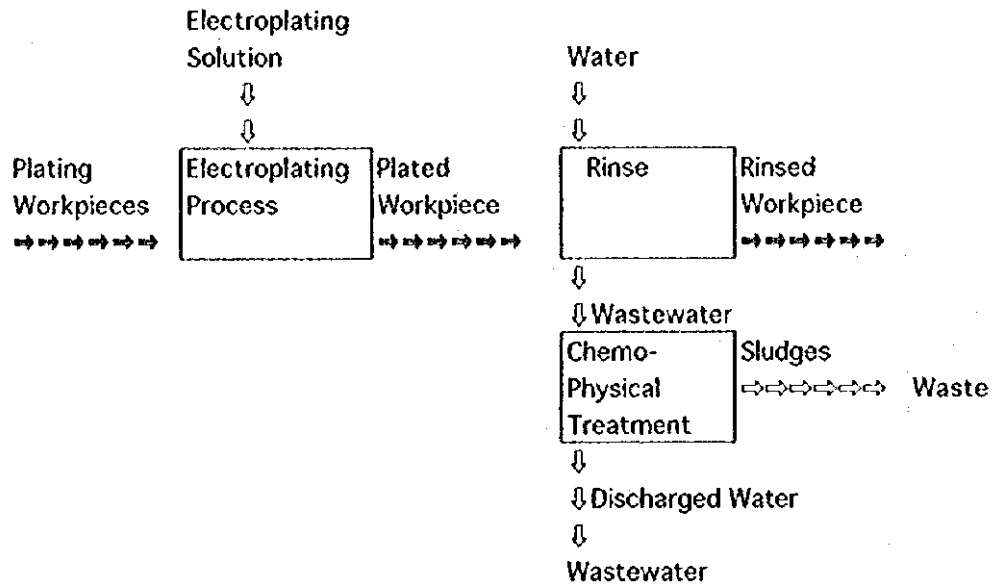


Fig.1 Typical Plating Process (Source: M. Pizzichini, "Membrane Technology: Applications to Industrial Wastewater Treatment (Hazardous Waste Reduction in the Metal-Finishing Industry)", 1995, Kluwer Academic Publishers)

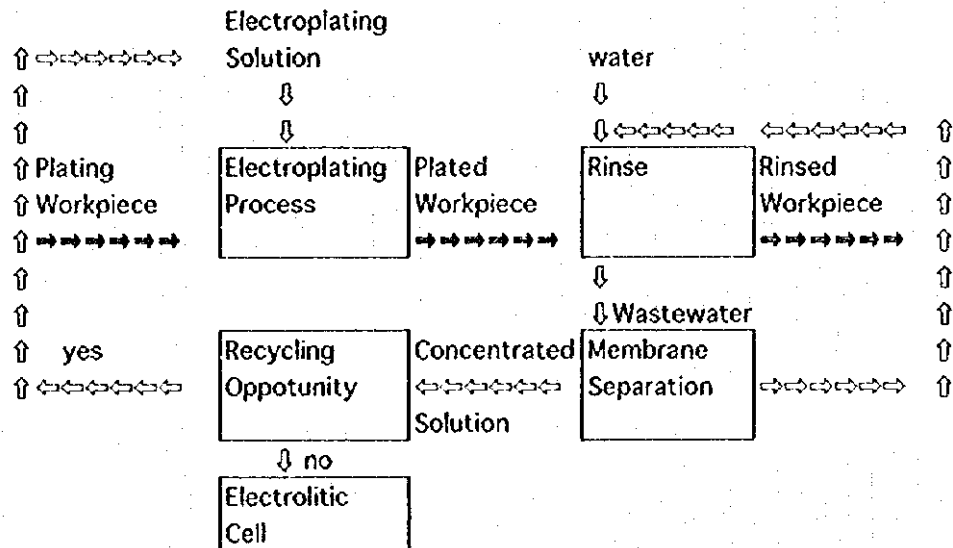
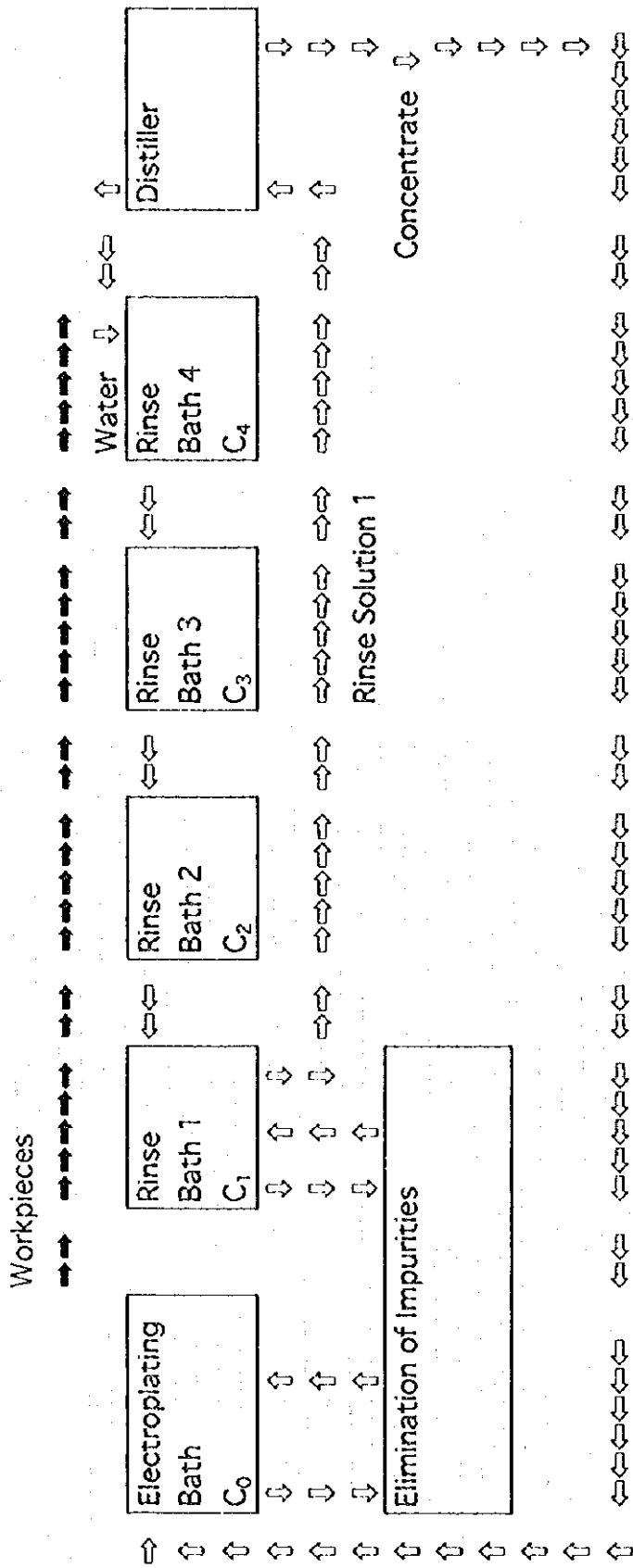


Fig.2 Plating Process Including Reuse (Source: M. Pizzichini, "Membrane Technology: Applications to Industrial Wastewater Treatment (Hazardous Waste Reduction in the Metal-Finishing Industry)", 1995, Kluwer Academic Publishers)



Concentration of Bath Solution

$C_0 : 100\text{g/l}$

$C_1 : 10\text{g/l}$

$C_2 : 1\text{g/l}$

$C_3 : 0.1\text{g/l}$

$C_4 : 0.01\text{g/l}$

Fig.3 Plating Process Including Multi-rinse, Elimination of Impurities and Distillation

**Appendix 11.2.3.2 A Treatment System for the Wastewater Containing Oil Products
in Japanese Locomotive Repair Workshop**

Appendix 11.2.3-2 A Treatment System for the Wastewater Containing Oil Products in Japanese Locomotive Repair Workshop

The treatment system for the wastewater containing oil products in Japanese locomotive repair workshop (Fig. 1 of Appendix 11.2.3-2) consists of three parts:

- Preliminary oil separation;
- Physicochemical purification; and
- Sludge treatment.

(1) Preliminary oil separation

Wastewater enters a collecting tank through a screen, which removes coarse and settleable solids. Rain water is temporarily stored in a storage tank. These different types of water is mixed in a preliminary oil separator to adjust the water quantity and quality, and then oil separation can be carried out by natural gravity. The first purpose is to eliminate floating hydrocarbon and a fraction of mechanical emulsion of hydrocarbon. The resulting water must be sufficiently oil-free to perform physicochemical purification with economical amounts of reagents. Depending on how fine the existing emulsions are, the resulting levels of insoluble hydrocarbon may in fact vary from 20 to 150-200 mg/l.

(2) Physicochemical purification

The wastewater treated in the preliminary separator is sent into a coagulation tank, where the wastewater is pH-adjusted with sulfuric acid or sodium hydroxide aqueous solution and is treated with inorganic coagulants and/or polymer coagulants. These chemicals are commonly used to aid the flotation process, and function to create a surface or a structure that can easily absorb or entrap air bubbles. Inorganic chemicals, such as the aluminum and ferric salts and activated silica, can be used to bind the particulate matter and the oil products together and, in so doing, create a structure that can easily entrap air bubbles. Various organic polymers can be used to change the nature of either the air-liquid interface or the solid-liquid interface or both.

Oil products and particulate matters, which are coagulated in the coagulation tank with coagulants, are sent into a dissolved air flotation tank. Flotation is a unit operation used to separate solid or liquid particles from a liquid phase. Separation is brought about by introducing fine gas (usually air) bubbles into the liquid phase. The bubbles attach to the particulate matter, and the buoyant force of the combined particle and gas bubbles is great enough to cause the particle to rise to the surface.

Particles that have a higher density than the liquid can thus be made to rise. The rising of particles with lower density than the liquid can also be facilitated (e.g., oil suspension in water).

In dissolved-air flotation (DAF) systems, air is dissolved in the wastewater under a pressure of several atmospheres, followed by release of the pressure to the atmospheric level. A portion of the DAF effluent (15% to 20%) is recycled, pressurized, and semi-saturated with air. The recycled flow is mixed with the unpressurized main stream just before admission to the flotation tank, with the result that the air comes out of solution in contact with particulate matter at the entrance to the tank. The particle with air rises on the surface of the flotation tank, and is recovered as a scum in a scum recovery tank. The treated wastewater is discharged.

(3) Sludge treatment

The recovered scum is stored, concentrated, and re-coagulated and dehydrated with polymer coagulants in a sludge tank. The sludge concentrated and dehydrated in the process of sludge treatment is sent into a rotary Kiln incinerator and incinerated. Water part produced in this process is returned into the coagulation tank.

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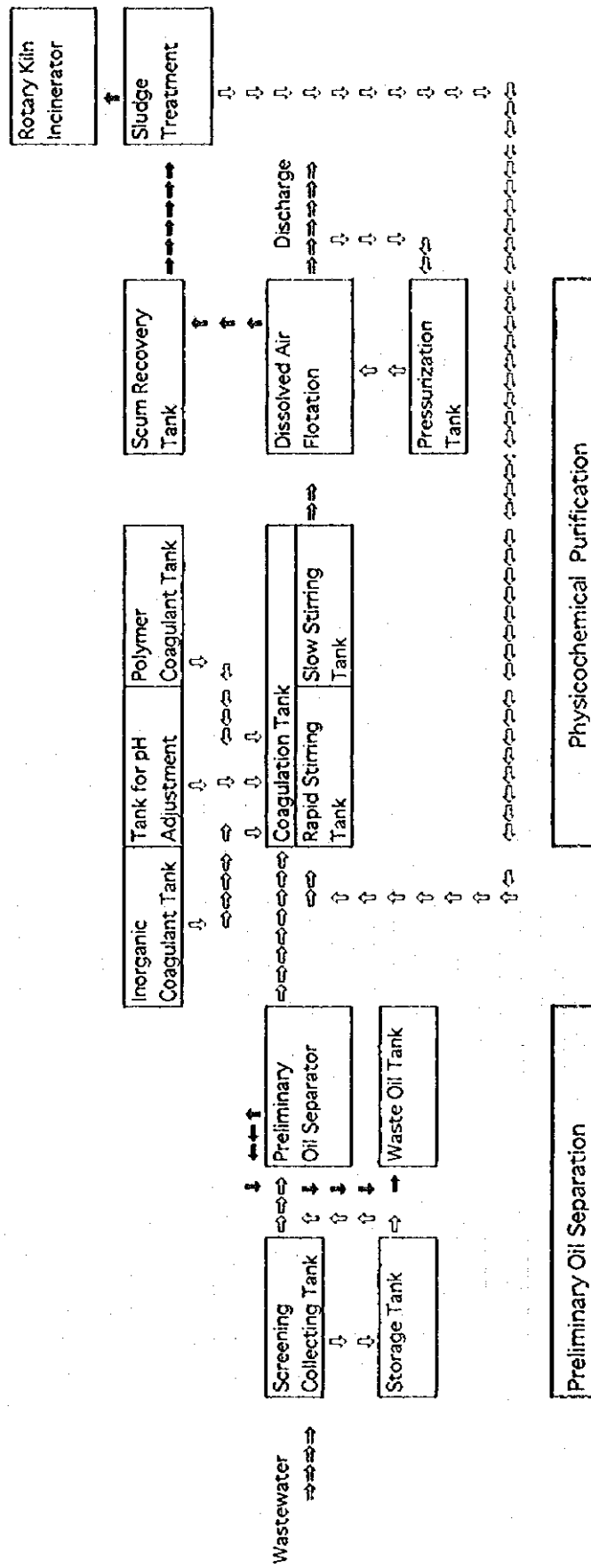


Fig. 1 A Treatment System for the Wastewater Containing Oil Products in Japanese Locomotive Repair Workshop

Appendix 11.2.3-3 Equipment for the Removal of Dust from Exhaust Gas

Appendix 11.2.3-3 Equipment for the Removal of Dusts from Exhaust Gas

The highest emission of particulate matter is caused by solid fuel furnaces due to the release of mineral fuel components. Except for few cases, even in large-scale industrial furnaces particle precipitators have not been installed either in oil furnaces operating with light fuel or in those operating with heavy fuel oil. There are several dry types of equipment for the removal of dusts from flue gases as follows:

- Gravity settling chamber
- Inertial particle collectors;
- Filters; and
- Electrostatic precipitators.

which are possible for dry collection and disposal.

(1) Gravity Settling Chamber

The gravity settling chamber is shown in Fig. 1.1 of Appendix 11.2.3-3. The gravity-type collection device depends solely on the gravitational pull on the particle to collect the dust. The separator consists of a housing and hopper in which the velocity of the gas stream is made to drop rapidly below the transport velocity of the dust particle. The velocity reduction is accomplished by the sudden expansion into the enlarged housing.

The gravity settling chamber is usually of simple design and can be manufactured of almost any material, assuming that it is not affected by temperature. Maintenance is minimal, provided that corrosion control is maintained. Applications for gravity settling chambers are limited due to the large space requirements and relatively low efficiency.

(2) Inertial Particle Collectors

1) Multiple Baffle Chamber (shown in Fig. 1.2 of Appendix 11.2.3-3)

Particulate matter can be separated from a gas by making use of their inherent forces of inertia. Obstacles are placed in the gas placed in the gas flow and divert it. Due to their mass inertia the particles carried along try to maintain their original direction. Thus, they either collide with the obstacles or reach area outside of the gas flow and are thus separated from the gas.

2) Cyclones

The gas is introduced tangentially into symmetrically rotating centrifugal separator, as shown in Fig. 1.3 of Appendix 11.2.3-3. Inside the cyclone, the gas swirls an immersed tube and the particulate is carried by inertia to the cylinder wall, from where they exit through the conical section on the bottom while the clean gas exits through the top. A cyclone alone is insufficient for the complete removal of particulate. Therefore it is used preliminary particulate removal.

(Advantages):

- Low cost of construction;
- Relatively simple equipment with few maintenance problems;
- Relatively low operation pressure drops;
- Temperature and pressure limitations imposed only by the materials of construction used; and
- Relatively small space requirements.

(Disadvantages):

- Relatively low overall particulate collection efficiencies, especially on particulate below 10 μ m in size; and
- Inability to handle tacky materials.

(3) Filters

Filters represent one of the oldest methods of removing particulate matter from a medium. Particularly in the recent past, with higher levels of removal of especially fine particles being increasingly required, filters have gained more and more importance. Filter materials are different types of fabrics or fleeces. Though fabric filters consisted of interwoven natural fibers, artificial fibers and fabrics made of fine metal threads have decidedly expanded the field of application of the fabric filter owing to their resistance against wearing and chemical influences.

The suitability of a fabric filter or fleece and its durability are determined by the operating temperature and the properties of the particles. Cotton can be used up to 80°C, wool or wool felt up to 110°C, polyacrylic nitride (orlon) or superpolyamide (nylon, perlon) up to 130°C. In addition, the two latter fabrics are almost nonreactive to moisture and chemical influences. For temperatures up to 260°C, glass fiber fabrics, e.g., are used.

For trouble-free operation moisture content and temperature of the gas must be within a certain limited range. If gas temperature falls below its dew point, clogging of the filter can ensue. Excessive gas temperature have an unfavorable effect on the durability of the fibers.

(Advantages):

- Extremely high collection efficiency on both coarse and fine particulate;
- Relatively insensitive to gas fluctuation;
- Filter outlet air may be recirculated within the plant in many cases;
- Corrosion and rusting of components are usually not problems;
- Use of selected fibrous or granular filter aids permits the high-efficiency collection of submicron smokes and gaseous contaminants;
- Filter collectors are available in a large number of configurations, resulting in a range of dimensions and inlet and outlet flange locations to suit installation requirements;
- Relatively simple operation;

(Disadvantages):

- Relative high maintenance requirements (bag replacement, etc.);
- Fabric life may be shortened at elevated temperatures and in the presence of acid or alkaline particulate or gas constituents;
- Hygroscopic materials, condensation of moisture, or tarry adhesive components may cause crusty caking or plugging of the fabric or require special additives;
- Replacement of fabric may require respiratory protection for maintenance personnel.

1) Tube Filters (shown in Fig. 2.1 of Appendix 11.2.3-3)

Depending on the performance required, a closed housing accommodates a number of filter tubes. The lower part of the housing functions as a hopper. During the filtering process dusty air enters it via the inlet. The coarse particles are immediately separated here and are removed with the already separated dust by a removing mechanism. Subsequently, the dirty air flows through filtering tubes, deposits the particles and leaves the collector, with the help of a fan, by the outlet. If the filtering layer becomes too thick and the pressure drop increases, the filter is shut down for cleansing. For this, the outlet is closed with a flap and pressurized air is blown in, washing out the tube in the opposite direction. Simultaneously, the tubes are vigorously rapped with the rapping mechanism, so that the filtrate layer falls off.

2) Baghouse Filters (shown in Fig. 2.2 of Appendix 11.2.3-3)

There is no difference between tube and frame filters in their basic mode of operation. The filtering elements consist of pillowcase-like bags pulled over tenting frames. The open slot on the one side is pulled over a flange and sealed. Filtering usually takes place from the outside to the inside. Cleaning is carried out by vibrating the frame or by alternating the air pressures to cause the filtering surfaces to flutter. During this, usually only the upper layers of

the filter cake will fall off, so that the primary layer of dust with its favorable filtering properties is preserved. The timing for cleaning is regulated by automatic pressure drop controllers.

(4) Electrostatic Precipitators

The main characteristics of electrostatic precipitators is the movement of particulate onto the walls of removal surfaces by electrical force of a high-voltage field. The precipitator is indicated by a metallic tube in which a wire which is electrically insulated against this tube is axially installed. The inside of the grounded tube is the particle collection surface. The central wire electrode is negatively charged by the high-voltage plant. Apart from the tube-type electrostatic precipitator there is the much larger group of the plate-type collectors with plate-like collection electrodes (Fig. 3.1 of Appendix 11.2.3-3).

The particle removal in an electrostatic precipitator (in Fig 3.2 of Appendix 11.2.3-3) can be divided into four basic processes as follows:

- Charging of the particulate;
- Migration of the particles to the collecting electrode;
- Deposition of the particles on the collecting electrode; and
- Removing the collected particles into the storage hopper.

(Advantages):

- Extremely high particulate collection efficiencies can be attained;
- Low pressure drop;
- Relatively low operating costs;
- Capable of operation under high pressure or vacuum conditions; and
- Capable of high temperature.

(Disadvantages):

- High capital cost;
- Very sensitive to fluctuations in gas stream conditions;
- Relatively large space requirements required for installation;
- Explosion hazard when treating combustible gases and/or collecting combustible particulate;
- Special precautions are required to safeguard personnel from the high voltage;
- Ozone is produced by the negatively charged discharge electrode during gas ionization; and
- Relatively sophisticated maintenance personnel required.

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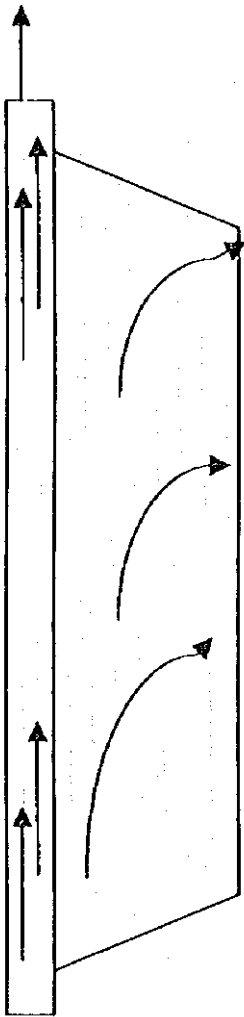


Fig. 1.1 Gravity Setting Chamber

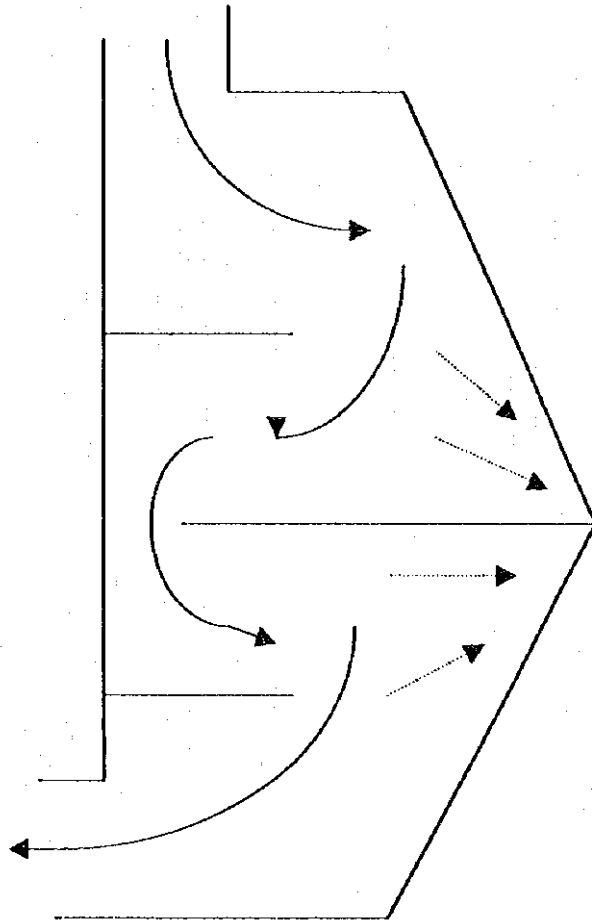


Fig. 1.2 Multiple Baffle Chamber

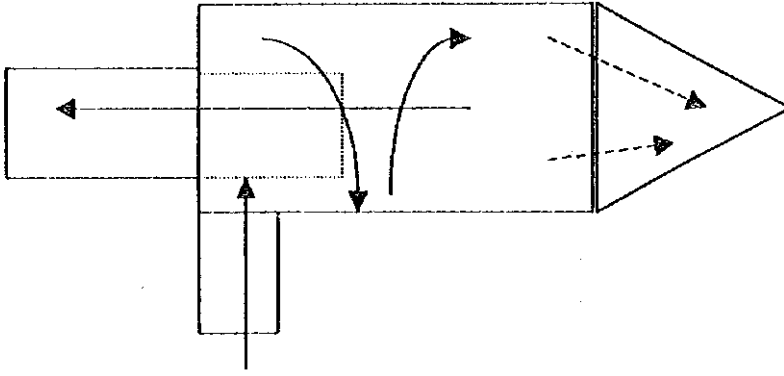


Fig. 1.3 Basic Cyclone Collector

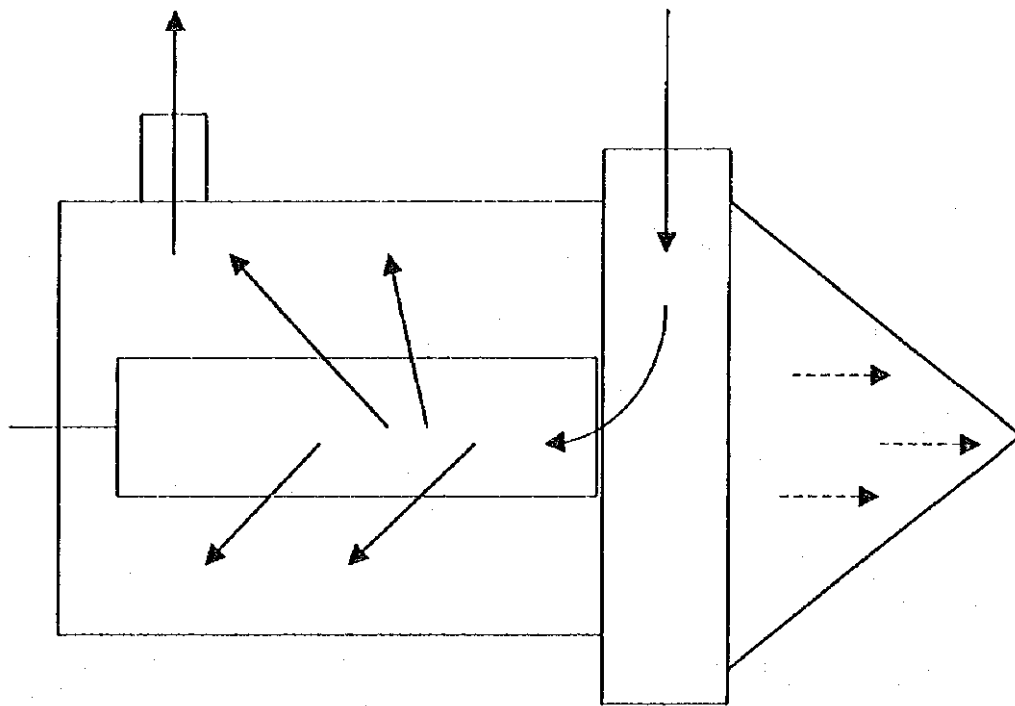


Fig.2.2 Baghouse Filter

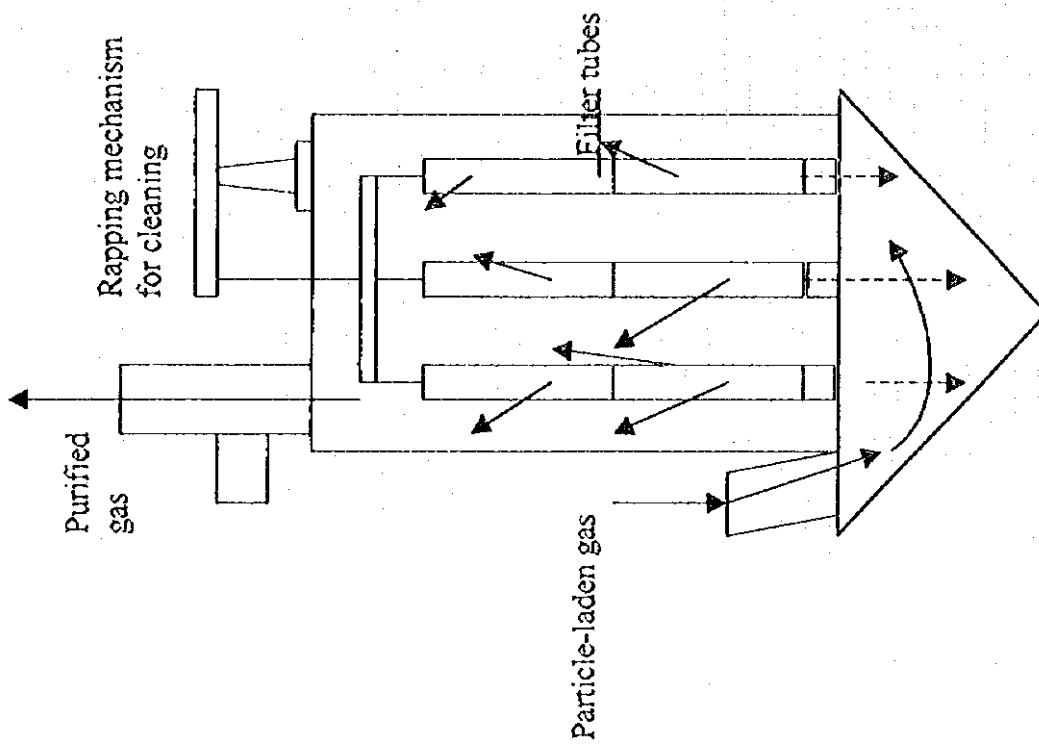


Fig.2.1 Tubular Bag Filter

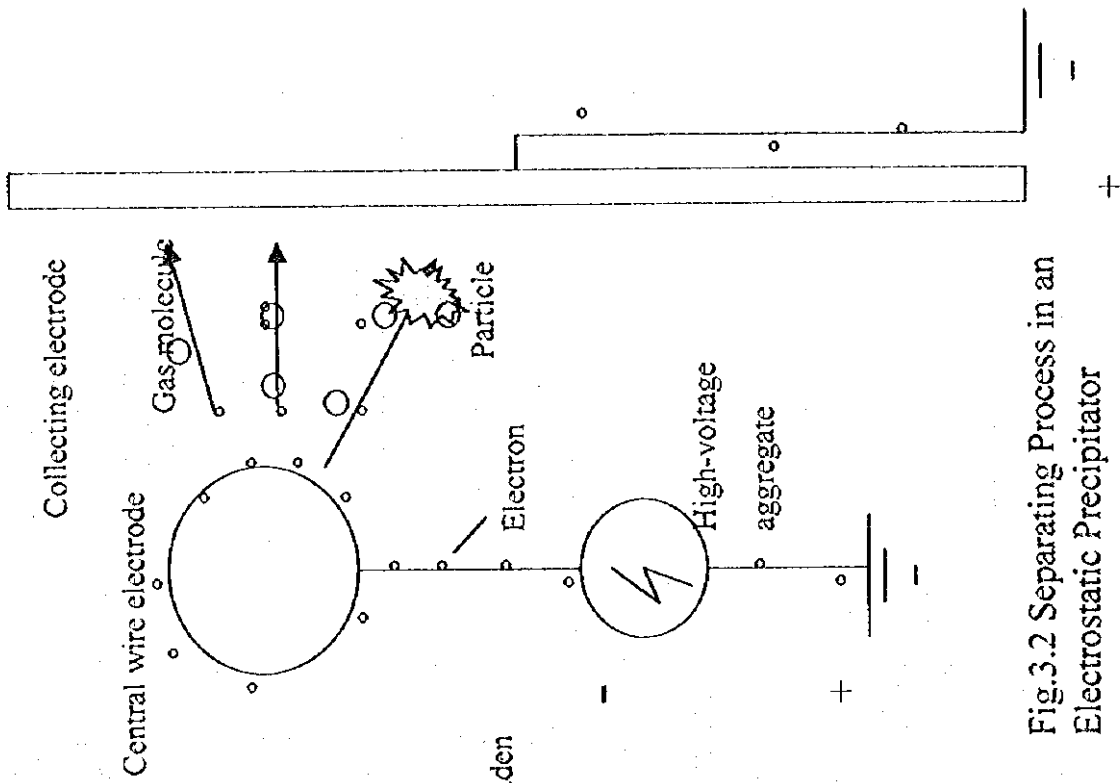


Fig.3.2 Separating Process in an Electrostatic Precipitator

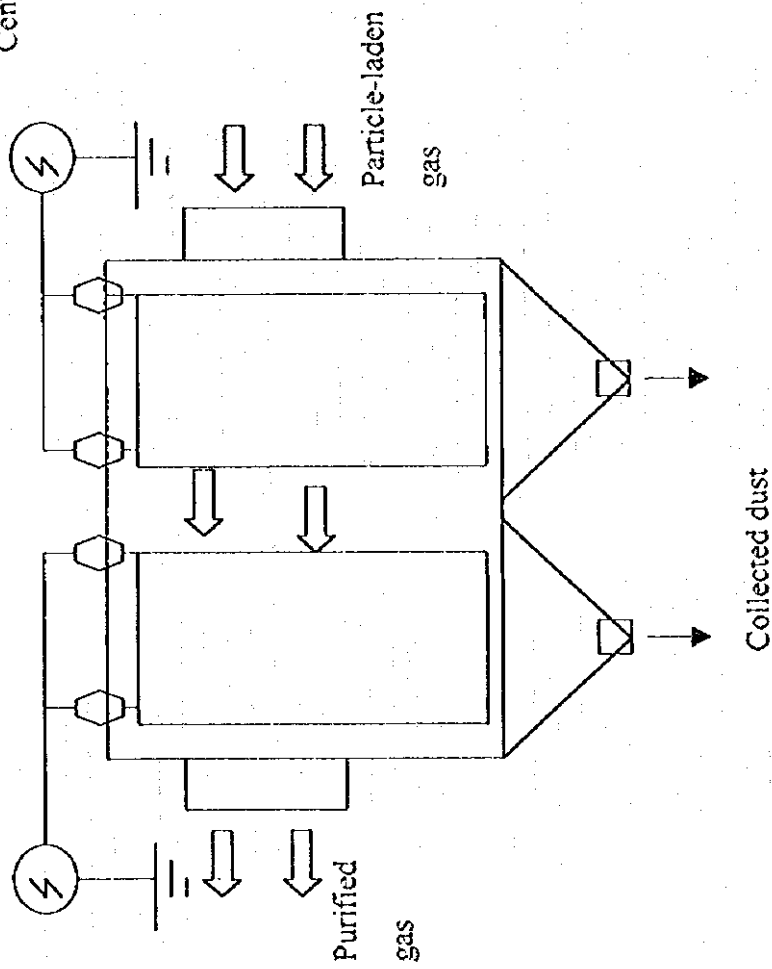


Fig.3.1 Electrostatic Precipitator

Appendix 11.2.3-4 Wet Scrubbers for the Removal of Dust and Gas Components from Exhaust Gas

Appendix 11.2.3-4 Wet scrubbers for the Removal of Dust and Gas Components from Exhaust Gas

The wet scrubber method is utilized for the removal of dust and gas components from exhaust gases, e.g., acid gas components as SO_2 , solvent components as acetone, and solid components as dust. The removal of gas and solvent components is shown in Fig. 1.1, 1.2 and 1.3 of Appendix 11.2.3-4 (Absorbers):

- Co-current type: the exhaust gas stream and liquid flow in the same direction through the scrubber (Fig. 1.1);
- Countercurrent type: the exhaust gas flows vertically upward while the liquid flows downward in direct opposition (Fig. 1.2); and
- Cross-flow type: the exhaust gas flows horizontally through the packing while the liquid flows vertically downward (Fig. 1.3).

The packing increases the contact surface between the exhaust gas and the liquid in every type of wet scrubbers.

For an exhaust gas containing dusts, a countercurrent type and a cyclone type of wet scrubber are used, as shown in Fig. 2.1 and Fig. 2.2 of Appendix 11.2.3-4, respectively. Other types of wet scrubber are:

- Moving-bed scrubbers: they incorporate a zone of movable packing where gas and liquid can mix intimately; and
- Orifice-type wet scrubbers: the gas stream comes into contact with a pool of liquid at the entrance to a constriction. Liquid is entrained and carried into the restriction, where greater liquid-particulate interaction occurs, resulting in a high frequency of particulate impact on the droplets. Upon leaving the restriction, most of water droplets are separated by gravity since the gas velocity is reduced from what it was in the restriction. Smaller droplets are subsequently removed by centrifugal force and impingement on baffles located in the upper part of the unit

(Advantages of wet scrubbers):

- No secondary dust sources;
- Relatively small space requirements;
- Ability to collect gases as well as particulate (especially "sticky" ones);

- Ability to handle high-temperature, high-humidity gas streams;
- Capital cost is low (if wastewater treatment system not required); and
- Ability to achieve high collection efficiencies on fine particulate (however, at the expense of pressure drop);

(Disadvantage of wet scrubbers):

- They may create waster disposal problem;
- Product is collected wet;
- Corrosion problems are more severe than with dry systems;
- Pressure drop and horsepower requirements may be high;
- Solids buildup at the wet-dry interface may be a problem; and
- Relatively high maintenance cost.

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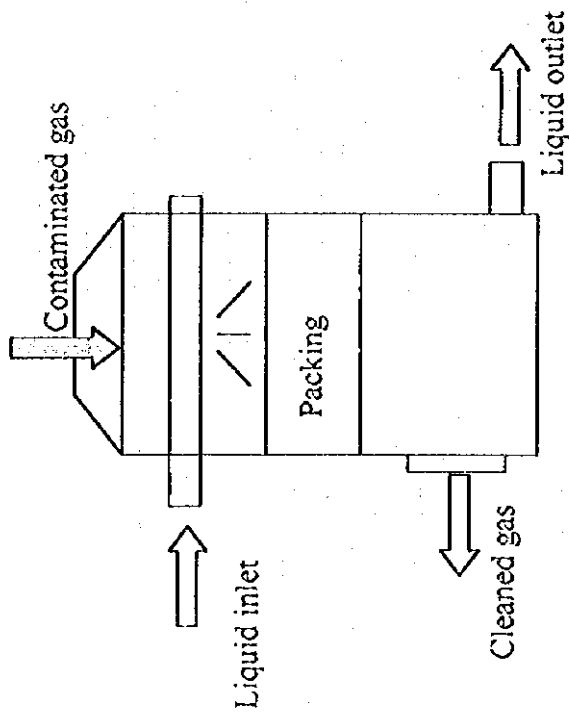


Fig. 1.1 Co-current Wet Scrubber

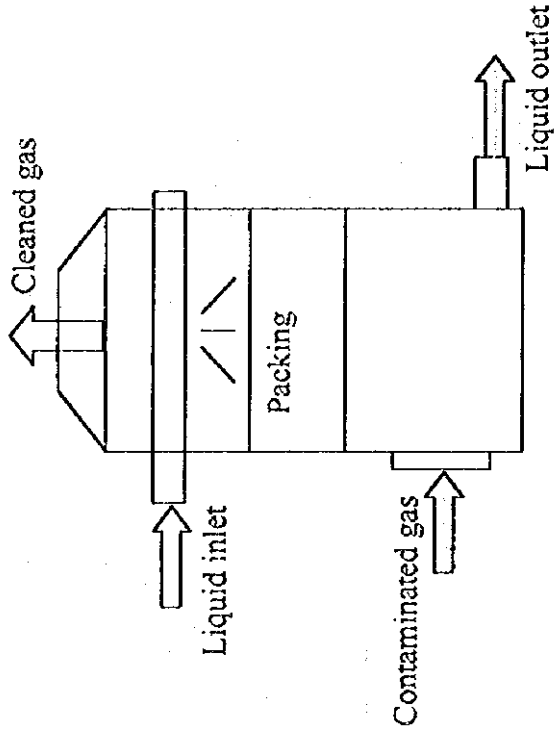


Fig. 1.2 Countercurrent Wet Scrubber

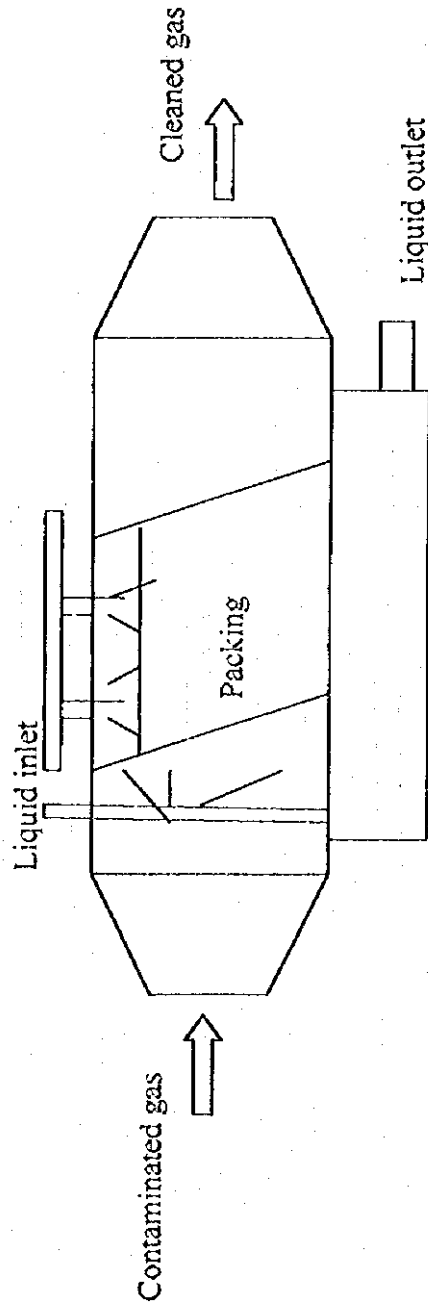


Fig. 1.3 Cross-flow Wet Scrubber

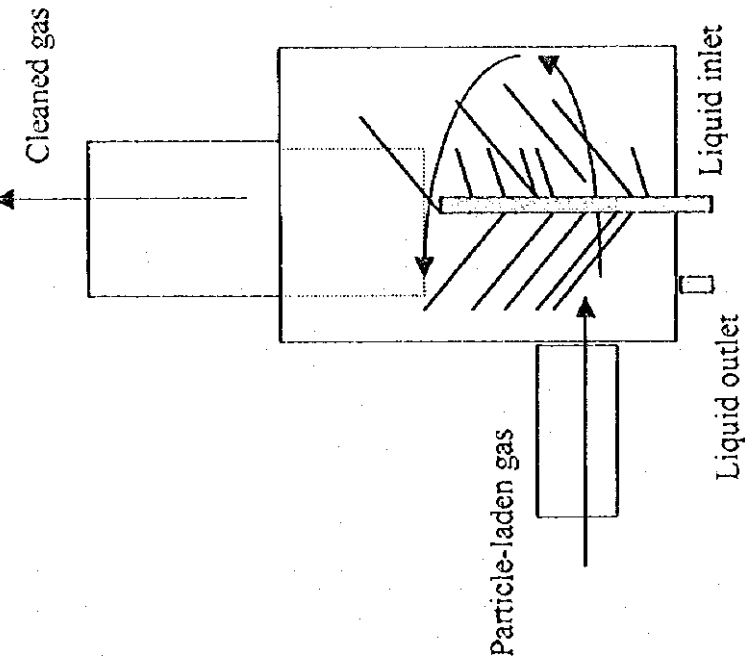


Fig. 2.2 Cyclone Scrubber

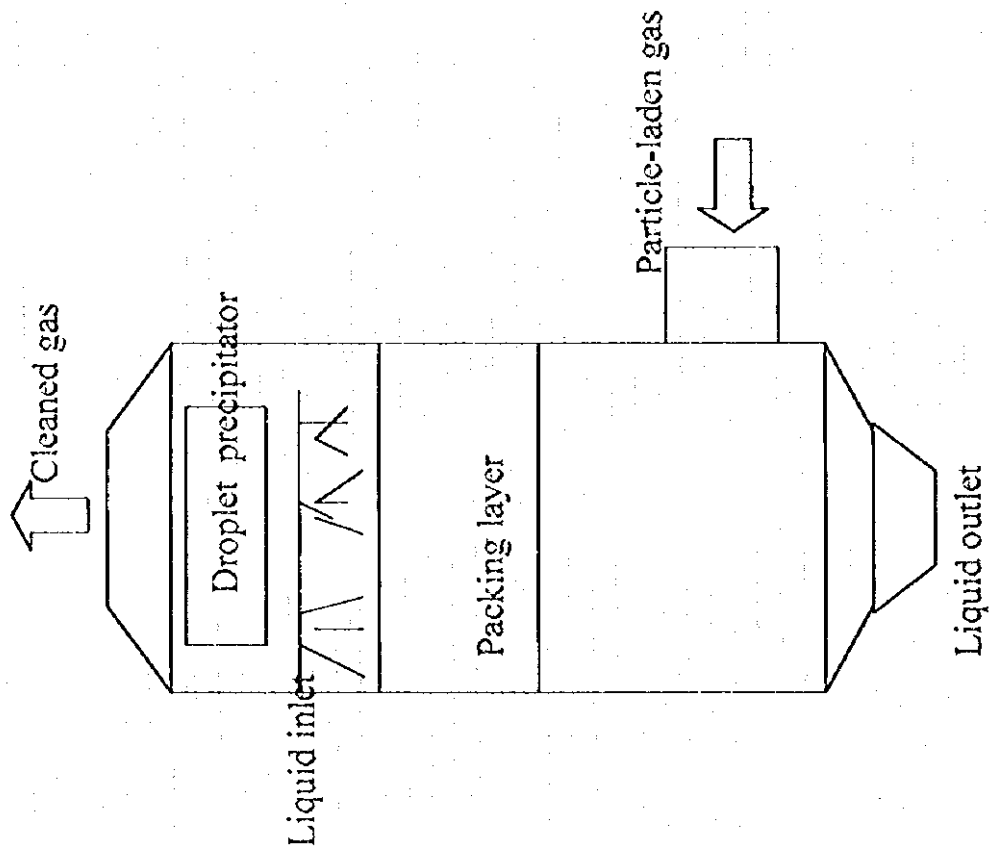


Fig. 2.1 Countercurrent Wet Scrubber for Flue Gas with Dust

Appendix 11.2.3-5 Adsorber for the Removal of Gas Solvent Components from Exhaust gases

Appendix 11.2.3-5 Adsorber for the Removal of Gas and Solvent Components from Exhaust Gases

Two major categories of adsorber that presently manufactured for industrial and commercial use are air purification devices (nonregenerative) and solvent recovery devices (regenerative).

Air purification applications are effective where the pollutants are emitted at very low concentrations (below 100 ppm) but need to be controlled because of their highly malodorous or toxic nature. These systems are cost-effective only at low concentrations because of their nonregenerative design.

In solvent recovery applications, activated carbon may be used to economically recover and reclaim solvents from process exhaust streams at concentrations in the range of 100 to 1000 ppm.

Fig. 1.1 of Appendix 11.2.3-5 presents a flow diagram of a dual stationary-bed solvent recovery system with auxiliaries for collecting the vapor-air mixture from various point sources, then transporting through the particulate filter and into the on-steam carbon adsorber, in this case bed 1. The effluent air, which is virtually free of vapors, is usually vented outdoors. The lower carbon adsorber (number 2) is regenerated during the service time of bed 1. A steam generator or other source of steam is required. The effluent steam-solvent mixture from the adsorber is directed through the condenser and the liquified mixture then run into the decanter and/or distillation column for separation of the solvent from the steam condensate.

The type shown in Fig. 1.2 of Appendix 11.2.3-5 employs vertical cylindrical beds wherein the solvent-laden air flows axially down through the bed. Water is used as coolant in the condenser. Steam, electric power to drive the blower, and cooling water are three operation cost items.

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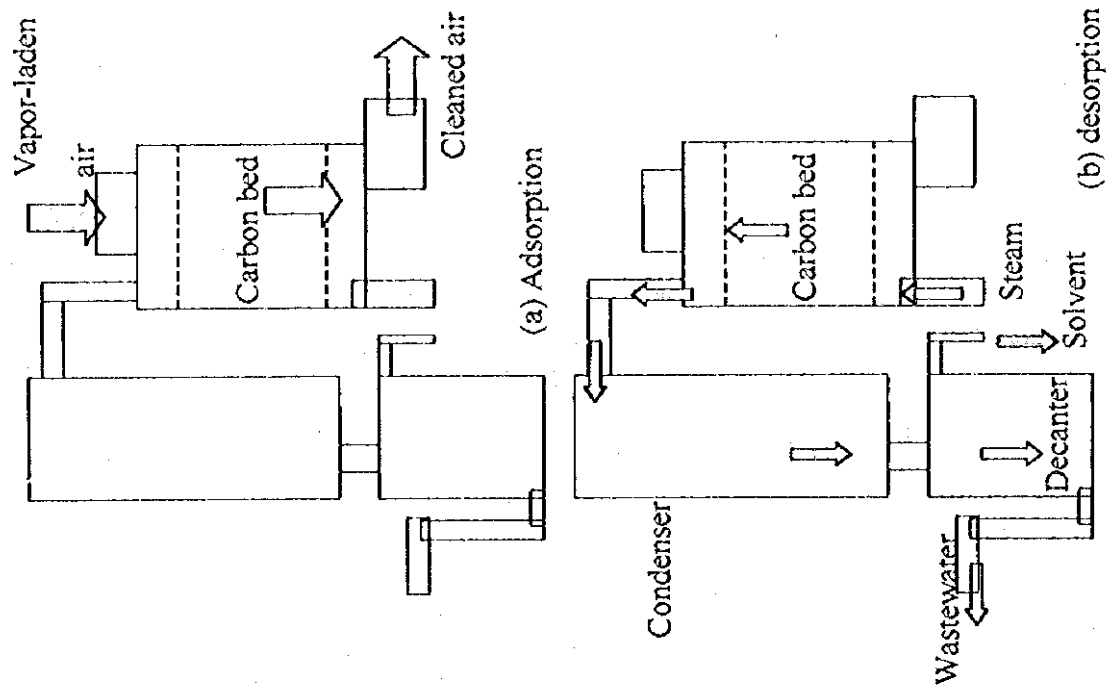


Fig. 1.2 Adsorber

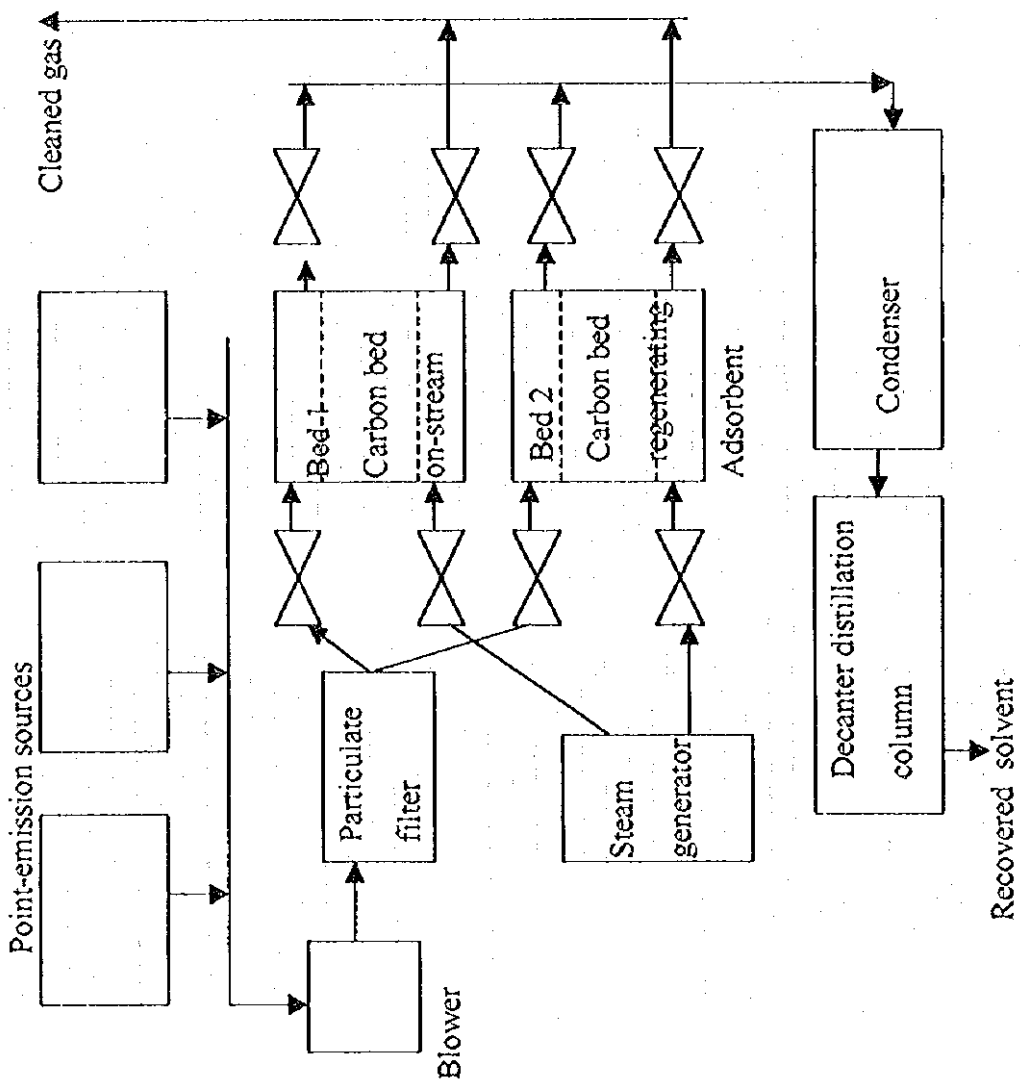


Fig. 1.1 Solvent Recovery System

Appendix 11.2.3-6 Removal of Dust and CO from the Flue Gas of Cupola and Electric Furnace

Appendix 11.2.3-6 Removal of Dusts and CO from the Flue Gas of Cupola and Electric Furnace

The removal of dusts from the flue gas of cupola is shown in Fig. 1 of Appendix 11.2.3-6. In this example, a cyclone type of dust collector is used. Appendix 11.2.3-3 describes on several types of dust collector. Waste streams consisting of baghouse dusts from cupola and electric furnaces that contain not only heavy metals such as zinc and lead but also flammable materials, can be returned to the cupola and electric furnaces. Because there are increasing levels of volatile lead and zinc in the dust, the efforts to recover these metals are also increasing. It is easily possible for up to 90% of the current quantities of dust to be processed for resource recovery.

The removal of dusts and CO from the electric furnace is shown in Fig. 2 of Appendix 11.2.3-6. Fume incinerators can be used to control the emission of gaseous or small-particulate air pollutants which are either combustible or which thermally decompose at high temperatures. Three rapid oxidation methods are used to destroy combustible contaminants:

- Thermal incineration;
- Catalytic incineration;
- Flares (direct flame combustion).

The main uses of fume incinerators are for the control of odor and smoke with some applications in hydrocarbon and carbon monoxide (CO) emission control.

Thermal incinerators are the most widely used method to control the release of hydrocarbon fumes, especially smokes and solvents from coating processes. Typically, thermal incinerator are constructed of a steel outer shell lined with refractory material. The refractory lining has purposes to protect the steel shell from direct exposure to the effects of high temperatures and corrosive materials, and also to improve the thermal efficiency of the unit by limiting heat loss. These incinerators are equipped with a burner at one end that fires a fuel, typically natural gas. There is also a fume inlet located near the burner where the gas stream to be oxidized enters the incinerator.

A catalytic incinerator is an alternative to a thermal incinerator as a means for oxidizing gaseous or oxygenated hydrocarbons to carbon dioxide and water. The oxidation reaction that occurs at the surface of the catalyst produces the same products, carbon dioxide and water, and liberates the same heat of combustion as a thermal incinerator would. A catalyst bed is located at a distance downstream from the burner sufficient to allow for a uniform preheated and distributed mixture of combustion products and waste gas stream. The catalyst bed in commercial units is typically a metal

mesh mat, ceramic honeycomb, or other ceramic matrix structure with a surface coating of finely divided platinum or other platinum-family metals, such as chromium, vanadium, nickel, or cobalt.

The flare system is used primarily as a safe method for disposing of excess waste gases. All process plants that handle hydrocarbons, hydrogen, ammonia, hydrogen cyanide, or other toxic or dangerous gases are subjected to emergency conditions that require the immediate release of large volumes of such gases for protection of plant and personnel. Flares are used for this purpose.

After completely combustion of CO with a thermal incinerator or a catalytic incinerator in Fig. 2 of Appendix 11.2.3-6., the exhaust gas is cooled and passes through a electrostatic precipitator to remove dusts. The removal of dust is described in Appendix 11.2.3-3.

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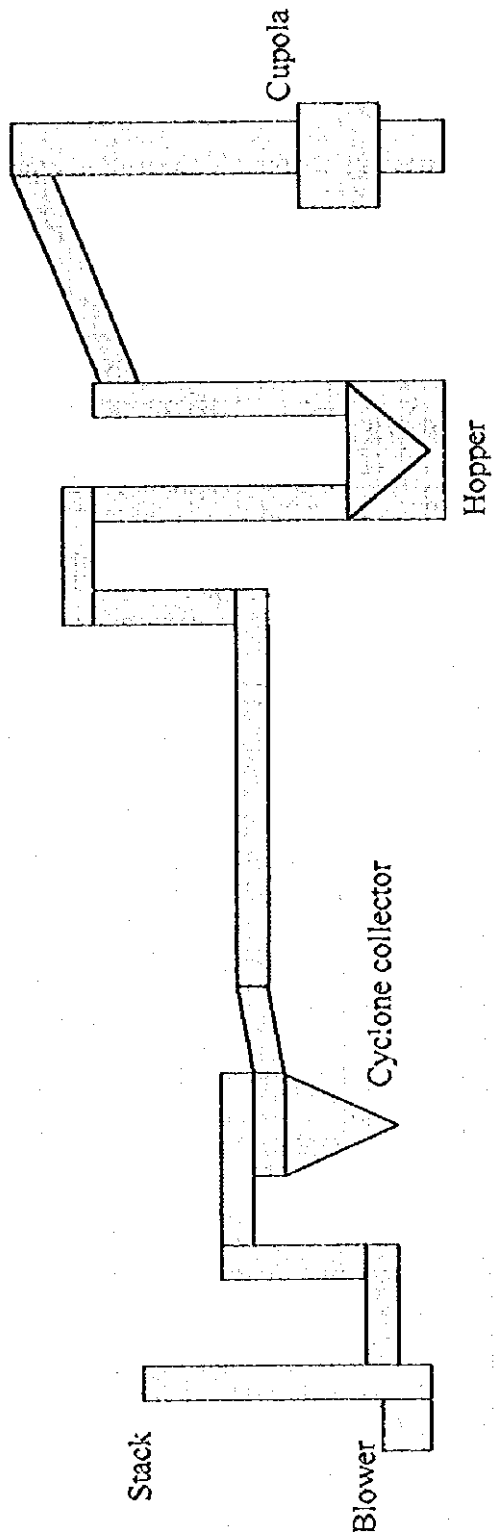


Fig. 1 Cupola with Cyclone Collector

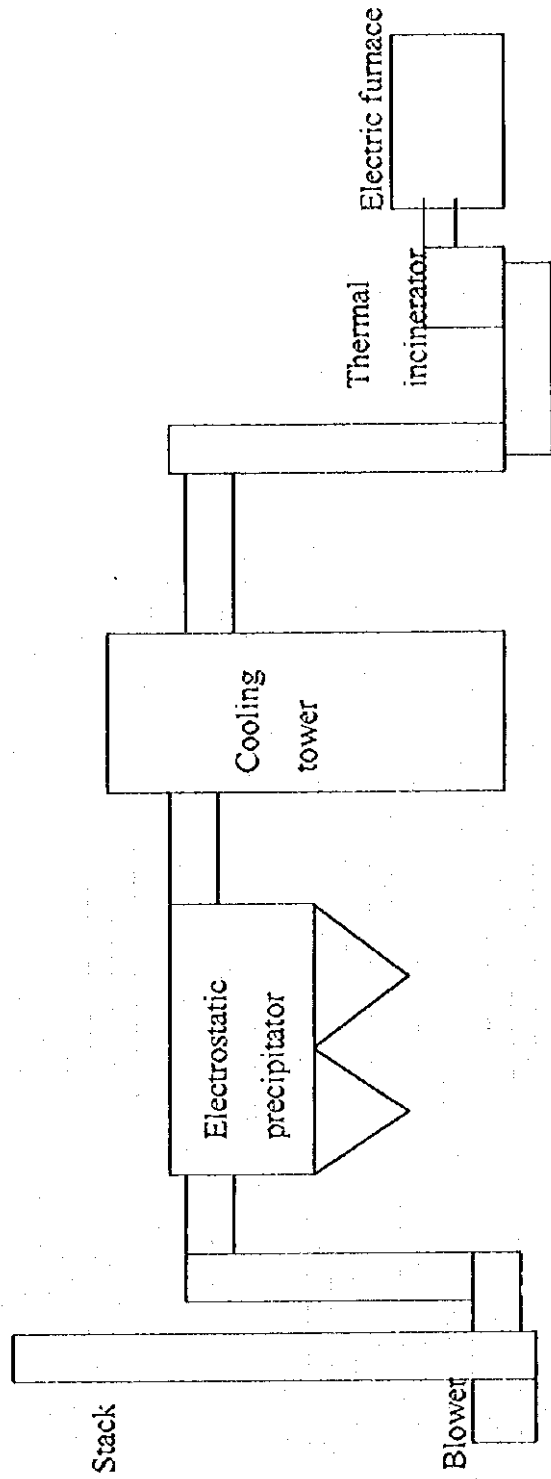


Fig. 2 Electric Furnace with Electric Precipitator

Appendix 11.2.3-7 Biological Methods for Reducing Wastes

Appendix 11.2.3-7 Biological Methods for Reducing Wastes

Biological methods for reducing wastes are classified into two following categories:

- Composting; and
- Anaerobic process.

(1) Composting

Composting is, just like landfilling and incineration, a classic method of waste treatment. It is an ecologically sound treatment method, because the organic share of the waste (generally about 40% by weight in household waste) is returned to the natural cycle. In comparison to other waste treatment methods, composting has only minor negative effects on the environment.

Waste which are to be composted must be primarily organic in nature and should have only minor contaminant concentrations. The most important compostable wastes in Tashkent Repair Workshop include:

- Biowaste (separately collected kitchen waste and green matter);
- Yard and park wastes.

The composting process has some very basic requirements. There must be adequate moisture, and the proper balance of carbon to nitrogen (C(weight)/N(weight) ratio, 25-30 to 1). These requirements can be easily managed to ensure a mature, uniform product. Other factors will influence composting and the rate at which it occurs, these are: nutrient supply, particle size, structural strength, frequency of turning (for aeration), acidity, and the size of the compost pile or heap.

There are three commonly practiced methods of composting: Bangalore, Indore, and Berkeley. The single outstanding difference between methods is the frequency of turning which affects the rate of decomposition.

Bangalore: The Bangalore method functions aerobically for several days and then becomes anaerobic, because no turning occurs. Although appropriate for both below- and above-ground composting it is more commonly carried out in pits. After 4 to 5 months the composting process is complete. One drawback with this methods is that without turning, the entire contents of pit do not reach high temperatures and not all pathogens and weed seeds are destroyed. Fly breeding and odor problems are often associated with this method so the top exposed portions must be covered, usually

with soil. Material near the outside of the pit should not be used, but transferred and incorporated into the next composting.

Indore: The Indore composting system relies on aerobic activity although portions of the pile or pit will likely become anaerobic between turnings. This method has better fly control, more rapid and uniform decomposition, and less moisture control problems than with the Bangalore method. During the period of active composting the contents are turned from 1-5 times over a period of 1-6 months. The longer the interval between turnings the longer the composting process. Many smaller compost operations use this less labor intensive method.

Berkeley: The Berkeley method for composting is named after the University of California at Berkeley where it was developed. It is considered to be the quickest method of achieving finishing compost, and it is the method which is likely to be the most effective method for production of either large or small quantities of compost. This method requires frequent turning and mixing of the heap, particularly during the initial stages of decomposition which intensifies the activity of microorganisms. The Berkeley method is normally carried out in above-ground stacks or windrows where air circulation is improved and the pile is accessible for turning. Since turning is frequent, problems associated with odors and flies are minimal. Compost should be ready for maturing within two or three weeks depending on the size of heap, frequency of turning, initial C/N ratio, and moisture content. Labor requirements are higher with this method than the others, but the shorter composting period reduces the space needed for a site. Where large quantities of compost are produced a mechanized system is often used.

There are modernized composting methods, but the description on these methods are omitted here.

(2) Anaerobic Processes

Biogas facilities were originally used in agriculture for the treatment of animal waste. They were also used in sewage treatment plants for sludge stabilization and for cleaning highly contaminated wastewater. The organic fraction of household waste (if it was biologically treated at all), was treated aerobically, i.e., it was composted. By the early 1980s, after sewage treatment had progressed sufficiently with the development of highly efficient digesters, biogas plants were increasingly used for the treatment of solid and sludgy organic wastes. The expectations were that fermentation would require less space, emit no odors, yield energy, and offer flexibility in its application.

The composting of organic production wastes (mostly in the food processing and beverage industry) is not feasible because of the high water content and the large space requirements. Incineration would lead to a significant reduction of volume, but would require considerable technical effort and

energy input. Thus, in-house anaerobic digestion is as an economical solution for companies, because of the minimal space requirements and the volume reduction it offers, while at the same time generating energy for the operator.

In nature, methane-forming bacteria are found whether biogenic-organic material is decomposed in oxygen-deficient environments, e.g., in swamps and sediments, and also in the stomachs of ruminants. The methane-forming bacteria, called obligate anaerobes, can only survive in an environment without oxygen. Since the energy yield without oxygen during substrate decomposition is only 1/7 that of aerobic bacteria, anaerobes multiply at a corresponding slower rate. In their metabolism, they are dependent on the preparatory work of and the symbiosis with other bacteria.

In the first phase, high-molecular compounds such as carbohydrates, fats and proteins react with water to form sugar, fatty acids, and amino acids. This stage is called hydrolysis. In the next phase of acid formation, the compounds are fermented by acid forming bacteria into propionic and butyric acids, hydrogen and carbon dioxide as well as lower alcohols. These groups of bacteria form a symbiotic relationship, because the acetogenic bacteria are inhibited by their own product, hydrogen, and depend on the methane-forming bacteria to detoxify their environment. Based on this symbiosis, the two combined steps of acetic acid formation and methane formation are the third phase, called methane fermentation phase. Since the energy yield of methane-forming bacteria is very low and causes them to multiply very slowly, the limiting factor for the rate of anaerobic decomposition is the forming of methane .

Equipment of anaerobic processes for reduce wastes are omitted here.

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Appendix 12.9 Rolling Stock Maintenance

Table 12.9-1 Weekly Schedule of Rolling Stock Maintenance Work

Date of shop-in	Kind of inspection	Rolling stock number	Steel repair work	Painting	Wheel set	Brake parts	Suspension metal	Engine		Torque converter		Electric parts	Reverse gear	Bogie assembly	Modification work
								Main motor	Auxiliary motor	Auxiliary motor	Reduce gear				
3/4	OH	EF65123	16 5	16 10										2 18	

Bogie insertion	Whole fixing	Performance test	ATS testing	Trial run	Delivery	Commercial line trial run	Remark
29	16 29	16 31	17 31	4/2	4/4		

Note OH: Overhaul
16 16: 0'clock
15 15: Date

Table 12.9-2

Daily Schedule of Rolling Stock Maintenance Work

Assembling	Steel repair work	Painting	Apparatus work	Main motor	Electric parts	Bogie assembling	Bogie insertion
EF65456		¹⁶ 6	¹⁶ 10	¹⁶ 10	¹⁶ 10	¹⁴ 14	⁹ 21
Out-going	Whole fixing	Performance test	Trial run	Additional repair work		Delivery	Remark
EF65789	¹⁶ 4	¹⁶ 5	⁹ 7			¹⁶ 10	Commercial line trial run ¹¹ 13

Note : ¹⁶ 6 ... Date ¹⁶ ... o'clock

Table 12.9-4 Table of Procurement and Stock for Parts(1997)

Parts number	Parts code	Parts name	Specification	Person in charge	Kind of rolling stock	Quantity equipped	Unit price	Quantity in '96							
								Brought over from '95	Procured	Brought over to '97	Actually applied				
1	2	3	4	5	wheelset	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

Application rate	Quantity to be procured in '97	Planned money amount in '97	Planned to be brought over	Purpose of storage
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